

1606



ENGINEERS

LEVEL BOOK

No. 410F

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and

MICRO SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet Wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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1606

CITY ENGINEER

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO,
CALIFORNIA.

The paper stock of this book is made of a high grade 50% rag paper having a water resisting surface. This book is sewed with Bing Special Enamel Waterproof Thread.

Made in U. S. A.

Bliss
Summer Major
Farrow
5/17/41

Sewer Levels for Interceptor Sewer
from U.S. Naval Reservation Line East on
San Antonio St. Note all houses on left of line
are above grade

B.M.	9.23	15.27	11.04	8P Sutcliffe & Kellogg
0100 Naval Res. Line on Ground	3.9	11.4		
0100 on Paring	9.02	11.3		
0100 95 Rt on Top cb	4.30	11.0		Red. by C. P. 4/41
165' Rt on Bank	9.5	5.5		ck. (C) 7/41 Pg. 1-13 inc.
180' " Beach	14.8	0.5		
1400 on Paring	9.77	10.50		
1400 95 Rt Top cb	4.84	10.43		
1405 House on Rt 90 Rt off on Top Foundation	6.57	8.7		
1465 S Line at Kellogg	5.29	10.0		
1478 Gutter	5.68	9.59		
1490 85 S Kellogg	5.03	10.24		
125 Rt on End of Paring	12.76	2.51		
145 Rt Beach	18.3	-3.0		
2403 N Gutter Kellogg	6.20	9.07		
2415 85 N Line Kellogg St	5.83	9.44		
2415 83 95 Rt Top cb	5.80	9.47		
2433 on h. W. Edge at House on Rt	5.86	9.41		
2433 112 Rt on Plumbing of House base	10.1	5.2		
2433 123 Rt Toilet's Basement on base	14.4	0.9		
3700	6.46	8.81		
3700 S Top cb.	6.52	8.75		

53
11.3
91
1

TP	2.75	13.79	4.23	15.27
3423 opp Plumbing of House on Rt			5.12	8.67
3423 71 East to Plumbing of Plumbing			7.3	6.15
3450			5.40	8.39
3469 S Side of house on Rt on to			5.53	8.26
TP	4.62	12.92	5.49	8.30
3469 Floor of House 56' Rt			7.50	5.47
4400			4.93	8.0
4450			5.26	7.66
5100			5.77	7.15
5100 123 Rt			11.5	1.4
" " on Beach			18.5	-5.6
TP	2.09	11.35	3.61	9.31
5415 N Line of Lawrence			4.06	6.89
5428 N Gutter of Lawrence			4.78	6.57
5440 21 E of Lawrence			4.49	6.86
5440 21 66 E Rt on End of Paring			8.30	3.1
" " 86 " " Beach			14.6	-3.2
5453 N Gutter Lawrence			5.29	6.06
5465 21 E Line of Lawrence			4.96	6.39
6400			5.23	6.12
6400 52 Rt on Plumbing of Foundation			11.06	0.29
6450			5.76	5.59

7700		6.33	5.02	
7757	W. Side Drilling on Rt &	6.94	4.41	
7757	56.5 Rt to lower floor.	9.50	1.85	Red. by W. J. 7/22/41
8700	&	7.35	4.00	
"	9.5 Rt Top ch.	7.50	3.85	
8700	30' Rt on Bank	7.4	4.0	
8700	56 Rt on Beach	13.9	-2.5	
+50		7.97	3.38	
+65	S Line McCall	8.20	3.15	
+65	9.5 Rt Top ch.	8.21	3.14	
+77	S Gutter	8.64	2.71	
L ⁴ + 90 ¹⁹	pairing bass net to 0.5 below Transition	8.19	3.16	
TP	3.47 <u>6.48</u>	8.29	3.01	
Check BM	N.W. McCall - San Antonio	2.00	<u>9.98</u> 9.00 - BM 0.98 - Diff	
8790 ¹⁹	20' Rt on End Piering	4.21	2.27	
" "	40 " " Beach	11.3	-4.8	
9700		3.73	2.75	
+04	N Gutter McCall	9.05	2.43	
+15 ²¹	N Line McCall	3.94	2.54	
+50		4.9	1.6	
+70		6.8	-0.3	
+86		8.9	-2.4	

10700		7.4	-0.9	
10700	20 Rt	9.9	-3.4	
" "	50 " on Beach	11.8	-5.3	
+50		7.3	-0.8	Red. by W. J. 7/22/41
11700		7.8	-1.3	
" "	25' Lt	7.2	-0.7	
11700	50 Rt	15.2	-8.7	
+50		9.2	-2.7	
12700		10.0	-3.5	
" "	30' Lt	7.6	-1.1	
" "	40 Rt	14.6	-8.1	
+25		11.1	-4.6	
+50		10.8	-4.3	
+50	25' Lt to Vertical Bank	9.5	-3.0	
13700		11.0	-4.5	
" "	20' Lt Base to Bank	8.1	-1.6	
" "	35 Rt	14.5	-8.0	
13701	125 ft base stairway	8.23	-1.75	
TP	13.36 <u>9.64</u>	10.20	-3.72	
13725		13.5	-3.9	
" "	14' Lt to Base of vertical bank	11.5	-1.9	
" "	17' Lt to Top Bank	+0.9	10.5	

13+25	30' Rt	17.4	-7.8	Red. by Con. 1/22/41
+50		13.3	-3.7	
+50	12' Lt to base of bank 15 " to top bank	11.9 +1.1	-2.3 10.7	
+50	35' Rt	17.3	-7.7	
+57	75 ft side of stormway to base of con stairway base of slab.	12.3	-2.7	
+65	70 ft to N side concrete stairway base	12.3	-2.7	
+70	℄	12.6	-3.0	
+70	10' Lt to base of bank	11.9	-1.8	
" "	12 "	+2.0	11.6	
" "	20 "	+7.0	16.6	
+70	30' Rt	16.8	-7.2	
13+71	℄	12.5	-3.2	
13+82	2' Lt to base of bank	12.3	-2.7	
13+82	Base of bank on ℄	11.9	-2.3	
13+82	1' Lt Top of bank	+7.0	16.6	
" "	13' Lt	+7.8	17.4	
" "	25 "	+8.4	18.0	
13+82	25' Rt	15.6	-6.0	
13+94	℄	2.9	6.7	
" "	4' Lt	+6.9	16.5	
" "	25' Lt	+8.4	18.0	
13+94	2' Rt	12.0	-2.4	
	25' Rt	15.7	-6.1	
14+00	℄	11.1	-1.5	
" "	2' Lt	+0.3	9.9	

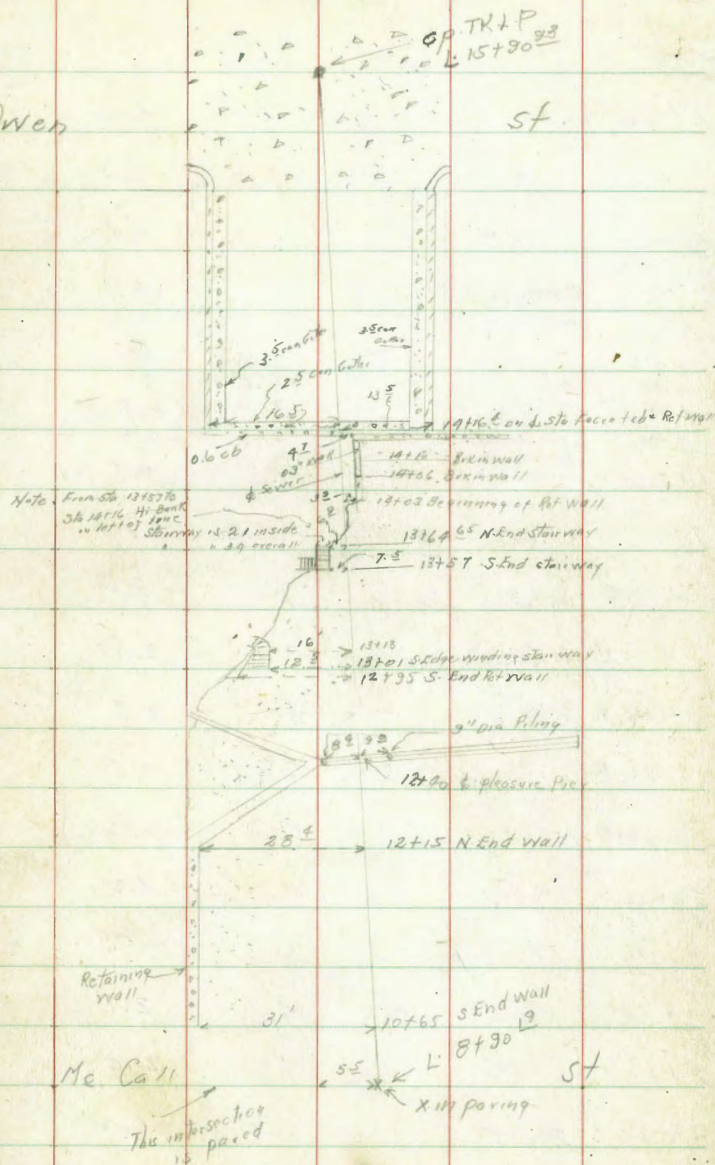
14+00	8' Lt	+8.3	17.9	Red. by Con. 5/22/41
	20 "	+8.4	18.0	
14+00	25' Rt	15.8	-6.2	
14+03	39' Rt inside edge Ret wall	9.30	0.34	
" "	55' Rt outside edge Ret wall	10.05	-0.41	
" "	55' Rt Beach Base wall	11.9	-2.3	
14+06	39' Rt inside edge Ret wall <small>Break in wall See sketch page 4</small>	9.30	0.34	
" "	55' " outside " " "	10.05	-0.41	
" "	55' Rt on Beach	12.0	-2.4	
14+07	℄	0.0	9.6	
" "	6' Lt	+3.2	12.8	
" "	13 "	+5.0	14.6	
" "	20 "	+5.4	15.0	
T.P.	4.36	12.60	1.90	8.24
14+10	℄ <small>Ret wall See sketch page 4</small>	2.2	10.4	
" "	10' Lt	0.0	12.6	
" "	25 "	+1.2	13.8	
" "	48' Rt outside 9" Con Ret wall	6.38	6.22	
" "	48" on Beach	14.6	-2.0	
14+16	04' Top of beach <small>See sketch page 4</small>	6.39	6.21	
" "	55' Rt Top Con Ret wall	6.32	6.28	
" "	55' on Beach	14.6	-2.0	
" "	28' Rt " "	16.8	-4.2	
" "	" Top con Ret wall	5.80	6.8	

T
1260

14+16 ^g	in gutter	6.79	5.81	
" "	16.5 ft W Top cb	5.69	6.91	
" "	25 on Ground	4.6	8.0	
" "	13.5 ft E Top cb	6.86	5.74	
14+19	N Edge connects gutter	6.69	5.91	
+50		5.3	7.3	
15+00		4.1	8.5	
+32	W Edge Res on Pt. 9	3.1	9.5	
+32	46' Pt. low pt in plumbing	5.77	6.83	
+50	"	2.7	9.9	
165 ²³	S Line Owen	2.57	10.03	
+78	S Gutter line Owen	2.88	9.72	
15+90 ²³	L. of Owen on tack	2.03	10.57	
TP	3.56	14.71	1.45	11.15 ✓ 11.17 ✓ check BM NW OWEN San Antonio
15+90 ²³	4.5 ft edge of Porch	9.49	5.22	0.02 diff
	65" on Beach	18.7	-4.0	
16+03	N Gutter line of Owen	5.06	9.65	
+15	N Line Owen	4.65	10.06	
+15	15' Pt. E Top cb	4.68	10.03	
+50		4.3	10.4	
+70		4.2	10.5	
+70	60' Pt. low pt in plumbing at Angiers Resort	6.11	8.60	

Red. by
D. J. J. J.

Owen



McCall

This intersection
is paved

ST

		<u>T</u> 1971		Red. by (19) 1/24/41
17+00			4.3	10.4
+50			5.4	9.3
18+00			7.2	7.5
+20	S. Side of Res on Pt		8.0	6.7
" "	80' RT to west floor <small>Plumbing not available</small>		9.1	5.6
+50			9.3	5.4
+94	S. Side Small Res on Pt		10.8	3.9
+94	30' RT to floor of Res		12.4	2.3
+94	16.5' RT. Possible future Residential Site		15.9	-1.2
19+00			16.1	3.6
T.P.	3.02	<u>6.13</u>	11.54	3.17
+15'	W Line of Perry		3.0	3.2
+15'	15' RT E Top cb		3.60	2.59
1940.8'	to Perry		3.5	2.7
+65'	N Line Perry		3.7	2.5
+65'	15' RT E Top cb		4.23	1.96
20+00			4.0	2.2
" "	180' RT		6.3	-0.1
+50			4.1	2.1
21+00			4.2	2.0
21+00	200' RT		6.4	-0.2
+50			4.3	1.9
22+00			4.5	1.7
" "	260' RT		6.4	-0.2

		<u>T</u> 619		5 0.4 Above of Perry floor of 1940. 165-35 lower than Res
20+50			5.0	1.2
+65 ⁵⁸	S. Line of Quatrough		5.2	1.0
" "	E Top cb		5.20	0.99
+90 ⁵⁸	L. on Ground		5.3	0.9
	<small>on 166'</small>			
T.P. of L	5.34	<u>6.00</u>	5.53	0.66
+90 ⁵⁸	200' RT of Quatrough		5.1	0.9
+90 ⁵⁸	L. 415 RT on Quatrough		7.0	-1.0
23+00			5.3	0.7
+15 ⁵⁸	N Line Quatrough		5.3	0.7
" "	16 ³ RT on Top cb		5.17	0.83
+35			5.3	0.7
"	50' RT		4.9	1.1
"	20' LT		4.2	1.8
+60			5.1	0.9
" "	60' RT		6.7	-0.7
" "	20' LT		4.1	1.9
24+00			5.4	0.6
" "	13' RT		6.6	-0.6
" "	28 "		9.8	-3.8
" "	15' LT		4.6	1.4

		<u>T</u> 6.00	Red. by @ 5/22/41	
24+50			5.6	0.4
" "	4' RT		6.1	-0.1
	20' RT		11.1	-5.1
24+50	15' LT		4.8	1.2
+75			6.2	-0.2
" "	2' RT		7.6	-1.6
" "	20' RT		11.5	-5.5
25+00			8.1	-2.1
" "	12' RT		10.6	-4.6
	10' LT		5.4	0.6
+50			7.7	-1.7
+70			6.3	-0.3
26+00			5.4	0.6
" "	4' RT		6.2	-0.2
" "	20' "		10.2	-4.2
" "	15' LT		2.3	3.7
26+41.5'	2.00.55 RT		3.88	2.12
" " "	10' RT		5.8	0.2
" " "	30' "		10.3	-4.3
" " "	15' LT		7.5	4.5

		T	Red. by @ 5/22/41	
T.P.	3.44	<u>556</u> ✓	3.88	2.12
27+00			2.9	2.7
" "	9' RT		4.5	1.1
" "	12' RT		7.1	-1.5
" "	35' RT		11.1	-5.5
" "	20' LT		+3.0	8.6
+50			2.8	2.8
28+00			3.6	2.0
	13' RT		5.9	-0.3
	14' RT		7.0	-1.4
	30' RT		9.6	-4.0
	20' LT		+0.5	6.1
	40' M.H.T. line		+3.0	8.6
+50			3.3	2.3
29+00			2.6	3.0
	16' RT		5.5	0.1
	18' "		7.0	-1.4
	30' "		9.5	-3.9
	20' LT		+1.5	7.1
+50			2.5	3.1

		Σ <u>5.56</u>			Red. by (W) 5/22/41
30+00			3.2	2.4	
" "	15' RT		5.3	0.3	
" "	17 "		7.0	-1.4	
" "	30 RT		9.6	-4.0	
	25' LT		10.3	5.9	
TP.	9.83	<u>6.76</u>	36.3	1.93	
+50			5.2	1.6	
+54 ⁶³	Top 30" Drain see sketch alignment box 1605		7.73	-0.97	
	6' RT End of Drain Top Pipe		11.86	-5.10	
+59 ⁶⁹	on Ground		8.0	-1.2	Note 29' west of outfall end pipe appears larger than 30" check with 3rd Dept.
+65			5.1	1.7	
30+83 ⁹⁹	L. o. stone		9.89	1.87	
31+00			5.6	1.2	
	8' RT		6.4	0.4	
	9' "		8.2	-1.4	
	30' "		10.5	-3.7	
	25' LT		2.4	4.4	
	40' M.H.T. line		0.2	6.6	
+47			5.7	1.1	
+50			8.4	-1.6	
+56			5.9	0.9	

		Σ <u>6.76</u>			25	27 7 Red. by (W) 5/22/41
32+00			6.0	0.8		
" "	6' RT		6.7	0.1		
" "	8 "		8.3	-1.5		
" "	30 "		11.1	-4.3		
" "	25' LT		2.8	4.0		
" "	59' " M.H.T.		10.7	7.5		
+50			5.9	0.9		
33+00			6.0	0.8		
" "	8' RT		6.9	-0.1		
" "	9' "		8.0	-1.2		
" "	30' "		11.5	-4.7		
" "	30' LT		2.1	4.7		
+56			5.9	0.9		
+6			8.1	-1.3		
+70			5.8	1.0		
34+00			5.9	0.9		
" "	10' RT		7.1	-0.3		
" "	12 "		8.3	-1.5		
" "	30 "		10.7	-3.9		
" "	30' LT		2.6	4.2		

		\bar{x} 6.76		Red. by (2) 7.2
34+50			6.3	0.5
35+00			6.0	0.8
" "	10' RT		7.2	-0.4
" "	11 "		8.1	-1.3
" "	30 "		11.0	-4.2
" "	30 LT		2.8	4.0
" "	56' MHT		0.8	6.0
+50			6.0	0.8
36+00			5.3	1.5
" "	20 RT		7.5	-1.0
" "	35 "		10.0	-3.2
	44' LT MHT		1.1	5.7
+50			4.7	2.1
T.P.	583	<u>8.08</u>	4.51	2.25
+82			5.4	2.7
" "	23 LT MHT		3.8	4.3
37+00			5.7	2.4
+14 ²⁵	L RT on stake		5.07	3.01
" "	13' LT MHT Approx		4.3	3.8
	43' RT		8.4	-0.3
	60 "		11.3	-3.2

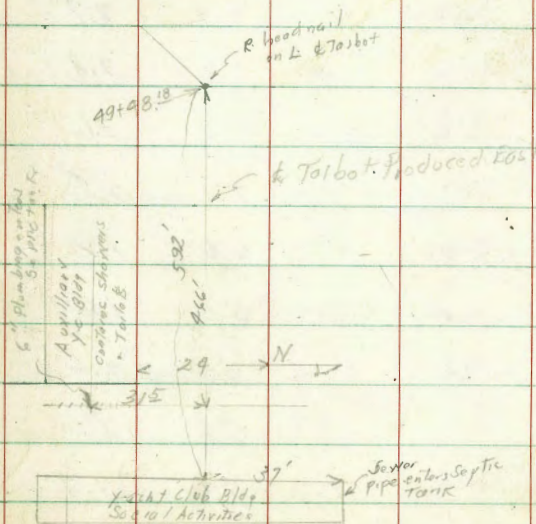
		\bar{x} 8.08		Red. by (2) 7.2/4
37+62			5.6	2.5
" "	21 LT MHT Approx		4.9	3.7
38+00			6.1	2.0
" "	31' RT		8.3	-0.2
" "	39 "		9.6	-1.5
" "	45 "		11.3	-3.2
" "	20 LT		5.2	+2.9
+60	¢		6.2	1.9
" "	32' LT MHT		4.7	3.4
39+00	¢		7.0	1.1
" "	23' RT		8.0	0.1
" "	26 "		9.4	-1.3
" "	40 "		11.3	-3.2
" "	25' LT		5.5	2.6
+50			7.0	1.1
40+00	¢		6.6	1.5
" "	25' LT		5.9	2.2
" "	21 RT		8.2	-0.1
" "	24 "		9.5	-1.4
" "	40 "		12.0	-3.9

		\bar{x} 8.08			Red. by @ 9/22/41
TP	7.54	6.62	9.00	-0.92	
40+46	18" Drain	See sketch Alignment Book 1605-P6 on ground	5.0	1.1	
" "	81' Lt inlet 18" Drain Floor		7.26	-0.64	
" "	88' Rt. outfall end Floor		14.51	-7.89	
" "	88' " " Top Pipe		12.86	-6.24	
+50			5.0	1.62	
41+00	£		4.7	1.9	
" "	25' Lt		3.9	2.7	
" "	22' Rt		5.7	0.9	
" "	29' "		7.9	-1.3	
" "	35' "		10.1	-3.5	
+65			4.9	1.7	
" "	41' Lt. M.H.T.		2.8	3.8	
42+00			5.1	1.5	
" "	22' Rt		6.6	0.0	
" "	23' "		7.9	-1.3	
" "	35' "		10.1	-3.5	
" "	25' Lt		3.6	3.0	
+50			5.9	0.7	
43+00			6.3	0.3	
" "	25' Lt		4.8	1.8	

		\bar{x} 6.62			Red. by @ 9/22/41
43+00	21' Rt		7.8	-1.2	
	25' "		8.5	-1.9	
	35' "		9.8	-3.2	
+65			6.7	-0.1	
" "	38' Lt M.H.T.		4.6	2.0	
44+00			7.1	-0.5	
" "	18' Rt		7.8	-1.2	
" "	35' "		9.7	-3.1	
" "	25' Lt		5.7	0.9	
T.P. station	5.15	5.32	6.45	0.17	
+65			5.7	-0.4	
" "	34' Lt M.H.T.		4.0	1.3	
45+00			6.3	-1.0	
" "	25' Lt		5.4	-0.1	
	30' Rt		6.6	-1.3	
	40' "		7.8	-2.5	
+65			6.2	-0.9	
" "	20' Lt		5.9	-0.6	
" "	27' " M.H.T.		3.7	1.6	
46+00			6.3	-1.0	
" "	15' Lt		5.7	-0.4	

46700	43' Rt	6.5	-1.2
" "	65 "	9.2	-3.9
46739 ⁸⁵	L on stake	5.78	-0.46
" " "	19' Lt M.H.T.	4.5	0.8
" " "	42 Rt Split of Angle	6.8	-1.5
" " "	60 " " " "	9.5	-4.2
462		5.6	-0.3
"	24' Lt M.H.T.	4.0	1.3
47400		5.5	-0.2
" "	15' Lt	5.6	0.3
" "	22 Rt	6.3	-1.0
" "	45 "	8.7	-3.4
460		5.5	-0.2
"	39' Lt	4.1	1.2
48400		6.2	-0.9
" "	35' Lt	4.0	1.3
" "	5' Rt	7.3	-2.0
" "	35 "	10.0	-4.7
450		7.0	-1.7
"	30' Lt	4.4	0.9
"	30 Rt	9.5	-4.2

48480		5.5	-0.2	
" "	30' Rt	9.0	-3.7	
" "	6 Lt Base Room	4.8	0.5	
	15 " Top Base	2.4	2.9	
49400		1.8	3.5	
T.P.	3.87	<u>7.61</u>	1.58	3.74
T.P.	4.31	<u>7.62</u>	4.30	3.31
T11			4.2	3.4
T20	oil parking		5.67	1.95
+ 448 ¹⁸	L on Redhead nail		4.65	2.97



49408 ¹⁸	100 Rt on L Tolbot	4.7	2.9
" "	200 " " " "	5.1	2.5

		π 762		Red. by @ 5/22/41
49+98 ¹⁸	300 Rt on $\frac{1}{2}$ Talbot	5.7	1.9	
" "	400 " " " "	6.4	1.2	
" "	466 Rt 6" $\frac{1}{2}$ inch center to top pipe	7.40	0.22	
" "	500 " " " "	6.6	1.0	
" "	592 " " " "	6.2	1.4	
" "	" Floor at Y.C. Bldg	3.4	4.2	
" "	" Top of 6" plumbing			
" "	" Waccawetches Sptic Tank	5.87	1.75	
" "	466 Rt Floor aux Bldg	6.70	0.92	
49+03 ¹⁸	N Line Talbot	4.7	2.9	
50+00		5.0	2.6	
" "	150 Rt.	5.2	2.4	
+25		4.9	2.7	
+45		3.8	3.8	
+70		4.0	3.6	
51+00		5.1	2.5	
" "	100 Rt	6.4	1.2	
" "	200 "	6.0	1.6	
" "	50' Lt	5.0	2.6	
# Note	Ground on left 15' above it			
+50		5.6	2.0	
+70		5.9	1.7	
52+00		4.6	3.0	
" "	150 Rt	6.8	0.8	
" "	250 "	7.0	0.6	

		π 762		\$ Cont'd 727	11
52+50			5.5	2.1	Red. by @ 5/22/41
53+00			5.7	1.9	
" "	150 Rt		7.2	0.4	
" "	300 "		7.4	0.2	
" "	612	8.85	4.89	2.73	
+50			6.5	2.4	
+70			6.2	2.7	
54+00			4.7	4.2	
" "	50 Rt		7.3	1.6	
" "	150 "		8.1	0.8	
" "	350 "		8.5	0.4	
+13 ¹⁸	20' Stab		4.68	4.17	
+50			5.6	3.3	
" "	W Line Canyon		6.87	1.98	
" "	160' Top "		7.56	1.29	
+88.23	\$ Canyon		7.85	1.00	
" "	210' Rt end of Paring		10.10	-1.35	
" "	300 "		9.9	-1.0	
" "	300 Rt 50 S		8.7	0.2	
" "	400 "		9.4	-0.5	
" "	400 Rt 100 S		7.9	1.0	
" "	" 100 N		7.7	1.2	

		<u>8.85</u>		Red. by ① 5/22/41
13	500 ft on Canyon	7.7	1.2	
	" " 150 S	7.5	1.4	
	" " 100 N	8.0	0.9	
	600 ft on Canyon	8.3	0.6	
	" " 150 S	8.0	0.9	
	" " 100 N	8.5	0.4	
	637 ft on Canyon of same	9.2	-0.3	
	" 150 S	9.0	-0.1	
	" 80 N	9.4	-0.5	
55+00	on Farm	7.77	1.08	
+13	N Gutter Canyon at Farm	7.57	1.28	
+23	N Line Canyon " "	6.90	1.95	
+50		7.1	1.8	
56+00		7.6	1.3	
+29	SS side at track between Bldgs	7.57	1.28	
+30 ^E	" " " "	7.60	1.25	
+30 ^S	.25' Pt Floor of Tunnel	7.19	1.66	
56+60	S Line Addison	7.5	1.4	
56+95 ⁵⁴	6.88 E Addison <u>8.00</u>	7.73	1.12	
	100 ft on E Addison	6.4	1.6	
	200 " " " "	6.8	1.2	

		<u>8.00</u>		9.6 Red. by ① 5/22/41
	200' Pt 60 N	6.6	1.4	
	300' Pt	8.1	-0.1	
	300 " 50 S	7.1	0.9	
	" " 60 N	11.4	-3.4	
	395 Pt E Addison	8.5	-0.5	
	355 " " "	10.7	-2.7	
	" " 50 S	7.7	0.3	
	400 Pt E Addison	9.6	-1.6	
	" " 75 S	8.4	-0.4	
	" " 100 N	10.4	-2.4	
	950 ^S E Addison	14.6	-6.6	
	" 75 S	8.4	-0.4	
57+00		6.9	1.1	
57+30 ⁵⁴	East Line Addison	7.0	1.0	
+50		7.1	0.9	
58+00		6.9	1.1	
	200 Pt	6.6	1.4	
+50		7.4	0.6	
59+00		7.2	0.8	
	35' Pt	6.9	1.2	
	150 "	12.0	-4.0	

		T 8.00		
TP on P.O.T 59+43.85	4.07	6.84	5.23	2.77
59+30 th S. Line Byron			6.8	0.0
59+65 th E. Byron on ix th shore			8.07	-1.23
" " 35 Pt on E. Byron			6.6	0.2
" " 55 " " "			9.8	-3.0
" " 125 " " "			8.3	-1.5
" " 150 " " "			11.6	-4.8
60+00 th N Line Byron			8.9	-2.1
+50			9.3	-2.5
61+00			9.2	-2.4
" 56' Lt			8.4	-1.6
" 84 Pt			8.0	-1.2
" 110 "			11.7	-4.9
+35			9.4	-2.6
+53			8.0	-1.2
+60			5.6	1.2
62+00 ³¹ S Line Carleton			5.2	1.6
+22			6.0	0.8
+35 ³² on ix th shore E. Carleton			9.68	2.16
T.P.	10.63	16.97	0.50	6.34

Red. by
② 5/22/41

ck. (W. Scott/41)
Pg. 1-13 inc.

		T 16.97		
T.P.	8.74	23.52	2.19	14.78
T.P.	8.31	28.84	2.99	20.53
T.P.	6.96	35.29	0.51	28.33
B.M.			4.41	30.88
				30.91
				0.03 diff
B.M.	6.89	9.05		2.16
62+41 ³³ L. 14' ix th shore E. Wood Gutter		6.80		2.25
" " 20' Pt			10.9	-1.8
" " 75 "			10.4	-1.3
+50			7.2	1.9
+75 on Top Dump			4.9	4.2
" on Ground			6.9	2.2
63+00			7.1	2.0
+50 on Dump			5.5	3.6
" on Ground			6.3	2.8
64+00			6.1	3.0
" " 100 Pt			7.6	1.5
64+00 S. Top Ck 23' Lt		6.19		2.89
+50		5.2		3.9
65+00		4.6		4.5
+50		3.9		5.2
+87 ³⁴ on pairing S Line of Scott		4.08		4.99
+92.27 into section existing sewer		3.85		5.20
Flow exists N.H. 11' top of		15.93		-6.88

Red. by
② 5/22/41

NE Locust
Canyon Rd

B.M. ixth shore
E. G. Gutter

Red. by
② 5/29/41
Pg. 13-21

ck. (W. Scott/41)
Pg. 13-21

		<u>X</u> 905		
66+00			3.73	5.32
66+11 ²²	L.Rt		3.57	5.48
+40 ²²	N.Line of Carleton		3.88	5.17
" "	E.Top cb		3.88	5.17
T.P.	2.85	<u>8.53</u>	3.37	5.68
+50			3.44	5.09
67+00			4.02	4.51
+50			4.61	3.92
68+00			5.10	3.43
" "	11' Rt. Top cb		4.94	3.59
+40 ²	End of paving		5.52	3.01
59'	S. Gutter Dickens		5.6	2.9
68+75 ⁹⁸	E. Dickenc on slab		5.13	3.40
" "	29' box line ex M.H. 2' 8" high		14.52	-6.00
" "	100' Rt on E. Byron		5.1	3.4
" "	113' Rt W. End Kottenborgs Boat factory on floor		8.13	0.40
" "	185' Rt		5.0	3.53
" "	200' Rt		9.2	-0.7
" "	200' " 100' North		10.7	-2.2
" "	200' " 75' S		9.0	-0.5
89+68	E. G. Ter		5.9	2.6
69+00			5.9	2.6

		<u>X</u> 853		
+10 ⁹⁸	E. Line Dickens		5.8	2.7
+50			5.7	2.8
70+00			6.3	2.2
" "	75' A		8.1	0.4
" "	165' "		10.6	-2.1
+50			6.9	1.6
71+00			7.6	0.9
+10 ⁴⁹	S. Line Emerson		7.6	0.9
+45 ⁴⁹	E. Emerson ^{stubout}		7.9	0.6
" "	60' Rt		9.1	-0.6
" "	100' " on E. Emerson		13.2	-4.7
+80 ⁴⁹	N. Line of Emerson		8.8	-0.3
72+00			9.0	-0.5
T.P.	3.19	<u>2.92</u>	⁸⁰ 8.23	-0.27
+50			3.9	-1.0
73+00			4.3	-1.4
" "	10' Rt		4.2	-1.3
" "	25' "		7.0	-4.1
+50			5.3	-2.4
+70			6.1	-3.2
+80 ⁶⁵	S. Line Fenelon		6.2	-3.2

T
2.92

7400			6.4	-3.5
+15 ⁶⁶	E. Fenelon on stn		6.53	-3.61
" "	40' Pt on Fenelon		7.7	-4.8
+50 ⁶⁶	E line Fenelon		6.7	-3.8
7500			6.4	-3.5
" "	20' Pt		6.7	-3.8
	30' "		7.7	-4.8
T.P.	6.01	2.40	6.53	-3.61
+50			6.6	-4.2
7600			7.0	-4.6
" "	40' Pt		7.6	-5.2
+53 ⁶²	S line Garrison		7.3	-4.9
+85 ⁶²	E. " on stn		7.92	-5.02
"	50' Pt on Garrison		7.7	-5.3
7700			8.2	-5.8
+15			7.4	-5.0
+20 ⁶²	N line Garrison		7.2	-4.8
+50			7.0	-4.6
7800			6.9	-4.5
" "	50' Pt		7.6	-5.2
+50			6.4	-4.0

15

T
2.40

7900			5.2	-2.8
" "	100' Pt		5.2	-2.8
+20			3.9	-1.5
+20 ⁶⁰	S line Hugo		1.1	1.3
+79 +55 ⁶⁰	on stn E. Hugo		1.33	1.07
T.P.	5.40	6.47	1.33	1.07
+79 +55 ⁶⁰	60' Pt on Hugo		4.2	2.3
" "	'75" " " Beach		8.5	-2.0
+90 ⁶⁰	N line Hugo		5.3	1.2
8000			5.3	1.2
+50			5.0	1.5
8100			4.9	1.6
" "	300' Pt		5.0	1.5
+50			4.6	1.9
+90 ³⁴	S line Ingle		5.5	1.0
8200			5.7	0.8
+25 ³⁴	E. Ingle		6.88	-0.41
+60 ³⁴	N line "		7.2	-0.7
4 90% Ground on Pt 13 above E.				
8300			7.0	-0.5
+50			6.9	-0.4

17
6.97

84400			6.7	-0.2
+60 ⁵⁶	S. Line Jarvis		6.3	0.2
+95 ⁵⁶	E. Jarvis		6.18	0.29
T.P.	5.14	<u>5.43</u>	6.18	0.29
85400			5.1	0.3
+70 ⁵⁶	N. Line Jarvis		5.2	0.2
+50			5.1	0.3
86400			5.4	0.0
+50			5.6	-0.2
+55	S. Side House on R.		5.6	-0.2
"	37' R. to Plumbing		5.50	-0.1
87400			5.9	-0.5
+70 ⁴⁰	S. Line Keats		5.9	-0.5
+65 ²⁰	E. Keats on stake		5.93	0.00
"	85' R. E. Keats		6.3	-0.9
"	" 56' North Floor House		4.50	0.93
87465 ⁴⁰	109' R. on E. Keats		6.4	-1.0
"	" 95' N Plumbing on floor		5.30	0.13
"	" 146' R. W Side Res on South		6.3	-0.9
"	" on plumbing E. 6550'		5.90	-0.5

17
5.43

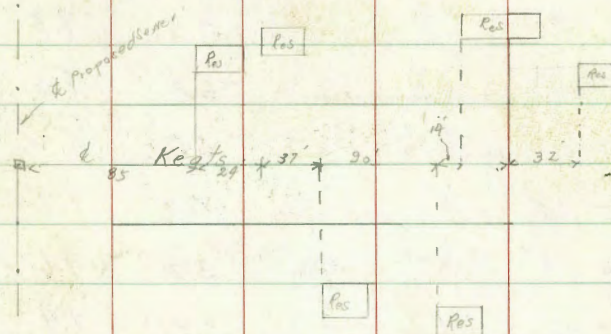
53
35
18

16

87465 ⁴⁰	700' R. E. Keats		6.2	-0.8
"	" " " W side of Res on stake		6.3	-0.9
"	" " " 120' S. Top Plumbing See 2041 page 17		3.50	1.9
"	" " " 250' R. on E. Keats		6.6	-1.2
"	" " " at Res 115' North Floor		4.50	0.9
87465 ⁴⁰	282' R. on E. Keats W Side Res on North		6.2	-0.8
"	" " " 81' N. on Floor		4.20	1.2
"	" " " 300' R. E. Keats		6.1	-0.7
"	" " " 360' " " "		6.7	-1.3
"	" " " 400' "		5.4	0.0
"	" " " 475' " " "		2.4	3.0
+ note Ground from Here on East 1/2 level out to Bay. Approx 2000'				
88400 ⁴⁰	N. Line Keats		5.6	-0.2
+50			5.1	0.3
+82	at House on R.		5.0	0.4
"	35' R. to Floor		2.80	2.63
89400			4.9	0.5
+28	House on R. E.		4.9	0.5
"	35' R. on floor		3.30	2.13
90400 ⁴⁰	S. Line at level		4.8	0.6
90435 ⁴⁰	E. Lower on stake		4.21	1.22

		<u>5.43</u>		
TP.	358	<u>4.80</u>	421	1.22
21+00			45	0.3
" "	75 RT		45	0.3
Note: Ground disabere 9 on left				
+50			50	-0.2
22+00			5.1	-0.3
+30	N Side Rec on RT	4	50	-0.2
"	Plumbing 73' RT		4.20	0.6
+50			4.9	-0.1
23+00			4.8	0.0
+53	East Side Rec on P	4	5.0	-0.2
	60' RT on floor		2.40	2.40
24+00			4.8	0.0
+11.76	L.L.F		4.50	0.30
T.P.	1153	<u>11.83</u>	4.50	0.30
+43			11.1	0.7
+50			8.8	3.0
+55			4.2	7.6
+64.74	POT on stake		4.03	7.80
+71			6.0	5.8
+72			8.5	3.3

Lowell



Jarvis

T
11.83

+80			8.9	2.9
+81			5.5	6.3
95+00			5.3	6.5
+50			5.1	6.7
96+00	# Ground Has a very slight slope toward bay approx 4m		5.5	6.3
+50			4.9	6.9
+75			9.8	7.0
+85			2.0	9.8
+90			2.5	9.3
97+00	So. Side narrow channel		6.8	5.0
+14	No. "	"	6.6	5.2
+22			1.9	9.9
+24			2.2	9.6
+30			3.9	7.9
+50			3.8	8.0
9.8+00			4.1	7.7
+50			4.5	7.3
99+00			4.4	7.4
TP on Pt.				
99+22.22	5.43	13.06	4.20	7.63
+50			5.1	8.0

T
13.06

18

100+00			5.3	7.8
+50			5.1	8.0
101+00			6.2	6.9
+50			5.8	7.3
102+00			5.4	7.7
+50			5.1	8.0
103+00			5.5	7.6
+50			5.5	7.6
104+00			5.4	7.7
+50			5.5	7.6
105+00			5.8	7.3
+50			5.9	7.2
106+00			5.8	7.3
+50			5.7	7.4
TP on Pt. 106+99.13	5.67	12.84	5.89	7.17
107+50			6.1	6.7
108+00			6.3	6.5
+50			5.5	7.3
109+00			5.8	7.0
+50			5.8	7.0

		\bar{x}		
		<u>12.84</u>		
110+00			5.2	7.6
+50			5.1	7.7
111+00			5.6	7.2
+50			6.1	6.7
112+00			6.5	6.3
+50			6.5	6.3
113+00			6.3	6.5
+11.32	on 1st stake	interactions Navy sewer	6.21	6.63
"	"	Flowline M. Hookett	21.36	-8.52
"	"	" " " " " " " " " " " "	21.90	-9.06
+50			5.6	7.2
114+00			5.8	7.0
T. Pan Pot.	6.27			
11414.92	on 1st stake	<u>12.91</u>	6.20	6.64
+50			6.4	6.5
115+00			6.4	6.5
+50			6.6	6.3
116+00			6.7	6.2
+50			6.3	6.6
117+00			5.4	7.5
+50			5.4	7.5

		\bar{x}		
		<u>12.91</u>		
118+00			5.2	7.7
+50			5.6	7.3
119+00	on 1st stake		6.61	6.30
+50			8.0	4.91
120+00			9.0	3.91
+50			9.6	3.3
TP.	6.33	<u>10.76</u>	8.48	4.43
121+00			7.8	3.0
+50			8.1	2.7
122+00			8.3	2.5
± From 122+00 to 122+60 Navy Trash Dump				
+50			7.9	2.9
+60			5.2	5.6
123+00			5.2	5.6
+50			4.8	6.0
+65.5000				
123187.23			3.83	6.93
124+00			3.8	7.0
+50			2.7	8.1
+11.000				
			4.15	6.61
125+00			2.7	8.1

7
10.76

125+50		28	8.0
+65	Fence	28	8.0
+67	Begin Top Soil Pk	28	8.0
TP	5.00	13.14	2.62 8.14
126+00	Topcb	5.37	7.77
" "	Getter paving	5.74	7.40
" "	Ground	5.0	8.1
+50	"	5.3	7.8
127+00	Topcb	5.07	8.07
	Ground	5.9	7.7
+50	Ground	5.0	8.1
128+00	Topcb	4.75	8.39
" "	Ground	5.0	8.1
+50	"	5.0	8.1
129+00		4.58	8.56
" "	Ground	5.0	8.1
+50	"	4.7	8.4
	Warden Road on Paving	5.26	7.88
130+00		5.31	7.83
+50		4.8	8.3

20

7
13.14

TP	5.50	14.10	4.54	8.60
Set BM			2.65	11.45
131+00	Topcb		5.35	8.75
	Ground		5.4	8.7
+50			5.2	8.9
132+00	Topcb		5.09	9.01
	Ground		5.1	9.0
+50			5.2	8.9
133+00	Topcb		5.45	8.65
	Ground		5.5	8.6
+50			5.69	8.41

8' 90°
 S. Side
 132+94.5
 POWDER Magazine
 8' 90°
 N. Side
 132+82.5
 Concrete walls
 E. Side

137+82.5	S. Side Powder Mag. Floor	11.00	3.10
132+94.5	N. Side " "		
134+00	Topcb	5.89	8.21
	Ground	5.9	8.2
+50		5.9	8.2

		<u>π</u> 19.10		
135+00	Topcb		5.73	8.37
"	Ground		5.6	8.5
+50	"		5.5	8.6
136+00	Topcb		5.33	8.77
"	Ground		5.3	8.8
+50			5.1	9.0
T.P.	5.63	<u>14.60</u>	5.13	8.97
137+00	Topcb		5.57	9.03
	Ground		5.6	9.0
+50	"		5.8	8.8
138+00	Topcb		5.92	8.68
	Ground		5.9	8.7
+50	"		6.1	8.5
139+00	Topcb		5.81	8.79
"	Ground		5.8	8.8
+50	"		5.6	9.0
140+00	Topcb		5.40	9.2
"	Ground		5.3	9.3
"	to Roseroll Road	on Barrig	5.60	9.00
141+00	Topstone	at	5.57	9.03
141+00	Topcb		5.11	9.49

		<u>π</u> 14.60			21
TP	4.69	13.94	5.35	9.25	Red. by C. J. J. J. J. Pg. 13-21
TP	11.89	24.27	1.56	12.38	
T.P.	12.75	36.20	0.82	23.45	ck. (W. G. J. J.) Pg. 13-21
T.P.	13.15	48.33	1.02	35.18	
TP	4.90	51.92	1.31	47.02	
Check BM			3.25	48.67	N.W. Reservoir + Dumas
				48.50	
				0.17 Diff	
BM	7.87	56.37		48.50	N.W. Reservoir + Dumas
Check	US Coast Geodetic		6.61	49.76	50' S of S. Edge of N.W. Reservoir at S. Side Road
				49.61	
				0.15 Diff	
BM-Top				9.03	
L. Stake	Alt. 200	5.51	<u>14.54</u>		
141+50				4.6	9.9
142+00				4.5	10.0
+50				5.3	9.2
143+00				5.1	9.4
"	20 ft			11.4	3.1
+50				6.3	8.2
+40				7.1	7.4
	S Edge con mark			7.80	6.74
144+00	N. Edge con mark			7.79	6.74
144	15 ft			10.8	3.7
	12 ft			4.9	9.6

7
14.50

190+23.80	int Power cable	7.6	6.9
+50		8.0	6.5
145+00		8.8	5.7
" "	15 Lt	6.6	7.9
" "	10 Rt Top L Wall	9.51	5.03
" "	" " Bottom Wall on ca	12.11	2.43
145+30 ⁵	2 3/4" Storm Drain on	8.3	6.2
+47	N End 6" Wall on ca	7.2	7.3
" "	Rt Top wall	9.40	5.10
" "	Bottom Wall	11.80	2.74
T.P.	310	<u>8.34</u>	9.30
145+56.81	S Topch on Paving	1.65	6.69
" "	Gutter " "	2.13	6.21
+66.87	4. Dunny Pad	2.08	6.26
+76.87	N Gutter	2.20	6.14
+76.87	N Top cb	1.76	6.58
+81		2.2	6.1
+92		5.3	3.0
	Top cobble wall	9.52	3.82

22

7
8.34

	Edge Mary Drill Hole Paving	5.50	2.84
146+00		5.3	3.0
+55 ⁵	Ground	5.4	2.9
"	Top cobble wall	4.66	3.68
+58 ⁵	S Edge of Paving	4.63	3.71
+70 ⁸	N Edge Paving	4.72	3.62
+74	Top cobble wall	4.78	3.56
"	Ground	5.3	3.0
147+00		5.3	3.0
"	19.6 Lt Base Wall	5.4	2.9
"	" Top Wall	+1.0	9.3
+50		5.3	3.0
148+00		5.4	2.9
+50		5.4	2.9
149+00		5.3	3.0
	TP. 5.67		
+53 ⁵⁵	L. <u>8.34</u>	5.67	2.67
"	Top Paving on Rt	5.52	2.82
"	5' Lt Base steps <small>on Paving stand</small>	5.4	2.9
"	" Top Reviewing stand	+0.5	8.8
150+00		5.4	2.9
"	3.6 Lt Paving	5.61	2.73

150t50		5.3	3.0
151+00		5.5	2.8
"	10.3 Rt on Paring	5.53	2.81
"	28 Lt Base wall	5.3	3.0
"	" Top wall	70.9	9.2
+50		5.4	2.9
+94 ^L	on Ground	5.3	3.0
"	Top Cobble wall	5.05	3.29
+97 ²	Edge of Paring	5.06	3.28
152+00	on Paring	4.95	3.39
"	15.6 Rt ^{Parade Ground} on Paring	5.60	2.74
+08 ^E	Edge of paring	4.98	3.36
+12 ⁶	Top cobble wall	5.01	3.33
"	on Grd	5.4	2.9
+50		5.3	3.0
+75		5.2	3.1
"	Rt ^{Edge of} ^{Parade} ^{Ground}		
+77	8.5 Lt Top on cobble wall	4.60	3.74
"	16.4 Base Wall	5.3	3.0
"	16.9 Top wall	70.3	8.6

+39		2.0	6.34
+91 ⁷³	S. Top cb. Porter Pood	1.94	6.40
"	S Gutter on Paring	2.45	5.89
153+00 ⁷³	4. Porter Pood	2.29	6.05
	^{Top Mt.} ^{Approx. do. Pt} ^{T.P. of 400' inside} ^{Parade}	70.62	<u>6.83</u> 2.13 6.21 ⁵
153+09 ⁷³	N. Gutter		0.92 5.91
"	Top cb		0.92 6.41
"			0.8 6.0
+26			3.3 3.5
+50			3.9 2.9
"	20 ²⁴		2.3 4.5
"	30 ⁴		7.1 7.9
154+00			4.1 2.7
"	20 ⁴		2.2 4.6
"	30 ⁴		7.1 8.3
T.P.	481	<u>8.12</u>	3.52 3.31 ⁵
154+49 ¹⁰	on Ground		
"	8.0 Lt Top cb		4.68 3.44
"	" Paring		5.19 2.93

+61 ³	S Edge Cannon Walk	4.35	3.77
+67 ⁸	N " " "	4.43	3.69
155+00		5.9	2.7
"	20' Lt	4.9	3.2
"	30 "	0.0	8.1
"	7.6 Rt Top. Cb	4.79	3.33
"	"	5.28	2.84
+50		4.9	3.2
+66 ⁸⁰	L. Rt	4.68	3.44
"	20' Lt	4.5	3.6
"	35 "	4.07	8.8
+88 ¹⁰	mtcb Top cb	4.40	3.7
"	Gutter	4.90	3.22
156+00		4.90	3.22
+53 ⁹	Endcks. ♀	4.48	3.64
"	7.1 Rt	4.05	4.07
"	13' Lt	3.97	4.15
157+00		4.43	3.69
+17	Lt	4.39	3.73
+50		4.43	3.69

158+00		4.44	3.68
+12 ²⁵	to Perry Road	4.42	3.70
+23 ²	Gutter	4.47	3.65
"	Top cb	4.13	3.99
T.P.	3.96	<u>8.41</u>	3.67
Flow line	ex M.H. 6 ft od L.	14.58 10.60	-6.17
158+33 ⁵⁴	1.00 2x2' hub	4.26	4.15
+50		4.2	4.2
159+00		4.5	3.9
+50		4.9	3.5
+52	3" Dia Tree 6' Rt		
+61	15" " Cypress Tree 6.5 Lt		
+70	10" " " 3.2 Lt		
+77	18" Dia " " 11 Lt		
160+00		5.5	2.9
+50		6.2	2.2
+80	18" Dia Cypress 6.5 Lt		
+97	18" " " 11.5 Lt		
161+00		6.9	1.5
+43	4" Dia cypress 10' Rt		
+50		7.2	1.2

π
8.41

161+99	6" Dia Cypress	1 Rt		
+56	3" "	9 Lt		
+61.9	int ex Serris	Ground		
+61.9	ex MH Flow	Line 7.2 Rt	15.93	-7.02.
+61.9	91.7 Lt to ex MH	Flow Line	15.75	-7.34
+66	5" Dia Cypress	1.4 Lt		
+78	1 1/2 Tamarack	4.4 Lt		
+78	8" "	7 Rt		
+89.22	1 Lt on Ground		6.9	1.5
"	6 Rt 8" Tamarack			
"	1 1/2 Tamarack	7.2 Lt		
+95.2	1 1/2 Dia "	0.9 Lt		
+96	8" " Tamarack	12 Lt		
162+00			6.6	1.8
+06	15 Lt 10" Tamarack			
+14	6.5 Rt 8" Tamarack			
+24	11.5 " 10" Acacia			
+31	6 Rt 10" "			
+49	8" Acacia	0.5 Rt		
+50			5.9	2.5
+59	11.3 Rt 4" Acacia			
+67	6" cypress on ♀			
+71	11.5 Rt 9" Acacia			

π
8.41

25

+72	10" Eucalyptus	1 Lt		
T.P.	5.99	<u>8.82</u>	5.58	2.83
+87	E Edge Walk		5.30	3.52
+93	W " "		5.34	3.48
+98	12.7 Lt 4" Eucalyptus			
163+00			5.3	3.5
+09	9.2 Lt 6" Acacia			
+20	16" " 8" Flowering Eucalyptus			
+41	16" Flowering Eucalyptus	4 Rt		
+50			4.8	4.0
+52	10" Flowering Eucalyptus	2.3 Rt		
	Ground		4.5	4.3
+64.5	Flow M.H	3.5 Rt	17.27	-8.45
"	Flow " "	81 Lt	17.82	-9.00
+71	6" Acacia	2.7 Lt		
+92	2.2 Rt 2" pepper			
T.P.	4.59	<u>8.75</u>	4.66	4.16
164+00			4.6	4.2
+01	2" Shrub	2.1 Rt		
+06	18" Acacia	6.5 Rt		
+09	12" Eucalyptus	16.5 Lt		
+14	2" shrub	5.8 Rt		

	+	π 8.75	-	Elev
169+19	4" Dia Tree	6.4 Rt		
+29	4 " "	2.2 Lt		
+35	4 " "	6.9 Rt		
+42	3 " "	4.7 "		
+95	15" Eucalyta	12.8 Lt		
+52	3" Dia Shrub	2.6 Rt		
+50			4.8	
+55	18" Dia Acacia	4 Lt		4.0
+59	3" Shrub	1.5 Lt		
+65	2" Dia "	2.2 Rt		
+66	2" "	4.3		
169+76 ²	Lt		5.09	3.66
+78	20" Dia Flo Wormp Eucalypta	12.6 Lt		
+84	18" " Acacia	5.3 Rt		
165+00			5.0	3.8
+05	18" Dia Acacia	1.2 Rt		
+14	18 " "	7.6 Lt		
+20	12 " Shrub	3 Lt		
+31	E Edge cur Walk		5.04	3.71
+35 SW	" "		5.02	3.73
+41	10" Shrub	1.5 Lt		

	π 8.75			26
+97 ⁴⁵	Fence	4.9		3.9
+1	8" Tree 10" Rt			
+52 ⁴	4" Dia Tree	2.5 Lt		
+56 ⁹	4" Dia Tree on 4			
T.P.	6.70	<u>8.47</u>	6.98	1.77
+63 ⁴²	Fence on Ground	5.6		2.9
+64 ²²	E-Edge Walk	5.59		2.88
+75 ⁴²	Top cb	5.75		2.72
" "	Gutter Paving	6.22		2.25
166+00	on Paving concrete	6.40		2.07
166+00 ¹	Beam Block Paving	6.52		1.95
T.P.	5.20	<u>7.66</u>	6.01	2.46
+50			5.30	2.36
+172				
N Frost			5.36	2.30
167+02 ²	N. b. Lytton Gutter	5.81		1.85
" "	" " Top cb	5.27		2.39
+17 ¹⁶	N. Lytton	4.8		2.9
" "	65 ft on the sernicista	4.86		2.80
+22	S. Edge Grease Rack	12.18		
+42	N "			



+44			56	2.1
+57			84	-0.7
+65			9.6	-1.9
+83 ²⁵	L 60 Stake		9.98	-2.32
168+00			10.1	-2.4
+50			10.2	-2.5
+75			10.9	-3.2
"	97' Rt Floor Apt House	→ 5.51		2.15
164+00	Ground	→ 8.5		-0.8
"	150' Lt	10.0		-2.3
T.P.	5.38	<u>5.73</u>	7.31	0.35
+12 ⁶	48" Dia Top Pipe		5.62	0.11
+21			7.0	-1.3
+50			7.1	-1.4
170+00			6.8	-1.1
"	150' Lt. Low Spot		9.2	-3.5
"	150 Rt		6.6	-0.9
"	200 "		9.8	0.9
+50			6.5	-0.8
171+00			6.2	-0.5
"	200' Rt		6.0	-0.3
"	125' Lt		8.6	-2.9

171+50			6.1	-0.4
172+00			5.8	-0.1
"	110' Lt		8.2	-2.5
"	300' Rt		6.2	-0.5
+50			5.9	0.2
173+00			6.0	-0.3
"	60' Lt Top Navy fill		7.3	-1.6
"	250' R " "		5.8	-0.1
+50			5.7	0.0
+68 ²	4.30" Dia Top pipe		5.99	-0.26
+91			6.3	-0.6
174+00	Top Navy fill end		4.8	0.9
TP	8.97	<u>9.78</u>	4.92	0.81
+12			5.1	4.7
+23 ⁶	L 60' 1x1 Stake		5.17	4.61
+50			5.0	4.8
175+00			5.0	4.6
+03 ²	5 Top cb		4.78	5.00
"	Ground		6.1	3.7
TP	4.63	<u>9.63</u>	4.78	5.00

175+09 ^E	2.8" Sewer on Ground	5.1	4.5
" "	Flow Line	8.93	0.70
" "	Flow Line	10.38	-0.75
+90 ^Z	N.C.B. Gutter	5.8	3.8
" "	Not Constructed		
+46		4.4	5.2
176+00		5.4	4.2
+50		5.6	4.0
177+00		5.6	4.0
+50		5.6	4.0
178+00		5.7	3.9
+32 ¹⁷	L. in Play Area	5.63	4.00
on L			
T.P.	6.66	10.66	5.63
+50		6.2	4.5
179+00		5.7	5.0
+68		5.8	4.9
+73		5.9	5.3
+89		5.2	5.5
+92	1 in 15 0.3 RI 8 ft. after eb		
180+00		6.5	4.2

+05	int. 8" T.C. Sewer	5.5	5.2
"	EX MH Lt Flow Line	9.59	1.07
"	EX MH Rt " "	10.70	-0.04
+37 ^E	P.C. Alley Ret. 475 cb Not constructed	5.6	5.1
+50		5.3	5.4
181+00		5.6	5.1
+50		6.5	4.2
182+00		6.6	4.1
T.P.	476	8.82	6.60
+50		4.8	4.0
+96	Approx N.C.B. Line Sectors cb Not constructed	5.2	3.6
183+00		5.3	3.5
+12	Elec conduit	7.63	1.13
+14	int 8" T.C. Sewer Grd	5.3	3.5
"	lt flow line MH	9.69	-0.87
"	Rt " " "	11.00	-2.78
183+20	Elec Conduit	6.77	2.05
Set BM		2.12	6.70
+50		5.4	3.4
184+00		5.6	3.2
+21		6.22	2.60
+32 ^E	L. & Reservoir	6.26	2.56
"	50' Lt	9.6	-0.8

SE TOP
41 Sectors
Diverse Sectors

7. Note Ground Wat at Reservoir
15.00' Consider 25.00' for 90'

T
882

7P	4.56	<u>8.11</u>	5.27	3.55
185+00			5.52	2.59
+50			5.37	2.74
186+00			5.21	2.90
" "	60' Lt		9.2	-1.1
+50			5.13	2.98
187+00			4.95	3.16
" "	100' Lt		9.1	-1.0
187+49	49 opp Men on d		4.97	3.14
" "	Set B Men Pick Men		9.18	-1.07
188+00			5.15	2.96
" "	60' Lt		8.6	-0.5
" "	100 Rt		8.4	-0.3
+50			5.20	2.9
189+00			5.32	2.79
" "	100' Lt		8.5	-0.4
" "	100 Rt		8.8	-0.7
+50			5.50	2.61
190+00			5.67	2.44
75 ⁰⁵	Side of Carby		5.88	2.23

T
811

29

191+00			5.96	2.15
" "	100' Lt		8.2	-0.1
" "	100 Rt		8.0	0.1
T.P.	1.05	<u>6.39</u>	2.77	5.34
+50			4.43	1.96
192+00			4.55	1.84
+50			4.71	1.68
193+00			4.89	1.50
" "	100' Lt		6.4	0.0
" "	100 Rt		6.2	0.2
+50			5.02	1.37
194+00			5.23	1.16
+50			5.49	0.90
195+00			5.53	0.86
" "	60' Lt		5.3	1.1
" "	100 Rt		6.1	0.3
+50			5.54	0.85
196+00			5.53	0.86
" "	60' Lt		5.2	1.2
" "	100 Rt		6.0	0.4
196+46.89	on spike &	Ingraham Rosarians	5.57	0.82
check BM			5.45	0.94
				0.56 BM
				0.38

Reading checked by M.R.H. 6/17/41

S.W.B.P.
Ingraham
Rosarians

Levels for Interceptor Sewer on
Rosecross North of Lytton, from 180+00 to N.E. & Junction.
Line Change

BM	0.80	7.50	6.70	SW Top IV Setts Unit 4 Posters
184100 ¹³		4.5	3.0	
+50		4.5	3.0	
185100		4.3	3.2	
+50		4.4	3.1	
186100		4.3	3.2	
+50		4.3	3.2	
187100		4.3	3.2	
+40		4.4	3.1	
+50		6.6	0.9	
"	2' Lt	4.1	3.4	
"	10' Rt	6.7	0.8	
188100		6.4	1.1	
" "	2' Lt	4.2	3.3	
" "	10' Rt	6.9	0.6	
+50		6.7	0.8	
2' Lt		4.5	3.0	
10' Rt		6.8	0.7	
189100		6.8	0.7	
" "	2.5 Lt	4.8	2.7	
" "	10' Rt	6.9	0.6	

π
7.50

T.P.	3.72	6.54	4.68	2.82'
+50			6.0	0.5
"	2.7 Lt		3.9	2.6
"	10' Rt		6.2	0.3
190100			6.0	0.5
"	10' Rt		6.2	0.3
"	2.5 Lt		4.1	2.4
+50			6.1	0.4
"	2' Lt		4.2	2.3
"	10' Rt		6.2	0.3
191100			5.9	0.6
"	2.5 Lt		4.5	2.0
"	10' Rt		6.0	0.5
+50			6.4	0.1
"	2' Lt		4.7	-1.8
"	10' Rt		6.4	0.1
192100			6.0	0.1
" "	2.5 Lt		4.8	1.7
" "	10' Rt		6.4	0.1
+50			6.1	0.4
"	2' Lt		5.0	1.5
"	10' Rt		6.1	0.4

		7 654			Ref. by
193100			63	0.2	6/10/41 9.21-30
" "	2' LT		53	1.2	
" "	10' RT		58	0.7	
+50	end basin		61	0.4	
"	3' LT		55	1.0	
"	10' RT		58	0.7	
194100			58	0.7	
+50			59	0.6	
195100			61	0.4	
+50			60	0.5	
+88 +	5' Edge Par. vs Jugoslav		6.07	0.47	
196100			6.00	0.54	
+28 ⁶⁸	+ & Jugoslav & Roseans		5.71	0.73	
check BM		62	5.72	0.92	South West Jugoslav & Roseans
				0.34	
				0.02	

Bliss Notes
Summer Mexico
G. Farrow. Rod
7/31/41

Levels for Peritoma Interceptor

Server. line change from 94+11 26 East
on Lowell and North through Naval

Training Sta. Grounds.

BM	8.49	8.50	0.01	1x1570x 94+11 26
94+60		7.9	0.6	Reduced by: M.R.G. 7/7/41
95+00		5.4	3.1	
150 POT. ixistore		3.94	4.56	checked W.B. 7/9/41
96+00		9.0	4.5	
+50		4.1	4.4	
+86		3.9	4.6	
97+00		4.9	3.6	
+50		5.7	2.8	
98+00		5.5	3.0	
+50		4.4	4.1	
+80		3.8	4.7	
99+00		4.7	3.8	
+15		4.3	4.2	
+50		4.9	3.6	
100+00		5.3	3.2	
+50		4.5	4.0	

T
8.50

32

100+77	13	4.52	3.98	
BM 2x2 5' base 24' base	6.75	10.85	4.40	4.10
101+00		6.9	4.0	About 70' N.W. of line on split of 4
+50		5.7	5.2	
+75		5.3	5.6	
102+00		5.7	5.2	
+35		6.5	4.4	
103+00		6.1	4.8	
+40		5.6	5.3	
+52		4.4	6.5	
+57	S Side Drainage channel	7.3	3.6	
+72	N " " "	7.5	3.4	
+77		4.8	6.1	
+89	96 POT. ixistore	5.20	5.65	
104+00		5.3	5.6	
+50		4.9	6.0	
105+00		5.6	5.3	
+30		6.0	4.9	
+70		4.2	6.7	
106+00		4.4	6.5	

T
10.85

106+50			50	5.9	
107+00			55	5.4	
T.P.	4.34	10:12	5.07	5.78	
+50			42	5.9	
108+00			42	5.9	
+50			44	5.7	
109+00			47	5.4	
+67 ²⁰	P.O.T. IXI stake		445	5.67	
BM	4.50	10.44	4.18	5.94	Approx BS H 109167 ²⁰ 5.94 - 0.00 see page 79 this book
110+00			50		
110+00			58	4.6	
+12			58	4.6	
+34			49	5.5	
+50			49	5.5	
+90			38	6.6	
111+00			45	5.9	
+50			55	4.9	
112+00			53	5.1	
+50			50	5.4	
113+00			49	5.5	

T
10.44

33

+50			52	5.2	
114+00			55	4.9	
+50			58	4.6	
+70			55	4.9	
+80			47	5.7	
115+00			49	5.5	
T.P.	4.57	10.38	4.63	5.81	
+30			60	4.4	
+50			60	4.4	
116+00			62	4.2	
+90 ⁸⁶	P.O.T. IXI stake		599	4.39	
+75			61	4.3	
+80			59	5.0	
117+00			55	4.9	
+50			64	4.0	
+95			66	3.8	
118+00			57	4.7	
+57 ¹⁰	on stake int Navy Saver		5.91	4.47	
" "	Flowline M.H. 115 Pt.		20.14	-3.76	
BM	3.08	9.84	3.60	6.78	X on W. Rim Base of 1941 15' N. 12' E. 10

16.76
0.02 error See page
used corrected 79

119+00			5.2	4.6	
+66			4.3	5.5	
120+00			5.4	4.4	
+50			5.3	4.5	
121+00			5.2	4.6	
+50			4.8	5.0	
122+00			4.1	5.7	
+20			4.0	5.8	
+50			4.7	5.1	
123+00			5.6	4.2	
+50			5.4	4.4	
123 ²³	POT:		5.31	4.53	
5.07					
Sef 8711	10.20		4.71	5.13	100' Pt. 123+00 ²³ 2"x2" stake Nail in Top
124+00			5.8	4.4	
+50			5.8	4.4	
125+00			6.3	3.9	
+50			6.7	3.5	
126+00			6.3	3.9	
+50			5.7	4.5	
127+00			5.3	4.9	

+35			4.6	5.6	
+50			5.3	4.9	
128+00			5.4	4.8	
+25			5.0	5.2	
+50			5.9	4.3	
+75			7.0	3.2	
129+00			7.4	2.8	
T.P.	526	8.63	6.83	3.37	
+50			6.0	2.6	
130+00			5.7	2.9	
+50			5.8	2.8	
131+00			5.8	2.8	
+967	L.Pt. on stake		5.63	3.0	
+50			5.4	3.2	
132+00			5.1	3.5	
+35			4.0	4.6	
+80			4.0	4.6	
133+00			4.7	3.9	
+50			4.8	3.8	
+70			4.8	3.8	
134+00			3.6	5.0	

T
8.63

T.P.	5.71	10.97	3.3 ⁷ ₆	5.26
+60			5.6	5.4
135+00			6.4	4.6
+50			7.2	3.8
136+00			7.5	3.5
+09 ⁷	POTonslake & White		7.27	3.70
T.P.	7.71	11.41	7.27	3.70
T.P.	5.18	12.91	3.68	7.73
check BM			1.80	11.11
				$\frac{11.12}{0.01 \text{ error}}$
	6.28	9.99	3.71	136+09 EZ POT corrected
+50			6.1	3.9
137+00			5.8	4.2
+50			6.3	3.7
138+00			6.0	4.0
+50			5.7	4.3
139+00			5.8	4.2
+50			5.8	4.2
140+00			5.8	4.2
+50			5.7	4.3

T
9.99

141+00			5.5	4.5
+50			5.5	4.5
142+00			5.5	4.5
T.P.	5.16	9.77	5.38	4.61
+50			5.4	4.4
143+00			5.8	4.0
+50			5.4	4.4
144+00			5.4	4.4
+50			5.4	4.4
145+00			5.4	4.4
+50			5.3	4.5
146+00			5.8	4.0
+50			6.1	3.7
+63 ¹²	POT	5.05	8.69	6.13
147+00			5.0	3.7
+57			5.6	3.1
+58			4.8	3.9
148+00			5.1	3.6
+50			5.4	3.3
+74			5.6	3.1
+79			3.1	5.6
+90			8.0	0.7
149+00			8.1	0.6

Continued Top page 38

Spl.	0.97	10.21		9.24	
T.P.	5.15	6.49	8.87	1.34	
15061 ^E	S Edge Tennis ct		5.30	1.19	
+50			5.30	1.19	
151400			5.30	1.19	
+25 ⁴	N Edge Tennis ct		5.36	1.13	
+45 ⁹⁰	2.36" Drain		5.4	1.1	
Flon. M.H.	Lt		8.89	-2.40	
" " "	Rt		11.55	-5.06	
+65	5.5 1' Dia Tomarack				
"	6 Rt 1' " "				
+78 ⁴	S Side Dancy Road		5.97	1.02	
+91 ⁴	N " " "		5.96	1.03	
152400			5.9	1.1	
" "	5.4 Lt 4" Tomarack				
" "	5 Rt 14" Dia Tomarack				
+107 ⁵⁶	S Edge Parade Ground		5.97	1.02	
+09 ⁵⁶	L		5.97	1.02	
T.P.	5.92	7.07	5.34	1.15	
+50			5.90	1.17	

H. Spot checked
out by C. N. E.
Cushings + Topographical

					7 7.07		36
153400				5.70	1.37		
+50				5.57	1.50		
154400				5.21	1.86		
+50				5.00	2.07		
155400				4.74	2.33		
+19.5	W Side Parade Ground		4.62	2.45			
+20 ²⁰	L Rt on 1st store		4.71	2.36			32.4 Front to wall
T.P. on L	5.92	7.78		4.71	2.36		
+50				5.4	2.4		
+85 ⁴	Top 1 st Pub/Wall		5.30	2.48			
+88 ⁶	S Edge A.C. Rampway		5.25	2.53			
156400 ²	N " " " Ramp		5.23	2.55			
+103 ⁸⁵	NE Edge 1 st Pub/Wall		5.29	2.49			
+50				5.4	2.4		
157400				5.3	2.5		
+50				5.3	2.5		
158400				5.2	2.6		
+139 ²²	L Rt			5.20	2.58		
+51 ⁷²	W Edge Parade Ground			5.46	2.32		
+87 ²⁵	L Lt			5.40	2.38		

T
7.78

159129 ²⁵	W Edge 19' ved P.E.	5.38	2.40
+36 ⁶⁸	5.34 L RT	7.89	5.23
+56		5.4	2.5
160100		5.3	2.6
+50		5.3	2.6
161100		5.4	2.5
+31 ³⁵	S Top Rubble wall	5.41	2.48
+34 ⁴⁵	" E. Pavement	5.41	2.48
+46 ⁷⁵	N " "	5.41	2.48
+42 ⁸	N Top Rubble wall	5.42	2.47
162100		5.3	2.6
+07		5.3	2.6
"	4.7 RT. W Edge P.G.	5.44	2.45
+21	18" Tree 8.5 LT		
"	12" " 0.5 RT		
+28 ⁸	S Top cl Porter Road	2.72	5.17
"	S Gutter	3.24	4.65
+46 ⁸	N "	3.20	4.69
"	N Top cl	2.72	5.17
+50		3.2	4.7
+55	18" Tree 1.5 RT		

T
7.89

37

+63		5.4	2.5
Check BM.		2.09	5.80
			5.77
			0.03 error
TP.	2.55	5.49 ✓	4.92
			2.94 ✓ corrected
			2.97 ✓
+70	3" Acacia	3.1 LT	
"	8" "	11' RT	
+83	8" "	7.5 RT	
+90	10" "	3.3 LT	
+93	7" "	7' RT	
163100		3.2	2.3
"	"	3" Acacia	5.6 LT
+04	6" "	4.5 RT	
+10	4" "	4' LT	
+14	6" "	6 RT	
+20	4" "	2.5 LT	
+22	3" "	3.7 RT	
+40	6" "	7' RT	
+42	6" "	7.5 LT	
+49	10" "	on d	
+50		3.4	2.1

NETOP
M.V. APPROX
20' RT 162100

T
5.49

+58	10" Accia 3.8 L		
+68	10" " 7 L		
+80	10" " 10.5 RT		
+86 ^L	5. Edge Cem. Cb.	2.71	2.78
T.P.	5.81 8.20	3.10	2.39
" "	6.4 L Topcb	5.23	2.97
164+00		5.52	2.68
+58		5.72	2.48
165+00		5.50	2.70
" "	6.4 L	4.96	3.24
+50 ³⁹	L RT	5.35	2.85
+80 ¹⁸	L L	4.99	3.21
" "	1.3 RT Topcb	4.55	3.65
166+00		5.06	3.14
+50		4.93	3.27
167+00		5.00	3.20
+20 ⁰²	L L	5.00	3.20
+56 ²	mt 87.0	4.98	3.22
+59 ^E	Gutter	4.99	3.21
"	Topcb	4.56	3.64
167+70 ²⁹	-158+33 ⁵⁹	4.49	3.71
check. BM		4.73	

RP. 12 Cb

3.97

3.59

5. Side Perry Road
N. 1/2 Mile West

Continued from
page 35

T
8.69

38

149+50		7.6	1.1
150+00		7.6	1.1
T.P.	6:20 12:07	2.82	5.87
check. BM		2.84	3.23
			3.24
			0.01 error

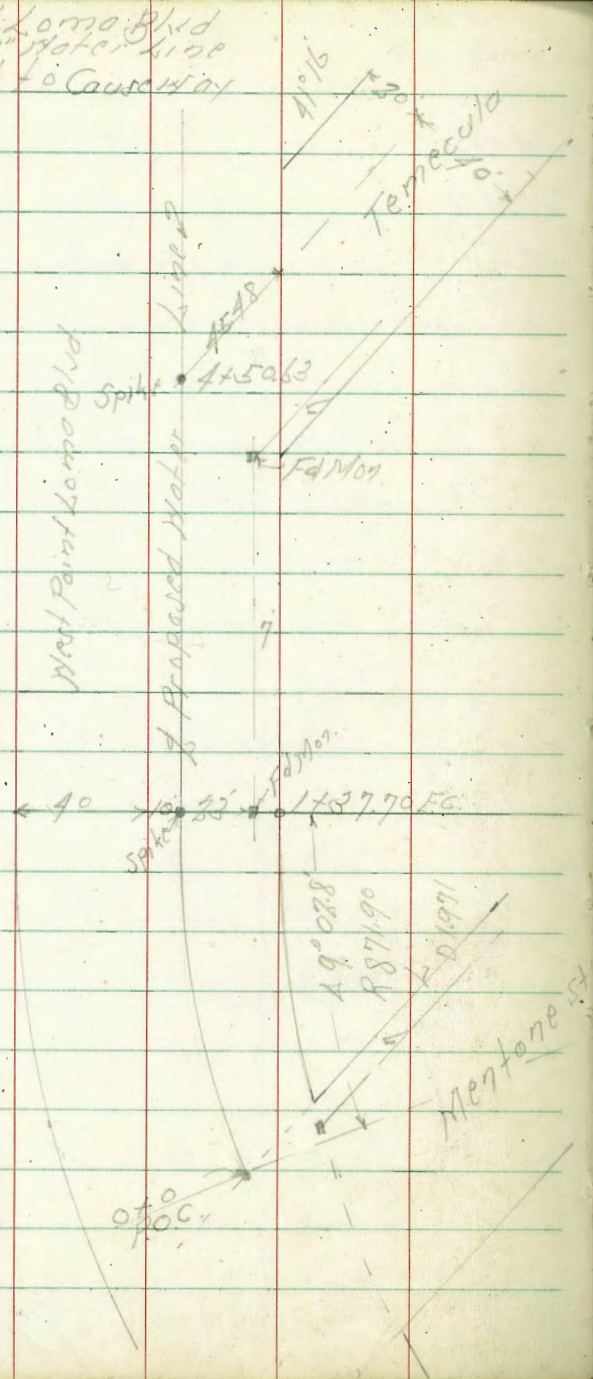
NK Cashing

+ 2.96

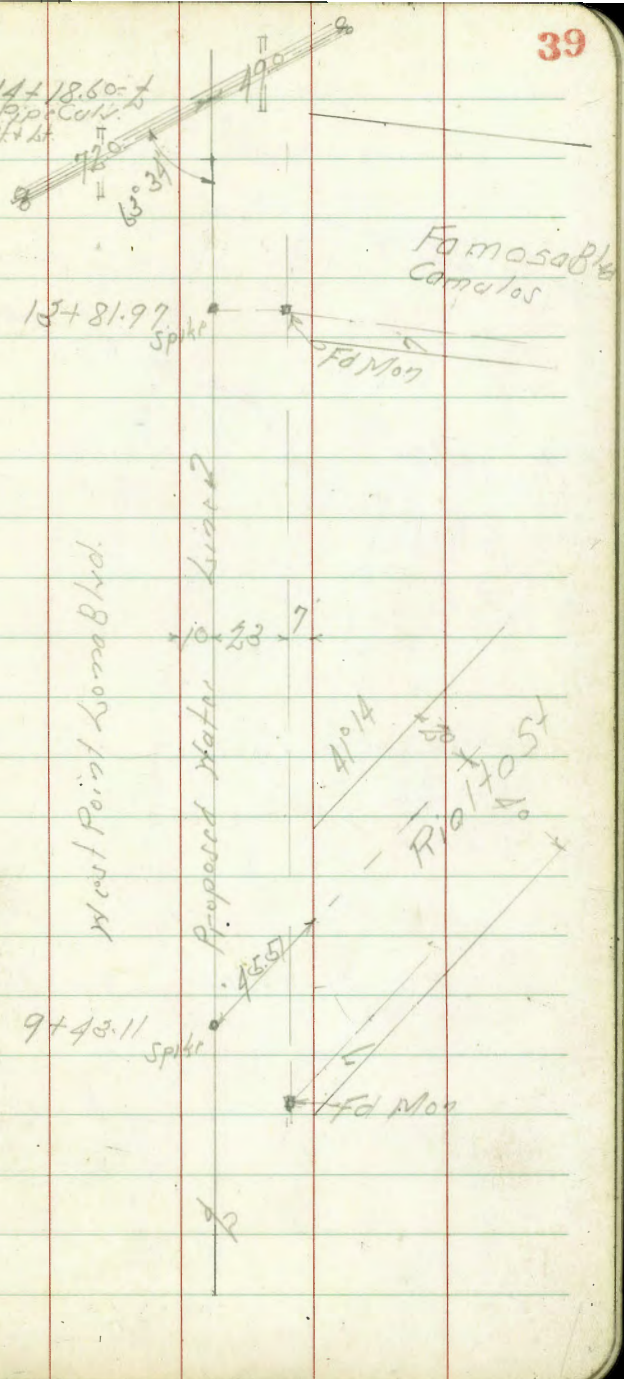
Note Levels from 150+00 - see page 36

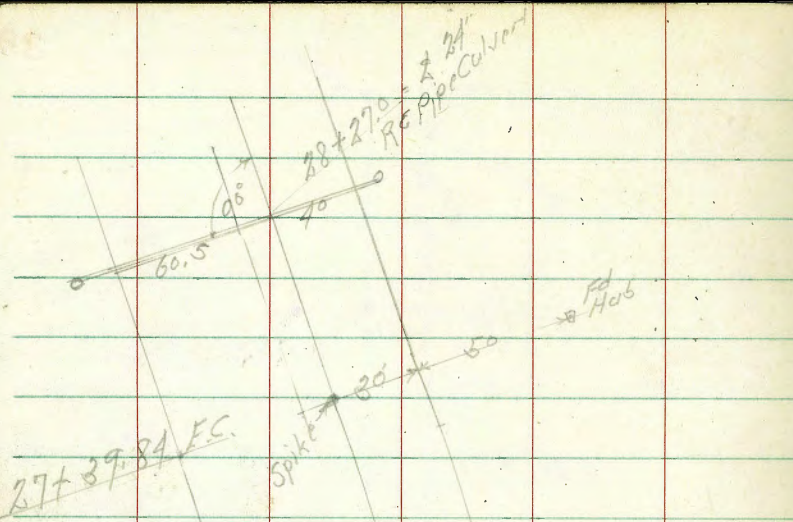
West Point Loma Blvd
 Proposed 12" Water Line
 Mentone St to Causeway

Sec
 G Book 178
 " " 1337
 " 1493
 " 1375



14+18.60-7
 Do. 48" RC Pipe Culvert
 + Curb 10' left Right of Way

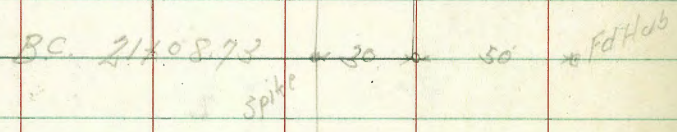




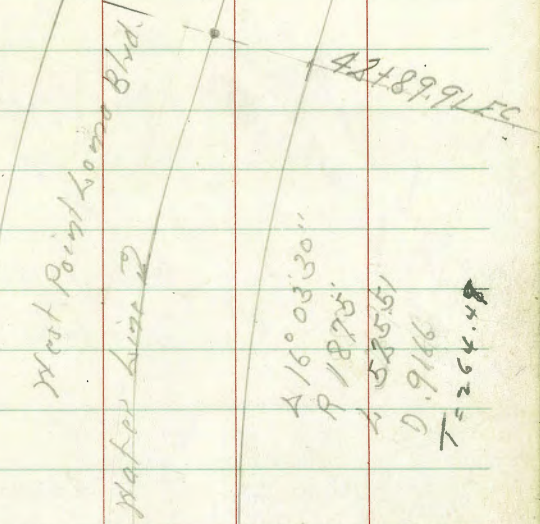
27+39.84 EC

$\Delta = 18.50$
 $R = 19200$
 $L = 6311$
 $D = 8952$

West Point Loma Blvd.
 Water Line 2
 Spike

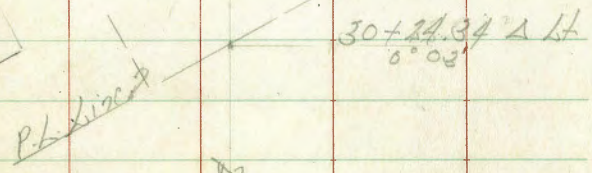


Prop



$\Delta = 16^{\circ} 03' 30''$
 $R = 1875$
 $L = 5856$
 $D = 9166$
 $T = 264.48$

27+64.40 BC



West Point Loma Blvd. Levels For
Proposed 12" Water Line
Meatone to Causeway

BM	5.85	25.90	20.05	
	Fly Line Meatone			
0+0 = Produced Fly	3.3		24.6	
+50	3.7		22.2	
1+0	4.0		21.9	
+37.70 = FC	4.3		21.6	
+50	4.4		21.5	
2+0	4.8		21.1	
+50	5.2		20.7	
3+0	5.5		20.4	
+50	5.9		20.0	
4+0	6.3		19.6	
+50.63 = Stub Tomacula	6.8		19.1	
25' S.Fly	7.5		18.4	
45.5 S.Fly = S.L. X P. Loma	6.0		19.9	
5+0	7.8		18.1	
TP	0.92	18.82	8.00	17.90
+50			2.0	16.8
6+0			3.7	15.1
+50			5.3	13.5
7+0			7.1	11.7

on S. 7' Moors
1437.70 FC
part of pipe

18.82

7+50			9.0	9.8
8+0			10.6	8.2
+50			12.0	6.8
TP	1.96	8.75	12.03	6.79
9+0			3.1	5.6
+42.11 = Stub Rialto			3.8	5.0
25' S.Fly			4.1	4.6
45.5 S.Fly = S.L. X P. Loma			2.6	6.1
10+0			4.5	4.2
+50			5.0	3.7
11+0			5.2	3.5
+50			5.6	3.1
12+0			5.9	2.8
+50			6.3	2.4
13+0			6.5	2.2
+50			7.1	1.6
TP	6.41	5.84	9.32	-0.57
14+0			4.3	1.5
+78.60 = 2.00 48" RC. Pipe Culv. End 048"			4.3	1.5
72' X Fly = Pipe Culv Top			8.36	-2.52
Flow Line			12.69	-6.85

Aug 1-41
Sisson
Hortland
X Moore

on S. 7' Moors
X P. Loma +
Camelot
187 81.97

	5.84			
49 S.F. Pipe Culv Top	7.24	-1.40	✓	
Floor Line	11.57	-5.73	✓	
14+50	4.5	1.3	✓	
15+0	4.6	1.2	✓	
+50	4.6	1.2	✓	
16+0	4.4	1.4	✓	
+50	4.2	1.6	✓	
17+0	4.1	1.7	✓	
+50	4.0	1.8	✓	
18+0	3.9	1.9	✓	
+50	3.7	2.1	✓	
TP	6.77	8.63	3.98	1.86
19+0		6.0	2.6	✓
+50		5.6	3.0	✓
20+0		5.3	3.3	✓
+50		5.0	3.6	✓
21+0		4.6	4.0	✓
+0873 B.C.H.		4.6	4.0	✓
TP	6.08	10.12	4.59	4.04
+50		6.0	4.1	✓

	10.12			
22+0	5.8	4.3	✓	
+50	5.4	4.7	✓	
23+0	5.1	5.0	✓	
+50	5.0	5.1	✓	
24+0	4.9	5.2	✓	
+50	4.9	5.2	✓	
25+0	5.0	5.1	✓	
+50	5.6	4.5	✓	
26+0	5.8	4.3	✓	
+50	6.0	4.1	✓	
27+0	6.4	3.7	✓	
+3984 EC	6.6	3.5	✓	
TP	4.22	7.11	7.23	2.89
+50		3.6	3.5	✓
28+0		3.5	3.6	✓
+27 = 2 24" RC Pipe Culv	3.6	3.5	✓	
12' at 24" RC Pipe				
46 S. Culv. on Top	5.47	1.64	✓	
Floor Line	7.69	-0.58	✓	
Outlet 24" RC Pipe				
60.5' H. Culv. on Top	6.23	+0.88	✓	
Floor Line	8.47	-1.36	✓	

0757' Hub
27+3984 EC

7.11 ✓

28+50			5.8	3.3	✓
29+0			4.0	3.1	✓
+50			4.3	2.8	✓
30+0			4.6	2.5	✓
+50			4.8	2.3	✓
31+0			5.1	2.0	✓
+50			5.3	1.8	✓
32+0			5.4	1.7	✓
+50			5.4	1.7	✓
33+0			5.3	1.8	✓
+50			5.2	1.9	✓
34+0			5.0	2.1	✓
+50			4.9	2.2	✓
TP	5.90	8.10 ✓	4.91	2.20	✓ Hail Pole
35+0			5.7	2.4	✓
+50			5.5	2.6	✓
36+0			5.3	2.8	✓
+50			5.2	2.8	✓
37+0			5.0	3.1	✓
+50			4.6	3.5	✓

8.10 ✓

37+64.40 BCR			4.5	3.6	✓
38+0			4.2	3.9	✓
+50			3.8	4.3	✓
39+0			3.5	4.6	✓
+50			3.1	5.0	✓
40+0			2.8	5.3	✓
+50			2.4	5.7	✓
TP	5.46	10.81	3.75	5.35	✓
41+0			4.9	5.9	✓
+50			4.7	6.1	✓
42+0			4.6	6.2	✓
+50			4.5	6.3	✓
+89.91 FC			4.5	6.3	✓
43+0			4.5	6.3	✓
+62.39 BCR			4.5	6.3	✓
44+0			4.5	6.3	✓
+50			4.3	6.5	✓
45+0			4.1	6.7	✓
+50			3.8	7.0	✓
+92.68 - FC + 411° 15'			3.6	7.2	✓

10.81 ✓

46+32.88 Δ 2/15°00'

BM

7.82

2.99

4.0 = 6.8 ✓

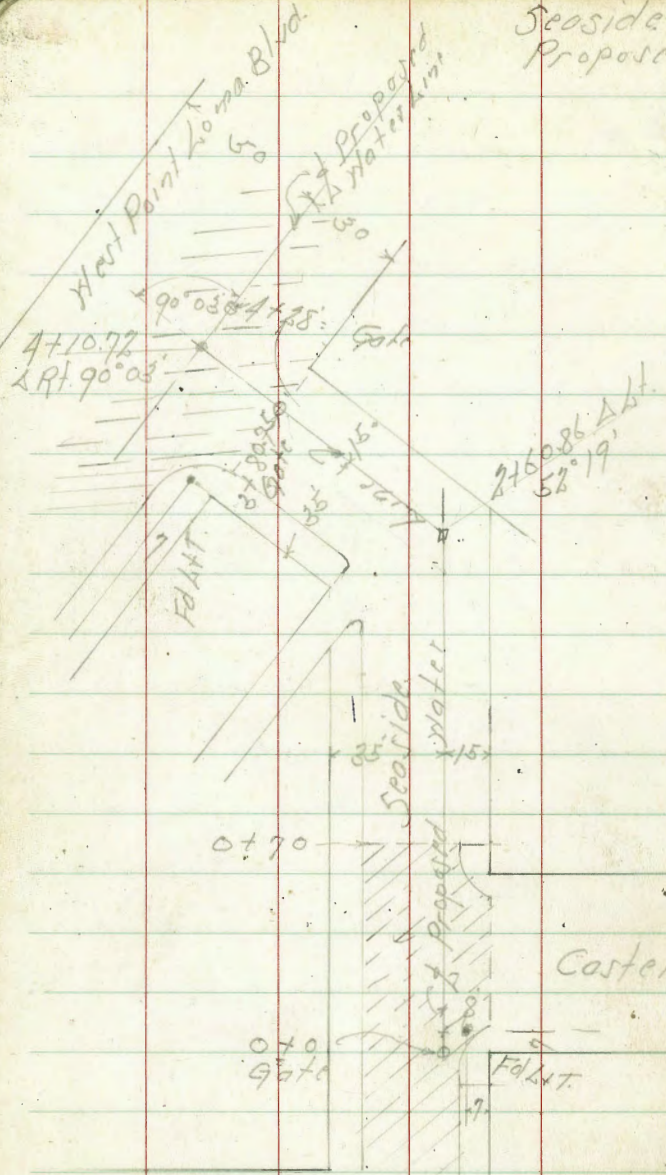
21.

BPZ Cal. HM.
10.1111
N. Pt. L. ma Bld
N. Coastway
3.0°

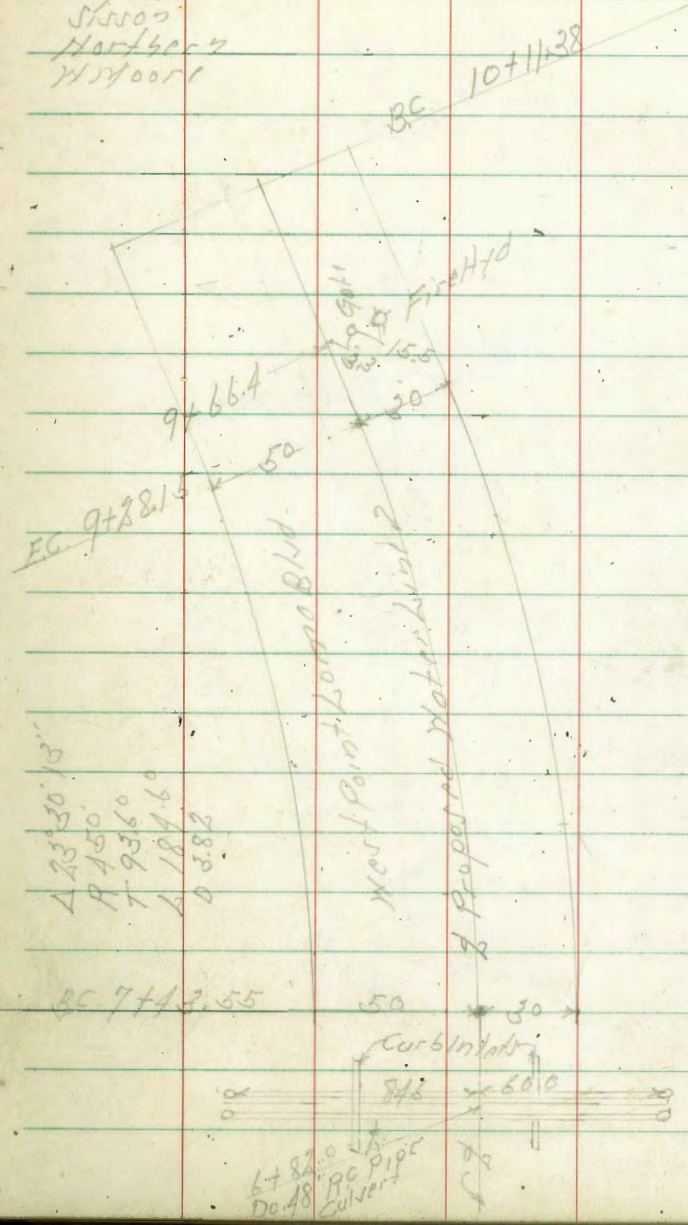
Seaside And
Proposed Water

West Point Loma Blvd.
Line Castelar St to Westmost

Indexed
LMI



Aug. 17 41
Sisson
Northcott
W. Moor



6+82.0
Do. 48
RC Pipe
Culvert

14+100.72
P.O.C.

13+1230.24
Fire Hyd.

1805 Fire Hyd

Hand Point

Yuma Blvd

City Prepared Water Line

12634

198719

01991

1805

10+113885

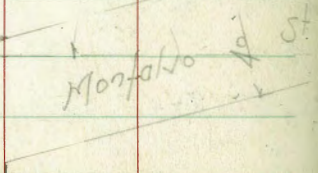
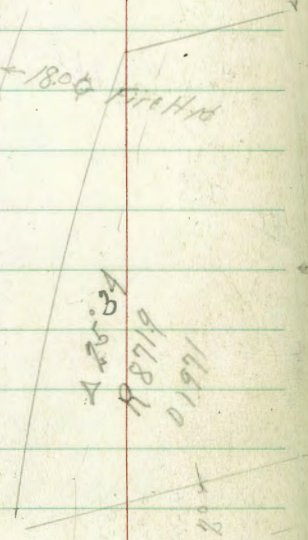
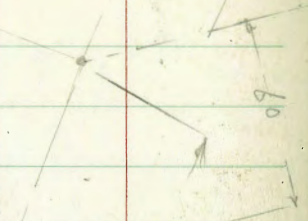
10+10.04

104.16

Montano

50 120

Mentoreff



Seaside & West Point Loma Blvd
Levels for Proposed Water Line
Castelar St to E.L. Montano

8/11/41
K. L. ...
N. ...
P. ...

B.M.	9.59	39.96	30.37	
TP	6.21	45.97	0.20	39.76
0+0 = St. Castelar St Front			2.66	43.31
+30 =			2.84	43.13
+90 = 1/2 Conc Pav			3.49	42.48
1+0			4.9	41.1
+50			7.1	38.9
2+0			10.5	35.5
TP	1.48	35.33	12.12	33.85
+50			3.1	32.2
+60.86 = At 5219			3.58	31.75
+75			4.2	31.1
3+0			5.4	29.9
+50			7.5	27.8
+80.75 = 5/4 Paving Gate			8.24	27.09
+88			8.92	26.41
4+10.72 = A Rt. 90° 03			8.97	26.36
+28 = Gate			9.71	25.62
+50			11.2	24.1
TP	0.08	23.95	11.46	23.87

Aug. 13-41 48

			23.95	
5+0			3.3	20.6
+50			6.1	17.8
6+0			8.5	15.4
+50			10.1	13.8
+82 = 2 Dead 8" RC Pipe Cully			10.3	13.6
60 ft off - 5' End Dead 8" RC Pipe Cully top			24.66	- 0.65
Flow Line			28.95	- 5.00
84.6 ft off - 1/2 End Dead 8" RC Pipe Cully top			25.00	- 1.05
Flow Line			29.35	- 5.40
7+0			10.0	13.9
+43.55 = B.C. Lt			8.5	15.4
8+0			5.5	18.4
+50			3.2	20.7
9+0			1.2	22.7
TP	7.92	30.34	1.53	22.42
+28.15 = EC			6.8	23.5
+50			6.3	24.0
+66.4			6.0	24.3
10+10.04 = Stub Montano			5.4	24.9
31.0 S.F. = 5/4 W.P. Lamin			3.8	26.5

5.82
- 5.11

3034 ✓

10+1138 = BCPH 5.4 24.9 ✓

+50 5.4 24.9 ✓

11+0 5.6 24.7 ✓

+50 5.8 24.5 ✓

12+0 6.1 24.2 ✓

+50 6.5 23.8 ✓

13+0 7.0 23.3 ✓

+50 7.3 23.0 ✓

14+00.22 - E.L. Meston 7.7 22.6 ✓

TP 1.96 2746 4.84 25.50 ✓

BM 7.40 20.06 ✓

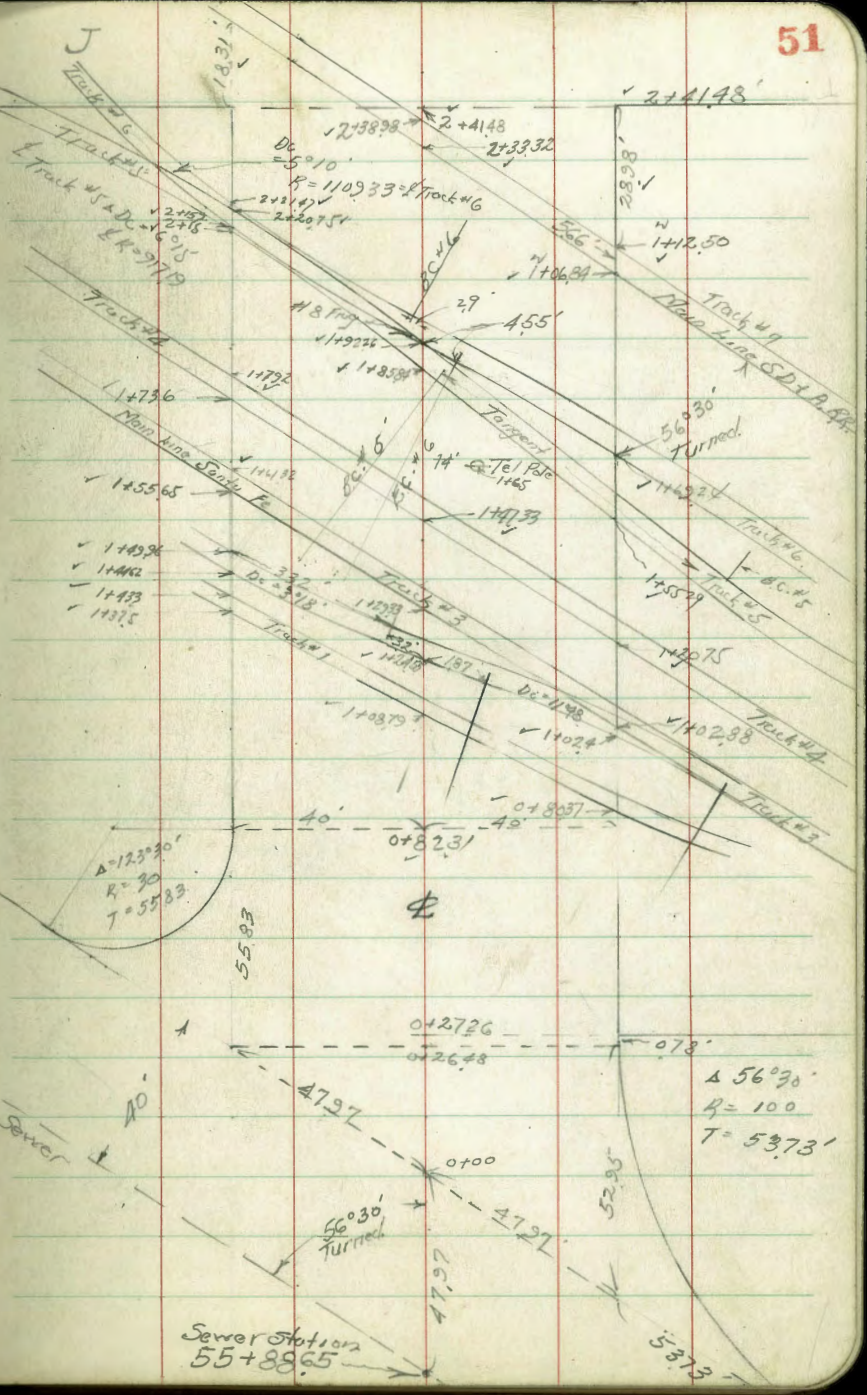
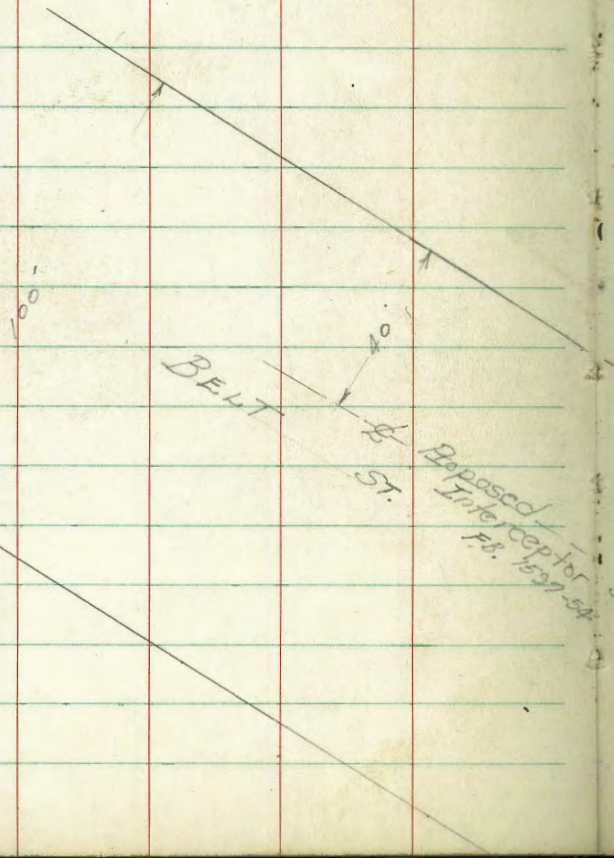
0757 Mon
F.C. Part of
Meston
20.06
Page 42

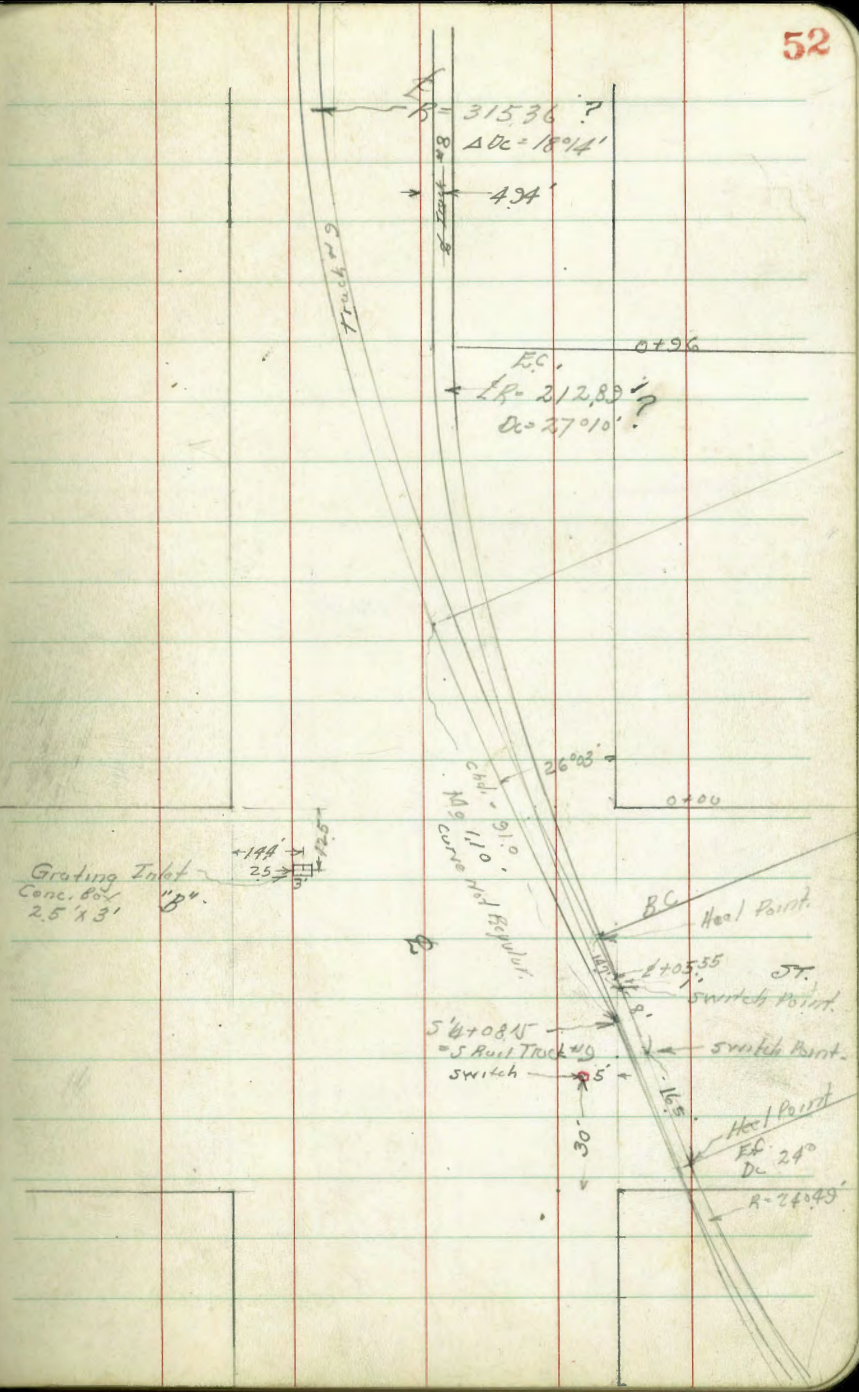
The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light green horizontal ruling. Each page has two vertical red margin lines, one on each side of the central gutter. The right page is numbered '50' in the top right corner. The notebook is bound in the center with visible stitching. The pages are blank, with no writing or markings.

Walker
Wells
D. Farrow
9-19-41

CROSS SECTION 1st AVE
from BELT ST
to ISLAND AVE.

80' Wide Indexed
14' cbs.
13' 1/4s
LM

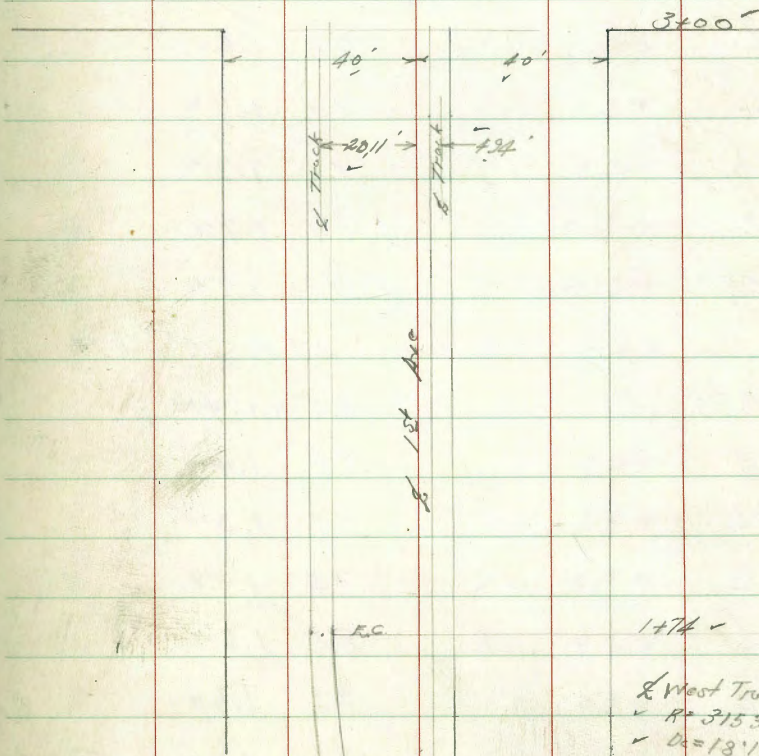




ISLAND

AVE.

80'



1+74 -

West Track
 11' 315.36' ?
 00 = 13' 14'

Walker
Wells
Farm
9-23-41

1st Ave Cross Sections
from Belt to Island
Sketch P-57

6.63 8.82 2.19

3.74 x 10
F.B. 1597
Press Plug

0+00 Section diag. on W. Belt

W.L. - 3583-80. Act. 7.0 1.87

W.L. 7.1 1.77

cb. 7.2 1.67

1/4 7.2 1.67

L 7.2 1.67

1/4 7.1 1.77

cb. 7.1 1.77

E. 7.1 1.77

+5373-BC. Act. 7.1 1.77

0+2648 Section Rt to 1st Ave

E-5 7.4 1.47

E. 7.4 1.47

cb. 7.5 1.37

1/4 7.4 1.47

L 7.2 1.67

1/4 7.2 1.67

cb. 7.1 1.77

W.L. 7.1 1.77

F.B. 1597-43

Cor Foundation N.E. Cor Belt & 1st Ave

8.82

0+8231 = W. S. to E.C. on W.

W-5 7.3 1.57

W 7.4 1.47

cb. 7.4 1.47

1/4 7.6 1.77

L 7.5 1.37

1/4 7.6 1.77

cb. 8.3 0.57

E. 8.4 0.47

+5 8.2 0.67

1+00

-5 7.4 1.47

E. 7.4 1.47

cb. 8.0 0.87

1/4 8.2 0.67

L 8.0 0.87

1/4 8.0 0.87

cb. 7.4 1.47

W 7.6 1.77

+5 7.6 1.77

T.P. C.08 7.73 7.17 1.65

Truck Levels West Line 1st Ave.

1+375 = S. Rail Truck #1 5.69 7.04 ✓

+433 = N " " #1 5.69 7.04 ✓

+44.62 = S " " #2 5.70 7.03 ✓

+49.96 = N " " #2 5.67 7.06 ✓

+55.65 = S " " #3 5.60 7.13 ✓

+61.62 = N " " #3 5.60 7.13 ✓

+73.6 = S " " #4 5.94 1.79 ✓

+79.2 = N " " #4 5.91 1.84 ✓

2+15.0 = S " " #5 5.80 1.93 ✓

+20.75 = N " " #5 5.77 1.96 ✓

2+15.9 = S " " #6 5.78 1.95 ✓

+21.47 = N " " #6 5.77 1.96 ✓

306
506 +0423 = S " " #7 5.29 7.44 ✓

" 709.9 = N " " #7 5.29 7.44 ✓

Truck Levels E Line 1st

1+08.79 = S. Rail Truck #1 5.89 1.85 ✓

1+13.51 = N " " #1 5.76 1.97 ✓

11.04
1+24.55 = S. Rail " #2 5.63 7.10 ✓

472
1+29.27 = N " " #2 5.62 7.11 ✓

1+29.23 = S. Rail Truck #3 5.63 7.10 ✓

3.72?
1+32.85 = N " " #3 5.62 7.11 ✓

14.38
1+47.33 = S " " #4 5.85 1.88 ✓

4.74
+52.05 = N " " #4 5.87 1.86 ✓

+85.84 = S " " #5 5.92 1.81 ✓

0.72
1+90.56 = N " " #5 5.89 1.84 ✓

+92.26 = S " " #6 5.89 1.84 ✓

+96.98 = N " " #6 5.86 1.87 ✓

2+33.92 = S " " #7 5.39 7.34 ✓

+38.98 = N " " #7 5.40 7.33 ✓

Truck Levels E Line 1st Ave

0+80.87 = S. Rail Truck #1 6.04 1.69 ✓

+80.2 = N " " #1 6.04 1.69 ✓

1+02.4 = S " " #2 5.68 7.05 ✓

1 " " #2 5.68 7.05 ✓

702.88 = S " " #3 5.66 7.07 ✓

702.88 = N " " #3 5.69 7.04 ✓

1+20.75 = S " " #4 5.86 1.87 ✓

1 " " #4 5.86 1.87 ✓

1+55.29 = S " " #5 5.90 1.83 ✓

1 " " #5 5.96 1.77 ✓

773

1+692/S. Rail Track #6	6.09	1.64
" " " #6	5.96	1.77
2+0184-S " #7	5.45	1.78
" " " #7	5.42	1.31

Cross Sections for Yardage Cont.

1+50

W-5	6.3	1.43
W	6.2	1.53
cb	6.1	1.63
1/4	6.4	1.33
L	6.3	1.43
1/4	6.5	1.73
Ecb	6.4	1.33
L	6.4	1.33
+5	6.4	1.33

2+00

-5	5.9	1.83
E	6.1	1.63
cb	5.9	1.83
1/4	6.2	1.53

773

L	6.3	1.43
1/4	6.3	1.43
cb	6.3	1.43
W	6.3	1.43
+5	6.1	1.63

2+4148 = Stone J-st ^{14' cbs} 18' 11/2'

-5	5.7	1.03
W	5.8	1.93
cb	5.7	1.03
1/4	5.7	1.03
L	5.6	1.13
1/4	5.5	1.73
cb	5.3	1.43
E	5.4	1.33
+5	5.5	1.73

S cb J-st

-5	5.6	1.73
E	5.1	1.63
cb	5.1	1.63
1/4	5.1	1.63
L	5.1	1.63

W 1/4	53	7.43
W cb.	57	7.03
W L.	57	7.03
+5	58	1.93
J 1/4 J ST.		
-5	56	7.13
W	57	7.03
cb.	55	7.73
1/4	51	7.63
E	51	7.63
1/4	46	3.13
cb.	47	3.03
E	54	7.33
✓ +4.2 = W Rail Track #9	518	7.55
75 on ground	54	7.33
J 1/4 + 0815		
J Rail Track #9	512	7.61
Also " " #8	512	7.61
E - J - St.		
1 E - 27 = E Rail #8 & #9	522	7.51
E	55	7.73

1 E + 3 = S Rail #8 & #9	505	7.68
cb.	49	7.83
1/4	44	3.33
E	51	7.63
1/4	51	7.63
W cb.	51	7.63
W	50	7.73
+5	50	7.73
J 1/4 J - St.		
-5	53	7.43
W	52	7.53
cb.	51	7.63
1/4	51	7.63
E	50	7.73
1/4	51	7.63
cb.	50	7.73
E	51	7.63
+5	47	3.03
N cb.		
-5	47	3.03
E	50	7.73

E cb.	50	4.73
1/4	49	4.83
L	49	4.83
1/4	49	4.83
W cb.	59	1.83
Inlet "B" P-62		
15' Rt. on Grating	595	1.78
" " " Flood	1060	-2.87
W	50	4.73
+5	52	4.53
0+00 = W.L. J-5A		
-5	51	4.63
W.L. on Boxing	541	4.34
W cb. " "	557	4.16
W 1/4 " "	521	4.54
L " "	487	4.86
1/4	470	3.03
✓ +38 = W Rail Truck #9	472	3.01
✓ +6 = " " " #8	483	4.90
✓ +87 = E " " #9	494	4.79
✓ +110 = E " " #8	507	4.74
E cb. on Boxing	500	4.73

E on Boxing	497	4.76
0+20		
E. Line on Boxing	465	3.08
E cb.	471	3.04
+85 = E Rail Truck #8	483	4.90
1/4 on Box.	462	3.11
+05 = W Rail Truck #8	462	3.11
+06 = E " " #9	462	3.11
+57 = W " " #9	434	3.39
L on Box	452	3.71
W 1/4 " "	492	4.81
W cb. " "	537	4.36
W " "	488	4.85
TP	524	1176
	1.91	582
0+505		
W on Boxing	866	3.10
cb " "	902	4.74
1/4 " "	845	3.31
+79 = W Rail #9	825	3.51
+123 = E " #9	830	3.46
L on Box	828	3.48

E 457 = W Rail #8	817	3.69
1105 = E " #8	838	3.38
1/4 on Por. ing.	827	3.49
cb. " "	837	3.39
E " "	821	3.55

0+75

E on Por.	778	3.98
cb. " "	793	3.83
1/4 " "	784	3.94
L " "	787	3.89
W 1/4 " "	820	3.56
W/cb " "	861	3.15
W " "	823	3.53

1+00

W on Por.	778	3.98
cb. " "	806	3.70
+38 on W Rail #9	799	3.77
1/2 on Por	799	3.77
+07 on R Rail #9	801	3.75
L on Por	743	4.33
+25 = W Rail #8	733	4.43
+73 = E " #8	742	4.34

E 1/4 on Por.	741	4.35
Ecb " "	748	4.78
E " "	734	4.44

1+50

E on Por	651	5.25
" cb. "	670	5.06
" 1/4 "	650	5.26
L " "	655	5.21
W 1/4 " "	707	4.69
W/cb " "	718	4.58
W " "	679	4.97

2+00

W on Por.	595	5.81
cb. " "	627	5.49
+35 on W Rail #9	622	5.54
+82 " E " #9	621	5.55
1/4 " Por.	603	5.73
L " "	557	6.19
+26 = W Rail #8	553	6.23
+73 = E " #8	557	6.19
E 1/4 on Por.	568	5.08

Ecb. on Pav. 595 5.81-

E " " 588 6.70-

2+50

E on Pav. 464 7.17-

cb. " " 524 6.54-

1/4 " " 484 6.97-

L " " 469 7.07-

1/4 " " 507 6.69-

cb. " " 527 6.49-

W " " 496 6.80-

2+59

W on Pav. 466 7.10-

wcb. " 507 6.69-

w 1/4 " 495 6.81

L " 456 7.70-

1/4 " 467 7.09

cb. " 509 6.67-

E " 374 8.07-

2+64 = End cb on W

W on Walk. 431 7.45-

Wcb. on cb. 458 7.18-

2+68

E on Pav. 429 7.47-

cb " " 498 6.78-

1/4 " " 452 7.74

L on Pav. 432 7.44-

1/4 " Pav. 478 6.98

Wcb on " 485 6.81-

Wcb on Topcb 451 7.75-

W.L. on Walk 416 7.60-

3+00 = Shine Island Ave

W on Walk. 345 8.31-

" " cb. 392 7.84-

" " Gut. pav. 448 7.78-

cb+35 = W Rail #9 429 7.47-

+82 = E " #9 430 7.46-

W 1/4 on Pav. 410 7.66

1/4 " " 381 7.95-

+26 = W Rail #8 376 8.00-

+73 = E " #8 375 8.01-

1/4 on Pav. 498 7.78

cb " " 343 8.33-

E " " 377 7.99-

		11.76			SE. 7 ¹ / ₂ block
T.P.	7.50	15.56	3.70	8.06	Island 4 ¹ / ₂ St Ave
chk B.P.			3.69	11.87	SW B.P.
				11.93	Market
				.06	1 ¹ / ₂ St Ave
					Record
					Err.

Walker
Furrow
10-16-41

Cross Sections Harbor Dr.
& First Ave Intersection

BM #10
P-54

	5.01	7.20	2.19
Inlet "A" on Grading	5.31	1.89	
" " " Flood Line	9.51	2.31	

Inlet "B" See P-58 For Elev.

Sec A

S.L.	5.2	7.0
L.	5.4	1.8
N.L.	5.5	1.7

Sec B

N.L.	5.6	1.6
L.	5.4	1.8
S.L.	5.2	7.0

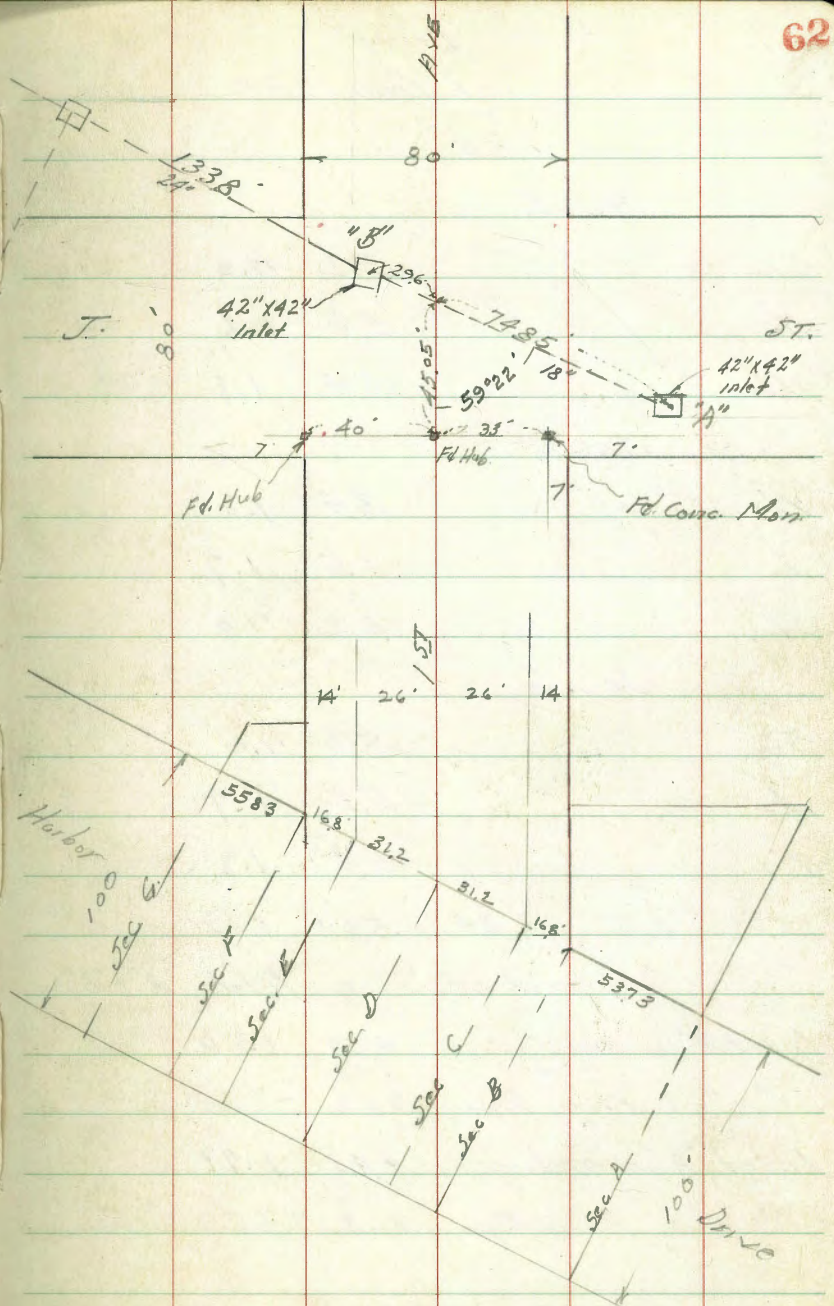
Sec C

S.L.	5.2	7.0
L.	5.3	1.9
N.L.	5.5	1.7

Sec D

N.L.	5.6	1.6
L.	5.4	1.8
S.L.	5.2	7.0

Cont. P-63



Harbor Drive

Cont. from p. 62

5
720

Sec E

SL 5.2 7.0

L 5.4 1.8

NL 5.4 1.8

Sec F

NL 5.4 1.8

L 5.5 1.7

SL 5.2 7.0

Sec G

SL 5.2 7.0

L 5.5 1.7

NL 5.4 1.8

TR 4.15 6.34 5.01 2.19

Additional shots on Inlets "A" & "B"

Inlet "B" on Grading 4.54 1.80
2.65

" " " Floor Pipe 2.19 -2.85

Inlet "A" on grading 4.43 1.91
1.20

" " " Floor Pipe 8.63 -2.29

386.82

0+31

F-113 = 1/4 Board Fence ✓

0+33

-5 2.7 3841

F 3.3 3835

4 3.4 ✓ 3834

+4 3.6 3832

W 2.8 ✓ 3840

+13 = 1/4 Picket Fence ✓

0+44

W-5.2 = 1/2 Garage Dirt Floor 2.8 3840 ✓

0+50

-5 2.8 3840

-0.2 = 1/4 Power Pole ✓

W 2.9 ✓ 3839

4 3.2 2.3 3836

F 3.2 ✓ 3836

+5 2.7 3841

0+69

W-0.4 = 1/2 10' Shed ✓

E-112 = 1/4 Board Fence ✓
1/4 Frame House

386.82

1+0

-5 2.7 3841

-10 = 1/4 Board Fence ✓
1/4 Frame House

F 3.1 ✓ 3837

4 3.2 ✓ 3836

+4 3.4 3834

W 2.7 ✓ 3841

+0.9 = 1/4 Lath Fence ✓

+10 2.8 3840

1+50

-2.2 = 1/4 3" Conc Wall Top ✓
1/4 Lath Fence 0.0 3868

-2.2 Ground 2.2 3846

W = 1/4 Power Pole ✓ 2.2 ✓ 3846

+3 2.9 ✓ 3839

4 2.8 2.9 3840

F 2.7 ✓ 3841

+0.3 = 1/4 Wire Fence ✓

+0.7 = 1/4 Board Fence ✓

+10 2.7 3841

7P 5.14 388.99 2.97 382.85

388.99

2+0

-10 4.9 384.1

-0.4 = N/4 Wire Fence ✓

F 4.6 384.4

⌘ 4.7 384.3

+5 4.9 384.1

W 4.9 384.1

+1.0 = 5/4 Sbd + N/4 8' Conc Wall Top 2.18 386.81 ✓

+10 5.0 384.0

2+21

W -7.4 = N/4 Sbd + S/4 Wire Fence ✓

2+29

W -11 = ⌘ 9' Lath House ✓

2+50

-10 4.9 384.1

-1.0 = Wire Fence ✓

-0.3 = W/4 Post Pole ✓

W 4.6 ✓ 384.4

⌘ 4.8 4.9 384.2

+5 4.7 384.3

388.99

F 5.2 ✓ 383.8

+10 5.3 383.7

2+75

-5 4.9 384.1

F 5.0 5.1 384.0

⌘ 5.0 5.1 384.0

W 4.9 384.1

+10 4.8 384.2

3+0

-10 4.7 384.3

-15 = N/4 Wire Fence + S/4 Picket Fence ✓

W 4.7 ✓ 384.3

⌘ 4.9 5.0 384.1

F 4.8 ✓ 384.1

+0.2 = S/4 Board Fence ✓

+10 4.8 384.1

3+30

+0.2 = N/4 Board Fence + S/4 Sbd ✓

3+50

-10 4.8 384.1

38899

F 4.7 ✓ 3843

+0.4 = Nly Shed + Sty Board Fence ✓

L 46 47 3844

W 46 ✓ 3844

+0.8 = Nly Power Pole ✓

+2.1 = Nly Picket Fence + Sty Board Fence ✓

+10 4.5 3845

3+75

-10 4.2 3848

W 4.2 3848

L 4.3 3847

+5 4.2 3848

F 4.6 3844

+10 4.7 3843

4+0

-10 4.4 3846

E = Board Fence 4.5 3845 ✓

+1 4.3 3847

L 42 43 3848

W 4.2 3848

+2.3 = Nly Board Fence ✓

38899

4+01

W-22 = Sty Bldg. ✓

4+23

W-21 = Nly Bldg. ✓

4+27

W-18 = Sty Shed ✓

4+33

W-18 = Nly Shed + Sty Lat^h Fence ✓

4+51

-10 3.8 3852

-1.4 = Nly Lat^h Fence + Sty Wire Fence ✓

-0.7 = Nly Power Pole ✓

W 3.9 3851

+2 4.3 3847

L 4.3 ✓ 3847

+5 4.4 3846

F 3.9 3851

+0.2 = Board Fence + Shed ✓

388.99

4+75

-10 4.4 384.6

-0.6 = Board Fence ✓

F 4.4 384.6

+3 4.5 384.5

L 4.5 384.5

+5 4.6 384.4

W 4.2 384.8

+1.0 = Wire Fence ✓

+1.0 4.2 384.8

5+0

-10 4.3 384.7

-1.0 = Wly Wire Fence x Sly Board Fence ✓

W 4.3 384.7

L 4.3 ✓ 384.7

F 4.1 384.9

+0.2 = Board Fence ✓

+1.0 4.2 384.8

5+11

F+0.1 = Wly Board Fence + Sly Shed ✓

388.99

5+24

F+0.2 = Wly Shed + Sly Board Fence ✓

5+35

-10 4.3 384.7

F 4.3 384.7

+0.2 = Board Fence ✓

L 4.5 384.5

W 4.2 384.8

+0.8 = Wly Board Fence ✓

+1.0 = Sly Shed ✓

+1.0 4.2 384.8

5+50

-1.0 = Wly Shed + Sly Board Fence ✓

W = Wly Power Pole / 4.2 384.8

L 4.6 ✓ 384.4

+7.3 = Board Fence ✓

F 4.6 384.4

+1.0 4.1 384.9

5+75

-7.0 4.0 385.0

F 4.3 384.7

388.99

2	4.4	3846
---	-----	------

H	4.2	3848
---	-----	------

+5	4.2	3848
----	-----	------

TP	4.75	390.08	366	385.33
----	------	--------	-----	--------

670

-10	4.5	3856
-----	-----	------

-2.0 = Board Fence			✓
--------------------	--	--	---

H	4.8	3853
---	-----	------

2	5.1	3850
---	-----	------

+5	5.1	3850
----	-----	------

F = Sly Sheds Wly Board Fence	5.3	3848	✓
----------------------------------	-----	------	---

+10	5.1	3850
-----	-----	------

6731

H-1.8 = Wly Power Pole			✓
------------------------	--	--	---

6737

F +0.2 = Wly Sheds & Sly Garage			✓
---------------------------------	--	--	---

6750.81 = S.L. E + W Alley

F	4.7	3854
---	-----	------

+0.35 = Wly Car Garage Photo Room	4.75	385.35	✓
-----------------------------------	------	--------	---

2	4.7	385.4
---	-----	-------

H	4.7	385.4
---	-----	-------

+ 2.2 = Wly Board Fence

390.08

TP	4.02	390.80	5.30	386.78
----	------	--------	------	--------

0-12 = WCB Line 33rd St

S on Parking		5.39	384.41
--------------	--	------	--------

2		5.43	384.37
---	--	------	--------

H		5.36	384.44
---	--	------	--------

0+0 = Wly 33rd St

H on Parking No Carb		4.74	386.06
----------------------	--	------	--------

2		5.04	385.76
---	--	------	--------

S = FLY Lot & Lot's Fence ✓		4.64	386.16
-----------------------------	--	------	--------

0+16

-10		5.0	385.8
-----	--	-----	-------

S		4.9	385.9
---	--	-----	-------

+0.8 = Sly Power Pole			✓
-----------------------	--	--	---

2		4.8	386.0
---	--	-----	-------

H		4.5	386.3
---	--	-----	-------

+10		4.1	386.7
-----	--	-----	-------

0+50

-10		4.4	386.4
-----	--	-----	-------

H		4.6	386.2
---	--	-----	-------

2		4.8	386.0
---	--	-----	-------

390.80

+5	4.9	385.9
5	5.2	385.6
+0.2 = Low Latex Fence		✓
+10	5.3	385.5

0+53

H-0.3 = Fly Sbrd

0+67

H-0.4 = Fly Sbrd

0+68

H-0.4 = Fly Bldg.

0+78

H-0.3 = Fly Bldg. + Fly Wire Fence

1+0

-10	5.6	585.2
5	5.4	585.4
2	5.1	585.7
H	5.3	585.5
+10	5.2	585.6

1+06

5 = Fly Low Latex Wire Fence = H.E. Car Garage ✓

H-0.8 = Fly Wire Fence ✓

390.80

1+25/8 = Fly H.S. Fly

-10	5.4	385.4
H	5.4	385.4
+4	5.7	385.1
2	5.3	385.5
5	5.4	385.4

1+40 H-W.L. H.S. Fly

5	5.4	385.4
2	5.5	385.3
H	5.6	385.2
+10	5.6	385.2

1+43

5 = Fly Board Fence ✓

5+0.8 = Fly Power Pole ✓

TP 5.33 390.81 5.32 385.48

0+2 Hub
N+S Fly
Fly

1+65

-10	4.9	385.9
H	5.3	385.5
2	5.5	385.3
+7.3 = Fly Board Fence		✓
5	5.4	385.4
+10	5.3	385.5

390.81

1+78

S-6.3 = 1/2 Garage Concrete Floor 5.49 385.32 ✓

1+89

S-0.3 = Wly Picket Fence ✓

2+0

-10 5.5 385.3

5 5.2 385.6

1/2 5.1 385.7

H 5.1 385.7

+10 4.9 385.9

2+10

S-0.5 = Wly Picket Fence ✓

S = 1/2 + Ely 3' Wide Cypress Hedge ✓

2+16

-10 4.7 386.1

H = SE Cor Stecco Bldg 4.8 386.0 ✓

1/2 4.9 385.9

5 4.8 386.0

+5 5.0 385.8

390.81

2+29

-5 5.2 385.5

5 5.0 385.8

+0.8 = SW Power Pole

1/2 5.2 385.6

H = SW Stecco Bldg 4.9 385.9 ✓

2+60

-0.1 = SW Cor Stecco Bldg ✓

H 5.7 385.1

1/2 6.0 384.8

5 5.8 385.0

+5 6.0 384.8

2+65.32 = F.L. Bancroft

-1.5 = 1/2 + Wly 3' Cypress Hedge ✓
5 on Curb End 6.48 384.33

5 on Pav 174 6.67 384.14

1/2 " " 6.69 384.12

H " " 6.49 384.32

H on Curb End 6.29 384.42

390.81

2477.32 = ECL line of Boocroft

H 27 Paving 7.49 383.32

4 " " 7.66 383.15

5 " " 7.51 383.30

TP 6.34 390.15 7.00 383.81

BM 4.84 385.81

SFBP
Admst
3202.51
385.80

The image shows an open notebook with two blank pages. The pages are cream-colored and feature light blue horizontal ruling. Vertical red lines create margins on both pages. The right page has the number '73' printed in red in the top right corner. The notebook is placed on a white surface, and the dark cover is visible at the edges.

Bliss Notes
 50 miles West
 Fortson Rd
 5/11/41

Indexed
 c.s.r.k.

Levels on Scott St from the E of

Carlton North to E of Lowell St

BM	1.27	<u>7.61</u>	6.34	NE 70° TR Carlton & Scott
0400	E Carlton road	1.95	5.6	Red. by ② 7/23/41
2135	on Perry W Line Dickens	4.58	3.0	ck. ② 7/23/41
2470	E Dickens	4.2	3.4	
5140	E Emerson	6.8	0.8	
TP	1.00	<u>3.14</u>	5.47	2.14
8+10	E Fenelon	6.5	-3.4	
10+80	E Garrison	8.0	-4.9	
13+15	W Line Hugo	4.7	-1.6	
+20		2.0	1.1	
13+50	E Hugo	2.1	1.0	
TP	3.30	<u>4.96</u>	1.48	1.66
16+20	E Inglow	5.5	-0.5	
18+90	E Jarvis	4.4	0.6	
21+60	E Keats	4.7	0.3	
24+30	E Lowell	3.4	1.6	
24+65	N. Line of Lowell	2.9	2.1	
24+80	Approx Naval Res. line	7.61	11.1	
TP	12.47	<u>12.75</u>	4.68	0.28
check Sta	BM NW Hemlock Pines	3.30	9.45	Iron SPIKES ch.

Walker Re. Cross SECTION East and West
 Hurdin 15' Alle Block 38 Normal Hts.
 Huntley Between 33rd + Bancroft St.
 12-28-45 South of Adams Ave

Re. by Wherry
 1-2-46

Sketch P64

Same as original notes

Note: Location fences Palae etc.

(390.88)

384.37

B.M. on East
 end cb. on North
 2+65.32
 Page 71

6.51 390.93

384.42

0-12 = West cb 33rd St

S cb Ret 5.25 385.63

S on Pav 5.46 385.42

S " " 5.51 385.37

N " " 5.49 385.39

N cb Ret 5.02 385.86

0-1.55 = West East cb + Walk

N on cb = W end 4.70 386.14

" Gut 4.82 386.06

S 5.15 385.73

+4 5.04 385.84

S on Pav 4.83 386.05

" " cb = W end 4.85 386.03

0+00 = W.L. 33rd

S on Ground 4.9 386.0

" " Pav 4.72 386.16

+25 on Pav 4.83 386.05

+3 " " 5.08 385.80

390.93

76

S on Pav 5.12 385.76

N " " 4.80 386.08

" on Ground 4.9 386.0

0+16

-5 4.4 386.5

N " " 4.6 386.3

S 4.9 386.0

0 5.1 385.8

+5 5.1 385.8

0+50

-5 5.3 385.6

5 5.3 385.6

S 5.0 385.9

N 4.6 386.3

+5 4.5 386.4

1+00

-5 5.3 385.6

N 5.3 385.6

S 5.3 385.6

5 5.5 385.4

+5 5.7 385.2

B.M.'s See p. 78

Wherry-

Adjusted to Conform to 1-2-46.

390.93 E+VY Alley
 816 38
 1+25.16 EL. South Alley (Cont. from P-76)

S	390.88	5.4	385.5
Q		5.5	385.4
N		5.4	385.5
+10		5.4	385.5

1+40.16 = W.L. Alley to South

-10		5.5	385.4
N		5.4	385.5
Q	5.7	5.8	385.1
S		5.5	385.4

1+65

-5		5.7	385.2
S		5.6	385.3
Q	5.6	5.5	385.4
N		5.3	385.6
+5		5.1	385.8

2+00

-5		5.1	385.8
N		5.0	385.9
Q		5.1	385.8
S		5.2	385.7
+5		5.6	385.3
+15		5.6	385.3

390.93

77

2+16

-5	390.88	5.3	385.6
S		5.1	385.8
+2		4.8	386.1
Q		5.1	385.8
N		4.8	386.1
+5		4.8	386.1

2+39

N at Bld.		4.8	386.1
Q		5.2	385.7
S		5.2	385.7
+5		5.4	385.5

2+60

-5		5.8	385.1
S		5.8	385.1
Q		6.2	384.7
N		5.8	385.1
+0.1 at Bld.		5.8	385.1

2+65.32 = E. Line Bancroft St.

N cb.		6.51	384.37
N Pav.		6.58	384.30

390.93
2+6532 Cont. from P 77

S on Pav. (390.88) 6.80 384.08

+5 = 8th. in Pav. 6.69 384.19

S on Pav. 6.76 384.12

" " cb. 6.56 384.32

2+7732 = E cb. Bancroft

TP #1 5.29 388.99 7.23 383.70 383.65

-25' on Pav. (388.94) 5.83 384.11

S 5.72 383.22

S on cb. 4.91 384.03

L = Low Point (Water standing) 5.78 383.16

N 5.58 383.36

" on cb. Red. 4.89 384.05

+25 on Gut. (Water standing) 5.61 383.33

" " cb. 4.77 384.17

TP #2 6.93 391.91 4.01 384.98

TP #3 5.42 393.56 3.77 388.14

chk NW 1/4 B.P. Adams = fella 503 388.53
388.32 = Record
0.21

Adams + 34th
chk SW 1/4 B.P. 4.04 389.52
389.27 Record
0.25

Locals Cont. from TP # 2 78

TP #4 5.86 390.84 384.98

(BM Gonia)
chk cb. Red. SE 32nd + Adams 4.99 385.85 = curb
385.80 = BM. P. 64

TP #4 6.59 393.86 3.57 387.27

TP #5 5.44 395.32 3.98 389.88

Bancroft + Adams
chk SE B.P. 4.20 391.12

390.26 = Record.
0.16

BM
TP #2 4.06 389.04 384.98

chk TP #1 5.35 383.69
383.70
0.01

chk. standing BM = cb. 4.62 384.42 ✓

TP #6 3.05 386.86 6.03 383.01

N.L. Madison
chk 0200 on Ecb. 3.78 382.28 382.21

" " " wcb. 3.88 382.18 382.13
0.05

0.07 Error

Levels for BM's on Interceptor Line Change

BM	4.11	11.29		7.18	2 x 2.574 x 2 50' at Sta 16+35.8 Old line
Set BM			5.35	5.94	85' at 10+21.72 New line

BM	2.57	11.21		8.64	
Set BM			4.45 6.76	6.76	X in P.M. Base at M.H.

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
1°	50.00	.22	11°	551.70	26.50	21°	1061.9	97.57
10'	58.34	.30	10'	560.11	27.31	10'	1070.6	99.16
20	66.67	.39	20	568.53	28.14	20	1079.2	100.75
30	75.01	.49	30	576.95	28.97	30	1087.8	102.35
40	83.34	.61	40	585.36	29.82	40	1096.4	103.97
50	91.68	.73	50	593.79	30.68	50	1105.1	105.60
2	100.01	.87	12	602.21	31.56	22	1113.7	107.24
10	108.35	1.02	10	610.64	32.45	10	1122.4	108.90
20	116.68	1.19	20	619.07	33.35	20	1131.0	110.57
30	125.02	1.36	30	627.50	34.26	30	1139.7	112.25
40	133.36	1.55	40	635.93	35.18	40	1148.4	113.95
50	141.70	1.75	50	644.37	36.12	50	1157.0	115.66
3	150.04	1.96	13	652.81	37.07	23	1165.7	117.38
10	158.38	2.19	10	661.25	38.03	10	1174.4	119.12
20	166.72	2.43	20	669.70	39.01	20	1183.1	120.87
30	175.06	2.67	30	678.15	39.99	30	1191.8	122.63
40	183.40	2.93	40	686.60	40.99	40	1200.5	124.41
50	191.74	3.21	50	695.06	42.00	50	1209.2	126.20
4	200.08	3.49	14	703.51	43.03	24	1217.9	128.00
10	208.43	3.79	10	711.97	44.07	10	1226.6	129.82
20	216.77	4.10	20	720.44	45.12	20	1235.3	131.65
30	225.12	4.42	30	728.90	46.18	30	1244.0	133.50
40	233.47	4.76	40	737.37	47.25	40	1252.8	135.35
50	241.81	5.10	50	745.85	48.34	50	1261.5	137.23
5	250.16	5.46	15	754.32	49.44	25	1270.2	139.11
10	258.51	5.83	10	762.80	50.55	10	1279.0	141.01
20	266.86	6.21	20	771.29	51.68	20	1287.7	142.93
30	275.21	6.61	30	779.77	52.89	30	1296.5	144.85
40	283.57	7.01	40	788.26	53.97	40	1305.3	146.79
50	291.92	7.43	50	796.75	55.13	50	1314.0	148.75
6	300.28	7.86	16	805.25	56.31	26	1322.8	150.71
10	308.64	8.31	10	813.75	57.50	10	1331.6	152.69
20	316.99	8.76	20	822.25	58.70	20	1340.4	154.69
30	325.35	9.23	30	830.76	59.91	30	1349.2	156.70
40	333.71	9.71	40	839.27	61.14	40	1358.0	158.72
50	342.08	10.20	50	847.78	62.38	50	1366.8	160.76
7	350.44	10.71	17	856.30	63.63	27	1375.6	162.81
10	358.81	11.22	10	864.82	64.90	10	1384.4	164.86
20	367.17	11.75	20	873.35	66.18	20	1393.2	166.95
30	375.54	12.29	30	881.88	67.47	30	1402.0	169.04
40	383.91	12.85	40	890.41	68.77	40	1410.9	171.15
50	392.28	13.41	50	898.95	70.09	50	1419.7	173.27
8	400.66	13.99	18	907.49	71.42	28	1428.6	175.41
10	409.03	14.58	10	916.03	72.76	10	1437.4	177.55
20	417.41	15.18	20	924.58	74.12	20	1446.3	179.72
30	425.79	15.80	30	933.13	75.49	30	1455.1	181.89
40	434.17	16.43	40	941.69	76.86	40	1464.0	184.08
50	442.55	17.07	50	950.25	78.26	50	1472.9	186.29
9	450.93	17.72	19	958.81	79.67	29	1481.8	188.51
10	459.32	18.38	10	967.38	81.09	10	1490.7	190.74
20	467.71	19.06	20	975.96	82.53	20	1499.6	192.99
30	476.10	19.75	30	984.53	83.97	30	1508.5	195.25
40	484.49	20.45	40	993.12	85.43	40	1517.4	197.53
50	492.88	21.16	50	1001.7	86.90	50	1526.3	199.82
10	501.28	21.89	20	1010.3	88.39	30	1535.3	202.12
10	509.68	22.62	10	1018.9	89.89	10	1544.2	204.44
20	518.08	23.38	20	1027.5	91.40	20	1553.1	206.77
30	526.48	24.14	30	1036.1	92.92	30	1562.1	209.12
40	534.89	24.91	40	1044.7	94.46	40	1571.0	211.48
50	543.29	25.70	50	1053.3	96.01	50	1580.0	213.86

2.13 on B.M.
 125.804 1498.5 on Top 1066
 1498.3 55/100
 8.0 on plumb 1495

4.77
 5.85
 1062

100 ft Locust in sc 8 year 35.259
 612
 29.139

179066
 120 38
 59072

So. of 5.72 line 15-225-612
 4.6
 5.1 on 70.6

959 934
 1091
 1063

DISTANCES FROM CENTER OF ROADWAY FOR
 CROSS-SECTIONING.
 Roadway 16 feet wide. Side Slopes 1 on 1 1/2
 For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20-16) * 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.