

1601

DEAR

EVERY

MEMBER

OF

1601

CITY ENGINEER

MICROFILMED

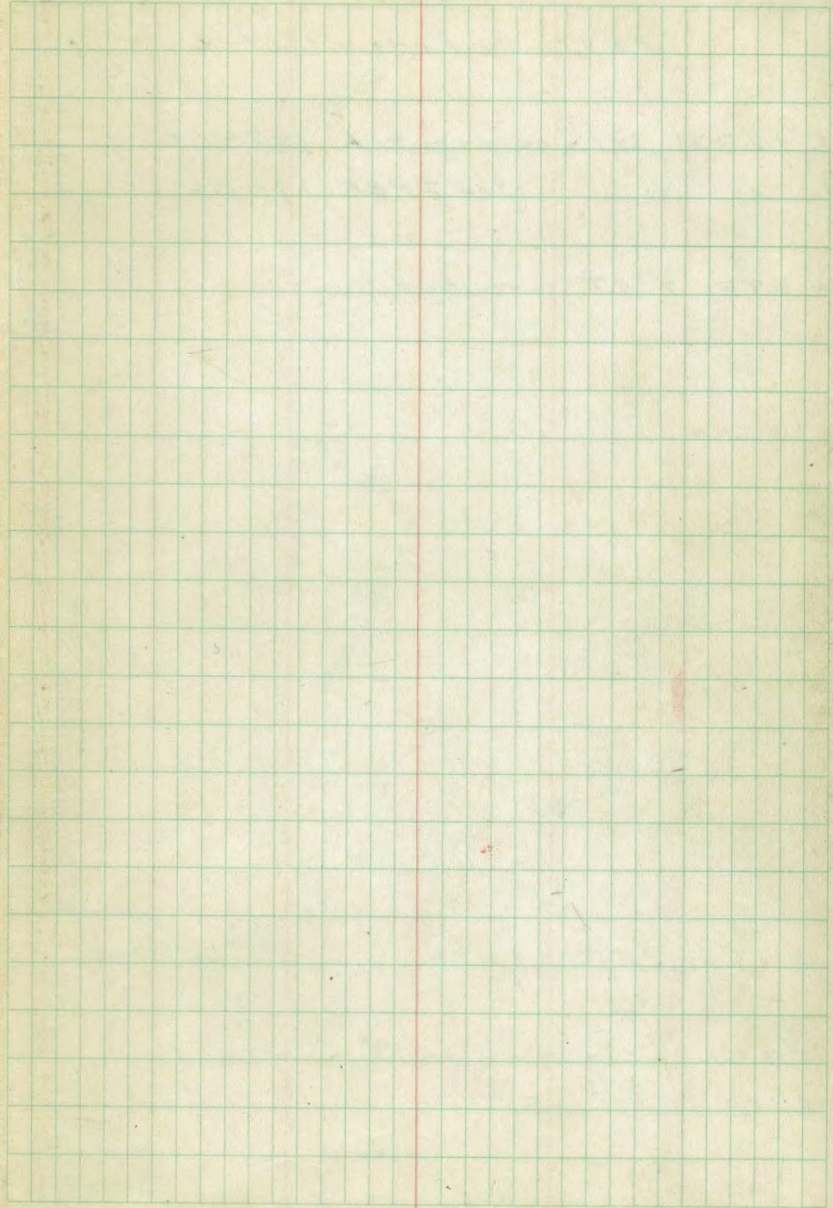
DEC 28 1964

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO,
CALIFORNIA.

Trojan Ave. 50th to Altadena 38-42

38330
 3745 .0146 west
 67-880
 28
 240

East
 3838 01.52
 3746
 6/9.4
 32
 30
 40



Survey of
C ST. EXT.

Moore
Osborne
Sord Meyer 4-17-41.

35TH to Federal Blvd.

5+57.31 SET 2x2 INT Wk 36TH ST

See T.P.BK. 19-99

Fd 2x2

4+75 P.O.T. 2x2 Hub

3+57.20

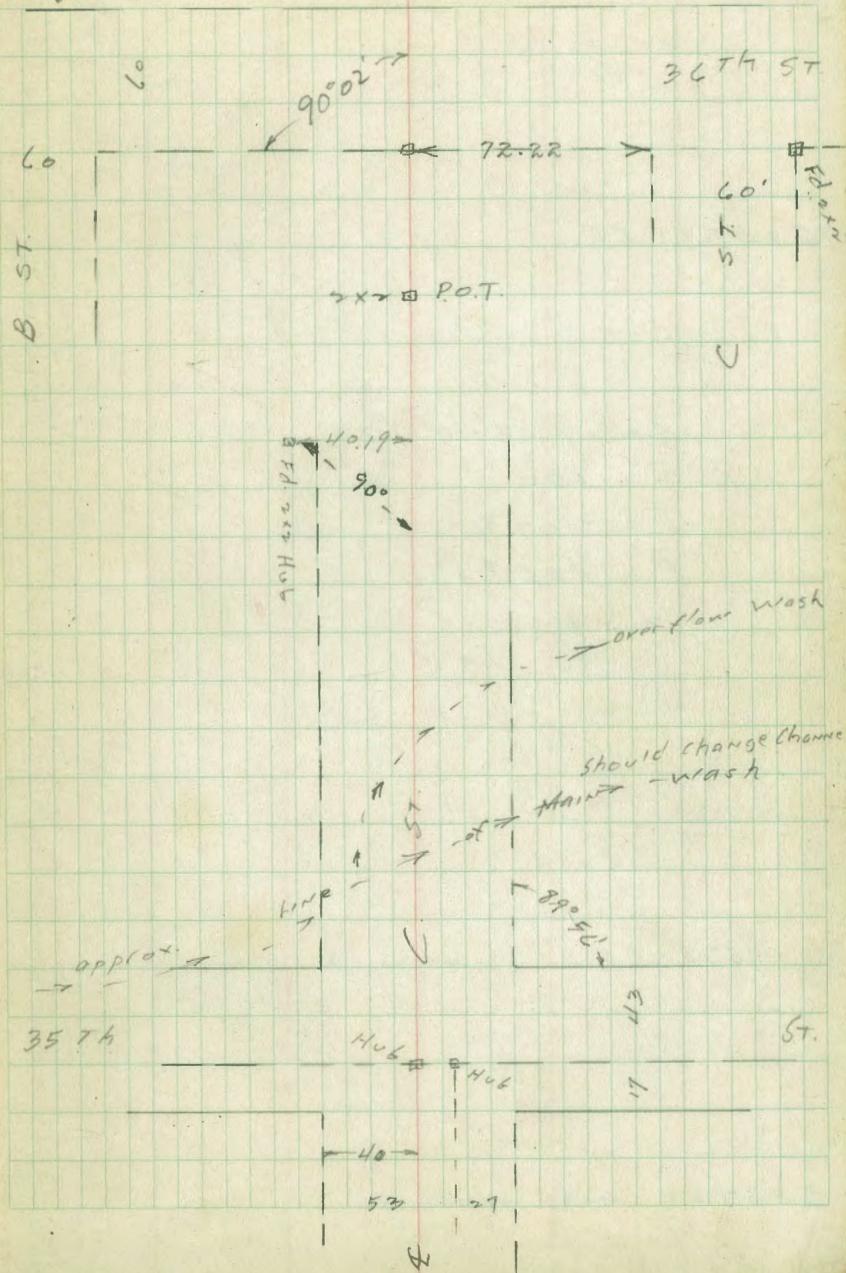
0+60 EL 35TH

0+17 Set 2x2 on R C ST.

0+00 WL 35TH

Indexed
LM

2

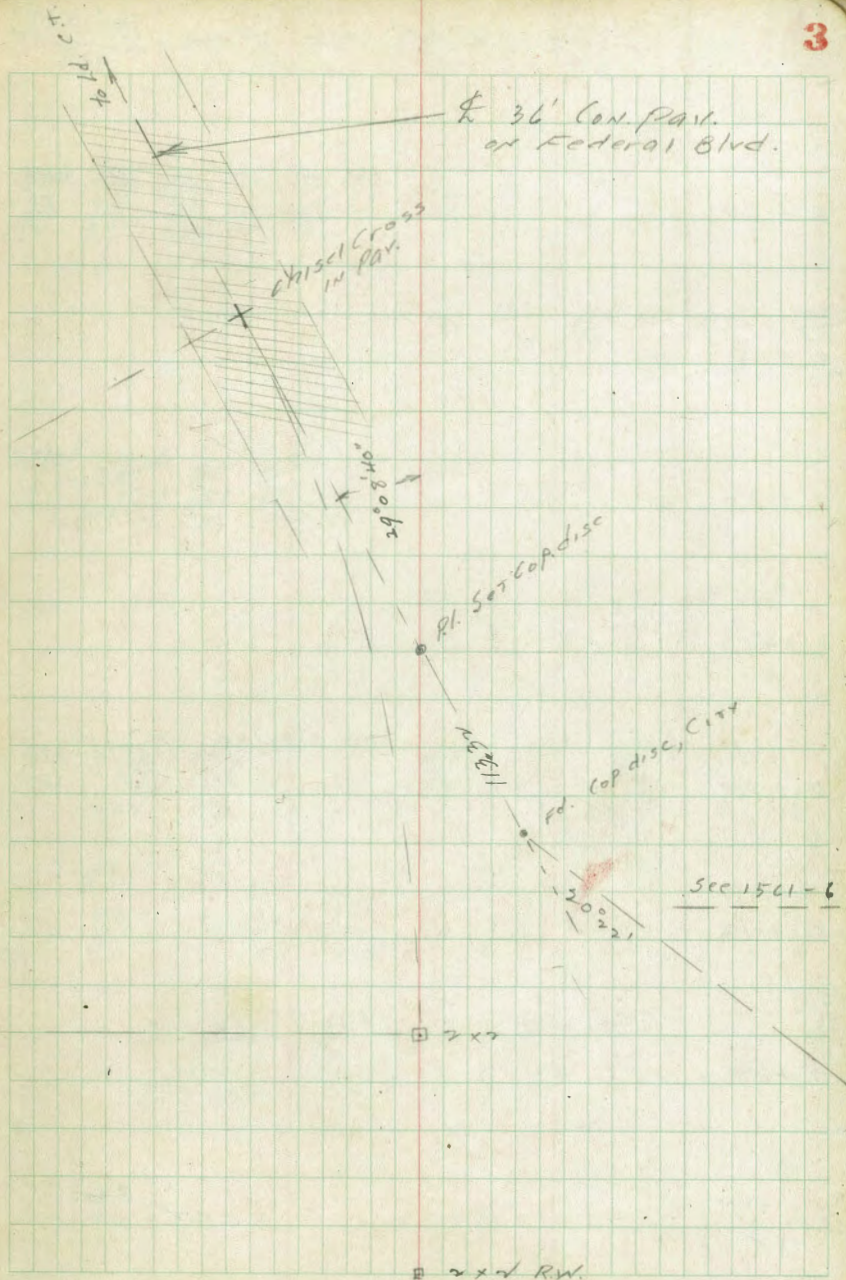


15+03.31 E.C.

$A = 29^{\circ}08'40''$ LT
 $R = 800$
 $T = 207.97$
 $L = 406.93$
2.1486

10+96.38 B.C. LT Set 2x2 RW 506

5+57.31 W.L. 36th ST.



Xsec of C ST EXT.
3574 To Fed. Blvd.

Indexed
LM

LT

£

RT

4

0 + 80

<u>572</u>	<u>572</u>	<u>602</u>
9.0	11.0	7.5
175	146	137

<u>578</u>	<u>572</u>	<u>580</u>	<u>571</u>	<u>568</u>	<u>585</u>	<u>581</u>
8.7	9.0	10.7	11.1	11.4	9.7	10.1
100	78	63	40	16	6	

0 + 63

<u>573</u>	<u>572</u>	<u>585</u>	<u>570</u>	<u>580</u>	<u>585</u>
10.9	9.0	9.7	11.7	10.7	9.4
	7	40	78	100	150

0 + 50

<u>610</u>	<u>607</u>
7.7	7.5
150	130

<u>578</u>	<u>572</u>	<u>582</u>	<u>585</u>	<u>578</u>	<u>607</u>
10.4	10.5	10.0	9.4	10.3	7.5
105	94	83	110	93	

0 + 45

<u>600</u>	<u>586</u>	<u>584</u>	<u>582</u>	<u>602</u>	<u>601</u>
8.7	9.6	9.8	10.0	8.0	8.1
	40	56	74	87	100

0 + 30

£ 3574

<u>612</u>	<u>587</u>	<u>581</u>
7.0	10.1	10.1
167	154	140

<u>585</u>	<u>588</u>	<u>593</u>	<u>581</u>	<u>622</u>	<u>645</u>	<u>600</u>	<u>595</u>
9.7	9.4	9.9	9.1	6.0	7.7	8.4	8.7
100	65	40	35	32		40	65

0 + 17

<u>589</u>	<u>593</u>	<u>602</u>	<u>614</u>	<u>612</u>
9.3	8.8	7.0	6.4	7.0
70	55	53	110	

0 + 00 = W.L. 3574 57

<u>621</u>	<u>621</u>	<u>609</u>	<u>601</u>	<u>603</u>
6.1	6.1	7.3	8.1	2.9
65	110		40	65

Con
N.M. Head 11.56 6818
B.M.

Edw.
56.67 3574

68.18

+10

+100

+75

+50

+20

+100

0+87

0+84

68.18

LT

E

RT

5

<u>63.2</u>	<u>63.2</u>	<u>62.3</u>	<u>570</u>
5.0	8.0	5.9	10.2
60	40	4	

<u>132</u>	<u>61.8</u>	<u>61.0</u>	<u>60.2</u>	<u>582</u>	<u>582</u>	<u>560</u>	<u>571</u>	<u>574</u>	<u>573</u>
5.0	6.3	7.2	7.5	10.0	10.0	12.2	11.1	10.8	10.9
75	60	40	15	12	10.0	35	40	68	90

<u>62.2</u>	<u>61.2</u>	<u>61.0</u>	<u>591</u>	<u>575</u>	<u>575</u>	<u>568</u>	<u>57.2</u>	<u>526</u>	<u>57.3</u>	<u>57.1</u>
5.0	7.0	7.2	9.1	10.7	10.7	11.4	10.5	10.6	10.9	11.1
85	75	50	40	15	10.7	8	13	20	70	100

<u>620</u>	<u>61.8</u>	<u>61.0</u>	<u>598</u>	<u>57.3</u>	<u>583</u>	<u>581</u>	<u>58.0</u>	<u>55.5</u>	<u>56.0</u>	<u>54.6</u>
6.2	6.4	6.9	9.2	9.9	9.9	10.1	10.2	12.7	12.2	13.0
90	75	55	50	40	9.9	40	75	100	105	150

<u>621</u>	<u>61.8</u>	<u>526</u>	<u>582</u>	<u>52.3</u>	<u>56.8</u>	<u>565</u>	<u>54.6</u>	<u>54.5</u>
6.1	6.2	10.6	10.0	10.9	11.3	11.8	13.0	13.7
100	72	57	20	10.9	40	100	130	150

<u>582</u>	<u>61.8</u>	<u>521</u>	<u>56.3</u>	<u>56.2</u>	<u>56.0</u>	<u>55.2</u>	<u>52.1</u>	<u>56.9</u>
10.0	6.3	11.1	11.7	11.5	12.2	13.0	11.1	11.3
150	117	85	40	11.5	40	100	130	150

<u>582</u>	<u>57.8</u>	<u>523</u>	<u>56.4</u>	<u>56.8</u>	<u>56.5</u>
9.0	10.3	10.9	11.6	11.3	11.7
150	135	100	60	40	117

<u>56.1</u>	<u>56.8</u>	<u>57.1</u>	<u>59.2</u>
12.1	12.2	10.1	9.2
40	40	60	100

68.18

3 + 25

+ 95

4 + 75

T.P. 12.47 91.96 0.53 79.49

+ 55

1 + 40

T.P. 12.25 80.00 0.41 67.77

+ 34

2 + 25

68.18

LT

R

RT

6

$\frac{88.2}{3.8}$	$\frac{828}{4.2}$	$\frac{873}{4.7}$	$\frac{865}{5.2}$	$\frac{864}{5.6}$
40	20		20	40

$\frac{835}{8.2}$	$\frac{846}{7.2}$	$\frac{865}{6.5}$	$\frac{853}{6.7}$	$\frac{85.1}{6.9}$
40	20		20	40

$\frac{78.6}{13.4}$	$\frac{79.2}{12.8}$	$\frac{80.8}{11.2}$	$\frac{81.4}{10.6}$	$\frac{82.2}{9.8}$
50	40	20		40

91.96

$\frac{72.6}{7.4}$	$\frac{723}{7.8}$	$\frac{725}{7.5}$	$\frac{729}{7.0}$	$\frac{745}{5.5}$	$\frac{745}{5.5}$
50	40	20		40	50

$\frac{71.8}{8.5}$	$\frac{723}{7.7}$	$\frac{663}{18.7}$
	40	65

TOP BANK

80.02

$\frac{70.9}{2.7}$	$\frac{71.8}{3.6}$	$\frac{592}{9.0}$	$\frac{56.31}{11.9}$
	16	40	65

TOP BANK

$\frac{679}{0.3}$	$\frac{679}{0.3}$	$\frac{695}{1.3}$	$\frac{699}{1.7}$	$\frac{61.5}{4.7}$	$\frac{584}{9.8}$	$\frac{566}{11.6}$	$\frac{55.6}{12.6}$
60	40	1	5	7	20	40	90

Note plus rods 68.18

T.P. 1.22 67.29 13.03 66.07

5+10

T.P. 0.44 79.10 12.73 78.66

+85

+75 P.O.T. on RW Hub

+70

T.P. 3.07 91.39 3.44 88.32

+50

H

3+57.2

91.96

LT

K

RT

7

$\frac{24.1}{5.0}$	$\frac{71.3}{7.8}$	$\frac{64.3}{9.8}$	$\frac{68.3}{10.8}$	$\frac{68.1}{11.1}$
40	20		20	40

		79.10		
$\frac{72.2}{5.1}$	$\frac{84.2}{6.7}$	$\frac{82.4}{9.0}$	$\frac{81.2}{10.2}$	$\frac{80.7}{10.7}$
40	20		20	40

$\frac{85.1}{4.3}$	$\frac{85.0}{3.4}$	$\frac{87.18}{4.21}$		
40	20			

$\frac{87.8}{3.6}$	$\frac{87.4}{3.9}$	$\frac{87.4}{4.0}$
	20	40

		91.39		
$\frac{90.0}{2.0}$	$\frac{89.1}{2.9}$	$\frac{88.1}{3.9}$	$\frac{88.0}{4.0}$	$\frac{88.0}{4.2}$
40			20	40

$\frac{89.3}{2.7}$	$\frac{88.5}{3.2}$	$\frac{88.3}{3.7}$	$\frac{87.9}{4.1}$	$\frac{87.5}{4.5}$
40	20	20	20	40

$\frac{89}{3.06}$	$\frac{88.4}{3.6}$	$\frac{88.0}{4.0}$	$\frac{87.2}{4.8}$	$\frac{86.9}{5.1}$
140.19	20	40	20	40

Old Hub

91.96

7+00

+50

6+17.31 FL 36 TH

+97.31 F 30 TH

5+57.31 WH 36 TH

+45

+30

5+24

67.29

Lr			Rr			Rr			8
$\frac{57.4}{8.9}$	$\frac{57.7}{9.6}$	$\frac{57.6}{9.7}$	$\frac{62.4}{11.9}$	$\frac{62.8}{12.5}$	$\frac{58.8}{8.5}$	$\frac{56.8}{10.5}$	$\frac{50.3}{17.0}$	$\frac{47.7}{17.1}$	
60	40	20		20	35	40	55	20	
$\frac{56.8}{10.5}$	$\frac{56.2}{11.1}$	$\frac{57.5}{9.8}$	$\frac{57.2}{10.1}$	$\frac{58.3}{9.0}$	$\frac{57.1}{10.4}$	$\frac{50.3}{17.0}$	$\frac{47.9}{17.4}$		
60	40	20		20	40	60	85		
$\frac{57.6}{9.7}$	$\frac{57.3}{10.0}$	$\frac{55.9}{11.4}$	$\frac{58.5}{11.8}$	$\frac{55.5}{11.5}$	$\frac{56.6}{10.7}$	$\frac{46.3}{16.0}$	$\frac{47.8}{17.5}$		
60	40	20		20	40	60	80		
$\frac{57.2}{10.1}$	$\frac{57.1}{10.0}$	$\frac{57.2}{10.1}$	$\frac{57.3}{10.0}$	$\frac{56.3}{11.0}$	$\frac{52.8}{9.5}$	$\frac{57.4}{9.9}$			
60	40	20		20	40	60			
$\frac{58.0}{9.3}$	$\frac{57.1}{10.2}$	$\frac{56.5}{10.8}$	$\frac{56.12}{11.17}$	$\frac{56.1}{10.8}$	$\frac{56.7}{10.6}$	$\frac{59.7}{7.6}$	$\frac{60.8}{7.5}$		
60	40	20	406	20	34	40	50		
$\frac{58.2}{8.6}$	$\frac{57.4}{9.9}$	$\frac{56.1}{11.2}$	$\frac{56.6}{10.7}$	$\frac{56.4}{10.9}$	$\frac{56.4}{10.9}$	$\frac{56.7}{8.6}$	$\frac{60.7}{6.6}$		
60	40	20		20	36	40	50		
$\frac{65.8}{1.5}$	$\frac{63.8}{3.5}$	$\frac{60.2}{7.1}$	$\frac{58.0}{9.3}$	$\frac{57.0}{10.3}$	$\frac{56.9}{10.4}$	$\frac{59.0}{8.0}$	$\frac{56.8}{10.5}$	$\frac{52.1}{10.2}$	
50	40	20		20	40	50	70	85	
				$\frac{60.7}{6.6}$	$\frac{58.2}{9.0}$	$\frac{57.0}{10.3}$	$\frac{57.2}{9.1}$		
				20	20	40	60		

67.29

+78

+71

8 + 75

+90

+68

+50

+38

7 + 30

67.29

L7

K

PT

9

$\frac{53.9}{13.4}$	$\frac{58.1}{9.7}$	$\frac{58.1}{9.7}$	$\frac{56.0}{11.3}$	$\frac{533}{14.0}$	$\frac{533}{14.0}$	$\frac{54.2}{13.1}$	$\frac{54.7}{12.6}$
65	50	40	20		20	40	60

$\frac{539}{13.4}$	$\frac{569}{10.4}$	$\frac{538}{13.5}$	$\frac{541}{13.2}$	$\frac{527}{14.6}$
65	55	40	20	

$\frac{55.1}{12.2}$	$\frac{55.4}{11.9}$	$\frac{55.1}{12.2}$	$\frac{54.8}{12.5}$	$\frac{54.7}{12.6}$	$\frac{54.6}{12.7}$	$\frac{54.2}{13.1}$
60	40	20		20	40	60

$\frac{54.9}{12.4}$	$\frac{55.1}{12.2}$	$\frac{55.1}{12.2}$	$\frac{54.9}{12.4}$	$\frac{54.9}{12.4}$	$\frac{54.6}{13.2}$	$\frac{54.4}{12.9}$
60	40	20	12.4	20	40	60

$\frac{54.3}{13.0}$	$\frac{54.3}{13.0}$	$\frac{54.2}{13.1}$	$\frac{54.0}{13.3}$	$\frac{54.0}{13.2}$	$\frac{54.6}{12.7}$	$\frac{56.4}{8.9}$
60	40	20		20	40	60

$\frac{60.3}{1.0}$	$\frac{61.3}{6.0}$	$\frac{66.0}{6.3}$	$\frac{61.8}{5.5}$	$\frac{61.1}{6.2}$	$\frac{60.9}{6.1}$	$\frac{61.1}{6.2}$
60	40	20	5.5	20	40	60

$\frac{58.5}{8.8}$	$\frac{57.8}{9.5}$	$\frac{58.7}{8.6}$	$\frac{58.5}{8.5}$	$\frac{58.5}{7.5}$	$\frac{62.1}{5.2}$	$\frac{61.9}{6.4}$
60	40	20	8.5	20	40	60

$\frac{57.7}{8.6}$	$\frac{57.5}{8.5}$	$\frac{57.3}{10.0}$	$\frac{50.8}{16.5}$	$\frac{52.1}{15.2}$
	20	40	60	75

67.19

TP. 9.71 67.14 9.86 57.43

10 + 9638 BC LT.

+50

10 + 00

+50

+13

9

9 + 92

67.29

LT

R

R

10

$\frac{566}{9.7}$	$\frac{56.9}{9.4}$	$\frac{56.8}{9.5}$	$\frac{57.3}{10.0}$	$\frac{57.1}{10.2}$	$\frac{56.2}{10.6}$	$\frac{55.2}{12.1}$
65	40	20	10.0	20	40	65

$\frac{56.1}{11.2}$	$\frac{57.3}{10.0}$	$\frac{57.3}{10.0}$	$\frac{57.4}{9.9}$	$\frac{57.3}{10.0}$	$\frac{57.1}{10.2}$	$\frac{56.6}{10.7}$
65	40	20	9.9	20	40	65

$\frac{57.2}{9.6}$	$\frac{57.2}{9.6}$	$\frac{55.7}{11.6}$	$\frac{55.1}{12.2}$	$\frac{56.1}{11.1}$	$\frac{55.9}{11.4}$	$\frac{56.2}{11.1}$
65	40	20	12.2	20	40	65

$\frac{58.5}{8.8}$	$\frac{58.6}{9.3}$	$\frac{58.1}{9.4}$	$\frac{57.1}{10.2}$	$\frac{57.3}{10.0}$	$\frac{54.2}{12.6}$	$\frac{54.7}{10.6}$	$\frac{54.2}{12.1}$
60	40	20	10.2	20	30	40	60

$\frac{55.1}{12.2}$	$\frac{55.2}{12.1}$	$\frac{55.2}{12.1}$	$\frac{58.2}{12.1}$	$\frac{54.3}{13.0}$	$\frac{54.9}{12.4}$	$\frac{54.8}{12.5}$
60	40	20	12.1	20	40	60

$\frac{566}{10.7}$	$\frac{58.3}{9.0}$	$\frac{57.5}{8.8}$	$\frac{54.5}{12.5}$
	20	40	60

$\frac{54.7}{12.6}$	$\frac{54.6}{13.3}$	$\frac{58.1}{9.2}$	$\frac{58.6}{9.2}$	$\frac{58.1}{9.4}$	$\frac{57.3}{9.1}$	$\frac{56.2}{10.6}$	$\frac{55.1}{12.2}$
60	50	40	20	9.4	20	40	60

67.29

+50

<u>578</u>	<u>589</u>
81	77
65	53

13:

<u>602</u>	<u>599</u>	<u>643</u>	<u>6212</u>	<u>6215</u>	<u>6335</u>	<u>6293</u>
74	77	38	150	441	427	449
40	30	13	3.5	ML Pav	14.6	33.4
					EPav	SL Pav

<u>571</u>	<u>581</u>	<u>574</u>	<u>586</u>	<u>638</u>	<u>6283</u>	<u>6289</u>
10.5	9.5	10.2	8.6	3.8	4.79	4.73
65	60	40	15		7.7	7.6
					ML Pav	EPav

+75

<u>571</u>	<u>580</u>	<u>576</u>	<u>571</u>	<u>541</u>	<u>626</u>	<u>636</u>	<u>6266</u>	<u>6262</u>
10.5	9.6	10.0	10.5	8.5	5.0	4.0	4.96	4.95
65	56	40	30	10		10	72.6	37.4
							ML Pav	EPav

12 +50

10.4
65

<u>563</u>	<u>583</u>	<u>565</u>	<u>580</u>	<u>604</u>	<u>604</u>	<u>636</u>	<u>6251</u>	<u>6250</u>
11.3	9.3	11.1	9.6	7.2	7.7	4.0	5.11	5.11
40	30	12	2	1		20	24	43.5
							ML Pav	EPav

TP

4.73 67.62 4.45 62.89 P.I. Cop. disc

67.62

14 +30

<u>571</u>	<u>562</u>	<u>564</u>	<u>569</u>	<u>601</u>	<u>621</u>	<u>633</u>	<u>624</u>
9.0	10.4	10.7	10.7	7.0	5.0	3.8	4.70
65	40	20	10.7	3	20	30	410 Pav

ML wash
shy wash

+90

<u>594</u>	<u>582</u>	<u>529</u>	<u>563</u>	<u>563</u>	<u>561</u>	<u>628</u>
9.7	8.5	9.2	10.8	10.8	11.0	4.3
65	40	20			40	50
					20	TOP

shy wash

11 +50

<u>595</u>	<u>525</u>	<u>571</u>	<u>563</u>	<u>564</u>	<u>567</u>	<u>556</u>	<u>559</u>	<u>623</u>
9.6	9.6	10.0	10.8	10.7	10.4	11.6	11.4	4.8
65	40	20		20	40	65	70	73

67.14

ML of cholla wash

Top bank dirt South

67.14

LT

±

PT

Cap. disc 13' Bdwn.
check 2 Fed. Blvd.

7.96 59.66 59.63
0.03

16 + 0.3.31

15 + 0.3.31 EC

+ 50

8.0
65

14

8.1
65

67.67

Notes Reduced Cells

65.61 65.93 65.61
4.41 1.29 2.01
18 Pav Pav 18 Pav.

602 594 65.4 64.48 64.79 64.41 65.2
7.4 8.4 2.4 3.13 2.83 3.21 2.4
65 110 26 18 283 19 40
Pav Pav Pav Pav Pav Pav

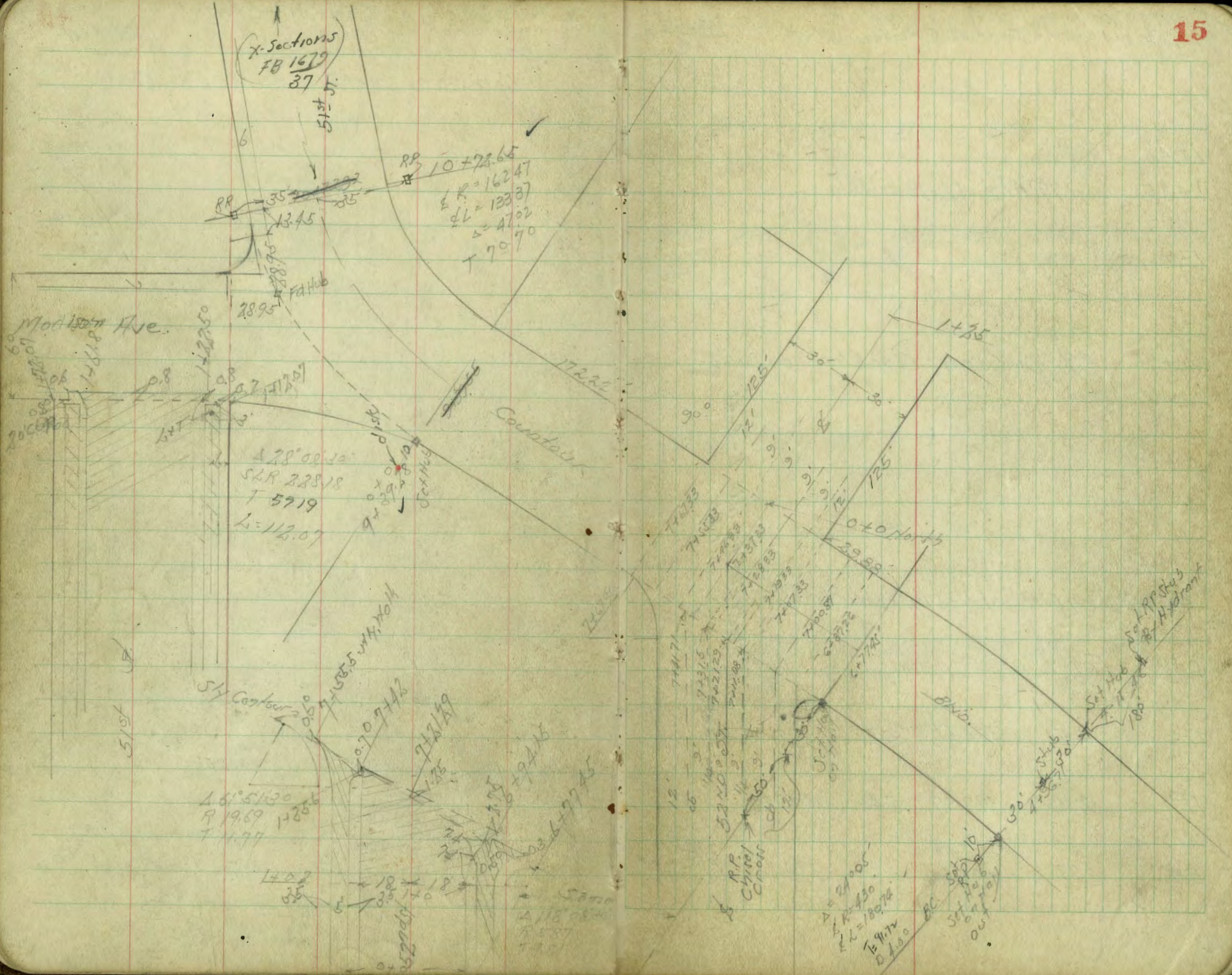
586 601 64.9 63.99 64.32 64.25 64.14 63.9 65.3
9.0 7.5 2.7 3.69 3.30 3.27 3.48 3.7 2.3
45 20 25 16.5 330 1.6 1.95 23 50
Pav Pav Pav 1/2 Pav Pav Pav Pav Pav

526 594 64.2 63.53 63.79 63.85 63.48 65.4
10.0 8.2 2.9 4.09 3.83 5.77 4.12 2.4
56 40 24 11.8 383 6.5 24.7 40
Pav Pav Pav 1/2 Pav Pav Pav St. Pav

67.67
↙

A table on page 12 with 4 columns and 20 rows. The columns are defined by vertical red lines. The first column is the widest, followed by three narrower columns of equal width. The rows are defined by horizontal blue lines. The table is currently empty.

A table on page 13 with 1 column and 20 rows. The column is defined by a vertical red line. The rows are defined by horizontal blue lines. The table is currently empty.



Cross Section of Monroe Ave
Dawson to East of Contour Blvd

Indexed
LM

St-H

Δ

Rt-S

Nov 4/1
S 1350
110-120-130
Moore

16

1+48

392.1 392.0 392.0 391.9 391.3
 $\frac{45}{30}$ $\frac{46}{18}$ $\frac{46}{18}$ $\frac{47}{18}$ $\frac{54.9/19.1}{19.1}$ $\frac{5.3}{30}$

1+25 179 Rt of Sly Power Pole

1+0

391.3 390.9 390.7 390.7 390.3 390.7 390.5
 $\frac{5.8}{30}$ $\frac{5.7}{18}$ $\frac{5.9}{15}$ $\frac{5.7}{15}$ $\frac{6.3}{15}$ $\frac{5.9}{18}$ $\frac{6.1}{30}$

0+76 = Do Garage Conc Floor on South

390.91

5.70

440 = Do Garage Conc Floor

0+50

390.0 389.7 389.3 389.8 389.1 389.7 389.8
 $\frac{6.6}{30}$ $\frac{6.9}{18}$ $\frac{7.3}{15}$ $\frac{6.8}{15}$ $\frac{7.5}{15}$ $\frac{6.9}{18}$ $\frac{6.8}{30}$

0+41

390.18

6.43

311 = Dig Hole

0+25 19.6 Rt of Sly Power Pole

0+0 = East Line of Dawson

389.2 389.0 388.8 388.9 388.4 388.9 389.4
 $\frac{7.4}{30}$ $\frac{7.6}{18}$ $\frac{7.8}{15}$ $\frac{7.7}{15}$ $\frac{8.2}{15}$ $\frac{7.7}{18}$ $\frac{7.2}{30}$

TP 4.53 396.61 5.29 396.68

High Pole
Monroe +
Contour

396.61

TP 2.16 397.37 5.40 395.21

BM 6.73 400.61 393.88

SWBP
E/Contour
53

Redy Plot on 18W 5-8-41
CBH

3+47.03 = E.L. Alhambra Park

386.1	386.8	387.8	389.3	389.9
10.5	9.8	8.8	7.3	6.7
30	18		18	30

3+0

387.4	388.1	388.3	388.6	389.0
8.7	8.5	8.3	8.0	7.6
30	18		18	30

2+93

388.62	388.53	
7.99	8.08	↓
37.8	30.5/100%	7.1/0.7
L. Garza Cont. 100%		

2+50

390.8	390.3	390.0	390.2	390.1	390.2
5.8	6.3	6.6	6.4	6.5	6.4
30	38	18		18	30

2+22.03 = E.L. Contour

391.4	391.1	391.0	391.8	390.7
5.2	5.5	5.6	5.8	5.9
30	18		18	30

1+81.77 = Δ on S.L. taken on split

392.0	391.9	392.7	391.4	391.2
1.6	1.7	1.9	5.2	5.4
38	30		30	38
396.61				

396.61

1+42.45

1+38

1+05

1+0

0+81

0+50

0+0 = HL Monroe

BM 3.06 39514

39208

Half Pale
Monroe
Contour
Page 16

1+21

2

R.F.

18

389.3	389.2	388.8	389.3	389.2	389.9	390.9
5.8	5.9	6.3	5.8	5.9	5.3	4.8
30	20	18	18	20	20	30

389.50

5.4
38.2 = 24' Cont
Walk

389.18

5.9
38.2 = 17' Cont
Walk

389.1	388.5	389.0	388.8	389.4	389.7
6.0	6.6	6.1	6.2	5.7	5.2
30	18		18	22	30

388.98

6.16
38.2 = 23' Cont
Walk

388.6	388.6	388.2	388.7	388.5	389.1	389.6
6.5	6.5	6.9	6.4	6.6	6.0	5.5
30	20	18		18	20	30

388.2	388.4	387.9	388.5	388.6	389.0	389.1
6.9	6.7	7.2	6.6	6.5	7.4	6.1
30	18	15		18	21.6	22
						30

39514

210 - BC Lt.

1498 22.5 Lt of $\frac{1}{2}$ - $\frac{1}{2}$ y Poxiv. Polli

1470

395.14 Ford

3890 3891

6.1 6.0
30 18

389.2 388.7 389.1

5.9 6.4 6.0
30 15

Cross Station Contour Blvd
 Monroe Ave to Madison Ave
 Alignment Page 14

Indexed
 LM

0+69 20.2 Pt of 2 = 5/4 Tol. Pok ✓
 0+83 22.4 Lt of 2 = 11/4 Part Pok ✓
 0+53.5

0+50

0+41

0+20

Red. Plot
 5-8-41
 = BH
 on Profile 1866

0+07.5 = 2 1/2 Roben Drive 7' Wide

0+0 = H.L. Monroe + 5 1/4 Contour

0-15

395.14 1/2 Ford

L.M. L RT=E 20

392.37

2.77
 30.4 = 2 1/2 Conc
 Walk

391.7	391.3	392.1	392.0	392.1
3.1	3.8	3.0	3.1	3.0
30	18		18	30

392.43

2.71
 30.3 = 2 1/2 Roben
 Drive 7' Wide

392.16

2.98
 30.4 = 2 1/2 Conc
 Walk

392.02

3.12
 30.3 = 2 1/2 Roben

391.4	391.5	392.4	392.0	391.9
3.7	3.6	2.7 = WH	3.1	3.1
35	18		18	35

391.87

2.77
 30.2 = 2 1/2 Conc
 Walk

395.14

2+29.14

2+18

1+99.76

1+83

1+50.92 = BL on Lt

1+68

1+0

0+89

0+74

20.2 ft of L = Fly to Blc

39514

Lt

L

ft

21

389.0	389.1	389.2	388.3	388.6	389.1
6.1 30	6.0 18	5.9	6.8 12	6.5 18	6.0 30

389.2	390.0	390.1	389.6	389.6	389.1	390.1
5.9 30	5.1 28	5.0 18	5.5 14	5.3	6.0 18	5.0 30

390.53

4.6
30 = 2.3 Conc
Half

390.6	390.6	390.3	390.6	390.3	390.7
4.5 30	4.5 18	4.8 14	4.5	4.8 18	4.4 30

391.95

3.19
30 = 1.3 Conc
Half

391.0	391.0	391.4	391.3	391.9
4.1 30	4.1 18	3.7	3.8 18	3.2 30

392.48

2.66
30 = 1.3 Conc
Half

392.64

2.50
30 = 1.7 Conc
Half

39514

3+90 21.6 Lt of 2 = 1/4 Paper Pole ✓

3+67 20 Rt of 2 = 1/4 Tol Pole ✓

3+58

3+50

3+16

3+05 = 1/2 9' Conc Drive

2+94 21' Rt of 2 = 1/2 12" Pole ✓

2+83

2+78 2/1

2+75 21' Rt of 2 = 8" Pole ✓

2+58 5/8

395/4

388.05 ✓
7.09
30 = 2.5' Conc
Walk

388.0	387.6	387.1	387.5	386.1	386.5	386.3
7.1	7.5	8.0	7.6	9.0	8.6	8.8
30	18	14		15	18	30

387.98	387.7	387.7	386.8	387.1	387.1
7.6	7.1	7.1	8.3	8.0	8.0
30 = 2.9' Conc Drive	18		13	18	30

388.32 ✓
6.82
31.5 = 2.9' Conc
Drive

388.48 ✓
6.66
31.0 = 2.4' Conc
Walk

388.5	388.0	388.4	387.4	387.7	387.8
6.6	7.1	6.7	7.7	7.1	7.3
30	18		12	18	30

388.4	388.4	388.7	387.6	388.1	388.6
6.7	6.7	6.4	7.3	7.0	6.5
30	18		12	18	30

395/4

5125 25 Δ of Δ = 1/4 Tol Polk ✓

5121

5101

4+96.71 = B.C. Lt. ✓

4+50

4+29

4+21

TP 4.18 390.94 8.28 386.76

4+0

395.14

4

2

91

23

386.60 ✓

1.34
386.3 - 23' Conc
Walk

386.63 ✓

1.31
386.3 - 28' Conc
Drive

387.4

3.5
30

386.5

4.4
18

386.6

4.3

385.6

5.3
18

386.6

4.3
30

387.2

3.7
30

386.6

4.3
18

386.2

4.7

385.5

5.4
18

385.7

5.2
30

385.93 ✓

5.01
30 - 28' Conc
Drive

387.30 ✓

3.64
30 - 28' Conc
Walk

390.94

387.42

7.72
30 - 28' Conc
Drive

387.1

8.0
18

386.8

8.3

385.4

9.7
18

385.4

9.7
30

395.14 ✓

6+75
6+50

23.2 Lt of $\frac{1}{2}$ = Wly Power Pole ✓

6+35

21.0 Pt of $\frac{1}{2}$ = Fly Tel Pole ✓

6+16

6+0

5+98

5+93

20.5 Lt of $\frac{1}{2}$ = Wly Power Pole ✓

5+79

5+50

5+35

390.94

4+

2

Pt.

24

386.6	385.3	384.7	383.9	384.4	383.2	383.8	383.4	384.4
4.3 30'	5.6 28'	6.2 18'	7.0 15'	6.5	7.7 15'	7.1 18'	7.5 26'	6.5 30'

385.20 ✓

5.14
24.5 = 27 Cone
Walk

387.3	386.4	385.5	385.5	384.9	385.1	386.0
3.6 30'	4.5 26'	5.1 18'	5.4	6.0 18'	5.8 25'	4.9 30'

386.20 ✓

4.74
24.3 = 27 Ribbon
7.0, 9.0

386.64 ✓

4.30
13.0 = 27 Cone
Drive

387.7	386.9	386.0	386.4	385.7	386.2	387.0
3.2 30'	4.0 27'	4.9 18'	4.5	5.2 18'	4.7 26'	3.9

387.24 ✓

3.70
19.3 = 23.5 Cone
Walk

11.7618 ✓

390.94

7+55.5

7+42 = WCB From South

7+37.33 = 52nd From N

7+21.29 = 52nd St From South

7+07.33 = E.L. 52nd St From North

6+94.15

TP 3.70 38944 5.20 385.74 67 E.C. No 3
67 South
6+77.45

6+77.45 E.C.

390.94

Lt.

S

Rt

383.49

5.95
39.1011

383.27

383.62

383.46

383.04

6.17 5.82
9.4 5.06
S End Pt

5.98 6.40
30.06 30.601

383.29 383.1 382.2 381.7 381.5 379.3 375.7

6.15 6.3 7.2 7.7 7.9 10.1 13.7
30.09 Par 18 18 30 80 130

383.96 383.91 383.4 382.5 381.1 381.8

5.48 5.53 6.0 6.9 7.3 7.6
30.09 Par 28.7 Par 18

384.23 384.19 383.6 382.9 382.3 382.1 379.9 379.6

5.71 5.75 5.8 6.5 7.1 7.3 9.5 9.8
30.09 Par 28.11 Par 18 18 30 80 130

384.62

384.27

384.60

384.21

4.88 5.17 4.84 5.23
1.06 9.67 27.5 cb 27.5

S End Pt

389.44

385.74 384.8 383.7 383.8 382.7 383.1

5.20 6.1 7.2 7.1 8.2 7.8
30 26 18 18 30

390.94

9150

9139.28 BC RT

910

8150

810 19' Lt of L = Sky Harbor Pt

7167.33 - W L 52' N. From North

389.14

Lt

L

Rt

3846	3842	3812	3842	3834	3842	3842	38451
48	52	61	52	60	52	52	493
30	20	18		10	18	30	60.251

8 Cox
Drill

3845	3838	3831	3840	3832	3835	3833
49	56	63	54	63	59	61
30	18	15		10	18	30

3830	3825	3811	3829	3824	3824	3829
64	69	73	65	70	70	65
30	18	14		18	30	40

3819	3813	3813	3814	3812	3818	3813
75	81	81	80	82	76	81
40	30	18		18	30	40

3815	3813	3814	3815	3813	3816	3813
79	81	80	79	81	78	81
40	30	18		18	30	40

3825	3821	3817	3813	3816	3787	3769	3686
69	73	77	81	78	107	125	108
30	18	18	18	30	80	100	130

10+72.65

3876	3870	3869	3857	3863
1.8	2.1	2.5	3.7	3.1
30	18		18	30

10+50

3871	3869	3866	3860	3860
2.1	2.5	2.8	2.1	3.1
30	18		18	30

10+81

38603

3.1

33.6 = 24096 ✓

2011

10+0

3861	3860	3851	3848	3847	3850
0.3	4	4.3	4.6	4.7	4.1
18	18		8	18	30

389.44

389.44

Cross Section Mad 1004 H. 5/5
118.07 E of F.L. 5/5 to F.L. 5/5

1+42.07

INDEXED
WK
JAN 18 1949

1+22.8 FCL 5/5

1+12.07 = F.L. 5/5

0+70

Redy Plot
CBH 5-8-41
on Profile 1864

0+35

0+0 = 9+89.28 Contour 1864

389.44

H-5

H-Rt.

28

386.90	387.0	387.2	387.2	387.6
2.54	2.4	2.8	2.2	1.8
292-114 Pa	18	18	18	38

386.64	386.24	386.62	386.11
2.80	2.20	2.82	2.33
378-90	376-90	392-90	392-90

386.9	386.8	386.9	387.1	387.8
2.5	2.6	2.5	2.3	1.6
30	18	18	18	30

387.4	386.5	386.2	385.4	386.3
2.0	2.9	2.2	4.0	3.9
30	25	18	14	

386.1	384.9
2.3	4.5
30	20

BM

5.96

38038

St. BP
1991
38037

TP

0.23

38628

5.57

38605

TP

3.75

39162

1.57

38787

1472.07 = H.L. 5/10/07

1461.8 = H.C.B. Ref

38944

47

2

R1

29

INDEXED
JAN 1 1962

3873

2.1
30

3873

2.1
18

3876

1.8

3871

2.3
18

3878

1.6
30

38719

2.5
30

38673

2.71
30

38720

2.24
30

38676

2.68
30

387-06 294-50

38944

Cross Section 52nd St. From Conour Blvd.
 100' S of FC on East
 See Sketch Page 15

INDEXED
 W K
 JAN 18 1949

1+17.8 07 W

1+02.7 02 E

1+0 = C6BC 02 E

0+25

0+50

0+25

0+0 = 100' S of FC on E

BM 548 391.22

385.74

09#CHut
 6+774502
 C67601
 Page 25

May 22-41
 5.550
 Northern
 11/18/49
 30

383.84 383.42
 7.38 7.80
 WCB 11.50

384.24 384.64
 6.98 6.58
 FCB FCB

384.23 383.78
 6.99 7.41
 18 18

384.25 384.61
 6.97 6.61
 18 18

384.22 384.37
 6.50 6.85
 18 18

384.68 388.02
 6.54 6.15
 18 18

385.22 384.82
 5.95 6.35
 18 18

385.12 385.44
 6.10 5.78
 18 18

385.83 385.43
 5.39 5.79
 18 18

385.56 385.93
 5.66 5.29
 18 18

386.23 385.76
 4.99 5.36
 18-CB 18-GW

385.93 386.32
 5.29 4.85
 18-Gut 18-CB

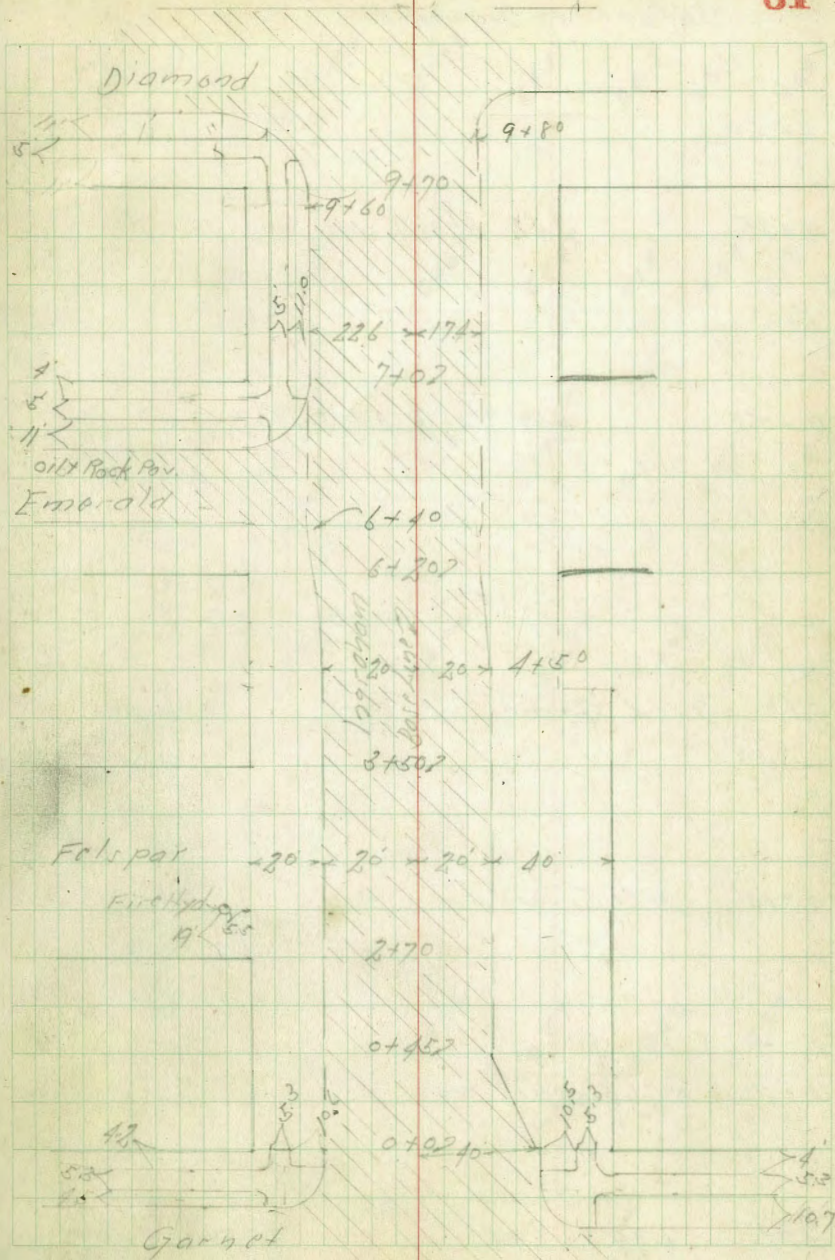
391.22

Cross Section Ingraham St.
Garnet to Diamond

Indexed
LM

May 29-41
Sisson
Kortberg
Moore
Albin

400
200
100
47.



Cross Section Ingham St
Garnet to Diamond

1+50

1+25

23.2 At of β = N4 Power Pole

1+0

0+52

41.2 R of β = E4 Td Pole

0+45

0+0

N L Garnet

0-14

H C b Garnet From West

0-20

= H C b Garnet From East

B.M.

6.79

6.933

6.254

SFBP
Garnet
Ingham

Reduced & Plotted Profile 1202
6-2-41 CRH.

	L.H.	β	R.T.	E
	65.6	65.2	64.59	64.22
	3.7 40	4.1 25	4.74 20	4.11
	65.17	64.3	65.1	65.5
	4.16 20	5.0 30	4.2 40	5.8 60
	64.9	64.5	63.97	64.47
	4.4 40	4.8 25	5.36 20	4.86
	64.47	63.8	64.3	64.3
	4.86 20	5.5 28	5.0 40	5.0 52
	63.8	63.8	63.26	63.78
	5.4 40	5.5 25	6.07 20	5.55
	63.76	63.3	63.7	64.4
	5.57 20	6.0 32	5.7 40	4.9 60
	63.3	63.30	62.63	63.00
	6.0 40	6.03 20	6.70 20	6.33
	63.12	62.76	63.97	62.72
	6.21 40	6.57 20	6.61 20	6.76 20
	62.57	62.57	62.56	62.97
	6.77 25	6.77 25	6.77 25	6.76 25
	69.33			

2+10 = 2 Felspar

2+90 = J.C.B.

2+70 = S.L. Felspar

2+69 22.8 Lt of B = W/Ly Perm Polr ✓

2+50

2+08' 41.3 Rt of B = E/Ly Tol Polr ✓

2+0

69.33

Lt

B

Rt

33

67.4	66.75	67.39	67.37	67.3	67.3	67.3	67.3	68.6
1.9 40	2.58 20	1.94	1.96 20	2.0 30	2.0 40	2.0 40	2.0 38	2.0 20

67.3	67.1	66.52	67.15
2.0 40	2.2 25	2.81 20	2.18

67.3	66.7	66.8	66.28	66.93	66.84	66.3	66.9	66.9	68.0
2.0 40	2.6 35	2.5 25	2.05 20	2.40	2.49 20	3.0 28	2.1 40	2.1 35	1.3 50

67.1	66.2	66.4	65.99	66.60	66.60	65.9	66.6	66.6	67.8
2.2 40	2.1 35	2.9 25	2.31 20	2.73	2.83 20	3.4 28	2.7 40	2.7 55	1.8 60

66.2	65.8	65.26	65.25	65.82	66.0	65.8	66.5
3.1 40	3.5 25	4.07 20-Feldsp Polr	3.48	3.51 20-Feldsp Polr	4.3 28	3.5 40	2.8 60

69.33

5+50

5+0

4+78

4+50

4+0

TP 7.73 76.61 0.45 68.88

3+50 = N.L. Feldspar 41.5 Pt of $\frac{1}{2}$ Fly Tot. Pole ✓

3+30 = N.C6

69.33

Lt

R

Rt

34

73.0	72.7	72.93	72.78	72.62	72.7	73.3	73.8
3.6 40	3.9 35	4.35 35	3.83	3.99 35	3.9 35	5.3 40	3.8 60

71.8	71.4	70.98	71.47	71.43	71.5	71.8	72.8
4.8 40	5.2 35	5.63 21.5 Edgt 18.17	5.4	5.18 18.4 Edgt 18.17	5.1 30	4.8 40	3.8 60

71.4	69.8	70.0	69.60	70.18	70.39	70.1	70.6	70.5	71.6
5.2 40	6.8 35	6.6 25	7.01 20	6.43	6.22 20	6.5 30	6.0 40	6.1 35	5.0 60

69.8	69.0	68.9	68.42	69.04	69.09	68.8	69.0	69.6
6.8 40	7.6 35	7.7 35	8.19 26	7.57	7.52 20	7.8 30	7.6 40	7.0 60

76.61

68.9	67.9	68.0	67.36	67.92	67.90	67.8	68.1	68.2	68.9
0.4 40	1.4 35	1.3 25	1.97 20	1.41	1.23 20 Edgt 18.17	1.5 30	1.2 40	1.1 35	0.1 60

68.8	67.8	67.7	67.06	67.63
0.5 40	1.5 35	1.6 25	2.27 20 Edgt 18.17	1.90

69.33

TP 10.72 85.70 1.63 74.98

7+0 = N.L. Emerald

6+8° = N.C6

6+60 = E Emerald

6+40 = S.C6

6+20 = S.L. Emerald

6+18 28.7 Lt = Wly. Pow. Pole ✓

6+16 Pt of S 2.74 = 2 Fire Hyd 4.15 Pt S = Ely Tol. Pk ✓

6+0

76.61

Lt.

S

Pt.

35

76.88	75.17	75.57	75.58	76.69	77.4
0.73	1.44	1.04	1.03	0.2	70.8
22.6	22.6	22.6	17.4	30	40

76.00	75.19	74.80	75.28	75.26	75.4	75.6
0.61	1.45	1.81	1.03	1.35	1.2	1.0
22.6	22.6	22.6	17.4	17.4	30	40

74.8	74.7	74.48	75.03	74.96	75.1	75.3
1.8	1.9	2.13	1.58	1.65	1.5	1.2
40	30	22.6	17.4	17.4	30	40

74.4	74.4	74.17	74.77	74.58	74.8	75.3
2.2	2.2	2.44	1.84	2.03	1.8	1.8
40	30	22.6	17.4	17.4	25	40

74.0	74.2	73.81	74.52	74.27	74.2	75.2	75.6
2.6	2.4	2.80	2.09	2.34	2.4	1.9	1.0
40	25	22.6	17.4	17.4	25	40	60

73.5	73.8	73.42	74.05	73.86	73.3	74.5	74.9
3.1	2.8	3.19	2.56	2.75	3.0	2.1	1.7
40	25	22.6	17.4	17.4	25	20	60

76.61

9+60 = C6 BC 07 Lt

9+50

9+0

8+50

8+0

7+52

7+50

All Rt of B = Fly Ted Pole

85.70

Lt

B

Rt

36

82.40	81.78	82.22	82.20	82.3	83.0	83.2
3.36	3.92	3.18	3.50	3.1	2.7	2.5
22.6	22.6		17.4	20	30	40

82.14	81.51	81.98	81.86	82.0	82.5	82.6
3.56	1.19	3.72	3.81	3.9	3.2	3.1
22.6	22.6		17.4	20	30	40

80.91	80.19	80.80	80.58	80.5	81.1	82.0
4.79	5.51	4.90	5.12	5.2	4.6	3.7
22.6	22.6		17.4	20	30	40

79.63	78.95	79.45	79.27	79.4	80.3	
6.07	6.75	6.25	6.43	6.3	5.1	
22.6	22.6		17.4	20	40	

78.35	77.67	78.19	78.01	78.1	79.2	79.8
7.35	8.03	7.51	7.69	7.6	6.5	5.9
22.6	22.6		17.4	20	35	40

77.10	76.35	76.90	76.66	76.9	77.8	78.9
8.60	9.35	8.80	9.04	8.8	7.9	6.8
22.6-C6	22.6-Grt		17.4-Fly Ted Pole	20	35	40
		85.70				

BM

0.51

85.19

NE Mon
Diamond
Ingram
85.22

10+10 = $\frac{1}{2}$ Diamond

9+90 = SCB of Diamond

9+70 = SL Diamond

9+64

27.5 ft of $\frac{1}{2}$ Fire Hyd ↓

85.70

Lt

R

R1

37

82.24	82.59	82.90	83.26	83.53
3.34 70	3.11 22.6	2.80	2.44 20	2.17 46

82.22	81.60	82.42	82.74	82.98	83.03	83.9
3.48 52.5-65.5	4.10 52.5-60	3.28 52.6	2.96	2.72 20	2.67 27-Edg Pol	1.8 40

82.54	81.88	82.52	82.49	82.7	83.4
3.16 23.2-66	5.82 23.8-60	3.18	3.21 17.4-Edg Pol	3.0 20	2.3 40

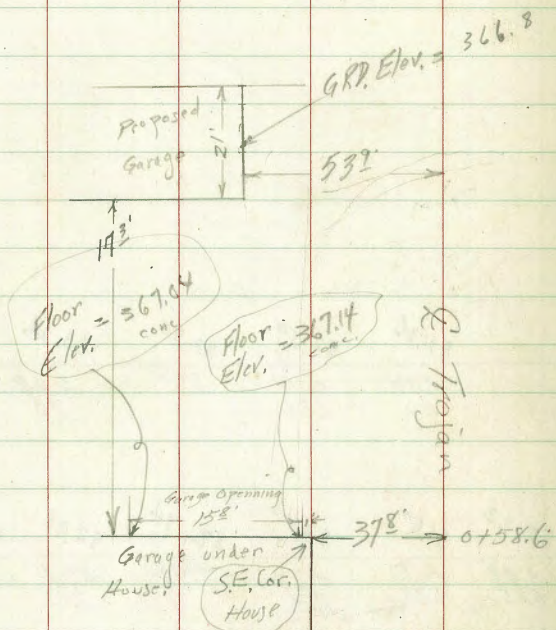
85.70

Gross Section Trojan Ave
50th St to Altadena

Indexed
LM

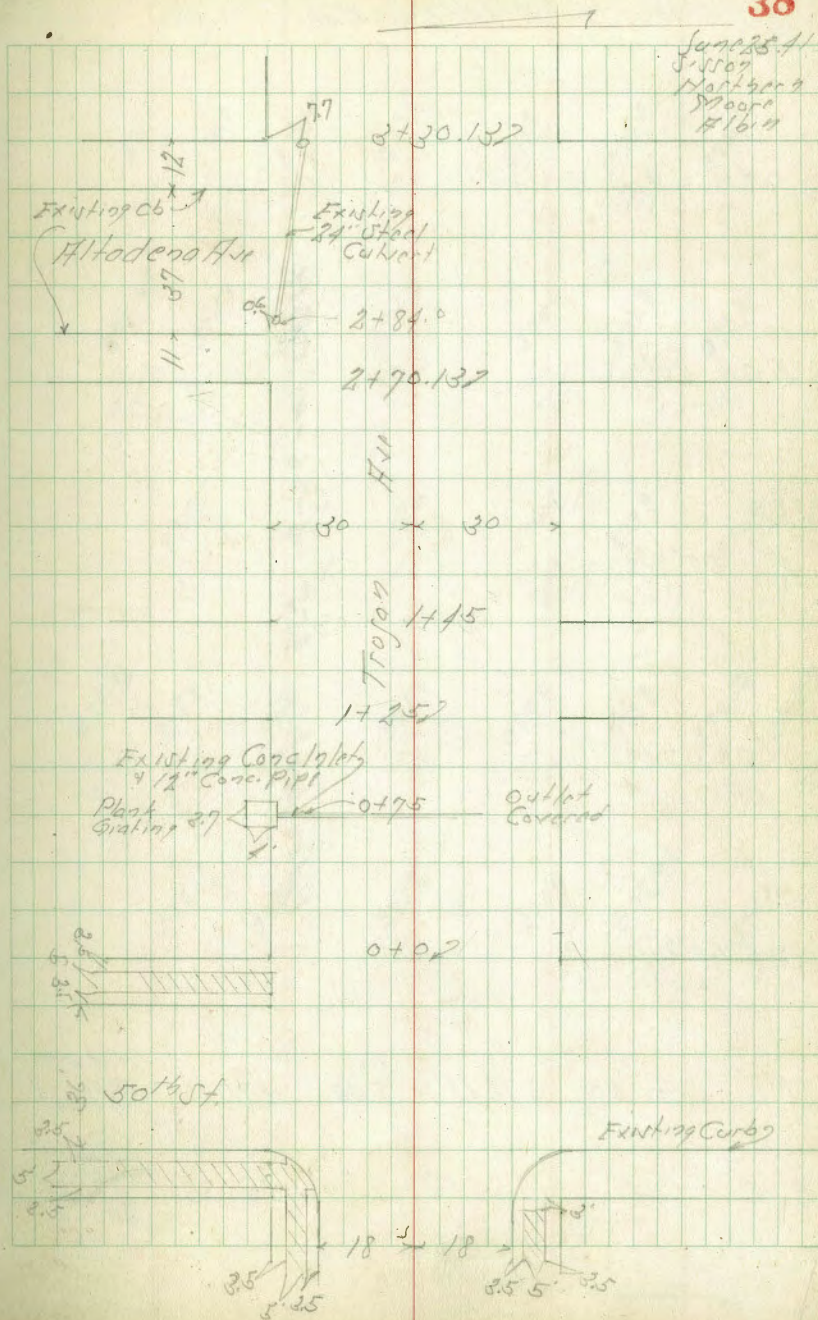
38

17.3
30.6
25.9
21
96.4



10-24-51
G. Roberts

used direct elev. Rod
BM NWSP 50th & Trojan E.L. 50th 0+00



June 25/11
S. 5507
N. 4400
S. Moore
#1611

Cross Section Trojan Ave
50th St to Alameda Ave

0+0 - FL 50th St

FC 50th St

50th St

WC 50th St

WL 50th St

TP 0.50 376.61 8.45 376.11

BM 1.41 384.58 383.15

N.M.B.P.
Trojan Ave
50th St

N.M.B.P.
Alameda Ave
50th St
8700 ft

Paten profile 855 6-26-41 C.B.M.

Lt. N

RT. S

39

375.2 1.4 30-cb	374.3 1.8 30-cb	373.4 2.1 30-cb	372.5 2.1 30-cb	373.5 2.1 30-cb	373.4 2.1 30-cb	372.9 2.1 30-cb	
375.72 0.89 30-cb	374.7 1.9 30-cb	374.4 2.1 30-cb	374.2 2.1 30-cb	374.0 2.1 30-cb	373.8 2.1 30-cb	373.3 2.1 30-cb	
375.5 1.6 30-cb	375.4 1.8 30-cb	375.0 1.6 30-cb	374.4 2.1 30-cb	373.9 2.1 30-cb	373.9 2.1 30-cb	371.9 2.1 30-cb	
375.92 0.69 30-cb	375.2 1.4 30-cb	375.1 1.8 30-cb	375.4 1.8 30-cb	374.6 2.0 30-cb	373.8 2.8 30-cb	374.7 2.1 30-cb	370.87 5.71 80-cb
376.16 0.45 18-cb	374.9 1.7 18	375.2 1.0 18	374.9 1.7 18	375.98 0.65 18-cb	375.98 0.65 18-cb	375.1 1.5 30	
			376.61				

1+95 = 5 L Alley

1+25 = 2 L Alley 20.5 Pt of 2 = 5 L Power Pole

1+0

0+95 = Condulet on Lt

0+50

0+25

376.61

372.3	371.4	370.3	369.8	369.1	370.0	369.9	369.3	368.5
4.3 70	5.5 60	6.6 80	7.8 90	9.0 100	10.2 110	11.4 120	12.6 130	13.8 140
371.0	370.7	369.8	369.3	369.2	369.6	369.3	368.5	367.6
5.6 70	6.9 80	8.2 90	9.5 100	10.8 110	12.1 120	13.4 130	14.7 140	16.0 150
368.3	368.2	369.1	369.6	368.9	364.2	362.7	361.0	
8.8 70	10.1 80	11.4 90	12.7 100	14.0 110	15.3 120	16.6 130	17.9 140	
369.5	360.5	370.5	367.4	368.7	369.5	369.0	361.3	366.5
9.8 70	11.1 80	12.4 90	13.7 100	15.0 110	16.3 120	17.6 130	18.9 140	20.2 150
368.2	369.1	370.2	370.3	369.6	369.6	367.3	364.7	362.0
10.1 70	11.4 80	12.7 90	14.0 100	15.3 110	16.6 120	17.9 130	19.2 140	20.5 150
369.5	371.6	371.3	371.1	371.1	370.9	369.8	368.3	
11.4 70	12.7 80	14.0 90	15.3 100	16.6 110	17.9 120	19.2 130	20.5 140	

376.61

Trojan Ave.

2+81.13 = WCB

2+70.13 = W.L. Hodens

2+50

2+25

2+0

1+70

876.61

LT

L

RT

41

370.45	369.9	369.1	368.2	367.9	364.8	361.9	361.0
6.16 30	6.17 30	7.5 21	7.8 18	8.7	11.8 18	14.7 30	15.6 40
370.7	369.8	369.1	368.2	368.6	368.2	366.0	363.8
6.5 30	6.8 20	7.5 18	7.8	8.0 7	8.4 18	10.6 30	12.8 40
370.4	369.1	369.4	369.6	369.5	370.0	367.7	366.3
6.7 30	6.7 20	7.2 18	7.0	7.1 5	6.6 18	8.9 30	10.2 40
371	370.2	369.5	369.8	369.6	370.4	370.1	369.3
5.5 30	6.1 20	7.1 18	6.8	7.0 6	6.2 30	6.5 30	7.5 30
	371.3	370.0	370.0	369.8	370.0	369.7	369.8
	6.5 30	6.6 30	6.6	6.8 8	6.6 18	6.9 30	7.8 40
	372	370.5	370.0	370.0	370.0	369.6	369.6
	6.4 30	6.7 18	6.6	6.6	6.6 8	7.1 30	8.0 40
			19.961				

BM - 1.83 383.15

SWBP
F1 Cojon
50' 54"
383.15

TP 887 384.98 0.50 376.11

3730.13 - EL Altodena

3730.13 - Fcb Lint

3700.13 - ~~S~~ Altodena

37840 = Inlet 24" Steel Cul. on Lt

376.61

Lt

Rt

Rt

42

367.1	364.8	364.7	364.7	364.3	362.4	358.5	356.5
9.5 30	11.8 24	11.90 24.3	11.9 18	11.8 12	12.3 18	18.1 30	20.1 40

362.1	361.8	361.3	364.3	362.8	361.3
7.40 30-54" 10	8.5 30-54" 10	10.3 18	11.0 12	12.8 30	15.3 40

369.5	368.3	366.3	363.8	362.1	360.6
7.1 30	8.6 18	10.3 12	12.8 18	14.5 30	16.0 40

366.57
10.04
29.1
F1.21
Steel Cul.
376.61

X sec DAWSON Ave 60' wide
 El Cagon to Monroe 17' curbs
 9' 1/4's

SW.B.P. 138 395.76 393.88. Sid St. El Cagon

N cb El Cagon		
E cb	8.91	386.05
E gut	9.53	385.73
cb pav	9.92	385.39
1/4 "	10.28	384.98
C "	10.71	384.55
1/4 "	11.26	384.00
cb "	12.00	383.26
w/c cb	12.00	383.22
w/c gut	12.67	382.59

0+00 TO 0+10.39 on w/c - N.E. El Cagon

w/c	11.5	383.8
cb Top	11.24	384.07
gut pav	11.87	383.39
1/4 "	11.21	384.05
C "	10.71	384.55
1/4 "	10.27	384.99
gut "	10.00	385.26
cb Top	9.44	385.80
E	8.8	86.5

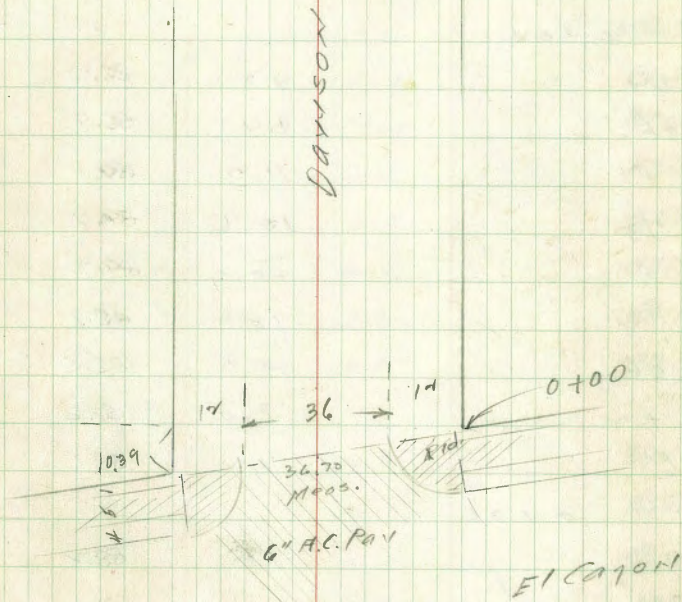
Notes Reduced 7.25.41.

INDEXED
 WIK
 JAN 18 1949

Moore
 G. Farrow
 7-26-41.

Monroe

4+9465



2nd and per. with N.H. ElCajon

E	8.6	886.7
cb	9.6	885.7
1/4	10.3	885.0
c	10.7	884.6
1/4	11.2	884.1
cb	11.5	883.8
+1	9.5	885.8
w	9.4	885.9
o + 04		
w	9.3	886.0
cb	9.4	885.9
+1	11.2	884.1
1/4	10.6	884.7
c	10.6	884.7
1/4	10.2	885.1
cb	9.8	885.5
+2	8.0	887.2
E	7.2	888.1
o + 36		
E	7.1	888.2
+11	7.1	888.2
cb	7.3	888.0
+2	8.4	886.2
1/4	8.6	886.7
c	8.7	886.6

7cl pole

1/4	9.1	386.7
cb	9.3	86.0
+2	8.5	86.8
w	8.8	86.5
T.P. 360.0 391.26 7.60 387.66		
o + 65		
-5	4.6	386.7
w	4.4	86.9
cb	4.7	87.0
1/4	3.8	87.5
c	3.6	87.7
1/4	3.5	87.8
cb	3.2	88.1
E	3.0	88.3
1 + 00		
E	2.2	89.1
cb	2.8	88.5
1/4	3.3	88.0
c	3.8	87.5
1/4	4.1	87.2
cb	4.4	86.9
w	4.8	86.5
+5	5.2	386.1

	1+35		
-5		5.3	86.0
W		5.0	86.3
cb		4.7	86.6
1/4		4.2	87.1
c		4.1	87.2
1/4		3.4	87.9
cb		3.0	88.3
E		2.5	88.8
	1+67		
E		3.0	88.3
+11	Tel pale ✓	3.7	87.6
cb		3.7	87.6
1/4		4.1	87.2
c		4.4	86.9
1/4		4.7	86.6
cb		5.0	86.3
W		5.3	86.0
+5		5.9	85.9
	2+00		
-5		5.6	86.7
W		5.2	86.1
cb		5.0	86.3
1/4		4.8	86.5
c		4.5	86.8

1/4		4.3	87.0
cb		4.0	87.3
E		3.1	88.2
	2+50		
E		3.3	88.0
cb		4.0	87.3
1/4		4.4	86.9
c		4.5	86.8
1/4		4.7	86.6
cb		4.9	86.9
W		4.7	86.6
+5		5.6	85.7
	2+84		
W	♀ 3' walk	4.55	887.71
	2+94		
W	♀ de-rib. ^{com} de.	4.50	86.76
E	" " " "	3.20	88.06
	3+00		
-5		5.7	85.6
W		4.6	86.7
cb		4.7	86.6
1/4		4.4	86.9
c		4.0	87.3
1/4		4.0	87.3
cb		3.9	87.9
E		3.4	87.9

	3 + 04			
E + 9	Tel Pole			
	3 + 41			
W F	2 do, Rib	CEM. Dn.	4.45	386.81
E	" "	" "	3.6	388.10
	3 + 60			
E	Lawn		3.7	88.1
cb	"		3.6	87.7
1/4			3.6	87.7
c			3.4	87.7
1/4			4.1	87.2
cb			4.5	86.8
W F	3.5	CEM walk	4.51	86.75
	4 + 00			
W			4.4	86.9
cb			4.1	87.2
1/4			3.9	87.4
c			3.4	87.9
1/4			3.5	87.8
cb			3.4	87.9
E			2.8	88.5
T.P.	5.31	393.11	3.46	387.80 ✓
	4 + 00			
W F	3'	CEM walk	6.40	386.91

	4 + 25			
W F	2 do, rib	CEM Dn.	6.00	387.11
	4 + 35			
E			4.2	88.9
+ 9	Tel Pole			
1/4			4.6	88.5
cb			5.3	87.8
1/4			5.0	88.1
c			5.0	88.1
1/4			5.6	87.5
cb			6.0	87.1
+ 1			5.3	87.8
W			5.3	87.8
	4 + 31			
W + 11	Power Guy Pole			
E F	4' CEM walk		3.64	389.99
	4 + 40			
W F	4' CEM walk		5.00	88.11
	4 + 49			
E F	4' CEM	" "	3.43	89.08
	4 + 54.65	SL Modroc		
W			4.8	88.3
cb			5.2	87.9
1/4			4.8	88.3
c			4.6	88.5

Xsec Monroe Ave 9' 1/2" wide
12' curbs

E.L. 52nd to E.L. Dawson Ave

52nd Con. Nail Pole 0.28 392.36
Monroe Con. Nail Pole 392.08

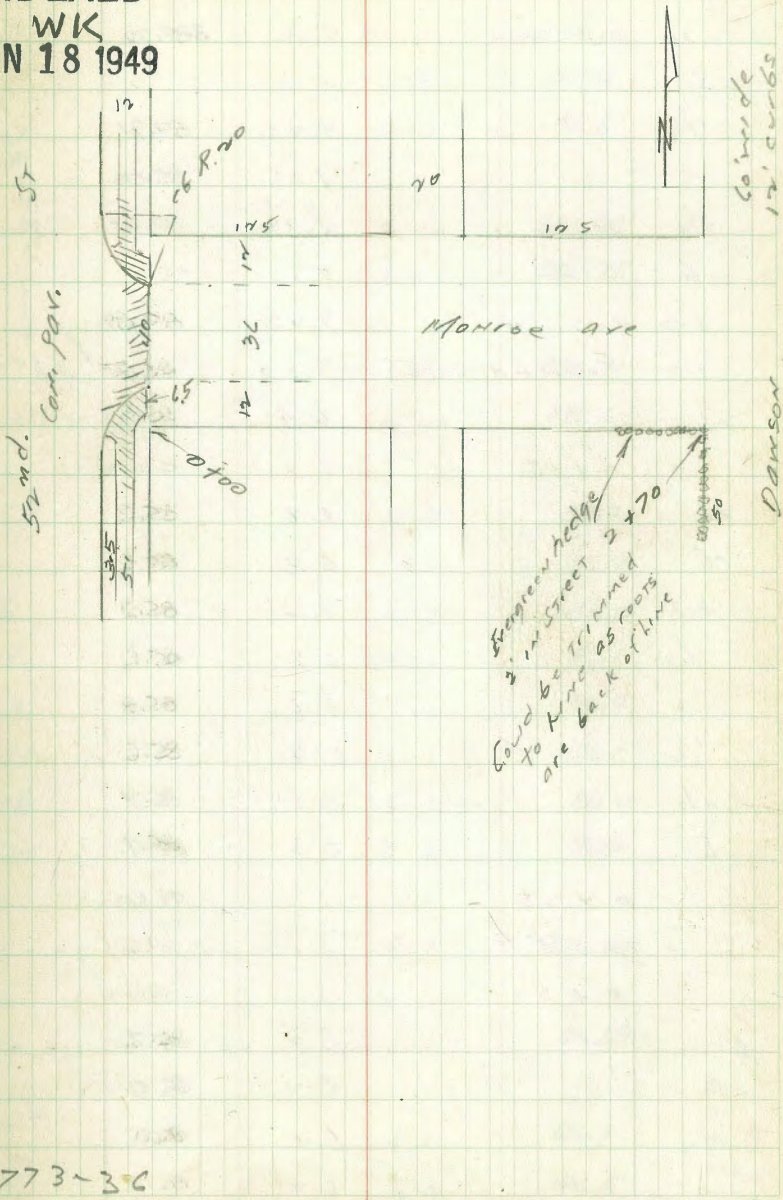
0-12	E.C. line	52nd		
S-8	cb P.C. Top	7.29	385.07	
"	gut	7.89	89.97	
S	par	7.77	84.59	
cb	"	7.73	89.63	
1/4	"	7.45	89.71	
c	"	7.60	89.76	
1/4	"	7.55	89.81	
cb	"	7.50	89.86	
N	"	7.43	89.93	
+8	cb P.C. gut	7.41	89.95	
"	cb " Top	7.01	85.35	
0-6				
N	Top cb	7.04	385.32	
"	gut	7.49	89.87	
c	"	7.45	89.91	
S	gut	7.65	89.71	
S	Top cb	7.21	85.15	
0+00	E.L. 52nd			
S	"	6.8	86.6	
+10	Top end curb	7.21	385.15	385.14 - 1773-3C

INDEXED

WK
JAN 18 1949

C. Moore 7-30-41.
G. Farrow

48



S + 10	gut pav	7.64	389.72
cb	"	-	
1/4	"	7.45	89.91
c	"	7.34	85.00
1/4	"	7.39	89.97
cb	"	-	
+ 2	gut "	7.47	89.89
+ 2	Top end curb	7.09	85.27
N		6.9	85.5
	0 + 15		
N		6.8	85.6
cb		6.8	85.6
+ 3		7.2	85.2
1/4		6.8	85.6
c		6.6	85.8
1/4		6.8	85.6
cb		6.7	85.7
S		6.3	86.1
	0 + 28		
S + 10	P.P		
	0 + 50		
S		6.7	86.7
cb		6.4	86.0
1/4		6.4	86.0
c		6.2	86.2

1773.36

385.27

1/4		6.5	385.9
cb		6.8	85.6
N		6.6	85.8
	0 + 58		
S + 3.7	w.l. Con. Drive apron	6.70	385.66
S		6.61	385.75
	0 + 66		
S		6.65	385.71
+ 3.7	EL Con. Drive apron	6.73	385.63
	1 + 00		
S		7.5	89.9
S		7.0	85.9
cb		6.4	86.0
1/4		6.3	86.1
c		6.0	86.2
1/4		6.3	86.1
cb		6.2	86.2
N		6.0	86.2
	1 + 03.5		
N - 0.3	w.l. Con. Drive apron	5.69	386.67
	1 + 23.4		
N - 0.3	EL Con. Drive apron	5.77	86.59
	1 + 35		
N		5.5	86.9
cb		5.9	86.5

1 + 23.7
S + 10 - P.P.

1/4		5.8	386.6
c	M.H. R.M	5.4	87.0
1/4		5.9	86.5
cb		6.3	86.1
s		6.4	86.0
+5		6.8	85.6
	1 + 70		
-5		6.6	85.8
s		5.9	86.5
cb		5.8	86.6
1/4		5.7	86.7
c		5.5	86.9
1/4		5.7	86.7
cb		5.8	86.6
N		5.4	87.0
	2 + 00		
N		4.9	387.5
cb		5.5	86.9
1/4		5.4	87.0
c		5.7	87.2
1/4		5.4	87.0
cb		5.7	87.2
s		5.6	86.8
+5		5.9	86.5

	2 + 0.7		
N	wk. Con apron	4.75	387.61
N + 1.1	" " "	4.94	387.99
	2 + 4.2.5		
N	EL apron	4.67	387.69
N + 1.1	" " "	4.80	387.56
	2 + 0.7.4		
S	wk. Con apron	4.97	387.39
S + 0.7	" " "	4.96	387.40
	2 + 19.2		
S	EL Con apron Drive	4.93	387.93
S + 0.7	" " "	4.91	387.93
	2 + 19.2 wk. Con. walk	0.17	IN ST.
	2 + 25.7 EL " "	" "	" "
	2 + 40		
S		4.5	387.9
cb		4.8	387.6
1/4		4.8	87.6
c		4.7	87.7
1/4		4.8	87.6
cb		5.0	87.4
N		4.5	87.9
	N + 70 wk. Davison		
N		4.0	88.4

ndc	4.4	388.0
1/4	4.4	88.0
c	4.1	88.3
1/4	4.3	88.1
cb	4.4	88.0
s	4.1	88.3

7 + 69

s + 10 P.P.

W cb Dawson

s	4.5	387.9
cb	4.3	88.1
1/4	4.1	88.3
c	4.0	88.4
1/4	4.2	88.2
cb	4.3	88.1
N	4.4	88.0

E Dawson

N	3.8	88.6
cb	3.8	88.6
1/4	3.8	88.6
c	3.8	88.6
1/4	3.9	88.5
cb	3.9	"
s	3.9	"

E cb Dawson

s	3.5	388.9
cb	4.0	88.2
1/4	3.8	88.6
c	3.6	88.8
1/4	3.6	"
cb	3.5	88.9
s	3.4	89.0

E L Dawson

PIL

Cross Section Littlefield St.
Denver St to Frankfort St.

Sketch Page 52

0+0 = 2' Lietot Beaver

INDEXED

WK
JAN 18 1949

0-25 = st. L. Lieto From South

NY Carb. Retain Denver

0-74.3 = opp C&FC on st.

BM

6.96

16.74

✓ M.F.B.P.
Littlefield
Denver St
Carb. Ret.

TP

3.92

53.70

10.52

49.78

TP

1.98

60.30

7.44

58.32

BM

10.13

65.76

55.63

NY Carb.
Frankfort
St
1926

Lt. H

Rt. 5

53

7.82 15.50 15.00 PM	46.67	6.82 15.00 15.00 PM	46.88	6.7 15.00 15.00 PM	47.0	6.5	47.2	6.5 15.00 15.00 PM	47.2	5.8 15.00 15.00 PM	47.9	6.0 15.00 15.00 PM	47.7	5.7 15.00 15.00 PM	48.0
7.64 15.00 15.00 PM	46.06	7.48 15.00 15.00 PM	46.22	7.4 15.00 15.00 PM	46.3	7.1	46.6	7.0 15.00 15.00 PM	46.7	6.5 15.00 15.00 PM	47.2	6.5 15.00 15.00 PM	47.4	6.2 15.00 15.00 PM	47.4
8.61 15.00 15.00 PM	45.09	8.48 15.00 15.00 PM	45.22	8.00 15.00 15.00 PM	45.70	8.18 15.00 15.00 PM	45.22	8.27 15.00 15.00 PM	45.43	8.28 15.00 15.00 PM	44.92	8.45 15.00 15.00 PM	44.80	8.90 15.00 15.00 PM	44.80
8.4 15.00 15.00 PM	45.50	8.81 15.00 15.00 PM	44.89	8.6 15.00 15.00 PM	45.1	8.3 15.00 15.00 PM	45.4	8.2 15.00 15.00 PM	45.5	6.5 15.00 15.00 PM	44.2	7.0 15.00 15.00 PM	46.7	7.1 15.00 15.00 PM	46.6

Red. 8/2/41 (W)
Checked 8/22/41 (W)
Plotted 8/25/41 (W)

1+0

0+93 - 8' Conc Drive on ht

0+65

H.F. Carb. Return

0+37 = opp C&C cont.

0+25 = E.L. Licta

53.70

St. N

pt. N

54

46.75	46.17	47.07	46.55	47.46	46.97	47.92	47.41	48.10	47.55
6.95 16.4	7.53 4.6	6.63 34.5	7.15 34.5	6.24 2.0	6.78 2.0	5.78 11.5	6.39 11.5	5.60 8.0	6.15 8.0
49.0	48.52	48.1	48.4	47.9	48.5	48.5	48.5	48.6	
4.7 2.5	5.8 15.0	5.6 10.0	5.3	5.8	5.2	5.2	5.2	5.2	
48.5	47.41	47.4	48.0	47.6	48.4	48.4	48.4	48.4	
5.4 2.4	6.39 10.0	6.39 10.0	5.7	6.1	5.2	5.2	5.2	5.2	
49.9	49.6	49.2	48.5	49.1	49.0	49.1	49.1	49.1	
3.8 1.5	4.1 1.5	4.6	5.1 1.0	4.6 1.2	4.9 1.5	4.6 1.2	4.9 1.5	4.6 1.2	
50.9	50.5	50.4	49.4	50.2	50.0	49.9	49.9	49.9	
2.8 2.5	2.2 2.5	2.5	2.5	2.5	2.5	2.5	2.5	2.5	
11.03	11.03	11.03	11.03	11.03	11.03	11.03	11.03	11.03	
26.7	24.8	24.8	24.8	24.8	24.8	24.8	24.8	24.8	
8.78	8.78	8.78	8.78	8.78	8.78	8.78	8.78	8.78	
Conc Drive	Conc Drive	Conc Drive	Conc Drive	Conc Drive	Conc Drive	Conc Drive	Conc Drive	Conc Drive	

53.70

3+80

3+75

3+50

H. E. Curb Return

3+30 = Opp CB EC 0724

7P 865 72.06 172 63.41

3+15 = E. L. Morozzi From South

65.13

68.00

4.06
65

60.74

11.32
44.77

72.1	70.9	69.9	69.0	68.5
20 25	12 18	22 15	20 10	20 6

67.79	69.1	68.6	68.1	67.7
427 31	250 15	25 15	40	101

68.0	67.6	66.8	66.3	66.2
4 25	45 15	53 10	58	59 10

60.19	61.18	60.56	61.62	61.03	62.00
1187 4472	1088 3334	1150 3334	1044 2736	1103 2206	1006 1119

65.6	62.49	62.7	63.4	63.9	64.3
65 25	957 11626	94 15	87 10	88	78 10

63.0	61.78	61.6	62.6	63.2	64.7
21 25	265 16-22	26 15	25	19	24 25

65.13

72.06

Cross Section Lido St
Tonopah St to Littlefield St.

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INDEXED

WK
JAN 18 1949

140

0750

BM

4.87

13.36

Mon 5/2
Tonopah St
N.W. 21070

0+0 = N.L. Tonopah

TP 2.26 48.23 6.08 45.97

TP 9.00 52.05 0.44 43.05

TP 11.61 43.49 0.49 31.88

TP 11.60 32.37 0.44 20.97

TP 11.03 21.21 0.73 10.18

BM 0.87 10.91 10.04

8 P.M. Cully
Mojave
Tecalate Creek

H.W

Rt. E

High 15.41
5/25/49
59
Horty
N. Moor

43.4

4.8
3.5

43.1

5.1
3.5

43.5

4.7
3.5

43.7

4.5
3.5

43.7

4.5
3.5

44.1

4.1
3.5

43.9

4.3
3.5

44.5

5.7
3.5

44.5

5.7
3.5

44.4

3.8

44.8

3.4

45.1

3.1

48.23

44.9

3.3
3.5

46.1

2.1
3.5

46.1

2.1
3.5

45.4

3.3
3.5

46.6

1.6
3.5

46.7

1.5
3.5

45.3

3.9
3.5

46.6

1.6
3.5

46.8

1.7
3.5

3795

3750

370

2750

270

1750

1823

73
25 40.9

78
25 40.4

88
25 40.1

92
25 40.9

95
25 42.1

95
25 42.4

74
25 40.8

76
25 40.6

78
25 40.4

80
25 41.4

80
25 42.2

85
25 42.8

75
25 40.7

76
25 40.6

77
25 40.5

84
25 41.8

85
25 42.7

89
25 43.3

73
25 40.9

74
25 40.8

76
25 40.6

80
25 41.9

85
25 42.8

89
25 43.3

68
25 41.4

69
25 41.3

72
25 41.0

81
25 41.9

82
25 43.0

87
25 43.5

62
25 42.0

65
25 41.7

66
25 41.6

85
25 42.7

85
25 43.0

88
25 43.9

60
25 42.2

65
25 41.7

66
25 41.6

85
25 42.8

85
25 42.6

88
25 44.0

1823

6+0

5+60

6+30

TP 8.61 51.63 5.21 43.02

5+0

4+50.12 = 11.6 Asber

4+00.12 = 5.6 Asber

18.23

38.1	39.0	39.4	40.2	41.0	41.8	42.4
$\frac{13}{10.5}$	$\frac{12.6}{2.5}$	$\frac{12.8}{1.5}$	11.1	$\frac{10.6}{1.5}$	$\frac{9.8}{2.5}$	$\frac{9.2}{2.5}$
37.6	39.2	40.2	41.7	42.6	43.4	44.0
$\frac{14.0}{1.0}$	$\frac{12.4}{2.5}$	$\frac{11.4}{1.5}$	9.9	$\frac{9.0}{1.5}$	$\frac{8.2}{2.5}$	$\frac{7.6}{2.5}$
40.5	41.9	42.8	43.9	44.8	45.6	45.8
$\frac{11.1}{2.5}$	$\frac{9.2}{2.5}$	$\frac{8.8}{1.5}$	7.7	$\frac{6.8}{1.5}$	$\frac{6.0}{2.5}$	$\frac{5.8}{2.5}$
42.0	42.4	43.0	43.8	44.6	45.1	45.6
$\frac{6.4}{2.5}$	$\frac{5.8}{2.5}$	$\frac{5.2}{1.5}$	4.1	$\frac{3.6}{1.5}$	$\frac{3.1}{2.5}$	$\frac{2.6}{2.5}$
40.9	41.6	41.8	42.7	43.3	43.6	
$\frac{7.2}{2.5}$	$\frac{6.6}{2.5}$	$\frac{6.4}{2.5}$	5.5	$\frac{4.9}{1.5}$	$\frac{4.6}{2.5}$	
40.9	41.5	41.9	42.6	42.9		
$\frac{7.2}{2.5}$	$\frac{6.7}{1.5}$	6.3	$\frac{5.6}{1.5}$	$\frac{5.3}{2.5}$		
			18.23			

4+61.02 = F.L. First Add to Ashers Clover Leaf Terr.

4+30

4+0

3+74.45 = F.L. Morcoci

3+49.45 = F.L. Morcoci

52.17

	42.9	42.4	42.5	35.5	34.4
	9.8 25	9.8 10	9.7	16.7	17.8 25
	44.7	44.2	44.4	44.4	34.5
	7.8 25	8.0	7.8	7.8	17.7 25
	46.0	45.8	45.8	45.8	34.2
	6.4 25	6.4	6.4	6.4	18.0 25
	46.9	46.3	46.4	46.4	34.2
	5.6 25	5.9	5.8	5.8	18.0 25
	47.2	46.7	46.8	46.8	33.2
	5.0 25	5.0	5.1	5.1	19.0 25
			52.17		

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WK
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2+50

2+0

1+50

1+0

0+50

0+0 = N.L. Topopah

52.17 B Ford

	St. 15	St. 16	St. 17	St. 18	St. 19
2+50	744.7 25	744.8 25	745.0 25	745.4 25	746.0 25
2+0	744.8 25	744.8 25	744.7 25	744.9 25	745.1 25
1+50	745.4 25	745.3 25	745.2 25	745.2 25	745.2 25
1+0	746.4 25	745.7 25	745.5 25	745.4 25	745.4 25
0+50	746.0 25	746.0 25	746.0 25	745.9 25	746.0 25
0+0 = N.L. Topopah	746.9 25	747.0 25	747.1 25	747.0 25	746.9 25

52.17

TP 686 67.85 0.90 60.99

7+50

7+0

6+50

6+0

5+50

5+0

61.89

~~68.9~~
58.0

~~70.0~~
54.9

~~68.2~~
53.7

~~67.5~~
54.4

~~68.8~~
54.1

~~68.0~~
52.8

~~68.5~~
58.7

~~68.6~~
55.3

~~67.6~~
54.3

~~67.1~~
55.1

~~67.2~~
54.5

~~68.8~~
53.1

~~68.8~~
59.1

~~67.1~~
55.8

~~67.8~~
54.6

~~67.6~~
55.6

~~67.2~~
54.7

~~67.4~~
53.5

~~67.6~~
59.4

~~65.6~~
56.6

~~67.7~~
55.2

~~65.6~~
56.3

~~68.0~~
55.1

~~67.9~~
54.0

~~67.0~~
59.9

~~65.0~~
56.9

~~67.8~~
55.8

~~65.0~~
56.9

~~67.3~~
55.7

~~68.0~~
53.9

RT

~~68.1~~
60.7

~~67.5~~
57.8

~~66.5~~
56.9

~~67.1~~
57.8

~~67.5~~
56.2

~~67.2~~
54.1

~~68.0~~
61.1

~~67.9~~
58.2

~~67.0~~
57.2

~~67.4~~
58.4

~~67.1~~
56.3

~~67.8~~
54.0

61.89

874

5.39

62.46

7.5
60.0
61.3
61.8

8 + 2561 = S.L. Littlefield

870

7795

67.85

9.0
65.0
58.9

7.5
72.5
60.4

6.6
65.6
61.3

6.1
66.1
61.8

7.1
67.1
63.5

8.5
73.5
64.4

9.0
65.0
58.9

7.9
72.9
60.0

7.7
72.7
60.7

6.7
66.7
61.2

5.5
65.5
62.3

4.6
64.6
63.3

3.3
63.3
64.6

9.8
69.8
58.1

8.8
68.8
59.1

7.7
67.7
60.2

6.9
66.9
61.0

6.1
66.1
61.7

5.1
65.1
62.8

4.0
64.0
62.9

67.85

4+61.23 = F.L. First Add to Asker Clover Leaf Terr.

4+30

4+0

5611

$\sqrt{2.0}$	$\sqrt{2.3}$	$\sqrt{2.3}$	$\sqrt{2.4}$	$\sqrt{2.0}$	$\sqrt{2.2}$	$\sqrt{2.2}$	$\sqrt{2.2}$	$\sqrt{2.2}$	$\sqrt{2.2}$
$\frac{1.1}{35}$	$\frac{1.8}{35}$	$\frac{1.9}{25}$	$\frac{1.7}{15}$	$\frac{1.9}{15}$	$\frac{1.9}{15}$	$\frac{1.8}{15}$	$\frac{1.9}{15}$	$\frac{1.9}{15}$	$\frac{1.4}{35}$
51.8	51.7	52.2	52.4	52.0	51.7	51.9	52.3	52.2	51.7
$\sqrt{4.3}$	$\sqrt{1.2}$	$\sqrt{1.2}$	$\sqrt{1.4}$	$\sqrt{1.2}$	$\sqrt{1.2}$	$\sqrt{1.5}$	$\sqrt{1.5}$	$\sqrt{1.7}$	$\sqrt{1.4}$
$\frac{1.8}{35}$	$\frac{1.2}{19}$	$\frac{1.2}{15}$	$\frac{1.4}{15}$	$\frac{1.2}{19}$	$\frac{1.2}{15}$	$\frac{1.2}{15}$	$\frac{1.5}{15}$	$\frac{1.7}{15}$	$\frac{1.4}{35}$
54.3	51.2	50.8	50.9	51.2	51.2	51.5	52.3	51.7	51.4
5611									

Cross Section #11 by Block 16
 First Addition to Fishers Clover Leaf Terrace
 From Topopah St to Fisher St

BM	7.22	50.58	43.36	Mon. S. h. Topopah St #112 2100
		0+0 = H.L. Topopah		
-10		3.1	47.5	
H		3.2	47.4	
L		3.4	47.2	
F		3.4	47.2	
+10		3.6	47.0	
		0+50		
-10		3.6	47.0	
F		3.7	46.9	
L		3.6	47.0	
H		3.8	46.8	(M)
+10		3.8	46.8	
		1+0		
-10		4.9	45.7	
H		4.8	45.8	
L		4.6	46.0	
F		4.6	46.0	
+10		4.5	46.1	
		1+50		
-10		5.5	45.1	
F		5.6	45.0	
L		5.2	45.4	
H		5.6	45.0	
+10		5.7	44.9	

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 WIK
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Aug-16-41 **73**

Sketch Page 5058			
	2+0		
-10		6.7	43.9
H		6.8	43.8
L		6.5	44.1
F		6.7	43.9
+10		6.6	44.0
	2+50		
-10		7.0	43.6
F		7.5	43.1
L		7.2	43.4
H		7.5	43.1
+10		7.6	43.0
	3+0		
-10		7.5	43.1
H		7.4	43.2
L		7.1	43.5
F		6.8	43.8
+10		6.7	43.9
	3+50		
-10		5.4	45.2
F		6.5	44.1
L		6.5	44.1
H		6.7	43.9
+10		6.9	43.7

5058

3765

-10	6.2	44.4
X	5.5	45.1
2	5.2	45.4
F	4.8	45.8
+10	5.2	45.4

3780

-10	5.1	45.5
F	5.5	45.1
2	5.6	45.0
X	5.6	45.0
+10	5.7	44.9

4+00.81 = 52.85605

-10	4.9	46.2
X	4.0	46.6
2	3.6	47.0
F	4.0	46.6
+10	3.4	47.2

Cross Section Alley Block 13
 First Addition to Ashers Clover Leaf Terr.
 Asher St to Hillfield St. Sketch page 52

50.58 at Ford

070 = N.L. Asher St.

-10		18	48.8
F		21	48.5
g		23	48.3
H		23	48.3
+10		22	48.4

INDEXED

WK

JAN 18 1949

0750

-10		0.8	49.8	
H		0.6	50.0	
g		0.4	50.2	
F		0.7	49.9	
+10		0.5	50.1	
IP	5.88	<u>56.03</u>	0.43	50.15

0775

-10		4.5	51.5
F		4.5	51.5
g		4.8	51.2
H		5.0	51.0
+10		5.3	50.7

170

-10		4.4	51.6
H		3.8	52.2
g		3.8	52.2
F		3.7	52.3
+10		4.0	52.0

Plotted 8-22-41

56.03

1725

-10		4.0	52.0
F		3.9	52.1
g		4.1	51.9
H		4.1	51.9
+10		4.2	51.8

1750

-10		5.5	50.5
H		5.1	50.9
g		4.7	51.3
F		4.2	51.8
+10		4.0	52.0

1775

-10		4.5	51.5
F		4.8	51.2
g		5.3	50.7
H		6.0	50.0
+10		6.7	49.3

270

-10		7.0	49.0
H		6.1	49.6
g		6.0	50.0
F		5.6	50.4
+10		4.9	51.1

Red. - 8.22.41 (W)
 Checked - " "

56.03

2+50

-10	4.9	51.1
F	5.2	50.8
2	5.5	50.5
W	5.6	50.4
+10	5.9	50.1

2+0

-10	6.0	50.0
W	5.6	50.4
2	5.5	50.5
F	5.2	50.8
+10	4.3	51.7

2+50

-10	4.5	51.5
F	4.6	51.4
2	4.9	51.1
W	5.1	50.9
+10	5.2	50.8

3+75.22 = St. Littlefield

-10	5.5	50.5
W	5.2	50.8
2	4.6	51.4
F	4.5	51.5
+10	4.1	51.9
BM	9.32	46.71

N.E. B.P.
 Littlefield
 + Denver
 46.71

2 Levels Fisher St.
 W.L. First Add to Fishers Clover Leaf Terrace
 to 250 West

Sept 2-4
 76
 S.W. 500

BM	2.52	<u>52.55</u>	50.03	
TP	0.54	<u>42.98</u>	10.11	42.44
0+0	W.L. First Add to Fishers Clover Leaf Terr	3.9	39.1	
+50		5.7	37.3	
1+0		7.8	35.2	
+50		10.0	33.0	
2+0		11.8	31.2	
+50		13.4	29.6	

092 Hub
 Fisher
 750
 Page 87

2 Levels Fisher St

F.L. First Add to Fishers Clover Leaf Terr to 250 West

BM	7.07	<u>57.10</u>	50.03
0+0	F.L. First Add to Fishers Clover Leaf Terr	5.0	52.1
+50		5.0	52.1
1+0		5.4	51.7
+50		5.8	51.3
2+0		5.3	51.8
+50		4.7	52.4

092 Hub
 Fisher
 Moreland
 Page 87

Red. 9/2/41
 chk. " (W)
 Plotted "

2 = P.L. Line Levels Tonopah St
 F.L. First Add to Ashers Clover Leaf Terr.
 to 250' East

BM	8.39	51.75		43.36	Mon 5-1 Tonopah 8 1/2 mi W of PSP
	F.L. First Add. to				
0+0 =	Ashers Clover Leaf	9.5			
TP	1.59	41.49	11.85	39.90	
+50			4.1	37.8	
+10			8.4	33.1	
+50			11.9	29.6	
TP	3.09	32.88	11.70	29.79	
+10			6.0	26.9	
+50			9.6	23.3	

2 = P.L. Line Levels Tonopah St
 F.L. First Add to Ashers Clover Leaf Terr. **77**
 to 250' West

BM	3.38	46.74		43.36	Mon 5-1 Tonopah 8 1/2 mi W of PSP
	F.L. First Add. to				
0+0 =	Ashers Clover Leaf	3.4		43.3	
+50			5.0	41.7	
+10			5.8	40.9	
+50			6.5	40.2	
+10			6.9	39.8	
+50			7.0	39.7	

Location + Levels on Sewer Laterals on East
 Side Alley Block 38 City Hts. Between 38th & 39th Sts
 From University to Park

BM	4.48	351.72	347.24	NW 8P 421.1396
	0+05.5 =	55' 11" of H.L. down		
EL + 5'	Top 4" Viff. Sewer Lat.	5.85	345.87	
" "	Ground	3.8	347.9	
TP	8.75	359.72	0.75	350.97
	0+63			
EL + 5'	Top 4" Viff. Sewer Lat.	10.65	349.07	
" "	Ground	8.4	351.3	
	1+32			
EL + 5'	Top 4" Viff. Sewer Lat.	10.71	349.01	
" "	Ground	7.0	352.7	
	1+59			
EL + 5'	Top 4" Viff. Sewer Lat.	8.88	350.84	
" "	Ground	6.7	353.0	
	2+43.5			
EL + 5'	Top 4" Viff. Sewer Lat.	7.52	352.20	
" "	Ground	4.5	355.7	
	3+31			
EL + 5'	Top 4" Viff. Sewer Lat.	5.95	353.77	
" "	Ground	3.7	356.0	
	3+82			
EL + 5'	Top 4" Viff. Sewer Lat.	4.92	354.80	
" "	Ground	3.2	356.5	
	4+73			
EL + 5'	Top 4" Viff. Sewer Lat.	5.60	354.12	
" "	Ground	3.5	357.7	

Profile = 2.891' - 5.01'

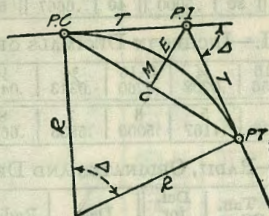
Oct. 13-43
 Sisson 8099
 Bliss 35972

Indexed
 e.s.k.

	5+76			
EL + 5'	Top 4" Viff. Sewer Lateral	4.62		355.10
" "	Ground	1.3		358.4
TP	1.57	351.70	9.59	350.13
BM	4.44	347.26		NW 8P 421.1396 347.31

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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CURVE FORMULAS

Radius= $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve= D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)

Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)

Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2})$ (5) $= R \text{vers} \frac{\Delta}{2}$ (6)

External= $E = T \tan \frac{\Delta}{4}$ (7) $= R + \cos \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)

Long Chord= $C = 2 R \sin \frac{\Delta}{2}$ (10) Δ =Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta=62^\circ 10'$ $D=8^\circ 20'$. From Table IV for 1° curve $T=3454.1$ and $\div 8\frac{1}{3}=414.49$ ft. From Table V correction=.36 or $T=414.85$ ft. P. C.=Sta. P.I.— $T=157+45.50$. Also from (4) $L=746.00$ and P. T.=Sta. P. C. + $L=164+91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset= $7.27 \frac{54.50}{100}=2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26)=2.16$ ft.

Deflections.—Deflection angle= $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft.=(in minutes) $.3 \times C \times D^\circ$ or=defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve=.3 $\times 54.5 \times 8\frac{1}{3}=136.2'$ or $2^\circ 16.2'$, or= $2.50 \times 54.5=136.2'$ from Table III. For Sta. 159 deflection angle= $2^\circ 16.2' + 8^\circ 20' \div 2=6^\circ 28.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve $E=960.6$ for $8^\circ 20'=960.6 \div 8\frac{1}{3}=91.27$ and from Table V correction=.10 or $E=91.37$ ft. Or suppose $\Delta=32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E=230.9$ and $\div 42=5.5$ or $D=5^\circ 30'$.

50

372.00
486
567.45

760
204
486

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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