1594

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

Waterline in Nursery Page 75 —

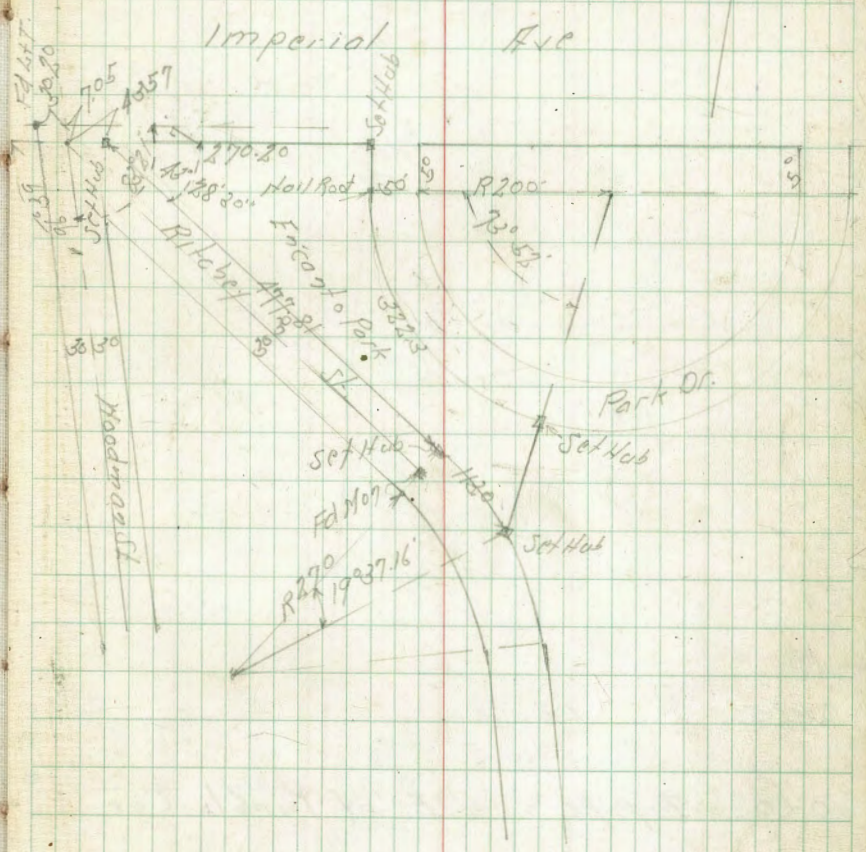
Sewer " " 80 —

Survey Encanto Park
Encanto Park Addition
Map No 1228

Indexed
C.S.K.

1

Feb 2-12
Station
Workbook
W Moore



Alignment Change Del Mar La Jolla Pipeline
Through Artillery Replacement Center
Torrey Pines Mesa

~~9+34.06~~ Δ Lt. 0°02'30" = ℄ 9+10

9+29.34 Δ LT. 2°34'

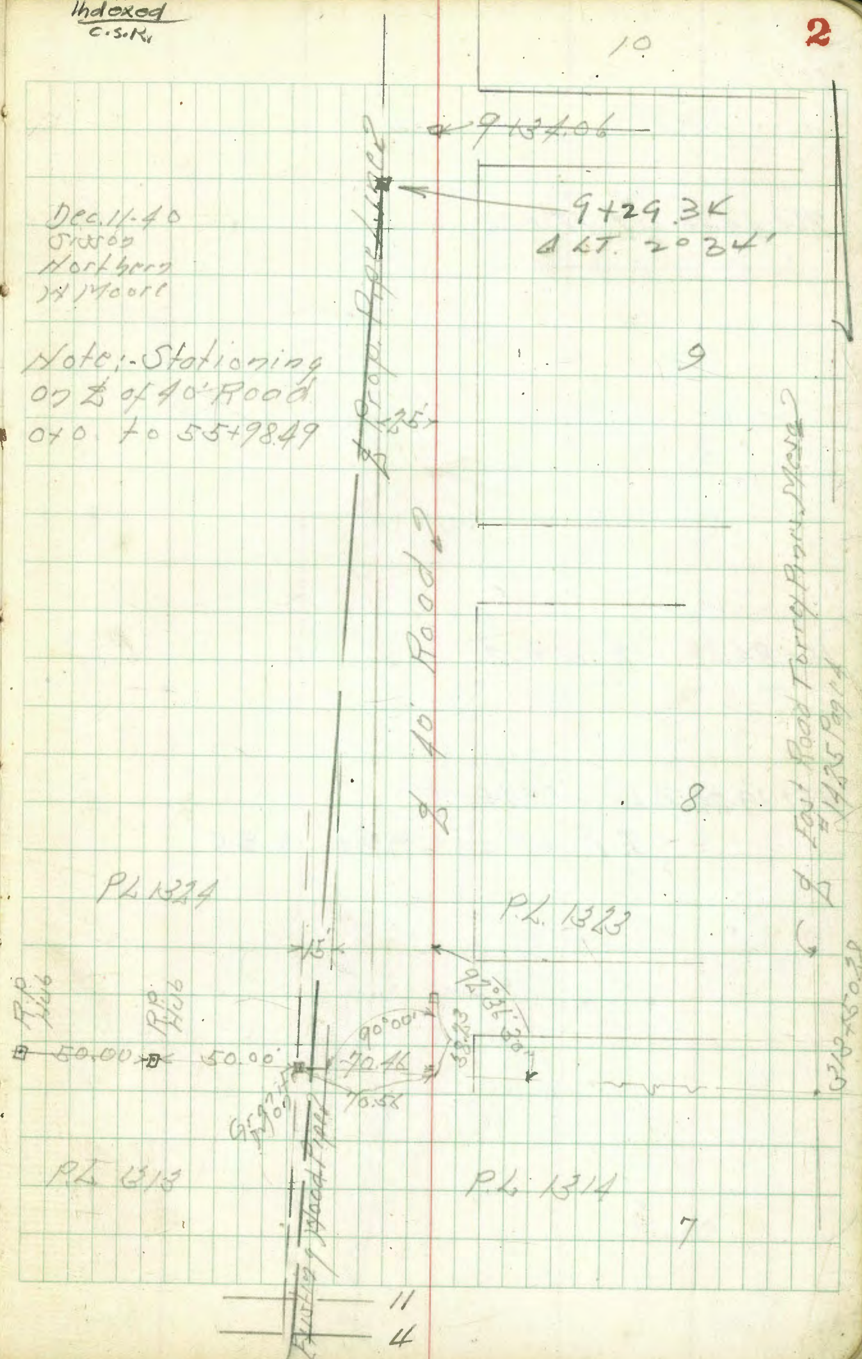
0+35 = ℄ 7+8

0+0 = ℄ pipe = 4' E of Pueblo Cor.

Indexed
C.S.K.

Dec 11-40
Strong
Northern
H Moore

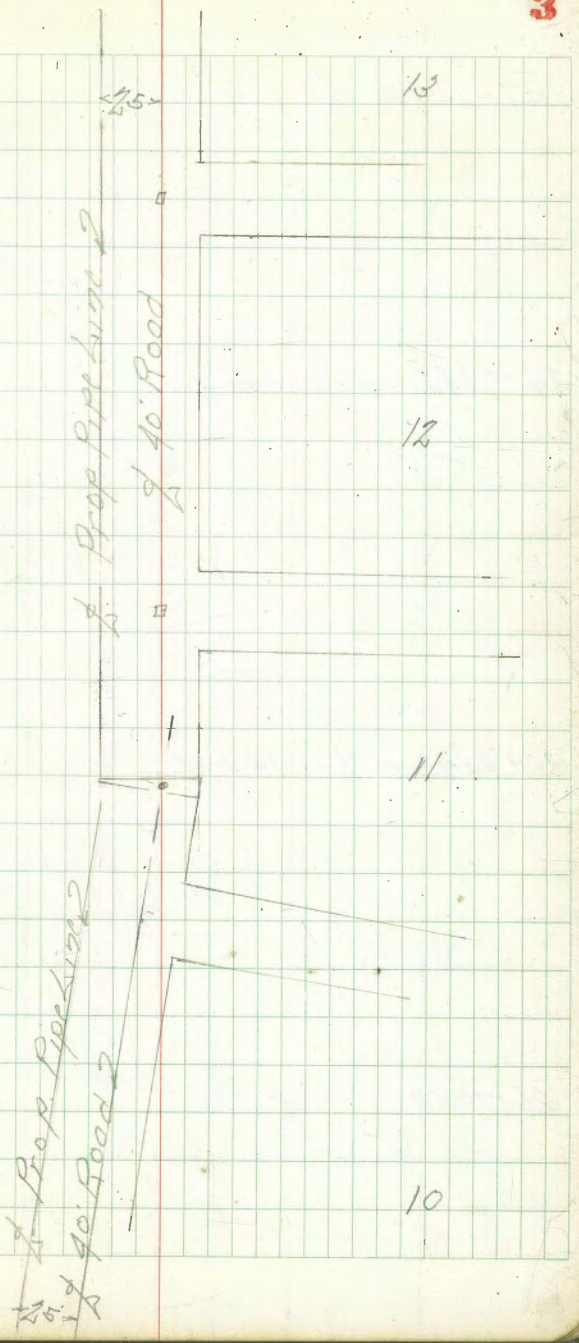
Note:- Stationing on ℄ of 40' Road 0+0 to 55+98.49



21+44.36 = ℄ 12 × 13

16+84.27 = ℄ 11 × 12

15+39.24 Δ Lt. 5°45'15"
ER of 1" pipe 650'

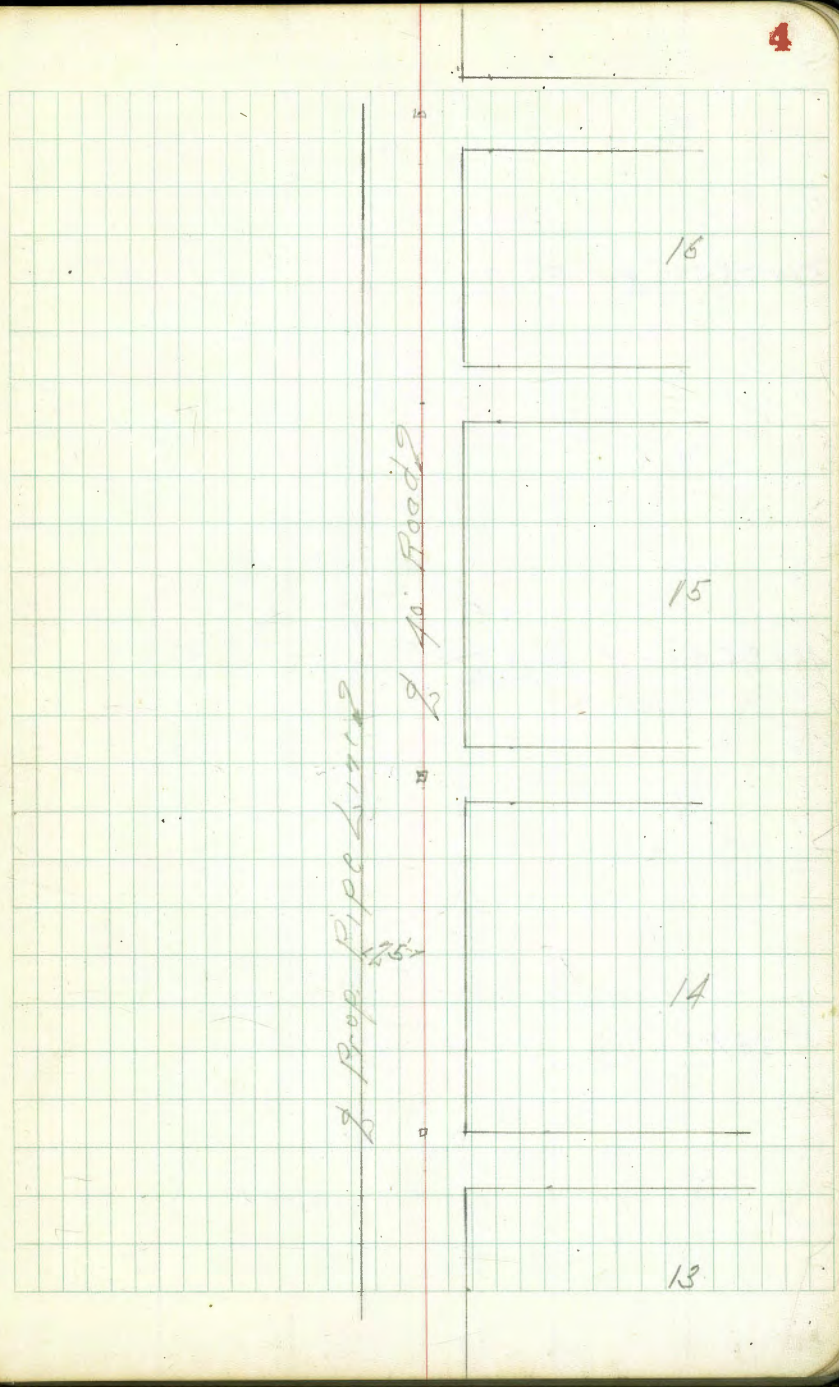


37+86.44 = ℄ 16×17

24+96.42 = ℄ 15×16.

30+48.42 = ℄ 14×15

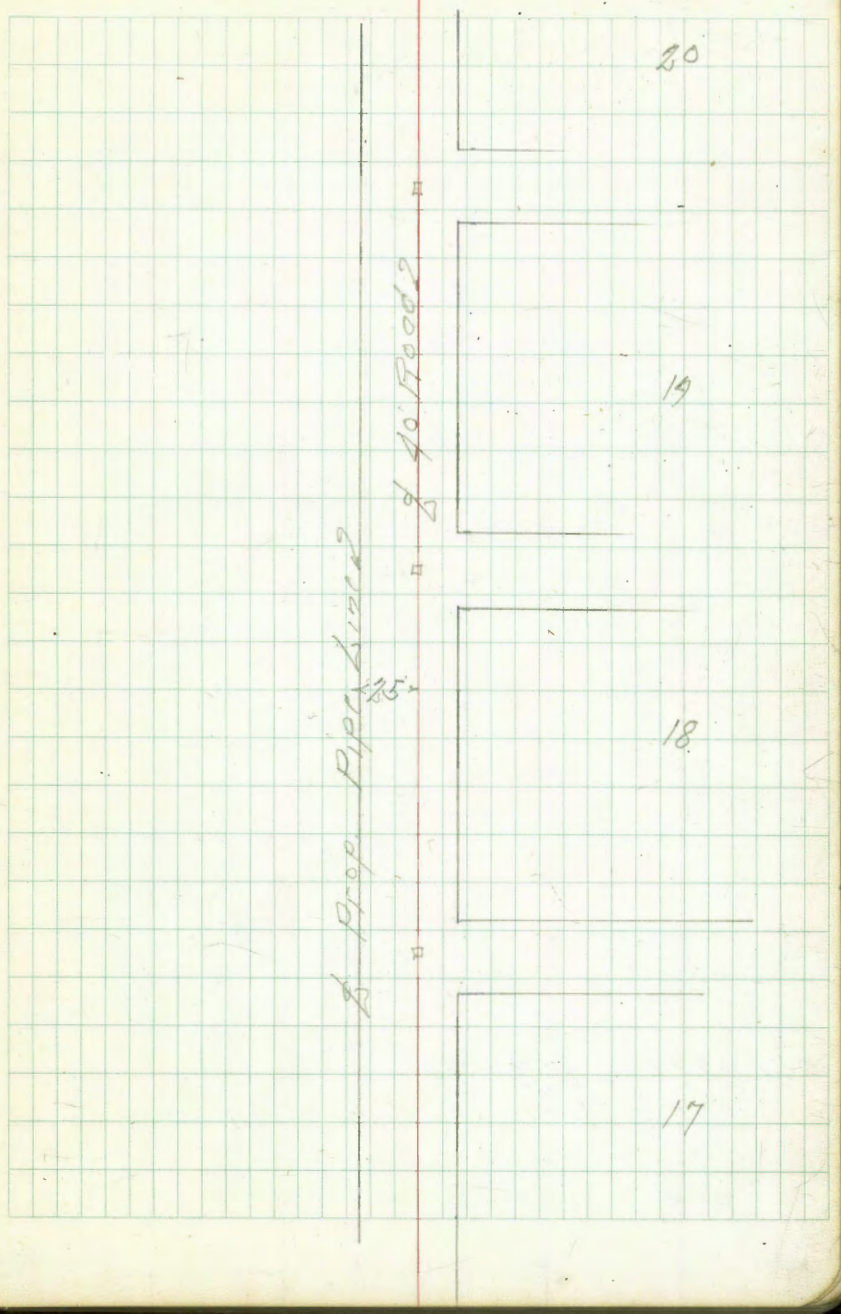
26+10.44 = 54.81×14



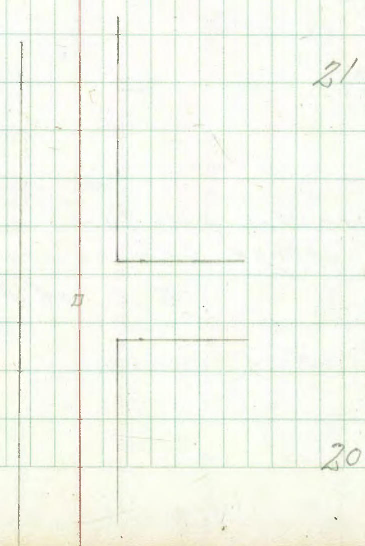
51+38.50 = Δ 19×20

46+85.53 = Δ 18×19

42+39.50 = Δ 17×18



55+9849 = 2 20 + 21



Moore
Osborne
Hale
12-16-40.

Proposed 21" Conc. Pipe line Thru Pueblo lots 1314 & 1311

Δ = 22° 35' Rt
R = 600
T = 119.8
L = 236.50

36+02.29 New P.I.

35+75.84 o/d P.I.

34+21 Tee to Marine Rifle Range

31+78 6" Tee to Marine Rifle Range

26+38.90 Δ 0° 01' Lt.

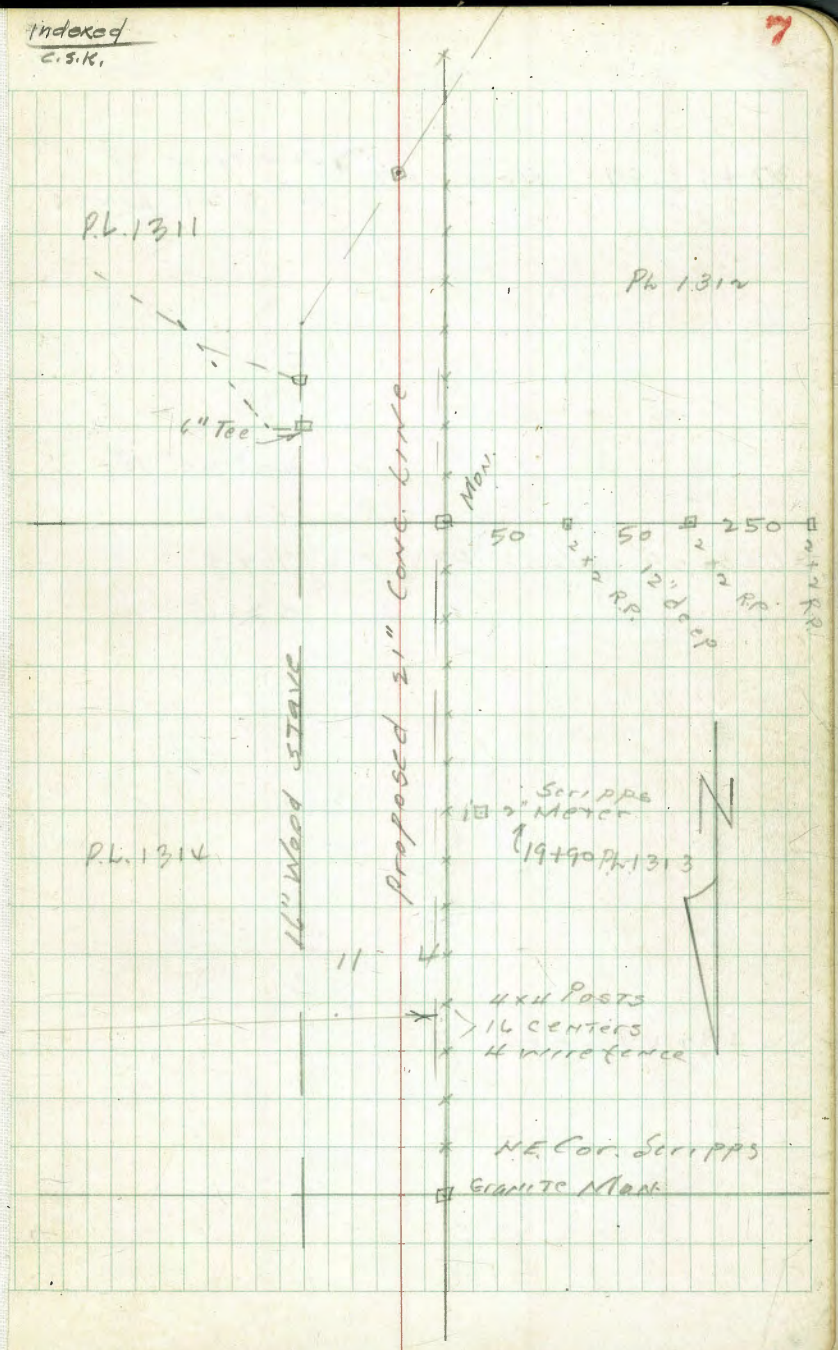
19+90 2" Scripps Meter

2 wire Tel. pole line
approx. 250' centers
" 1.5 E of Pueblo line

0+00

Indexed
C.S.K.

7

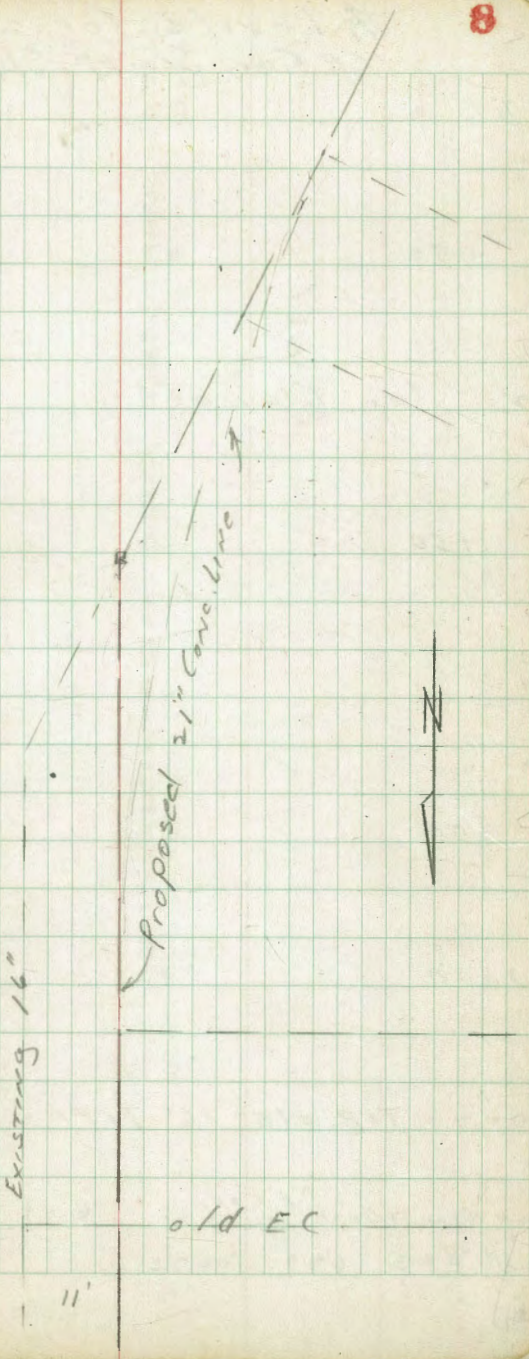


37+18.99 New E.C. Junction of 16" & 21" Lines

Δ 22° 35' Rt
R 600
T 119.8
L 236.5

36+02.29 New P.I.

34+82.49 New B.C.



℄ Levels for 21" Conc. Pipe
NE Cor. Scripp Sly

3

+50

2 for Blowoff

+50

1

+50

0+00

0-40 Top old 16" Pipe

on Gran. Mon NE Cor. Scripps	✓	6.99		355.58	355.64
B.M. #65	6.39	360.57		354.18	1½" Pipe

LT ℄ RT

355.1 ✓
5.5
355.1 ✓
5.5
354.8 ✓ 353.8 ✓
5.8 4.8
20
355.0 ✓
5.6
355.0 ✓
5.6
355.6 ✓
5.0
354.7 ✓
5.9
352.9 ←
7.70
11

360.57

1+50				
6				
2+50				
T.P.	1 w 3x	368.75	4.16	356.41
5				
1+50				
x				
3+50				
		360.57		

360.0
8.8
358.0
10.8
347.9
11.9
368.75
355.8
12.8
355.2
355.1
5.5
355.0
5.6
360.57

+50

10

+50

9

+50

8

+50

7+00

368.75

N

368.8 ✓

0.0

367.3 ✓

1.5

366.3 ✓

2.5

365.8 ✓

3.0

364.2 ✓

4.6

363.3 ✓

5.5

363.4 ✓

5.4

361.7 ✓

7.1

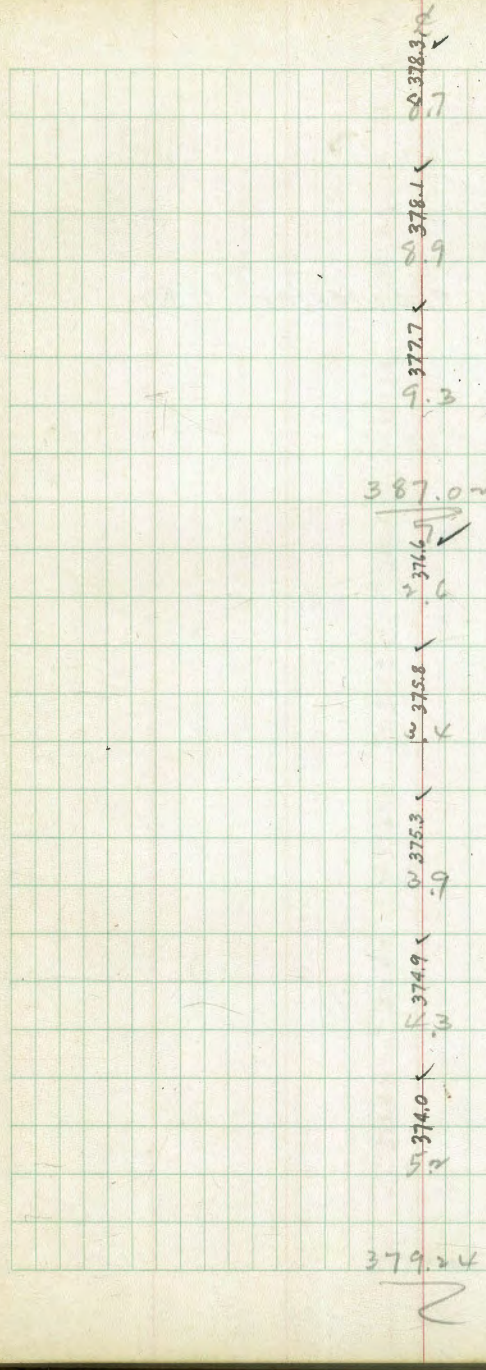
368.75 ✓

+50				
14				
+50				
13				
+50				
12				
+50				
11+00				
T.P.	10.70	379.24	0.21	368.54
		368.75		

374.2 .0
373.8 .4
373.6 .6
372.4 1.8
371.8 2.4
372.0 2.2
370.7 3.5
369.9 4.3

379.24

+18				
18				
+50				
T.P.	9.8	387.0	2.0	377.18
17				
+50				
16				
+50				
15				
		379.24		



20		382.1 ✓	4.9	
+90	2" Scripps Meter 6' Rt	381.8 ✓	5.2	2" Meter to 6 Scripps
+50		381.1 ✓	5.9	
19		380.4 ✓	6.6	
+50		378.9 ✓	8.1	
+75		377.9 ✓	9.1	
+24		375.4 ✓	11.6	
+19		375.4 ✓	11.6	
	387.02		387.02	

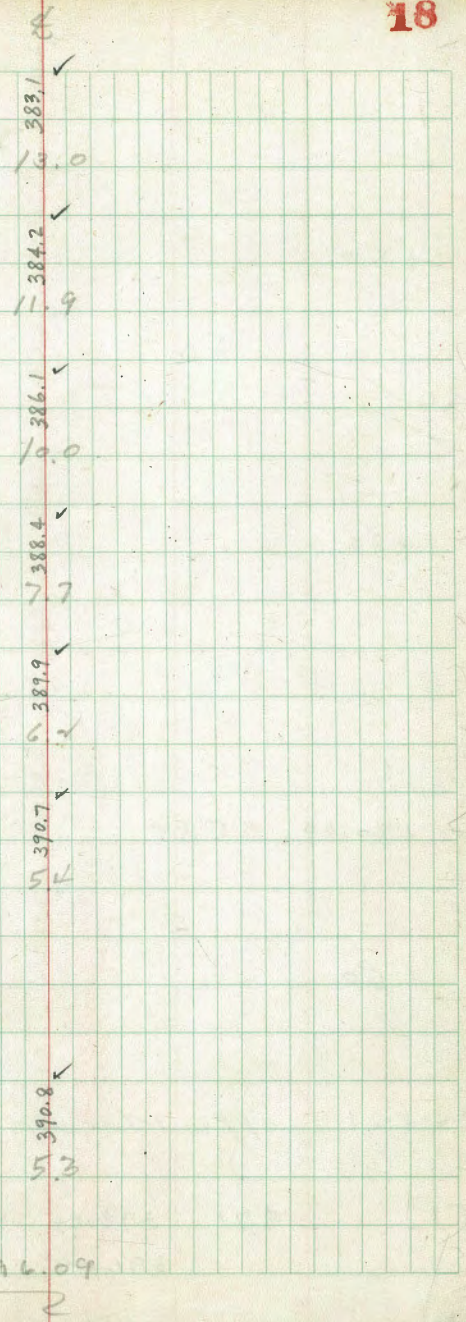
~4					
+50					
~3					
+50					
T.P	9.50	394.77	1.75	385.27	
~2					
+50					
~1					
+50					
B.M.#50			5.59	381.43	381.46
		387.0~			

388.0
386.4
385.5
385.1
394.77
384.5
383.8
383.6
383.1
387.0~

31				
+50				
30				
+50				
29				
+50				
+25				
T.P.	9.74	396.09	8.42	386.35
28				
		394.77		

391.2
4.9
390.6
5.5
390.0
6.1
389.4
6.7
388.2
7.9
386.1
10.0
386.1
10.0
396.09
386.4
8.4
394.77

34					
+50					
33					
+50					
32					
+78	OPP. Marine Toe				
+75	BM #53	15' Rt.	4.56	389.51	389.58
+50					
		396.09			



37					
+50					
36					
+50					
35					
+82.49	B.C. RT.				
+50					
34+21	opp.	Marine Tec			
T.P.	9.71	393.65 ✓	12.15	383.94 ✓	
		396.09			

LT | RT

8 386.6 ✓

7.1

383.8 ✓

9.9

Top 16" → 11.30 / 4' 382.35 ✓

382.5 ✓

11.2

384.0 ✓

9.7

384.9 ✓

8.8

Top 16" → 10.95 / 11 382.7 ✓

384.6 ✓

9.1

383.8 ✓

9.9

383.0 ✓

10.7

393.65

44 + 20				
T.P.	9.55	384.87	10.63	376.32
43 + 15				
40 + 95				
T.P.	7.96	386.95	9.66	383.99
38 + 60				
37 + 60	from E.C. Sly Rods = Top 16" pipe			
37 + 18.99	New E.C.			
		393.65		

16" x 16" wood Stave

373.8
11.10
384.87
376.7
10.26
379.1
7.88
386.95
386.0
7.72
386.6
7.10
387.5
6.72 = ground
393.65

385.9
7.8
Top 16"

54+08	Top E. Pav.		4.77	375.98	of old
53+80					
T.P.	5.97	382.75	8.09	374.78	
53					
51					
50+00					
48+95					
47+78	Blowoff & City 4" Connection to City Pump of Pueblo Farm				
46+05					
		384.87			

Biological Rd

2 old 16"

374.5
8.73
382.75
375.2
7.63
378.5
4.60
379.2
5.70
377.9
7.50
369.9
15.00 short Trestle
372.4
14.50
384.87

69+70	= air valve			
T.P.	0.02	348.97	12.44	348.95
68				
65+80				
T.P.	0.66	361.39	12.93	360.73
T.P.	0.75	373.66	4.96	372.91
T.P.	0.27	377.87	11.36	377.60
62+40				
60+40	4" Stand pipe			
59				
TP	6.54	388.96	0.35	382.40
54+75				
		382.75		

330.3 ½ old 16" on Top

18.70

See F.B. 1070 p2 and 26

348.97

345.4

16.0

358.2

32.0

361.39

376.0

12.95

381.3

7.69

381.9

7.02

388.96

375.3

7.45

382.75

Moore
Osborne
S'Meyer
5-1-41.

Survey and levels for Contours of Balboa Park Nursery N. of Navy Hospital

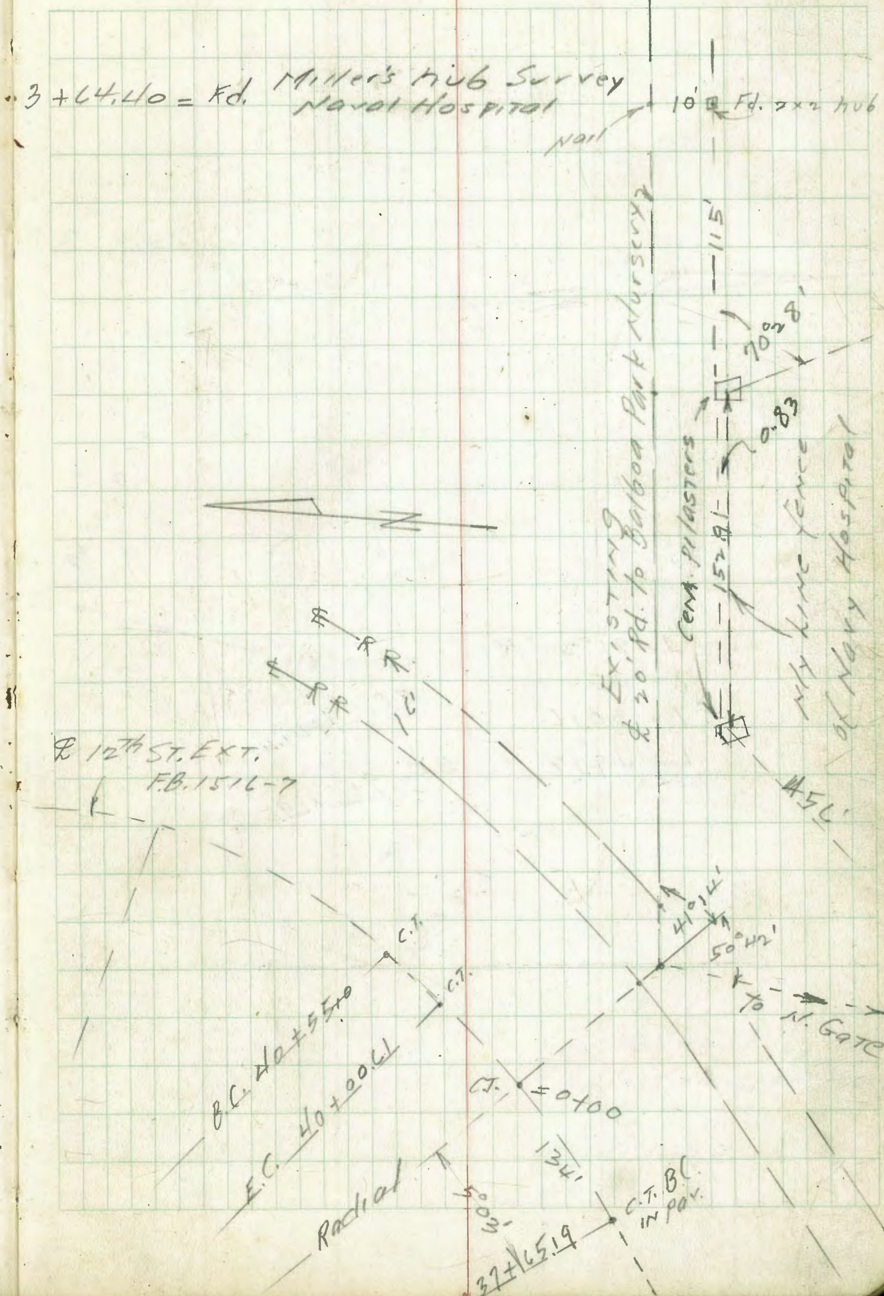
0 + 61.18 ℄ of S Track

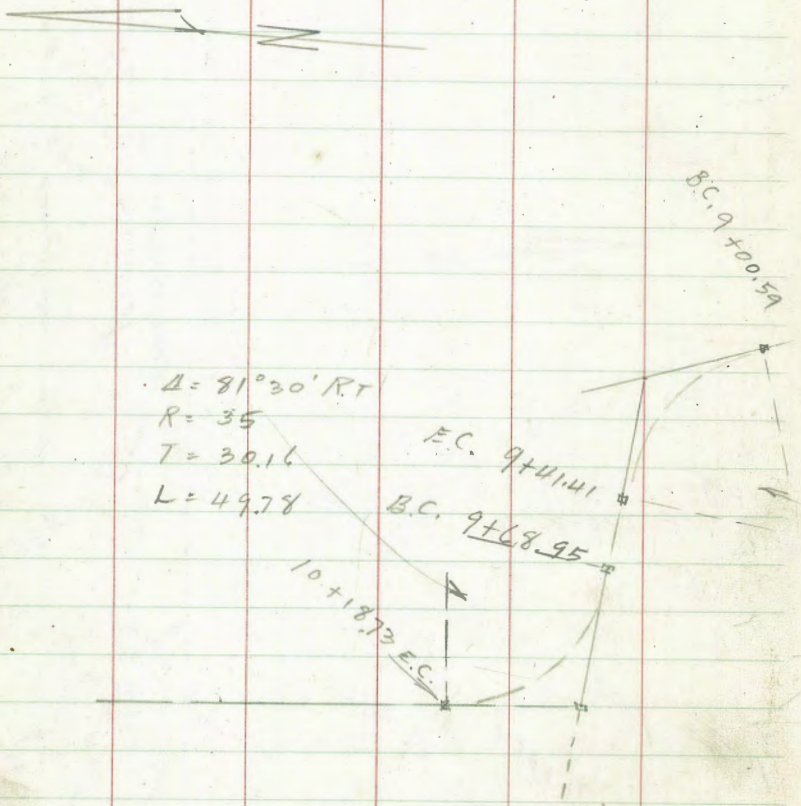
0 + 51.27 Δ 41°14' LT   Cop Tack in Pav

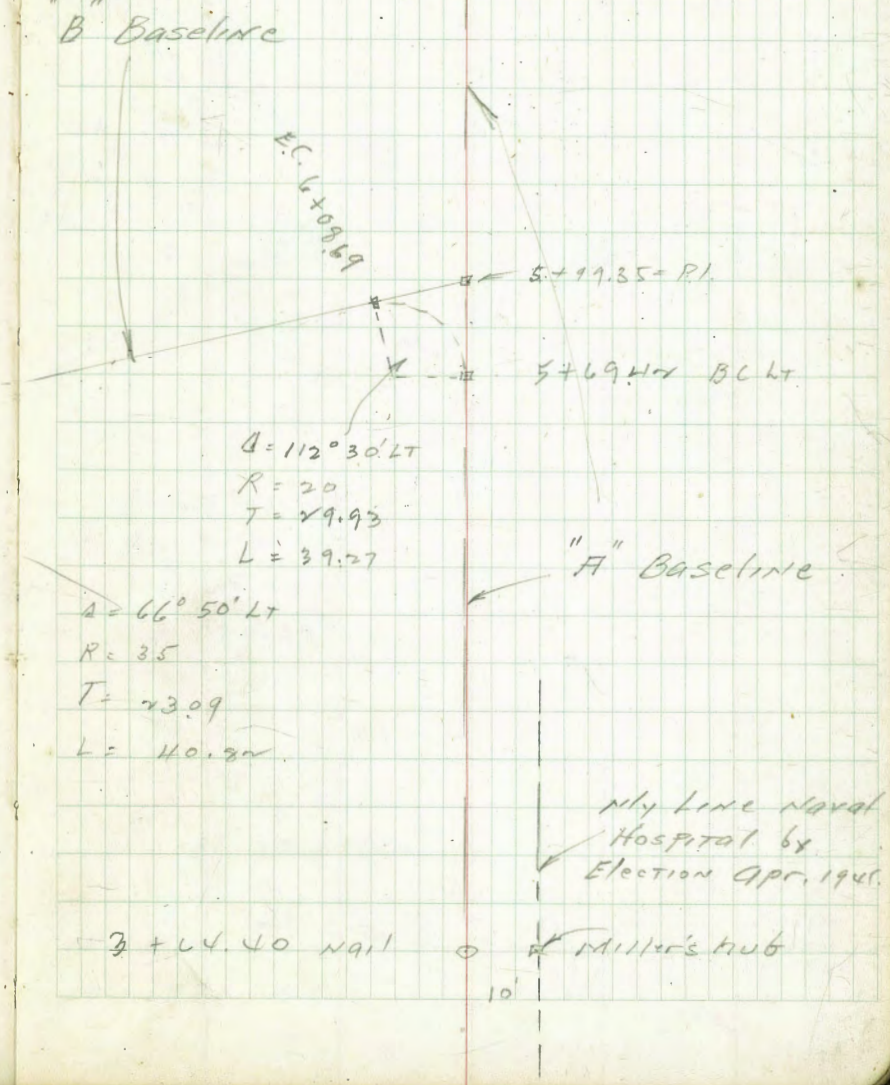
0 + 42.42 ℄ of N. St. RR Track

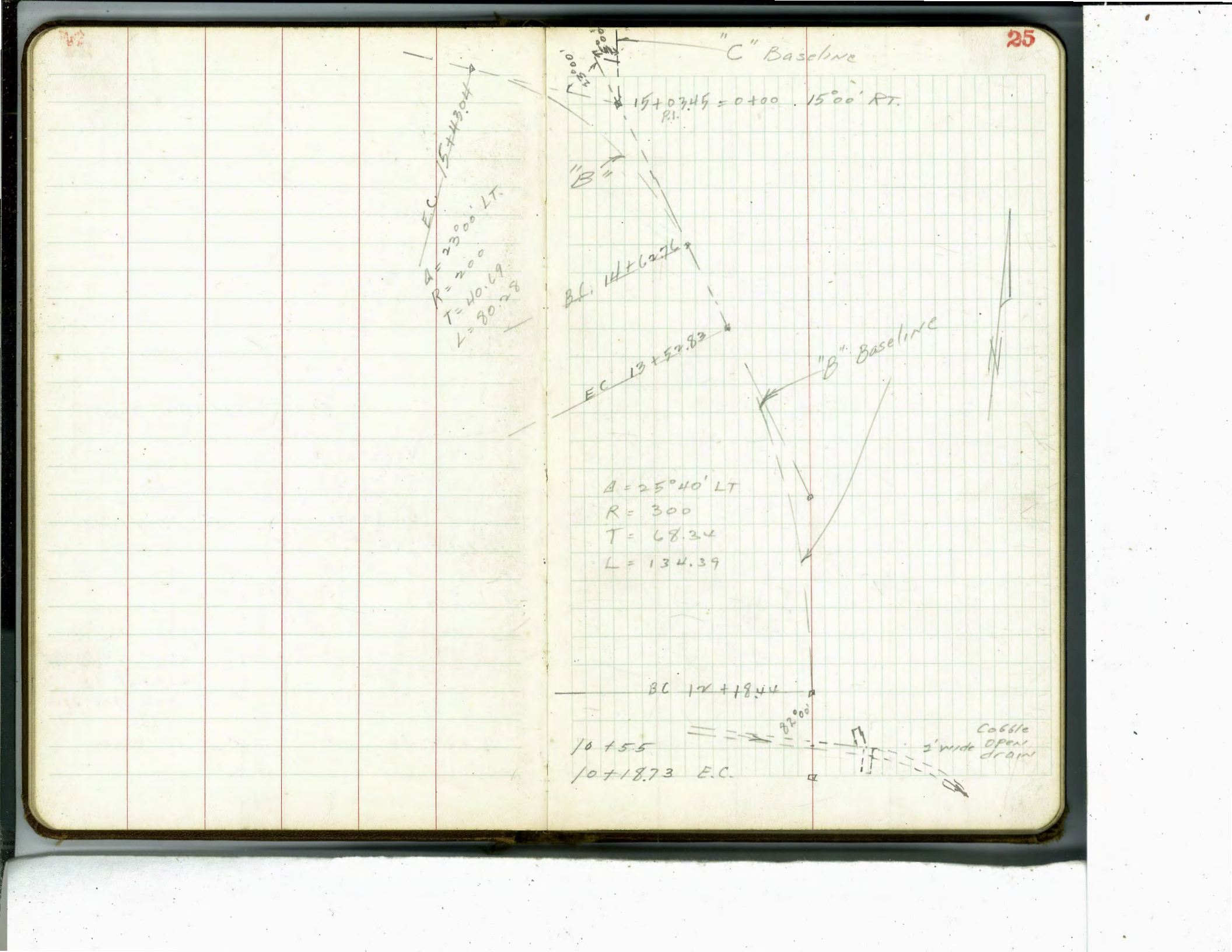
0 + 00 = ℄ 12th St Ext.   Field Bk. 1516-7

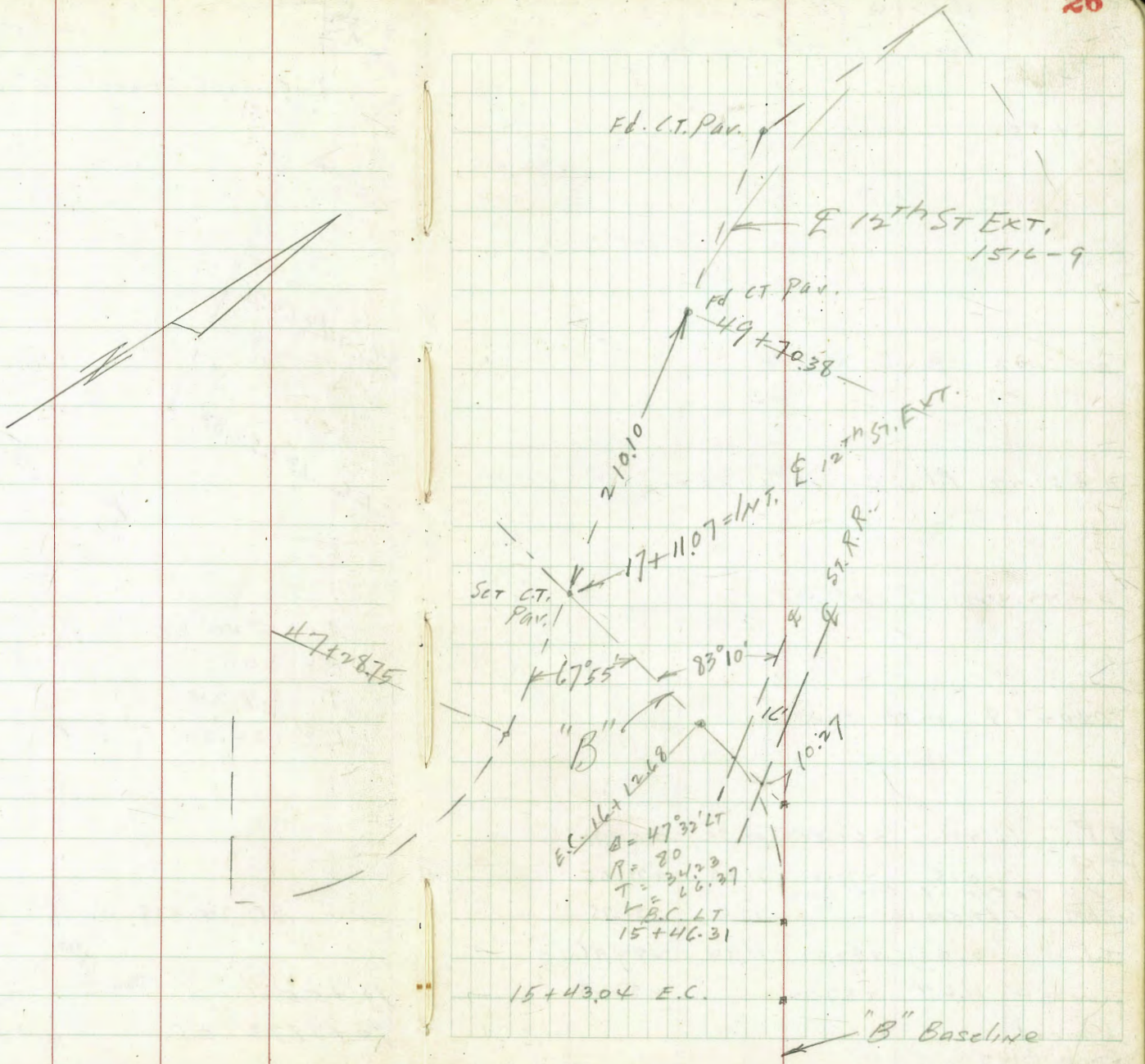
indexed
c.s.k.




Δ = 81°30' Rt
R = 35
T = 30.16
L = 49.78
B.C. 9+00.59
E.C. 9+41.41
B.C. 9+68.95
10+18.73 E.C.


"B" Baseline
E.C. 6+89.69
5+11.35 = P.I.
5+69.44 BC Lt
Δ = 112°30' Lt
R = 20
T = 29.93
L = 39.27
"A" Baseline
Δ = 66°50' Lt
R = 35
T = 23.09
L = 40.90
nly Line Naval Hospital 6x Election Apr. 1941.
3+44.40 Nail
Miller's hub
10'


"C" Baseline
15+03.45 = 0+00 . 15.00' RT.
P.I.
"B"
B.C. 14+62.76
EC 13+57.83
"B" Baseline
Δ = 25°40' LT
R = 300
T = 68.34
L = 134.39
BC 12+18.44
82°00'
10+55
10+18.73 E.C.
Cobble
2' wide
open
drain
EC 15+43.04
Δ = 23°00' LT.
R = 200
T = 40.69
L = 80.28


Fd. C.T. Pav.
℄ 15th ST EXT.
151C-9
Fd CT Pav.
49+70.38
℄ 12th St. Ext.
N 10.10
17+11.07=INT.
St. R.R.
SCT C.T. Pav.
47+28.75
67°55'
83°10'
"B"
10.27
12.68
B = 47°33' LT
R = 80
T = 34.23
L = 66.37
E.C. LT
15+46.31
15+43.04 E.C.
"B" Baseline

Levels for Contours
Sec.s at 90° off Baseline

+50

1

0+61.18 ℄ S RR Tr.

0+51.27 P.I. Δ 41°14' LT

0+42.42 ℄ N RR Tr.

0+00 ℄ 12th Pav.

T.P.	2.71	261.61	12.90	258.90
T.P.	0.15	271.80	11.86	271.65
Set BM. SE Cor of Metal Base of LT Stand.			1.26	281.75
T.P.	0.55	283.51	4.94	282.96
NW BP	4.62	287.90		283.28

Laurel Park Blvd

LT "A" RT

256.0 / 5.6 / 85	253.7 / 7.9 / 50	4' Eucal. / 16	252.21 / 9.4
Toe RR fill			
			254.31 / 7.3
			255.56 / 6.05
			255.33 / 6.28
			255.26 / 6.35
			255.01 / 6.60
			261.61

4 + 50					
599.35 - P.T.					
T.P.	5.80	258.92	8.9	253.12	
5 + 69.42	B.C. LT.				
4 + 10					
	RAIN				
3 + 64.40 ✓					
+ 68					
2					
1 + 89					
		261.61			

LT "Ⓐ" RT

B.C. = RIM CANON

LT				"Ⓐ"
			244.2 / 14.7 / 50	244.2 / 14.7
			246.7 / 12.2 / 50	246.3 / 12.6
				258.92
			248.6 / 13.0 / 32	15.6
		250.9 / 10.7 / 100	247.5 / 14.1 / 50	244.8 / 16.8
	254.4 / 7.2 / 150	251.1 / 10.5 / 100	248.3 / 13.3 / 50	245.2 / 16.4
256.2 / 5.4 / 150	3' Eucal. 107	253.2 / 8.4 / 100	250.4 / 11.2 / 50	247.6 / 14.0
	257.4 / 4.2 / 160 Toe fill	254.2 / 7.4 / 100	252.0 / 9.6 / 50	250.2 / 11.4

6' Eucal. 24

261.61

LT "A"

9+75

8+75

8+25

+80 = beg. of Acacia and Eucal. grove

+40

7+00

N 58.9 W

	212.5		217.5
R.C. →	41.4 / 32		41.4
	217.5		225.2
R.C. →	41.4 / 36		33.7
	224.8		231.9
R.C. →	34.1 / 40		27.0
	232.9		238.3
R.C. →	26.0 / 31		20.4
	239.3		241.9
R.C. →	19.6 / 37		17.0
	243.1		243.3
R.C. →	15.8 / 34		15.6

N 58.9 W

					Lt		"B"	Rt				
T.P.	13.00	267.85	407	254.85								
+50					2.00/100 · 256.9	2.8/50 · 256.1	1.8 · 254.1	7.4/50 · 251.5	5.0/100 · 253.9	3.2/180 · 255.7	7.0/200 · 251.9 R.C.	
8					3.3/100 · 255.6	3.9/50 · 255.0	6.6 · 252.3	9.7/50 · 249.2	9.6/100 · 249.3	7.1/150 · 251.8	7.6/180 · 251.3	10.7/204 · 248.2 = R.C.
+50					7.0/100 · 251.9	6.2/50 · 252.7	8.0 · 250.9	11.7/55 · 247.2		12.2/100 · 246.7	11.1/170 · 247.8	15.0/200 · 243.9 R.C.
7					8.2/50 · 250.7	7.9/15 · 251.0	9.4 · 249.5		12.1/50 · 246.8		14.7/110 · 244.2 R.C.	
+50						9.4/25 · 249.5	10.4 · 248.5	13.1/40 · 245.8		15.7/85 · 243.2 = R.C.		
6+08.69 E.C.							11.90 · 247.02 on hub					
5+89.05							17.4 · 246.5					
		258.92					258.92					

10+55 Int. of Cobble drain 82° LT.

10+18.73 E.C.

Large Eucal. Trees along Toe R.R. fill Trees approx 20' out from ℄ So. Track of R.R

9+93.84

9+68.95 B.C. RT

9+41.41 E.C.

9+21

9+00.59 B.C.

9+00.59 BC LT.

Toe R.R. fill 285 — 259.7 / 8.0

267.85

LT "B" RT

259.5 8.4 / 10 F.L.
260.5 7.4
258.5 9.4 / 10 F.L. on plank bridge over cobble drain

Toe fill
265.6 2.3 / 125
263.5 4.4 / 100
261.3 6.6 / 50
259.5 8.4
256.7 11.2 / 50
257.2 10.7 / 100
259.1 8.8 / 150
259.9 8.0 / 200
261.2 6.7 / 255
256.9 11. / 275

258.2 9.7

Eucal. Trees planted on Rim Canon

256.7 11.2

255.5 12.4

255.2 12.7
24" Eucal. / 15
30" Eucal. / 32

254.6 13.3 / 40
257.3 10.6 / 100
255.4 12.5 / 150
255.4 12.5 / 190
253.3 14.6 / 200
R.C.

260.2 7.7 / 250
260.7 7.2 / 200
259.7 8.2 / 150
257.9 10.0 / 100
256.7 11.2 / 50
254.6 13.3
2 Eucal. / 15
Group / 35
Eucal. cover area of 20' R

267.85

Station					
13+00					
12+90					
Center Curve on Radial					
12+18.44	B.C. Lt		12+13	115' Rt = 4' Eucal.	
T.P.	11.66	275.73	3.78	264.07	
+50					
+45					
+10					
11+00					
		267.85			

"B"

Lt — Rt

10" Eucal / 9

1' Eucal / 12

	Lt		Center	Rt				
Elev.	269.2	266.5	265.4	268.5	270.1	269.4	268.1	264.6
Rod / Dist.	6.5 / 87	9.2 / 50	10.3	7.2 / 50	5.6 / 88	6.3 / 130	7.6 / 160	11.1 / 175 R.C.
Elev.	267.8	265.7	263.3	265.6	268.1	267.2	266.7	262.7
Rod / Dist.	7.9 / 91 Toe fill	10.0 / 50	12.4	10.1 / 50	7.6 / 100	8.5 / 150	9.0 / 185	13.0 / 200 R.C.
Elev.	265.5	264.1	262.1 (275.73)	263.2	266.1	266.2	265.9	261.9
Rod / Dist.	2.4 / 95 Toe fill	3.8 / 50	5.8	4.7 / 50	1.8 / 100	1.7 / 150	2.0 / 200	6.0 / 215 R.C.

3' Eucal. / 111

4' Eucal / 91 tree

	Lt		Center	Rt					
Elev.	265.2	262.8	261.0	260.7	262.9	263.8	263.6	263.3	260.3
Rod / Dist.	2.7 / 107 Toe fill	5.1 / 50	6.9	7.2 / 50	5.0 / 100	4.1 / 150	4.3 / 200	4.6 / 330	7.6 / 240 R.C.

267.85

15+43.04 E.C.

Center Curve

T.P.	9.00	281.40	3.33	272.40

14+62.76 B.C. Lt.

14

13+52.83 E.C. = S. edge Eucal. + Acacia Grove

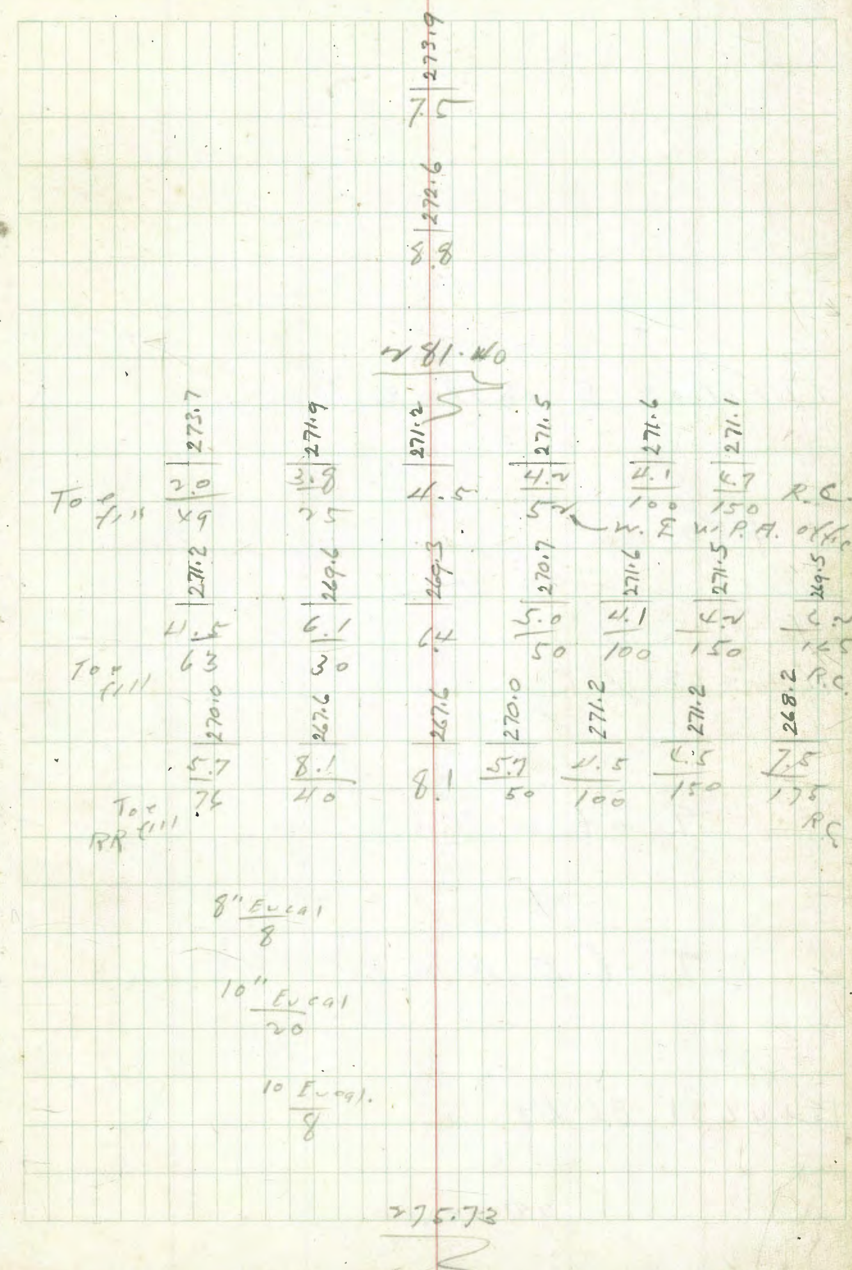
+25

+37

13+32

275.73

Lt "8" Rt.



17+11.07 ℄ 12th St. Pav

+50

16+12.68 E.C.

℄ of W Tr.

℄ of E RR Tr.

15+46.31 BC Lt

281.40

Over for "C"

Lt Rt.

"B"

1.3	280.1 ℄ Pav
2.4	279.0
4.6	276.8
5.8	276.6
4.8	276.6
7.3	274.1

281.40

1+94

+50

1+00

+95

+70

+55

+50

+40

0+00

~81.40

LT "C" Rt

274.4 | Z.0 / 40 — 272.8 | 8.6 — 271.0 | 10.4 / 50 — 266.9 | 14.5 / 97 R.C.

2' Eucal. / 67

273.4 | 8.0 / 32 Fence — 271.7 | 9.7 — 270.3 | 11.1 / 40 — 266.6 | 14.8 / 80 R.C.

273.3 | 8.1 / 29 Fence → Row Eucal. — 271.4 | 10.0 — 269.1 | 12.3 / 50 — 266.0 | 15.4 / 90 R.C.

2' Eucal. / 38

2' Eucal. / 67

12" Tel. P. 1½" Eucal. / 22

274.7 | 6.7 / 35 — 16" Eucal. / 25 — 272.3 | 9.1 — 270.3 | 11.1 / 50 — 265.2 | 16.2 / 120 R.C.

10" Eucal. / 15

Toe Fill — 273.9 | 7.5 / 40 — 272.9 | 8.5 / 20 — 272.4 | 9.0 — 271.7 | 9.7 / 50 — 271.3 | 10.1 / 100 — 271.2 | 10.2 / 150

Dec 5

~81.40

Check to Orig. BM			4.72	283.27	283.28
T.P.	8.32	288.03	1.29	279.71	
3+40					
3+25					
3+15					
3+00					
2+50					

281.40

LT "C" RT

R.C.
275.8
5.0
40

274.7
6.7
2 0
R.C.

276.0
1.4
5

275.7
5.7
5 0

275.4
6.0
50

268.0
13.4

271.6
9.8 = R.C.

272.2
9.2

272.9
8.5

270.2
11.2
25 = R.C.

271.4
10.0
50

269.4
12.0
70 R.C.

281.40

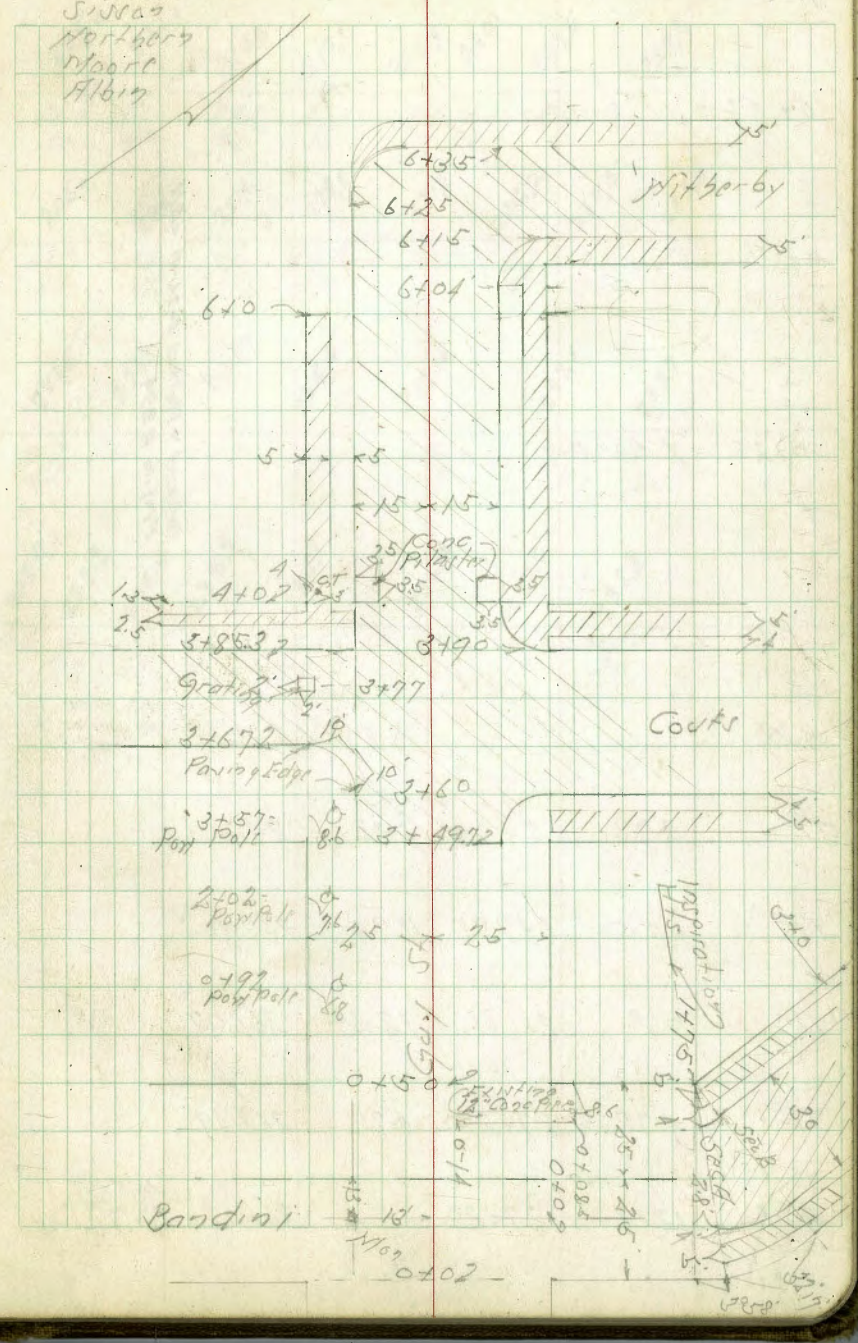
Cross Section Guy St Bandini to Witherby

Bandini Guy to Inspiration Heights

Indexed
M

May 22-41

37



Cross Section Guy St
Bandini to Hitherby

0+50 = W.L. Bandini					
0+36					
0+25 = ℄ Bandini					
0+0 = E.L. Bandini					
B.M.			8.28	236.13	13' N. of Bandini & Guy St.
TP	3.78	244.41	9.32	240.63	
TP	0.05	249.95	11.95	249.90	
TP	0.78	261.85	12.20	261.07	
TP	4.78	273.27	4.71	268.49	
BM	12.18	273.20		261.02	H.F.B.P. Sunset & Hitherby

Reduced & Plotted 5-26-41 C.B.H.
Profile #394

Lt: S — ℄ — Rt: N

0+50:
208.0 — 211.1 — 215.2 — 217.1 — 224.1 — 230.1 — 237.5 — 237.8
36.4/60 — 33.3/40 — 29.2/25 — 27.3/15 — 18.3 — 14.3 (10.0' 6" C.I.P.) — 6.9/15 — 6.6/25

0+36:
205.7 — 226.0 — 227.4 — 229.8 — 231.2 — 236.2 — 237.3 — 237.8
38.7/80 — 18.4/32 — 17.0/25 — 14.6/15 — 13.2 — 8.2/6 — 7.1/15 — 6.6/25

0+25:
222.5 — 228.3 — 230.7 — 234.4 — 237.15 — 237.1 — 237.7
21.9/56 — 16.1/40 — 13.7/25 — 10.0/15 — 7.26 = MH Rim — 7.3/15 — 6.7/25

0+0:
235.0 — 235.3 — 234.4 — 235.5 — 236.1 — 236.4 — 237.0 — 238.8
9.4/35 — 9.1/25 — 10.0/20 — 8.9/16 — 8.3/15 — 8.0 — 7.4/15 — 5.6/25

244.41

Station	Lt						℄	Rt				
1+42				238.1 6.3/40	238.9 5.5/25	239.1 5.3/15	239.8 4.6	240.0 4.4/15	239.9 4.5/25			
1+36				233.5 10.9/40	236.1 8.3/25	238.2 6.2/15	239.5 4.9	239.9 4.5/15	239.9 4.5/25	240.0 4.4/30		
1+12			220.1 24.3/55	219.6 24.8/40	221.6 22.8/25	224.4 20/15 ?	233.9 11.5	235.3 9.1/9	239.3 5.1/15	239.2 5.2/25	239.1 5.3/30	
0+92		214.8 29.6/65	214.0 30.4/55	215.6 28.8/40	223.4 21.0/25	229.1 15.3/15	232.1 12.3	233.9 10.5/8	238.6 5.8/15	238.6 5.8/25	238.5 5.9/30	
0+73			217.5 26.9/55	222.4 22.0/40	224.2 20.2/25	228.6 15.8/15	231.3 13.1	232.4 12.0/6	236.0 8.4/15	238.1 6.3/18	237.9 6.5/25	237.9 6.5/30
0+58	32.2/60	27.4/45	215.4 29.0/37	214.4 30.0/30	218.4 26.0/25	223.0 21.4/15	230.6 13.8	236.4 8.0/15	238.0 6.4/19	237.7 6.7/25	237.9 6.5/30	

24441

244.41

Guy St

370				
2+65				
TP	4.56	247.01	1.96	242.45
2+30				
2+0				
1+75				
1+55				
		244.41		

Lt | ℄ | Rt

244.1	244.3	243.2	245.2	243.7	244.1	245.1
2.9 / 25	2.7 / 15	3.8	3.8	3.63 / 15	2.9 / 23	1.9 / 25
244.9	244.1	244.0	242.7	242.8	242.7	243.2	243.4	244.1
2.1 / 25	2.9 / 23	3.0 / 15	4.3 / 9	4.3	4.13 / 13	3.8 / 15	3.6 / 23	2.9 / 25
				247.01				
244.4	242.9	242.5	241.6	241.9	241.8	243.1
0.0 / 25	1.5 / 21	1.9 / 15	2.8 / 8	2.5	2.6 / 15	1.63 / 25
241.0	241.0	240.5	241.0	241.2	241.3	242.6
2.1 / 30	3.4 / 25	3.9 / 15	3.4	3.3 / 15	3.1 / 18	1.9 / 25
239.6	239.8	239.9	240.3	240.9	240.9	242.1
1.8 / 25	1.6 / 25	1.5 / 15	1.1	3.5 / 15	3.5 / 20	2.3 / 25
				241.45	242.48
				1.96 / 225.41	1.93 / 30 / 247.01
			244.41		

3+85.3

3+75 = ℄

3+67.2

3+60 = EC6

3+50 = ℄ ℄ Court

3+25

247.01

Lt ℄ Rt

238.76	240.10	241.03	241.35			
8.25 / 35	6.91 / 25	5.98 / 15	5.86			
238.57	239.93	240.99	241.57	242.40	243.02	
8.44 / 35	7.08 / 25	6.02 / 15	5.44	4.61 / 15	3.99 / 25	
238.88	241.41	241.23	241.70			
8.13 / 35	6.60 / 25	5.78 / 15	5.31			
240.7	241.42	241.53	241.97	242.45	242.76	243.51
6.2 / 25	5.69 / 15	5.48 / 15	5.04	4.56 / 15	4.25 / 25 Gut	3.50 / 25 CL
241.0	241.91	242.46	242.77	243.51	243.9	
6.0 / 25	5.10 / 15 SH Pav	4.55 / 15 Pav	4.24 / 15 Gut	3.50 / 15 CL	3.1 / 25	
243.6	243.3	242.8	242.8	243.4	244.0	245.6
3.4 / 25	3.7 / 15	4.2 / 10	4.2	3.6 / 15	3.0 / 20	1.4 / 25

247.01

Gun St.

	Lt			Rt
5+00	243.83 3.18 15	243.10 3.91 15	244.00 3.01	243.99 3.02 15	244.52 2.49 15
4+75	243.40 3.61 15	242.87 4.14 15	243.84 3.17	243.86 3.15 15	244.31 2.70 15
4+50	242.72 4.29 15	242.29 4.72 15	243.26 3.75	243.33 3.68 15	243.79 3.22 15
4+25	242.00 5.01 15	241.64 5.37 15	242.69 4.32	242.74 4.27 15	243.16 3.85 15
4+00 = W/L Cout	240.6 6.4 25	241.35 5.66 15-Cb	240.87 6.14 15-Gut	242.06 4.95	242.07 4.94 15-Gut	242.62 4.39 15-Cb
3+90 = W/Cb	239.0 8.0 35	240.3 6.7 25	240.99 6.02 15	241.50 5.51	241.73 5.28 15	241.95 5.06 25-Gut	242.51 4.50 25-Cb
	247.01			247.01		

Station	Lt.	Lt.	℄		Rt	Rt	Rt
6+35 = NCb Witherby	? 240.8 6.2/15		241.01 6.00 Cb	240.51 6.50 Gut		240.91 6.10/15	241.41 5.60/15
6+15 = ECb Witherby	240.72 6.29/15	240.31 6.70/15	240.75 6.26		241.15 5.86/15	241.28 5.73/25	241.60 5.41/25
6+04 = Cb BC on Rt	241.02 5.99/15	240.48 6.53/15	241.32 5.69		241.44 5.57/15	241.92 5.09/15	
5+75	241.87 5.14/15	241.40 5.61/15	242.31 4.70		242.30 4.71/15	242.78 4.23/15	
5+50	242.64 4.37/15	242.14 4.87/15	243.01 4.00		243.06 3.95/15	243.52 3.49/15	
5+25	243.24 3.77/15 Cb	242.78 4.23/15 Gut	243.71 3.30		243.67 3.34/15 Gut	244.17 2.84/15 Cb	

247.01

247.01

Cross Section Bandini St.
Guy St. to Inspiration Hts

Indexed
LM

Red. & Plot. 5-26-41 CBM.

1+0					
0+65					
0+30					
0+08.5 = Inlet 12" Conc Pipe					
0+07.5	18' Lt of ℄ = Wly Pow Pole				✓
0+0 = N.L. Guy St.					
0-14 = outlet 12" Conc Pipe					✓
B.M	11.91	248.04		236.13	13' Mon Bandini & Guy

(Lt=W) ℄ (Rt=E)

1+0

247.3	246.7	246.0	246.6	246.0	244.9	246.5	246.6
0.7 / 25	1.3 / 15	2.0 / 12	1.4 (℄)	2.0 / 11	3.1 / 13	1.5 / 15	1.4 / 25

0+65

244.0	243.9	243.4	243.1	243.4	242.7	242.8	243.8	243.9
4.0 / 25	4.1 / 20	4.6 / 15	4.9 / 11	4.6 (℄)	5.3 / 15	5.2 / 17	4.2 / 20	4.1 / 25

0+30

240.6	240.3	238.9	239.9	340.0	339.9	340.9	341.2
7.4 / 24	7.7 / 20	9.1 / 15	8.1 / 13	8.0 (℄)	8.1 / 15	7.1 / 18	6.8 / 25

0+08.5

236.66
11.38
16.4 = F.L.
12" Conc Pipe

0+0

238.0	238.0	237.9	236.7	237.4	238.2
10.0 / 25	10.0 / 15	10.1 (℄)	11.3 / 13	10.6 / 15	9.8 / 25

0-14

234.17
13.87
16.5 = F.L.
12" Conc Pipe

248.04

1+70

Sec B = 1+75 Ahead

Sec A = Sta

1+75

1+65

1+80

TP 12.27 260.10 0.21 247.83
248.04

Lt Ctr Rt

256.50 255.94 256.82 256.67 257.38
3.40 4.16 3.28 3.43 2.72
15 15 15 15 15

255.03 254.55 255.46 255.33 256.03
5.07 5.55 4.64 4.77 4.07
15 15 15 15

255.3 254.64 254.03 254.59 254.18 254.80 255.0
4.8 5.46 6.07 5.51 5.94 5.30 5.1
25 15.1-06 15.1-Out 14.9-Out 14.9-06 25

255.3 255.1 254.0 254.3 254.0 254.9
4.8 5.0 6.1 5.8 6.1 5.4
25 20 15 15 25

252.6 252.4 252.1 251.4 252.4 252.8
7.5 7.9 8.0 8.7 7.7 7.3
25 15 15 20 25

250.4 250.0 249.1 249.5 249.3 248.6 249.7 249.6
9.7 10.1 11.0 10.6 10.8 11.5 10.4 10.5
25 15 8 13 15 18 25

260.10

BM			10.96	261.03	N.E. B.P. Sargett & Witherby 261.02
TP	2.27	271.99	2.21	269.72	
3+0					
TP	12.01	271.93	0.18	259.92	
2+50					
		260.10			

Lt		℄	Rt	
262.33	261.76	262.47	262.12	262.76
9.60 / 15	10.17 / 15	9.46	9.81 / 15	9.17 / 15
259.42	258.90	271.93 / 259.66	259.40	260.07
0.68 / 15 = Cb	1.20 / 15 = Gut	0.44	0.70 / 15 = Gut	0.03 / 15 = Cb
		260.10		

Cross Section Alley Block 15 Sub Lots 20 to 50
Block N Terralta From Polk to Orange
Between Central & 41st

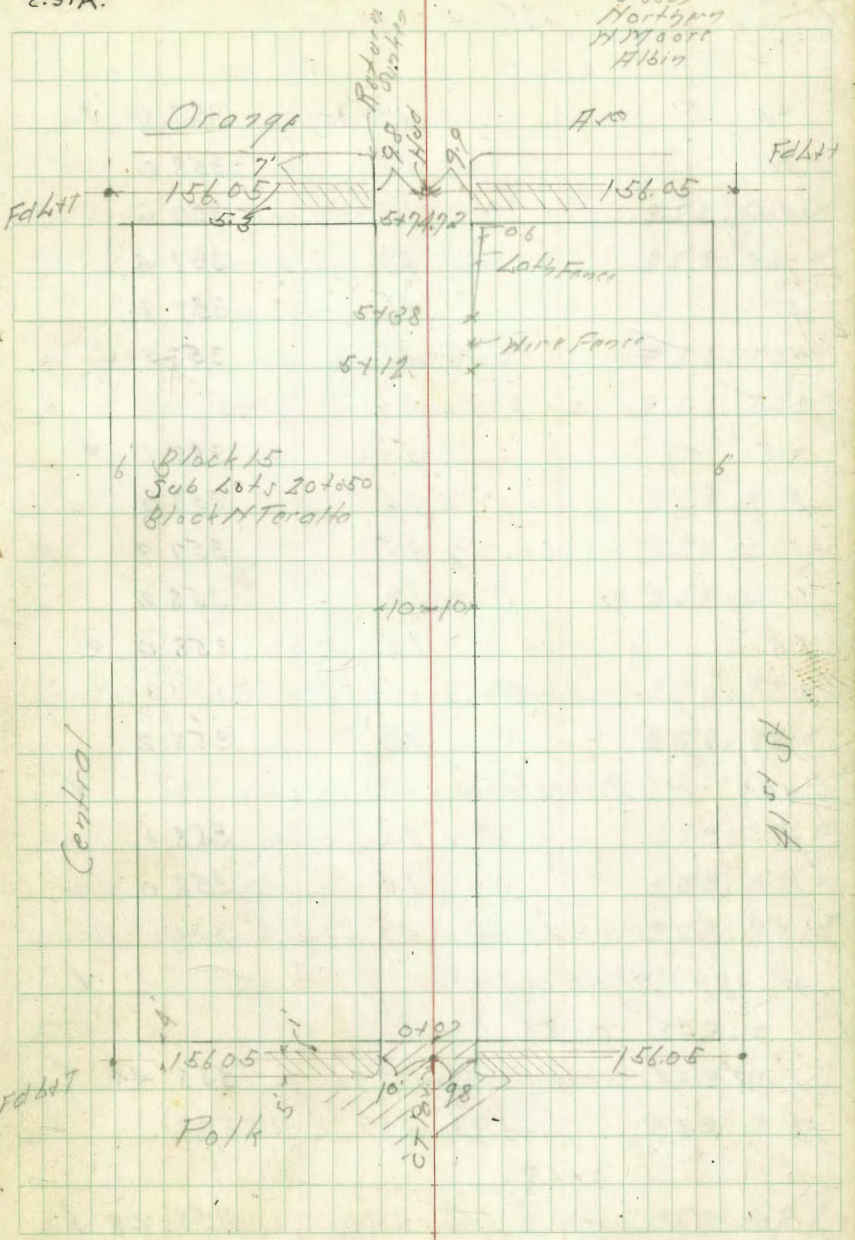
BM	6.65	358.58	See Note P-51	351.93	NW BP University & Central
TP	4.34	361.19 361.38	1.73	356.85	
	0-6 = N Cb Polk				
-140	= E.L. Central Top Cb		4.43	356.95 ✓	
	Gutter on Pav		4.70	356 68 ✓	
-70	Cb		4.38	357 00	
	Gutter on Pav		4.77	356 61	
M	Cb		4.51	356 87	
	Gutter on Pav		5.04	356 34	
Δ	on Paving		5.15	356 23	
E	Cb		4.71	356 67	
	Gutter		5.10	356 28	
+70	Cb		4.75	356 63	
	Gutter		5.20	356 18	
+140	Cb = W.L. 41st St		4.91	356 47	
	Gutter		5.40	355.98	
	0+0 = W.L. Polk Ave				
E	Top Cb		4.58	356 80	
	Gutter on Pav		4.77	356 61	
Δ	" "		4.80	356 58	
	Gutter " "		4.56	356 82	
W	Top Cb		4.47	356.91	
	+0.3' = Sky Picket Fence			✓	

Reduced & Plotted 6-7-41
Profile No. 2962 C.S.H.

Indexed
C.S.K.

Jones-41
S-5507
Northern
Highway
Albin

47



36138

36119

0+15

-5		3.5	357.9	✓
W		3.4	358.0	
+4		3.8	357.6	
Δ		4.0	357.4	
E		3.6	357.8	
+5		3.6	357.8	✓

0+30

-5		3.3	358.1	✓
E		3.4	358.0	
Δ		3.5	357.9	
W		3.2	358.2	
+5		3.4	358.0	✓

0+50

W		3.2	358.2	
+0.7' = W Ly Picket Fence				✓
Δ		3.3	358.1	
E		3.4	358.0	

0+51

W +2.3 = W Ly Anchor Pole ✓

0+56

E -2.9 = Δ Garage Conc Floor		2.94	358.44	✓

36412

TP	591	363.93	3.17	358.02

0+69

W -5.2 = Δ Garage Dirt Floor		5.84	358.28	✓

36412

363.93

0+77

W +2.3 = W Ly Pow Pole ✓

0+82

W -5' = E Ly Conc Apron	5.51	358.61	✓
W -6' = Δ Garage Conc Floor	5.36	358.76	✓

0+94

W -13.8 = Δ Garage Conc Floor	5.35	358.77	✓
E -5' = Δ Garage Dirt Floor	5.37	358.75	✓

1+0

E	5.3	358.8	
Δ	5.5	358.6	
W	5.5	358.6	

1+07

W -7.5 = E Ly Conc Apron	5.40	358.72	✓
W -13.0 = Δ Garage Conc Floor	5.40	358.72	✓

1+14

E -3.2 = Δ Garage Conc E	4.84	359.28	✓
E -0.4 = W Ly Conc Apron	4.90	359.22	✓
W -16.6 = Δ Garage Conc Floor	4.85	359.27	✓

1+50

W	5.1	359.0	
Δ	4.9	359.2	
E	4.8	359.3	

1+56

E -3.8 = Δ Garage Conc Floor	4.64	359.48	✓

		364.12 ✓			
		363.93			
		1+68			
E-2.9	℄ Garage	Dirt Floor	4.6	359.5	✓
		1+77			
W+2.3	= W ly Post Pole				✓
		1+89			
W-7'	℄ Garage	Dirt Floor	4.9	359.2	✓
		2+0			
E			4.6	359.5	
℄			4.6	359.5	
W			4.6	359.5	
		2+05			
W-6'	℄ Garage	Dirt Floor	4.7	359.4	✓
		2+09			
E-7'	℄ Garage	Conc Floor	4.26	359.86	✓
		2+15			
W-4'	℄ Shed as Garage	Dirt Floor	4.6	359.5	✓
		2+19			
W+1.0'	= S ly Board Fence				✓
E-7'	℄ Garage	Dirt F.	4.1	360.0	✓
		2+27			
E-0.7	= S ly Shed				✓
		2+35			
E-0.7	= N ly Shed				✓
TP	5.30	365.00	4.23	359.70	
		365.19			

		365.19		49
		365.00		
		2+37		
E-3.9	= N ly Conc Apron		4.88	360.31 ✓
E-5.6	= S ly Do. Garage Conc Floor		4.79	360.40 ✓
		2+50		
W			4.9	360.3
+1.1	= N ly Board Fence = S ly Shed			✓
℄			5.1	360.1
E			4.9	360.3
		2+56		
E-3.9	= N ly Conc Apron		4.89	360.30 ✓
E-5.6	= N ly Do Garage Conc F		4.78	360.41 ✓
		2+58		
E+0.6	= S ly Picket Fence			✓
		2+64		
W+0.9'	= N ly Shed = S ly Board Fence			✓
		2+71		
W+1.1	= N ly Board Fence = S ly Shed			✓
E-0.8	= N ly Picket Fence			✓
		2+77		
W+2.4	= N ly Post Pole			✓
		3+0		
-10			4.6	360.6 ✓
E			4.7	360.5
℄			4.9	360.3
W			4.6	360.6

365.19

365.00

3+03

E-44.5 = ℄ Garage Conc Floor 4.30 360.89 ✓

3+24

W+1.2 = N ly Shed = S ly Lath Fence ✓

3+50

-10	3.9	361.3	✓
W	3.6	361.6	
℄	3.9	361.3	
E	3.8	361.4	
+10	3.8	361.4	

3+59

E-3.3 = ℄ Garage Dirt F 3.7 361.5 ✓

3+70

W+1.8 = ℄ 8' Conc Slab 3.24 361.95 ✓

3+75

W+1.9 = N ly Lath Fence ✓

3+76

W+2.2 = W ly Pow Pole ✓

E-1.6 = S ly Wire Fence ✓

4+0

-10	3.6	361.6	✓
E	3.5	361.7	
℄	3.7	361.5	
W	3.6	361.6	
+10	3.7	361.5	✓

365.00

4+25

E-2.0 = N ly Wire Fence ✓

4+27

E-2.2 = S ly Do Garage Conc Floor 2.86 362.33 ✓

4+40

W+0.7 = S ly Conc Apron	3.09	362.10	✓
W-0.3 = S ly 1 Car Garage Conc Floor	2.97	362.22	✓

4+49

E-2.2 = N ly Do Garage C.F. 2.90 362.29 ✓

4+50

W	3.2	362.0
℄	3.3	361.9
E	3.2	362.0

4+55

E-5' = ℄ Shed or Garage Dirt Floor 3.2 362.0 ✓

4+66

E-0.6 = ℄ Garage Plank Floor 2.7 362.5 ✓

TP 5.07 366.97 3.10 361.90

367.16

4+71

W+0.6 = E ly Conc Apron	4.97	362.19	✓
W-0.2 = N ly 1 Car Garage Conc Floor	4.84	362.32	✓

4+72

W+0.3 = S ly Conc Apron	4.81	362.35	✓
W-4' = S ly 2 Car Garage Conc Floor	4.40	362.76	✓

W+1.8 = W ly Pow. Pole

367.16
366.97

Station / Description	Rod	Elev.	
4+96			
W +0.2 = Ely Conc Apron	4.76	362.40	✓
W −4′ = Nly 3 Car Garage Conc Floor	4.41	362.75	✓
4+97	"		
E −1.1 = ℄ Garage D.F	4.8	362.4	✓
5+0			
E	4.8	362.4	
℄	4.6	362.6	
W	4.3	362.9	
+0.6 = Sly Lath Fence			✓
5+12			
E = Sly Wire Fence			✓
5+35			
W −0.6 = Nly Lath Fence = Sly Bldg.			✓
5+40			
W −0.6 = Sly Garage Conc F. W Entrance	3.86	363.30	✓
5+50			
W	4.1	363.1	
+0.8 = Wly Pow Pole			✓
℄	4.4	362.8	
E	4.4	362.8	
5+58			
W −0.6 = Nly Garage C.F W Entrance = Sly Lath Fence	3.80	363.36	✓

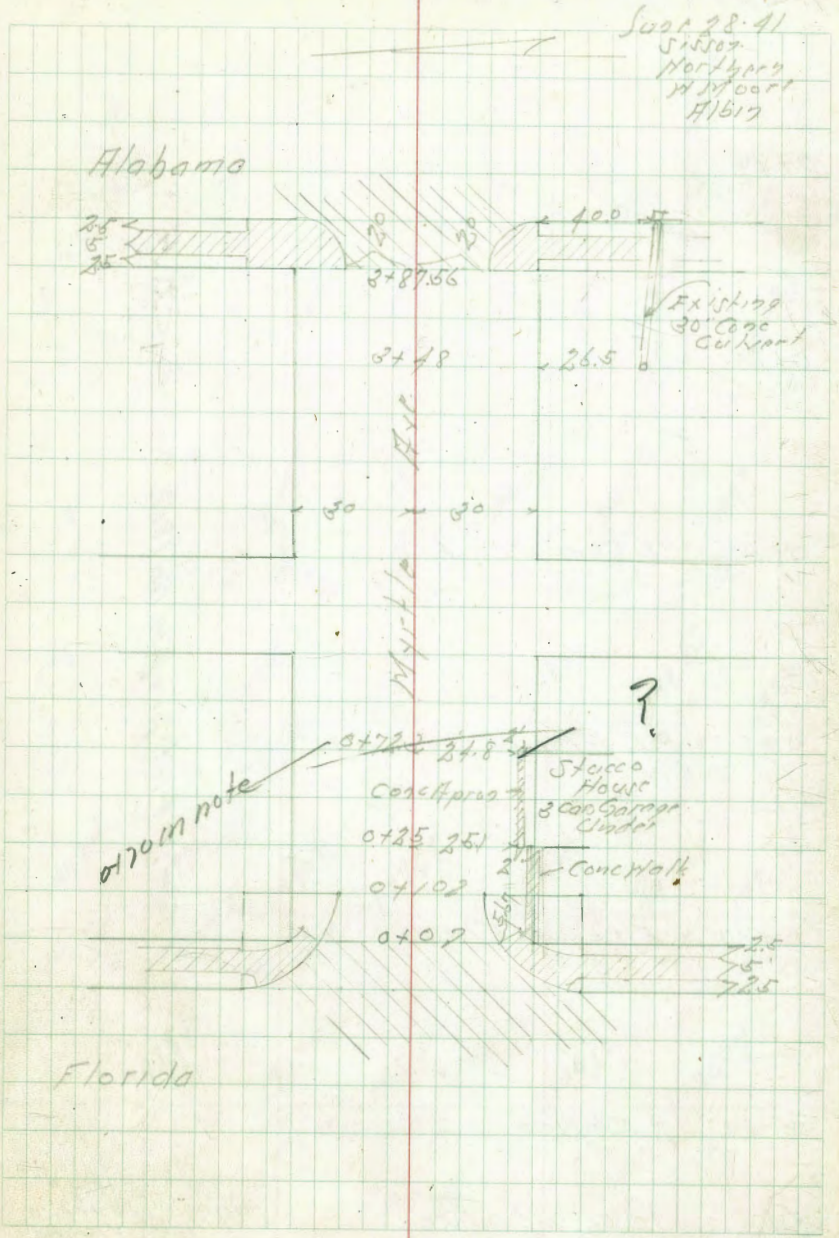
367.16
366.97

Station / Description	BS	H.I.	FS		Elev.
5+74.70 = S ℄ Orange Ave					
W = Nly Lath Fence					
W Cb			4.17		362.99 ✓
Gutter			4.4		362.8
℄			4.7		362.5
E Gutter			4.6		362.6
E Cb			4.50		362.66 ✓
5+88.7 = S Cb Orange					
−55′ Cb			4.79		✓ 362.37
Gutter on Paving			5.26		✓ 361.90
E Cb			4.62		362.54 ✓
Gutter Dirt			5.1		362.1
℄ "			5.0		362.2
W Gutter "			5.0		362.2
W Cb			4.63		362.53
+70 Cb			4.27		✓ 362.89
+140 = E ℄ Central Top Cb			3.95		✓ 363.21 correct
Gutter on Paving			4.81		✓ 362.85
BM			3.16	363.81	N.W. BP Orange & Central 363.97
BM			4.35	362.62	N.W. BP Orange & Alley 362.81
TP	1.58	364.95	3.60	363.37	
TP			8.11	356.84	P 47 356.84

See Book 56 P. 61 Alley Blk 27 notes

Cross Section Myrtle Ave.
Florida to Alabama

indexed
LM



Cross Section Myrtle Ave
Florida to Alabama

0+45

0+25

0+10 = Cb Ends Rt & Lt

0+0 = E.L. Florida

0-10 = E Cb Line Florida

0-30 = ℄ Florida

BM	10.51	208.50		197.99	SWBP Myrtle+ Florida

Red. & Plot profile No 1812 7-1-41 C.B.H.

Sta	Lt.=N				℄				Rt.=S
0+45		204.3 / 4.5 / 30	202.3 / 6.2 / 20	201.8 / 6.7 / 15	201.9 / 6.6	202.5 / 6.0 / 20	202.73 / 5.77 / 25.2 = N/4 Conc Apron	202.77 / 5.73 / 27.1 = N 1/3 Car Garage Conc Floor	
0+25	203.6 / 4.9 / 30	202.1 / 6.4 / 26	201.5 / 7.0 / 20	200.3 / 8.2 / 12	200.4 / 8.1	200.0 / 8.5 / 17	201.1 / 7.4 / 20	202.20 / 6.30 / 25.1 = N/2 Conc Walk	202.3 / 6.2 / 30
0+10	201.8 / 6.7 / 30	200.47 / 8.03 / 20 = Cb	199.5 / 9.0 / 20 = Gut		199.4 / 9.1	199.1 / 9.4 / 20 = Gut	200.03 / 8.47 / 20 = Cb	199.9 / 8.6 / 30	
0+0	199.3 / 9.2 / 30	199.36 / 9.14 / 22.8 = Cb	198.61 / 9.89 / 22.8 = Gut		198.56 / 9.94	198.16 / 10.34 / 22.8 = Gut	198.85 / 9.65 / 22.8 = Cb	198.6 / 9.9 / 30	
0-10	199.04 / 9.46 / 40 = Cb	198.36 / 10.14 / 40 = Gutter	198.04 / 10.46 / 20		197.79 / 10.71	197.44 / 11.06 / 20	197.12 / 11.38 / 40 = Gutter	197.98 / 10.52 / 40 = Cb	
0-30	197.85 / 10.65 / 60	197.70 / 10.80 / 20			197.46 / 11.04	197.12 / 11.38 / 20	196.97 / 11.53 / 30		

208.50 ✓

TP	11.52	241.60	1.14	230.08	
2+0					
1+70					
TP	11.83	231.22	0.10	219.39	Nail Power Pole 3½ 1+48
1+50					
1+48	3½ Rt of ℄ = Sly Power Pole				
1+30					
1+0					
TP	11.08	219.49	0.09	208.41	
0+70					
		208.50			

Lt ℄ Rt June 30-41

Lt		℄			Rt	
236.3 +5.1 30	233.3 +2.1 20	225.2 6.0	218.3 12.9 20	215.2 16.0 30	213.4 17.8 48	209.7 21.5 60 = Bot Hollow
227.8 3.4 30	225.6 5.6 20	222.4 8.8	217.7 13.5 20	215.0 16.2 30	211.4 19.8 50	
		231.22 ✓				
221.2 +1.7 30	220.9 +1.4 20	219.4 0.1	217.2 2.3 20	216.0 3.5 30	215.4 4.1 40	
216.9 2.6 30	216.9 2.6 20	216.1 3.4	214.9 4.6 20	214.4 5.1 30	213.3 6.2 40	
210.9 8.6 30	210.7 8.8 20	210.4 9.1	210.5 9.0 20	210.0 9.5 30	209.1 10.1 40	
		219.49 ✓				
205.8 2.7 30	204.5 4.0 20	204.3 4.2	203.0 5.5 20	202.68 5.82 24.9 = NE Cor Gar Apron	202.70 5.80 26.9 = Fl. 13 Cal Garage Conc Floor	
		208.50 ✓				

Myrtle Ave

3+75				
3+48				
2+80	22.0 Lt of ℄ = Ely Lath Fence			
TP	11.51	251.81	1.80	239.80
2+70	38.9 Lt of ℄ = Lath Fence			
2+78	31.0 Lt of ℄ = Wly Lath Fence			
2+65				
2+30				
		241.60		

Lt	℄	Rt
252.0	251.8	247.1
+0.7	0.0	0.2
30	20	
251.9	251.3	250.8
+0.6	0.0	0.5
30 = Sly Stucco House	20	
251.8	251.3	246.2
+0.5	0.0	5.1
30	20	10
		251.31 ✓
250.6	245.1	237.4
+0.0	+3.5	4.2
30	20	
243.8	240.6	233.8
+2.2	1.0	7.8
30	20	
237.5	237.5	229.7
3.1	4.1	11.9
30	20	
		241.60 ✓

Rt						
246.2	239.2	239.6				
6.1	12.1	16.5				
30	40	60				
239.5	234.8	226.2	221.9	224.1		
11.8	16.5	25.1	29.4	27.2		
20	30	48	55	53.5 = Sly Stucco House		
242.6	235.1	233.0	227.8	231.4		
8.7	16.2	18.3	23.5	29.8		
	20	30	45	66 = Sly Stucco House		
237.4	230.9	228.1	223.9	217.8		
4.2	10.7	13.5	17.7	23.8		
	20	30	45	69 = Sly Stucco House		
233.8	227.6	225.1	220.6	214.6		
7.8	14.0	16.5	21.0	27.0		
	20	30	43	53 = Sly Stucco House		
229.7	223.3	221.0	216.6	210.8		
11.9	18.3	20.6	25.0	29.8		
	20	30	45	55 = Sly Stucco House		

BM			4.54	251.51	N.W. B.P. Mystic Alabama 251.50
2+97.56 = W Cb Line Alabama					
3+87.56 = W by Line of Imp. Alabama					
TP	4.82	256.05	0.08	251.23	
		251.21			

251.47 | 250.93 | 250.90 | 250.77 | 250.58 | 250.50 | 251.04

4.58 30-Cb | 5.12 30-Gut | 5.15 20 | 5.28 | 5.47 20 | 5.55 30-Gut | 5.01 30-Cb

251.7 | 251.47 | 250.90 | 250.98 | 250.60 | 251.05 | 251.2

4.4 30 | 4.58 20-Cb | 5.15 20-Gut on Pav. | 5.07 | 5.45 20-Gut on Pav. | 5.00 20-Cb | 4.9 30

256.05 ✓

Cross Section Alley Block B Montecello
From Collier to Adams Bet. Winona & 50th St

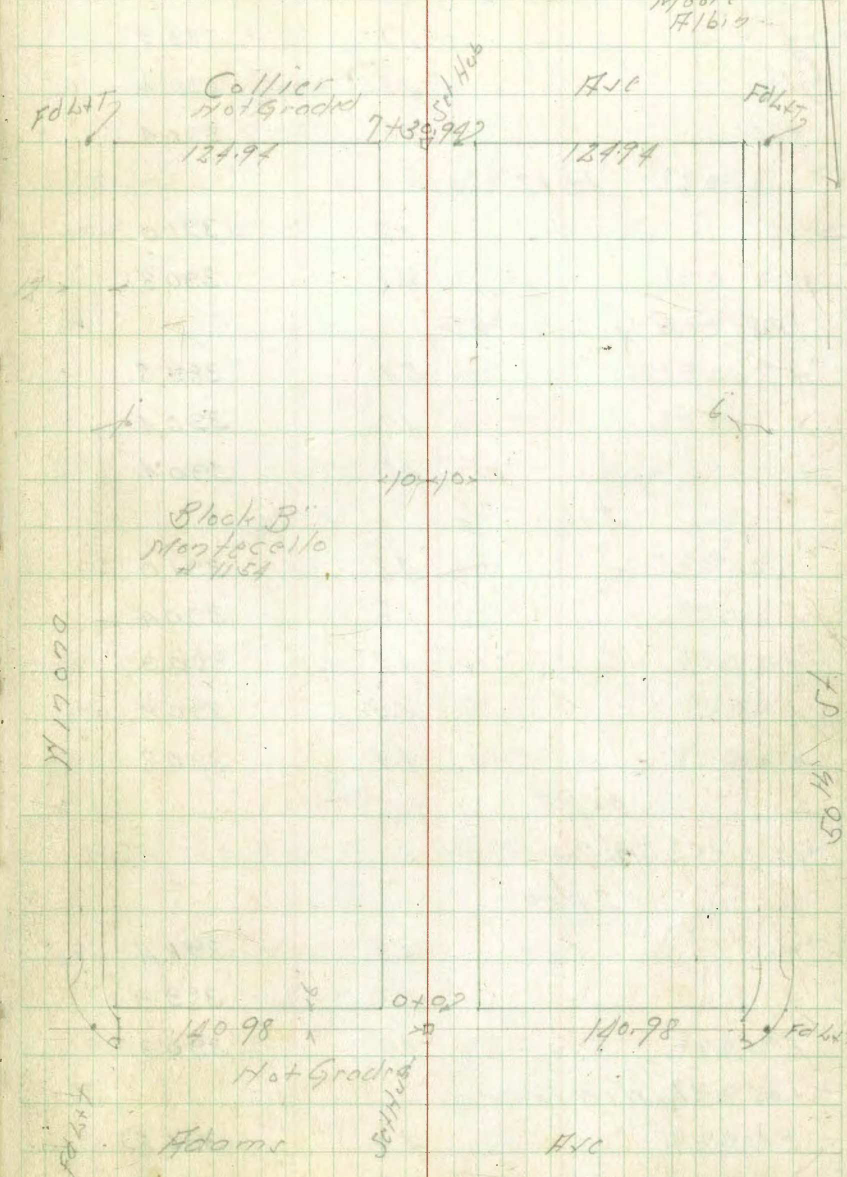
BM	5.88	395.21	✓	389.33	N.E.B.P. Adams & Winona
	0-12 = N Cb Line Adams				
W-12.5' : F.L. Winona = Cb Top			5.98	389.23	
W-12.5' .. : Gut. on Pav.			6.35	388.86	
E-12.5 : W.L. 50th St Cb Top			7.17	388.04	
E-12.5 .. Gut. on Pav.			7.54	387.67	
	0+0 - N.L. Adams				
-10			5.7	389.5	
E			5.4	389.8	
℄			5.3	389.9	
W			5.1	390.1	
+10			5.0	390.2	
	0+15				
W-2.0 = S Fly House Under Construction					
	0+35				
W-2.0 = N Ely House Under Const.					
	0+50				
-10			4.9	390.3	
W			5.0	390.2	
℄			5.8	389.4	
E			5.6	389.6	
+10			5.6	389.6	
	1+0				
-10			4.9	390.3	
E			5.1	390.1	

Red's Plat New Profile 7-1-41 CBH

Indexed LM

Map 1154

June 30-1941
Sisson
North...
Moore
Albin



	395.21		
B	5.3	389.9	
W	4.8	390.4	
+10	4.8	390.4	
1+47			
-10	4.2	391.0	
W	4.9	390.3	
+2.8 = W 1½" Power Pole			
B	5.4	389.8	
E	4.8	390.4	
+10	4.8	390.4	
2+0			
-10	4.2	391.0	
E	4.8	390.4	
B	4.9	390.3	
W	4.3	390.9	
+10	4.4	390.8	
2+25			
W = S 1/4 High Board Fence			
2+50			
W	3.8	391.4	
B	5.3	389.9	
E	4.9	390.3	
+0.1 = S 1/4 Wire Fence			
+10	4.4	390.8	
2+75			
W+2.9 = W 1/4 10" Power Pole			

	395.21		
2+76			
W = W 1/4 High Board Fence			
3+0			
-10	4.4	390.8	
-0.4 = W 1/4 Wire Fence			
E	4.8	390.4	
B	5.4	389.8	
W	4.5	390.7	
+10	4.1	391.1	
TP 569	395.58	5.22	389.89
3+50			
-10	4.3	391.3	
W	5.0	390.6	
B	5.6	390.0	
E	5.5	390.1	
+10	5.5	390.1	
3+74			
W+2.1 = W 1/4 Power Pole			
3+75			
E-0.4 = S 1/4 Wire Fence			
4+0			
-10	4.8	390.8	
E	4.7	390.9	
B	4.8	390.8	
W	4.8	390.8	
+10	4.6	391.0	

395.58

4+26

E-0.2 = Nly Wire Fence

4+50

-10	4.6	391.0
W	4.7	390.9
℄	5.2	390.4
E	4.8	390.8
+10	4.7	390.9

4+74

W+2.0 = Nly 12' Power Pole

4+75

E-0.3 = Sly Wire Fence

5+0

-10	4.6	391.0
E	4.8	390.8
℄	5.1	390.5
W	5.2	390.4
+10	5.1	390.5

5+25

E = Nly Wire Fence

E-2.8 = Sly Wire Fence

5+50

-10	5.2	390.4
W	4.9	390.7
℄	4.9	390.7

395.58

E	4.5	391.1
+10	4.5	391.1

5+74

E-2.8 = Nly Wire Fence

5+76

W = Wly 8' Power Pole

6+0

-10	4.5	391.1
E	4.6	391.0
℄	4.9	390.7
W	4.9	390.7
+10	4.8	390.8

6+50

-10	4.4	391.2
W	4.0	391.6
℄	4.0	391.6
E	4.2	391.4
+10	3.9	391.7

7+0

-10	4.2	391.4
E	4.2	391.4
℄	4.1	391.5
W	4.4	391.2
+10	4.3	391.3

		395.58			
TP	4.25	395.91	3.92	391.66	
		7+30.94 = S. L. Collier			
-137'	= E. Cb Line Winona Top Cb		3.88	392.03	
-137	Gutter on Paving		4.35	391.56	
-10			5.1	390.8	
W			4.9	391.0	
+0.5	= Wly Power Pole				
℄			4.8	391.1	
E			5.0	390.9	
+10			4.8	391.1	
+137	= W Cb Line 50th St Top curb		5.55	390.36	
+137	Gutter on Paving		6.01	389.90	
TP	3.49	395.56	3.84	392.07	
BM			6.25	389.31	N. E. B. P. Adams & Winona 389.33

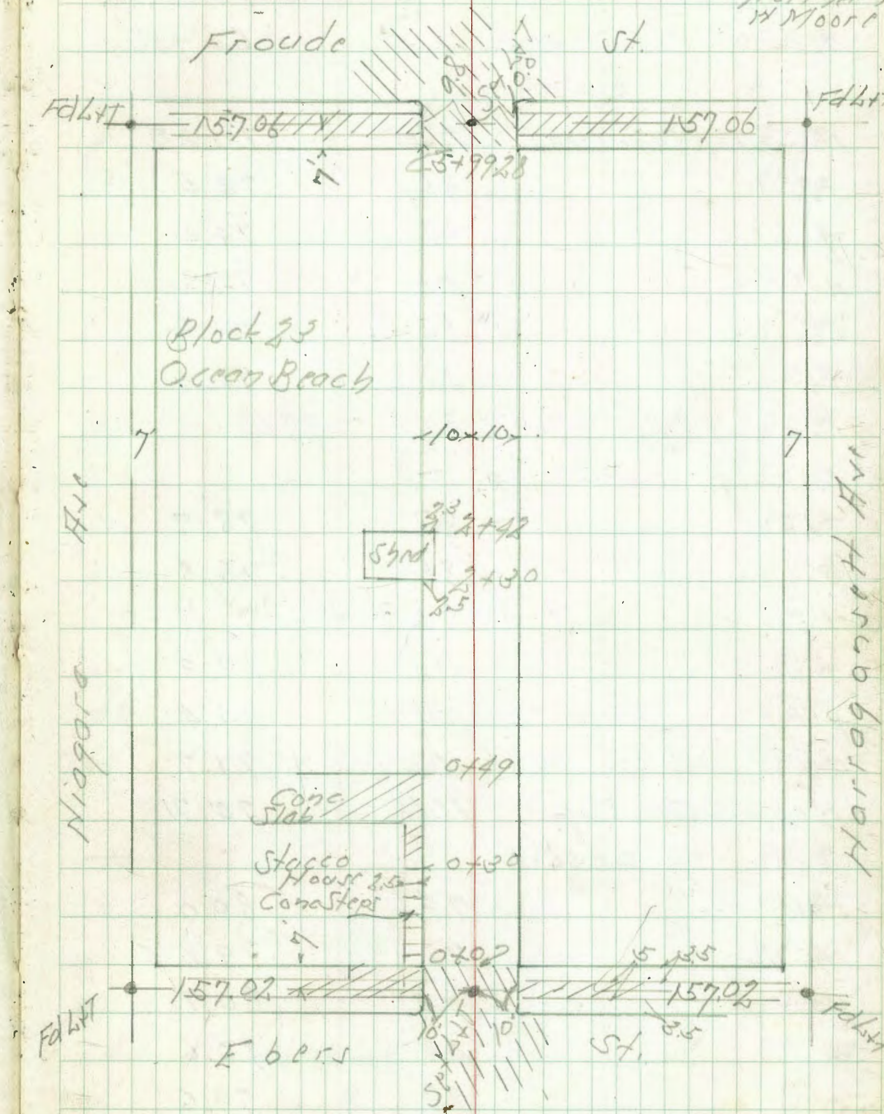
Cross Section Alley Block 23 Ocean Beach
From Ebers to Froude
Between Niagara & Narragansett

BM	12.14	55.20 ✓		43.06	SW BP Newport & Ebers
TP	11.84	66.24 ✓	0.80	54.40 ✓	
		0-12 = E Cb of Ebers			
N on Paving			10.05	56.19 ✓	
¢ . .			9.83	56.41 ✓	
S . .			9.56	56.68 ✓	
		0+0 = E L Ebers			
S Top cb			8.21	58.03 ✓	
S Gutter on Pav			8.51	57.73 ✓	
¢ . .			9.25	56.99 ✓	
N Gutter . .			9.35	56.89 ✓	
N Top cb			9.02	57.22 ✓	
		0+08			
N = Sly Conc Steps			5.98	60.26	
+0.5			1.8	64.4	
¢			2.6	63.6	
+8			2.5	63.7	
S			+3.5	69.7	
+10			+3.6	69.8	
TP	12.19	78.13	0.30	65.94	
		0+19			
-10			6.1	72.0	
S			6.2	71.9	
¢			6.9	71.2	

7/24-41 GBH
Profile 289L

Indexed LM

July 22-41
S-550
Northberg
H Moore



78.13

N. Ground			8.1	70.0	
N = N/y Conc Steps			13.38	64.75	
	0+30				
N = Top Conc Steps			7.85	70.28	
+2			4.6	73.5	
℄			3.7	74.4	
+7			5.3	72.8	
S			3.3	74.8	
+10			4.2	73.9	
TP	9.25	87.37	0.01	78.12	
	0+49				
-10			8.7	78.7	
S			8.6	78.8	
+5			9.9	77.5	
℄			10.1	77.3	
+7			12.0	75.4	
+9			16.7	71.7	
N = E/y Conc Slab			16.66	70.71	
	0+55				
-10			7.4	80.0	
N			7.8	79.6	
℄			7.3	80.1	
S			6.8	80.6	
+10			7.8	79.6	

87.37

	0+75				
-10			4.5		82.9
S			4.8		82.6
℄			4.6		82.8
N			4.5		82.9
+10			5.1		82.3
	0+97				
-10			1.6		85.8
-5			0.2		87.2
N			0.1		87.3
+5			1.4		86.0
℄			1.2		86.2
+6			0.0		87.4
+8 = S/y Power Tel Pole				✓	
S			0.0		87.4
+10			0.7		86.7
TP	12.23	99.58	0.02	87.35	N of I Pole 0+97
	1+06				
-10			10.7		88.9
S			10.7		88.9
℄			11.2		88.4
N			10.6		89.0
7+4 = ℄ Garage Conc Floor			10.59	✓	88.99
	1+19				
N = N/y Board Fence				✓	

		99.58			
	1+40				
-10			6.8	92.8	
-5			6.0	93.6	
N			5.7	93.9	
S			5.8	93.8	
S			5.8	93.8	
+10			5.0	94.6	
	1+70				
-10			+0.7	100.0	
S			0.8	98.8	
S			0.8	98.8	
N			0.1	99.5	
TP	12.02	111.32	0.28	99.30	
	1+94				
S+1.4 = Sly Pow x Tel. Pole				✓	
	1+96				
N+0.4 = Ely Board Fence				✓	
	2+0				
-10			6.5	104.8	
N			6.8	104.5	
S			7.0	104.3	
+7			6.5	104.8	
S			5.8	105.5	
+10			5.3	106.0	

		111.32			
	2+25				
-10			1.7	109.6	
S = Nly Lath Fence ✓			2.7	108.6	
+0.1 = Nly 1.8 x 1.3 Conc Block			1.17	110.15	
+2			4.1	107.2	
S			4.3	107.0	
N			3.2	108.1	
+10			3.8	107.5	
TP	11.87	123.07	0.12	111.20	
	2+46				
S+0.7 = Nly Lath Fence ✓					
S-0.4 = Ely Lath Fence ✓					
	2+48				
N+0.3 = Nly Board Fence				✓	
	2+50				
-10			12.5	110.6	
N			11.4	111.7	
+3			12.5	110.6	
S			12.6	110.5	
+7			12.4	110.7	
S			11.5	111.6	
+2			10.2	112.9	
+10			10.2	112.9	
	2+73				
S+0.7 = Ely Lath Fence				✓	
	2+99				
S+1.6 = Sly Pow x Tel Pole				✓	

		122.07			
		3+00			
-10			5.6	117.5	
S			6.0	117.1	
+2			6.9	116.2	
[illegible]			7.1	116.0	
+7			7.2	115.9	
N	= Board Fence	✓	6.7	116.4	
+10			7.2	115.9	
		3+50			
-10			2.8	120.3	
N	= Board Fence	✓	3.0	121.1	
[illegible]			3.1	121.0	
S			1.5	121.6	
+10			1.1	122.0	
TP	12.00	134.89	0.18	122.89	
		3+98			
S+1.6	= Sly Pam x Tel. Pole	✓			
		4+00			
-10			8.1	126.8	
S			8.1	126.8	
+0.4	= Nly Board Fence	✓			
[illegible]			8.8	126.1	
N	Ely Board Fence		8.4	126.5	
+0.8	= Nly Lath	✓			

		134.89			
		4+50			
-10			5.5	129.4	
-1			4.8	130.1	
N			2.9	132.0	
[illegible]			2.8	132.1	
+6			2.7	132.2	
S			1.9	133.0	
+10			1.5	133.4	
TP	11.99	146.58	0.30	134.59	
		5+00			
-10			6.9	139.7	
S			6.6	140.0	
+0.3	= Board Fence	✓			
+3			7.4	139.2	
[illegible]			7.7	138.9	
N			8.0	138.6	
+0.8	= Ely Lath Fence	✓			
+10			8.3	138.3	
		5+25			
-10			2.6	144.0	
N			4.0	142.6	
[illegible]			3.9	142.7	
+6			3.8	142.8	
S			2.8	143.8	
+10			3.2	143.4	

		146.58			
TP	7.46	153.77	0.27	146.31	
5+55 = Wly Conc Drive on South					
-33.0 = Wly Do Garage Conc Floor ✓			8.41	145.36	
-19.0 = Brk Conc. Drive ✓			8.46	145.31	
S			6.4	147.4	
+0.3 = Wly Conc Drive ✓			6.08	147.69	
℄			6.5	147.3	
+7			6.3	147.5	
N			5.8	148.0	
+10			5.1	148.7	
5+70 = Ely Conc Drive					
-10			2.5	151.3	
N			2.8	151.0	
+3			4.3	149.5	
℄			4.3	149.5	
S = Ely Conc Drive ✓			4.17	149.60	
+19 = Brk. Conc Drive ✓			8.11	145.66	
+33 = Ely Do Garage Conc Floor ✓			8.16	145.61	
5+90					
-10			0.9	152.9	
S			1.3	152.5	
+4			2.1	151.7	
℄			2.4	151.4	
+8			2.3	151.5	
N			1.9	151.9	
+3		+0.4		154.2	

		153.77			
5+99.28 = N.L. Froude St.					
N Top cb			2.26	✓	151.51
N on Paving			2.68	✓	151.09
℄ " "			2.70	✓	151.07
S " "			2.25	✓	151.52
S Top cb			1.60	✓	152.17
6+03.28 = Break in Paving					
S Top cb			1.68	✓	152.09
S on Paving			2.04	✓	151.73
℄ " "			2.40	✓	151.37
N " "			2.57	✓	151.20
N Top cb			2.33	✓	151.44
6+11.28 = N Cb Line Froude					
N on Paving			2.96	✓	150.81
℄ " "			2.63	✓	151.14
S " "			2.40	✓	151.37
TP	0.34	151.40	2.71	151.06	
TP	0.49	139.93	11.96	139.44	
TP	0.82	128.60	12.15	127.78	
TP	0.47	116.84	12.23	116.37	
BM			12.59	104.25	SWBP NW Porter Froude 104.31

Bliss
Sommer, Meyer
8/7/41

Levels on Curbs and on Flow Lines of Culverts from S Line Colton Ave to 150 ± S of the North Line of R.R. Ave

BM	10:75	19.32		8:57	N.W. 7 ± FH R.R. Ave at Crosby
			0+00		
Flow Line 36" culvert S Line Colton			13.93	5.89	
W Top cb			5.30	14.02	
" Gutter at paving			6.02	13.30	
E " "			5.94	13.39	
E Top cb			5.39	13.98	
			1+40 ± N Line Alley		
E Top cb			7.65	11.67	
" Gutter			8.30	11.02	
W "			8.41	10.91	
W Top cb			7.75	11.57	
			1+60 ±		
W Top cb			8.20	11.12	
" Gutter			8.96	10.36	
E "			8.67	10.65	
E Top cb			8.00	11.32	
			2+80 ± E Conc cb on East		
E Gutter			10.63	8.69	
" Top cb			10.24	9.08	
T.P.	5:71	19.28	10.75	8.51	
W Edge walk			4.99	9.29	
E " "			4.85	9.43	

Indexed

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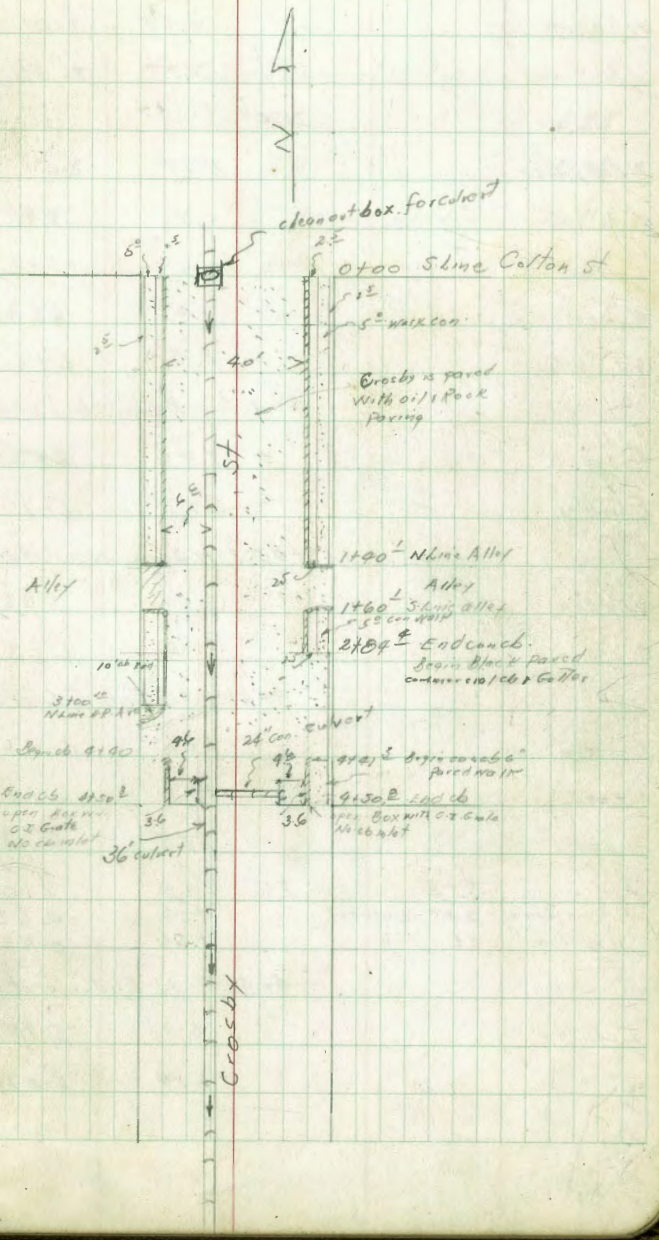


		19.28		
		3+00 ℄ N Line R.R. Ave.		
W Top cb			6.27	8.01
" Gutter			5.77	7.51
		3+14½		
W End Return			5.77	8.51
" " Gutter	Ground		5.9	8.4
		4+90 Begin cb on W Side of Crosby		
W Top cb			7.95	683
W Gutter			8.15	6.13
		4+91½ Begin cb East Side Crosby		
E Top cb			7.96	682
E Gutter			8.27	601 6.01
		9+95.7 N Edge Culvert Box on W Side Crosby		
W Edge			8.99	5.99
E "			7.95	6.33
		4+50.3 S End Culvert Box on W Side Crosby		
E Edge			7.86	6.42
W Edge			7.79	6.49
Top cb			7.55	6.73
TP	5.18	12.21	7.25	7.03
Flow Line	24" Culvert		11.58	0.63
" "	36 "		11.96	0.25
		4+46 ± N End Culvert Box East Side Crosby		
E Edge			6.31	5.90 5.90
W "			6.14	6.07

12.21

4+48 ℄ 24" culvert

Flow Line	11.35	0.86
4+50.8 S End Culvert Box E Side Crosby		
W Edge Box	5.66	6.55
E " "	5.83	6.38
E Top cb	5.95	6.76
Check Sighting BM	3.63	8.78 8.57 0.0 Correct

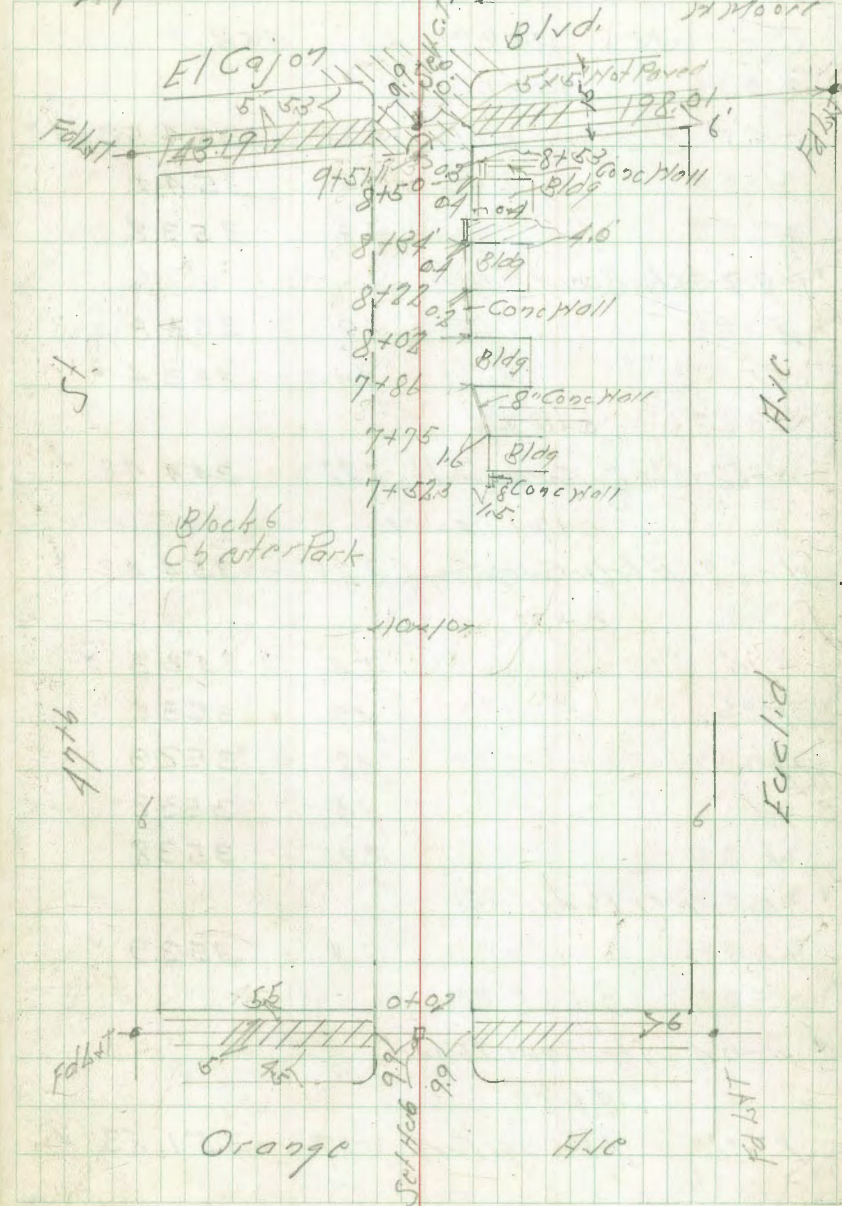
Cross Section Alley Block 6 Chester Park
From Orange Ave to El Cajon Blvd

BM	8.27	358.96		350.69	NWBP Orange & Euclid
0+15 = N Cb Line Orange					
E Cb Top			4.90	354.06	
E Gutter Ground			5.8	353.2	
℄			5.4	353.6	
W Gutter "			5.3	353.7	
W Cb Top			4.37	354.59	
0+0 = N.L. Orange Ave					
W Cb Top & Ground			4.35	354.61	
+2			4.8	354.2	
℄			4.8	354.2	
E Cb Top & Ground			4.77	354.19	
0+08					
E-1.6 = SW Cor House					
0+37					
E			5.0	354.0	
℄			4.7	354.3	
W			4.6	354.4	
+0.3 = Wly Tel Pole					
+5			4.0	355.0	
0+32					
W-0.7 = S'ly Lath Fence					
0+40					
E-1.6 = N.W. Cor House					
0+48					
W-0.8 = N'ly Lath Fence					

Red. Plot Profile 2668 9-4-41 G.S.H.

Indexed LM

Sept. 2. 41
Sisson
Northberg
J.J. Moore



		358.96			
TP	3.58	357.70	4.84	354.12	
		0+51			
-5.8 = ℄ 2' Conc Walk			5.18	354.52	✓
W			3.5	354.2	
℄			3.9	353.8	
✓ +9.9 = S½ Board Fence					
E			3.9	353.8	
+5			4.3	353.4	✓
		0+51			
W-8.2 = S½ Do Garage Conc Floor			3.22	354.48	✓
		0+73			
W-8.2 = N½ Do Garage Conc Floor			3.28	354.42	✓
		0+80			
-10			5.4	352.3	✓
E			4.7	353.0	
℄			4.8	352.9	
+6			4.5	353.2	
W			3.9	353.8	
✓ +0.3 = N½ Power Pole					
+10			3.8	353.9	✓
		0+82			
✓ W-0.4 = S½ Board Fence					
		0+90			
E-22° = ℄ Garage Conc			5.87	351.83	✓

		357.70			
		1+10			
-5			4.5	353.2	
✓ -0.3 = N½ Board Fence					
W			4.5	353.2	
℄			5.2	352.4	
✓ E - Board Fence			5.4	352.3	
+10			6.1	351.6	✓
		1+07			
W-6.5 = ℄ Garage Dirt Floor			4.4	353.3	✓
		1+15			
✓ W-0.2 = S½ Board Fence					
		1+33			
✓ W = N½ Board Fence S½ Wire					
		1+50			
-10			8.2	349.5	✓
E			7.6	350.1	
✓ +11 = Board Fence					
+2			6.6	351.1	
℄			6.8	350.9	
W			6.0	351.7	
+5			5.7	352.0	✓
		1+67			
✓ W-0.1 = N½ Wire Fence S½ Lots					
		1+92			
✓ W-0.6 = N½ Lots Fence					

357.70		
1+94		
W-1.2 = ℄ 4" Wire to House		
2+10		
-1.0	7.3	350.4 ✓
-0.8 = S'ly Picket & Wire Fence		
-0.2 = W'ly Pow. Pole		
W	7.8	349.9
℄	8.5	349.2
E = Board Fence	8.4	349.3
+1.0	9.0	348.7
+10	9.2	348.5 ✓
2+50		
-10	9.5	348.2 ✓
W Board Fence E = S'ly Shed	8.8	348.9
℄	9.0	348.7
W S'ly Wire Fence	9.1	348.6
+0.1 = Picket & Wire Fence		
+10	8.9	348.8 ✓
2+65		
W = S'ly Board Fence		
2+76		
E -0.1 = ℄ Garage Conc Floor	9.64	348.06 ✓
2+90		
W = W'ly Board Fence		
0+95		
W -4.0 = ℄ Garage Dirt Floor	9.1	348.6

357.70		
3+0		
-5	8.9	348.8
W = W'ly Power Pole	9.4	348.3
℄ = S'ly 2' Conc Walk	9.4	348.3
E = S'ly Shed	9.60	348.10
3+07		
E+2.5 = S'ly Conc Apron	9.73	347.97
E+0.4 = S'ly Do Garage Conc Floor	9.63	348.07
3+25		
W-0.3 = S'ly Wire Fence		
3+34		
E+3.3 = W'ly Conc Apron	9.87	347.83
E+0.3 = S'ly Do Garage Conc Floor	9.59	348.11
3+49		
E+0.2 = W'ly Do Garage Conc Floor	9.6	348.1
℄	9.3	348.4
W	8.8	348.9
+10	8.6	349.1
3+75		
-10	8.7	349.0
W	9.1	348.6
℄	9.3	348.4
E	9.6	348.1
+10	9.8	347.9 ✓

357.70

4+70

-10		9.8	347.9 ✓
℄		9.6	348.1
℄		9.6	348.1
℄		9.1	348.6
+0.2 = W'ly Power Pole			
+1.4 = N'ly Wire Fence			
+10		8.3	349.4 ✓

4+02

E-0.9 = S.W. Cor. Stucco Bldg

4+06

W-5.0' = ℄ Garage Conc. F. 8.04 349.66 ✓

4+22

= S'ly Wire Fence

E-7.0 = N.W. Cor. Stucco Bldg

4+42

W-6.3 = ℄ Garage Conc. Floor 8.37 349.33 ✓

4+50

-5		8.6	349.1
-0.3 = S'ly Picket Fence			
℄		9.0	348.7
℄		9.6	348.1
℄		9.8	347.9
-1.2 = N'ly Wire Fence			

4+58

E-3.4 = ℄ 12' Shed Usnt. 9.90 347.80
℄ Garage Conc. Slab

357.70

4+68

E-3.4 = ℄ Garage Conc. Floor		9.97	347.73 ✓
TP	4.70 357.66	9.74	347.96

4+91

E-3.2 = ℄ Garage Conc. Floor 4.94 347.72 ✓

5+00

-10		5.4	347.3 ✓
℄		5.2	347.5
℄		4.8	347.9
+9.7 = W'ly Power Pole			
℄		4.4	348.3
+0.1 = Picket Fence			
+10		4.4	348.3 ✓

5+03

E-2.7 = S.W. Cor. House

5+22

E-2.6 = N.W. Cor. House

5+43

E-2.5 = ℄ Garage Dirt Floor 5.4 347.3 ✓

5+50

-5.5 = S'ly Conc. Apron		4.78	347.88
-0.2 = N'ly Picket			
-0.2 = S'ly Conc. Apron		4.91	347.75 ✓
℄		5.0	347.7
℄		5.3	347.4

	352.66		
E		5.6	347.1
45		5.9	346.8
	5+59		
E-4.6=⅞ Garage Conc Floor		5.47	347.19
	5+66		
E-0.2=Sly Wire Fence			
	5+71		
W=N ly Conc Apron		4.83	347.83
W-6.5=N ly 2 Car Garage Conc Floor		4.75	347.91
	5+75		
E-0.3=N ly Wire Fence			
E-2.0=SW Cor House			
	5+90		
W-6.0=⅞ Garage Conc Floor		4.58	348.08
	5+94		
E-0.3=Sly Wire Fence			
	6+0		
-5		6.13	346.53
-0.3=N ly Wire Fence			
E		5.8	346.9
⅞		5.6	347.1
+9.5=W ly Power Pole			
W		5.3	347.4
	6+02		
W+0.3=Sly Conc Apron		5.10	347.56
W-5.7=Sly 2 Car Garage Conc Floor		4.87	347.79

	352.66		
	6+03		
E-2.0=SW ¼ Car Garage Conc Floor		5.95	346.71
	6+35		
W+0.3=N ly Conc Apron		5.30	347.36
W-5.8=N ly 2 Car Garage Conc Floor		4.85	347.81
	6+47		
E-2.0=N ly 4 Car Garage Conc Floor		5.99	346.67
	6+50		
-10		5.6	347.1
W		5.7	347.0
⅞		5.8	346.9
E		6.2	346.5
TP	4.40 351.12	5.94	346.72
	6+61		
E-10.2=SW 3 Car Garage Conc Floor		4.37	346.75
E-1.3=Sly Conc Apron		4.49	346.63
W-7.0=⅞ Garage Conc Floor		2.98	348.14
	6+89		
E-10.2=N ly 3 Car Garage Conc Floor		4.54	346.58
E-1.2=N ly Conc Apron		4.62	346.50
	6+90		
W-6.8=⅞ Garage Conc Floor		3.58	347.54
	7+0		
E		5.1	346.0
⅞		4.9	346.2

	351.12			
W			4.2	346.9
+10			4.0	347.1 ✓
7+02				
✓ W+1.3 = Sly Board Fence				
7+08				
E −5.8 = ℄ Garage Conc Floor			4.94	346.18 ✓
7+33				
✓ W+1.3 = Wly Power Pole				
7+43				
E −5.0 = ℄ Garage Conc F			5.19	345.93 ✓
7+52				
W			5.0	346.1
✓ +1.3 = Board Fence				
℄			5.1	346.0
E			5.2	345.9
✓ +1.6 = Sly 2.6 Conc Wall, 8" Wide Top			4.08	347.04 ✓
+10			6.0	345.1 ✓
7+55				
✓ E −1.6 = SW Cor House				
TP	4.03	351.23 ✓	3.92	347.20
7+75				
−5			5.6	345.6
✓ −1.6 = Top Conc Wall			3.94	347.29 ✓
E			4.7	346.5
℄			5.0	346.2

351.23		
W	5.0	346.2
+10	5.0	346.2 ✓
7+86		
E = Top Conc Wall	3.99	347.24 ✓
7+90		
✓ W+1.7 = Board Fence to South		
✓ W+0.9 = " " to North		
8+02		
W	5.1	346.1
℄	5.2	346.0
E Ground	4.5	346.7
E Top 8" Conc Wall	4.04	347.19 ✓
+1	5.5	345.7
+10	5.9	345.3 ✓
8+06		
W+0.2 = ℄ 6' Conc. Under Clothsline	5.06	346.17 ✓
8+22		
E+0.2 = Top Conc Wall 8"	3.95	347.28 ✓
8+28		
✓ W+0.3 = Nly Board Fence		
8+32		
✓ W+0.8 = Wly Power Pole		
8+34		
E+0.4 Top 6" Conc Wall	4.23	347.00 ✓
E −0.1 on Conc Walk	5.56	346.67 ✓

351.23

8+45

W-0.7 = N E Cor. Garage w/ Dirt Floor	4.8	346.4	✓
8+50			
-1.0	5.6	345.6	✓
-0.9	5.6	345.6	
-0.4 = Top 8" Conc Wall	4.63	346.60	✓
E	4.8	346.4	
℄	5.0	346.2	
W	4.9	346.3	
+1.0	4.8	346.4	✓
9+0			
-1.0	4.5	346.7	✓
W	4.6	346.6	
℄	4.9	346.3	
E	4.6	346.6	
+5 = Wly Bldg.	5.4	345.8	
9+22			
E	4.9	346.3	
℄	5.0	346.2	
✓ +9.8 = S E Cor. Block Paving	4.86	346.37	✓
W	4.84	346.35	
+8.8 = Ely Bldg	4.67	346.56	
9+27			
✓ E-0.8 = Ely Tel Pole			

351.23

9+51.11 S ℄ El Cajon Blvd on Diagonal

W Cb Top + Block Paving			4.87		346.36 ✓
W Gutter on Paving			5.16		346.09 ✓
℄ on M.H. Rim			5.45		345.78
E Gutter on Paving			5.46		345.77 ✓
E			5.20		346.03
S Cb Line El Cajon					
E on Paving			5.56		345.67
℄ " "			5.51		345.72
W " "			5.44		345.79
TP	5.80	351.87	5.16	346.07	
BM			4.68	347.19	S W BP El Cajon + 4th St 347.20

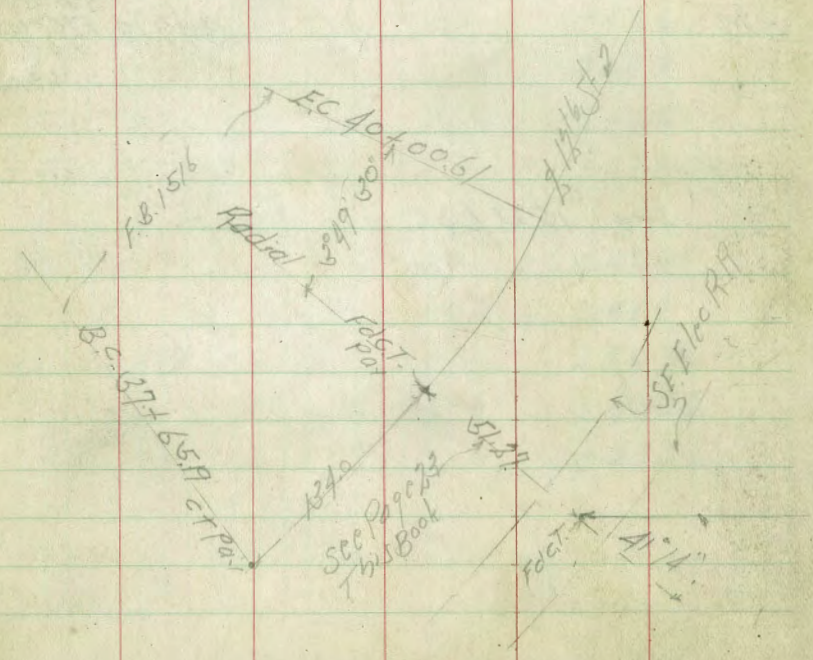
See 1521/36

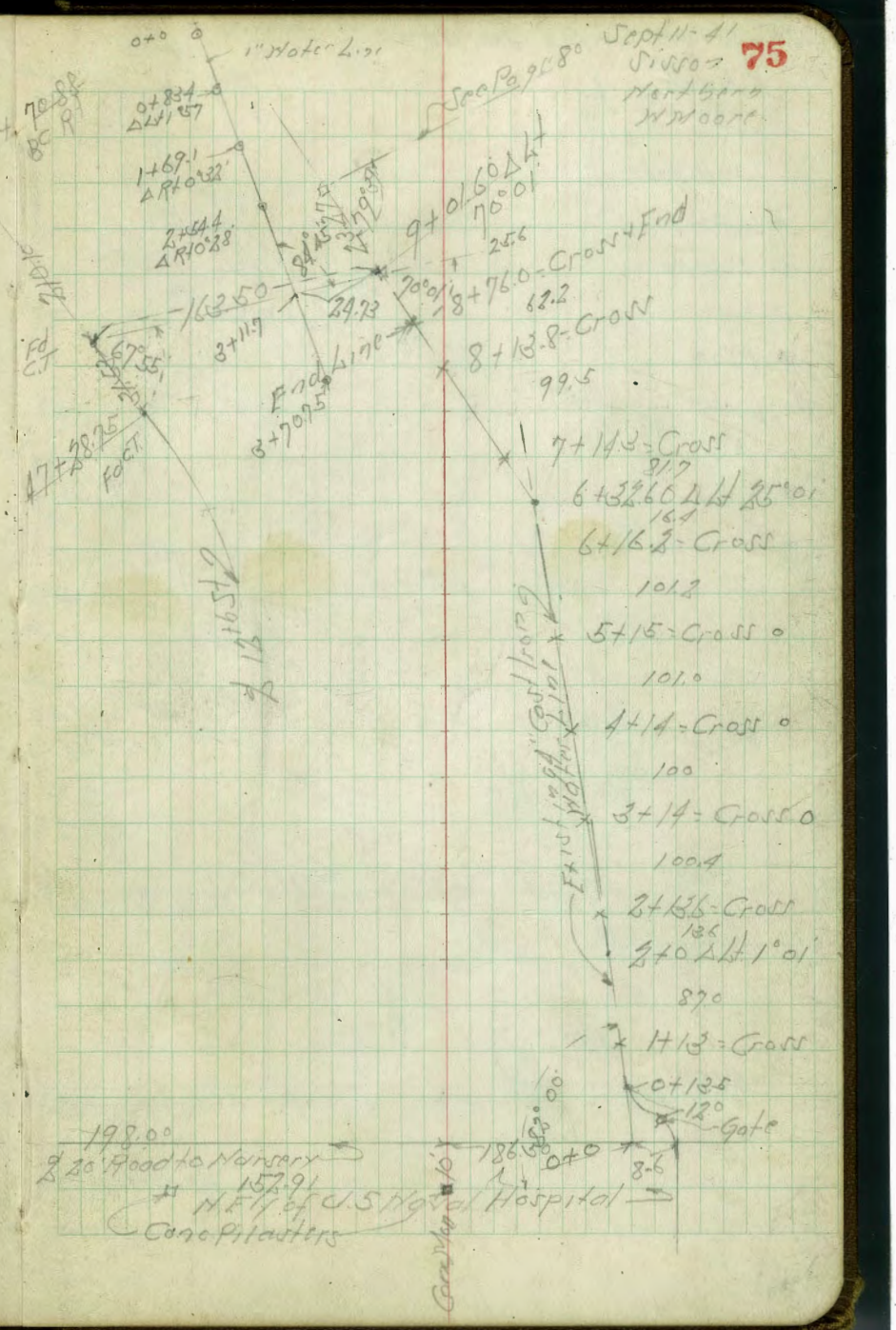
Location of 4" Cast Iron Water Line Through Nursery Balboa Park

Indexed LM

For Side Line See Page 81

See 925 P 44 + 77

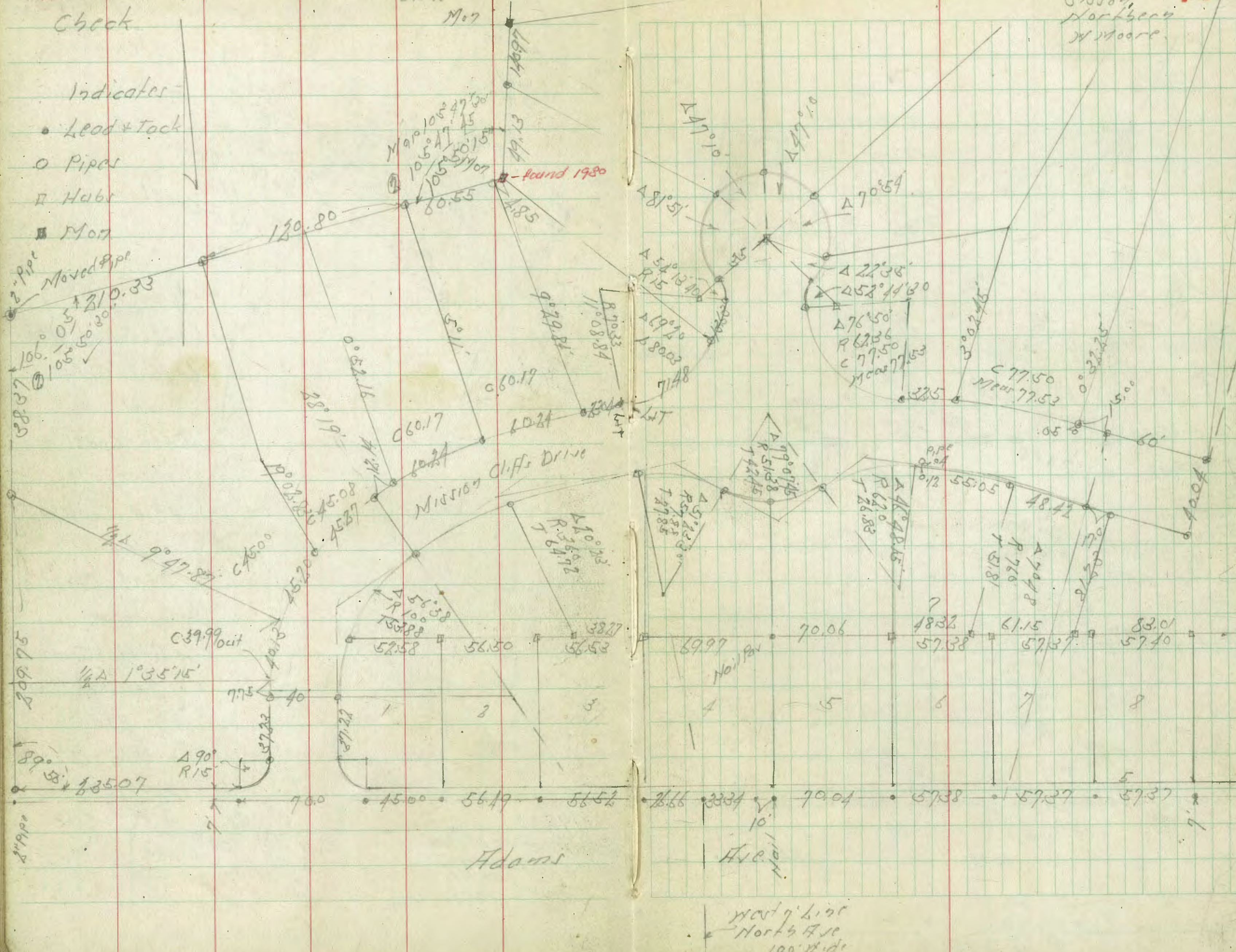


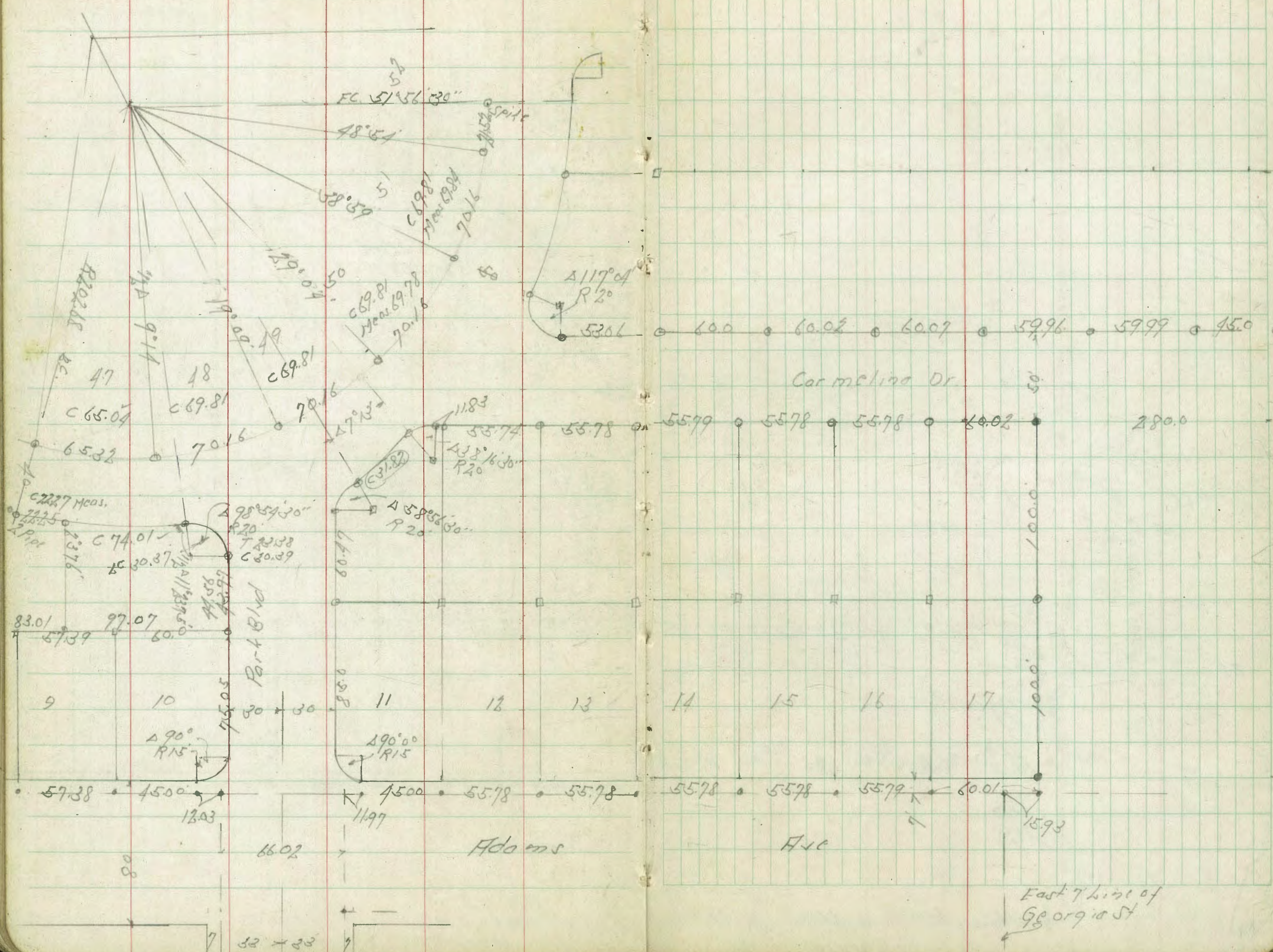


Mission Cliffs Gardens
Check

Indexed
C.S.K.

Jan. 19-42
Sisson,
Northberg
W. Moore

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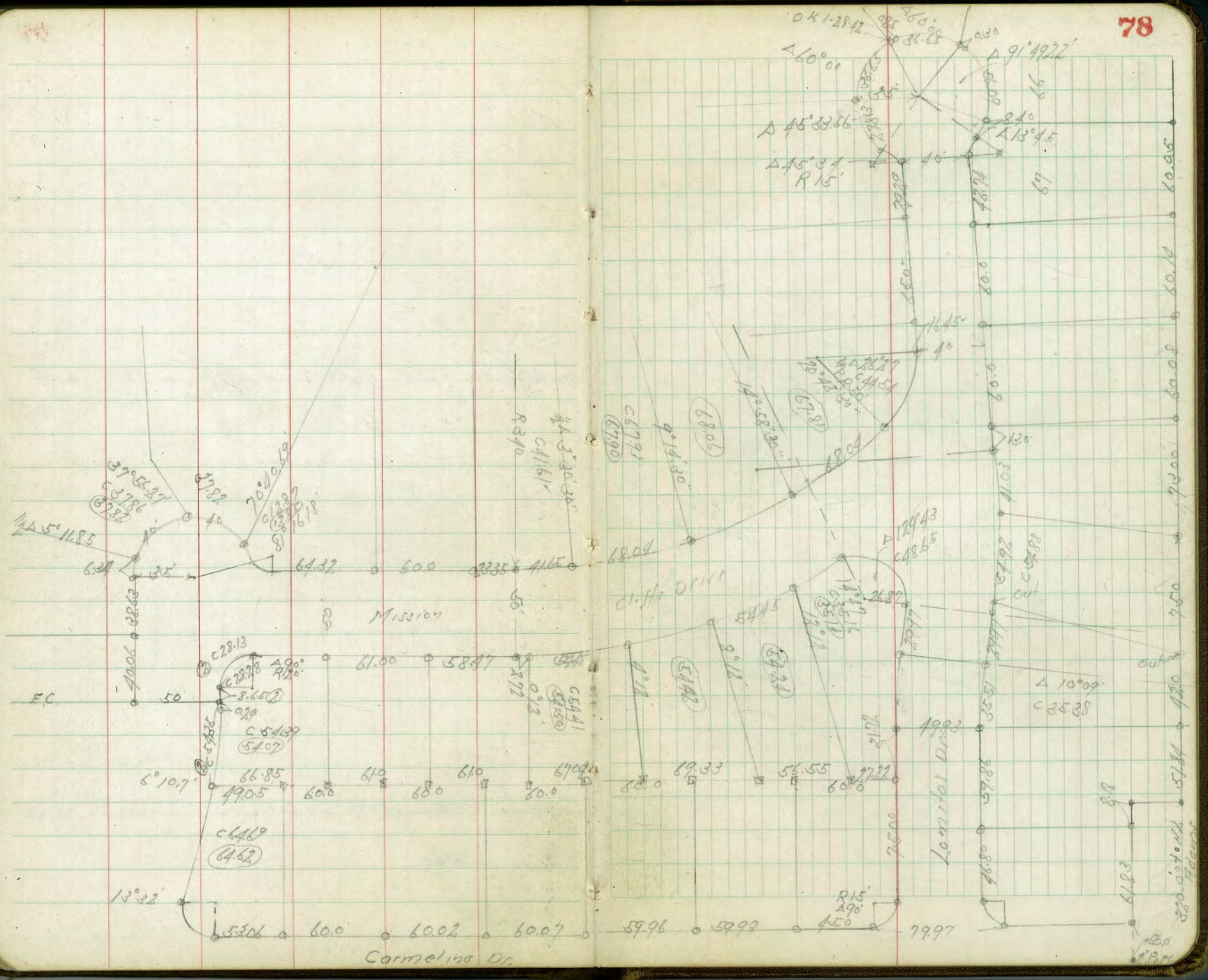
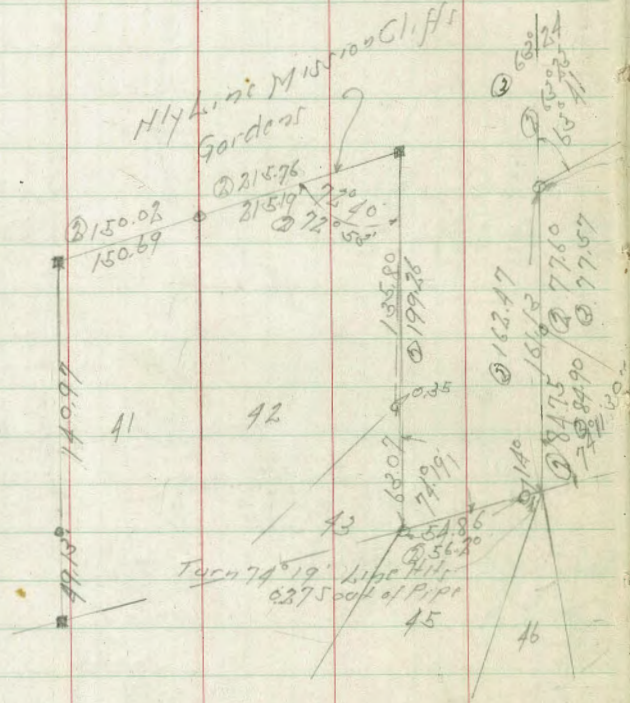
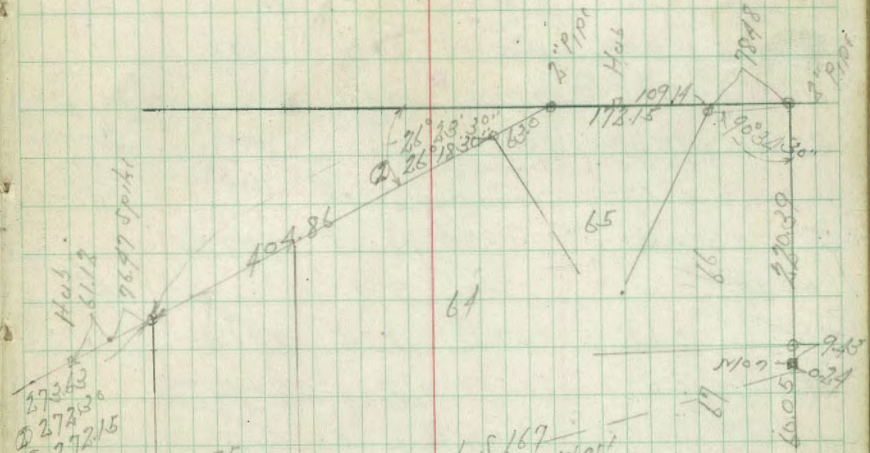
48°54'
38°59'
Spike
Δ117°04'
R 20
53.06
60.0
60.02
60.07
59.96
59.99
45.0
Carmelino Dr.
47
48
49
50
51
52
c 65.04
65.32
c 69.81
70.16
c 69.81
Meas 69.78
70.16
Δ7°13'
11.83
55.74
55.78
55.79
55.78
55.78
60.02
280.0
Δ33°16'30"
R 20
c 37.82
Δ58°56'30"
R 20
c 22.27 Meas.
Δ98°54'30"
R 20
c 74.01
c 30.39
83.01
57.39
97.07
60.0
Portal Blvd
100.0
9
10
11
12
13
14
15
16
17
Δ90°
R 15
Δ90°00'
R 15
57.38
45.00
12.03
11.97
45.00
55.78
55.78
55.78
55.78
55.79
60.01
15.93
66.02
Adams
Ave
East Line of
Georgia St


Mission
Cliff Drive
Carmelina Dr.
EC
R240
R15'
R12'
Δ 91°49'27"
Δ 60°00'
Δ 45°33'56"
Δ 45°31'
Δ 13°45'
Δ 10°09'
Δ 5°11'85
Δ 3°30'34"
Δ 37°55'37"
Δ 70°40'09"
Δ 14°58'30"
Δ 12°43'
Δ 6°10'7
Δ 18°32'
Δ 90°
C 28.13
C 54.39
C 64.69
C 48.65
C 41.51
C 35.38
61.00
58.47
66.85
49.05
64.32
60.0
68.0
59.96
59.99
79.97
19.33
56.55
45.0

N4 Line Mission Cliffs Gardens



Sec. 26-43



Location of 4" Cast Iron Sewer Pipe
To serve Nursery / Balboa Park.
Level Taken on Top of 4" Pipe.

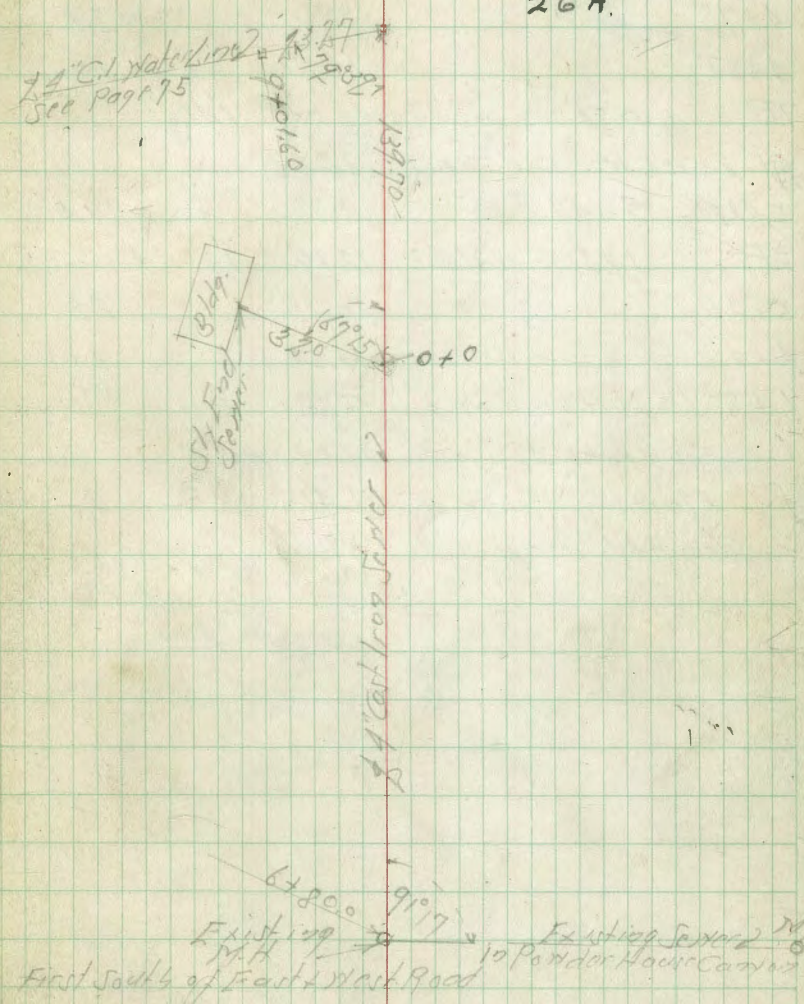
	B.S.	H.I.	F.S.	Elev.	
BM	4.66	287.94		283.28	N.W. B.P. Laurel & Park Blvd
TP	1.43	280.14	9.23	278.71	
TP	2.55	270.49	12.20	267.94	Depth of Ditch
32.5 of 0+0 = N'ly Bldg			2.80	267.69	
Top 4" C.I. Sewer Pipe 0+0 = ∆ 67°15' Clean Out			8.90	261.59	
TP	0.51	258.75	12.25	258.24	
0+44			9.11		1.7
TP	0.62	247.12	12.25	246.50	
TP	0.00	234.99	12.13	234.99	
1+14			9.35		1.5
TP	0.50	223.73	11.76	223.23	
1+48			6.77		1.5
1+78 = Clean Out Top			9.02		
1+78 Top 4" Pipe			11.62		3.1
TP	0.25	211.87	12.11	211.62	
TP	0.41	200.70	11.58	200.29	
TP	0.01	188.64	12.07	188.63	
2+56			2.38	186.26	1.5
2+88			10.86		1.7
TP	0.33	176.94	12.03	176.61	
3+38 = Clean Out Top			7.16		
3+38 Top 4" Pipe			9.20		2.4
TP	0.41	165.20	12.15	164.79	
3+68			5.82		1.6
4+16			12.07		1.3

Indexed
C.S.K.

(26A / 27A)

Jan. 27 42
Sisson
Northern
H. Moore

Sewer Book
26 A.



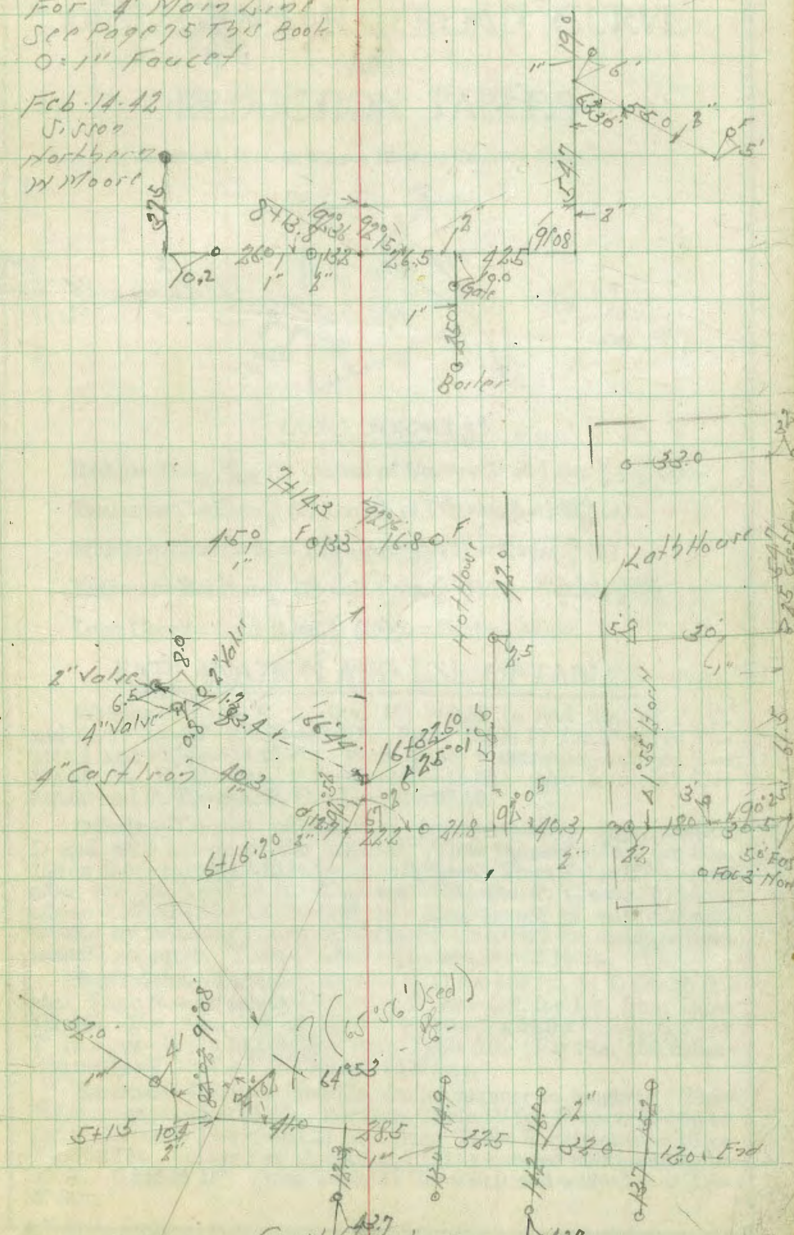
		165.2°			
4+54			14.41		2.4
TP	0.55	153.65	12.10	153.10	
4+78			8.97		2.1
4+87			14.07		1.0
TP	0.84	142.44	12.05	141.6°	
5+12	= Clean out Top		3.23		
5+12	Top 4" Pipe		3.8°		1.5
TP	1.24	131.58	12.10	130.34	
5+35			10.34		2.2
6+0			11.54		3.3
6+8°	= MH on Rim		7.88		
Flow Line 4"			13.83		
Flow			16.41		
Ground Average			9.8		
			83.4 / 1.4		

Location 1"+2" Water Lines in Nursery Balboa Park

For 4" Main Line See Page 75 This Book

⊙ = 1" Faucet

Feb. 14. 42
Sisson
Northcraft
W Moore



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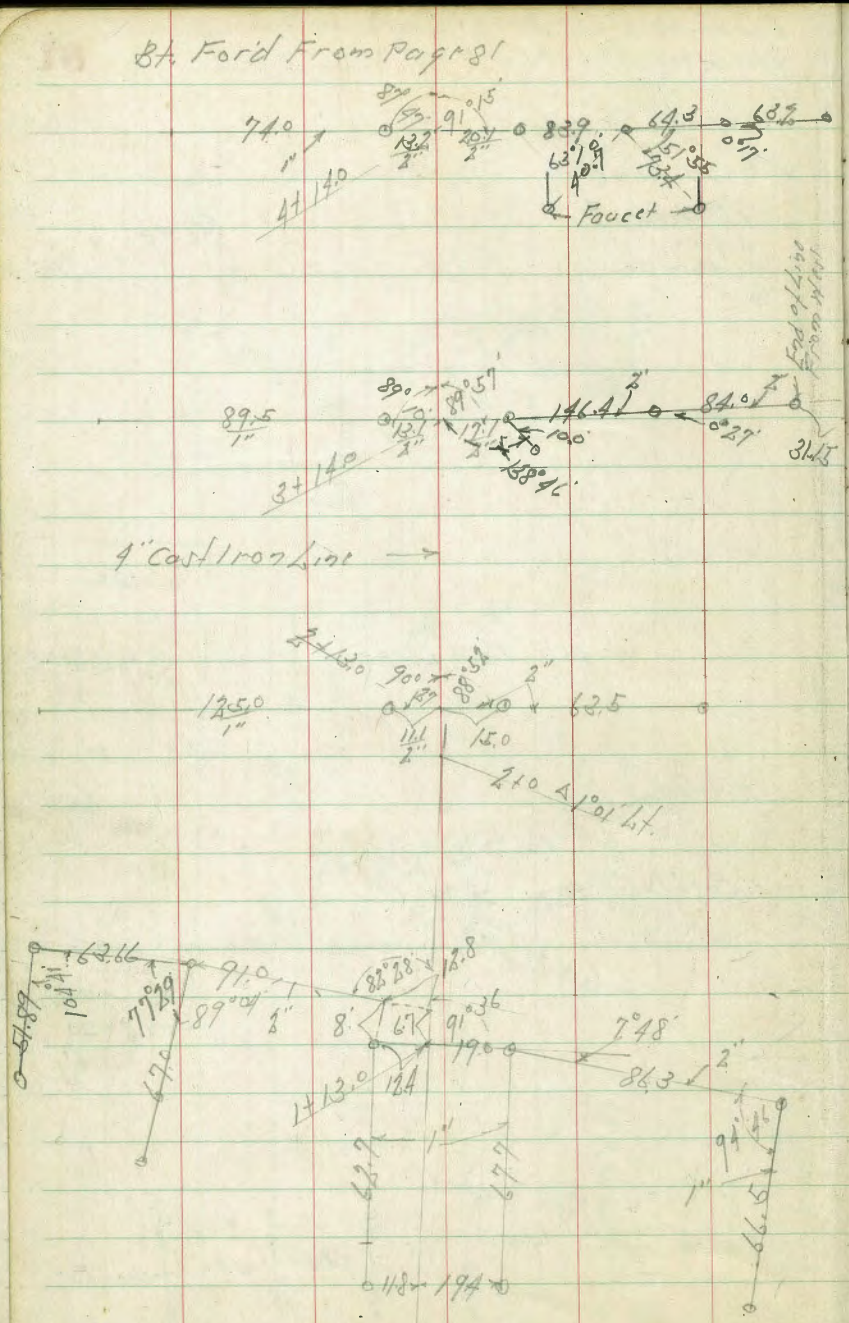
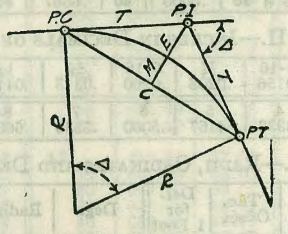


DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES



CURVE FORMULAS

Radius=R=$\frac{50}{\text{sin. } D/2}$ (1) Degree of Curve=D and sin. $\frac{D}{2}=\frac{50}{R}$ (2)

Tangent=T=R tan $\frac{\Delta}{2}$ (3) Length of Curve=L=$100\frac{\Delta}{D}$ (4)

Middle ordinate=M= R(1—cos. $\frac{\Delta}{2}$) (5) =Rvers $\frac{\Delta}{2}$ (6)

External=E=T tan $\frac{\Delta}{4}$ (7) =R÷cos. $\frac{\Delta}{2}$—R (8)=R exsec $\frac{\Delta}{2}$ (9)

Long Chord=C=2 R sin. $\frac{\Delta}{2}$ (10) Δ=Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. Δ=62° 10′ D=8° 20′. From Table IV for 1° curve T=3454.1 and ÷8⅓=414.49 ft. From Table V correction=.36 or T=414.85 ft. P. C.=Sta. P.I.—T=157+45.50. Also from (4) L=746.00 and P. T.=Sta. P. C.+L=164+91.50.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset=7.27 (54.50÷100)²=2.16 ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus (54.50)²÷(2 x 688.26)=2.16 ft.

Deflections.—Deflection angle=½ D for 100 ft., ¼ D for 50 ft., etc. For c ft.=(in minutes) .3 x C x D° or=defl. for 1 ft. from Table III x C. For Sta. 158 of above curve=.3 x 54.5 x 8⅓=136.2′ or 2° 16.2′, or=2.50 x 54.5=136.2′ from Table III. For Sta. 159 deflection angle=2° 16.2′ +8° 20′ ÷2=6° 26.2′, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve E=960.6 for 8° 20′=960.6÷8⅓=91.27 and from Table V correction=.10 or E=91.37 ft. Or suppose Δ=32° and E is measured and found to be 42 ft. What is D? From Table IV E=230.9 and ÷42=5.5 or D=5° 30′.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20—16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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