1595

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

The paper stock of this book is made of a **high grade 50% rag** paper having a **water resisting surface.** This book is sewed with Bing **Special Enamel Waterproof Thread.**

Made in U. S. A.

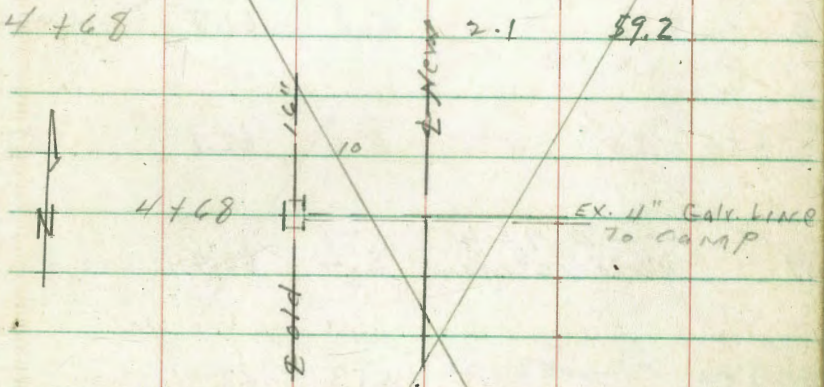
Levels on Proposed 2" Water Conc. Pipe Line.
Torrey Pines Mesa.

BM. #45	7.10	361.28	354.18	1½" pipe
0+00 N/L Scripps Prop.		5.3	356.0	
0+50 N/L		5.1	56.2	
1		4.7	56.6	
+50		4.0	57.3	
+70		2.6	58.7	
2		4.0	57.3	
+50		4.5	56.8	
3		4.6	56.7	
+50		5.0	56.3	

Line Change
See P. 9

Melexed C.S.I.C. 361.28

4+00		4.2	357.1
+50		3.1	58.2
4+68		2.1	59.2
4+68			Ex. 4" Galv. Line To Camp
5+00		1.5	59.8
T.P.	7.66	367.59 1.35	359.93
5+50		7.5	60.1
6		6.3	61.3
+50		6.4	61.2



		367.59			
7 +00			5.2	362.4	
7 +00	Cross old 16" Wood LINE		8.4	59.2	Top Pipe
+50			5.7	61.9	
8			5.8	61.8	
+50			5.5	62.1	
9	New ℄ 9.5 W of old 16" Main		5.2	62.4	
+50			5.3	62.3	
10			5.7	61.9	
+50			5.4	62.0	
11			5.7	61.9	
T.P	8.1 W	370.6 W	5.09	362.50	

	370.62			2
11 +50		8.4	362.2	
12		8.0	62.6	
+50		6.7	63.9	
13		7.6	63.0	
+50		6.8	63.8	
13 +55 to 14 +60		10 ~~Large Eucal. Trees 18" diam. on LINE~~ Trees out		
14		6.3	64.3	
+50		6.0	64.6	
15		6.8	63.8	
+39.2 W	P.I. Δ = 7°30' Lt. 5°45'15"	7.2	63.4	650 R ℄ 21' P.I.C

STAKE ↗ Meas.

	370.62		
15+50		7.1	363.5
16		7.0	63.6
+50		7.8	62.8
17		7.5	63.1
T.P. +24	368.80	6.06	364.56
+50		6.5	62.3
18		6.5	62.3
+04		9.0	59.8
+07		9.0	59.8
+12		6.5	62.3

	368.80		
+20		6.6	362.2
+24		8.5	60.3
+28		8.5	60.3
+33		6.6	62.2
+50		6.4	62.4
19+00		7.2	61.6
+50		8.0	60.8
20		8.2	60.6
+50		7.7	61.1
21		7.4	61.4

		368.80			
21+50			9.0	359.8	
22			7.5	61.3	
T.P.	5.60	368.60	5.80	363.0	
+50			6.7	61.9	
23			6.7	61.9	
+50			5.3	63.3	
24			5.1	63.5	
+50			5.8	62.8	
25			5.2	63.2	
+10			4.6	64.0	

		368.60			
+50			5.2	363.4	
+75			4.9	61.7	
26			6.8	61.8	
+50			8.3	60.3	
27			8.1	60.5	
+50			9.1	59.5	
28			9.5	59.1	
T.P.	1.49	369.4	7.15	361.45	361.66
+50			2.2	358.7	
29			5.1	57.8	

BM = 24000.00 N, 16000.00 E.

	362.94		
+50		5.6	357.3
30		5.5	57.4
+51		6.0	56.9
31		6.5	56.4
+50		6.9	56.0
32		7.1	55.8
+50		7.2	55.7
33		7.5	55.4
+50		8.5	54.4
33+85		8.6	54.3

	362.94			
33+85	18' West	9.8	353.1	For Blow off in Canon
" "	30' "	13.8	49.1	
34		8.7	54.2	
+50		8.1	54.8	
35		7.5	55.4	
+50		5.8	57.1	
36		6.1	56.8	
+50		4.8	58.1	
37		3.5	59.4	
T.P.	9.38	367.95	4.37	358.57

		347.95							
37+50			9.3	358.7					
38			9.7	58.3					
+50			9.6	58.4					
39			7.6	60.4					
+50			6.5	61.5					
40			6.3	61.7					
+50			5.8	62.6					
check	to 1/2" Pipe #35		5.07	362.88 ✓	362.93				
+80	in wash		5.8	62.2	to west				
41			5.0	63.0					

		347.95							
+50			5.2	362.8					
42			5.0	63.0					
+50			4.9	63.1					
43			4.8	63.2					
+50			4.7	63.3					
44			4.4	63.6					
TP		6.40	370.70 ✓	3.45	367.30 ✓				
+50			7.0	63.7					
45			6.6	64.1					
+50			7.0	63.7					

	370.70			
46		6.8	363.9	
+50		6.6	64.1	
47		6.8	63.9	
+50		7.2	63.5	
48		6.8	63.9	
+50		6.1	64.6	
+88 E 30'	5 t w dirt Rd.	5.6	65.1	
49		5.6	65.1	
+50		5.8	64.9	
+68 in wash		8.0	62.7	

	370.70			6
+90		5.6	365.1	
50		5.4	65.3	
+50		5.1	65.6	
51		5.2	65.5	
+50		5.2	65.5	
52		5.0	65.7	
+50		5.0	65.7	
53		4.7	66.0	
T.P.	2.70	369.94	3.46	367.24
+50			3.5	66.4

	369.94			
54		4.0	365.9	
+50		4.6	65.3	
55		5.4	64.5	
BM #31		9.55	360.39	360.41

Bliss Notes
Sommermeyer & Beggs Prod.
12/21/41

℄ Rosecrans

41+93.99 L.W.

20'

℄ Proposed Sewer

41+40 ±ot Rock + Oil Paving

Sketch showing retracement of Sewer 5' South of the Northly line of Frontier St at Pacific

Note Stations to New ch. East of EC. 17+19.16 Given as ± because of the difficulty of reconning line through Parked Cars

Note
Elec Lite Power Poles (New) are set 3' from N. Line. N. Line Taste of Poles

℄ Proposed Sewer

9.5

Paved Area

N. Line Frontier

23+00± End Oil & Rock Paving

21+63.5 End A.C. Paving

12' Gas Pumps

Concrete Loading Rock for Gas pumps

20+06

19+86±

40±

17+19.16 EC

See Page 24 Data on this for curve

16+50± ±ot Newick

15+95.9 ±ot W Edge Pacific Ave

℄ Consolidated Overhead

℄ Proposed Sewer

Pacific

Line Change

0+0 to 9+29.34 = Δ 2°34' Lt.

BM #45	10.31	364.49		354.18	½" Pipe
0+0			9.8	54.7	
+50			10.0	54.5	
1			9.9	54.6	
+50			8.7	55.8	
+65			8.8	55.7	
+70			7.3	57.2	
2			7.5	57.0	
+50			9.6	54.9	
3			9.5	55.0	
+50			9.4	55.1	
4			8.8	55.7	
+50			7.8	56.7	
5			6.7	57.8	
+50			5.9	58.6	
6			5.5	59.0	
+50			4.1	60.4	
7			3.1	61.4	

364.49

7+50		3.3	361.2
8		3.3	61.2
+50		2.6	61.9
9		2.5	62.0
+29.34 = Δ 2°34' Lt.		2.3	62.2
+50	same as PT	2.2	62.3

= Intersection of Line to North which is 5' W of WL of 40' Road.

New Line 4' E of Pueblo Line and 11' W of ℄ of 16" Wood Line

Location changed to 10' W of W.L.

Moore
6-4-41. Interceptor Sewer
via Frontier St. Pacific to Rosecrans

27 + 01 ℄ P.P.

26 + 83 beg. Evergreen hedge 3' wide 8' high
Trunks 5' Rt.

26 + 75

26 + 00 Int. 36" Corr. I. P. C.M. 1.9 Rt. to Inlet

24 + 01 ℄ P.P.

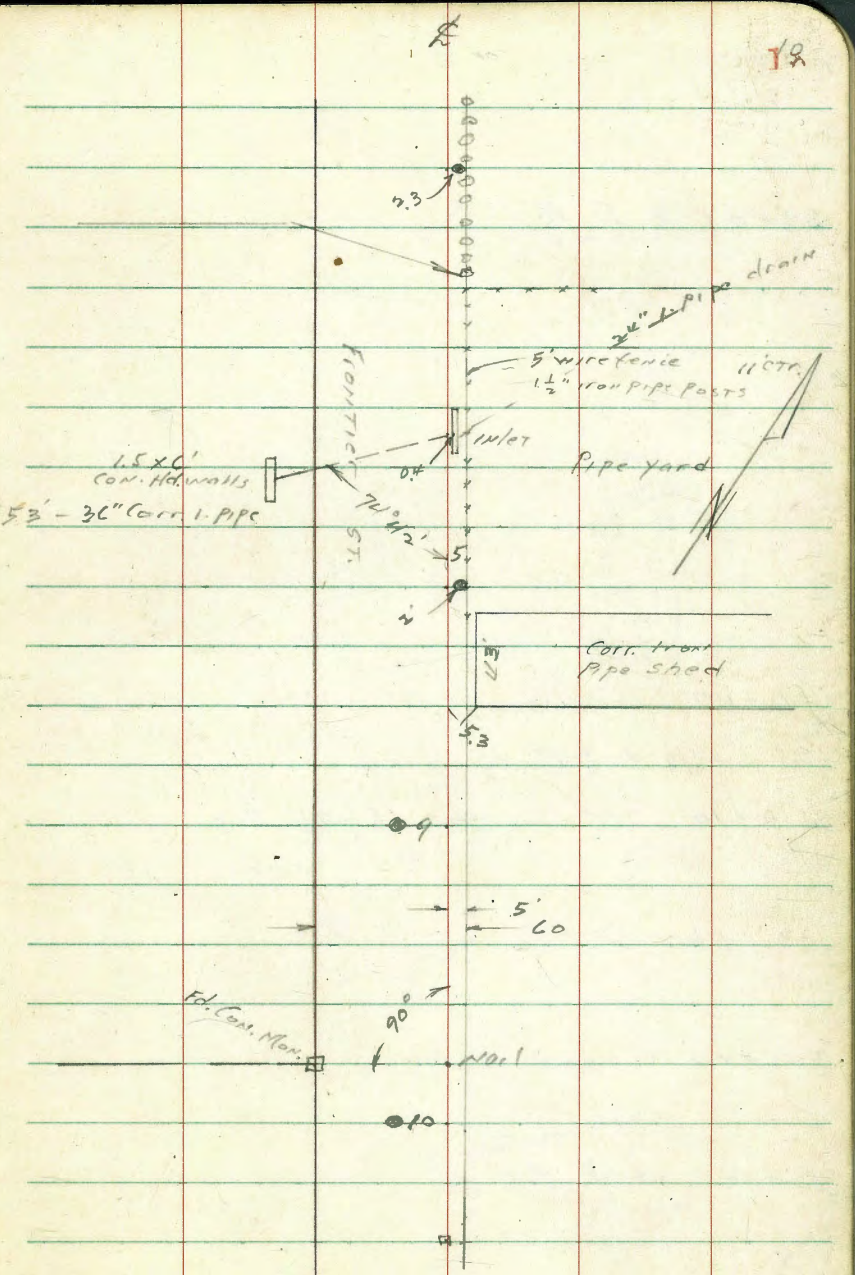
23 + 09

21 + 00 ℄ P.P.

18 + 37.40 Cor. Mon. Pueblo Cor.

18 + 00 ℄ P.P.

16 + 83.00 E.C. From F.B. 1604



39+01 E P.P.

36+47

35+79 ℄ P.P.

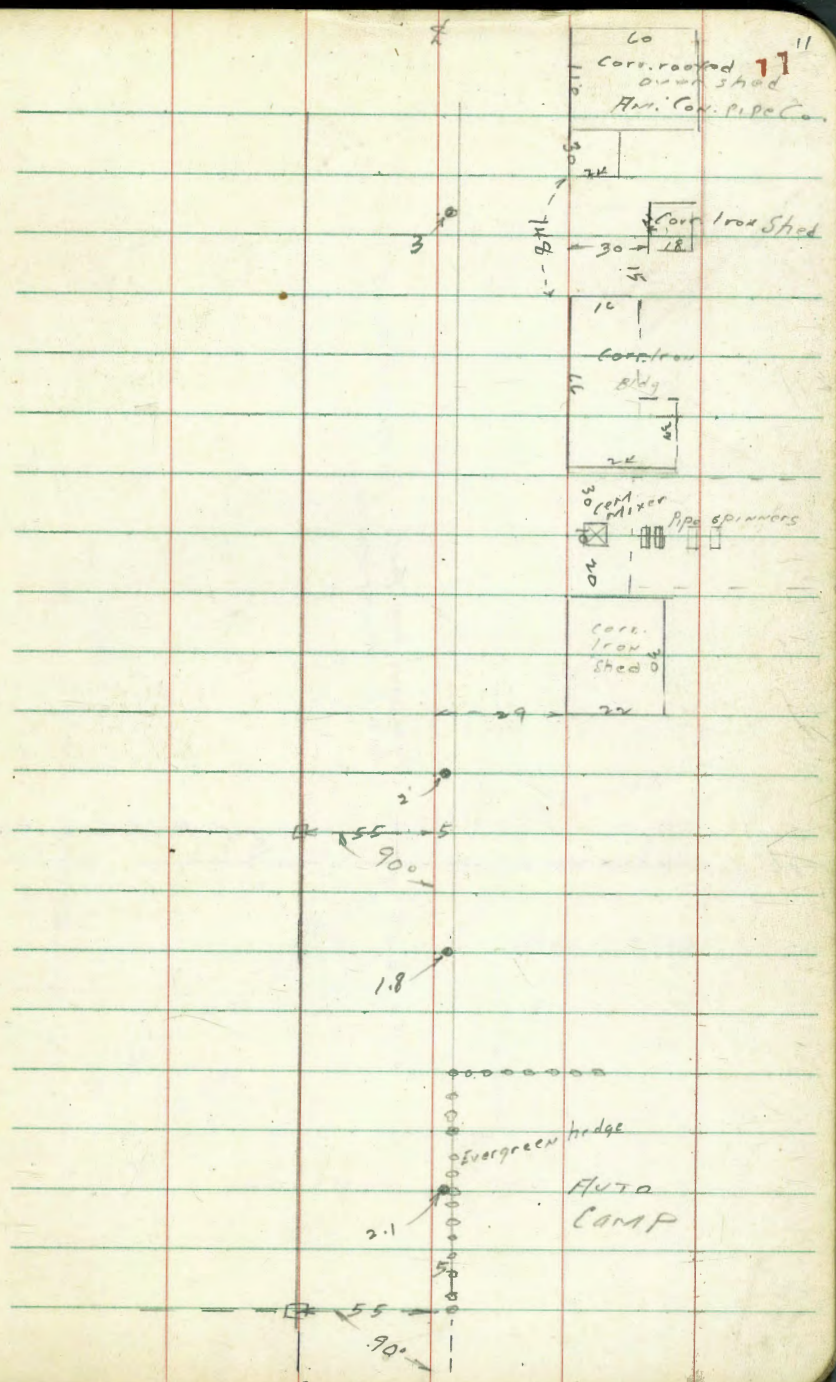
35+11.10 Fd. Con. Mon. Pueblo Cor.

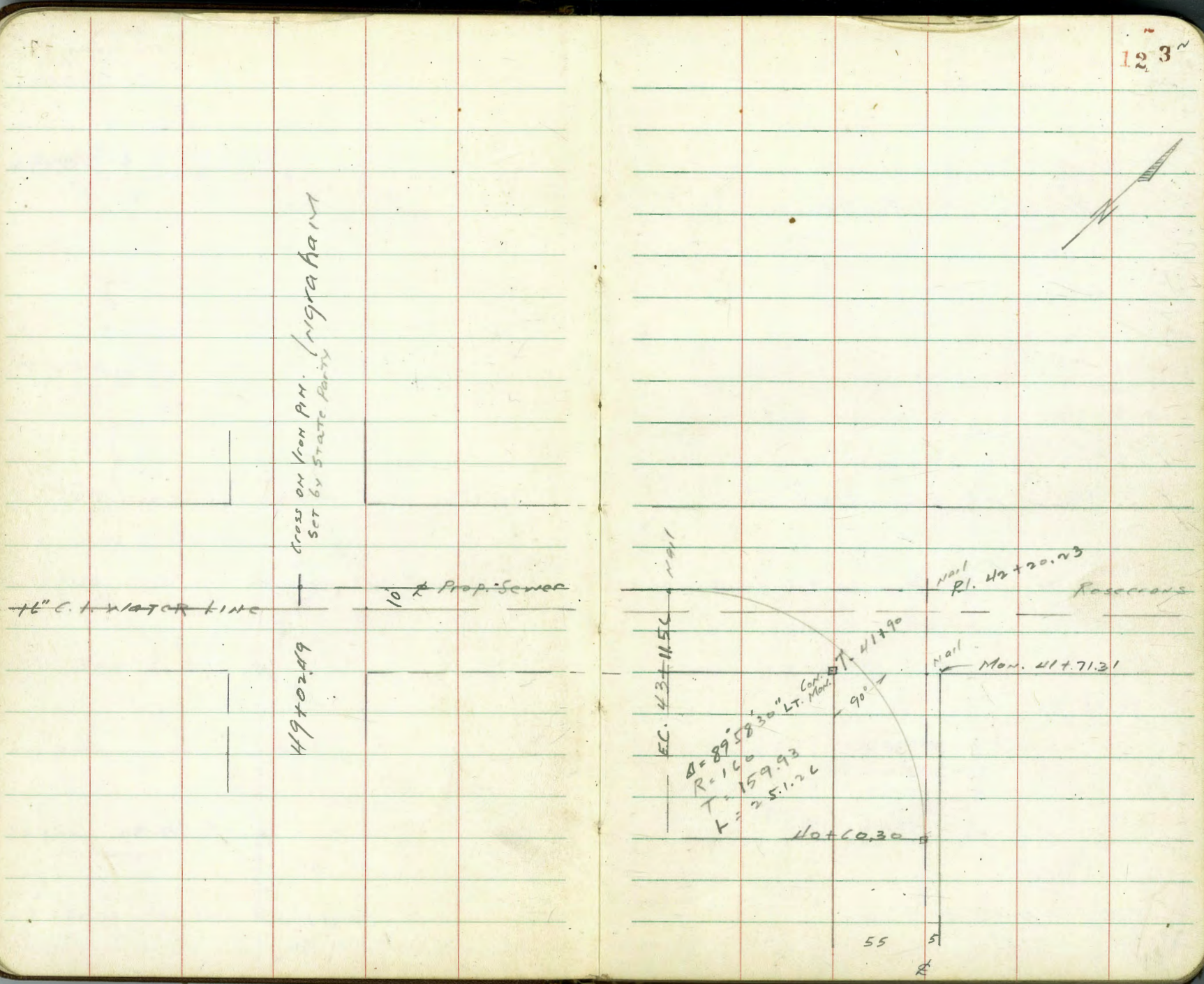
33+00 ℄ P.P.

32+40 end hedge

30+00 ℄ P.P.

28+50.77 Fd. Con. Mon. Pueblo Cor.




Cross on iron pin. (Migrant
Set by State Party
10" Prop. Sewer
Nail
Nail
Pl. 42+20.23
Reservoir
Nail
Mon. 41+71.31
Cor. Mon.
T. 41+90
90°
EC. 43+11.54
Δ=89°58'30" LT.
R=160
T=159.93
L=251.26
40+60.30
55
5

Line change of 6-11-41

Interceptor Sewer

via Pacific from

Barnett to Rosecrans

Acct. of water, rel. St. lights etc.

6+25 ℄ 5 Lt St. Lite

6+01 end A.C. Pav of Texaco Oil Sta

5+07.4 ℄ Texaco gas pumps & 5 gas tanks

4+08 ℄ 10 Lt = St. Lite

3+70.36 E.C. N

Δ = 37°30' R

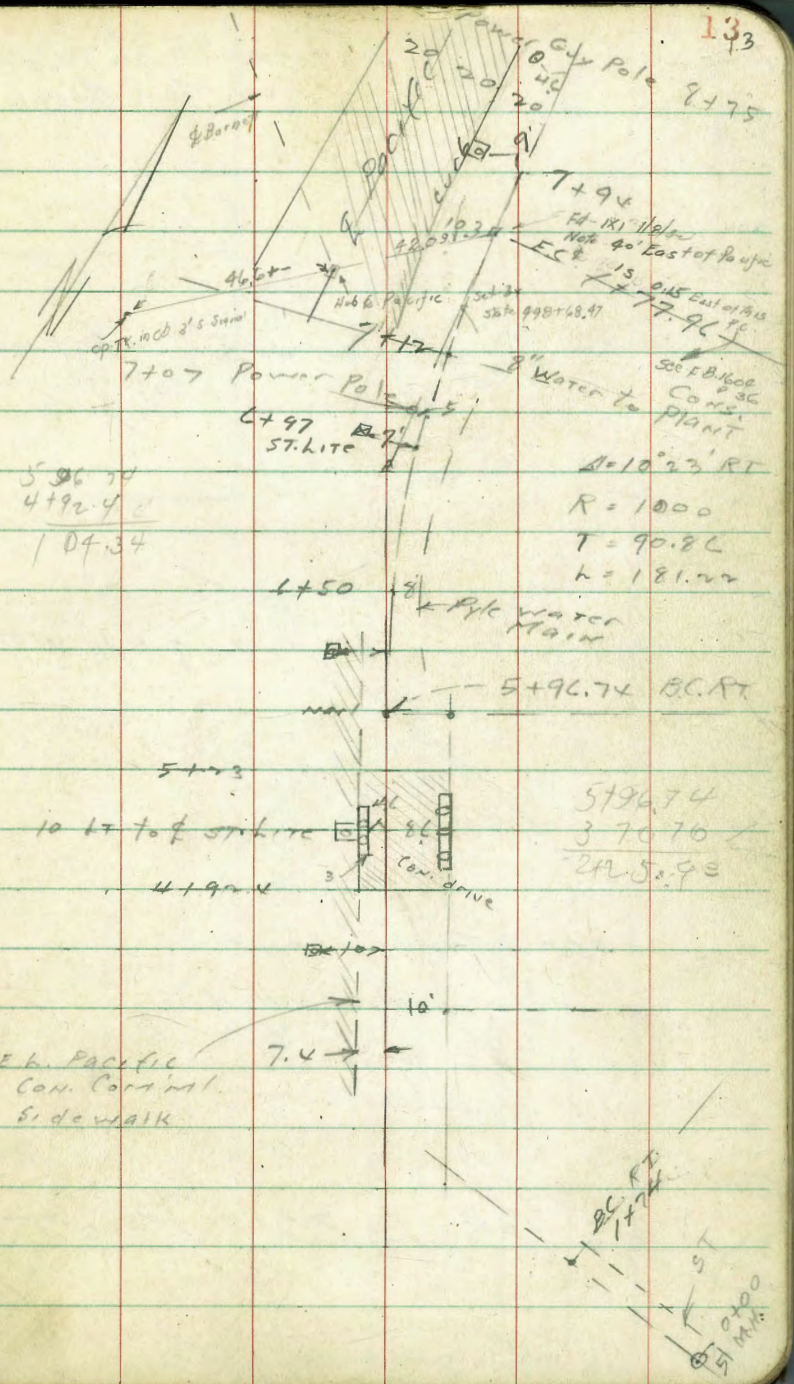
R = 303.4'

T = 102.99

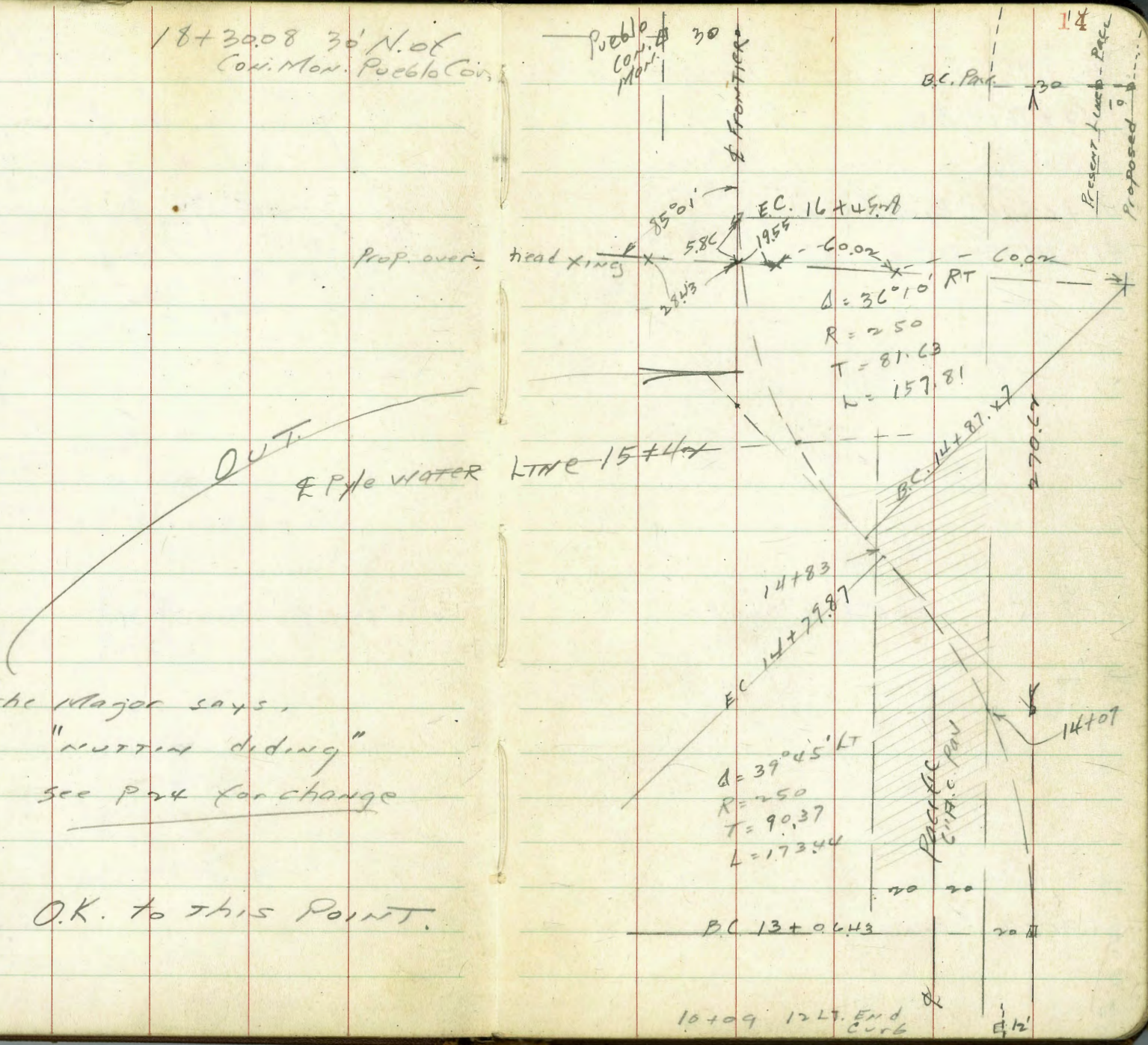
L = ~~196.16~~ 198.57

~~1+[illegible]~~ BC

0+00.21 = 0+00 of old line.



18+30.08 30' N. of Con. Mon. Pueblo Con.



the Major says,
"Nutting Riding"
see Park for change

O.K. to this Point.

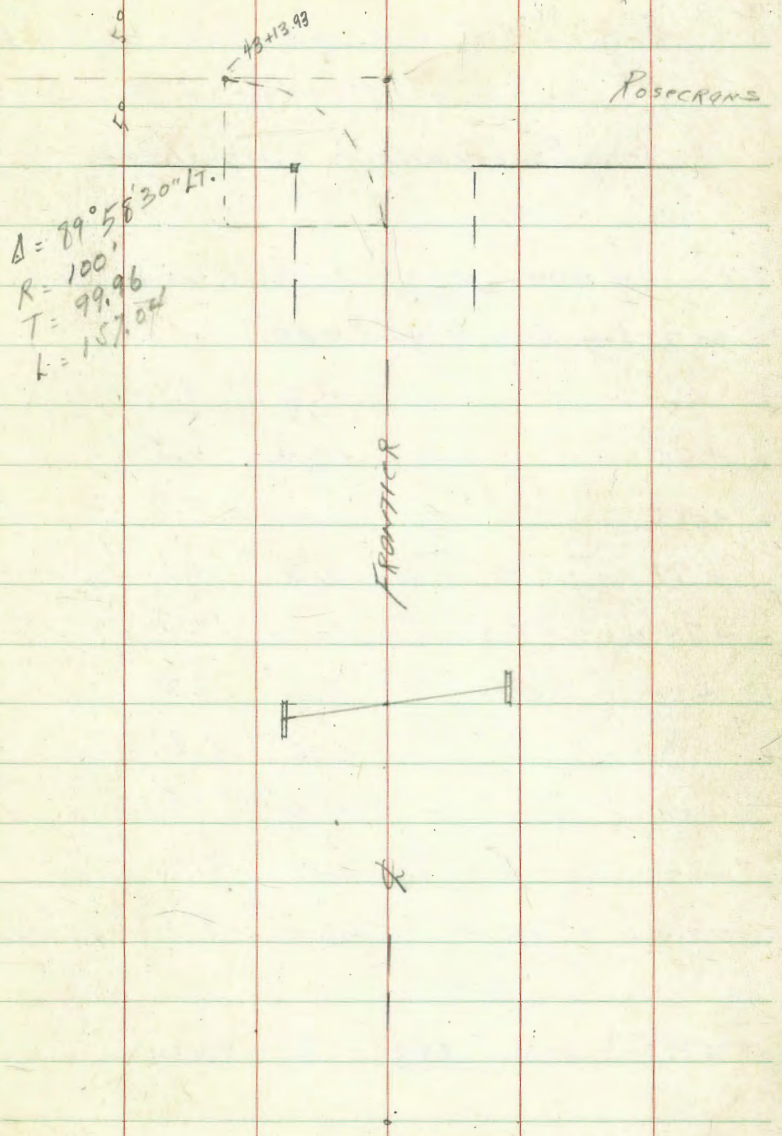
(48+96.97) = Center of Ingraham and Rosecrans.

(42+71.07) E.C.

44° 59.25
38° 57.1
24° 37.7
10° 8.2C

•41+62.99 Pueblo Cor.

(41+14.03) B.C.L.



G.R.M.
(25+85.85) 36" Conc. Iron Pipe Culv.

18+30.08 P.C. to Line

Moore
Osborne
D. Farrow

6-14-41

Levels for Interceptor Sewer
beg. at Pump at Wilthercby &
Kurtz via Pacific & Frontier
to Rosecrans & Ingraham

T.P.	4.991	6.196	4.68	1.204
+27	beg. Conc. Drive		4.69	1.19.
3			4.8	1.1.
+75			5.4	0.5.
2 +25			5.0	0.9.
+97			4.8	1.1.
+74.21	BC R7		4.7	1.2.
+50			4.7	1.2
1			4.6	1.3.
+50			4.4	1.5.
+25			3.1	2.8.
0+00.21 = M.H.			2.15	373. 2x2 Hub
BM. BP.	3.143	5.884		2.454

Top W. end of 1.5. Ret. wall on N. side Wilthercby Kurtz

7+77.9℄ = E.C.			6.5	2.1.	
T.S.	6.10	4.69	3.487	2.509.	
+50			4.0	2.2.	
7+19	Top 8" water Pipe		5.5	-2.3.	
7+00			5.00	1.0.	ground.
7			4.0	2.2.	
+50			5.0	1.2.	
+30	Now off the Pav.		4.1	2.1.	
6+01	end of AC Pav		4.96	1.24.	
5+96.7	BC. Rt.		5.00	1.20.	AC Pav.
+50	AC Pav.		5.02	1.18.	
+23	Wedge Conc. dr.		5.05	1.15.	beg. AC Pav
5	Conc Dr.		5.12	1.06.	
+92	S. edge Conc Dr. end AC Pav		5.12	1.08.	Texaco Oil Sta
+50			5.00	1.20.	
+34	end Conc Dr. beg AC		4.86	1.34.	
4	Conc.		4.96	1.24.	
+70.36	= E.C. Conc.		5.16	1.04.	
3+50		Conc	5.24	0.94.	
		6.19℄			

+83 W edge Pav		6.89	1.97	
+79.87 E C Pav.		6.80	2.00	
+50 Pav C"HC		6.70	2.16	
+09.07 E edge Pav		6.88	1.98	
14		6.9	2.0	
+50		7.2	1.7	
+04.43 BOLT		7.0	1.9	
13		6.9	2.0	
TP	6.03	8.859	5.78	2.879
+50		6.7	1.9	
12		6.6	2.0	
+50		6.5	2.1	
11		7.2	1.4	
+50		7.1	1.5	
10		6.7	1.9	
+50		6.7	1.9	
9		7.6	1.0	
Ed. BM. by State		5.90	2.709	2.72
+50		4.8	1.8	
8+00		7.5	2.1	
	8.609			

RR. spike in Guy Pole 5' Lt of 8+75

22			4.7	2.8	
+50			4.7	2.8	
21			4.8	2.7	
T.P.	4.845	7.453	5.977	2.628	
+50			5.9	2.7	
20			5.8	2.8	
+50			5.7	2.9	
19			5.8	2.8	
+50			6.0	2.6	
B.M.			6.59	2.015	Sq. ½" iron pin & Pacific Pow. on B.C. RT. Pacific & Frontier
18			5.7	2.9	
+50			6.2	2.4	
17			6.1	2.5	
T.P.	5.367	8.605	5.621	3.238	
16+45.8 E.C.			6.5	2.4	
16			6.2	2.7	
+50			6.4	2.5	
15			7.5	1.4	
14+87.4 7B.C RT.			7.0	1.9	
		8.859			

			4.8	3.1'		
+50			4.8	3.1'		
			4.8	3.1'		
+50			4.9	3.0'		
			4.9	3.0'		
+50			4.8	3.1'		
			4.9	3.0'		
T.P.	7.498	7.871	7.08	0.373	Mkd. 0.51	on Cons. Aircraft B.M. S.E. Cor. of Culv. Top Hd.wall
N5+85.85	Int. 36" Culv.		4.6	2.9'		Fl. outlet 11.14 Lt. See P.10 11.05 Rt. Fl. inlet Culv.
						This Culv. takes storm water from Old Tarmac & Mission Hills
+50			4.6	2.9'		
N5			4.8	2.7'		
+50			4.8	2.7'		
N4			5.0	2.5'		
+50			4.7	2.8'		
N3			4.7	2.8'		
+50			4.9	2.6'		
		7.453				

+50			5.1	2.7
T.P.	5.24	7.83	5.07	2.59
35			5.1	2.5
+50			5.1	2.6
34			5.1	2.6
+50			4.9	2.8
33			5.0	2.7
+50			5.0	2.7
32			5.0	2.7
+50			4.7	3.0
31			4.8	2.9
T.P.	4.68	7.66	4.885	2.98
+50			4.9	3.0
30			4.9	3.0
29 +50			4.7	5.2
		7.871		

B.M. 30d spike			4.568	3.186'
+50			4.7	3.1
+1403 BC LT.			4.8	3.0
41			4.8	3.0
+50			4.9	2.9
40			4.8	3.0
T.P	4.80	7.754	4.88	4.95
+50			4.9	2.9'
39			5.1	2.7'
+50			5.1	2.7'
38			5.0	2.8'
+50			5.0	2.8'
37			5.1	2.6'
+50			5.1	2.7'
36			5.1	2.7'
		7.834		

NWly Cor. Power Pole Rosecrans & Frontier

48			5.7	0.8 ✓					
+50			5.3	1.2 ✓					
47			5.1	1.4 ✓					
+50			4.8	1.7 ✓					
46			4.6	1.9 ✓					
+50			4.4	2.1 ✓					
45			4.3	2.2 ✓					
+50			4.2	2.3 ✓					
44			4.1	2.4 ✓					
T.P.	3.767	6.49	5.031	2.723 ✓					
+50			5.1	2.7 ✓					
43			4.9	2.9 ✓					
+71.07 E.C.			4.7	3.1 ✓					
+50			4.6	3.2 ✓					
+15 Now on Pav.		0.1	4.5	3.3 ✓					
42			4.2	1.6 ✓					
41+75			4.2	3.6 ✓					
		7.754							

F.B. 1423 - 25

El. 0.487 from La Playa

					Sw. for Ingraham				
check to BP Cur. 6					Rosecrans	4.85	0.53 ✓	0.56-LITY	
								0.03	
48+96.97 E					Ingraham Rosecrans	5.0	0.4 ✓		
48+48.97 beg. C-H-C Pav.					end 0.1	4.7	0.7 ✓		
T.P.			4.568	5.38		5.678	0.81 ✓		
				6.49					

Moore Osborne Corner 6-25-41

Line Change, Pac. & Frontier. Via Frontier to Roseerans

Δ = 89°58'30" LT

Please Calc. Sta.

Move all pav. job on Roseerans. all orig. pts. out

was Sta. 18+30.08 on ℄ Frontier St

18+07.04 = 55' N of Con. Mon. Pickle Cor.

Also see p 10 this Book.

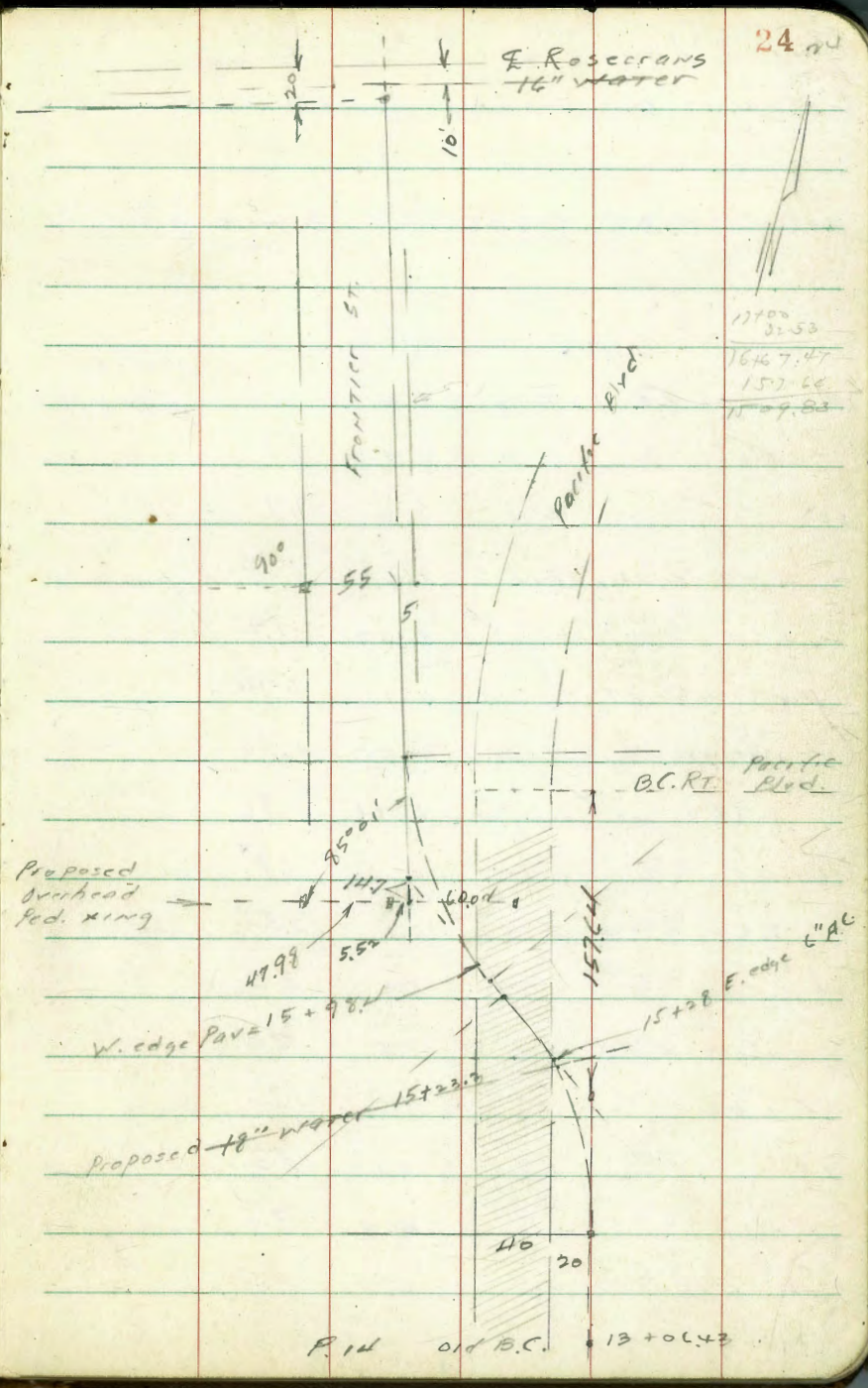
17+14.16 E.C.

Δ = 3C°10' Rt
R = 200
T = 55.30
L = 112.25

15+87.91 B.C. Rt.
15+76.78 E.C.

Δ = 39°45' Lt
R = 200
T = 72.30
L = 138.75

14+37.53 B.C. Lt.



Levels on Line Change

6-25-41. on Frontier St. Pac. to Rosecrans

B.M.	6.35	8.365	2.015	City Datum =
				Red. by ⓦ 6/26/41
14+37.53 B.C. Lt.		6.2	2.2	
+50		6.7	1.7	
15		6.7	1.7	
+28 E. edge Pav.		6.63	1.74	
+50		6.47	1.90	
+76.28 EC.		6.43	1.94	
+87.91 BC Rt		6.53	1.84	
+98.4 W. edge Pav.		6.51	1.86	
16		6.5	1.9	
+50		6.1	2.3	
17		5.1	3.3	
+14.16 EC.		5.5	2.9	
+50		5.1	3.3	
18		5.1	3.3	
+50		4.8	3.6	
19		4.7	3.7	

1/2" Iron Bolt on B.C. & Pacific at Frontier in Paving

8.365

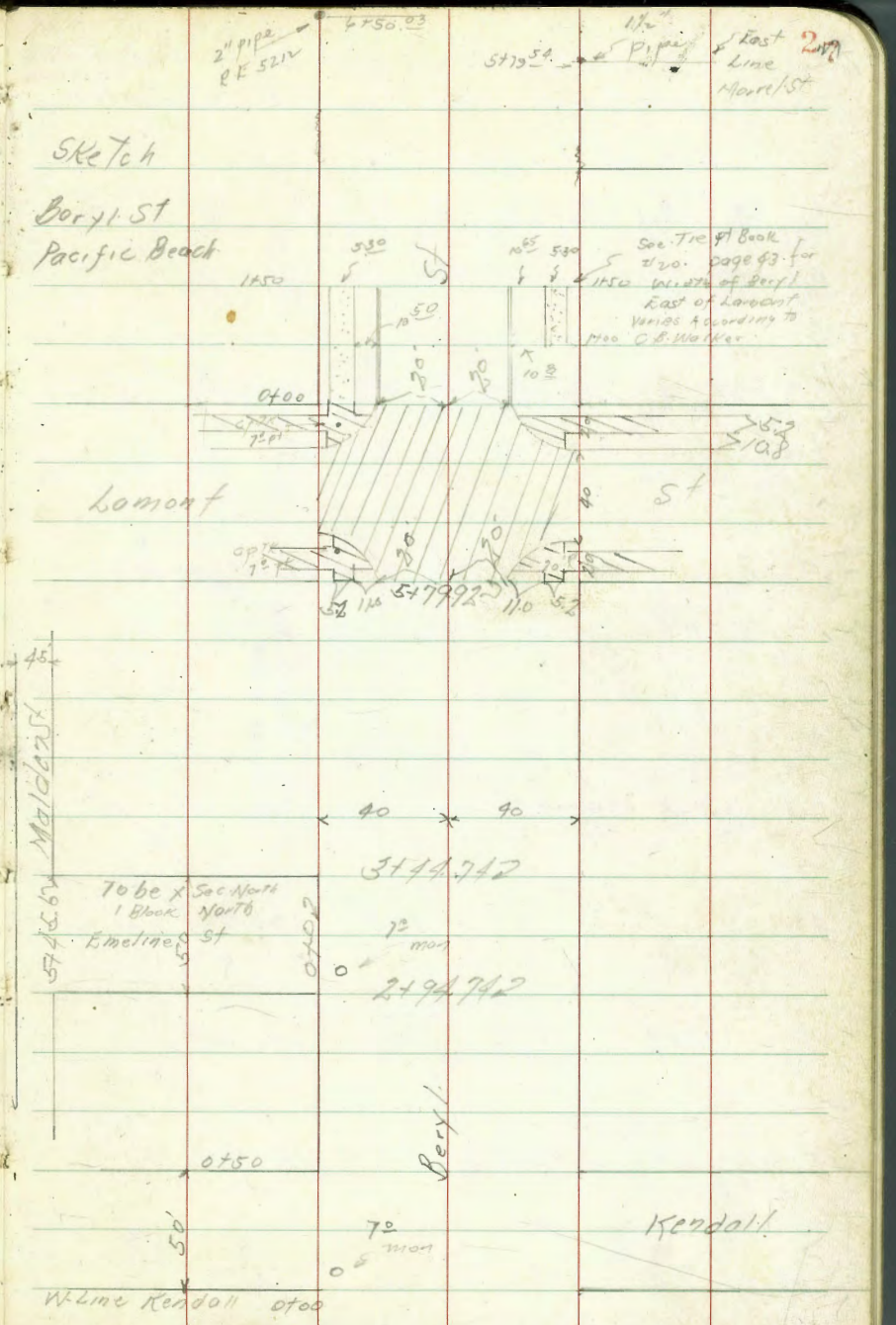
19+50			4.8	3.6	
20			4.7	3.7	
+50			4.9	3.5	
21			4.9	3.5	
+50			5.2	3.2	
T.P.	4.03	7.18	5.215	3.15	
22			4.0	3.2	
+50			4.2	3.0	
23			4.3	2.9	
+10			6.6	0.6	& wash on
+50 = Nat. ground		Elev. New	7.1	0.1	New Fill
24			7.2	0.0	
+50			7.0	0.2	
25			7.2	−0.2	

		7.18			
25+50			7.9	-0.7	
+	Please Calc Sta. EL. 36" Pipe Culv.		10.76	-3.58	Inlet
+	Top hd. wall		6.65	+0.53	P10
+	ground		9.2	-2.0	This Book
26			8.1	-0.9	
+50			8.1	-0.9	
27			6.4	0.8	
+50			6.2	1.0	
28			5.1	2.1	
T.P	4.92	7.59	4.53	2.65	
+50			6.2	1.4	
29			6.0	1.6	
+50			5.6	2.0	
30			5.7	1.9	
+50			5.9	1.7	
31			6.1	1.5	
+50			5.7	1.9	
32					

		7.59		
32+50			6.0	1.6
33			6.5	1.1
+50			7.2	0.4
34			7.6	0.0
+50			7.6	0.0
T.P	5.43	7.85	5.17	2.42
35			7.2	0.5
+50			6.1	1.8
+85			6.7	1.2
36	Stock Pile clay Material		0.8	7.1
+45	"		2.2	5.5
+50	"		3.7	4.2
+60			5.5	2.4
37			5.6	2.3
+50			5.6	2.3
38			5.6	2.3
+50			6.2	1.7
39			6.9	1.0

		7.85			Red. by ⓦ 6/26/41
39+50			6.0	1.9	
40			6.3	1.6	
T.P.	4.77	7.75	4.87	2.98	
41+50			6.3	1.5	
41			6.6	1.2	
41+50			6.6	1.2	
41+75			6.4	1.4	
42+17.19 = A 89°58'30" Lt.			5.4	2.6	
Calc. Sta. Please. P. in this Book.					
check to B.M. P. 22			4.58	3.17	3.186

C.R.H., has this stuff been indexed?



X. Section Beryl St Pacific Beach from W Line Kendall to East of Morrell

See Sketch Page 27

0+40					
0+33	22.5 Lt of Δ : Δ 4' Euc Tree				✓
0+25					
0+22	22.5 Lt of Δ = Δ 3' Eucalyptus Tree				
0+10 = WC 5					
0+0 = W Δ Kendall From N				Reduced and Plotted Profile 1814 7-30-41 EBH	
BM			3.74	173.87	N WY Mon Beryl Kendall
TP	663	177.61	12.07	170.98	
TP	0.06	183.05	11.16	182.99	
BM	7.86	194.15		186.29	S.E. Δ T Wilburn LaMont

Indexed
LMT

Levels July 23-41 2846
S.J.S.07
Northern
Rt = S W Moore

Lt = N			Δ						
174.9	174.7	174.4	173.7	172.7	173.0	172.3	169.9	168.1	166.1
2.7	3.9	4.2	4.0	4.9	4.6	5.3	7.7	9.5	11.5
40	30	20	16		5	20	30	40	55
175.1	174.8	175.6	175.2	173.6	172.7	172.5	173.2	172.4	170.1	168.6	166.1
2.5	2.8	2.0	2.4	4.0	4.9	5.1	4.4	5.2	7.5	9.0	11.5
40	30	25	20	16		5	10	20	30	40	55
174.5		173.7		173.5	172.4	172.2	173.1	172.7	170.0	168.9	166.0
3.1		3.9		4.1	5.2	5.4	4.5	4.9	7.6	8.7	11.6
40		35		20		5	10	20	30	40	55
176.7	173.1			173.6	172.0	171.7	172.9	172.2	169.5	168.2	165.8
0.9	4.5			5.0	5.6	5.9	4.7	5.4	8.1	9.4	11.8
40	27			20		5	10	20	30	40	55

177.61

		Lt			℄			Rt		
		1738	171.7	169.9	169.2	167.6	167.4	168.2	166.8	164.9	163.3
		3.8 40	5.9 30	7.7 20	8.4 18	10.0	10.2 2	9.4 5	10.8 20	12.7 40	14.3 55
2+00											
1+85	37.0 Lt of ℄ = ℄ of Cypress Ter.	1743	172.6	171.3	170.4	169.1	168.9	169.4	167.7	165.5	164.0
1+75		3.3 40	5.0 25	6.3 20	7.3 18	8.5	8.7 2	8.2 5	9.9 20	12.1 40	13.6 55
1+50		1749	1734		1712	1702	1701	1686	1665	1638	
		2.7 40	4.2 30		6.4 20	7.4	6.9 5	9.0 20	11.1 40	13.8 55	
1+00		1753	1734		1724	1714	1716	1692	1669	1641	
		2.3 40	4.2 30		5.2 20	6.2	6.0 5	8.4 20	10.7 40	11.5 55	
0+90	21.0 Rt of ℄ = ℄ Fire Hyd.	1754	1735		1728	1718	1717	1722	1698	1672	1652
0+80		2.2 40	4.1 30		4.8 20	5.8	5.9 2	5.4 5	7.8 20	10.4 40	12.0 55
0+50 = EL Kendall		1756	1733		1721	1722	1722	1727	1719	1691	1676	1658
		2.0 40	4.3 27		4.5 20	5.4	5.4 3	4.9 6	5.7 20	8.5 30	10.0 40	11.8 55
	177.61					177.61					

Beryl St

3+48	25.0 Rt of ℄ = ℄ Euc Tree				✓
3+44.74 = E.L. Emelene					
3+37	25.0 Rt of ℄ = ℄ Euc Tree				✓
3+34.74 = Ecb Line					
3+19.74 = ℄ Emelene					
3+04.74 = Wcb Line					
2+96	26.0 Rt. of ℄ = ℄ Euc Tree				✓
2+94.74 = W.L. Emelene					
2+93	22.0 Lt of ℄ = Power Pole				✓
TP	4.17	170.28	11.50	166.11	Rail Pole 2+93
2+50					
		177.61			

Lt		℄		Rt		30
	164.6	163.7	162.5	162.3	162.1	161.3	159.1	158.3
	5.7 40	6.6 30	7.0 20	7.8	8.0 5	8.2 10	9.0 20	11.2 40	12.0 55
	164.4	163.9	163.6	162.6	162.3	162.7	161.5	159.3	158.0
	5.9 40	6.4 30	6.7 20	7.7	8.0 5	7.7 10	8.8 20	11.0 40	12.3 55
	165.1	164.2	163.7	163.1	162.9	163.5	162.2	160.1	159.6
	5.2 40	6.1 30	6.6 20	7.2	7.4 5	6.8 5	8.1 20	10.2 40	11.7 55
	166.6	165.4	164.1	163.7	163.5	164.0	163.1	161.3	160.2
	3.7 40	4.9 30	6.2 20	6.6	6.8 4	5.3 7	7.2 20	9.0 40	10.1 55
	167.6	166.5	165.7	164.5	164.1	163.9	164.5	163.7	161.7	160.5
	2.7 40	3.8 30	4.6 20	5.8 18	6.2	6.4 5	5.8 7	6.6 20	8.6 40	9.8 55
				170.28						
	171.1	169.2	167.5	166.9	165.5	165.5	166.4	165.2	163.4	162.2
	6.5 40	8.4 25	10.1 20	10.7 18	12.1	12.1 3	11.2 6	12.4 20	14.2 40	15.4 55
				177.61						

		Lt.	℄	Rt.
5+50		1669	1637	1650
		3.4	4.6	5.3
		40	30	20
5+41	21' Rt of ℄ = ℄ 10" Olive Tree ✓	1643	1637	1648
		6.0	6.6	5.5
		20	20	20
5+35	22' Lt of ℄ = ℄ Anchor Pole ✓	1637	1637	1639
5+08	25' Rt of ℄ = ℄ 24" Euc Tree ✓	6.6	6.6	7.4
5+0		6	9	40
		1631	1650	1648
		8.3	5.5	5.5
		55	20	20
		1676	1668	1636
		3.7	3.5	4.7
		40	30	20
		1652	1649	1647
		5.1	5.1	5.6
		15		10
		1647	1634	1636
		5.6	6.9	7.7
		20	40	55
4+75		1684	1668	1653
		1.9	3.5	5.0
		40	30	20
		1646	1642	1646
		5.7	6.1	5.7
		15		10
		1644	1630	1622
		5.9	7.3	8.1
		20	40	55
4+68	35' Rt of ℄ = ℄ 30" Euc Tree ✓	1669	1657	1649
4+50	35' Rt of ℄ = ℄ 24" Euc Tree ✓	6.5	4.6	5.4
		40	30	20
		1637	1634	1632
		6.6	6.9	7.1
		15		6
		1634	1631	1626
		6.9	7.2	7.7
		10	20	40
		1620		
		8.3		
		55		
4+0		1655	1645	1629
		4.8	5.8	7.4
		40	30	20
		1624	1634	1621
		7.9	7.9	8.7
		17		10
		1611	1584	1581
		9.2	10.9	13.2
		20	30	40
		1578		
		13.5		
		55		
3+96	26.5' Lt of ℄ = ℄ Power Pole ✓			
3+88	25.0' Rt of ℄ = ℄ 14" Euc Tree			
3+67	25.0' Rt of ℄ = ℄ 22" Euc Tree ✓			
		16480 ✓		
		5.48		
		39.7 = ℄ Conc Walk		
	170.38	170.38		

Beryl St.

BM	441	165.24	9.25	160.93	SE 7 Lt Beryl St Lamont

6+59.92 = E.L Lamont = 0+0 East

6+39.92 = E Cb Line

6+19.92 = ℄ Lamont

5+99.92 = W Cb Line

5+79.92 = W L Lamont St

5+73

170.28

Lt		℄		Rt	
162.4		162.18		161.53	
7.9		8.10		8.75	
40		20=Cb		20=Gut	
161.26		160.15		160.65	
9.02		10.13		9.63	
		20=Gut		20=Cb	
161.0					
9.3					
40					
162.20		161.67		161.30	
8.08		8.61		8.98	
40=Cb		40=Gut		20	
160.95		160.34		159.91	
9.23		9.94		10.37	
		20		40=Gut	
160.69					
9.57					
40=Cb					
162.33		161.55		161.15	
7.95		8.73		9.13	
40		20			
160.97		160.47			
9.31		9.81			
20		40			
162.20		161.68		161.26	
8.08		8.60		9.07	
40=Cb		40=Gutter		20	
161.05		160.75		160.28	
9.23		9.53		10.00	
		20		40=Gut	
161.18					
9.10					
40=Cb					
162.4		162.16		161.51	
7.9		8.12		8.77	
40		20=Cb		20=Gutter	
161.55		160.61		161.42	
8.73		9.47		8.86	
		20=Gutter		20=Cb	
161.5					
8.8					
40					
163.4		163.5		162.3	
4.9		6.8		8.0	
40		35		20	
162.1		161.8		164.3	
8.2		8.5		6.0	
		6		10	
163.8		163.7		162.6	
6.5		4.6		7.7	
20		30		40	

170.28

1+70			
1+79	25' Rt of ℄ = ∠ 40° Fac Tree	✓	
1+50			
1+15			
1+0	21.8' Lt of ℄ = ∠ Power Pole	✓	
0+99	25' Rt of ℄ = ∠ 30° Fac Tree	✓	
0+79	25' Rt of ℄ = ∠ 36° Fac Tree	✓	
0+58	24.5' Rt of ℄ = ∠ 24° Fac Tree	✓	
0+50			
0+38	24.5' Rt of ℄ = ∠ 18" Fac Tree	✓	
0+35			
0+28	24.5' Rt of ℄ = ∠ 24" Fac Tree	✓	

16534

1618	1603	1595	1598	1596	1591	1585	1586	1583	1580
3.5	5.0	5.8	5.5	5.7	6.2	6.8	6.7	7.0	7.3
40	35	20	15		12	20	30	40	50
1619	1606	1603	1597	1595	1585	1582	1589		1589
3.4	4.7	5.0	5.9	5.8	6.8	6.4	6.4		6.4
40	35	25	20		20	20-Elec	35-Sh Mill		40
1619	1611	1599	1600		1588	1591	1592		
3.4	4.7	5.4	5.3		6.5	6.15	6.1		
40	25	20			20	20	40		
1611	1611.7	1609.4	1600	1601	1591	1594.5	1595.0		1593
4.2	4.7	4.0	5.3	5.2	6.2	5.89	5.84		6.6
40	35	20	20		20	20	35-Sh Mill		40
1616	1611.58	1608	1606		1596	1598	1602		
3.7	3.76	4.5	4.7		5.5	5.26	6.1		
40	20	20			20	20	40		
1619	1611.77	1610	1608		1599	1602.4	1611		1603
3.4	3.57	4.3	4.5		5.4	5.10	4.3		5.0
40	20-CL	20-Gut			20-Gut	20-CL	25		40

16534

Beryl St

3+31

3+20 25' Rt of ℄ = ℄ 24" Euc Tree ✓

3+0

2+96 = ℄ 6.8' ℄ Ribbon Conc Drive 2' Ribbon out ℄

2+90 24' Rt of ℄ = ℄ 15" Euc Tree ✓

2+70 24' Rt of ℄ = ℄ 12" Euc Tree ✓

2+50

2+15

16534

16169 ✓
3.65
40.8-7.3 Conc Wall

164.7	160.7	160.3	159.7	159.1	157.6	158.5 ✓	158.3	157.1	156.8
3.6	4.6	5.0	5.6	6.2	7.7	6.8	7.0	8.2	8.5
40	20	15		12	17	20	30	40	50

16189 ✓
3.45
41.0-7.3 Conc 2' Rib

16249 ✓
2.85
40.9-7.3 Conc Wall

162.2	161.5	161.1	160.9	160.5	158.1	159.8	157.7	158.4	157.8
3.1	3.8	4.2	4.4	4.8	7.2	5.5	5.6	6.9	7.5
40	20	15		12	18	20	25	40	50

163.0	162.5 ✓	161.5	160.5	160.0	159.6	158.3	159.0	158.0	157.8
2.3	2.8	3.8	4.8	5.3	5.7	7.0	6.3	7.3	7.5
40	30	20	16		12	17	20	40	50

16534

4+35 22' Rt of ℄ = ℄ 12" Fac Tree ✓

4+33 = ℄ 27 Conc Walk on Lt

4+09' = ℄ 65' ℄ Ribbon Conc Dr. 2' Ribbon

4+0

3+94 22' Rt of ℄ = ℄ 24" Fac Tree ✓

19' Rt of ℄ = ℄ 10" Fac Tree ✓

3+87 14 Rt of ℄ = ℄ 14" Fac Tree ✓

3+80 = ℄ 3' Conc Walk on Lt

3+59 = ℄ 7' ℄ Ribbon Conc Drive 2' Ribbon on Lt

3+50 23' Lt of ℄ = ℄ Power Pole ✓

16534

Lt.	℄	Rt.
159.46 ✓	158.91 ✓	
5.88	6.43	
40.3: Top Step	39.3 - ℄ 27 Conc Step Top Low	
	159.76 ✓	
	5.58	
	40.2 - ℄ 22 Rib Conc Dr.	

159.8	159.5	159.2	158.1	157.1	156.0	155.3	155.9	154.1	154.0	153.3
55	58	61	72	82	93	100	99	112	112	120
40	30	20	10		12	16	20	30	40	50

160.78 ✓

4.56

40.8: ℄ 23' Conc Wall

161.29 ✓

4.05

41.2 - ℄ 22 Rib Conc Dr.

161.0	160.9	159.8	158.6	157.7	157.3	156.3	156.6	156.9	154.7	154.3
43	49	55	67	76	80	90	87	94	106	110
40	30	20	10		13	17	20	30	40	50

16534

Bert / St.

5+49 24' Lt of ℄ = ℄ Power Pole ✓

6+39.54 = ℄ Morrell

5+22 22' Rt of ℄ = ℄ 24" Euc Tree ✓

4+99.54 ℄ Morrell From South

4+93 23' Rt of ℄ = ℄ 18" Euc Tree ✓

4+90 = ℄ Garage Conc. Floor on Lt ✓

4+85 20' Rt of ℄ = ℄ 6" Euc Tree ✓

4+82 = ℄ 4' Conc Slab on Lt ✓

4+77 21' Rt of ℄ = ℄ 9" Euc Tree ✓

4+63 21' Rt of ℄ = ℄ Do. 24" Euc Tree ✓

4+50 23.6' Lt of ℄ = ℄ Power Pole ✓

TP 2.56 157.86 100.4 155.30

4+45 22' Rt of ℄ = ℄ 18" Euc Tree ✓

4+42 19' Rt of ℄ = ℄ 18" Euc Tree ✓

16534

Lt. ℄ Rt.

152.2 151.7 150.8 149.9 149.6 ✓ 148.7 148.3 147.4 146.7

5.7 6.2 7.1 8.0 8.2 9.2 9.6 10.5 11.2

40 30 20 10 Rich 12 20 40 50

152 154.5 153.5 151.7 151.6 150.8 149.9 150.2 148.9 148.2

3.7 3.4 4.4 6.3 6.3 7.1 8.0 7.7 9.0 9.7

40 30 20 12 14 10 20 40 50

157.58 ✓

0.28

35.4 ± ℄ Garage Conc. Floor

157.61 ✓

0.25

40 ± ℄ 4' Conc Slab

154.5 156.7 156.0 154.9 154.4 153.7 152.7 153.0 151.2 150.3

0.4 1.2 1.9 3.0 3.5 4.2 5.2 4.9 6.7 7.6

40 30 20 12 13 14 20 40 50

157.86

7+00					
6+75					
6+50					
TP	5.80	151.38	12.28	145.58	
6+00					
5+93	= ℄ 85 Conc Drive on ℄				
5+79.54	F.L. Morrell				
		157.86			

℄ ℄ RT

1487	1484	1490	1447	1445	1466	1451	1430	1417	1399	1369
2.7	3.0	2.4	6.7	6.9	4.8	6.3	8.4	9.7	11.5	14.5
40	30	20	16	4		10	20	30	40	55
1472	1465	1465	1455	1450	1460	1452	1430	1397	1389	
4.1	4.8	4.9	5.9	6.4	5.4	6.2	8.4	11.7	13.5	
40	30	20	17	5		10	20	40	50	
1471	1467	1459	1449	1448	1437	1433	1418	1409	1405	
4.3	4.7	5.5	6.5	6.6	7.7	8.1	9.6	10.5	10.9	
40	30	20		5	10	20	30	40	50	
				151.38						
1489	1473	1459	1457	1449	1442	1438				
9.0	10.6	12.0	12.2	13.0	13.7	14.1				
40	20		12	20	40	50				
	1459.21									
	8.65									
	40									
1499	1495	1489	1482	1472	1468	1472	1464	1460		
8.0	8.4	9.0	9.7	10.7	11.1	10.7	11.5	11.9		
40	30	20	15		10	20	40	50		
				157.86						

Beryl St.

BM			13.07	106.14	SW BP Diamond & Lamont 106.03
TP	0.47	119.21	11.52	118.74	
TP	1.08	130.26	11.10	129.18	
TP	1.10	140.25	12.20	139.18	
870					
7+60					
7+30					
		151.38			

	Lt			Rt	
	141.7	141.3	140.8	140.3	138.3
	9.7 50	10.1 40	10.6 20	11.1 10	13.1
	142.7	141.7	141.2	140.7	139.7
	8.7 50	9.7 40	10.2 20	10.7 20	11.7
	146.6	146.8	146.3	143.9	143.4
	4.8 40	4.6 30	5.1 20	7.5 17	8.0 15

138.6	137.1	136.5	135.1	134.3	
12.8 8	14.3 13	14.9 20	16.5 40	17.1 55	
138.6	137.1	136.5	134.9	133.9	
12.3 15	13.8 20	14.9 30	16.5 40	17.5 55	
142.9	139.9	139.9	140.1	136.9	136.3
8.5	11.5 15	11.5 20	11.3 25	14.5 35	15.1 40

Cross Section Emelene St. Beryl St to Walden St.

TP	11.66	189.47	0.15	177.81	
1+30					
1+0					
0+73					
0+50					
0+15					
0+0 = N.L. Beryl St					
BM	11.85	177.96		166.11	Nail Pole 2+93.07 Beryl LH Page

Notes reduced topo trad 7-30-41 GBM

Lt. ℄ ℄ Rt = E

174.4	179.3	177.3	175.4	175.8	176.0	176.5	176.8
0.6	0.7	0.7	2.6	2.2	2.0	1.5	1.2
25	15	7	4		13	15	25
174.6	174.4	174.4	172.9	173.6	173.6	173.4	173.8	174.1
3.4	3.6	3.6	5.1	4.4	4.4	4.6	4.2	3.9
25	15	8	4			13	15	25
							172.61	173.19
							5.89	4.81
							26.1	41.6
							7.86 DF1	9 Gage Corr 66
171.5	171.1	170.5	168.8	169.5	169.2	169.2	170.0	170.5	170.5
6.5	6.9	7.5	9.2	8.5	8.8	8.8	8.0	7.5	7.5
25	15	7	4	3		13	15	20	25
168.8	167.5	166.9	165.5	165.8	166.0		167.8	167.9
9.2	10.5	11.1	12.5	12.2	12.0		10.2	10.1
25	15	10	6		15		22	25
167.6	166.5	164.5	165.0		164.3		164.6	
10.4	11.5	12.5	13.0		13.7		13.4	
25	15	6			15		25	

177.96

		Lt				℄		Rt				40
3+29		187.7 1.8 25	187.7 1.8 15	187.7 1.8 13	186.5 3.0 11	186.9 2.6 9	187.1 2.4	187.0 2.5 5	187.4 2.1 8	187.6 1.9 15	187.5 2.0 25	187.6 ✓ 1.9 27.7 = N'ly Garage Dirt Floor So Entrance
3+0	15 Rt of ℄ = N'ly Wire Fence ✓	187.0 2.5 25	186.2 3.3 15	185.7 3.8 11	185.8 3.7	186.5 3.0 15	186.2 3.3 25	186.0 3.5 35				
2+50	15 Rt of ℄ = S'ly Wire Fence ✓	185.5 4.0 25	185.2 4.3 15	185.0 4.5 12	184.1 5.4 8	184.4 5.1	184.5 5.0 15	184.2 5.3 25	184.0 5.5 35			
2+18		182.18 ✓ 7.32 26.7 = N'ly Conc Apron	182.40 ✓ 7.10 29.2 = N'ly Do Garage Conc Floor									
2+03		184.1 5.4 25	183.9 5.8 15	183.3 6.2 10	180.9 8.6 7	182.1 7.4 5	182.3 7.2	182.4 7.1 10	182.7 6.8 15	182.1 7.4 25	182.11 ✓ 7.39 26.7 = S'ly Conc Apron	182.22 ✓ 7.28 29.2 = S'ly Do Garage Conc.
1+65		182.1 7.4 25	181.7 7.8 15	180.9 8.6 8	178.9 10.6 6	179.4 10.1 4	179.4 10.1	179.7 9.8 15	179.8 9.7 25	179.3 10.2 35		

189.47

189.47

Emelene St

5+16				
570				
4+65				
4+36				
4+21	159 Lt of ℄ = Sly Wire Fence			
4+0.				
3+93	16 Lt of ℄ = Sly Wire Fence			
TP	11.65	201.11	0.01	189.46
3+60				
		189.47		

Lt	℄	Rt
		197.1 ✓
		4.0 25 = Garage Dirt Floor
198.2 2.9 25	197.9 3.2 20	197.1 4.0 15
196.2 4.9	196.1 5.0 3	197.0 4.1 7
197.0 4.1 15	195.9 5.2 25	196.1 5.0 35
196.1 5.0 25	195.6 5.5 18	194.5 6.6 15
194.0 7.1	194.1 7.0 5	194.7 6.4 8
194.7 6.4 15	194.5 6.6 25	194.2 6.9 35
194.4 ✓ 6.7 43 = Garage Dirt Floor	193.7 7.4 25	192.4 8.7 15
192.8 8.3 12	192.5 8.6	192.5 8.6 9
193.1 8.0 11	193.0 8.1 15	193.0 8.1 25
192.8 8.3 35	191.9 9.2 25	191.8 9.3 15
190.7 10.4 15	190.6 10.5	190.4 10.7 8
191.0 10.1 10	191.0 10.1 15	191.2 9.9 25
191.0 10.1 35	201.11	
189.4 0.1 25	189.1 0.4 15	188.3 1.2 15
188.4 1.1	188.1 1.4 5	188.9 0.6 10
189.2 0.3 15	189.1 0.4 25	188.7 0.8 35
	189.47	

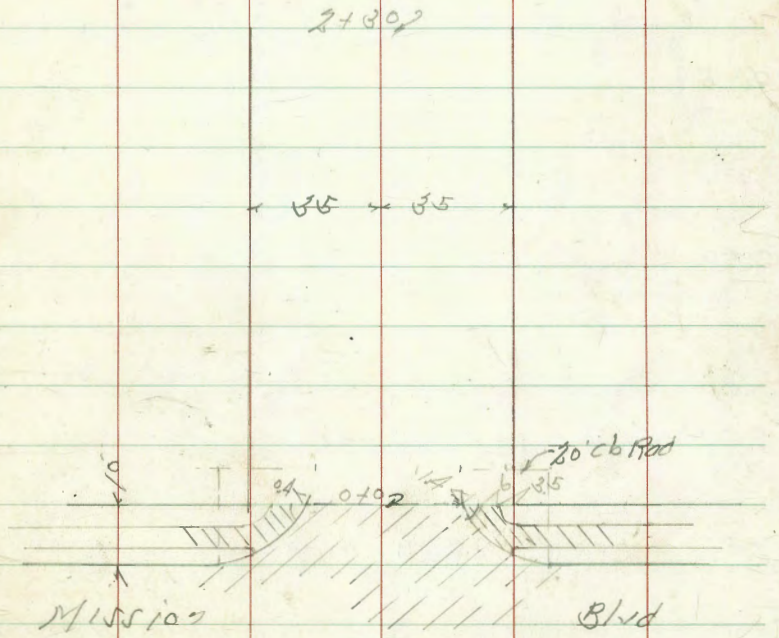
							Lt.		Z		Rt.		12
BM			11.07	186.30	S.T.Lft Hilbert Lamont 186.29.								
TP	051	19737	11.95	196.86									
S+456 = S.L. Malden St.							202.4 6.4 25	201.4 7.4 20	201.1 7.7 13	199.9 8.9	199.6 9.2 5	200.0 8.8 25	
TP	779	20881	0.09	201.02					20881				
		201.11											

Cross Sapphire St.
Mission Blvd to 230 ft West.

Indexed
LM

Aug-26-A1
Sinso
Northern
W Main

43



Cross Section Sapphire St.
West Line Mission Blvd to 230 West.

Red. & Plot. 8-27-1941 Profile 2838 Cook

1+50					
1+0					
0+50					
0+0 = W L Mission Blvd					
0-10 = W C/L Mission Blvd					
PI	3.82	103.53	7.52	99.71	
BM	102	107.23		106.21	NW B.P. Main Turnout x Mission Blvd

Lt: 5 | ℄ | Rt: N

95.3	95.2	94.5	95.0	95.1	95.2	95.1	96.8	97.1
8.2	8.3	9.0	8.5	8.4	8.3	8.4	7.7	7.4
35	25	20	10		10	20	25	35
95.7	95.6	95.2	95.6	95.9	95.9	95.9	96.8	97.1
7.8	7.9	8.3	7.9	7.6	7.6	7.8	6.7	6.4
35	25	20	10		10	20	25	35
96.7	96.3	95.9	96.2	96.6	96.6	96.4	97.6	98.3
6.8	7.2	7.6	7.3	6.9	6.9	7.1	5.9	5.2
35	25	20	10		10	20	25	35
97.3	97.39	96.90	97.19	97.46	97.63	97.64	98.15	98.4
6.2	6.14	6.63	6.34	6.07	5.90	5.89	5.38	5.1
35	25-CL	20	10		10	20 Gutter	25-CL	35
96.86	96.21	96.67	97.15	97.53	97.94	98.57		
6.67	7.32	6.86	6.38	6.00	5.59	4.96		
4-CL EC	40-EC	20		20	40-Gutter	40-CL EC		

103.53

2+30

2+10

1+90

103.53

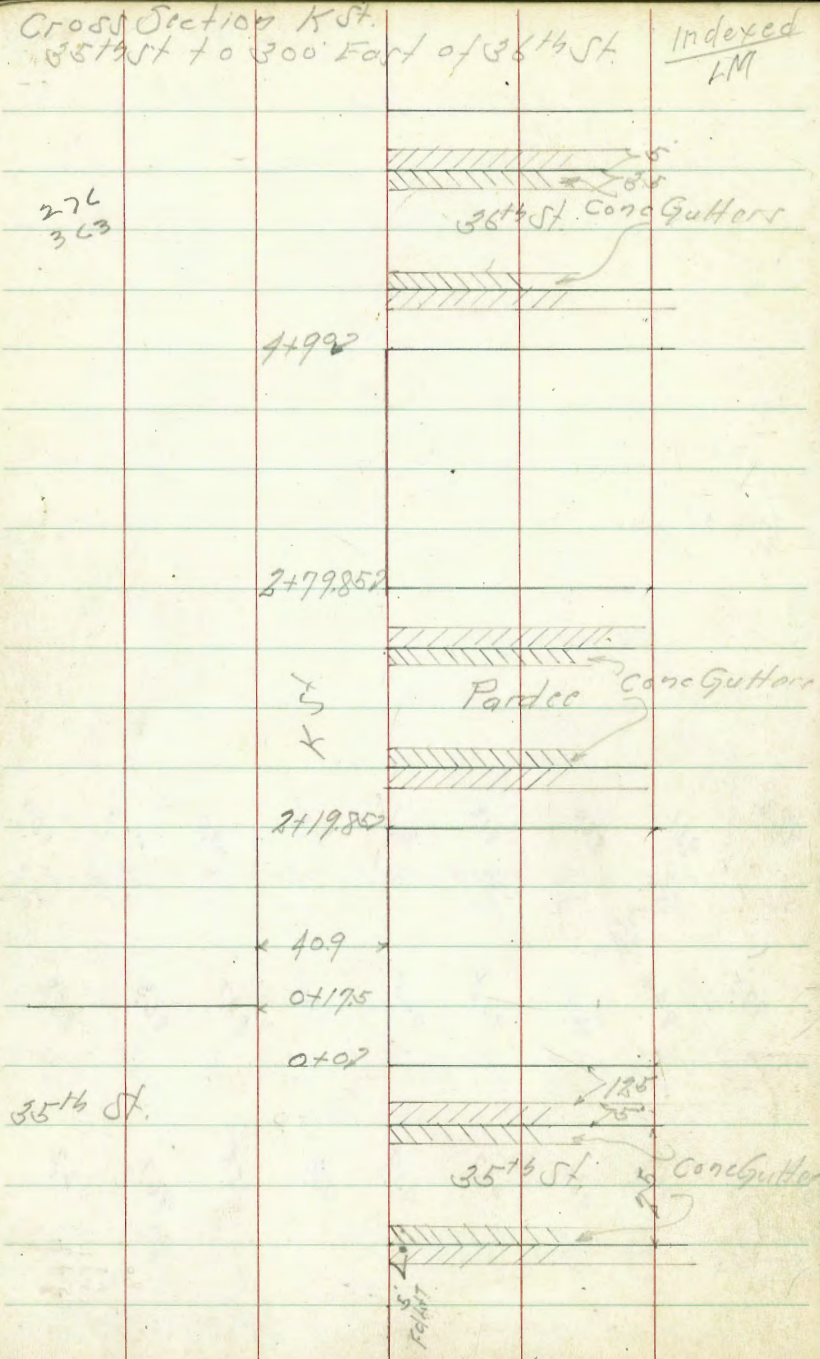
Lt

Rt

92.8	93.1	86.0	81.8	80.1	77.5	77.0	77.3	80.9
10.7	10.4	17.5	21.7	23.4	26.0	26.5	26.3	22.6
50	35	20	10		10	20	25	35
	Top Bank							
93.3	94.4	94.1	94.5	94.5	93.0	88.7	86.3	86.8
10.7	9.1	9.4	9.0	9.0	11.5	14.8	17.7	16.7
50	35	20	10		10	20	25	50
				Top Bank				
94.1	93.1	94.9	94.4	94.7	94.9	95.0	95.8	96.1	97.2
9.4	8.1	8.6	9.1	8.8	8.6	8.5	7.7	7.4	11.3
50	35	25	20	10		10	20	25	50
				103.53				Top Bank	

Cross Section K St. 35th St to 300' East of 36th St. Indexed LM

Sept 8-41 Sisson Northern Pacific



Cross Section K SA
35th St to 200' E of 36th St

0+19 = E.L. 35th St From N

0+14 10.5 Rt of ℄ = Sly Anchor Pole ✓

0+0 = E.L. 35th St. 20.5 Rt of ℄ = Wly Wire Fence ✓

0-17.5 = EOB Line

0-30 = ℄ 35th St.

0-42.5 = WOB Line 35th St

Reduced and Plotted 9-16-41 CSH

TP	7.73	105.49	0.94	97.76	
BM			11.25	87.45	SW Cor. Pardee + KSt.
BM	11.87	98.70		86.83	SW Cor. 35th + 36th

Lt = N		℄		Rt = S	
101.3	100.7	99.9	99.7	98.8	98.4	97.0
4.2	4.8	5.6	5.8	6.7	7.1	8.5
30	20.5	10		10	20.5	35
100.2	99.9	99.2	98.8	98.6	98.0	97.3
5.3	5.6	6.3	6.7	6.9	7.5	8.3
30	20.5	10		10	20.5	30
100.3	99.3	98.5	97.7	96.7	95.89	96.56	94.11	94.89
5.2	6.2	7.0	7.8	8.8	9.67	8.93	11.38	10.60
30	20.5	10		10	20.5-Gut	20.5-Cb	35.5	35.5-Cb
								94
99.5	98.9	98.2	97.7	97.0	96.1	94.6
6.0	6.6	7.3	7.8	8.5	9.4	10.9
30	20.5	10		10	20.5	35
98.9	98.5	97.0	96.7	96.3	95.25	95.95	94.40
6.6	7.0	8.5	8.8	9.2	10.24	9.54	11.09
30	20.5	10		10	20.5-Gutter	20.5-Cb	35.5-Cb

105.49 ✓

1+50	19.1 Rt of Δ = Lot 4 Fence	✓
1+24	18.6 Rt of Δ = W'ly Lot 4 Fence	✓
1+17	= Δ Garage Conc Floor on Rt	✓
1+0	Rt of Δ 18.6 = E'ly Wire Fence	✓
0+75	19' Rt of Δ = Wire Fence	✓
0+50	19.6 Rt of Δ = Wire Fence	✓
	105.49	

	Lt	Δ	Rt
	99.2 6.8 30	98.6 6.9 20.5	97.7 7.8 10	96.9 8.6	96.1 9.4 10	95.7 9.8 20.5	95.2 10.3 30
	100.4 5.1 30	99.6 5.9 20.5	98.7 6.8 10	97.9 7.6	97.8 7.7 10	96.7 8.8 20.5	
				97.75 7.74 ✓ 18.9=W'ly Conc Apron 22' Wide		97.77 7.72 ✓ 21.2=Δ Garage Conc Floor & Wall	
	101.2 4.3 30	100.6 4.9 20.5	99.6 5.9 10	99.1 6.4	98.9 6.6 10	98.3 7.2 20.5	97.7 7.8 30
	102.0 3.5 30	101.7 3.8 20.5	100.6 4.9 10	100.0 5.5	99.2 6.3 10	98.7 6.8 20.5	98.4 7.1 26.5=W'ly House
	101.7 3.8 30	101.6 3.9 20.5	101.2 4.3 10	100.6 4.9	99.5 6.0 10	98.8 6.7 20.5	98.2 7.3 30
			105.49				

KSK

2+37.35 = NCL

2+33 20.5 Rt of ℄ = Ely's Cypress Hedge ✓

2+19.85 = NL Pardee

2+10

TP 4.31 97.98 11.82 92.67

1+81 20' Rt of ℄ = NW Ely's Cypress Hedge : Ely Lath Fence ✓

1+75

1+69

10549

	Lt	℄	Rt
	90.4 / 7.6 / 30	90.1 / 7.9 / 20.5	89.1 / 8.9 / 10	88.6 / 9.4	88.1 / 9.9 / 10	86.87 / 11.11 / 20.5 - Gutter	87.45 / 10.53 / 20.5 - CL	86.67 / 11.31 / 35 Gutter	87.34 / 10.64 / 35 CL
		91.7 / 6.3 / 20.5	90.7 / 7.3 / 10	89.2 / 8.8	88.6 / 9.4 / 10	88.8 / 9.2 / 20.5		
	91.9 / 8.1 / 30	93.4 / 6.6 / 20.5	93.4 / 5.6 / 10	91.3 / 6.7	91.0 / 7.0 / 10	90.6 / 7.4 / 20.5	90.0 / 8.0 / 30	
				97.98				
	97.0 / 8.5 / 30	96.6 / 8.9 / 20.5	95.7 / 9.8 / 10	94.8 / 10.7	94.6 / 10.9 / 15	93.9 / 11.6 / 20.5	93.1 / 12.4 / 26	
					95.72 / 9.72 / 1 Pb = NL 6' Concrete Wall			
				10549				

3+50					
3+10					
TP	10.77	107.72	1.03	96.95	
2+90					
2+79.85 = E.L. Pardee					
2+68.35 = EC6					
2+49.85 = L Pardee					
		97.98			

Δ7		Δ		Δpt.	
103.3	103.2	103.0	102.5	102.0	101.6	101.3
1.4	1.5	1.7	2.2	2.7	6.1	6.4
30	Δ 20.5	10		10	Δ 20.5	30
98.3	97.7	98.1	98.5	98.0	97.1	96.5
9.4	10.0	9.6	9.2	9.7	10.6	11.2
30	Δ 20.5	10		10	Δ 20.5	30
			107.72			
94.7	94.4	94.5	9.55	95.9	94.6	93.7
3.3	3.6	3.5	2.5	2.1	3.4	4.3
30	Δ 20.5	10		10	Δ 20.5	30
93.2	92.7	92.2	91.6	90.9	89.4	89.0
4.8	5.3	5.8	6.4	7.1	8.6	9.0
30	Δ 20.5	10		10	Δ 20.5	30
90.3	90.0	89.5	88.9	88.6	87.17	87.97	87.05	87.85
7.7	8.0	8.5	9.1	9.4	10.81	10.01	10.93	10.13
30	Δ 20.5	10		10	Δ 20.5 -EC6	Δ 20.5 -EC6	35 -EC6	35 -EC6
89.9	89.6	89.0	88.7	88.4	88.2		87.8	
8.1	8.4	9.0	9.3	9.6	9.8		10.2	
30	Δ 20.5	10		10	Δ 20.5		35	
			97.98					

K St.

TP	1.70	100.69	11.88	98.99	
4+90 – W.L. 38th St From South					
4+80					
4+40					
4+10					
TP	4.00	110.87	1.35	106.87	
3+85					
		107.72			

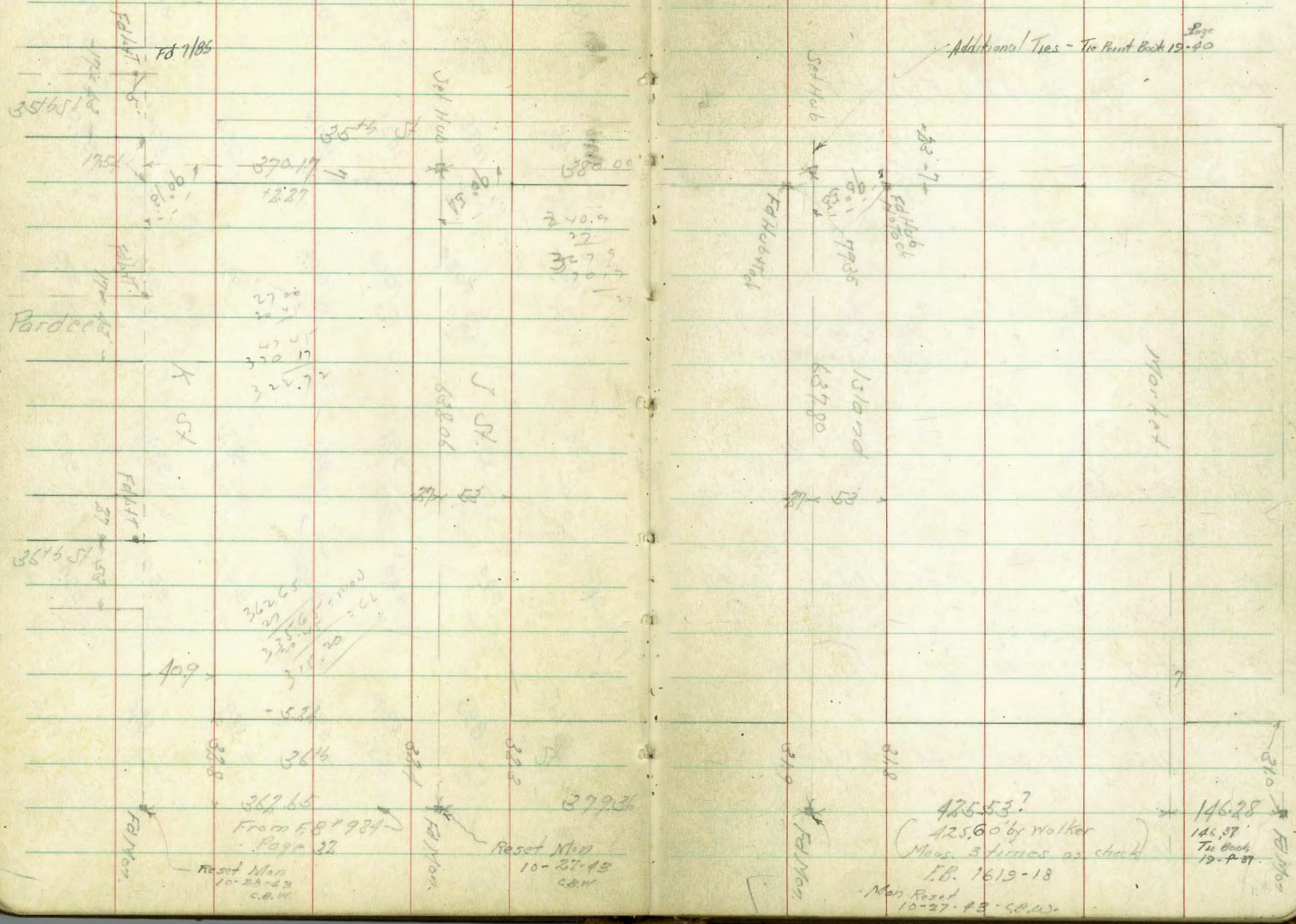
Lt. Ct. Rt.

	1006 9.8 30	101.6 8.8 20.5	102.0 8.4 10	101.3 9.1	102.4 8.0 10	101.9 8.5 20.5	
4+80	102.0 8.4 30	102.0 7.4 20.5	103.5 6.9 10	104.4 6.0	104.6 5.8 10	103.6 6.8 20.5	103.3 7.1 30
4+40	107.4 3.0 30	107.3 3.1 20.5	107.4 3.0 10	106.7 3.7	105.8 4.6 10	105.4 5.0 20.5	105.8 4.6 30
4+10	106.7 3.7 30	106.7 3.7 20.5	106.6 3.8 10	106.5 3.9	105.9 4.5 10	105.3 5.1 20.5	104.8 5.6 30
				110.37			
3+85	105.9 1.8 30	105.8 1.9 20.5	105.7 2.0 10	105.2 2.5	104.7 3.0 10	104.4 3.3 20.5	104.7 3.0 30
				107.72			

						4.		2		RP			
						101.3	100.2	99.0	98.2	97.5	96.5	95.2	
						4.7	5.8	7.0	7.8	8.5	9.5	10.8	
						30	20.5	10		10	20.5	30	
2+0						104.5	103.5	102.1	100.6	99.6	99.0	98.0	
						1.5	2.5	3.9	5.4	6.4	7.0	8.0	
1+50						30	20.5	10		10	20.5	30	
						103.5	102.0	101.3	100.6	99.9	98.8	97.0	
						2.5	4.0	4.7	5.4	6.1	7.2	9.0	
1+0						30	20.5	10		10	20.5	30	
TP	6.97	105.96	1.70	98.99					105.96				
						99.8	99.3	99.1	98.9	98.7	98.4	97.7	
						0.9	1.4	1.6	1.8	2.0	2.3	3.0	
0+65						30	20.5	10		10	20.5	30	
						95.5	94.4	94.0	94.0	94.5	95.0	95.4	
						5.2	6.3	6.7	6.7	6.2	5.7	5.3	
0+30						30	20.5	10		10	20.5	30	
						91.5	89.9	89.4	89.4	88.9	88.5	89.5	
						9.2	10.8	11.3	11.3	11.8	12.2	11.2	
0+0 = E.L. 36.45 ft. From North					SE Mon	30	20.5	10		10	20.5	30	
BM			12.18	88.51	KSH 36.45				100.69				
		100.69											

Reduced & Plotted
9-16-41 GBH

Tie Points 35th St J + Island



From F.B. #984 Page 32

Reset Mon 10-28-43 C.B.W.

Reset Mon 10-27-43 C.B.W.

Additional Ties - Tie Point Book 19 Page 40

425.60' by Walker
(Meas. 3 times as check)
F.B. 1619-18

Mon Reset 10-27-43 C.B.W.

146.37 Tie Book 19-P.37

Cross Section J St
35th St. to 200' East of 36th St.

80' wide
14 cbs
18' Qtr

1+0	39.8	Lt of Z = Fly Wire Fence			
0+75					
0+50	39.5	Lt of Z = Wly Lattice Fence Lt of Z = Fly Wire Fence			
0+0 =	E.L. 35th St.	40' Lt of Z: Wly Wire Fence			
BM			10.64	105.30	Hub E 724 35th St & Line SSH.
TP	5.82	115.94	0.12	110.12	
TP	11.60	110.24	0.44	98.64	
BM	11.62	99.08		87.45	SW Lat 7 KSH + Pardee Page 47

Indexed
C.S.K.

Lt = N			Δ		Rt = S		
113.9 2.0 40	112.7 3.7 26	112.3 2.6 13	112.6 3.6	111.5 4.4 13	111.0 4.9 26	110.5 5.4 40	110.0 5.9 50
113.3 2.6 40	111.7 4.2 26	111.5 4.4 13	112.6 3.3	111.6 4.3 13	110.4 5.5 26	109.7 6.2 40	109.3 6.6 50
112.1 3.8 40	110.5 5.4 26	110.2 5.7 13	109.7 6.2	109.4 6.5 13	108.9 7.0 26	108.6 7.3 40	108.1 7.8 50
110.1 5.8 40	108.8 7.1 26	108.1 7.8 13	107.3 8.6 13	106.5 9.4	106.0 9.9 13	105.4 10.5 26	105.2 10.7 40	104.5 11.4 50

115.94 ✓

Plotted on Profile 497
9-17-41 CSK

		Lt.	℄	Rt.
		115.3	115.6	115.7	111.9	110.9	110.4	110.0	109.8
		0.6	0.3	2.2	4.0	5.0	5.5	5.9	6.1
		40	26	13		13	26	40	50
		115.6	114.5	113.7	112.5	111.8	110.7	110.1	109.1	108.5
		0.3	1.4	2.2	3.4	4.1	5.2	5.8	6.8	7.4
		40	25	26	13		13	26	40	50
		115.7	114.5	113.7	112.4	111.6	111.1	110.8	110.3	110.0
		0.2	1.4	2.2	3.5	4.2	4.8	5.1	5.6	5.9
		40	25	26	13		13	26	40	50
		115.57 ✓	115.44							
		0.27	0.50							
		40	86.7 = Sly 44 Conc Wall							
		40 = Conc Walk								
		114.4	114.8	113.6	113.2	112.7	112.3	111.6	111.4	111.0
		0.5	1.1	2.3	2.7	3.2	3.6	4.3	4.5	4.9
		40	26	22	13		13	26	40	50
		114.9	114.3	113.2	112.7	112.2	111.7	111.1	110.9
		1.0	1.6	2.7	3.2	3.7	4.2	4.8	5.0
		40	26	13		13	26	40	50
				115.94					

3+27	290' Rt of ℄ = Sly Power Pole ✓
3+0	
2+50	40' Lt of ℄ = Ely Wire Fence ✓ Conc Posts ✓
2+0	40' Lt of ℄ = Wly Lath & Ely Wire ✓ Fence ✓ Conc Posts
1+66	= ℄ 44' Conc Walk on Lt ✓
1+50	39.8' Lt of ℄ = Wly Lath Fence ✓
1+21	330' Rt of ℄ = Sly Power Pole ✓
	115.94

JSK

4+75					
4+50					
4+27	39.5 Rt of ℄	= Ely Picket Fence	✓		
4+0					
3+79	30' Rt of ℄	= Sly Power Pole	✓		
3+77	40.2 Rt of ℄	= Wly Picket Fence	✓	Rail Pole	
TP	1.69	112.54	5.09	110.85	3+27 on Rt
3+50					
3+37 =	℄ 15 Conc Walk on Rt		✓		

11594

Lt ℄ Rt

103.8	103.8	103.5	103.7	103.6	104.9	104.9	104.9	104.6	105.1	104.7	104.0
8.7	8.7	9.0	9.8	8.9	7.6	7.6	7.6	7.9	7.4	7.8	8.5
50	40	26	13		9	13	26	33	36	40	50
104.8	104.7	104.6	105.3	105.9	107.0	107.0	106.8	107.0	106.5	106.1	
7.7	7.8	7.9	7.3	6.6	5.5	5.5	5.7	5.5	6.0	6.4	
50	40	26	13		7	13	26	31	40	50	
108.4	108.4	108.7	108.8	109.3	109.8	109.0	108.4	109.1	108.6	107.9	
4.1	4.1	3.8	3.7	3.2	2.7	3.5	4.1	3.4	3.9	4.6	
50	40	26	13		5	13	26	30	40	50	
111.7	111.3	110.8	110.5	110.0	109.7		109.2	109.0			
0.8	1.2	1.7	2.0	2.5	2.8		3.3	3.5			
40	26	13		13	26		40	50			

112.54

113.9	113.0	111.8	111.3	110.6	110.7	110.4	110.2			
2.0	2.9	4.1	4.6	5.3	5.2	5.5	5.7			
40	26	13		13	26	40	50			

110.14
5.80
39.1 = ℄ 15.0 Conc Walk

11594

TP	11.88	118.02	0.13	106.14	
B.M			2.05	104.22	Mon. Ex. 38th 13.2 of SSt.
5+98.7	W.L 36th St				
5+66					
5+40					
5+25					
TP	5.58	106.27	11.85	100.69	
5+0					
		112.54			

	Lt		Ct		Rt	
		103.0		102.3		101.8		101.1		99.9		99.6		98.3		97.5
		3.3		4.0		4.5		5.2		6.4		6.7		8.0		8.8
		40		26		13				13		26		40		50
5+66	102.6		101.6		99.8		99.1		98.4		97.7		96.2		96.0		94.8		93.1
	3.7		4.7		6.5		7.2		7.9		8.6		10.1		10.3		11.5		13.2
	50		40		26		13				13		26		25		40		50
5+40	99.0		98.3		98.3		97.7		97.8		96.2		97.1		96.7		96.7		
	7.3		8.0		8.0		8.6		8.5		8.1		9.7		9.6		9.6		
	50		40		26		13				13		26		40		50		
5+25	100.3		99.8		100.1		99.7		99.2		99.4		98.5		97.4		96.9		
	6.0		6.5		6.7		6.6		7.1		6.9		7.8		8.9		9.4		
	50		40		26		13				13		26		40		50		
								106.27											
5+0	102.4		102.1		101.8		101.2		101.0		102.0		102.0		101.6		102.0		100.9
	10.1		10.4		10.7		11.3		11.5		10.5		10.5		10.9		10.5		11.6
	50		40		26		13				13		26		33		40		50
								112.54											

				∫ St.
2+0				
1+50				
1+0				
TP	6.66	122.40	1.28	116.74
0+50				
0+0 = F.L. 36 ft St.				
		118.02		

Lt		Z		Rt	
112.9	112.3	112.0	111.4	110.0	109.4	109.1
5.1	5.7	6.0	6.6	8.0	8.6	8.9
40	26	13		13	26	40
114.1	113.6	112.9	112.3	111.5	110.7	110.0
3.9	4.4	5.1	5.7	6.5	7.3	8.0
40	26	13		13	26	40
113.9	102.9	112.0	111.3	110.6	109.8	108.7
4.1	5.1	6.0	6.7	7.4	8.2	9.3
40	26	13		13	26	40
114.8	113.0	114.2	113.7	111.5	110.4	109.1
3.2	3.0	3.8	5.2	6.5	7.6	8.9
40	26	13		13	26	40
107.8	106.7	106.0	105.7	104.2	113.5	102.0
10.3	11.2	12.0	12.3	12.8	1.45	16.0
40	26	13		13	26	40
			118.03			

Cross Section Island Ave
35th St to 150 East of 36th St

80' Wide
14' Cbs
13'0

TP	11.68	119.58	0.50	107.90	
1+35					
1+00					
0+70					
0+50					
0+00 = F L 35th St					
TP	0.96	108.40	11.95	107.44	
TP	2.61	119.39	0.41	116.78	
BM	11.89	117.19		105.30	Hub E 74 35th St 12' Lines St Page 54

Plotted 9-17-41 CBH

Sept. 15-41
S. Street
Rls Northerly
Westerly

59

Lt-N		Δ				
113.8	112.9	111.0	108.9	105.3	102.7	102.2	103.4
+5.4	+4.5	+2.6	0.0	-2.1	-5.7	-6.2	-5.0
40	26	13		13	26	26	40
113.9	111.4	106.4	103.6	100.0	98.3	100.3	
+5.5	+3.0	-2.0	-4.8	-8.4	-10.1	-8.1	
40	26	13		13	26	40	
108.8	105.7	102.7	99.9	95.8	95.1	98.9	
+0.4	-2.7	-5.7	-8.5	-12.6	-13.3	-9.5	
40	26	13		13	26	40	
104.6	101.1	98.7	93.7	91.9	93.1	97.8	
-3.8	-7.3	-11.7	-14.7	-16.5	-15.3	-10.6	
40	26	13		13	26	40	
99.4	94.2	89.4	87.6	86.8	90.9	95.9	
-9.0	-14.2	-19.0	-20.8	-21.6	-17.5	-12.5	
40	26	13		13	26	40	

108.40 ✓

3+30					
TP	10.86	127.59	2.85	116.73	
3+0					
2+70					
2+40					
2+0					
1+70					
		119.58			

Lt					Rt	
1242 6.4 40	1196 8.0 26	1186 9.0 13	1178 9.8	1172 10.4 13	1167 10.1 26	1161 10.9 40
			127.59			
1206 +1.0 40	1195 9.1 26	1182 11.4 13	1170 12.6	1161 13.5 13	1156 13.0 26	1153 13.3 40
1204 +0.8 40	1186 1.0 26	1172 2.4 13	1164 3.2	1158 3.8 13	1153 3.3 26	1148 3.8 40
1180 1.6 40	1167 3.9 26	1158 5.8 13	1155 4.1	1150 4.6 13	1143 5.6 26	1136 6.0 40
1164 3.7 40	1150 4.6 26	1137 5.9 13	1130 6.6	1117 7.9 13	1107 8.9 26	1099 9.7 40
1138 5.8 40	1136 7.0 26	1117 8.1 13	1101 9.5	1088 10.8 13	1076 12.0 26	1073 12.3 40
			119.58			

Island Ave

				Lt		℄		Rt		
5+50		127.9 +0.3 40	125.8 1.8 26	123.3 4.3 13	121.4 6.2 10	121.4 6.2	120.5 7.1 13	118.5 9.1 26	117.1 10.5 40	
5+0		126.0 1.6 40	124.2 3.4 26	122.7 4.9 13	120.3 7.3 8	120.0 7.6	119.6 8.0 13	118.1 9.5 26	116.9 10.7 40	
4+51 =	26.5 Rt of ℄ = S'ly Power Pole ✓									
4+50			123.4 4.2 40	121.2 6.4 26	120.0 7.6 13	118.6 9.0	116.4 10.2 13	118.0 9.6 16	117.0 10.6 26	115.6 12.0 40
4+49	36.5' Lt of ℄ = N'ly Tel Pole ✓									
4+0		121.1 6.5 40.6 = W'ly Dirt Garage Floor ✓	121.1 6.5 40	119.8 7.8 26	119.2 8.4 13	117.8 9.8	116.8 10.8 13	115.9 11.7 26	115.2 12.4 40	
3+70		120.7 6.9 40	119.5 8.1 26	118.6 9.0 13	117.6 10.0	116.8 10.8 13	116.0 11.6 26	115.4 12.2 40		
3+45		121.2 6.4 40	119.7 7.9 26	118.5 9.1 13	117.6 10.0	116.6 11.0 13	116.1 11.5 26	115.9 11.7 40		

127.59

127.59

BM			8.58	88.49	Mon SE K + 36th St 88.51
TP	2.02	97.07	10.87	94.05	
BM	0.71	104.92	11.62	104.21	Mon FL 36th St 13' L in S St
TP	0.34	115.83	12.10	115.49	
1+50					
1+0					
0+50					
BM			6.67	120.92	Mon F.L. 36th 13' L in Island
0+0 = F.L. 36th St.					
5+99 = W.L. 36th St.					

127.59

Lt ℄ Rt

119.1 8.5 40	120.0 7.6 26	120.6 7.0 13	120.5 7.1	120.1 7.5 13	119.5 8.1 26	118.9 8.7 40		
122.7 4.9 40	122.8 4.8 26	122.4 5.2 13	121.8 5.8	121.3 6.3 13	120.7 6.9 26	120.1 7.5 40		
124.8 2.8 40	124.8 2.8 30	122.6 5.0 26	122.8 4.8 13	123.1 4.5 6	121.8 5.8	121.0 6.6 13	120.1 7.5 26	119.4 8.2 40
127.8 +0.2 40	125.7 1.9 26	124.9 2.7 20	122.9 4.7 17	122.8 4.8 13	122.6 5.0	121.2 6.4 13	119.8 7.8 26	118.4 9.2 40
128.2 +0.6 40	125.7 1.9 26	123.8 3.8 16	122.3 5.3 13	122.2 5.4	121.0 6.6 13	119.5 8.1 26	118.0 9.6 40	

127.59

CROSS-SECTION OF THOR ST. - MAIN TO DALBERGIA

60 St. - 10' Curbs 10' 1/4"

Indexed
LM

B.M. S E.B.P. Main + Thor.		7.05
6.86	13.91	
0-12 = N. cb. line of Main		
W-10 = P.C. of Ret. 20' Rad. Top. cb.	6.31	7.40
gut.	6.99	6.92
W- on A.C. pave	6.93	6.88
cb " "	6.76	7.15
E " "	6.50	7.41
cb	6.27	7.64
E.	6.22	7.69
E+10 = P.C. of Ret. 20'R. - gut	6.21	8.20
top cb.	5.58	8.33
Halfway around Return		
E - Top cb.	5.74	8.17
gut	6.26	7.65
W - Top cb.	6.38	7.53
gut.	6.94	6.97

9-24-41
Osborne Rand Svelmoe.

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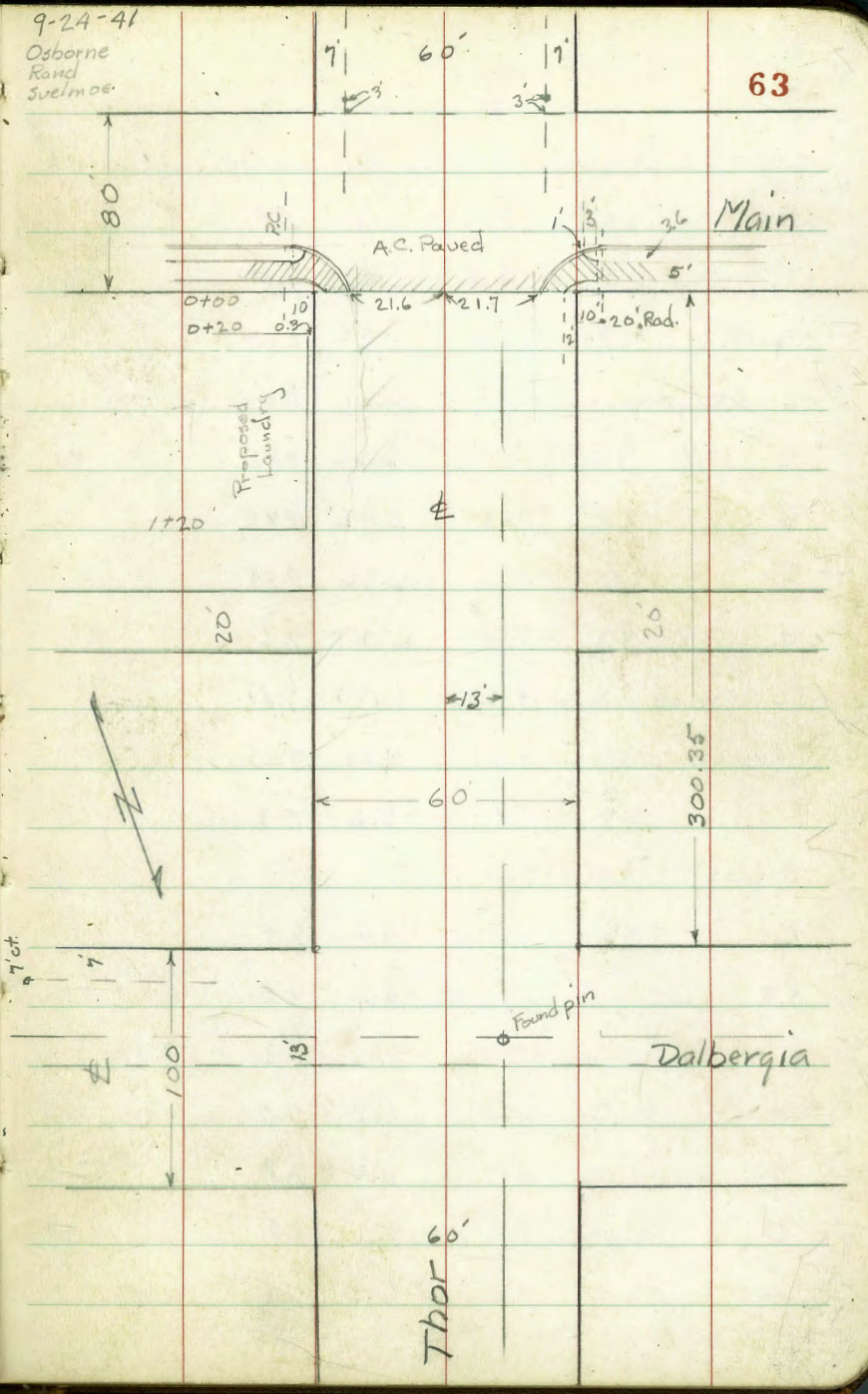


13.91

0+00 = N.L. Main - on Edge of A.C. pave.		
W.	6.1	7.8
+8.3 = End cb. + pave. Top cb.	6.41	7.50
gut	6.93	6.88
cb - on Edge AC pave	6.87	7.04
1/4 " " " "	6.66	7.25
℄	6.46	7.45
1/4	6.36	7.55
cb. " " " "	6.27	7.64
+1.6 = End cb. - gut	6.30	7.61
top cb.	5.88	8.03
E	5.6	8.3
0+05		
E.	4.4	9.5
+8	4.4	9.5
cb	5.6	8.3
+2	6.2	7.7
1/4	6.2	7.7
℄	6.1	7.8
1/4	6.4	7.5

13.91

+8	6.4	7.5
cb	5.8	8.1
+2	4.8	9.1
W	4.8	9.1
0+20		
W	4.3	9.6
cb	4.6	9.3
+3	6.2	7.7
1/4	5.9	8.0
℄	5.7	8.2
1/4	5.8	8.1
+7	6.1	7.8
cb	4.4	9.5
E.	4.1	9.8
E + 0.3 = S.W. Cor. of New Laundry Bld.		
0+47 = ℄ 9A Opening of Bld. on E.		
E - 0.3 on Conc. floor.	2.73	11.18
E	3.4	10.5
cb.	3.9	10.0
+3	5.8	8.1

13.91

1/4	5.5	8.4
℄	5.2	8.2
1/4	5.5	8.4
+6	5.7	8.2
+8	4.6	9.3
cb	4.5	9.4
W	4.6	9.9
0+84 = ℄ Sing. gar. on W.		
W - 33.9 = Gar. on Conc. floor	4.28	9.63
W - 5.1 End of 2 strips 1.7 wide		
S - strip - on Conc	4.42	9.49
N - " " "	4.43	9.48
W	4.7	9.2
cb	5.1	8.8
1/4	5.1	8.8
℄	4.9	9.0
1/4	5.2	8.7
+6	5.4	8.5
cb	3.7	10.2
℄	3.6	10.3

13.91

1+08 = Pepper tree 2' dia. on W. 10.6 in st.

1+20 = N.W. Cor bld. 0.3 back on E

1+38 = P. Pole on W. 1.2 dia ℄ 8.4 in st.

I.P.	5.75	8.16 on 13 pin
(No Reading) → 5.75 13.91		
1+40.18 = S.L. Alley		
E - 0.4 Top of 0.5 Conc. foundation for boiler room	2.52	11.39
E	3.3	10.6
cb	4.4	9.5
+2	4.9	9.0
1/4	5.0	8.9
℄	4.7	9.2
1/4	5.1	8.8
cb	4.8	9.1
W	4.6	9.3
1+50.18 = ℄ Alley		
W	4.5	9.4
cb	4.7	9.2
1/4	5.0	8.9
℄	4.7	9.2

13.91

1/4	5.0	8.9
cb	4.7	9.2
E	4.5	9.4
1+60.18 - N.L. Alley		
E	4.1	9.8
cb	4.2	9.2
+3	5.0	8.9
1/4	5.1	8.8
℄	4.8	9.1
1/4	5.3	8.6
cb	4.5	9.4
W	4.1	9.8
2+00		
W	4.3	9.6
cb	4.6	9.3
+3	5.4	8.5
1/4	5.2	8.7
℄	5.0	8.9
1/4	5.1	8.8
cb	4.9	9.0
E	4.4	9.5

13.91

2+50		
E	4.7	9.2
cb	5.1	8.8
1/4	5.1	8.8
℄	4.9	9.0
1/4	5.1	8.8
cb	4.4	9.5
W	4.2	9.7
2+98 - P. pole on W. 1.2 in dia. E 11.7 in st.		
3+00.35 = S.L. Dalberg la		
W	5.3	8.6
cb	5.3	8.6
1/4	5.1	8.8
℄	4.8	9.1
1/4	4.8	9.1
cb	4.4	9.5
E	3.7	10.2
3+30		
E	4.2	9.7
cb	4.4	9.5

13.91

1/4	4.6	9.3
℄	5.0	8.9
1/4	5.2	8.2
cb	4.5	9.4
ω	5.5	8.4
+10	6.7	7.2
3+50.35 = ℄		
ω-10	4.1	9.8
ω	3.9	10.0
cb	3.6	10.3
1/4	5.5	8.4
℄	5.1	8.8
1/4	4.6	9.3
cb	4.2	9.7
E	3.9	10.0
3+62		
E	4.2	9.7
cb	4.5	9.4
1/4	4.8	9.1
℄	5.2	8.7

13.91

1/4	5.9	8.0
cb	5.5	8.4
ω	6.9	7.0
ω+10	7.4	6.5
4+00.35 = N.L. Dalbergia		
ω-10	7.9	6.0
ω	7.6	6.3
cb	7.0	6.9
1/4	6.9	7.0
℄	6.5	7.4
1/4	6.5	7.4
cb	5.8	8.1
E.	5.6	8.3
check B.M.	6.87	7.04 7.05 ✓

X-SECT. OF ALLEY - BLK. 3 WILSHIRE PLACE

15' Wide
Indexed
LM

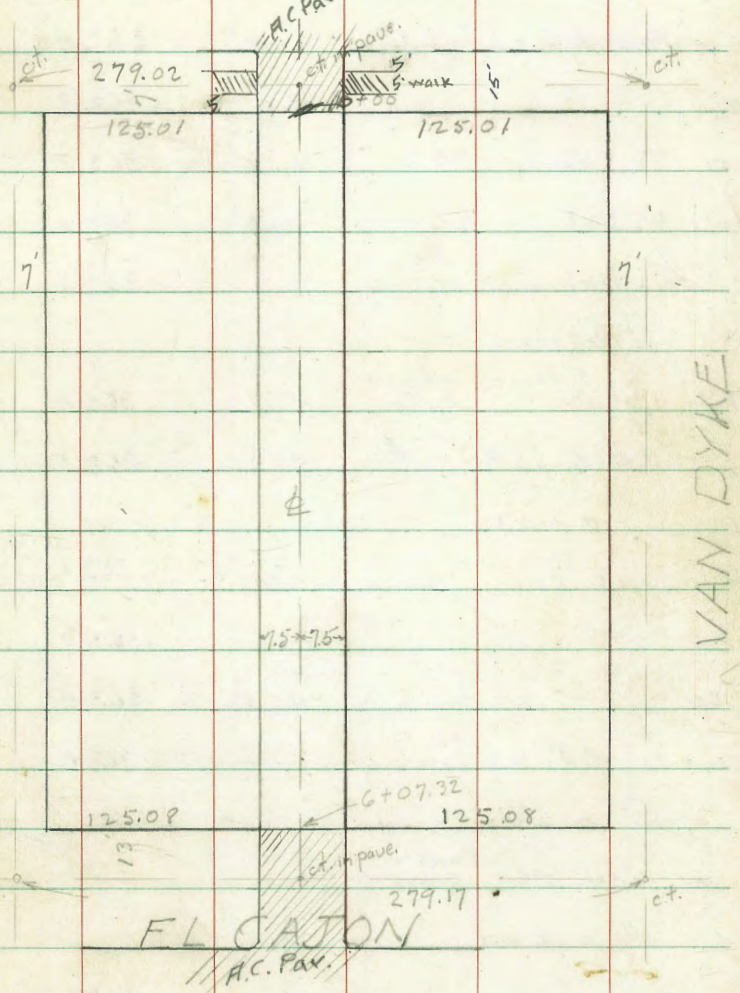
Moore
Rand
Svc Moe
10-1-41.

68

NWBP	4.37	368.91	USC	364.66 364.54	42nd & Meade
NWBP	Copeland & Meade		4.51	364.40	364.36
T.P.	2.97	367.49 367.37	4.51	364.40	
	0-15 S Sutter Meade				
W Pav			5.89	361.60	
C "			6.07	361.47	
E "			6.13	361.36	
	0+00 S L Meade Curve				
E c6			5.31	362.18	
E Pav.			5.44	362.05	
C "			5.54	361.95	
W "			5.33	362.16	
W c6			5.04	362.45	
	0+10				
-2 House foundation			4.3	363.2	
W			4.7	362.8	
C S.M.H.			4.8	362.7	
E			4.6	362.9	

Red-Plat on # 2713
10-2-41 C.B.M.

USC Bolt 1537 - 6.5 ft. yard 44.4



	367.37 367.49			
	0+15			
E-6.1	& Sw. gar. floor cem.	4.45	363.04	N. entrance
E-1.15	NW Cor. above garage	4.45	363.04	
E		4.6	362.9	
C		4.7	362.8	
W		4.5	363.0	
+4	against House foundation	4.2	363.3	
	0+37			
E-1.0	S. Line above gar.	4.5	363.0	
E-1.0	Beg. Bd. dwelling	4.5	363.0	
	0+33			
W-0.15	N end Cem. Cobble wall	4.4	363.1 3' H. gd. 1.0 w.	
C		4.6	362.9	
E		4.5	363.0	
+1	Bd. dwelling,	4.5	363.0	
	0+40			Base of grd. wall
W-0.4	P.C. Cobble wall	4.4	363.1 3' High	
	0+43			
W		4.4	363.1	
W-4	Cem. walk N end apron	4.10	363.39 E.C. Cobble wall	
	0+57			
E-0.9	end Bd. dwelling and beg. of Bd. Shed			

	367.37 367.49			
	0+46			
W-4	Cem apron	4.10	363.39	
W-7	Nt Sw. gar	3.90	363.59 Cem fl.	
	0+55			
W-7	St gar.	3.91	363.58 "	
W-4	St apron	4.15	363.34	
W		4.4	363.1	
C		4.7	362.8	
E		4.8	362.7	
+0.9	Bd. shed	4.8	3627	
	0+58			
W-0.9	N.E. Bd. shed			
	0+76			
	S. end Bd. Shed. & Beg. Bd. Fence on E. side 0.8 Back			
	0+87			
E-0.8	end Bd Fence			
E-0.5	Beg. Bd. Shed.			
W-0.8	S.E. Bd "			
	0+87			
E-0.5	Shed	5.0	362.5	
E		5.0	362.5	

		367.37 369.49		
C		5.1	362.4	
W		5.1	362.9	
+3	& Sew. gar.	4.8	362.7	dirt fl. ✓
	0+91			
W-0.7	beg. Wire Lath fence			←
	0+93			
E-0.6	end Bd. Shed.			
	1+00			
W	P. Pole 1.3 d.	5.7	362.3	✓
C		5.3	362.2	
E		5.3	362.2	
+5		5.8	361.7	
		366.71		
T.P.	4.51	366.59	5.79	362.08
	1+15			
E-4.8	Mk. do garage	4.60	362.11	conc. floor
	1+33			
E-4.8	Sh. do. "	4.67	362.09	" "
E		4.6	362.1	

		366.59 366.71		70
C		4.8	361.9	
W		4.7	362.0	
+0.8	End wire lath fence			
+15		4.7	362.0	
	1+36			
E-4.8	Mk do. gar.	4.64	362.07	Conc. fl.
	1+39			
W-28	& Sew. gar.	4.13	362.58	✓
W-5		5.1	361.6	
W		4.6	362.1	
C		4.6	362.1	
E		4.6	362.1	
+4.8	conc. gar floor	4.64	362.07	✓
	1+54			
E-4.8	Sh do. gar.	4.65	362.06	Conc. fl.
	1+72			
-10		5.1	361.6	
E		4.9	361.8	
C		4.5	362.2	
W		4.6	362.1	

		366.59 366.71		
W + 5		4.9	361.8	
W + 28 & Sin. gar		4.35	362.36 Cem. Fl.	✓
	2 + 00			
— 5		4.7	362.0	
W P. Pole 1.3 dia.		4.7	362.0 on line	✓
C		4.8	361.9	
E		4.8	361.9	
+ 15 Lawn		5.1	361.6	✓
	2 + 25			
— 30		5.6	361.1	
E		4.6	362.1	
C		4.6	362.1	
W		4.1	362.6	
+ 3.7 & Sin. gar.		3.75	362.96 Cem. Fl.	✓
	2 + 57			
— 15		4.2	362.5	
— 3.7 Lath fence				
W		4.1	362.6	
C		4.2	362.5	
+ 6.3 Beg. Bd. fence		4.0	362.7 4' High	✓
E		4.1	362.6 1.2 in alley	
+ 30		4.8	361.9	

		366.59 366.71			71
	2 + 77				
W — 3.6 & Sin. gar.			3.5	363.2 dirt Fl.	✓
	2 + 86				
E + 0.8 End 4' Bd. fence				0.8 in alley	
	2 + 86.1				
E + 0.8 Beg. Bd. Shed					"
	2 + 94				
E + 0.8 end Bd Shed					"
	2 + 94.1				
E + 0.8 Beg. Bd. Shed.					"
	3 + 07				
W — 3.9 & Sin. gar			2.78	364.43 Cem. Fl.	✓
W — 3.8 ground			2.8	363.9	
W			2.9	363.8	
C			3.2	363.5	
+ 6.8 Bd. Shed.			3.0	363.7	
	3 + 07				
E + 0.7 end Bd. Shed.				0.7 in alley	
T.P.	5.20	369.14 369.02	2.72	363.82	

		369.07 / 369.14			
	3+08				
E – 5.9 N.L. da. gar		5.07	364.12	A.C. floor	
	3+20				
W 0.7 P Pole on Line					
	3+25				
E – 5.9 SL da. gar.		4.98	364.16	" "	
E		4.9	364.2		
C		5.0	364.1		
W		4.9	364.2		
	3+39				
E Beg. Bd. fence on Line				4' high	
	3+44				
W – 47.3 E Sw. gar.		4.87	364.27	Cem. fl.	
W – 40		4.9	364.2		
W		4.7	364.4		
C		4.8	364.3		
E 4' Bd. fence 0.1 Back		4.7	364.4		
	3+57				
E end Bd. fence on Line				4' high	
W – 2.8 Beg. Bd fence 4' high					

		369.07 / 369.14			
	4+00				
E – 20			4.4	364.7	
E			4.3	364.8	
C			4.2	364.9	
W			3.9	365.2	
+ 2.8 Bd Shed			4.0	365.1	
	4+08				
W – 2.8 end Bd. fence & Shed.					
E + 0.1 N.L. Bd. gar.					dirt fl. North entrance
E – 5 ℄ door			4.3	364.8	
	4+24				
W – 2.8 ℄ 8" pepper Tree					
	4+25 = also Beg. 6' wire fence 0.2 Back				
E – 0.2 SW Cor Bd garage			3.9	365.2	
C			3.9	365.2	
W			3.8	365.3	
	4+31				
W 1' P. Pole on Line					
T.P.	5.01	370.31 / 370.19	3.84	365.18	

370.19
370.31

	4+40		
W-4	N.L. do. gar.	5.0	365.3 dirt floor
	4+43		
E-0.1	4 in wire fence		
	4+55		
W1-4	SL do. gar.	5.10	3653 " "
W1		4.9	365.4
C		5.1	365.2
E		4.9	365.4
E+1.0	end wire fence		
	4+60		
W-3.8	NL do. gar	4.70	365.61 CCM. Fl.
	4+61		
E-3.3	NL do. gar.	5.0x	365.27 " "
	4+76		
W-3.5	SL do. gar.	4.69	365.62 " "
	4+80		
E-3.4	SL do. gar.	4.97	365.34 " "
	5+0x		
E-3.4	℄ Sim. gar.	4.55	365.76 " "
E-1.4	℄ Ccm. apron	4.6x	365.67
E		4.8	365.5

370.19
370.31

7.33

C		4.9	365.4
W		4.8	365.5
+3.5	S.L. 20' frame dwelling.		
	5+10		
E-6.1	NL 4 car garage	4.61	365.70 CCM. Fl.
E-0.3	" Ccm. apron	4.7x	365.59
	5+29		
E-0.25	℄ apron	4.87	365.44
	5+47		
W-3.7	frame dwelling	5.1	365.2
W1		4.8	365.5
C		4.9	365.4
E		4.9	365.4
+0.x	SL Ccm. apron	4.90	365.41
+6.5	SL 4 car garage	4.59	365.72 CCM. Fl.
	5+53		
E-0.x	℄ 8' Ccm.	4.88	365.43 walk
	5+57		
E+0.x	beg. A.C. Pav.	4.8c	365.45 IN oil STA.

370.19
370.31

	5+58		
W	+0.4 13 d. P. Pole		
	5+60		
W	-1. ℄ N' Conc. Walk	5.74	364.57
W	-0.5 ℄ C" Conc. Ret. Wall	4.74	365.57 Top
	5+62.5		
W	-0.35 N E Cor Tile Bldg.		
	5+80		
E	on H.C. Pav.	5.09	365.22 0.2 in gully
C		5.1	365.2
W		5.0	365.3
	6+00		
W		5.6	364.7
C		5.9	364.4
+7.3	H.C. Pav.	5.47	364.84 0.1 Sta.
	6+06		
W	E N' Conc. Slab.	5.87	364.44 Should be cut off
W	+1.N " "	5.87	364.44
	6+07.3 N	N.L. El Cajon Ave =	
E	C6	70.19 5.58 64.61	364.73

370.19
370.31

74

E	Pav	5.80	364.51
C	"	6.26	364.05
W	"	6.04	364.27
W	C6	5.97	364.34
	13' S of N.L. El Cajon Ave		
W	C6	6.05	364.26
W	Pav	6.25	364.06
C	"	6.51	363.80
E	"	6.08	364.23
E	C6	5.86	364.45
	25' S of N.L. = N. C6. Line El Cajon Ave		
E	Pav	6.03	363.68
C	"	6.04	363.69
W		6.06	363.65
			363.66
SW BP	El Cajon & Van Dyke	6.05	363.54 363.56
			0.02

S.E. Cor Tile Bldg.

Indexed
LM

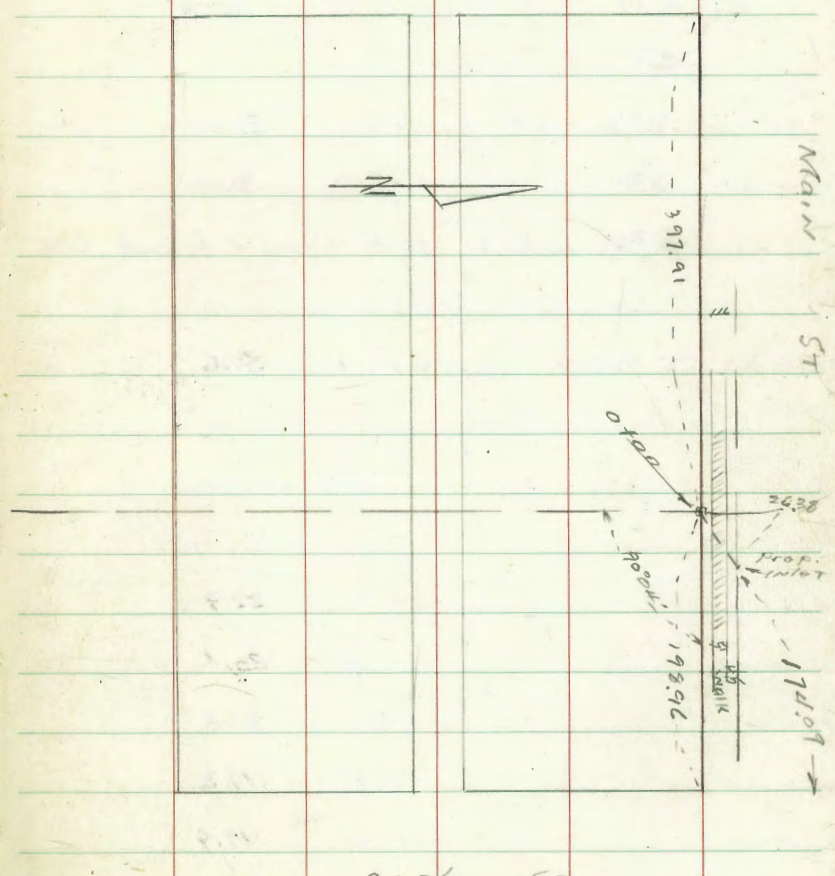
Moore
10-28-41

Proposed cb inlet & drain
on Main St. bet. 29th & 30th.

SWBP	5.43	43.23 ✓	38.00	29th & Main
T.P.	Hub	43.78 ✓	4.17	39.06

Levels on Curb, gut. & T s'walk
on S. side Main
100' W of 30th ST

gut		4.50	38.78
cb		3.91	39.32
wk		3.83	39.45
	150' W		
gut		4.94	38.34
cb		4.44	38.84
wk		4.95	38.33
	174.09 W		
gut		4.96	38.32
cb		4.49	38.79
wk		5.32	37.96



		43.28 ✓		
	198.96	W of 30th		
qvt			4.85	38.93
rb			4.55	38.73
wlk			5.10	38.18
	7th	W		
qvt	in drive		4.71	38.57
wlk			4.10	39.18
	rb + walk O.K. from here W			
	Levels for drain			
0+00	St Main		5.7	37.6
T.P.	0.87	31.10	13.05	30.73
0+46			8.7	22.9
0+73			11.0	20.1
0+57			9.3	21.8
0+83			11.8	19.3
1+25			11.2	19.9
1+50			10.5	20.7
1+75			10.8	20.3

31.10

1793		10.2	19.9
2+15		12.4	18.7
2+26		12.6	18.5
2+37		8.8	22.3
3+37		11.6	19.5
4+10		11.7	19.4
4+20		12.1	19.0
4+70		18.4	12.7

4+10 = approx. M.H.T. of Bay
for new bdg. of dredged
harbor fill

Bliss-Notes
Summerhayes
Beggs - Rod
windy, Paving

Profile Levels Ft Loma Intercepter Sewer

from 16+00 Frontier + Pacific to 91+93 ℄

Frontier + Rosecrans. See Sketch page 7 this book

BM.	7.57	8.10		0.53	Top .36 is Cut on Rod Bench mark. Elev. 25730+- See page 25
T.P.	5.59	8.85	4.79	3.31	
15+98 ±	edge paving	Pacific Hiway	6.99	1.86	
" "	Ground		7.8	1.1	
16+50			7.1	1.8	
16+50+-	Newy 6" cb. Top		5.95	2.90	
17+00			5.6	3.3	
+14 16	Note EC. crosses top of EC. New 6" cb. Top cb.		5.32	3.53	
+17	Gutter A.C. Paving		5.96	2.89	
+50	A.C. Paving		5.70	3.15	
18+00			5.50	3.35	
T.P.	4.67	8.20	5.32	3.53	
+50			4.94	3.76	
19+00			4.39	3.81	
+12. Elec Co Manhole Rpt ℄					
+50			4.36	3.84	
+86 ±	See sketch Page 7 Con. Loading Park.		4.37	3.83	
20+00			4.32	3.88	
+06			4.32	3.88	

Indexed 8-26-52

T. 8.20

77

20+50				3.98	4.22
" "	9.5 Lt	N. Edge Paved st.		4.85	3.35
21+00				4.10	4.10
" "	9.5 Lt			4.85	3.35
+50				4.10	4.10
" "	9.5 Lt			4.86	3.34
+63 ±	End A.C.	Begin oil + Rock		4.30	3.90
" "	9.5 Lt			4.84	3.36
T.P.	4.92	8.27		4.85	3.35
22+00				4.52	3.75
" "	9.5 Lt			4.90	3.37
+50				4.55	3.72
" "	9.5 Lt			4.98	3.29
23+00	End oil + Rock	Begin Dirt		4.53	3.74
" "	9.5 Lt			4.90	3.37
23+00	Dirt			4.6	3.7
+50				5.0	3.3
" "	9.5 Lt			4.95	3.32
" "	5' Rt			6.0	2.3
" "	6 "			8.3	0.0
24+00	Pole Line		30° Set Prop	5.0	3.3
" 9.5 Lt	Paving			4.93	3.34
" 4.5' Rt				5.2	3.1

		8.27			
25+50			5.1	3.2	
" 9.5 Lt			4.93	3.34	
" 2.5 Rt			5.3	3.0	
" 5' Rt			6.6	1.7	
26+00			4.9	3.4	
" "	9.5 Lt Paving		4.83	3.44	
" "	1.5° Rt		4.9	3.4	
" "	5 "		7.0	1.3	
26+50			4.9	3.4	
" "	9.5 Lt Paving		4.67	3.60	
" "	1.5° Rt		4.9	3.4	
" "	5' "		7.3	1.0	
T.P	4.80	8.43	4.65	3.63	
26+00			4.9	3.5	
" "	9.5 Lt Paving		4.71	3.72	
"	1.5° Rt		9.6	-1.2	
27+50			5.0	3.4	
"	2' Rt		5.0	3.4	
"	4 "		6.5	1.9	
27+00			4.8	3.6	
" "	9.5 Lt Paving		4.57	3.86	
"	3' Rt		4.6	3.8	

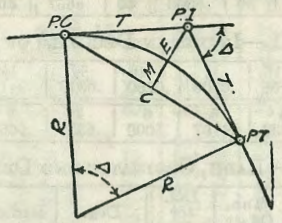
		8.43			78
27+50			4.7	3.7	
" "	3' Rt		5.0	3.4	
28+00			4.5	3.9	/
" "	9.5 Lt Paving		4.53	3.90	
"	4.5 Rt		4.6	3.8	
28+50			4.5	3.9	✓
" "	4' Rt		4.5	3.9	
29+00			4.5	3.9	✓
" "	9.5 Lt		4.55	3.88	
" "	5' Rt		4.5	3.9	
29+50			4.5	3.9	✓
" "	4.0 Rt		4.5	3.9	
30+00			4.6	3.8	
" "	9.5		4.54	3.89	
" "	3.5 Rt		4.6	3.8	
T.P	4.57	8.47	4.53	3.90	
29+50			4.6	3.9	
"	3.5 Rt		4.7	3.8	
31+00			4.6	3.9	
" "	9.5 Lt	Paving	4.59	3.88	
" "	4.5 Rt		4.7	3.8	

		8.47			
31+50			48	3.7	
" "	3.5 Rt		4.9	3.6	
32+00			4.7	3.8	
" "	9.5 Lt		4.57	3.90	
" "	3.5 Rt		4.8	3.7	
+50			4.5	4.0	
" "	2.5 Rt		4.6	3.9	
33+00			4.8	4.1	
" "	9.5 Lt		4.57	3.90	
" "	3.5 Rt		4.5	4.0	
+50			4.5	4.0	
" "	3.° Rt		4.5	4.0	
34+00			4.5	4.0	
9.5 Lt			4.61	3.86	
2.5 Rt			4.5	4.0	
34+20	L.P. 3.5 S of N Line			4.0	
34+50			4.5	4.0	
" "	2.5 Rt		4.5	4.0	
35+00			4.7	3.8	
9.5 Lt			4.60	3.87	
1.5 Rt			4.7	3.8	

		8.47			
TP.	4.83	8.72	4.58	3.89	79
35+50			4.7	4.0	
" "	2.5 Rt		4.7	4.0	
36+00			5.0	3.7	
9.5 Lt			4.83	3.89	
2.5 Rt			5.0	3.72	
+50			5.2	3.8	
37+00			6.1	3.6	
9.5			4.81	3.91	
+40			6.2	3.5	
+50			5.0	3.3	
" " 2' Rt			6.2	3.5	
38+00			4.9	3.8	
9.5 Lt Paving			4.81	3.91	
1.5 Rt			4.9	3.8	
2.° Rt			5.8	3.9	
+50			4.8	3.9	
" 4' Rt			4.8	3.9	
39+00			5.0	3.72	
" 9.5 Lt Paving			4.82	3.90	
" 4' Rt			5.0	3.72	

		T 872			
39+50			4.8	3.9	
4' Rt			4.8	3.9	
40+00			4.8	3.9	
9.5 Lt			4.83	3.89	
6.5 Rt			4.8	3.9	
+50			4.8	3.9	
5-5 Rt			4.6	4.1	
41+00			4.9	3.8	
9.5 Lt	Paving		4.84	3.88	
5' Rt			4.9	3.8	
41+90	1st Rock Oil Paving		4.91	3.81	
41+93 99	L. Lt		5.18	3.54	
TR	3.19	7.02	4.89	3.83	
Check BM			6.43	0.59 ✓	SW. BP Pasecnaus Engraham
				0.56	
				0.03 error	

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES



CURVE FORMULAS

Radius=R=$\frac{50}{\text{sin. } D/2}$ (1) Degree of Curve=D and sin. $\frac{D}{2}=\frac{50}{R}$ (2)

Tangent=T=R tan $\frac{\Delta}{2}$ (3) Length of Curve=L=100$\frac{\Delta}{D}$ (4)

Middle ordinate=M= R(1—cos. $\frac{\Delta}{2}$) (5) =R vers $\frac{\Delta}{2}$ (6)

External=E=T tan $\frac{\Delta}{4}$ (7) =R÷cos. $\frac{\Delta}{2}$—R (8)=R exsec $\frac{\Delta}{2}$ (9)

Long Chord=C=2 R sin. $\frac{\Delta}{2}$ (10) Δ=Central Angle

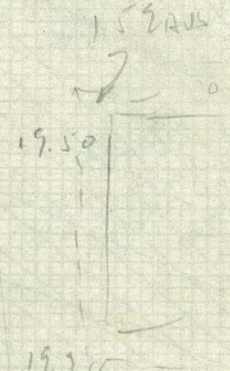
EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. Δ=62° 10′ D=8° 20′. From Table IV for 1° curve T=3454.1 and÷8⅓=414.49 ft. From Table V correction=.36 or T=414.85 ft. P. C.=Sta. P.I.—T=157+45.50. Also from (4) L=746.00 and P. T.=Sta. P. C.+L=164+91.50.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent-offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset=7.27 (54.50÷100)²=2.16 ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus (54.50)²÷(2 x 688.26)=2.16 ft.

Deflections.—Deflection angle=½ D for 100 ft., ¼ D for 50 ft., etc. For c ft.=(in minutes) .3 x C x D° or=defl. for 1 ft. from Table III x C. For Sta. 158 of above curve=.3 x 54.5 x 8⅓=136.2′ or 2° 16.2′, or=2.50 x 54.5=136.2′ from Table III. For Sta. 159 deflection angle=2° 16.2′+8° 20′÷2=6° 26.2′, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve E=960.6 for 8° 20′=960.6÷8⅓=91.27 and from Table V correction=.10 or E=91.37 ft. Or suppose Δ=32° and E is measured and found to be 42 ft. What is D? From Table IV E=230.9 and÷42=5.5 or D=5° 30′.



499.53

T 318.90

55+26.85

44346.47 on Pacific

R. 1500

Δ. 24°-00-22 = P.P.L.P.C.P 25' each way

T 318.9~

L 628.48

on Kurtz

Mason Mon to int Eº 142.48

157.64

157.60

142.48

93.95 E. +-

350:27 Mon - d. Smith.

8.60 . End p. to con ℄.

58.15 across st. from ℄

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)÷2 or 2 ft. added to 41.9 =43 9. For slopes of 1 on 1 see inside of front cover.

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