1581

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

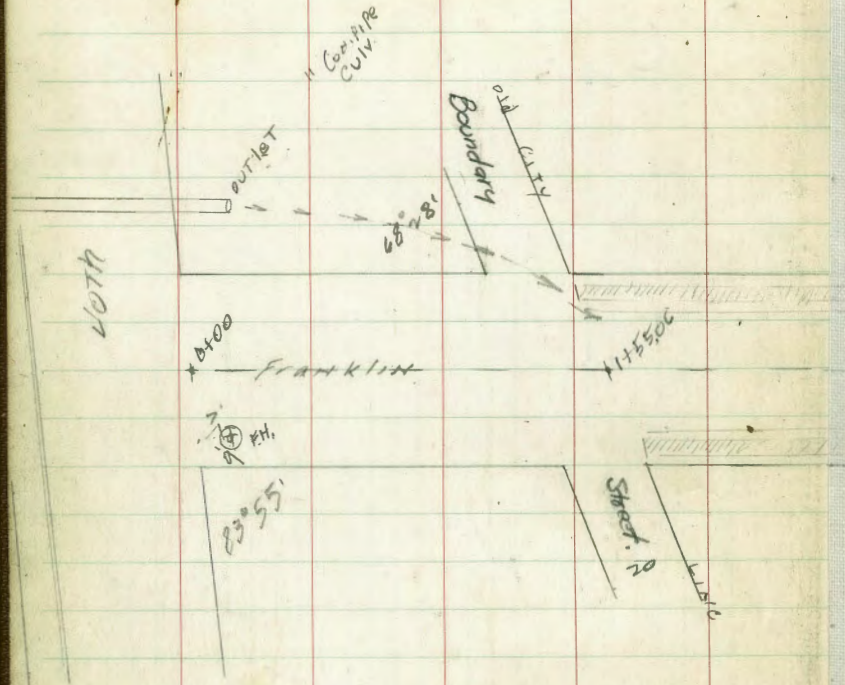
1581

14 courses
7-17-40

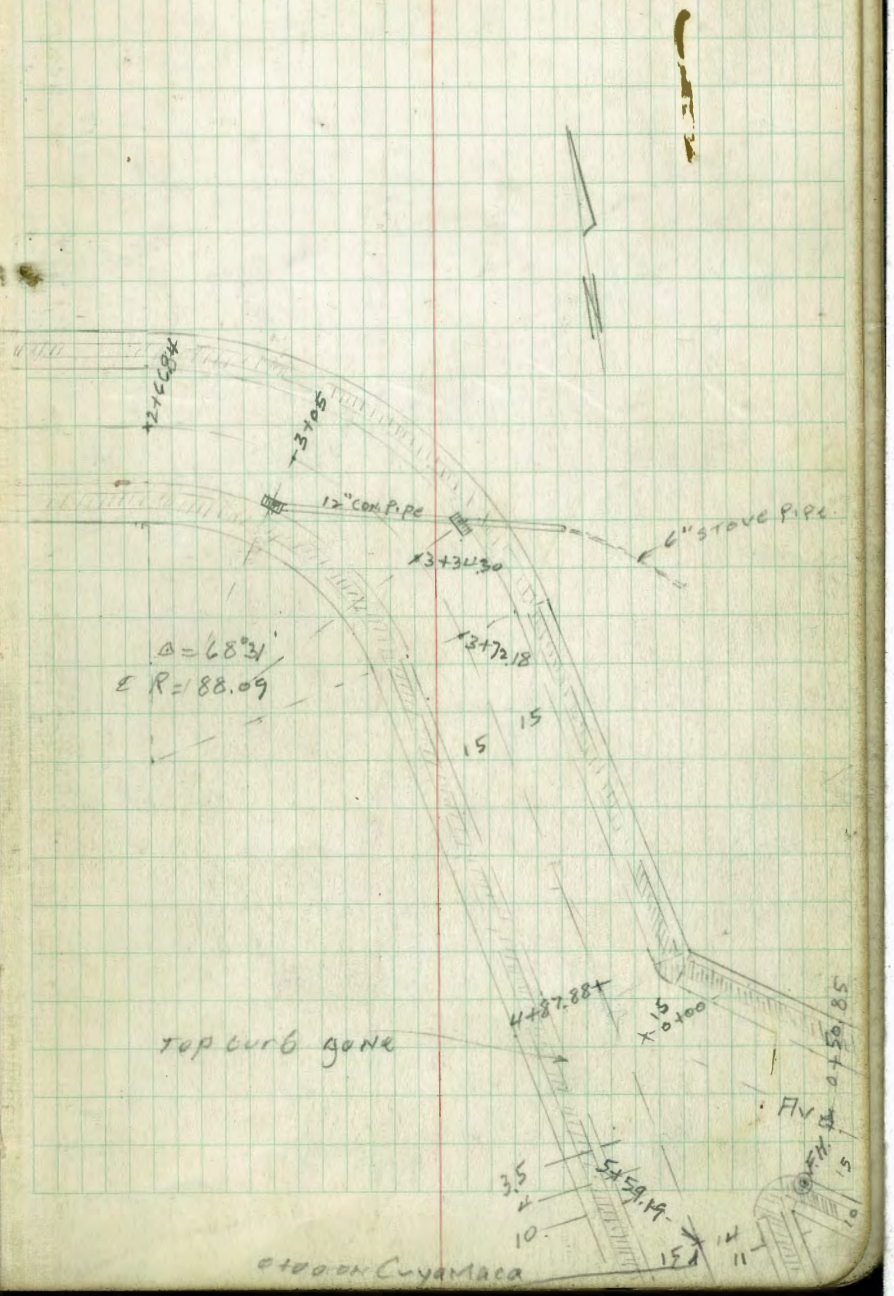
Indexed
C.S.K.

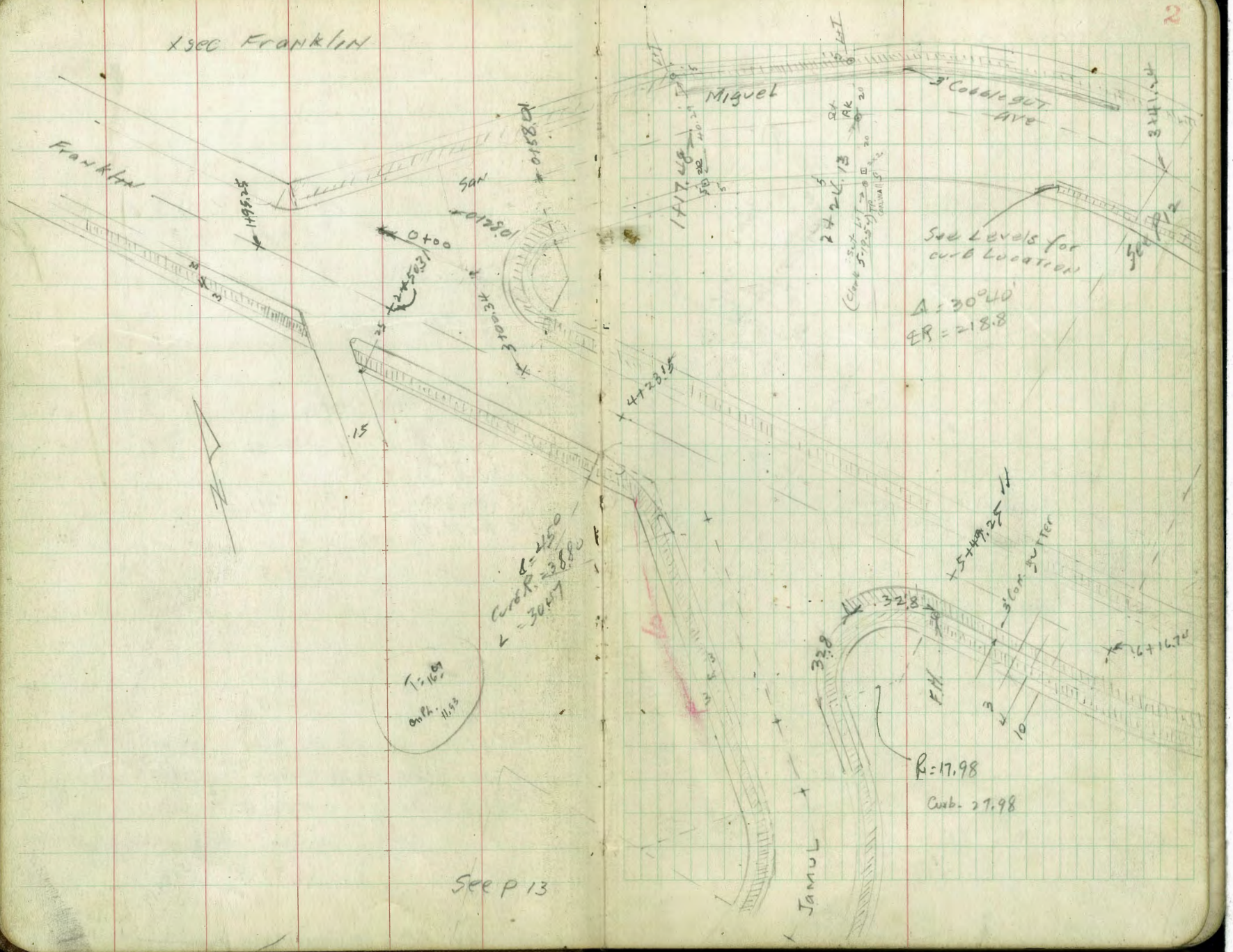
1

X Sec Franklin Ave

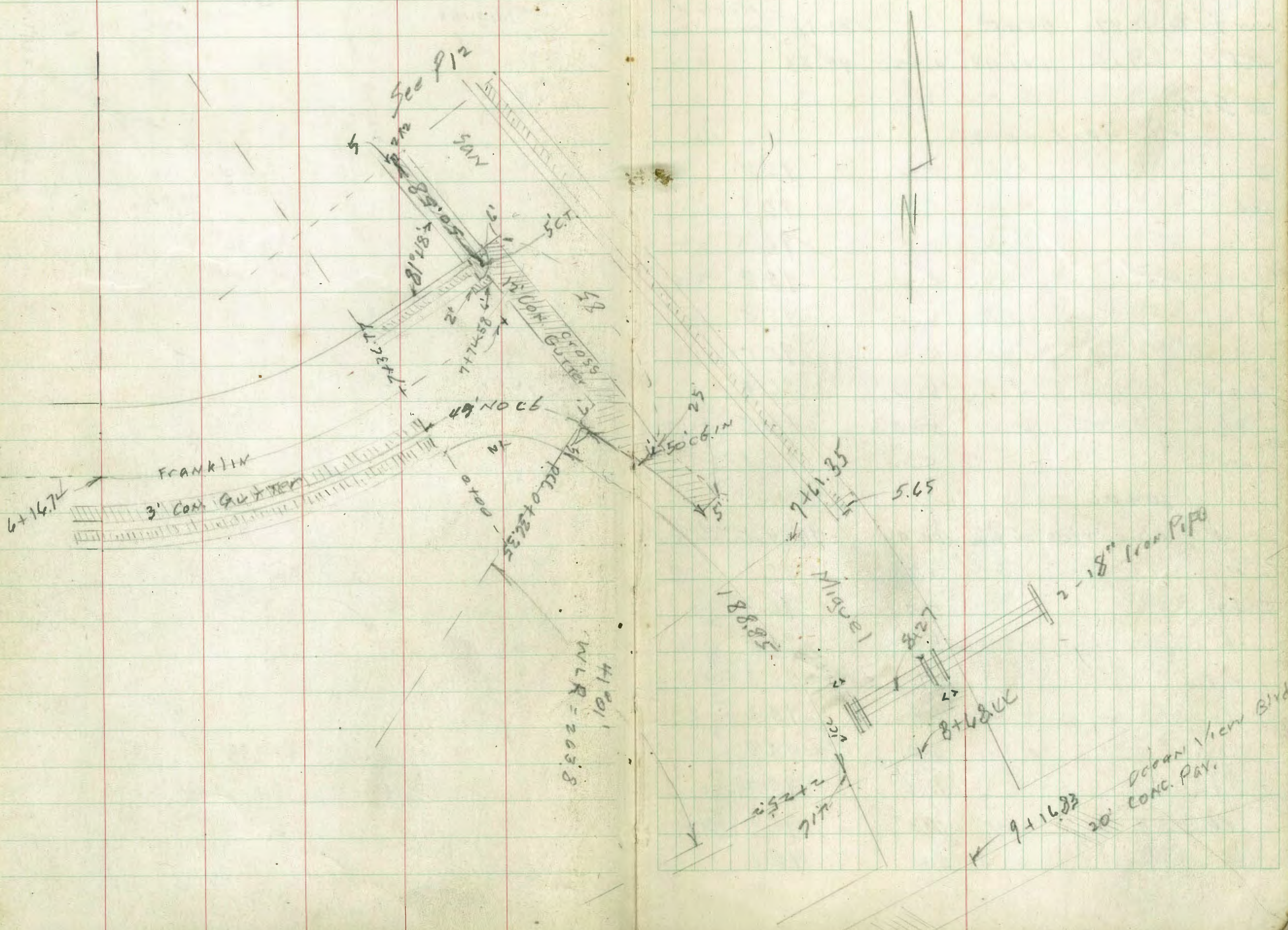


THIS for 2" PAV.
Where curb is in poor condition or has not been put in, it is proposed to put in a wooden header on gutter grade




X sec Franklin
Franklin
San
0+00
Miguel
3' Concrete Gutter
See Levels for curb Location
Δ = 30°40'
ER = 18.8
See P 13
Jamul
R=17.98
Curb 17.98

X sec Franklin



Moore
7-17-40

XSCC Franklin

50' wide
10' curbs

NW 7'CT.	12.87	95.05		82.18	North of Ocean View B.
T.P.	7.15	101.98	8.22	94.83	

℄ STA.
E.L. 40th = 0+00

S		5.2	96.8
c6		5.7	96 3
1/4		5.7	96.3
C		6.2	95 8
1/4		6.5	95 5
+ 2		6.5	95 5
+ 4		5.6	96 4
c6		5.5	96 5
N		5.2	96 8

#M Cole

0+06

— 5	EL. OUTLET 24" CMP. PIPE	10.94	91.04	Under 40th ST.
N		6.7	95.3	
+ 2		5.7	96 3	
c6		5.5	96 5	
+ 5		5.7	96 3	
1/4		6.8	95 2	
C		6.6	95 4	
1/4		6.3	95 7	
c6		6.3	95 7	
S		5.4	96 6	

Plotted by
Reduced

101.98

0+50

S	9.4	92 6
+ 6	9.3	92 7
c 6	10.6	91 4
1/4	10.4	91 6
C	10.5	91 5
1/4	10.4	91 4
+ 5	9.5	92 5
c 6	9.4	92 6
N	9.2	92 8
+ 10	11.1	90 9

T.P.	0 36	89.60	12.74	89 26

1+00

— 10	1.2	88 4
N	1.5	88 1
c6	1.8	87 8
+ 1	3.0	86 6
1/4	2.6	87 0
C	2.5	87 1
1/4	2.6	87 0
9th T	3.0	86 6
c 6	2.0	87 6
S	1.0	88 6

89.60

1+55.0 Sec. on old City Line

S cb	6.30	83.30
1/4	6.7	83.4
C	6.0	836
1/4	6.1	835
N cb	6.31	8329
2+00		
N cb	7.75	8185
gut	8.1	815
1/4	7.6	820
C	7.5	821
1/4	7.7	819
gut	7.8	818
S cb	7.70	8190
2+33.7		
S cb	8.54	8104
1/4	8.6	810
C	8.1	815
1/4	8.1	815
N cb	8.40	8120
2+66.84 B.C.	Curve in 4 equal parts (2.33)	
N cb	8.93	8067
1/4	8.5	811
C	8.6	810
1/4	9.2	804

West Curb poor Cond. on Curve

on W sdw	8.84		8076
Part #1	(2+93.14)		
W cb	887		8073
1/4	9.3		803
C	8.7		809
1/4	8.7		809
E cb	9.05		8055
T.P. - 10.44	91.14	8.90	80.70
3+05 on E			
Top iron grate W. gut	11.25		7989
FL. 12" Pipe	13.67		7747
Part #2	(3+19.51)		
E cb	10.77		8037
1/4	10.5		806
C	10.7		809
1/4	10.9		802
+6	11.2		799
W sdw	10.31		8083
3+34.3 on E			
Top iron grate E. gut	11.33		7981
FL. 12" Conc. Pipe	14.93		7621
Part #3	(3+45.54)		
W sdw	10.00		8114
cb+1	11.0		80.1

1/4		10.4	807
C		10.0	811
1/4		10.3	808
OUT		10.8	803
E CB		10.40	8074
	3+72.18 E.C. ✓		
E CB		9.46	8168 ✓
OUT		10.1	810
1/4		9.5	816
C		9.6	815
1/4		9.9	812
OUT		10.3	808
W CB		9.37	8177
	4+00 ✓		
W CB		8.51	8263
OUT		9.5	816
1/4		9.0	821
C		8.8	823
1/4		8.7	824
OUT		9.7	819
E CB		8.36	8278
	4+50 N		
E CB		6.29	8485
OUT		7.0	841
1/4		6.8	843

C	6.9	842
1/4	6.8	843
OUT	7.2	839
W CB	6.24	8490
4+87.88 opp. NE Cor.		
W CB	5.13	8601
OUT	5.9	852
1/4	5.5	856
C	5.4	857
1/4	5.7	854
OUT	5.7	854
E CB PC RET	4.86	8628
5+23.53		
E CB on ground	5.0	861
1/4	5.0	861
C	5.0	861
1/4	5.1	860
OUT	5.5	856
W CB Poor	4.75	8639
5+59.19 = 0+00 on Cuyamaca		
W CB	4.77	8637
OUT	5.2	859
1/4	4.8	863
C	4.7	864
1/4	5.0	861
OUT	5.4	857
E CB PC RET.	4.71	8643

X Sec Franklin

Cuyamaca Ely to San Miguel

91.14

0+00 See P.C	at 90° with NE Cor	
N L	4.7	864
N C6	4.95	8619
QUT	5.6	855
1/4	5.2	859
C	5.0	861
Sec. on E L Franklin to N.		
N C6	5.07	86.07
QUT	5.4	857
1/4	5.3	858
C	5.3	858
1/4	5.1	860
C6 on ground	5.7	854
+4 QUT	5.6	855
+4 Top C6	4.91	8623
S	4.9	862
0+25.44		
C	5.3	858
N L	5.4	857
QUT	5.6	855
N C6	5.06	8608

91.14

Fd. B.M. BP NE Cor Franklin + Cuyamaca 5.03 86.11

Office Bk. 86.15 0.04 error

8614 Walker Sewer Book

0+50.85		
N C6	5.20	8594
QUT	5.9	852
1/4	5.7	854
C	5.7	854
1/4	5.8	853
QUT	6.0	851
S C6	5.00	8614
1+00		
9 C6	6.49	8465
QUT	7.5	836
1/4	7.1	840
C	6.8	843
1/4	6.9	842
QUT	7.1	840
N C6	6.50	8464
1+50		
N C6	8.14	8300
QUT	8.7	824
1/4	8.6	825
C	8.4	825
1/4	8.7	824
QUT	8.8	
S C6	8.06	823
		8308

91.14

1+95.25 opp Δ Pt on N

S cb		9.42	8172
gut		10.2	809
1/4		10.1	810
c		10.0	811
1/4		10.2	809
gut		10.2	809
N cb	in driveway	10.22	8092
" "	invoid 60	9.80	8134
T.P.	0.58 81.81	9.91	81.23 ✓

2+20.28

S.L. Top encl cb Rct	1.07	80.74
" gut W alley	1.6	80.4
cb	0.75	81.06
gut	1.5	803
1/4	1.5	803
c	1.4	804
1/4	1.3	805
cb	1.4	804
NL	1.7	801

2+42.31

S cb alley Rct	1.45	8036
gut	2.8	79.0

81.81

2+45.31

NL	1.9	799
cb	2.0	798
1/4	2.3	795
c	2.5	793
1/4	2.8	790
gut	2.9	789
S cb	1.69	8012

2+50.31

SL 43 Top alley Rct	1.43	8018
" gut	2.1	797

2+70.34

S cb	3.51	7830
gut	4.5	773
1/4	4.3	775
c	4.0	778
1/4	3.7	781
cb	3.4	784
NL	3.2	786

3+00.34 opp cb BC on N.

N cb	4.93	7688
gut	5.7	761
1/4	5.7	761
c	5.8	760
1/4	6.2	756

81.81

QUT			6.5	753
S C6			5.71	7610
	3+50			
S C6			9.45	7236
QUT			10.1	717
1/4			9.5	723
C			9.2	726
1/4			9.2	726
QUT			9.4	724
N C6			8.60	7321
	4+00			
N C6			12.22	6959
QUT			12.9	689
1/4			12.6	692
C			12.6	692
1/4			12.7	691
QUT			13.6	682
S C6			13.01	6880
T.P.	0.53	49.38	12.96	68.85
	4+23.5 C6 P.C. on Sp.			
S C6			2.05	6733
QUT			2.4	670
1/4			1.5	679

49.38

C		1.4	680
1/4		1.5	679
QUT		1.9	675
N C6		1.30	6808
	4+39.22 C6 P.I.		
N C6		2.1	6707
QUT		3.0	664
1/4		2.5	669
C		2.2	672
1/4		2.2	672
C6		3.1	663
+29	QUT	3.1	663
"	Top C6 CENTER CURVE	2.78	6660
	S end curb curve		
C6		3.35	6603
QUT		3.7	657
	4+60		
S		3.8	656
C6		3.2	662
1/4		3.1	663
C		3.2	662
1/4		3.5	659
QUT		4.0	654
N C6		3.29	6609

	4+90		
N 06		4.55	6483
gvT		5.1	643
1/4		4.8	64.6
C		4.6	648
1/4		4.4	650
c6		4.4	650
S		4.4	650
	5+13		
S		5.8	636
c6		5.6	638
1/4		5.7	637
C		5.8	636
1/4		6.0	634
gvT		6.3	631
N c6		5.47	6391
	5+49.25		
N c6		8.42	6096
gvT		9.0	604
1/4		8.6	608
C		8.3	611
1/4		8.3	611
+4.5 edge Con gvT		8.47	6091
gvT		8.66	6072
S c6		8.06	6132

Cop. Tab. #1	S.W. Cor. JAMU / FRANKLIN	2.69	66.69 BM.
T.P.	0.8N	58.91	11.29 58.09
	5+85		
S c6		0.89	58 02
gvT		1.47	5744
+3	edge GvT.	1.23	5768
1/4		1.1	578
C		1.2	577
1/4		1.4	575
gvT	IN drive	1.65	5726
	6+16.72 B.C. LT	Curve in 6	Equal parts
N c6		3.92	5499
gvT		4.5	544
1/4		4.0	549
C		3.8	551
1/4		3.7	552
+2.5		3.85	5506
gvT		4.16	5475
S c6		3.58	5533
	Part #1 (6+36.7)		
S c6		5.31	5360
gvT		5.91	5300

58.91

+3 edge Con. gut	5.60	5331
1/4	5.4	535
C	5.5	534
1/4	5.8	531
gut	6.3	526
N cb	5.66	5325
#2 (6+56.7)		
N cb	7.24	5167
gut	8.0	509
1/4	7.5	514
C	7.1	518
1/4	7.0	519
+4.5 edge Con. gut	7.2	517
gut	7.37	5154
S cb	6.74	5217
#3 (6+76.7)		
S cb	8.34	5057
gut	8.99	4992
+3 edge Con. gut	8.69	5022
1/4	8.6	503
C	8.6	503
1/4	9.1	498
gut	9.6	493
N cb	8.95	4996

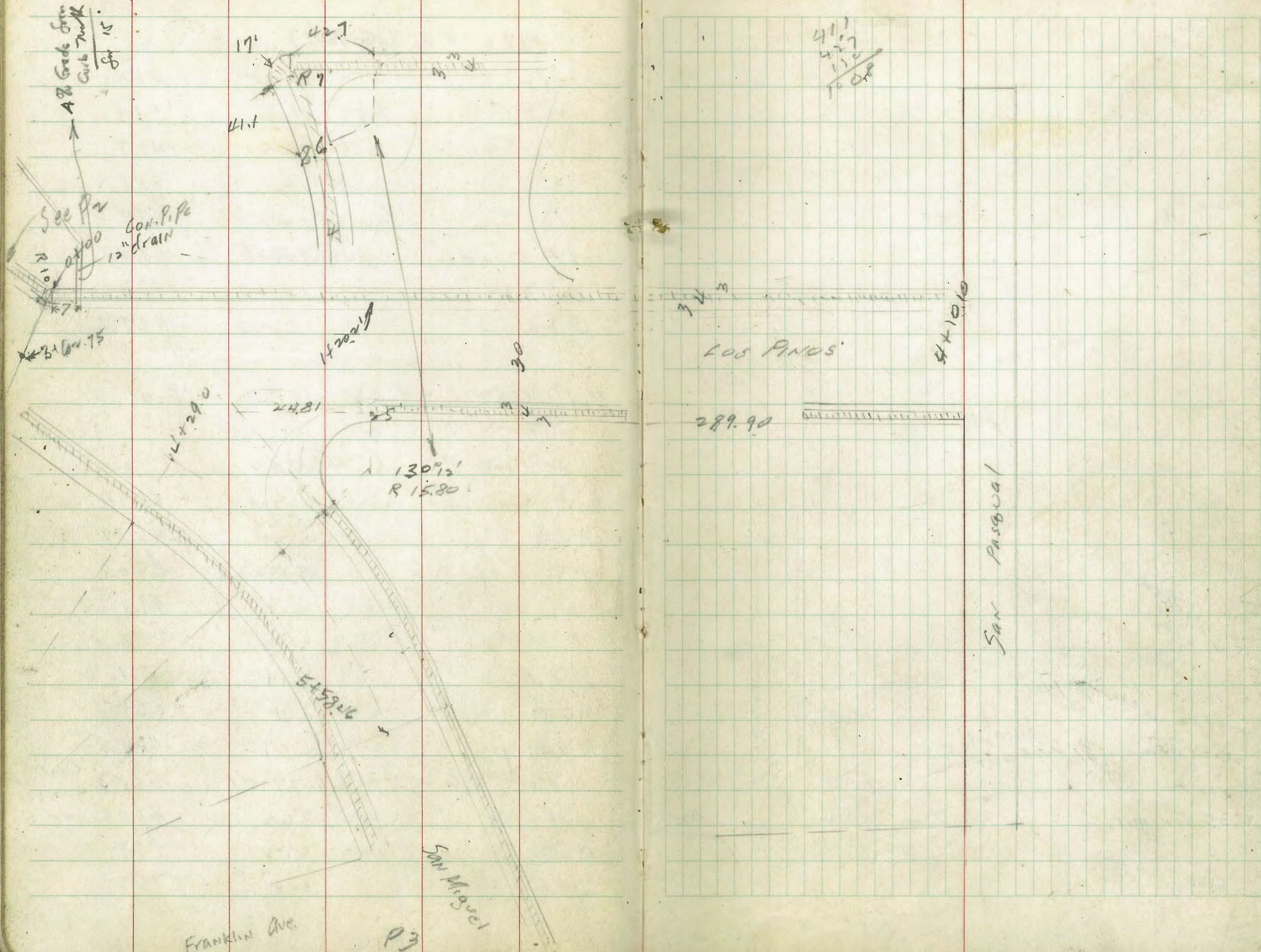
Part #4 (6+96.7)

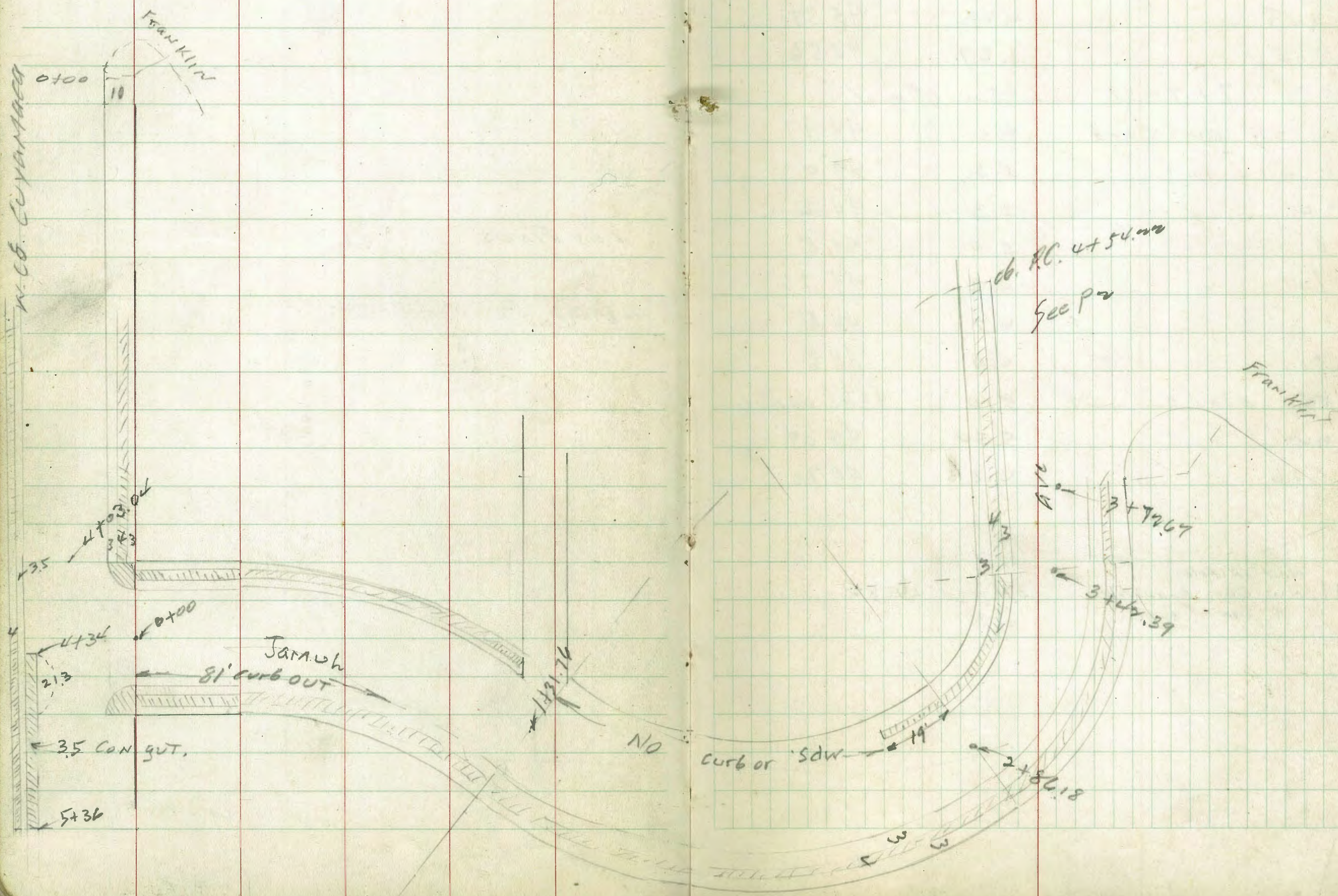
N cb	10.45	4846
gut	11.0	479
1/4	10.3	487
C	10.1	488
1/4	10.1	488
+4.5 edge Con. gut	10.38	4853
gut	10.65	4826
S cb	10.03	4888
T.P. 1.5N 49.53	10.90	48.01

Part #5 (7+16.7)

S cb 1N	2.74	4679
gut	2.74	4679
+3 edge Con gut	2.44	4709
1/4	2.1	474
C	2.0	475
1/4	2.1	474
gut	3.1	464
N cb	2.61	4692
Part #6 7+36.77 E.C. - end of 3' Con. gutter on S.		
N cb	3.65	4588
gut	4.2	453
1/4	3.2	462

Contd. P 12


17'
42.7
R 7
41.1
8.6
See P2
Con. Pipe
12" drain
0+00
3+60.75
1+20.21
3.0
24.81
130°12'
R 15.80
5+58.26
San Miguel
Franklin Ave.
P3
Los Pinos
289.90
4+10.10
San Pascual


Franklin
0+00
10
4+34
0+00
21.3
81' curb out
3.5 con gut.
5+36
No
curb or sdw
19'
2+86.18
3+44.39
3+72.67
See p
Franklin

Franklin from P11		49.53		
c		3.0	46	5
3/4		3.3	46	2
+4.5	end 3' Gutter	3.88	45	65
gut		4.14	45	39
S c6		3.47	45	86
	7+74.58 w/ San Miguel			
SL -11	dirt Curb	4.6	44	9
11 - 10	gut	5.5	44	0
SL		5.3	44	2
c6		5.0	44	5
1/4		4.8	44	7
c		4.7	44	8
1/4		4.9	44	6
+5	edge Conc. gut	5.10	44.43	on North
gut		5.50	44	03
N c6		4.83	44	70
BM	Nail in Pole NW Cor Franklin & San Miguel	3.71	45.82	

Indexed C.S.K.

X Sec Cuyamaca

					Cuyamaca Franklin
NEBP	4.93	91.04		86.11	

P.C for 0+00 = Ł Sta. = -1 (See Sketch Page 1 X Sec. SE 39 T 15 R 6

0+40 beg. fair cb on W

E cb			4.57	8647
qu T			5.0	860
1/4			4.5	865
C			4.3	867
1/4			4.4	866
qu T			4.9	861
W cb			4.55	8649
	1+00			
W cb			4.50	8654
qu T			4.7	863
1/4			4.3	867
C			4.3	867
1/4			4.4	864
qu T			5.0	860
E cb			4.44	8658
	1+50			
E cb			4.37	8667
qu T			4.7	863
1/4			4.4	866

Reduced & Plotted by HMC. 8-7-40.

91.04

C	4.1	869
1/4	4.2	868
qu T	4.4	866
W cb Top off	4.40	8664
2+00		
W cb	4.14	8688
qu T	4.4	864
1/4	4.0	870
C	3.9	871
1/4	4.1	869
qu T	4.3	867
E cb	4.01	8703
2+25		
E cb	3.98	8706
qu T	4.3	867
1/4	4.1	869
C	3.9	871
1/4	4.2	868
qu T	4.8	862
W cb Top gone	4.10	8694
2+50		
W cb Top gone	5.0N	8602
qu T	5.6	854
1/4	5.0	860
C	4.9	861

1/4		5.1	859
QUT		5.3	857
E CB		4.93	8611
	2+75		
E CB		4.04	8500
QUT		6.7	843
1/4		6.6	844
C		6.5	845
1/4		6.6	844
QUT		7.0	840
W CB	TOP gone	6.24	8480
	3+00		
W CB		8.14	8290
QUT		9.2	818
1/4		8.7	823
C		8.6	824
1/4		8.6	824
QUT		8.7	823
E CB		8.5	8289 X
	3+05 To 340 ON E. CB OUT.		
	3+50		
E CB		12.05	78.99
QUT		13.1	779
1/4		12.9	781
C		12.8	782

1/4	12.9	781	
QUT	13.3	777	
W CB	12.3K	7870	
T.P.	0.22	78.24	13.02	78.02	
	4+03.04 N.L JANIW		75.0N Correction
W CB	~~3.80~~	~~7444~~	
QUT	3.8	744	
1/4	3.1	751	
C	2.9	753	
1/4	3.1	751	
QUT	3.7	745	
E CB	3.66	7458	
	4+28.06 @ JANIW		
E	4.1	741	
CB	3.9	743	
1/4	3.8	744	
C	3.7	745	
1/4	3.9	743	
QUT	4.4	738	
W CB	4.08	7416	
	4+34 beg. 3.5 CON. GUTTER ON WEST		
W CB	4.15	7409	
QUT	4.71	7353	3.5
+1	4.85	7339	
+3.5	4.50	7374	

4+53.06 St Jan 1st

W cb		4.25	7399
QUT		4.94	7330
+1		5.26	7298
+3.5	edge QUT	4.94	7330
1/4		5.1	731
C		5.4	728
1/4		5.7	725
QUT		5.9	723
E cb		4.19	7405
E.L.	Cor RCT	3.83	7441

4+53.06 to Ocean View Blvd
No curb or sdw in

5+00

E		9.3	689
cb	dirt	9.7	685
QUT		11.0	672
1/4		10.8	678
C		10.0	682
1/4		9.8	684
+4	edge QUT	9.56	6868
+6.5		9.85	6839
QUT		9.60	6864
W cb		8.90	6934

5+36 end Conc. QUT on West

W cb	12.51	6573
QUT	13.09	6515
+1	13.33	6491
+3.5	13.10	6514
1/4	13.0	652
C	12.8	654
1/4	13.0	652
QUT	13.2	650
cb	12.9	653
E	12.6	656

5+50

E	13.5	647
cb	13.7	645
EL	13.6	646

5+60 N L 20' Par Strip.

EL	14.83	6341
C	14.06	6418
WL	13.32	6492

B.M. N.E. 5' C.T.
Cuyamaca 4 Jan 1st 36.4 74.60

K Sec Jamul

indexed c.s.k.

NE C.T.	1.1 L	75.7 L	74.60	Cuyamaca Jamul

OO = E & Cuyamaca

N cb	1.26	7448	
qvt	1.9	738	
1/4	1.6	741	
c	1.6	741	
1/4	1.9	738	
qvt	2.2	735	
S cb	1.42	7432	

0+37.92 BCRT 4 equal parts

S cb dirt	2.8	729	
qvt	3.5	722	
1/4	3.2	725	
c	3.0	727	
1/4	2.9	728	
qvt	3.0	727	
N cb	2.48	7326	

#1 @ 23.96 = (0+61.38)

N cb	3.06	7268	
qvt	3.7	720	
1/4	3.6	721	
c	3.6	721	
1/4	3.6	721	

Reduced & Plotted by HMC. 8-40

75.7 L

qvt	3.9	718	
L cb	3.2	725	

#2 (0+89.84)

S cb Top cut	3.72	7202	
qvt	4.2	713	
1/4	4.2	715	
c	4.3	714	
1/4	4.3	714	
qvt	4.3	714	
N cb	3.60	7214	

#3 (1+08.3)

N cb	4.16	7158	
qvt	4.8	709	
1/4	4.9	708	
c	4.9	708	
1/4	4.8	709	
qvt	4.9	708	
S cb	4.20	7154	

1+19

N end alley RET	4.26	7148	
N cb	4.40	7134	
qvt	5.7	705	

#4 = 1+31.76 PRC Curve in 6 equal pts

S cb	4.85	7089	
qvt	5.5	702	

75.7K

r/4			5.3	704
C			5.3	704
l/4			5.5	702
QUT			5.6	701
cb			5.2	705
N	QUT		5.1	706
N L	TOP		4.6	711
	#1	(457.5)		
N			5.7	700
cb			6.1	696
QUT			4.7	690
l/4			4.3	694
C			6.1	696
l/4			6.2	695
QUT			4.4	693
S cb			5.06	7008
	#2	(483.23)		
S cb			6.55	6919
QUT			7.2	685
l/4			6.9	688
C			6.9	688
l/4			7.2	685
QUT			7.4	681
cb			6.8	689
N			5.9	700

75.7K

19

#3	(2+08.9C)		
N	7.4	683	
cb	7.7	680	
QUT	8.2	675	
l/4	8.0	677	
C	7.7	680	
l/4	7.7	680	
QUT	7.9	678	
S cb	7.36	6838	
#4	(2+32.7)		
S cb	8.00	6714	
QUT	8.3	674	
l/4	8.3	674	
C	8.4	673	
l/4	8.7	670	
QUT	8.9	668	
cb	8.6	671	
N	8.2	675	
#5	(2+60.23)		
N	8.6	671	
cb	9.2	665	
QUT	9.5	662	
l/4	9.3	664	
C	9.0	667	
l/4	9.0	667	

75.7℄

QUT		9.1	66	6
S		8.66	67	08
	+2.5 beg. CONC curb on N			
N c6		8.96	66	78
#6 = P.C.C. 2+86.18				
S c6		9.27	66	47
QUT		9.5	66	2
1/4		9.6	66	1
C		9.5	66	2
1/4		9.7	66	0
QUT		10.1	65	6
N c6		9.62	66	12
CTR. CURVE (3+19.3)				
N c6		10.30	65	44
QUT		10.7	65	0
1/4		10.1	65	6
C		10.0	65	7
1/4		10.3	65	4
c6		10.6	65	3
S c6		9.96	65	80
T.P.	3.3℄	69.3℄	9.76	65.98
	3+42.39 E.C.			
E c6		4.30	65	04

69.3℄

QUT	4.7	64 6
1/4	4.4	64 9
C	4.0	65 3
1/4	4.1	65 2
QUT	4.5	64 8
W c6	4.11	65 23
3+72.47 PC. RET SE Cor Frankfort Jan 01		
W c6	4.37	64 97
QUT	4.8	64 5.
1/4	4.4	64 7
.	4.6	64 7
1/4	5.0	64 3
QUT	5.3	64 0
E c6	4.72	64 62
Part #1		Ret. in 4 cg. Part
E c6	5.16	64 18
QUT.	5.9	63 4
Part #2		
E c6	6.15	63 19
QUT Con QUT	6.76	62 58
+3 " "	6.58	62 76
Pt #3		
E c6	7.00	62 34
QUT	7.57	61 77
+3	7.32	62 02

Pt #4 P.O.

69.34

4+04

E L	4.1	63 2
cb	5.7	636
1/4	5.4	639
c	5.3	640
1/4	5.0	643
gut	4.9	644
W cb	4.38	6496

4+30

W cb	3.92	6542
gut	4.4	649
1/4	4.4	649
c	4.3	650
1/4	4.1	652
cb	4.2	651
E.L. IN FRANKLIN	4.6	647

4+54.22 W cb P.C.

c = cars in way

W 1/4 See P 9

gut

W cb

ch To B.M.	=49	4645	4649
P 10			0.04
			error

RETURN N± Cor. 21
San Miguel & Franklin

0.86 8=09 $1=23

P.C. 3+00.34 ±E Franklin
5 equal parts

cb	5=10	7689
gut	4.0	761
#1		
cb	4.43	7766
gt	4.9	772
#2		
cb	3.58	7851
gt	4.2	779
#3		
cb	3.09	7900
gt	3.6	785
#4		
cb	3.24	7885
gut.	3.7	784

#5 = E.C. end cb & sdwlk S.

cb	3.69	7840
gt.	4.6	775

Cor
3776.7
=9.33

indexed
C.S.R.

Q 1.7

X sec San Miguel Sec Pr d 3

1+17.48 Δ 12° 47' Rt on SPLIT
Beg. 3' inside stone cut on N.

1+00

0+58.01 end of 4 sdwk on SOUTH
c6. E.C.

0+40

0+28.01

0+00 - N.L Franklin on Diag.
℄ STA.

T.P 98 0.86 82.09 81.23

CTR. of 10' c6	LT		℄	Rt		
73.25 R.	72.7	72.8	72.5	72.0	71.4	72.8	72.9
8.8 c6	9.2 9T	9.8 1/4	9.6	10.1 1/4	10.7 9T	9.2 c6	9.2 S
74.81	74.2	74.2	74.1	73.6	73.0	74.1	74.9
7.8 c6	7.9 9T	7.9 1/4	8.0	8.5 1/4	9.1 9T	8.0 c6	7.2 S
77.95	77.3	77.5	77.6	77.4	77.5	78.40
4.14 c6	4.8 9T	4.6 1/4	4.5	4.7 1/4	4.6 9T	3.69 c.b. 15' end
79.30	78.5	78.6	78.8	78.7	78.6
2.79 c6 15'	3.4 9T	3.5 1/4	3.3	3.4 1/4	3.5 c6 ground
79.56	78.9	79.1	79.4	79.4	79.3	78.7
2.53 c6	3.4 9T	3.0 1/4	2.7	2.7 1/4	2.8 c.b.	3.4 S ground
80.86	80.5	80.1	80.0	79.9	79.6	78.8
1.23 c6	1.6 9T	2.0 1/4	2.1	2.7 1/4	2.5 c6	3.3 S ground

82.09
C

#3 (2+92.39)

T.P 0.43 57.17 13.04 54.74

#2 (2+70.97)

#1 (2+47.55)

+24.13 BC Pt. Curve 5 eq. pts

1+54

T.P. 0.54 69.78 12.85 69.24
87.09

LT | ℄ | RT

LT				℄			RT
54.15	53.4	53.9	53.7	53.3	53.0	53.4	54.0
3.0 2	3.8	3.3	3.5	3.9	4.2	3.8	3.2
CB	QT	1/4		1/4	QT	CB	S

57.17

56.75	56.0	56.3	56.0	55.6	55.3	56.4	56.5
13.03	13.8	13.5	13.8	14.2	14.5	13.4	13.3
CB	QT	1/4		1/4	QT	CB	S

59.26	59.7	59.7	58.6	58.2	57.9	58.8	59.3
10.52	11.1	11.1	11.2	11.6	11.9	11.0	10.5
CB	QT	1/4		1/4	QT	CB	S

61.95	61.5	61.3	61.2	61.1	61.1	61.8	62.2
7.83	8.3	8.5	8.6	8.7	8.7	8.0	7.6
CB	QT	1/4		1/4	QT	CB	S

64.53	64.0	64.0	63.6	63.6	63.6	64.1	64.2
5.25	5.8	5.8	6.2	6.2	6.2	5.7	5.6
CB	QT	1/4		1/4	QT	CB	S

Eaton

69.23	68.8	68.94	68.7	68.3	68.1	69.1	69.3
0.55	1.0	0.84	1.1	1.5	1.7	0.7	0.5
CB	QT	1/4		1/4	QT	CB	S

69.78

T.P.	35 ↓	50.88	9.83	47.34	Rock Inter. San Miguel Los Rios

3 + 47.7

3 + 57

3 + 47

#5 3 + 41.2 ↓ E.C ✓

(3+17.81)

#4 end of 3' cobble stone Cent. out on ↗

(3+03.8)

#3 + 9 beg. cb & walk on So. or Rt

57.17

LT			℄			Rt
48.05 / 9.1 ↗ cb Mid. Ret.	47.5 / 9.7 9T	47.8 / 9.2 1/4	48.0 / 9.2	48.0 / 9.2 1/4	47.5 / 9.7 9T	47.77 / 9.40 12.5 cb
48.54 / 8.63 15 cb	48.1 / 9.1 9LT	48.3 / 8.9 1/4	48.6 / 8.6	48.4 / 8.8 1/4	48.0 / 9.2 9LT	48.00 / 9.17 12.5 cb
			49.2 / 8.0	49.1 / 8.1 1/4	49.0 / 8.2 9T.	49.30 / 7.87 14.7 cb
49.65 / 7.52 cb	49.2 / 8.0 9LT	49.5 / 7.7 1/4	49.6 / 7.6	49.4 / 7.8 1/4	49.3 / 7.9 9LT	49.82 / 7.35 14.7 cb
51.63 / 5.54 cb 15	51.1 / 6.1 9LT	51.5 / 5.7 1/4	51.5 / 5.7	51.3 / 5.9 1/4	51.1 / 6.1 9LT	51.50 / 5.67 14.5 cb
					52.3 / 4.9 9LT	52.78 / 4.39 14.7 cb

57.17

#1 (4+80.8)

#1 (4+58.9)

4+08

4+09 B.C. RT Curve I eg. PTS.

4+00

3+80

F.L. of outlet 12" Con. Pipe 46.16 46.72 on N.

50.88

✓

45.98 / 4.90 / 16.7 c6 | 45.6 / 5.3 / 9T. | 46.3 / 4.6 / 1/4 | 46.2 / 4.7 | 45.7 / 5.2N / 1/4 | 45.4 / 5.5 / 9T | 46.05 / 4.8 / 12.5 c6

✓

46.70 / 4.18 / 18! c6 | 46.3 / 4.6 / 9T | 46.9 / 4.0 / 1/4 | 46.4 / 4.5 | 45.8 / 5.1 / 1/4 | 45.56 / 5.3N / 9T. | 45.56 / 5.3N / 12.1 c6 Inclusive

46.83 / 4.05 / 18 c6 Rec. PC. | 46.5 / 4.4 / 9T

✓

48.0 / 2.9 / N | 47.5 / 3.4 / c6 | 47.1 / 3.8 / 1/4 | 46.6 / 4.3 | 46.2 / 4.7 / 1/4 | 45.9 / 5.0 / 9T | 46.55 / 4.33 / 12.5 c6

47.5 / 3.4 / N | 47.2 / 3.7 / c6 | 46.9 / 4.0 / 1/4 | 46.6 / 4.3 | 46.6 / 4.3 / 1/4 | 46.6 / 4.3 / 9T. | 46.91 / 3.97 / 12.5 c6

45.07 / 2.81 / 18 c6 | 47.3 / 3.6 / +8 | 47.1 / 3.8 / c6 | 47.2 / 3.7 / 1/4 | 47.3 / 3.6 | 47.4 / 3.5 / 1/4 | 47.0 / 3.9 / 9T. | 47.43 / 3.45 / 12.5 c6

50.88

check to B.M. nail Pole P.I.	5.0 ℄	45.8 ℄	45.8 ℄ 0.0 ℄

6 + 05

5 + 85

#5 5 + 58.4 6 E.C. ✓
4 + 29
29.46
25.89

#4 (5+32.6)

#3 (5+06.7)

4 + 86.1 0 where c6. Ret. Should be

50.88

LT	℄	RT
44.68 / 6.20 / 16.6 c6	44.2 / 6.7 / 9T	44.7 / 6.2 / 1/4
44.8 / 6.1	44.5 / 6.4 / 1/4	44.42 / 6.46 / 8.7 Cem 9T.
43.58 / 7.30 / Cem	44.68 / 6.20 / 13.7 c6	PC. Ret.
44.84 / 6.0 ℄ / 16.5 c6	44.4 / 6.5 / 9T	45.0 / 5.9 / 1/4
44.9 / 6.0	44.7 / 6.2 ℄ / 1/4	44.5 / 6.4 ℄ / 9T
44.99 / 5.89 / 12 c6		
45.10 / 5.78 / 16.2 c6	44.6 / 6.3 / 9T.	45.5 / 5.4 ℄ / 1/4
45.3 / 5.6	45.0 / 5.9 / 1/4	44.5 / 6.4 ℄ / 9T
45.34 / 5.5 ℄ / 12.5 c6		
45.25 / 5.63 / 16.3 c6	44.9 / 6.0 / 9T	45.8 / 5.1 / 1/4
45.9 / 5.0	45.3 / 5.6 / 1/4	44.8 / 6.1 / 9T
45.56 / 5.3 2 ℄ / 13.7 c6		
✓ 45.53 / 5.35 / 15.8 c6	45.2 / 5.7 / 9T	46.0 / 4.9 / 1/4
45.9 / 5.0	45.6 / 5.3 / 1/4	45.0 / 5.9 / 9T
45.71 / 5.17 / 13.0 c6		
45.91 / 4.97 / 16.5 c6	45.5 / 5.4 ℄ / 9T.	

50.88

7+61.35	BC Rt.	Curve 4 eq. pts.		
T.P.	3.89	48.17	6.60	44.28
7+40				
7+15				
6+75				
6+50				
6+30				
		50.88		

Lt | ℄ | Rt

42.33 / 5.84 / 14.0 c6 in drive — 42.9 / 5.3 / 1/4 — 43.1 / 5.1 — 43.0 / 5.2 / 1/4 — 42.8 / 5.4 / 9T — 44.1 / 4.1 / c6 — 44.6 / 3.6 / W 25

48.17

43.34 / 7.54 / 15.5 c6 — 42.9 / 8.0 / 9T — 43.2 / 7.7 / 1/4 — 43.3 / 7.6 — 43.3 / 7.6 / 1/4 — 43.0 / 7.9 / 9T — 44.0 / 6.9 / c6 — 44.9 / 6.0 / W

43.72 / 7.16 / 17 c6 — 43.2 / 7.7 / 9T — 43.6 / 7.3 / 1/4 — 43.7 / 7.2 — 43.6 / 7.3 / 1/4 — 42.96 / 7.94 / 9T / 12.4 — 42.41 / 8.47 / 9T / 17 — 43.74 / 7.14 / 17.1 c6

43.87 / 7.01 / 17.1 c6 — 43.5 / 7.4 / 9T — 44.1 / 6.8 / 1/4 — 44.3 / 6.6 — 44.4 / 6.5 / 1/4 — 43.88 / 7.00 / 14.5 9T. — 42.98 / 7.90 / 20.5 9T. — 43.33 / 7.55 / 27.4 9T. — 44.66 / 6.22 / 27.4 c6

44.13 / 6.75 / 16.9 c6 — 43.8 / 7.1 / 9T — 44.3 / 6.6 / 1/4 — 44.5 / 6.4 — 44.4 / 6.5 / 1/4 — 44.11 / 6.77 / 12.3 9T — 43.19 / 7.69 / 18.3 9T. — 44.08 / 6.80 / 24.3 9T.

44.40 / 6.48 / 16.9 c6 — 44.0 / 6.9 / 9T — 44.6 / 6.3 / 1/4 — 44.7 / 6.2 — 44.6 / 6.3 / 1/4 — 44.38 / 6.50 / 10.7 — 43.34 / 7.54 / 16.7 — 44.28 / 6.60 / 22.7 c6M Cross 9T.

50.88

Cross cut very low! In fact too low! Built 6x super good (o.

#4 8+68.44 E.C.

40.8
7.4
30

#3 (8+41.66)

41.53
6.4C
Hd. wl

#2 + 11 - 8+27 do. 18" I.P. Culv.
Should build curb inlets
1.7 bet Hd walls

#2 (8+14.89)

#1 (7+88.12)

7+47 end cb on E

48.17

LT & RT.

42.2 / 6.0 / 25 | 42.2 / 6.0 / CB | 42.5 / 5.7 / 1/4 | 42.7 / 5.5 | 42.6 / 5.4 / 1/4 | 43.2 / 5.0 / CB | 43.2 / 5.0 / 25

41.2 / 7.0 / 25 | 42.4 / 5.8 / CB | 42.4 / 5.8 / 1/4 | 42.5 / 5.7 | 42.5 / 5.7 / 1/4 | 42.5 / 5.7 / 9T | 42.8 / 5.4 / CB | 44.1 / 4.8 / 25

38.60 / 5.57 / 28 FL OUTLET | 39.05 / 9.14 / FL. 11.7 - 11 | 41.70 / 6.47 do. / FLWL.

39.89 / 8.28 / 12.5 FL. INLET | 42.89 / 5.28 do. / 12.9 HWL

42.2 / 6.0 / E / 25 | 42.2 / 6.0 / CB | 42.0 / 6.2 / 9T | 42.5 / 5.7 / 1/4 | 42.6 / 5.6 | 42.6 / 5.6 / 1/4 | 42.3 / 5.9 / 9T | 42.9 / 5.3 / CB | 43.6 / 4.4 / 25

43.1 / 5.1 / E / 25 | 43.1 / 5.1 / CB | 42.6 / 5.6 / 9T | 42.6 / 5.6 / 1/4 | 42.7 / 5.5 | 42.8 / 5.4 / 2/4 | 42.6 / 5.6 / 9T | 44.0 / 4.2 / CB | 44.0 / 4.2 / W / 25

42.84 / 5.33 / 14 CB | 42.7 / 5.5 / 9T

48.17

BP. N E Cor Bridge on
B.M. Ocean View 100' E 5.73 4~.44 42.43
of San Miguel

9+16.83 N edge Pav Str. P

8+99.73 NL Ocean View

48.17

42.11
6.06
~5 P

42.80
5.37
Pav.

43.89
4.78
~5 Pav

42.6 42.6 42.6 42.8 43.0 43.1 43.7 44.2
5.4 5.6 5.6 5.4 5.2 5.1 4.5 4.0
~5 ~6 1/4 1/4 gr. 1.5 ~5

48.17

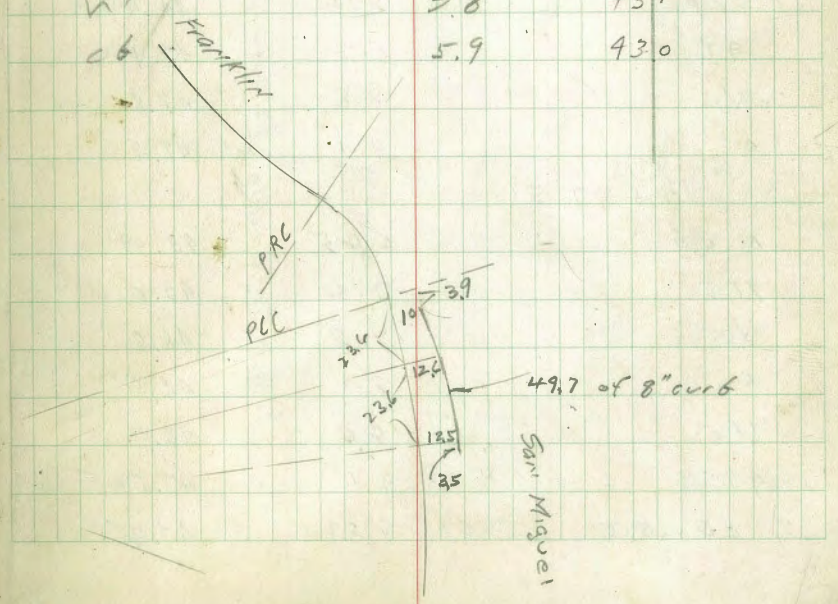
Xsec W c6 San Miguel
bet. Franklin & Ocean View Blvd.

Nail in Pole	3.05	48.87	45.82 P.I.
	0+00 PRC		
W		2.7	46.7
c6 end curb		3.02	45.85
	1/2 Curve		
W		3.4	45.5
c6		3.6	45.3
gT		4.3	44.6
	0+36.35 PCC. Curve in 8 pts		L=188.85
W		3.6	45.3
c6		4.0	44.9 (23.6)
gT		4.8	44.1
	#1		
W		3.4	45.5
c6		4.4	44.5
+24 Cem. c6		4.47	44.40
	#2		
W		3.9	45.0
c6		5.0	43.9
+24 Cem c6		5.08	43.79
	#3		
W		3.9	45.0
c6		4.9	44.0

48.87

End Tocklin. "2

#4		
W	4.3	44.6
c6	4.8	44.1
#5		
W	5.0	43.9
c6	5.2	43.7
#6		
W	5.1	43.8
c6	5.7	43.2
#7		
W	5.3	43.6
c6	5.9	43.0
#8 = E.C.		
W	5.8	43.1
c6	5.9	43.0



Indexed C.S.M.

Subgrade - X Sec Los Pinos Ave

T.P rock	9.30	56.64	47.34	P.K

Section on diag. N.L San Miguel
0+00 = Intersection " " Los Pinos

N c6		8.56	48.08
gT		9.4	47.2
1/4		9.1	47.5
c		8.8	47.8
1/4		8.5	48.1
c6	ground	9.1	47.5
+ gT		9.8	46.8
c6	Mid. Ret	9.38	47.26 ✓
	0+40		
N c6		8.15	48.49
gT.		8.7	47.9
1/4		8.8	47.8
c		9.1	47.5
	0+77.51		
N c6		6.45	49.99
gT		7.6	49.0
1/4		7.8	48.8
c		8.1	48.5
1/4		8.4	48.0
gT		9.1	47.5
S c6	E.C.	8.09	47.95

Redr Profile made 5-12/40 C.B.H.

56.64

	1+20 N 1		
S c6		6.17	50.47 Property Should be P.C.
gT		6.6	50.0
1/4		5.9	50.7
c		5.5	51.1
1/4		5.4	51.2
gT		5.4	51.2
N c6		4.63	52.01
	1+50		
N c6		3.20	53.44
gT		3.9	52.7
1/4		3.9	52.7
c		4.0	52.6
1/4		4.4	52.2
gT		5.1	51.5
S c6		4.6 N	52.02
	1+96		
S c6	end curb on S.	2.5 2.44	54.1 54.00
gT		2.9	53.7
1/4		2.4	54.2
c		2.1	54.5
1/4		1.9	54.7
gT		1.8	54.8
N c6		1.14	55.50
T.P.	1.17	47.17	0.64 56.00

2+30

N cb	10.44	56.73
qT	11.2	56.0
1/4	11.0	56.2
c	11.0	56.2
1/4	11.4	55.8
qT	11.9	55.3
S cb	11.8	55.4
S	12.0	55.2

2+50

S	10.8	56.4
cb	10.8	56.4
qT	11.0	56.2
1/4	10.2	57.0
c	10.0	57.2
1/4	9.9	57.3
qT	9.88	57.29
N cb	in drive	

2+94 to 3+20 curb out

N cb	6.60	60.57
qT	7.3	59.9
1/4	7.3	59.9
c	7.4	59.8
1/4	7.9	59.3
qT	8.4	58.6
S cb	8.0	59.2
S	8.0	59.2

67.17

3+25 beg. curb + gdr ox So.

S	6.1	61.1
cb	5.9	61.23
qT	6.5	60.7
1/4	6.1	61.1
c	5.8	61.4
1/4	5.7	61.5
qT	5.4	61.8
N cb	4.67	62.50

3+50

N cb	3.72	63.45
qT	4.5	62.7
1/4	4.8	62.4
c	5.0	62.2
1/4	5.4	61.8
qT	5.9	61.3
S cb	5.70	61.47

3+75

S cb	5.76	61.41
qT	6.0	61.2
1/4	5.5	61.7
c	5.0	62.2
1/4	4.7	62.5
qT	4.4	62.8
N cb	3.66	63.51

4+10.10 WL San Pasqual 3		
N	3.6	63.8
cb end cb	4.0N	63.15
gt	4.7	62.5
1/4	5.1	62.1
C	5.5	61.7
1/4	6.0	61.2
gut	6.5	60.7
5 cb cb end	5.93	61.24
℄ 30' ST		
S	8.0	59.2
c R.N.I M.H.	5.6	61.6
N	3.8	63.4
℄ +8		
N	3.9	63.3
C	4.0	61.2
S	8.N	59.0
E L 30' ST		
S	10.1	57.1
C	8.0	59.2
N	5.K	61.8
EL +10		
N	58	61.4
c	9.5	57.7
S	11.6	55.6

67.17

T.P.	12.78	54.39

Indexed
C.S.K.

X Sec San Pasqual 30' Wide

Los Pinos N/V

N∠ Los Pinos = 00

From P.3 67.17

0+00				
W			1.3	65.9
+3			1.9	64.3
C			3.3	63.9
+10			1.6	64.6
E			3.8	63.4
+10			4.7	62.5
0+25				
-10			2.5	64.7
E			2.1	65.0
+3			0.9	66.3
C			0.9	66.3
+12			0.9	66.3
W			+0.4	67.6
T.P.	12.71	79.49	0.39	66.78
0+50				
-1			7.5	72.0
W			9.4	70.1
C			10.1	69.3
E			10.0	69.5
0+75				
E			7.6	71.9
C			6.4	73.1
W			5.7	73.8
+1			4.1	75.4
1+00				
-1			0.9	78.6
W			1.5	78.0
C			3.4	76.1
E			3.4	76.1
15			1.1	78.3
T.P.	6.36	85.33	0.51	78.97
1+25				
-10			2.3	83.0
E			6.1	79.2
C			6.6	78.7
W			5.5	79.8
+1			4.8	80.5
1+50				
-1			3.8	81.5
W			4.6	80.7
C			5.4	79.9
+10			5.0	80.3
E			4.1	81.2
+7			1.5	83.8

Xex San Pasqual 30' Wide
Los Pinos to Ocean View Blvd

T.P. P.33	0.48	54.87	54.39	
	00 = S.L Los Pinos P33			
	0+50			
W		1.3	53.6	
C		1.7	53.2	
E		1.6	53.3	
+5		2.1	52.8	
	1+00			
-10		11.6	43.3	
E		8.8	46.1	
C		8.6	46.3	
W		8.4	46.5	
	1+18			
W	Sin. gut. Cem.	10.03	44.84	
+3	& Cem. apron	10.40	44.27	
+6	" " "	10.70	44.17	
	1+30			
W		11.9	43.0	
C		11.5	43.4	
E		12.1	42.8	
+10		16.1	38.8	

Red. to Profile made GBH 8-12-40

54.87

T.P.	0.35	42.86	12.36	42.51
	1+45	So. Cholla Creek		
W			1.8	41.1
C			7.3	35.6
E			10.5	31.4
+15			11.0	31.9
	1+70			
-20			10.1	32.8
E			10.5	32.4
C			10.5	32.4
W			11.8	31.1
+20			10.6	32.3
	2+00			
-20			10.6	32.3
W			9.9	33.0
C			10.1	32.8
E			9.2	33.7
+20			8.0	34.9
	2+50			
-20			10.0	32.9
E			9.1	33.8
C			9.2	33.7
W			9.9	33.0
+10			10.5	32.4
+15			12.3	30.6
+20			12.5	30.4

42.86

2+75		
-20	12.6	30.3
-15	11.4	31.5
W	10.3	32.6
C	10.4	32.5
E	7.7	35.2
+20	6.3	36.6
3+00		
-20	5.1	37.8
E	5.5	37.4
C	6.1	36.8
W	9.0	33.9
+10	11.9	31.0
+25	12.9	30.0
3+20		
-20	13.0	29.9
-10	8.5	34.4
W	5.4	37.5
C	5.6	37.3
E	5.8	37.1
+20	6.0	36.9
3+40		
-20	7.0	35.9
E	7.4	35.5
C	8.0	34.9
W	8.5	34.4
+20	8.9	34.0
3+45		
-20	5.7	37.2
W	6.0	36.9
C	4.5	36.4
E	5.3	37.6
+5	7.1	35.8
+20	6.9	36.0
4+00		
E	5.0	37.9
C	6.2	36.7
W	6.0	36.9
4+37 N of O.V. Blvd		
W	4.9	38.0
C	5.2	37.7
E	5.2	37.7
N edge Str. @ O.V.		
E	5.83	37.03
C	5.60	37.26
W	5.34	37.52
ch to BM on Bridge	0.44	42.42 42.43

Moore
Osborne
Hale
1-C-41.

X sec of Sandlock Grade (Texas St.)
Mission Ave. to Carlino del Rio.
See F.B. 1442-11 for align.

5+00.06 Δ 15° 32' 30" Rt.

4+45 Bot. Steel Bridge Ties

2+35.90 Δ 21° 05' Lt.

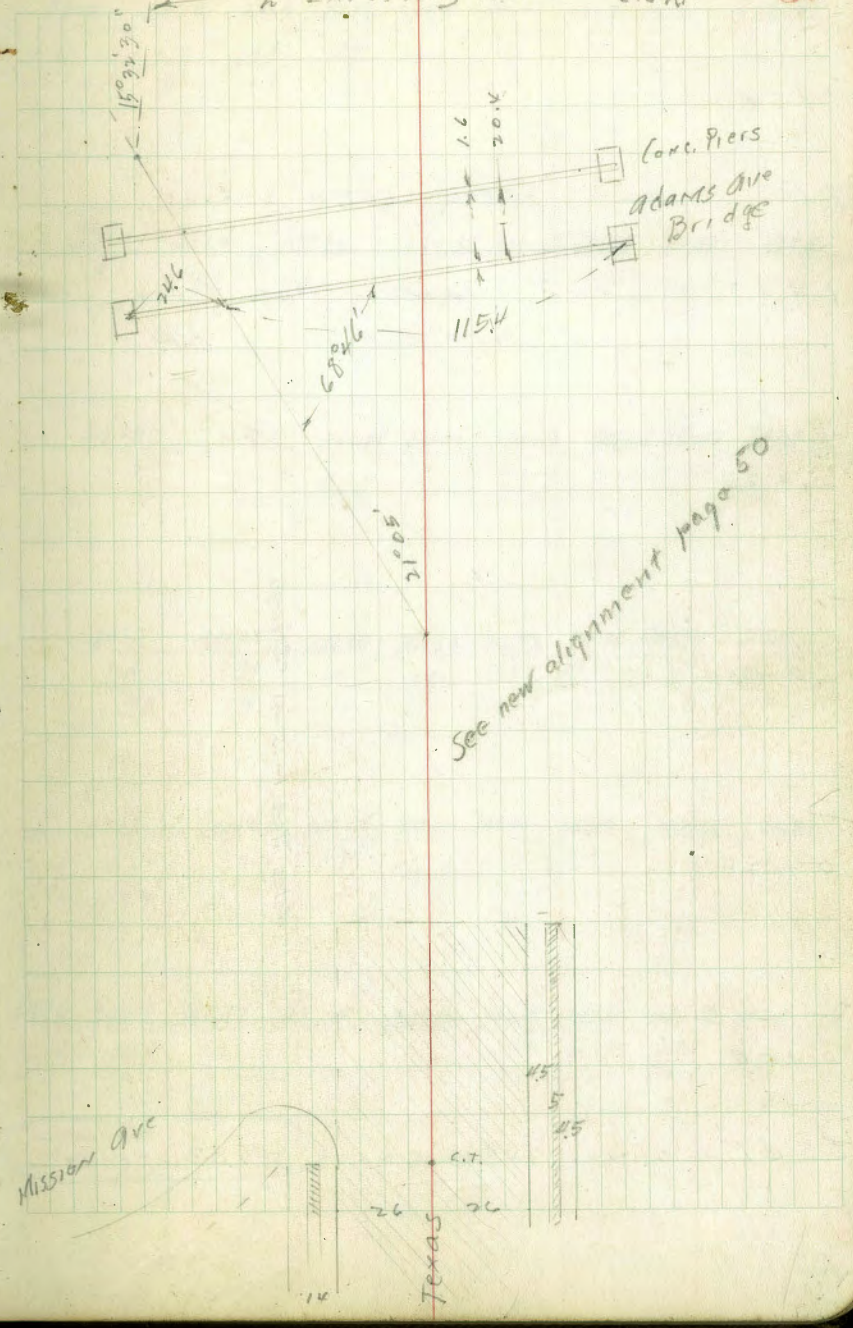
1+03.10 end Par.

0+00 C.T. Par.

℄ EXISTING R.O.W.

Indexed
C.S.K.

37



1+50				
T.P.	0.24	335.69	12.70	335.45
1+03.10	end standard par. + beg. 20' strip oil pav. = O.P.			
0+75				
0+50				
0+25				
0+00				
SEBP	2.14	348.15	346.03	Madison Texas

Notes Med 1-15-41 Pittsburgh

LT				℄		RT		
333.6	332.0	331.2	331.8	332.3	331.9	331.7	334.2	334.7
2.1 / 40	3.7 / 33	4.5 / 18	3.9 / 11 O.P.	3.4 O.P.	3.8 / 16 O.P.	4.0 / 26	1.5 / 26	1.0 / 40

335.69

339.1	337.4	337.24		337.35	337.27	336.99	337.58	338.3
9.1 / 40	10.8 / 26	10.91 / 13		10.80	10.88 / 13	11.16 / 26	10.57 / 26	9.9 / 40

340.3	339.91	340.01	340.19	340.03	339.65	340.27	340.6	
7.9 / 40	8.24 / 26	8.14 / 13	7.96	8.12 / 13	8.50 / 26	7.88 / 26	7.6 / 40	

341.7	341.25	341.46	341.64	341.52	341.24	341.84	342.3	
6.5 / 40	6.90 / 26	6.69 / 13	6.51	6.63 / 12	6.91 / 26	6.31 / 26	5.9 / 40	

342.3	341.93	342.25	342.47	342.40	342.23	342.82	343.2	
5.9 / 40	6.2 24 / 9T	5.90 / 13	5.68	5.75 / 13	5.92 / 26	5.33 / 26	5.0 / 40	

344.0	343.11	342.47	342.89	342.96	342.79	342.50	343.06	343.6
4.2 / 40	5.04 / 26 / 66	5.68 / 26 / 9T.	5.26 / 13	5.19	5.36 / 12	5.45 / 26 / 9VT	5.09 / 26 / 66	4.6 / 40

348.15

Lt ℄ Rt.

4+00

327.9 303.4 303.4 303.4 302.9 303.5 285.3 286.8 298.8
+17.5 7.0 7.0 7.0 7.5 4.9 25.1 23.6 11.6
30 9 4 7.0 16 ~3 50 73 100 Bot. Pier
O.P. O.P. O.P.

T.P. 0.33 310.44 17.9~ 310.11

310.44
5

3+50

335.2 326.4 308.9 308.7 308.8 308.2 308.8 293.8 292.0 303.4
+12.2 +3.4 14.1 14.3 14.2 14.8 14.~ 30.~ 31.0 19.6
40 25 14 7 14 ~3 50 62 81
O.P. O.P. O.P.

2+90

336.3 330.8 315.9 315.5 315.9 315.5 316.5 302.4 300.2 309.0
+13.3 +7.9 7.1 7.5 7.1 7.5 6.5 20.6 22.8 14.0
40 26 18 11 25 57 65 85
O.P. O.P. O.P.

2+70

332.0 317.4 317.8 318.3 317.9 318.5 311.3 312.0
+9.0 5.6 5.~ 4.7 5.1 4.5 11.7 11.0
40 20 13 O.P. 8 29 47 60
O.P. O.P.

T.P. 0.15 323.03 12.81 322.88

323.03

328.8 327.4 321.6 322.0 322.4 322.3 322.4 325.4 333.2
6.9 7.3 14.1 13.7 13.3 12.4 13.3 10.3 2.5
40 32 26 17 13.3 5 12 20 40
O.P. O.P. O.P.

2+35.9 Sec. on Spl.T of ℄

2+00

330.1 331.1 325.5 325.9 325.7 326.4 326.9 332.0 333.2
5.6 4.6 10.~ 9.8 9.0 9.3 8.8 3.7 2.5
40 30 18 14 O.P. 1~ 20 30 40
O.P. O.P.

335.69

335.69

LT | ℄ | RT

6+50

311.1 + 27.7 = 58

291.4 (+1.75 = 48) | 273.5 (−0.4 = 4 o.p.) | 273.9 (11.6 o.p.) | 273.2 (−0.7 = 17 o.p.) | 274.5 (+0.6 = 20) | 274.5 (+0.6 = 24) | 250.9 (+23.0 = 60) | 250.4 (+23.5 = 70) | 264.9 (−9.0 = 88) | 274.4 (+0.5 = 120)

6+00 to 6+00

6+00

297.1 + 17.3 = 46

292.2 (+0.4 = 10) | 279.6 (−0.2 = 5 o.p.) | 279.8 (5.7 o.p.) | 279.4 (−0.4 = 16 o.p.) | 280.6 (+0.8 = 25) | 255.5 (+24.3 = 59) | 255.5 (+24.3 = 64) | 264.5 (−15.3 = 70) | 277.1 (−2.7 = 108)

T.P. 0.85 = 285.48 | 12.86 = 284.63

285.48

5+50

286.5 + 11.0 = 15

285.7 (11.8 = 5 o.p.) | 285.9 (11.6 o.p.) | 285.2 (12.3 = 16 o.p.) | 286.8 (10.7 = 23) | 261.6 (35.9 = 63) | 261.5 (36.0 = 68) | 284.5 (13.0 = 103)

5+00.06 = ℄ Sec. on Sp 17

291.1 + 6.2 = 27

300.7 (+3.2 = 20) | 293.6 (3.9 = 6) | 292.2 (5.3) | 292.1 (5.4 = 1 o.p.) | 291.2 (6.3 = 21 o.p.) | 291.3 (6.2 = 25) | 269.3 (28.2 = 67) | 269.3 (28.2 = 68) | 292.6 (4.9 = 110)

295.7 | 295.1

4+75

ground Bot. Pier → 1.8 = 7.5 = 2.4

T.P. 0.11 = 297.49 | 13.04 = 297.38

297.49

301.06 + 9.38 = 310.44 / 3 = Bot. steel Bridge Tie

4+45

310.4 + 0.0 = 20

298.2 (12.2 = 7) | 298.3 (12.1 = 7 o.p.) | 298.2 (12.2 o.p.) | 297.3 (13.1 = 18 o.p.) | 297.1 (13.3 = 25) | 278.4 (32.0 = 55) | 277.4 (33.0 = 70) | 296.7 (13.7 = 110)

Bot. Pier

310.44 / 2

9+00					
T.P.	0.18	247.82	12.89	247.64	
8+47.52	Δ 37° 59′ LT. Sec. on Split				
7+69.07	Δ 45° 00′ RT. Sec. on Split				
T.P.	0.14	260.53	12.79	260.39	
+35					
7+00					
T.P.	0.49	273.18	12.79	272.69	
		285.48			

9+00 (LT. … ℄ … RT; Mouth of Ravine)

281.3 | 276.1 | 249.4 | 246.4 | ℄ 246.4 | | 249.9 | 233.2 | 228.2 | 228.2 | 239.4

+34.9/59 | +29.7/43 | +3.0/25 | 0.0/19 | 1.4 | —/2 O.P. | +3.5/17 | −13.2/37 | −18.2/47 | −18.2/72 | −7.0/134 — Mouth of Ravine

T.P. 247.82 ℄

8+47.52

294.1 | 285.0 | 257.2 | 253.2 | 252.6 | 254.2 | 253.3 | 242.6 | 235.2 | 234.1 | 253.1

+39.9/70 | +30.8/55 | +3.0/36 | −1.0/30 O.P. | −1.6/13 O.P. | 6.3 | −0.9/12 | −11.6/33 | −19.0/51 | −20.1/59 | −1.1/69

7+69.07

282.3 | 275.3 | 260.0 | 260.2 | 261.0 | 241.4 | 239.8 | 258.0

+22.3/48 | +15.3/28 | 0.5 O.P. | +0.2/19 O.P. | +1.0/28 | −18.6/58 | −20.2/70 | −2.0/103

T.P. 260.53 ℄

+35

273.2 | 269.2 | 263.7 | 263.9 | 263.5 | 264.3 | 264.5 | 244.2 | 242.1 | 249.0 | 267.4

+9.3/57 | +5.3/42 | −0.2/2 O.P. | 9.3 O.P. | −0.4/18 O.P. | +0.4/20 | +0.6/25 | −19.7/59 | −21.8/71 | −14.3/76 | +3.5/108

7+00

293.1 | 272.9 | 267.6 | 267.9 | 267.3 | 269.4 | 247.9 | 247.8 | 256.2 | 266.9

+25.2/44 | +5.0/38 | −0.3/3 O.P. | 5.3 O.P. | −0.6/18 O.P. | +1.5/25 | −20.0/60 | −20.1/70 | −11.7/76 | −1.0/104

T.P. 273.18 ℄

	LT														RT
			243.8	230.2	220.1	219.2	219.1	218.9	220.6	220.1	214.1	202.7	202.5	205.0	226.3
+50			+24.7	+11.1	+1.0	+0.1		-0.2	+1.5	+1.0	-5.0	-16.4	-16.6	-14.1	+7.2
			45	17	1X	10	4.2	9	11	20	30	35	45	50	97
						O.P.		O.P.							
			242.0	226.0	221.0	221.1	221.0	220.7	212.4	208.4	208.4		224.6		
11+32.44	Δ 15°01' Rt.	Sec. on Split	+21.0	+5.0	0.0	+0.1	2.3	-0.3	-8.6	-12.6	-12.6		+3.6		
			75	18	13	8		11	50	62	72		96		
						O.P.		O.P.							
T.P.	1.0 X	223.29	1X.93	222.25			223.29								
			244.2	237.1	223.8	224.4	224.5	224.4	225.1	210.9	211.0		225.0		
11			+19.7	+12.6	-0.7	-0.1	10.7	-0.1	+0.6	-13.6	-13.5		+0.5		
			45	25	19	1X		6	14	49	61		90		
						O.P.		O.P.							
			253.4	243.6	229.5	229.3	229.5	229.3	230.2	213.8	213.8		217.8		232.9
+50			+23.9	+14.1	0.0	-0.2	5.7	-0.2	+0.7	-15.7	-15.7		-11.7		+3.1
			46	36	20	15		5	16	39	44		59		96
						O.P.		O.P.							
T.P.	0.10	235.18	17.7 X	235.08			235.18								
			268.0	259.4	234.8	234.6	234.8	234.6	236.3	220.8	220.7		232.0		
10+00			+33.2	+24.6	0.0	-0.2	13.0	-0.2	+1.5	-14.0	-14.1		-2.8		
			47	32	16	11		8	17	46	56		92		
						O.P.		O.P.							
			273.7	263.3	244.7	244	244.6	244.4	244.1	226.6		224.4	241.6		
9+40.43	Δ 19°01' Rt	Sec. on Split	+32.1	+27.7	+1.1	-0.2	6.2	-0.2	+2.5	-15.0		-17.2	0.0		
			60	45	18	9		9	32	50		65	127		
						O.P.		O.P.							
		247.8 X					247.82								

					Lt.					℄			Rt				
					248.6	201.2	184.3	183.1	183.3	183.1	184.8	168.5	168.5	174.5	185.1
1℄ + 6.54	∠ 10°9' Lt. Section Split				+65.3	+17.9	+1.0	−0.2	3.0	−0.2	+1.5	−14.8	−14.8	−8.8	+1.8
					99	27	19	14 O.P.		7 OP	17	28	38	40	65
T.P	0.55	186.32	12.71	185.77				186.32							
					243.0	209.6	191.8	190.3	190.6	190.4	191.0	174.0	174.0	178.9	193.2
1℄					+52.4	+19.0	+1.2	+0.3	7.9	−0.2	+0.4	−16.6	−16.6	−11.7	+2.6
					77	23	16	12 OP		8 O.P.	13	20	37	40	67
					237.9	213.3	197.3	196.1	196.3	196.0	198.0	184.1	180.1	192.3	201.2
+50					+41.6	+16.0	+1.0	−0.2	2.2	−0.3	+1.7	−16.2	−16.2	−4.0	+4.9
					70	22	16	12 O.P.		7 O.P.	13	32	40	45	74
T.P	0.12	198.48	12.93	198.36				198.48							
					234.2	213.1	202.1	200.8	201.1	200.8	201.1	187.5	183.5	191.9	199.1	204.1
13 +10					+33.1	+12.0	+1.0	−0.3	10.7	−0.3	0.0	−13.6	−13.6	−9.2	−2.0	+4.0
					89	24	17	13 O.P.		8 O.P.	12	24	39	41	52	64
					245.8	221.2	208.7	207.4	207.7	207.4	208.1	194.1	194.1	198.7	211.3	
+50					+38.1	+13.5	+1.0	−0.3	3.6	−0.3	+0.4	−13.6	−13.6	−9.0	+3.6	
					56	21	16	12 O.P.		8 O.P.	14	32	40	45	76	
T.P	0.81	211.29	12.81	210.48				211.29								
					249.0	227.2	214.1	212.9	213.1	212.9	213.5	203.1	199.0	199.0	220.4	
1℄					+35.9	+14.1	+1.0	−0.2	9.9	+0.2	+0.4	−10.0	14.1	14.1	+7.3	
					52	17	14	10 O.P.		8 O.P.	16	30	41	71	94	
		223.29						223.29								

17

218.1	172.6	157.1	155.9	156.1	156.4	157.0	150.1	144.3	144.3	150.3	159.6
+ 62.0 / 103	+ 14.5 / 21	+1.0 / 15	− 0.2 / 10 o.P. 5.8		+0.3 / 11 o.P.	+0.9 / 16	−6.0 / 38	−11.8 / 40	−11.8 / 50	−5.8 / 52	+3.5 / 75

T.P. 0.42 161.87 12.94 161.45

161.87

+50

229.2	178.3	161.9	161.8	161.9	162.1	162.6	157.8	151.0	150.9	152.9	162.6	166.7
+ 67.3 / 115	+ 16.4 / 18	0.0 / 11	− 0.1 / 8 o.P. 12.5		+0.2 / 12 o.P.	+0.7 / 17	−4.1 / 31	−10.9 / 33	−11.0 / 38	−9.0 / 41	+0.7 / 69	+4.8 / 84

16+02. Sec. on SPLIT LC Δ 10°59' LT.

237.7	184.5	168.4	167.2	167.4	167.6	168.2	157.4	154.9	154.9	162.4	170.6
+ 70.3 / 137	+17.1 / 27	+1.0 / 13	−0.2 / 10 7.0		+0.2 / 10	+0.8 / 19	−10.0 / 49	−12.5 / 51	−12.5 / 57	−5.0 / 58	+3.2 / 78

+75

237.9	187.7	171.3	170.5	170.7	172.0	171.5	157.5	157.5	162.5	170.9
+ 62.2 / 135	+ 17.0 / 22	+0.6 / 9	− 0.2 / 6 o.P. 3.7		+0.3 / 14 o.P.	+0.8 / 21	−13.2 / 42	−13.2 / 50	−8.2 / 51	+0.2 / 124

T.P. 0.92 174.39 12.85 173.47

174.39

+50

233.2	186.8	176.1	173.0	173.1	172.9	173.8	159.6	159.6	166.6	176.8
+ 60.1 / 108	+ 13.7 / 19	+3.0 / 13	− 0.1 / 7 o.P. 13.2		−0.2 / 13 o.P.	+0.7 / 21	−13.5 / 36	−13.5 / 44	−6.5 / 47	+3.7 / 120

15

243.8	196.2	179.8	178.8	179.0	278.8	180.4	171.0	164.4	164.4	170.4	180.2
+ 64.8 / 100	+17.2 / 21	+0.8 / 14	−0.2 / 10 o.P. 7.3		−0.2 / 10 o.P.	+1.4 / 18	−8.0 / 36	−14.6 / 38	−14.6 / 46	−8.6 / 49	+1.2 / 74

186.32

186.32

Sta.					LT				℄			RT				
20	End of ℄ Levels and + or − Rods off ℄				141.0 +17.5/47	126.5 +3.0/38	123.5 0.0/23	123.6 +0.1/18 o.p.	123.5 13.0	123.5 0.0/3 o.p.	124.5 +1.0/10	118.5 −5.0/22	114.4 −9.1/25	114.5 −9.0/38	122.9 −0.6/47	129.3 +5.8/62
+50					160.3 +31.9/68	144.6 +16.2/26	128.4 0.0/20	128.7 +0.3/14 o.p.	128.4 8.4	128.4 0.0/4 o.p.	129.4 +1.0/16	120.4 −8.0/30	119.4 −9.0/34	119.5 −8.9/46	129.5 +1.1/49	136.1 +7.7/61
19					183.4 +50.5/79	152.1 +19.2/25	132.9 0.0/18	132.7 −0.2/14 o.p.	132.9 3.6	132.8 −0.1/6 o.p.	133.9 +1.0/26	127.9 −5.0/46	124.2 −8.7/49	124.3 −8.6/57	135.3 +2.4/62	139.3 +6.2/71
T.P.	0.13	136.50	12.85	136.37					136.50							
+50					199.6 +61.4/88	162.3 +24.1/27	139.2 +1.0/17	138.1 −0.1/12 o.p.	138.2 11.0	138.0 −0.2/7 o.p.	138.8 +0.6/21	134.1 −4.1/35	128.0 −10.2/36	128.1 −10.1/41	136.1 −2.1/47	141.0 +2.8/59
18					203.1 +59.2/87	165.4 +27.5/25	145.3 +1.4/17	143.7 −0.2/12 o.p.	143.9 5.3	143.8 −0.1/8 o.p.	143.9 0.0/21	140.7 −3.2/23	132.7 −11.2/51	132.7 −11.2/57	140.7 −3.2/58	151.8 +7.9/80
T.P.	0.25	149.22	12.90	148.97					149.22							
17+44.21	Sec. on SPLIT Δ7°½				211.8 +61.3/102	169.2 +18.7/26	150.0 −0.5/19	150.2 −0.3/15 o.p.	150.5 11.4	150.5 0.0/6 o.p.	151.3 +0.8/16	145.6 −4.9/56	136.6 −13.9/64	136.6 −13.9/67	148.6 −1.9/68	156.8 +6.3/78
		161.87							161.87							

			LT		℄		RT			
			101.7	102.3	101.9	101.9	103.2	103.2	94.1	96.0	104.5	104.9
			13.0 / 40	12.4 / 26	12.8 / 24 O.P.	12.8 / 3 O.P.	11.5	11.5 / 2	20.6 / 9	18.7 / 23	10.2 / 31	9.8 / 50
			105.8	107.1	106.1	106.3	107.1	107.1	100.3	99.7	110.7	112.1
			8.9 / 40	7.6 / 26	8.6 / 24 O.P.	8.4 / 1 O.P.	7.6	7.6 / 4	14.4 / 11	15.0 / 22	4.0 / 34	2.6 / 50
							114.66					
			109.0	110.7	110.5	111.2	103.3	103.3	116.1	118.2		
			18.4 / 40	16.7 / 22 O.P.	14.9 O.P.	16.2 / 4	24.1 / 10	24.1 / 18	11.3 / 24	9.2 / 60		
			115.4	115.1	115.0	114.7	116.3	106.4	106.3	120.5	124.0	
			12.0 / 20	12.3 / 17 O.P.	12.4	12.7 / 4 O.P.	11.1 / 13	21.0 / 21	21.1 / 28	6.9 / 43	3.4 / 60	
			117.9	118.0	117.7	117.2	118.0	109.0	109.2	121.9	125.4	
			9.5 / 40	9.4 / 15 O.P.	9.7	10.2 / 8 O.P.	9.4 / 20	18.4 / 30	18.2 / 37	5.5 / 49	2.6 / 60	
			119.0	119.2	119.9	118.6	119.3	110.3	110.4	123.0	127.9	
			8.4 / 40	8.2 / 14 O.P.	8.3	8.8 / 6 O.P.	8.1 / 20	17.1 / 28	17.0 / 36	4.4 / 47	+0.5 / 60	
							127.36					

+50				
22				
T.P.	0.12	114.64	12.82	114.52
+50				
21				
20+47.81	A 11°30' RT			
20+50	beg. of full sec. by wye level			
T.P. N.E. Cor	0.48	127.36	9.62	126.88
		136.50		

Top Culv. Hd. wall

25				
+50				
+30				
NL				
T.P.	0.5L	89.92	12.75	89.38
+50				
23				
T.P.	0.54	102.13	13.07	101.59
		114.66		

LT L RT

79.3 79.2 78.8 79.0 78.6 73.7 72.0 79.1 78.7

10.6 10.7 11.1 10.9 11.3 16.2 17.9 10.8 11.2
40 24 2 O.P. 5 9 19 27 40

83.8 84.0 83.6 84.4 84.4 77.1 76.7 83.8 83.5

6.1 5.9 6.3 5.5 5.5 12.8 13.2 6.1 6.2
40 24 4 O.P. 2 8 24 25 40

85.4 85.5 85.5 86.2 86.2 79.2 79.4 85.8 84.3

4.5 4.4 4.2 3.7 3.7 10.7 10.5 4.1 5.4
40 24 4 O.P. O.P. 5 9 27 29 50

88.5 88.9 88.5 88.4 89.3 82.5 81.8 88.9 87.8

1.2 1.0 1.2 1.5 0.6 7.2 8.1 1.0 2.1
40 30 24 4 1 14 25 50
O.P. O.P.

89.92

93.0 93.2 92.7 92.8 93.2 93.5 86.0 86.1 92.1 92.6

6.1 8.9 6.2 6.3 8.9 8.6 14.1 16.0 9.0 9.5
40 28 25 4 4 7 22 26 50
O.P. O.P.

98.3 98.4 97.5 97.5 98.6 98.6 89.6 89.8 98.7 97.4

3.8 3.7 4.6 4.6 3.5 3.5 12.6 12.8 3.4 4.7
40 27 25 5 3 10 21 28 50
O.P. O.P.

102.13

	LT		℄		RT			
28	52.9	53.5	53.6	54.4	49.7	50.1	54.2	50.0
	11.9 / 40	11.3 / 27 0.P	11.7 0.P	10.4 / 7	15.1 / 11	14.7 / 29	10.6 / 34	14.8 / 40
+50	56.8	57.1	57.0	54.9	53.5	52.3	57.5	53.1
	8.0 / 40	7.7 / 27 0.P	7.8 0.P	7.9 / 5	11.3 / 9	12.5 / 28	7.3 / 34	11.7 / 40
27	60.8	60.9	60.6	61.6	57.2	56.8	60.8	57.9
	4.0 / 40	3.9 / 27 0.P	4.7 0.P	3.7 / 5	7.6 / 9	8.0 / 31	4.0 / 35	6.9 / 40
26+65.58 Δ 1°30'50"RT	63.4	63.9	63.6	64.3	60.9	60.3	64.4	62.1
	1.4 / 40	0.9 / 21 0P	1.7 0.P	0.5 / 6	3.9 / 9	4.5 / 32	0.4 / 36	2.7 / 40
T.P. 0.75 64.84 13.04 64.09			64.84					
26	68.7	69.6	69.4	69.5	65.3	64.4	68.6	68.1
	8.4 / 40	7.5 / 21 0.P.	7.7 0.P	7.4 / 6	11.8 / 17	12.7 / 27	8.5 / 30	9.0 / 40
25+50	75.7	74.5	74.0	75.0	74.3	67.6	69.4	73.6	73.1
	1.4 / 40	2.6 / 27 0P.	3.1 0.P.	2.1 / 3	2.8 / 7	9.5 / 9	7.7 / 26	3.5 / 31	4.0 / 40
T.P. 0.00 77.13 12.79 77.13 89.92			77.13					

BM. 3 nails Cypress Camino del Rio check to SECor 4 Sandrock Cr.	6.25	47.40	47.69 0.29	
29+50 ℄ Camino del Rio				
29				
+60				
+57.7 = Inlet end do. Box Culv.				
+54				
28+37.74 P.C. on W.L.				
T.P.	1.76	53.65 64.84	11.95	51.89

Lt	℄	Rt
47.7 6.0 40	47.7 6.0	47.4 6.3 40
46.2 48.6 48.5 49.1 48.7 48.3 45.9 7.5 5.1 5.2 4.6 5.0 5.4 7.8 40 32 25 OP 22 35 40 OP OP		
48.3 50.2 50.3 50.4 49.9 49.7 46.7 5.4 3.5 3.4 3.3 3.8 4.0 7.0 40 31 23 OP 22 35 40 OP. OP		
	43.02 10.63 27 = ℄ do. Box Culv.	
48.4 50.3 50.5 50.7 50.9 45.2 45.7 50.5 46.5 5.3 3.4 3.2 3.0 2.8 8.5 8.0 3.2 7.2 40 31 23 OP 6 13 31 36 40		
49.1 51.0 51.2 51.5 52.5 47.1 46.8 51.9 47.5 4.6 2.7 2.5 2.2 1.3 6.4 6.9 1.8 6.2 40 32 23 OP. 7 11 29 34 40		
	53.65	

Proposed align. of
Sandrock Grade (Texas St.)

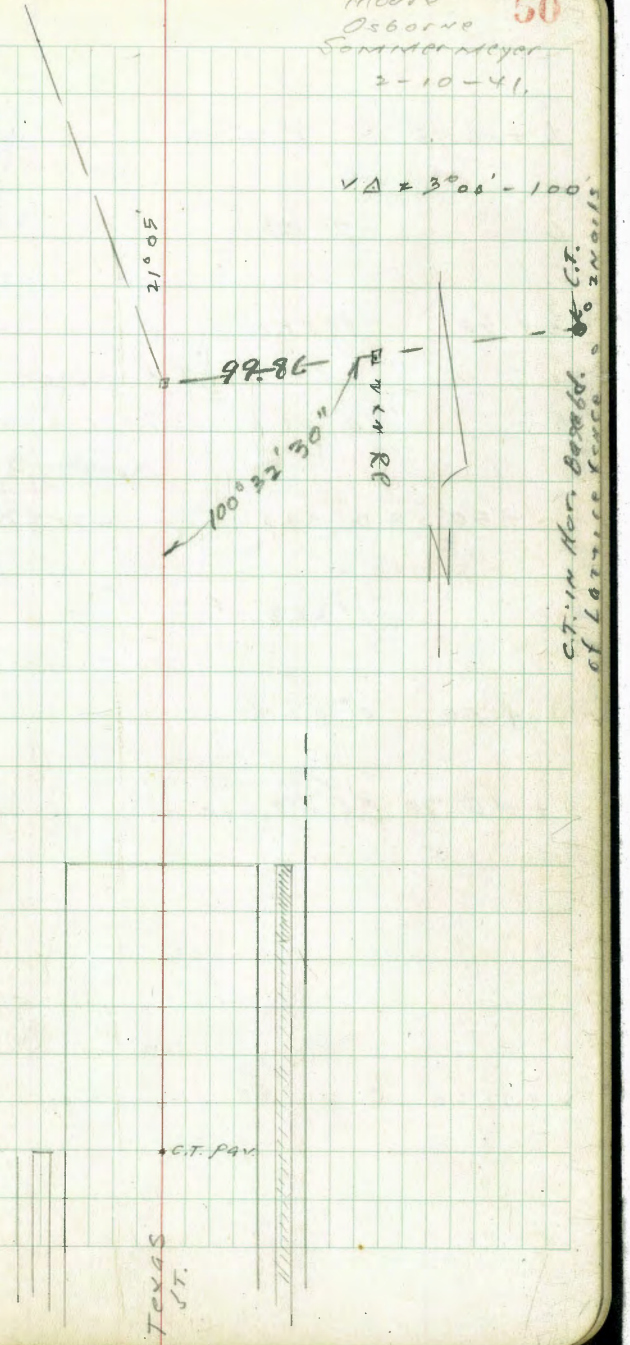
2+77.60 Δ = 21° 05' LT 2x2

0+00

indexed
c.s.k.

Moore
Osborne
Sommermeyer
2-10-41.

VΔ = 3°05' - 100'



6 + 16.95 F.C. 7° 46.25

6 7° 17.1

+ 50 5° 51.1 Δ = 15° 32' 30" RT.

D = 1000

5 4° 25.2 T = 136.46

L = 271.25

+ 50 2° 59.3 1.7188

1° 33.3

+ 50 0° 07.1

3 + 45.70 B.C. RT.

2 + 77.60 Δ 21° 05' LT.

9C339
42
19WC78
38535C
J0.46=38

V.Δ = 15° 33' - 42"

C.T. with #No.15 97°46'15"

on Hor. Cross Brace of Bridge

40.46

2 x 2 R.P.

Sec P 56 for Bridge

21° 05'

12 + 95.40 E.C. 10° 31.5

+50 9° 13.5

12 7° 47.5

11 + 50 6° 21.6

11 + 22.3 5° 34.0 = 24' 18" Con. P. Pipe Culv.

11 4° 55.6

Δ = 21° 03' Rt

+50 3° 29.7 ℄ R = 1000

T = 185.79

10 2° 03.7 L = 367.39

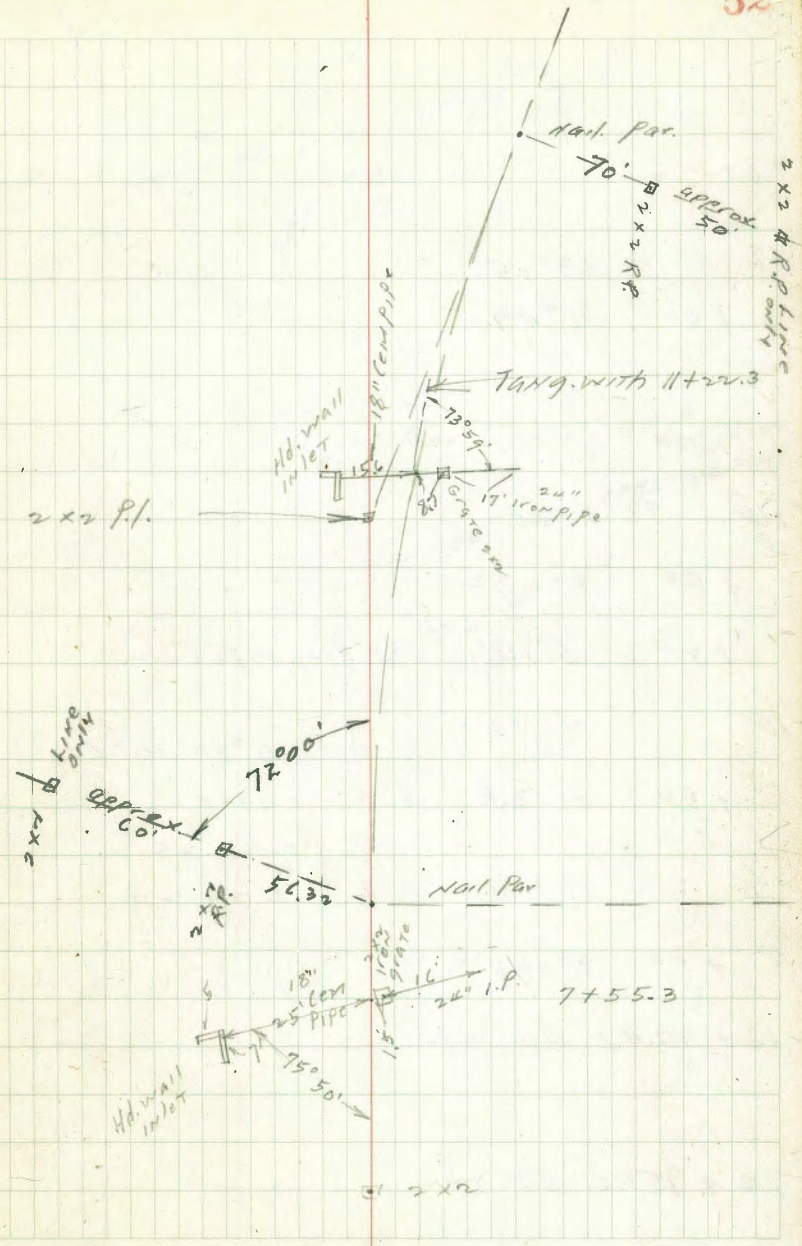
+50 0° 37.8

V. Δ = 20° 10' - 60'

93869
60
5631140

9 + 28.01 BC Rt

6 + 16.95 E.C.



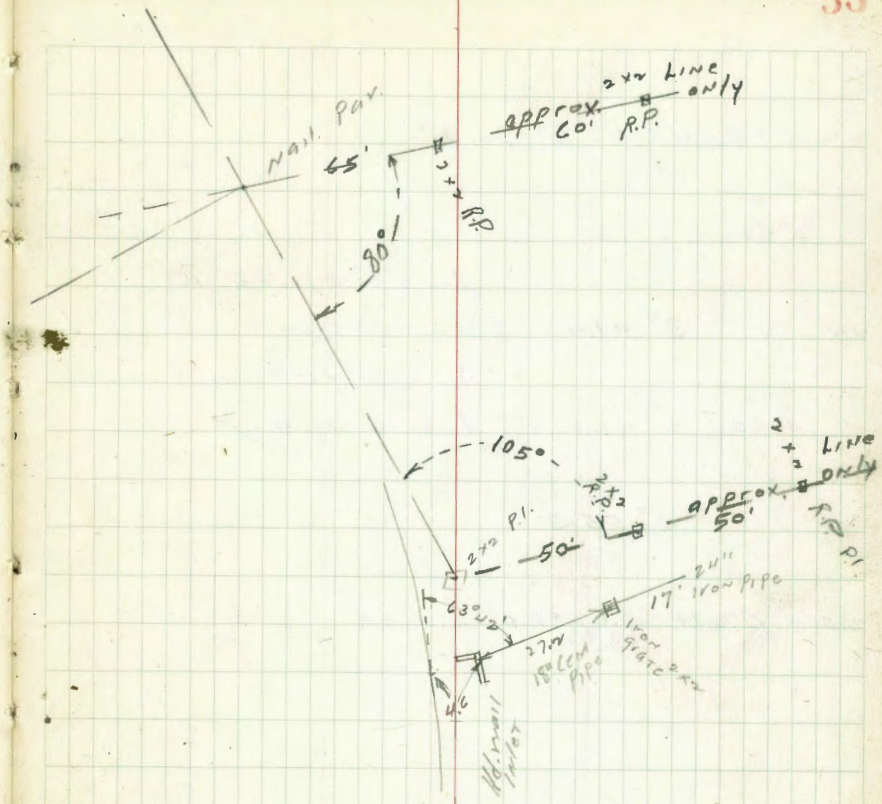
18 + 46.67 E.C. 14° 35.25

18	13° 15'	
+ 50	11° 49.0	
17	10° 23.1	
+ 50	8° 57.2	
16	7° 31.2	
+ 50	6° 05.3	
+ 20	5° 14' (26')	18" Conc. Pipe Culv.
15	4° 39.3	
+ 50	3° 13.4	
14	1° 47.5	
+ 50	0° 21.5	

Δ = 29° 10' 30" LT
R = 1000
T = 260.25
L = 509.20

13 + 37.47 B.C. LT.

12 + 95.40 E.C.



20 + 67.84
18 + 46.67
2 21.17

22 + 95.24 E.C. 6° 30.8

+50 5° 13.1

Δ = 13° 01' 45" Rt

22 3° 47.2 LR = 1000

T = 114.17

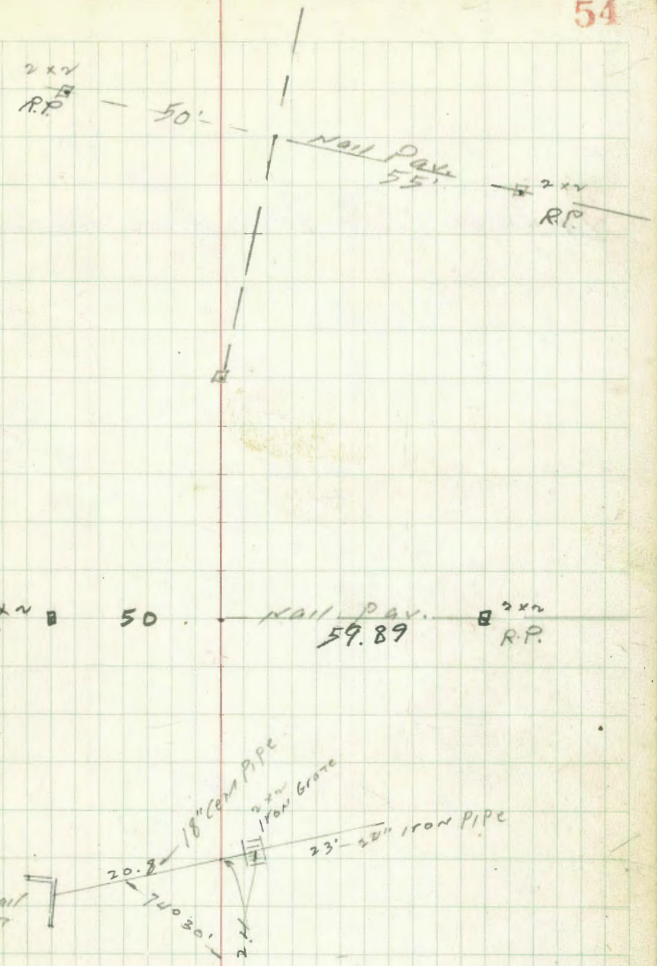
+50 2° 21.2 L = 227.40

21 0° 55.3

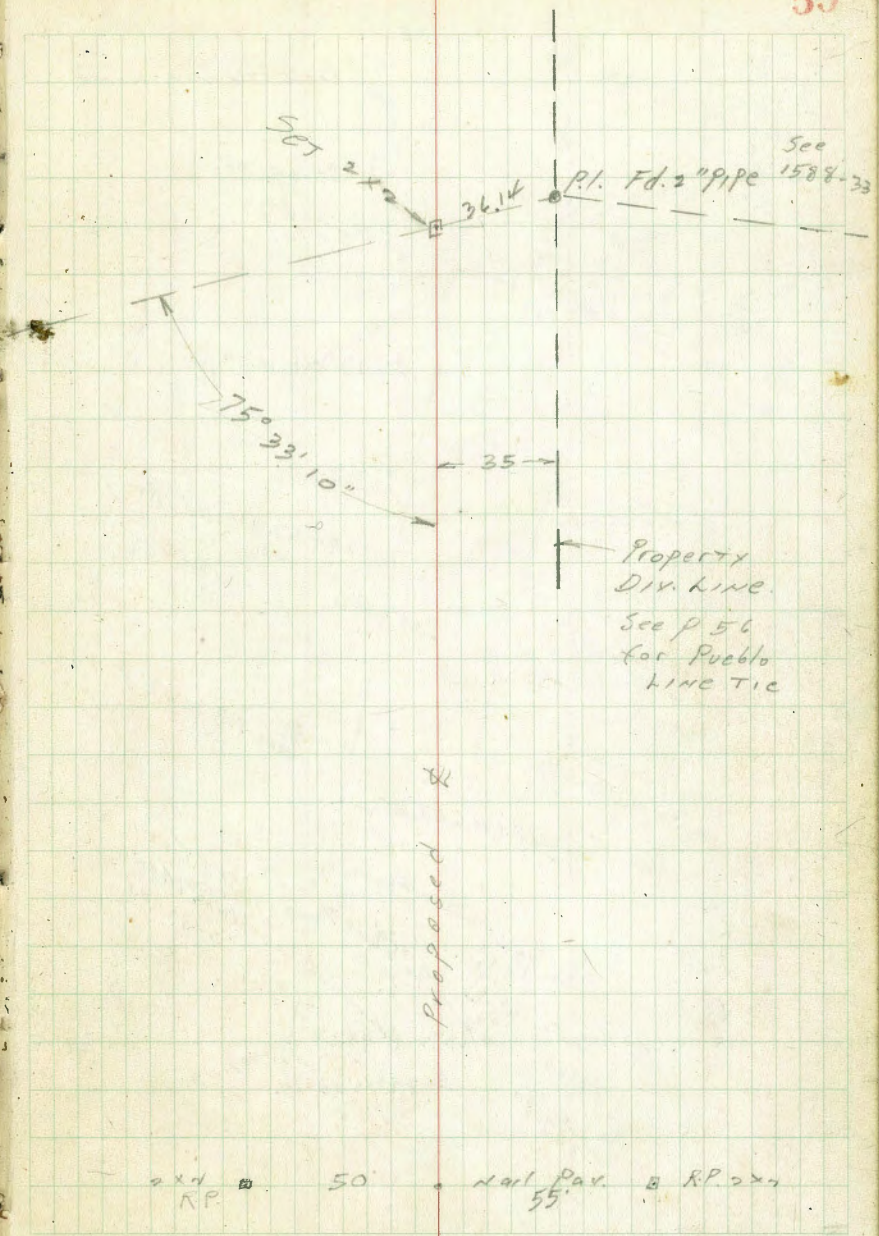
20 + 67.84 B.C. Rt

19 + 61.5 18" Conc pipe Culv.

18 + 46.67 E.C.

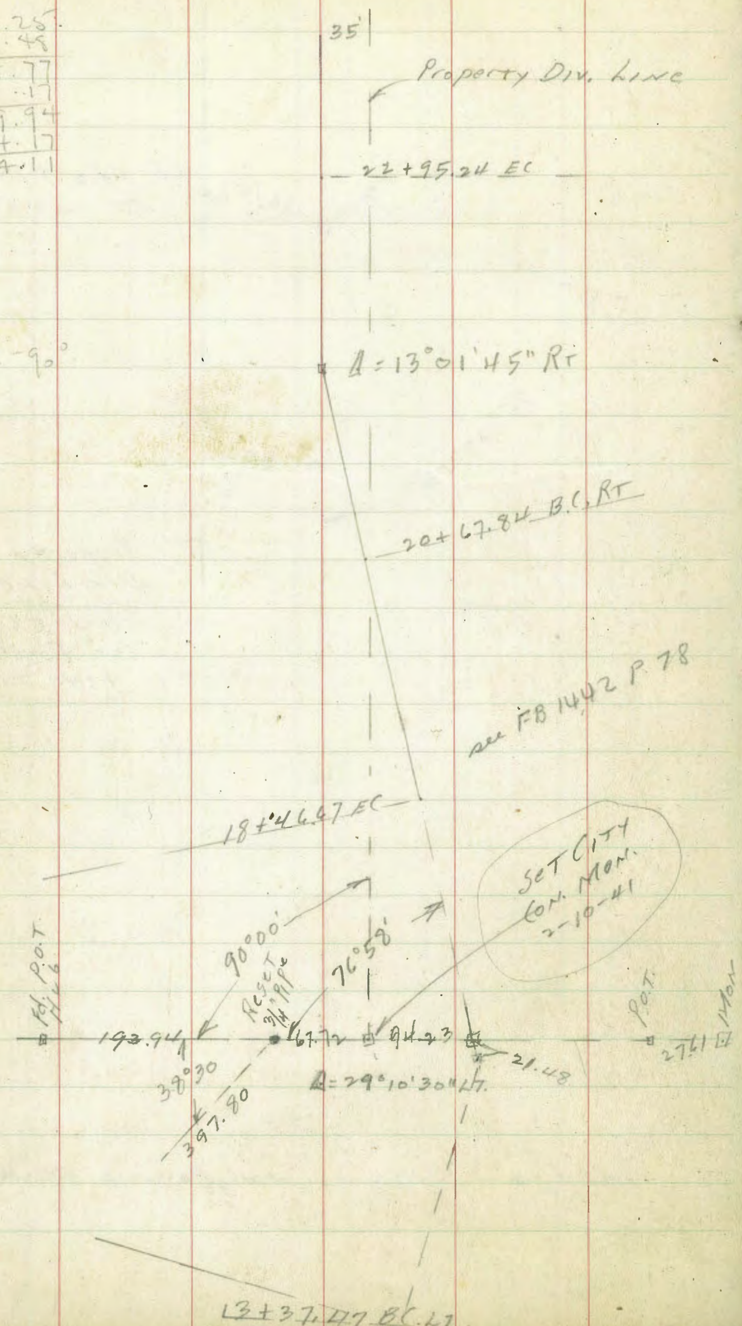


29+42.42 Int. E Camino del Rio

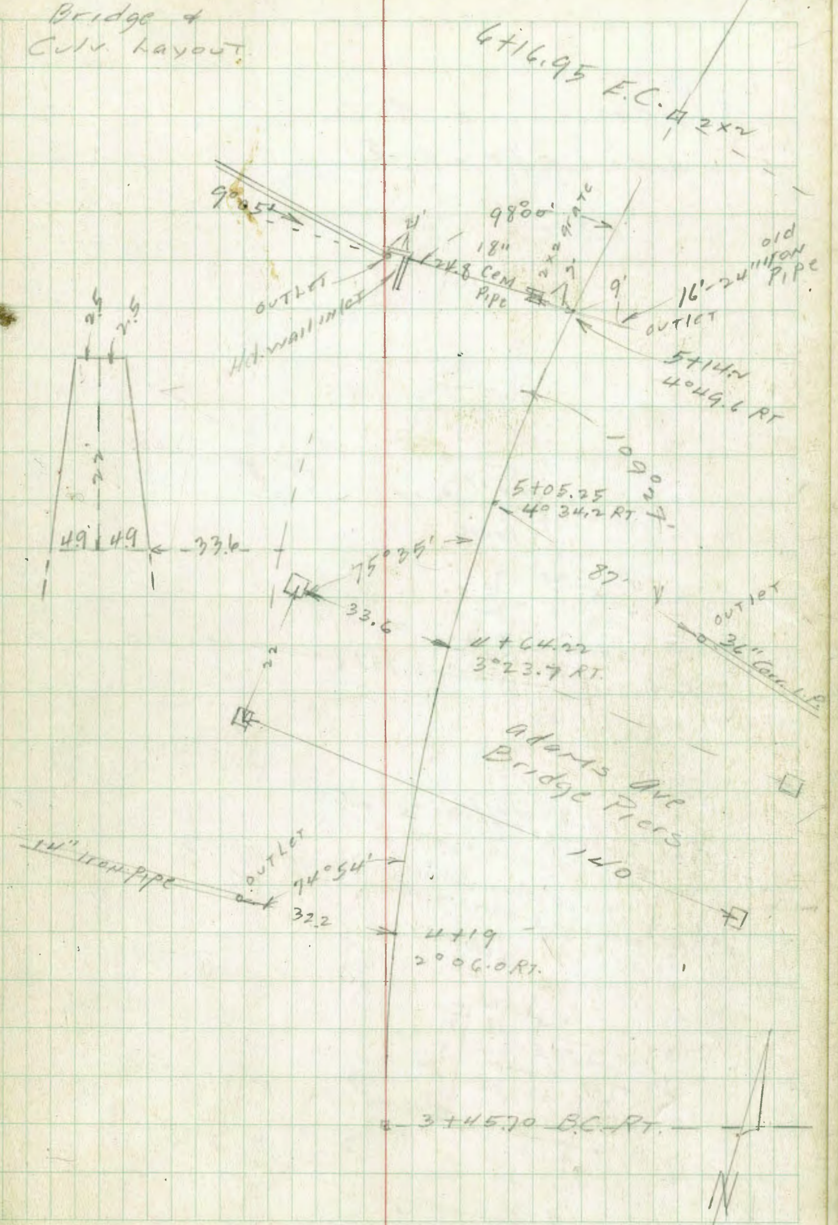


22+95.24 E.C.

260.25
- 21.48
238.77
221.17
459.94
114.17
574.11

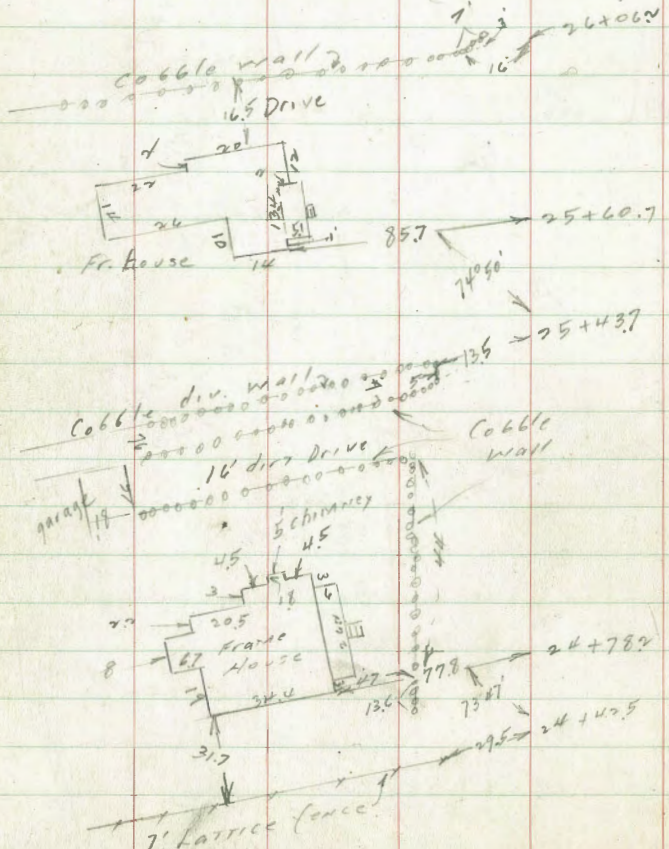


Overhead Bridge & Culv. Layout



Lt &

location of Houses
on left of ℄



18" Conc. Pipe
6' wing wall Inlet
28+89
90°
28+50
28+38.5
See P 49
Inlet do. Box Con. Culv.
Large Cypress
Eucal
Cypress

Moore
4/21/41.

Xsec S½ Russ Blvd.
27th to 27th

SW BP 196.9N 27th & B St

0-10 E½ c6. line 27th

S - 10 c6
" " gut
S c6
S gut
S + 5 N E Con. Con. Box
S +10
S +20
&
C

0+00 E.L. 27th

S
+ 5
+ 10
+ 20
C

Mr. Rhodes says
not this block

N½ of Russ & Grove
Eucalyptus & Acacia Trees

Russ Blvd.

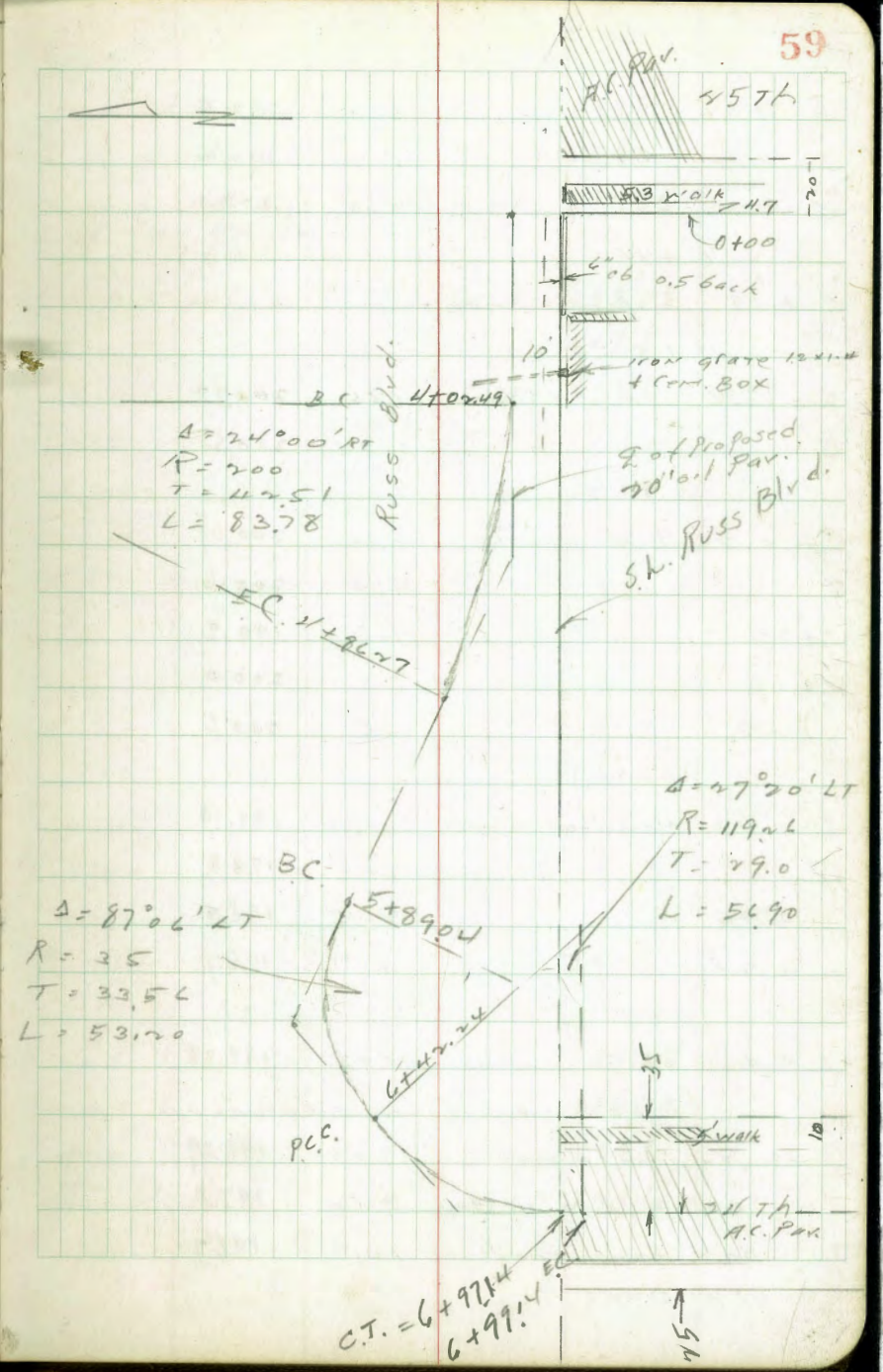
2' dl. Pepper Tree
5'x5' walk
W.L. 27th 6+01
5' dl. Euca Tree
0+00 E.L. 27th
5' walk
11.7
5' SB. Con. Vault over
5' walk needs Replacing

Oil Pav.

Indexed LM

Moore levels for Pav. Strip
4-21-41 on Russ Blvd
+57 ft. to 0+4 TH

NW BP	5.48	207.43	201.95 +57 ft + Est.
0 – 50 = E +57 ft			
S – 10 Pav		4.43	203.00
S "		4.36	203.07
+20		3.3	204.1
0 – 20			
S – 10 c6		4.53	202.90
" " gut		5.08	202.35
SL c6		4.45	202.98
" gut		4.93	202.50
SL +20		4.3	203.1
0+00 WL +5 ft			
S – 0.5 6" c6		4.22	203.21
S		4.5	202.9
+10		4.9	202.5
+14		4.9	202.5
+16		4.3	203.1
+20		4.1	203.3
0+13			
S – 0.5 6" c6		4.15	203.28
S – 0.5 FL 4" drain pipe		4.69	202.74
S		4.8	202.6



S + 10		5.4	202.0
S + 14		5.N	202.N
S + NO		4.3	203.1
	0 + 14		
S + 19	2' Pepper Tree		
	0 + 51.6		
S − 0.7	End C" curb	C.6C	200.77
S		C.9	200.5
	0 + 53		
S − 0.7	E 4' Conc walk	C.7N	200.69
S		C.8	200.6
+ 10		7.5	199.9
+ 15		9.4	200.0
+ NO		C.8	200.6
	0 + 9N		
S − 0.7	E edge Con. apron	8.30	199.13
S		8.C	198.8
+ 10		8.5	198.9
+ 20		8.7	198.7
	1 + 17		
S − 0.C	on Conc. apron	9.05	198.38
	1 + 20 on Line of drain		
S E on	iron plate	9.1N	198.29
S	FL 4" pipe in Box	9.C0	197.8
S	Bot. Sand Trap of Box.	10.7	196.7

			Inlet = 1 + NN.N on South
S + 10	ground	8.7	198.7
S + NO	"	9.N	198.N
S + NN.N	FL. Outlet 4" pipe	9.88	197.55
	Outlet = 1 + 24		
S + 24 = N'd. palm.			
	1 + 31		
S − 0.5	W. edge Conc apron	8.75	198.68
S		8.9	198.5
+ 10		8.8	198.6
+ 15		8.8	198.6
+ 20		9.N	198.N
T.P. 4.43		N0N.95	8.91	198.5N
	1 + 75		
S		3.8	199.N
+ 10		4.4	198.6
+ 14		4.C	198.4
+ NO		5.3	197.7
	1 + 8N		
S − NN E N.5	Conc walk	3.7N	199.21
	1 + 94		
S + 0.C E 11.5	Conc. apron	3.70	199.25
S − 1.5 E	Sin. gar. Conc	3.NN	199.73
+ 10		4.N	198.8
+ 20		4.4	198.6

	2+07		
S +0.8	℄ 12' Cem. apron	3.55	199.40
S −1.6	℄ Sin. gar. Cem	3.31	199.64
	2+16		
S +0.8	℄ 3' conc. walk	3.69	199.26
	2+20		
S +16	℄ 2.5 di. pine Tree		
	2+21		
	beg. Cypress hedge on South line		
	2+40		
	end " " " " "		
	2+43		
S +19.3	℄ 2' di. Pine Tree		
	2+47		
S +0.3	℄ of 3' long wire fence		
	2+63		
S		2.9	200.1
+10		3.1	199.9
+20		3.1	199.9
	2+69		
S +17	℄ 1.2' di. Pine Tree		
	2+93		
S −0.3	℄ 14' Cem apron	4.41	198.54
S −2.8	℄ Sin. gar. Cem	4.16	198.79

Pave around Tree

	3+07		
S −0.3	℄ Sin gar cent.	4.63	198.32
S +10		4.6	198.4
+20		4.3	198.7
	3+14		
S +0.3	to Hedge 18" Eugenia Tree		
	3+16		
	beg. Cypress hedge on S L.		
	3+50		
	end " " " "		
	3+51		
S +0.25	NE Cor house	6.3	196.7 ground
+10		6.5	196.5
+20		6.3	196.7
	3+69		
S +0.1	NW Cor house		
	3+71		
S	℄ 4' Cem walk	7.67	195.33
	3+88.5		
S −0.5	℄ 15.x do. gar. Cem.	8.0 ~	194.93 Floor Level
	3+80 ← back up		
S +23.5	℄ 2' Pine Tree		
	3+96		
S		8.1	194.9

	70+95			
5+5		8.9	194.1	
+10		9.0	194.0	
+20		8.8	194.2	
	4+05			
S	℄ 7.8 Sin gar Conc	9.3	193.61	Fl. Level
S		9.5	193.5	
+10		9.5	193.5	
+20		9.2	193.8	
	Note: B.C. RT = 4+07.49			
	℄ Curve (from here to end ℄ will be base Line)			
12 LT		12.5	190.5	
C		12.1	190.9	
12 RT		11.7	191.3	
T.P.	0.95 190.98	12.92	190.03	
	4+60			
23 LT	℄ Conc apron	2.3	188.66	
27 LT	℄ Sin gar conc	2.0	188.92	
	4+81			
27 LT	℄ 87 conc apron	2.65	188.33	
31 LT	℄ Sin gar. conc	2.41	188.57	

	4+84.27 = EC		
12 LT		2.9	188.1
C		2.5	188.5
12 RT		1.7	189.3
	4+93		
33 LT	℄ 11.5 Conc apron	3.32	187.16
39	℄ gar conc	3.32	187.66
	5+08		
10.5 RT	1.3 dl. oak Tree		
	5+19		
10 LT	1.5 dl. " "		
	5+38		
12 LT		5.9	185.1
C		5.7	185.3
12 RT		4.9	186.1
12.8 RT	1.2 dl. oak Tree		
	5+64		
8' LT	1.4 dl. oak Tree		
	5+85		
7.5 RT	1.0 dl. " "		
	5+89.04 BC LT		
12 LT		9.3	1817
6 LT		9.2	1818
C		9.4	1816
12 RT		8.4	182.6

		190.98		
	Center Curve			
1N	LT		11.9	179.1
C			12.1	178.9
1N	RT		11.9	179.1
T.P.	18N	180.38	1+4N	178.56
	6+47.74 P.C.C.			
1N	LT		2.5	177.9
C			3.8	176.6
1N	RT		4.0	176.4
	Center Curve			
1N	LT		4.3	176.1
C			4.7	175.7
1N	RT		5.1	175.3
	Center Curve + N			
16	LT	I 5' di. Palm		
	6+97.1N = S.A. Russ Blvd.			
6	LT	Pav.	4.83	175.58
C		"	5.20	175.18
6	RT	"	5.55	174.83
W	c6		5.88	174.50
E	c6		3.48	176.90
on S.A. Russ				

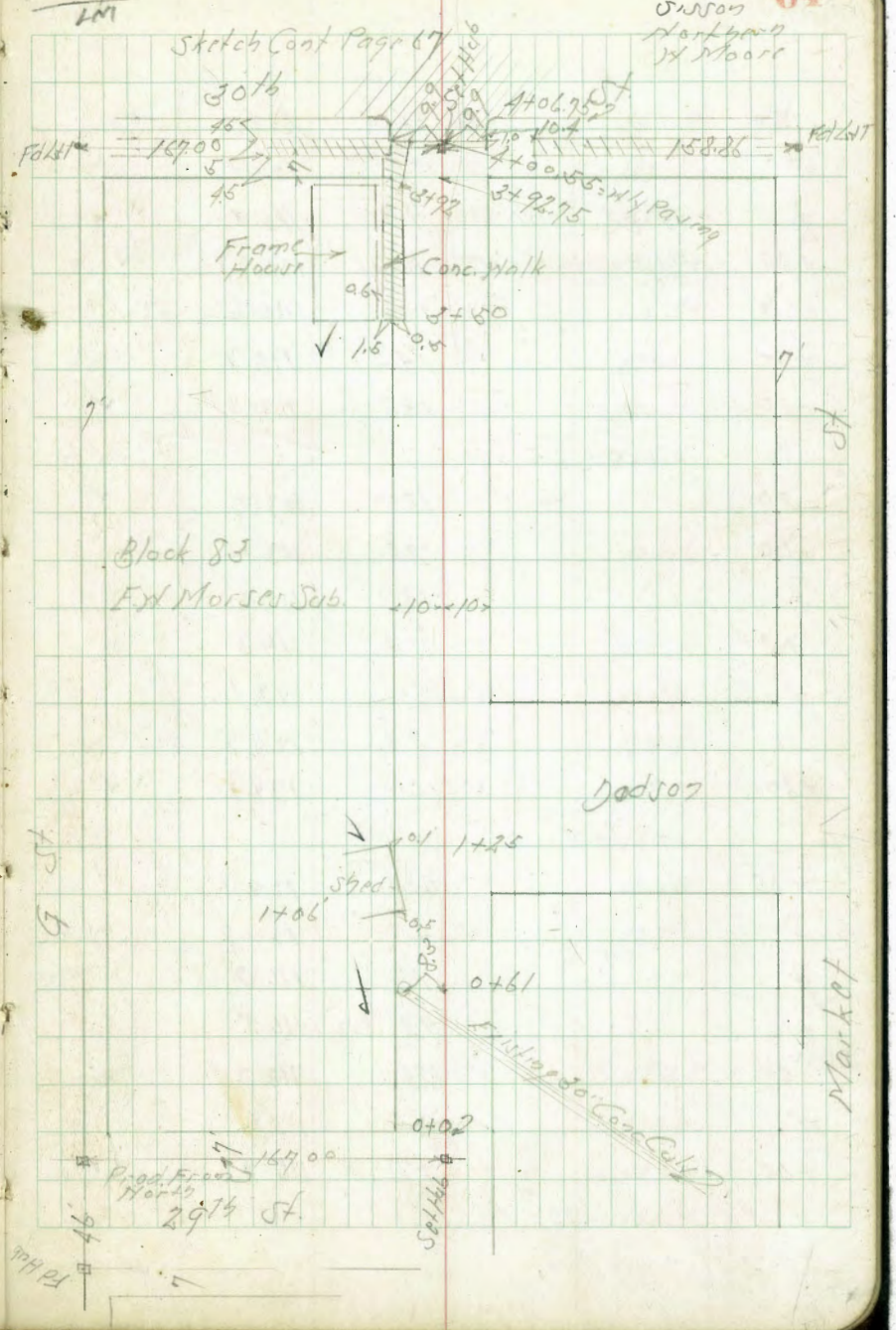
Cross Section Alley Block 83 F.W. Morses Sub
From 29th St to 30th Pl. Between 5th & Market

					S.F.B.P.
BM	0.76	167.75		166.99	FS 1+20 to 5th
TP	0.25	156.94	11.06	156.69	
TP	0.16	146.35	10.75	146.19	
TP	0.70	134.91	12.14	134.21	
TP	2.94	125.72	12.13	122.78	
		0+0 = EL. 29th St			
-15			9.8	115.9	✓
N			8.9	116.8	
℄			6.2	119.5	
S			0.9	124.5	
+20 = Top Filled Lot			+6.5	132.2	✓
	0+25				
-16 = Top Filled Lot			+7.5	133.2	✓
S			2.9	122.8	
℄			7.4	118.3	
N			10.7	115.6	
+15			12.8	112.9	✓
	0+50				
-20 = ℄ West			14.0	111.7	✓
-10			14.2	111.5	
N			12.6	113.1	
℄			8.9	116.9	
S			4.6	121.1	
+20			+7.0	132.2	✓

Notes Plotted 5-6-41 C.B.H.

Indexed
LM

April 1941 64
Simson
Northrup
W Moore



125.72

0+61

-20		76.3	132.0	✓
S		5.0	120.7	
℄	on Top 8" Sewer Pipe Conc Cvlt	9.90	115.8	✓
+8.2	= ⅛ Ends 30" Conc Cvlt Flow Line	15.25	110.32	✓
N		15.1	110.6	
+10		14.4	111.3	
+20		13.2	112.5	✓

0+75

-20		12.0	113.7	✓
-10		12.0	113.7	
N		13.7	112.6	
+2		11.4	1143	
℄		8.6	112.1	
S		4.4	121.3	
+20		16.0	131.2	✓

1+0

-15		4.4	129.1	✓
S		4.8	120.9	
℄		9.0	116.7	
+1		9.2	116.5	
+5		12.4	113.3	
N		10.3	1154	
+15		9.7	116.0	✓

1+18

S+1.2=Sly Power Pole ✓

125.72

1+25

-15		5.7	120.0	✓
N		7.2	118.5	
+4		7.7	118.0	
℄		10.0	115.7	
+0.4	= Top 8" Sewer Pipe	8.92	116.80	✓
+4		6.7	119.0	
S		5.3	120.4	
+15		0.7	125.0	✓

1+41

N -0.3 = ℄ Garage Dirt Floor		5.1	120.6	✓

1+50

-10		3.6	122.1	✓
S		4.4	121.3	
+5		6.8	118.9	
℄		6.6	119.1	
+5		5.1	120.6	
N		3.7	122.0	
+15		2.5	123.2	✓
TP	11.84	134.62	2.91	122.78

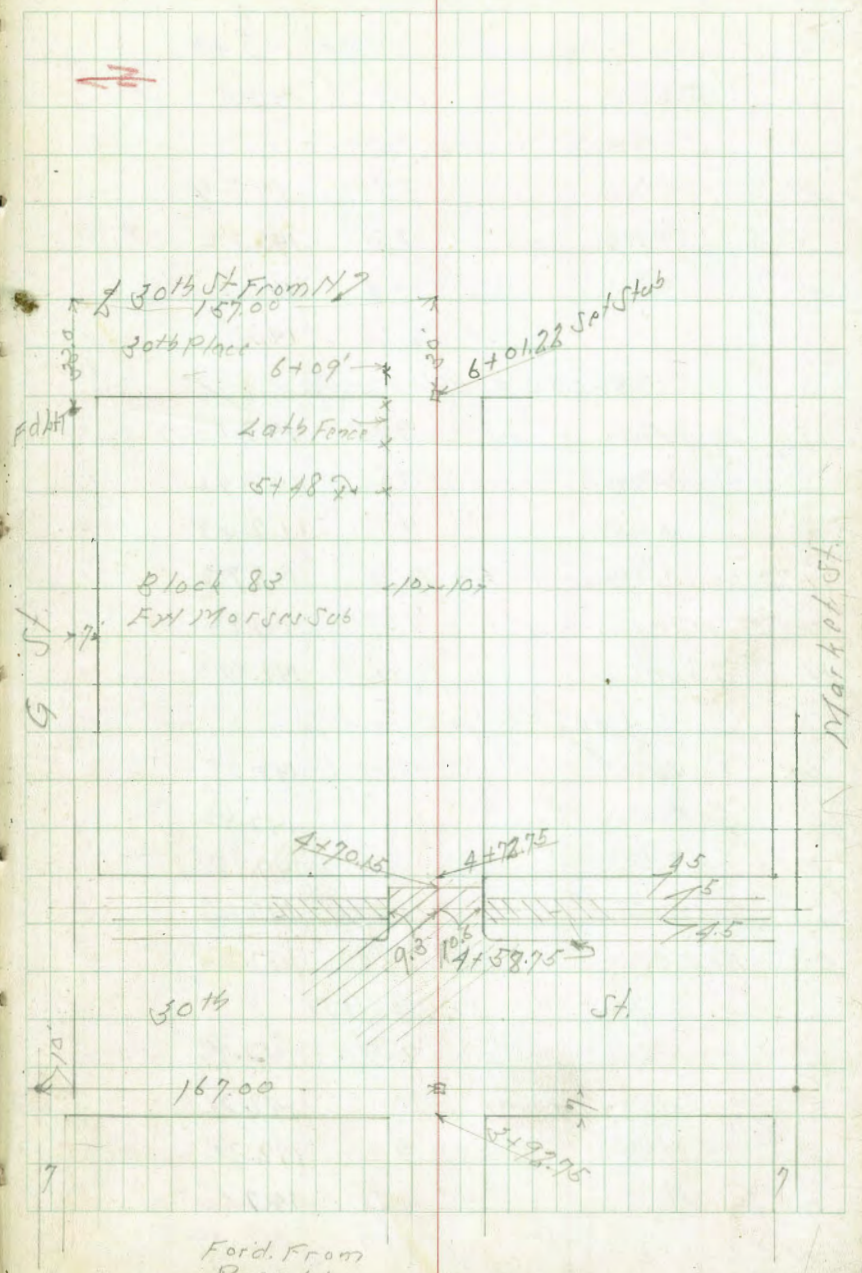
1+80

-15		9.8	124.8	✓
N		11.6	123.0	
+3		11.7	122.9	
+5		13.2	121.4	

		134.62			
Δ			13.5	121.1	
+2			12.0	122.6	
S			11.4	123.2	
+15			10.0	124.6	✓
	2+0				
-15			8.3	126.3	✓
S			10.1	124.5	
Δ			10.6	124.0	
+6			12.6	122.0	
N			10.5	124.1	
+15			8.5	126.1	✓
	2+25				
-15			7.5	127.1	✓
-8			8.7	125.9	
-4			9.6	125.0	
N			9.0	125.6	
Δ			8.5	126.1	
S			7.5	127.1	
+15			4.8	129.8	✓
	2+50				
-15			2.6	132.0	✓
S			4.4	130.2	
Δ			5.3	129.3	
N			6.4	128.2	
+8			7.2	127.4	
+10			6.3	128.3	
+20			5.1	129.5	✓

		134.62			
	2+75				
-20			4.2	130.4	✓
-5			4.4	130.2	
N			4.2	130.4	
Δ			2.5	132.1	
S			1.3	133.3	
+15			+1.8	136.4	✓
TP	11.75	145.52	0.85	133.77	
	2+90				
S-0.7	= S½ Power Pole				
	3+0				
-15			6.6	138.9	✓
S			8.4	132.1	
+5			9.2	136.3	
Δ			9.5	136.0	
+5			9.7	135.8	
N			10.1	135.4	
+15			11.2	134.2	✓
	3+20				
-15	= E½ Dirt Road to Garages		8.9	136.6	✓
N			8.4	137.1	
Δ			7.2	138.3	
S			6.4	139.1	
+15			4.1	139.4	✓

	145.52			
	3+29			
-15		3.4	142.1	✓
-10		4.3	141.2	
5		5.2	140.3	
+5		6.0	139.5	
℄		5.4	140.1	
N		5.0	140.5	
+4.3 = Fly Conc Apron		4.68	140.84	✓
+5.6 = Fly Do Garage Conc Floor		4.61	140.91	✓
	3+46			
N-5.6 = Fly Do Garage Conc Floor		4.19	141.33	✓
N-4.3 = Fly Conc Apron		4.25	141.27	✓
	3+50			
-10		4.6	140.9	
N		5.5	142.0	
+0.5 = Top Conc Wall Steps Back House	Bottom	2.59	142.93	✓
℄		2.5	143.0	
5		2.9	142.6	
+10		1.4	144.1	
+20		1.2	144.3	✓
TP	12.17	157.28	0.41	145.11
	3+75			
-10		11.6	145.7	
S		12.0	145.3	
℄		12.6	144.7	



157.28

+9.5 = Sly 2' Conc Walk	11.85	145.43	
N	11.8	145.5	
3+92.75 = W ℄ 30th St			
N	9.9	147.4	
+0.5 = Sly 2' Conc Walk	9.96	147.32	✓
℄	10.4	146.9	
S	10.3	147.0	
4+00.55 = W ly Paving			
S Top Cb	9.42	147.86	
S Gutter on Paving	9.86	147.42	
℄ " "	9.83	147.45	
+7.2 = Sly Conc Walk	9.36	147.92	
N Gutter on Paving	9.36	147.92	
N Top Cb	9.01	148.27	
4+06.75 = W Cb 30th St			
N Top Cb	9.19	147.09	
N Gutter on Pav	9.86	147.42	
℄ " "	10.10	147.18	
S Gutter "	10.25	147.03	
S Top Cb	9.64	147.64	
4+58.75 = E Cb 30th St			
S Top Cb	9.43	147.86	
S Gutter on Paving	10.07	147.21	
℄ " "	9.90	147.38	
N Gutter " "	9.68	147.60	
N Top Cb	9.09	148.19	

157.28

4+70.15 = Ely Paving			
N Top Cb = Ely End	8.75	148.53	✓
N Gutter on Paving	9.11	148.17	✓
℄ " "	9.54	147.74	✓
S Gutter " "	9.55	147.73	✓
S Cb Top	9.20	148.08	✓
4+72.25 = E ℄ 30th St			
S Cb Top = Ely End	9.15	148.13	✓
S Ground	8.7	148.6	
℄	8.8	148.5	
+1	8.1	149.2	
N	8.0	149.3	
4+81			
N +3.6 = N ly Tel Pole			
4+85			
-10	7.1	150.2	
N	6.9	150.4	
+5	6.4	150.9	
℄	7.1	150.2	
+5	7.1	150.2	
S	6.1	151.2	
+1	6.1	151.2	
+6	9.2	148.1	
+15	9.9	147.4	

157.28

	5+00			
-20		10.3	147.0	
-8		9.7	147.6	
5		4.8	152.5	
+5		5.6	151.7	
℄		5.7	151.6	
+5		5.5	151.8	
N		6.0	151.3	
+10		6.7	150.6	
	5+25			
-10		4.9	152.4	
N		4.2	153.1	
℄		3.6	153.7	
5		3.2	154.1	
+6		9.6	147.7	
+20		10.3	147.0	
	5+43			
N-6.5	= ℄ Garage Block Floor	3.23	154.05	✓
	5+48			
-20		9.9	147.4	
-6		9.4	147.9	
5		4.7	152.6	
+3		2.0	155.3	
℄		2.6	154.7	
N	= N℄ 40th Fence	3.1	154.2	
+6		3.5	153.8	

NOTES REDUCED BY: M.R.Y.

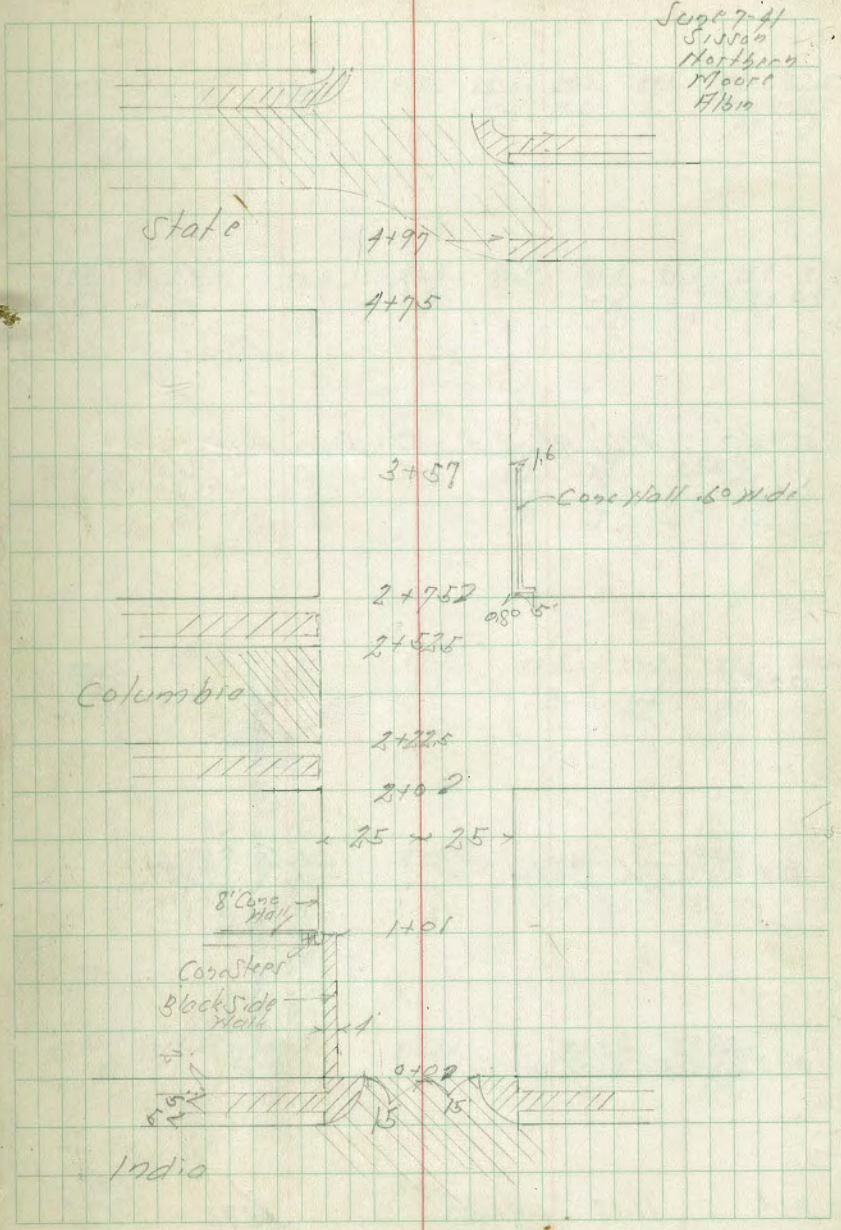
157.28

TP	669	162.31	1.66	155.63
	5+75			
-5			7.1	155.2
N			7.0	155.3
℄			6.4	155.9
+5			5.9	156.4
5			5.3	157.0
+2			5.3	157.0
+5			15.5	146.8
+20			15.6	146.7
	6+01.22 = N℄ 30th Place			
-20			14.3	148.0
-7			14.0	148.3
-1			9.0	158.3
5			9.1	158.2
+5			5.3	157.0
℄			5.6	156.7
N			6.0	156.3
+10			6.4	155.9
TP	1060	167.97	4.91	157.37
	S.W. Cor 30th Place N ℄ St			
30th Place Fnd Pipe Bottom			11.03	156.94
	Gutter		11.43	156.54
BM			0.95	167.02 S.E. BP F 30th St 166.99

Cross Section Opas St. India to State

Indexed
LM

Surge 7-41
Sisson
Northern
Moore
Hibin



Cross Section Clpas

Station				
0+89				
0+73				
0+47	17.6 Rt of ℄ = Sly Power Pole			
0+38				
0+22				
0+0	= E.L. India			
0-12	= E Cb of India			
BM	11.38	95.31	83.93	S.E.B.P. U post India

Red. Bernard Hough
Platted on double sack
6-9-41

Lt. = N ℄ Rt. = S

95.7 / +0.4 / 25 = Sly House	95.6 / +0.3 / 21 = Sly Black Walk	95.3 / 0.0 / 15	94.0 / 1.3	95.2 / 0.1 / 12	94.3 / 1.0 / 15	88.6 / 6.7 / 22	88.0 / 7.3 / 25	87.5 / 7.8 / 40
92.99 / 2.32 / 25 = Sly Stucco House	92.78 / 2.53 / 21 = Sly Black Walk	92.6 / 2.7 / 15	92.4 / 2.9	92.5 / 2.8 / 11	89.9 / 5.4 / 15	86.6 / 8.7 / 18	86.7 / 8.6 / 25	86.7 / 8.6 / 35
87.99 / 7.32 / 25 = Walk	87.93 / 7.38 / 21 = Sly Black Walk	87.1 / 8.2 / 15	87.1 / 8.2	87.3 / 8.0 / 15	85.5 / 9.8 / 22	85.5 / 9.8 / 25	85.5 / 9.8 / 35	
85.51 / 9.80 / 25 = Sly Stucco House	85.46 (5) / 9.86 / 21 = Sly Black Walk	85.7 / 9.6 / 15	85.5 / 9.8	85.9 / 9.4 / 15	84.7 / 10.6 / 22	84.6 / 10.7 / 25	84.6 / 10.7 / 35	
83.94 / 11.37 / 15 = Cb	83.55 / 11.76 / 15 = Gut	84.02 / 11.29	84.00 / 11.31 / 15 = Gut	84.00 / 11.31 / 15 = Cb				
83.93 / 11.38 / 25 = Cb	83.14 / 12.17 / 25 = Gut	83.37 / 11.94 / 15	83.77 / 11.54	83.66 / 11.65 / 15	83.93 / 11.38 / 25 = Cb			

95.31

1+76				
1+57	- E/y Conc Dr + W/y Conc Wall on Lt			
TP	11.54	118.58	0.16	107.04
1+46				
1+18				
1+09				
1+01				
TP	11.94	107.20	0.05	95.26
		95.31		

Lt. ℄ Rt

112.36 6.32 25 = Top Conc Strip | 111.3 7.3 25 | 111.4 9.4 17 | 109.2 8.9 15 | 109.4 9.2 | 109.6 9.0 15 | 119.6 +1.0 25

107.19 11.39 25 = E/y Conc Dr + W/y Conc Wall | 107.6 11.0 20 | 107.3 11.3 15 | 107.6 11.0 | 106.6 11.0 25 | 107.9 1.6 25

118.58

106.99 0.21 25 = W/y Conc Dr Wall | 105.6 1.6 15 | 104.8 2.4 | 104.7 2.5 15 | 115.4 +8.2 25

102.4 4.8 25 | 100.3 6.9 15 | 99.9 7.3 | 100.5 6.7 12 | 102.4 4.8 15 | 110.2 +3.0 25

102.40 4.80 25 = E/y Conc Wall

96.36 10.84 25 = W/y Conc Wall | 96.37 10.83 | 97.4 9.8 15 | 97.1 10.1 | 97.6 10.0 11 | 98.3 8.9 15 | 98.3 8.9 17 | 95.1 12.1 25 | 89.0 18.2 25 = S/y Block Wall

107.20

Upas

2+75 = E.L. Columbia

TP 11.87 130.06 0.39 118.19

2+65 25' Lt of ℄ = ℄ Fire Hyd

2+52.5 = E.Cb Columbia

2+37.5 = ℄ Columbia

2+22.5 = W.Cb Columbia

2+19

2+10 17.4' Rt of ℄ = S/L Power Pole

2+0 = W.L. Columbia

118.58

Lt ℄ Rt

74

117.7 118.1 118.8 119.5 121.4 129.28

12.4 / 25 | 13.0 / 15 | 11.3 | 10.6 / 15 | 8.7 / 25 | 0.78 / 25 S.S. Mh Conc Mon Top

115.94 / 2.64 / 26 Cb | 115.25 / 3.33 / 24.6 Cut | 116.1 / 2.5 / 15 | 117.2 / 1.4 | 118.4 / 0.7 / 15 | 119.5 / +0.9 / 25

115.19 / 3.39 / 25 Con Pav | 115.7 / 2.2 / 15 | 116.0 / 2.1 | 116.8 / 1.8 / 15 | 118.6 / +1.0 / 25

114.94 / 3.64 / 25 Cb | 114.40 / 4.18 / 25 Cut | 114.5 / 4.1 / 15 | 114.8 / 3.8 | 115.3 / 3.3 / 10 | 116.3 / 2.3 / 15 | 119.4 / +0.8 / 25

114.4 / 4.2 | 114.8 / 3.8 / 8 | 116.6 / 2.0 / 15 | 117.3 / 1.3 / 25

115.22 / 3.34 / 25 Cb Cut Pav | 114.8 / 3.8 / 20 | 112.2 / 6.4 / 15 | 112.2 / 6.4 | 113.2 / 5.4 / 12 | 5 / 116.7 / 2.7 / 15 | 1233 / 113.5 / 0.7 / 20 | 113.9 / +1.7 / 25

118.58

TP	11.19	152.39	0.0	141.20
4+05				
3+95				
TP	11.31	141.20	0.17	129.89
3+59				
3+53				
3+25				
3+21	17.5 Rt of ℄ = Sly Pow Pole			
3+0				
		130.06		

Lt ℄ Rt

137.66	137.4	136.8	136.4	137.1	151.2	154.2
3.54 25	3.8 25	4.4 15	4.8	4.1 15	+10.0 9	+13.0 25
135.8	135.1	134.6	135.1	139.6	151.4	152.8
5.4 25	6.1 15	6.6	6.1 5	1.6 11	+10.2 13	+11.6 25

141.20

127.5	128.8	128.8	129.2	129.8	135.1	143.4	143.7
3.6 10	1.3 25	1.3 15	0.9	0.3 15	+5.0 15	+13.3 17	+13.6 25
125.7	127.6	127.9	128.1	128.9	130.6	130.5	139.6
4.1 10	2.5 25	2.2 15	2.0	1.2 15	+0.4 25	+0.4 26.5 Bott Wall	+9.5 Top Wall
120.3	123.2	124.1	124.3	125.8	126.8	126.8
9.8 10	6.9 25	6.0 15	5.8	4.3 15	3.3 25	3.3 26 Bott Wall
120.2	120.9	121.9	122.3	123.1	123.1
9.9 25	9.1 15	8.2	7.8 15	7.0 25	7.0 26 Bott Wall

130.06

Lt ℄ Rt

Cloudy

BM			6.84	113.10	SEBP Victor & Columbia 113.14
TP	0.83	119.94	11.37	119.11	
TP	0.54	130.48	12.05	129.94	
TP	0.63	141.99	11.89	141.36	
TP	1.47	153.25	14.79	151.78	
4+97					
4+90					
4+85	12.4 Rt of ℄ = 5½ Impervious				
TP	14.51	163.57	0.23	152.06	
4+75 = W.L. Static					
4+40					
		152.39			

158.2 160.0 162.7 162.88

5.4/25 3.6/15 0.9 0.69/25 Topsoil

161.8 155.6 158.1 161.2 162.1 162.9 163.3

11.8/40 8.0/25 5.5/15 2.4 1.5/7 0.7/15 0.8/25

163.57

150.9 151.0 151.91 152.4 150.8 149.8 157.8 161.2 162.4

2.4/25 1.4/15 0.48 4.7 = Outlet 18" Storm Flow Line 0.0 1.6 2.6/3 +5.4/7 +8.8/15 +10.0/25

142.8 142.4 142.9 142.8 154.1 158.2 156.6

9.6/25 10.0/15 10.4 9.6/4 +1.7/7 +5.8/17 +6.2/20

152.39

Indexed
C.S.K.

Moore Rand 1-16-42

Curb & Paving Levels on Diamond St.
Ingraham to Jewel

Profile 1101

Red. & plot. 1-17-42 CSK

North = LT RT.

		NL Pav. 10	℄ Pav	SL Pav 10	Curb 20	Curb grade
2+00		87.33	87.33	87.18	86.83	
		4.58	4.58	4.73	5.08	84.81
		87.33	87.33	87.08	86.83	
1+70	beg. cb on South	86.70	86.72	86.66	86.27	
		5.71	5.19	5.25	5.64	84.27
		86.70	86.72	86.66	86.27	
1+50		86.39	86.38	86.28		
		5.54	5.53	5.63		
		86.39	86.38	86.28		
0+95	End cb on South	85.30	85.32	85.32	85.27	
		6.61	6.59	6.69	6.64	84.83
		85.30	85.32	85.32	85.27	
0+45	beg. cb on South	84.37	84.38	84.24	84.18	
		7.54	7.53	7.67	7.73	83.84
		84.37	84.38	84.24	84.18	
0+00 = E.L. Ingraham		83.56	83.59	83.36		
		8.35	8.34	8.45		
		83.56	83.59	83.46		
E.L. of Hd. C.T	8.34	91.91				1.52 %
			91.91			
			2			

Diamond Ingraham

76

Lt 10 | ℄ | Rt 10 | Curb 50

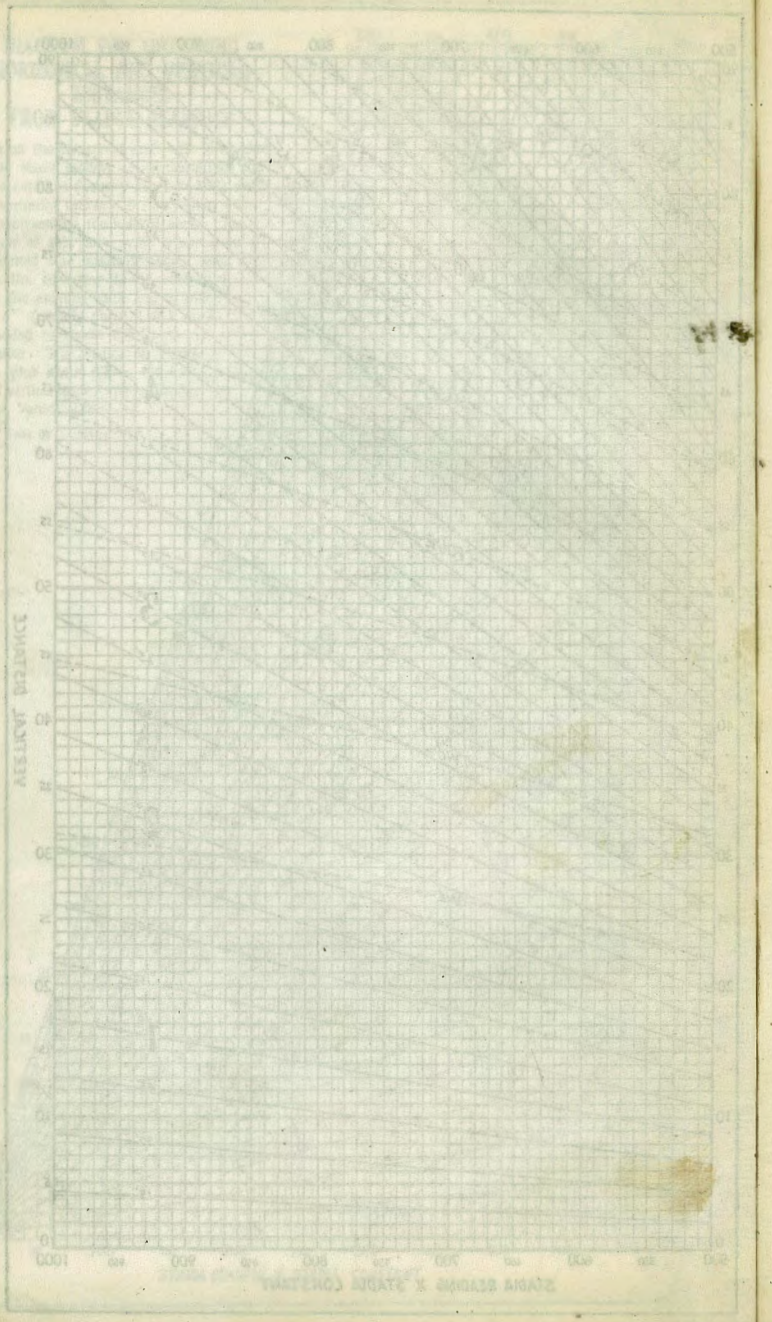
	88.62	88.63	88.46	88.25
	3.49	3.48	3.45	3.66
	88.62	88.63	88.46	88.25	88.19

x + 70 End cb. on South

	88.26	88.24	88.09	87.99
	3.65	3.67	3.82	4.12
	88.26	88.24	88.09	87.79	87.80

x + 50

91.91



$$
\begin{array}{r}
345.7 \\
136.5 \\
\hline
482.2 \\
514 \\
\hline
32
\end{array}
$$

$$
\begin{array}{r}
15\ 32\ 30 \\
7\ 46\ 15 \\
\hline
97\ 46\ 15
\end{array}
$$

$$
\begin{array}{r}
21\ 05 \\
\hline
10\ 32\ 30 \\
90 \\
\hline
100\ 32\ 30
\end{array}
$$

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20—16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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