

1608

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and

SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 66 feet wide Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on 1½ see inside of back cover.
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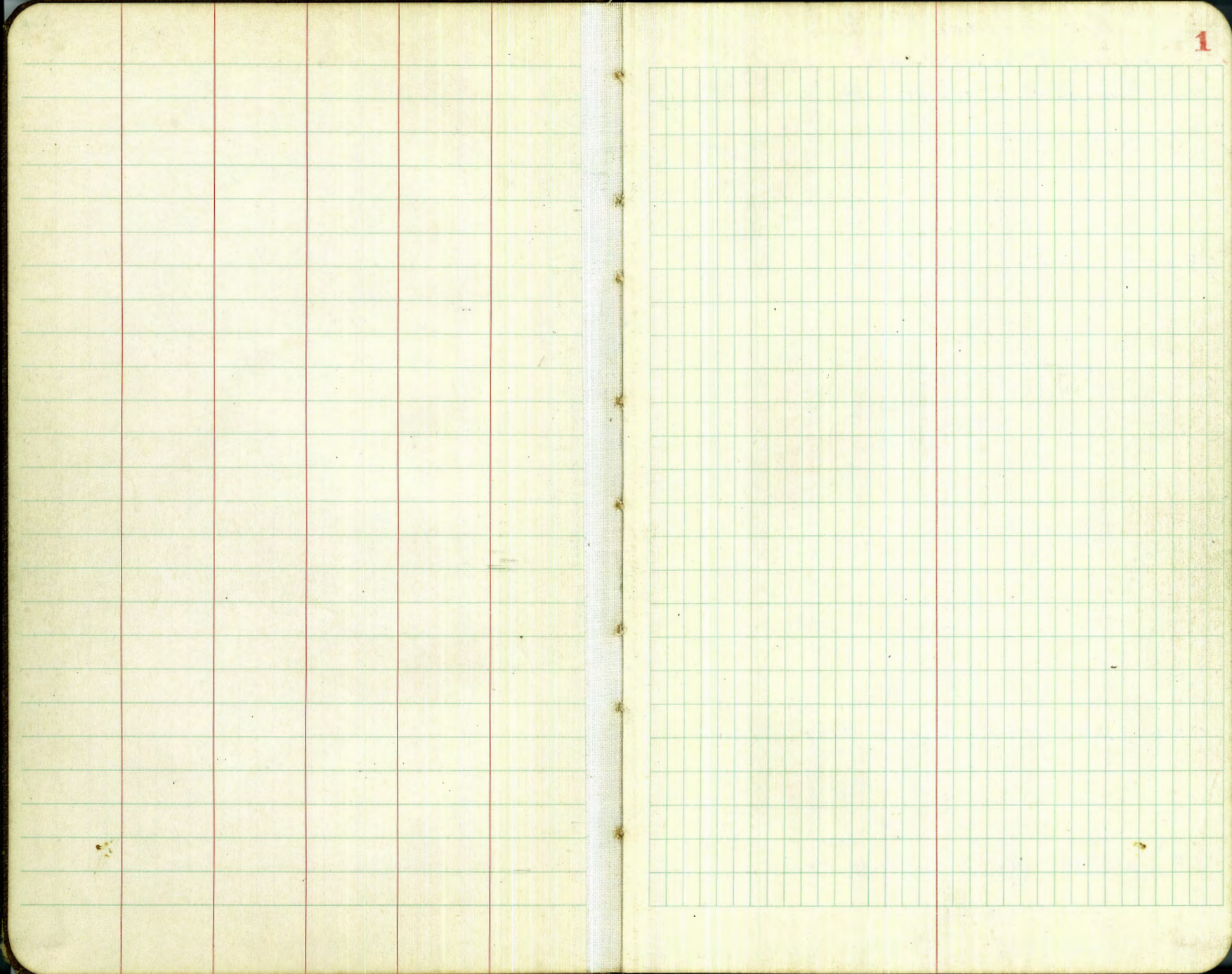
1608

CITY ENGINEER

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO,
CALIFORNIA.

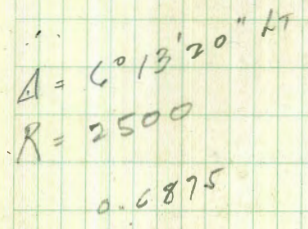
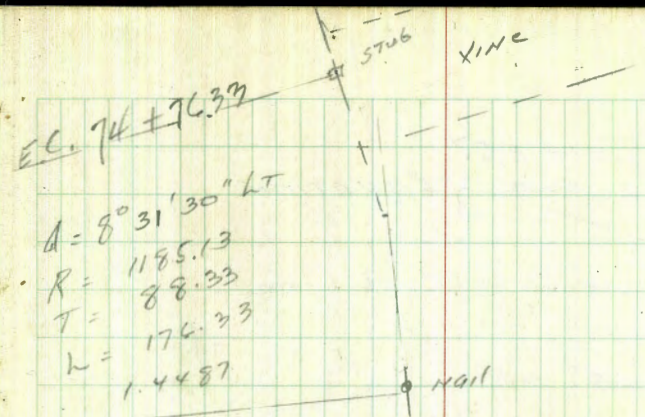
The paper stock of this book is made of a high grade 50% rag paper having a water resisting surface. This book is sewed with Bing Special Enamel Waterproof Thread.

Made in U. S. A.



Interceptor Sewer
line change at
Pacific + Vine St.

73+00 P.C.C.



road Rec $\frac{16.45}{26}$

70+28.49 B.C.L.T. on $\frac{1}{2}$ Prop. Sewer

68+45.74 B.C. Ely Line Pacific



81+09.86 = old E.C.
81+08.67 = P.O.T. } EQUATION

80+60.36 INT. WITH CURB LINE

80+16.98 EC

79+93 ST. LITE

79+50 OR E. OF E. EDGE WALK

79+29.47 B.C.L.T. OR WEST OF E. EDGE WALK

78+72 ST. LITE

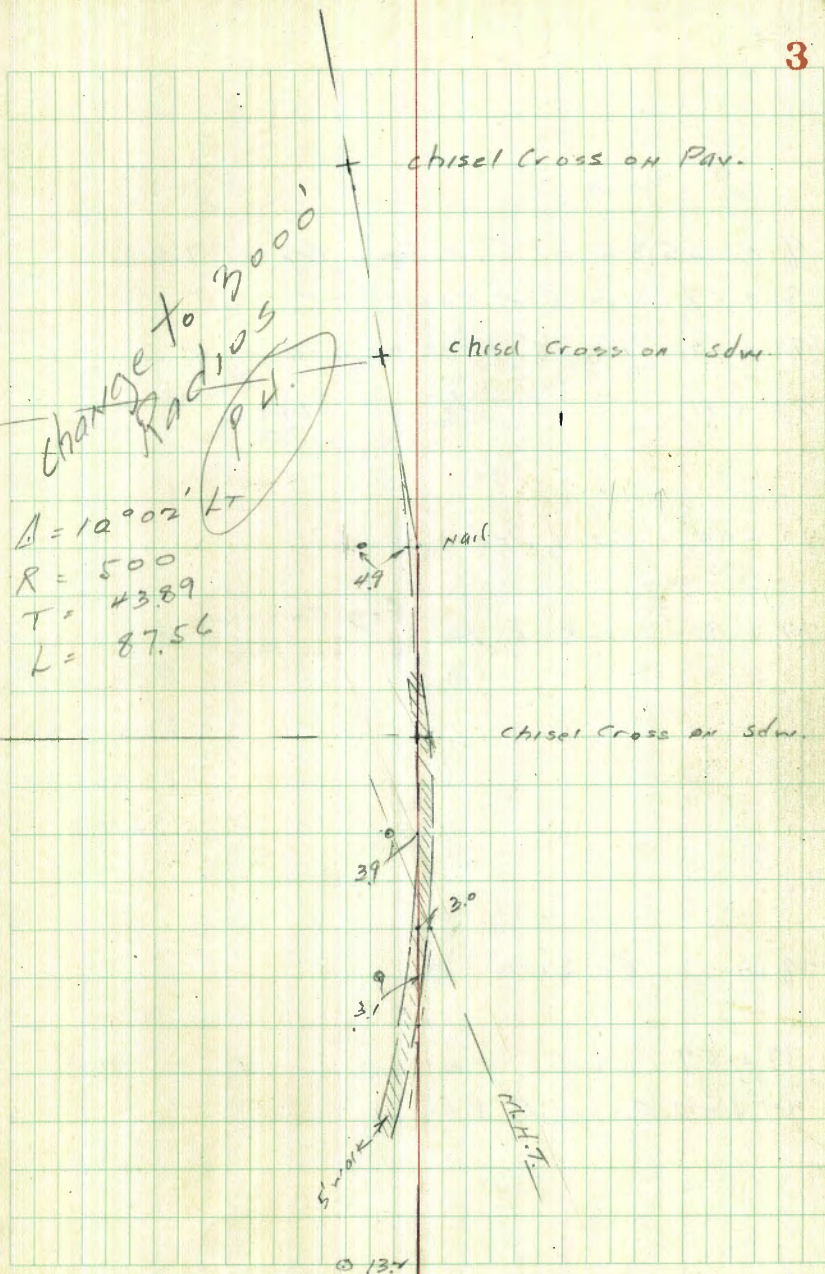
77+94.1

77+57 ST. LITE

76+44.5 = INT. WITH E. EDGE OF 5' WALK

76+27 ST. LITE

75+13 ST. LITE



81+35.30 = E.C. = Egn. 82+37.03

81+58 end Con. Pav

81+30 Int. 18" Con. Pipe drain

81+11 9.6 RT to ST. LITE

79+94 ST. LITE

79+18 Int. 2' cb. Pav. $\Delta = 10^{\circ}00'$ LT

6" Con. Pav

$R = 3000$

$T = 263.35$

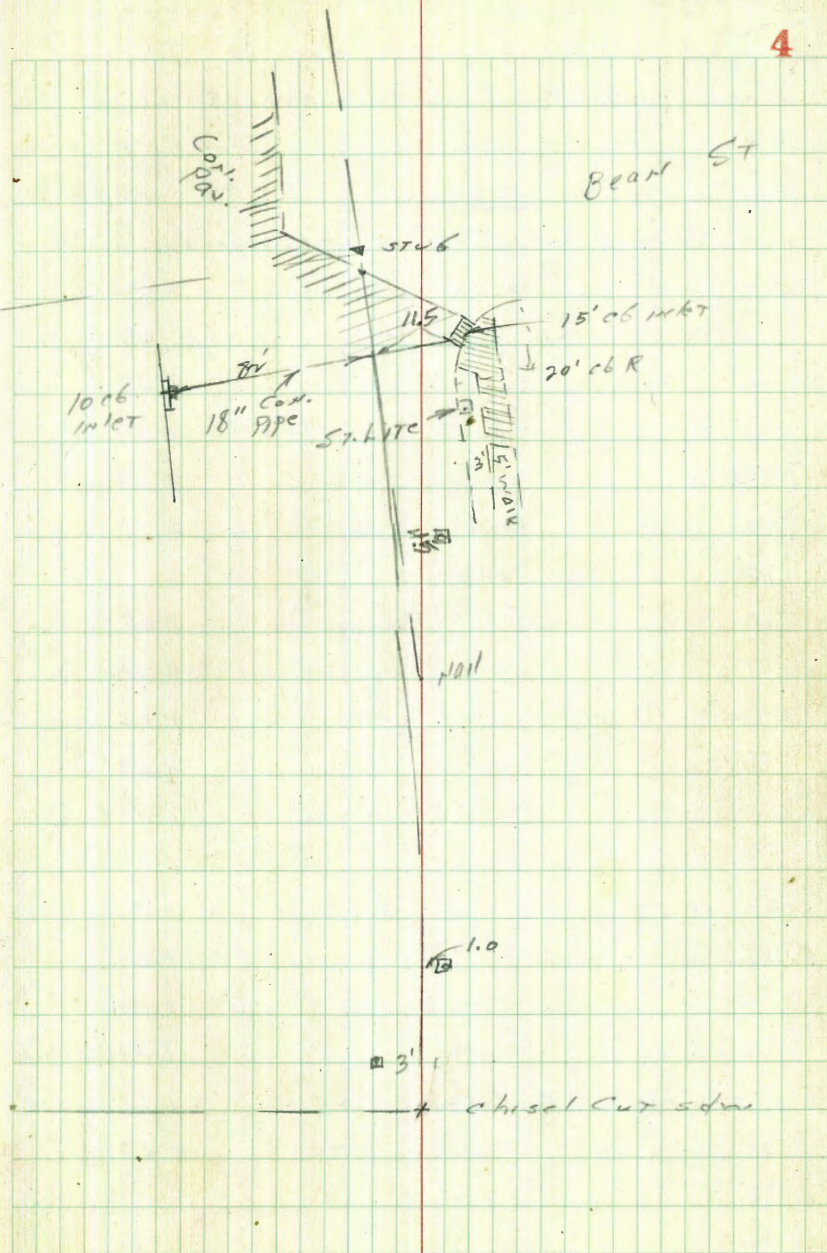
$L = 525.34$

0.573

78+74 ST. LITE

77+57 ST. LITE

77+09.96 BC LT



7-30-41 E. Moore
E. Farrow

51 Roadway
12.75 '1/4

add. Levels on G ST.

Ret. to Pac. see 1537-1

SWBP	2.77	<u>5.73</u>	296	G + KETNER
	0 + 0 w.k. Ket. No change beg. oil Pav.			
	0 + 15			
S	gut	oil Pav.	3.71	2.02
1/4	"	"	3.20	2.53
C	"	"	3.04	2.69
1/4	"	"	3.15	2.58
N	gut	"	3.00	2.73
	0 + 50			
N	gut	oil	3.30	2.43
1/4	"	"	3.49	2.24
C	"	"	3.21	1.92
1/4	"	"	4.10	1.63
S	gut	"	4.40	1.33
	1 + 00			
S	gut	"	4.96	0.77
1/4	"	"	4.44	1.29
C	"	"	4.27	1.46
1/4	"	"	4.14	1.59
+ 57	edge oil Pav to West		3.85	1.88
N	gut	"	3.60	2.13

Plot on Paper Profile at Scale

checked & replotted 10/6/41 Olson

Indexed
LM

573

	1 + 33	open ditch on N unchanged.		
N	gut + 7	oil	4.46	1.27
1/4	"	"	4.58	1.15
C	"	"	4.20	1.13
1/4	"	"	4.81	0.92
S	gut	"	5.12	0.61
	1 + 50			
S	gut	oil	5.14	0.59
1/4	"	"	4.78	0.75
C	"	"	4.73	1.00
1/4	"	"	4.72	1.01
+ 5.7	"	"	4.57	1.16
	1 + 75			
N	gut + 7	oil	4.93	0.80
1/4	"	"	4.86	0.87
C	"	"	4.95	0.78
1/4	"	"	5.00	0.73
S	gut	"	5.07	0.66
S	Curb Top		5.01	0.72
	2 + 00.11 E L Calif.			
S	gut	oil	5.01	0.72
1/4	"	"	4.73	1.00
C	"	"	4.57	1.16
1/4	"	"	4.46	1.27
+ 5.7	"	"	4.53	1.20

3+09				
N gut	+7	oil	4.34	1.39
1/4		"	4.34	1.41
c		"	4.36	1.37
1/4		"	4.53	1.20
S gut			4.61	1.12
S			4.6	1.1
3+24.7 Conc. unchanged				
T.P.	5.03	6.98	4.18	1.55
3+00				
-10			5.7	1.3
S			5.5	1.5
cb			5.4	1.6
1/4			5.3	1.7
c			5.3	1.7
1/2			5.3	1.7
cb			5.3	1.7
N			5.2	1.8
+10			5.2	1.8
3+24.7 E.H. Ramp just constructed				
-10	ground		4.9	2.1
N	on oil		4.83	2.15
cb	" "		5.33	1.65 ✓

1/4		5.3	1.7
c		5.4	1.6
1/4		5.4	1.6
cb		5.7	1.4
S		5.7	1.4
+10		5.7	1.4
3+78.5 = w/h Ramp to loading Plat.			
-10		4.5	2.5
S		4.5	2.5
cb		5.0	2.0
1/4		5.1	1.9
c		5.1	1.9
1/4		5.0	2.0
cb	on oil	5.00	1.98 ✓
N	" "	4.47	2.51
+10	ground	4.5	2.5
4+15			
-10		4.5	2.5
N		4.7	2.3
cb		4.9	2.1
1/4		4.9	2.1
c		4.9	2.1
1/4		4.7	2.3
cb		4.4	2.6
S	15' walk 3' wide	4.00	2.98
Sedge on sk G ST.			

Santa Fe RR
has filled hole
N of G ST.

4 + 40

S	3.4	36
cb	4.7	28
1/4	4.4	26
c	4.6	24
1/4	4.4	26
cb	4.4	26
N	4.4	26
+10	4.2	28

4 + 75.7 = E L Pacific

-10	4.0	30
N	4.0	30
cb	4.0	30
1/4	3.6	34
c	3.6	34
1/4	3.7	33
cb	3.8	32
S	4.0	30

5 + 27.7 E edge Pav on Pac.

E Pav.	3.3	335 ✓
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Add. Levels on F St.

Kettner to Pacific
See FB. 1532-6-7

SEBP 4.60 10.05 5.45 F&Kettner

wk Kettner 0+100
0+05

S 4.4 5.5

cb 4.4 5.7

gut 5.3 4.8

1/4 4.8 5.3

c 4.7 5.4

1/4 4.9 5.2

cb Topid wall 4.5 5.6

N 4.6 5.5

0+50+

N 4.45 5.60

cb 4.7 5.4

1/4 4.9 5.2

c 4.8 5.3

1/4 4.8 5.3

cb 5.4 4.7

+2 4.8 5.3

S 4.6 5.5

0+75

S 4.6 5.5

+10 4.8 5.3

8-5-41 Red. Plot
C.D.H.
chk. v Plotted 10-6-41
0/304

cb 5.6 4.5

+3 5.1 5.0

1/4 4.9 5.2

c 4.8 5.3

1/4 4.9 5.2

cb 4.9 5.2

N 4.4 5.7

0+84.4

N 4.7 5.4

cb 5.1 5.0

1/4 4.9 5.2

c 4.8 5.3

1/4 4.9 5.2

+6 4.8 5.3

cb FL Box in lot 6.4 3.7 ✓

+3 5.2 4.9

S 5.2 4.7

0+93

S Top E.R. spur 5.07 4.98

cb 5.0 5.1

1/4 4.8 5.3

c 4.7 5.4

1/4 4.8 5.3

cb Top grate 5.6 4.5 ✓

+6 over SUMP 5.0 5.1

N 4.8 5.3

10.05

1+21.90
 S Consider 5.15 4.90 New
 S+8.3 Car. II 5.13 4.92 Work
 No change on track #1

T.P. 3.24 8.19 5.10 4.95

1+44
 S con. sdw 3.67 4.52.2
 +8.3 " " 3.83 4.36
 cb 3.9 4.3
 cb Box outlet 5.2 3.0
 1/4 3.6 4.6
 c 3.7 4.5
 1/4 3.7 4.5
 cb 3.8 4.4
 N 3.5 4.7

1+71
 N 4.1 4.1
 cb 4.6 3.6
 +1 OUT DRAW 6.3 1.9
 +3 4.5 3.7
 1/4 4.5 3.7
 c 4.6 3.6
 1/4 4.5 3.7

8.19

9

1/4 + 6 4.4 3.6
 cb 5.0 2.8
 +1 4.4 3.8
 S 4.3 3.9

1+00.11 Et Cal.

S 4.5 3.7
 cb 4.7 3.5
 PUT 5.5 2.7
 1/4 4.8 3.4
 c 4.9 3.9
 1/4 5.0 3.2
 cb 4.9 3.3
 N 4.5 3.7

No change on Car. PAN. 5+ = 1532-6

3+00

N 4.8 3.4
 cb 4.8 3.4
 1/4 4.8 3.4
 c 4.8 3.4
 1/4 4.9 3.3
 cb 5.0 3.2
 S 5.0 3.2

Sta 3+17.4		P E New Track	
S	E rail	4.86	3.33
S	W "	4.86	3.33
C	E "	4.68	3.51
C	W "	4.69	3.50
N	E "	4.52	3.67
N	W "	4.52	3.67
Sta 3+29.1		P of Middle New Tr.	
N	E rail	4.53	3.66
N	W "	4.56	3.63
C	E "	4.28	3.51
C	W "	4.29	3.50
S	E "	4.84	3.35
S	W "	4.85	3.34
Sta 3+40.2		P W New Track	
S	E rail	4.86	3.33
S	W "	4.86	3.33
C	E "	4.66	3.53
C	W "	4.69	3.50
N	E "	4.57	3.62
N	W "	4.56	3.63
-10	3+60	5.2	3.0
S		5.1	3.1
cb		4.8	3.4
1/4		4.7	3.5

C		4.7	3.5
1/4		4.8	3.4
cb		5.0	3.2
N		5.4	3.0
+15		4.9	3.3
-15	11+00	5.4	2.8
N		5.1	3.1
cb		4.9	3.3
1/4		4.9	3.3
C		4.6	3.6
1/4		4.7	3.5
cb		4.8	3.4
S		4.8	3.4
+10		4.9	3.3
	11+50		
-10		4.8	3.4
S		4.8	3.4
-6		4.9	3.3
1/4		4.7	3.5
C		4.6	3.6
1/4		4.6	3.6
cb		4.8	3.4
N		5.2	3.0
+10		5.0	2.8

819

4 + 757

N	5.7	3.0
cb	4.9	3.3
1/4	4.3	3.9
c	4.2	4.0
1/4	4.4	3.8
cb	4.6	3.6
S	5.0	3.2

5 + 7.7

♀ E edge Pav. on Pacific	4.07	4.12
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No change of Tracks
on Pacific

11

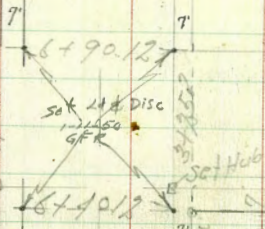
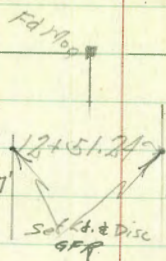
Tie Points 41st Morrison 42nd St.
Market St. F St & Hilltop St.

Indexed
LM

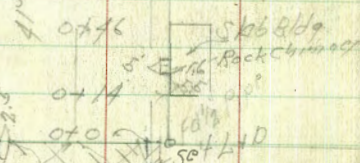
INDEXED
MK

NOV 27 1950

Hilltop



30 x 23 x 7



Additional Ties - P 60

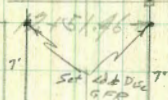
Plotted on Tie sheets 1-3-45
C.S.P.
7' Ties - Plotted - 3-20-50
M.C.

Nov. 14. 41

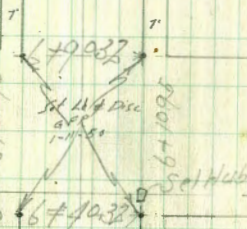
S. 5507
North 7er?
Hilltop

13

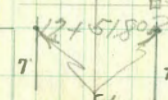
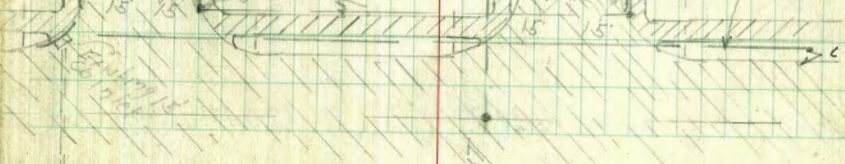
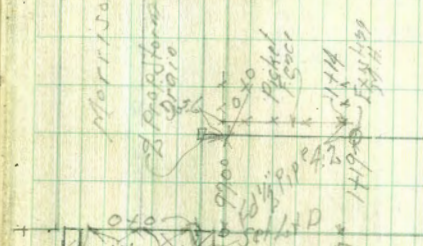
DRIVE



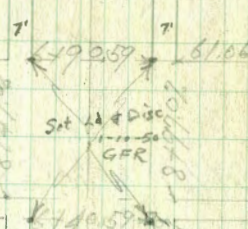
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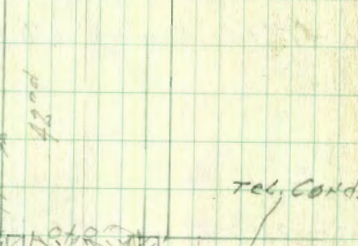
block 5
Morrison's
Maricopa Park



25 x 18 x 7



Set 14 & Disc
GPR
Set 14 & Disc
GPR



Tel. Cord.

Cross Section 41st St
Market St to Hilltop St.

Indexed
LM

1+0

0+53 22.7 Rt of L: Fly Anchor Pole

0+50

0+14

Re- \pm sec
This block
IN 1779

0+0 = H.L. Market = Hwy Paving

0-1414 = Opp $\frac{1}{2}$ Cb Returns

0-20 = H Cb line Market St

BM

7.43

132.82

125.39

H N B P
Market St
1st St

Notes reduced & plotted 1/12/54 CCH

Profile 16-28657-2562

Nov 14.41

Lt: W

Z

Rt: E

14

1274 5 30	1270 58 20	1264 64 10	1263 65 10	1253 75	1252 76 20	1246 82 26	1244 84 30	1238 90 40
1268 50 30	1265 60 20	1258 70 15	1248 80	1247 81 15	1250 78 30	1250 78 30	1251 79 40	
1264 64 30	1257 71 20	1245 83 7	1242 86	1239 89 15	1242 86 20	1241 87 30	87 30	
1252 76 30	12484 798 40-66	12424 858 20-60hr	12417 865	12350 932 20-60hr	12407 875 20-66	1240 88 30	1240 88 30	
12490 799 25-69-Cb	12428 854 25-9-60hr	12395 947 25-9-60hr	12395 887 25-9-Cb					
12533 747 40-Cb sec	12479 803 40-60hr	12422 860 40	12385 894	12347 935 20	12314 968 40-60hr	12371 911 40-Cb sec		
			132.82					

41st St.

TP 5.28 137.97 0.13 132.69

2+50

2+0

2+70

2+50

2+0

1+50

132.82

4+

2+

P+

15

133.4

7.06
3.0

132.8

7.0
3.0

132.6

6.2
3.0

132.6

6.2
3.0

131.9

6.9
3.0

131.8

7.0
3.0

132.1

6.7
3.0

131.9

6.9
3.0

130.5

6.2
3.0

132.4

6.4
3.0

131.5

7.0
3.0

130.9

7.9
3.0

130.5

7.0
3.0

130.6

6.2
3.0

130.6

6.4
3.0

130.4

6.4
3.0

130.8

7.0
3.0

132.4

6.4
3.0

132.6

6.2
3.0

132.2

6.5
3.0

131.4

7.4
3.0

130.2

7.6
3.0

129.9

6.9
3.0

129.6

6.2
3.0

129.8

6.0
3.0

131.6

7.5
3.0

131.3

7.5
3.0

131.3

7.0
3.0

130.9

7.9
3.0

130.0

7.0
3.0

129.7

6.1
3.0

129.8

6.0
3.0

129.1

6.7
3.0

129.2

6.6
3.0

130.2

7.6
3.0

130.2

7.6
3.0

129.5

6.3
3.0

129.8

7.0
3.0

128.3

7.5
3.0

128.3

7.5
3.0

128.5

7.6
3.0

127.9

7.9
3.0

127.2

5.6
3.0

128.0

7.8
3.0

127.5

5.5
3.0

127.2

5.6
3.0

126.4

6.4
3.0

126.3

6.5
3.0

126.4

6.4
3.0

126.4

6.4
3.0

125.8

7.0
3.0

132.82

4155

5725

570

475

4155

4130

470

13797

132.5	131.8	131.2	130.9	130.1	130.2	129.8
6.5 0.5	6.0 0.0	6.8 1.0	7.1	6.9	7.8 2.0	8.0 2.5
132.2	132.3	132.4	132.1	130.1	129.9	130.1
6.5 0.0	6.5 0.0	6.7 0.0	6.9	7.9	8.1 1.0	7.9 1.0
131.5	130.9	130.9	129.9	129.6	129.8	129.0
6.5 0.5	7.1 0.0	7.6 1.0	8.1	8.0 1.0	8.0 1.0	9.0 0.0
132.8	131.8	130.0	129.8	129.5	129.7	128.8
6.5 0.5	6.2 1.0	8.0 1.0	8.7	8.5 1.0	8.0 1.0	9.0 0.0
134.4	134.2	133.7	131.7	129.8	129.8	129.7
6.5 0.0	6.0 0.0	6.0 1.0	6.0	8.2 1.0	8.2 1.0	8.0 1.0
134.0	133.6	133.0	131.1	131.3	130.5	130.5
6.0	6.0 1.0	6.0 1.0	6.9	6.7	7.5 1.0	7.5 1.0
			137.97			
					129.8	128.4
					128.8	127.4
					128.5	128.3
					128.8	128.5
					129.0	128.3
					129.6	128.3
					129.9	128.8
					130.1	128.5
					130.2	129.3

6+90.12 - HL F St.

6+65.12 = 1/2 F

BM 10.93 142.75 6.15 131.82 SI Pipe
F + 4/15/02

6+40.12 = SL F St.

6+0

5+75

5+50

13797

Lt

L

Rt

17

133.7

9.1
30

133.4

9.4
30

133.1

9.7

132.5

10.3
10

132.7

10.1
10

132.1

10.7
30

133.6

9.2
30

133.4

9.4
20

132.8

10.0

132.3

10.5
20

132.5

10.4
25

132.3

10.5
30

133.7

4.8
30

133.3

4.7
20

132.9

5.1
10

142.75

132.3

5.7

132.1

5.9
10

132.0

6.0
20

132.0

6.0
30

132.6

5.4
30

132.3

5.7
20

132.4

5.6
10

132.8

5.2

131.9

6.1
1

131.6

6.4
20

131.9

6.1
24

130.9

7.1
30

130.2

7.8
10

133.5

4.6
30

133.1

4.9
20

133.0

5.0
10

133.5

4.5

131.9

6.1
4

131.2

6.8
20

131.5

6.5
25

131.0

7.0
30

129.0

9.0
45

134.3

5.7
30

133.6

4.4
20

132.4

5.6
10

131.6

6.4

130.8

7.2
30

130.5

7.5
20

130.5

7.5
25

130.1

7.9
30

129.5

8.4
10

137.97

410157

PL

9+0

8+50

8+0

7+67 = opp 4 Core Walk on Lt.

7+50

7+25

142.75

L

R

PL

18

1357

7.1
40

1365

6.5
30

1363

6.5
20

1365

6.6
10

1364

6.4

1370

6.5
30

1369

5.9
20

1370

5.8
25

1381

4.7
30

1380

4.8
40

1345

8.0
40

1347

8.1
30

1349

7.9
20

1348

8.0
10

1345

8.0

1343

8.5
10

1344

8.4
20

1346

8.8
30

1347

8.1
40

1340

8.8
40

1338

9.0
30

1339

8.9
20

1338

9.0
10

1335

9.6

1334

9.4
50

1336

9.2
20

1328

10.0
30

1324

10.4
40

133.78

8.97

30 = 4.0

Hall

1336

9.2
30

1334

9.4
20

1331

9.7
10

1329

9.9

1329

9.0
10

1330

9.8
20

1326

10.2
30

1319

10.9
40

1338

9.0
30

1335

9.3
20

1334

9.4
10

1331

9.7

1327

10.1
10

1328

10.0
20

1323

10.5
30

1320

10.9
40

142.75

41st St.

11+50

11+0

TP 11.38 153.91 0.22 142.53

10+50

10+0

9+50

9+25

142.75

Lt.

R

Pt.

19

144.6

9.5
20

144.1

9.8
20

144.1

9.8
20

143.4

10.5
15

143.7

10.2
20

143.9

10.0
20

143.9

10.0
20

143.9

10.0
20

142.2

11.7
20

142.1

11.8
20

142.1

11.8
20

142.5

11.4
20

142.5

11.4
20

142.4

11.5
20

142.6

11.0
20153.91

140.3

2.5
20

140.4

2.4
20

141.0

1.8
20

141.1

1.7
20

141.2

1.5
20

141.6

1.2
20

141.7

1.1
20

142.2

0.6
25

141.9

0.9
20

141.9

0.9
20

138.6

4.2
20

139.0

3.8
20

139.7

3.1
20

139.7

3.1
20

140.0

2.8
20

140.7

3.1
20

140.8

2.0
20

141.5

1.5
20

141.6

1.4
20

137.6

5.2
20

137.6

5.2
20

138.3

4.5
20

138.5

4.0
20

139.1

3.7
20

140.0

2.8
20

139.6

3.2
20

139.8

3.0
20

140.6

3.2
20

140.1

3.2
20

136.8

6.0
20

137.1

5.7
20

137.3

5.5
20

137.3

5.5
20

138.0

4.8
20

139.0

3.8
20

138.4

4.4
20

138.4

4.4
20

139.6

3.2
20

139.2

3.6
20142.75

41st St.

BM

0.96

152.95

2 Mon
Hilltop
152.99

12+51.24 S.L. Hilltop

12+25

12+0

11+90 Opp to 42 Conc Walk on ft.

153.91

L1

L2

L1

20

150.9 5.0 3.0	150.5 5.0 2.0	150.6 5.0 2.0	149.9 5.0 2.0	149.9 5.0 2.0	149.8 5.0 2.0	149.8 5.0 2.0	150.5 5.0 2.0	150.2 5.0 2.0
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149.3 5.0 2.0	148.9 5.0 2.0	148.6 5.0 2.0	148.6 5.0 2.0	147.3 5.0 2.0	147.3 5.0 2.0	148.1 5.0 2.0	148.1 5.0 2.0	148.2 5.0 2.0	147.9 5.0 2.0
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147.7 5.0 2.0	147.1 5.0 2.0	146.9 5.0 2.0	146.5 5.0 2.0	147.8 5.0 2.0	145.7 5.0 2.0	146.1 5.0 2.0	146.5 5.0 2.0	146.1 5.0 2.0
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147.13

5.0

2.0

147.13

✓

153.91

Cross Section Morrison St.
Market St. to Hilltop St.

Indexed
LM

L.M.

Z

RI = F, No. 17-91

21

0+75

Notes Reduced Plotted 11-21-41 CBM

0+50

0+10

0+0 = N.L. Market: N.Y. Parking

0-14.14: Opp. Cb Returns

0-20 = N Cb. in Market St.

BM

178

127.17

125.39

N.Y. B.P.
Market St.
21st St.

122.0 1224 1230 1226 1225 1225 1230 1231 1225
 $\frac{5.2}{3.5}$ $\frac{4.8}{3.5}$ $\frac{4.2}{3.5}$ $\frac{4.6}{3.6}$ $\frac{4.7}{3.7}$ $\frac{4.7}{3.6}$ $\frac{4.2}{3.5}$ $\frac{4.1}{3.5}$ $\frac{4.7}{3.5}$

1223 1223 1220 1196 1212 1212 1219 1215 1209
 $\frac{4.9}{3.5}$ $\frac{4.9}{3.5}$ $\frac{5.2}{3.5}$ $\frac{5.6}{3.6}$ $\frac{6.0}{3.0}$ $\frac{6.0}{3.0}$ $\frac{5.3}{3.5}$ $\frac{5.7}{3.5}$ $\frac{6.3}{3.5}$

1213 1201 1198 1196 1196 1197 1202 1203 1199
 $\frac{5.2}{3.5}$ $\frac{2.1}{3.0}$ $\frac{2.4}{3.5}$ $\frac{2.6}{3.0}$ $\frac{2.6}{3.0}$ $\frac{2.5}{3.0}$ $\frac{2.0}{3.5}$ $\frac{6.9}{3.5}$ $\frac{7.3}{3.0}$

1198 119.63 119.07 119.62 119.69 12033 120.5
 $\frac{2.4}{3.5}$ $\frac{7.54}{3.5}$ $\frac{8.10}{3.5}$ $\frac{7.55}{3.5}$ $\frac{7.48}{3.5}$ $\frac{6.84}{3.5}$ $\frac{6.7}{3.5}$

119.60 118.67 119.91 120.51
 $\frac{7.57}{3.5}$ $\frac{8.50}{3.5}$ $\frac{7.26}{3.5}$ $\frac{6.66}{3.5}$

119.73 118.84 118.59 118.97 119.56 119.90 12032 120.76
 $\frac{7.44}{3.5}$ $\frac{8.33}{3.5}$ $\frac{8.58}{3.5}$ $\frac{8.20}{3.5}$ $\frac{7.61}{3.5}$ $\frac{7.27}{3.5}$ $\frac{6.85}{3.5}$ $\frac{6.41}{3.5}$

127.17

TP 11.36 136.48 2.05 125.12

370 246 Pt of 2 - 5/4 Lath Fence ✓

2150

2125

210

1451 285 Pt of 2 = 5/4 Wire Fence ✓

1450

1440 244 Pt of 2 = 1/4 Picket Fence ✓

140 244 Pt of 2 = 5/4 Picket Fence ✓

12717

Lt

Rt

Rt

1235	1238	1242	1246	1245	1248	1251
3.7	3.4	3.0	3.6	3.7	3.1	3.1
30	25	15	10		15	25

1240	1240	1240	1242	1240	1241	1243
3.2	3.2	3.2	3.0	3.2	3.1	3.2
35	25	15	10		15	25

1226	1230	1240	1239	1236	1237	1242	1246
1.6	1.2	3.2	3.0	3.6	3.5	3.0	3.6
35	25	15	9		10	15	25

1222	1229	1237	1239	1240	1243	1249
5.0	2.0	3.5	3.3	3.2	2.9	2.2
35	25	15	9		15	25

1228	1233	1238	1239	1242	1246	1249
4.4	3.0	3.4	3.3	3.0	2.6	2.3
35	25	15	9		15	25

1228	1228	1237	1234	1237	1236	1238	1240
4.4	4.1	3.5	3.8	3.5	3.6	3.4	3.2
35	25	15	9		15	25	25

12717

6+0

130.1	130.1	130.8	129.8	130.2	130.1	129.9
$\frac{6.4}{35}$	$\frac{6.4}{25}$	$\frac{5.7}{15}$	$\frac{6.7}{8}$	6.3	$\frac{6.4}{15}$	$\frac{6.6}{25}$

5+50

128.7	128.8	129.3	128.3	128.7	128.6	129.1	128.8	128.7
$\frac{7.8}{35}$	$\frac{7.7}{25}$	$\frac{7.3}{15}$	$\frac{8.2}{8}$	7.8	$\frac{7.9}{3}$	$\frac{7.4}{10}$	$\frac{7.5}{15}$	$\frac{7.8}{25}$

5+0

128.1	128.1	128.0	127.5	127.2	127.2	127.5	127.3	127.7
$\frac{8.4}{35}$	$\frac{8.4}{25}$	$\frac{8.5}{15}$	$\frac{9.0}{9}$	9.3	$\frac{9.3}{6}$	$\frac{9.0}{10}$	$\frac{9.2}{15}$	$\frac{8.8}{25}$

4+50

126.9	126.6	126.5	126.2	126.2	126.2	126.5
$\frac{9.6}{35}$	$\frac{9.9}{25}$	$\frac{10.0}{15}$	$\frac{10.3}{8}$	10.3	$\frac{10.3}{15}$	$\frac{10.0}{25}$

4+25

247 Rt of $\frac{1}{2}$ = Nly High Fence ✓

4+0

125.0	124.6	124.8	125.5	125.3	125.4	125.4
$\frac{11.5}{35}$	$\frac{11.9}{25}$	$\frac{11.7}{15}$	$\frac{11.0}{7}$	11.2	$\frac{11.1}{15}$	$\frac{11.1}{25}$

3+75

242 Rt of $\frac{1}{2}$ = Nly Lot's Fence = Nly 1/2 rd Fence ✓

3+50

122.0	123.2	124.1	124.9	124.7	124.8	125.5
$\frac{12.5}{35}$	$\frac{13.2}{25}$	$\frac{13.1}{15}$	$\frac{11.6}{8}$	11.8	$\frac{11.7}{15}$	$\frac{11.0}{25}$

13648

13648

7P 12.13 148.12 0.49 135.99

7+81 243 Pt of 2 - Sky Lark's Fence ✓

7+50

7+25

6+90.22 - N.L. F.S.H.

6+65.32 - 1

6+40.32 - J.L. F.S.H.

6+20

13648

L+

L

Pt.

24

135.9	135.6	135.3	134.3	134.4	134.4	135.0	134.9
0.6	0.9	1.2	2.2	2.1	2.1	1.5	1.6
25	25	15	7		25	10	25

134.9	134.7	134.5	133.5	133.7	134.5	134.4	134.3
1.6	1.5	2.0	0.0	2.8	2.0	2.1	2.2
25	25	15	7		10	15	25

133.5	133.3	132.5	133.0	133.4	133.3	133.4
2.0	2.2	1.0	2.5	2.1	2.2	2.1
25	15	7		10	15	25

132.5	132.5	131.8	132.3	132.8	132.6
1.0	1.0	1.7	1.2	2.2	2.9
25	15	8		15	25

131.7	132.0	131.1	131.5	131.7	132.1	132.0
2.8	1.5	5.4	5.0	1.8	4.1	4.5
25	15	8		7	15	25

131.1	131.2	131.3	130.6	130.8	130.8	131.1	131.0	130.8
5.2	5.3	5.2	5.9	5.7	5.7	5.1	5.5	5.2
25	25	15	8		7	10	15	25

13648

TP 11.62 159.33 0.41 147.71

10+50

10+0

9+50

9+0

8+50

8+17 242 Rt of 1/2 = N4 Lot 5 Fence ✓

8+0

148.12

1450 5.6 25	1452 3.9 25	1455 3.6 17	1451 5.0 15	1455 3.6 2	1460 2.1	1463 1.8 15	1460 3.1 21	1462 1.0 25	1463 1.8 25
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1425 5.6 25	1426 5.5 25	1433 4.0 15	1428 5.0 17	1429 5.3 2	1435 2.5	1437 4.2 15	1434 4.0 22	1437 4.2 25	1438 1.2 25
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1402 7.9 25	1405 7.6 25	1411 7.0 15	1407 7.4 11	1408 7.0	1413 5.8 5	1416 6.5 15	1411 2.0 22	1411 7.0 25	1417 6.4 25
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1388 9.3 25	1391 9.0 25	1395 8.6 15	1390 9.1 11	1393 8.8	1397 8.4 3	1397 8.4 15	1392 8.9 21	1395 8.6 25	1399 8.2 25
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1381 10.0 25	1381 10.0 25	1381 10.0 15	1375 10.6 8	1378 10.3	1379 10.2 7	1381 10.0 15	1379 10.2 25
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1375 10.6 25	1371 11.0 25	1366 11.5 15	1364 11.7 15	1358 12.3 5	1360 12.1	1360 12.1 8	1364 11.7 15	1365 11.6 25	1369.7 11.5 25 148.12 ✓
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148.12

BM

1.69

157.64

SE 74th
Hilltop
Morrison

12 + 51.46 = S.L. Hilltop

12 + 0

11 + 50

11 + 0

159.33

1582

1577

1577

1575

1573

1566

2.6
351.6
181.6
10

1.8

2.0
152.2
25

1557

1559

1554

1550

1545

1553

1548

1543

1542

2.6
352.4
252.9
204.0
104.5
2

4.0

4.6
155.0
255.1
25

1518

1516

1518

1513

1512

1519

1519

1517

1517

2.5
352.2
252.5
208.0
108.1
2

7.4

7.4
157.6
257.6
25

1485

1484

1486

1480

1485

1491

1491

1489

1491

1491

10.8
3510.9
2510.7
1811.3
1510.8
2

10.2

10.3
1510.4
2110.7
2810.2
25159.33

TP 10.34 139.79 2.14 129.45

2+50 25 Lt of 2 - Lot 4 Fence ✓

2+0

2+52 246 Lt of 2 - Sky Lot 4 Fence ✓

2+50

2+0

1+50

1+02 16.8 Lt of 2 - N 1/4 T&E Pole ✓

1+0

131.59

128.5

127.9

128.4	128.4	127.2	128.3	128.6	128.6	129.0	129.1	129.7	129.8
3.2	3.2	4.4	3.3	3.0	3.0	2.6	2.5	1.9	1.8
25	22	20	18	15	15	15	21	25	25

127.6	127.9	126.9	127.8	128.0	127.9	128.1	128.2	128.4
4.0	3.7	4.7	3.8	3.6	3.7	3.5	3.4	3.3
25	15	21	21	15	15	15	15	25

127.7	127.1	128.1	128.2	128.1	128.1	128.2	128.4	129.1	129.6
3.9	4.5	3.5	3.4	3.5	3.5	3.4	3.3	2.5	2.0
25	22	19	15	10	15	15	20	25	25

127.6	127.8	128.4	129.0	128.4	128.2	128.4	128.8	128.9	129.3
4.0	3.8	3.2	2.6	3.2	3.4	3.2	2.8	2.7	2.5
25	25	15	10	10	15	15	20	25	25

126.3	126.5	126.7	127.1	126.8	127.0	127.4	128.0
5.0	5.1	4.9	4.5	4.5	4.6	4.2	3.6
25	25	15	10	15	15	25	25

125.1	125.4	126.3	126.6	126.1	126.1	126.2	126.4	127.0
3.5	3.3	5.0	5.0	3.5	3.5	3.4	3.2	4.6
25	25	15	11	9	15	15	25	25

131.59

6+0

5+50

5+0

4+50

4+25

4+0

253 Lt of A = 174 Lats x Sly wire Fence

139.79

129.3

10.7
35

134.1	134.3	134.9	134.7	135.2	135.0	135.3	135.9	135.7	135.5
5.7 35	5.5 35	4.9 15	5.1 10	4.6 5	4.8	4.5 15	5.9 30	4.1 25	4.3 35

131.5	132.0	132.5	132.2	132.9	132.9	133.5	133.3	133.6
8.3 35	7.8 25	7.3 15	6.6 9	6.9	6.9 16	6.3 15	6.5 25	6.2 25

130.2	130.4	130.7	131.6	131.3	131.3	131.4	131.9	131.5	131.6
9.6 35	9.4 25	9.1 15	8.2 9	8.5 5	8.5	8.4 15	7.9 19	8.3 25	8.2 25

129.5	129.7	130.1	130.1	130.3	130.3	130.4
10.3 35	10.1 25	9.7 15	9.7	9.5 15	9.5 25	9.4 35

129.8	129.4	129.7	129.9	130.0	130.4	131.2	130.9
10.5 35	10.4 20	10.1 15	9.9 9	9.8	9.4 15	8.6 25	8.9 35

129.7	129.6	128.3	129.5	129.8	129.7	130.0	130.3	130.9	130.9
10.1 25	10.2 30	11.5 15	10.3 15	10.0 10	10.1	9.8 15	9.5 15	8.9 25	8.9 35

139.99

8+02 251 Rt of 2: Sky Lot 4 Fence

8+0

7+48

7+25

6+90.59 = N L F St

TP 12.17 151.68 0.28 139.51

6+65.59 = L

BM

2.00 137.79

6+40.59 = S L F St

139.79

Hub St.
Fst. Post 7'
4178 42

Lt

S

Rt

30

1452	1455	1458	1454	1460	1462	1473	1479	1478	1480
6.5 25	6.2 25	5.9 15	6.3 10	5.7	5.5 8	4.4 14	3.8 15	3.9 25	3.7 25

1428	1432	1429	1423	1428	1430	1441	1447	1449	1452
8.9 25	8.5 25	8.8 15	9.4 10	8.9	8.7 8	7.6 15	7.0 17	6.9 25	6.4 25

1412	1417	1417	1412	1412	1415	1426	1429	1434
10.5 25	10.0 25	10.0 15	10.5 5	10.5	10.2 8	9.1 15	8.8 20	8.0 25

1395	1398	1394	1394	1393	1400	1408	1409
12.2 25	11.9 15	12.3 5	12.3	12.4 8	11.7 15	10.9 17	10.8 25

151.68

1379	1382	1385	1381	1380	1379	1388	1393	1393
1.9 25	1.6 15	1.8 8	1.7 8	1.8	1.9 7	1.9 15	0.5 17	0.5 25

1368	1369	1368	1368	1372	1379	1380
2.0 25	1.9 15	2.0 5	2.0	2.6 15	1.9 17	1.8 25

139.79

10+50

10+0

9+50

TP 4.44 156.12 0.0 151.68

9+27 246 Rt of $\frac{1}{2}$ = 1/4 Lat's Fence ✓

9+04

9+0

8+93 220 Rt of $\frac{1}{2}$ = 1/4 16' olive tree ✓

8+50

151.68

Nail Drive
Trace Pool
8+93 0.244 ✓

150.9	150.8	150.8	151.2	150.7	150.8	151.0	151.4	151.5	151.5
$\frac{1.3}{35}$	$\frac{0.9}{25}$	$\frac{0.9}{21}$	$\frac{0.5}{15}$	$\frac{1.0}{12}$	$\frac{0.9}{9}$	$\frac{0.7}{7}$	$\frac{0.3}{15}$	$\frac{0.2}{25}$	$\frac{0.2}{35}$
148.5	148.8	149.1	148.5	149.0	149.1	149.9	150.66	150.0	150.3
$\frac{2.2}{35}$	$\frac{2.0}{25}$	$\frac{2.6}{15}$	$\frac{2.2}{12}$	$\frac{2.7}{9}$	$\frac{2.6}{6}$	$\frac{1.8}{15}$	$\frac{1.0}{24.8}$	$\frac{1.5}{25}$	$\frac{1.4}{35}$

151.68

151.8	151.9	152.1	151.7	151.5	151.8	152.0	152.0	151.6	151.5
$\frac{1.3}{35}$	$\frac{1.3}{25}$	$\frac{1.0}{20}$	$\frac{1.4}{15}$	$\frac{1.6}{15}$	$\frac{1.4}{19}$	$\frac{1.1}{11}$	$\frac{1.1}{15}$	$\frac{1.5}{25}$	$\frac{1.6}{35}$

156.12

151.49 ✓

0.19
248 = 1/4 Lat's
Fence

152.5	152.4	151.8	151.5	151.7	151.9	151.7	151.1	150.9
$\frac{0.6}{35}$	$\frac{0.9}{25}$	$\frac{1.6}{15}$	$\frac{1.6}{15}$	$\frac{1.7}{7}$	$\frac{1.7}{10}$	$\frac{1.4}{15}$	$\frac{0.7}{25}$	$\frac{0.9}{35}$

152.5	151.9	151.4	151.0	151.1	151.5	150.8	150.3	150.1
$\frac{0.6}{35}$	$\frac{1.2}{25}$	$\frac{1.7}{15}$	$\frac{0.7}{15}$	$\frac{0.8}{8}$	$\frac{1.3}{25}$	$\frac{0.9}{15}$	$\frac{0.8}{25}$	$\frac{0.6}{35}$

BM 1.77 159.64

TP 5.30 159.41 2.01 154.11

BM 2.19 153.93

127 51.80 = S. L. Hilltop

1240

11750

1170

156.12

ST 7. Hilltop
Hilltop 7
Hilltop 7
157.84
Pop 21

ST 7. Hilltop
Hilltop 7
Hilltop 7

153.9 153.9 153.5 152.9 152.9 153.3 153.7 153.5
 $\frac{22}{25}$ $\frac{22}{25}$ $\frac{26}{25}$ $\frac{22}{25}$ $\frac{22}{25}$ $\frac{28}{25}$ $\frac{27}{25}$ $\frac{26}{25}$

153.1 152.9 152.5 152.3 152.2 152.4 152.1 152.1 152.4
 $\frac{20}{25}$ $\frac{22}{25}$ $\frac{26}{25}$ $\frac{22}{25}$ $\frac{22}{25}$ $\frac{27}{25}$ $\frac{20}{25}$ $\frac{20}{25}$ $\frac{27}{25}$

152.5 152.3 151.9 151.8 151.7 151.8 151.4 151.2 151.5
 $\frac{26}{25}$ $\frac{28}{25}$ $\frac{27}{25}$ $\frac{26}{25}$ $\frac{27}{25}$ $\frac{27}{25}$ $\frac{27}{25}$ $\frac{29}{25}$ $\frac{26}{25}$

152.2 152.0 151.5 151.5 151.3 151.2 151.5 150.9 150.6 150.4
 $\frac{29}{25}$ $\frac{27}{25}$ $\frac{26}{25}$ $\frac{26}{25}$ $\frac{28}{25}$ $\frac{29}{25}$ $\frac{27}{25}$ $\frac{27}{25}$ $\frac{25}{25}$ $\frac{27}{25}$

156.12

Cross Section F St.
 Rowco St to East End Morrison Marsden Park

LT-11

Rt-5 Nov. 18-41

33

Indexed
 LM

1+32.5 180 Rt of L: Sky Power Pole
 1+0

0+75

0+50

0+25

Notes Reducibly Plotted 11-21-41
 C.B.H.

0+0 = E.L. Rowco St

TP 1038 154.35 0.03 143.97

BM 1218 144.00 131.82

SE Pipe
 FSL 411/41
 Page 17

1441 10.3 35	1441 10.3 35	143.6 10.8 30	143.6 10.8 35	143.7 10.7	143.8 10.6 35	143.5 10.9 35	143.8 10.6 35	143.5 10.9 35
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1467 7.7 35	1463 8.1 35	1458 8.6 32	1456 8.8 35	1453 9.1	1458 8.6 35	1458 8.6 35	1458 8.6 35	145.5 8.0 35
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1474 5.9 35	1482 6.4 35	1471 7.0 31	1471 7.0 35	1471 7.0	1481 5.6 35	1478 6.6 35	1477 6.7 35	1474 7.0 35
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1471 5.7 35	1492 4.9 35	1490 5.1 30	1493 5.1 35	1492 5.1 35	1488 5.6	1498 4.6 35	1500 4.4 35	1500 4.4 35	1500 4.4 35
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1521 8.3 35	1520 8.3 35	1512 8.3 35	1510 8.3 35	1509 8.3 35	1523 7.7 35	1526 7.8 35	1527 7.8 35	1527 7.8 35
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154.35

TP 5.56 137.38 10.93 131.82

3+25 = F.L. 41st ST.

2+65 = H.L. 41st ST.

2+30

2+0

1+77

1+30

1+40.5 15th RT of $\frac{1}{2}$ = 5/4 Anchor Pole

TP 0.54 142.75 12.14 142.21

1+32.5 = $\frac{1}{2}$ F.L. 41st ST.

154.35

1355

$\frac{7.2}{6.5}$

1355

$\frac{7.2}{6.5}$

1348

$\frac{8.0}{6.5}$

1348

$\frac{8.0}{6.5}$

1352

$\frac{7.6}{6.5}$

1352

$\frac{7.6}{6.5}$

1354

$\frac{7.4}{6.5}$

1353

$\frac{7.5}{6.5}$

1351

$\frac{7.7}{6.5}$

1372

$\frac{5.6}{6.5}$

1370

$\frac{5.8}{6.5}$

1365

$\frac{6.0}{6.5}$

1365

$\frac{6.0}{6.5}$

1365

$\frac{6.0}{6.5}$

1369

$\frac{5.9}{6.5}$

1357

$\frac{6.1}{6.5}$

1370

$\frac{5.8}{6.5}$

1370

$\frac{5.8}{6.5}$

1369

$\frac{5.9}{6.5}$

138.05

4.70

26.9

15.5000

1000 E.M.

1407

$\frac{2.1}{3.5}$

1409

$\frac{1.9}{2.5}$

1405

$\frac{2.8}{2.0}$

1405

$\frac{2.8}{1.5}$

1403

$\frac{2.5}{2.5}$

1400

$\frac{2.8}{1.0}$

1400

$\frac{2.8}{1.5}$

1400

$\frac{2.8}{2.5}$

1401

$\frac{2.7}{3.5}$

1414

$\frac{1.20}{6.5}$

1423

$\frac{1.21}{2.5}$

1418

$\frac{1.26}{1.5}$

1419

$\frac{1.25}{1.0}$

1418

$\frac{1.26}{1.5}$

1418

$\frac{1.26}{1.5}$

1414

$\frac{1.20}{3.5}$

1416

$\frac{1.28}{3.5}$

154.35

570

475

7750

4725

470

3750

187.38

47

2

91

35

134.1	133.6	133.1	132.2	131.6	131.2	130.8	130.1
$\frac{5.5}{3.5}$	$\frac{5.8}{3.5}$	$\frac{5.5}{3.5}$	$\frac{5.2}{3.5}$	$\frac{5.8}{3.5}$	$\frac{6.2}{3.5}$	$\frac{6.6}{3.5}$	$\frac{7.2}{3.5}$

132.6	132.1	131.8	131.1	130.9	130.3	130.2	129.6	129.1
$\frac{7.5}{3.5}$	$\frac{5.5}{3.5}$	$\frac{5.6}{3.5}$	$\frac{6.3}{3.5}$	$\frac{6.5}{3.5}$	$\frac{7.1}{3.5}$	$\frac{7.2}{3.5}$	$\frac{7.8}{3.5}$	$\frac{8.5}{3.5}$

131.0	130.7	130.4	129.9	129.9	129.4	129.4	129.1	128.8
$\frac{6.4}{3.5}$	$\frac{6.7}{3.5}$	$\frac{7.0}{3.5}$	$\frac{7.5}{3.5}$	$\frac{7.5}{3.5}$	$\frac{8.0}{3.5}$	$\frac{8.0}{3.5}$	$\frac{8.5}{3.5}$	$\frac{8.6}{3.5}$

129.9	129.5	129.2	129.0	129.1	129.4	129.0	128.4
$\frac{7.5}{3.5}$	$\frac{7.9}{3.5}$	$\frac{8.2}{3.5}$	$\frac{8.4}{3.5}$	$\frac{8.3}{3.5}$	$\frac{8.0}{3.5}$	$\frac{8.4}{3.5}$	$\frac{9.0}{3.5}$

129.4	129.2	130.6	129.8	129.6	129.6	129.3
$\frac{8.0}{3.5}$	$\frac{8.2}{3.5}$	$\frac{7.8}{3.5}$	$\frac{7.6}{3.5}$	$\frac{7.8}{3.5}$	$\frac{7.8}{3.5}$	$\frac{8.1}{3.5}$

131.8	131.6	132.1	132.4	132.1	131.5	130.9	131.4	131.3
$\frac{5.6}{3.5}$	$\frac{5.8}{3.5}$	$\frac{5.5}{3.5}$	$\frac{5.5}{3.5}$	$\frac{5.8}{3.5}$	$\frac{5.9}{3.5}$	$\frac{6.5}{3.5}$	$\frac{6.0}{3.5}$	$\frac{6.1}{3.5}$

187.38

F 51

TP 8.81 14218 301 134.87

7+65

7+30

7+0

6+50

6+10.95 = F.L. Morrison

5+60.95 = W.L. Morrison

5+25

13738

61

2

191

36

1363 11 35	1357 17 25	1352 22 15	1347 27 8	1345 29	1340 21 10	1338 26 15	1334 10 25	1333 11 25
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1357 17 35	1354 20 25	1347 27 15	1343 31	1337 18 10	1330 14 15	1331 16 25	1331 13 35
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1347 27 35	1338 26 25	1336 28 15	1333 11	1329 15 15	1327 12 15	1325 19 25	1324 15 35
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1337 27 35	1334 10 25	1329 15 15	1329 15	1324 5.0 15	1324 5.0 15	1321 5.0 25	1321 5.0 35
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1341 5.0 35	1337 5.7 15	1332 11 15	1326 18	1319 5.6 10	1318 5.6 15	1314 6.0 25	1307 6.7 35
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137

9+5795 = FL Morrissey Marsden Park

9+48

9+21

8+97.02 = FL 42nd St.

BM

5.38

137.80

Hub SL Fst
E 7' line 42nd
137.79
page 308+47.02 = W.L. 42nd St

8+0

143.18

Lt

Z

Rt

37

142.4

0.8
25

141.6

1.6
15

140.7

25

139.8

0.2
15

139.2

4.0
25

138.5

3.7
25

142.78

0.10
35
0.10
0.10

142.12

1.06
25
1.06
1.06
0.10
0.10

142.12

1.06
25

141.9

1.3
25

140.8

2.4
15

140.9

3.2

139.2

4.0
15

138.6

4.6
25

138.4

4.8
25

140.9

2.3
25

140.4

2.8
15

139.3

3.9

138.4

4.8
15

138.1

5.1
25

139.5

3.7
25

138.6

4.6
15

137.9

5.3

137.1

6.1
15

136.9

6.3
25

137.8

5.4
25

137.4

5.8
25

136.7

6.5
15

136.5

6.7

136.1

7.1

135.4

7.8
15

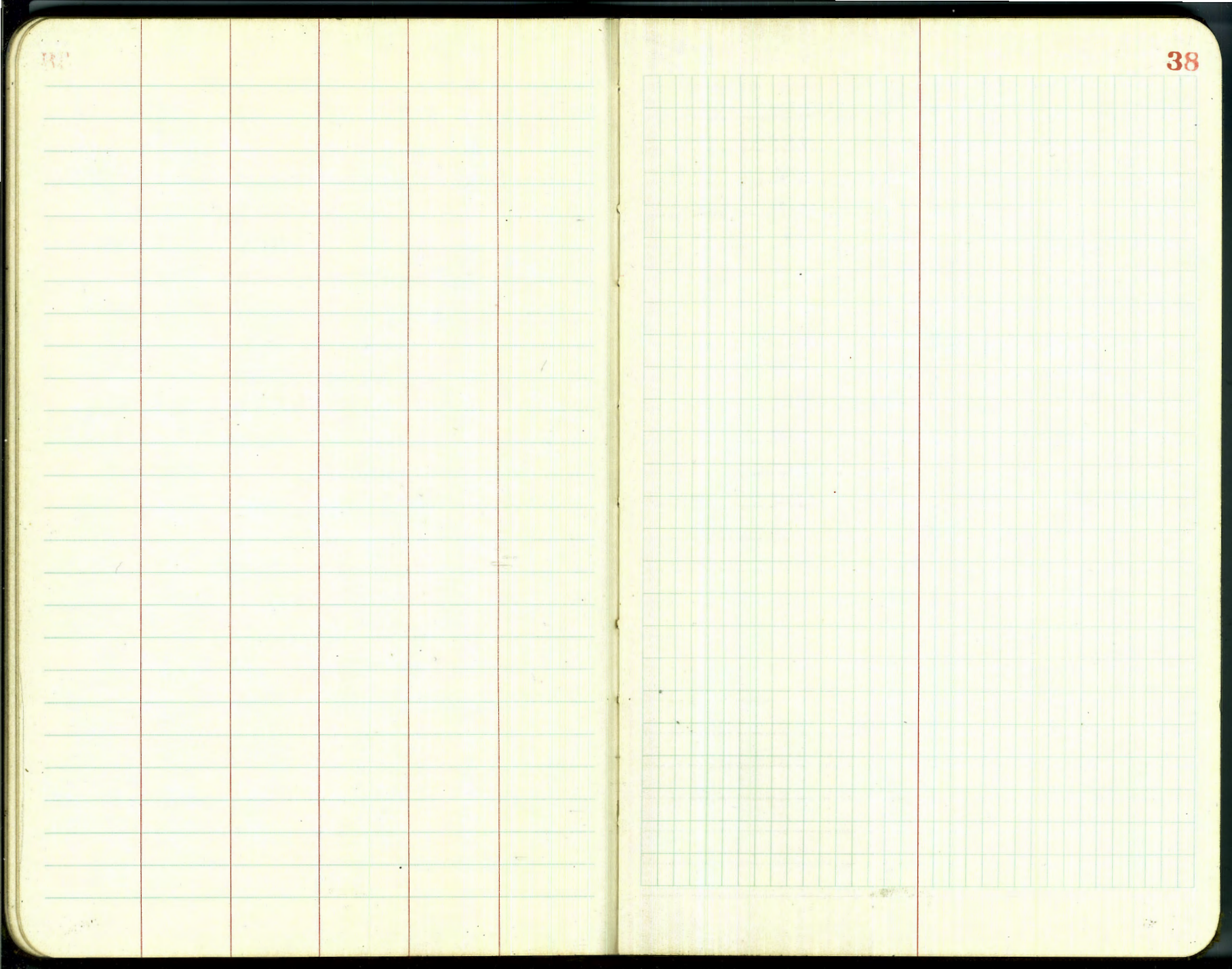
135.1

8.1
25

134.7

8.5
25

143.18



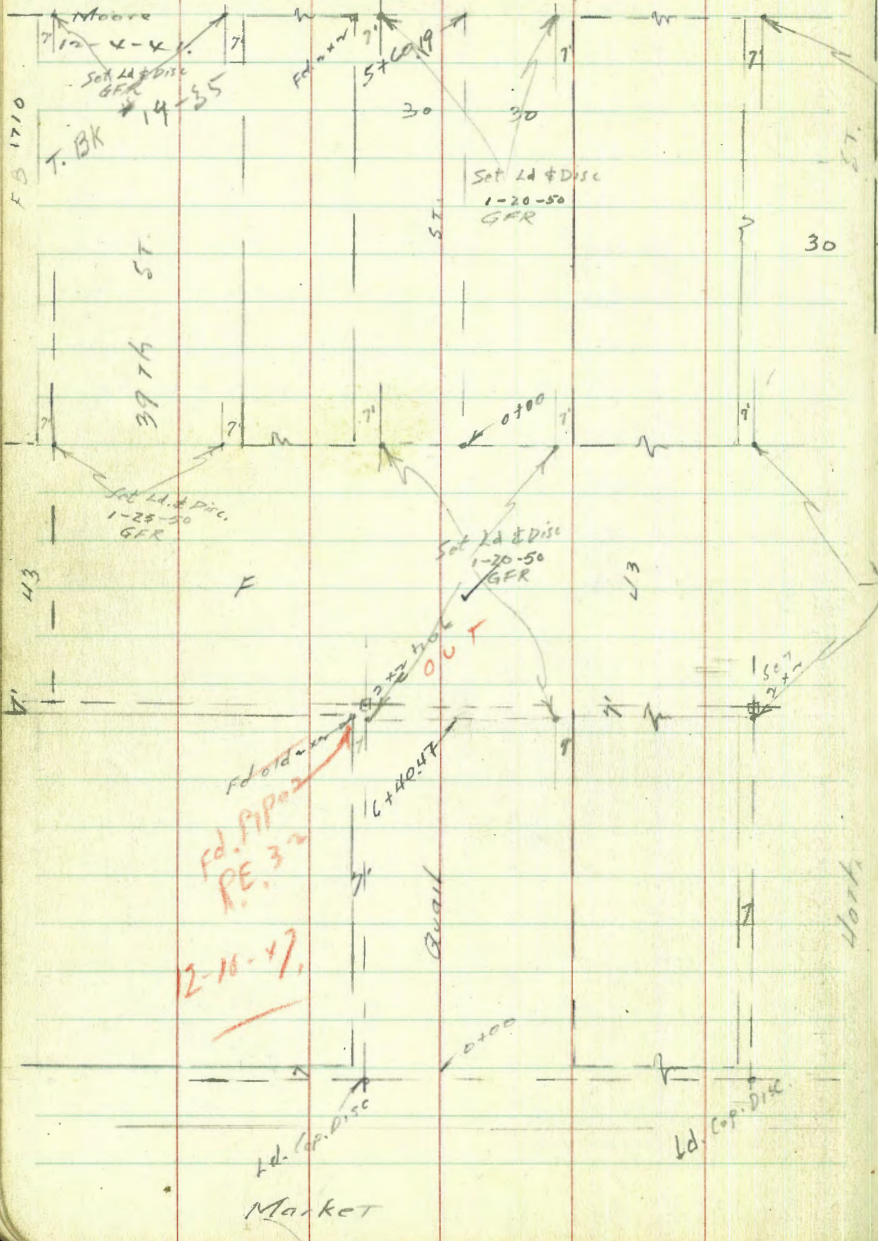
2 Levels Proposed Storm Drain
 Across Block 5 Morrison's Marscece Park
 See Sketch Page 13

Indexed
 LM

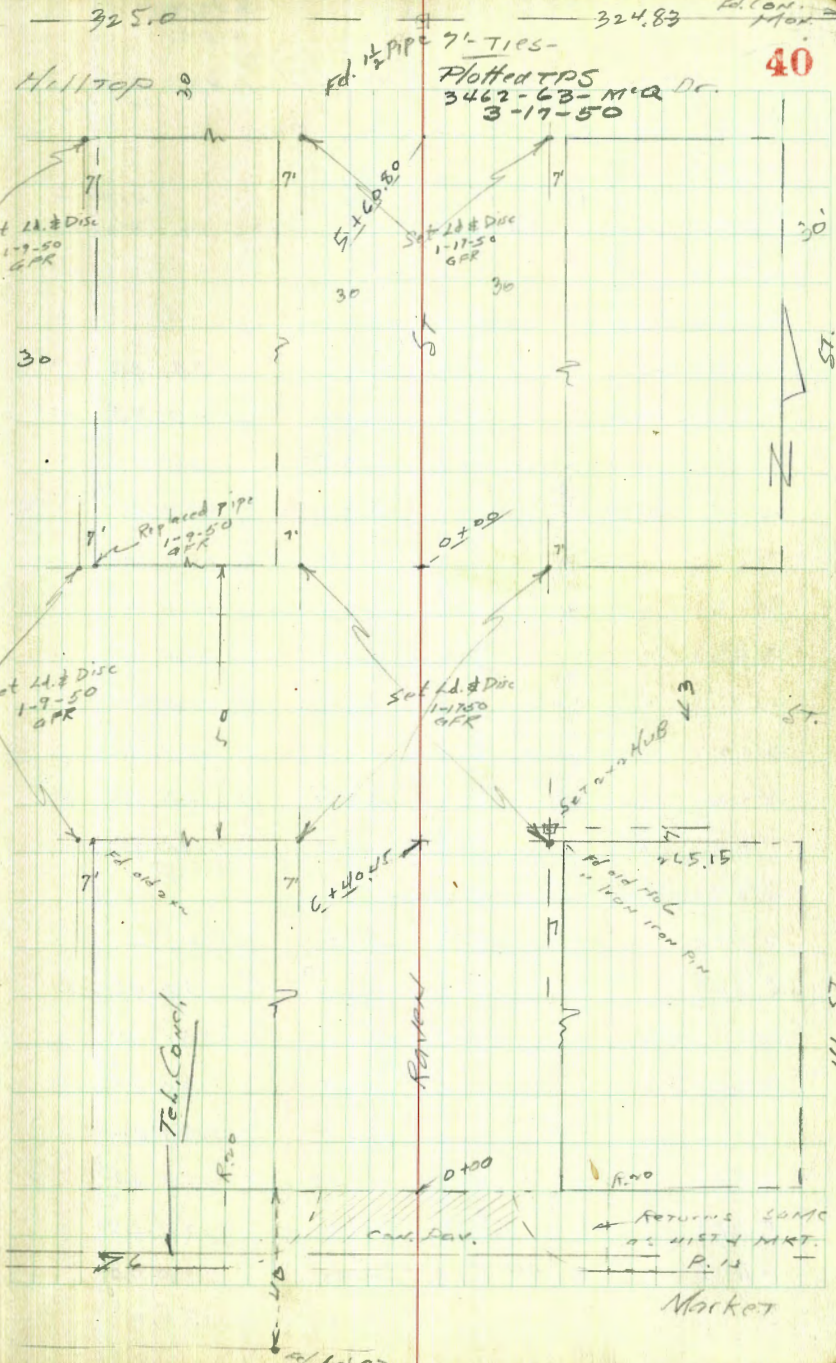
Nov 18-41

BM	1.13	129.89	128.76	5th St Market + 42nd St
0+0	EL Morrison St.		6.4	123.5
+25			7.3	122.6
+50			7.7	122.2
+75			8.0	121.9
+85			7.6	122.3
+10			6.8	123.1
+19	2 Existing Sewer Man Hole on Rim flam Libe		6.37	126.52
			12.74	117.15
+50			5.9	124.0
+75			5.9	124.0
+10			5.6	124.3
2 +65.95	N. L. 42nd St.		4.79	125.10
				0.05/06

TIE PTS.
Quail, Hoth
& Raven



Fd. Pipe
PE. 32
2-10-47



324.83 Ed. Con. Mon. **40**

RETURNS SOME
AS 41574 MRT.
P. 13

Indexed
c.s.K.

Xsec Raven St. 60' wide 10' curbs
Market to Hilltop Dr. 10' 1/4 5

Nov BP 12.44 137.81 125.39 Market

0-20

E-10 cb. 3.37 134.44

" Pav 4.03 133.78

E " 3.78 134.03

cb " 3.63 134.18

1/4 " 3.51 134.30

c " 3.44 134.37

1/4 " 3.45 134.36

cb " 3.58 134.23

wl " 3.75 134.06

+20 " 3.89 133.92

" cb 3.48 134.53

0+00 NL Market

wl 2.7 135.1

cb 7.83 134.98

gut pav 2.44 134.37

1/4 " 3.34 134.47

c " 3.27 134.52

1/4 " 3.37 134.44

gut " 3.54 134.27

cb 2.91 134.90

E 2.8 135.0

Rect Plot 12-13-1941-

137.81

41

0+04

E 2.1 135.7

cb 2.3 135.5

+20 3.0 134.8

1/4 2.8 135.0

c 2.8 135.0

+5 2.6 135.2

1/4 0.0 137.8

T.P. 12.50 148.28 2.03 135.78

cb 9.6 138.7

wl 8.5 139.8

0+50

wl 7.3 141.0

cb 7.2 141.0

1/4 8.6 139.7

c 9.7 138.6

1/4 9.9 138.4

cb 10.1 138.2

E 10.9 137.4

+10 11.5 136.8 ✓

1+00

-10 10.5 137.8 ✓

E 9.6 138.7

cb 8.4 139.9

cb + v	7.9	140.4
1/4	7.7	140.6
c	7.4	140.9
1/4	7.1	141.2
cb	6.2	142.1
v	5.4	142.9
1450		
w 9 u' cement walk	3.74	144.54 ✓
cb	4.0	144.3
1/4	4.4	143.9
c	4.7	143.6
1/4	5.2	143.1
cb	5.8	142.5
E	6.4	141.9
+10	7.0	141.3 ✓
1455		
E-17 wood porch to house	7.30	140.98
2401		
E E u' cement walk	3.73	144.55 ✓
cb	3.4	145.1
1/4	2.4	145.9
c	2.3	146.0
1/4	1.8	146.5
cb	0.6	147.7
w	0.3	148.0
T.P.	7.57	155.79 ✓
	0.06	148.22

2450		
w	6.2	149.6
cb	7.2	148.6
1/4	7.3	148.5
c	7.4	148.2
1/4	7.4	148.2
cb	8.4	147.4
E	9.2	146.6
+10	9.9	145.9 ✓
2475		
w 9 3' cement walk	5.71	150.08 ✓
2494		
E-17 wood porch to house	8.57	147.22 ✓
3400		
-10	8.0	147.8
E	7.2	148.6
cb	6.7	149.1
1/4	6.0	149.8
c	5.9	149.9
1/4	6.3	149.5
cb	5.5	150.3
v	5.3	150.5
3409		
w 9 3' cement walk	4.95	150.84 ✓
3443		
E-20 14' cement porch	7.44	148.35 ✓

3 + 50

w	3.8	152.0
cb	4.0	151.8
1/4	5.1	150.7
c	5.1	150.7
1/4	5.1	150.7
cb	5.8	150.0
E	6.5	149.3
+10	7.1	148.7 ✓

4 + 00

-10	6.6	149.2 ✓
E	5.8	150.0
cb	5.1	150.7
1/4	4.6	151.2
c	4.6	151.2
1/4	4.5	151.3
cb	3.4	152.4
w	2.9	152.9

4 + 50

w	2.5	153.3
cb	2.7	153.1
1/4	3.4	152.6
c	4.2	151.6
1/4	4.3	151.5
cb	4.9	150.9
E	5.8	150.0
+10	6.3	148.5

5 + 00

-10	6.4	149.4 ✓
E	6.1	149.7
cb	5.3	150.5
1/4	3.8	152.0
c	3.8	152.0
1/4	3.9	151.9
cb	2.3	153.5
w	2.0	153.8

5 + 50

w	2.1	155.7
cb	1.1	154.7
1/4	3.4	152.6
c	3.1	152.7
1/4	3.1	152.7
cb	4.6	151.2
E	5.9	149.9
+10	6.8	149.0 ✓

T.P. 6.89 159.51 3.17 152.62

1000 PIN
S.E. Cor
E + Raven

6 + 00

-10	9.0	150.5 ✓
E	8.3	151.2
cb	7.5	152.0
1/4	11.9	154.6

c		5.0	154.5
1/4		4.9	154.6
+v		4.7	154.8
cb	lawn	2.9	156.6 ✓
w	"	1.9	157.6
	6+1.5 Top		
w	- 10 Bot. com. step	1.03	158.48 ✓
"	- 12 1/2 Top com. porch	0.0 ✓	159.49 ✓
	6+10.45 = S.H.F. ST. =	50' wide 10' curbs 7.5' / 1.5'	
w	lawn	1.4	158.1
cb	"	1.8	157.7
1/4		4.1	155.4
c		4.9	154.6
1/4		5.0	154.5
cb		5.9	153.6
E		6.8	152.7
	S cb		
E		7.0	152.5
cb		6.0	153.5
1/4		5.3	154.2
c		5.7	153.8
1/4		5.1	154.4
+v		3.1	156.4
cb		2.3	157.2
w		1.1	158.4

w	S cb + 13	1.4	158.1
cb		2.2	156.9
+v		5.1	154.4
1/4		6.5	153.0
c		6.7	152.8
1/4		6.7	152.8
cb		6.4	153.1
E		7.3	152.2
	♀		
E		8.5	151.0
cb		7.7	151.8
1/4		6.7	152.8
c		6.9	152.6
1/4		6.8	152.7
cb		5.0	153.9
w		3.7	155.8
	Σ + v		
w		5.0	153.9
cb		6.7	152.8
1/4		6.8	152.7
c		7.2	152.3
1/4		7.2	152.3
cb		8.3	151.2
E		8.8	150.7

	N $\frac{1}{4}$		
E		8.7	1508
cb		8.3	1512
$\frac{1}{4}$		7.8	1517
c		7.4	1521
$\frac{1}{4}$		7.3	1522
cb		7.2	1523
W		7.1	1524
	N cb		
W		7.3	1522
cb		7.4	1521
$\frac{1}{4}$		7.6	1519
c		7.7	1518
$\frac{1}{4}$		8.0	1515
cb		8.3	1512
E		8.5	1510
	0 + 00 = N.L.F. ST.		
F		7.9	1516
cb		8.4	1511
$\frac{1}{4}$		8.3	1512
c		8.0	1515
$\frac{1}{4}$		7.7	1518
cb		7.5	1520
W		4.5	1530
	0 + 07		
- 7		0.0	1595

W		3.6	1559
+3		6.1	1534
cb		7.3	1522
$\frac{1}{4}$		7.7	1518
c		8.0	1515
$\frac{1}{4}$		8.0	1515
cb		8.1	1514
E		7.6	1519
	0 + 24		
W	- 0.6 ^{E of 11'} CENT. STAIRS	5.92	153.59
	0 + 50		
E		7.2	152.3
cb		7.4	151.9
$\frac{1}{4}$		7.3	152.2
c		7.6	151.9
$\frac{1}{4}$		7.3	152.2
cb		6.9	152.6
+7		5.6	153.9
W		4.0	155.5
+6		0.6	158.9 ✓
	1 + 00		
-3		1.3	158.2
W		2.9	156.6
+6		5.2	154.3
cb		6.5	153.0
$\frac{1}{4}$		6.7	152.8

159.51

c		6.9	152.6	
1/4		6.9	152.6	
cb		7.4	152.3	
E		7.0	152.5	
	1 + 50			
E - 10		10.0	149.5	✓
E - 3		8.5	151.0	✓
E		6.5	153.0	
cb		6.6	152.9	
1/4		6.4	153.1	
c		6.5	153.0	
1/4		6.3	153.2	
cb		6.4	153.3	
W	1507 " C-6670 wall	5.5	154.0	✓
	at 1410 = beg. of 4' C-6670 wall			W - 0.3 ✓
	at 1436			✓
W - 0.3	E 3' ^{beg. of} _{CON. STEP}	5.85	153.66	✓
	1 + 60			
W - 0.3	end C-6670 wall + beg. of wire fence + hedge			
	1 + 80.5			
E + 0.5	E of 21' ^{cont.} _{sdw.}	6.11	153.40	✓
	2 + 00			
W		4.8	154.7	
cb		5.4	154.3	
1/4		5.9	153.6	
c		6.1	153.4	

159.51

46

1/4		6.1	153.4	
cb		6.3	153.2	
E		6.4	153.3	
+ 10		9.3	150.2	✓
	2 + 50			
- 10		10.6	148.9	✓
E		5.6	153.9	
cb		5.8	153.7	
1/4		5.3	154.2	
c		5.4	154.1	
1/4		5.3	154.2	
cb		5.7	154.8	
W		4.3	155.2	
	3 + 00			
W	end Hedge 0.3 back	3.5	156.0	
cb		4.1	155.4	
1/4		4.5	155.0	
c		4.6	154.9	
1/4		4.5	155.0	
cb		5.1	154.4	
E		5.1	154.4	
+ 10		10.4	149.1	✓
	3 + 50			
- 10		7.5	152.0	✓
E		4.0	155.5	
cb		3.7	155.8	

		159.51		
1/4			3.1	156.4
c			3.3	156.2
1/4			3.3	156.2
cb			3.0	156.5
+8			2.4	157.1
w			1.5	158.0
	4+00			
w			0.0	159.5
+2			0.7	158.8
cb			1.0	158.5
1/4			1.7	157.8
c			1.7	157.8
1/4			1.8	157.7
cb			1.9	157.6
E			2.1	157.4
+10			7.0	152.5 ✓
T.P.	17.69	171.03 ✓	1.17	158.34
	4+50			
-10			17.0	154.0
E			10.9	160.1
cb			10.9	160.1
1/4			11.0	160.0
c			11.1	159.9
1/4			10.9	160.1

				171.03	
cb			10.4	160.6	47
+2			8.8	162.2	
w			8.0	163.0	
	4+83				
w	2 1/2' CON. STEPS	6.4		164.89 ✓	TOP BOT. STEP
	4+98				
E +0.5	TOP of 4' CON E STEP to steps down	6.50		164.53 ✓	
	5+00				
w			4.5	166.5	
cb			6.8	164.2	
+5			7.6	163.4	
1/4			7.3	163.7	
c			7.7	163.8	
1/4			7.7	163.8	
cb			7.0	164.0	
E	ON CON. STEP	6.50		164.53 ✓	
+14	BOT. of STEPS	12.80		158.23 ✓	
	5+40				
E			2.8	168.2	
cb			3.7	167.3	
1/4			3.6	167.4	
c			3.5	167.5	
1/4			3.7	167.3	
cb			2.7	168.3	
w			1.6	169.4	

171.03

5460.8 = S.L. Hilltop drive

w		+0.5	171.5
cb		0.8	170.2
1/4		1.4	169.6
c		1.6	169.4
1/4		1.8	169.2
cb		1.9	169.1
E		1.8	169.2

T.P.	11.84	182.64	0.5	170.78
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T.P.	0.57	181.31	1.88	180.74
------	------	--------	------	--------

Set B.M.		10.18	171.13
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TOP 1 1/2" Iron pipe @ Quail + Hilltop

Xsec F ST

50' wide
10' c6s
75' 11us

Raven to Quail

B.M. S.E.

1000 pin

7.55 160.17

159.60

Raven &
F ST

0+0 = with Raven this book

0+50

S	7.5	157.7
c6	7.0	158.2
1/2	1.6	158.6
+3	1.4	158.8
c	4.8	155.4
1/2	6.1	154.1
c6	6.2	154.0
+3	5.4	154.8
N	4.8	155.4
+2	0.3	159.9
	1+00	
-5	3.3	156.9
N	4.8	155.4
c6	5.7	154.5
1/2	6.0	154.2
c	5.7	154.5
1/2	5.1	155.1
c6	5.3	154.9
S	5.5	154.7

Reduced & Plotted 12-15-91 C.B.H.

	1+03		
N-6	2 7.5 cent. wk.	3.45	156.92 ✓
	1+13		
N-6	2 Sing. gar dirt	4.1	156.1 ✓
	1+50		
S		7.5	152.7
c6		7.3	152.9
1/2		7.2	153.0
c		7.1	153.1
1/2		7.2	153.0
c6		7.2	153.2
N		6.2	154.0
	2+00		
-5		5.6	154.6
N		8.1	152.1
c6		8.8	151.4
1/2		8.9	151.3
c		8.2	152.0
1/2		7.8	152.4
c6		7.7	152.5
S		7.7	152.5
	2+50		
S		7.9	152.3
+6		8.5	151.7
c6		8.2	151.8
1/2		7.8	152.4

160.17

1/4 + 3	7.4	152.8
C	8.3	151.9
1/4	10.1	150.1
cb	10.0	150.2
+ 5	9.2	151.0
N	8.2	152.0
+ 3	6.2	154.0

7 + 65 EL North St = 60'

N	9.6	150.6
cb	10.1	150.1
1/4	10.2	150.0
C	10.3	149.9
+ 3	8.0	152.2
1/4	8.1	152.1
cb	9.2	151.0
+ 8	9.5	150.7
S	8.8	151.4

9 North

S	11.1	149.1
C	10.4	149.8
N	9.6	150.6

0 + 0 = W N North

N	10.5	149.7
cb	10.7	149.5
1/4	10.8	149.4
C	11.3	148.9

160.17

1/4	11.6	148.6	50
cb	12.1	148.1	
S	13.0	147.2	
	0 + 50		
- 10	16.1	144.1	
S	15.7	144.5	
cb	15.3	144.9	
1/4	14.8	145.4	
C	12.8	147.4	
1/4	12.5	147.7	
cb	12.5	147.7	
N	12.1	148.1	

T.P 191 149.73 12.35 147.82

1 + 00

N	3.5	146.2	
cb	3.5	146.2	
1/4	3.5	146.2	
C	3.4	146.3	
1/4	5.5	144.2	
cb	6.2	143.3	
S	7.0	142.7	
+ 10	7.6	142.1	
	5 + 50		
- 10	9.8	139.9	

149.73

S	9.2	1405
cb	8.3	1414
+5	8.0	1417
1/4	6.5	1432
+5	4.5	1452
cb	4.6	1451
N	4.6	1451
r + 00		
N	5.5	1442
cb	5.6	1441
1/4	5.7	1440
C	5.6	1441
+3	5.7	1440
1/4	7.3	1424
cb	8.4	1413
S	9.1	1406
+10	9.4	1403
r + 25		
-10	7.8	1419
S	8.0	1417
cb	7.6	1421
1/4	6.7	1430
+2	6.0	1437
C	5.9	1438
1/4	6.1	1436
cb	5.9	1438

149.73

51

N	5.4	1443
r + 25	FL Quail	
N	6.0	1437
cb	6.6	1431
1/4	6.6	1431
C	6.0	1437
1/4	5.4	1445
cb	5.6	1441
S	5.95	14378 Rock

X sec of Quail St.

60' wide
10' CB
10' 1/4

Indexed
C.S.R.

Market to Hilltop

Note! Sch. & Ret. same as 41 St.

NWBP 11.04 136.43 125.39

Market
& 41 St.

T.P. 2.65 130.42 6.66 129.77

Cap dist NW
Market &
Quail

T.P. 9.26 130.92 8.76 121.66

0-20

-10 cb 8.75 122 17

-10 pay 9.25 121.67

wf " 9.64 121.28

cb " 9.74 121.18

1/4 " 9.90 121.02

c " 10.06 120.86

1/4 " 10.24 120.68

cb " 10.46 120.46

E " 10.65 120.27

+10 " 10.71 120.21

+10 cb 10.02 120.90

0+00

E 9.6 121.3

cb 9.75 121.17

9UT pay 10.37 120.55

1/4 " 10.08 120.84

c " 9.84 121.10

1/4 " 9.75 121.17

Reduced & Plotted 12-15-41 CBA

9UT 9.90 121.02

cb 9.35 121.57

wf 9.1 121.8

0+05

wf 9.3 121.6

cb 9.0 121.9

1/4 9.6 121.3

c 9.6 121.3

1/4 9.5 121.4

cb 9.5 121.4

E 8.9 122.0

0+10

E 8.7 122.2

cb 9.3 121.6

1/4 9.5 121.4

c 9.5 121.4

1/4 9.5 121.4

cb 9.3 121.6

wf 11.3 119.6

+10 11.9 119.0

0+50

wf 7.1 123.8

cb 7.3 123.6

1/4 7.8 123.1

c 7.7 123.2

1/4 7.7 123.2

130.9v

cb		7.0	123.9
E		6.9	124.0
	0+75		
E		5.0	125.9
cb		4.5	126.4
1/4		6.3	124.6
c		6.3	124.6
1/4		6.3	124.6
cb		5.1	125.8
w		4.0	126.9
	1+15		
w		3.7	127.2
cb		4.0	126.9
1/4		4.3	126.6
c		4.5	126.4
1/4		4.6	126.3
cb		4.3	126.6
E		4.5	126.4
	1+50		
E		3.7	127.7
cb		3.0	127.9
+5		2.5	128.4
1/4		3.3	127.6
c		3.7	127.7
1/4		3.1	127.8
+5		1.5	129.4

130.9v

53

cb		1.0	129.3	
w		1.3	129.6	
	1+75			
w		2.3	128.6	
cb		2.4	128.5	
1/4		2.3	128.6	
c		2.3	128.6	
1/4		2.4	128.3	
+5		2.0	128.9	
cb		2.6	128.3	
E		3.1	127.8	
T.P.	10.74	140.41	1.05	129.57
	7+00			
E		12.4	128.2	
cb		11.7	128.9	
1/4		11.4	129.4	
c		11.1	129.5	
1/4		11.4	129.4	
+5		9.7	130.9	
cb		10.1	130.5	
w		10.8	129.8	
	7+50			
w		9.0	131.6	
cb		9.0	131.0	

140.61

1/4	9.8	130.8
+4	9.4	131.2
c	9.4	131.2
1/4	9.4	131.0
cb	9.5	131.1
E	10.2	130.4

3+00

E	7.9	132.7
cb	7.5	133.1
+5	7.1	133.5
1/4	7.6	133.0
c	7.2	133.3
1/4	7.6	133.0
cb	7.7	132.9
vy	7.3	133.3

3+35

w	6.5	134.1
cb	6.0	134.6
1/4	6.3	134.3
+5	5.8	134.8
c	5.9	134.7
1/4	6.2	134.4
cb	6.0	134.6
E	6.1	134.5

3+65

E	5.6	137.0
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140.61

54

cb	4.0	136.6
1/4	4.8	135.8
c	4.6	136.0
1/4	4.6	136.0
cb	4.8	135.8
w	4.7	136.4

4+00

w	3.8	136.8
cb	3.4	137.2
1/4	3.3	137.3
c	3.0	137.6
1/4	3.1	137.5
+5	2.6	138.0
cb	1.7	138.9
E	2.0	138.6

T.P. 10.61 150.92 0.30 140.31

4+50

E	10.6	140.3
cb	10.6	140.3
+3	10.6	140.3
+6	11.3	139.6
1/4	11.5	139.4
c	11.4	139.5
1/4	11.5	139.4

150.92

cb		12.1	138.8
w		12.8	138.1
	5+00		
w		11.2	139.7
cb		10.7	140.2
+L		10.7	140.2
1/4		9.8	141.1
c		9.8	141.1
1/4		9.7	141.2
cb		9.0	141.9
E		8.8	142.1
	5+50		
E		8.1	142.8
cb		7.6	143.3
1/4		8.1	142.8
c		8.4	142.5
1/4		8.7	142.2
cb		8.7	142.2
w		9.2	141.6
	6+00		
w		6.8	144.1
cb		6.9	144.0
1/4		7.4	143.5
c		7.1	143.8
1/4		6.9	144.0
cb		7.1	143.8

150.92

E		8.0	142.9	55
	6+40.47 S.L	F ST. =	50' width 10' cbs 7.5 1/45	
E	Rock	7.11	143.81	= 143.78 P. 57
cb		6.3	144.6	
1/4		5.9	145.0	
c		6.1	144.8	
1/4		6.3	144.6	
cb		6.3	144.6	
w		6.0	144.9	
	5 cb			
w		5.5	145.3	
cb		5.5	145.4	
1/4		6.2	144.7	
c		6.2	144.7	
+3		5.8	145.1	
+5		4.9	146.0	
1/4		5.2	145.7	
cb		5.8	145.1	
E		6.7	144.2	
	5 1/4			
E		6.3	144.6	
cb		5.6	145.3	
1/4		5.2	145.7	
+5		4.9	146.0	
+7		6.1	144.8	
c		6.2	144.7	

150,92

1/4		6.7	144.2
+3		5.5	145.4
cb		5.3	145.6
w		5.1	145.8
E	F ST		
w		8.4	142.5
cb		8.4	142.7
1/4		7.7	143.7
c		7.1	143.8
1/4		7.5	143.4
cb		7.3	143.6
E		7.2	143.7
	N 1/4		
E		7.8	143.1
cb		7.8	143.1
1/4		7.9	143.0
c		7.7	143.2
1/4		8.0	142.9
cb		8.5	142.4
w		8.4	142.3
	N cb		
w		8.5	142.4
cb		8.4	142.5
1/4		8.3	142.6
c		8.1	142.8
1/4		8.0	142.9

150,94

56

cb		7.9	143.0
E		7.8	143.1
	0 + 00 = N L F ST.		
E		7.1	143.8
cb		7.4	143.5
1/4		8.0	142.9
c		8.0	142.9
1/4		8.1	142.8
cb		8.4	142.7
w		8.4	142.5
	0 + 50		
w		5.7	145.7
cb		6.1	144.8
1/4		6.4	144.5
c		6.3	144.6
1/4		5.8	145.1
cb		5.6	145.3
E		4.8	146.1
	0 + 67		
w	+ 1.7 & 10' ^{cont.} Drive	4.60	146.32 ✓
w	- 4.3 " "	3.68	147.28 ✓
	0 + 73 Beg. Cypress hedge	w - 0.3	✓
	0 + 91.7		
w	+ 1.0 & 3.5 wide ^{TOP} _{cont.} strip	3.13	147.79 ✓
	1 + 00		
E		1.5	149.4

		150.9		
cb		3.1	147.8	
1/4		3.2	147.7	
c		3.5	147.4	
1/2		3.7	147.2	
cb		3.8	147.1	
w		3.0	147.9	
	1+10 Beg. Cypress hedge	E+3.5	✓	
	1+13 end "	"	W-0.3	✓
	1+38.3			
w		1.0	149.9	✓
cb		1.6	149.3	
1/4		1.9	149.0	
c		1.3	149.6	
1/2		1.7	149.7	
cb		1.2	149.7	
+8	Top Bot. Cem. STEP	+0.25	151.17	3' wide ✓
T.P.	11.75	161.66	0.51	150.41
	1+64			
E		9.1	152.6	
+3	end Cypress hedge			✓
cb		10.7	151.0	
1/2		11.0	150.7	
c		10.8	150.9	
1/4		11.2	150.5	

		161.66		
cb		11.2	150.5	57
w		10.4	151.3	
	2+00			
w		8.7	153.0	
cb		9.2	152.4	
1/2		9.4	152.3	
c		9.0	152.7	
1/4		9.3	152.4	
cb		9.4	152.3	
+8		7.9	153.8	
E		6.9	154.8	
	2+14			
	W+0.52 13' wide Cem. walk	7.80	153.86	✓
	2+19 W+3.7 beg. hedge			✓
	2+48 " " end "			✓
	2+50			
E		4.3	157.4	
+4		5.4	156.3	
cb		6.3	155.4	
1/2		5.8	155.9	
c		6.0	155.1	
1/4		7.1	154.6	
cb		7.3	154.4	
w		6.4	155.3	
	3+00			
w		4.2	157.5	

161.66

cb		4.5	157.2
+7		4.7	157.0
1/4		4.2	157.5
c		4.1	157.6
1/2		4.2	157.5
cb		4.0	157.7
+7.		3.5	158.2
E		1.4	160.3
	3+50		
E		0.0	161.7
+3		1.3	160.4
cb		1.7	160.0
1/4		1.5	160.2
c		1.5	160.2
1/4		1.6	160.1
cb		2.8	158.9
+2		1.9	159.8
w		1.7	160.0
T.P.	12.09 173.51	0.24	161.42
	H+00		
w		10.7	162.8
cb		11.6	161.9
+6		11.4	162.1
1/2		10.5	163.0

173.51

58

c		10.7	162.8
1/4		11.0	162.5
cb		11.2	162.3
+7		9.7	163.8
E		8.3	165.2
	H+50		
E		6.4	167.1
+2		7.7	165.8
cb		8.5	165.0
1/4		8.6	164.9
c		8.3	165.2
1/4		8.6	164.9
+8		9.3	164.2
cb		8.7	164.8
w		8.4	165.1
	S+00		
w		6.1	167.4
+8		6.3	167.2
cb		6.9	166.6
1/4		6.2	167.3
c		6.0	167.5
1/2		6.1	167.4
+6		6.1	167.4
cb		5.1	168.4
E		4.7	168.8

17351

5+40

E	2.7	170.8
cb	3.1	170.4
+3	3.9	169.6
1/4	3.9	169.6
C	3.9	169.6
1/2	4.2	169.3
+8	4.9	168.6
cb	4.1	169.4
w	3.7	169.8

5+60.19 = 5 h Hilltop Dr.

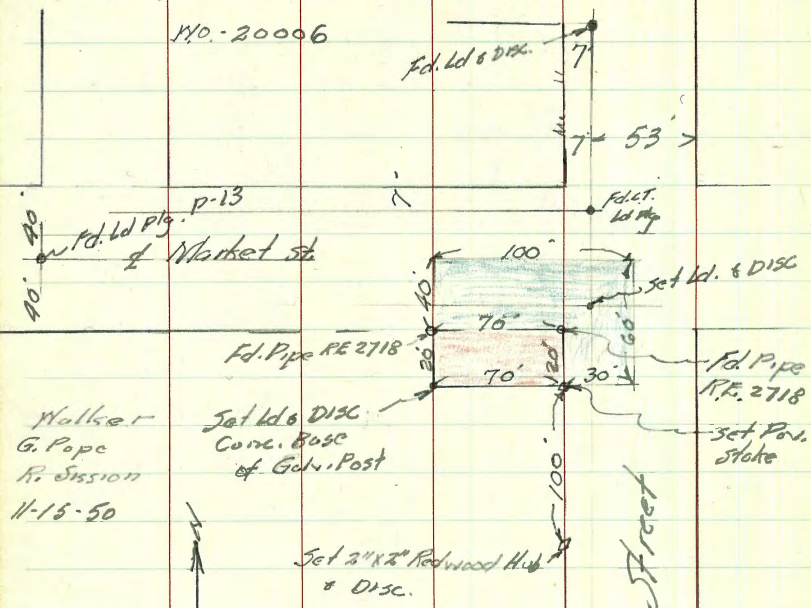
w	2.8	170.7
cb	3.2	170.3
1/4	2.8	170.7
C	2.7	170.8
1/2	2.5	171.0
cb	2.3	171.2
E	1.5	172.0

1/2" Pipe	Hilltop	2.33	171.18	171.12
	7 Quail			

Survey Parcel 1
Plot # 4-31

S.W. Cor Market & 41st St.

No. 20006



Walker
G. Pope
R. Sisson
11-15-50

Set lds DISC
Cone. Base
of Golv. Post

Parcel 1 = Blue & Red.
" Surveyed = Red.

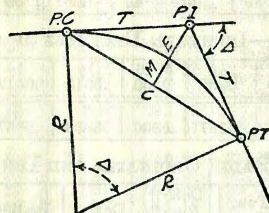
INDEXED

NOV 27 1950

(Additional Ties P-13)

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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CURVE FORMULAS

$$\text{Radius} = R = \frac{50}{\sin \frac{D}{2}} \quad (1) \text{ Degree of Curve} = D \text{ and } \sin \frac{D}{2} = \frac{50}{R} \quad (2)$$

$$\text{Tangent} = T = R \tan \frac{\Delta}{2} \quad (3) \text{ Length of Curve} = L = 100 \frac{\Delta}{D} \quad (4)$$

$$\text{Middle ordinate} = M = R(1 - \cos \frac{\Delta}{2}) \quad (5) = R \text{vers} \frac{\Delta}{2} \quad (6)$$

$$\text{External} = E = T \tan \frac{\Delta}{4} \quad (7) = R \div \cos \frac{\Delta}{2} - R \quad (8) = R \text{exsec} \frac{\Delta}{2} \quad (9)$$

$$\text{Long Chord} = C = 2 R \sin \frac{\Delta}{2} \quad (10) \Delta = \text{Central Angle}$$

EXPLANATION AND USE OF TABLES

Stations.—Given P. I. = Sta. 161 + 60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{3} = 414.49$ ft. From Table V correction = .36 or $T = 414.85$ ft. P. C. = Sta. P. I. - $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T. = Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = $158 - \text{Sta. P. C.} = 54.50$, hence offset = $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^\circ$ or = defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8\frac{1}{3} = 136.2'$ or $2^\circ 16.2'$, or = $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 91.27$ and from Table V correction = .10 or $E = 91.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

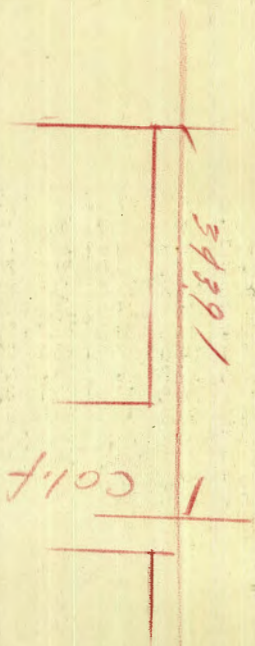
Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
31°	1589.0	216.3	41°	2142.2	387.4	51°	2732.9	618.4
10'	1598.0	218.7	10'	2151.7	390.7	10'	2743.1	622.8
20	1606.9	221.1	20	2161.2	394.1	20	2753.4	627.2
30	1615.9	223.5	30	2170.8	397.4	30	2763.7	631.7
40	1624.9	226.0	40	2180.3	400.8	40	2774.0	636.2
50	1633.9	228.4	50	2189.9	404.2	50	2784.2	640.7
32	1643.0	230.9	42	2199.4	407.6	52	2794.5	645.2
10	1652.0	233.4	10	2209.0	411.1	10	2804.9	649.7
20	1661.0	235.9	20	2218.6	414.5	20	2815.2	654.3
30	1670.0	238.4	30	2228.1	418.0	30	2825.6	658.8
40	1679.1	241.0	40	2237.7	421.4	40	2835.9	663.4
50	1688.1	243.5	50	2247.3	425.0	50	2846.3	668.0
33	1697.2	246.1	43	2257.0	428.5	53	2856.7	672.7
10	1706.3	248.7	10	2266.6	432.0	10	2867.1	677.3
20	1715.3	251.3	20	2276.2	435.6	20	2877.5	682.0
30	1724.4	253.9	30	2285.9	439.2	30	2888.0	686.7
40	1733.5	256.5	40	2295.6	442.8	40	2898.4	691.4
50	1742.6	259.1	50	2305.2	446.4	50	2908.9	696.1
34	1751.7	261.8	44	2314.9	450.0	54	2919.4	700.9
10	1760.8	264.5	10	2324.6	453.6	10	2929.9	705.7
20	1770.0	267.2	20	2334.3	457.3	20	2940.4	710.5
30	1779.1	269.9	30	2344.1	461.0	30	2951.0	715.3
40	1788.2	272.6	40	2353.8	464.6	40	2961.5	720.1
50	1797.4	275.3	50	2363.5	468.4	50	2972.1	725.0
35	1806.6	278.1	45	2373.3	472.1	55	2982.7	729.9
10	1815.7	280.8	10	2383.1	475.8	10	2993.3	734.8
20	1824.9	283.6	20	2392.8	479.6	20	3003.9	739.7
30	1834.1	286.4	30	2402.6	483.3	30	3014.5	744.6
40	1843.3	289.2	40	2412.4	487.2	40	3025.2	749.6
50	1852.5	292.0	50	2422.3	491.0	50	3035.8	754.6
36	1861.7	294.9	46	2432.1	494.8	56	3046.5	759.6
10	1870.9	297.7	10	2441.9	498.7	10	3057.2	764.6
20	1880.1	300.6	20	2451.8	502.5	20	3067.9	769.7
30	1889.4	303.5	30	2461.7	506.4	30	3078.7	774.7
40	1898.6	306.4	40	2471.5	510.3	40	3089.4	779.8
50	1907.9	309.3	50	2481.4	514.3	50	3100.2	784.9
37	1917.1	312.2	47	2491.3	518.2	57	3110.9	790.1
10	1926.4	315.2	10	2501.2	522.2	10	3121.7	795.2
20	1935.7	318.1	20	2511.2	526.1	20	3132.6	800.4
30	1945.0	321.1	30	2521.1	530.1	30	3143.4	805.6
40	1954.3	324.1	40	2531.1	534.2	40	3154.2	810.9
50	1963.6	327.1	50	2541.0	538.2	50	3165.1	816.1
38	1972.9	330.2	48	2551.0	542.2	58	3176.0	821.4
10	1982.2	333.2	10	2561.0	546.3	10	3186.9	826.7
20	1991.5	336.3	20	2571.0	550.4	20	3197.8	832.0
30	2000.9	339.3	30	2581.0	554.5	30	3208.8	837.3
40	2010.2	342.4	40	2591.0	558.6	40	3219.7	842.7
50	2019.6	345.5	50	2601.1	562.8	50	3230.7	848.1
39	2029.0	348.6	49	2611.2	566.9	59	3241.7	853.5
10	2038.4	351.8	10	2621.2	571.1	10	3252.7	858.9
20	2047.8	354.9	20	2631.3	575.3	20	3263.7	864.3
30	2057.2	358.1	30	2641.4	579.5	30	3274.8	869.8
40	2066.6	361.3	40	2651.5	583.8	40	3285.8	875.3
50	2076.0	364.5	50	2661.6	588.0	50	3296.9	880.8
40	2085.4	367.7	50	2671.8	592.3	60	3308.0	886.4
10	2094.9	371.0	10	2681.9	596.6	10	3319.1	892.0
20	2104.3	374.2	20	2692.1	600.9	20	3330.3	897.5
30	2113.8	377.5	30	2702.3	605.3	30	3341.4	903.2
40	2123.3	380.8	40	2712.5	609.6	40	3352.6	908.8
50	2132.7	384.1	50	2722.7	614.0	50	3363.8	914.5

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
61°	3375.0	920.2	71°	4086.9	1308.2	81°	4893.6	1805.3
10'	3386.3	925.9	10'	4099.5	1315.6	10'	4908.0	1814.7
20	3397.5	931.6	20	4112.1	1322.9	20	4922.5	1824.1
30	3408.8	937.3	30	4124.8	1330.3	30	4937.0	1833.6
40	3420.1	943.1	40	4137.4	1337.7	40	4951.5	1843.1
50	3431.4	948.9	50	4150.1	1345.1	50	4966.1	1852.6
62	3442.7	954.8	72	4162.8	1352.6	82	4980.7	1862.2
10	3454.1	960.6	10	4175.6	1360.1	10	4995.4	1871.8
20	3465.4	966.5	20	4188.5	1367.6	20	5010.0	1881.5
30	3476.8	972.4	30	4201.2	1375.2	30	5024.8	1891.2
40	3488.3	978.3	40	4214.0	1382.8	40	5039.5	1900.9
50	3499.7	984.3	50	4226.8	1390.4	50	5054.3	1910.7
63	3511.1	990.2	73	4239.7	1398.0	83	5069.2	1920.5
10	3522.6	996.2	10	4252.6	1405.7	10	5084.0	1930.4
20	3534.1	1002.3	20	4265.6	1413.5	20	5099.0	1940.3
30	3545.6	1008.3	30	4278.5	1421.2	30	5113.9	1950.3
40	3557.2	1014.4	40	4291.5	1429.0	40	5128.9	1960.2
50	3568.7	1020.5	50	4304.6	1436.8	50	5143.9	1970.3
64	3580.3	1026.6	74	4317.6	1444.6	84	5159.0	1980.4
10	3591.9	1032.8	10	4330.7	1452.5	10	5174.1	1990.5
20	3603.5	1039.0	20	4343.8	1460.4	20	5189.3	2000.6
30	3615.1	1045.2	30	4356.9	1468.4	30	5204.4	2010.8
40	3626.8	1051.4	40	4370.1	1476.4	40	5219.7	2021.1
50	3638.5	1057.7	50	4383.3	1484.4	50	5234.9	2031.4
65	3650.2	1063.9	75	4396.5	1492.4	85	5250.3	2041.7
10	3661.9	1070.2	10	4409.8	1500.5	10	5265.6	2052.1
20	3673.7	1076.6	20	4423.1	1508.6	20	5281.0	2062.5
30	3685.4	1082.9	30	4436.4	1516.7	30	5296.4	2073.0
40	3697.2	1089.3	40	4449.7	1524.9	40	5311.9	2083.5
50	3709.0	1095.7	50	4463.1	1533.1	50	5327.4	2094.1
66	3720.9	1102.2	76	4476.5	1541.4	86	5343.0	2104.7
10	3732.7	1108.6	10	4489.9	1549.7	10	5358.6	2115.3
20	3744.6	1115.1	20	4503.4	1558.0	20	5374.2	2126.0
30	3756.5	1121.7	30	4516.9	1566.3	30	5389.9	2136.7
40	3768.5	1128.2	40	4530.4	1574.7	40	5405.6	2147.5
50	3780.4	1134.8	50	4544.0	1583.1	50	5421.4	2158.4
67	3792.4	1141.4	77	4557.6	1591.6	87	5437.2	2169.2
10	3804.4	1148.0	10	4571.2	1600.1	10	5453.1	2180.2
20	3816.4	1154.7	20	4584.8	1608.6	20	5469.0	2191.1
30	3828.4	1161.3	30	4598.5	1617.1	30	5484.9	2202.2
40	3840.5	1168.1	40	4612.2	1625.7	40	5500.9	2213.2
50	3852.6	1174.8	50	4626.0	1634.4	50	5517.0	2224.3
68	3864.7	1181.6	78	4639.8	1643.0	88	5533.1	2235.5
10	3876.8	1188.4	10	4653.6	1651.7	10	5549.2	2246.7
20	3889.0	1195.2	20	4667.4	1660.5	20	5565.4	2258.0
30	3901.2	1202.0	30	4681.3	1669.2	30	5581.6	2269.3
40	3913.4	1208.9	40	4695.2	1678.1	40	5597.8	2280.6
50	3925.6	1215.8	50	4709.2	1686.9	50	5614.2	2292.0
69	3937.9	1222.7	79	4723.2	1695.8	89	5630.5	2303.5
10	3950.2	1229.7	10	4737.2	1704.7	10	5646.9	2315.0
20	3962.5	1236.7	20	4751.2	1713.7	20	5663.4	2326.6
30	3974.8	1243.7	30	4765.3	1722.7	30	5679.9	2338.2
40	3987.2	1250.8	40	4779.4	1731.7	40	5696.4	2349.8
50	3999.5	1257.9	50	4793.6	1740.8	50	5713.0	2361.5
70	4011.9	1265.0	80	4807.7	1749.9	90	5729.7	2373.3
10	4024.4	1272.1	10	4822.0	1759.0	10	5746.3	2385.1
20	4036.8	1279.3	20	4836.2	1768.2	20	5763.1	2397.0
30	4049.3	1286.5	30	4850.5	1777.4	30	5779.9	2409.9

2 36.02
1 18.01

38
288
292



152.63

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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