

1603

DIETZGEN

ENGINEERS
FIELD OFFICE
N. A. C. E.

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.

Copyright, 1914, by Eugene Dietzgen Co.

1603

S.E.B.P. San Francisco

Pl. - 0.600

400' N.N.W. S.F.P. 200' E.C. 8.P. + 0.631

P.S. 514

CITY ENGINEER'S OFFICE

The paper stock of this book is made of a high grade 50% rag paper having a water resisting surface and is sewed with Bing Special Enamel Waterproof Thread.

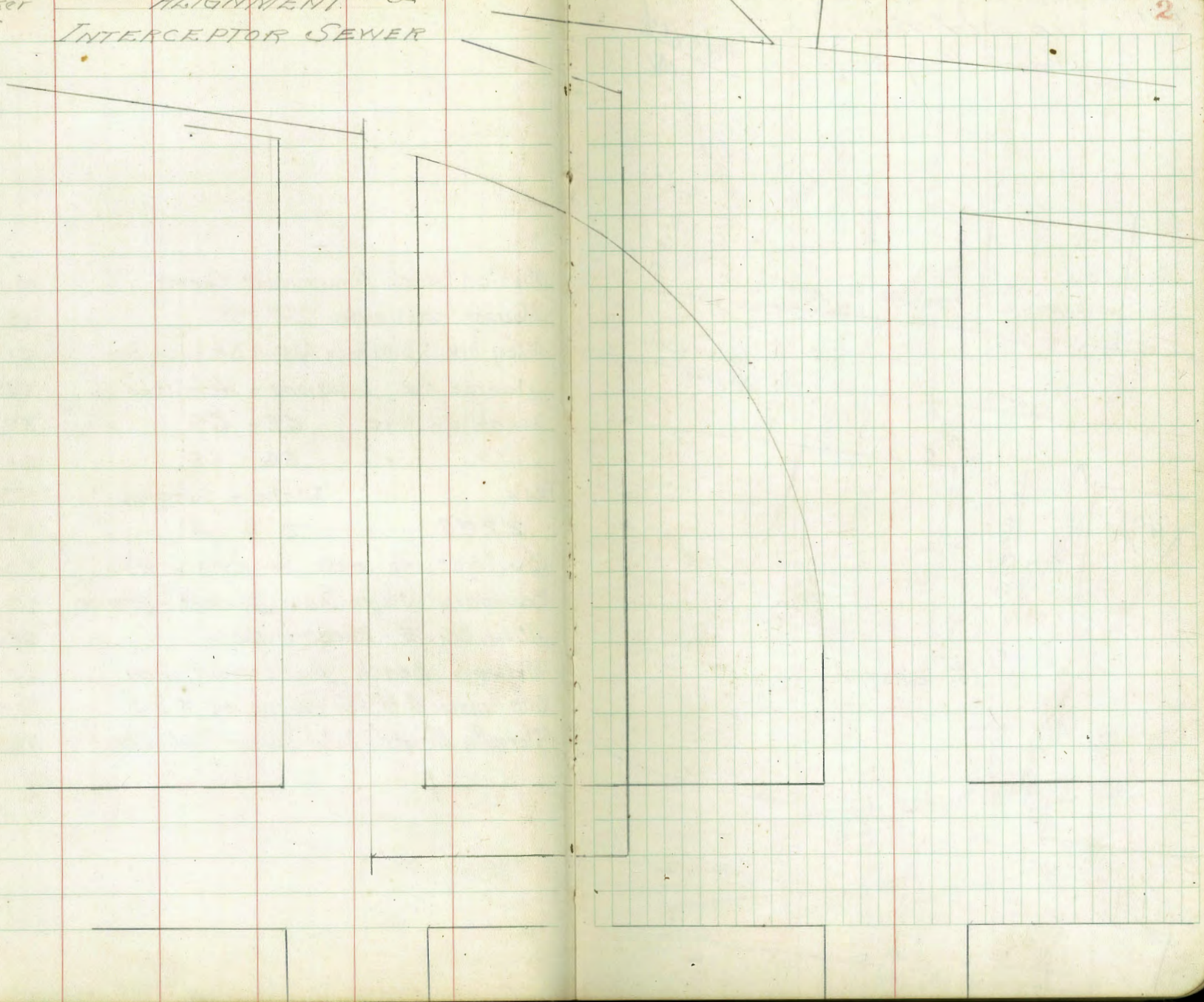
Made in U. S. A.

Mission Beach Amusement Center	10 - 17
Houses east side 6 th St.	18 - 20
Alley Blk. 5 Bird Rock Add - 11 B.R. by the Sea	21 - 25
Monroe Ave Louisiana - Hamilton	26 - 34
Brooklyn Ave 65 - 69	35 - 50
✓ ✓ 66 - 65	51 - 55
Park Idaho - Oregon	56 - 56
22ND B - A	57 - 59
Dwight cb levels Granada - 29	60 - 61
Boundary storm Drain Bancroft - Orange	62 - 63
Alley Blk. 5 Reed & Hubbell	64 - 68
Mission Beach Amusement Area	69 - 72
San Antonio & McCall Intersection - X-Sect.	73 - 75
Glorietta Heights Subdivision - Field Check	76

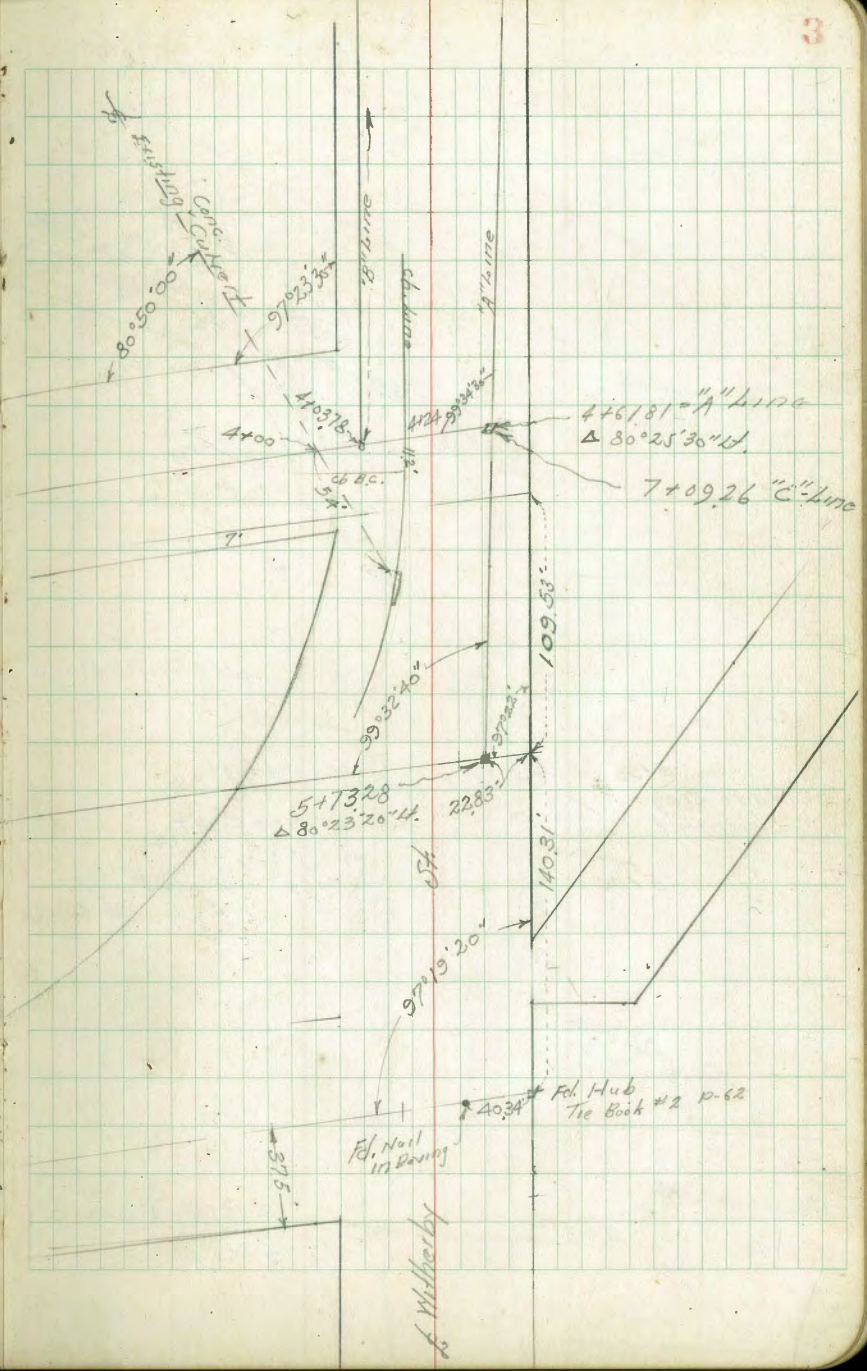
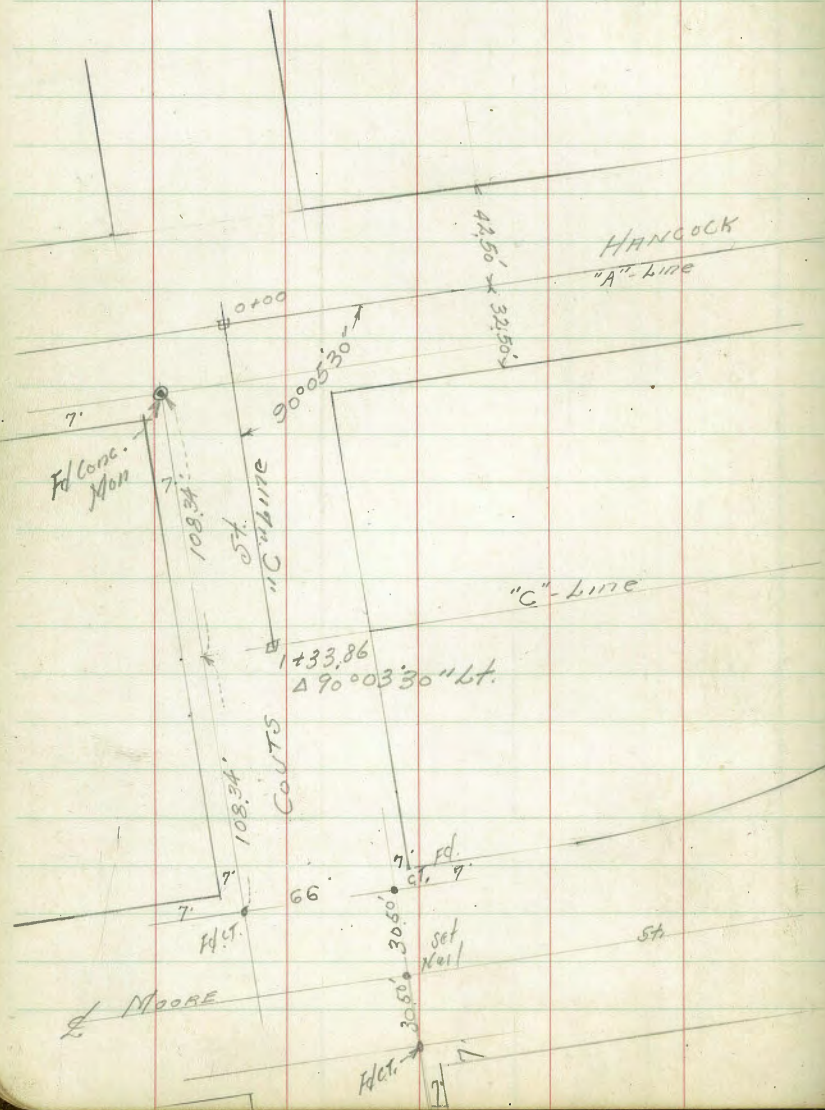
Walker
Bliss

ALIGNMENT
INTERCEPTOR SEWER

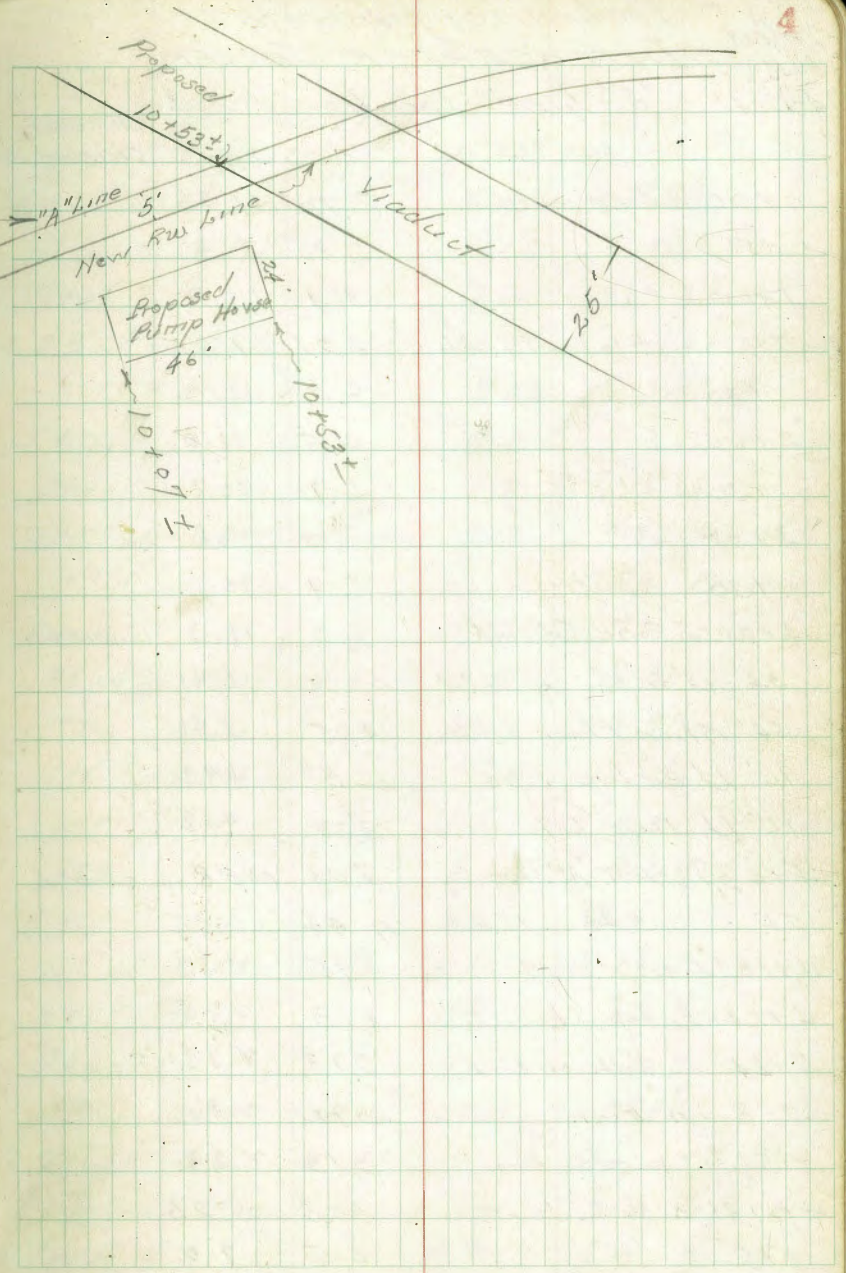
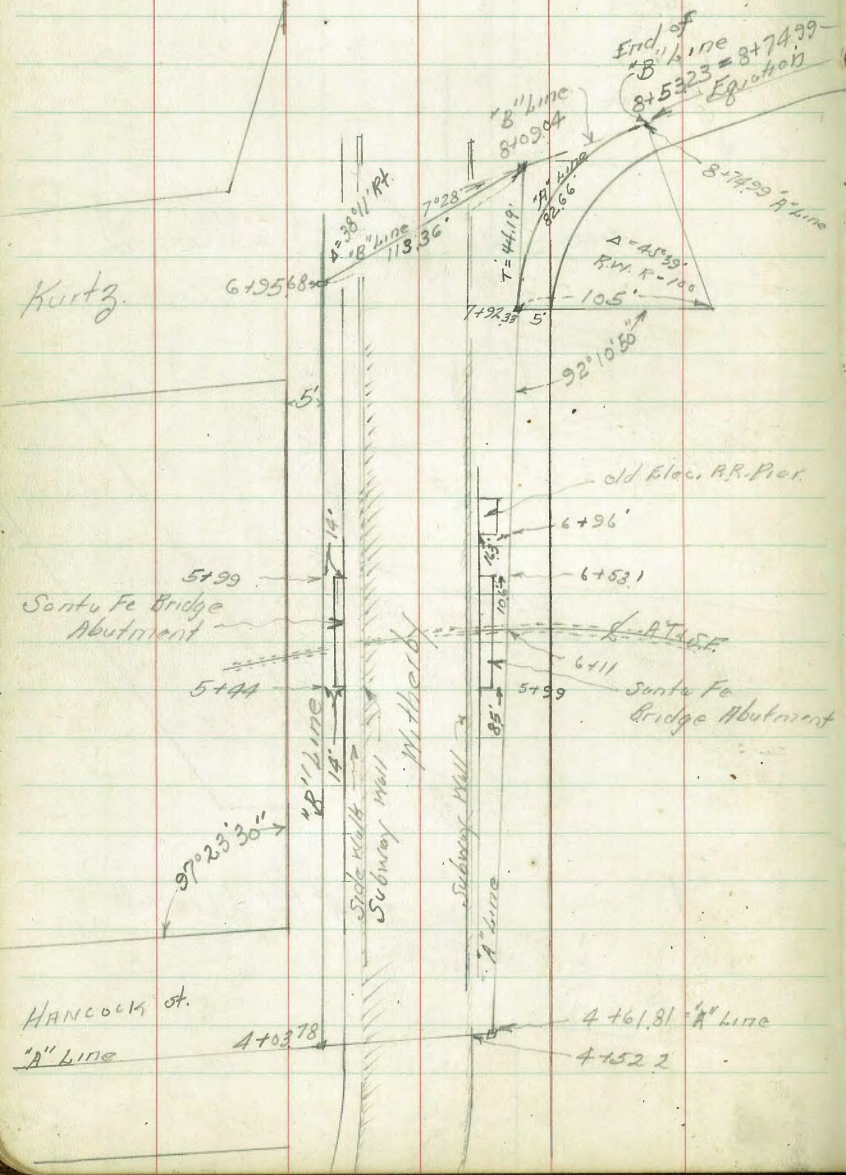
2



Walker
Bliss
INTERCEPTOR SEWER
IN Old TOWN
Levels P-5-8
Indexed
LM



Kurtz.



Walker - Preliminary Levels -
Bliss INTERCEPTOR SEWER

Station	11.55	14.06	2.51	B.M. State Chisled square
0+00 "A" line on stub.	2.70	11.36		
+50	2.85	11.3		
1+00	3.1	11.0		
T.P. 5.61 17.46	2.21	11.85		
+50	6.3	11.2		
2+00	6.5	11.0		
+50	6.7	10.8		
3+00	7.0	10.5		
+50	6.7	10.8		
4+00 2' Conc. Culvert	6.2	11.3		Ground
54' Rt. on cb over Inlet.	10.05	7.41		
54' Rt. on Floor 30" Apo	14.05	3.41		
96' Lt. on top Pipe	12.53	4.93		
96' Lt. Floor, Curb.	13.28	4.18		
4+03.78 = P.O.T. "A" line	7.08	10.38		on stub.
T.P. 5.46 11.48	11.44	6.02		
4+18 = Edge Walk	8.75	7.73		
4+24 = E. top cb	8.73	7.75		
4+24 = E. Gut. on Pav.	9.13	7.35		
+38 on Pav.	9.02	7.46		
752.2 = Wedge Pav.	9.19	7.29		
4+61.81 = Δ 80° 25' 30" Lt.	5.23	6.25		
+75	4.5	7.0		
+85	7.1	4.4		

Station	8.94	2.54
(4+72) 10' Lt. on Nchd	8.94	2.54
" " " " Pav.	10.11	1.37
5+00	7.2	4.3
9.3' Lt. on Wall	12.50	-1.02
" " " Pav.	9.02	2.46
5+50	8.2	3.3
5+90	7.7	3.8
12.5' Lt. = Subwoy Wall Face	9.02	2.46 top Wall
" " on Pav.	13.07	-7.59 Paving
6+00	4.3	-7.2
8.5' Lt. on Abutment	3.17	8.31
6+06	1.6	9.9
78.6' = H&Y Rail	9.74	10.74
6+15	1.2	10.3
+23	3.7	7.8
6+53	3.0	8.5
10.6' Lt. on Wall Abut.	3.20	8.28
6+75	4.2	7.3
7+00	5.7	5.8
T.P. 2.18 9.86	3.80	7.68
(6+61.8 = Elec. Pole 1.8' Rt 1.6' dia.)		
(7+00) 16.3' Lt. on Abutment	2.6	7.3
7+20 E	4.7	5.2
17' Lt. on Wall Subwoy	7.46	2.40
17' " " Pav.	14.46	-4.60

	9.86				
(7+20 cont.)	23.5 RT	7.4	2.5	Apparant Floor Hummer	House Consolidated Air
7+50		5.7	4.2		
7+92.33 ± = B.C. Pt.		6.5	3.4	R. Proposed Pipe = 10.5'	
18' Lt. on Subway Wall		7.43	7.43		
18' Lt. " " Por		11.40	1.54	at Wall	
8+00		6.5	3.4		
+50		7.2	2.7		
+74.99 = EC		7.0	2.9		
37' Lt. NWY edge Por.		8.59	1.27	Radius to Next R.W.	
9+00		6.3	3.6		
+50		5.7	4.2		
9+65		7.7	2.2		
10+00		8.1	1.8		
TR	8.58	9.33	2.11	0.75	
	10+07 ± = NWY edge	Proposed Pump House			
71' Lt. on NWY edge Por.		8.31	1.02		
50' Lt.		8.0	1.3		
L		7.7	1.6		
25' RT		7.6	1.7		
50' RT		7.3	2.0		
	10+53 ± = NWY edge	Proposed Pump House			
50' RT		8.0	1.3		
25' RT		8.3	1.0		
L		8.3	1.0		
50' Lt.		8.1	1.2		
72' Lt. on NWY edge Por.		8.59	0.74		

House Consolidated Air

9.33

chk. BP 511.

8.29

1.04
1.01 - State Highway
0.03

NWY Cot. Witherb Pacific

South NWY end Subway Wall
chk. Brass Plug

6.86

2.47

Bot. Hunoody to Pacific

Elev. " " = ?

Walker. Preliminary Levels.
Bliss INTERCEPTOR JEWEL "B" LINE
4-21-41 Location P-4

	3.27	13.65	10.38	H. Stake 410378 P.5
4+0378 1/2" line				
= 4+0378 "B" line = this line	3.27	10.38		on Hub.
4+24 = opposite NLY end Subway Wall				
13.5' Rt. on Wall	11.30	2.35		
13.5' Rt. on Walk.	12.33	1.32		
19.5' Rt. on cb.	12.38	1.27		
19.5' Rt. " Paving,	12.98	0.67		
6' Rt.	3.6	10.1		
L	3.6	10.1		
4+33	4.3	9.4		
10.5' Lt. Eloc Pole	4.3	9.4		
4+50	6.3	7.4		
9' Rt.	7.0	7.7		
5+00	9.5	4.2		
14.0' Rt. on Wall Subcarp,	11.18	2.47		
14' Rt. on Walk.	14.83	-1.18		
20' Rt. " cb.	14.86	-1.21		
20' Rt. " Paving.	18.38	-4.73		
5+34 Toe Limb. AT&SF.	9.8	3.9		
14' Rt. on Wall	11.16	2.49		
14' " " Walk.	15.81	-2.16		
20' Rt. on cb.	15.87	-2.22		
20' Rt. " Paving.	21.17	-7.52		

13.65

(5+25) 8.5' Lt. = Eloc Pole			
" 4' Rt. = Deadmans.			
" 7' " = " "			
5+44 = NLY edge AT&SF Abutment.			
10' Rt. on ELY edge Wall	5.36	8.29	
14' Rt. " WLY " "	5.36	8.29	
5+45 = Signal Post.	4.2	9.5	Conc. Base
4.7' Rt. = " " "	2.49	11.16	
5+55.08 = NLY Rail Santa Fe	2.98	10.67	
5+66 = Upright Switch	3.5	10.2	
2' Lt. " " "	3.0	10.7	
5+71 = Signal Post	4.3	9.4	
2.5' Rt. on " "	2.3	11.4	Conc. Base
5+80	8.6	5.1	Santa Fe.
5+99 = SLY end Abutment	9.6	4.1	
8.5' Rt. on Ground at Wall	9.6	4.1	
9' Rt. " Wall ELY edge	5.41	8.24	
14' Rt. " " WLY " "	5.41	8.24	
6+08 = Toe Santa Fe Wall = Top Subway Wall			
14' Rt. = WLY edge Wall	11.19	2.46	
14' Rt. on Walk.	15.84	-2.19	
20' Rt. " cb.	15.86	-2.21	
20' Rt. " Paving	21.15	-7.50	
(6+22) 3.5' Rt. = ELY edge on Ground	10.5	3.2	ELY edge Eloc. RR Pier
(6+34) 3.9' Rt. " " "	10.2	3.5	Conc. Pier Ground.
6+50	9.0	4.7	

*
13.65

6+95.68 = Δ 38° 11' Rt	9.43	9.43	4.22
14' Rt. on Wall	11.22	11.22	2.43
14' Rt. " Walk	13.97	13.97	-0.32
20' Rt. on cb	14.06	14.06	-0.41
20' Rt. " Pav.	16.96	16.96	-3.31
(7+14) Tel Pole 3.0' Lt.	10.8	10.8	2.9
(7+16) Tel. 14 ft. 9.5' Lt.	10.80	10.80	2.9
7+19.2 on Wall	11.22	11.22	2.43
7+19.2 " Walk	13.57	13.57	0.08
7+29.4 on cb	13.97	13.97	0.18
7+29.4 " Pav.ing	15.72	15.72	-2.07
7+55.4 = 2' "	14.95	14.95	-1.30
7+85.8 = Wht edge Dring	13.87	13.87	-0.22 at wall
7+85.8 on West Wall	11.17	11.17	2.48 Subing
8+09.04 = Δ 7° 28' Rt.	10.97	10.97	2.68
8+53.23 " B" line = End.	10.7	10.7	3.0
-8+74.99 " A" line			
chk. BR end Wall on W	11.18	11.18	2.47 P-6
			2.47
			60.0

Walker. Preliminary Levels.

8155

5-21-41 Interceptor Sewer "C" Line

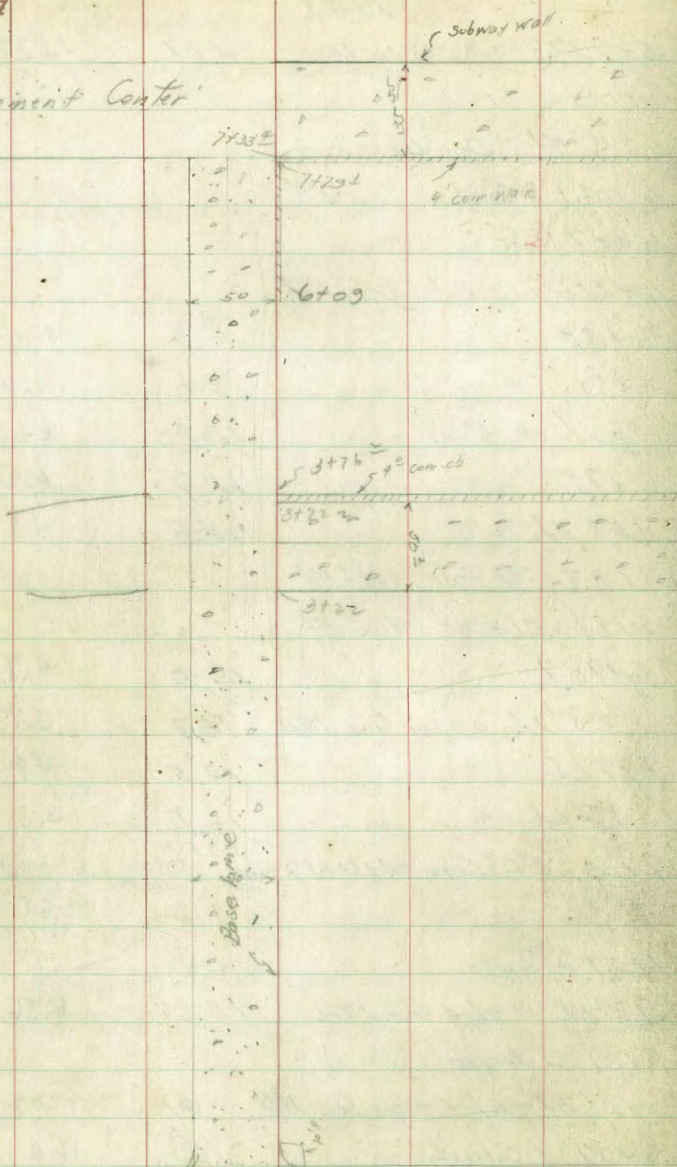
Location 19-3

	11.91	23.27	11.36	El. Hub 0+00 "A" Line P.S.
0+00 "A" Line = 0+00 "C" Line = this line	11.91	23.27	11.36	on stub
+50	9.5	13.8		
0+82	7.1	16.2		
+88	4.6	18.7		
1+08	5.8	17.5		
+33.86 = $\Delta 90^{\circ}03'30''$ Lt.	4.87	18.45		(Lobby) on stake
1+50	4.9	18.4		
2+00	5.0	18.3		
2+50	5.3	18.9		
3+00	5.3	18.0		
+50	5.3	18.0		
4+00	6.2	17.1		
+50	5.8	17.5		
+85	6.2	17.1		
+89 = ELY edge Walk.	7.87	15.40		
4+97.5 = " cb.	8.25	15.02		
T.P.	4.29	19.43	8.13	15.14
4+97.5 = ELY Gut. Parking	4.88	14.55		
5+14.5 on Pav.	4.79	14.64		
+29 " W edge Pav.	5.71	13.72		
5+35	6.3	13.1		
+42	3.0	16.1		
+50	3.6	15.8		

1943

5+73.28 = $\Delta 80^{\circ}23'20''$ Lt.	4.11	15.32	
6+00	5.6	13.8	
8.5' Rt. - Deadwater			
(6+06) 8.5' Rt. "			
(6+07) 8.5' " "			
(6+21) Guy Pole 8.5' Rt.			
6+35	6.8	12.6	
+50	8.4	11.0	
16' Lt. on Pav.	12.80	6.63	
6+75	12.9	6.5	
12.5' Lt. " "	14.6	4.8	
6+83 = Tel Pole = 11' Rt.			
6+87 = Elec " 11.5' Rt.			
6+90.7	14.5	4.9	
2.5' Lt. on Cor Gas MH	15.7	3.7	WLY edge
6+97.5	14.5	4.9	
3.5' Lt. " " " "	16.1	3.3	" "
7+09.26 "C" Line = 4+61.81 "A" Line	13.17	6.26	
		6.25 = Stake P.S.	on 1st 51101.
(4+87) "A" Line			
9.8' Rt. W edge Gas MH	12.87	6.56	
6+91 "C" Line			
11' Rt. = ELY edge Gas MH	9.41	10.02	3.8' x 3.8'
6+37 = 2' Cutvert.	7.4	12.0	
7' Lt. = 2' Cleanout Box	10.19	9.24	2.5' x 2.5'
13' Lt. Floor Line	16.0	3.4	at cb.

Amusement Center



San Fernando Place 18+2

Sketch of Ground layout between
N. Line San Fernando Place and So
Line Amusement Center Mission Beach.
W. Line Mission Blvd. and Pavement West



Area between base line and X-ray

0+00 to 3+00	48640
3+76 to 6+29	21854
sq. ft.	70496

To surface above areas with
6" of material will require
1305 cu yds dirt.
HW 3-16-42

Bliss
Sommer Meyer
G. Farrow
7116741
BM.

	t	π	-	Elev	SEBP
	7.69	7.09		-0.60	500 Farnside Place & Mission Blvd
0400 Paving			6.59	0.50	
10' East			6.61	0.48	
" " Topcb			6.08	1.01	
25' " Paving			6.65	0.44	
" " Topcb			6.12	0.97	
50' " Paving			6.74	0.35	
50' " Topcb			6.20	0.89	
50' " 10' North			6.2	0.9	
75' " Paving			6.81	0.28	
" " Topcb			6.30	0.79	
" " 10' North			6.2	0.9	
100' " Paving			6.95	0.14	
" " Topcb			6.40	0.69	
125' East Paving			6.99	0.10	
" " Topcb			6.96	0.63	
150' " Paving			7.05	0.04	
" " Topcb			6.52	0.57	
" " 10' North			6.5	0.6	
175' " Paving			7.08	0.01	
" " Topcb			6.76	0.33	
185' East W-Gutter Mission Blvd			7.64	-0.55	
		0725			
0725			6.55	0.54	
" 25' East			5.7	0.4	

Plotted on Sta. Kees paper.
7-18-1940 - C.B.H.

7.09

11

50' East	5.3	1.8
75' "	5.8	1.3
100' "	6.6	0.5
125' "	6.3	0.8
150' "	5.3	1.8
" " 9' South	5.3	1.8
" " 5 North	5.1	2.0
" " 10 "	3.4	3.7
168' East	4.8	2.3
172' "	6.1	1.0
176' " Edge Walk	6.75	0.34
186' " Topcb	7.00	0.09
" " Gutter	7.56	-0.47
	0750	
0400	6.55	0.54
15' East	5.1	2.0
25' "	5.4	1.7
50' "	4.4	2.7
50' " 3' North	3.8	3.3
75' "	4.9	2.2
" " 8 North	4.0	3.1
100' "	5.6	1.5
125' "	4.6	2.5
150' "	4.1	3.0
156' "	3.1	4.0
156' " 10' North	4.1	3.0

0+50

170 East	4.7	2.4
" " 5 North	5.1	2.0
178.75 East Edge Walk	6.69	0.40
188.75 " Topcb	6.96	0.13
" " Gutter	7.55	-0.46

0+75

0+00 Paving	6.52	0.57
25 East	5.2	1.9
50 "	3.7	3.4
75 "	3.9	3.2
81 "	3.3	3.8
100 "	4.1	3.0
" " 10 South	4.4	2.7
" " 10 North	3.5	3.6
115 "	3.8	3.3
125 "	4.5	2.6
" " 15 North	4.3	2.8
150 "	4.5	2.6
" " 10 North	5.6	1.5
162 "	6.0	1.1
180.90 " Edge Walk	6.69	0.40
130.90 " Topcb	6.94	0.15
" " Gutter	7.50	-0.41
T.P.	6.28 6.46 6.91	0.18

1700

0+00	5.84	0.62
" 8' East	4.7	1.8
25 "	4.7	1.8
50 "	4.7	1.8
75 "	3.2	3.3
83 "	2.3	4.2
100 "	1.7	4.8
125 "	4.6	1.9
150 "	5.3	1.2
181.2 " Edge Walk	6.04	0.42
120.6 " Topcb	6.30	0.16
" " Gutter	6.85	-0.39

1+25

0+00	5.70	0.67
10' East	4.5	2.0
35 "	4.4	2.1
54 "	1.5	5.0
75 "	1.9	4.6
82 "	3.0	3.5
100 "	4.0	2.5
125 "	4.7	1.8
150 "	5.7	0.8
177.7 Edge Walk	6.03	0.43
188 " Topcb	6.24	0.42
" " Gutter	6.90	-0.44

7
646

150

Paving	5.73	0.73
15' East	5.0	1.5
35 "	3.0	3.5
50 "	1.5	5.0
62 "	1.7	4.8
75 "	3.1	3.4
85 "	5.1	1.4
90 "	5.1	1.4
100 "	3.6	2.9
100 " 6 North	3.5	3.0
125 "	4.6	1.9
150 "	5.2	1.1
169.6 " Edge walk	5.93	0.53
180.2 Topcb	6.17	0.39
" " Gutter	6.80	-0.34

175

Paving	5.72	0.74
Ground area	5.1	1.4
25' East	4.6	1.9
30 "	3.6	2.9
45 "	3.5	3.0
" " 7 South	2.6	3.9
50 "	2.6	3.9
68 "	2.5	4.0
73 "	4.0	2.5

7
646

13

175

100 East	5.9	0.6
" " 10 South	5.5	1.0
" " 10 North	4.4	2.1
110 "	5.3	1.2
120 "	4.3	2.2
150 "	5.1	1.4
156.2 Edge walk	5.92	0.68
168 " Topcb	6.15	0.31
" " "	6.78	-0.32
2400		
otro paving	5.68	0.78
" Ground	4.6	1.9
30 East	4.7	1.8
40 "	3.2	3.3
58 "	3.6	2.9
" " 7 South	2.4	4.1
75 "	5.2	1.3
" " 5 South	5.2	1.3
100 "	4.7	1.8
" " 10' North	4.2	2.3
125 "	5.2	1.8
146.2 Edge walk	5.88	0.58
151.2 Topcb	6.05	0.31
" " " Gutter	6.60	-0.14

T
646
2+25

0+00 8' West	5.5	1.0
0+00 Paving figured	5.74	0.72
0+00 Ground	3.8	2.7
30' East	4.0	2.5
50 "	3.9	2.6
85 "	5.0	1.5
85 " 9' South	3.9	2.6
90 "	4.2	2.3
100 "	4.4	2.1
120 "	5.3	1.2
127 ⁰ " Edge Walk	5.90	0.56
138 ⁺ " Top cb	6.03	0.43
" Gutter	6.52	-0.06

2+50

0+00 paving	5.61	0.85
0+00 Ground	4.9	1.6
10' East	4.0	2.5
25 "	4.3	2.3
50 "	4.7	1.8
75 "	4.7	1.8
85 "	3.9	2.6
93 "	4.0	2.5
100 "	4.7	1.8
" " 5' North	5.0	1.5
" " 10 "	4.4	2.1

T
646

14

117 East Edge Walk	5.83	0.63
127 ⁵⁺ Top cb	5.99	0.47
" Gutter	6.48	-0.02

2+83

0+00 paving	5.59	0.87
" 6' West	5.5	1.0
" 6 " 6' North	3.0	3.5
0+00 6' North	3.1	3.4
10' East	4.5	2.0
25 "	4.7	1.8
50 "	5.0	1.5
75 "	4.9	1.6
82 "	4.6	1.9
85 "	5.4	1.1
100 "	5.9	0.6
106 " Edge Walk	5.62	0.84
116 ⁵⁺ Top cb	5.92	0.54
" " " Gutter	6.38	0.08

3+06

0+00 paving figured	5.62	0.84
0+00 Ground	2.6	3.9
" 6' West	5.1	1.4
" 8' North	5.1	1.4
18 East	4.2	2.3
50 "	5.0	1.5

75' East	4.8	1.7
90 "	5.2	1.3
100 "	5.7	0.8
101 Edge of Walk	5.56	0.90
111.5 Top cb	5.78	0.68
" " Gutter	6.31	0.15

3+72 S Edge Paving. See sketch

0+00	5.50	0.96		
50' East	5.71	0.75		
" " 5' South	5.1	1.4		
75 "	5.78	0.68		
" " 5' South	5.3	1.2		
97.5 Top cb	5.30	1.16		
" " Gutter	5.87	0.59		
T.P.	4.69	6.20	4.95	1.51

3+72 ² N. Edge Paving. See sketch

0+00	5.24	0.96
0+00 4' N. Edge Com cb	4.85	1.35
35' East	5.25	0.95
" 4' North Com cb	4.89	0.31
70' East	5.41	0.79
" 4' North	4.88	1.32
89.5 Int. Com cb + Com Sidewalk	4.98	1.22
94.5 East Edge Walk + Top cb	5.19	1.01
" " Gutter See sketch	5.50	0.70
104.5 W Gutter Missed Blvd	6.03	0.17

3+85

0+00 on Paving	5.18	1.02
7' East	4.6	1.6
20 "	5.3	0.9
50 "	5.3	0.9
75 "	5.5	0.7
89. "	5.6	0.6
89.5 " Edge Com Sidewalk	4.93	1.27
94.5 " Edge Red. Top Walk	5.28	0.92
104.5 Top cb	5.50	0.70
104.5 " Gutter	5.98	0.23

4+25

0+00 Edge Paving	5.10	1.10		
25' East	5.00	1.20		
50 "	5.00	1.20		
89 Ground	5.0	1.2		
89.5 Edge Com Walk	4.88	1.32		
94.5 " Red "	5.22	0.98		
T.P.	5.14	6.99	4.85	1.35

4+75

0+00 Paving	5.15	1.34
25' East	5.5	1.0
50 "	5.2	1.3
75 "	5.9	1.1
89 " Ground	5.2	1.3
89.5 " Edge Com Walk	5.10	1.39
94.5 " " Red "	5.41	1.08
104.5 " Top cb	5.58	0.91
" " " Gutter Missed Blvd	6.03	0.10

π
6.49

5+00

0+00 Edge Paving	5.19	1.30
Ground	5.2	1.3
25' East	5.8	0.7
50 "	5.7	0.8
75 "	5.6	0.9
89 "	5.5	1.0
89 [±] Edge Corn Walk	5.07	1.42
94 [±] " " Pedestrian Walk	5.91	1.08
104 [±] Top Cb	5.53	0.96
" " Gutter	6.07	0.42

5+50

0+00 Paving	5.12	1.37
0+00 Ground	5.2	1.3
25' East	5.5	1.0
50 "	5.5	1.0
67 "	5.6	0.9
75 "	5.3	1.2
89 "	4.9	1.0
89 [±] Edge Corn Walk	4.98	1.51
94 [±] " " Ped "	5.32	1.17
104 [±] Top Cb	5.50	0.99
" " Gutter	6.00	0.49

6+00

0+00 Paving	4.83	1.60
0+00 Ground	4.9	1.6
5' East	4.3	2.2

π
6.49

16

10' East	5.2	1.3
25 "	5.0	1.5
50 "	5.0	1.5
75 "	5.0	1.5
89 "	5.10	1.39
89 [±] Edge Corn Walk	5.10	1.39
94 [±] " " Ped "	5.25	1.24
104 [±] Top Cb	5.42	1.07
" " Gutter	5.92	0.57

6+09. See sketch

0+00 Top Corn Gutter ^{Sec} sketch	9.39	2.15
--	------	------

6+25

0+00	4.84	1.65
4' East Top Corn Cb	4.13	2.36
10 "	4.2	2.3
25 "	4.6	1.9
50 "	4.9	1.6
70 "	4.5	2.0
75 "	4.0	2.5
89 "	4.6	1.9
89.5 Corn Walk	4.77	1.72
94 [±] Ped "	5.17	1.32
104 [±] Top Cb	5.34	1.15
" " Gutter	5.87	0.62

π
6.49
6750

6700	478	1.71
9' East	458	1.91
25 "	46	1.9
50 "	4.3	2.2
75 "	4.7	1.8
89 "	4.7	1.8
89.5 Com. Walk	4.55	1.94
94.5 "	5.14	1.35
104.5 Top cb	5.28	1.21
" " Gutter	5.85	0.64

6725

0100 Par 49	4.72	1.77
4' East	4.14	2.35
25 "	4.2	2.3
50 "	3.8	2.7
75 "	4.3	2.2
89.5 Ground	4.6	1.9
" " Edge Com walk	4.58	1.91
94.5 " Rd "	5.11	1.38
104.5 East Top	5.27	1.22
104.5 " Gutter	5.77	0.72

7729⁴ Edge Com cb

0100	4.52	1.97
0100 43 North Edge paving	4.52	1.92
4' East	4.04	2.45
" " 43 North	4.60	1.89

π
6.99

17

25' East	4.11	2.38
" " 43 North	4.65	1.84
50 " Com cb	4.25	2.24
50 " 4.3 North	4.78	1.71
75 " Com cb	4.33	2.16
" " 43 North	4.92	1.57
89.5 East int Com walk	4.42	2.07
" " 43 North	4.37	1.52
94.5 Edge Rd Walk	4.94	1.55
104.5 Top cb	4.50	1.99
" " Gutter	5.02	1.47
" " 4.3 North	4.91	1.58

T.P. 3.37	4.91	4.95	1.54
Check starting BM	5.49	-0.58	
		-0.60	
		0.02 error	

29.1

43

37.4

Robinson Ave

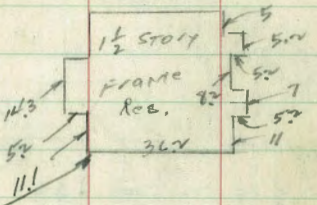
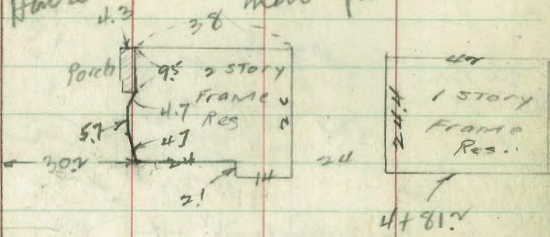
See 2047
9

East
Present line
6th Ave

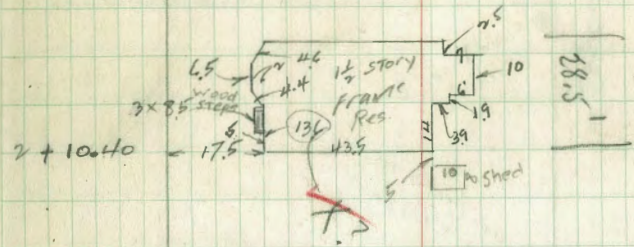
Bambrough
property

4+80.2

House moved back
new fdn



4+27 ← 28.8



1+95

1+45.5

Present
F line
6th Ave

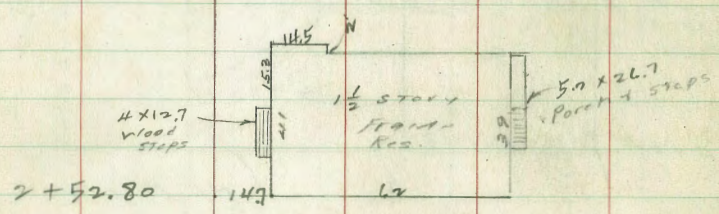
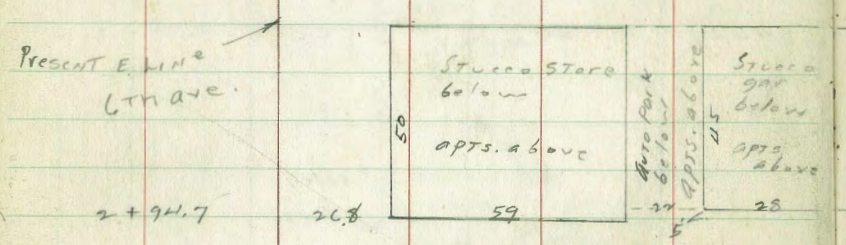
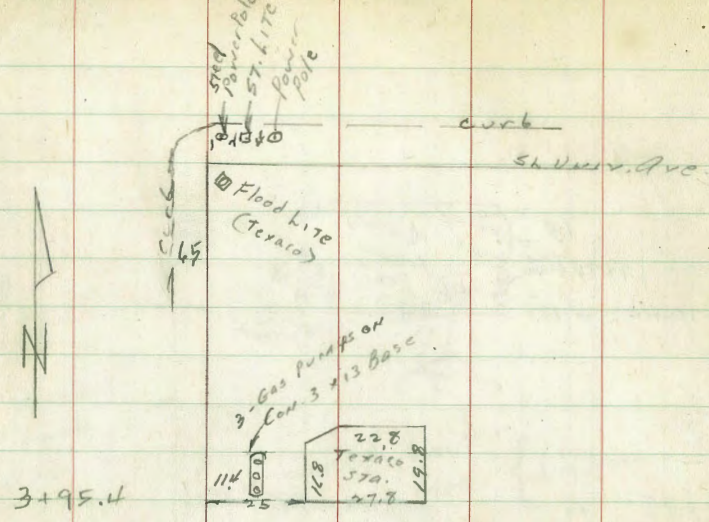
0+00

Picket fence

Asph. Parking

Piggley
Wiggley

Robinson Ave



11136

+3		5.0	108.4
+		3.3	108.1
+6		3.0	108.4
H		2.2	109.1
+10		1.2	110.2 ✓
TP	10.16	120.77	0.75 110.61

0+50

-10		9.2	111.6 ✓
H		9.9	110.9
+		10.2	110.6
S		10.0	110.8

0+75

-10		8.8	112.0
-10	= Fly Board Fence		✓
S		8.6	112.2
+		8.2	112.6
H		7.9	112.9
+10		7.1	113.7 ✓

0+85

S+3.3	= 1/4 5 Feet Trees Avg. 8" Diam.		✓
	140		
-10		5.0	115.8 ✓
H		5.6	115.2
+		5.8	115.0
S		6.1	114.7
+10		6.5	114.3 ✓

120.77

22

1+03

S+3.5 = 1/2 4 1/2 5 Feet Trees
Avg. 8" Diam ✓

		1+10.05 = 1/2 4 1/2 5 Feet Trees Avg. 8" Diam	
-10		6.0	114.8 ✓
S		5.6	115.2
+		5.5	115.3
H		5.1	115.7
		1+22 Squared	
H-10.0	= 1/2 Conc Apron	3.76	117.01 ✓
H-13.5	= 1/2 Garage Concrete	3.18	117.59 ✓
		1+25.47 = 1/2 4 1/2 5 Feet Trees Avg. 8" Diam	
H		4.4	116.4
+		5.0	115.8
S		5.0	115.8
+10		5.1	115.7 ✓
BM		5.53	115.21 ✓

1+29

H+7.5 = 1/2 1/2 Cypress Hedge ✓
3.71, 6.6
1+63

-10		3.1	117.7 ✓
S		2.6	118.2
+	= 1/2 1/2 Cypress Hedge	2.4	118.4
TP	5.59	124.90	1.46 119.31
H		6.0	118.9
+4.4	= 1/2 1/2 Conc Walk	5.32	119.58 ✓

124.90

1+72

S +6.0 = 2 24" Euc Tree ✓

1+78

H -1.6 = S 1/4 1.8 Conc Walk 4.50 120.40 ✓

1+83

S +5.5 = 2 18" Euc Tree ✓

1+98

S +6.0 = 2 9" Euc Tree ✓

2+0

-1.3 = S 1/4 1.8 Conc Walk 3.25 121.65 ✓

H

3.4 121.5

S

4.0 120.9

S

4.6 120.3

-1.0

4.7 120.2 ✓

2+11

S +6.5 = 2 12" Euc Tree ✓

2+20

S +7.5 = 2 20" Euc Tree ✓

H -1.0 = S 1/4 1.8 Conc Walk 2.28 122.62 ✓

2+28

-5.8 = H 4 Stucco Garage 2.7 122.2

S

3.0 121.9

+7.0 = 2 10.14" Euc Tree ✓

S

2.7 122.2

H

2.3 122.6

23

124.90

2+35.52 = H 2 Haverly on Drip

H TopCb 2.59 122.31 ✓

H Gutter on Pav mg 2.83 122.07 ✓

S " " 3.14 121.76 ✓

S Gutter " " 2.98 121.92 ✓

S TopCb 2.91 121.99 ✓

H Curblinc Haverly

S on Pav mg 3.93 120.97 ✓

S " " 3.76 121.14 ✓

H " " 3.58 121.32 ✓

BM	6.44	121.68	115.24	072 Hab Page 22 14/17.96
	0 + 0 = H.L. Ex. W. Alley on Dig			
F		5.3	116.4	
♂		5.8	115.9	
W		6.1	115.6	
	0 + 12			
	E + 0.1 = S. Fly Garage ✓			
	0 + 35			
-10		6.2	115.5 ✓	
W		5.0	116.7	
♂		4.8	116.9	
F		4.7	117.0	
	+ 6.1 = N. Fly Garage ✓			
	0 + 70			
-10		4.6	117.1 ✓	
F		4.8	116.9	
♂		4.9	116.8	
W		5.4	116.3	
	1 + 0			
-10		6.4	115.3 ✓	
W		5.7	116.0	
♂		5.0	116.7	
F		4.7	117.0	
+10		4.1	117.6 ✓	
	1 + 36			
	W = Fly Power Pole ✓			

Reduced & Plotted 8-6-41 G.B.H.

		121.68		
		1 + 54		
-10		5.7	118.0 ✓	
F		4.8	117.4	
♂		5.0	116.7	
W		5.5	116.2	
	+ 7.5 = S. Fly Conc Floor 568			
	1 + 74			
	W-2.1 = N. Fly Conc Floor 565			
	N. Fly used as Garage			
	= S. Fly Wire Fence ✓			
	2 + 0			
-10		5.8	115.9	
W		5.3	116.4	
♂		5.0	116.7	
F		4.4	117.3	
+10		3.8	117.9	
TP	4.17	120.90	4.95	116.73
	2 + 40			
	W-0.4 = N. Fly Wire Fence ✓			
	2 + 42			
	W + 2.5 = Fly Express Hedge Run E + W ✓			
	2 + 50			
-10		2.7	118.2	
F		3.5	117.4	
♂		4.1	116.8	
W		4.6	116.3	
+10		5.1	115.8	

120.90

3x0

-10	5.3	115.6
H	4.5	116.4
L	3.8	117.1
F	2.8	118.1
+10	2.1	118.8

3x50

-10	3.6	117.3
F	4.5	116.4
L	5.0	115.9
H	5.9	115.0
+10	6.2	114.7

4x0

-10	7.7	113.2
H	7.2	113.7
L	5.8	115.1
F	5.1	115.8
+10	4.3	116.6

4x50

-10	6.0	114.9
F	6.9	114.0
L	7.5	113.4
H	8.3	112.6
+10	8.8	112.1

120.90

5x0

-10	10.4	110.5
H	9.8	111.1
L	9.3	111.6
F	8.3	112.6
+10	7.3	113.6

5x45

-10	8.8	112.2
F	9.6	111.3
L	9.8	111.1
H	10.4	110.5
+10	11.2	109.7

TP 3.10 112.25 11.65 109.25

5x58.20 = SL Bird Rock Fly or Jig

H TopCb	3.05	109.30 ¹
H Gutter on Pan	3.11	109.24 ¹
L " " "	3.11	109.24 ⁴
F Gutter on " "	3.58	109.77 ¹
F TopCb	3.06	110.29 ¹

SCb Lim Bird Rock Fly

F on Pan	3.21	109.14 ¹
L " " "	3.76	108.59 ¹
H " " "	4.25	108.10 ¹

TP 0.42 101.00 11.77 100.58

TP 0.36 89.51 11.85 89.15

BM 10.44 79.07

98146P49 - 79.05

25

SWBP
to be labeled
Bird Rock Fly

80' wide
 14' Curbs
 13' 1/2 S
 1/2 sec of Monroe Ave
 Louisiana to Hamilton

Indexed
 LM

More
 Esboise
 S. 11100
 Brand

8-15-41
 See F.B. # 1747 pp. 1-12
 10/30/46

SEBP 4.37 343.33' 338.96 Monroe Texas

0-20 = E of Louisiana

S curb		5.97	337.36
S pav		4.57	336.76
cb	Hole	6.57	336.74
1/4	"	6.89	336.84
c	"	6.39	336.94
1/4	"	6.74	337.07
cb	"	6.14	337.19
N	"	6.00	337.33
N	cb	5.40	337.93

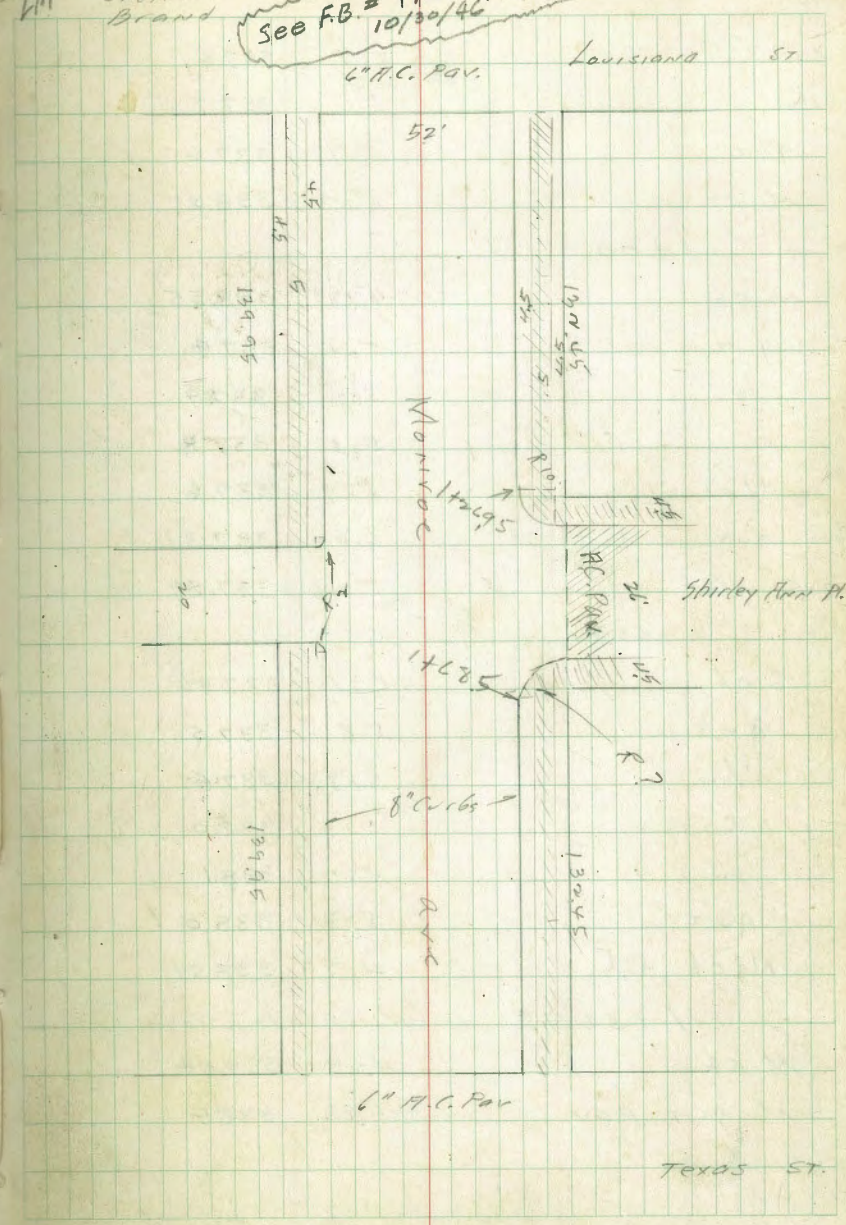
0+00 E L Louis

N cb		5.47	337.86
90T pav		5.95	337.38
1/4	"	5.87	337.46
c	"	5.81	337.52
1/4	"	6.09	337.24
90T	"	6.31	337.02
S cb		5.86	337.47

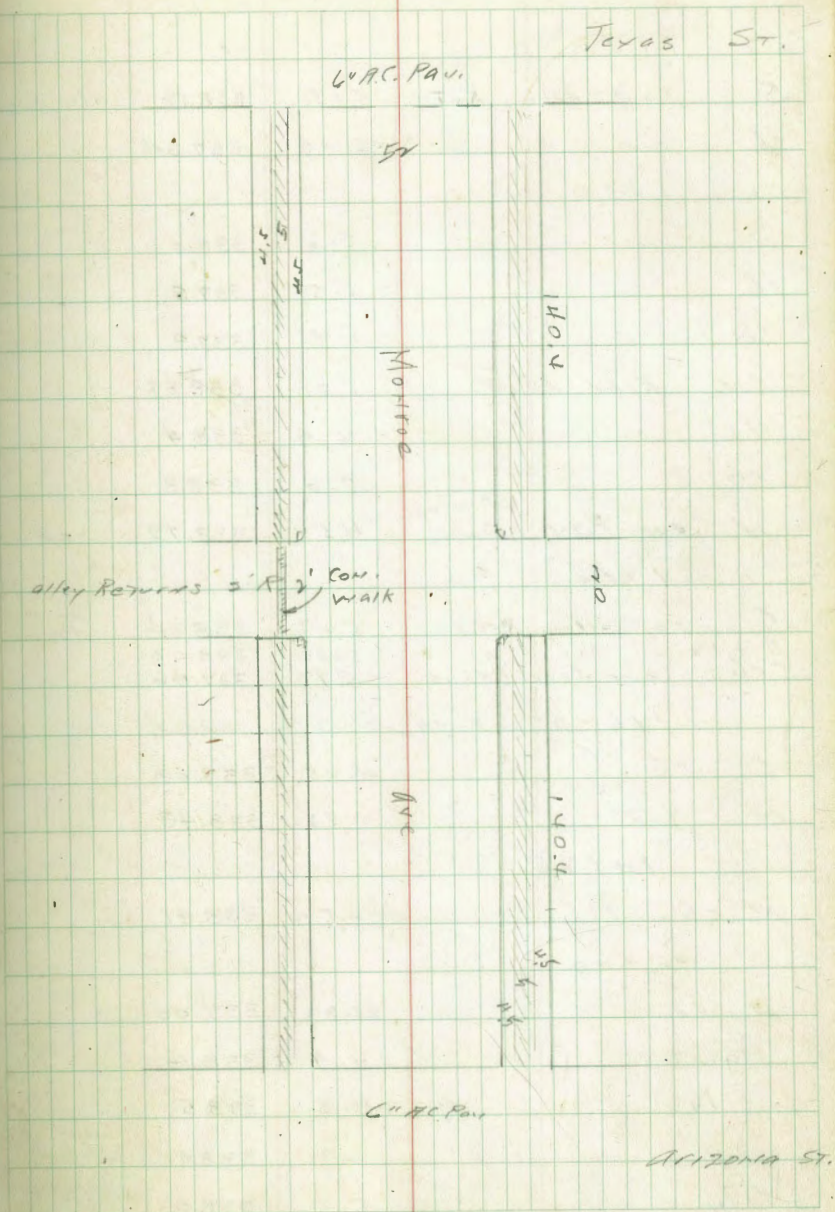
0+50

S cb		5.60	337.73
90T		6.1	337.2
1/4		5.9	337.4

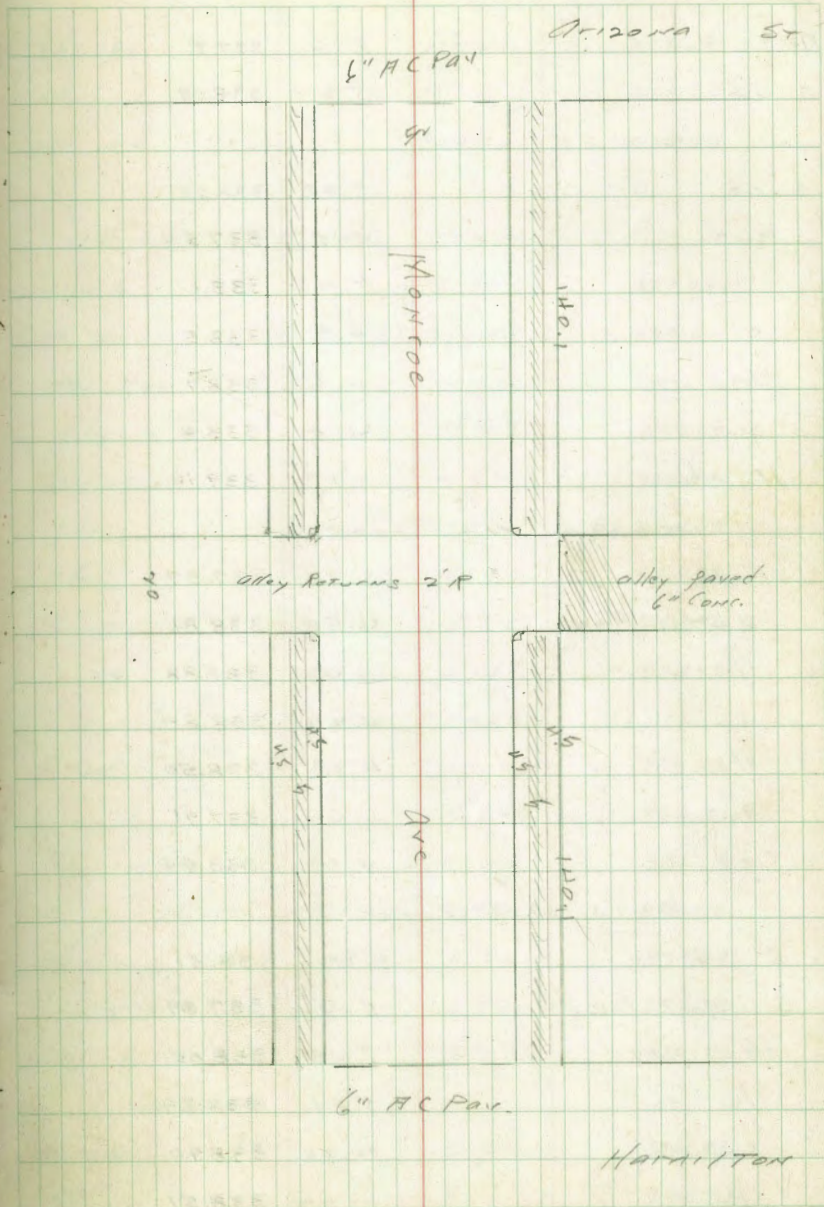
Note Reduced and Plotted by
 Max R. Gale 8/16/41



c	5.7	337.6
1/4	5.6	337.7
gut	5.7	337.6
N cb	5.12	338.21
1+00		
N cb	4.78	338.55
gut	5.4	337.9
1/4	5.4	337.9
c	5.5	337.8
1/4	5.7	337.6
gut	6.0	337.3
S cb	5.44	337.89
1+26.95		
S cb	5.37	337.96
gut	5.8	337.5
1/4	5.7	337.6
c	5.3	338.0
1/4	5.4	338.1
gut	5.3	338.0
N cb P.C.	4.79	338.54
1+36.95 w cb Shirley Ave		
N cb	4.79	339.04
N gut Pav	4.83	338.50



1+40				
S	Top alley Ret	5.11	338.17	also dict
sb	" " "	5.49	337.84	
1+50				
S		5.3	338.0	
cb		5.5	337.8	
1/4		5.4	337.9	
c	Rim M.H	5.01	338.32	
1/4		4.9	338.4	
cb		5.0	338.3	
N	on Pav Shirley Ann	4.54	338.79	
1+60				
S	Top alley RET.	5.79	338.04	
S+12	" " "	5.30	338.03	
S cb	on Gen Drive	5.87	337.46	
1+60.95 E cb Shirley Ann				
N	cb	4.25	339.08	
N	gut	4.85	338.48	
1+68.5				
N	cb P.C. Return	4.52	338.81	
2+00				
N	cb	4.33	339.00	
	gut	4.9	338.4	
1/4		4.8	338.5	
c		4.9	338.4	
1/4		5.3	338.0	



qut		5.6	337.7
S cb		5.24	338.09
	+ .50		
S cb		5.08	338.25
qut		5.5	337.8
1/4		5.7	338.1
c		4.9	338.5
1/4		4.6	338.7
qut		4.5	338.8
N cb		4.17	339.16
	+ 99.9		W L Texas
N cb		3.94	339.39
qut	pay	4.54	338.81
1/4	"	4.45	338.88
c	"	4.49	338.84
1/4	"	4.83	338.50
qut	"	5.42	337.91
S cb		4.89	338.44
	+ 14		W L CB Texas ST
S cb		4.82	338.51
S qut	pay	5.44	337.89
cb	pay	5.28	338.05
1/4	"	5.04	338.29
c	"	4.93	338.40
1/4	"	4.82	338.51

cb pay		4.64	338.69
N "		4.48	338.85
N cb		3.90	339.43
	0-14		E CB Texas
N cb		3.34	339.99
N qut		4.02	339.31
cb pay		4.71	339.12
1/4 "		4.32	339.01
c "		4.54	338.79
1/4 "		4.68	338.65
cb "		4.90	338.43
S qut "		5.12	338.17
S cb		4.38	338.95
	0-10		E L Texas
S cb		4.24	339.09
S qut		4.82	338.51
1/4 pay		4.20	339.13
c "		3.97	339.36
1/4 "		3.84	339.49
qut "		3.95	339.38
N cb		2.37	339.96
	0-50		
N cb		2.47	340.86
qut		3.0	340.33

1/4		2.8	340.5	
c		3.1	340.2	
1/4		3.4	339.7	
gut		4.1	339.2	
S c6		3.79	340.04	
T.P.	12.20	352.76	337	339.96
	1700			
S c6		11.90	340.86	
gut		12.5	340.3	
1/4		12.2	340.6	
c		11.7	341.1	
1/4		11.3	341.5	
gut		11.6	341.2	
N c6		10.96	341.80	
	1740.4			
N Top alley Ret.		9.96	342.80	
N gut		10.0	342.8	
N c6 Top cent		10.18	342.58	
N c6 gut		10.4	342.4	
1/4		10.3	342.5	
c		10.5	342.3	
1/4		11.0	341.8	
S gut		11.9	340.9	

S c6		11.34	341.42
S L Top alley Ret		10.94	341.82
S		11.0	341.76
	1760.4		
S Top c6		10.15	342.61
S L gut		10.2	342.6
S c6 Top cent Ret		10.38	342.38
gut		11.2	341.6
1/4		10.6	342.2
c		10.0	342.8
1/4		9.8	343.0
gut		9.7	343.1
N c6 " " "		9.23	343.53
N L " " "		8.99	343.77
N L gut,		9.2	343.6
	2700		
N c6		7.66	345.10
gut		8.2	344.6
1/4		8.3	344.5
c		8.7	344.1
1/4		8.9	343.9
gut		9.5	343.3
S c6		8.93	343.83
	2720		
S c6		8.14	344.62

gUT	8.5	344.3
1/4	7.8	345.0
c	7.6	345.2
1/4	7.3	345.5
gUT	7.7	345.6
N cb	6.71	346.05

2 + 30

N cb	5.88	346.88
gUT	6.5	346.3
1/4	6.7	346.1
c	6.8	346.0
1/4	7.1	345.7
gUT	7.7	345.1
S cb	7.20	345.56

2 + 40

S cb	6.18	346.58
gUT	6.4	346.4
1/4	6.7	346.6
c	6.0	346.8
1/4	5.8	347.0
gUT	5.7	347.1
N cb	5.04	347.72

2 + 60

N cb	2.91	349.85
gUT	3.7	349.1

1/4	4.1	348.7
c	4.7	348.6
1/4	4.5	348.3
gUT	4.9	347.9
S cb	4.28	348.48

T.P. 12.94 344.38¹ 1.37 351.44

3 + 00.8 = w h 9.12.20.19

S cb	12.07	352.36
gUT pay	12.86	351.52
1/4 "	12.17	352.21
c "	11.69	352.69
1/4 "	11.45	352.93
gUT "	11.31	353.07
N cb	10.50	353.88

3 + 14.8 w cb 9.2.20.19

N h cb	10.38	354.00
" gUT	10.97	353.41
cb pay	10.99	353.39
1/4	10.85	353.53
c	11.05	353.33
1/4	11.51	352.87
cb	12.25	352.13
S h gUT	12.72	351.66
S h cb	12.11	352.27

0-14 F C6 Arizona			
SL	cb	10.42	353.96
SL	qut	11.06	353.32
	cb pay	11.00	353.38
1/4	"	10.48	353.90
c	"	9.92	354.44
1/4	"	9.69	354.69
q6	"	9.62	354.74
NH	qut	9.35	355.03
NH	cb	8.82	355.54

0+0 FL Arizona

N	cb	8.80	355.58
qut	pay	9.58	354.80
1/4	"	9.31	355.07
c	"	9.42	354.94
1/4	"	10.11	354.27
qut	"	10.97	353.41
S-cb		10.32	354.06

0+20

S	cb	7.26	357.12
qut		8.11	356.3
1/4		7.4	357.0
c		6.8	357.6
1/4		6.8	357.6
qut		6.7	357.7
N	cb	5.90	358.48

0+40			
N	cb	3.22	361.16
qut		4.1	360.3
1/4		4.2	360.2
c		4.1	360.1
1/4		4.7	359.7
qut		5.3	359.1
S	cb	4.42	359.96
0+50			
S	cb	2.95	361.43
N	cb	1.86	362.52
0+60			
N	cb	0.57	363.81
qut		1.4	363.0
1/4		1.7	362.7
c		1.6	362.8
1/4		2.1	362.3
qut		2.6	361.8
S	cb	1.56	362.82

T.P. 1247 376.48 0.37 364.01

0+70

S	cb	12.63	363.85
N	cb	11.63	364.85

0 + 80		
N cb	10.50	365.92
9UT	11.5	365.0
1/4	11.5	365.0
C	11.4	365.1
1/4	11.9	364.6
9UT	12.5	364.0
S cb	11.67	364.86
1700		366.24
S cb in driveway	10.94	9.74 → 366.74
9UT		
1/4	10.1	366.4
C	9.5	367.0
1/4	9.8	366.7
9UT	9.7	366.8
N cb	8.50	367.96
1705		
N cb	8.76	368.22
S cb	9.30	367.18
1740		
N L Top cb	6.18	370.30
N L " pav	6.18	370.30
N cb Ret.	6.57	369.91
9UT	7.3	369.2
1/4	7.3	369.2

C	7.2	369.3
1/4	7.9	368.6
9UT	8.3	368.2
S cb Ret	7.90	368.58
S L Top cb	7.50	368.92
S L 9UT	7.9	368.6
1750		
N L on end ^{alley} pav.	6.21	370.27
1760		
S L Top cb	6.57	369.91
S L dirt	7.6	368.9
S cb	6.70	369.72
9UT	7.5	369.0
1/4	6.9	369.6
C	6.4	370.1
1/4	6.5	370.0
9UT	6.5	370.0
N cb	5.75	370.73
N L pav.	5.74	370.74
N L curb	5.50	370.94
1700		
N cb	4.50	371.96
9UT	5.1	371.4
1/4	5.0	371.5
C	5.0	371.5

1/4	5.3	371.2
gut	5.8	370.7
S cb	5.24	371.24
2 + 41		
S cb	3.88	372.60
gut	4.5	372.0
1/4	4.0	372.5
c	3.7	372.8
1/4	3.8	372.7
gut	3.9	372.6
N cb	3.24	373.24
2 + 75		
N cb	2.17	374.31
gut	2.9	373.6
1/4	2.7	373.8
c	2.8	373.7
1/4	3.1	373.4
gut	3.5	373.0
S cb	2.88	373.60
3 + 00.7 W L Hamilton		
S cb	1.97	374.51
gut Pak.	2.52	373.96
1/4	2.02	374.46
c	1.78	374.70
1/4	1.77	374.71

gut Pak.	2.05	374.43
N cb	1.45	375.03
3 + 00.7 = W L Hamilton		
N L curb	1.26	375.22
N L gut Pak	1.78	374.70
cb Pak	1.75	374.73
1/4	1.59	374.89
c	1.67	374.81
1/4	1.95	374.53
cb	2.28	374.20
S L gut "	2.52	373.95
S L curb	1.94	374.54 ✓
SEEP		
check to Mancos & Hamilton	1.73	375.25 375.30
		0.05

Cross Section Brooklyn Ave
65th to 69th St.

Indexed
LM

Sept. 19. 41
Sutton
Hartbar
W Moore

Existing 4" Conc Walk



0+0.2
7+95.61

Fd Mon 67th St

4+35.612

30 x 30

8' Brooklyn Ave

6" Conc Wall

1+30

1+15

1+0

Cobble Steps Wall 2 1/2' High

0+17.76

0+0

21.0

9.00

15.51

Fd Mon

0-59.76

6+50.812

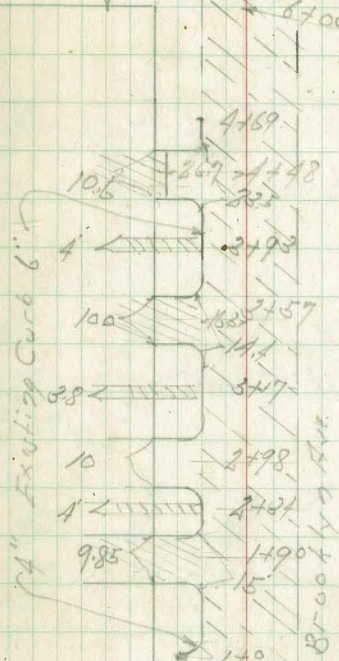
65th St

Conc Pav

4 1/2' Blocks Pav

69th St

4409 = Existing St. 22" Pipe Culvert



Existing Curd 6"

0+0
8+46.44

Fd Mon

7+86.44

oil pav 68th St

30 x 30

Cross Section Brooklyn Ave
66th St to 69th St.

0+17.76 = E.L. Madera on St.

0+0 = F.L. 66th St.

0-30 = H.L. 66th St From South

0-59.76 = Opp H.L. Madera on St.

BM		8.98	232.60	Mon. 7 Brooklyn H.L. 66th St
TP	6.65	241.58	11.42	234.98
TP	3.07	246.35	0.02	243.28
TP	11.74	243.30	0.18	231.56
BM	1.34	231.74	230.40	H.L. 66th St Woodman? 57% Imperial

Lt=H

2

Rt=S

36

234.7 6.9 7.0	233.1 6.5 6.0	232.6 9.0 2.0	233.9 7.7 1.0	233.7 7.9	233.3 8.3 1.0	234.5 7.1 1.0	235.0 6.6 6.0 Boyle Hall
	234.0 7.6 6.0	233.6 8.2 1.0	232.9 8.7	232.7 8.9 2.0	232.2 8.6 6.0 Boyle Cable Hall		
	232.6 9.0 6.0 Boyle Hall	232.4 9.1 1.0 Boyle Hall	232.6 9.0	232.2 9.1 2.0	231.8 9.8 6.0	231.9 9.7 1.0	
239.4 6.2 6.0	235.6 6.0 1.0	232.7 8.9 6.0	233.0 8.6	231.6 10.0 1.0 Boyle Hall	231.2 9.7 6.0	230.6 11.0 1.0	
			241.58 ✓				

1750

TP 11.79 264.03 0.08 252.24

1730

1728 22' Lt of 1/2 = 11 1/2" Pepper Tree

1715 = 1/4 Conc Hall or Lt ✓

170

TP 11.38 252.32 0.64 240.94

0794 23' Lt of 1/2 = 11 1/8" Pepper Tree ✓

0775

0763 21' Lt of 1/2 = 10 1/2" Pepper Pole ✓

0750

241.58

2496
114
30

2528
112
30

2570
100
30

2558
82
10

2571
69

2587
56
10

2587
56
30

2605
64
30

2640 ✓

2488
314
30

2475
48
30

2478
45
30

2480
43
10

2508
15

2578
0
10

2526
10
30

2745
10
30

243.09

933
100
30 = 1/2 Top Hall

2407
116
30

2415
108
30

2408
115
30

2406
117
10

2413
110

2428
95
10

2439
84
30

2442
61
30

2620 ✓

2338
78
15

2366
65
30

2375
41
10

2378
68

2382
64
10

2395
71
30

2406
60
30

2330
80
30

2331
80
30

2344
72
30

2357
59
10

2352
64

2352
64
10

2369
57
30

2378
60
30

24158 ✓

L

L

PK

37

2+22 20.2 Pt of 1/2 - 54 Power Pole ✓

3+0

2+97 21.5 Lt of 1/2 = 114 12" Pepper Tree ✓

2+76 21.6 Lt of 1/2 = 114 14" Pepper Tree ✓

2+75

2+50

TP 11.77 287.02 0.16 275.25

2+25

2+0

TP 11.62 275.41 0.24 263.79

1+95 20.5 Pt of 1/2 = 54 Power Pole ✓

1+75

264.03

Lt

R

R

38

285.2
1.0
10287.4
1.0
10287.6
1.0
10289.2
1.0
10289.3
1.7
10284.6
1.0
10284.4
1.0
10283.9
1.0
10283.7
1.0
10283.1
1.0
10283.1
1.0
10283.2
1.0
10283.9
1.0
10283.8
1.7
10283.7
1.0
10283.4
1.0
10282.9
1.0
10282.5
1.0
10278.3
1.0
10278.9
1.0
10279.2
1.0
10279.9
1.0
10279.9
1.0
10279.9
1.0
10280.1
1.0
10280.1
1.0
10

287.02 ✓

274.0
1.0
10275.0
1.0
10274.8
1.0
10274.8
1.0
10275.2
1.0
10276.3
1.0
10277.1
1.0
10277.1
1.0
10266.2
1.0
10267.2
1.0
10267.7
1.0
10268.1
1.0
10269.0
1.0
10270.6
1.0
10271.3
1.0
10272.6
1.0
10

275.41 ✓

259.4
1.0
10260.9
1.0
10262.4
1.0
10263.8
1.0
10265.7
1.0
10266.5
1.0
10266.2
1.0
10267.0
1.0
10

264.03 ✓

4+65.61 = 2 67¹/₂ St

BM 5.32 290.07 Mon 2
Brooklyn 2
67¹/₂ St

4+35.61 = 2 67¹/₂ St

4+35 20.6 Rt of 2 = 5/4 Power Pole ↓

4+18 20.5 Lt of 2 = 1/4 18" Paper Tree ↓

4+0

3+98 20.6 Lt of 2 = 1/4 18" Paper Tree ↓

3+75

3+58 21 Lt of 2 = 1/4 18" Paper Tree ↓

3+50

TP 8.57 295.39 0.20 286.82

3+25

287.02

39

LT	Z	RT
2935 60 00	2916 65 00	2901 47 10
289.0 6.4 10	2883 7.1 50	2872 7.8 00
292.7 2.7 00	292.0 1.4 10	2909 1.5 10
289.9 5.5 10	289.1 1.5 10	2882 6.5 20
287.9 7.5 10	287.9 7.5 10	2862 9.2 40
289.8 5.6 00	289.5 5.9 00	2886 6.8 10
287.2 8.2 10	286.9 6.5 00	2860 9.1 10
288.6 5.8 00	288.2 7.2 00	287.5 7.9 10
286.8 8.6 10	286.8 8.6 10	285.9 9.5 10
285.9 9.5 10	285.9 9.5 10	285.4 10.0 40
287.7 7.7 10	287.7 7.7 10	286.8 8.6 10
285.7 1.3 10	285.7 1.3 10	284.8 2.2 10
286.7 0.6 00	286.5 0.5 00	286.2 0.8 00
287.02		287.02

0+42

0+39 - Ely Dr. Garage 07 Lt.

0+25 - W'y Dr. Garage on Lt.

0+13 21' RT of Z - Sky Power Pole
 TP 5.96 296.03 5.32 290.07

0+0
 4+95.61 = E.L. 67' 1/2 St

4+89

4+83 = Z 8.5 Conc Drive 07 Lt

295.39

LT RT

294.10
 1.92
 29.8 23.600
 10.1

293.19

2.84
 30 - Ely Garage
 60% 11.06

293.21

2.88
 30 - W'y Garage
 60% 11.01

293.1

294.0

291.0

299.9

290.6

290.1

288.9

297.8

296.03 ✓

294.2

293.3

291.9

290.6

289.3

289.9

288.7

294.1

293.0

291.8

290.4

289.3

288.1

286.9

295.13

294.02

295.39 ✓

TP 1.34 297.33 0.04 295.99

2+27

2+0

1+89.48

208 = Lt of Lt = 114 18" Palm Tree ✓
219 Rt of Lt = Sky Power Pole ✓

1+50

1+0

0+78

21.6 Rt of Lt = Sky Power Pole ✓

0+50

296.03

295.2	296.0	295.3	294.4	292.7	292.2	291.7	291.3	290.3	290.0
107 80	0.0 14	0.7 10	1.6 14	0.1 10	0.1 80	1.0 10	1.1 10	0.5 60	0.0 40
296.0	295.8	294.9	292.7	292.3	291.9	290.9	290.4	290.1	
0.0 80	0.17 14	1.1 10	0.3 11	0.7 10	1.1 10	0.5 10	0.5 60	0.5 40	
	295.96								
	0.04 14								
	295.7	294.8	292.8	292.6	292.2	291.4	289.9	288.5	
	0.0 80	1.1 10	1.1 12	0.1 10	0.8 15	1.6 10	0.6 60	1.5 10	
	295.7	294.7	293.0	292.5	291.9	290.6	289.3	288.0	
	0.0 80	1.0 10	0.0 14	0.5 10	1.1 11	1.5 10	1.1 60	0.0 10	
	294.9	294.0	292.4	291.6	290.8	291.6	290.4	289.3	287.2
	0.1 10	1.0 10	0.6 16	1.1 10	1.0 10	1.1 10	0.5 10	0.5 60	1.1 10
				291.6	290.3				

5+49 20.3 Lt of L = Nly 8" Acacia Tree ✓
 5+28 20.2 Lt of L = Nly 6" Acacia Tree ✓
 5+0

4+81 22.3 Rt of L = Sky Power Pole ✓

4+50

4+0

3+56 22.0' Rt of L = Sky Power Pole ✓

3+46 21.3 Lt of L = Nly 24" Palm Tree ✓

3+0

2+50

297.23

292.3	291.2	290.0	289.5	288.7	289.5	288.5	287.6	286.4
6.50	6.10	7.10	7.80	8.60	7.80	8.80	9.70	10.80
293.8	293.2	290.8	290.3	289.8	290.4	289.3	288.6	287.7
6.50	6.10	6.50	7.00	7.50	6.90	8.00	8.70	9.60
294.1	293.1	290.9	290.5	290.3	290.8	289.7	288.7	287.6
6.50	6.10	6.40	6.80	7.00	6.50	7.60	8.60	9.70
294.0	294.03	293.7	292.7	291.3	290.9	290.6	289.0	288.3
6.50	6.30	6.10	6.60	6.90	6.40	6.70	6.80	9.00
294.7	294.1	293.1	291.7	291.4	290.7	290.2	289.7	288.7
6.50	6.10	6.20	6.50	6.90	6.50	7.10	6.80	8.60
296.2	295.67	294.9	292.6	292.0	291.4	290.6	289.9	289.2
6.50	6.60	6.40	4.70	6.30	6.50	6.70	7.40	8.10
	24" Sky Walk							
			297.33 ✓					

6783 19.4 Rt of $\frac{1}{2}$ = Shy 12" Tree ✓
 6762 19.9 Rt of $\frac{1}{2}$ = Shy 12" Tree ✓
 6750

6744 19.3 Rt of $\frac{1}{2}$ = Shy 10" Tree ✓
 6740
 6726 18.7 Rt of $\frac{1}{2}$ = Shy 6" Tree ✓
 6711 22.5 Rt of $\frac{1}{2}$ = Shy Parker Pole ✓
 6704

670
 5789 20.1 Lt of $\frac{1}{2}$ = 11y 6" Acacia Tree ✓
 5778 = $\frac{1}{2}$ 15' Conc Drive on Lt

TP 2.74 291.08 8.99 288.34 ✓
 5768 200' Lt of $\frac{1}{2}$ = 11y 6" Acacia Tree ✓
 5750

297.23

LT RT
 2873 2863 2846 2849 2895 2847 2843 2840
 30 30 35 32 36 30 30 40

289.51
 1.57
 294 = 11' Conc
 Hall

290.34
 0.74
 294 = 11' Conc
 Hall

289.6 288.3 287.1 2870 2862 2867 2861 2854 2846
 15 30 28 20 40 41 49 15 50 20 57 30 65 40

29107 29022 288.98
 0.86
 288 = 8' Conc Drive
 289.7 = 15' Conc
 Drive

2926 2910 2886 2886 2879 2880 2867 2858
 47 63 87 87 94 23 10.6 16.5
 30 20 9 12 30 30 40

297.23 ✓

8703

7+86.44 = W.L. 68th St

210' Lt of L = N/4 Anchor P
218' Rt of L = S/4 Power Pole

7+80 19.5' Rt of L = S/4 12" Tree ↓

7+65 19.5' Rt of L = S/4 12" Tree ↓

7+58 = 2 3.5' Conc Walk on Rt

7+50 19.2' Rt of L = S/4 10" Tree ↓

7+40 20.2' Lt = N/4 6" Tree ↓

7+18 20' Lt = N/4 6" Tree ↓

7+0

6+93 20' Lt of L = N/4 8" Tree ↓

6+90 = 2 7' Conc Drive on Rt

TP 135 285.72 6.71 284.37
291.08

	Lt.		Rt.
281.2	280.4	279.9	279.4
5.5 30	5.3 30	5.8 10	5.3 10
278.7	278.2	277.7	
7.0 10	5.5 30	5.0 30	
282.0	282.2	281.6	280.4
5.7 30	5.5 30	4.1 15	5.3 11
280.4	279.6	280.5	280.1
5.3 30	6.1 11	5.3 30	5.7 30
279.5	279.5		
5.3 30	5.7 30		
280.25	279.9		
5.47 30	5.79 30		
282.9	282.5	282.0	281.7
5.8 30	5.3 30	5.7 10	4.0
280.8	281.2	280.6	280.1
4.9 10	4.5 30	5.1 30	5.6 30
280.4	280.9	280.4	279.5
5.4 30	4.8 30	5.2 10	6.2 40
285.3	284.4	283.8	283.3
0.4 30	1.0 30	2.9 11	2.4
282.6	283.1	281.9	280.9
5.1 10	4.6 15	5.8 30	4.8 30
285.4	284.7	283.1	283.6
0.3 30	1.0 30	2.6 11	2.1
283.1	283.1	282.6	283.1
2.6 11	2.6 10	4.1 30	4.1 30
283.5	283.53	283.22	
4.1 30	4.1 30	2.50 30	
285.72			

280.25
5.47
30
280.25
5.79
30
280.25
5.79
30
280.25
5.79
30

283.53
4.1
30
283.22
2.50
30
283.22
2.50
30

1+0 = 1/4 4' Conc Lt.

0+86 20' Lt of 1/2 = Fly Cobble Wall ✓

0+50

0+43 = 1/2 4' Conc Walk on Lt.

0+40 22' Rt of 1/2 = Fly Power Pole ✓

TP 5.25 284.77 6.20 279.52 on 2 Mon
Brook 1/2
4 68' 1/2 St

0+0 8+46.44 = E.L. 68' 1/2 St

8+34

8+16.44 = 1/2 68' 1/2 St.

BM 6.20 279.52 1/2 Mon
Brook 1/2
68' 1/2 St
285.72

41

2

Rt Sept 23/145

281.3
5.5
30
281.33
5.44
20-1/4 Conc
Cb
280.6
4.7
16-1/4 Conc
1/4
280.4
4.4
219.3
5.5
16-1/4 Conc
1/4
279.9
4.9
20
279.4
5.4
30
279.3
5.5
40

281.4
5.4
30
281.4
5.4
19
280.2
4.6
14-1/4 Conc
1/4
280.1
4.7
278.9
5.9
17-1/4 Conc
1/4
279.5
5.5
20
279.0
5.5
30
278.5
5.5
40

281.60
5.17
30-1/4 Conc
Walk

281.2
4.5
30
281.2
4.5
20
280.0
5.7
13
281.77 ✓
37.6
61
278.5
7.8
18
278.7
7.0
20
278.6
7.1
30

280.7
5.0
30
280.2
5.5
20
279.7
6.0
10
279.2
6.5
278.5
7.2
10
277.9
7.8
20
277.2
8.5
30

281.7
5.0
30
281.1
5.6
20
280.5
5.8
10
279.9
5.8
279.4
6.3
10
278.9
6.8
20
278.4
7.0
30

285.72 ✓

2117

2102

210

1768

21.4 Rt of 2-5/4 Power Pole ✓

1750

1735

1711 = 2 8 Cone Drive on Rt

28477

28029

4.48
31 = 2.8 Cone
Driv

28023

4.54
40 = 0.7 Dr.

28023

4.54
31 = 2.35
Cone Walk

2819

2.7
30

28159

3.18
15.8 = 6

3813

3.5
15.8 = 6.4 Hr

3809

3.9

379.9

4.9
16.5 = 1.9 Hr

3802

4.6
30

2813

3.5
30

2810

3.8
30

28129

3.48
15 = 6

2807

4.1
15 = 6.4 Hr

2805

4.3

2795

5.3
15 = 5.4 Hr

2797

5.1
20

2796

5.3
30

2797

5.1
40

27981

4.96
31 = 2.35
Cone Walk

27986

4.91
40 = 0.7 Walk

279.81

4.96
29.7 = 2.8 Cone
Driv

279.62

5.15
40 = 0.7 Dr.

28477 ✓

3740 = 10' Conc Drive 3.7' Conc Ribbon

3728 19.8 Pt of L = 5 1/4 Small Poles ✓

3716

3709 = CB EC on Lt

3705 19.7 Pt of L = 5 1/4 " Tree ↓

3787.5 = CB BC on Lt

3754 21.6 Pt of L = 5 1/4 Power Pole ✓

3750

3746

28477

Lt

L

Rt

47

280.02

4.25
30 = 1/2 Conc Dr.

279.77

5.00
30 on Dr.

279.97

4.80
30 = 1/2 4' Conc Walk

280.03

4.74
40 on Walk

2893

1.5
30

282.55

2.22
16 = CB

281.8

3.0
16 = gutter

281.4

3.4

280.3

4.5
15 = 1/2 Par

280.5

4.3
30

280.1

4.7
30

282.7

2.1
30

282.46

2.31
16 = CB

281.9

2.9
16 = gutter

281.5

3.3

280.5

4.3
16 = 1/2 Par

280.9

3.9
30

280.5

4.3
30

280.2

4.6
30

282.1

2.7
30

281.92

2.85
16 = CB

281.5

3.3
16 = gutter

281.3

3.5

280.6

4.3
15 = 1/2 Par

280.8

4.0
30

280.5

4.3
30

280.45

4.32
37 = 1/2 Conc Dr.

280.25

4.52
40 on Dr.

28477 ✓

4+36

4+0

3+98 = 210' Rto of L = Fly Box on Pak ✓

3+91 = 192' Rto of L = Fly 8" Trac ✓

3+83 = L 1' Conc Walk on Rt

3+59 = L 102' Conc Drive on Rt

TP 0.94 28185 3.86 28091

3+71 = 195' Rto of L = Fly 18" Blac ✓

3+50

3+48 = 192' Rto of L = Fly 8" Trac ✓

3+43 = Fly 4' cb w/ 6" cb on bt ✓

28477

279.1 2.7 30	278.76 3.09 16=cb	277.9 3.9 16=gutter	277.3 4.5	276.2 5.6 15=Fly	276.5 5.6 20	275.9 5.9 20	275.7 6.1 20
--------------------	-------------------------	---------------------------	--------------	------------------------	--------------------	--------------------	--------------------

281.1 3.7 30	280.23 1.63 16=cb	279.5 2.3 16=gutter	279.1 2.7	278.0 3.8 15=Fly	278.3 3.5 20	278.0 3.8 20	276.8 5.0 20
--------------------	-------------------------	---------------------------	--------------	------------------------	--------------------	--------------------	--------------------

279.04
2.81
29.5=2' Conc Walk

279.19
2.66
47' on Walk

278.80
2.05
28.5=2' Conc Drive

279.61
2.31
46' on Dr.

28185. ✓

2824 2.4 30	281.89 2.82 18=cb	281.3 3.5 16=gutter	280.8 4.0	279.7 5.1 15=Fly	279.9 4.9 20	279.8 5.0 20	280.0 4.8 20
-------------------	-------------------------	---------------------------	--------------	------------------------	--------------------	--------------------	--------------------

282.39
2.38
16=4' cb to start

281.95
2.82
16=6' cb to start

281.4
3.4
16=gutter

284.77 ✓

5760

5737

30.8 ft of L = Sky Power Pole ✓

5734

TP

0.09 271.42 10.52 271.33

5715

5704

21.6 ft of L = 8" Olive Tree ✓

570

4795

= L 8' Conc Dr on Pl

4782

18.5 ft of L = Sky 8" Tree ✓
21.72 ft of L = 8" Olive Tree

4769

= Fly CB on L ✓

281.85

49

2720
+56
30

2714
0.0
20

2695
1.9
1/6 = 11.1 ft

2693
2.1

2684
3.0
1/6 = 11.1 ft

2689
2.5
20

2679
3.5
30

2673
4.1
40

2734
+2.0
30

2715
+0.1
1/6 = 11.1 ft

2712
0.3

2705
0.9
1/6 = 11.1 ft

2711
0.8
20

2711
0.5
30

2717
+0.9
1/6 = 11.1 ft

2685
1.9
40

271.42 ✓

271.51

271.53

10.34

10.52

271.3

40 on Wall

3764

2752

2742

2739

2732

2731

2724

2720

6.4
30

6.8
20

7.6
1/6 = 11.1 ft

7.9

8.6
1/6 = 11.1 ft

8.7
20

9.4
30

9.8
40

272.92

272.54

272.12

8.9

9.3

9.7

2776

277.05

2761

2757

2748

2753

2743

2737

4.2
30

4.8
1/6 = 11.1 ft

5.7
1/6 = 11.1 ft

6.1

7.0
1/6 = 11.1 ft

6.5
20

7.5
30

8.1
40

281.85 ✓

BM

6.34 253.52

2 PIPES W.
Box Calc.
Imperial
69 3/4
253 1/4

TP 0.65 259.86 12.21 259.21

6 + 20.72 = 26 69 1/4

6 + 13 = Fly Oil Paving

6 + 09 = Ex Nking 22" Steel Pipe Cut Joint

6 + 05.72 = 24 69 1/4

5780

271.42

266.1 53 10	264.9 66 30	263.7 77 30	262.7 87 30	261.9 95	261.2 102 10	260.4 110 20	260.0 114 60	258.7 127 40
263.6 78 30	262.4 90 30	261.45 99 18 Fly 2 1/2"	263.7 73 13 1/4 1 1/2"	262.2 82	262.3 91 10	261.1 103 23 1/2 25	260.5 109 25	258.20 122 28 1/2 30
269.4 80 30	267.7 97 25	264.3 71 15	265.2 82 16 1/2 1 1/4"	264.5 89	263.0 84 15 1/2 1 1/4"	261.4 90 25	260.5 98 30	259.7 117 40
270.8 96 30	270.0 104 30	267.5 89 15 1/2 1 1/4"	267.1 93 15 1/2 1 1/4"	266.0 54 13 1/2 1 1/4"	265.4 60 30	264.2 68 30	263.3 81 40	

Cross Section Brooklyn Ave.
66th St to 65th St.

1+46 21 1/2 of 1/2 = Sly Power Pole ✓
1+20

TP 11.53 267.35 0.15 255.82

1+0

0+70 20 1/2 of 1/2 = Sly Power Pole ✓

TP 12.20 255.97 0.05 243.77

0+47

0+30

0+0 = H.L. 66th St From South

BM 11.22 242.82 222.60

1400 ft
Brooklyn Ave
H.L. 66
1972

Lt-5

RT-11

51

Sept 22-41

2471	2533	2546	2559	2570	258.2	259.3	259.9	261.2
202 50	14.0 40	12.7 30	11.4 20	10.0 10	9.1	8.0 10	7.4 20	6.1 30

267.35 ✓

2302	244.7	249.6	251.9	253.1	254.3	257.8	255.4	256.4
25.8 50	11.0 30	6.4 20	4.1 10	2.9	1.7 10	1.2 20	0.6 30	1.0 40

2312	231.0	231.7	236.7	243.3	246.3	248.2	249.4	250.0
24.8 45	25.0 30	24.3 24	19.3 15	18.7	9.7 10	7.0 20	6.6 30	6.0 40

255.97 ✓

231.8	231.5	232.1	231.9	233.3	236.6	239.6	242.5	245.0
18.0 40	17.3 30	11.7 20	11.9 10	10.5	7.8 10	4.7 20	6.0 30	1.3 40

229.8	231.7	231.6	232.0	233.0	232.9	235.3	238.9	241.8
14.0 40	12.1 30	12.2 20	11.8 10	10.8	10.9 10	8.5 20	4.9 30	3.0 40

232.0	231.8	232.5	233.0	233.1	232.3	232.3	232.5
11.8 40	12.0 30	11.2 20	10.8 10	10.7	11.5 10	11.5 20	11.0 30

242.82 ✓

3743 21.3 Lt of L = Sky Power Pole ✓

270

2780

2751

2730 21 Lt of L = Sky Power Pole ✓

270

TP 3.53 270.63 0.25 267.10

1780

267.35

51

52

51

52

2621	2629	2633	2632	2634	2637	2642	2650
8.5 70	7.7 60	7.3 20	7.4 10	7.7	6.9 10	6.5 20	5.6 60

2644	2648	2650	2648	2650	2646	2650	2669
6.3 70	5.8 50	5.6 20	5.8 10	5.6	6.0 10	5.6 20	5.7 60

2642	2651	2656	2665	2674	2678	2677	2683	270.50
6.4 70	5.5 30	5.0 20	4.1 10	5.8	3.8 20	4.9 20	7.0 60	0.12 30

90.55
271.1
Gobbler
Polaris
0.12
30
Top
Gobbler
Polaris

2636	2644	2653	2663	2676	2688	2700	2713
7.0 70	6.3 30	5.0 20	4.0 10	5.0	1.8 20	0.6 20	+0.7 30

0.7
30
Wire
Fence

2609	2628	2640	2650	2662	2672	2683	2701
9.7 75	7.8 60	6.6 20	5.6 10	4.4	3.4 10	2.3 20	0.5 30

0.5
30
Wire
Fence

270.63 ✓

2600	2618	2627	2639	2646	2657	2663	2673
7.0 75	5.8 50	4.6 20	3.9 10	2.7	1.6 10	1.0 20	0.0 30

0.0
30
Wire
Fence

267.35 ✓

5+02 29.1 = Picket Fence Set. ✓

5+0

4+70

4+47 28.5 Lt of L = Fly Picket Fence ✓

4+45

4+44 21.5 Lt of L = Fly Picket Fence ✓

4+0

3+70

3+45

270.63

Lt

L

Rt

53

2564 142 70	2571 135 30	2577 130 30	2586 120 30	2591 115	2591 115 15	2597 109 30	2605 101 40		
2588 128 70	2570 136 30	2573 133 30	2587 119 10	2588 118	2588 118 10	2588 118 30	2597 109 30	2600 106 40	
2549 157 70	2570 136 30	2580 126 30	2585 121 30	2589 117	2588 118 10	2591 115 30	2608 98 30	2611 95 40	
2585 131 40	2588 118 30	2591 115 30	2590 116 10	2594 112	2594 112 15	2596 110 30	2606 100 30	2610 96 40	
2589 117 40	2598 108 30	2608 99 30	2606 100 10	2601 105	2605 107 10	2602 104 15	2609 97 30	2616 90 30	2617 89 40
2597 109 40	2601 105 30	2608 98 30	2612 94 10	2612 94	2615 91 15	2623 85 30	2627 79 30	2630 76 40	
270.63 ✓									

6+66 = Existing 22" Steel Pipe

IP 4.70 268.99 6134 264.29

6+50.81 = E.L. 65' 25" From H

6+35

6+07' 292 L of L - W/4 Picket Fence

6+0

5+85

5+82 22.50 ft = 54 Power Pole ✓

5+40

270.63

262.46	265.1	266.2	266.6	266.6	266.8	268.0	265.07	266.5
57.5	59	38	34	34	33	1.0	39.1	2.5
57.5	1.5	38	34	34	33	1.8	39.1	3.0
						268.99 ✓		Flow 2.11

264.1	264.1	265.8	265.3	265.4	265.2	266.4	267.1	267.1
5.6	5.5	1.8	5.0	5.2	5.4	1.3	3.5	3.5
7.0	3.0	3.3	1.6	1.8	8.4	1.8	3.0	7.0

263.5	263.5	264.5	264.3	264.2	264.0	265.9	266.3	266.9
2.0	7.0	5.1	6.0	6.4	5.6	7.7	1.0	4.2
4.0	3.0	3.0	4.4	6.4	9.6	1.6	3.0	4.0

262.1	262.3	262.5	262.6	261.9	261.8	261.4	262.8	263.5	263.8
8.5	8.0	8.1	8.0	8.7	8.8	9.2	7.8	7.6	6.8
7.0	3.0	3.0	7.0	8.7	8.8	11	1.8	3.0	4.0

261.2	261.4	261.6	261.8	261.2	260.9	260.6	261.9	263.0	263.0
9.4	9.2	9.0	8.8	9.4	9.7	10.0	8.7	7.6	7.6
7.0	3.0	3.0	1.0	5.4	9.7	1.2	1.5	3.0	4.0

258.6	258.8	259.0	260.3	259.8	259.7	260.9	260.2
12.0	11.8	11.5	12.0	10.8	10.9	9.7	9.4
4.0	3.0	1.5	3.0	10.8	1.5	3.0	4.0

270.63 ✓

Foot Bridge Brooklyn Ave & 45th St

	4.67	271.76		267.09	BM 4LT
IT.P	0.21	260.91	1186	259.90	65th Brooklyn
TP	0.30	248.73	1174	248.37	
407 W of W.L. 65th St			1278	235.94	
E. End Foot Bridge Deck					
475.5 W of W.L. 65th St			1557	233.16	
W. end Foot Bridge Deck					

copied from paper by A.F.B

Oct. 23-41

BM 10.80 223.74

SE Top W. of
Imperial
65th St
223.64

TP 0.40 234.54 1221 234.41

TP 0.55 246.35 1154 245.80

TP 0.24 257.34 1189 257.10

6+80.81 = 65th St on Par. 29

BM 1.90 267.09

Lt &
Brooklyn
45th St

6+73 = Fly Edge Block Par. 29

268.99

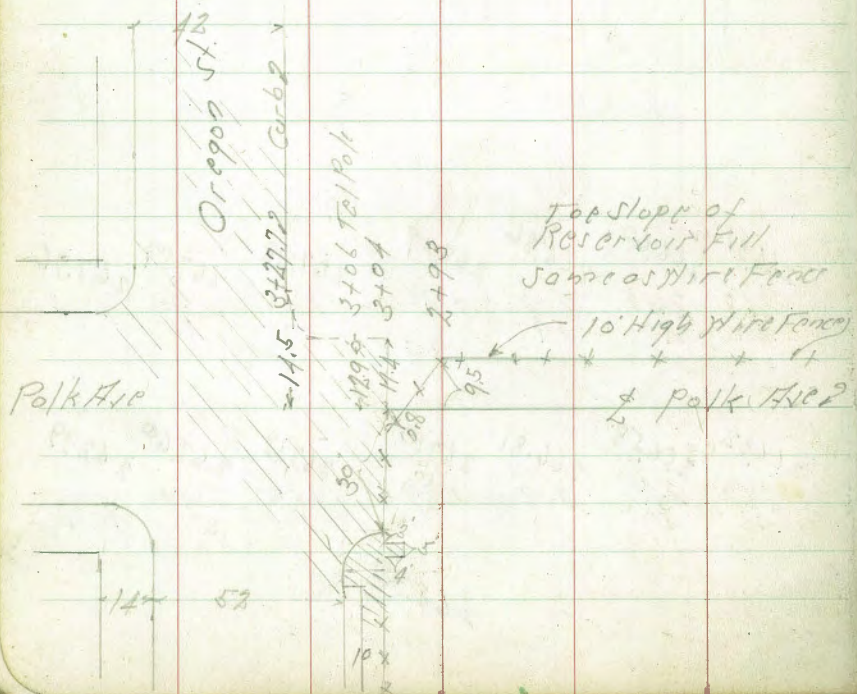
266.31 266.60 266.86 267.09 267.38 267.59 267.96
 2.68 2.89 2.12 1.90 1.81 1.40 1.03
 30 20 10 30 10 20 30

266.32 266.58 266.81 267.10 267.39 267.60 267.99
 2.67 2.41 2.18 1.89 1.60 1.39 1.00
 30 20 10 30 20 30 30

268.99

Location of Improvements
Polk Ave Idaho to Oregon

INDEXED
E.F.B.



B.M. 465 150.07 145.42

0-14 = N Cb line BSt

H Topcb	5.23	144.84
H Gutter	5.84	144.23
Cb	5.69	144.38
1/4	5.42	144.65
1/2	5.28	144.79
3/4	5.02	145.05
Cb	4.86	145.21
F Gutter	4.53	145.54
F Cb	4.09	145.98

0+0 = N.L. BSt

F Cb Top	4.13	145.94
F Gutter	4.83	145.24
1/4	4.82	145.25
1/2	4.95	145.12
3/4	5.26	144.81
H Gutter	5.91	144.16
H Cb Top	5.42	144.65
H L on walk	5.00	145.07

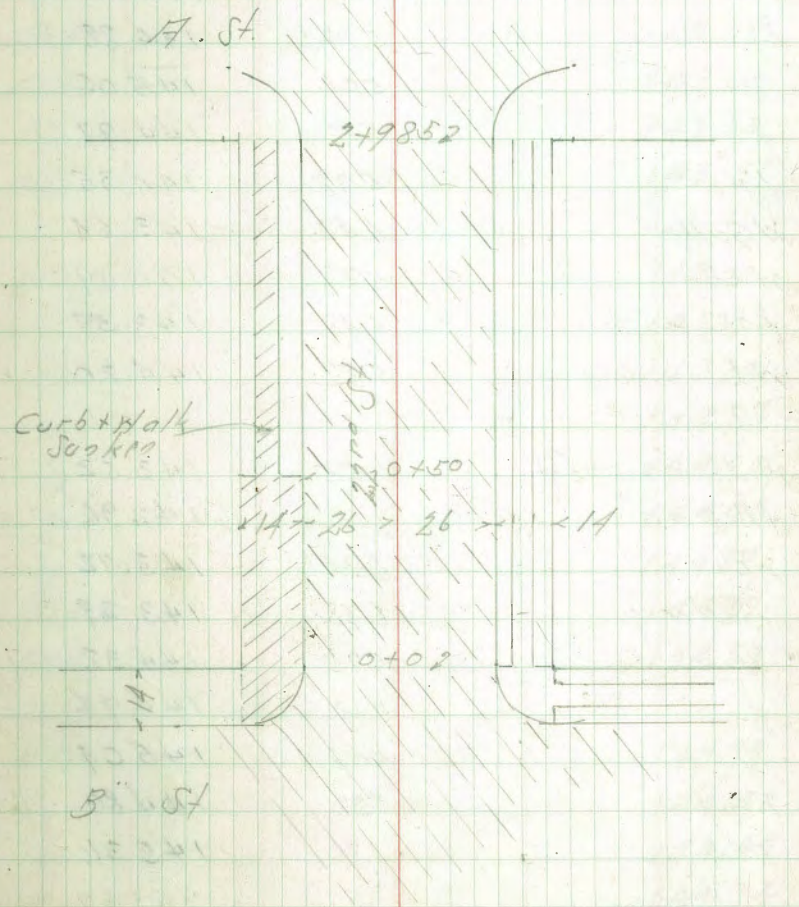
0+14 = Break in Cb x Walk on N

H L on walk	5.50	144.57
H Cb	5.59	144.48
H Gutter	6.09	143.98
1/4	5.42	144.65

Red. Plot. Mobile 1533
S.W.H. 12-12-41

80' wide
14' Cb
13' HSt

Dec. 9-41
S.W.B.P.
H. H. Hart
S. W. L. Moore



150.07

2	4.89	145 18
1/4	4.81	145 26
E Gutter	4.97	145 10
ECb Top	4.41	145 66

0+35

ECb	4.71	145 36
E Gutter	5.19	144 88
1/4	5.01	145 06
2	5.10	144 97
1/4	5.72	144 35
M Gutter	6.43	143 64
M Cb	5.98	144 09
+ 0.8 on Walk	6.48	143 59
M L on Walk	5.87	144 20

0+50

M L on Walk	6.55	143 52
M L 2 on	7.11	142 96
M Cb	6.35	143 72
Gutter	6.78	143 29
1/4	5.75	144 32
2	5.13	144 94
1/4	5.03	145 04
E Gutter	5.27	144 80
ECb	4.86	145 21

150.07

ECb Top	5.30	144.77
Gutter	5.51	144.56
1/4	5.32	144.75
2	5.42	144.65
1/4	5.95	144.12
Gutter	6.93	143.14
M Cb	6.46	143.61
+ 7 on Walk	6.75	143.32
M L on Ground	6.6	143.5

1+0

M L on Ground	7.1	143.0
+ 7 on Walk	7.24	142.83
M Cb	6.73	143.34
Gutter	7.20	142.87
1/4	6.07	144.00
2	5.52	144.55
1/4	5.48	144.59
Gutter	5.70	144.37
ECb	5.54	144.53

1+25

ECb	5.08	144.99
Gutter	5.65	144.42
1/4	5.60	144.47
2	5.73	144.34

58

150.07

1/4	6.11	143.96
H Gutter	6.97	143.10
HCB	6.48	143.59
+7 on Walk	6.32	143.75
H.L. on Ground	6.3	143.8
TP	5.28	149.39
	5.96	144.11

1+50

H.L. on Ground	6.0	143.4
+7 on Walk	5.72	143.67
HCB	5.86	143.53
Gutter	6.37	143.02
1/4	5.53	143.86
1/2	5.21	144.18
1/4	5.02	144.37
Gutter	5.13	144.26
FCB	4.39	145.00

1+75

FCB	4.54	144.85
Gutter	5.30	144.09
1/4	5.24	144.15
1/2	5.42	143.97
1/4	5.84	143.55
Gutter	6.69	142.70
HCB	6.13	143.26
+7 on Walk	6.02	143.37
H.L. on Private Walk	5.9	143.5

149.39

2+0

HCB	6.30	143.09
Gutter	6.90	142.49
1/4	6.05	143.34
1/2	5.62	143.77
1/4	5.42	143.97
Gutter	5.46	143.93
FCB	4.67	144.72

2+50

FCB	5.07	144.32
Gutter	5.80	143.59
1/4	5.79	143.60
1/2	6.05	143.34
1/4	6.53	142.86
Gutter	7.38	142.01
HCB	6.88	142.51

2+98.5 - Cb B.C

HCB	7.38	142.01
Gutter	7.86	141.53
1/4	6.92	142.47
1/2	6.37	143.02
1/4	6.12	143.27
Gutter	6.10	143.29
FCB	5.38	144.01

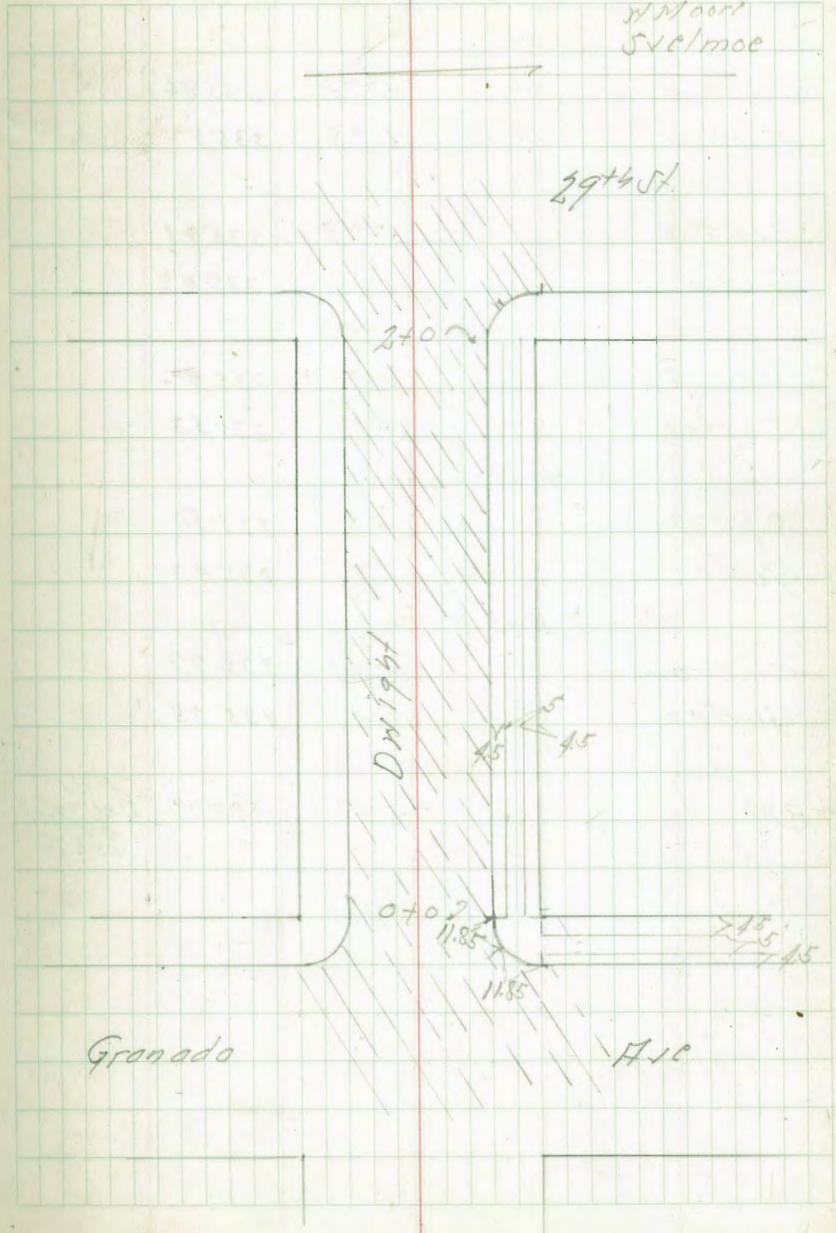
Dwight St. South Curb Levels
Granada Ave to 29th St.

INDEXED
E.P.B.
J.J. BP
Dwight St
Granada

B.M	6.15	341.70	335.55
South End Curb Return			
Top Curb	6.20		335.7
Gutter	6.56		335.04
1/2 Return			
Top Curb	6.11		335.59
Gutter	6.57		335.16
0+0 = E.L. Granada			
Scb Top	6.10		335.60
Gutter	6.37		335.33
0+25			
Scb Top	6.17		335.53
Gutter	6.32		335.38
0+50			
Scb Top	6.11		335.59
Gutter	6.28		335.42
0+75			
Scb Top	6.02		335.68
Gutter	6.23		335.47
1+0			
Scb Top	5.98		335.72
Gutter	6.24		335.46
1+25			
Scb Top	5.91		335.76
Gutter	6.25		335.45

Old Road

Dec. 9. 41
Sisson
W.P. Sisson
S.V.C./moe



3417°

1+5°

Scb Top 5.84 335.86

Gutter 6.28 335.42

1+7.5

Scb Top 5.79 335.91

Gutter 6.25 335.45

2+0 = H.L. 29' 1/2 S

Scb Top 5.88 335.82

Gutter 6.17 335.53

Return

Cb Top 5.80 335.90

Gutter 6.28 335.42

S End Return

Cb Top 5.93 335.77

Gutter 6.35 335.35

BM. 5.93 335.77

S.F.R.P.
D.V. 12/24/54
335.89

Proposed Storm Drain Between

Boundary - Bancroft & Orange Ave
 BM 6.89 365.00 358.11
 TP 5.18 355.90 12.28 352.72

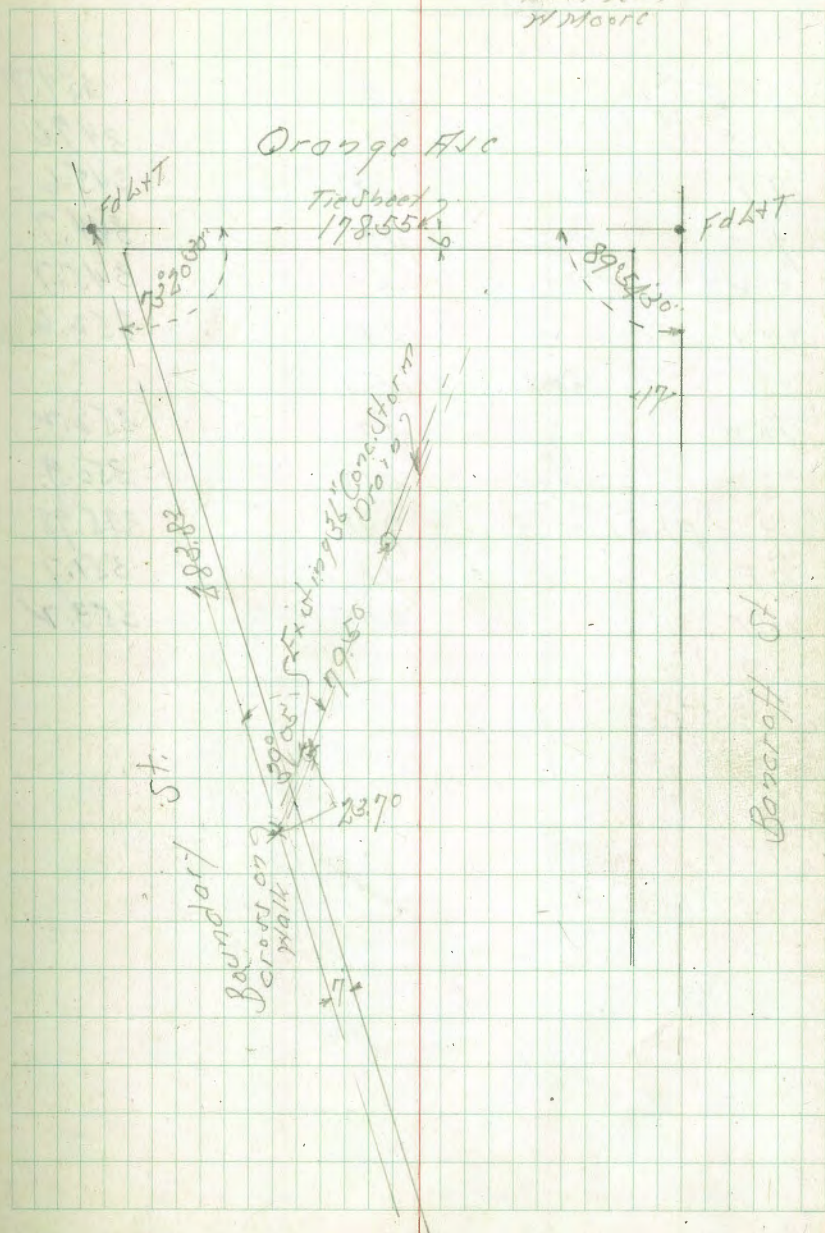
0+0 = 6.5 ft. of Existing 36" Storm Drain

12'E	5.3	350.6
8'	6.8	349.1
8' W = Fly Conc Walk	6.3	349.6
0+06 = 11' 1/2" Conc Storm Drain		
11' W	5.6	350.3
8' = Floor L. 70 3/4" R.C.P.	11.63	344.27
14'E	5.5	350.4
0+30		
17'E	1.8	354.1
5'E	11.0	344.9
8'	11.2	344.7
2' W	11.0	344.9
12' W	4.5	351.4
0+55		
13' W	3.7	352.2
8'E	9.2	346.7
8'	9.9	346.0
9'E	10.1	345.8
12'E	4.8	347.1
20'E	0.4	355.5

Red. & Plotted 2/24/42

Included
 6.5 ft.

Dec. 17-41
 Sisson
 Hartberg
 Moore



55590

0765

20 F	1.2	354.7
11 E	6.3	349.6
9 F	10.3	345.6
7	11.2	344.7
8 W	10.2	345.7
15 W	6.3	352.6

0785.5 = 51/2 End

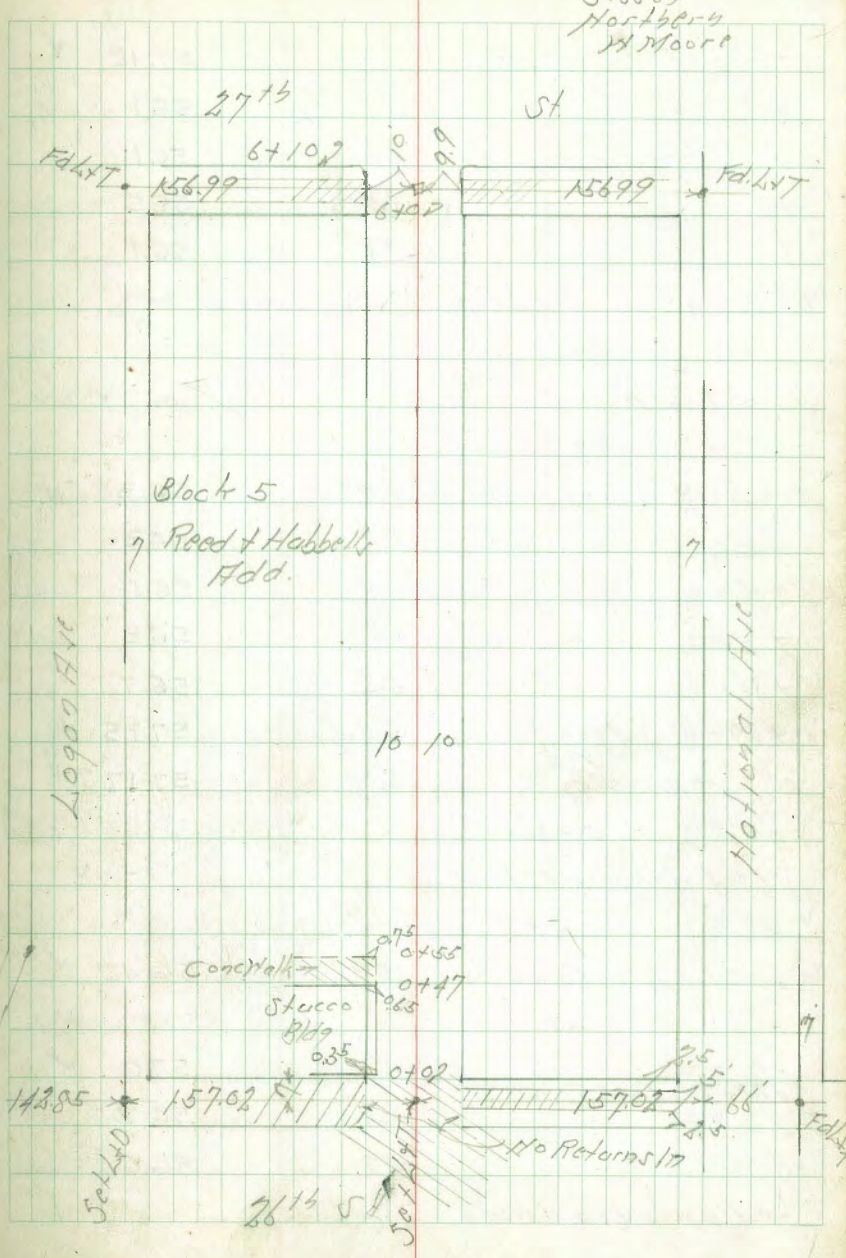
10 W	3.7	352.2
3 W	5.0	350.9
7 = Flow Line	9.9	345.98
5 F	4.2	351.7
10 F	2.7	353.2

Cross Section Alley Block 5 Reed + Habbell
 From 26th St to 27th St. Between Logan + National

Indexed
 as is.

Dec. 17-41
 Sisson
 Northern
 Missouri

B.M.	8.90	58.86	49.96	N.E.B.P. National 426th St.
	0-10 = Fly Conc Walk			
S	on Paving	5.25	53.61	'
L	"	5.02	53.84	'
H	"	4.68	54.18	'
	0+0 = Fly 26th St			
H	on Conc Walk	3.77	55.09	'
L	on Paving	4.22	54.64	'
S	"	4.33	54.53	'
	-0.25 = Fly Wire Fence 0+02			
S	= Fly Power Pole			
	0+25			
S		3.3	55.6	
+3		3.9	55.0	
L		3.7	55.2	
+4		3.4	55.5	
+9.4	= Fly Stucco Bldg	2.6	56.3	✓
	0+45			
H+1.8	= Fly Tel Pole			✓
	0+47			
H+0.65	= Fly Conc Steps	1.67	57.19	✓
	0+51			
S-0.8	= Fly Wire Fence			✓
	0+55			
H	on Fly Conc Walk	1.73	57.13	✓



58.86

+0.75 = Sty Conc Walk	1.74	57.12	✓
+5	2.8	56.1	
$\frac{1}{2}$	2.8	56.1	
+6	3.4	55.5	
5	2.8	56.1	
TP 6.46 62.46	2.86	56.00	✓
0+64			
N+0.9 = Nly Lot 4 Fence			✓
0+75			
-0.5 = $\frac{1}{2}$ 3' Conc Walk	6.08	56.38	✓
5	6.2	56.3	
+5	6.4	56.1	
$\frac{1}{2}$	6.0	56.5	
+8	5.8	56.7	
+8.9 = Sty 4' Conc Walk	5.31	57.15	✓
N on Walk	5.29	57.17	✓
0+82			
S+0.4 = Sty Power Pole			✓
0+97			
S-0.1 = $\frac{1}{2}$ 76 Conc slab	5.97	56.49	✓
1+0			
N 4.1 = Fly Lot 4 Fence	5.5	57.0	✓
$\frac{1}{2}$	5.8	56.7	
5	5.9	56.6	
-0.1 = Nly Board Bldg			✓

65

62.46

1+06			
N+1.0 = $\frac{1}{2}$ Garage Dirt Floor	5.6	56.9	✓
1+12			
N+1.0 = Nly Board Fence			✓
1+21			
S+0.1 = $\frac{1}{2}$ Garage Conc Floor	5.26	57.20	✓
1+30			
N+1.1 = Fly Board Fence			
Nly 5' bed			
1+33			
S = $\frac{1}{2}$ Garage Conc Floor	5.05	57.41	✓
+5	5.6	56.9	
$\frac{1}{2}$	5.3	57.2	
+5	5.2	57.3	
+8	4.6	57.9	
+8.9 = Sty Shed Conc Found.	4.04	57.42	✓
1+44			
S = $\frac{1}{2}$ Garage Dirt Floor	5.2	57.3	✓
1+50			
N = Fly Shed Conc Found	4.08	58.38	✓
+1.8 = Nly Board Fence			✓
+2.2 = Nly Tel Pole			✓
$\frac{1}{2}$	5.0	57.5	
S = Fly Garage	4.9	57.6	✓
-N = Nly Board Fence			✓

62.46			
	1+78		
S-1.1	Fly Board Fence		✓
	1+80		
S-5.0	Fly Do Garage Conc Floor	4.35	58.11 ✓
N+0.9	2.25 Conc Walk	3.92	58.54 ✓
	1+99		
S-5.0	Fly Do Garage Conc Floor	4.30	58.16 ✓
S+0.3	Fly Power Pole		✓
	2+0		
S		4.3	58.2
✓		4.4	58.1
N		4.0	58.5
	2+01		
S-0.4	Fly Board Fence		✓
	2+02		
N+1.7	Fly Board Fence		✓
TP	5.00	63.26	4.20 58.26
N-2.5	Fly Do Garage Conc Floor	4.31	58.95 ✓
	2+09		
S-0.4	Fly Board Fence		✓
	2+19		
N-2.7	Fly Do Garage Conc Floor	4.55	58.71 ✓
S-2.0	Garage Conc Floor	4.77	58.49 ✓
	2+21		
N+0.8	Fly Shed		✓

63.26			
	2+38		
S-0.6	Fly Shed		✓
	2+49		
N+1.1	Fly Shed		✓
	2+50		
N		4.9	58.4
+	2.4	Fly Tel Pole	✓
✓		5.1	58.2
✓		5.4	57.9
	2+55		
S-0.6	Garage Dirt Floor	5.5	57.8 ✓
	2+60		
S-0.6	Fly Board Fence		✓
	2+75		
S-0.6	Fly Board Fence		✓
N+0.8	Fly Picket Fence		✓
	2+83		
S-6.3	Garage Dirt Floor	6.0	57.3 ✓
	2+89		
S-0.5	Fly Board Fence		✓
	3+0		
S	Fly Power Pole	5.3	58.0 ✓
✓		5.3	58.0
N		5.3	58.0

6326

3+17

H = 8 7.5 Conc Walk 5.16 58.10 ✓

H+25 = 5/4 9 Conc Walk 5.42 57.84 ✓

3+27

S-0.8 = Fly Board Fence Wly Shed ✓

3+33

H = 8 5 Conc Walk 5.29 57.97 ✓

H+36 = 5/4 6 Conc Walk 5.46 57.80 ✓

3+43

H+0.4 = 2 Garage Dirt Floor 5.4 57.9 ✓

3+47

S-0.7 = Fly Board Fence Wly Shed ✓

3+49

H+2.8 = Wly Tel Pole ✓

3+50

H 5.2 58.1

L 5.2 58.1

S 5.2 58.1

3+60

H+0.2 = 2 De Garage Dirt Floor 5.3 58.0 ✓

3+70

H-0.2 = Wly Board Fence ✓

3+74

S-1.0 = Fly Board Fence ✓

TP 5.18 63.39 5.05 58.21 ✓

6339

3+98

S-16.3 = 2 De Garage 6.1 57.3 ✓
Dirt Floor

4+0

= 16.1 = Wly De Garage 6.00 57.39
Conc Floor

-1.1 = 5/4 Porch

S 4.8 58.6

L 5.0 58.4

H 5.0 58.4

4+07

H+0.9 = Fly Board Fence Wly Shed ✓

4+15

S-16.1 = Fly De Garage 6.03 57.36
Conc Floor

4+24

H+0.8 = Fly Shed ✓

4+25

S-0.7 = Wly Board Fence

4+30

H 5.2 58.2

L 4.9 58.5

S 4.8 58.6

S 4.7 58.7

4+64

H-1.5 = Wly 3 Car Garage 5.2 58.2 ✓
Dirt Floor

4+76

S-1.5 = Fly Board Fence ✓

H+2.8 = Wly Tel Pole ✓

63.39		
	4+82	
S-1.5	= 1/2 Garage Dirt Floor	4.8
		58.6 ✓
	4+90	
S-1.4	= 1/2 Garage Dirt Floor	4.8
		58.6 ✓
	4+98	
N-0.7	= Fly 3 Car Garage Dirt Floor	4.8
		58.6 ✓
	5+0	
S	= Fly Power Pole	4.6
		58.8 ✓
		4.5
		58.9
+8.8	= 1/4 Do Garage Dirt Floor	4.6
		58.8 ✓
N		4.7
		58.7
	5+23	
N+1.5	= Fly Do Garage Dirt Floor	4.3
		59.1 ✓
	5+46	
S-0.2	= Fly Picket Fence	
		59.1 ✓
	5+50	
N		4.2
		59.2
+1.7	= Board Fence	
		4.2
		59.2
S		4.3
		59.1
	5+68	
S-0.3	= Fly Picket Fence	
		59.1 ✓
	5+76	
-1.4	= Fly House	3.7
		59.7
S		3.9
		59.5

63.39		
	+5	4.6
		58.8
		4.6
		58.8
	+5	4.5
		58.9
	N	3.9
		59.5
	5+97	
N+2.2	= Fly Tail Pole	
		58.6 ✓
TP	3.50	62.03
		4.86
		58.53 ✓
	6+0	= Fly 2.7+5.5
N	Top Cb	3.76
		58.27 ✓
	= Fly Board Fence	
+1.1	= Fly 0.6 Conc Wall	2.36
		59.67 ✓
	+5	4.2
		57.8
	+0.7 Man Hole	4.20
		57.83 ✓
	+5	4.3
		57.7
S	Top Cb	4.25
		57.78 ✓
S	= Fly 0.6 Conc Wall	2.06
		59.97
	6+10	= Fly Cb Line 2.7+5.5
S	Top Cb	4.40
		57.63 ✓
	+0.2 Ground	4.7
		57.3
N	Top Cb	3.93
		58.10 ✓
TP	4.02	59.77
		6.28
		55.75
BM		5.23
		54.54
		NW BP
		Nations
		4.27154
		54.52

3/26/42
Bliss Notes
Summer Street
Bepp. 700

ReX Section of Parking Area South of
Amusement Center Mission Beach

B.M. 5.84 5.24 -0.60

SEBP.
Opp. Fireman's
Place Mission
Bliss

Note: East Edge of
Paving has been damaged

0725 on Paving	4.78	0.46
" 25' East	4.6	0.6
" 50 "	4.5	0.7
" 75 "	4.4	0.8
" 100 "	4.4	0.8
" 125 "	4.6	0.6
" 150 "	4.6	0.6
" 176.8 " Edge walk	4.88	0.36

0750

178.25 East Edge of walk	4.82	0.42
150 " "	4.6	0.6
125 " "	4.7	0.5
100 " "	4.6	0.6
80 " "	4.1	1.1
70 " "	4.6	0.6
50 " "	4.7	0.5
25 " "	4.6	0.6
0700 Ground	4.5	0.7
" " on Paving	4.69	0.55

1100

0700 on Paving Grd Same	4.64	0.60
25' East	4.5	0.7

Red. Plot. Roll 6774
3-30-42 C.B.H.

Indexed
c.s.k. T
524

50' East	4.7	0.5
75 "	4.6	0.6
100 "	4.2	1.0
125 "	4.6	0.6
150 "	4.8	0.4
175 "	4.5	0.6
180 "	4.4	0.8
181 2/3 Edge of walk	4.81	0.43

1150

169.6 East Edge of walk	4.69	0.55
" " Ground	4.6	0.6
150 East	4.4	0.8
125 "	4.1	1.1
100 "	4.3	0.9
75 "	4.3	0.9
30 "	4.5	0.7
25 "	4.7	0.5
0700 Grd	4.4	0.8
" " Paving	4.53	0.71

2100

0700 Grd	4.4	0.8
" " Paving	4.44	0.80
25' East	4.6	0.6
50 "	4.5	0.7
75 "	4.4	0.8
100 "	4.7	0.5

524

125' East	4.1	1.1
133 "	4.9	0.8
140.8 " Edge of walk	4.63	0.61

2750

127.4 East Edge of walk	4.58	0.66
105' East	4.0	1.2
100 "	4.2	1.0
90 "	4.7	0.5
75 "	4.7	0.5
50 "	4.5	0.7
25 "	4.3	0.9
0+00 on paving Grd Same	4.44	0.80

3706

0+00 on paving Grd Same	4.42	0.82
25' East	4.5	0.7
50 "	4.6	0.6
75 "	4.5	0.7
100 "	4.2	1.0
edge of walk	4.32	0.92

T.P. 2.70 6.31 1.63 3.61

3776

94.5 East edge Ped Sidewalk	5.29	1.02
89.5 " Com. Sidewalk	5.05	1.21
75 "	4.8	1.5

631

70

50 East	5.0	0.8
25 "	5.0	0.8
5' "	5.0	0.8
0+00 on paving	5.31	1.00

3785

0+00	5.28	1.03
1' East	4.7	1.6
25 "	4.9	1.4
33 "	4.7	1.6
37 "	4.4	1.9
50 "	4.6	1.7
75 "	4.8	1.5
89.5 " Com Walk	5.03	1.28
94.5 " Ped "	5.36	0.95

4725

94.5	5.32	0.99
89.5	4.96	1.35
80 " East	4.2	2.1
75 " "	4.5	1.8
50 "	4.5	1.8
25 "	4.8	1.5
6 "	4.7	1.6
0+00 Com. Grd Same	5.22	1.09

4775

0+00 on con.	5.15	1.16
1' East	5.0	1.3

25' East	4.6	17
50' "	4.7	16
75' "	4.8	15
89' "	4.9	16
89 ⁵ "	4.70	161
94 ⁵ "	5.23	108
5400		
94 ⁵ East		
89 ⁵ "		
" " on Grd	4.8	15
75 East	5.0	13
50 "	4.6	17
25 "	4.5	18
15 "	4.3	20
0700 Ground	5.0	13
0100	5.03	128
3150		
0700 on Con	4.98	133
" " G-d	4.8	15
10 East	4.7	16
15 "	4.3	20
25 "	4.4	19
50 "	4.2	21
75 "	4.3	20
87 "	4.5	18
94 ⁵ " Redwalk	5.13	1.18

6400		
94 ⁵ East Redwalk	5.05	
89 ⁵ Com "		
" Ground	4.4	19
75 East	4.1	22
50 "	4.1	22
25 "	4.2	21
0700 Grd	4.5	17
" " Com	4.75	156
6425		
0700 on Com	4.66	165
3 East	4.2	21
4 East Com Walk	4.2	21
25 "	4.0	23
50 "	4.0	23
70 "	3.7	26
75 "	4.0	23
89 ⁵ " Grd	4.3	20
" " Com Walk	4.63	168
94 ⁵ Redwalk	4.98	133
6450		
94 ⁵ East	4.94	137
89 ⁵ Grd "	4.4	19
" Walk	4.91	190
75 East	4.1	22
60 "	3.6	27
50	3.6	27

T
6.31

25 East	3.7	2.6
15 "	3.7	2.6
0100 con Grd Same	4.62	
	6.75	
0100 con	4.54	1.77
4 East Cam 61	4.0	2.3
22 "	3.5	2.8
25 "	3.4	2.9
50 "	3.6	2.7
70 "	3.6	2.7
75 "	3.8	2.5
89 ⁵ Grd	4.3	2.0
" Con	4.42	1.89
94 ⁵ " walk	4.91	1.40

7123⁵

94 ⁵ East walk	4.77	1.54
89 ⁵ "	4.24	2.07
75 "	4.0	2.3
50 "	3.8	2.5
25 "	3.6	2.7
10 "	3.6	2.7
4 "	3.9	2.4
0100 on con	4.41	1.90

Note on East 0100 0.06 higher
orig. Rod Man Hold in wrong place

6.3
436
+95

72

Moore
Hazard
Hoopes
5-28-42

McCall = 6.25 1/2 x 5
2 sec Intersection of San Antonio = 7.5 "

SW BP 3.07 7.67 4.60 McCall San Antonio

20' wly of wly line SAN ANTONIA

S cb	1.25	6.92
gut	2.06	5.61
1/4	1.50	6.17
c	1.39	6.28
1/4	1.71	5.96
gut	2.35	5.32
N cb	1.70	5.97
N L	0.8	6.9

wly. S Ant

N L	2.11	5.6
N cb	3.64	9.03
gut	4.02	3.55
1/4	3.65	4.02
c	3.30	4.27
1/4	3.44	4.23
gut	4.98	3.69
S cb	3.23	4.88

w cb

SL cb	3.76	4.91
" gut	4.09	3.58
cb line fav	4.33	3.39

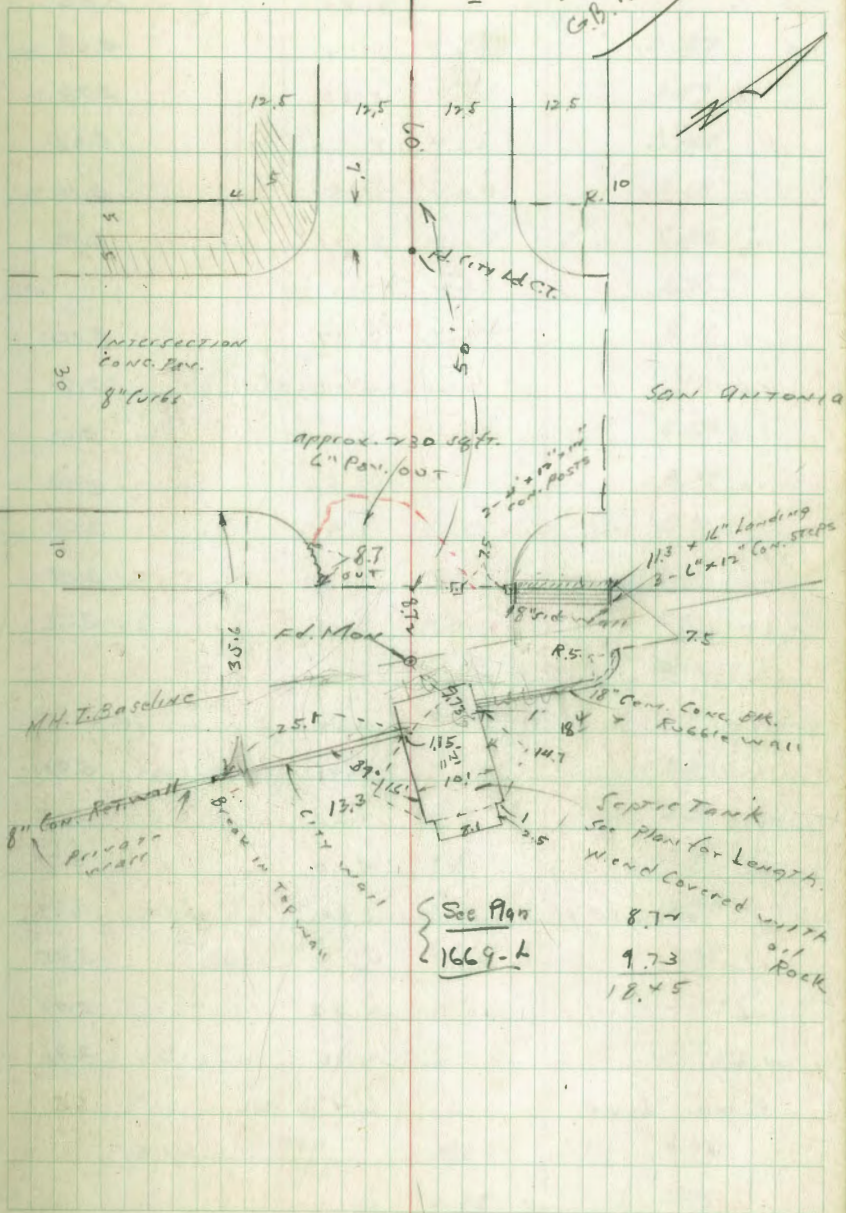
Indexed
C.S.K.

to Rosecrans
Set City disc.

McCall

See
G.B. 203-45

73



See Plan
1669-2

8.71
9.73
18.45
Wend Covered with
oil
Rock

S 1/4	3.84	3.85
c	3.24	4.03
1/2	3.89	3.78
ck Pav.	4.60	8.07
nk gut	4.51	3.16
" cb	3.71	3.96
wily 1/2 S.A.		
nk	4.57	3.10
cb	4.76	2.91
1/2	4.05	3.62
c	3.84	3.83
1/4	3.99	3.68
cb	4.53	3.12
SL	4.11	3.56
E S.A.		
- 10	4.14	3.55
sh	4.26	3.81
cb	4.63	3.02
1/2	4.10	3.57
c on S.M.H. Rim	3.80	3.87
1/2	4.22	3.95
cb	4.88	2.79
nk	4.76	2.91
+ no dirt	6.4	1.5

Ely 1/4		
x	5.10	2.57
cb	5.08	2.59
1/4	4.60	3.07
c	4.49	3.18
1/4	4.42	3.25
cb	4.91	2.76
SL	4.56	3.11
Ely cb San Antonio		
- 40 cb	4.08	3.59
- 40 gut	4.50	3.17
- 20 cb	4.35	3.32
- 20 gut	4.77	2.90
SL cb	4.47	3.20
SL cb	4.54	3.13
sh gut	4.90	2.77
cb on dirt	4.9	2.8
1/4 " "	4.9	2.8
c " "	4.8	2.9
1/4 Pav.	5.19	2.98
cb " has up by St. Dept.	5.43	2.99
nk gut	5.40	2.27
xh cb end	5.05	2.62
Ely San A.		
nk Top 16" Con Top	4.65	3.02
1/2 cb	4.88	2.79

N	GUT	5.22	2.25
N	L	5.25	2.22
C	DIRT	6.6	1.1
C	+V	5.1	2.6
1/4		5.2	2.5
CL	gone	5.1	2.6
S L		4.2	3.5

18.45 Ely of EL SAN ANTONIO

Sec. on line of Ret. Wall

S.L.	Top private wall	5.70	1.97
S.L.	" CITY "	7.60	0.07
S.L.	sand beach	11.7	-3.5
♀	Top city wall	7.65	0.02 Tank and Septic
♀	Beach	11.5	-3.8
+10	Top Tank & wall	7.65	0.02
"	beach	10.8	-3.1
N	Top wall	7.17	0.50
N	beach	10.4	-2.7
	E edge Septic Tank		
Top		7.64	0.03
beach		11.8	-4.1

Notes Reduced - 5.29.92

Bliss
Sommermyer
899

12/15/92 Field Check of Glorietta Heights

Sketch Not to Scale

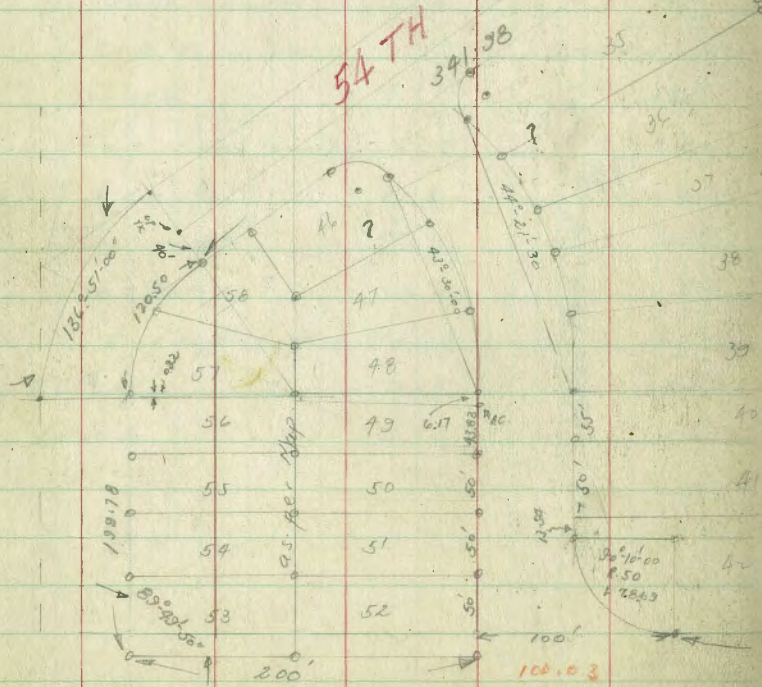
Note: All Lots on outside Boundaries were chained
and check very closely with map.

Copy of Map filed
in Work Order No.
27367, Sub. Abandoned.

REC. 9-29-50

ST.

54TH

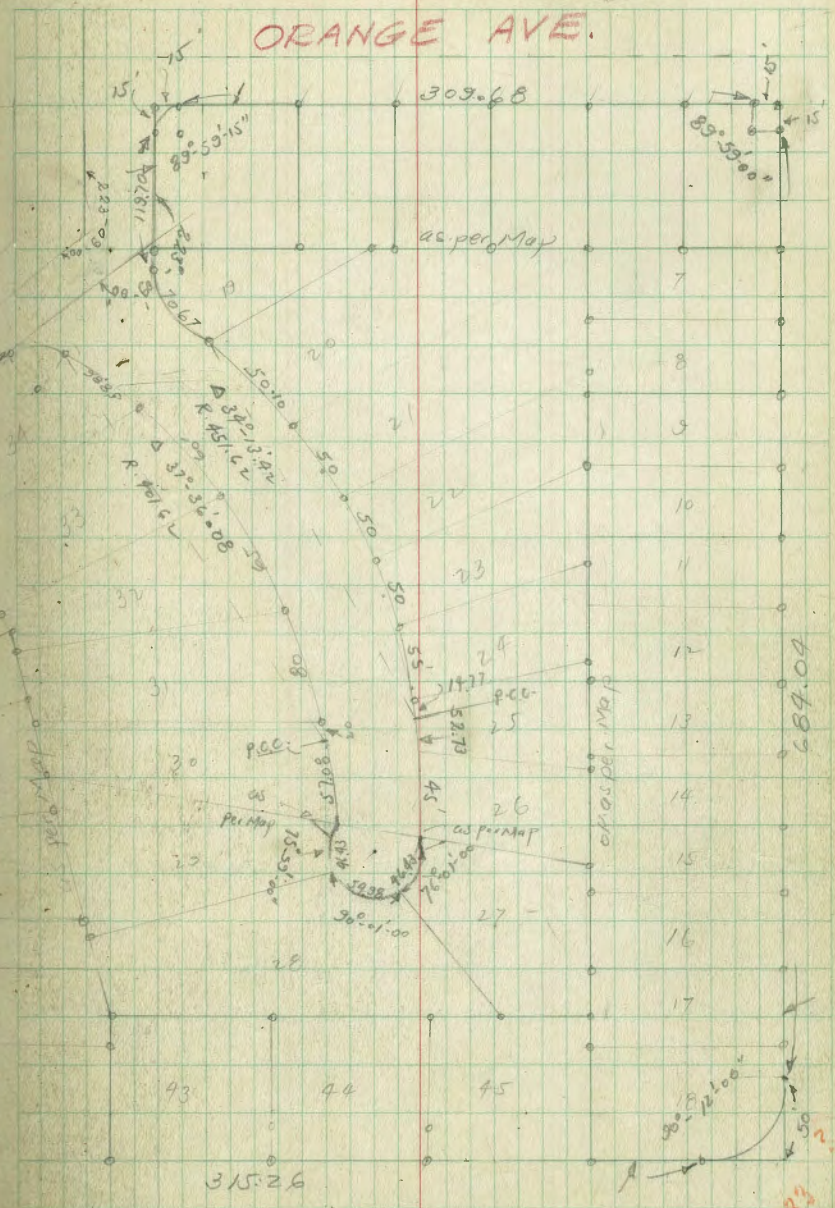


INDEXED
ASK

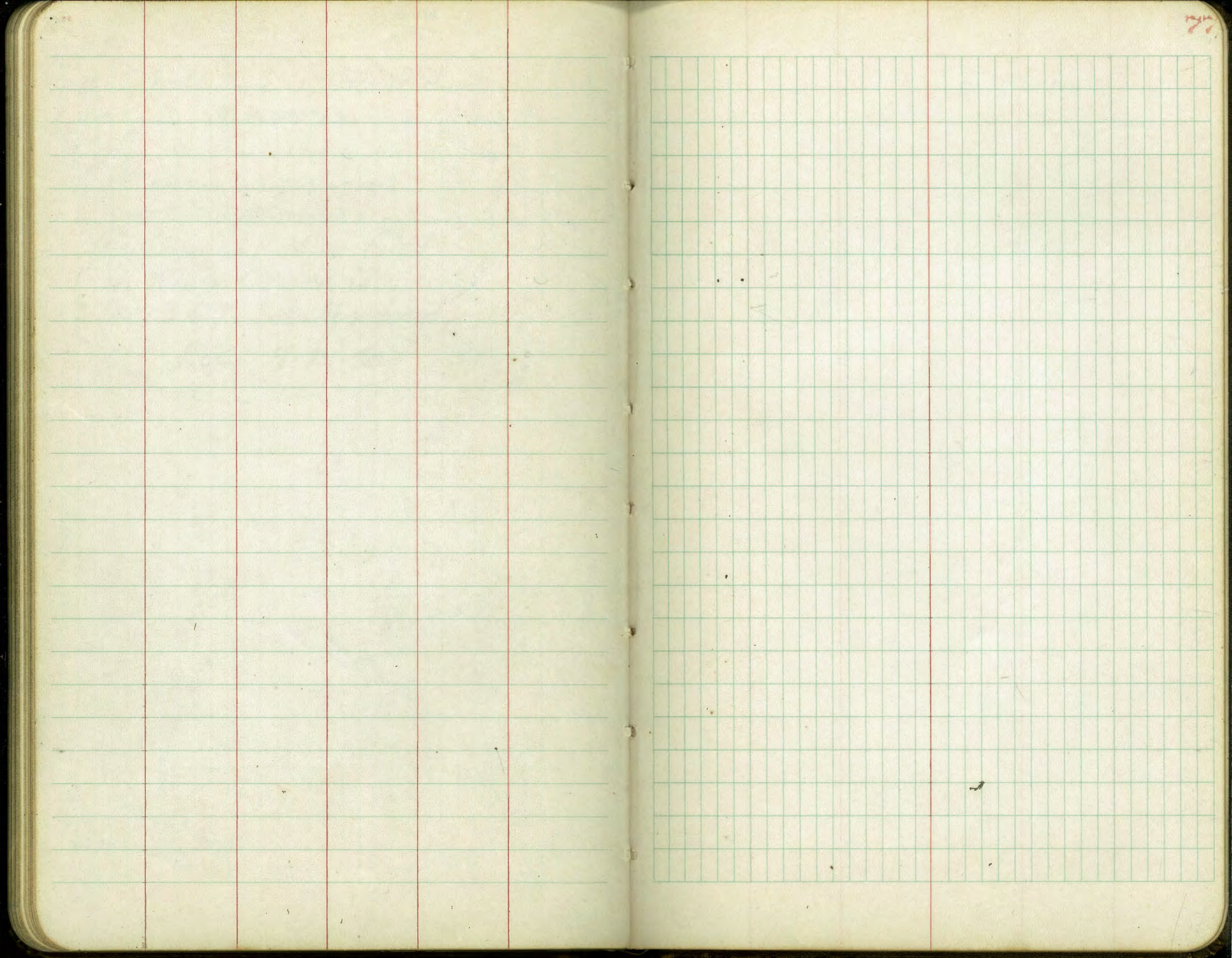
ORANGE AVE.

T.P. 3661
424.75' E.S.

76



T-499.83

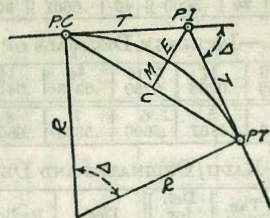


75
5296
127.96

75

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

Radius= $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve= D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)

Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)

Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2})$ (5) $= R \text{vers} \frac{\Delta}{2}$ (6)

External= $E = T \tan \frac{\Delta}{4}$ (7) $= R \div \cos \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)

Long Chord= $C = 2 R \sin \frac{\Delta}{2}$ (10) $\Delta = \text{Central Angle}$

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta=62^\circ 10'$ $D=8^\circ 20'$. From Table IV for 1° curve $T=3454.1$ and $\div 8\frac{1}{2}=414.49$ ft. From Table V correction=.36 or $T=414.85$ ft. P. C.=Sta. P.I.— $T=157+45.50$. Also from (4) $L=746.00$ and P. T.=Sta. P. C. + $L=164+91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset= $7.27 \frac{54.50}{100}=2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26)=2.16$ ft.

Deflections.—Deflection angle= $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft.=(in minutes) $.3 \times C \times D^\circ$ or=defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve=.3 $\times 54.5 \times 8\frac{1}{2}=136.2'$ or $2^\circ 16.2'$, or= $2.50 \times 54.5=136.2'$ from Table III. For Sta. 159 deflection angle= $2^\circ 16.2' + 8^\circ 20' \div 2=6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve $E=960.6$ for $8^\circ 20'=960.6 \div 8\frac{1}{2}=91.27$ and from Table V correction=.10 or $E=91.37$ ft. Or suppose $\Delta=32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E=230.9$ and $\div 42=5.5$ or $D=5^\circ 30'$.

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
91°	5830.5	2444.9	101°	6950.6	3278.1	111°	8336.7	4386.1
10'	5847.5	2457.1	10'	6971.3	3294.1	10'	8362.7	4407.6
20'	5864.6	2469.3	20'	6992.0	3310.1	20'	8388.9	4429.2
30'	5881.7	2481.5	30'	7012.7	3326.1	30'	8415.1	4450.9
40'	5898.8	2493.8	40'	7033.6	3342.3	40'	8441.5	4472.7
50'	5916.0	2506.1	50'	7054.5	3358.5	50'	8468.0	4494.6
92°	5933.2	2518.5	102°	7075.5	3374.9	112°	8494.6	4516.6
10'	5950.5	2531.0	10'	7096.6	3391.2	10'	8521.3	4538.8
20'	5967.9	2543.5	20'	7117.8	3407.7	20'	8548.1	4561.1
30'	5985.3	2556.0	30'	7139.0	3424.3	30'	8575.0	4583.4
40'	6002.7	2568.6	40'	7160.3	3440.9	40'	8602.1	4605.6
50'	6020.2	2581.3	50'	7181.7	3457.6	50'	8629.3	4628.6
93°	6037.8	2594.0	103°	7203.2	3474.4	113°	8656.6	4651.3
10'	6055.4	2606.8	10'	7224.7	3491.3	10'	8684.0	4674.2
20'	6073.1	2619.7	20'	7246.3	3508.2	20'	8711.5	4697.2
30'	6090.8	2632.6	30'	7268.0	3525.2	30'	8739.2	4720.3
40'	6108.6	2645.5	40'	7289.8	3542.4	40'	8767.0	4743.6
50'	6126.4	2658.5	50'	7311.7	3559.6	50'	8794.9	4766.9
94°	6144.3	2671.6	104°	7333.6	3576.8	114°	8822.9	4790.4
10'	6162.6	2684.7	10'	7355.6	3594.2	10'	8851.0	4814.1
20'	6180.2	2697.9	20'	7377.3	3611.7	20'	8879.3	4837.8
30'	6198.3	2711.2	30'	7399.9	3629.2	30'	8907.7	4861.7
40'	6216.4	2724.5	40'	7422.2	3646.8	40'	8936.3	4885.7
50'	6234.6	2737.9	50'	7444.6	3664.5	50'	8965.0	4909.9
95°	6252.8	2751.3	105°	7467.0	3682.3	115°	8993.8	4934.1
10'	6271.1	2764.8	10'	7489.6	3700.2	10'	9022.7	4958.6
20'	6289.4	2778.3	20'	7512.2	3718.2	20'	9051.7	4983.1
30'	6307.9	2792.0	30'	7534.9	3736.2	30'	9080.9	5007.8
40'	6326.3	2805.6	40'	7557.7	3754.4	40'	9110.3	5032.6
50'	6344.8	2819.4	50'	7580.5	3772.6	50'	9139.8	5057.6
96°	6363.4	2833.2	106°	7603.5	3791.0	116°	9169.4	5082.7
10'	6382.1	2847.0	10'	7626.6	3809.4	10'	9199.0	5107.9
20'	6400.8	2861.0	20'	7649.7	3827.9	20'	9228.0	5133.3
30'	6419.5	2875.0	30'	7672.2	3846.5	30'	9259.0	5158.8
40'	6438.4	2889.0	40'	7695.3	3865.2	40'	9292.2	5184.5
50'	6457.3	2903.1	50'	7719.7	3884.0	50'	9319.5	5210.3
97°	6476.2	2917.3	107°	7743.2	3902.9	117°	9349.9	5236.2
10'	6495.2	2931.6	10'	7766.8	3921.9	10'	9380.5	5262.3
20'	6514.3	2946.5	20'	7790.5	3940.9	20'	9411.3	5288.6
30'	6533.4	2960.3	30'	7814.3	3960.1	30'	9442.2	5315.0
40'	6552.6	2974.7	40'	7838.1	3979.4	40'	9473.2	5341.5
50'	6571.9	2989.2	50'	7862.1	3998.7	50'	9504.4	5368.2
98°	6591.2	3003.8	108°	7886.2	4018.2	118°	9535.7	5395.1
10'	6610.6	3018.4	10'	7910.4	4037.8	10'	9567.2	5422.1
20'	6630.1	3033.1	20'	7934.6	4057.4	20'	9598.9	5449.2
30'	6649.6	3047.9	30'	7959.0	4077.2	30'	9630.7	5476.5
40'	6669.2	3062.8	40'	7983.5	4097.1	40'	9662.6	5504.0
50'	6688.8	3077.7	50'	8008.0	4117.0	50'	9694.7	5531.7
99°	6708.6	3092.7	109°	8032.7	4137.1	119°	9727.0	5559.4
10'	6728.4	3107.7	10'	8057.4	4157.3	10'	9759.4	5587.4
20'	6748.2	3122.9	20'	8082.3	4177.5	20'	9792.0	5615.5
30'	6768.1	3138.1	30'	8107.3	4197.9	30'	9824.8	5643.8
40'	6788.1	3153.3	40'	8132.3	4218.4	40'	9857.7	5672.3
50'	6808.2	3168.7	50'	8157.5	4239.0	50'	9890.8	5700.9
100°	6828.3	3184.1	110°	8182.8	4259.7	120°	9924.0	5729.7
10'	6848.5	3199.6	10'	8208.2	4280.5	10'	9957.5	5758.6
20'	6868.8	3215.1	20'	8233.7	4301.4	20'	9991.0	5787.7
30'	6889.2	3230.8	30'	8259.3	4322.4	30'	10025.0	5817.0
40'	6909.6	3246.5	40'	8285.0	4343.6	40'	10059.0	5846.5
50'	6930.1	3262.3	50'	8310.8	4364.8	50'	10093.0	5876.1

TABLE V.—CORRECTIONS FOR TANGENTS AND EXTERNALS.

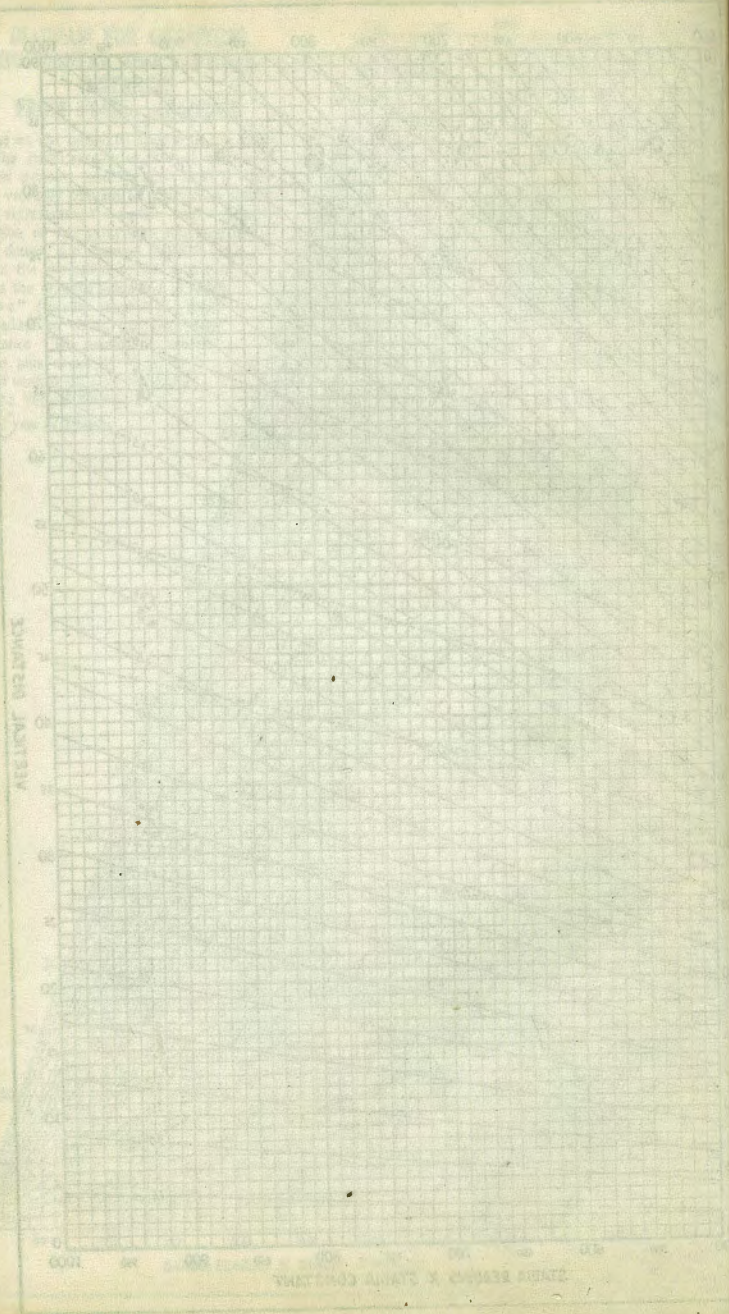
These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table IV) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.58	.65	.72	.79
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.86	.90
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.04	1.14
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.51	4.89
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.85	5.28	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.032	.035	.039	.043	.047	.051	.054
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.266	.353	.440	.528	.617	.707	.797	.877	.971	1.07	1.18	1.29
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790</								



$$\begin{array}{r} 1061 \\ - 375 \\ \hline 1406 \end{array}$$

$$\begin{array}{r} 1061 \\ - 635 \\ \hline 1696 \end{array}$$

$$\begin{array}{r} 524 \\ - 469 \\ \hline 055 \end{array}$$

$$\begin{array}{r} 520 \\ - 432 \\ \hline 088 \end{array}$$

809.04
 23.2
 785.8
 847.5
 2.20
 1049.5
 42
 1053

1143 1143
 695 343
 1838 1486

1242 1242
 875 345
 21.17 15.87

1240
 875
 3615

1385
 179 59.66
 99° 32' 40"
 80° 23' 20"

115
 45
 160

FB 10.55

~~826.44~~
~~868.61~~
~~450.83~~

10.02 1002
 345 5.79
 13.47 15.72

Hub NW 7th - Hancock
 Noel

To Tie Hub. N. of NW 7th - Noel
 Noel

Hub 1. Track. NW to Jolo
 Old

Hub 7th - Noel

103503
 5
 517515
 207066
 587575

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
 For Single Track Embankment.

15.7
 2.5
 18.2
 9.5
 8.7

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) * 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.