1580

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

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MICROFILMED

1580

The paper stock of this book is made of a **high grade 50% rag** paper having a **water resisting surface** and is sewed with Bing **Special Enamel Waterproof Thread.**

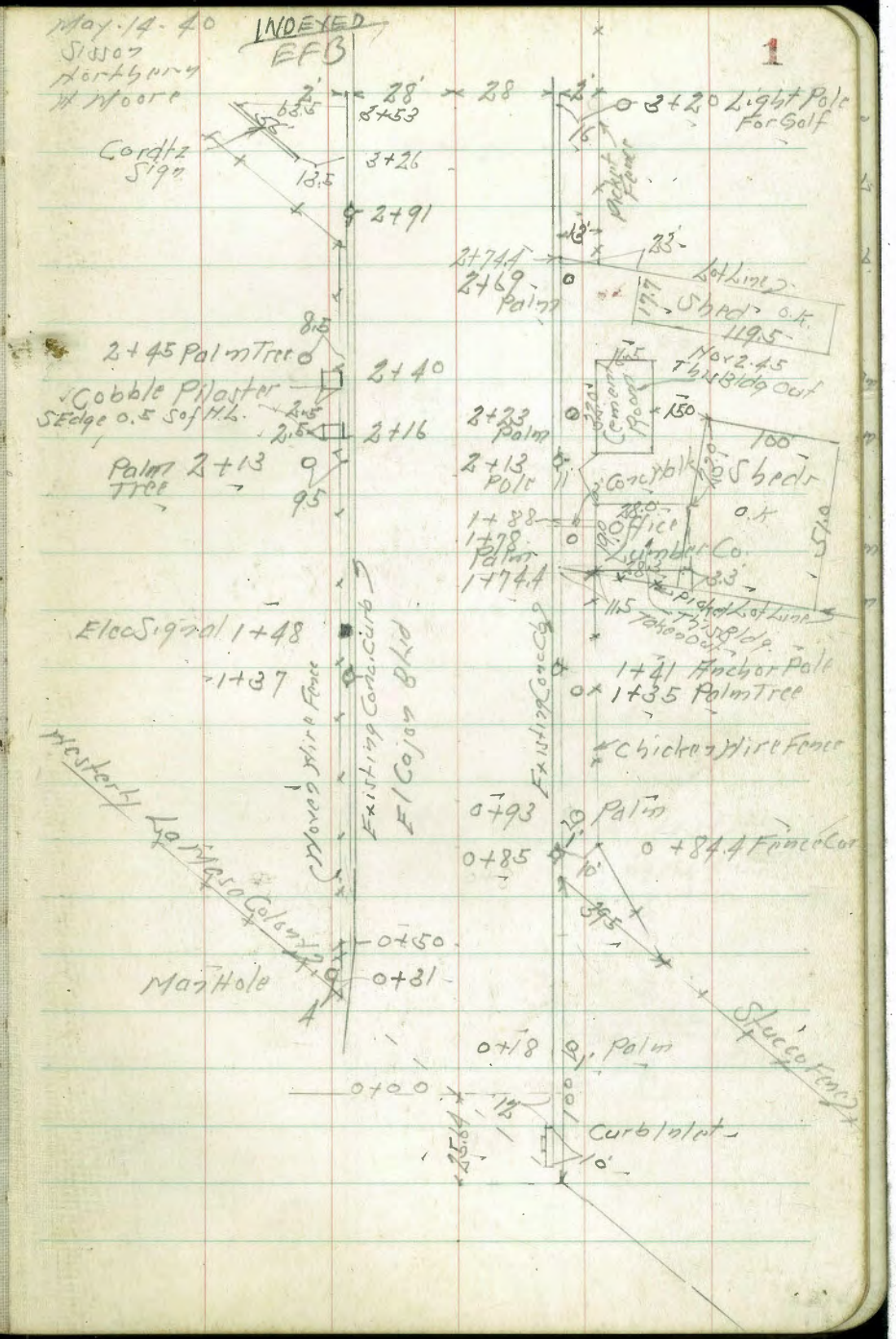
Made in U. S. A.

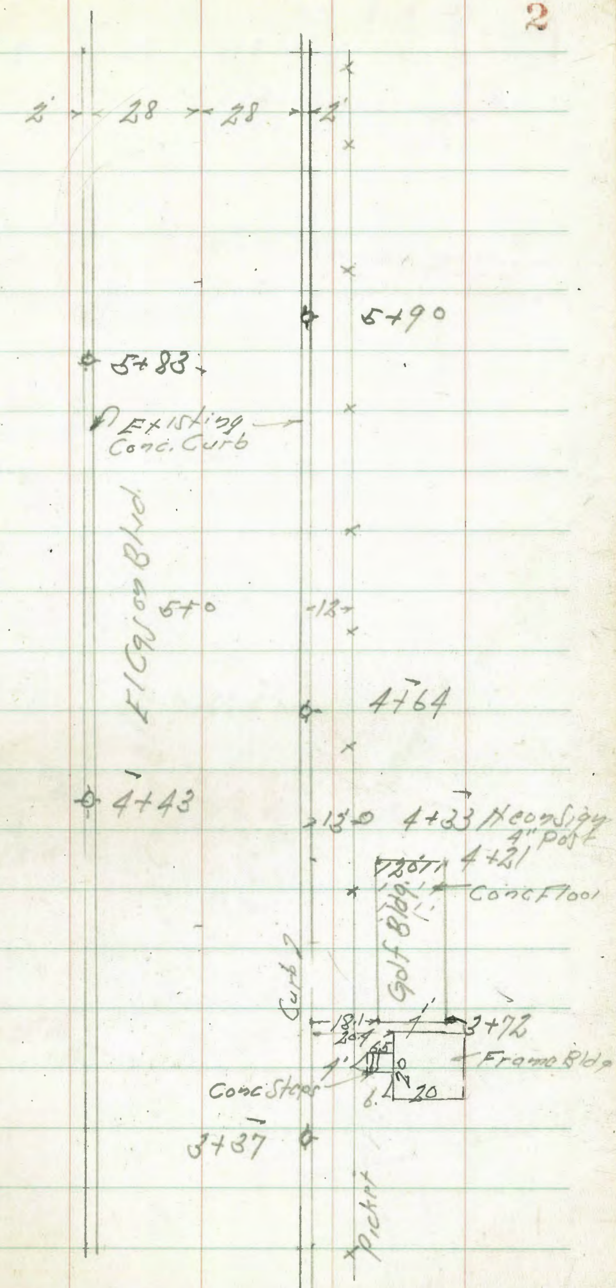
Alignment El Cajon Boulevard
Westerly Line of La Mesa Colony to Seminole Dr.

⊕ Indicates Power + Telephone Poles

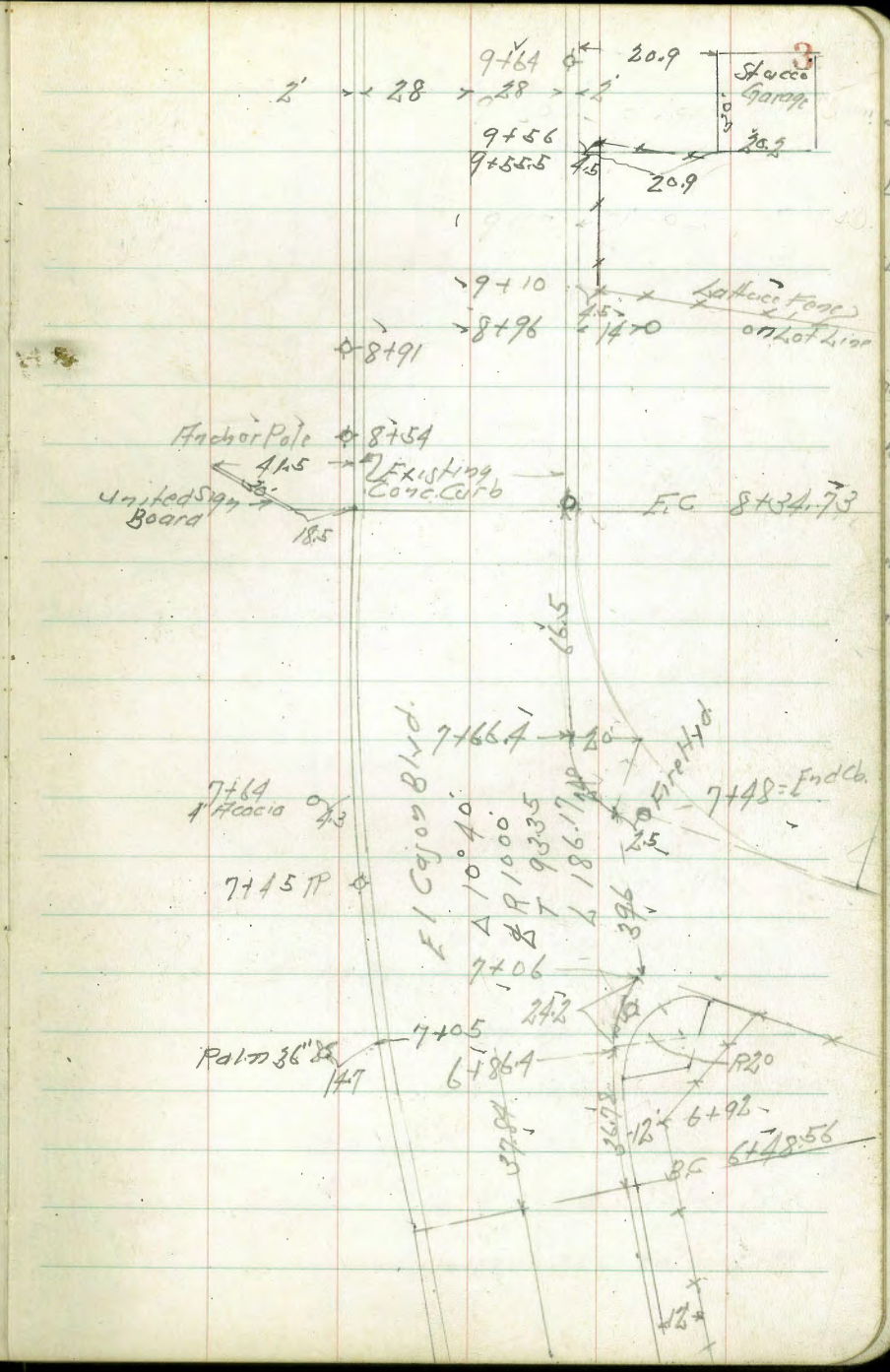
Telephone Poles are Located on N.L.

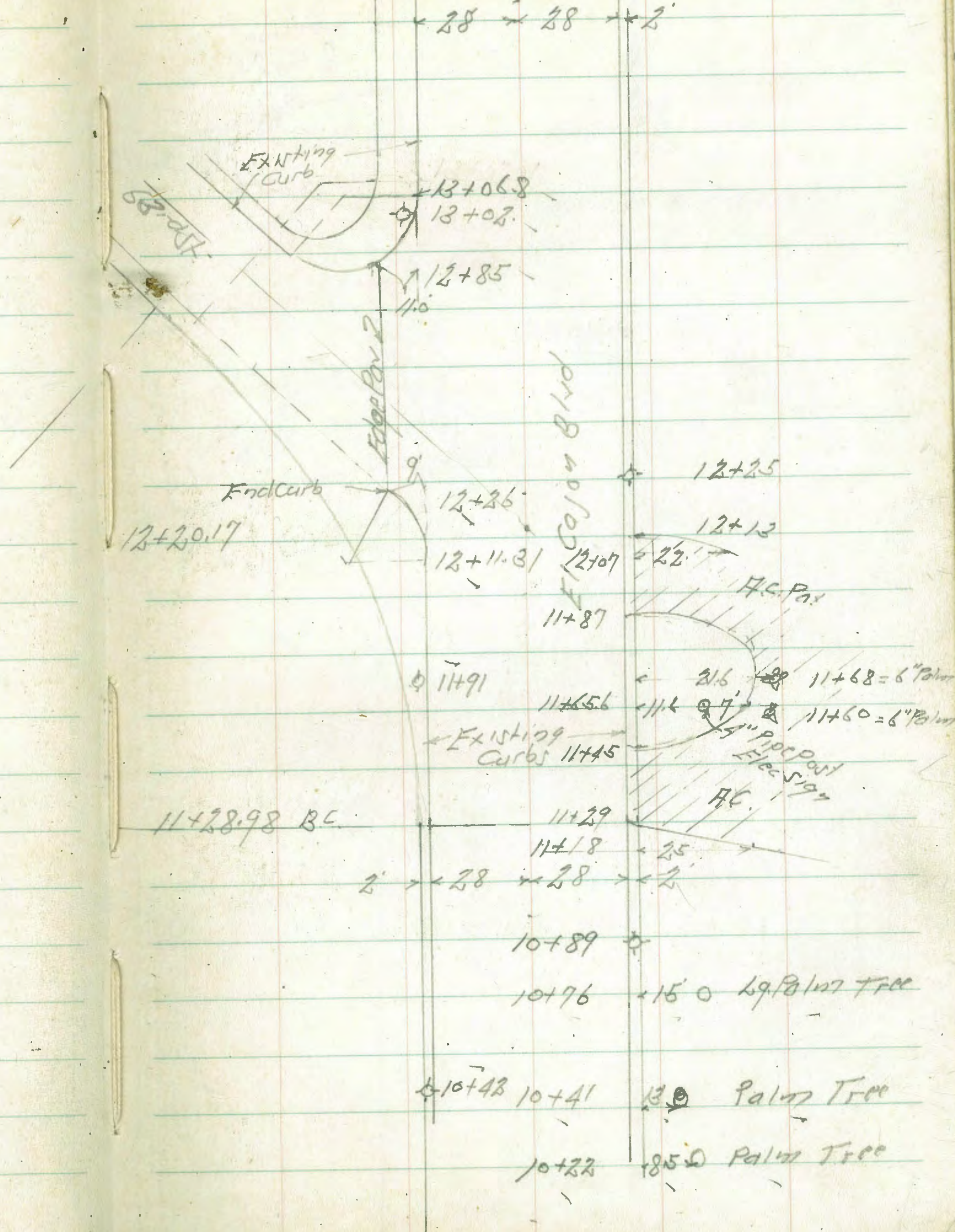
Power Poles " " " S.L.

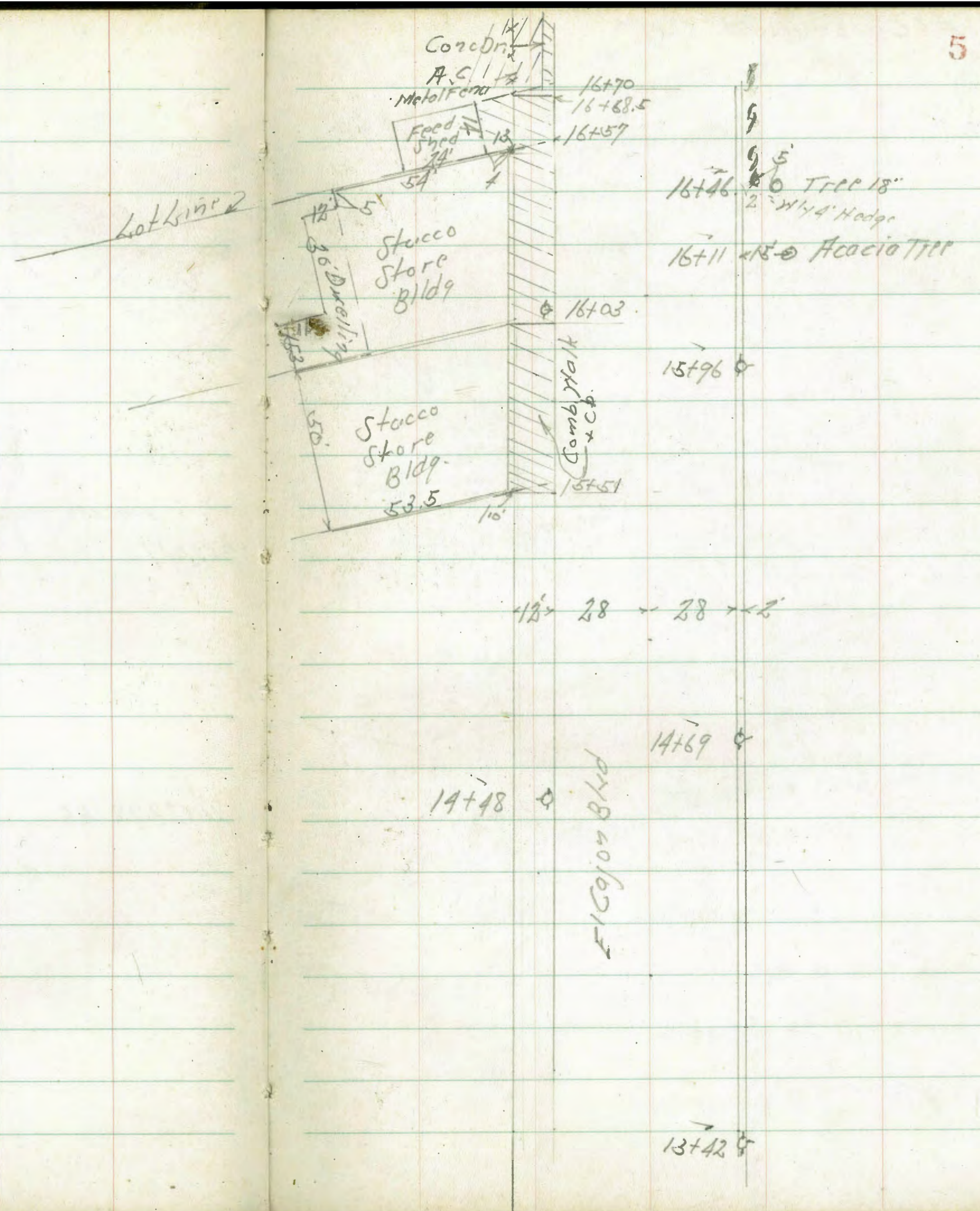



2'
28
28
2'
5+90
5+83
Existing
Conc. Curb
El Cajon Blvd
12
4+64
4+43
13.0
4+23 Neon Sign
4" Post
4+21
Conc Floor
Golf Bldg
Curb
18.1
3+72
Frame Bldg
Conc Steps
20
3+37
Picket

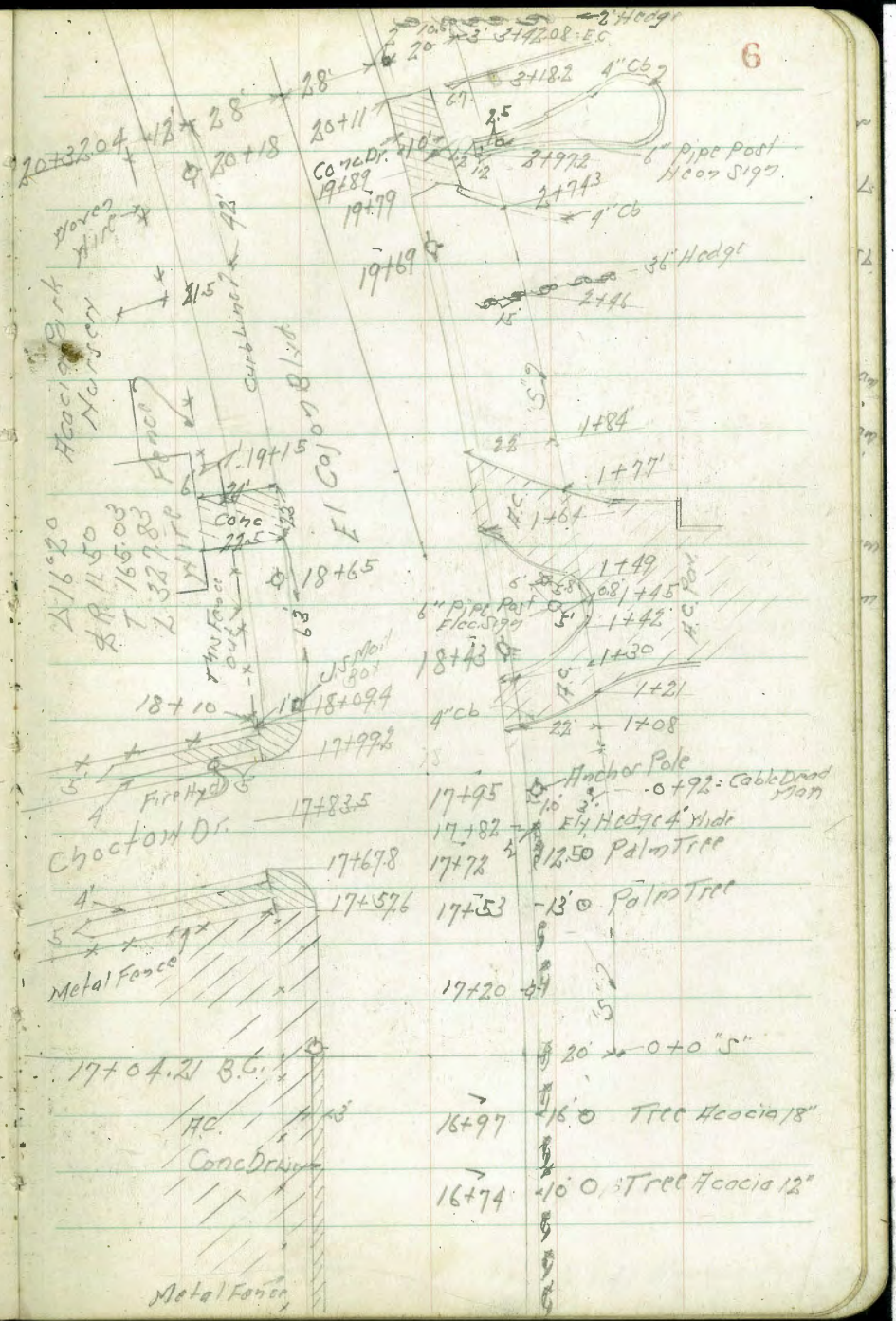
El Cajon Blvd

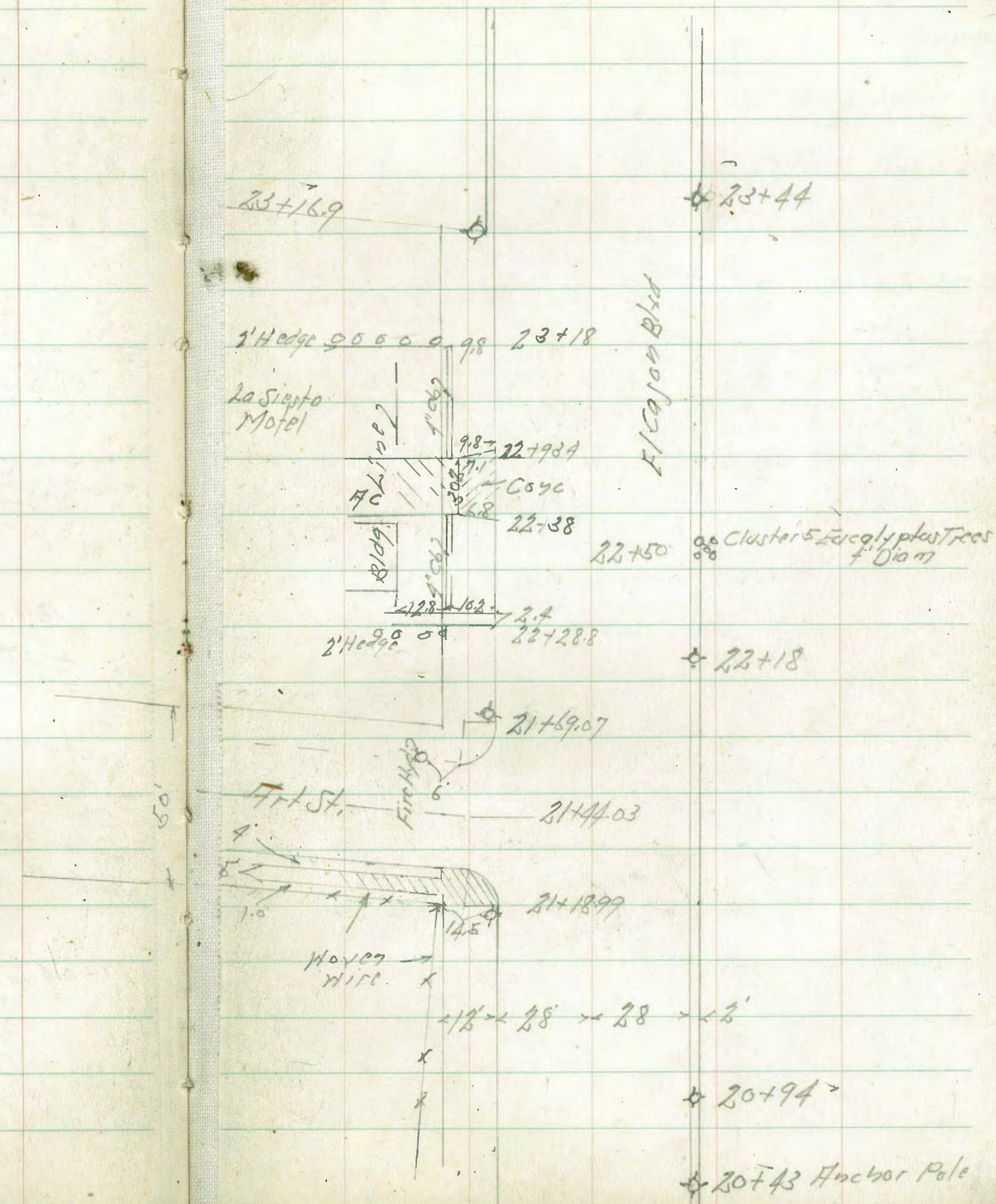


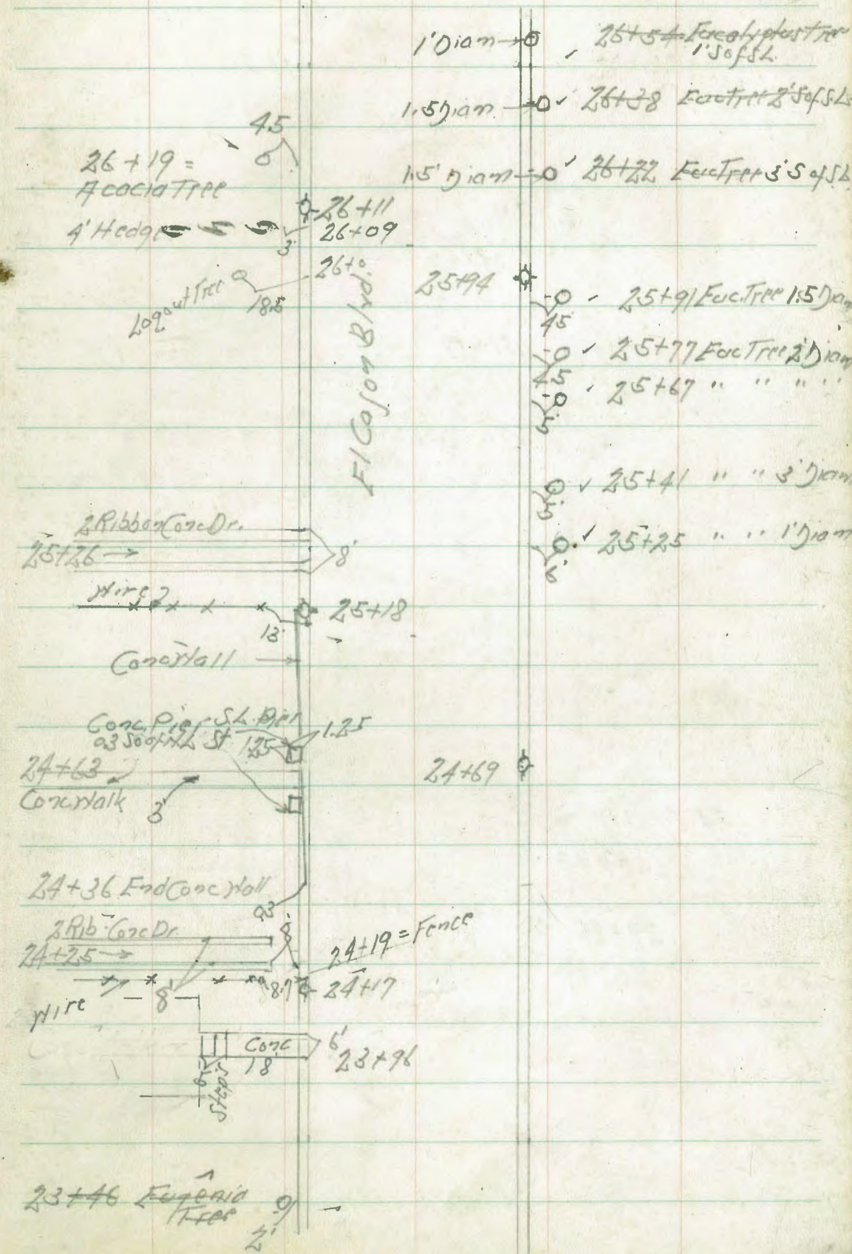

28
28
2'
Existing Curb
13+06.8
13+02
12+85
11.0
Edge Pav't
El Cajon Blvd
End Curb
12+36
12+25
12+13
12+20.17
12+11.81
12+07
22
A.C. Pav't
11+87
11+91
21.6
11+68 = 6" Palm
11+65.6
11.6
7'
11+60 = 6" Palm
Existing Curbs
11+45
Elec Sign
A.C.
11+28.98 B.C.
11+29
11+18
25
2'
28
28
2'
10+89
10+76
15
Lg. Palm Tree
10+43
10+41
13
Palm Tree
10+22
8.5
Palm Tree


Conc Dr.
A.C.
Metal Fence
16+70
16+68.5
Feed Shed
24'
16+57
54'
Lot Line 2
5'
Stucco Store Bldg
36' Dwelling
16+03
15+96
Comb. Walk + Cb.
Stucco Store Bldg.
50'
53.5
10'
15+51
16+46
Tree 18"
w/4' Hedge
16+11
15
Acacia Tree
12
28
28
2
14+69
14+48
Cajon Blvd
13+42

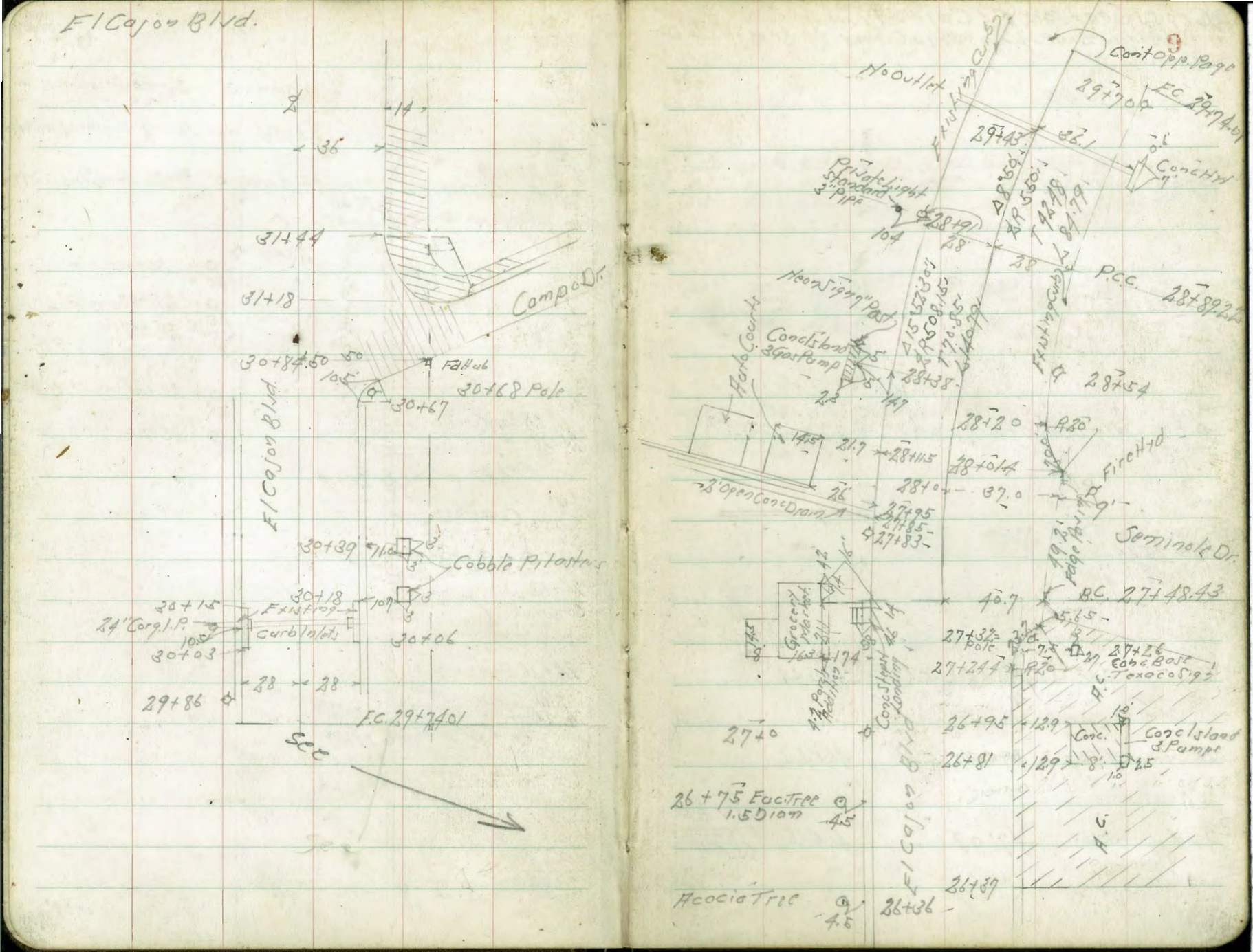
El Cajon Blvd.




23+16.9
1'Hedge
9.8
23+18
La Siesta Motel
Bldg
AC Line
9.8
22+93.4
Cove
22+38
El Cajon Blvd
23+44
22+50
Cluster 5 Eucalyptus Trees 4' Diam
12.8
16.2
2.4
2'Hedge
22+28.8
22+18
21+69.07
Fire Hyd
Art St.
50'
21+44.03
21+18.99
14.5'
Woven Wire
12' 28 28 2'
20+94
20+43 Anchor Pole



1'Diam
~~25+54 Eucalyptus Tree~~ 1'S of SL
1.5 Diam
~~26+38~~ Euc Tree 2'S of SL
1.5' Diam
~~26+22~~ Euc Tree 3'S of SL
45
26+19 = Acacia Tree
4' Hedge
26+11
26+09
26+0
Loquat Tree
18.5
25+94
25+91 Euc Tree 1.5' Diam
25+77 Euc Tree 2' Diam
25+67 " " " "
25+41 " " 3' Diam
25+25 " " 1' Diam
El Cajon Blvd
2 Ribbon Conc Dr.
25+26
8'
Wire
25+18
13'
Conc Wall
Conc Pier SL Pier
1.25
24+63
Conc Walk
24+69
24+36 End Conc Wall
2 Rib Conc Dr
24+25
24+19 = Fence
24+17
Wire
8'
Conc
18
6'
23+96
~~23+46~~ Eugenia Tree
2'


El Cajon Blvd.
14'
36'
31+44
31+18
Comp. Dr.
30+84.50
50
10.5'
Fd Hd
30+68 Pole
30+67
El Cajon Blvd.
30+39
11.0'
Cobble Pilasters
30+18
30+15
Exist Inlet
24" Corg. I.P.
Curb Inlet
30+03
30+06
28
28
29+86
E.C. 29+74.01
Sec
No Outlet
Exist 12" C.M.P.
Conc. Top. Page
29+70
E.C. 29+74.01
29+43
86.1
Conc. Hdwl
Private Light Standard 3" Pipe
Δ 8°50'
R 550'
T 42.48
L 84.79
28+49
10.4
28
28
P.C.C. 28+89.27
Neon Sign "Post"
Exist 12" C.M.P.
Δ 15°53'30"
R 508.15'
T 70.85'
L 140.79'
Conc Island 3 Gas Pump
Ford Courts
28+38
14.7
28+54
28+20
R 20'
28+14
Fire Hd
21.7
28+11.5
28+0
37.0
25' Open Conc. Drain
27+95
27+85
27+83
Seminole Dr.
19.2' face to face
40.7
B.C. 27+48.43
Grocery Market
Conc. Storm Drain Inlet
27+37
Pole
27+26
Conc. Base
27+24
R 20'
26+95
12.9'
Conc.
Conc Island 3 Pumps
26+81
12.9'
27+0
El Cajon Blvd.
26+75 Euc. Tree 1.5 Diam
26+89
Acacia Tree
26+36
4.5

Cross Section El Cajon Blvd.
Westerly Line of La Mesa Colony to Seminole Dr.

May 16-40
Sisson
Northern
W Moore

Reduced AEBrCBA 8-1-44

Sta.						Lt.	℄	Rt.
0+50						463.0 / 5.6 / 50'; 464.4 / 4.2 / 43'; 464.26 / 4.30 / 28cb; 463.64 / 4.92 / 28Gut; 463.99 / 4.57 / 14'	464.04 / 4.52	463.77 / 4.79 / 14; 463.25 / 5.31 / 28; 463.42 / 5.14 / 28 Dr.; 463.2 / 5.4 / 40'; 462.5 / 6.1 / 50'
0+25.6						464.2 / 4.4 / 50; 464.11 / 4.45 / 29.7cb; 463.50 / 5.06 / 29.7 Gut; 463.92 / 4.64 / 14'	463.92 / 4.64	463.64 / 4.92 / 14; 463.13 / 5.43 / 28 Gut; 463.75 / 4.81 / 28cb; 463.5 / 5.1 / 41'; 462.9 / 5.7 / 50'
0+0 = Wly La Mesa Colony						463.9 / 4.7 / 50; 464.15 / 4.41 / 28cb; 463.29 / 5.27 / 28 Gut.; 463.79 / 4.77 / 14	463.76 / 4.80	463.49 / 5.07 / 14; 462.85 / 5.71 / 28 Gut; 463.62 / 4.94 / 28cb; 463.4 / 5.2 / 45; 463.0 / 5.6 / 50
0-25.64							463.81 / 4.75	463.49 / 5.07 / 14; 462.68 / 5.88 / 28 Gutter; 463.69 / 4.87 / 28 Cb Top; 463.5 / 5.1 / 42; 462.7 / 5.9 / 50'
							468.56	
TP	4.12	468.56	5.67	464.44				
TP	4.48	470.11	5.46	465.63				
BM	5.43	471.09		465.66	N.W. B.P. El Cajon + 63rd St.			

TP	4.97	469.79	3.74	464.82
3+0				
+50				
2+0				
+50				
1+0				
	468.56			

Lt ℄ Rt

Sta.											
3+0	464.9 / 3.7 / 50'	465.14 / 3.42 / 28 Cb	464.49 / 4.07 / 28 Gut.	465.01 / 3.55 / 14'	465.08 / 3.48	464.94 / 3.62 / 14'	464.13 / 4.43 / 28 Gut.	465.00 / 3.56 / 28 Cb	464.5 / 4.1 / 34'	464.0 / 4.6 / 38'	464.4 / 4.2 / 50
+50	464.6 / 4.0 / 50'	463.96 (464.96) / 3.60 / 28 Cb	464.30 / 4.26 / 28 Gut.	464.79 / 3.77 / 14	464.88 / 3.68	464.71 / 3.85 / 14'	464.18 / 4.38 / 28 Gut	464.31 / 4.25 / 28 in Dr.	464.4 / 4.2 / 50'		
2+0	464.0 / 4.6 / 50	464.1 / 4.5 / 43'	465.1 / 3.5 / 39'	464.81 / 3.75 / 28 Cb	464.17 / 4.39 / 28 Gut	464.64 / 3.92 / 14	464.61 / 3.95	464.41 / 4.15 / 14'	463.99 / 4.57 / 28 Gut	464.13 / 4.43 / 28 in Dr.	464.1 / 4.5 / 50'
+50	463.6 / 5.0 / 50'	463.8 / 4.8 / 46	464.8 / 3.8 / 40	464.66 / 3.90 / 28 Cb	463.98 / 4.58 / 28 Gut.	464.43 / 4.13 / 14	464.43 / 4.13	464.28 / 4.28 / 14	463.71 / 4.85 / 28 Gut.	464.37 / 4.19 / 28 Cb	464.3 / 4.3 / 50
1+0	463.3 / 5.3 / 50'	463.5 / 5.1 / 47	464.7 / 3.9 / 43'	464.46 / 4.10 / 28 Cb	463.83 / 4.73 / 28 Gut	464.24 / 4.32 / 14	464.26 / 4.30	464.05 / 4.51 / 14	463.59 / 4.97 / 28 Gut	464.23 / 4.33 / 28 Cb	464.0 / 4.6 / 50

468.56

El Cajon Blvd.

Lt ℄ Rt

Sta.												
6+0	464.4 / 5.4 / 50	464.4 / 5.4 / 37	465.71 / 4.08 / 28cb	465.05 / 4.74 / 28 Gut	465.63 / 4.16 / 14	465.77 / 4.02	465.63 / 4.16 / 14	465.11 / 4.68 / 28 Gut	465.74 / 4.05 / 28cb	465.4 / 4.4 / 32	464.0 / 5.8 / 40	464.2 / 5.6 / 50
+50	465.4 / 5.4 / 50	464.3 / 5.5 / 40	465.3 / 4.5 / 34	465.57 / 4.22 / 28cb	464.95 / 4.84 / 28 Gut	465.51 / 4.28 / 14	465.67 / 4.12	465.55 / 4.24 / 14	464.97 / 4.82 / 28 Gut	465.57 / 4.22 / 28cb	5.8 / 42	5.7 / 50
5+0	465.4 / 4.4 / 50	465.49 / 4.30 / 28cb	464.86 / 4.93 / 28 Gut	465.45 / 4.34 / 14	465.65 / 4.14	465.49 / 4.30	464.99 / 4.80 / 28 Gut	465.62 / 4.17 / 28cb	464.8 / 5.0 / 34	463.0 / 6.1 / 42	464.1 / 5.7 / 50	
+50	465.4 / 4.4 / 50	465.35 / 4.44 / 28cb	464.75 / 5.04 / 28 Gu	465.33 / 4.46 / 14	465.50 / 4.29	465.35 / 4.44 / 14	464.77 / 5.02 / 28 Gut.	465.44 / 4.35 / 28cb	463.9 / 5.9 / 38	464.0 / 5.8 / 50		
4+0	465.7 / 4.1 / 50	465.32 / 4.47 / 28cb	464.68 / 5.11 / 28 Gut	465.23 / 4.56 / 14	465.41 / 4.38	465.27 / 4.52 / 14	464.70 / 5.09 / 28 Gut	465.37 / 4.42 / 28 cb	465.3 / 4.5 / 29	464.2 / 5.6 / 36	464.2 / 5.6 / 50	
3+50	465.4 / 4.4 / 50	465.2 / 4.6 / 33	465.6 / 4.2 / 30	465.32 / 4.47 / 28cb	464.67 / 5.12 / 28 Gut	465.17 / 4.62 / 14	465.29 / 4.50	465.15 / 4.64 / 14	464.56 / 5.23 / 28 Gut	465.21 / 4.58 / 28cb	464.6 / 5.2 / 50	

469.79

469.79

Lt ℄ Rt

7+48

7+26

7+06

6+86.4

TP 5.29 470.61 4.47 465.32

6+48.56 = BC.

469.79

464.6	465.0	465.88	466.31	465.96	466.11	465.96	465.44	466.14	465.65	465.6
6.0	5.6	4.73	5.30	4.65	4.50	4.65	5.17	4.47	4.96	5.0
50'	29'	28 Cb	28 Cut	14'		14'	28'	40 Cb	40 Cut	50'

464.5	464.6	465.48	465.98	466.08	465.89	465.45	465.96	465.7
6.1	6.0	5.13	4.63	4.53	4.62	5.16	4.65	4.9
50'	36'	28 Cut Prof.	14'		14'	28'	41.25 Edge Br.	50'

464.7	464.7	465.86	465.23	465.88	465.89	465.91	465.50	465.32	465.96	465.4
5.9	5.9	4.75	5.38	4.73	4.62	4.70	5.11	5.29	4.65	5.3
50'	40'	28 Cb	28 Cut	14'		14'	28'	39.3 Cut	39.3 Cb	50'

464.5	464.5	465.28	465.22	465.85	466.00	465.85	465.40	465.84	465.55	464.6	464.6
6.1	6.1	4.83	5.39	4.76	4.61	4.76	5.31	4.67	5.1	6.0	6.0
50'	35'	28 Cb	28 Cut	14'		14'	28 Cut	28 Cb	34	40	50

470.61

464.3	464.4	465.2 (465.69)	465.10	465.28	465.89	465.09	465.19	465.82	464.4	464.5
5.6	5.4	4.10	4.69	4.01	3.90	4.00	4.60	3.97	5.4	5.3
50'	35'	28 Cb	28 Cut	14'		14'	28 Cut	28 Cb	40	50

469.79

May 17-40

Sta.					
9+50					
9+0					
8+50					
TP	4.96	470.98	4.59	466.02	O.D. F.C. Mon. C.D.N. 8+34.73 30' Lt
8+34.73 F.C.					
8+0					
7+664					

47061

Lt — ℄ — Rt.

9+50: 465.5/5.5/50' · 465.9/5.1/34 · 466.98/4.60/28=Cb · 465.76/5.22/28'Gut. · 466.23/4.75/14' · 466.33/4.65 · 466.11/4.87/14' · 465.64/5.34/28=Gut · 466.09/4.89/28:Cb · 465.9/5.1/50'

9+0: 465.5/5.5/50' · 465.5/5.5/33' · 466.2/4.8/31' · 466.31/4.67/28=Cb · 465.75/5.23/28=Gut · 466.33/4.75/14 · 466.25/4.73 · 466.08/4.90/14 · 465.61/5.37/28Gut · 465.68/5.30/28=Dr. · 466.0/5.0/50'

8+50: 465.3/5.7/50' · 465.3/5.7/35 · 466.13/4.85/28=Cb · 465.55/5.43/28:Gut. · 466.16/4.82/14 · 466.25/4.73 · 466.02/4.96/14' · 465.55/5.43/28=Gut · 465.95/5.03/28=Cb · 465.5/5.5/32' · 465.7/5.3/50'

470.98

8+34.73: 465.2/5.4/50' · 465.3/5.3/35' · 466.25/4.36/28=Cb · 465.63/4.98/28=Gut. · 466.14/4.47/14' · 466.20/4.41 · 466.05/4.56/14' · 465.52/5.09/28=Gut. · 465.92/4.69/28Cb · 465.6/5.0/30' · 465.3/5.3/50

8+0: 465.3/5.3/50' · 465.4/5.2/29 · 466.12/4.49/28=Cb · 465.54/5.07/28Gut · 466.10/4.51/14 · 466.22/4.39 · 466.05/4.56/14' · 465.59/5.02/28Gut · 465.90/4.71/28=Dr. · 465.6/5.0/50

7+664: 464.9/5.7/50 · 465.2/5.4/29' · 466.02/4.59/28=Cb · 465.39/5.22/28Gut · 466.00/4.61/14 · 466.12/4.49 · 466.03/4.58/14' · 465.44/5.17/28Gut · 465.91/4.70/28=Cb · 465.8/4.8/50

470.61

El Cajon Blvd.

	Lt			℄		Rt				
12+0	465.7 5.3 50	465.66 5.32 28=Cb	465.10 5.88 28=Gut	465.58 5.40 14	465.68 5.30	465.60 5.38 14	464.98 6.00 28=Gut	465.63 5.35 28=Cb	465.4 5.6 36	464.8 6.2 50
11+50	465.8 5.2 50'	465.93 5.05 28=Cb	465.35 5.63 28=Gut	465.88 5.10 14'	465.94 5.04	465.86 5.12 14	465.36 5.62 28=Gut	465.95 5.03 28=Cb	465.7 5.3 35'	465.6 5.4 50'
11+28.98	465.7 5.3 50'	46604 4.92 28=Cb	465 46 5.52 28=Gut	465.93 5.05 14'	46608 4.90	46601 4.97 14	465.53 5.45 28=Gut	466.11 4.87 28=Cb	465.7 5.3 35	465.8 5.2 50'
11+0	466.0 5.0 50'	46622 4.72 28=Cb	465.66 5.32 28 Gut	46618 4.80 14	46628 4.70	466.19 4.79 14	465.73 5.25 28=Gut.	46634 4.64 28=Cb	466.1 4.9 30'	466.0 5.0 50'
10+50	4660 5.0 50	46544 4.54 28=Cb	46585 5.13 28=Gut	46644 4.54 14	46647 4.51	46631 4.67 14'	465.84 5.14 28=Gut	46648 4.50 28=Cb	4661 4.9 30'	465.9 5.1 50
10+0	465.56 5.4 50'	4660 5.0 38'	466 45 4.53 28=Cb	46587 5.14 28=Gut	466 30 4.68 14	46644 4.54	46635 4.63 14'	465.75 5.13 28=Gut	46592 5.06 28=Drive	4662 4.8 50

470.98

470.98

Lt. ℄ Rt

13+06.8
464.6 (4.9 / 50') · 465.0 (4.5 / 38') · 465.18 (4.28 / 28=Cb) · 464.57 (4.89 / 28=Gut) · 465.00 (4.46 / 14) · 465.13 (4.33) · 464.99 (4.47 / 14) · 464.49 (4.97 / 28=Gut) · 464.51 (4.95 / 28=Drive) · 464.0 (5.5 / 35') · 463.7 (5.8 / 50')

12+85
465.2 (4.3 / 50) · 465.21 (4.25 / 39=Cb) · 464.43 (5.03 / 39=Gut) · 464.69 (4.77 / 28) · 465.21 (4.25 / 14) · 465.29 (4.17) · 465.20 (4.26 / 14') · 464.62 (4.84 / 28=Gut) · 465.15 (4.31 / 28=Cb) · 463.8 (5.7 / 40') · 463.8 (5.7 / 50)

12+50
465.41 (4.05 / 50') · 465.26 (4.20 / 37.3=Edge Pav) · 465.02 (4.44 / 28) · 465.39 (4.07 / 14') · 465.49 (3.97) · 465.36 (4.10 / 14') · 464.84 (4.62 / 28=Gut) · 464.96 (4.50 / 28=Dr.) · 464.7 (4.8 / 50')

12+26
465.3 (4.2 / 50) · 465.39 (4.07 / 37=Cb End) · 464.81 (4.65 / 37=Gut) · 465.06 (4.40 / 28) · 465.51 (3.95 / 14) · 465.59 (3.87) · 465.42 (4.04 / 14) · 464.93 (4.53 / 28') · 465.53 (3.93 / 28') · 465.0 (4.5 / 40) · 464.5 (5.0 / 50')

TP 3.80 469.46 5.32 465.66 H.W.B.P. El Cajon+63rd

469.46

12+11.31
465.8 (5.2 / 50') · 465.65 (5.33 / 28=Cb) · 465.05 (5.93 / 28=Gut) · 465.51 (5.47 / 14) · 465.64 (5.34) · 465.50 (5.48 / 14') · 464.98 (6.00 / 28=Gut) · 465.58 (5.40 / 28=Cb) · 465.3 (5.7 / 35) · 464.7 (6.3 / 50)

470.98

470.98

15+51 = Mly Existing C&G Walk

TP 4.64 468.87 5.23 464.23

15+0

14+50

14+0

13+50

469.46

Lt | ℄ | Rt

Lt				℄			Rt			
464.6	464.62	464.34	463.65	464.07	464.09	463.95	463.40	463.52	463.7	463.2
4.3	4.25	4.53	5.23	4.80	4.78	4.93	5.17	5.35	5.2	5.7
LP	41 on Walk	28=C6	28=Gut	14		14	28=Gut	28=Gut	31	50

468.87

Lt				℄			Rt			
464.1		464.35	463.74	464.19	464.35	464.06	463.44	463.96	463.9	462.6
5.1		5.11	5.72	5.27	5.21	5.10	6.05	5.50	5.6	6.9
50		28=C6	28=Gut	14		14	28=Gut	28=C6	35	50
463.6	464.2	464.49	463.91	464.39	464.46	464.25	463.53	464.15	463.9	462.6	462.6
5.9	5.3	4.97	5.55	5.07	5.00	5.21	5.92	5.31	5.6	6.9	6.9
50	35	28=C6	28=Gut	14		14	28=Gut	28=C6	35	42	50
463.8	464.1	464.14	464.10	464.59	464.68	464.46	463.84	464.45	463.9	463.7	462.6
5.7	5.4	4.72	5.36	4.87	4.78	5.00	5.62	5.01	5.6	6.8	6.9
50	35	28=C6	28=Gut	14		14	28=Gut	28=C6	35	43	50
464.0	464.0	464.5	464.31	464.91	464.81	464.70	464.18	464.75	464.4	464.1	462.8
5.5	5.5	5.0	5.15	4.75	4.65	4.76	5.28	4.71	5.1	5.4	6.7
50	41	29	28=Gut Trnch	14		14	28=Gut	28=C6	29	35	50

469.46

El Cajon Blvd.

17+67.8

17+57.6 = W.L. Choctaw

TP 4.68 468.79 4.76 464.11

17+04.21 = B.C. Lt.

16+50

16+0

468.87

Lt ℄ Rt

464.1 464.09 463.49 463.41 463.85 463.92 463.70 463.12 463.77 463.4 463.3

4.7 4.70 5.30 5.38 4.94 4.87 5.09 5.67 5.02 5.4 5.5
41.8=Cb 41.8=Gut 28 14 14 28=Gut 28=Cb 33 50

464.2 464.02 463.39 463.82 463.94 463.71 463.16 463.77 463.4 463.2

4.6 4.77 5.40 4.97 4.85 5.08 5.63 5.02 5.4 5.6
50 28=Cb 28=Gut 14 14 28=Gut 28=Cb 33 50

468.79

463.9 464.17 464.07 463.47 463.95 463.98 463.81 463.25 463.92 463.3 463.4

5.0 4.70 4.80 5.40 4.92 4.89 5.06 5.62 4.95 5.6 5.5
50 31=Conc. Dr. 28=Cb 28=Gut 14 14 28=Gut 28=Cb 35 50

464.96 464.22 463.59 464.02 464.04 463.87 463.37 464.01 463.8 463.4

3.91 4.65 5.28 4.85 4.83 5.00 5.50 4.86 5.1 5.5
41=Conc. Floor 28=Cb 28=Gut 14 14 28=Gut 28=Cb 29 50

464.66 464.29 463.65 464.03 464.12 463.97 463.41 464.05 463.9 463.3 463.4

4.21 4.58 5.22 4.84 4.75 4.90 5.46 4.82 5.0 5.6 5.5
41 N.W. Walk 28=Cb 28=Gut 14 14 28=Gut 28=Cb 29 35 50

468.87

Lt ℄ Rt

Station												
19+50	463.8 / 5.0 / 50'	463.8 / 5.0 / 40'	463.26 / 5.53 / 28=Drive	463.15 / 5.64 / 28=Gut	463.62 / 5.17 / 14	463.68 / 5.11	463.58 / 5.21 / 14	463.07 / 5.72 / 28=Gut	463.62 / 5.17 / 28=Cb	463.7 / 5.1 / 37	463.5 / 5.3 / 50	
19+0	463.7 / 5.1 / 50'	464.0 / 4.8 / 31	463.93 / 4.86 / 28=Cb	463.28 / 5.51 / 28=Gut	463.73 / 5.06 / 14	463.79 / 5.00	463.58 / 5.21 / 14'	463.03 / 5.76 / 28=Gut	463.62 / 5.17 / 28=Cb	463.6 / 5.2 / 50		
18+50	463.4 / 5.4 / 50'	463.9 / 4.9 / 42	464.04 / 4.75 / 28=Cb	463.37 / 5.42 / 28=Gut	463.82 / 4.97 / 14	463.88 / 4.91	463.68 / 5.11 / 14'	463.13 / 5.66 / 28=Gut	463.72 / 5.07 / 28=Cb	463.8 / 5.0 / 36	463.2 / 5.6 / 40	463.1 / 5.7 / 50
18+09.4 = E.L. Choctaw	464.2 / 4.6 / 50'	463.96 / 4.83 / 28=Cb	463.34 / 5.45 / 28=Gut	463.82 / 4.97 / 14	463.84 / 4.95	463.69 / 5.10 / 14	463.12 / 5.67 / 28=Gut	463.71 / 5.08 / 28=Cb	463.8 / 5.0 / 38'	463.0 / 5.8 / 50		
17+99.2	464.0 / 4.8 / 50	463.99 / 4.80 / 39.2=Cb.Ec.	463.30 / 5.49 / 39.2=Gut	463.39 / 5.40 / 28	463.81 / 4.98 / 14	463.86 / 4.93	463.68 / 5.11 / 14	463.10 / 5.69 / 28=Gut	463.74 / 5.05 / 28=Cb	463.7 / 5.1 / 38	463.2 / 5.6 / 50	
17+83.5	463.8 / 5.0 / 50	463.83 / 4.96 / 40.5=H.Pav.	463.42 / 5.37 / 28	463.86 / 4.93 / 14	463.89 / 4.90	463.75 / 5.04 / 14	463.09 / 5.70 / 28=Gut	463.17 / 5.62 / 28=Drive	463.1 / 5.7 / 50			

468.79

468.79

Lt ℄ Rt

Station					
21+18.99 = H.L. Art					
21+0					
20+50					
20+32.04 E.C.					
TP	4.31	467.64	5.46	463.33	on E.C. Mon 20+32.04 28' Lt.
20+0					
		468.79			

21+18.99

463.1	463.21	463.09	462.46	462.87	462.99	462.76	462.17	462.79	462.3	462.2
4.6	4.43	4.55	5.18	4.77	4.65	4.88	5.47	4.85	5.3	5.4
50	46	28:Cb	28	14		14	28:Gut	28:Cb	36	50

21+0

462.8	463.17	462.50 (10)	462.99	463.07	462.83	462.30	462.91	462.8	462.3	462.3
4.8	4.47	5.14	4.65	4.57	4.81	5.34	4.73	4.8	5.3	5.3
50'	28:Cb	28:Gut	14'		14'	28:Gut	28:Cb	34	40	50

20+50

463.2	463.46	462.80	463.33	463.39	463.16	462.59	463.27	463.3	462.2	462.1
4.4	4.18	4.84	4.31	4.25	4.48	5.05	4.37	4.3	5.4	5.5
50'	28:Cb	28:Gut	14'		14'	28:Gut	28:Cb	35'	43'	50

20+32.04 E.C.

463.2	463.59	462.90	463.43	463.48	463.27	462.73	463.40	463.1	462.6
4.4	4.05	4.74	4.21	4.16	4.37	4.91	4.24	4.5	5.0
50	28:Cb	28:Gut	14'		14	28'	28:Cb	37	50

467.64

20+0

463.4	463.3	463.67	463.01	463.54	463.59	463.38	462.85	462.94	463.54	463.59	463.1
5.4	5.5	5.12	5.78	5.25	5.20	5.41	5.94	5.85	5.25	5.20	5.7
50'	35'	28:Cb	28:Gu	14'		14'	28:Gut	28:Dr	33:Dr	38:S/Dr	50

468.79

El Cajon Blvd.

Lt ℄ Rt

Station												
22+50	461.1 6.5 50'	461.8 5.8 44'	462.09 5.55 28:Cb	461.45 6.19 28:Gut	462.07 5.57 14	462.27 5.37	462.04 5.60 14	461.72 5.92 28=Gut	462.36 5.78 28:Cb	462.2 5.4 32'	461.5 6.1 36	461.7 5.9 50'
22+0	461.6 6.0 50'	462.2 5.4 40	462.39 5.25 28:Cb	461.76 5.88 28 Gut	462.32 5.32 14	462.53 5.11	462.31 5.33 14'	461.78 5.86 28 Gut	462.42 5.22 28:Cb	462.1 5.5 34	461.7 5.9 50	
21+69.07 = E.L. Ard St	462.1 5.5 50'	462.7 4.9 40'	462.47 5.17 28:Cb	461.84 5.80 28:Gut	462.51 5.13 14	462.73 4.91	462.51 5.13 14'	461.96 5.68 28 Gut	462.57 5.07 28:Cb	462.3 5.3 35	462.1 5.5 50'	
21+59	461.7 5.9 50'	462.60 5.04 38.7:Cb Ent	461.91 5.73 38.7:Gut	462.04 5.60 28	462.62 5.02 14	462.81 4.83	462.59 5.05 14	462.00 5.64 28:Gut	462.63 5.01 28:Cb	462.5 5.1 35	462.0 5.6 50	
21+44.03	462.4 5.2 50'	462.54 5.10 39.4:MH Box	462.30 5.24 28'	462.76 4.88 14'	462.87 4.77	462.64 5.00 14	462.07 5.57 28:Gut	462.74 4.90 28:Cb	462.1 5.5 37'	462.0 5.6 50		
21+29	462.97 4.67 50:Cb	463.06 4.58 39.4:Cb EC	462.40 5.24 39.4 Gut	462.40 5.24 28	462.84 4.80 14'	462.94 4.70 0	462.70 4.94 14'	462.13 5.51 28:G	462.77 4.87 28:Cb	462.3 5.3 35	462.0 5.6 50'	

467.64

467.64

24+63					
24+25					
24+0					
23+50					
TP	3.02	464.96	5.70	461.94	Nail Power Pole 23+44
23+0					
		467.64			

Lt ℄ Rt

May 23-40

24+63

459.42	459.56	460.73	460.06	460.75	461.01	460.74	460.22	460.81	460.7	460.2
5.54 / 50 Walk	5.40 / 30 = Walk	4.23 / 28 : Cb	4.90 / 28 = Gut	4.21 / 14	3.95	4.22 / 14	4.74 / 28 = Gut	4.15 / 28 : Cb	4.3 / 35	4.8 / 50

24+25

459.77	459.83	460.7	460.45	460.38	461.05	461.31	461.00	460.39	461.07	460.1	460.0
5.19 / 50 = Drive	5.13 / 38 : Dr.	4.3 / 33'	4.51 / 28 : Dr.	4.58 / 28 : Gut	3.91 / 14	3.65	3.96 / 14	4.57 / 28 : Gut	3.89 / 28 Cb	4.9 / 40'	5.0 / 50

24+0

459.6	459.9	461.12	460.48	461.21	461.46	461.18	460.53	461.24	461.2	460.2
5.4 / 50	5.1 / 31	3.84 / 28 = Cb	4.48 / 28 = Gut	3.75 / 14	3.50	3.78 / 14	4.43 / 28 : Gut	3.72 / 28 = Cb	3.8 / 33	4.8 / 50

23+50

460.0	460.4	461.41	460.87	461.48	461.66	461.41	460.83	461.45	460.9	460.6
5.0 / 50	4.6 / 33	3.55 / 28 = Cb	4.09 / 28 = Gut	3.48 / 14	3.30	3.55 / 14	4.13 / 28 = Gut	3.51 / 28 = Cb	4.1 / 36	4.4 / 50

464.96

23+0

461.1	461.6	461.74	461.13	461.77	461.94	461.70	461.20	461.81	461.8	460.7	460.7
6.5 / 50	6.0 / 44	5.90 / 28 : Cb	6.51 / 28 : Gut	5.87 / 14	5.70	5.94 / 14	6.44 / 28 : Gut.	5.83 / 28 : Cb	5.8 / 33	6.9 / 46	6.9 / 50

467.64

	Lt	℄	Rt
27+0	460.7 / 460.1 / 458.31 / 457.73 / 458.32 / 458.45 / 458.21 / 457.64 / 458.23 / 462.3 / 461.0		
	4.3 50' / 4.9 36' / 6.65 28:Cb. / 7.23 28:Gut / 6.64 14' / 6.56 / 6.75 14' / 7.22 28:Gut / 6.73 28:Cb / 5.7 30' / 4.0 50'		
26+50	460.6 / 460.7 / 458.6 / 458.64 / 458.58 / 459.21 / 459.37 / 459.16 / 458.71 / 459.27 / 460.9 / 461.0		
	4.4 50' / 4.3 41' / 6.4 36' / 6.32 28:Dr. / 6.38 28:Gut / 5.75 14' / 5.59 / 5.80 14' / 6.35 28:Gut / 5.69 28:Cb / 4.1 31' / 4.0 50'		
26+0	460.1 / 460.2 / 459.95 / 459.36 / 459.89 / 460.11 / 459.88 / 459.46 / 460.11 / 460.7 / 460.7		
	4.9 50' / 4.8 34' / 5.01 28:Cb. / 5.60 28:Gut / 5.07 14' / 4.85 / 5.08 14' / 5.50 28:Gut / 4.85 28:Cb / 4.3 33' / 4.3 50'		
25+50	460.0 / 460.35 / 459.71 / 460.25 / 460.48 / 460.27 / 459.79 / 459.86 / 460.0 / 460.3		
	5.0 50' / 4.61 28:Cb / 5.25 28:Gut / 4.71 14' / 4.48 / 4.69 14' / 5.17 28:Gut / 5.10 28:Dr. / 5.0 34' / 4.7 50'		
25+26	459.64 / 459.96 / 459.93 / 459.83 / 460.40 / 460.65 / 460.43 / 459.92 / 460.51 / 460.7 / 460.1		
	5.32 50' 60°Dr. / 5.00 30°Dr. / 5.03 28Dr. / 5.13 28Gut / 4.56 14' / 4.31 / 4.53 14' / 5.04 28Gut / 4.45 28:Cb / 4.3 34' / 4.9 50'		
25+0	459.3 / 460.1 / 460.55 / 459.91 / 460.58 / 460.78 / 460.52 / 459.99 / 460.58 / 460.6 / 459.9		
	5.7 50' / 4.9 29' / 4.41 28:Cb / 5.05 28:Gut / 4.38 14' / 4.18 / 4.44 14' / 4.97 28Gut / 4.38 28:Cb / 4.4 40' / 5.1 50'		

464.96

464.96

June 10-40

Lt ℄ Rt

28+20

456.1	455.53	455.99	456.05	455.94	455.54	456.13	456.6	456.3
4.55 50	5.02 28 Dr.	4.56 14	4.50	4.61 14	5.01 28 C	4.42 28 Cb	4.0 40	4.32 50

28+01.4

457.3	457.2	456.4	455.83	456.32	456.38	456.31	455.89	455.63	456.31	457.1
5.2 50	5.1 45	4.2 41	4.77 28 Gut Dr.	4.53 14	4.17	4.24 14	4.66 28	4.92 37.5 Gut	4.24 37.5 Cb	3.5 50

27+73

459.0	458.7	456.9	456.43	456.37	456.91	458.97	456.85	456.44	456.89	457.3
1.6 50	1.9 45	3.7 34	4.12 28 Dr.	4.18 28 Gut	3.64 14	3.58	3.70 14	4.11 28	3.66 39.5 Gut Cb	3.3 50

27+42.8

459.3	457.53	456.89	457.42	457.53	457.37	456.92	457.23	457.92	458.6
1.3 40	3.02 28 Cb	3.66 28 Gut	3.13 14	3.02	3.18 14	3.63 28	3.32 40.7 Gut	3.63 40.7 Cb	3.0 50

27+24.4

459.7	459.3	458.1	457.84	457.23	457.73	457.91	457.74	457.26	#52 83	460.6	460.4	459.6
0.9 50	1.3 36	2.5 30	2.71 28 Cb	3.32 28 Gut	2.82 14	2.64	2.81 14	3.39 28 Gut	2.70 28 Cb	0.0 50	0.2 38	1.0 50

460.55

TP 2.46 460.55 6.57 458.39 27+21

3 Hail's Pole

464.96

Lt. Z Rt.

TP	4.50	457.34	7.71	452.84
29+74.01 EC				
29+43				
29+0				
28+89.22 PCC				
28+50				

460.55

+44.3	4450	452.6	453.00	452.39	452.93	453.05	452.95	452.49	453.20	452.9	451.5	451.2 / 451.1
16.3 60	15.6 47	8.0 33	7.55 28-CL	8.16 28	7.62 14	7.50	7.60 14	8.06 28-Gut	7.35 28-CL	7.7 34	9.1 40	9.2 50 / 9.5 60
446.1	446.6	453.5	453.67	453.06	453.45	453.59	453.55	453.05	453.69	453.6	451.46	448.18	450.3	449.9
14.5 60	14.0 47	7.1 32	6.88 28-CL	7.49 28-Gut	7.10 14	6.96 60	7.00 14	7.50 28-Gut	6.86 28-CL	7.0 31	9.09 36-HW	12.37 36-FL	10.3 45	10.7 60
454.7	454.7	454.60	454.00	453.38	454.50	454.37	454.05	454.64	454.6	454.0	452.1	451.0
5.9 60	5.9 50	5.95 28-CL	6.55 28-Gut	6.17 14	6.05	6.18 14	6.50 28-Gut	5.91 28-CL	6.0 34	6.6 45	8.5 50	9.6 60
454.3	455.1	454.14	454.65	454.77	454.60	454.22	454.77	455.0	454.6	451.6	451.8
6.3 50	5.6 30	6.41 28-Gut	5.90 14	5.78	5.95 14	6.33 28-Gut	5.78 28-CL	5.6 38	6.0 46	9.0 50	8.8 60
455.3	454.89	455.42	455.56	455.41	454.99	455.57	455.58	455.1
5.3 50	5.46 28-Out	5.13 14	4.99	5.14 14	5.55 28-Gut	4.96 28-CL	4.8 40	5.5 50

460.55

					Lt.		℄		Rt.
31+18									
TP	3.84	456.67	4.51	452.83					
30+84.5									
30+67 =Cb BC on S Rt.									
30+50									
30+10									
		457.34							

31+18

447.4	448.2	449.0	451.6	452.24	451.63	452.25	452.55	452.55	452.56	452.37	452.94
9.3	8.5	7.7	5.1	4.43	5.04	4.42	4.12	4.13	4.11	4.30	3.73
60	50	41	34	28=Cb	28=Gut	14		14	28	50=Gut.	50 Cb

30+84.5

444.0	445.2	446.7	451.9	452.44	451.81	452.31	452.58	452.65	452.74	452.82	452.5
12.7	11.5	10.0	4.8	4.23	4.86	4.36	4.09	4.02	3.93	3.86	4.2
60	50	42	32	28=Cb	28=Gut	14	0	14	28	50 1/4 Pav.	60

456.67

30+67

443.1	445.1	452.2	452.50	451.90	452.37	452.63	452.71	452.53	452.88	452.8	452.6
12.6	11.6	5.1	4.84	5.44	4.97	4.71	4.63	4.81	4.46	4.5	4.7
60	43	32	28=Cb	28=Gut	14		14	28=Gut	28=Cb	40	60

30+50

444.3	446.2	452.2	452.51	451.92	452.39	452.58	452.54	452.14	452.69	452.6	452.7	452.9
13.0	11.1	5.1	4.83	5.43	4.95	4.76	4.80	5.20	4.66	4.7	4.6	4.4
60	43	32	28 Cb	28=Gut	14		14	28	28=Cb	35	50	60

30+10

		446.9	445.62	452.3	452.75	451.74	452.47	452.66	452.39	451.46	452.51	452.7	452.1	452.7
12.0	11.0	10.4	11.72	5.0	4.59	5.60	4.87	4.68	4.95	5.88	4.83	4.6	5.2	4.6
60	50'	41	38.5 F.L.	32	28=Cb	28= Grating	14		14	28 Gut on Grd.	28 Cb	40	45	60

457.34

Lt ℄ Rt.

BM 4.18 452.49 ✓ SW B.P. F. Cajon + Rolando 452.46

	452.5	452.5	452.6	452.16	451.55	452.04	452.24	452.31	452.26	452.05	452.71	452.95
32+0	4.2 / 60	4.2 / 50	4.1 / 40	4.51 / 30 / 28 CL	5.12 / 28	4.63 / 14	4.43	4.34 / 14	4.41 / 28	4.67 / 36 Gut	3.96 / 36 CL	3.72 / 50 Hole
	449.7	450.2	450.7	452.6	452.34	451.67	452.19	452.41	452.49	452.38	452.22	452.86	453.07
31+44	7.0 / 60	6.5 / 50	6.0 / 40	4.1 / 35	4.83 / 28 CL	5.00 / 28 Gut	4.48 / 14	4.86	4.18 / 14	4.29 / 28	4.45 / 36 Gut	3.81 / 36 CL	3.66 / 50 Hole

456.67

456.67

Moore
Osborne
Hale
12-7-40 X sec alley 20' wide
Blk 60 Ocean Beach

NEBP 3.72 14.27 11.05
Bacon
+
Newport

0-17 E gutter Bacon

S	pav.	4.34	9.93
C	"	4.41	9.86
N	"	4.43	9.84

0+00 = E.L. Bacon

N	Top c6	3.46	10.81
N	Pav	3.59	10.68
C	"	4.01	10.26
S	"	3.61	10.66
S	c6	3.48	10.79

0+07

N +0.9 1.4 dr. Tel. Pole

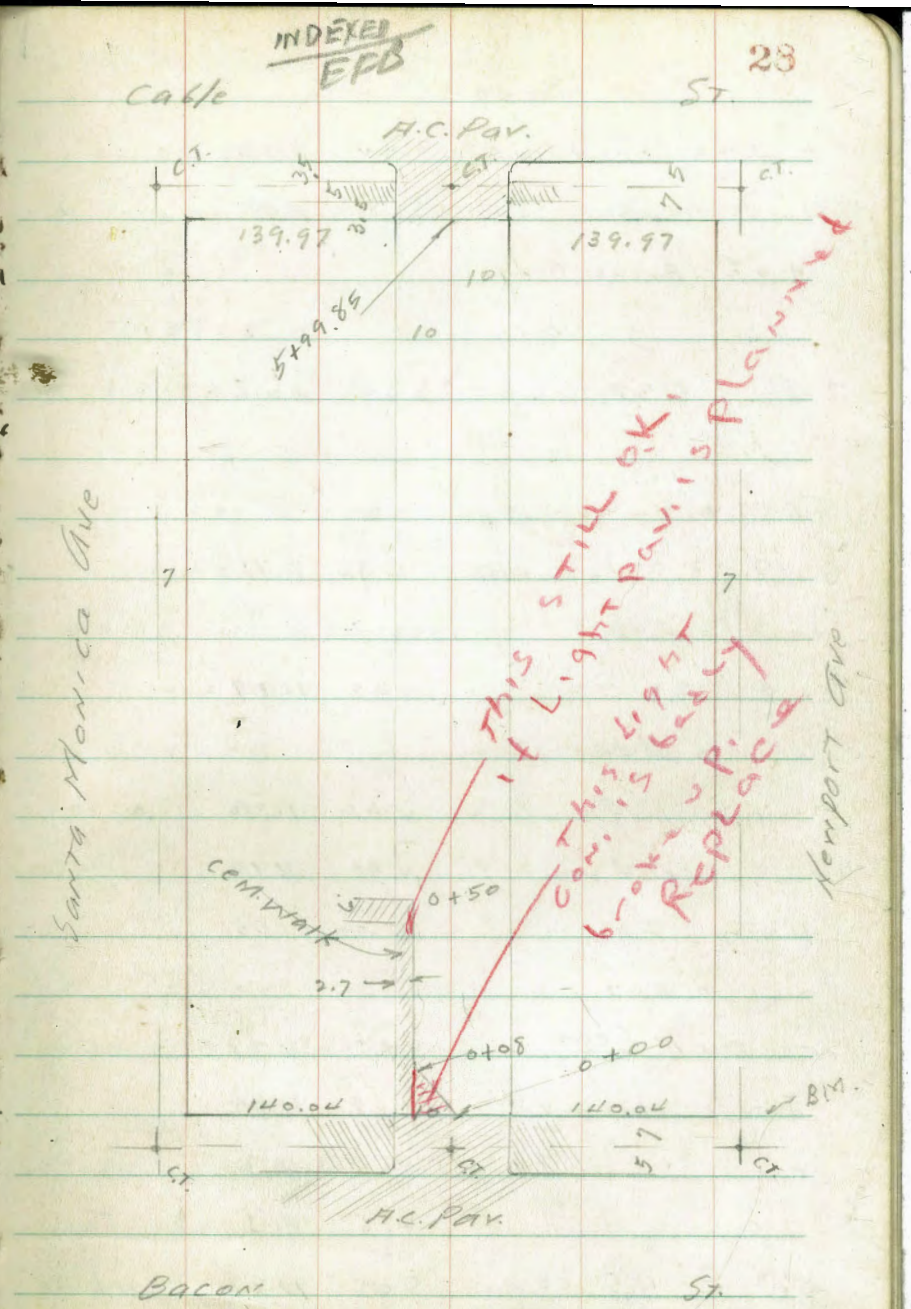
0+08

S		3.5	10.8
C		3.8	10.5

Note! Suggest 1.0' exception on either side alley in paving acct. of garages etc. over line.

INDEXED
EPB

23



	14.27		
C +7.3 CCNK WK		3.27	11.03
N " "		3.18	11.09
+0.2 Brick Bldg			
T.P.	5.38	16.01	3.64	10.63
	0+29		
S ℄ 3.3 door sill		4.90	11.11
	0+40		
S ℄ 3.3 " "		4.93	11.08
	0+42		
N - 0.3 Bldg		4.91	11.10
N CCNK walk		4.91	11.10
+2.7 " "		5.00	11.01
	0+47		
N ℄ 6' CCNK WK		4.62	11.39
+2.7 edge wk.		4.69	11.32
C		4.7	11.3
+6		4.5	11.5
S ℄ 4.5 CCNK WK		5.01	10.87	ON LINE

	16.01		
	0+50		
N beg. Bd. fence		0.4 back	= Cor. Bldg.
N end " "	0+58.5	"	0.1 "
	0+55		
+1.5 1.2 P.P.			
0+50 to 1+00 Salt hedge on S.L. line			
	0+60		
N-4.3 WL 3 car gar.		3.7	12.3	dirt
	0+88		
N-4.4 E.L. " " "		3.8	12.2	"
N		3.8	12.2	
C		4.0	12.0	
S		3.7	12.3	
	1+00		
N +0.4 beg. Bd. fence				OH in valley
	1+23		
N +1.3 8.6' Tel. Pole			
	1+25		
N +0.8 end Bd fence			

16.01

1+25

N +0.8 W.L. Bd. shed gar. = 0.8 in alley dirt

1+30

N +0.8 E " " 3.7 12.7 "

C 3.5 12.8

S 3.3 12.7

+20 3.3 12.7

1+46

N +1.0 E.L. Bd. shed above (1.0 in alley)

1+55

N +0.9 W.L. Bd 2 car gar. 3.5 12.5 dirt

1+74

0.8 in alley

N +0.7 E.L. " " 3.4 12.6 "

+5 3.1 12.9

C 3.3 12.7

+6 3.4 12.6

S 1.4 P.P. 2.9 13.1

+20 3.0 13.0

1+74.1

N +0.2 beg. Bd. shed (in alley)

16.01

1+95

N E.L. Bd shed

1+95.5

N -0.3 W.L. Bd gate

2+04

N E.L. " "

2+04.1

N -3.6 W.L. 2 car gar 3.2 12.8 dirt

2+23

S +20 door step 1.7 14.5

dry goods store

S 2.2 13.8

C 2.4 13.6

N 2.8 13.2

+3.5 E.L. 2 car gar. 2.9 13.1 "

2+24

N -5 W.L. 2 car gar. 2.4 13.6 "

2+48

N -5 E.L. " " 2.4 13.6 "

2+50

N -20 2.4 13.6

N -0.3 beg. picket fence = 0.3 back of alley line

16.01

N		2.4	13.6	
+5		2.0	14.0	
C		2.1	13.9	
+5		2.2	13.8	
S		1.6	14.4	
+1.1 NW Cor	Cem. Brick Bldg.	1.6	14.4	✓
T.P.	6.40 21.28	1.13	14.88	Nail Tel. Pole

2+41

N+1.8 0.7 dr. Tel. P. ✓

2+75

S −1.0 E 10' door | Cem. Sill | 5.97 | 15.31 | Exit Theatre ✓

3+00

S −1.0 NE Cor. Theatre ✓

S 6.0 15.3

C S.M.H. Rim 6.66 14.62

N 7.0 14.28

3+27

S +0.3 1.4 P.P. ✓

21.28

3+25

N end Picket fence on line ✓

N W.L. Sin. gar. ✓

3+32

N +0.3 E 10' gar door 6.5 14.8 0.3 in alley dirt floor ✓

3+39

N +0.1 E.L. Sin. gar. ✓

N −0.1 beg 6d. fence ✓

3+50

N −0.3 Bd fence ✓

N	5.9	15.4	
C	6.1	15.2	
S	5.9	15.4	
+10	6.0	15.3	

3+65

N −0.3 end Bd fence ✓

3+70

N −9.3 E Sin. gar. 5.74 15.54 Cem. ✓

N " Cem apron 5.74 15.54 ✓

21.28

3+95

N +0.5 1' Tel. P.

4+00

-10	5.2	16.1
S	5.2	16.1
C	5.5	15.8
N	5.3	16.0
+10	5.3	16.0

4+47

N +0.9 1' Tel. P.

4+50

-20	4.9	16.4
N	4.4	16.9
C	4.9	16.4
+9.7 1.2 P.P		
S	4.7	16.6
+20	4.5	16.8

4+55

-20	6.9	14.4
-3	6.2	15.1

21.28

S	4.9	16.4
C	4.8	16.5
N	4.8	16.5

5+00

-10	4.6	16.7
N	4.4	16.9
C	4.6	16.7
S	4.8	16.5
+3	5.9	15.4
+20	6.3	15.0

5+29

N +1.2 1' Tel. P.

5+50

-.20	5.9	15.4
-.3	5.4	15.9
S	4.5	16.8
C	4.4	16.9
N	4.1	17.2
+10	4.3	17.0

21.28

5+85

-10	3.9	17.4	
N	4.5	16.8	
C	4.9	16.4	
S	5.0	16.3	
+20	5.5	15.8	
5+99.85	W/L Cable	ST	
S C6	4.95	16 33	
S Pav	5.18	16.10	✓
C "	5.41	15.67	
N "	5.22	16.06	
N C6	5.03	16.25	
W gut Cable			
N Pav	5.70	15.55	
C "	5.74	15.54	
S "	5.73	15.25	
NEBP Newport Cable	5.26	16.02	1401

Moore Xsec Linwood 50' wide 10' curbs 7½ 1½ s

1-20-41. Pringle To Mission Hills Blvd

13' hd. + CT	2.06	198.52 ✓		196.46	Pringle Cor
T.P.	0.55	185.96 ✓	13.11	185.41 ✓	
T.P.	0.23	173.29 ✓	12.90	173.06 ✓	

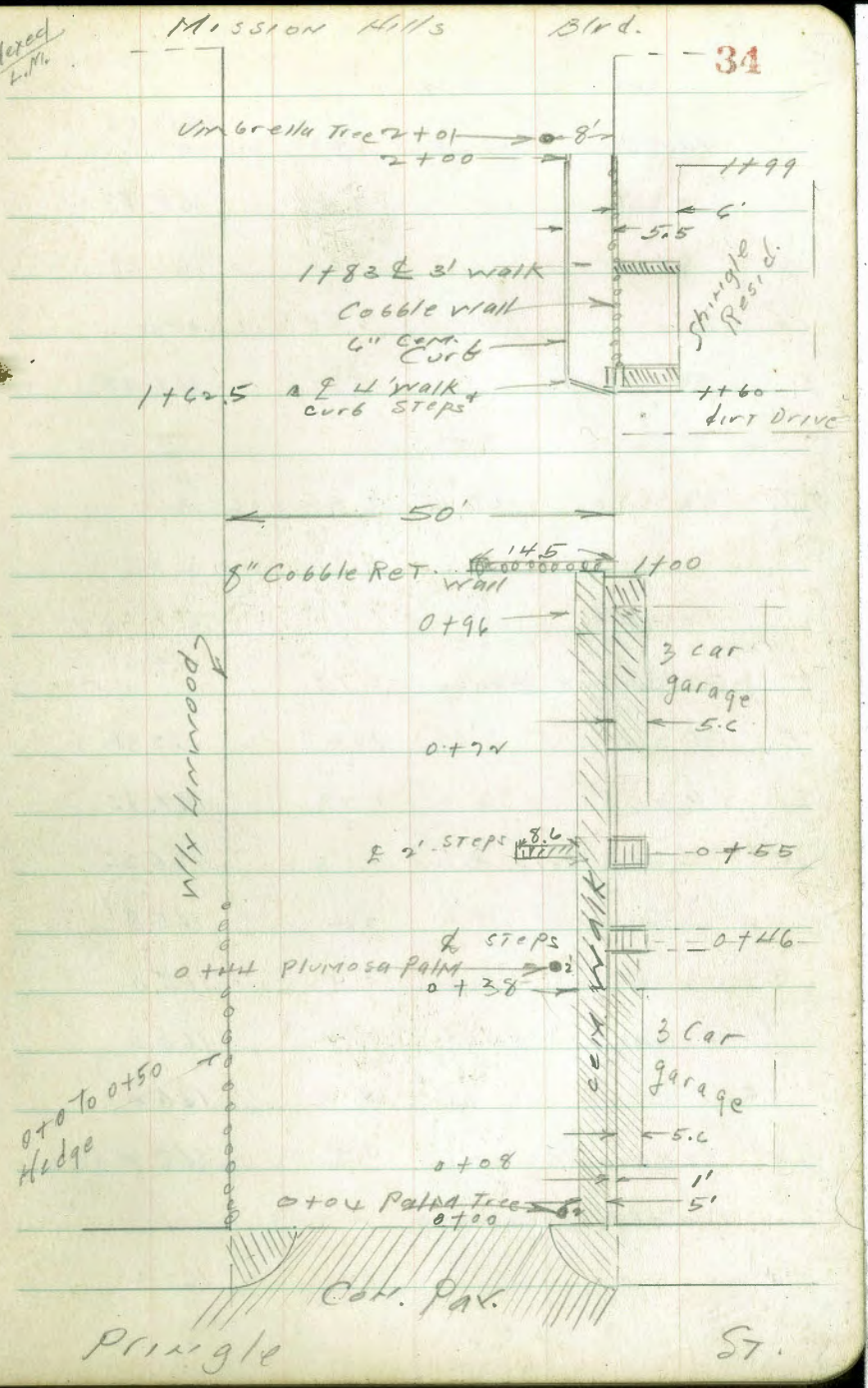
0-10 = Nly c6. Line of Pringle

E c6	6.14	167.15	
E gut	6.46	166.83	
c6 Pav	7.11	166.18	
1/4 "	7.67	165.67	
c "	8.75	165.04	
1/4 "	9.06	164.23	
c6 "	9.95	163.34	
W gut	10.88	162.41	
W c6	10.23	163.06	

0+0 Nly Pringle

W Cor. Ref.	9.88	163.41	
c6	10.12	163.17	
gut Pav	10.56	162.73	
1/4 "	9.41	163.88	

Red and Plotted 1-24-1941



		173.29		
C	Pav		8.26	165.03
1/4	"		7.46	165.83
gut	"		7.06	166.23
cb			6.25	167.04
E	Cor. Ret.		5.87	167.42
T.P.		2.10	6.98	166.31
		168.41		
	0+08			
- 5.5	S end	3 car garage	0.78	167.63 cemt
E +1			1.10	167.31
E +6			1.49	167.12
cb	S edge Cem drive		2.15	166.26
1/4			2.4	165.8
C			3.4	165.0
1/4			4.2	164.2
cb			4.4	164.0
W	Hedge		4.7	163.7
	0+39			
W	"		5.1	163.3
cb			4.8	163.6
1/4			4.6	163.8
C			4.2	164.2
1/4			3.5	164.9
cb	N edge Cem drive		2.13	166.28
+4	walk		1.41	167.00
+9	"		1.18	167.23
+5.5	N end 3 car gar		0.87	167.54
	0+44			
- 5			0.90	167.51
E +1			1.19	167.22
E +6			1.46	166.95
cb			1.6	166.8
+4			1.9	166.5
+6			3.2	165.2
1/4			3.6	164.8
C			4.3	164.1
	0+46 & 4' Cem steps			
E +1	E. edge 5' Cem walk		1.20	167.21
E -	Top step		+ 0.90	169.31

0455 & 4' conc. steps

E ~ 6	Top step	+ 3.0	168.7
E	bot. steps	1.41	167.00
+1		1.47	166.94
+6		1.70	166.71
c6		1.78	166.63
+3.7	Top 7 steps	1.97	166.44
+4.6	bot. "	2.92	165.49
1/4		3.6	164.8
C		4.5	163.9
	0+70		
C		4.6	163.8
E 1/4		3.5	164.9
+7		3.7	165.2
+4		2.3	166.1
c6		2.1	166.3
+4 conc walk		2.78	165.13
+9 " "		2.18	166.23
	0+72		
E - 5.4	S.L. 3 car gar.	1.82	166.59 conc. XL
E +1		2.25	166.16

E + C	conc	2.36	166.05
c6		2.5	165.9
1/4		3.6	164.8
C		4.6	163.8
1/4		5.3	163.1
c6		5.7	162.7
W		6.1	162.3
+10		6.6	161.8
	0+96		
-10		8.0	160.4
2.1		7.0	161.4
o6		6.4	162.0
1/4		5.8	162.6
C		5.0	163.4
1/4		4.2	164.2
c6		3.5	164.9
+4 end 5' conc wk.		3.78	165.13
+9 " " " "		3.23	165.18
E +5.6 N end 3 car gar.		1.82	166.59
	0+99		
E - 5.4		2.0	166.4

168.41

E		3.N	165.2
c6		3.6	164.8
+4.5 end	rem. Cobble Wall	3.7	164.7
1/4	.	4.4	164.0
C		5.1	163.3
	1+00		
C		5.0	163.4
1/4		4.4	164.0
+N.5		3.7	164.7
+3 Top end	Cobble Ret Wall	0.70	167.71
c6	" wall	0.67	167.74
+5	" "	0.55	167.86
+5.5	" "	+0.85	169.26
E	" "	+1.0	169.4
	1+15		
W +8.8	& 14" P.P. + Tel.		
T.P.	2.8N 167.93	3.30	165.11
	1+25		
E		0.0	167.9

check levels

NWCP	9.41	110.48		101.07
TP	11.93	121.39	1.0N	109.46
TP	12.35	133.43	0.31	121.08
TP	12.57	145.9N	0.08	133.35
TP	12.89	158.49	0.3N	145.60
TP	12.5N	170.64	0.37	158.1N
T.P.	3.70	167.76	6.58	164.06
check to T.P.			2.8N	164.94

165.11 High 0.17

13' C.T. Pringle & Linwood 3.63 164.13

Why { Art' deduct 0.17 to agree with Orig. Xsec.

37 Winder Columbia

167.93

cb		2.4	165.5
1/4		4.2	163.7
C		4.7	163.2
1/4		5.2	162.7
cb		5.3	162.6
W		8.8	159.1
+10		10.4	157.5
	1+50		
-20		11.9	156.0
W		8.0	159.9
cb		4.4	163.5
1/4		4.4	163.5
C		4.1	163.8
1/4		3.5	164.4
cb		2.9	165.0
E S.L. 9' dirt drive		1.7	166.2
+10 " " " "		0.0	167.9
	1+62.5 = A in 6" curb		
E-1 Top Top Step		0.14	167.29
E+1 " Bot. "		1.73	166.20
" " ground		2.5	165.4

167.93

+5.5 A Top 6" curb		2.54	165.39
cb		3.1	164.8
E 1/4		3.6	164.3
C		4.0	163.9
	1+83		
E-6 E 3' cent walk		2.50	165.43
E " "		2.63	165.30
+1 ground		2.9	165.0
+5.5 6" curb		2.82	165.11
+4 ground		3.2	164.7
cb		3.6	164.3
1/4		4.0	163.9
C		4.0	163.9
1/4		4.1	163.8
cb		4.8	163.1
W		10.0	157.9
+20		12.8	155.1
	2+00		
-20		13.5	154.4
W		10.6	157.3
cb		5.6	162.3

167.93

1/4	4.0	163.9
C	4.2	163.7
1/4	4.2	163.7
C6	3.9	164.0
+4.5 end 6" Curb	3.37	164.56
E	2.8N	165.11
+1 Top Cobble Wall	0.38	167.55
2+20		
-10	1.1	166.8
E	N.0	163.9
+5	3.2	164.7
C6	3.5	163.4
1/4	3.6	164.3
+4	3.8	164.1
C	5.2	162.9
1/4	7.9	160.0
C6	10.3	157.7
W	12.1	155.8
+20	14.8	153.1
2+30		
-20	15.2	152.7
W1	13.2	154.7

167.93

C6	11.6	156.3
1/4	10.6	157.3
C	9.4	158.5
1/4	7.4	160.5
C6	7.3	160.6
E	6.4	161.5
+10	4.0	163.9
2+35		
W +8.9 & 14" P.P.		
2+50		
-10	10.7	157.2
E	11.7	156.2
C6	12.6	155.3
1/2	13.4	154.5
C	14.2	153.7
1/2	15.0	152.9
C6	15.8	152.1
W1	16.2	151.7
+20	18.8	149.1

		167.93		
T.P.	0.87	155.96	12.84	155.09
	2+70			
- 20			12.2	143.7
W			10.5	145.4
C6			9.5	146.4
1/4			9.0	146.9
C			8.4	147.5
1/4			7.5	148.4
C6			6.3	149.6
E			4.5	151.4
+ 10			2.8	153.1
T.P.	0.32	143.33	12.95	143.01
	3+00 S/y Mission Hills Blvd.			
- 10			2.0	141.3
E			3.7	139.6
C6			4.0	139.3
1/4			4.1	139.2
C			5.2	138.1

		143.33		
1/4			8.9	134.4
C6			8.0	135.3
+2.2	& 14" P.P.			
W			8.7	134.6
+ 20			9.8	133.5
T.P.	0.05	130.59	12.79	130.54
	& Mission Hills Blvd			
&	for Sewer		2.6	128.0
13' line	in drain		4.6	126.0
	N.L. Mission Hills Blvd. = 0+00			
&			12.0	118.6
13' line			13.3	117.3
T.P.	0.83	118.30	13.17	117.47
	0+15			
13' line			8.0	110.3
&			5.3	113.0
	0+35			
&			12.6	105.7
13' line			14.9	103.4
T.P.	2.64	107.87	13.07	105.23

19.7.87

0 + 54

E M.H.R.M 7.4 100.5 IW47

" F.h. 15.80 92.97 G.R.H. please check

13' Line 8.1 99.8

0 + 80 Bot. wash

13' Line 12.5 95.4

10 7.94
15 7.9
92.1

Moore
1-20-41.

Xsec Russell St. 70' wide
Locust to Evergreen 18' c6s
8.5 1/4 s

Indexed
J.M.

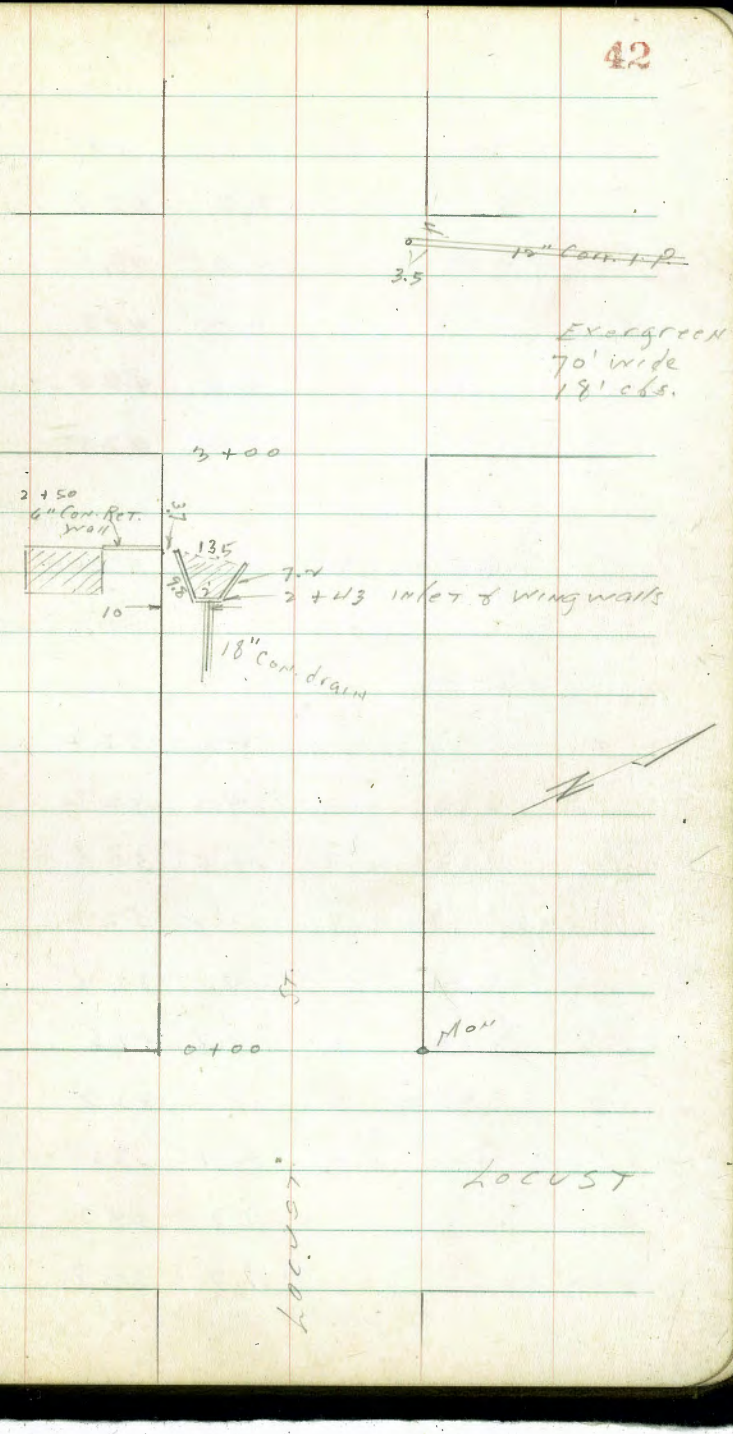
Rosections
Russell

SWBP	12.47	18.21		5.54
T.P.	12.79	30.98	0.0N	18.19
T.P.	12.87	43.79	0.1N	30.86
T.P.	10.20	53.67	0.2N	43.47

WL Locust = 0+00

N on Conc. Mon.	12.22	41.45
c6	11.1	42.6
1/4	10.7	43.0
c	10.3	43.4
1/4	10.1	43.6
c6	10.1	43.6
+8	10.2N	43.5
+12	9.6	44.1
S	9.7	44.0
0+50		
-5	2.5	51.2
S	2.8	50.9
c6	3.7	50.0

42



53.47

1/4			4.6	49.1
C			4.8	48.9
1/4			4.6	49.1
C6			4.7	49.0
N			5.9	47.8
+5			6.N	47.5
T.P.	1+94	66.43	0.18	53.49

0+75

-5			14.2	52.2
N			14.2	52.2
C6			14.5	51.9
1/4			14.N	52.2
C			14.0	52.4
1/4			13.8	52.6
+7			13.7	52.7
C6			13.8	52.6
S			11.7	54.7
+10			11.7	54.7

66.43

1+00

-10			8.5	52.9
S			8.5	52.9
C6			8.4	58.4
1/4			9.1	57.3
C			10.3	56.1
1/4			10.0	56.4
C6			10.0	56.4
N			9.1	57.3
+5			9.0	57.4

1+25

N			1.N	65.2
C6			3.4	63.0
1/4			4.5	61.9
C			5.3	61.1
1/4			4.7	61.7
C6			5.3	61.1
S			5.9	60.6
+10			5.9	60.5
T.P.	1+84	79.25	0.0N	66.41

1+50

-10	14.1	65.2
5	13.8	65.8
c6	13.6	65.7
+3	12.2	62.1
1/4	11.2	68.1
c	11.3	68.0
1/4	10.3	69.0
c6	8.6	70.7
N	5.9	73.3

1+75

N	+4.8	84.1
c6	+1.3	80.6
1/4	0.2	79.1
c	1.8	77.5
1/4	1.7	77.6
5	5.2	74.1
c6	8.0	71.3
5	9.4	69.7
+10	9.9	69.4

79.25

2+00

-10	6.8	72.8
5	6.0	73.3
+12	5.4	73.9
c6	1.9	77.4
T.P. 12.55 91.58	0.22	79.03
+4	10.4	84.2
1/4	9.5	82.1
c	8.4	83.2
1/4	6.0	85.6
c6	3.6	88.0
N	+1.9	93.5

2+06

E M.H. Rim	7.12	84.46
Fline F.W.	1852	72.94

2+25

N	+8.0	99.6
c6	+2.6	94.2
1/4	2.0	89.6
c	3.0	88.6
1/4	5.8	85.8

91.58

+4		7.4	84.4
c6		10.8	80.8
+7		14.4	77.4
5		14.5	77.1
+10		14.6	77.0
	2+43		
5		12.3	79.3
+3		12.3	79.3
+10	Top 8" Hd. wall	13.99	77.59
+10	F.L. 18" Conc. pipe	16.37	75.21
	2+45		
5 - 18.4	E 9' gar. Conc. fl.		80.35 under house
T.P.	11.10	90.54	79.44
	2+50		
5	Top end 6" Con. Ret wall	9.94	80.62
5	ground	10.4	80.1
+3.7	Top wing wall	12.86	77.68
+4	con. apron	14.89	75.65
+14		14.89	25.65

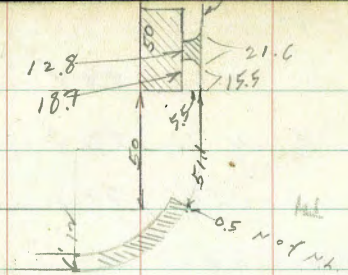
90.54

c6		9.4	81.1
1/4		4.7	85.8
c		2.8	87.7
1/4		+2.0	92.5
c6		+6.9	97.4
4		+13.4	103.9
	2+70		
4		+15.9	106.4
c6		+5.5	96.0
1/4		+0.7	91.2
c		3.8	86.7
1/4		5.7	84.8
+3		10.8	79.7
c6		11.1	79.4
5		4.3	86.2
+10		1.7	88.7
	3+00 E L Evergreen		
5	Top 3/4" pipe	+8.09	98.63
c6		+5.4	95.9
1/4		0.1	90.4
c		2.7	87.8

	90.54		
c + 4		7.3	83.2
1/4		5.6	84.9
cb		+0.5	91.0
N		+10.3	100.8
T.P.	1+41	100.97 1.98	98.56
	E cb on Evergreen		
N		0.6	100.4
cb		11.2	89.8
+ 3		14.7	86.3
+ 5		14.7	86.3
1/4		13.6	87.4
c		7.5	93.5
1/4		4.0	97.0
cb		1.0	100.0
S		+3.7	104.7
	E Evergreen		
S		+11.1	112.1
cb		+4.8	105.8
1/4		+0.3	101.3
c	S.M.H. Rim	3.73	97.24
1/4		7.7	93.3

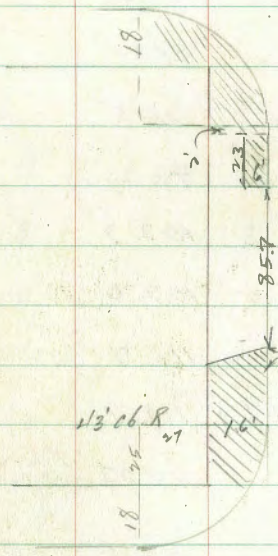
	100.97			
cb		11.6	89.4	
+ 4		11.7	89.3	
N		1.7	99.3	
	W cb Evergreen			
N		5.7	96.3	
+ 7		9.0	92.0	
+ 1 N		9.2	91.8	
cb		5.5	95.5	
1/4		1.8	98.2	
c		+1.3	102.3	
1/4		+6.0	107.0	
cb		+10.3	111.3	
S		+17.9	118.9	
	N +3.5 W cb + 14	5.24	95.73	F.L. outlet 12" Corr. I.P.
	W L Evergreen			
S		+22.4	123.4	
cb		+15.1	116.1	
1/4		+11.4	112.4	
c		+6.3	117.3	
1/4		+3.4	114.4	
cb		0.8	100.2	
+ 5		5.0	95.0	
+ 11		6.1	94.9	
N		2.1	98.9	

Indexed
L M



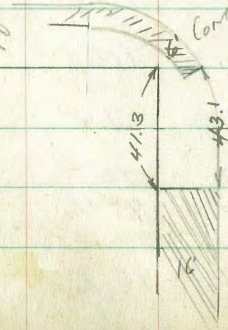
Byron

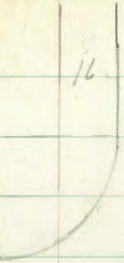
Sdwk. location
on West side
Rosecrans
Addison to curtis
Moore
2-18-X1.



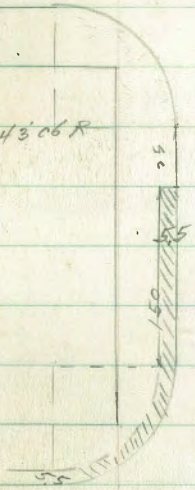
Note! from Addison
to Xenophon all New
State curb = C"

Addison



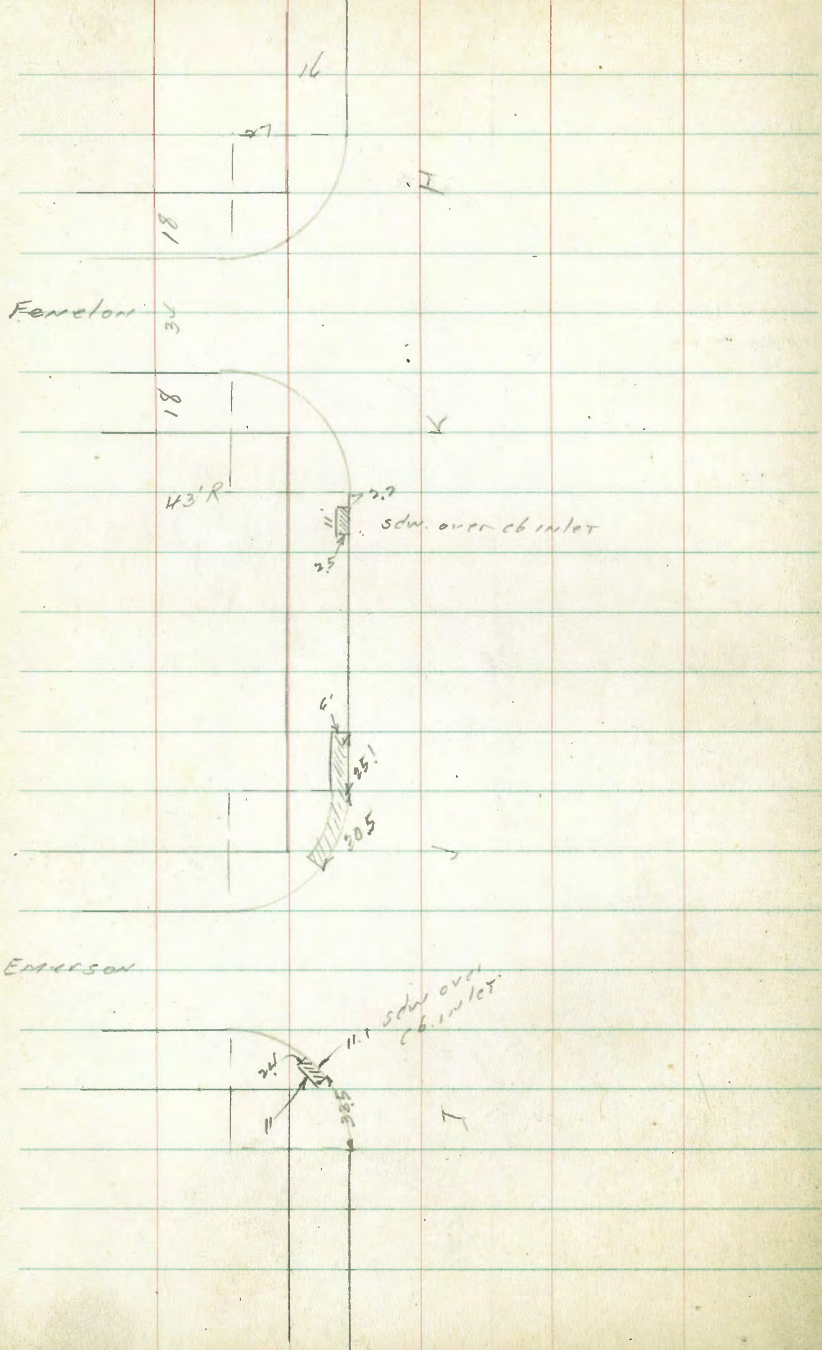


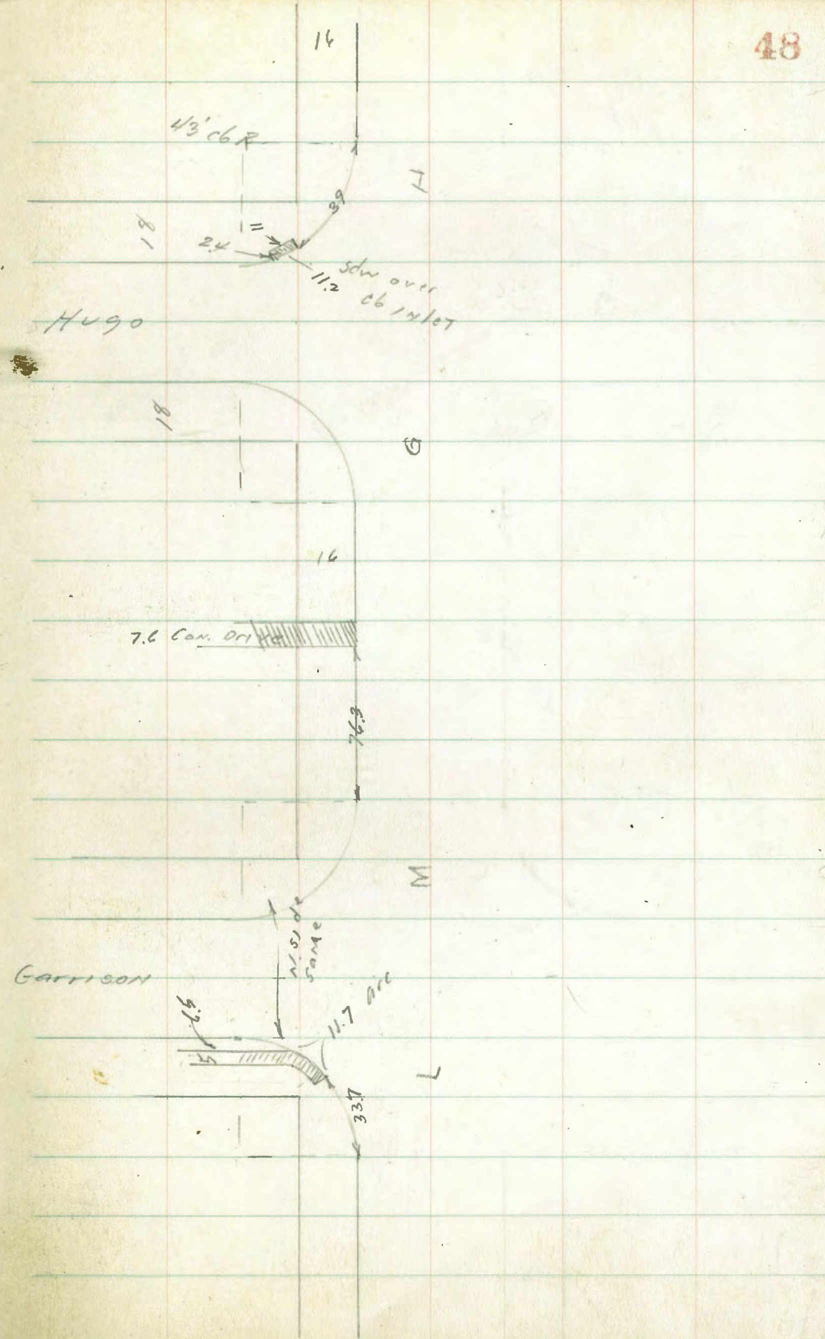
Dickens

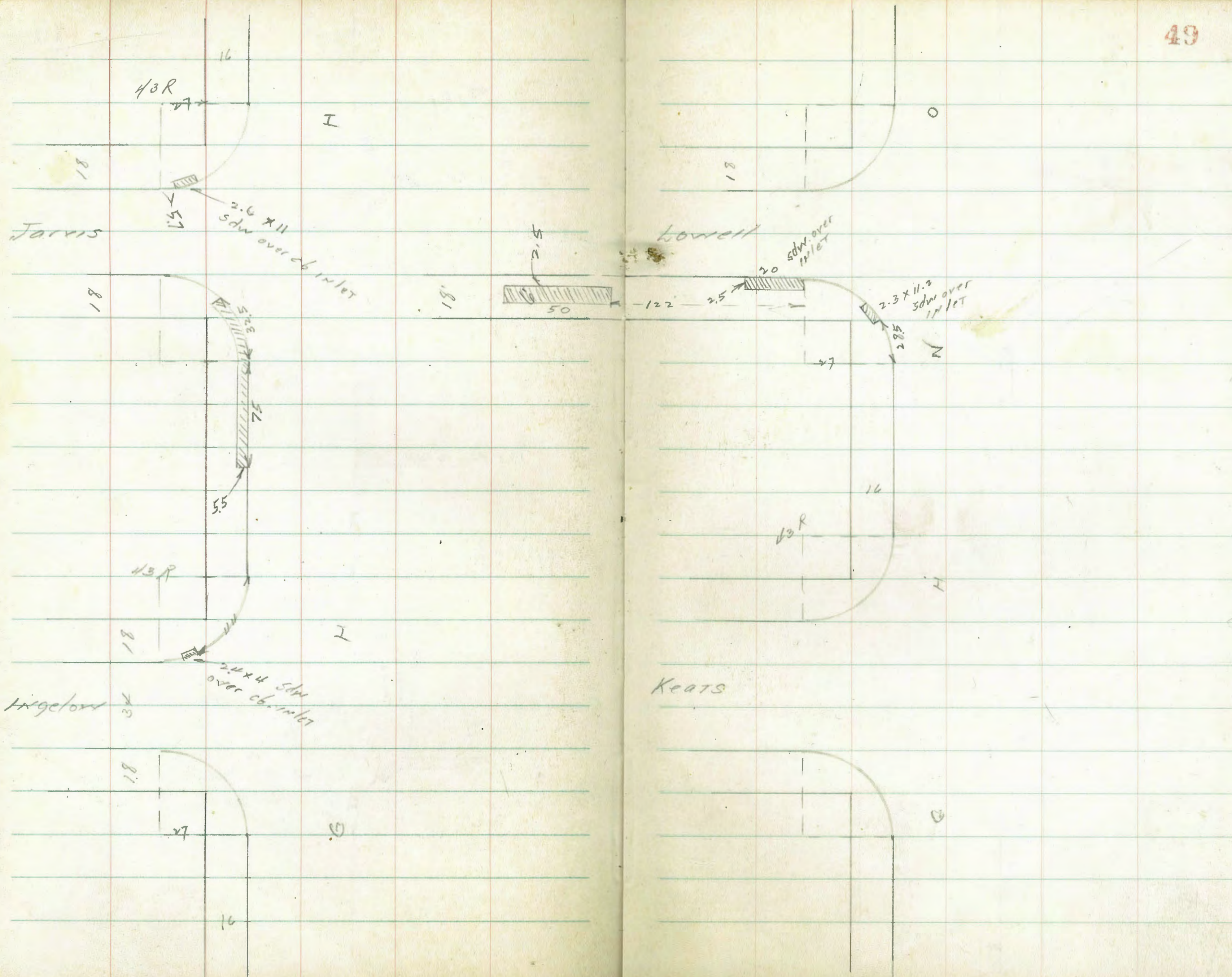


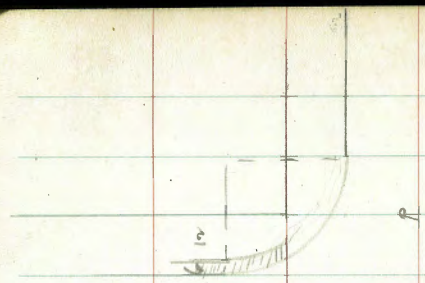
See 15.7
F.B. 15.24

Carleton

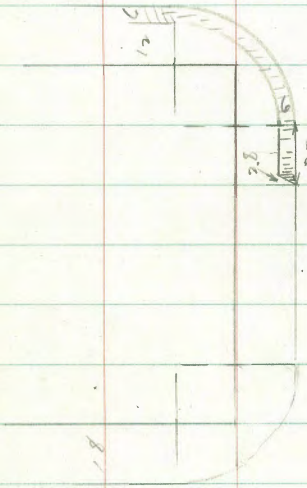

16
18
Fenelon
18
43'R
sdw. over cb inlet
25.1
30.5
Emerson
sdw over cb inlet
33.5


16
43' cb R
39
18
2.4
sdw over cb inlet
11.2
Hugo
18
16
7.6 Com. Drive
76.3
Garrison
11.7 drive
33.7

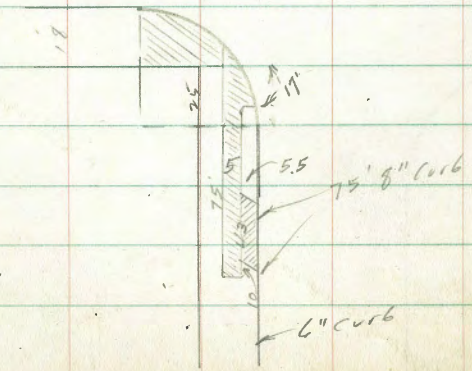

Jarvis
Lowell
Bigelow
Keats
43 R
2.6 x 11 sdw over cb. inlet
2.4 x 4 sdw over cb. inlet
20 sdw over inlet
2.3 x 11.2 sdw over inlet
5.5
50
122
2.5

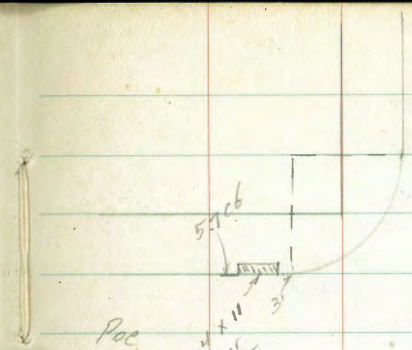


Newell

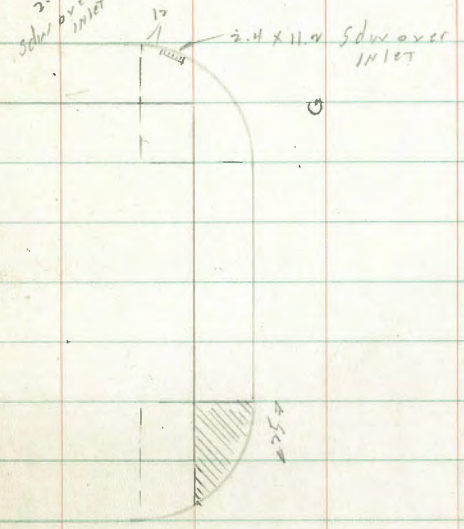


McCauley

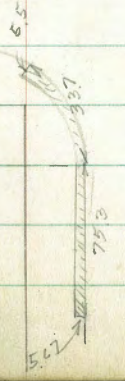


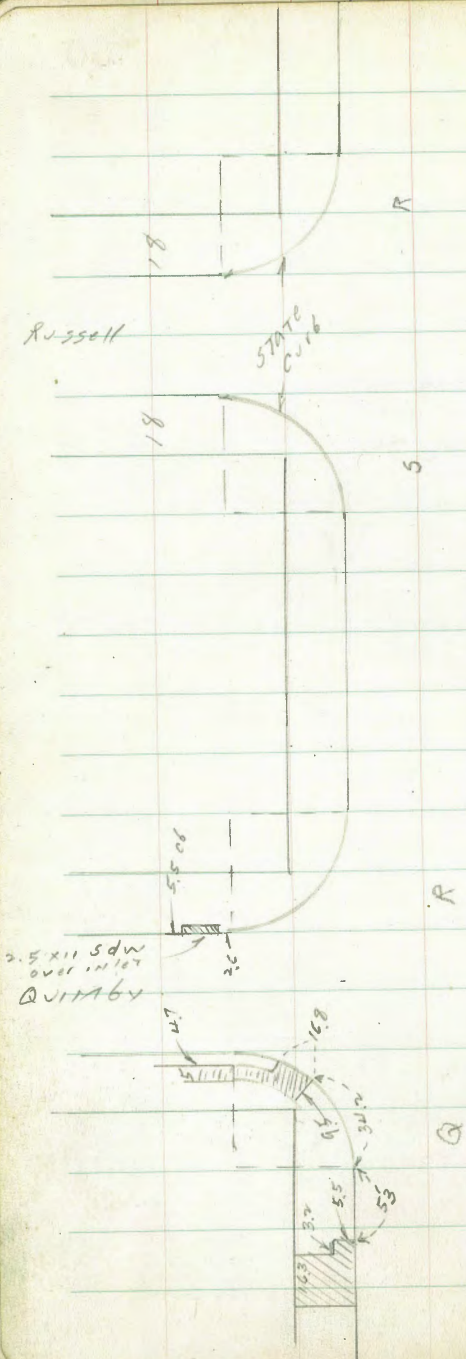


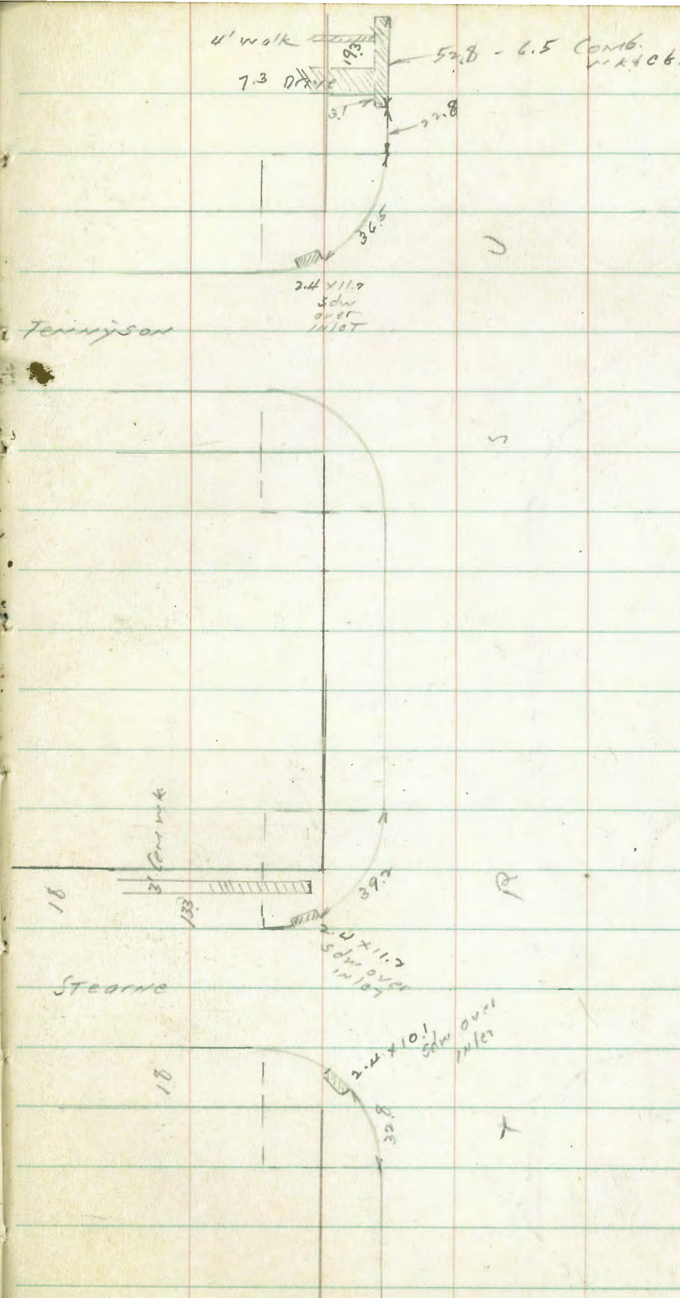
Poe

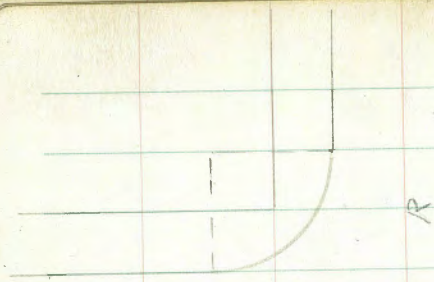


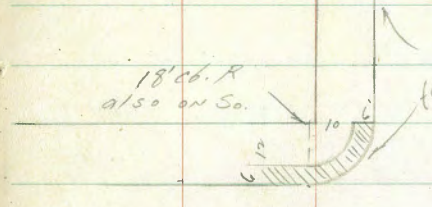
Oliphant




R
18
Russell
STATE Curb
18
S
5.5 cb
R
2.5 x 11 sdw over inlet
Quimby
4.7
16.8
34.2
Q
3.2
5.5
53
13.3

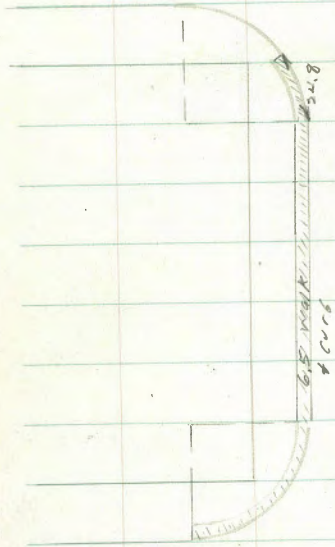

4' walk
19.3
7.3 Drive
52.8 - 6.5 Comb. walk & cb.
3.1
22.8
36.5
U
2.4 x 11.7 sdw over inlet
Tennyson
S
3' Cem walk
13.3
18
39.2
R
2.4 x 11.7 sdw over inlet
Stearns
2.4 x 10.1 sdw over inlet
18
32.8
T

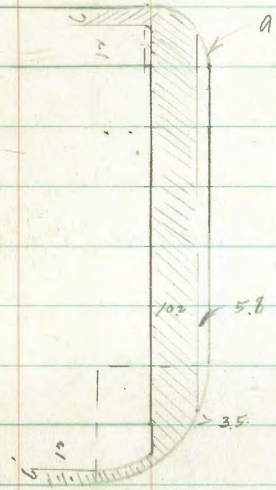




Voltaire

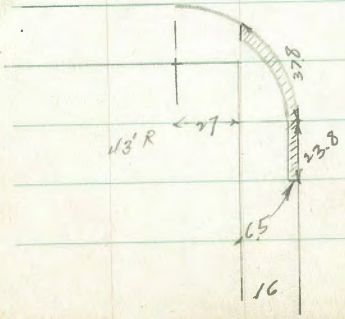
Xenophon

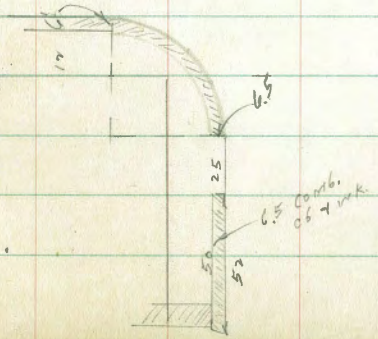


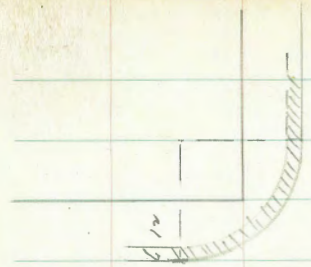


Udal

Whittier

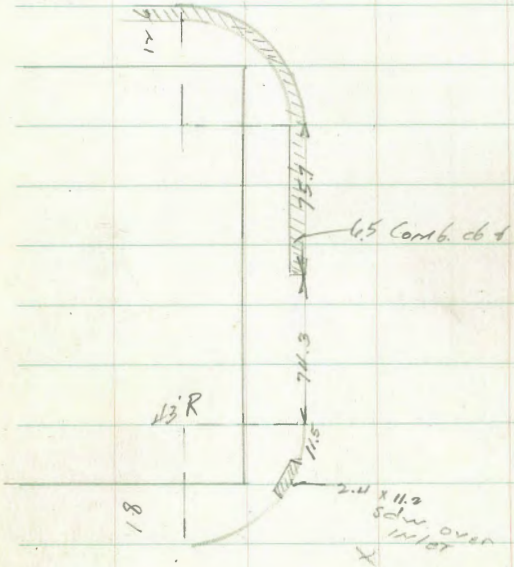




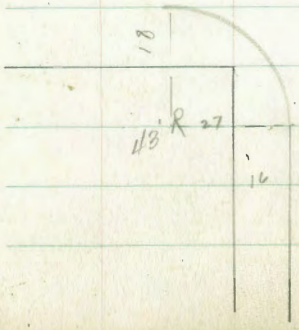


Zota to SW Return of Browning curb & sdwk all in O.K. including ALCOTT St.

Zota

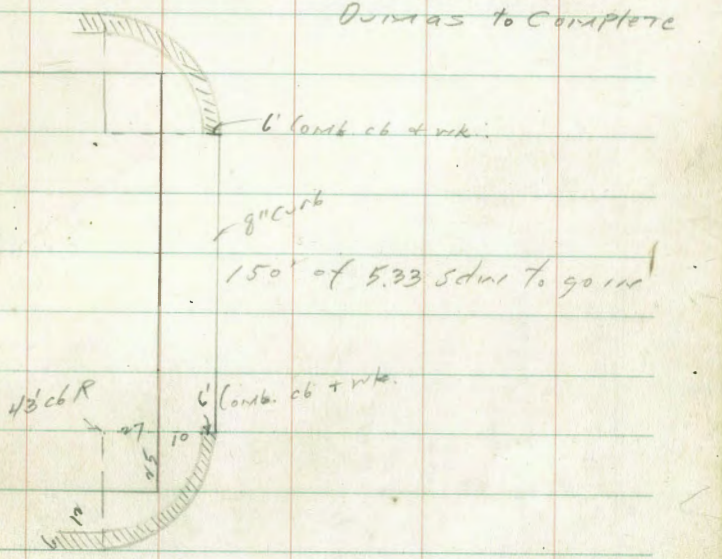


Yonge



Curtis

PUT IN 75' of ~~5.83~~ sdwk to c6 P.C. on SW Cor Dumas to Complete

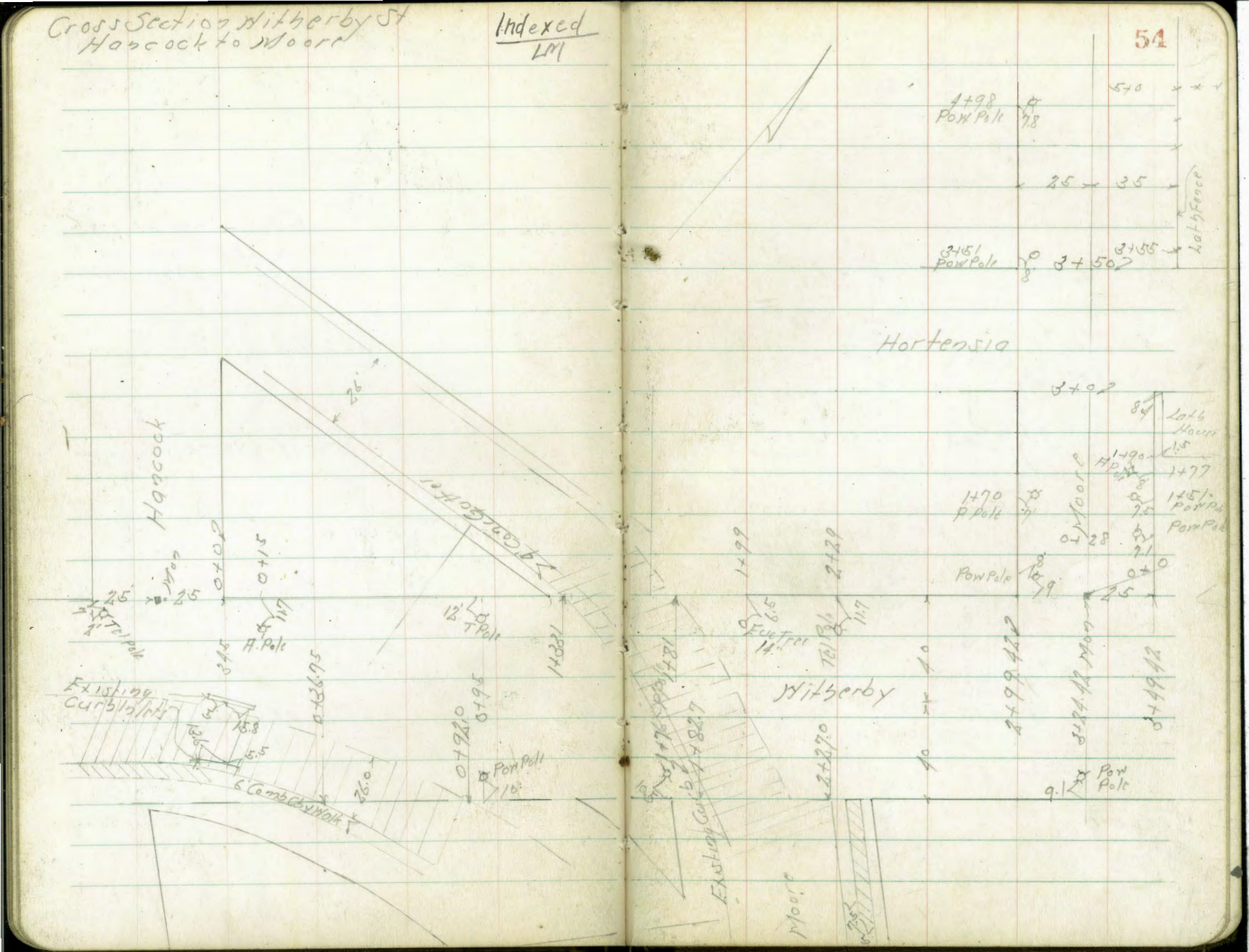


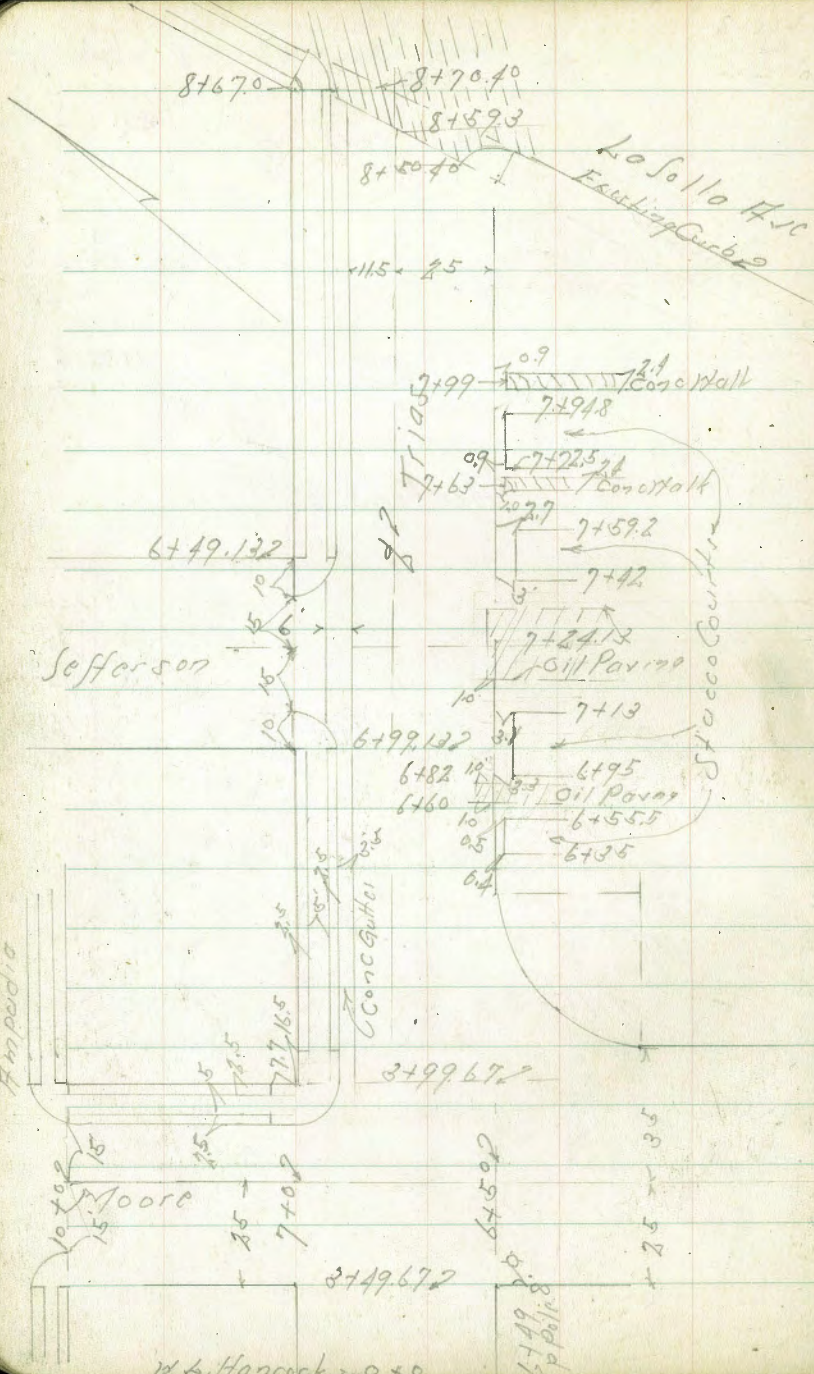
Browning

c6 & sdwk all in O.K. from Dumas N/L to Lytton

Cross Section Withersby St
Hancock to Moore

Indexed
LM




8+67.0
8+70.40
8+59.3
8+50.40
La Salle St
Existing Curb
Trias
Conc Walk
7+94.8
Conc Walk
7+59.2
7+42
7+24.17
Oil Paving
7+13
6+95
Oil Paving
6+55.5
6+35
Stucco Gutter
6+49.132
6+99.132
Jefferson
Conc Gutter
3+99.672
Ampudia
Moore
3+49.672
W. L. Hancock = 0+0

Cross Section Witherby St.
Hancock to Moore

March 28 '41
Sisson
W Moore

TP	10.87	27.13	0.23	16.26
0+60				
0+36.75				
0+0 = E.L. Hancock				
0-25 = ℄ Hancock				
0-50 = W.L. Hancock				
TP	0.23	16.49	12.07	16.26
BM	0.60	28.33		27.73

B.P. S Cb Moore-So Witherby

Reduced & Plotted on Profile #950
4-3-41 C.D.H.

Lt:N ℄ Rt:S

Each reading: elevation / rod / distance (= note)

Station										
0+60	15.3 / 1.2 / 40	15.2 / 1.3 / 20	15.6 / 0.9	16.1 / 0.4 / 10	12.8 / 3.7 / 19	13.23 / 3.26 / 22.7 = Pav	13.97 / 2.52 / 40 on Pav			
0+36.75	14.0 / 2.5 / 40	13.9 / 2.6 / 20	14.7 / 1.8	10.9 / 5.6 / 7	11.09 / 5.40 / 11.5 = Pav Edge	11.27 / 5.22 / 40 = Gut	11.83 / 4.66 / 40 = Cb			
0+0	12.9 / 3.6 / 40	12.7 / 3.8 / 19	8.54 / 7.95 / 5.5 = Cb	7.56 / 8.93 / 5.5 = Gut	8.27 / 8.27	8.64 / 7.85 / 12.5 ℄ Pav	7.72 / 8.77 / 26.6 = Gut	8.58 / 7.91 / 26.6 = Cb	8.9 / 7.6 / 32.1	13.2 / 3.3 / 40
0-25	11.1 / 5.4 / 40	10.7 / 5.8 / 25	6.1 / 10.4 / 12	6.09 / 10.40 / 6.2 = Pav Edge	6.03 / 10.45	5.91 / 10.58 / 20 = Gut	6.36 / 10.13 / 20 = Cb	6.5 / 10.0 / 26	11.5 / 5.0 / 36	12.2 / 4.3 / 40
0-50	10.3 / 6.2 / 40	9.6 / 6.9 / 30	4.9 / 11.6 / 20	4.29 / 12.20 / 10 = Pav Edge	4.16 / 12.33	3.89 / 12.60 / 16 = Gut	4.40 / 12.09 / 16 = Cb Top	4.3 / 12.2 / 22	11.1 / 5.4 / 34	11.6 / 4.9 / 40

16.49

Lt Z Rt

23.5	23.1	22.87	23.04	23.39	23.79
3.6	4.0	4.26	4.09	3.74	3.34
40	20	10: Pav Edge		20	40

21.6	21.68	21.91	22.17	22.50	22.78	23.93
5.5	5.45	5.22	4.96	4.63	4.35	3.20
40	37.8: Pav Edge	20		20	4%: Gut	40: Cb

20.04	19.91	21.30	20.7	20.9	21.6
7.09	7.22	5.83	6.4	6.2	5.5
40 on Pav	19: Gut	19: Cb		20	40

18.91	20.27	19.5	19.8	20.1	20.1
8.22	6.86	7.6	7.3	7.0	7.0
40: Gut	40: Cb	20		20	40

17.7	18.0	18.6	18.6	19.0
9.4	9.1	8.5	8.5	8.1
40	20		20	40

16.9	17.0	17.7	17.7	17.9	15.9	15.96
10.2	10.1	9.4	9.4	9.2	11.2	11.17
40	20		20	30	35	40: Pav Edge

27.13

1+0

1+82.7

1+50

1+33.1

1+10

0+92

27.13

Witherby St

2+99.42 W L Moore from H

2+91

2+75

2+52

2+45

TP	11.41	38.03	0.51	26.62

2+27 = End Cb + Walk on Rt

27.13

	Lt		℄		Rt	
33.8 / 4.2 / 40	34.4 / 3.6 / 20		36.0 / 2.0	36.2 / 1.8 / 20	36.5 / 1.5 / 30	37.3 / 0.7 / 40
28.1 / 9.9 / 50	28.7 / 9.3 / 40	33.1 / 4.9 / 34	33.6 / 4.4 / 20	34.8 / 3.2	35.2 / 2.8 / 20	36.6 / 1.4 / 40
26.8 / 11.2 / 50	27.4 / 10.6 / 40	30.9 / 7.1 / 34	31.7 / 6.3 / 20	32.6 / 5.4	32.6 / 5.4 / 20	34.2 / 3.8 / 40
25.9 / 12.1 / 50	26.7 / 11.3 / 40	28.1 / 9.9 / 20	28.4 / 9.6	29.1 / 8.9 / 20	28.7 / 9.3 / 30	30.7 / 7.3 / 40
25.8 / 12.2 / 50	25.8 / 12.2 / 40	27.1 / 10.9 / 20	27.6 / 10.4	27.8 / 10.2 / 20	26.9 / 11.1 / 40	

38.03

25.1 / 2.0 / 50	25.4 / 1.7 / 40	25.5 / 1.6 / 20	26.5 / 0.6	25.5 / 1.6 / 20	25.09 / 2.04 / 40 Gut.	25.72 / 1.41 / 40 : cb

27.13

					Mon Z Moore NL Witherby
BM		11.05	36.87		
3+49.12 = EL Moore					
3+24.42 = Z Moore From N					
TP	9.85	47.42	0.46	37.57	
		38.03			

Lt	Z	Rt
40.6	41.7	42.9
6.8	5.7	4.5
40	20	
43.8	44.0	
3.6	3.4	
20	40	
36.6	37.5	38.7
10.8	9.9	8.7
40	20	
39.3	40.5	
8.1	6.9	
20	40	

47.42

Cross Section Moore St
Witherby to Ampudia

Indexed
LM

Reduced and Plotted on Profile # 854
4-4-41 C.B.H.

Sta.					
2+50					
TP	4.66	34.07	11.72	29.41	
2+0					
1+50					
1+0					
0+50					
0+0 = N.L. Witherby					
BM	4.76	41.13		36.37	℄ Mor. St / Moore St / N.L. Witherby / Pg. 59

March 29-41
Rt. Sisson
E. W. Moore

Lt. ℄ Rt.

2+50: 23.4 (10.7/35), 24.5 (9.6/25), 27.8 (6.3/10), 28.2 (5.9), 29.2 (4.9/10), 29.8 (4.3/20), 31.8 (2.3/25), 32.7 (1.4/30)

34.07

2+0: 23.8 (17.3/40), 24.0 (17.1/32), 26.7 (14.4/25), 28.7 (12.4/10), 29.7 (11.4), 29.7 (11.4/10), 30.7 (10.4/19), 33.3 (7.8/25)

1+50: 26.4 (14.7/40), 26.1 (15.0/31), 29.4 (11.7/25), 29.9 (11.2/15), 31.4 (9.7), 31.9 (9.2/10), 33.0 (8.1/25), 34.6 (6.5/35)

1+0: 25.4 (15.7/40), 26.1 (15.0/32), 30.9 (10.2/25), 31.4 (9.7/15), 32.9 (8.2), 34.6 (6.5/10), 36.6 (4.5/25), 38.1 (3.0/35)

0+50: 24.9 (15.2/40), 26.7 (14.4/31), 29.9 (11.2/25), 31.4 (9.7/23), 32.4 (8.7/15), 34.4 (6.7), 36.4 (4.7/10), 38.7 (2.4/25), 40.1 (1.0/35)

41.13

4+50

4+25

4+0

3+50 - ½ Hortensia

3+25 = ¼ Hortensia

3+0 = ¼ Hortensia

24.07

Lt Z Rt

23.5	24.8	25.5	25.5	25.9	26.2	27.0	27.4	27.5
10.6	9.2	8.6	8.6	8.2	7.9	7.1	6.7	6.6
35	25	20	13		13	16	25	35

24.6	25.0	25.9	25.5	25.9	26.2	27.0	27.1	28.9
9.6	9.1	8.2	8.6	8.2	7.9	7.1	7.0	5.2
35	25	15	12		15	18	30	35

24.8	25.4	25.7	25.3	25.8	26.3	29.7	29.9	
9.3	8.7	8.4	8.8	8.3	7.8	4.4	4.2	
35	25	16	11		17	28	35	

24.8	25.1	25.1	23.8	25.1	27.2	29.2	29.6	29.8
9.3	9.0	9.0	10.3	8.0	6.9	4.9	4.5	4.3
35	25	19	15		10	14	25	35

23.7	24.5	25.1	27.1	29.1	29.6	29.8	
10.4	9.6	8.0	7.0	5.0	4.5	4.3	
35	25	10		15	25	35	

24.5	25.6	27.6	28.6	29.1	29.1	30.2	32.2	
9.6	8.5	6.5	5.5	5.0	5.0	3.9	1.7	
35	25	10		10	22	25	35	

24.07

Moore St.

6+25				
6+0				
5+50				
5+0				
TP	4.94	30.94	8.07	26.00
4+80				
4+70				
		34.07		

Lt ℄ Rt

6+25

24.0	24.5	26.1	25.9	26.1	26.1	27.9	28.6	29.3
6.9	6.4	4.8	5.0	4.8	4.8	3.0	2.3	1.6
35	25	16	14		15	19	35	50

6+0

23.9	24.6	25.8	25.6	25.8	26.0	27.7	28.3	28.5
7.0	6.3	5.1	5.3	5.1	4.9	3.2	2.6	2.4
35	25	17	15		13	17	25	35

5+50

24.5	25.4	26.1	25.7	25.9	26.4	27.5	27.9	28.1
6.4	5.5	4.8	5.2	5.0	4.5	3.4	3.0	2.8
35	25	18	15		14	17	25	35

5+0

24.1	25.0	26.0	25.6	25.9	26.1	27.2	27.6	27.9
6.8	5.9	4.9	5.3	5.0	4.8	3.7	3.3	3.0
35	25	18	15		13	15	25	35

30.94

4+80

23.6	24.6	26.0	25.7	25.9	26.2	27.4	26.0	25.8	27.5	27.8
10.5	9.5	8.1	8.4	8.2	7.9	6.7	8.1	8.3	6.6	6.3
35	25	16	14		13	15	18	33	28	35

4+70

23.6	24.2	25.8	25.6	25.9	26.1	26.8	25.7	26.1	26.3	26.5
10.5	9.9	8.3	8.5	8.2	8.0	7.3	8.4	8.0	7.8	7.6
35	25	16	14		13	15	19	30	35	45

34.07

	Δ1		Δ2		Rt	
8+00	8' E of WL - Wly Power Pole					
	2.99	29.7	28.8	29.0	29.3	29.4	29.3	30.25
	1.9	2.1	3.0	2.8	2.5	2.1	2.5	1.51
	25	17	15	25		7.5	15	15=CbTop
7+50	28.5	28.5	27.4	27.7	28.0	28.1	28.0	29.03
	3.3	3.3	4.4	4.1	3.8	3.7	3.8	2.73
	25	20	15	7.5		7.5	15	15
TP	1.53	31.76	0.71	30.23	Nail Pole N Cb Trias 50' E Moore			
				31.76				
7+00 = N.L. Trias	26.4	27.1	26.9	26.4	26.9	27.0	27.1	27.89
	4.5	3.8	4.0	4.5	4.0	3.9	3.8	3.05
	35	25	20	15		7.5	15	15=CbTop
6+75 = Δ Trias	25.9	26.1	26.3	26.79		27.3	27.5	
	5.0	4.8	4.6	4.15		3.6	3.4	
	35	25	15	on NH Rim		15	25	
6+62	25.6	25.7	26.2	26.8	26.9	27.2		
	5.3	5.2	4.7	4.1	4.0	3.7		
	35	25	15		20	35		
6+50 = S.L. Trias	24.9	25.1	26.1	26.0	26.6	26.8	28.3	28.6
	6.0	5.8	4.8	4.9	4.3	4.1	2.6	2.3
	35	25	16	14		17	21	35
	30.94				30.94			

Moore St.

Station	Note		Lt		℄			Rt	
10+0	= S.L. Ampudia	28.7 / 3.1 / 25	28.06 / 3.70 / 15=Cb Top	27.8 / 4.0 / 15	28.4 / 3.4 / 7.5	28.8 / 3.0	28.6 / 3.2 / 7.5	28.6 / 3.2 / 15	29.07 / 2.69 / 15=Cb Top
9+50	7.7 E of W.L. = W.L. Power Pole	29.0 / 2.8 / 25	29.4 / 2.4 / 18	28.4 / 3.4 / 15	28.8 / 3.0 / 7.5	29.1 / 2.7	29.1 / 2.7 / 7.5	29.0 / 2.8 / 15	29.78 / 1.98 / 15
9+0		29.8 / 2.0 / 25	28.9 / 2.9 / 15	29.3 / 2.5 / 7.5		29.6 / 2.2	29.8 / 2.0 / 7.5	29.9 / 1.9 / 15	30.51 / 1.25 / 15
8+75		29.8 / 2.0 / 25	29.3 / 2.5 / 15	29.5 / 2.3 / 7.5		29.8 / 2.0	30.0 / 1.8 / 7.5	30.1 / 1.7 / 15	30.81 / 0.95 / 15
8+50		30.3 / 1.5 / 25	29.4 / 2.4 / 15	29.6 / 2.2 / 7.5		30.0 / 1.8	30.0 / 1.8 / 7.5	30.0 / 1.8 / 15	30.92 / 0.84 / 15
8+25		30.3 / 1.5 / 25	29.8 / 2.0 / 18	29.2 / 2.6 / 15	29.5 / 2.3 / 7.5	29.8 / 2.0	29.9 / 1.9 / 7.5	29.8 / 2.0 / 15	30.70 / 1.06 / 15=Cb Top

31.76

31.76

Cross Section Trion St
Hancock to La Jolla Ave.
See Sketch Page 55

1+48 7.6 S of N.L. = Nly Tel Pole

Station	Lt			¢			Rt	
1+0	28.4 5.0 25	28.5 4.9 15	28.5 4.9 7.5	28.4 5.0	28.2 5.2 5	28.9 4.5 7.5	28.8 4.6 15	28.8 4.6 25
0+50 = E.L. Hancock	25.8 7.6 25	26.0 7.4 15	26.4 7.0 7.5	26.3 7.1		26.2 7.2 7.5	25.9 7.5 15	26.2 7.2 25
0+40	25.0 8.4 25	25.2 8.2 15	25.4 8.0 7.5	26.0 7.4	25.8 7.6 7.5	25.7 7.7 15	25.5 7.9 25	
0+25 = ¢ Hancock	23.9 9.5 25	24.1 9.3 15	24.3 9.1 7.5	24.5 8.9 MH	24.6 8.8 7.5	24.8 8.6 15	25.0 8.4 25	
0+10	22.0 11.4 35	22.3 11.1 25	22.7 10.7 15	22.8 10.6 7.5	23.1 10.3	23.2 10.2 7.5	23.2 10.2 15	23.4 10.0 25

0+08 7.7 S of N.L. = Nly Tel. Pole

Station								
0+0 = W.L. Hancock	20.4 13.0 35	20.8 12.6 25	21.2 12.2 15	21.6 11.8 7.5	22.1 11.3	22.3 11.1 7.5	22.0 11.4 15	21.9 11.5 25

TP 3.15 33.38 30.23 Nail Pole NCB T.T. Co. .50' E N ov'l

33.38

Reduced and Plotted on Profile # 854
4-4-41 G.B.H.

3+99.67 = EL Moore

3+49.67 = NL Moore

3+48 7.15 of NL = Hy Tel Pole

3+0

2+50

TP 6.21 36.44 3.15 30.23

2+48 7.15 of NL = Hy Tel Pole

2+0

1+50

33.38

	Lt			℄			Rt	
27.93	27.12	27.34	27.5	27.5	27.1	27.1	28.1	28.3
8.5	9.33	9.10	8.9	8.9	9.3	9.3	8.9	8.1
15	15	11.5	7.5		7.5	15	18	25
=Cb	=Gut	=Edge Concrete						
27.0	26.3	26.2	26.1		26.1	25.7	25.2	
9.4	10.1	10.2	10.3		10.3	10.7	11.2	
25	15	7.5			7.5	15	25	
28.2	28.2	26.9	26.6	26.4	26.4	26.8	25.8	25.3	24.9
8.7	8.8	9.5	9.8	10.0	10.0	9.6	10.6	11.1	11.5
25	15	13	7.5		4	7.5	15	25	35
28.9	28.9	28.3	28.2	28.0	28.0	28.6	27.6	27.4	
7.5	7.5	8.1	8.2	8.4	8.4	7.8	8.8	9.0	
25	18	15	7.5		4	7.5	15	25	
				36.44					
29.2	29.4	28.9	28.9	28.8	28.7	29.2	28.6	28.4	
4.2	4.0	4.5	4.5	4.6	4.7	4.2	4.8	5.0	
25	17	15	7.5		4	7.5	15	25	
29.4	29.8	29.1	29.1	28.9	28.8	29.2	28.9	29.3	
4.0	3.6	4.3	4.3	4.5	4.6	4.2	4.5	4.1	
25	17	15	7.5		4	7.5	15	25	
				33.38					

Trias St

Station					Lt			℄			Rt			
6+50					40.60 6.70 15	39.80 7.50 15	40.02 7.28 11.5	40.1 7.2 7.5	40.2 7.1	40.0 7.3 7.5	39.8 7.5 12	40.8 6.5 15	41.8 5.5 25	
6+0					37.64 9.66 15	36.84 10.46 15	37.02 10.28 11.5	37.0 10.3 7.5	37.0 10.3	36.9 10.4 7.5	36.7 10.6 11	37.9 9.4 15	38.1 9.2 25	
									47.30					
TP	11.32	47.30	0.46	35.98										
5+50					34.64 1.80 15	33.84 2.60 15	34.09 2.35 11.5	34.1 2.3 7.5	34.1 2.3	34.1 2.3 7.5	34.1 2.3 11	35.0 1.4 15	35.0 1.4 25	
5+30					33.62 2.82 15	32.78 3.66 15	33.03 3.41 11.5	33.2 3.2 7.5	33.1 3.3	33.3 3.1 7.5	33.2 3.2 10	33.9 2.5 15	34.1 2.3 25	
5+0					32.17 4.17 15	31.48 4.96 15	31.72 4.72 11.5	31.7 4.7 7.5	31.8 4.6	31.7 4.7 7.5	31.6 4.8 11	32.5 3.9 15	32.5 3.9 25	
4+50					30.05 6.39 15 Cb	29.21 7.23 15 Gut	29.44 7.00 11.5 Edge Conc Gutter	29.3 7.1 7.5	29.2 7.2	29.0 7.4 7.5	28.7 7.7 12	29.7 6.7 15	30.0 6.4 25	30.0 6.4 35
		36.44							36.44					

7+39.13 = EC5

7+24.13 = Z Jefferson

7+09.13 = JWC5

6+99.13 = JWL Jefferson

6+82 = EJy oil Paving

6+60 = WJy oil Paving

47.30

47.30

45.52	44.54	44.35	44.55	44.8	45.1	45.1	45.9	46.4
1.78	2.76	2.95	2.75	2.5	2.2	2.2	2.0	0.9
25 CL	17.3	15	11.5	7.5		7.5	15	25
Ground								

44.0	43.93	43.68	43.90	44.3	44.89	44.4	44.5	45.35
2.3	3.37	3.62	3.40	3.0	2.41	2.9	2.8	1.95
25	17.3	15	11.5	7.5	Rt Rmp	7.5	15	25 oil paving

43.59	43.31	43.11	43.30	43.6	43.9	43.7	43.5	44.6	45.3
3.71	3.99	4.19	4.00	3.7	3.4	3.6	3.8	2.9	2.0
25 CL + G	round	15	11.5	7.5		7.5	15	15	25
	17.3 = Edge Good Gut								

43.51	42.74	42.94	43.0	43.2	43.1	43.1	44.5	44.7
3.79	4.56	4.36	4.3	4.1	4.2	4.2	2.8	2.6
15 CL	15 Gut	11.5 Edge Cont Gut	7.5		7.5	15	15	25

43.51
3.79
24

42.32
4.98
24

Trios St.

Lt ℄ Rt

8+50.40 = Opp Curb End on Rt. ✓

52.60 51.77 52.01 52.8 53.2 53.4 53.81 53.66 54.12 54.6
4.83 5.66 5.42 4.6 4.2 4.0 3.82 3.77 3.81 2.8
15 15 11.5 7.5 7.5 15 = Pav 16 = Gut 16 = Cb 25

8+30

51.80 50.96 51.16 51.2 51.3 51.5 52.1 53.6
5.63 6.47 6.27 6.2 6.1 5.9 5.3 3.8
15 = Brk Cb 15 11.5 7.5 7.5 15 25

8+0

48.63 48.83 48.8 49.0 49.0 49.3 51.3
8.80 8.60 8.6 8.4 8.4 8.1 6.1
15 = Gut in Drive 11.5 7.5 7.5 15 25

7+99 = ℄ 24' Conc Walk ✓

51.34
6.09
23.9

7+63 = ℄ 24' Conc. Walk ✓

48.11
9.32
26

TP 10.71 57.43 0.58 46.72

57.43

7+49.13 = E.L. Jefferson

45.59 44.84 45.10 45.2 45.1 45.7 45.8 47.1 47.3
1.71 2.46 2.20 2.1 1.6 1.6 1.5 0.2 0.0
15 = Cb. 15 = Gut 11.5 = Edge Conc Gut 7.5 7.5 15 20 25

47.30

47.30

BM			8.82	43.75	SE BP Hampden Lafalla 43.75
TP	0.72	52.57	5.58	51.85	

8+70.4 = Wly Cb LaSalle Ave Taken on Diagonal

8+59.3 = Wly Paving Taken on Diagonal

8+59.3 = Edge Paving on ℄

57.43

Lt ℄ Rt 70

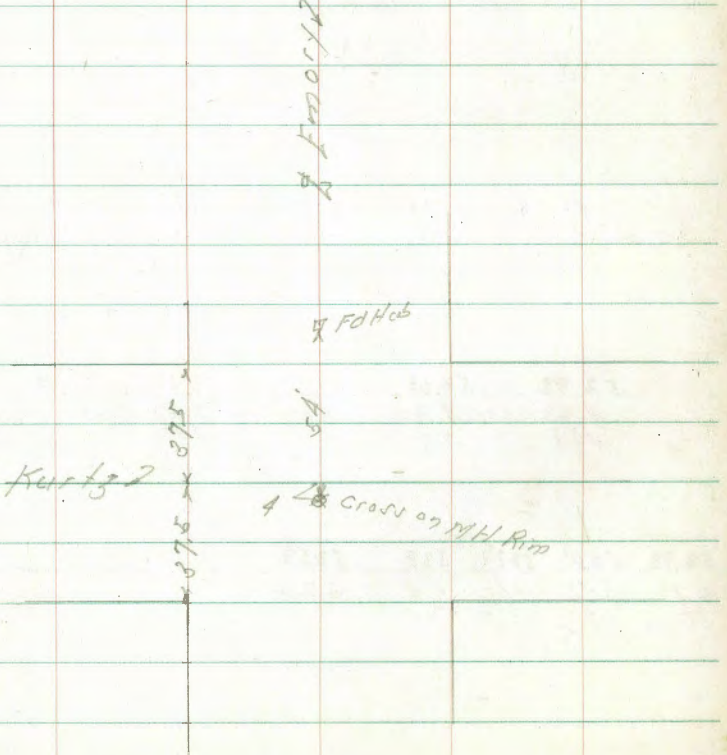
52.88	52.45	53.26	54.15	54.41
4.55	4.98	4.17	3.28	3.07
24-Cb	24-Gut		34-Gut	34-Cb

52.92	52.63	53.66	54.13
4.51	4.80	3.77	3.81
16.8	16.8	18.0	18.0-Cb

52.73	52.01	52.28	53.0	53.53
4.70	5.42	5.15	4.9	3.90
15-Cb	15-Gut	11.5	7.5	

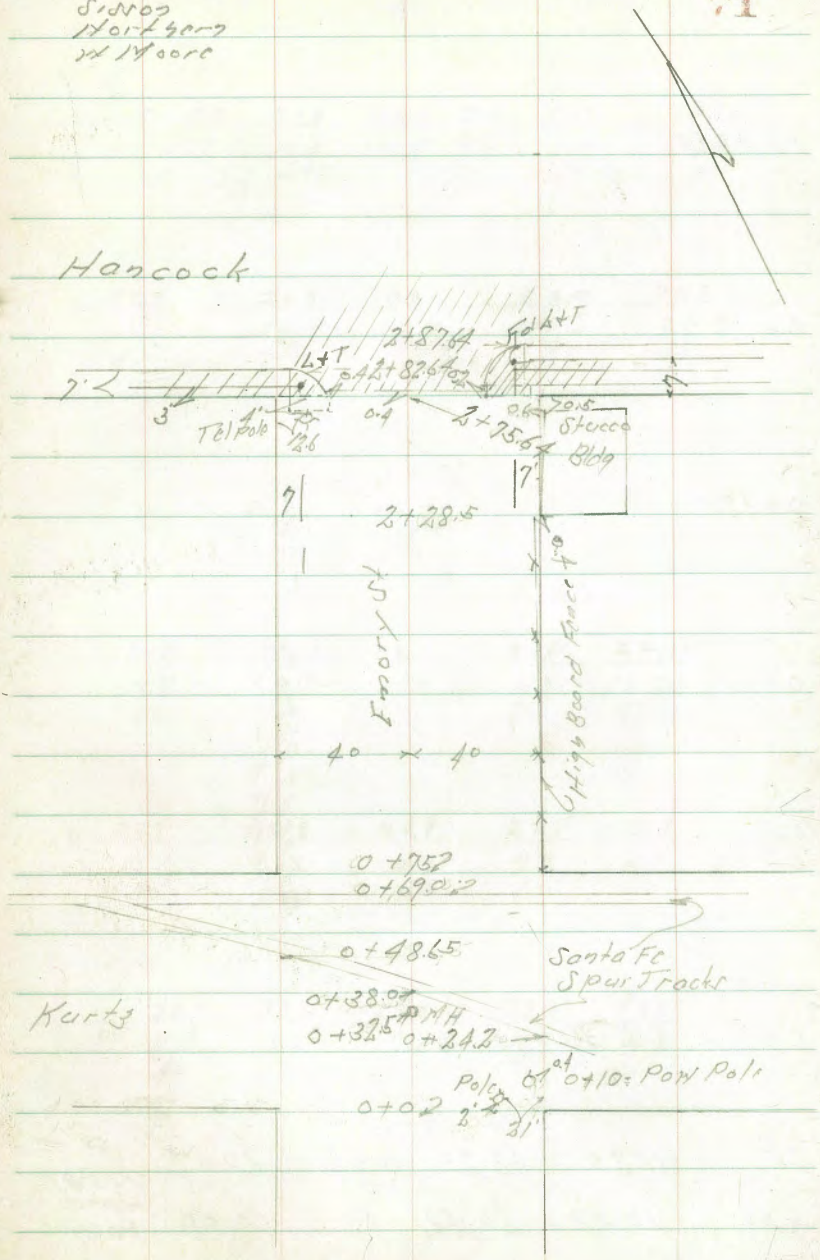
57.43

Cross Section Emory St
Kurtz to Hancock



April 1-41
Sidney
Northern
W Moore

Hancock



Cross Section Emory St.
Kurtz to Hancock

Lt. W | ℄ | Rt. E

0+48.65
21.95 / 10.27 / 40 = Top Rail — 21.9 / 10.3 / 20 — 22.0 / 10.2 — 22.4 / 9.8 / 10 — 24.7 / 7.5 / 20 — 26.2 / 6.0 / 40

0+38
22.2 / 10.0 / 40 — 21.3 / 10.9 / 20 — 22.11 / 10.11 Top Rail — 22.0 / 10.2 / 20 — 22.3 / 9.9 / 40

0+32.5
21.78 / 10.44 = MH Rim

0+24.2
21.5 / 8.7 / 40 — 23.0 / 9.2 / 20 — 22.1 / 10.1 — 21.0 / 11.2 / 20 — 22.14 / 10.08 / 40 = Top Rail

0+10
23.1 / 9.1 / 40 — 22.8 / 9.4 / 20 — 21.9 / 10.3 — 22.5 / 9.7 / 20 — 22.3 / 9.9 / 40

0+0 = S.L. Kurtz
23.7 / 8.5 / 40 — 23.6 / 8.6 / 20 — 23.0 / 9.2 — 23.2 / 9.0 / 20 — 23.0 / 9.2 / 40

32.22

Reduced & Plotted on # 2204
4-5-41- C.B.H.

TP	11.85	32.22	0.06	20.37	
BM	10.43	20.43		10.00	N.E.B.P. Haraszthy & Pacific

Emory St

TP	10.64	42.73	0.13	32.09				
	Lt			℄		Rt		
1+0	29.6 2.6 40	29.4 2.8 20	28.7 3.5	28.6 3.6 20	27.7 4.5 40	27.6 4.6 50		
0+83	29.2 3.0 40	29.0 3.2 20	28.6 3.6 5	27.1 5.1	26.4 5.8 10	27.2 5.0 20	27.1 5.1 40	26.9 5.3 50
0+75 = N L Kurtz	24.5 7.7 40	24.9 7.3 20	25.7 6.5	27.0 5.2 20	26.9 5.3 40			
0+72	23.1 9.1 40	23.8 8.4 20	24.4 7.8	25.9 6.3 20	26.8 5.4 40			
0+69.0 = N Rail	23.53 8.69 40	24.45 7.77 20	25.45 6.77	26.33 5.89 20	27.07 5.15 40 = Top Rail			
0+55	21.8 10.4 40	22.4 9.8 20	25.3 6.9	25.9 6.3 20	26.4 5.8 40			

32.22

32.22

	Lt			Rt	
2+75.64 = S.L. Hancock	41.3	41.22	40.57	41.15	41.37	41.27	40.87	41.58	41.7
	1.4	1.51	2.19	1.58	1.36	1.46	1.86	1.18	1.0
	40	26.5 CL	26.5 CL	13		13	26	26 CL	40
2+65	38.2	38.4	39.6	40.2	40.2	40.4	41.4	41.4	
	4.5	4.3	3.1	2.5	2.5	2.3	1.3	1.3	
	50	40	30	20		20	28	40	
2+45	36.5	37.1	38.7	39.2	39.1	39.4	39.6	38.4	
	6.2	5.6	4.0	3.5	3.6	3.3	3.1	4.3	
	50	40	30	20		20	30	40	WY 8169
2+25		35.6	35.7	38.2	37.9	37.3	36.5	34.9	34.7
		7.1	7.0	4.5	4.8	5.4	6.2	7.8	8.0
		50	40	20		20	30	40	50
1+85		33.7	33.8		34.6	34.7	34.0	33.3	33.0
		9.0	8.9		8.1	8.0	8.7	9.4	9.7
		40	20			20	30	40	50
1+45			32.0	31.8	32.5		32.4	31.5	31.3
			10.7	10.9	10.2		10.3	11.2	11.4
			40	20			20	40	50
	42.73				42.73				

Emory St

BM		1.49	61.24	SFBP Winsor + Keffner 61.28
TP	11.36	62.73	0.24	51.37

2+87.64 = 5 Cb From East

2+82.64 = 5 Cb From West

TP	10.54	51.61	1.66	41.07

42.73

40.82	41.04	41.36	41.49	41.52	41.22	41.13	41.69
10.79	10.57	10.75	10.12	10.09	10.39	10.48	9.93
40	26	13		13	26	40=Gut	40=Cb

41.19	40.49	40.86	41.27	41.43	41.44	41.03	41.10	41.57
10.42	11.02	10.75	10.34	10.18	10.17	10.58	10.6	10.04
40 Cb	40=Gut	26	13		13	26	27.5=Gut	27.5 Cb

51.61

Walker
Hendricks
Hardin
Hunter
3-12-46

RE - CROSS SECTION ALLEY BLK. 60
Ocean Beach

B.M. N.E.B.P. CABLE & NEWPORT Page 28

	4.65	20.66		16.01
T.P.	2.34	16.95	6.05	14.61
T.P.	5.16	15.81	6.30	10.65
chk. N.E.B.P. Bacon & Newport		15.82 π Corrected	4.77	11.04
			N. 05 = BM P. 28	
			0.01	
T.P.	7.04	17.70	5.16	10.66

0-12 = E Gut. Bacon

S	7.76	9.94
℄	7.83	9.87
N	7.85	9.85

0+00 = E.L. Bacon

N Top cb.	6.90	10.80
" Gut. Pave	7.02	10.68
℄ "	7.43	10.27
S " "	7.03	10.67
S Top cb.	6.98	10.80

0+08

S	7.1	10.6
℄	7.4	10.3
+7.3 on Conc. Walk	6.64	11.06
N " " "	6.61	11.09

Between SANTA MONICA And NEWPORT
from BACON ST to CABLE ST. 76
Original sections Page 28

17.70

0+29 = ℄ 3.3 Door (Conc.) on South	6.54	11.16	on line
0+40 = ℄ 3.3' Door on South	6.62	11.08	on line
0+42 = Brk in walk on N			
N. on Conc. Walk	6.60	11.10	
+2.7 S edge "	6.68	11.02	

0+47

N on Walk	6.31	11.39	
+2.7 on edge Walk	6.38	11.32	
℄	6.6	11.1	
S = ℄ 4.5 Conc. walk	6.72	10.98	on Line

Location
Note: for Fences, Poles etc. if No change from original Location will indicate with Red check Mark in Notes P. 28, 33

0+88

N 4.4 = Cor. 4 Car Gar. First	5.6	12.1	
N	5.6	12.1	
℄	5.8	11.9	
+6	5.8	11.9	
S	5.3	12.4	

1+30 = ℄ Gar. on N

1770

1+30			
N+13.8 ℄ Gur on N	5.5	12.2	Dirt Floor
℄	5.5	12.2	
+7	5.4	12.3	
S	4.7	13.0	
+5	5.4	12.3	
1+74			
N+0.7	5.4	12.3	
℄	5.0	12.7	
+7	4.9	12.8	
S	4.5	13.2	
+5	5.6	12.1	
+15	5.9	11.8	
2+23			
-20 on Conc. Door Step.	3.47	14.23	
" " Conc. Slab	3.82	13.88	
-17.2 on N edge "	3.84	13.86	
S	4.2	13.5	
℄	4.4	13.3	
N	4.6	13.1	
+8.5 = S.E. Cor. 2 Car Gar	4.8	12.9	Dirt

1770

2+31 = West Ent.			
S-5.8 = ℄ Gar. Door	3.89	13.81	Conc. Too Apron Main Floor
" "	3.74	1396	
2+50 Cor. Thr. Bldg			
N-20	4.1	13.6	
N	4.1	13.6	
+5	3.8	13.9	
℄	4.0	13.7	
+7	4.0	13.7	
S	3.6	14.1	
2+75 see page 31 for Theatre Entrance El = 15.31			
3+00			
S-1' Cor. Thr. Bldg.	2.2	15.5	
S	2.8	14.9	
℄ on Rim S. MH.	3.07	14.63	
N	3.2	14.5	
+10	3.9	13.8	
3+30 = ℄ 4.3' Conc. Walk to Door on South			
S-20' on Slab at Bldg.	2.9	14.8	
S-16.7 " " N edge.	3.11	14.59	
(3+22) = ℄ Door 20' South. Sl.	2.9	14.8	

1770

3+50

N	2.4	15.3
℄	2.6	15.1
S	2.7	15.0
+10	3.5	14.2

3+58 ℄ Door way to Bld. on South (conc)

S-40' at Bld	2.8	14.9
S-20	3.8	13.9
S-10'	3.3	14.4
S	2.5	15.2
TP 4.74 20.66	1.78	15.92
	5.1	Dirt Floor
3+88.3 ℄ Dble Gar. on N	15.6	6.3 Back

4+04 = 1' Tel Pole on N 0.6' in Alley

4+00

-10'	4.6	16.1
S	4.6	16.1
℄	5.1	15.6
N	4.7	16.0
+10	4.7	16.0

4+13

N	4.4	16.3
+2	4.8	15.9
℄	4.8	15.9

4+13 20.66

℄ +7	4.9	15.8
S	5.2	15.5
+4	5.9	14.8
+15	6.5	14.2
+40	6.4	14.3 slope cont for 50' on South

4+33 ℄ Dirt Drive to Fire Station

-40	4.0	16.7
S	4.4	16.3

4+50 = Tel Pole on S 1' in Alley.

-10	4.1	16.6
S	4.2	16.5
℄	4.4	16.3
N	4.2	16.5
+10	4.0	16.7

4+55

-10	3.9	16.8
N	4.1	16.6
℄	4.4	16.3
S	4.4	16.3
+10	5.7	15.0
+20	5.9	14.8

5+00

-20	5.5	15.2
-10	5.4	15.3
S	4.4	16.3
℄	4.1	16.6
N	3.8	16.9

5+02

S-20	4.4	16.3
S	4.4	16.3

5+39 = ℄ Doorway on South on Line

S Conc. Floor Form	4.02	16.64	Floor under Const.

5+50

S at Bld	4.4	16.3
℄	4.0	16.7
N	3.7	17.0

5+85

N	3.8	16.9
+2	4.2	16.5
℄	4.5	16.2
S	4.3	16.4

5+99.85 = W. L. CABLE at

S on Cb	4.38	16.28

S. Gut. Pav	4.58	16.08
℄ on "	5.00	15.66
N " Gut.	4.62	16.04
N on Cb.	4.43	16.23

W. Gut. CABLE

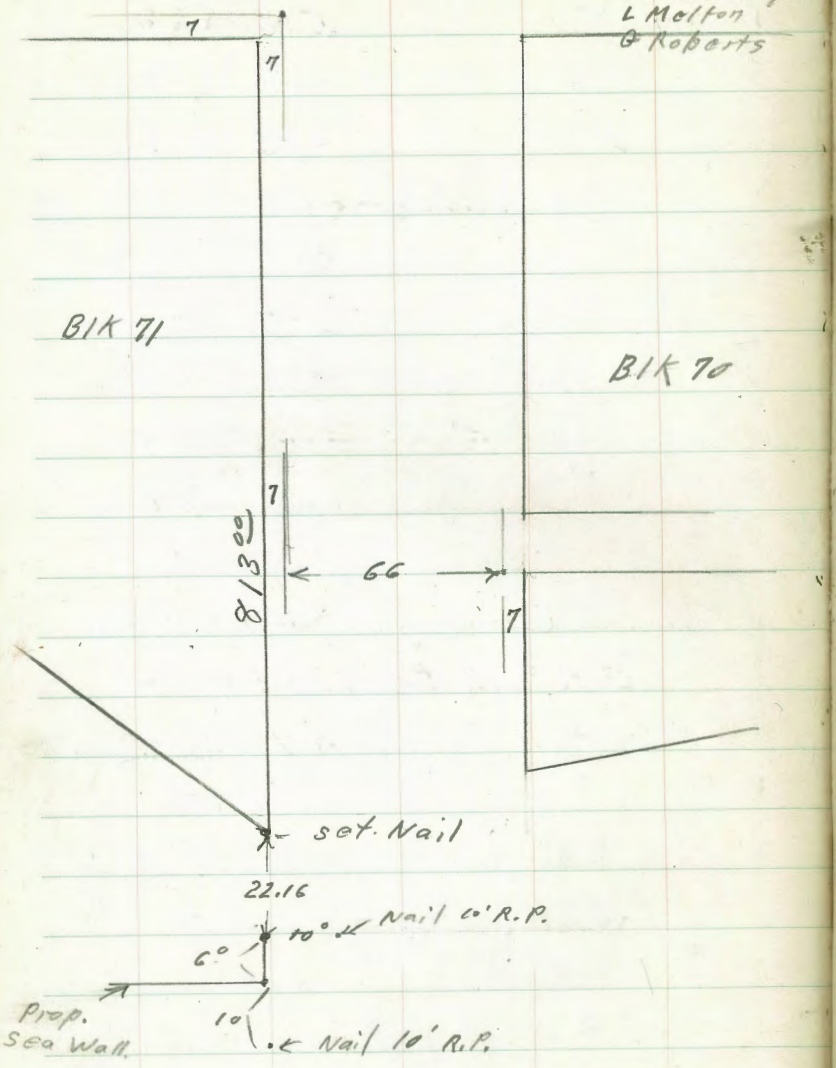
N on Pav.	5.06	15.60
℄ " "	5.15	15.51
S " "	5.12	15.54
Chk. Sterling B.M.	4.64	16.02
		16.01
		0.01

These Cross section notes are O.K. as to grade as of date. 4-9-47 C.H.S

A-10-47

Set. S.W.ly. Cor. BLK 71 O.B.

Sommermeyer
L Melton
& Roberts



DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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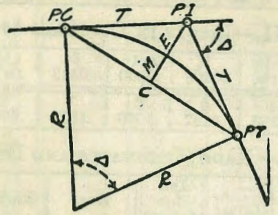

CURVE FORMULAS

Radius=R=$\frac{50}{\text{sin. } D/2}$ (1) Degree of Curve=D and sin. $\frac{D}{2}=\frac{50}{R}$ (2)

Tangent=T=Rtan$\frac{\Delta}{2}$ (3) Length of Curve=L=100$\frac{\Delta}{D}$ (4)

Middle ordinate=M= R(1—cos. $\frac{\Delta}{2}$) (5) =Rvers $\frac{\Delta}{2}$ (6)

External=E=Ttan$\frac{\Delta}{4}$- (7) =R÷cos.$\frac{\Delta}{2}$-R (8)=Rexsec$\frac{\Delta}{2}$ (9)

Long Chord=C=2 R sin.$\frac{\Delta}{2}$ (10) Δ=Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161 +60.35 to find Sta. of P. C. and P. T. Δ=62° 10′ D=8° 20′. From Table IV for 1° curve T=3454.1 and÷8⅓=414.49 ft. From Table V correction=.36 or T=414.85 ft. P. C.=Sta. P.I.—T=157 +45.50. Also from (4) L=746.00 and P. T.=Sta. P. C. +L=164 +91.50.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent-offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset=7.27 (54.50÷100)²=2.16 ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus (54.50)²÷(2 x 688.26)=2.16 ft.

Deflections.—Deflection angle=½ D for 100 ft., ¼ D for 50 ft., etc. For c ft.=(in minutes) .3 x C x D° or=defl. for 1 ft. from Table III x C. For Sta. 158 of above curve=.3 x 54.5 x 8⅓=136.2′ or 2° 16.2′, or=2.50 x 54.5=136.2′ from Table III. For Sta. 159 deflection angle=2° 16.2′ +8° 20′÷2=6° 26.2′, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve E=960.6 for 8° 20′=960.6÷8⅓=91.27 and from Table V correction=.10 or E=91.37 ft. Or suppose Δ=32° and E is measured and found to be 42 ft. What is D? From Table IV E=230.9 and÷42=5.5 or D=5° 30′.

42

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20—16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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