1584

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

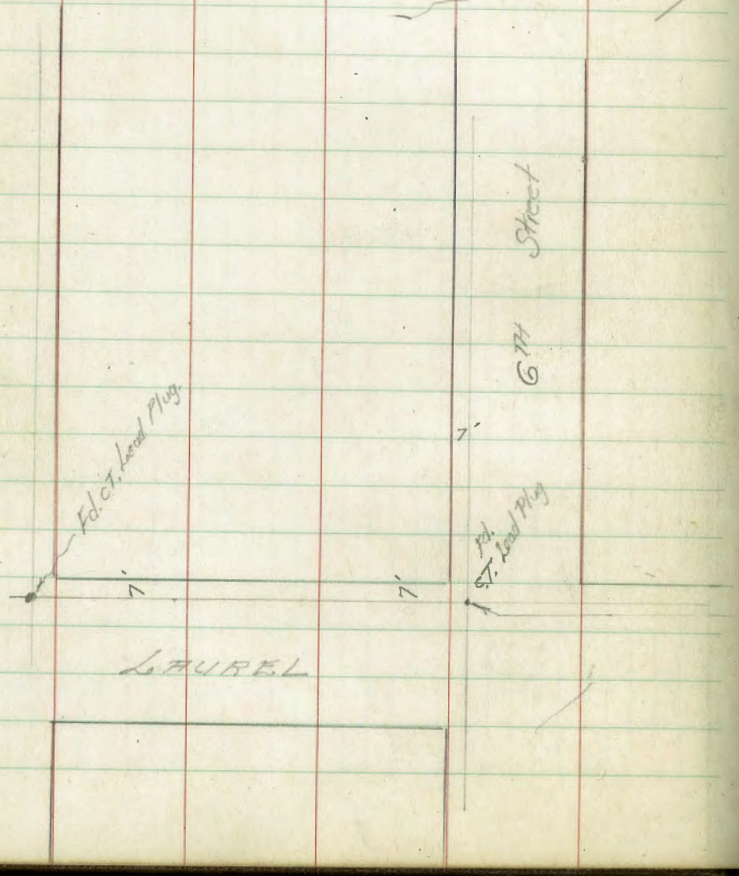
Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

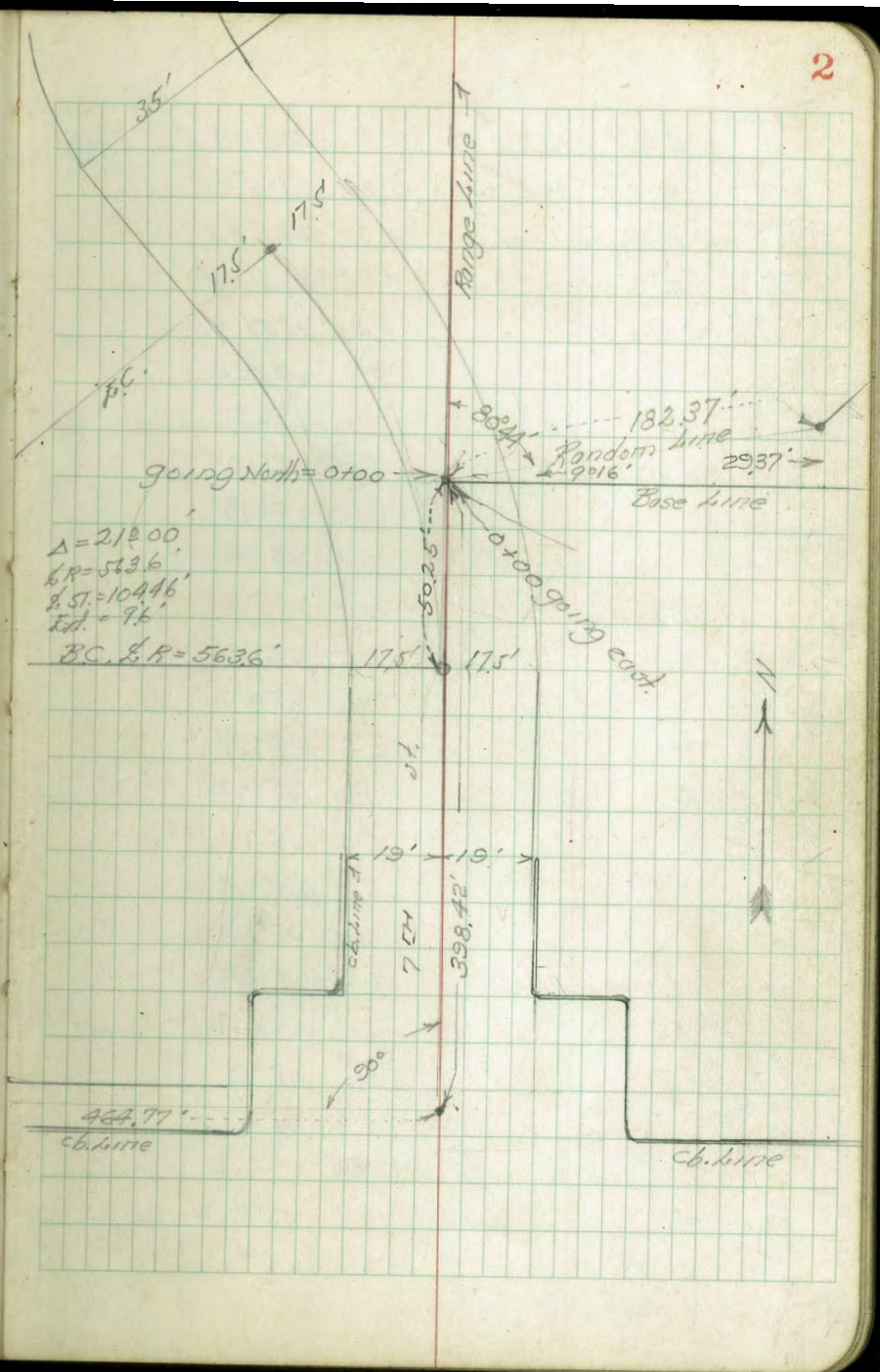
Walker
Isbell
7-22-40

Topographical Survey

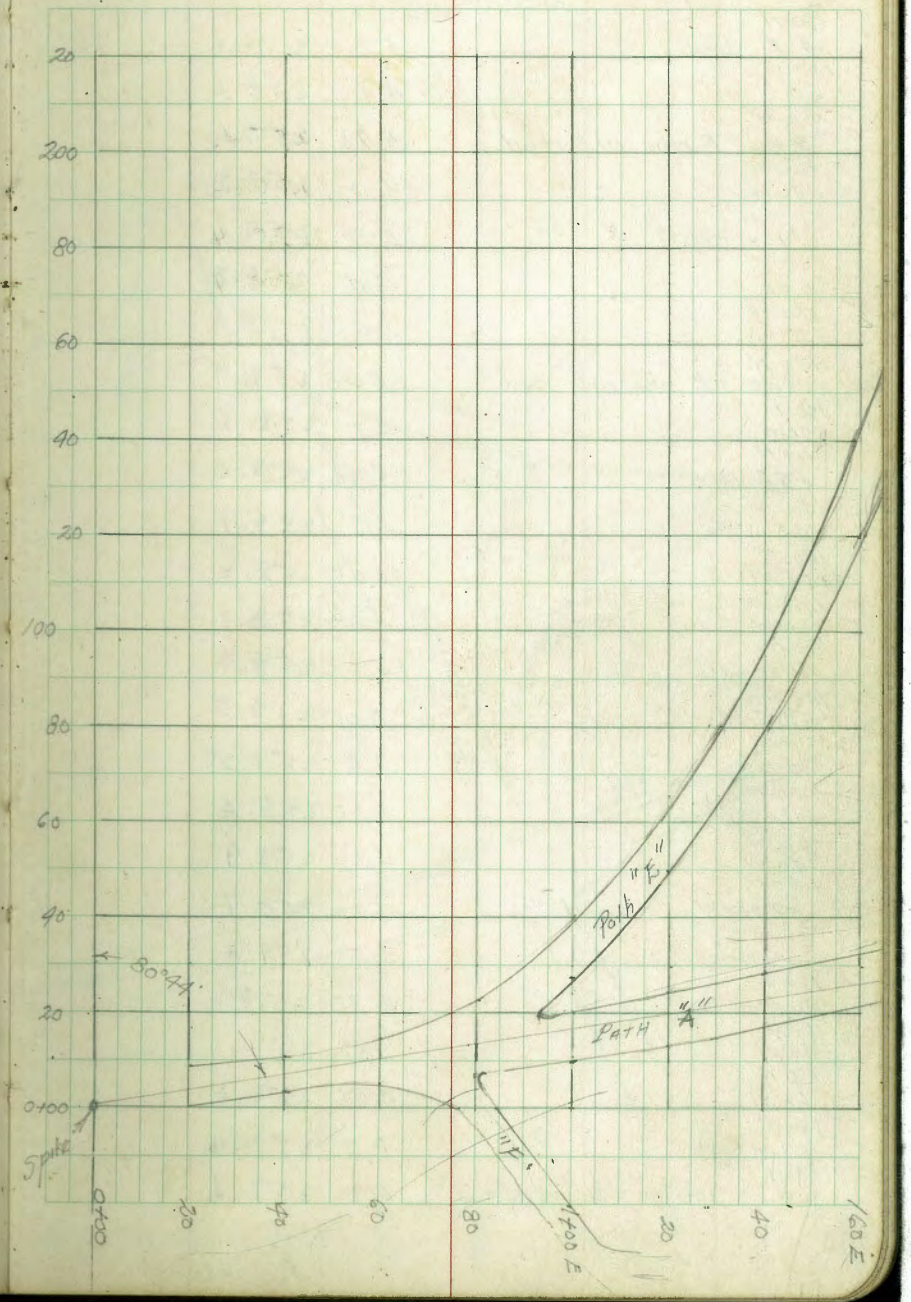
Indexed
c.s.k.

For "Rose Garden"
North of Bowling Green at N.W. Cor
of 7th And Laurel



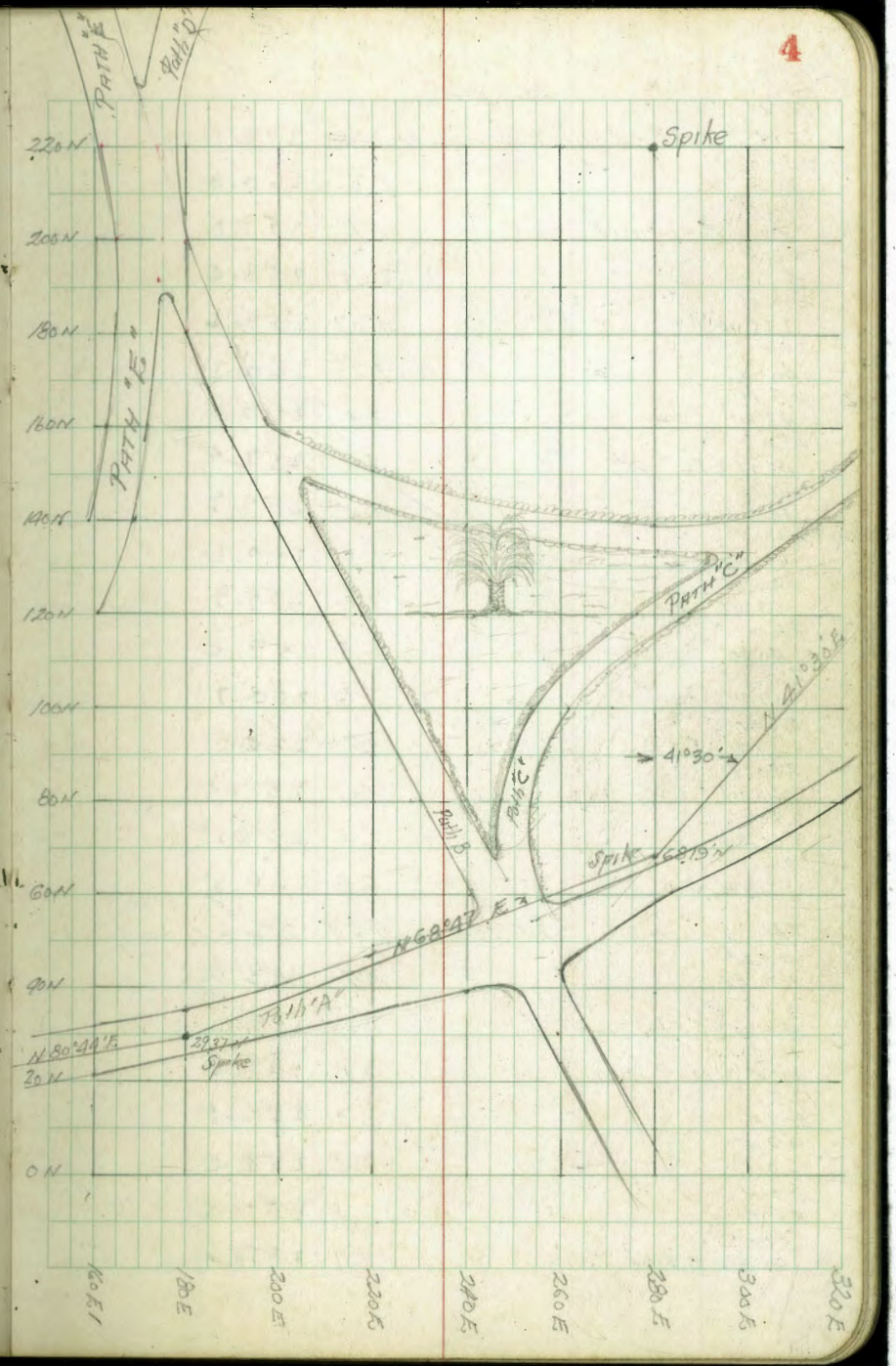


	6.77	262.25		255.48	SYM. BP. Maple 6" ⌀ on spike
TP	7.29	263.34	6.20	256.05	0+00
0+00 N 19.5 W	= W edge of road.		7.91	255.43	
0+00 N 16 E.	= E. " " "		7.96	255.38	
0+00 N 20 E.	= S edge Trail		7.4	255.9	
2 S 20 E.			7.9	255.4	
15 S 20 E.			7.0	256.3	
9 N 20 E.	= N edge Trail		7.3	256.0	
10 N 20 E.			6.5	256.8	
20 N 00 E.			6.7	256.6	
20 N 21.5 W	= W edge of road.		7.5	255.8	
20 N 13 E.	= E. " " "		7.5	255.8	
40 N 00	" "		6.3	256.6	
40 N 25 W	= W " " "		6.9	256.4	
40 N 10.5 E.	= E " " "		7.0	256.3	
40 N 12 E.			6.2	257.1	
60 N 00 E.			5.9	257.4	
60 N 20 W			6.0	257.3	
60 N 29 W	= W edge of road.		6.4	256.9	
60 N 6.5 E.	= E. " " "		6.6	256.7	
60 N 8 E.			5.6	257.7	
80 N 00			5.8	257.5	
80 N 20 W			5.5	257.8	
80 N 34 W	= W " " "		6.1	257.2	
80 N 2 E.	= E. " " "		6.2	257.1	

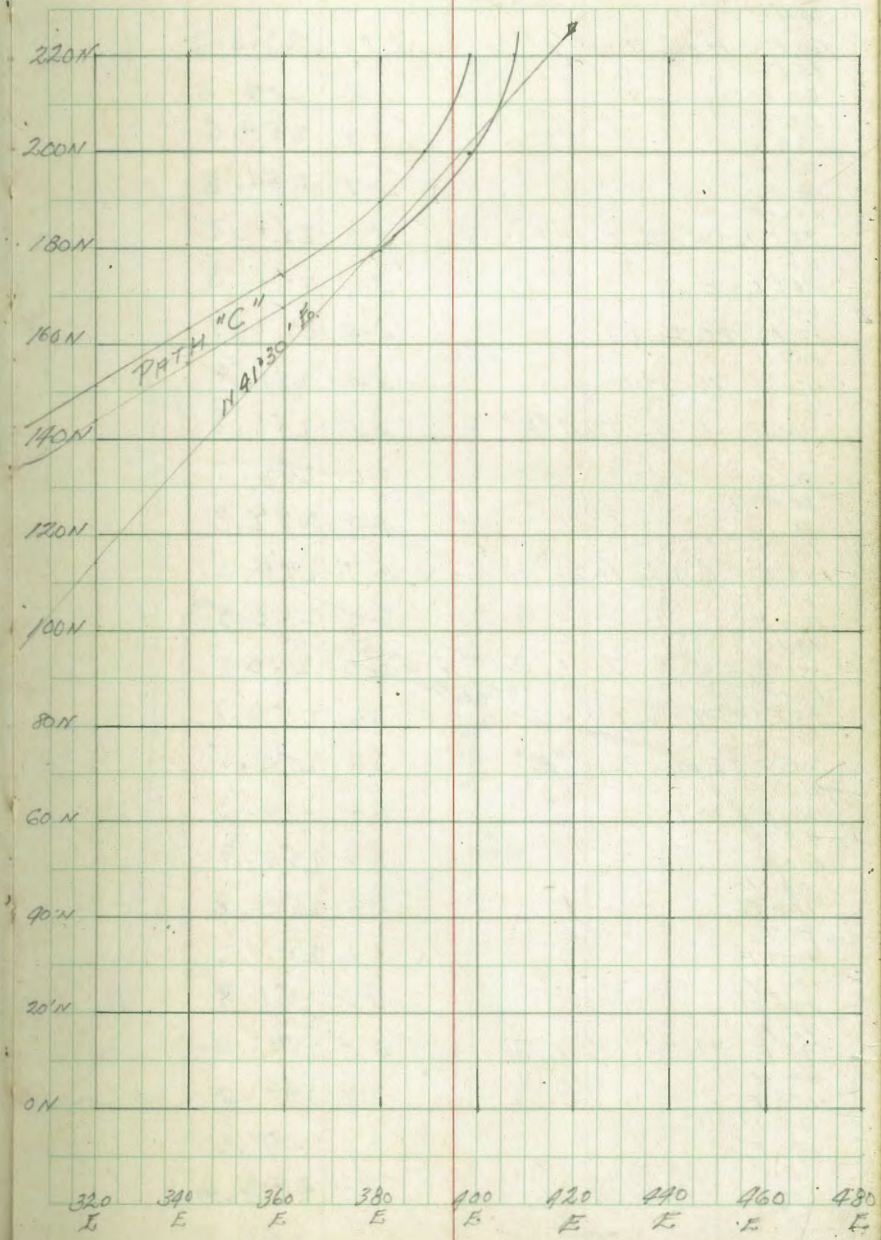


2.63.34

80 N 4 E.		52	258.1
100 N 00		4.7	258.6
100 N 3 W = E. edge of road.		5.75	257.6
100 N 20 W	" "	5.0	258.3
100 N 39 W = W " " "		5.7	257.6
120 N 00		4.4	258.9
120 N 7 W		4.4	258.9
120 N 9 W = E. edge of road		5.40	257.9
120 N 20 W		4.71	258.6
120 N 45.5 W = W " " "		5.34	258.0
140 N 13.5 W		4.2	259.1
140 N 15.5 W = E " " "		5.05	258.3
140 N 30 W	" "	4.60	258.7
140 N 40 W		4.57	258.7
140 N 52.5 W = W " " "		5.00	258.3
160 N 20 W		3.8	259.5
160 N 22 W = E. " " "		4.65	258.6
160 N 40 W	" "	4.15	259.9
160 N 59 W = W " " "		4.60	258.7
180 N 28.5 W		3.5	259.8
180 N 30.5 W = E. " " "		4.30	259.0
180 N 40 W	" "	3.81	259.5
180 N 60 W		4.07	259.2
180 N 67 W = W " " "		4.3	259.0
189 N 31 W = Int. Trail & Road = S edge Trail "E"		4.0	259.3

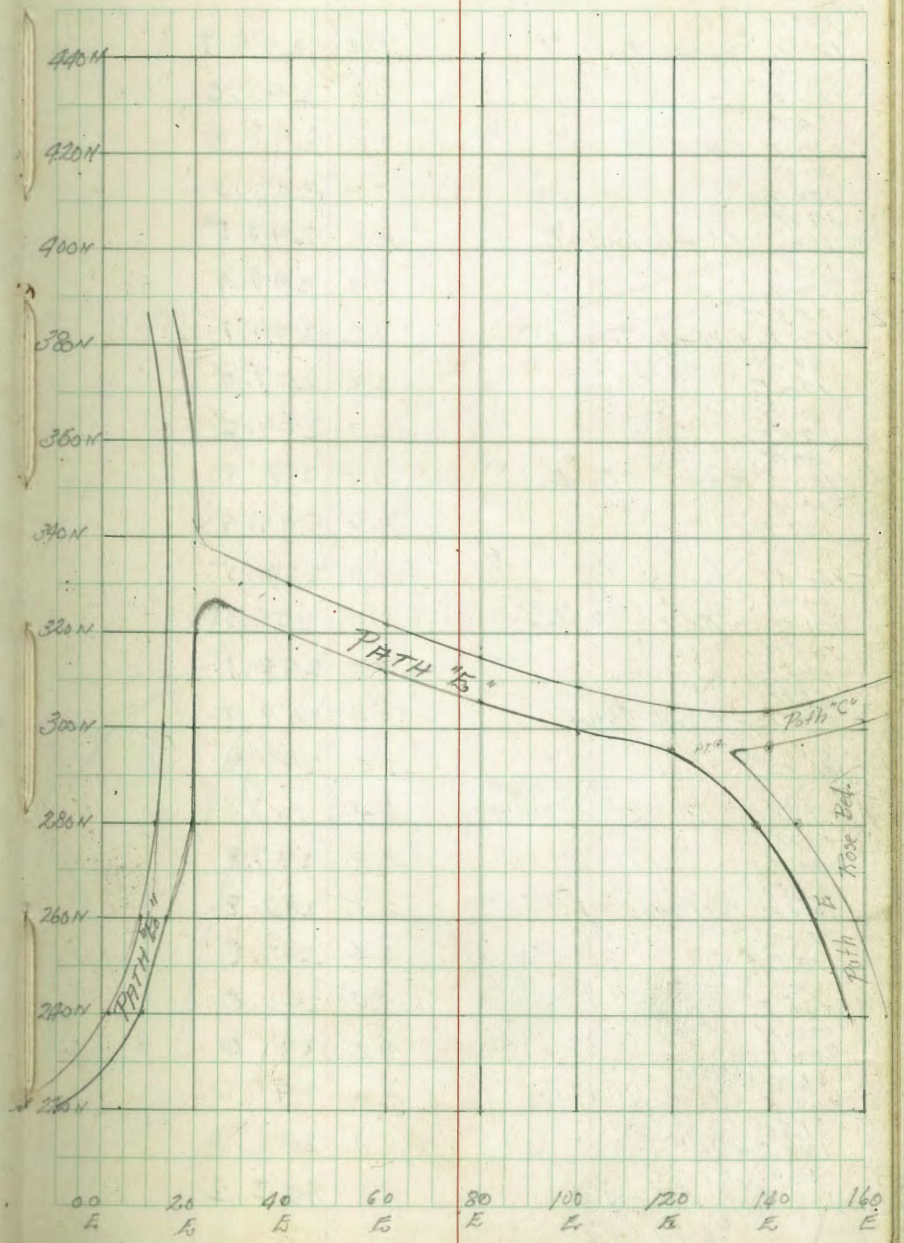


		263.34			
192 N			4.2		
35 W = foot Trail with road = N edge Trail 'E'				259.1	
200 N					
35 W			3.3	260.0	
200 N					
37 W = E edge Oil road.			4.1	259.2	
200 N					
60 W	"	"	3.65	259.6	
200 N					
735 W = W "	"	"	4.07	259.2	
220 N					
40 W			3.2	260.1	
220 N					
43 W			3.3	260.0	
220 N					
45 W = E "	"	"	3.9	259.4	
240 N					
46 W			3.6	259.7	
240 N					
51 W			3.1	260.2	
240 N					
53 W = "	"	"	3.4	259.9	
260 N					
40 W			4.3	259.0	
260 N					
59 W			2.6	260.7	
260 N					
61 W = E "	"	"	3.20	260.1	
280 N					
40 W			6.0	257.3	
280 N					
66 W			2.4	260.9	
280 N					
68 W = E "	"	"	2.8	260.5	
TP	027	256.32	7.29	256.05	0+00 on spike
00 N					
40 E			0.5	255.8	
3' N					
40 E = S edge Trail			1.1	255.2	
10.5 N					
40 E = N "	"		1.1	255.2	
12.5 N					
40 E			0.2	256.1	
00 N					
60 E			2.3	254.0	
3.5 N					
60 E			2.3	254.0	
5' N					
60 E = S edge Trail			2.9	253.4	

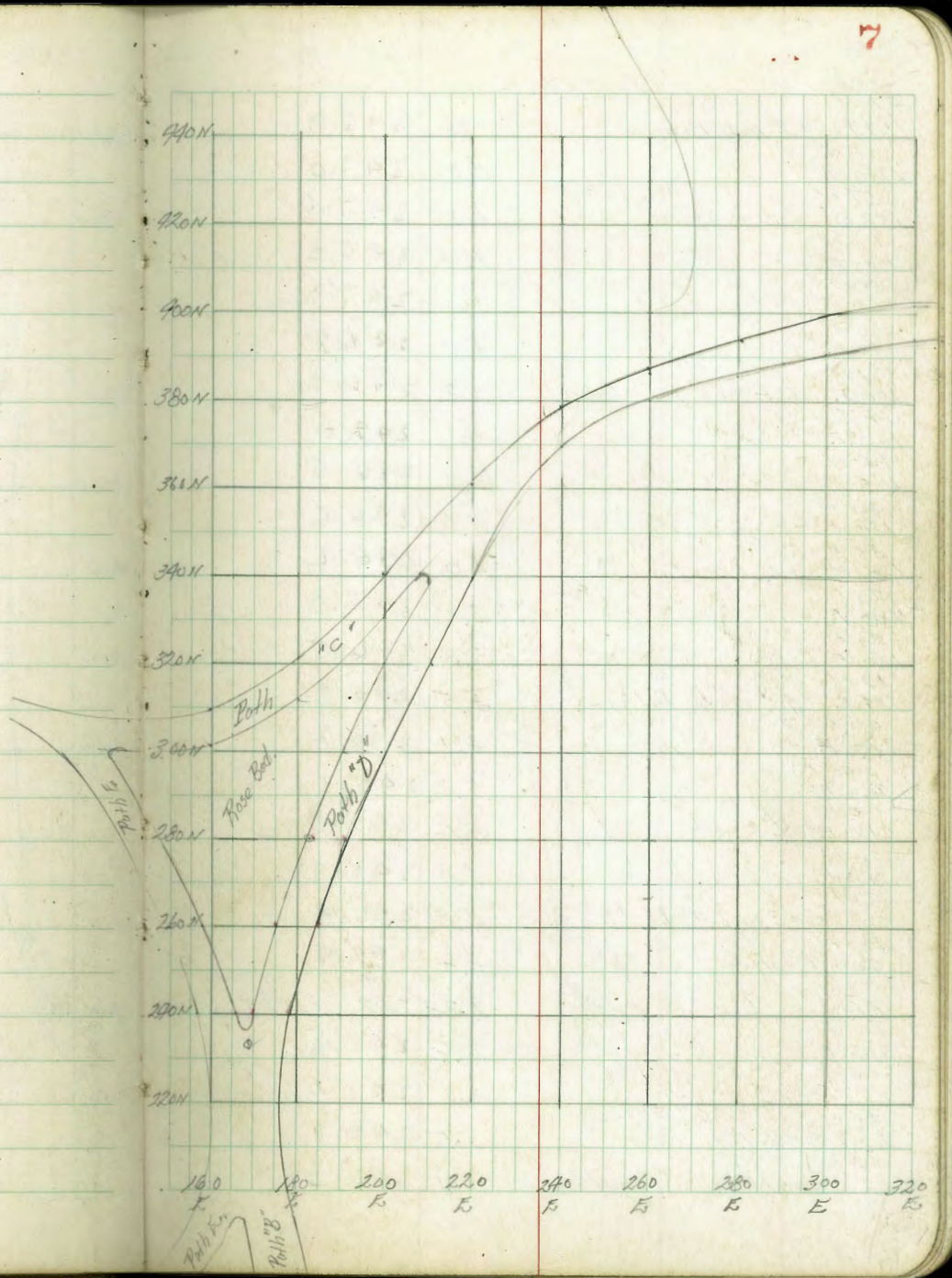


256.32

14 N 60 E. = N edge Trail "A"	2.7	252.6
15.5 N 60 E.	1.7	254.6
20 N 60 E.	1.7	254.6
00 N 80 E.	4.7	251.6
00 N 76.5 E. = N edge Trail "F"	4.6	251.7
00 N 84.5 E. = E. " " "	5.0	251.3
6.5 N 80 E. = P.I. Trails.	4.4	251.9
20 N 80 E. = no trail	4.4	251.9
23 N 80 E. = N edge Trail "E"	4.5	251.8
25 N 80 E.	3.6	252.7
40 N 80 E.	4.0	252.3
13 S 103 E. = E. Date Palm	5.7	250.6
00 N 100 E.	6.0	250.3
10 N 100 E. = S edge Trail "A" "A" & "E"	6.0	250.3
19 N 93 E. = P.I. Trail (N + E. edge)	5.6	250.7
27 N 100 E. = E edge Trail "E"	5.8	250.5
40 N 100 E. = N " " "	6.0	250.3
43 N 100 E.	5.4	250.9
60 N 100 E.	5.5	250.8
80 N 100 E.	5.1	251.2
100 N 100 E.	4.5	251.8
94 N 99 E. = 16" dia Fire Tree	4.3	252.0
00 N 120 E.	7.3	249.0
00 N 140 E.	8.7	247.6
8 N. 3 dia 133 E. = Date Palm.	7.7	248.6
2 South 30" dia 147 E. = Date Palm	8.7	247.6

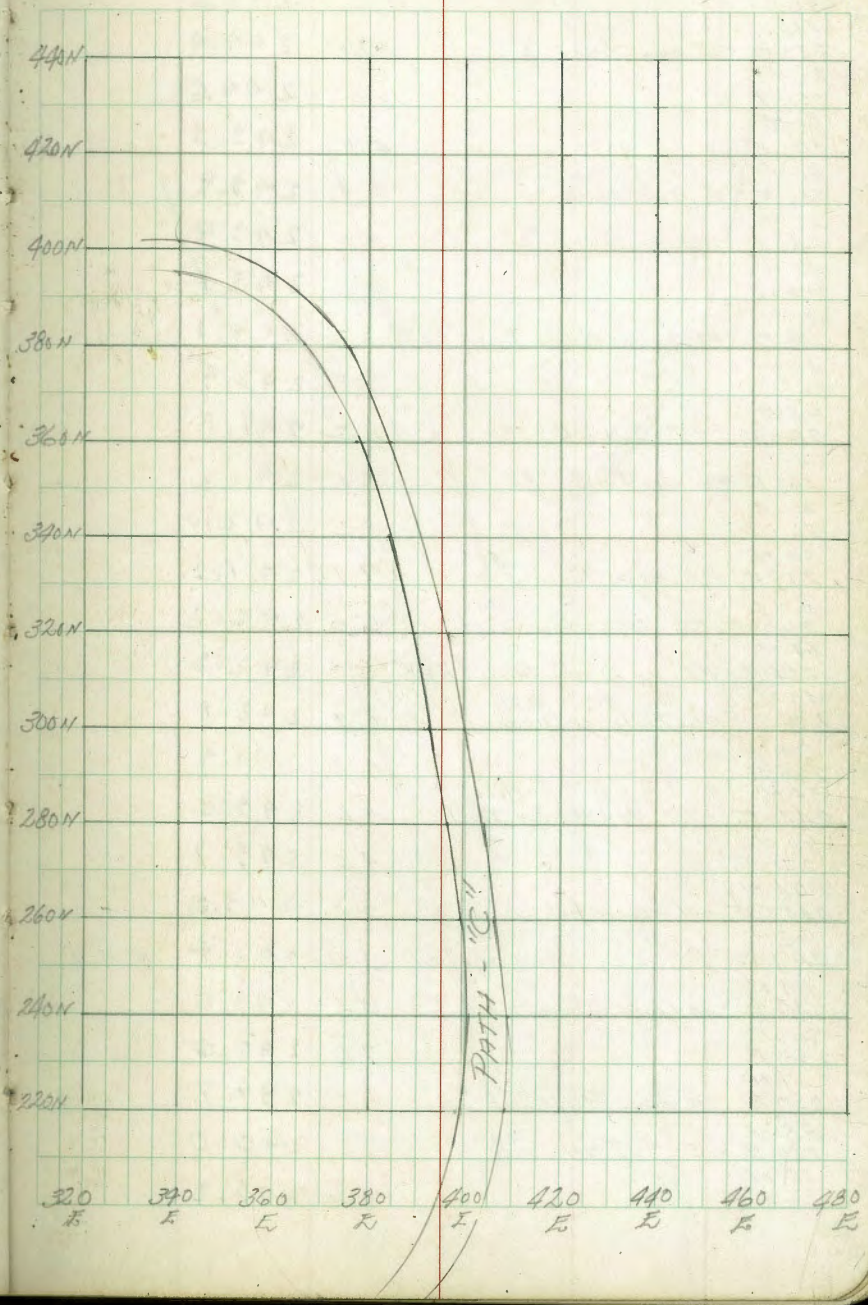


		256.32		
13 N				
120 E = S edge Trail "A"			7.4	248.9
20 N				
120 E			7.3	249.0
24 N				
120 E = N " " "			7.5	248.8
40 N				
120 E			7.0	249.3
49 N				
120 E = S edge Trail "E"			6.8	249.5
60 N				
120 E			6.9	249.4
655 N				
120 E = N edge Trail "E"			7.2	249.1
67 N				
120 E			6.6	249.7
80 N				
120 E			6.7	249.6
80 N				
130 S E = N " " "E"			7.5	248.8
80 N				
129 E			6.9	249.4
80 N				
146 E			7.8	258.5
80 N				
141 E = E " " "E"			7.8	258.5
60 N				
140 E			8.2	248.1
41 N				
138 E = 2 Date Palms			8.4	247.9
20 N				
140 E			8.4	247.9
TP	2.35	250.27	8.40	247.92
40 N				
140 E			2.3	247.9
27.5 N				
140 E = N edge Trail "A"			2.5	247.7
17 N				
140 E = S " " "A"			2.4	247.8
00 N				
160 E			3.4	246.8
20 N				
160 E			3.2	247.0
21 N				
160 E = S " " "A"			3.2	247.0
31.5 N				
160 E = N " " "A"			3.4	246.8
40 N				
160 E			3.0	247.2



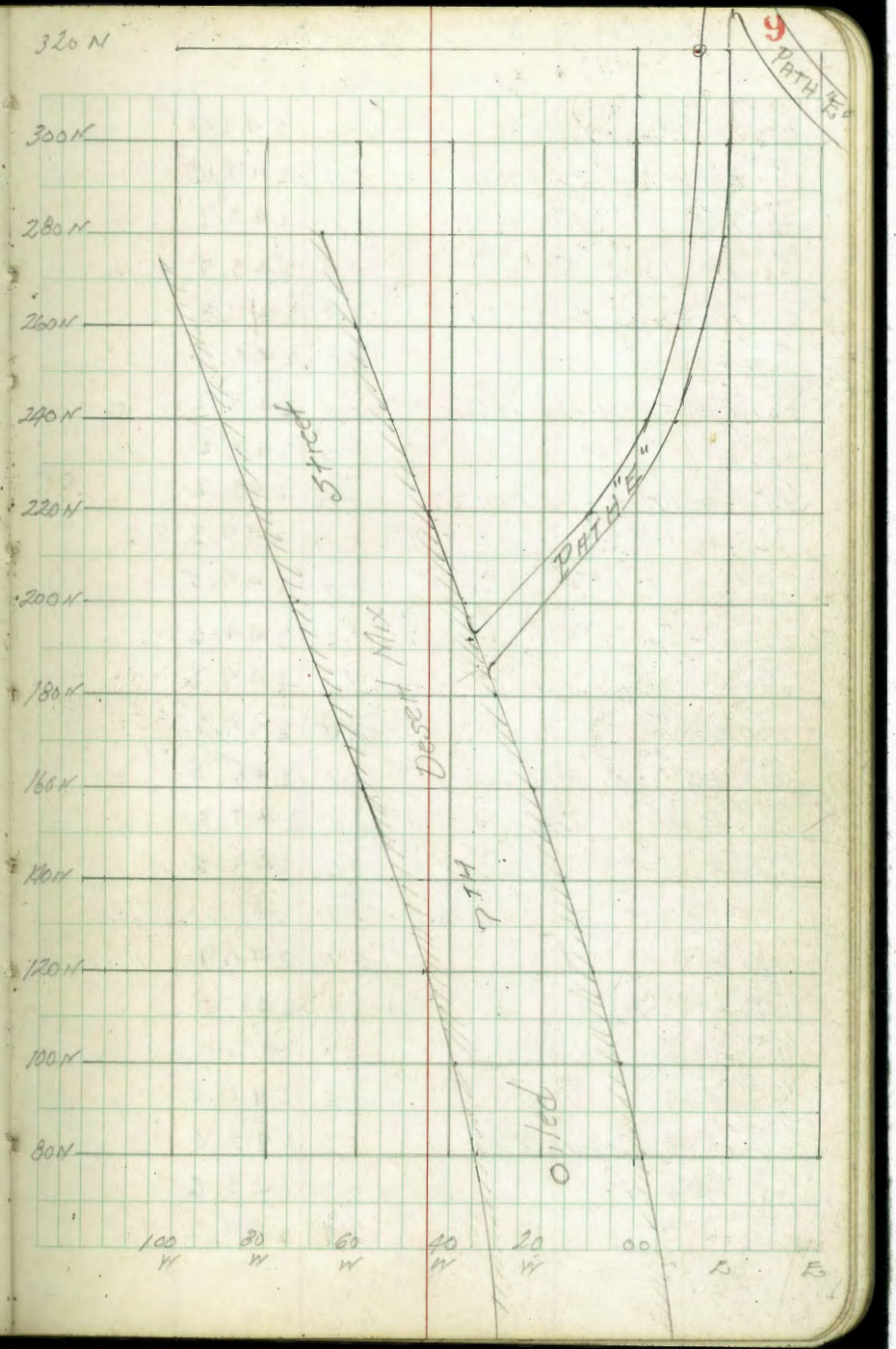
2.50.27

47 N 167 E.	3' dia. = L Date Palm	3.4	246.8	
60 N 160 E		3.2	247.0	
57 N 158 E.	16" dia. 30 high = L Date Palm	3.2	247.0	
60 N 180 E.		3.9	246.3	
80 N 160 E.		3.0	247.2	
80 N 180 E.		3.5	246.7	
71 N 180 E.	= L 28" dia Date Palm.	3.3	246.9	
14 S 160 E.	= L 30" " " "	3.2	247.0	
44 N 185 E.	= L 3' " " "	3.6	246.6	
40 N 180 E.		3.6	246.6	
35.5 N 180 E	= N. edge Trail "A"	4.0	246.2	
25 N 180 E.	= S. " " "A"	3.9	246.3	
20 N 180 E		3.8	246.5	
13 N 184 E.	= 36" date Palm	3.5	246.8	
00 N 180 E.		4.1	246.2	
00 N 200 E		5.2	245.0	
00 N 218 E.	= L 30" date Palm	5.4	244.8	
20 N 200 E.		4.8	245.4	
29 N 200 E.	= S edge Trail "A"	4.8	245.4	
40 N 200 E	N " " "A" ✓	4.8	245.4	
TP	5 17 248.16	7.28	242.99	on Spike 52.65 N 240 E.
60 N 200 E.		2.6	245.6	
60 N 220 E.		3.3	245.0	
54 N 226 E.	36" dia. = L Date Palm	3.5	244.7	
47 N 220 E.	= N. edge Trail "A"	3.9	245.3	



24816

40 N 220 E.		3.6	244.6
33.5 N 220 E.	= S. edge Trail "A"	3.8	244.4
20 N 220 E.		3.6	244.6
20 N 240 E.		4.9	243.3
41 N 236 E.	36" dia. = E. Date Palm	4.3	243.9
38 N 240 E.	= Sedge Trail "A"	4.8	243.4
40 N 240 E.		5.1	243.1
40 N 240 E.	= P.I. South + W. edge Trails "A+B"	5.7	243.1
40 N 260 E.		6.3	241.9
47 N 260 E.	= P.I. South + E. " "	6.4	241.8
24 N 260 E.	= W edge Trail "B"	6.6	241.6
20 N 260 E.		6.2	242.0
20 N 273 E.	= E. edge Trail "B"	7.1	241.1
00 N 260 E.	= S. 30" date Palm	6.0	242.2
54 N 254 E.	= P.I. N + E. edge Trails "A+B"	6.0	242.2
58 N 256 E.	"C" Path = edge Trails on Curve.	6.1	242.1
60 N 240 E.		6.3	241.9
54 N 244 E.	("A + B" Paths.) = P.I. W & N edge Trails	5.2	243.0
60 N 240 E.		4.5	243.7
60 N 240.5 E.	= W edge Trail "B"	5.2	243.0
63 N 247 E.	Triangle "B"+"C" = P.I. ELY + WLY edge Trail	5.4	242.8 4' Ext.
64 N 245 E.	= on Curve Above Trail "C"	5.2	243.0
80 N 280 E.		7.6	240.6
67 N 280 E.	= N. edge Trail "A"	8.5	239.7
58 N 280 E.	= S. " Trail "A"	8.2	240.0
80 N 260 E.		6.0	242.2



80 N 253 E = E edge Path "C"	5.5	242.7	
80 N 247 E = W " " "	5.4	242.8	
80 N 245 E	4.5	243.7	
80 N 240 E	4.3	243.9	
80 N 238 E = E edge Path "B"	4.8	243.4	
80 N 230 E = W " " "B"	4.5	243.7	
100 N 261.5 E = SLY edge Path "C"	5.0	243.2	
100 N 260 E	5.0	243.2	
100 N 253.5 E = NLY edge Path "C"	5.0	243.2	
100 N 251 E	3.9	244.3	
100 N 240 E	3.7	244.5	
100 N 229 E	3.6	244.6	
100 N 227 E = E Edge Path "B"	4.0	244.2	
100 N 219 E = W " " "	3.7	244.5	
100 217 E	3.1	245.0	
80 N 200 E	2.4	245.8	
80 N 220 E	3.6	244.6	
T.P. 565. 248.80	5.01	243.15	Oil Rock 100 N 255 E.
100 N 280 E	6.9	241.9	
120 N 320 E	7.3	241.5	
120 N 300 E	5.7	243.1	
100 N 300 E	8.8	240.0	
120 N 287 E = S edge Path "C"	5.2	243.6	
120 N 276 E = W " " "	5.2	243.6	
120 N 273 E	4.2	244.2	

120 N 260 E	4.0	244.8
121 N 246 E = S 30" Date Palm	3.7	245.1
120 N 240 E	3.7	245.1
120 N 218.5 E	3.3	245.5
120 N 217.5 E = E edge Path "B"	3.7	245.1
120 N 209 E = W " " "	3.5	245.3
120 N 207 E	2.7	246.1
120 N 200 E	2.5	246.3
100 N 200 E	2.8	246.0
105 N 211 E = S 30" Date Palm.	3.3	245.5
124 N 193 E = S 28" " "	2.1	246.7
120 N 180 E	2.0	246.8
100 N 180 E	2.0	246.8
140 N 199 E = W edge Path "B"	2.6	246.2
140 N 197 E	2.1	246.7
140 N 206.5 E = E " " "	2.9	245.9
140 N 207 E	2.6	246.2
140 N 220 E	3.0	245.8
142.5 N 220 E	2.8	246.0
143.5 N 220 E = S edge Path Triangle	3.3	245.5
151 N 220 E = N " "	3.1	245.6
152 N 220 E	2.8	246.0
160 N 220 E	2.6	246.2
150 N 202 E = P.T. E edge Path B + Triangle	2.5	246.3 3' Ext.
160 N 200 E	2.2	246.6

			248.80		
159 N					
200 E.	= E edge Path "B"	2.7	246.1		
160 N					
197.5 E.	= P.I. E + N-Ly edge Path.	2.7	246.1	1.5' Ext.	
160 N					
180 E.		1.2	247.6		
149 N	30" dia.				
180 E.	= ℄ Date Palm.	1.1	247.7		
160 N					
186 E.		1.4	247.4		
160 N					
168 E.	= W edge Path "B"	2.1	246.7		
138 N					
240 E.	= S edge Path Triangle	3.6	245.2		
137 N					
240 E.		3.2	245.6		
145.5 N					
240 E.	= N " " "	3.5	245.3		
146 N					
240 E.		3.0	245.8		
180 N					
240 E.		3.0	245.8		
180 N					
240 E.		2.7	246.1		
180 N					
260 E.		2.0	246.8		
160 N					
260 E.		2.7	246.1	✓	
142 N					
260 E.		3.3	245.5		
141.5 N					
260 E.	= N edge Path.	3.9	244.9		
134.5 N					
260 E.	= S " " Triangle	4.0	244.8		
135 N					
260 E.		3.7	245.1		
133.0 N					
280 E.		4.1	244.7		
133.5 N					
280 E.	= S edge Path Triangle	4.4	244.4		
139 N					
280 E.	= N " "	4.3	244.5	△ in Path N edge.	
141 N					
280 E.		3.5	245.3		
133.5 N					
296 E.	= P.I. edge Path "C"	4.8	244.0	6.5' Ext	
160 N					
280 E.		2.5	246.3		
180 N					
280 E.		1.7	247.1		

			248.80		
200 N					
280 E.		1.2	247.6		
200 N					
260 E.		1.4	247.4		
220 N					
260 E.		1.1	247.7		
220 N					
280 E.	on Spike	.078	248.02		
220 N					
300 E.		1.1	247.7		
200 N					
300 E.		1.4	247.2		
180 N					
300 E.		2.3	246.5		
160 N					
300 E.		2.8	246.0		
143 N					
300 E.		3.8	245.0		
141.5 N					
300 E.	= N edge Path "C"	4.6	244.2		
130 N					
300 E.	= S " " "	5.0	243.8		
140 N					
320 E.		4.7	244.1		
144 N					
320 E.	= S edge " "	4.6	244.2		
151.5 N					
320 E.	= N " " "	4.4	244.4		
158 N					
340 E.		3.6	245.2		
160 N					
320 E.		3.4	245.4		
180 N					
320 E.		2.7	246.1		
200 N					
320 E.		2.1	246.7		
220 N					
320 E.		1.4	247.4		
220 N					
340 E.		1.6	247.2		
240 N					
340 E.		1.1	247.7		
240 N					
320 E.		1.1	247.7		
240 N					
300 E.		0.6	248.2		
240 N					
340 E.		2.5	246.3		
180 N					
340 E.		3.1	245.7		

	248.80		
165.5 N		3.6	245.2
340 E.			
163.5 N		1.4	244.4
340 E. = N edge Path "C"			
156 N		4.4	244.4
340 E. = " " "			
140 N		6.5	242.3
340 E.			
140 N		8.1	240.7
360 E.			
160 N		5.2	243.6
360 E.			
167 N		4.3	244.5
360 E. = S edge Path "C"			
174.5 N		4.3	244.5
360 E. = N " " "			
176 N		3.7	245.1
360 E.			
180 N		3.5	245.3
360 E.			
200 N		2.5	246.3
360 E.			
220 N		1.7	247.1
360 E.			
240 N		1.3	247.5
360 E.			
240 N		1.5	247.3
380 E.			
220 N		1.7	247.1
380 E.			
200 N		2.6	246.2
380 E.			
191.5 N		2.9	245.9
380 E.			
189.5 N		3.7	245.1
380 E. = N edge Path "C"			
180 N		3.9	244.9
380 E. = S " " "			
179 N		3.5	245.3
380 E			
160 N		6.4	242.4
380 E.			
150 N		4.3	244.5 ✓
400 E.			
TP	541	310	245.70
183 N	251.11	58	245.3
390 E. = ∅ 12" Oak Tree.			
184 N		6.6	244.5
407 E. = ∅ 12" "			

Off Rock 195 N 390 E

251.11		
198 N		
403 E. = ∅ 14" oak Tree	4.4	246.7
200 N		
398.5 E. = SW edge Path "C"	4.6	246.5
206 N		
417.5 E. = ∅ 10" Oak Tree	4.9	246.2
200 N		
389.5 E. = WSW edge Path "C"	5.2	245.9
200 N		
388 E.	4.7	246.4
200 N		
420 E.	6.0	245.1
220 N		
420 E.	5.3	245.8
240 N		
420 E.	5.3	245.8
233 N		
418 E. = 10" Oak Tree	5.1	246.0
219 N		
427 E. = 10 " "	5.7	245.2
232 N		
430 E. = 10 " "	6.8	244.3
243 N		
427 E. = 12" " "	6.5	244.6
220 N		
399 E. = WSW edge Path "C"	4.3	246.8
220 N		
408 E. = ESE " " "	4.3	246.8
220 N		
400 E.	4.0	247.1
240 N		
401 E. = WSW " " "	4.5	246.6
240 N		
409.5 E. = E " " "	4.6	246.5
246 N		
413 E. = ∅ 12" oak Tree	4.4	246.7
260 N		
399 E. = N edge Path "C"	4.8	246.3
260 N		
395 E.	4.3	246.8
260 N		
406.5 E. = E " " "	4.8	246.3
260 N		
420 E.	6.8	244.3
260 N		
430 E.	8.6	242.5
209 N		
422 E. = 8" Oak Tree	7.0	244.1
267 N		
410 E. = 20" " "	4.6	246.5
260 N		
380 E.	3.8	247.3

		251.11			
260 N 360 E.			3.2	247.9	
280 N 380 E.			3.7	247.4	
TP	3.38	249.53	4.96	246.15	on Rock 282 N 400 E.
260 N 340 E.			1.3	248.2	
260 N 320 E.			1.4	248.1	
260 N 300 E.			1.1	248.4	
280 N 300 E.			0.7	248.8	
300 N 300 E.			0.6	248.9	
320 N 300 E.			0.8	248.7	
340 N 300 E.			1.1	248.4	
360 N 300 E.			1.6	247.9	
380 N 300 E.			2.2	247.3	
398 N 300 E.			2.2	247.3	
391 N 300 E.	= S. edge Path "C"		2.7	246.8	
398 N 300 E.	= N " " "		2.8	246.7	
414 N 300 E.			5.3	244.2	
420 N 300 E.	= Rim Canyon		8.3	241.2	
420 N 320 E.	= " "		5.7	243.6	
407 N 326 E.	= ℄ 22" dia Redwood		2.5	247.0	
405 N 320 E.			2.5	247.0	
401.5 N 320 E.	= N edge Path "C"		2.8	246.7	
394 N 320 E.	= S " " "		2.8	246.7	
393 N 320 E.			2.2	247.3	
381 N 320 E.			1.9	247.6	
360 N 320 E.			1.3	248.2	

	249.53		
340 N 320 E.		1.1	248.4
320 N 320 E.		1.0	248.5
300 N 320 E.		0.9	248.6
280 N 320 E.		1.1	248.4
280 N 340 E.		1.1	248.4
300 N 340 E.		1.0	248.5
320 N 340 E.		1.0	248.5
340 N 340 E.		1.0	248.5
360 N 340 E.		1.4	248.1
380 N 340 E.		1.9	247.6
398 N 340 E.		2.2	247.3
394.5 N 340 E.	= S. edge Path "C"	2.8	246.7
401.5 N 340 E.	= N " " "	2.9	246.6
402 N 340 E.		2.6	246.9
406 N 350 E.	= ℄ 14" Redwood	3.6	245.9
420 N 340 E.		5.6	243.9
420 N 352 E.	= ℄ 14" "	5.4	244.1
415 N 362 E.	= ℄ 14 "	5.2	244.3
420 N 360 E.		5.8	243.7
410 N 360 E.		3.0	246.5
395 N 360 E.	= N edge Path "C"	3.4	246.1
387 N 360 E.	= S " " "	3.1	246.4
386 N 360 E.		2.4	247.1
380 N 360 E.		2.3	247.2
360 N 360 E.		1.9	247.6

340N 360E.		1.4	248.1
320 N 360 E.		1.2	248.3
300 N 360 E.		1.4	248.1
280 N 360 E.		1.3	248.2
300 N 380 E.		2.2	247.3
320 N 380 E.		2.5	247.0
340 N 380 E		2.6	246.9
340 N 382.5 E.		2.7	246.8
340 N 384 E = W edge Path "C"		3.6	245.9
340 N 390.5 E = E " " "		3.6	245.9
360 N 376 E		2.6	246.9
360 N 377.5 E = W " " "		3.3	246.2
360 N 384 E = E " " "		3.3	246.2
380 N 380 E.		3.7	245.8
380 N 375.5 E = E " "		3.2	246.3
380 N 366 E =		2.5	247.0
380 N 367 E = W " " "		3.1	246.4
400 N 380 E.		5.4	244.1
396 N 380 E = ℄ 14" Redwood.		5.0	244.5
400 N 391 E = ℄ 12" "		6.8	242.7
384 N 388 E = ℄ 14" "		5.3	244.2
374 N 384 E = ℄ 12" "		3.8	245.7
380 N 400 E.		8.1	241.4
382 N 401 E = Dble 10" Redwood		8.1	241.4
367 N 400 D = ℄ 12" "		6.8	242.7

360N 400E.	5.6	243.9
364 N 411 E. = 16" Redwood.	8.9	240.6
358.5 N 400 E = ℄ 12" "	5.4	244.1
363 N 390 E = ℄ 20" "	3.3	246.2
351 N 412 E = ℄ 14" "	8.2	241.3
340 N 400 E	4.9	244.6
340 N 398 E = ℄ Dble 14" Redwood	4.3	245.2
342 N 420 E	9.7	239.8
336 N 420 E = ℄ 12" "	9.6	239.9
340 N 400 E	4.0	245.5
320 N 396.5 E = E edge Path "C"	3.7	245.8
320 N 389.5 E = W " " "	3.6	245.9
340 N 388 E	2.9	246.6
324 N 401 E = ℄ 12" Redwood.	4.6	244.9
328 N 414 E = ℄ 12" "	7.5	242.0
321 N 418 E = ℄ 16" "	8.7	240.8
320 N 420 E.	9.3	240.2
310 N 420 E = ℄ 14" "	8.7	240.8
300 N 420 E.	8.3	241.2
296 N 425 E = ℄ 20" "	9.2	240.3
282 N 426 E = ℄ 10" Oak Tree	8.4	241.1
290 N 430 E.	8.8	240.7
280 N 420 E.	7.7	241.8
287 N 410 E = ℄ 18" " "	5.0	244.5
280 N 403.5 E. = E edge Path "C"	3.4	246.1
280 N 396.5 E = W " " "	3.3	246.2

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280 N 395 E.			2.7	246.6	
300 N 400 E. = E edge Path "C"			3.6	245.9	
300 N 392.5 E. = N " " "			3.5	246.0	
300 N 391 E			2.8	246.7	
T.P.	4.29	250.94	2.88	246.65	Nail 400 N 340 E.
416 N 280 E. = Rim Canyon			7.2	243.7	
400 N 280 E.			4.7	246.2	
395 N 280 E. = N edge Path "C"			3.9	247.0	
386 N 280 E. = S " " "			3.8	247.1	
385 N 280 E.			3.3	247.6	
380 N 280 E.			3.3	247.6	
360 N 280 E.			2.7	248.1	
340 N 280 E			2.4	248.5	
320 N 280 E.			2.1	248.8	
300 N 280 E.			2.1	248.8	
280 N 280 E.			2.2	248.7	
260 N 280 E.			2.4	248.5	
240 N 280 E.			2.7	248.2	
340 N 260 E			2.3	248.6	
360 N 260 E			2.6	248.3	
378 N 260 E.			3.1	247.8	
380 N 260 E. = S edge Path "C"			3.5	247.4	
387 N 260 E. = N " " "			3.5	247.4	
400 N 260 E.			5.3	245.6	
408 N 260 E. = Rim Canyon			6.6	244.3	
396 N 240 E. = " "			5.5	245.4	

250.94

380 N 240 E.		3.2		247.7
378 N 240 E. = N edge Path "C"		3.3		247.6
369.5 N 240 E. = S " " "		3.3		247.6
368 N 240 E.		2.8		248.1
392 N 220 E		6.4		244.5
380 N 220 E.		4.7		246.2
362 N 220 E. = N edge Path "C"		3.7		247.2
372 N 200 E. = Rim Canyon.		6.1		244.8
360 N 200 E.		5.2		245.7
341 N 200 E. = N edge Path "C"		4.3		246.6
T.P. 404	251.28	370	247.24	350 N 216 E. on Rock
360 N 240 E.		3.1		248.1
340 N 240 E.		2.8		248.4
320 N 260 E.		2.5		248.7
300 N 260 E.		2.4		248.8
280 N 260 E.		2.8		248.4
260 N 260 E.		2.9		248.3
240 N 260 E.		3.2		248.0
220 N 240 E.		4.4		246.8
240 N 240 E.		3.9		247.3
260 N 240 E.		3.8		247.4
280 N 240 E.		3.5		247.7
300 N 240 E.		3.2		248.0
300 N 240 E.		3.1		248.1
		3.0		248.2

331.5 N = S edge Path "C"				
200 E.		4.6	246.6	
329 N				
200 E. in triangular Rose Bed		3.8	247.4	
354.5 N				
220 E = P.I. NELY " "		3.9	247.3	17.5 Est
339 N				
220 E. = Path "D" ELY edge		4.0	247.2	
336 N				
220 E.		3.4	247.8	
320 N				
220 E.		3.6	247.6	
300 N				
220 E.		3.5	247.7	
280 N				
220 E.		4.1	247.1	
260 N				
220 E.		4.1	247.1	
240 N				
220 E.		4.1	247.1	
220 N				
220 E.		4.1	247.1	
200 N				
220 E.		4.3	246.9	
180 N				
220 E.		4.9	246.3	
180 N				
200 E.		4.3	246.9	
200 N				
200 E.		4.3	246.9	
220 N				
200 E.		4.3	246.9	
240 N				
200 E.		4.3	246.9	
260 N				
200 E.		4.3	247.9	
280 N				
200 E.		4.1	247.1	
300 N				
201 E. = ELY edge Path "D"		4.1	247.1	
300 N				
191 E. = WLY " " "		4.3	246.9	
320 N				
200 E. = " " " "		4.2	247.0	
348 N				30" dia
252 E. = 6 Young Date Palm.		2.8	248.4	4' High Trunk
340 N				
180 E. = Rim Canyon.		7.2	244.0	
326 N				
173 E. = 24" Oak Tree.		5.6	245.6	

324 N			
180 E.	4.6	246.6	
321.5 N			
180 E. = North edge Path "C"	4.9	246.3	
312 N			
180 E. = S " " "	5.0	246.2	
310 N			
180 E in triang. Rose Bed.	4.3	246.9	
300 N			
190 E. " " " "	4.3	246.9	
280 N			
180 E. " " " "	4.2	247.0	
280 N			
183 E. = WLY edge Path "D"	4.3	246.9	
280 N			
192 E = ELY " " "	4.2	247.0	
280 N			
193 E.	3.9	247.3	
260 N			
175.5 E. = WLY edge " "	4.3	246.9	
260 N			
185 E. = ELY " " "	4.2	247.0	
240 N			
170 E = WLY " " "	4.1	247.1	
240 N			
178 E = ELY " " "	4.2	247.0	
240 N			
180 E.	3.9	247.3	
220 N			
180 E.	3.9	247.3	
200 N			
180 E.	3.9	247.3	
199 N			
180 E = E edge Path "B"	4.1	247.1	
180 N			
186 E. = " " " "	4.4	246.8	
192 N			
174 E = P.I. W edge Path "B" East edge E	4.1	247.1	5' Est.
200 N			
165 E = WLY edge Path "E".	4.0	247.2	
200 N			
163 E.	3.5	247.7	
200 N			
160 E	3.5	247.7	
220 N			
160 E.	3.7	247.7	
220 N			
162 E = W " " "	4.0	247.2	
220 N			
171 E = E " " D	4.0	247.2	

251.28

233 N 168 E = PT. WLY edge Path "D" ELY edge Path "E"			4.1	247.1	SLY end Rose Bed 1.5 Ext
240 N 186.5 E = W edge Path "E"			4.3	246.9	
240 N 165.5 E = E " " "			4.3	246.9	
260 N 160 E.			4.3	246.9	
260 N 157.5 E. = E " " "			4.7	246.5	
260 N 149 E. = W " " "			4.6	246.6	
280 N 160 E	in triang Rose Bed.		4.6	246.6	
300 N 160 E.	" " " "		4.6	246.6	
302 N 160 E. = SLY edge Path "C"			5.2	246.0	
309.5 N 160 E = NLY " " "			5.1	246.1	
312 N 160 E.			4.8	246.4	
320 N 160 E.			6.1	245.1	
327 N 160 E = Rim Canyon.			8.2	243.0	
317 N 151 E = 8" 15" Oak Tree.			5.8	245.4	
320 N 140 E = Rim Canyon.			7.5	243.7	
303.5 N 140 E = NLY edge Path "C"			5.4	245.8	
297 N 140 E = SLY " " "			5.3	245.9	
296 N 140 E in Triang. Rose Bed.			4.9	246.3	
297 N 134.5 E = PT. E edge Path E. South edge Path "C"			5.4	245.8	1.5' Ext
280 N 146 E = E edge Path "E"			5.0	246.2	
280 N 137 E = W " " "			5.0	246.2	
260 N 140 E			3.9	247.2	
JP.	5.27	253.22	3.33	247.95	on Lath 220 N 180 E
180 N 160 E.			5.3	247.9	
180 N 163 E.			5.3	247.9	

253.22

180 N 164.5 E = W edge Path "E"	5.9	247.3	
180 N 172.5 E = E " " "	5.8	247.4	
160 N 160 E.	5.2	248.0	
160 N 161.5 E.	5.2	248.0	
160 N 162.5 E = W edge " "	5.7	247.5	
160 N 171.5 E = E " " "	5.6	247.6	
140 N 158.5 E = W " " "	5.5	247.7	
140 N 157.5 E.	5.0	248.2	
140 N 168 E = E " " "	5.5	247.7	
140 N 180 E.	6.2	247.0	
120 N 161.5 E = " " " "	5.3	247.9	
120 N 151.5 = W " " "	5.3	247.9	
120 N 151 E.	4.7	248.5	
100 N 160 E.	5.4	247.8	
100 N 152 E. = E " " "	5.0	248.2	
100 N 142 E = W " " "	4.9	248.3	
100 N 140 E.	4.3	248.9	
100 N 120 E.	3.2	250.0	
100 N 100 E.	1.3	251.9	
120 N 120 E	3.3	249.9	
120 N 140 E.	4.4	248.8	
140 N 140 E.	4.7	248.5	
120 N 120 E.	3.5	249.7	
140 N 100 E.	1.5	251.7	
160 N 100 E.	2.2	251.0	

253.22

160 N 120 E.			3.7	249.5	
160 N 140 E.			4.9	248.3	
T.P.	5.50	257.36	1.36	251.86	
T.P. Chk. on Spike	1.66	257.71	1.31	256.05	0+00 Spike P-3 No. 1 in Tree
T.P.	4.00	261.03	0.68	257.03	87 N 93 E.
20 N 20 E.			4.0	257.0	
20 N 40 E			4.5	256.5	
20 N 60 E			6.7	255.3	
54 N 65 E. = 2 18" Euc. Tree.			6.6	254.4	
58 N 55 E. = " 14" " "			5.9	255.1	
49 N 52 E. = 2 20" " "			5.2	255.8	
56 N 41 E. = 2 12" " "			4.4	256.6	
40 N 40 E.			4.7	256.9	
40 N 20 E.			3.7	257.3	
44 N 27 E. = 2 12" " "			3.8	257.2	
52 N 32 E. = 2 12" " "			4.0	257.0	
59 N 27 E. = 2 16" " "			3.4	257.6	
60 N 20 E.			3.4	257.6	
60 N 40 E.			4.5	256.5	
60 N 60 E.			6.4	254.6	
60 N 80 E			8.5	252.5	
65 N 69 E. = 2 16" Euc. Tree.			7.2	253.8	
71 N 50 E. = 2 16" " "			5.2	255.8	
72 N 31 E. = 2 18" " "			3.8	257.2	
80 N 20 E.			3.2	257.8	

261.03

80 N 40 E.		4.3	256.7
80 N 60 E.		6.1	254.9
80 N 80 E		8.2	252.8
91 N 56 E. = 2 12" Euc. Tree		5.3	255.7
90 N 32 E. = 2 12" " "		3.7	257.3
86 N 23 E. = 2 14" " "		3.3	257.7
93 N 17 E. = " 24" " "		2.8	258.2
97 N 26 E. = " 12" " "		3.4	257.6
105 N 22 E. = " 14" " "		3.2	257.8
111 N 17 E. = " 12" " "		3.1	257.9
118 N 22 E. = " 14" " "		3.2	257.8
100 N 20 E.		3.2	257.8
100 N 40 E.		4.2	256.8
100 N 60 E.		5.8	255.2
100 N 80 E.		7.6	253.4
120 N 80 E.		7.1	253.9
120 N 60 E.		5.9	255.1
120 N 40 E.		4.3	256.7
120 N 20 E.		3.2	257.8
108 N 42 E. = 2 12" Euc. Tree		4.0	257.0
111 N 84 E. = " 18" " "		7.2	253.8
140 N 80 E.		7.7	253.3
140 N 60 E.		6.2	254.8
140 N 40 E.		4.7	256.3
140 N 20 E.		3.0	257.8

140 N 00 E		2.1	258.9
125 N 20 E = ℄ 12" Euc Tree		3.2	257.8
124 N 11 E = ℄ 16" " "		2.9	258.1
136 N 11 E = ℄ 14" " "		2.8	258.2
140 N 21 E = ℄ 14" " "		3.1	257.9
128 N 98 E = ℄ 18" Blue Gum.		8.7	252.3
160 N 80 E.		8.5	252.5
160 N 60 E		6.9	254.1
160 N 40 E		5.3	255.7
160 N 20 E		3.7	257.3
160 N 00 E = ℄ Euc Tree 20"		2.2	258.8
145 N 14 E = ℄ 16" Euc Tree		2.8	258.2
155 N 17 E = ℄ 14" " "		3.3	257.7
158 N 30 E = ℄ 12" " "		4.2	256.8
147 N 89 E = ℄ 22" " "		8.4	252.6
180 N 140 E		12.8	248.2
180 N 120 E		11.9	249.1
180 N 100 E		10.4	250.6
180 N 80 E		9.1	251.1
180 N 60 E		7.6	253.4
180 N 40 E		6.1	254.9
180 N 20 E		4.4	256.6
180 N 00 E		2.6	258.4
180 N 20 W		1.1	259.9
169 N 5 E. = ℄ 20" Euc. Tree		2.4	258.6

167 N 20 W 14 E = ℄ Euc Tree		3.0	258.0
167 N 31 E = ℄ 18" Euc. Tree		4.2	256.8
172 N 22 E = ℄ 14" " "		3.9	257.1
175 N 38 E = ℄ 16" " "		5.4	255.6
168 N 77 E = ℄ 14" " "		8.5	252.5
200 N 140 E		12.8	248.2
200 N 120 E		11.8	249.2
220 N 140 E		12.7	248.3
240 N 140 E		13.4	247.6
240 N 120 E		13.0	248.0
220 N 120 E		12.3	248.7
222 N 120 E = 16" Blue Gum		12.3	247.7
226 N 138 E = 20" " "		12.4	248.6
233 N 117 E = 16" " "		12.5	248.5
72 N 87 E = 20" Euc Tree		8.7	252.3
200 N 100 E		11.0	250.0
200 N 80 E		9.8	251.2
200 N 60 E		7.5	252.5
200 N 40 E		7.1	253.9
200 N 20 E		5.4	255.6
200 N 000 E		3.3	257.7
200 N 20 W = East edge Path		2.1	258.9
200 N 28 W - W " "		1.7	259.3
189 N 22 E = ℄ 16" Euc. Tree		4.8	256.2
196 26 E = " 14" " "		5.2	255.8

26103

198 N 34 E = ℄ 14" Euc. Tree	6.4	254.6	
199 N 90 E = ℄ 18" " "	10.0	251.0	
220 N 100 E.	12.4	248.6	
220 N 90 E.	11.4	249.6	
220 N 60 E.	9.7	251.3	
220 N 40 E.	7.9	253.1	
220 N 20 E.	6.2	254.8	
220 N 0+00 E.	4.2	256.8	
220 N 4.5 W = E edge Path "E"	4.5	256.5	
220 N 10 W = W " " E	4.2	256.8	
220 N 13 W	3.2	257.8	
220 N 20 W	2.4	258.6	
212 N 47 E = ℄ 18" Euc. Tree.	7.8	253.2	
240 N 100 E.	13.1	247.9	
240 N 80 E	12.4	248.6	
240 N 60 E	11.4	249.6	
240 N 40 E	9.4	251.6	
240 N 20 E	7.3	253.7	
240 N 8 E = East edge Path "E"	6.6	254.4	
240 N 2 E = W " " "	6.2	254.8	
240 N 00 E	5.6	255.4	
240 N 20 W	3.3	257.7	
230 N 28 W = ℄ 36" Date Palm.	2.2	258.8	
237 N 27 W = ℄ 12" Thorny Tree	2.6	258.4	name ?
230 N 35 W = ℄ 18" " "	1.3	259.7	"

261.03

249 N 36 W = E 24" Euc. Tree	2.2		258.8	
239 N 51 E = ℄ 18" " "	9.3		251.7	
228 N 58 E = ℄ 18" " "	10.1		250.9	
242 N 60 E = ℄ 18" " "	11.2		249.8	
242 N 31 E = ℄ 18" Blue Gum.	8.3		252.7	
240 N 84 E = ℄ 22" " "	12.3		248.7	
246 N 90 E = ℄ 14" Euc Tree.	12.8		248.2	
249 N 110 E = ℄ 20"	13.6		247.4	
TP 1151	264.11	8.43	252.60	00 Rock 253 N 9 E
260 N 20 W	8.3		255.8	
260 N 00 E	10.4		253.7	
260 N 7 E	10.8		253.3	
260 N 8.5 E = W edge Path "E"	11.6		252.5	
260 N 14 E = E " " "E"	11.9		252.2	
280 N 20 W	7.9		256.2	
300 N 20 W	10.8		253.3	
300 N 40 W	8.3		255.8	Above TP.
TP 020	252.80	1151	252.60	
280 N 00 E	0.8		252.0	
280 N 10 E	1.4		251.4	
280 N 11.5 E = W edge path E	2.0		250.8	
280 N 19 E = E " " "	2.1		250.7	
300 N 20 E = E " " "	3.2		249.6	
300 N 13 E = W " " "	3.2		249.6	
300 N 11 E	2.6		250.2	

300N 00 E.		1.9	250.9	
320N 20E = East edge Path "E"		4.1	248.7	
320N 135E = W " " "		4.0	248.8	
320N 12E		3.2	249.6	
320N 00 E		2.4	250.4	
328N 20E = P.I. East edge Path E		4.6	248.2	
338.5N 20E = North edge Path E	from East.	4.9	247.9	
340N 10E		4.6	248.2	
357N 20E = Rim Canyon.		6.8	246.0	
342N 24E = ℄ 18" Oak Tree.		5.0	247.8	
351N 28E = ℄ 18" Date Palm		6.3	246.5	2.5 High = Trunk.
345N 40E = Rim Canyon.		7.8	245.0	
340N 40E		6.8	246.0	
330N 40E = N edge Path E.		5.7	247.1	
319N 40E = S " " "		5.6	247.2	
318N 40E		5.2	247.6	
300N 40E		4.7	248.1	
280N 40E		3.8	249.0	
284N 32E = ℄ 28" Blue Gums.		3.0	249.8	Dble. Tree
260N 40E		2.9	249.9	
260N 20E.		0.8	252.0	
260N 60E		4.0	248.8	
280N 60E		5.0	247.8	
300N 60E		5.9	246.9	
310N 60E		5.8	247.0	

312N 60E = S edge Path "E"	6.2		246.6
322N 60E = N " " "	6.3		246.5
342N 60E = Rim Canyon.	9.2		243.6
344N 57E = ℄ 12" Oak Tree.	9.5		243.3
339N 44E = ℄ 12" " "	7.2		245.6
329N 67E = ℄ 18" " "	7.3		245.5
337N 80E	10.0		242.8
320N 80E	7.1		245.7
315N 80E = N edge Path E	6.6		246.2
305N 80E = S " " " ✓	6.5		246.3
303N 80E	5.9		246.9
300N 80E	5.9		246.9
T.P. 4.71	6.50	246.30 ✓	305N 90E on Rock.
280N 80E	3.7		247.3
260N 80E	3.2		247.8
260N 100E	3.8		247.2
260N 120E	4.3		246.7
280N 120E	4.4		246.6
280N 100E	4.3		246.7
293N 100E = S edge Path "E"	4.9		246.1
308N 100E = N " " "	5.0		246.0
320N 100E	6.1		244.9
333N 100E = Rim Canyon.	8.2		242.8
325N 89E = ℄ 20" Oak Tree	6.1		244.9
328N 120E = Rim Canyon.	8.9		242.1

		251.01			
320 N 120 E			7.3	243.7	
304 N 120 E	= N edge Path "C" = N edge Path E		5.1	245.9	
294 N 120 E	= S " " E		5.0	246.0 ✓	
TP	5.15	252.40	3.76	247.25	220 N
chk. P17			4.41	247.99	180 E
				247.94 - both P-17	
				0.05 Error	

Walker
Bliss
Isbell
8-29-40

CAMINO DEL RIO

Location Telephone Poles.

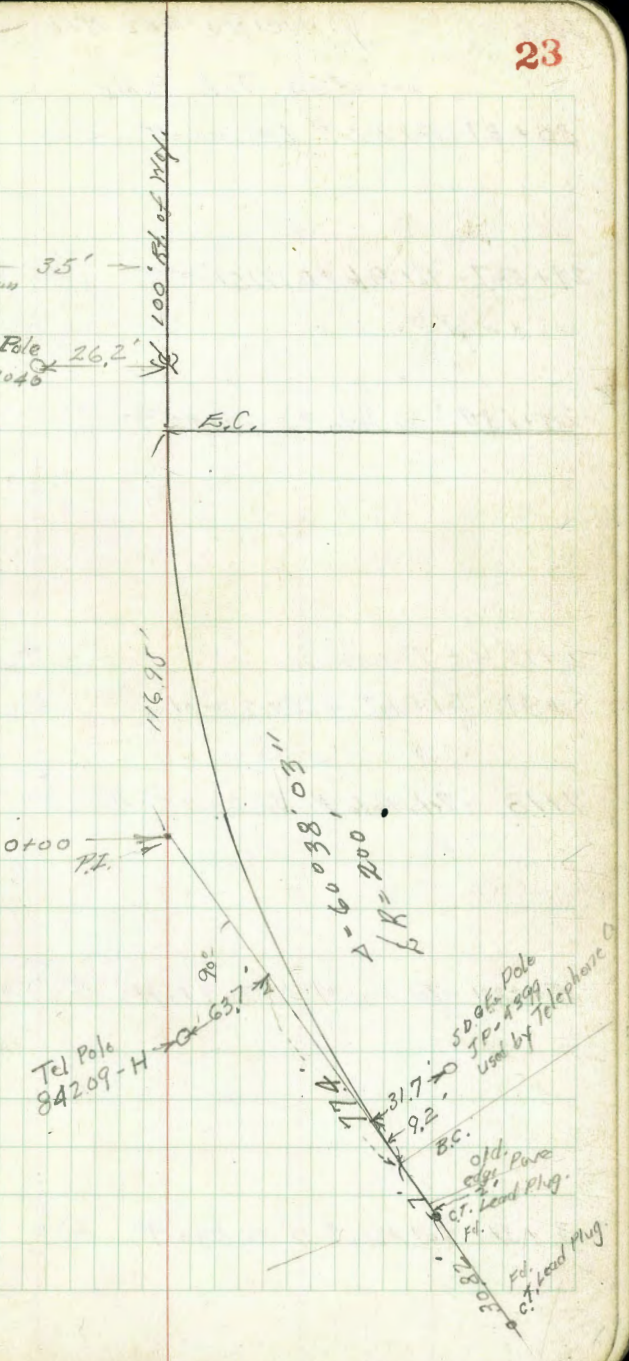
From Taylor St. To City Boundary.

1+32 = Deadman

1+31.7 = ℄ Tel. Pole (used by Elec Co. As Guy)

0+00 = P.I. FB. 1528

INDEXED
EFB



CAMINO DEL RIO

Location Tel. Poles

30+87 = Tel Pole # D 19200-T

29+58.7 = Tel Pole # D 17151-T

28+63.9 = Tel Pole # D-17152 T

9+12.6 = Deadman

8+91 = Tel Pole # 422023-H

7+18 = Tel. Pole # 422022-H

5+38.9 = Tel Pole # 422021-H

3+31 = Tel Pole # D 32530 T

← 42.6' →

← 40' →

← 39' →

31'
Deadman
Tel Pole 31.3'

Tel Pole
← 35.3' →

Tel Pole
← 39.5' →

Tel Pole
← 41.8' →

Camino Del Rio
Location Tel. Poles.

37+79.7 = Tel Pole Anchor.

37+56.7 = Tel. Pole # 307420-H

36+27.6 = Tel Pole # D 19196-T

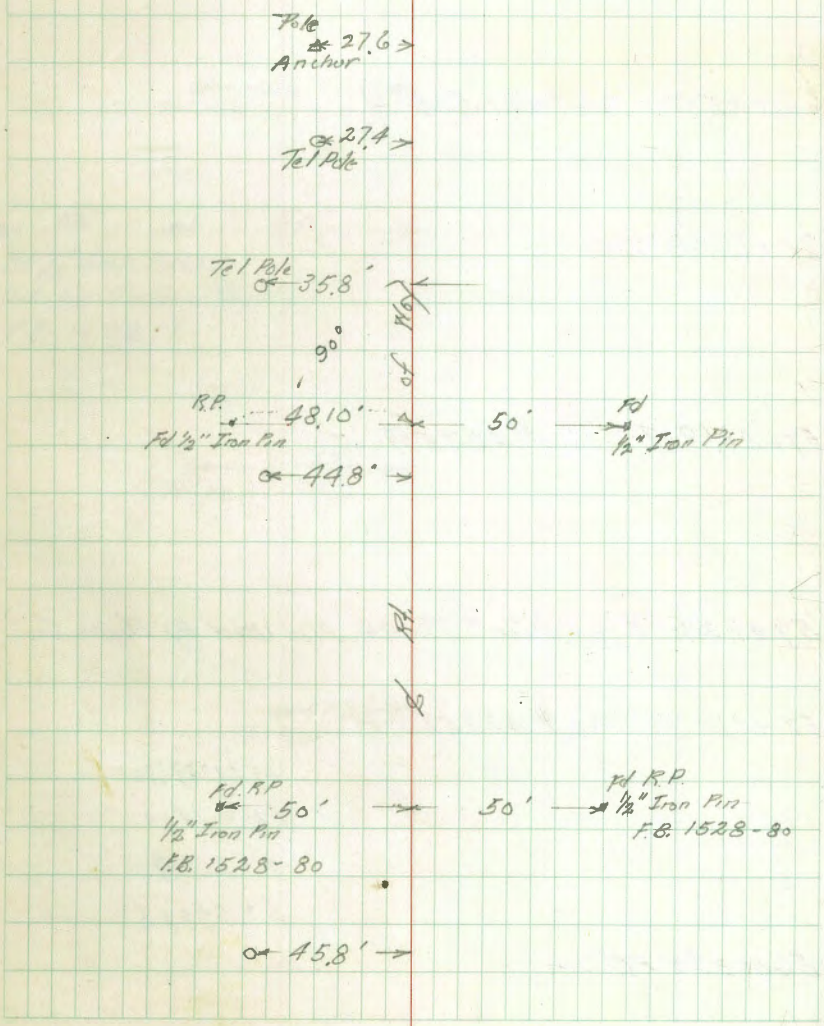
34+96.39 = E.C.

34+75.0 = Tel Pole # 307419-H

Δ = 3°48'12" Lt.
R = 2000'
S.T. = 66.40
L = 132.76

33+63.63 = B.C.

32+22.5 = Tel Pole # 412526-H



CAMINO DEL RIO

Location Telephone Poles.

65+82 = Tel. Pole # 427507-H

65+48 = Gas + Elec. Pole # 79049 Used by Tel. Co.

62+85 = Tel Pole # 427508-H

61+37.08 = E.C.

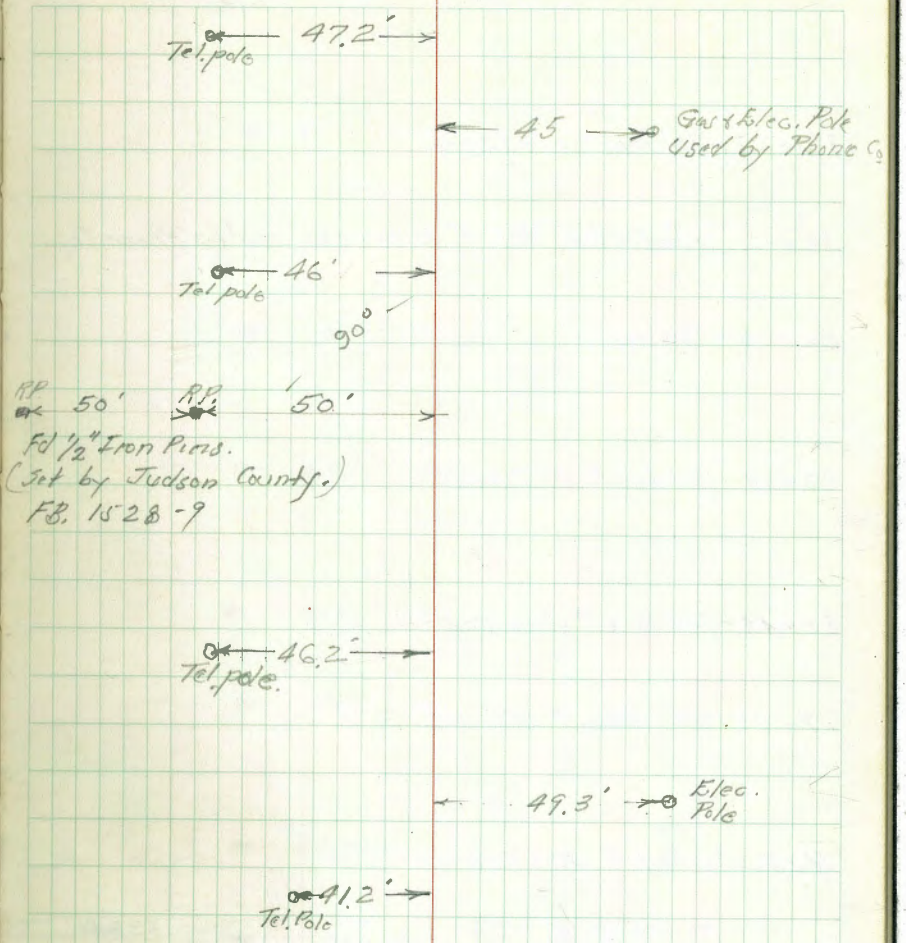
59+88.60 = Tel. Pole # 427509

57+92.6 = Elec. Pole # 79044 Also used By Phone Co.

57+85.1 = Tel Pole # 427510-H

Δ = 21°49'30"
D = 14°00
T = 269.87
L = 533.28

56+03.80 = BC. Lt.



Camino Del Rio

Location Tel. Poles.

86+27 = Tel Pole # 418324-H

86+12 = Gas + Elec Pole # P 79060 Used by Phone Co.

86+00 = Deadman

83+33 = Tel Pole # 427501-H

80+42 = Tel Pole # 427502-H

77+48 = Tel Pole # 427503-H

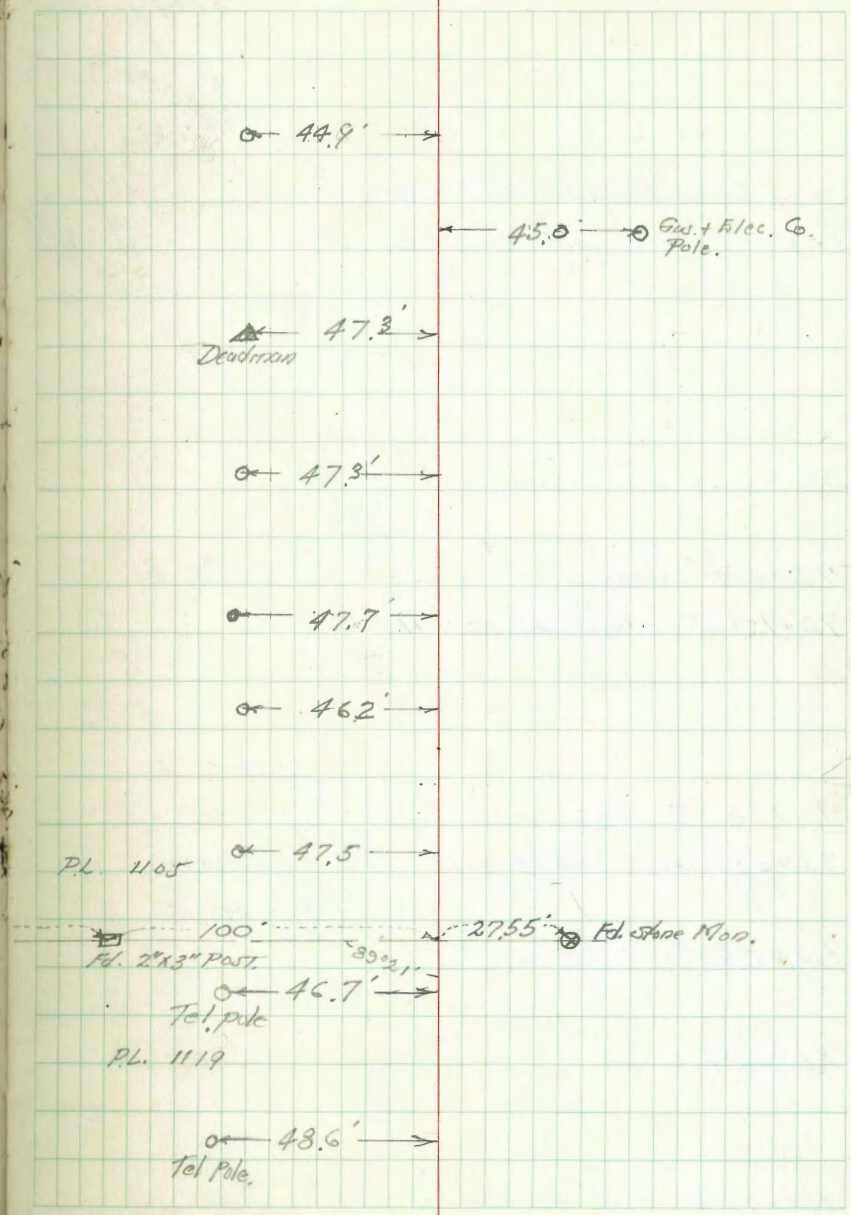
74+56 = Tel Pole # 427504-H

592.60'
Fd 2" Pipe Hub in top.

73+39.11

71+63 = Tel. Pole # 427505-H

68+72 = Tel Pole # 427506-H



Camino Del Rio
Location Tel. Poles.

3+84 Branch Line = Tel Pole # 418320-H

3+81 = " " = Guy Deadman

94+57.04

Main Line Cont P-30

92+28.3 = Tel. Deadman

92+15.6 = Tel. Pole # 418321-H

Δ 28°05' Lt.

90+38 = Deadman

90+35 = Tel Pole # 418322-H

R = 1000'

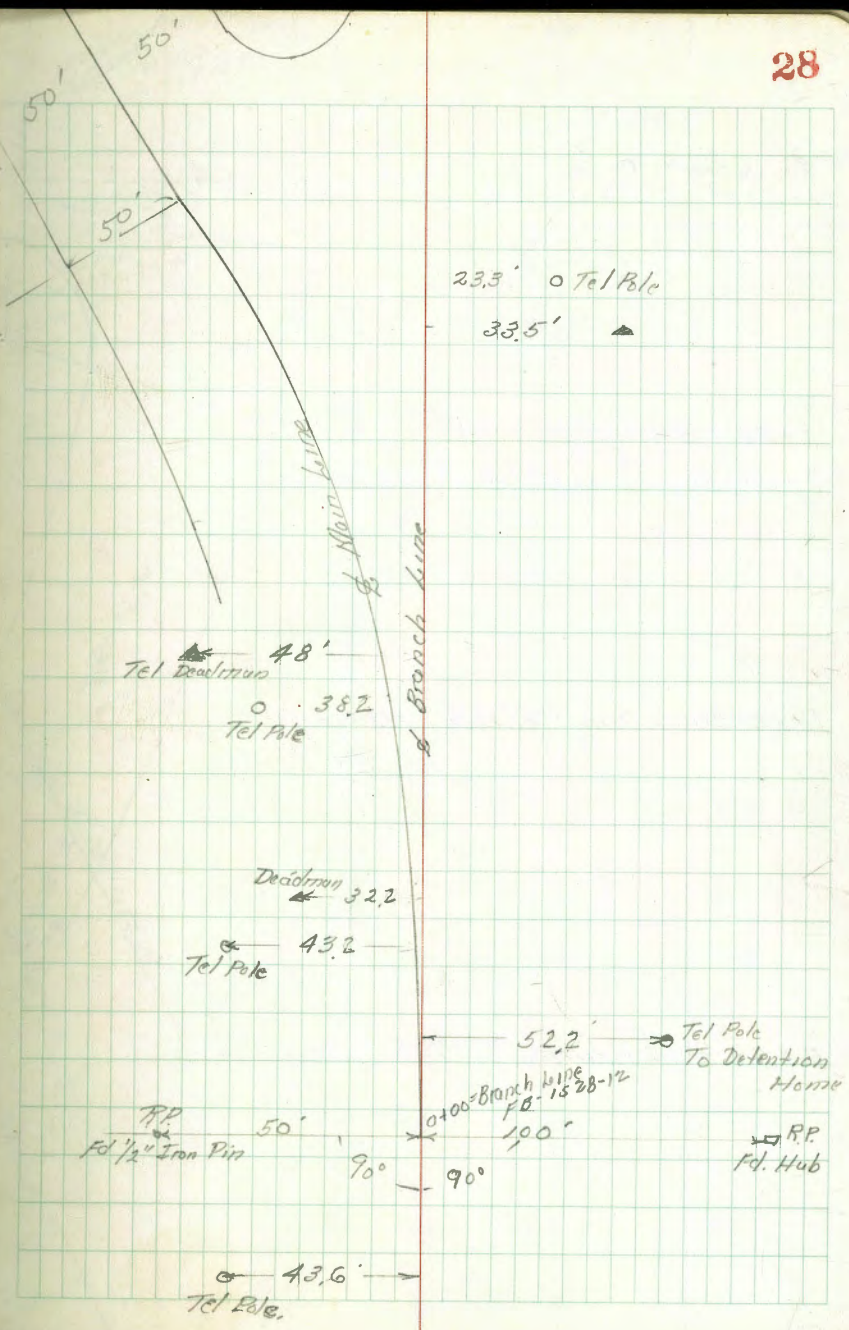
ST = 250.10

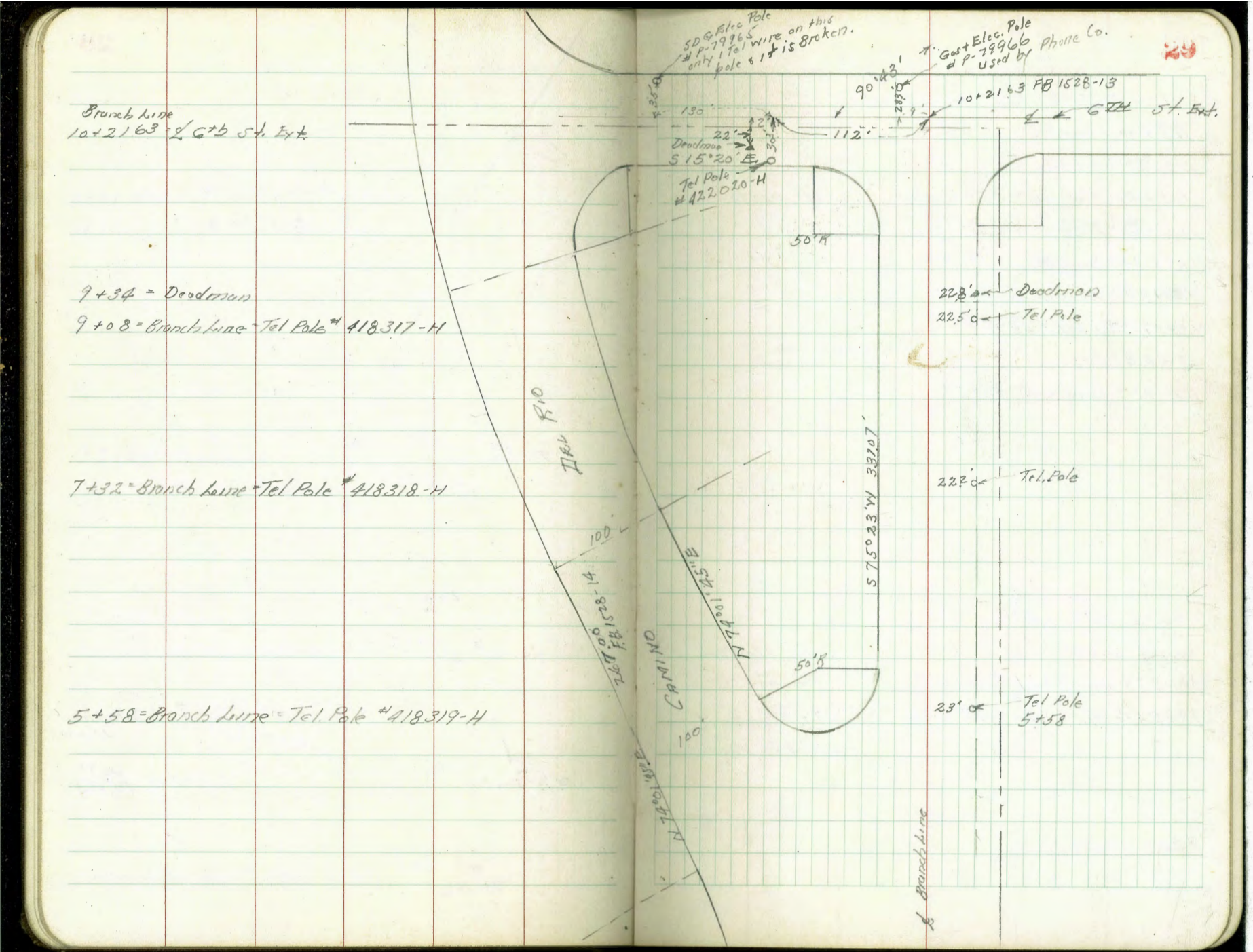
L = 490.15

90+32.8 = Tel. Pole # 420770

89+66.89 = B.C. Lt.

88+18 = Tel. Pole # 418323-H




SDG&E Elec. Pole
#P-79965
only 1 Tel wire on this
pole & it is broken.
Gas + Elec. Pole
#P-79966
used by Phone Co.
90°43'
10+21.63 FB 1528-13
℄ 6 TH 5+ Ext.
130'
112'
22'
Deadman
S 15°20' E.
Tel Pole
#422020-H
50' R
Branch Line
10+21.63 = ℄ 6+5 5+ Ext.
9+34 = Deadman
9+08 = Branch Line - Tel Pole # 418317-H
7+32 = Branch Line - Tel Pole # 418318-H
5+58 = Branch Line - Tel. Pole # 418319-H
R 10
DEL
CAMINO
N 74°00' 15" E
S 75°33' W 337.07'
N 74°01' 45" E
100'
22.8' ℄ Deadman
22.5' ℄ Tel Pole
22.7' ℄ Tel. Pole
23' ℄ Tel Pole
5+58
℄ Branch Line

CAMINO DEL RIO

Location Tel. Poles.

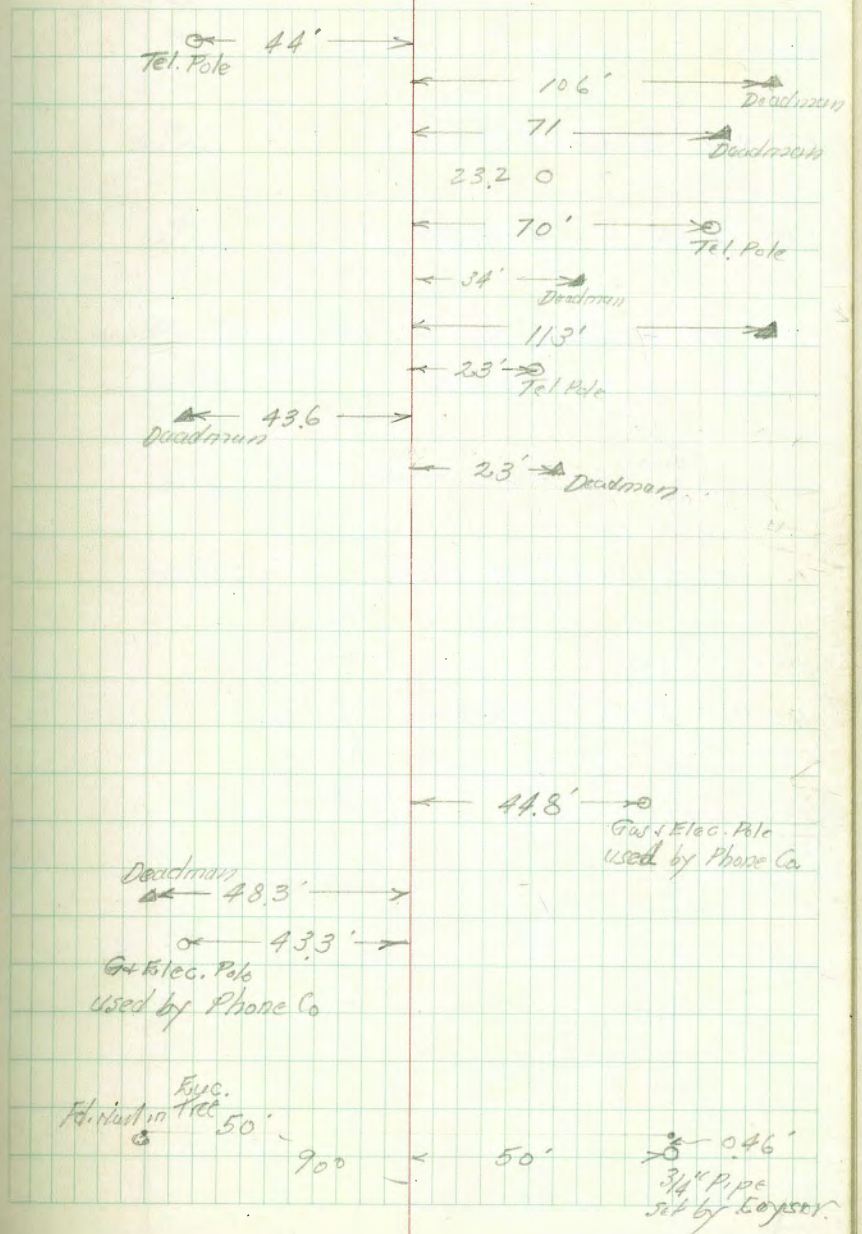
113+50.5 = Tel. Pole # 412521-H
113+50 = Deadman
113+50 = Deadman
113+49.5 = Tel Pole # 4572 = Match to 113+37 = # 4572
113+45 = Tel. Pole Number gone
113+41 = Deadman
113+39 = Deadman
113+37 = Tel Pole # 4572
113+28 = Deadman
112+91 = Deadman

79967
98+36 = Gas + Elec Pole used by Phone Co

98+25 = Deadman Gas + Elec.
98+24.4 = Gas + Elec Pole # 79980

Δ = 27° 42' 30" Rt.
℄ R = 1000'
" S.T. = 246.61'
" L = 483.58'

97+24.04 = B.C.



CAMINO DEL RIO

Location Tel. Poles

122+71 = Tel Pole # 89544-H

121+17 = Tel Pole # 89543-H

119+72 = Tel Pole # 89542-H

118+30 = Gas & Elec Pole # 79078 Used by Phone Co

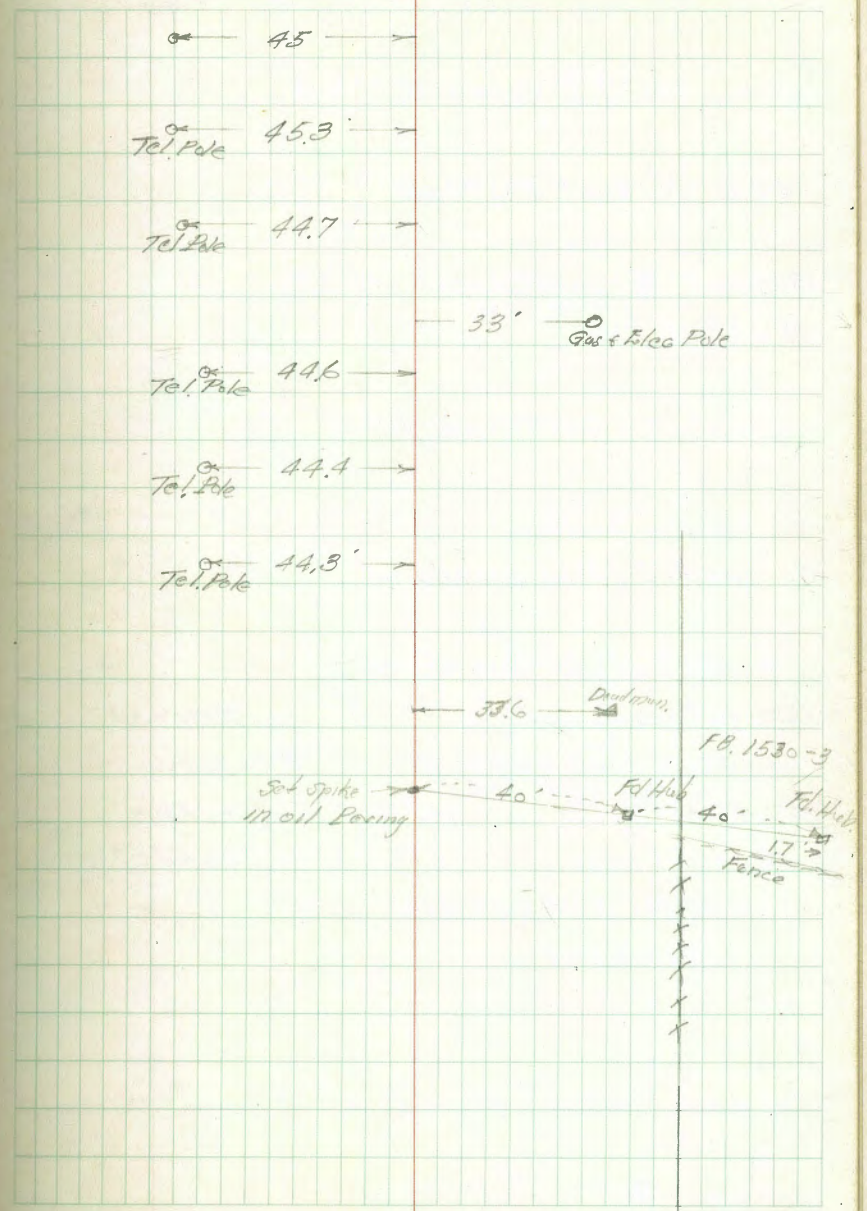
118+21 = Tel Pole # 416742-H

116+66 = Tel Pole # 416741-H

115+06 = Tel. Pole # 416740-H

113+97.5 = Deadman

113+65.18 = Δ 100° Lt.



CAMINO DEL RIO

Location Tel Poles.

135+95 Gas + Elec. Pole 89549-H

134+50 = Tel Pole # 89548-H

133+10.5 = Tel Pole # 89547-H

132+85.81 = E.C.

131+68.6 = Tel Pole # 89546-H

130+41.5 = Deadman

130+40.4 = Tel Pole # 409954-H

128+89.3 = Tel Pole # 430763-H

128+50.5 = Deadman

128+49 = Tel Pole # 416739-H

127+98.43 = P.I.

126+96.4 = Deadman

126+96 = Tel Pole # 416738-H

126+70.40 = B.C. L.H.

125+53 = Tel Pole # 416743-H

124+12 = Tel Pole # 89545-H

$\Delta = 14°35'30"$ Lt

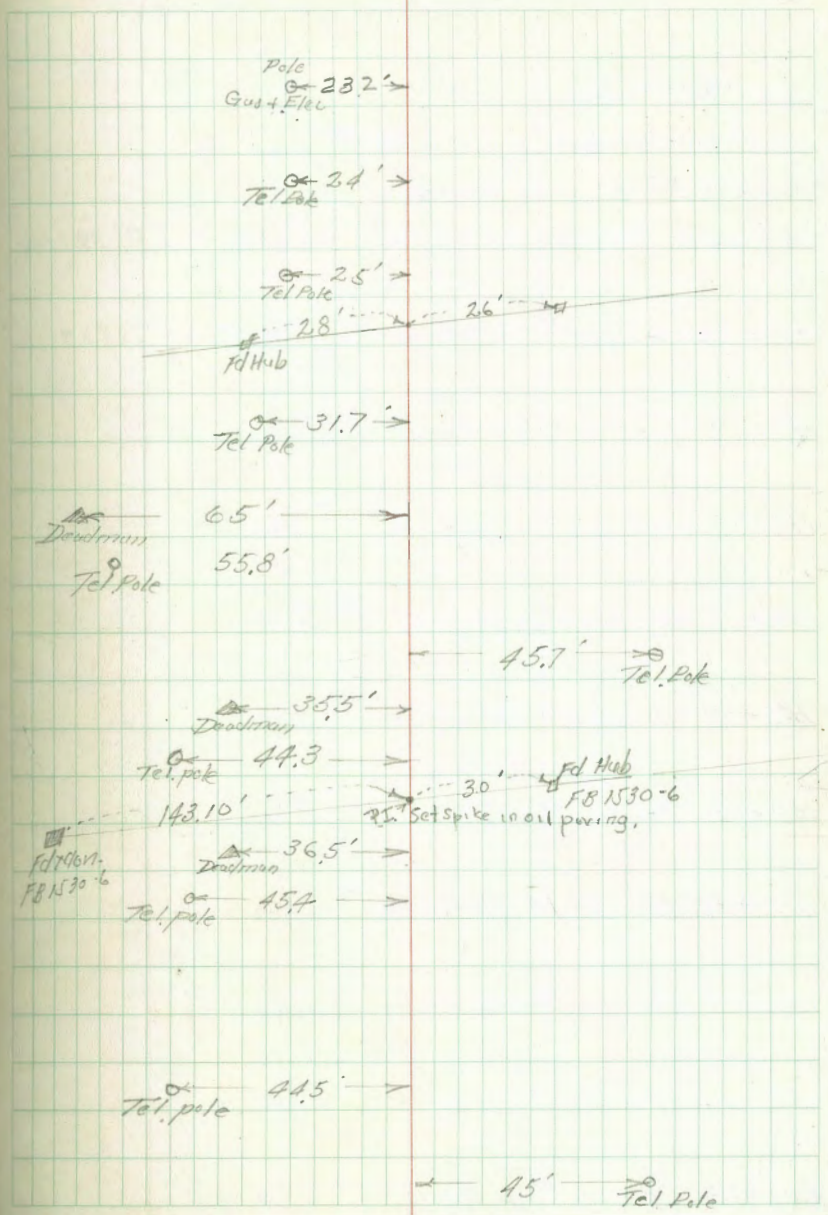
$D_c = 10°00'$

$R = 1000'$

$T = 128.03'$

$L = 254.67'$

℄



Camino Del Rio

Location Tel Poles.

154+96 = Deadman

154+93.4 = Tel Pole # D-19228-T

154+78.93 = BC. See P-34

153+48 = Tel Pole # 87895-H = Gas + Elec # JP-79914

151+33 = Tel Pole # 87894-H = Gas + Elec # JP. 79913

149+59 = Tel Pole # 87893-H

148+15 = Tel Pole # 87892-H

146+63 = Tel Pole # 87891-H

145+17 = Tel Pole # 307677-H

143+63 = Tel Pole # 87890-H

142+19 = Tel Pole # 87889-H

140+67 = Tel Pole # 87888-H

138+14 = Tel Pole # 89550-H

137+73 = Tel Pole # 407212-H

23' →

Tel Pole 33' →

23.4' →

23.3' →

Tel Pole 23' →

Tel Pole 23.2 →

Tel Pole 23.2' →

Tel Pole 24' →

Tel Pole 23.6' →

Tel Pole 23 →

Tel Pole 23' →

Tel Pole 23.2' →

Tel Pole 23.3 →

CAMINO DEL RIO

Location Telephone Poles

165+74.4 J.P. 79892 Tel # 418311

165+68.85 = E.C.

164+23 = Deadman

164+23 = J.P. 79893 # 418312 = Tel.

162+68 = Tel Pole & Elec Pole J.P. # 79894 - Elec No) 418313-H

161+29.12 = 8.6 Rt

161+10 = Tel Pole # 87898-H

159+54 = Tel Pole # 418314-H

159+18.59 = E.C.

157+69 = Deadman

157+69 = Tel Pole # 418815-H

$\Delta = 25°13'10"$ Lt.

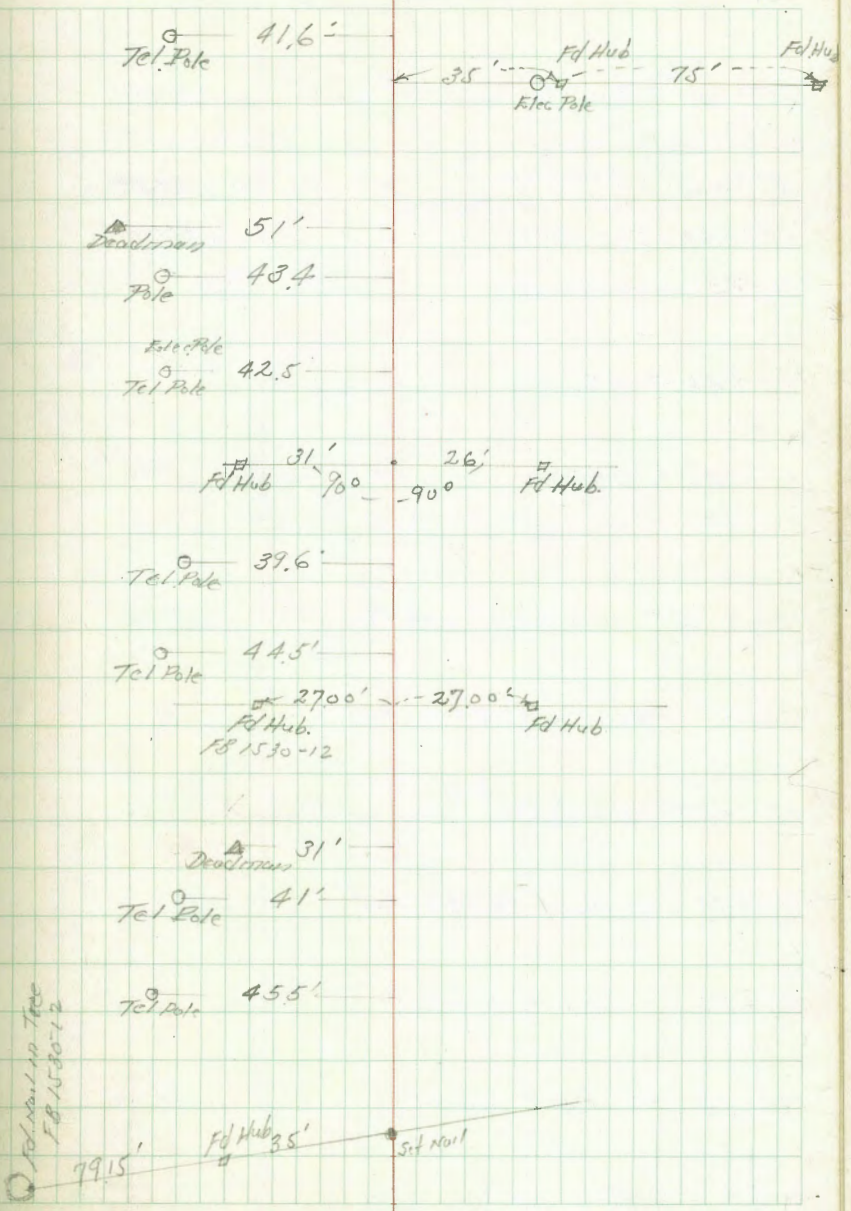
D R = 1000'

T. = 223.70

L = 440.16'

156+36 = Tel Pole # 87896-H

154+78.43 = P.C. Lt



CAMINO DEL RIO

Location Tel Poles

179+72.3 = Elec. Pole used by Phone Co Δ = 22°07'

Σ R = 1000'

179+45 = Deadman #2
Tel = #418305-H Σ ST. = 1954.0'

179+43 = J.P. 79962 Σ L = 386.01'

179+43 = Deadman

178+46.04 = B.C.

177+32 = Deadman

177+32 = Tel Pole #418306

175+74 = Tel. Pole #418307

173+73 = Tel Pole #418308-H

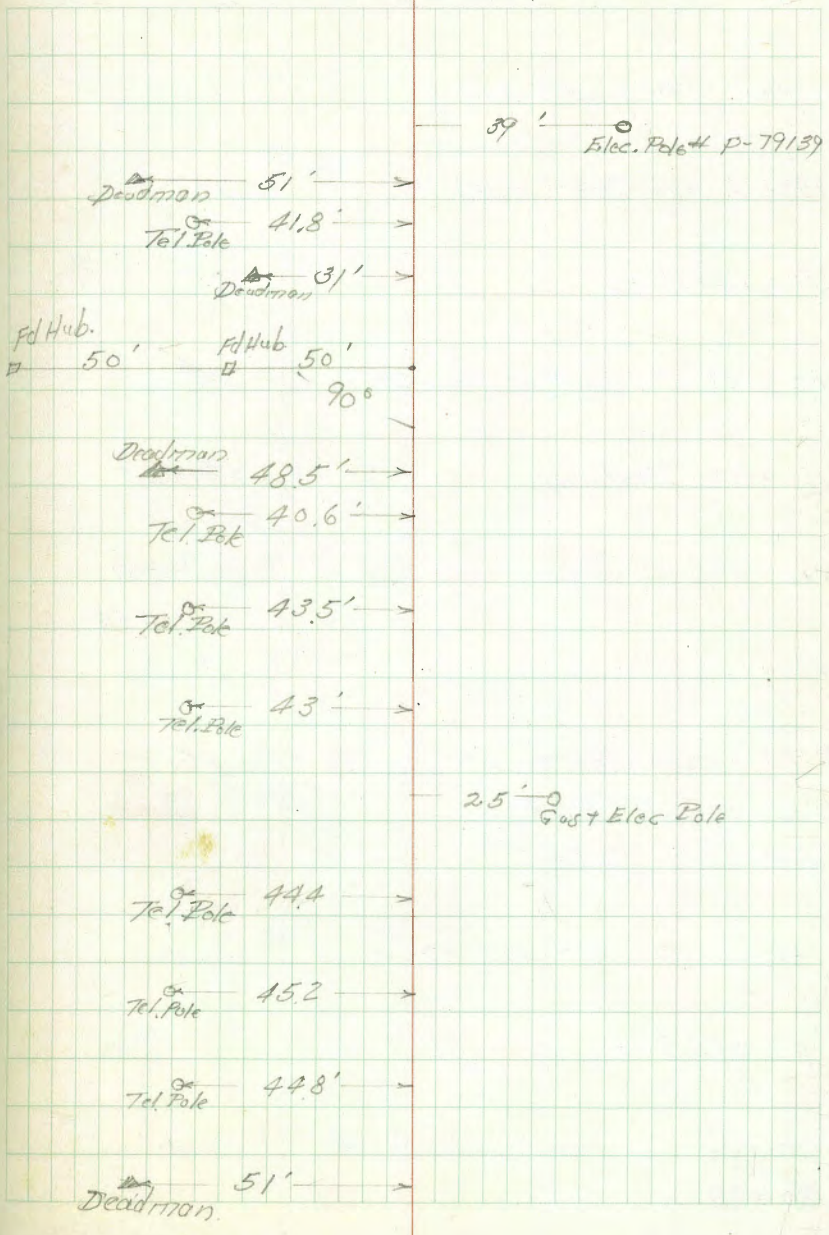
172+20 = G+ Elec Pole #P. 79136. Used by Phone Co.

170+76 = Tel Pole #307676-H

169+22 = Tel Pole #418309

167+80 = Tel Pole #418310

165+74.8 = Deadman.



CAMINO DEL RIO

Location Tel. Poles.

191+12 = Tel Pole # 89354-H

189+62 = Tel Pole # 89353-H

188+49.91 = E.C.

188+07 = Tel Pole # 418301-H

186+72 = Deadman

186+47.3 = Tel Pole # 401302-H

186+16.8 = Deadman

184+54.2 = ELEC. POLE # used by Phone Co.

184+50.4 = Tel. Pole #

184+45.38 = 86 Lt.

182+61 = Tel Pole # 422108-H

182+32.95 = E.C.

180+84 = Tel Pole # 422107-H

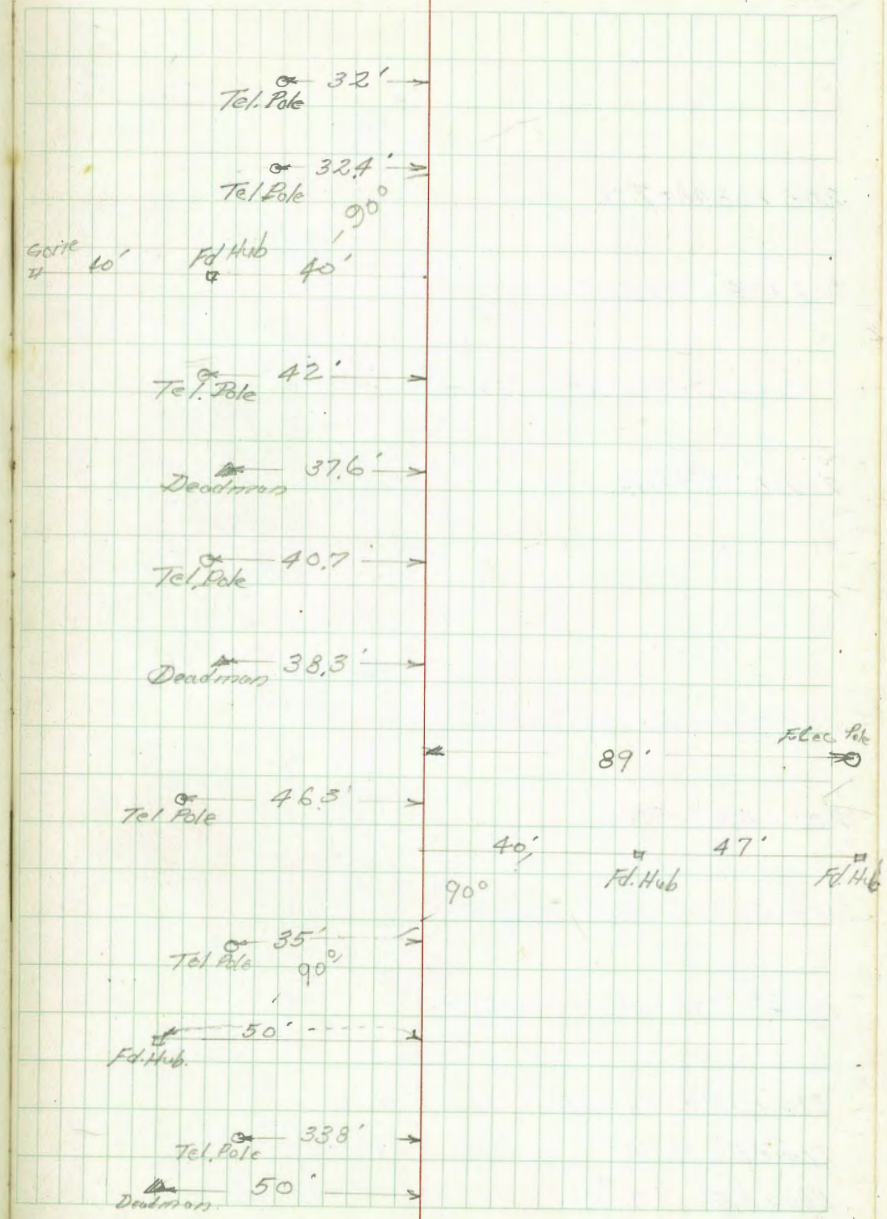
180+83

Δ 23°10'40"

℄ R = 1000'

℄ ST = 205.07

℄ L = 404.53



CAMINO DEL RIO

Location Tel Poles

205+08.48 = P.O.T.

204+34 = Tel. Pole # D-19259-T

202+25.8 = Tel Pole # 89357-H

202+21.32 = E.C.

Δ = 6°18'30"

℄ R = 1600'

℄ T = 88.16'

℄ L = 176.16'

200+61 = Tel Pole # 430766-H

200+45.16 = S.C.

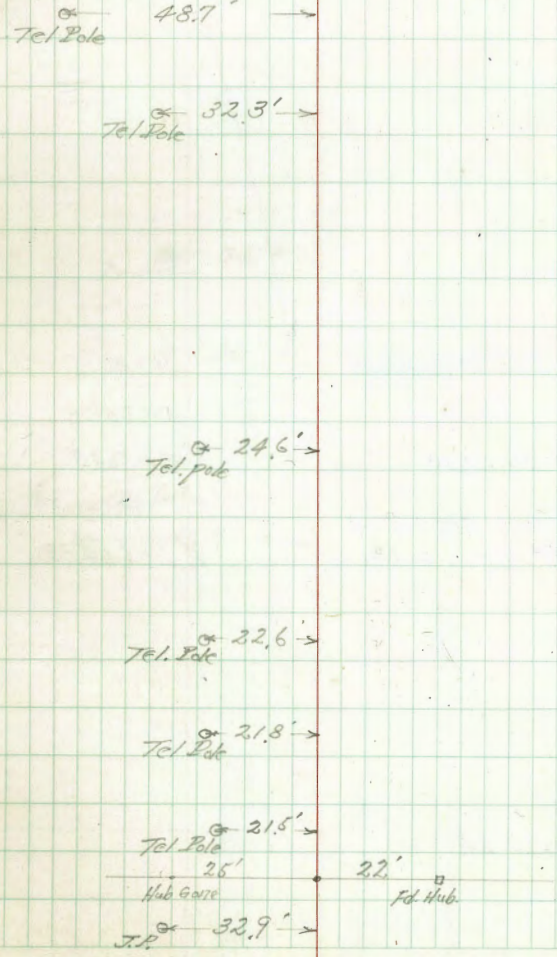
198+29 = Tel Pole # 306148

196+76 = Tel Pole # 89356-H

194+85.5 = Tel Pole # 89355-H

194+50 = P.O.T.

193+05 = J.P. # 79876 = Elec C. # 416721-H = Tel Pole



CAMINO DEL RIO

Location Telephone Poles.

207 +57 = Deadman

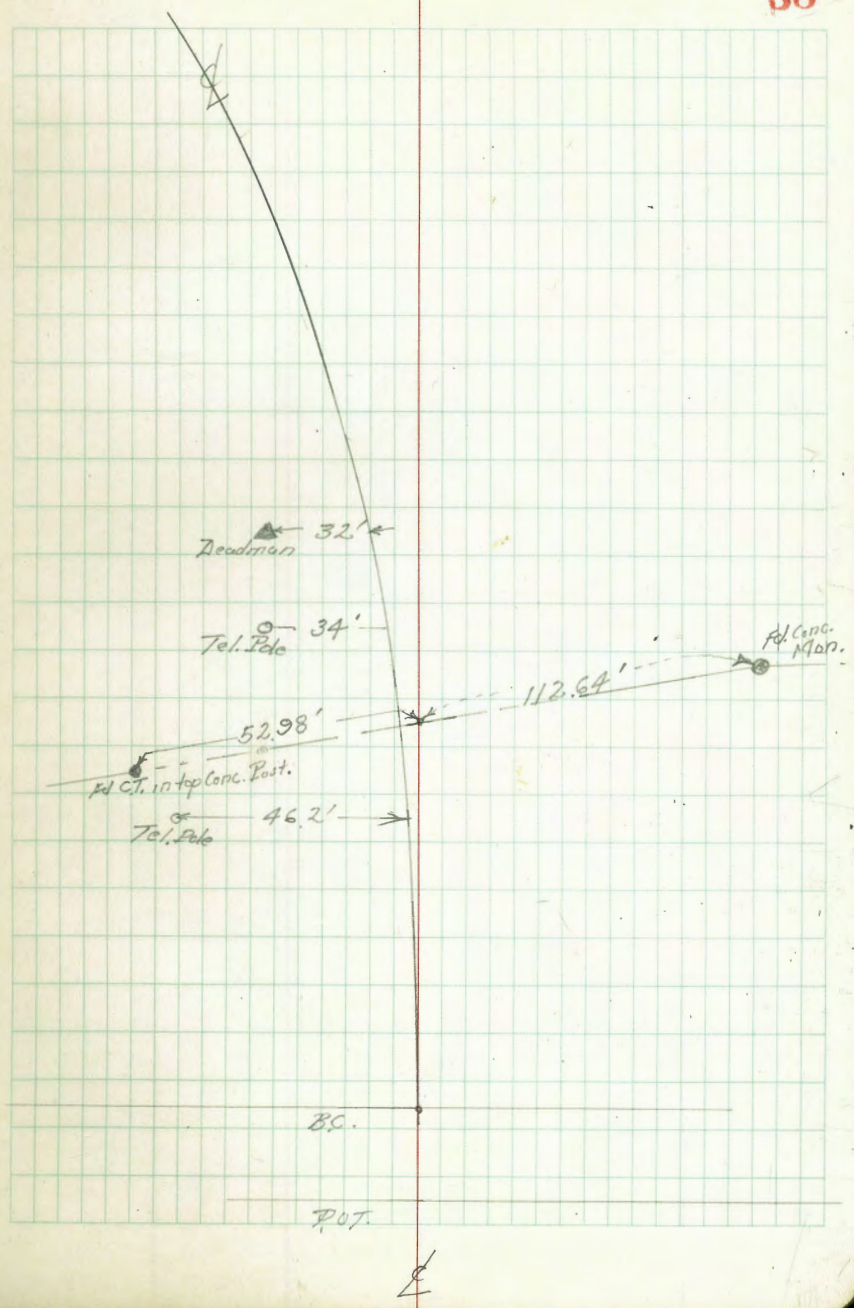
207+36 = Tel. Pole # 89358-H

206+59.98 = C.T. in Lime

206+40 = Tel Pole # 414742-H
= J.P. # 79888-G & Elec.

205 +35.51 = B.C. L.H.

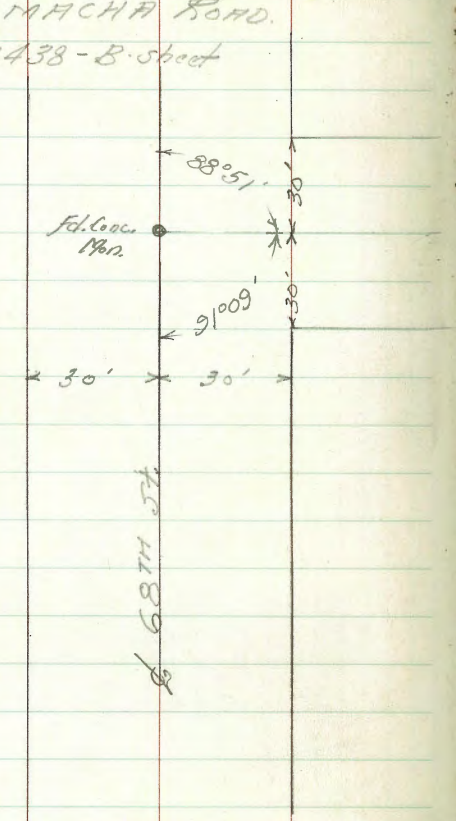
Δ = 20°08'
ℒ R = 1864.96'
ℒ T = 331.08
ℒ L = 655.33



Walker
Bliss
Isbell
12-12-40

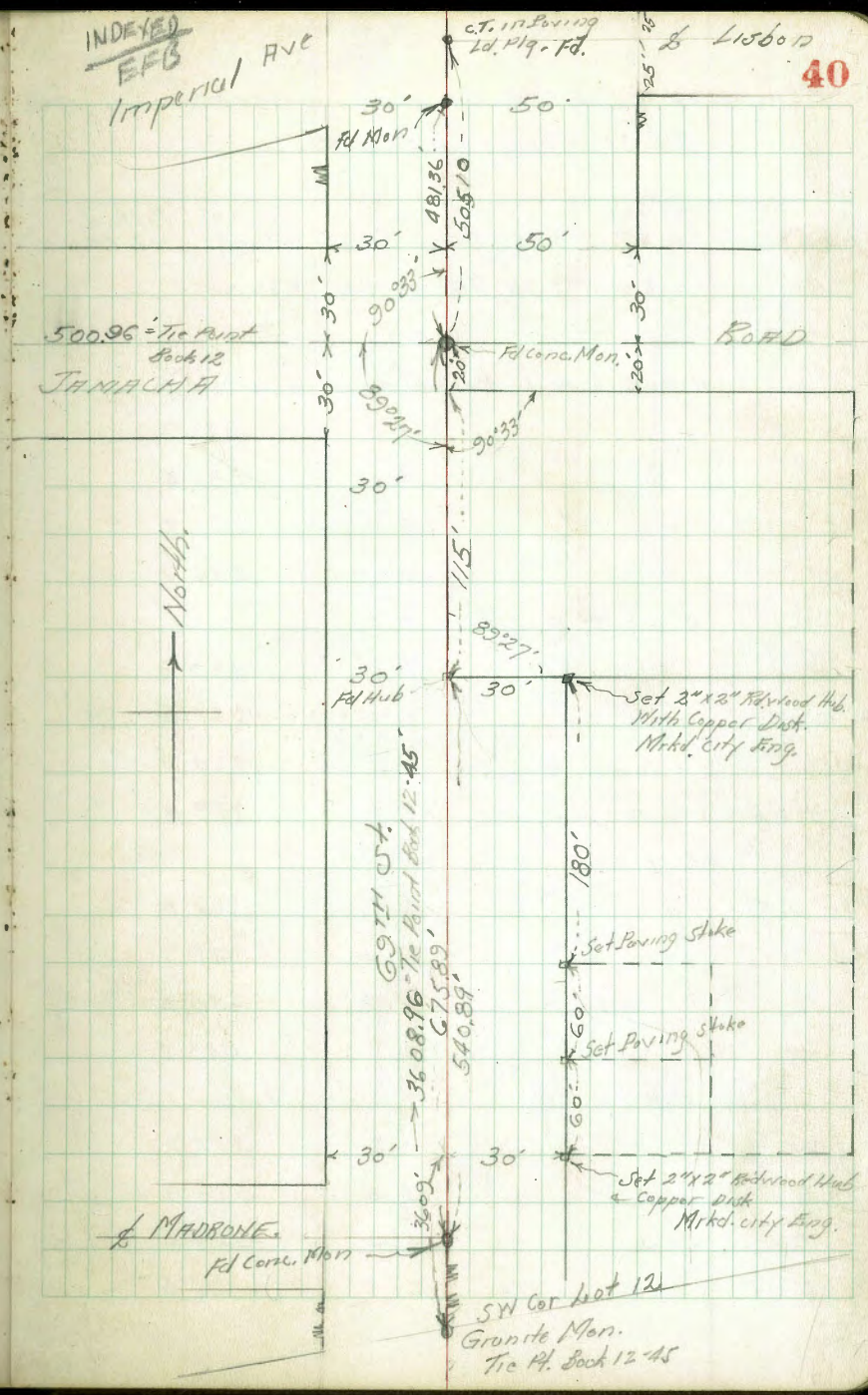
Survey of Opening Line on East Side 69th St. South of Jamacha Road.

Drawing 2438-B Sheet



INDEXED
EFB

Imperial Ave



Moore
Osborne
Hale
12-27-40.

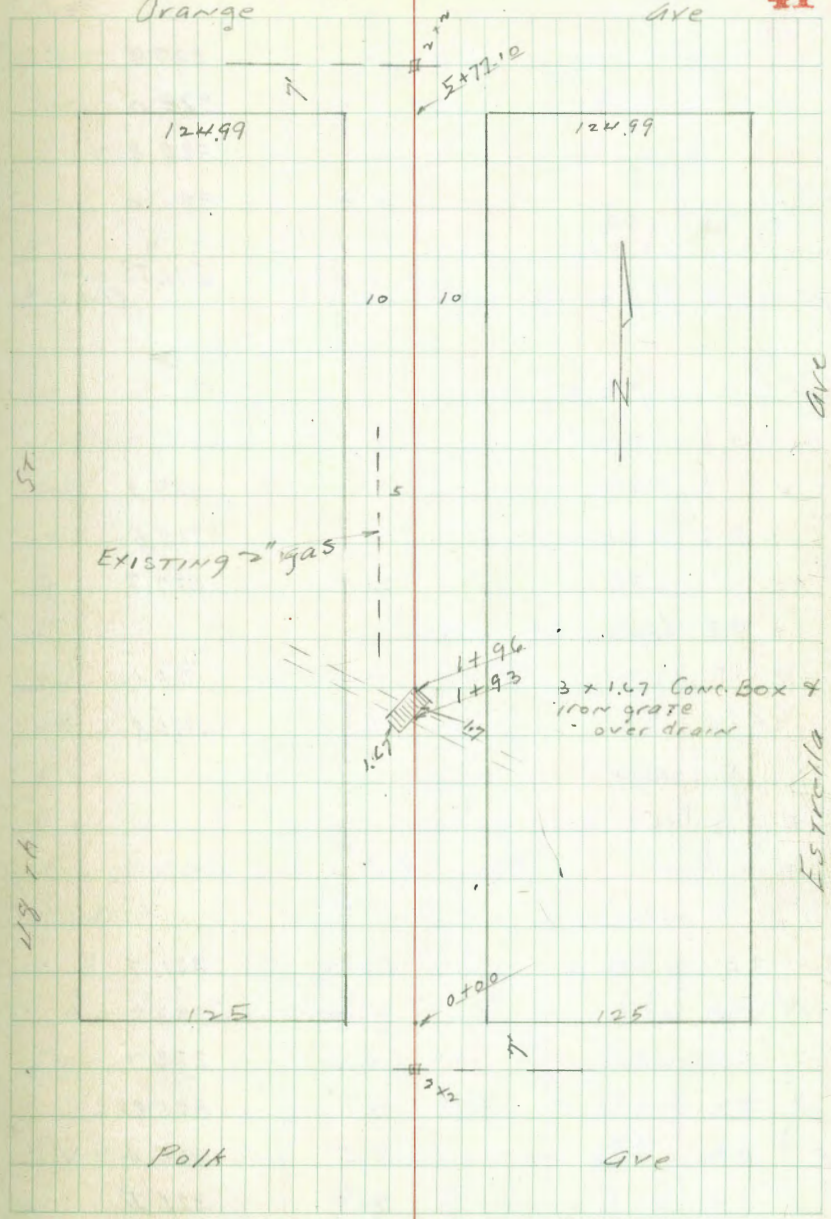
X sec & alley 20' wide
Blk 31 Fairmont Add.

NEBP	1.57	344.94		343.27	Polk & 48th St
T.P.	2.60	334.85	12.59	332.25	
	0+00 = N & Polk (NOT graded)				
-15			5.0	329.9	
E			8.5	331.4	
C			3.1	331.8	
W			0.0	334.9	
	0+25				
W'			1.0	333.9	
C			3.4	331.5	
E			4.0	330.9	
+15			6.6	329.3	
	0+50				
-15			5.9	329.0	
E			5.0	329.9	
C			4.7	330.2	
W'			1.7	333.2	
	0+75				
W			3.8	331.1	
C			5.0	329.9	
E			5.5	329.4	
+15			6.5	328.4	

Recd & Plot. 12-28-41 <B.H.

INDEXED
EFB

41



	1+00		
-1.5		7.0	327.9
E		5.9	329.0
C		6.1	328.8
W1		3.9	331.0
	1+06		
W-6.6 S.E. Cor do. gar. S'ly entrance		3.2	331.73 cem. floor
	1+25		
W-0.8 in P.P.			
W		5.0	329.9
+8		7.4	327.5
C		7.2	327.7
+9.7 beg. Lath house			
E		6.8	328.1
+15		8.1	326.8
	1+47		
E end Lath House			
E beg. wire fence & Conc. Ret. wall			
	1+50		
E-30		13.2	321.7
-24		11.2	323.7
-9		11.2	323.7
-8		9.1	325.8
E Top Cobble Ret. wall		8.5	326.4 V
C		8.4	326.5

C+4	8.3	326.6
W	5.6	329.3
+10	4.5	330.4
	1+59	
E & 3' Cobble steps	9.16	325.69 ✓ end gate
E-4 " " 3 steps down	11.0	323.9 V
	1+78	
W-10	4.7	328.2
-1.2 S.E. Cor chick shed		
W	8.0	326.9
+4	8.7	326.2
C	8.8	326.1
E	9.1	325.8
+1 Top Cobble Ret. wall	9.1	325.8 V
+2	10.6	324.3
+20	10.2	324.7
+21	9.1	325.8
	1+93	
-25	8.0	326.9
-1	8.8	326.1
-0.3 Top Cobble wall	8.1	326.8 V
E	8.7	326.2
C Top iron grate	9.4	325.43 ✓
C Ft Con. Box	13.6	321.23
W	8.7	326.2

334.85

W +1	NE Cor chick shed		7.7	327.2
+20				
	2+09			
-20			7.9	327.0
W	fence on line		8.1	326.8
C			8.4	326.5
+8.2	E 3' Cobble steps		7.2	327.7 Bot. step
E	on step		6.4	328.5
+1.2	E 3' Cobble walk		6.2	328.7 end wire fence and Cobble wall
T.P	11.8 X	339.91	6.78	328.07
	2+26			
W +0.4	1.4 P.P.	W.L	end wire fence beg picket	
	2+30			
-10			9.8	330.1
E			9.8	330.1
C			11.5	328.4
W			11.5	328.4
+25			11.0	328.9
	2+64			
-25			8.6	331.3
W			7.9	332.0
C			7.7	332.2
+9.7	SW Cor	chick shed	7.2	332.7

339.91

2+75			
W-0.3 end Picket fence			
W-2.6 beg. " "			
3+00			
E+0.4 chick shed	5.9		334.0
C	6.1		333.8
W	6.3		333.6
+10	6.7		333.2
3+24			
E+0.4 NW Cor. chick shed			
3+25			
W-2.1 end			
W-1.7 SE Cor house cem. fd.			
W-0.2 1.2 P.P.			
W	5.1		334.8
C	5.3		334.6
+8.2 SW Cor Sm. gar + shed			
E	4.9.		335.0
3+31			
E+1.8 E Sm. gar.	4.9		335.0 C. in X.
3+48			
E+1.4 NW Cor above gar + shed			
E+0.8 beg. Lath fence			
3+55			
W-0.9 NE Cor. house cem. fd.			
" 0.6 beg. Lath fence + gate			

3+57

E	4.1	335.8
C	4.3	335.6
W	4.0	335.9
+0.9 E 4' Conc. walk	3.98	335.93 ✓

3+59

E +0.4 end Lath fence
E -0.2 SW Cor frame house

3+62

W -0.4 end Lath fence
W -0.4 SE Cor. Bd shed

3+72

E -0.2 NW Cor frame house
E -0.2 beg picket fence

3+75

E +0.4 end above "
W +0.2 NE Cor Bd shed
" " beg. picket fence

3+76

-5 drainage ditch	3.4	336.5 ✓
W	3.5	336.4
C	3.7	336.2
E	3.7	336.7

4+00

-5	2.7	337.7

E	2.7	337.7
C	2.5	337.4
W	2.3	337.6

4+10

W -3.7 end picket fence

4+16

W -3.7 E Sm. gar.	1.5	338.4 ✓ dirt

TP 1001 348.10 1.82 338.09

4+21

E -5.1 E Sm. gar.	9.3	338.97 ✓ conc.

4+24

W	9.8	338.3
C	9.9	338.2
E	9.3	338.8

+0.3 beg. picket fence

4+54

E -0.3 @ in " "

4+65

-4.2 Sm. gar	7.08	341.02 ✓ conc.
-0.1 E conc. apron	7.23	340.87 ✓ level
E	7.3	340.8
C	7.5	340.6
W	7.3	340.8

	4+78		
E −0.1	end Picket Fence		
E +0.1	Sw Cor gar. 6.07		341.03 ✓ CEM. K.
	4+79		
W +0.2	1.2 PP.		
	4+90		
W 10		6.0	342.1
W		6.3	341.8
C		6.3	341.8
+9.7	NW Cor gar 6.07		341.03 ✓ CEM. K.
E	SW Cor Bd. shed		
	5+03		
E +0.1	NW Cor Bd. Shed ✓		
" "	beg. Bd fence ✓		
	5+15		
E		4.6	343.5
C		5.0	343.1
W		4.4	343.7
+10		4.5	343.6
	5+27		
E −0.1	end Bd. Fence N		
	5+33		
E −5.4	& S, W. gar.	4.0	344.1 dirt ✓
	5+50		
−5		4.0	344.1

W		4.0	344.1
C		4.1	344.0
E		3.8	344.3
+5		3.8	344.3
	5+77.10 = SL Orange Arc		345.2
−5		2.9	only graded
E		3.2	344.9
C		3.8	344.3
W		3.6	344.5
+5		3.5	344.6
T.P.	4+24	348.49	3.65 344.45
check to BM	SE 48th Orange	5.75	342.94 342.96

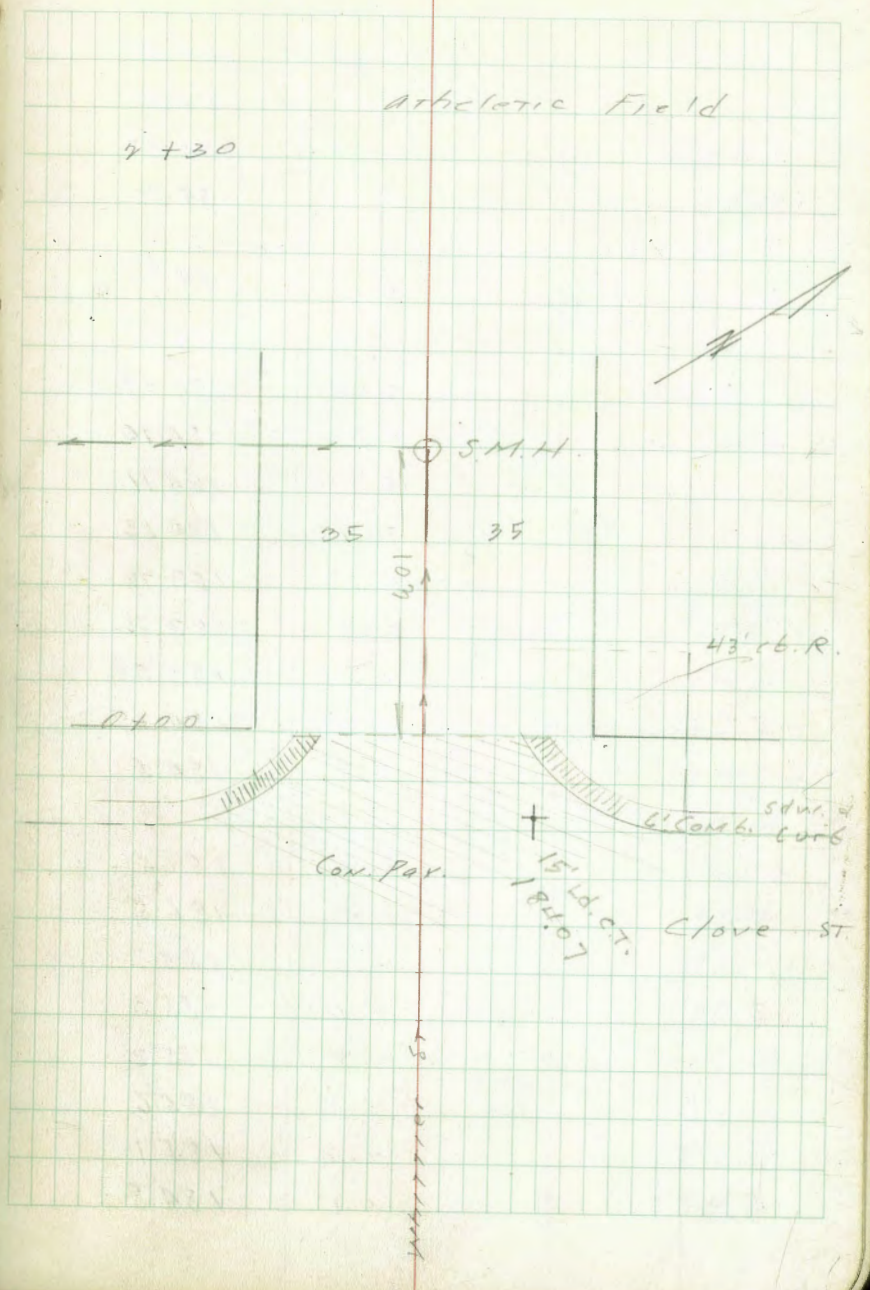
Moore
Osborne
Sommermeyer

X sec Whittier 70' wide 18' c&s 8.5 1/4 — Indexed L.M.L.

1-31-41 Wly of Clove

NWBP	10.90	172.40		161.50	Chatsworth Zola
T.P.	12.27	182.18	2.49	169.91	
T.P.	8.18	189.93	0.43	181.75	
NWI. 15' Ld. C.T.	Clove Whittier		5.86	184.07	
check to SE F.H.	"		1.93	188.00	188.05
0-18					
-25 c6 P.C.			4.97	184.96	
-25 gut			5.47	184.46	
S	Pav		5.28	184.65	
c6	"		5.23	184.70	
1/4	"		5.30	184.63	
C	"		5.42	184.51	
1/4	"		5.48	184.45	
c6	"		5.72	184.21	
N	"		6.39	183.54	
+25 gut	"		7.46	182.47	
+25 c6 P.C.			6.95	182.98	
0-9.8					
N c6			6.12	183.71	
N gut	Pav		6.65	183.28	
c6	"		5.93	184.00	
N 1/4	"		5.65	184.28	
C	"		5.57	184.36	

Red'd Plot on Profile 1409 - 1-31-41 CBK



1989.93

S 1/4	Pav	5.48	184.45
c6	"	5.46	184.47
S gut	"	5.55	184.38
S c6		5.03	184.90
0+00 Wly. Line Clove St			
S beg. Evergreen Hedge		5.0	184.9 1 IN ST.
c6 end return		5.3N	184.61
gut pav		5.8N	184.09
S c6	"	5.83	184.10
1/4	"	5.8N	184.11
C	"	5.81	184.12
1/4	"	5.95	183.98
N c6	"	6.17	183.76
gut	"	6.34	183.59
c6 end Return		5.8N	184.09
N		5.N	184.5
0+25			
N		3.N	186.5
+N		3.N	186.5
+3		4.7	185.2
c6		4.6	185.3
1/4		4.7	185.2
C		4.3	185.6
1/4		4.8	185.1
c6		5.1	184.8

1989.93

S	4.8	185.1
0+75		
S	5.1	184.8
c6	4.9	185.0
1/4	4.7	185.2
C	3.5	186.4
1/4	3.5	186.4
c6	3.7	186.2
N	3.N	186.7
0+50		
N	3.3	186.6
c6	4.0	185.9
1/4	4.5	185.4
C	4.7	184.2
1/4	4.N	183.7
c6	5.9	184.0
S end hedge	6.7	183.2 IN ST.
0+75		
S	8.5	181.4
c6	7.8	182.1
1/4	7.8	182.1
C	7.7	182.2
+1	7.0	182.9
1/4	6.9	183.0
c6	6.6	183.3
N	5.7	184.2

		18993		
	1+00			
N			7.3	182.6
c6			9.9	180.0
1/4			9.9	180.0
c			9.9	180.0
1/4			9.7	180.2
c6			9.8	180.1
S			10.7	179.2
	1+03			
9 S MH Rim			9.80	180.1
F.L.			16.50	173.43
	1+12			
N			10.4	179.5
c6			10.7	179.2
1/4			10.5	179.4
c			10.5	179.4
1/4			11.0	178.9
c6			10.8	179.1
S			11.1	178.8
T.P.	1+13	180.61	10.55	179.28
	1+14			
c			1.7	178.9
N 1/4			1.5	179.1

180.61

c6	1.5	179.1
+10	1.6	179.0
+13	12.0	168.6
N	12.0	168.6
+20	12.2	168.4
1+25		
+25	13.4	167.2
N	12.7	167.9
c6	11.9	168.7
+4	11.6	169.0
+5	2.1	178.5
1/4	2.1	178.5
c	2.6	178.0
1/4	3.0	177.6
c6	3.2	177.4
S	2.0	178.6
+15	2.7	177.9
1+50		
+15	4.1	176.5
S	4.5	176.1
c6	4.1	176.5
1/4	3.7	176.9
c	3.6	177.0
+45	3.4	177.2
1/4	12.0	168.6

18041

N c6			13.0	167.6
N			13.2	167.4
+20			13.5	167.1
	1+75			
-20			13.5	167.1
N			13.3	167.3
c6			13.1	167.5
+4			12.1	168.5
1/4			5.1	175.5
+2			3.3	177.3
C			3.9	176.7
1/4			4.0	176.6
c6			4.8	175.8
S			5.3	175.3
+15			5.7	174.9
	2+00			
-15			7.4	173.2
S			6.8	173.8
c6			6.2	174.4
1/4			5.8	174.8
C			5.7	174.9
+7			5.4	175.2
1/4			13.8	166.8
c6			13.6	167.0
N			13.5	167.1
+20			13.7	

18041

2+27		
-20	14.0	166.6
N	14.2	166.4
c6	14.1	166.5
+5	12.0	168.6
1/4	6.7	173.9
C	7.0	173.6
1/4	7.3	173.3
c6	8.4	172.2
S	9.0	171.6
+15	9.0	171.6
2+30 E edge - 47th. Field		
S	14.6	166.0
C	14.4	166.2
N	14.0	166.6

T.P. 9.75 / 99.98 0 3 8 180-3

check to 15' CT 591 18407 18407

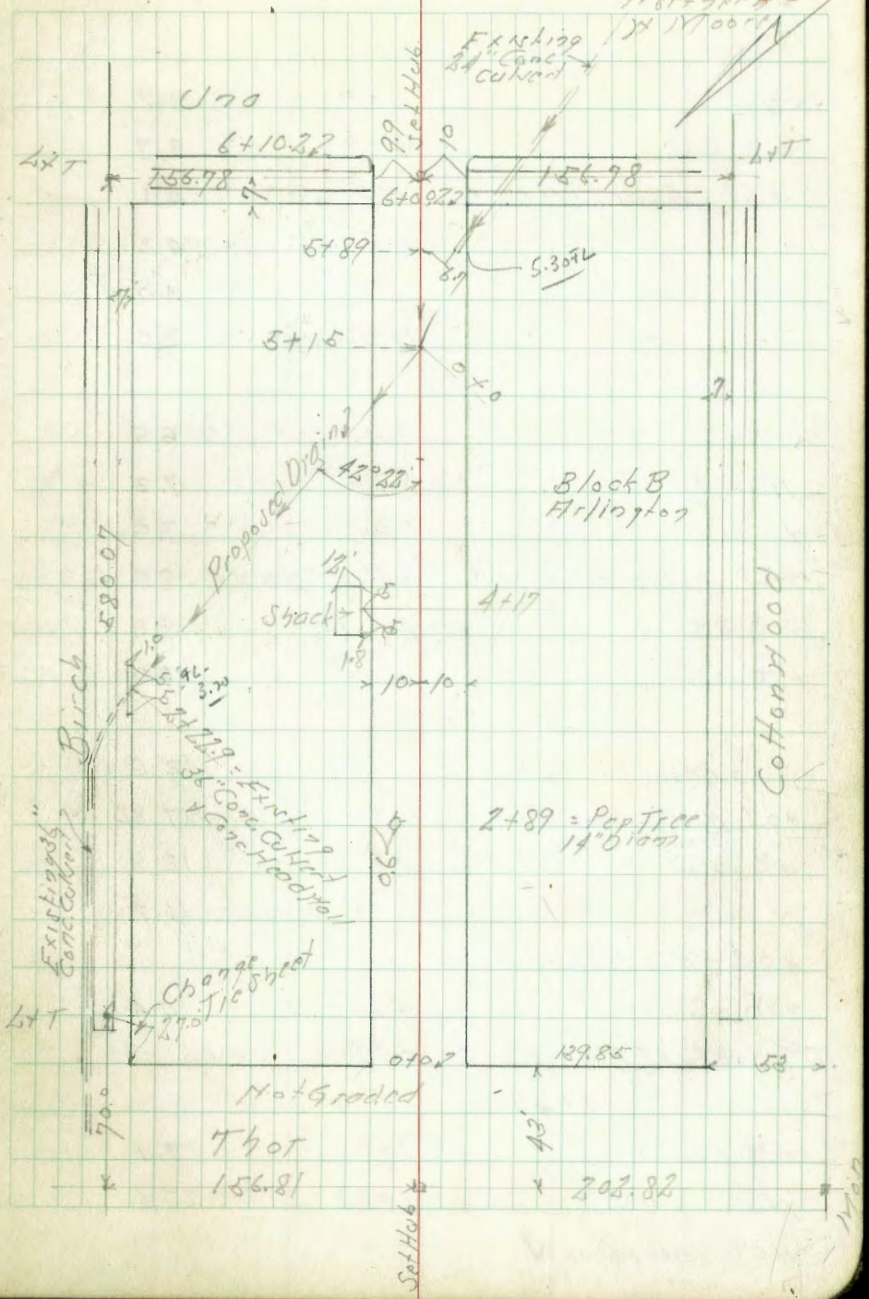
Feb-1941
Sisson
Northern

Cross Section Alley Block B Arlington
Thor to Una Between Cottonwood & Birch

Indexed

BM	6.74	13.79 ✓		7.05	S.E.B.P. Moist & Thor
TP	4.22	9.76 ✓	8.35	5.44	
TP	11.77	16.02 ✓	5.51	4.25	Hub & Alley 13' Lt Thor
		0+00 = E Δ Thor			
-10			12.1		3.9
S			12.3		3.7
+2	= W Δ Lot's Fence ✓				
Δ			12.0		4.0
N			11.6		4.4
+10			11.7		4.3
		0+18			
S+3	= S'ly Power Pole ✓				
		0+39			
-10			12.1		3.9
N			12.0		4.0
Δ			12.0		4.0
+8.8	= W'ly Conc Wall (Top) & Board Fence + E'ly Lot's Fence ✓		10.47		5.55 ✓
S			11.9		4.1
+10			12.0		4.0
		0+51			
S+1.0	= N'ly Conc Ramp		12.22		3.80 ✓
S-5.0	= S'ly " "		10.68		5.39 ✓
		0+64			
S+1.2	= E'ly Conc Wall Top		10.53		5.49 ✓

Red = Plot on New Profile 2-20-41 CSH



	16.02			
	0+70			
-10		10.7	5.7	
S		10.7	5.7	
+1.2 = Board Fence ✓		11.9	4.1	
⊄		11.8	4.2	
H		12.0	4.0	
+10		12.4	3.6	
	1+00			
-10		9.5	6.5	
H		8.7	7.3	
⊄		8.5	7.5	
+8.8 = Board Fence ✓		7.5	8.5	
S		6.5	9.5	
+10		6.0	10.0	
	1+20			
S = Base Conc Wall		3.4	12.6	
+0.4 = Hly Conc Wall Top ✓ Ground to Foot		+1.80	17.82 ✓	
⊄		3.8	12.2	
H		4.1	11.9	
+0.3 = Hly Lath Fence ✓				
+10		5.6	10.4	
TP	12.27 27.82 ✓	0.47	15.55	
	1+40			
-10		10.7	17.1	
H		10.2	17.6	
+0.7 = Lath Fence ✓				

	27.82		
⊄ ✓		9.9	17.9
+9.7 = Board Fence + Top Conc Wall		8.70	19.12 ✓
S		8.6	19.2
	1+53 ✓		
S+0.5 = Ely Board Fence + Wly Shed ✓			
	1+61		
-0.4 = Ely Shed + Wly Shed ✓			
S		4.6	23.2
+1.8 = Sly Power Pole ✓			
⊄		4.6	23.2
+9.3 = Ely Lath Fence ✓			
+9.8 = Wly Frame House ✓			
H		4.3	23.5
+10 = Wly House		6.1	21.7
	1+67		
S-0.4 = Ely Shed ✓			
	1+77		
H		1.5	26.3
+0.1 = Ely Frame Ho ✓			
+0.7 = Wly Lath Fence ✓			
⊄		1.7	26.1
S		1.7	26.1
+0.1 = Wire Fence ✓			
+10		2.0	25.8
TP 4.95 32.59 ✓	0.18	27.64	

	32.59		
	1+94		
S = ℄ Garage Dirt Floor	4.9	27.7	✓
	2+40		
S	4.6	28.0	
℄	4.4	28.2	
+9.4 = Fence			
N	4.3	28.3	
+10	4.0	28.6	
	2+07		
S-0.3 = ℄ Garage Dirt Floor	4.5	28.1	✓
	2+26		
N of 3.3' Conc Walk	3.33	29.26	✓
+0.3 = S'ly + E'ly 3.3' Conc Walk			
℄	3.8	28.8	
S	4.0	28.6	
+0.3 = N'ly + W'ly 2.5' Conc Walk + E'ly Shed	3.95	28.64	✓
	2+40		
S-0.4 = Fence			
N+0.1 = Fence			
	2+55		
-10	4.3	28.3	
S	4.3	28.3	
℄	4.2	28.4	
N	4.0	28.6	
+5	4.0	28.6	

	32.59		
	2+80		
-10	6.4	26.2	
N = E'ly Fence	5.5	27.1	✓
℄	5.5	27.1	
+7	5.0	27.6	
+7.6 = S'ly Pair Pole			✓
+8.5 = W'ly Wire Fence			✓
S = E'ly Fence	4.7	27.9	✓
+10	4.5	28.1	
	2+94		
N+0.7 = ℄ 3.3' Conc Walk	6.88	25.71	✓
	3+07		
-10	5.4	26.2	
S	5.9	26.7	
+1.5 = W Wire Fence	7.5	25.1	✓
℄	8.0	24.6	
+9.5 = S'ly Conc Wall 0.5' Wide	7.90	24.69	✓
N	8.0	24.6	
	3+35		
-10	13.8	19.8	
N	11.9	20.7	
+8	10.2	22.4	
℄	10.3	22.3	
+8.8 = W Wire Fence	10.3	22.3	✓
S	9.8	22.8	
+10	9.3	22.3	

	22.59		
3+70			
-10		11.4	21.2
S		12.0	20.6
+0.8 = Wire Fence ✓			
+5		12.7	19.9
∅		13.2	19.4
+3		13.3	19.3
N		14.7	17.9
+10		17.0	15.6
TP	0.50, 21.03	12.06	20.53
4+0			
-10		10.3	10.7
N		8.4	12.6
+8		6.6	14.4
∅		6.3	14.7
+5		6.4	14.6
+7.7 = Sly Pow Pole ✓			
+9.7 = Ely Wire Fence ✓			
S		4.3	16.7
+10		3.3	17.7
4+17			
N -1.8 = Door of Floor of Shack		10.35	10.68 ✓
4+25			
S		6.6	14.4
+0.6 = Wly Shed ✓			

	21.03			
+2		7.8		13.2
+5		9.7		11.3
∅		9.4		11.6
+5		10.4		10.6
N		10.8		10.2
+15		14.4		6.6
TP	2.22 10.94 ✓	12.31	8.72	
4+40				
S+0.5 = Ely Shed ✓				
4+70				
-15		5.8		5.1
N		5.0		5.9
+6		3.3		7.6
∅		3.5		7.4
+6		3.3		7.6
S		1.0		9.9
+10		0.0		10.9
4+80				
S+0.1 = Wly Wire Fence ✓				
5+0				
-10		2.2		8.7
S		2.3		8.6
+0.5 = Wire Fence ✓				
+2.6 = Sly Pow Pole ✓		3.1		7.8
∅		4.6		6.3

10.94

N	5.0	5.9
+15	5.3	5.6
5+20		
-10	5.2	5.7
N	4.5	6.4
+0.1 = Wly Wire Fence ✓		
S	5.0	5.9
+9.6 = Ely Wire Fence ✓		
S	3.1	7.8
+10	2.5	8.4
5+27		
N-1.5 = Sly 10' Shed ✓		
5+36		
N-0.2 = Sly 75 Shed ✓		
5+40		
-10	5.8	5.1
S	5.0	5.9
S	4.9	6.0
N	5.0	5.9
+10	4.8	6.1
5+60		
-10	4.6	6.3
N	4.4	6.5
+0.2 = Ely Wire Fence ✓		
S	4.8	6.1

10.94

+7	4.9	6.0
S	4.2	6.7
+9.2 = Nly Wire Fence ✓		
+10	3.9	7.0
5+89 = Opp. Existing 18" Culv		
S	3.0	7.9
+2.3 = Outlet 18" Conc Culv Flow Line	5.64 ✓	5.30
+7	4.4	6.5
S	4.3	6.6
+5	4.2	6.7
+9.3 = Fence ✓		
N	3.9	7.0
+10	3.8	7.1
6+00.2 Wly Dip		
N Top Cb	2.33	8.61
Gutter	3.9	8.0
S	3.5	7.4
Gutter	3.0	7.9
S Top Cb	2.28	8.66
6+10.2 = Wly Cb Dip		
S Top Cb	2.44	8.50
Gutter Ground	3.0	7.9
S	3.2	7.6
Gutter Ground	3.0	7.9
N Top Cb	2.37	8.57

Proposed Drain Across Block 8 Arlington

		10.94		See Sketch Page 50	
0+0 =	5+15 Z Alley		4.8	6.1	
+50			5.7	5.2	
1+0			6.0	4.9	
+50			6.3	4.6	
2+0			6.6	4.3	
+22.9 = 24.7	Flow Line Existing 36" Conc Culv		7.74	3.20	
	Top Conc. Head Wall		3.16	7.78	
TP	12.49	20.33	3.10	7.84	
BM			6.75	13.58	N.W.P. Tack Cottonwood + Cmo
TP	2.20	21.24	1.29	19.04	
BM			7.78	13.46	S.E.B.P. Maintained 13.46

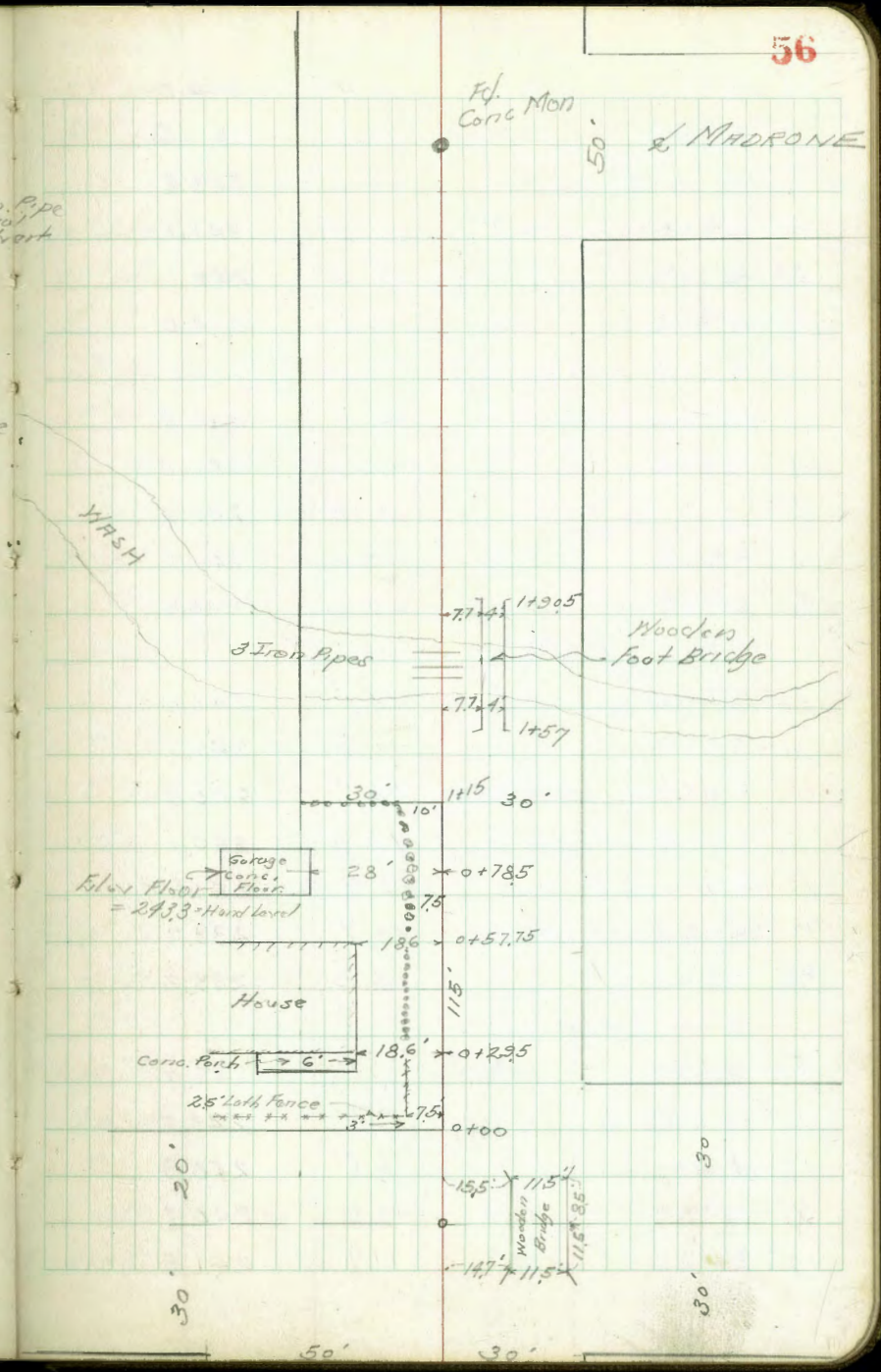
Walker Bl. 88
5-14-41

69TH St. & Levels from JAMACHA to MADRONE.

See p. ~~72~~ 40 = Survey.

		1.59	255.03		253.44	BM. top 2" Iron Pipe 69th & Imperial SW. Cor Box Culvert
T.P.	#1	3.30	~~250.58~~ 250 58	P-58 5	247 28	
		~~3.33~~	250.68	7.74	247.29	
		0 - 11.5 - South end Wooden Bridge				
21.2' Rt. on Bridge				4.56	246.03	
" " "		Flow		6.9	243.7	Under Bridge
0+00				4.9	245.8	
+50				5.3	245.3	
1+00				5.4	245.2	
			253.37	6.30	244.28	P-58
T.P.	#2	9.09	~~253.98~~	~~5.79~~	244.89	
		1+48				
℄				9.3	244.1	
12' Rt.				8.6	244.8	
19' Rt.				10.4	243.0	
25' Rt.				10.8	242.6	
27' Rt.				9.1	244.3	
30' Rt.				9.1	244.3	
10' Lt.				9.6	243.8	
30' Lt.				9.1	244.3	
		1+53				
30' Lt.				9.0	244.4	
12' Lt.				8.9	244.5	
10' Lt.				9.7	243.7	
℄				9.4	244.0	

Plotted on Profile 1-15-41 CBH



~~25398~~ 25337

2' Rt.		9.4	244.0	
5' Rt.		11.8	241.6	
7.7 Rt.	High Pt. on Bridge	7.6	245.8	
15' Rt.	in channel	12.3	241.1	
28' Rt.		11.3	242.1	
30' Rt.		9.4	244.0	
	1+58			
30' Rt.	in channel	12.6	240.8	
15' "	" "	12.6	240.8	
℄	" "	11.8	241.6	
15' Lt.		12.6	240.8	
30' Lt.	" "	12.6	240.8	
	1+70 - ℄ channel			
30' Lt.	in channel	11.4	242.0	
15 "	" "	11.7	241.7	
11' "	Flow 2' Iron Pipe	12.5	240.9	
℄	in channel Iron	13.3	240.1	
13' Rt.	end 2' Pipe	12.8	240.6	Flow
13' Rt.	in channel	13.7	239.7	
30' "	" "	14.2	239.2	
	1+80			
30' Rt.		9.7	243.7	
16' Rt.	on Bank	9.7	243.7	
13' Rt.	in channel	12.5	240.9	
℄	" "	12.6	240.8	
12' Lt.	" "	11.9	241.5	

~~25398~~ 25337

17' Lt.	on Bank	10.4	243.0
30' Lt.	" "	10.0	243.4
	1+85		
30' Lt.		10.4	243.0
15' Lt.		10.0	243.4
℄		9.4	244.0
7.7 Rt.	on Ft. Bridge	7.6	245.8
13' Rt.		9.6	243.8
30' Rt.		9.6	243.8
	2+00		
30' Rt.		9.3	244.1
16' Rt.		9.8	243.6
14' Rt.		8.5	244.9
℄		9.1	244.3
13' Lt.		10.1	243.3
15' Lt.		8.7	244.7
30' Lt.		8.7	244.7
	2+25		
30' Lt.		8.6	244.8
15' Lt.		8.7	244.7
℄		8.5	244.9
15' Rt.		9.1	244.3
20' Rt.		9.6	243.8
30' Rt.		9.7	243.7
2+50 - ℄		6.0	247.4
2+75 ℄		3.0	250.4

		253.37 / ~~253.98~~		69TH St.	
T.P	12.55	265.56 / ~~266.17~~	0.36	253.01 / ~~253.62~~	
3+00 ℄			12.0	253.6	
+25			8.5	257.1	
+50			4.6	261.0	
+75			0.3	265.3	
		277.82		264.68	
T.P	13.14	~~278.43~~	0.88	~~265.29~~	
4+00			9.1	268.7	
+25			5.9	271.9	
+50			2.6	275.2	
		286.02		276.96	
T.P	3.06	~~282.63~~	0.86	~~277.57~~	
4+75			7.4	278.6	
5+00			4.9	281.1	
+25			3.5	282.5	
+50			2.3	283.7	
+90			1.6	284.4	
6+00			4.1	281.9	
+30.9 = N.L. Madrone			5.9	280.1	
				278.11	on Conc.
+55.9 = ℄ "			7.91	~~278.72~~	Mon.
		273.58		273.13	
T.P	0.45	~~274.19~~	12.89	~~273.74~~	
		260.92		260.53	
T.P	0.39	~~261.53~~	13.05	~~261.14~~	
		250.14		248.08	
T.P	2.06	~~250.75~~	12.84	~~248.69~~	
		253.90		247.69	
T.P. Iron Pipe	6.21	~~254.51~~	2.45	248.30	
chk. Stirling B.M.			0.44	253.46	69th + Imp.
				253.44	
				0.02	Error,

Recheck T.Rs from Stirling B.M.

044	253.88			253.44	
T.P #1	330	250.58	660	247.28	chk T.P. #1 D-56
chk T.P. #2			630	244.28	- 0.61 Low
chk. 0+00 ℄			4.7	245.9	0.1
chk 1+48			6.4	244.2	

Survey Lease Mission Beach Amusement Center

Indexed
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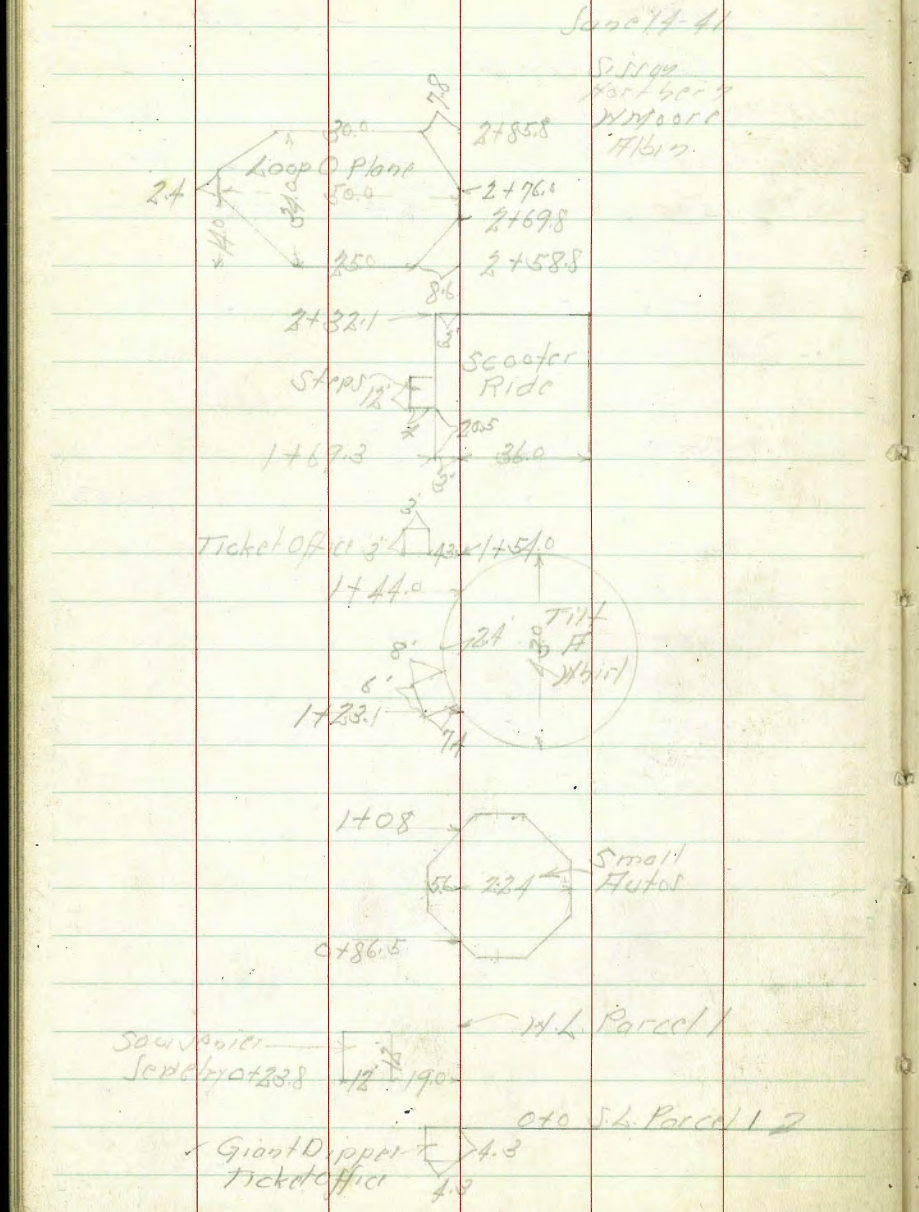
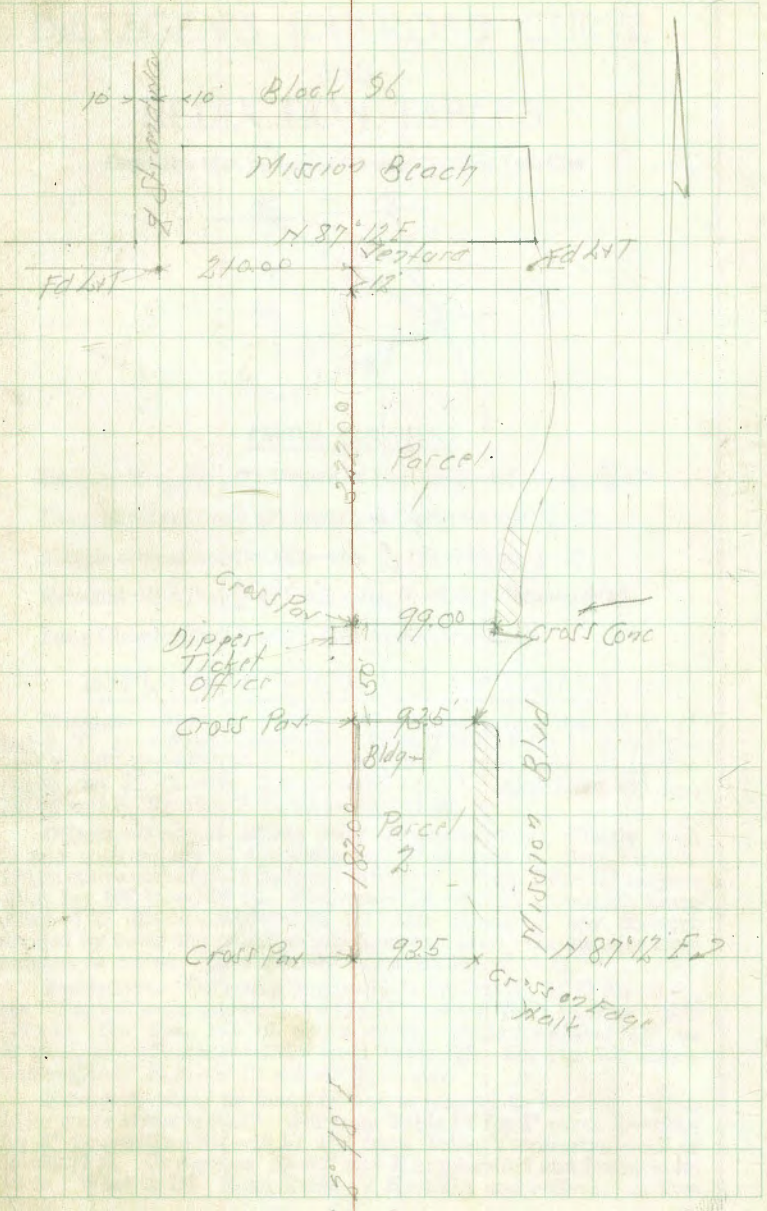
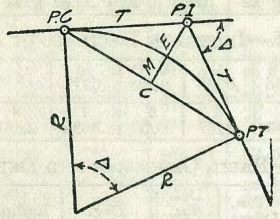




DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES



CURVE FORMULAS

Radius=R=$\frac{50}{\text{sin. } D/2}$ (1) Degree of Curve=D and sin. $\frac{D}{2}=\frac{50}{R}$ (2)

Tangent=T=R tan $\frac{\Delta}{2}$ (3) Length of Curve=L=$100\frac{\Delta}{D}$ (4)

Middle ordinate=M= R(1—cos. $\frac{\Delta}{2}$) (5) =R vers $\frac{\Delta}{2}$ (6)

External=E=T tan $\frac{\Delta}{4}$ (7) =R÷cos. $\frac{\Delta}{2}$—R (8)=R exsec $\frac{\Delta}{2}$ (9)

Long Chord=C=2 R sin. $\frac{\Delta}{2}$ (10) Δ=Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. Δ=62° 10′ D=8° 20′. From Table IV for 1° curve T=3454.1 and÷8⅓=414.49 ft. From Table V correction=.36 or T=414.85 ft. P. C.=Sta. P.I.—T=157+45.50. Also from (4) L=746.00 and P. T.=Sta. P. C.+L=164+91.50.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset=7.27 (54.50÷100)²=2.16 ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus (54.50)²÷(2 x 688.26)=2.16 ft.

Deflections.—Deflection angle=½ D for 100 ft., ¼ D for 50 ft., etc. For c ft.=(in minutes) .3 x C x D° or=defl. for 1 ft. from Table III x C. For Sta. 158 of above curve=.3 x 54.5 x 8⅓=136.2′ or 2° 16.2′, or=2.50 x 54.5=136.2′ from Table III. For Sta. 159 deflection angle=2° 16.2′+8° 20′÷2=6° 26.2′, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve E=960.6 for 8° 20′=960.6÷8⅓=91.27 and from Table V correction=.10 or E=91.37 ft. Or suppose Δ=32° and E is measured and found to be 42 ft. What is D? From Table IV E=230.9 and÷42=5.5 or D=5° 30′.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)÷2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.

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