1616

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

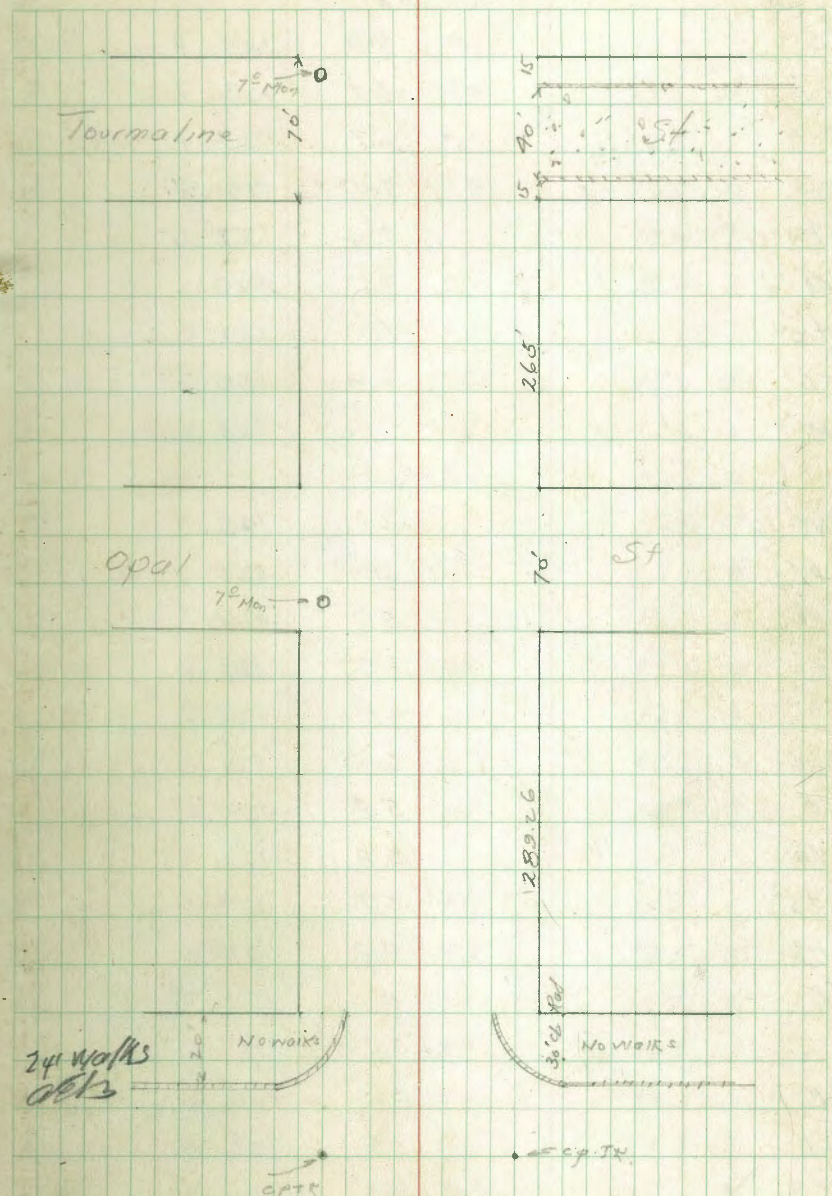
Bliss Notes
Sommermyer ⊼
Beggs Rod.
10/11/41

80' St
20' cbs
10' 1/4's

X Sec Everts Loring to Tourmaline

	2.57	135.55		132.98	Mon SW 7' Set on X Sec of Opal See Book
T.P.	1.33	129.83	7.05	128.50	
		Sec on N Cb Line of Loring			
E-10 Cb P.C. Top cb			6.55	123.28	
Gutter			7.30	122.53	
E			7.52	122.31	
cb			8.06	121.77	
1/4			8.26	121.57	
℄			8.44	121.39	
1/4			8.77	121.06	
cb			9.02	120.81	
W			9.52	120.31	
+10 Curb BC Gutter			9.80	120.03	
" Top cb			9.17	120.66	
		0+00 N Line of Loring			
W			8.3	121.5	
W Top cb			7.81	122.02	
Gutter			8.38	121.45	
1/4			7.89	121.94	
℄			7.51	122.32	
1/4			7.33	122.50	
Gutter			7.26	122.57	
Top cb			6.49	123.34	
E			6.1	123.7	

Red. Plot.
ECB 10/15/41



2' walks
ECB

	T 129.83		
	0+03		
E		4.9	124.9
cb		6.1	123.7
+1		6.7	123.1
1/4		7.0	122.8
℄		7.2	122.6
1/4		7.5	122.3
+07		7.9	121.9
cb		6.2	123.6
W		6.5	123.3
	0+20		
W-10		6.1	123.7
W		6.0	123.8
17		5.7	124.1
cb		6.0	123.8
+5		6.4	123.4
1/4		6.2	123.6
℄		5.8	124.0
1/4		5.8	124.0
+5		5.8	124.0
cb		4.8	125.0
E		4.1	125.7
	0+40		
E		3.2	126.6
cb		3.8	126.0
+5		3.9	125.9
+6		4.5	125.3

	T 129.83		
1/4		4.5	125.3
℄		4.4	125.4
1/4		4.7	125.1
cb		4.8	125.0
W		5.1	124.7
+10		5.0	124.8
	0+70		
W-10		3.8	126.0
W		3.8	126.0
cb		3.6	126.2
1/4		3.4	126.4
℄		3.0	126.8
1/4		3.3	126.5
+4		3.4	126.4
+5		2.9	126.9
cb		2.6	127.2
E		2.1	127.7
	1+00		
E		1.2	128.6
cb		1.3	128.5
+4		1.9	127.9
+5		2.4	127.4
1/4		2.3	127.5
℄		2.4	127.7
1/4		2.6	127.2

		↑ 129.83			
cb			2·8	127.0	
W			3.2	126.6	
+10			3·2	126.6	
TP	12·60	141.10	1.33	128.50	
		1+50			
W-10			12·9	128.2	
W			12·9	128.2	
cb			12.5	128.6	
¼			12·3	128.8	
℄			11·9	129.2	
¼			12·0	129.1	
+4			12·1	129.0	
+5			11.7	129.4	
cb			11.5	129.6	
E			11.0	130.1	
		2+00			
E			9 5	131.6	
cb			9 8	131.3	
+5			10.2	130.9	
+6			10·7	130.4	
¼			10·6	130.5	
℄			10·4	130.7	
¼			10·7	130.4	
cb			10·7	130.4	
W			10·9	130.2	
+10			10·9	130.2	

		↑ 141.10		
		2+50		
W		9 3	131.8	
cb		9 0	132.1	
¼		9.0	132.1	
℄		8 8	132.3	
¼		9 0	132.1	
+4		9 1	132.0	
+5		8·9	132.7	
cb		8·1	133.0	
E		7.9	133.2	
	according To Tie pt Book	2+89.24	S. Line of Opal	
E		6.6	134.5	
cb		6·9	134 2	
+4		7.1	134.0	
+5		7.8	133.3	
¼		7.7	133.4	
℄		7.6	133.5	
¼		7 8	133.3	
cb		7.7	133.4	
W		8.0	133.1	
check starting BM SW 73 pm		8.4	132.98	
		0+00	N. Line of Opal	
W		6.2	134.9	
cb		5·6	135.5	
¼		5.5	135.6	
℄		5.4	135.7	

		T 141.10		
1/4			5.1	136.0
cb			4.7	136.4
E			4.5	136.6
		0+40		
E			3.2	137.9
cb			2.9	138.2
1/4			3.5	137.6
℄			4.1	137.0
1/4			4.3	136.8
cb			4.6	136.5
W			5.1	136.0
+10			5.2	135.9
		0+50		
W-10			5.0	136.1
W			4.9	136.2
cb			4.3	136.8
1/4			4.0	137.1
℄			3.6	137.5
1/4			3.0	138.1
cb			2.9	138.2
+5			3.4	137.7
E			3.4	137.7
		0+65		
E			4.2	136.9
+10			3.7	137.4
cb			3.9	137.2

		T 141.10		
1/4			3.9	137.2
℄			4.0	137.1
1/4			3.8	137.3
cb			3.7	137.4
W			4.5	136.6
+10			4.7	136.4
		0+75		
W+10			4.5	136.6
W			4.2	136.9
cb			4.1	137.0
1/4			4.2	136.9
℄			4.1	137.0
1/4			4.0	137.1
cb			4.0	137.1
+5			3.6	137.5
E			2.5	138.6
		0+85		
E			2.4	138.7
cb			4.1	137.0
1/4			4.5	136.6
+5			3.8	137.3
℄			3.9	137.2
1/4			4.3	136.8
cb			4.3	136.8
+10			4.4	136.7
W			4.8	136.3
+10			4.4	136.7

		141.10		
		1+00		
W-10			4.8	136.3
W			4.7	136.4
CL			4.0	137.1
+5			4.5	136.6
1/4			5.0	136.1
+5			4.0	137.1
℄			3.8	137.3
1/4			2.9	138.2
CL			2.2	138.9
E			2.1	139.0
		1+12		
E			1.9	139.2
+10			2.0	139.1
CL			2.2	138.9
1/4			2.5	138.6
℄			2.7	138.4
1/4			3.4	137.7
+8			4.7	136.4
CL			4.7	136.4
+10			5.0	136.1
W			4.3	136.8
+10			4.8	136.3
		1+20		
W-10			5.0	136.1
YY			5.6	135.5

		141.10		
+10			4.5	136.6
CL			3.3	137.8
1/4			2.8	138.3
℄			2.5	138.6
1/4			2.3	138.8
CL			2.1	139.0
E			1.8	139.3
T.P.	8.66	147.34	2.42	138.68
		1+40		
E			7.4	139.9
CL			8.0	139.3
1/4			8.2	139.1
℄			8.4	138.9
1/4			8.5	138.8
CL			8.9	138.4
W			9.7	137.6
+10			10.2	137.1
		1+70		
W-10			9.1	138.2
YY			8.6	138.5
CL			8.3	139.0
1/4			8.0	139.3
℄			7.5	139.8
1/4			7.2	140.1
CL			7.1	140.2
E			7.1	140.2

147.34

2+30		
E	5.3	142.0
cb	6.1	141.2
1/4	6.4	140.9
℄	6.7	140.6
1/4	7.0	140.3
cb	7.4	139.9
W	8.2	139.1
+10	8.7	138.6
2+60		
W-10	9.2	138.1
W	8.8	138.5
cb	7.5	139.8
1/4	7.0	140.3
℄	6.6	140.7
1/4	6.4	140.9
cb	6.1	141.2
E	5.6	141.7
2+65 · S. Line Tourmaline		
E	6.0	141.3
cb	6.8	140.5
1/4	7.1	140.2
℄	7.7	139.6
1/4	8.1	139.2
cb	8.3	139.0
W	9.1	138.2
+10	9.4	137.9

147.34

+15 Sec on S cb Line Tourmaline

W			9.6	137.7
cb			9.1	138.2
1/4			8.6	138.7
℄			8.3	139.0
1/4			7.9	139.4
cb			7.7	139.6
E on Paving Gutter			6.96	140.38
E on Top cb			6.34	141.00
T.P.	7.27	148.98	5.63	141.71
Set B.M.	H.T. pt on cocked Mon.	S.W. 7^2 pt Everts & Sapphire	8.22	140.76
T.P.	0.67	138.47	11.18	137.80
T.P.	2.77	132.19	9.05	129.42
Set B.M. SW 7^2 Mon.		Dawes & Sapphire	5.41	126.78

10/14/41
Bliss
Sommermyer
Peggs

X-Section Sapphire St from the East Line of Dawes to E. Line Everts

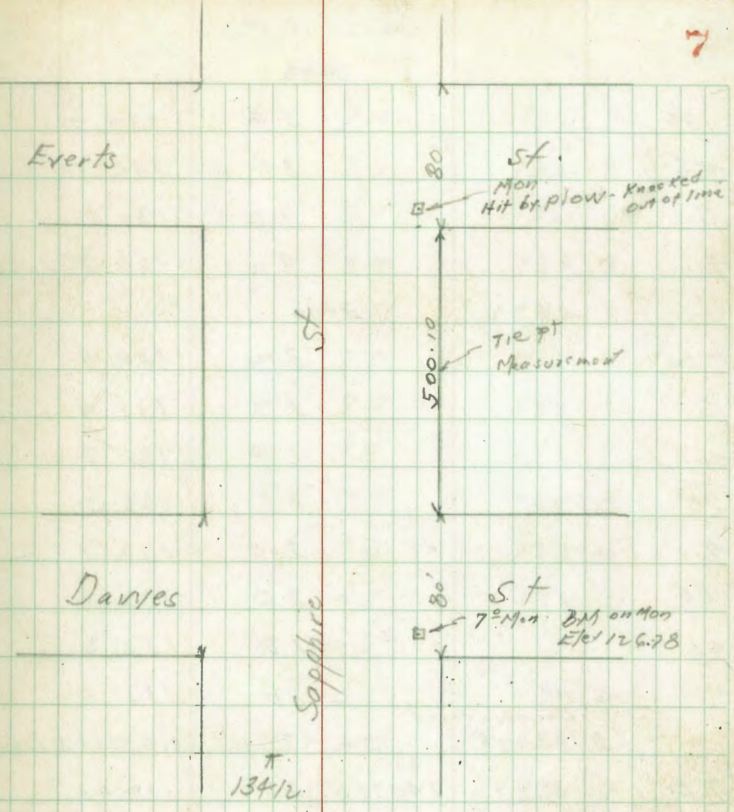
70' st
15' cbs
10'4'

	7.34	134.12		126.78	SW. Mon. See pg. Dawes + Sapphire St.
S-10			6.8	127.3	
S			6.3	127.8	
cb			5.7	128.4	
1/4			5.7	128.4	
℄			5.4	128.7	
1/4			5.3	128.8	
cb			5.1	129.0	
N			4.8	129.3	

Line abandoned — 0+10 Shad Mon. Telephone pole 10' N. of S. Line
D 18500 T — 0+21.5 Telephone pole 10' N of S. Line
" "

			0+50	
N			4.2	129.9
cb			4.4	129.7
1/4			4.6	129.5
℄			4.5	129.6
1/4			4.9	129.2
cb			5.0	129.1
S			5.4	128.7
+10			5.7	128.4
		1+00		
-10			5.0	129.1
S			4.8	129.3
cb			4.3	129.8
1/4			4.1	130.0

ENB Ret. plat. 10/15/41



	1+00	
℄	4.1	130.0
1/4	4.0	130.1
cb	3.9	130.2
N	3.6	130.5
	1+50	
N	2.5	131.6
cb	2.8	131.3
1/4	3.0	131.1
℄	3.4	130.7

		134.12		
		1+50		
1/4			3.4	130,7
cb			3.4	130.7
S.			4.0	130.1
+10			4.2	129.9
		2+00		
-10			3.2	130.9
S			2.7	131.4
cb			2.4	131.7
1/4			2.1	132.0
℄			2.0	132.1
1/4			2.0	132.1
cb			1.9	132.2
N			1.8	132.3
	Line abandoned			
	D 184997	2+15 Tel. pole	3.4 N of S line	
TP	8.27	140.70	1.69	132.43
		2+33		
N			7.6	133.1
cb			7.9	132.8
1/4			8.1	132.6
℄			8.3	132.4
1/4			8.4	132.3
cb			8.8	131.9
S.			9.2	131.5
+10			9.0	131.7

		140.70		
		2+65		
S-10			7.9	132.8
S			7.9	132.8
+10			8.1	132.6
+13			8.8	131.9
cb			8.7	132.0
S			7.8	132.9
1/4			7.7	133.0
℄			7.8	132.9
1/4			7.7	133.0
cb			7.3	133.4
N			6.7	134.0
		3+00		
N			6.5	134.2
cb			6.5	134.2
1/4			6.7	134.0
℄			6.7	134.0
1/4			6.6	134.1
+5			6.6	134.1
cb			7.4	133.3
+6			8.1	132.6
+7			6.9	133.8
S			6.8	133.9
+10			7.2	133.5
		3+30		
S-10			5.9	134.8

T
140·70

3+30

S.		6.1	134.6
+2		6.8	133.9
+5		6.9	133.8
+8		5.9	134.8
cb		5.8	134.9
1/4		5.8	134.9
℄		5.8	134.9
1/4		5.7	135.0
cb		5.6	135.1
N.		5.5	135.2

3+58

N		4.9	135.8
cb.		4.8	135.9
1/4		4.8	135.9
℄		4.9	135.8
1/4		4.9	135.8
cb		5.1	135.6
+5		5.7	135.0
S.		5.3	135.4
+10		5.2	135.5

4+00

-10		3.7	137.0
S.		3.7	137.0
cb.		3.8	136.9
1/4		3.6	137.1
℄.		3.6	137.1

T
190·70

1/4		3.4	137.3
cb		3.2	137.5
N		3.3	137.4

Telephone line abandoned
41+179 H 4+04 pole 3.5 S of S. Line

4+15 D Man 4' S of So. Line

4+50

N.		1.8	138.9
cb		1.2	139.5
1/4		1.6	139.1
℄		1.6	139.1
1/4		1.6	139.1
cb		1.9	138.8
S.		1.8	138.9
+10		1.8	138.9
T.P.	7.40	147.08 1.02	139.68

5+00 10 W Line Evers

S.-10		6.4	140.7
S.		6.0	141.1
cb		6.3	140.8
1/4		6.0	141.1
℄		6.1	141.0
1/4		6.0	141.1
cb		5.8	141.3
N		5.9	141.2

T 147.08

W cb of Everts

N		5.1	142.0
cb		5.5	141.6
1/4		5.3	141.8
℄		5.4	141.7
1/4		5.3	141.8
cb		5.2	141.9
S		5.1	142.0

℄ Everts - Sapphire

S		4.4	142.7
cb		4.3	142.8
1/4		4.4	142.7
℄		4.5	142.6
1/4		4.6	142.5
cb		4.6	142.5
N		4.5	142.6

E cb Everts

N		2.9	144.2
cb		3.2	143.9
1/4		3.2	143.9
℄		3.0	144.1
1/4		3.0	144.1
cb		3.5	143.6
S		3.6	143.5

E Line Everts = School Prop Line

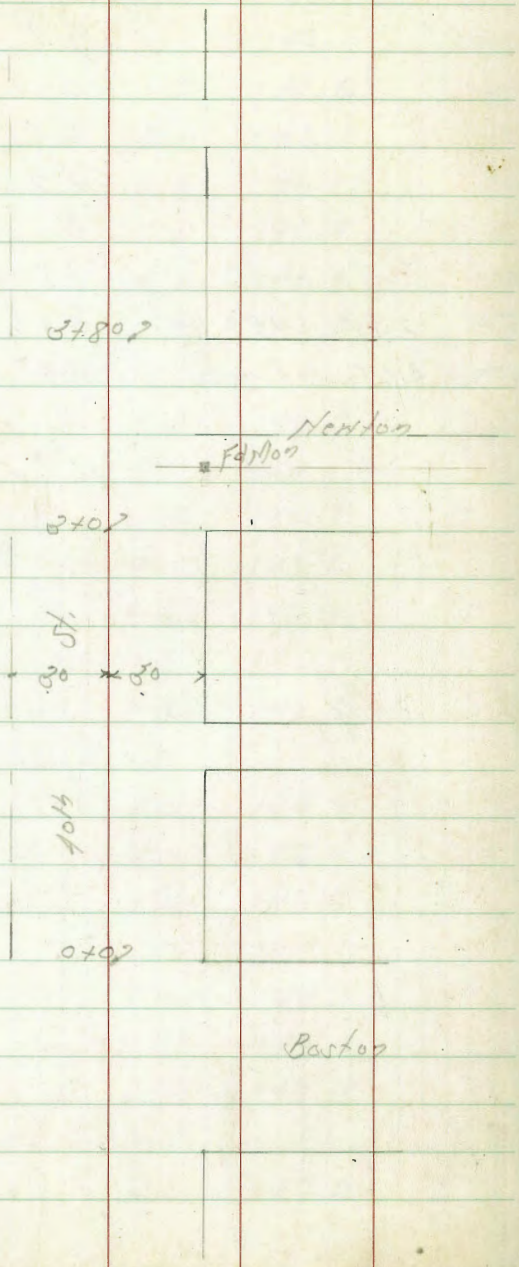
S		2.1	145.0

T 147.08

cb		2.1	145.0
1/4		2.2	144.9
℄		2.1	145.0
1/4		1.9	145.2
cb		2.1	145.0
N		1.7	145.4
T.P.	2.75	14444	
		5.39	141.69 +
check BM Opp 1st Everts		11.47	13.297 +
			13.299
			0.01 error

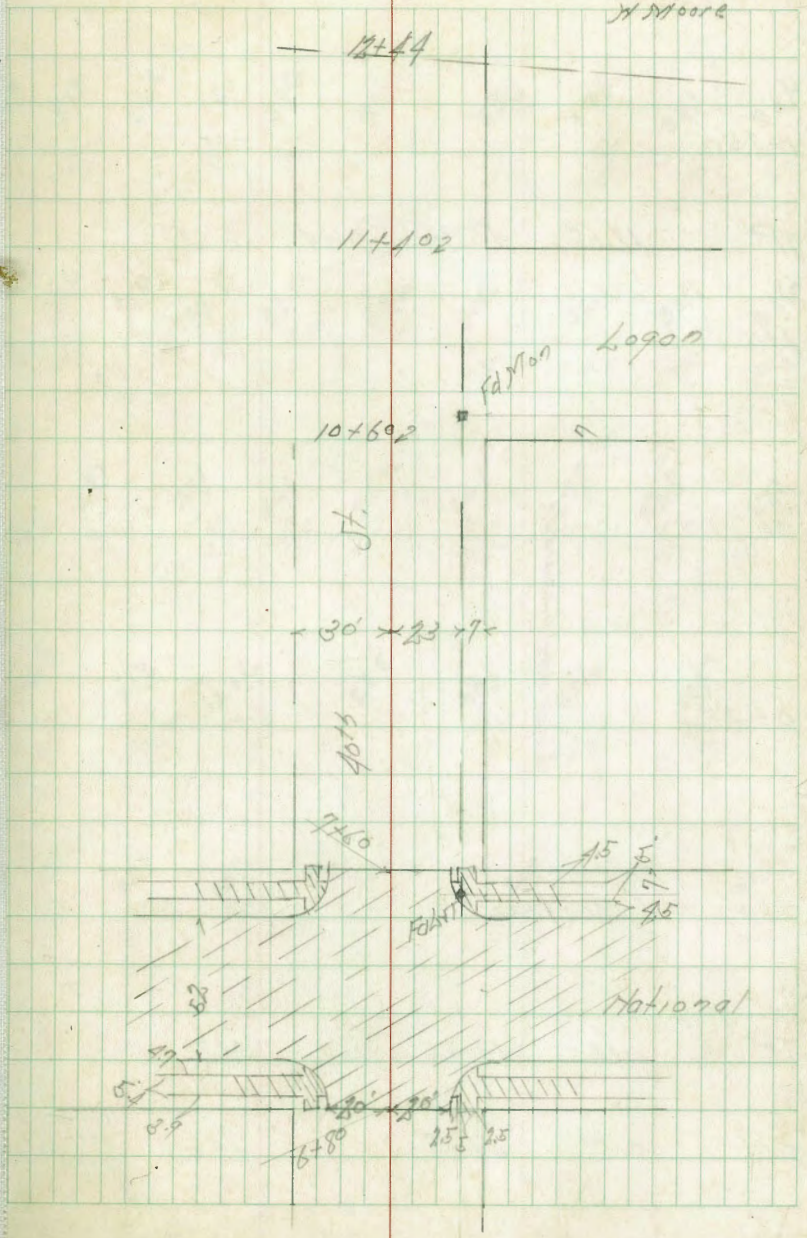
Cross Section 40+55 St.
Boston Ave to North of Logan Ave

Indexed
4 M



Oct 31 41
Sisson
Northern
M Moore

11



40th St.

1+35					
TP	12.15	45.36	0.34	33.21	
1+0					
0+70	Reduced & Plotted 11-15-41 GDK				
0+35					
0+0 = N.L. Boston					
TP	0.34	33.55	11.67	33.21	
BM	0.51	44.88		44.37	N/on E.L. 40th St. & of Newton

Lt = W | ℄ | Rt = E

38.4 7.2/40	37.3 8.3/30	36.4 9.2/20	36.1 9.5/9	33.6 12.0/6	33.6 12.0	33.9 11.7/15	34.4 11.2/25	34.1 11.5/30	33.6 12.0/40

45.36

36.6 [illegible]/40	34.6 11.0/30	34.0 10.4/20	33.5 [illegible]/9	31.0 [illegible]/6	30.6 15.0	30.6 15.0/15	32.1 [illegible]/25	31.9 [illegible]/30	31.6 [illegible]/40
27.0 6.6/40	27.1 6.5/30	27.1 6.5/10	26.1 7.5/5	26.2 7.4	26.1 7.5/15	27.8 5.8/25	27.8 5.8/30	27.7 5.9/40	
20.6 13.0/40	21.3 12.3/30	21.6 12.0/15	22.5 11.1	22.1 11.5/10	22.6 11.0/30	22.5 11.0/40			
19.7 12.9/40	20.1 13.5/30	20.3 13.3/15	20.5 13.1	20.7 12.9/15	20.2 13.4/30	20.1 13.5/40			

33.55

40th St.

3+82 — 28.8 Rt of ℄ – Ely Power Pole ✓

3+80 = N.L. Newton

3+40 = ℄ Newton

TP	11.68	56.04	1.00	44.36	Mon EL 40th 13 L of Newton

3+0 = S.L. Newton

2+50

2+0

1+94 — 27 Rt of ℄ – Ely Power Pole ✓

1+50 = ℄ Alley

45.36

Lt — ℄ — Rt

51.0 / 5.0 / 40	50.3 / 5.7 / 30	49.7 / 6.3 / 20	49.2 / 6.8 / 9	47.6 / 8.4 / 7	47.7 / 8.3	47.2 / 8.8 / 10	46.5 / 9.5 / 22	46.9 / 9.1 / 30	46.5 / 9.5 / 30	
49.2 / 6.8 / 40	48.6 / 7.4 / 30	47.8 / 8.2 / 20	46.9 / 9.1 / 10	45.8 / 10.2 / 3	45.8 / 10.2	45.7 / 10.3 / 15	45.2 / 10.8 / 30	44.5 / 11.5 / 40		
					56.04					
47.4 / +1.8 / 40	46.6 / +1.0 / 30	45.6 / 0.0 / 15	45.6 / 0.0 / 5	44.1 / 1.5 / 3?	44.1 / 1.5	44.1 / 1.5 / 15	43.9 / 1.7 / 30	43.5 / 2.1 / 40		
44.2 / 1.4 / 40	43.8 / 1.8 / 30	43.5 / 2.1 / 20	43.0 / 2.6 / 6	40.7 / 4.9 / 3	40.7 / 4.9	41.2 / 4.4 / 10	41.3 / 4.3 / 20	40.9 / 4.7 / 30	40.8 / 4.8 / 40	
41.5 / 4.1 / 40	40.6 / 5.0 / 30	40.0 / 5.6 / 20	39.8 / 5.8 / 8	38.1 / 7.5 / 5	38.1 / 7.5	38.2 / 7.4 / 10	38.3 / 7.3 / 20	38.6 / 7.0 / 25	38.2 / 7.4 / 30	38.0 / 7.6 / 40
39.5 / 6.1 / 40	38.4 / 7.2 / 30	37.7 / 7.9 / 20	37.2 / 8.4 / 9	35.6 / 10.0 / 6	35.4 / 10.2	35.5 / 10.1 / 15	35.9 / 9.7 / 25	35.8 / 9.8 / 30	35.7 / 9.9 / 40	
					45.36					

90+55 St.

6+67	30.1 Rt of ℄ = Ely Tel Pole ✓			
6+50				
6+0				
TP	18.08	67.98	0.14	55.90
5+61	29.4 Rt of ℄ = Ely Tel Pole ✓			
5+50				
5+21.5	29.1 Rt of ℄ = Ely Power Pole ✓			
5+0				
4+50				
4+0				
		66.04		

Lt ℄ Rt.

61.7	61.0	60.0	59.1	58.9	57.3	57.2	56.8
6.8	7.0	8.0	8.6	9.1	10.7	10.8	11.2
30	15	13		11	20	30	40
60.3	59.6	57.1	56.9	56.6	54.4	54.0	52.8
7.7	8.4	10.9	11.1	11.4	13.6	14.0	15.2
30	18	13		15	21	30	40

67.98

58.1	58.0	57.0	55.2	55.2	54.8	52.7	52.2	51.5
+1.5	+2.0	+1.0	0.8	0.8	1.2	3.3	3.8	4.5
30	20	15	12		17	22	30	40
56.6	55.4	54.7	52.7	52.3	51.6	51.0	50.84	
+0.6	0.6	0.3	2.3	2.7	4.4	5.0	5.16	
30	20	13		15	20	30	38	
53.6	52.4	51.6	50.5	50.3	49.9	49.8	49.0	48.5
2.4	3.6	4.4	5.5	5.7	6.1	6.2	7.0	7.5
33	30	20	12		15	20	30	40
51.8	51.0	50.1	49.7	48.8	48.3	48.0	47.7	47.0
4.2	5.0	5.9	6.3	7.2	7.7	8.0	8.3	9.0
40	30	20	11	10		15	30	40

56.04

40+55 Lt.

7+75

7+60 - ℄ Lt National

7+46 = ℄ Cb Line

7+20 = ℄ National

6+94 = ℄ Cb Line

6+80 = ℄ Lt National

67.98

Lt. ℄ Rt

66.0	65.5	65.4	65.3	67.1	66.7	64.3
2.0	2.5	2.6	2.7	0.9	1.2	1.7
30	15		7	16	45	30

65.8	65.15	64.49	64.38	64.04	63.90	62.60	63.23	63.96
2.8	2.83	3.49	3.60	3.94	4.38	5.38	4.75	4.4
30	30-Cb	45-Gutter	10		10	40-Gutter	40-Cb	30

65.15	64.42	64.10	63.71	63.89	62.96	62.58	62.29	63.06
2.83	3.56	3.88	4.37	4.19	5.07	5.40	5.69	4.92
30-Cb	30-Gutter	20	10		10	20	30-Gutter	30-Cb

64.24	63.90	63.64	63.28	62.93	62.58	62.23	
3.71	4.08	4.34	4.70	5.05	5.40	5.75	
30	20	10		10	20	30	

63.02	62.38	62.08	61.80	61.47	61.19	60.79	60.53	61.07
4.96	5.60	5.90	6.18	6.51	6.79	7.19	7.43	6.91
30-Cb	30-Gutter	20	10			20	30-Gutter	30-Cb

63.0	62.75	62.22	62.08	61.85	61.31	60.80	61.12	61.0
5.0	5.13	5.76	5.90	6.13	6.67	7.18	6.86	7.0
30	40-Cb	40-Gutter	10		10	20-Gutter	40-Cb	30

67.98

40+65ft.

10+0				
9+50				
9+0.	30.1 Rt of ℄ = My Picket Fence.			
TP	8.86	72.06	8.28	64.70.
8+70				
8+40				
8+04	30.2 Rt of ℄ = My Picket Fence ✓			
8+0				
		67.98		

Lt.		℄	Rt	
65.8	65.4	65.3	65.1	64.9
7.3	7.7	7.8	8.0	8.2
40	30	15	5	
65.3	65.9	67.6	68.5	
7.8	7.3	5.5	4.6	
10	19	30	40	
65.6	65.3	64.8	64.6	64.5
7.5	7.8	8.3	8.5	8.6
40	30	15		7
62.6	62.4	62.5	63.5	
10.5	10.7	10.6	9.6	
15	25	30	40	
65.9	65.6	64.9	64.7	64.4
7.3	7.5	8.3	8.4	8.7
40	30	18		10
62.0	60.3	58.6		
11.1	12.3	14.3		
18	30	40		

72.06

66.0	65.6	65.4	65.1	64.7	63.7	62.7
2.0	2.4	2.6	2.9	3.3	4.3	5.3
30	15		10	30	30	40
66.9	66.4	66.2	65.7	64.6	64.3	
1.1	1.6	1.8	2.3	3.4	3.7	
30	15		18	30	38.5	

Garage Driveway ✓

67.2	67.2	66.9	66.8	66.9	67.1	66.3	65.8
0.8	0.8	1.1	1.2	1.1	0.9	1.8	2.3
30	20	15		15	23	30	35

67.98

12+44 = P.L. Line					
12+10					
11+60					
TP	10.54	83.56	0.04	73.02	
11+40 = N.L. Logan					
11+10 = ℄					
BM			5.83	67.23	S.E. 7" Mon Logan +40th 67.28
10+60 = S.L. Logan					
10+30					
		73.06			

16 V2

℄ ℄ RI

80.3	80.5	80.3	80.3	79.2	79.1	78.9	78.4
3.3	3.1	3.3	3.3	4.4	4.5	4.7	5.7
10	30	15		15	25	30	40
76.7	77.1	76.6	76.5	76.4	76.8	77.7	77.6 77.4
6.9	6.5	7.0	7.1	7.2	6.8	5.9	6.0 6.2
40	30	15		10	20	25	30 40
74.3	74.7	74.4	74.1	74.6	74.5	74.5 75.4	75.2
9.2	8.9	9.2	9.5	9.0	9.1	9.1 8.2	8.4
10	30	20	10		15	20 25	30

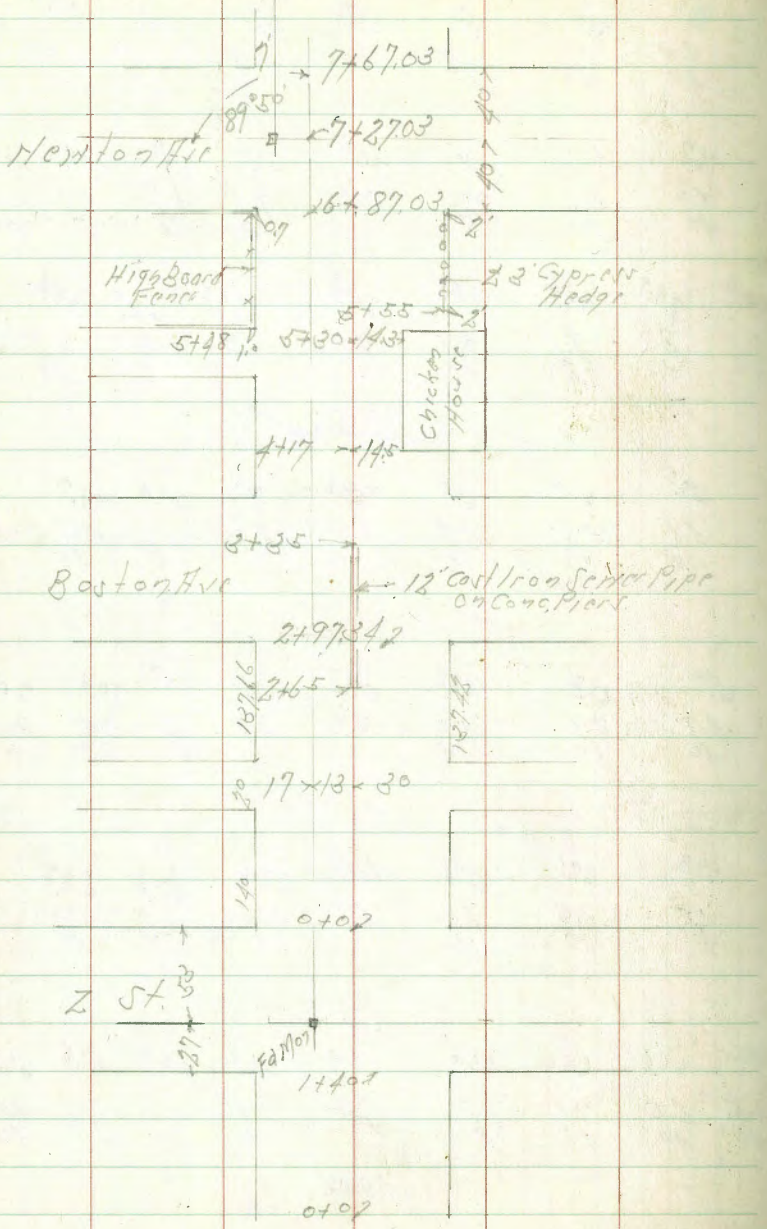
83.356

69.5	69.3	69.3	69.3	70.1	71.4	73.1	73.7
3.6	3.8	3.8	3.8	3.0	1.7	+0.6	+0.6
40	30	15		15	15	25	30
68.4	68.2	68.1	68.1	68.2	68.9	70.3	70.7
4.7	4.9	5.0	5.0	4.9	4.2	2.8	2.4
10	30	15		10	18	23	30
67.3	67.1	67.1	67.0	67.4	67.6	68.2	
5.8	6.0	6.0	6.1	5.7	5.5	4.9	
40	30	15		15	27	30	
66.6	66.6	66.0	65.9	65.7	65.8	66.2	67.5 66.7 68.9
6.5	6.5	7.1	7.2	7.4	7.3	6.9	5.6 4.9 4.3
40	30	15	5		10	30	43 30 40

73.06

Cross Section 41st St.
Z St to Boundary St.

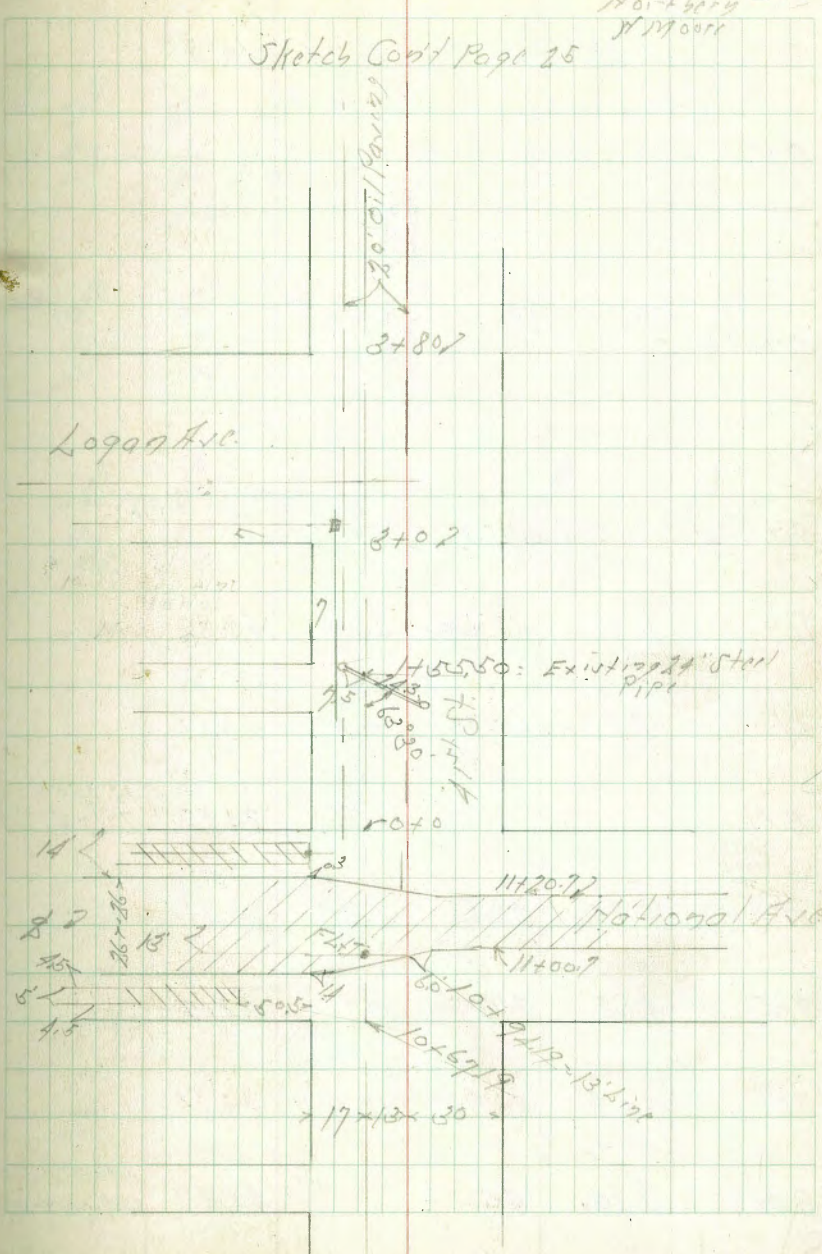
Indexed
LM



Nov 7-91
Sisson
Northern
Wilmoore

17

Sketch Cont'd Page 25



41st St

TP	0.42	41.22	11.74	40.80	
0+70					
0+35					
0+0	= 140 S of S.L. Z st.				
TP	11.74	52.54	0.15	40.80	
TP	12.27	40.95	0.00	28.68	
BM			3.78	24.90	B'Mon Z st & 41st St
TP	5.45	28.68	3.77	23.23	
TP	4.83	27.00	11.77	22.17	
TP	0.58	33.94	12.11	33.36	
BM	1.10	45.47		44.37	Mon E L 40th B Line Norton

Reduced & Plotted 11-17-41 C.B.H.

Lt: W			℄	Rt: E	
36.5	37.9	39.9	42.1	43.8	44.7
16.0 / 45	14.6 / 30	12.6 / 15	10.4	8.7 / 15	7.8 / 30
42.0	42.9	44.8	47.0	49.1	51.2
10.5 / 45	9.6 / 30	7.7 / 15	5.5	3.4 / 15	1.3 / 30
47.8	48.8	50.8	53.0	54.9	57.3
4.7 / 45	3.7 / 30	1.7 / 15	+0.5	+2.4 / 15	+4.8 / 30

52.54

41st St.

1+0

0+50

0+0 = N.L. Z St.

℄ Z St

1+40 = S.L. Z St.

TP	0.63	29.65	12.20	29.02
1+0				
		41.22		

Lt.			℄		Rt.		
23.5 6.2 40	23.5 6.2 30	23.9 5.8 15	24.1 5.6	24.1 5.6 15	24.1 5.6 30	23.7 6.0 40	
23.7 6.0 40	23.6 6.1 30	23.8 5.9 15	23.8 5.9	23.5 6.2 15	23.9 5.8 30	23.9 5.8 40	
23.3 6.4 40	23.2 6.5 30	23.3 6.4 15	23.4 6.3	23.7 6.0 15	23.6 6.1 30	23.7 6.0 40	
23.4 6.3 45	23.9 5.8 30	24.1 5.6 15	24.66 4.99 on MH Rim	24.6 5.1 10	25.5 4.2 15	25.5 4.2 30	25.2 4.5 40
27.3 2.4 45	27.7 2.0 30	27.9 1.8 15	28.0 1.7	28.3 1.4 15	28.4 1.3 30	28.4 1.3 40	
			29.65				
33.2 8.0 45	33.9 7.3 30	34.5 6.7 15	34.8 6.4	35.8 5.4 15	36.8 4.4 30		
			41.22				

4+54					
2+85					
2+70					
2+65	= South End 12" Cast Iron Sewer Pipe on Concrete				
2+57					
TP	5.85	28.37	7.13	22.52	Stake on line 2+65
2+43					
2+0					
1+50					
		29.65			

12.8	12.6	13.0	14.3	15.7	15.9	18.8	
15.6	15.8	15.4	14.1	12.7	13.5	9.6	
50 = N1 Main Channel	30	15		15	30	40	
12.9	14.3	14.6	16.44	15.1	18.1	23.8	24.1
15.5	14.1	13.8	11.93	13.3	10.3	4.6	4.3
45 = Bottom Main Channel	30	15	0.0 = Top of C.I. Sewer Pipe		10	30	40
14.5	15.7	15.8	22.4	22.0	23.2	23.8	23.9
13.9	12.7	12.6	6.0	6.4	5.2	4.6	4.5
50	30	22	15		10	30	40
				28.87			
15.1	22.5	22.8	23.2	23.7	23.6	24.0	
14.6	7.3	6.9	6.5	6.0	6.1	5.7	
50	30 = Top of Channel	15		15	30	40	
23.1	23.1	23.6	24.5	24.2	24.2	24.3	
6.6	6.6	6.1	5.2	5.5	5.5	5.4	
40	30	10		15	30	40	
23.5	23.5	23.7	24.2	24.0	24.1	24.3	
6.2	6.2	6.0	5.5	5.7	5.6	5.4	
40	30	15		15	30	40	
			29.65				

41st St

TP	4.66	30.83	2.20	26.17
4+50				
4+0				
3+62				
3+40				
3+35: N'ly End 12" Cast Iron Sewer Pipe				
3+30				
2+97.34 - S.L. Boston				

28.37

Lt | ℄ | Rt.

4+50: 23.0 5.4/40 | 23.0 5.4/30 | 23.1 5.3/15 | 23.8 4.6 (℄) | 23.3 5.1/15 | 15.5 = N'ly Bldg

4+0: 22.8 5.6/40 | 22.9 5.5/30 | 22.9 5.5/15 | 23.4 5.0 (℄) | 23.0 5.4/15 | 23.1 5.3/30 | 23.2 5.2/40

3+62: 23.2 5.2/40 | 23.3 5.1/30 | 23.2 5.2/15 | 23.6 4.8 (℄) | 22.8 5.6/15 | 22.4 6.0/30 | 18.0 10.4/40

3+40: 23.2 5.2/40 | 23.1 5.3/30 | 22.8 5.6/15 | 22.1 6.3 (℄) | 16.0 12.4/10 | 14.8 13.6/20 | 14.3 14.1/30 | 13.9 14.5/45

3+30: 23.0 5.4/45 | 22.9 5.5/30 | 17.0 11.4/15 | 16.39 11.98 0.18 opp. C.I. Sewer Pipe | 14.7 13.7 (℄) | 13.8 14.6/15 | 13.7 14.7/30 | 12.9 15.5/45: N'ly Main Channel

2+97.34: 14.8 13.6/45 | 12.7 15.7/30 | 13.1 15.3/15 | 12.7 15.7 (℄) | 13.9 14.5/10 | 15.4 13.0/15 | 15.9 12.5/30 | 16.2 12.2/45

28.37

41st St.

Station	Note	Lt 40	Lt 30	Lt 15	℄	Rt 15	Rt 30	Rt 40
7+67.03	= N.L. Newton		25.4 5.4 30	25.3 5.5 15	25.2 5.6	25.3 5.5 15	25.1 5.7 30	
6+87.03	= S.L. Newton. 28.8 Lt of ℄ = W'ly Power Pole ✓		25.0 5.8 30	25.1 5.7 15	25.8 5.0	25.8 5.0 15	26.1 4.7 30	
6+50		25.6 5.2 40	24.7 6.1 30	25.1 5.7 15	25.8 5.0	25.7 5.1 15	26.0 4.8 30	26.0 4.8 40
6+0		24.6 6.2 40	24.6 6.2 30	24.8 6.0 15	25.7 5.1	25.4 5.4 15	25.6 5.2 30	25.6 5.2 4
5+50		24.3 6.5 40	24.4 6.4 30	24.7 6.1 15	25.3 5.5	25.0 5.8 15	24.8 6.0 30	24.8 6.0 34.8 = W'ly 53rd?
5+28	15' Lt of ℄ = W'ly Power Pole ✓							
5+0		22.7 8.1 40	23.7 7.1 30	24.0 6.8 15	24.3 6.5	24.5 6.3 15		

30.83

30.83

41+57					
10+50					
TP	11.29	38.55	0.57	27.26	
10+0					
9+50					
9+0					
8+50					
8+0					
		30.83			

L4		L		R1		
27.4	28.0	28.0	27.6	27.3	26.9	26.9
11.2	10.6	10.6	11.0	11.2	11.7	11.7
40	30	15		15	30	40
			55.55			
			2			
26.3	26.8	26.5	26.4	26.3	26.7	26.3
4.5	4.0	4.3	4.4	4.5	4.6	4.5
40	30	15		15	30	40
25.9	26.2	25.9	26.0	26.0	25.9	26.0
4.9	4.6	4.9	4.8	4.8	4.9	4.8
40	30	15		15	30	40
25.9	26.0	26.2	26.4	26.3	25.8	25.8
4.9	4.8	4.6	4.4	4.5	5.0	5.0
40	30	15		15	30	40
25.9	25.9	26.0	26.1	26.1	26.0	26.0
4.9	4.9	4.8	4.7	4.7	4.8	4.8
40	30	15		15	30	40
25.9	25.8	25.8	26.1	25.8	25.6	25.6
4.9	5.0	5.0	4.7	5.0	5.2	5.2
40	30	15		15	30	40
			30.83			
			2			

41st St.

BM			3.27	35.28 ✓	N.W.B.P. National & 41st St 35.25

Lt — ℄ — Rt

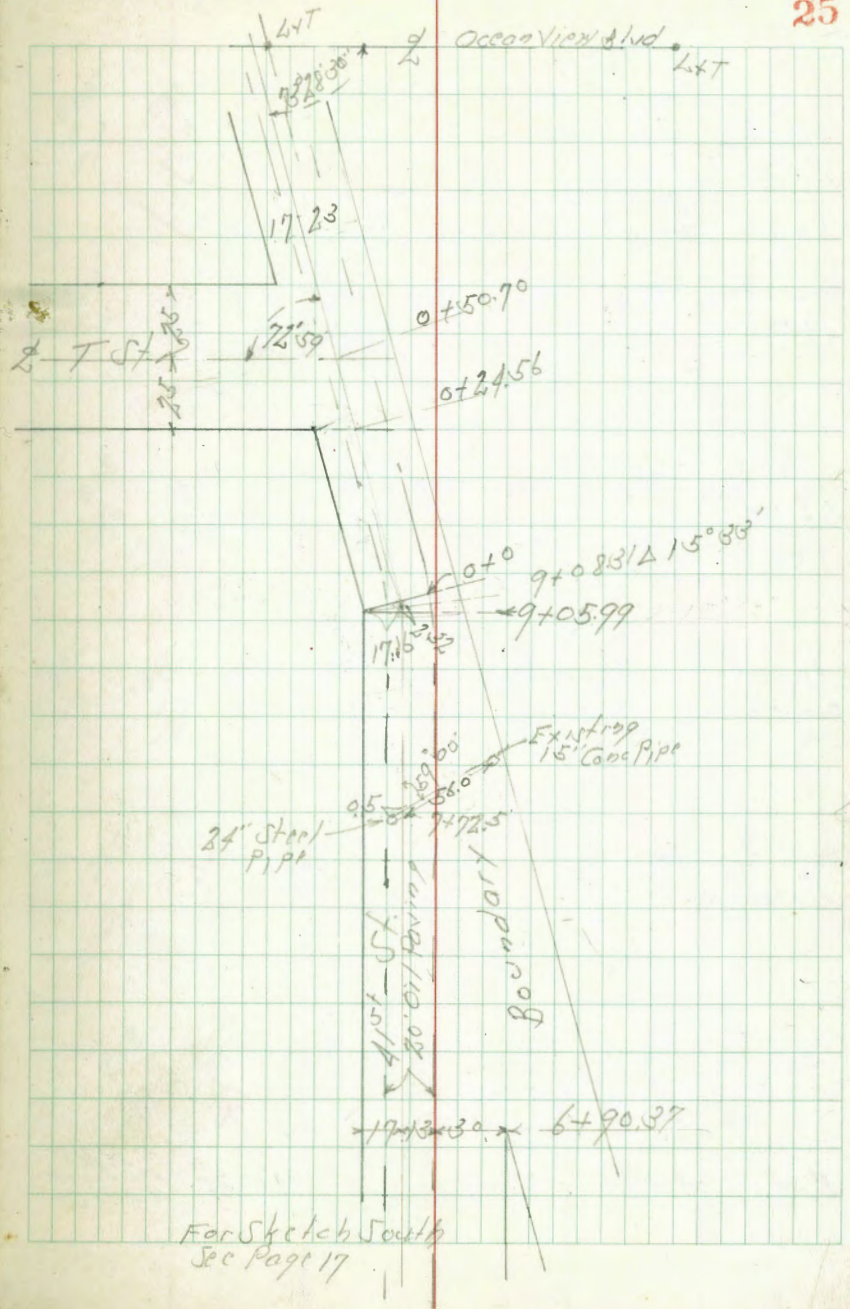
Station									
11+33.19 : N Cb Line National	37.51 / 1.04 / 80-Cb	36.83 / 1.72 / 80-Gutter	35.19 / 3.36 / 29.7-Cb End	34.56 / 3.99 / 29.7-Gutter	34.2 / 4.4 / 15	34.0 / 4.6	33.3 / 5.3 / 15	32.6 / 6.0 / 30	32.1 / 6.5 / 40
11+20.7 - N.L. Strip Paving to East	37.00 / 1.55 / 80	35.61 / 2.94 / 50	34.76 / 3.79 / 30	34.18 / 4.37 / 15	33.60 / 4.95	33.39 / 5.16 / 6-Δ Pav.	33.05 / 5.50 / 15	32.41 / 6.14 / 30	31.54 / 7.01 / 50
11+07.19 = ℄ National Ave	36.83 / 1.72 / 80	34.55 / 4.00 / 30	33.90 / 4.65 / 15	33.47 / 5.08	32.87 / 5.68 / 15	32.23 / 6.32 / 30	31.45 / 7.10 / 50		
11+00.7 = S.L. Strip Paving to East	36.62 / 1.93 / 80	34.29 / 4.26 / 30	33.63 / 4.92 / 15	33.15 / 5.40	32.98 / 5.57 / 6 = Δ Paving	32.64 / 5.91 / 15	32.00 / 6.55 / 30	31.24 / 7.31 / 50	
10+81.19 = S Cb Line National	35.50 / 3.05 / 80.5 = Cb	35.08 / 3.47 / 80.5 Gutter	33.02 / 5.53 / 28.6 - Cb Top End	32.60 / 5.95 / 28.6 - Gutter	34.2 / 4.4 / 15	33.7 / 4.9	32.9 / 5.7 / 15	31.9 / 6.7 / 30	31.2 / 7.4 / 40
10+67.19 = S.L. National	32.6 / 6.0 / 40	29.8 / 8.8 / 30	29.0 / 9.6 / 15	28.2 / 10.4	27.8 / 10.8 / 15	27.5 / 11.1 / 30	27.3 / 11.3 / 40		

38.55

38.55

41st St.

Nov. 13-41



41st St.

1+50					
1+41	20' Rt of ℄ = Ely Anchor Pole 21.5 Lt of ℄ = Wly Power Pole				✓
1+0					
0+70					
0+35					
0+07					
0+0 = H.L. National Ave					
BM	3.54	38.79		35.25	N.W. B.P. National + 41st St

Lt = W ℄ Rt = E

Station					℄				
1+50	30.5 / 8.3 / 40	29.9 / 8.9 / 30	29.6 / 9.2 / 22	31.3 / 7.5 / 19	31.0 / 7.8	28.9 / 9.9 / 10	28.4 / 10.4 / 30	28.3 / 10.5 / 40	
1+0	30.4 / 8.4 / 30	30.3 / 8.5 / 25	31.2 / 7.6 / 20	30.8 / 8.0 / 3	29.7 / 9.1	28.3 / 10.5 / 5	27.9 / 10.9 / 20	27.8 / 11.0 / 30	27.7 / 11.1 / 45
0+70	32.8 / 6.0 / 30	31.9 / 6.9 / 27	32.1 / 6.7 / 15	31.8 / 7.0 / 3	30.3 / 8.5	28.4 / 10.4 / 5	28.0 / 10.8 / 20	27.6 / 11.2 / 30	27.5 / 11.3 / 45
0+35	35.6 / 3.2 / 30	34.1 / 4.7 / 26	33.8 / 5.0 / 15	33.3 / 5.5 / 2	32.8 / 6.0	39.3 / 9.5 / 6	28.0 / 10.8 / 20	27.5 / 11.3 / 30	27.5 / 11.2 / 45
0+07	36.4 / 2.4 / 30	34.5 / 4.3 / 25	34.3 / 4.5 / 15		33.9 / 4.9	29.5 / 9.3 / 7	29.1 / 9.7 / 20	27.3 / 11.5 / 30	27.3 / 11.5 / 45
0+0	35.8 / 3.0 / 30	34.5 / 4.3 / 25	34.2 / 4.6 / 15		34.1 / 4.7	33.4 / 5.4 / 15	32.9 / 5.9 / 25	27.7 / 11.1 / 30	27.5 / 11.3 / 45

38.79

41st St.

Sta.					
3+40 = ℄ Logan					
3+0 = S.L. Logan From West					
2+99	20.8 Lt of ℄ = N'ly Power Pole				✓
TP	11.38	49.71	0.46	38.33	
2+70					
2+35					
2+0					
1+55.5	= 24" Steel Pipe Culvert. 13' Line Sta. on Diagonal				√
		38.79			

Lt. ℄ Rt.

41.2 / 8.5 / 30	41.2 / 8.5 / 23	42.3 / 7.4 / 19	42.4 / 7.3	42.4 / 7.3 / 2	45.0 / 4.7 / 5	45.1 / 4.6 / 15	45.9 / 3.8 / 60	
38.9 / 10.8 / 30	37.6 / 12.1 / 24	38.4 / 11.3 / 19	38.3 / 11.4	38.3 / 11.4 / 2	42.5 / 7.2 / 5	42.2 / 7.5 / 15	42.5 / 7.2 / 30	30.8 = N'ly Cor. House ✓
			49.71					
36.6 / 2.2 / 40	35.1 / 3.7 / 30	35.0 / 3.8 / 25	35.4 / 3.4 / 20	35.0 / 3.8	35.0 / 3.8 / 2	40.8 / +2.0 / 5	41.0 / +2.2 / 15	41.2 / +2.4 / 30 = S'ly Cor Board House ✓
31.4 / 7.4 / 40	32.6 / 6.2 / 30	33.4 / 5.4 / 20	33.3 / 5.5	33.3 / 5.5 / 2	39.8 / +1.0 / 5	37.7 / 1.1 / 15	37.7 / 1.1 / 30	34.8 / 4.0 / 40
30.3 / 8.5 / 40	30.8 / 8.0 / 30	30.7 / 8.1 / 24	32.0 / 6.8 / 19	31.8 / 7.0	32.4 / 6.4 / 15	32.2 / 6.6 / 30	29.2 / 9.6 / 50	

28.83 / 9.96 / 7.5 = Inlet 24" Steel Pipe Flowline

18' Line

27.87 / 10.92 / 24.0 = Outlet

38.79

41st St.

6+0					
5+96	19.8 Lt of ℄ = W'ly Power Pole				✓
5+50					
5+0					
4+50					
TP	9.83	59.35	0.19	49.52	
4+47	19.9 Lt of ℄ = W'ly Power Pole				✓
4+0					
3+80 = N.L. Logan					
		4971			

Lt.				℄				Rt.
51.8 7.6 40	52.5 6.9 30	53.1 6.3 22	54.4 5.0 19	54.1 5.3	54.2 5.2 2	58.4 1.0 6	60.4 +1.0 15	63.0 +3.6 30
51.0 8.4 40	50.8 8.6 30	51.5 7.9 24	52.6 6.8 20	52.9 6.5	52.9 6.5 3	55.9 3.5 6	57.2 2.2 15	60.0 +0.6 30
50.5 8.9 45	49.6 9.8 30	50.1 9.3 22	51.6 7.8 19	51.3 8.1	51.3 8.1 3	53.7 5.7 5	56.0 3.4 15	59.9 +0.5 30
48.9 10.5 40	48.1 11.3 30	47.8 11.6 22	49.7 9.7 18	49.7 9.7	49.7 9.7 3	53.6 5.8 6	56.6 2.8 15	61.3 +1.9 30
				59.35				
45.9 3.8 30	45.1 4.6 25	45.3 4.4 21	46.3 3.4 18	46.6 3.1	46.6 3.1 3	48.4 1.3 4	50.5 +0.8 15	52.4 +2.7 30
	44.4 5.3 30	43.3 6.4 23	45.3 4.4 19	45.4 4.3	47.0 2.7 12	49.4 0.3 30		
				49.71				

8+0

7+72.5 = Existing 24" Steel + 15" Conc Pipe Culvert
13' Line Sta. on Diagonal

7+70

7+40

7+20 18.8 Lt of ℄ = Wly Power Pole ✓

6+90.87 = W.L. Boundary on Rt

6+50

59.85

Lt ℄ Rt

56.4 3.0 40	55.9 3.5 30	55.3 4.1 16	56.1 3.3 13	56.1 3.3	56.0 3.4 7	56.7 2.7 20	56.9 2.5 30	54.6 4.8 35

53.08
6.27
0.5 = Outlet 24" Steel Pipe Flow Line

13' Line

54.60
4.75
56 = Inlet 15" Conc. Pipe Flow Line

54.1 5.3 40	53.3 6.1 30	53.0 6.4 25	53.8 5.6 16	55.5 3.9 13	55.3 4.1	55.2 4.2 5	55.8 3.6 22	57.0 2.4 30

53.1 6.3 40	52.8 6.6 30	53.1 6.3 19	54.7 4.7 14	54.6 4.8	54.9 4.5 5	54.7 4.7 20	55.9 3.5 30

52.6 6.8 40	52.8 6.6 30	54.2 5.2 19	54.6 4.8	54.8 4.8 5	56.1 3.3 3	57.6 1.8 15	59.1 0.3 30

52.4 7.0 40	53.4 6.0 30	54.3 5.1 20	54.6 4.8	57.8 1.6 4	60.4 +1.0 15	63.0 +3.6 30

59.85

BM			2.21	82.20	NWT Lt Ocean View Ave & 49th St 82.18
TP	11.23	84.41	1.93	73.18	
TP	8.24	75.11	4.04	66.87	
0+24.56 = S.L.T. St on Diagonal					
0+0					
9+05.99 = ℄ of Lt					
8+75					
8+56	18.7 Lt of ℄ = Wly Power Pole				
8+50					
TP	11.99	70.91	0.43	58.92	
8+25					
		59.35			

Lt — ℄ — Rt

68.2 2.7/20.9 = WL — 67.4 3.5 — 66.8 4.1/17 = Bldg

67.5 3.4/20 — 66.8 4.1/18 — 66.7 4.2/10 — 66.8 4.1 — 66.5 4.4/6 — 66.8 4.1/10 — 66.3 4.6/16 = Wire Fence

67.5 3.4/30 — 66.7 4.2/28 — 66.8 4.1/15 — 66.3 4.6/3 — 66.5 4.4 — 66.3 4.6/6

68.6 2.3/30 — 68.0 2.9/24 — 64.1 6.8/18 — 63.8 7.1 — 63.8 7.1/5 — 64.8 6.1/8 — 64.5 6.4/15

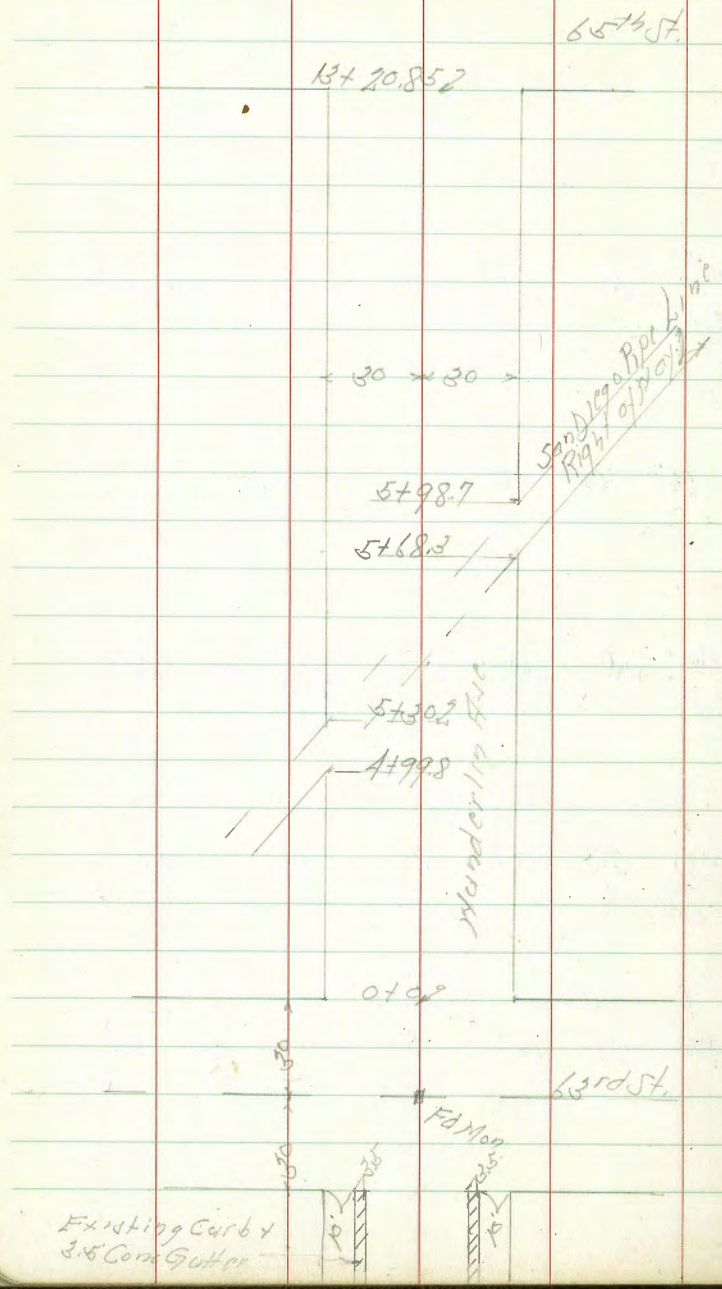
63.1 7.8/30 — 61.2 8.7/16 — 60.9 10.0/13 — 60.5 10.4 — 60.2 10.7/15 — 59.1 11.8/22

70.91

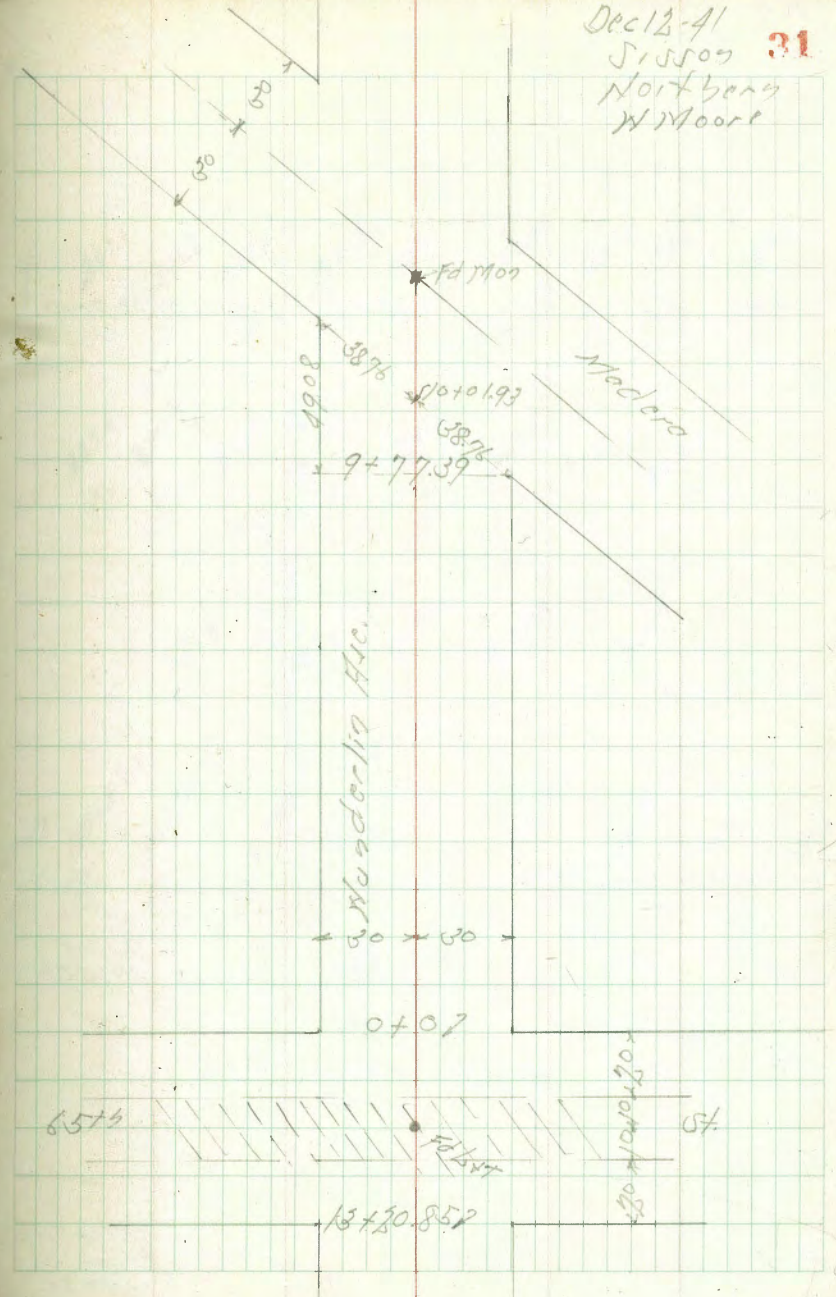
58.8 0.6/30 — 57.6 1.8/17 — 58.1 1.3/14 — 57.7 1.7 — 57.1 2.0/8 — 57.7 1.7/22 — 55.8 2.6/30

59.35

Cross Section Wunderlin Ave
63rd St to Madera



Dec 12-41
Sisson
Northberg
W Moore
31



Wunderlin Ave

0+0 = E.L. 63rd St			29.8 Lt of ℄ = Wly Wire Fence		
0-10					
0-30 = ℄ 63rd St.					
0-60 = W.L. 63rd St					
BM	9.79	309.38	7.62	299.59	℄ Man. Wunderlin Ave 63rd St
TP	12.25	307.21	0.15	294.96	
TP	12.28	295.11	0.26	282.83	
BM	11.89	283.09		271.20	SE Top F.H. at Brooklyn & 63rd St

Notes Reduced & Plotted 12-17-1941
C.B. Haugh

Lt = N ℄ S = Rt.

301.1	301.8	302.2	301.7	302.7	303.7	302.6	305.8	306.3
8.3	7.6	7.2	7.7	6.7	6.2	6.8	3.6	3.1
30	20	13	6		15	20	25	30

299.6	300.4	300.9	300.4	301.7	302.1	302.3	302.9
9.8	9.0	8.5	9.0	7.7	7.3	7.1	6.5
30	20	14	11		10	20	30

297.9	298.6	299.9	300.9	301.4
11.5	10.8	9.5	8.5	8.0
30	20		20	30

295.8	296.28 ✓	295.50 ✓	295.92 ✓	197.2	296.78 ✓	296.51 ✓	297.19 ✓	297.4
13.6	13.10	13.88	13.46	12.2	12.60	12.87	12.19	12.0
30	20 = Cb End	20 = Gutter	16.5 = Edge		16.5 = Edge Conc Gutter	20 = Gutter	20 = Cb End	30

309.38

Station					
1+25					
1+17	28.9 Lt of ℄ = Fly wire Fence ✓				
1+0					
0+75					
0+62	= ℄ 10 Conc Drive on Lt				
0+50					
TP	10.69	319.77	0.30	309.08	
0+25					
		309.38			

✓ Lt — ℄ — Rt

Station												
1+25	316.1 / 3.7 / 40	316.1 / 3.7 / 30	316.4 / 3.4 / 20	316.4 / 3.4 / 10	316.8 / 3.0	316.5 / 3.3 / 11	317.2 / 2.6 / 20	317.2 / 2.6 / 30				
1+0	313.1 / 6.7 / 40	313.4 / 6.4 / 30	313.8 / 6.0 / 20	313.9 / 5.9 / 10	314.3 / 5.5	314.1 / 5.7 / 11	314.5 / 5.3 / 13	315.0 / 4.8 / 20	315.6 / 4.2 / 25	315.9 / 3.9 / 30		
0+75	310.5 / 9.3 / 40	310.8 / 9.0 / 30	310.9 / 8.9 / 20	311.0 / 8.8 / 10	311.5 / 8.3	311.2 / 8.6 / 8	311.7 / 8.1 / 20	313.6 / 6.2 / 27	313.6 / 6.2 / 30			
0+62	308.79 / 10.98 / 40 on Drive	✓ 309.68 / 10.09 / 29.4 S/10 Conc Drive										
0+50	307.7 / 12.1 / 40	308.1 / 11.7 / 30	308.8 / 11.0 / 20	308.5 / 11.3 / 13	309.0 / 10.8	308.7 / 11.1 / 7	308.8 / 11.0 / 15	309.0 / 10.8 / 20	310.8 / 9.0 / 28	310.8 / 9.0 / 30		
					319.77							
0+25	304.4 / 5.0 / 40	304.7 / 4.7 / 30	305.4 / 4.0 / 20	305.7 / 3.7 / 14	305.2 / 4.2 / 11	306.2 / 3.2	306.0 / 3.4 / 9	306.6 / 2.8 / 13	305.5 / 3.9 / 20	305.5 / 3.9 / 23	308.3 / 1.1 / 26	308.3 / 1.1 / 30
					309.38							

Wunderlin Ave.

2+44	=	℄ 3' Conc Walk on Lt			
2+25					
2+04		28.0' Lt of ℄ = Nly 24" Pepper Tree			
2+0					
1+75					
TP	4.27	323.95	0.09	319.68	
1+53	31.8 Rt of ℄ = Sly Power Pole				
1+50					
		319.77			

Lt — ℄ — Rt

✓

321.15 / 2.80 / 30 on Walk	320.38 / 3.57 / 22.0 = Sly 3' Conc Walk								
321.6 / 2.3 / 30	320.7 / 3.2 / 20	319.5 / 4.4 / 10	319.0 / 4.9	318.1 / 5.8 / 11	317.4 / 6.5 / 20	316.4 / 7.5 / 30	315.3 / 8.6 / 40		
321.7 / 2.2 / 30	321.1 / 2.8 / 20	320.0 / 3.9 / 12	319.3 / 4.6	318.6 / 5.5 / 10	318.1 / 5.8 / 20	317.3 / 6.6 / 30	316.4 / 7.5 / 40		
320.7 / 3.2 / 30	320.6 / 3.3 / 20	319.7 / 4.2 / 9	319.7 / 4.2	319.4 / 4.5 / 11	319.3 / 4.6 / 15	319.0 / 4.9 / 20	318.2 / 5.7 / 30	317.1 / 6.8 / 40	

323.95

318.9 / 0.9 / 40	318.7 / 1.1 / 30	318.6 / 1.3 / 20	318.6 / 1.3 / 10	319.0 / 0.8	318.7 / 1.1 / 11	319.1 / 0.7 / 20	318.3 / 1.5 / 30	317.7 / 2.1 / 40

319.77

Station	Notes		Lt. ℄ Rt
3+63	20.0 Rt of ℄ = S'ly Anchor Pole	✓	315.8 (8.1 / 30), 315.0 (8.9 / 20), 314.1 (9.8 / 10), 313.3 (10.6), 312.4 (11.5 / 10), 311.5 (12.4 / 20), 310.3 (13.6 / 30), 309.2 (14.7, 14.5 / 40 [illegible] Plant Floor)
3+50			
3+28	29.8 Rt of ℄ = E'ly Picket Fence	✓	316.7 (7.2 / 30), 315.8 (8.1 / 20), 314.7 (9.2 / 10), 313.9 (10.0), 313.0 (10.9 / 10), 312.2 (11.7 / 20), 311.7 (12.2 / 30), 311.1 (12.8 / 40)
3+11	22.0 Lt. of ℄ = N'ly Wire Fence	✓	312.71 ✓ (11.24 / 30 ℄ 4.8 Conc. Wall), 312.75 ✓ (11.20 / 39: S'ly Wall)
3+01	30' Rt of ℄ = W'ly Picket Fence	✓	
3+0			318.4 (5.5 / 30), 317.0 (6.9 / 20), 315.5 (8.4 / 7), 315.2 (8.7), 314.3 (9.6 / 10), 313.6 (10.3 / 20), 313.0 (10.9 / 30), 312.4 (11.5 / 40)
2+98	27.7 Lt of ℄ = N'ly 30" Pepper Tree	✓	
2+77	28.0 Lt of ℄ = N'ly 18" Pepper Tree	✓	
2+75		✓	319.97 (3.98 / 30 on Wall), 319.42 (4.53 / 25.5 S'ly Wall [illegible] Conc.), 318.6 (5.3 / 20), 316.9 (7.0 / 7), 316.5 (7.4), 315.4 (8.5 / 10), 314.7 (9.2 / 20), 314.0 (9.9 / 30), 313.1 (10.8 / 40)
2+50	21.6 Rt of ℄ = S'ly Power Pole	✓	320.6 (3.3 / 30), 319.6 (4.3 / 20), 318.5 (5.4 / 10), 317.9 (6.0), 317.0 (6.9 / 11), 317.3 (6.6 / 12), 316.3 (7.6 / 20), 315.0 (8.9 / 30), 314.4 (9.5 / 40)

32395

323.95

Wunderlin Ave

TP	0.50	300.71	12.13	300.21	
5+37	12.5 Lt of ℄ = N'ly 6" Peppertree				✓
5+30.2 = E.L. Pipe Line R of W on Lt					
	24.6 Lt of ℄ = E'ly Wire Fence				✓
4+99.8 = W.L. Pipe Line R of W on Lt.					
4+75					
TP	0.33	312.34	11.94	312.01	
4+50					
4+0					
3+77					
		313.95			

Lt.				℄			Rt.	
302.2 10.1 / 40	301.1 11.2 / 30	302.1 10.3 / 20	300.9 11.4 / 10	300.6 11.7	300.1 12.2 / 10	299.9 12.4 / 20	299.0 13.3 / 30	298.5 13.8 / 40
307.4 4.9 / 30	307.3 5.0 / 20	306.5 5.8 / 10		306.3 6.0	305.9 6.4 / 7	304.6 7.7 / 12	303.8 8.5 / 20	303.3 9.0 / 30	302.5 9.8 / 40
311.9 0.4 / 30	311.6 0.7 / 20	310.3 2.0 / 10		309.6 2.7	308.6 3.7 / 10	307.2 5.1 / 20	306.0 6.3 / 30	304.9 7.4 / 40
				312.34				
313.3 10.6 / 30	313.1 10.8 / 20	312.1 11.8 / 10		311.8 12.1	310.7 13.2 / 10	309.4 14.5 / 20	307.9 16.0 / 30	306.4 17.5 / 40
314.9 9.0 / 30	314.3 9.6 / 20	313.5 10.4 / 15		312.8 11.1	311.9 12.0 / 10	310.7 13.2 / 20	309.2 14.7 / 30	307.7 16.2 / 40
315.4 8.5 / 30	314.7 9.2 / 20	313.7 10.2 / 15		313.0 10.9	311.9 12.0 / 10	310.7 13.2 / 20	309.4 14.5 / 30	308.0 15.9 / 44.2 ✓ Edge of Dirt Road
				313.95				

Wanderlin Ave.

7+20				
7+0				
6+70				
TP	0.35	288.82	12.24	288.47
6+35				
5+98.7 = F.L. Pipe Line Rd W on Rt				
5+68.3 = W.L. Pipe Line Rd W on Rt				
		300.71		

Lt. ℄ Rt

	280.7 8.1 30	279.1 9.7 20	277.7 11.1 10	276.5 12.3	275.1 13.7 10	274.6 14.2 20	274.7 14.1 30	275.5 13.3 40
281.8 7.0 40	279.5 9.3 30	279.7 9.1 20	279.4 9.4 10	279.7 9.1	278.9 9.9 15	279.3 9.5 20	279.7 9.1 30	280.2 8.6 40
	285.3 3.5 30	285.1 3.7 20	284.4 4.4 10	284.4 4.4	284.0 4.8 10	283.7 5.1 20	283.7 5.1 30	283.7 5.1 40

288.82

289.5 11.2 30	288.6 12.1 20	288.0 12.7 12	288.6 12.1	287.8 12.9 13	288.4 12.3 20	288.1 12.6 30	288.1 12.6 40	
292.6 8.1 30	292.4 8.3 20	292.2 8.5 10	292.7 8.0	292.3 8.4 10	291.4 9.3 20	290.9 9.8 30	291.8 8.9 35	291.4 9.3 45
296.4 4.3 30	296.6 4.1 20	296.2 4.5 10	295.6 5.1	294.8 5.9 10	295.5 5.2 12	295.1 5.6 20	294.2 6.5 30	293.9 6.8 40

300.71

9+40				
8+65				
TP	0.54	265.63	12.08	266.09
8+30				
TP	0.53	277.17	12.18	276.64
8+0				
7+75				
7+50				
		288.82		

Lt. Ø Rt

257.0	256.4	255.9	255.5	255.2	255.0	254.4	255.8	256.2
8.6	9.2	9.7	10.1	10.4	10.6	10.2	9.8	9.4
40	30	20	10		10	20	30	40
264.9	264.9	264.4	264.1	264.0	264.0	263.9	263.8	263.4
0.7	0.7	1.2	1.5	1.6	1.6	1.7	1.8	2.2
40	30	20	10		10	20	30	40
				265.63				
273.0	272.4	271.8	272.3	272.0	271.2	270.4	269.2	267.8
4.7	4.8	5.4	4.9	5.2	6.0	6.8	8.0	9.1
30	20	10	7		10	20	30	40
				277.17				
277.8	277.6	276.5	276.1	274.8	273.9	272.6	270.7	
1.0	1.2	12.3	12.7	14.0	14.9	16.2	18.1	
30	20	12		10	20	30	40	
279.7	279.0	278.0	277.3	276.2	274.8	173.2	271.2	
9.1	9.8	10.8	11.5	12.6	14.0	15.6	17.6	
30	20	10		10	20	30	40	
280.6	279.6	278.4	277.7	275.4	273.6	272.1	271.2	
8.2	9.2	10.4	11.1	13.4	15.2	16.7	17.6	
30	20	10		10	20	30	40	
				288.82				

Wanderlin Rvc.

10+35					
TP	11.98	27761	0.00	265.63	Rail fence Post on 27 102.05
10+0					
9+65					
9+50					
9+37					
9+20	30.4 Lt of L. W.L. Wire Fence				
		26563			

Lt.		Rt.
269.5	269.1	268.3
8.1	8.5	9.3
40	30	20
267.9	267.2	266.1
9.7	10.4	11.5
10		10
265.5	264.9	263.3
12.1	12.7	14.3
50	30	45

27761

263.4	262.4	261.2	260.4	259.3	257.8	257.6	255.6	254.1
2.2	3.2	4.4	5.2	6.3	7.8	8.0	10.0	11.5
40	30	20	10		10	20	30	45

255.4	255.2	254.6	254.0	253.4	252.8	251.8	251.0	248.1
10.3	10.4	11.0	11.6	12.2	12.8	13.8	14.6	17.5
40	30	20	10		10	20	30	50

248.7	247.6	248.3	249.6	249.9	249.5	248.1	247.0	242.6
16.9	18.0	17.3	16.0	15.7	16.1	17.5	18.6	23.0
50	30	20	10		10	20	30	55

250.9	248.8	246.6	245.5	245.4	245.3	245.3	245.1	248.4
14.7	16.8	19.0	20.1	20.2	20.3	20.3	20.5	17.2
50	30	20	10		10	20	30	60

254.6	253.0	251.6	250.4	249.6	249.0	249.3	249.7	250.1	250.9
11.0	12.6	14.0	15.2	16.0	16.6	16.3	15.9	15.5	14.7
40	30	20	10		10	20	30	40	50

26563

Dec 15-41

12+50				
12+0				
TP	4.54	29316	0.75	28862
11+50				
11+25				
11+0	30.4 Lt of ℄ Wire Fence			✓
TP	11.88	28937	0.12	27749
10+70				
		27761		

Lt. ℄ Rt. 40

291.9	291.0	290.0	289.1	288.2	287.6	287.1	286.6	
1.3	3.3	3.2	4.1	5.0	5.6	6.1	6.6	
30	20	10		10	20	30	40	
29.13	290.9	289.6	288.9	288.1	287.4	286.8	286.2	286.0
1.9	3.3	3.6	4.3	5.1	5.8	6.4	7.0	7.3
40	30	20	10		10	20	30	40
			29316					
287.5	287.2	287.1	287.3	286.4	285.8	285.5	285.1	284.6
1.9	2.2	2.3	2.1	3.0	3.6	3.9	4.3	4.8
35	30	20	10		10	20	30	40
285.0	284.6	284.4	285.8	285.9	285.7	285.4	284.6	281.7
4.4	4.8	5.0	3.6	3.5	3.7	4.0	4.8	7.7
35	30	20	10		10	20	30	45
281.7	281.7	281.8	281.9	283.7	283.2	282.0	280.8	277.9
7.7	7.7	7.6	7.5	5.7	6.2	7.4	8.6	13.0
10	30	20	10		10	20	30	45
			28937					
276.4	275.7	275.6	275.4	274.5	274.0	273.8	273.0	272.1
1.3	1.9	2.0	2.2	3.1	3.6	3.8	4.6	5.5
40	30	20	10		10	20	30	45
			27761					

Wonderlin Ave.

BM	6.26	286.90	Lt T Z Wonderlin 7 65th St	
13+50.85 = Z 65th St				
13+40.85 - Wly Conc. Paving				
13+35				
13+32				
13+20.85 = WL 65th St	50.5 Lt of Z = Ely Wire Fence			
13+0				

293.16

Lt — Z — Rt

Row											
Elev.	290.91	289.55	288.27	287.79	287.35	286.90	286.51	286.12	285.68	284.65	283.63
Rod	2.25	3.61	4.89	5.37	5.81	6.26	6.65	7.04	7.48	8.51	9.53
Dist.	80	55	30	20	10		10	20	30	55	80
Elev.	290.89	289.55	288.28	287.82	287.41	286.96	286.52	286.12	285.71	284.63	283.64
Rod	2.27	3.61	4.88	5.34	5.75	6.20	6.64	7.04	7.45	8.53	9.52
Dist.	80	55	30	20	10		10	20	30	55	80
Elev.		288.4	287.8	287.5	286.9	286.6	286.3	285.9	285.5		
Rod		4.8	5.4	5.7	6.3	6.6	6.9	7.3	7.7		
Dist.		30	20	10		10	20	30	40		
Elev.	290.9	290.7	290.4	288.3	287.7	286.9	287.7	287.8	287.2		
Rod	2.3	2.5	2.8	4.9	5.5	6.3	5.5	5.4	6.0		
Dist.	30	20	11	7		12	20	30	40		
Elev.	291.1	290.6	290.1	289.0	288.3	288.0	287.7	287.3			
Rod	2.1	2.6	3.1	4.2	4.9	5.2	5.5	5.9			
Dist.	30	20	10		10	20	30	40			
Elev.	291.8	290.6	290.2	289.4	288.7	288.0	287.4	287.0			
Rod	1.4	2.6	3.0	3.8	4.5	5.2	5.8	6.2			
Dist.	30	20	10		10	20	30	40			

293.16

	20.8 Lt of ℄ = N'ly 18" Pepper Tree	✓
0+90	19.7 Rt of ℄ = S'ly 4" Tree	✓
0+86		
0+75	20.0 Rt of ℄ = S'ly 6" Tree	✓
0+64	21.0 Lt of ℄ = N'ly 36" Euc Tree	✓
0+54	20.5 Rt of ℄ = S'ly 8" Acacia Tree	✓
0+50	20.5 Rt of ℄ = S'ly Power Pole	✓
0+41	20.3 Rt of ℄ = S'ly 8" Acacia Tree	✓
0+31	20' Rt of ℄ = S'ly 3" Shrub	✓
0+15	21.3 Lt of ℄ = N'ly 24" Euc Tree	✓
0+0 / 13+80.85	= EL 65th St — 30' Rt of ℄ = N'ly Wire Fence	✓
13+70		
13+65		
13+60.85	= E'ly Conc Paving	
	293.16	

8.51

Lt ℄ Rt 5

✓ 284.35
8.81
299= ℄ Conc Walk

	288.2 5.0/30	287.4 5.8/20	287.0 6.2/12	286.1 7.1/9	286.0 7.2	285.8 7.4/16	285.5 7.7/17	285.9 7.3/20	285.4 7.8/30	284.7 8.5/35
	289.4 3.8/30	289.0 4.2/20	288.4 4.8/12	287.0 6.2/9	286.7 6.5	286.7 6.5/10	286.3 6.9/19	287.5 5.7/20	286.9 6.3/30	286.3 6.9/40
	289.8 3.4/30	289.6 3.6/20	288.8 4.4/15	286.7 6.5/9	286.5 6.7	286.2 7.0/10	285.8 7.4/18	286.5 6.7/20	287.2 6.0/30	286.6 6.6/40
		287.8 5.4/30	287.2 6.0/20	286.8 6.4/10	286.3 6.9	286.0 7.2/10	285.5 7.7/20	285.4 7.8/30	285.2 8.0/40	
290.77 2.39/80	289.37 3.79/55	288.07 5.09/30	287.65 5.51/20	287.12 6.04/10	286.69 6.47	286.31 6.85/10	285.93 7.23/10	285.51 7.65/30	284.49 8.67/55	283.52 9.64/80

293.16

Wunderlin Ave.

3+50				
3+0				
TP	3.52	288.34	3.26	284.82
2+50				
2+0	30.0 Rt of ℄ = E'ly Wire Fence ✓			
1+94	20.2 Rt of ℄ = S'ly 10" Pepper Tree ✓			
1+69	19.8 Rt of ℄ = S'ly 4" Pepper Tree ✓			
1+50				
1+49	20.4 Rt of ℄ = S'ly Power Pole ✓			
TP	3.26	288.08	8.34	284.82
1+19	20.2 Rt of ℄ - S'ly 14" Pepper Tree ✓			
1+14	21.0 Lt of ℄ = N'ly 30" Euc. Tree ✓			
1+0				
		293.16		

Lt. ℄ Rt.

	1	2	3	4	5	6	7	8	9	10	11
3+50		286.1 / 2.2 / 30	285.1 / 3.2 / 20	283.7 / 4.6 / 12	283.7 / 4.6	283.6 / 4.7 / 7	283.9 / 4.4 / 9	283.1 / 5.2 / 12	282.7 / 5.6 / 20	282.2 / 6.1 / 30	281.8 / 6.5 / 40
3+0		285.0 / 3.3 / 30	284.0 / 4.3 / 20	283.4 / 4.9 / 11	283.1 / 5.2	282.7 / 5.6 / 9	283.0 / 5.3 / 11	281.8 / 6.5 / 20	281.4 / 6.9 / 30	280.8 / 7.5 / 40	
					288.34						
2+50		284.7 / 3.4 / 30	284.0 / 4.1 / 20	283.6 / 4.5 / 14	283.0 / 5.1 / 9	282.7 / 5.4	282.5 / 5.6 / 10	282.8 / 5.3 / 12	281.7 / 6.4 / 20	281.1 / 7.0 / 30	280.6 / 7.5 / 40
2+0		284.6 / 3.5 / 30	283.8 / 4.3 / 20	283.5 / 4.6 / 14	283.0 / 5.1 / 8	282.9 / 5.2	282.7 / 5.4 / 11	282.9 / 5.3 / 13	281.9 / 6.2 / 20	281.5 / 6.6 / 30	280.9 / 7.2 / 40
1+50	286.0 / 2.1 / 30	285.1 / 3.0 / 30	284.8 / 3.3 / 20	284.7 / 3.4 / 14	283.6 / 4.5 / 8	283.5 / 4.6	283.2 / 4.9 / 12	283.4 / 4.7 / 14	282.9 / 5.2 / 20	282.5 / 5.6 / 30	281.5 / 6.6 / 40
					288.08						
1+0		287.0 / 6.2 / 30	286.2 / 7.0 / 20	286.0 / 7.2 / 14	285.0 / 8.2 / 9	284.9 / 8.3	284.5 / 8.7 / 10	284.5 / 8.7 / 15	284.1 / 9.1 / 20	283.8 / 9.4 / 30	283.4 / 9.8 / 40
					293.16						

6+35				
6+09	14.0 Rt of ℄ = Sly Power Pole			✓
6+00				
TP	6.54	294.45	0.43	287.91
5+50				
5+37	22.0 Lt of ℄ = Sly 10" Olive Tree			✓
5+00				
4+63	21.5 Lt of ℄ = Sly 8" Olive Tree			✓
4+50				
4+00				
		288.34		

Lt ℄ Rt

293.0	291.9	290.4	289.3	288.5	287.9	287.0	285.8
1.5	2.6	4.0	5.2	6.0	6.6	7.5	8.7
3.0	4.0	4.0		6.0	7.0	8.0	9.0
291.0	290.0	288.7	288.5	288.1	288.4	287.4	287.3	287.1
3.5	4.5	5.8	6.0	6.4	6.1	7.1	7.3	7.4
3.0	4.0	6.0		7.0	7.0	8.0	9.0	9.0

294.45

288.6	287.0	285.4	285.1	284.7	285.1	284.4	283.4	282.4	281.8
3.0	4.0	5.7	6.2	6.6	6.2	6.9	7.9	8.9	9.5
3.0	4.0	11		6	8	13	13	13	14
285.3	284.3	283.0	282.5	282.5	282.9	280.4	279.9	278.6	
3.0	4.0	6.3	6.8	6.8	6.4	7.9	8.4	9.7	
3.0	4.0	16		6	7	14	13	14	
284.1	282.9	282.9	282.5	282.0	281.9	282.7	281.6	280.8	280.2	279.8
3.3	5.4	5.4	6.8	6.2	6.4	6.6	6.7	7.5	8.1	8.5
3.0	4.5	4.0	16		4	6	10	13	13	14
285.7	285.3	283.9	283.5	283.0	283.3	282.6	282.5	282.3	282.4
2.6	3.0	4.9	4.8	5.2	5.0	5.7	5.8	6.0	5.9
3.0	4.0	15		6	8	11	13	13	14

288.34

Hunderlin Ave.

TP	0.29	271.37	11.92	271.08
8+02		216 Rt of Z - Sly Power Pole		✓
8+0				
7+70				
TP	0.57	282.00	12.02	282.43
7+35				
7+06				
7+0				
6+70				
		294.15		

Lt. Z Rt

Lt.				Z			Rt		
274.8	274.1	273.3	271.8	271.3	269.7	269.0	268.1		
8.2	8.9	9.7	11.2	11.7	13.3	14.0	14.9		
30	20	10		10	20	30	40		
279.0	278.1	277.1	276.3	275.5	274.4	273.6	272.9		
4.0	4.9	5.9	6.7	7.5	8.6	9.4	10.1		
30	20	10		10	20	30	40		
			282.00						
284.1	283.9	282.4	281.7	280.4	279.9	279.2	277.7		
10.4	11.6	13.1	13.8	14.1	14.6	15.3	16.8		
30	20	10		10	20	30	40		
287.8	287.1	286.9	285.4	283.9	282.8	281.3	280.3		
6.7	7.4	7.6	9.1	10.6	11.7	13.2	14.2		
30	20	10		10	20	30	40		
290.3	288.5	287.7	286.9	286.5	284.9	283.3	282.1	280.9	
4.7	6.0	6.8	7.6	8.0	9.6	11.2	12.4	13.6	
30	25	20	15		10	20	30	40	
292.1	291.0	289.7	288.1	287.0	286.9	286.6	285.5	284.1	
3.4	4.5	5.8	7.4	8.5	7.6	7.9	9.0	10.4	
30	20	10		10	20	25	30	40	
			294.15						

9+70					
9+65					
TP	5.25	252.57	12.03	247.32	
9+35					
9+0					
TP	0.70	259.35	12.22	259.15	
8+65					
8+35					
		271.37			

Lt Ct Rt

246.5	246.9	247.0	247.0	246.8	246.6	246.4	245.5	245.2
6.1	5.7	5.6	5.6	5.8	6.0	6.2	7.1	7.4
40	30	20	10		10	20	30	40
247.6	248.4	248.0	248.0	247.1	246.8	246.5	246.1	246.1
5.0	4.2	4.6	4.6	5.5	5.8	6.1	6.5	6.5
40	30	20	10		10	20	30	45
				252.57				
252.8	251.7	250.5	249.8	249.1	248.4	247.8	247.2	246.0
6.6	7.7	8.9	9.6	10.3	11.0	11.6	12.2	13.4
40	30	20	10		10	20	30	45
258.9	256.0	254.9	254.1	251.9	250.3	249.2	248.0	246.9
0.5	3.4	4.5	5.3	7.5	9.1	10.2	11.4	12.5
30	20	16	10		10	20	30	45
				259.35				
265.4	265.0	264.0	261.7	260.0	258.6	257.9	258.6	
6.0	6.4	7.4	9.7	11.4	12.8	13.5	14.8	
30	20	10		10	20	30	20	
269.5	268.2	267.7	267.0	265.9	265.0	263.7	262.9	
1.9	3.2	3.7	4.4	5.5	6.4	7.7	8.5	
30	20	10		10	20	30	40	
				271.37				

Wunderlin Ave.

Station						Lt				℄				Rt.
BM	5.09	247.48	℄ Mon Wunderlin + Modera 247.49											
10+01.93 = W.L Modera on ℄ Wunderlin on Diag.						248.9 3.7/38.7	249.1 3.5/25.8	249.7 2.9/12.9		247.9 4.7	247.2 5.4/12.9	245.8 6.8/25.8	244.5 8.1/38.7=SL	
9+90				247.5 5.1/40	247.5 5.1/30	246.9 5.7/20	247.0 5.6/10			246.6 6.0	246.5 6.1/10	246.0 6.6/20	246.3 6.3/30	245.6 7.0/40
9+83 = Ely of Wash				247.1 5.5/40	246.0 6.6/30	245.3 7.3/20	245.0 7.6/10			244.5 8.1	244.3 8.3/10	244.4 8.2/20	244.6 8.0/30	245.1 7.5/45
9+75 = Wly + Bottom of Wash				244.9 7.7/40	245.8 6.8/30	245.3 7.3/20	245.0 7.6/10			244.9 7.7	244.2 8.4/10	243.6 9.0/20	243.8 8.8/30	243.7 8.9/50

252.57

252.57

Moore Road 1-5-42.

Xsec 39th St 60' wide 10' curbs 10' 1/4"

Hilltop to F St.

B.M. & Pipe	2.37	(173.50)		(171.13)	Hilltop & Quail
S.L. Hilltop = 0+0					
E			6.0	167.5	
c6			6.4	167.1	
1/4			6.3	167.2	
c			5.7	167.8	
1/4			5.2	168.3	
+5			5.9	167.6	
c6			5.0	168.5	
W			3.3	170.2	
	0+50				
W			7.0	166.5	
c6			9.1	164.4	
1/4			9.4	164.1	
c			9.6	163.9	
1/4			9.8	163.7	
c6			9.5	164.0	
E			9.4	164.1	
	1+00				
E			13.7	160.3	
c6			13.3	160.2	
1/4			13.2	160.3	
c			13.1	160.4	

Red T-Plot on Profile # 2436 1-6-42 <B.M.

Indexed C.S.K. 173.50

1/4			13.2	160.3
c6			12.6	160.9
W			11.2	162.3
T.P.	0.69	161.14	13.05	160.45
	1+50			
W			2.8	158.3
c6			3.4	157.7
1/4			4.3	156.8
c			4.3	156.8
1/4			4.5	156.6
c6			4.6	156.5
E			4.6	157.5
	2+00			
E			7.4	153.7
c6			7.8	153.3
1/4			7.8	153.3
c			7.5	153.6
1/4			7.7	153.4
c6			7.0	154.1
W			6.1	155.0
	2+07			
W. 7 3' conc. steps up			6.37	154.82 Bot. Step

39th 16.14

	2+50			
W'			8.2	152.9
cb			9.2	151.9
1/4			9.9	151.2
C			10.0	151.1
1/4			10.3	150.8
cb			10.2	150.9
E			10.0	151.1
	3+00			
E			11.6	149.5
cb			11.3	149.8
1/4			11.3	149.8
C			11.3	149.8
1/4			11.0	150.1
cb			10.6	150.5
W'			10.0	151.1
	3+50			
W'			11.3	149.8
cb			11.6	149.5
1/4			12.1	149.0
C			12.3	148.8
1/4			12.1	149.0
cb			12.2	148.9
E			11.6	149.5
T.P.	1.62	150.30	12.46	148.68

150.30 39th 49

149.83

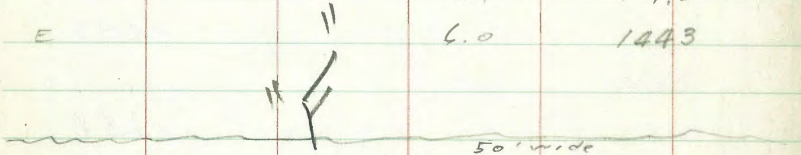
	3+72		
W'	& 3.2 cent. steps up	0.47	Bot. Step
	3+89		
E	& 0.62 cent. walk	1.93	148.37
	4+00		
E		2.3	148.0
cb		2.3	148.0
1/4		2.1	148.2
C		2.0	148.3
1/4		2.1	148.2
cb		1.7	148.6
W'		1.0	149.3
	4+50		
W'		1.9	148.4
cb		2.6	147.7
1/4		2.9	147.4
C		2.9	147.4
1/4		3.0	147.3
cb		3.1	147.4
E		3.4	146.9
+10		5.8	144.5
	5+00		
-10		7.3	147.0
E		4.3	146.0
cb		3.9	146.4
1/4		4.0	146.3

39th

150.30

39 7th

C	3.C	146.7
1/4	3.C	146.7
cb	3.5	146.8
W	3.0	147.3
5+59.8 = N.L. F ST.		
W	3.7	146.6
cb	4.4	145.9
1/4	4.C	145.7
C	4.8	145.5
1/4	5.4	144.9
C	5.7	144.6
E	C.0	144.3



50' wide
10' cbs
7.5 1/4 =

X sec of F ST.

Quail to Sidney

W.L. Quail = 0+00 See 1608

Same H.L.

0+35

Reduced & Plotted 1-6-42 CBH

S	7.4	143.1
cb	C.8	143.5
+5	7.4	143.1
1/4	8.4	141.9
C	8.5	141.8
1/4	8.4	141.9
cb	8.4	141.9
+6	8.4	142.1
N/	7.6	142.7

150.30

50

0+60

N/	8.4	141.9
cb	8.8	141.5
1/4	8.7	141.6
C	8.C	141.7
+5	5.5	144.8
1/4	5.4	145.2
cb	5.8	144.5
S	7.1	143.2

1+00

-10	9.9	140.4
S	9.C	140.7
cb	9.0	141.3
1/4	9.0	141.3
C	9.4	140.9
1/4	9.4	140.9
cb	9.4	141.1
N/	9.0	141.3

1+25.

N/	9.4	140.9
cb	9.4	140.9
1/4	9.5	140.8
C	9.C	140.7
+3	10.4	140.1
1/4	11.3	139.0
cb	12.0	138.3

S		150.30	12.7	137.6
+10			13.1	137.2
	1+50			
-10			13.1	137.2
S			12.6	137.7
c6			11.9	138.4
1/4			11.7	138.6
C			11.2	139.1
1/4			9.8	140.5
c6			9.6	140.7
N			9.6	140.7
+10			9.7	140.6
	1+68			
-10			11.1	139.2
-6	Fl. inlet 12" Conc. pipe this C.M.P. should be longer		12.98	137.32
N			9.5	140.8
c6			9.5	140.8
1/4			9.8	140.5
+3			10.8	139.5
	Sta. 1+67			
C	Fl. outlet		13.5	136.8
C			11.2	139.1
1/4			11.8	138.5
c6			12.8	137.5
S			13.2	137.1
+10			13.5	136.8
	7+00			
-10			12.5	137.8

S		12.1	138.2
c6		11.6	138.7
1/4		10.8	139.5
C		10.0	140.3
+3		9.7	140.6
1/4		8.7	141.6
c6		9.0	141.3
N		8.7	141.6
+10		10.4	139.9
	7+30		
-10		9.4	140.9
-5		7.4	1429
N		7.2	1431
c6		7.5	142.8
1/4		7.4	142.9
+2		7.5	142.8
C		8.6	141.7
1/4		9.4	140.9
-6		10.8	139.5
S		11.1	139.2
+10		11.4	138.9
	8+65 E.L. 39TH		
-10		8.0	142.3
S		7.7	142.6
c6		7.8	142.5
1/4		8.0	142.3

150.30

c		7.8	142.5
1/4		7.0	143.3
+ r		5.8	144.5
N c6		5.C	143.7
	E 39+h		
N c6		4.8	145.5
1/4		4.8	145.5
c		5.0	145.3
1/4		5.0	145.3
c6		5.C	144.7
S		5.8	144.5
+10		5.5	144.8
	W.L 39+h = 0+00 on N.L.F.ST.		
S		7.3	148.0
c6		7.3	148.0
1/4		7.6	147.7
c		3.3	147.0
1/4		3.9	146.4
N c6		4.0	146.3
T.P.	8.50	157.10	1.70	148.60
	0+35 at 90°		
- S		3.7	153.4
N'		6.3	150.8
c6		8.0	149.1

157.10

1/4		8.7	148.9
c		7.4	149.7
1/4		5.7	151.4
c6		6.0	151.1
S		6.5	150.6
	0+73.47 E.L. Bdry. or angle		
S		4.1	153.0
c6		3.6	153.5
1/4		2.9	154.2
C		3.7	153.4
1/4		4.8	152.3
c6		4.3	152.8
N'		2.8	154.3
	W.L Bdry 25.5 on angle		
N'		2.2	154.9
c		2.6	154.5
S		3.2	153.9
T.P.	3.40	148.08	12.44	144.68

check to B.M. B.F. So. Curb of 8 r 1 = 139.87 139.9r

Market & old City Line

Brass plug is out, lead still in place

52

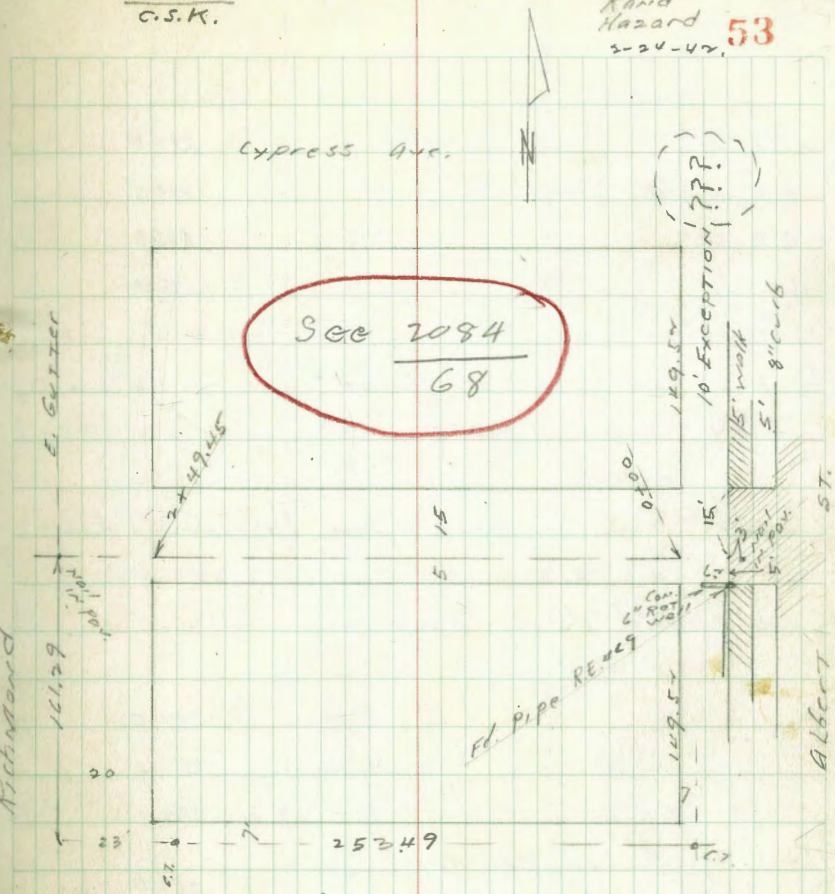
Indexed
C.S.K.

Moore
Rand
Hazard
3-24-47.

53

Xsec alley 20' wide
Blk 231 Univ. Hts.

NEBP	11.83	291.14	280.31	Cypress Albert
	0-70 W. cut. on Albert			
N pav.		6.81	285.33	
S "		6.50	285.64	
	0-10			
S c6		5.58	286.56	
S pav		5.97	286.17	
C "		6.19	285.95	
N "		6.08	286.06	
N c6		5.94	286.20	
	0-6			
S+r 6eq. Cypress hedge				3' in alley
	0-3.8			
N		5.1	286.9	
C		5.5	286.6	
S Bot. wall		3.5	288.6	
S Top "		3.1	289.0	
	0+00 W L Albert. Please check this closing.			for
S		3.3	288.8	
C		5.1	287.0	
N		4.7	287.4	



Reduced + Plotted
2-26-1941
C.B.K.
Tie point 336

	0+37			
N		4.4	287.7	
+N	10" Tel. P.	3.8	288.3	
C		3.8	288.3	
S		3.7	288.4	
	0+47			
S +3	End Cypress hedge			3' in alley
S −1.4	N.E. Cor. porch			
	0+56			
S −1.7	NW Cor. porch & beg. Lattice fence			
	0+72.7			
S −0.5	end Lat. fence			
	0+74			
S		4.5	287.6	
C		4.7	287.4	
N		5.0	287.1	
+1.7	SE. Cor Bd. gar.		287.0	E. entrance
+7.3	E gar dirt fl.	5.1		
	0+75.5			
S −3.6	EL. do. gar.	4.57	287.57	Conc. fl.
	0+90.5			
S −3.6	W.h. do. g	4.60	287.54	
	0+95.5			
S −3.4	EL. do. gar.	5.34	286.82	

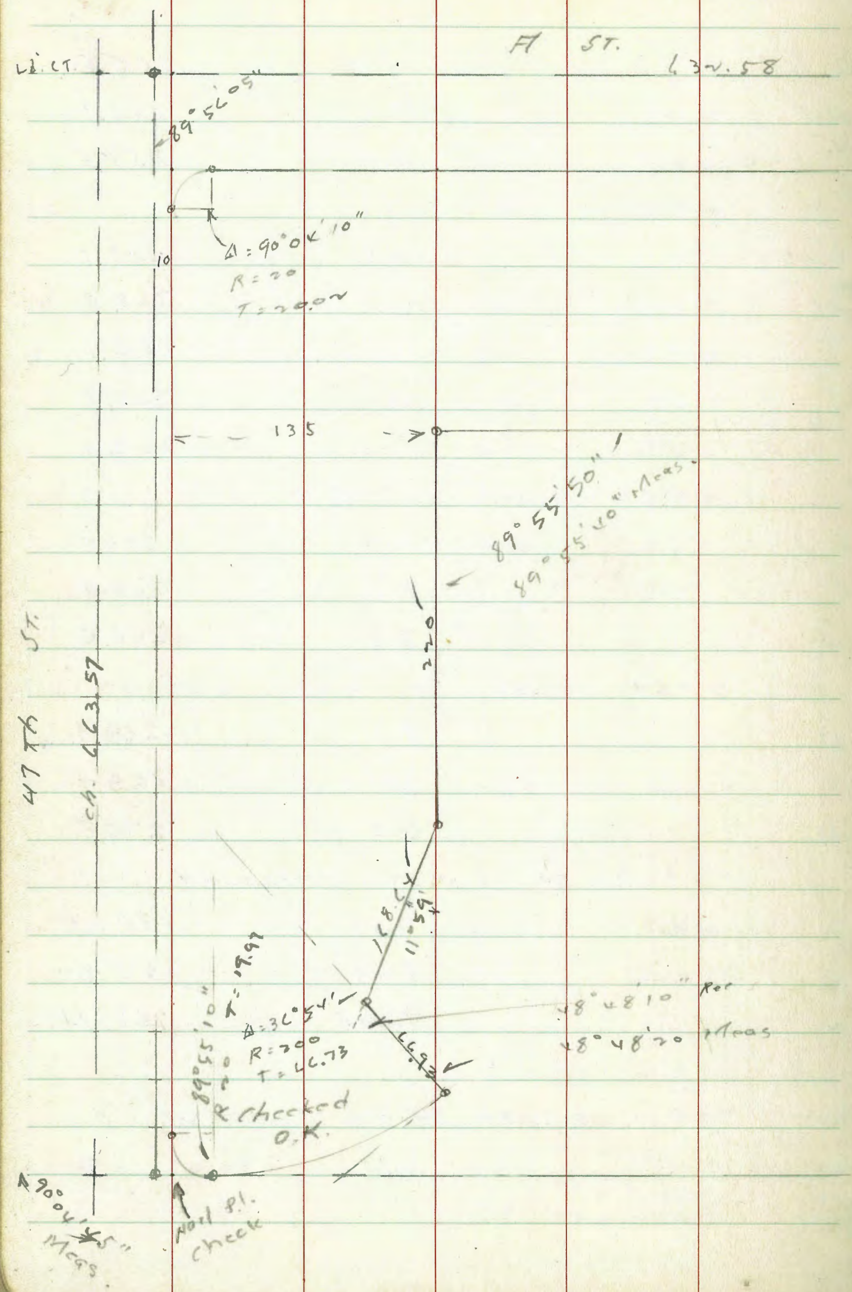
	1+00		
N		5.9	286.2
C		5.8	286.3
S		5.7	286.4
	1+10.3		
S −3.4	W.h. do. gar.	5.33	286.81 Conc. fl.
	1+14		
S −3.4	EL. Sin. gar.	5.80	286.34
	1+21		
S −3.4	W.h. " "	5.84	286.30
	1+25.5		
S	16" P.P.	6.6	285.5
C		7.0	285.1
N		7.5	284.6
T.P.	1.40	=87.79	6.45	=85.89
	1+37		
S −4.8	EL. Sin. gar.	4.44	285.07
	1+47		
S −4.8	W.h. " "	4.48	285.01
	1+53.5		
S on line	NE Cor porch	3.1	284.2 on ground Won't stand much cut here
	1+67		
S −0.4	NW Cor porch and beg. Lat. fence	4.0	283.3

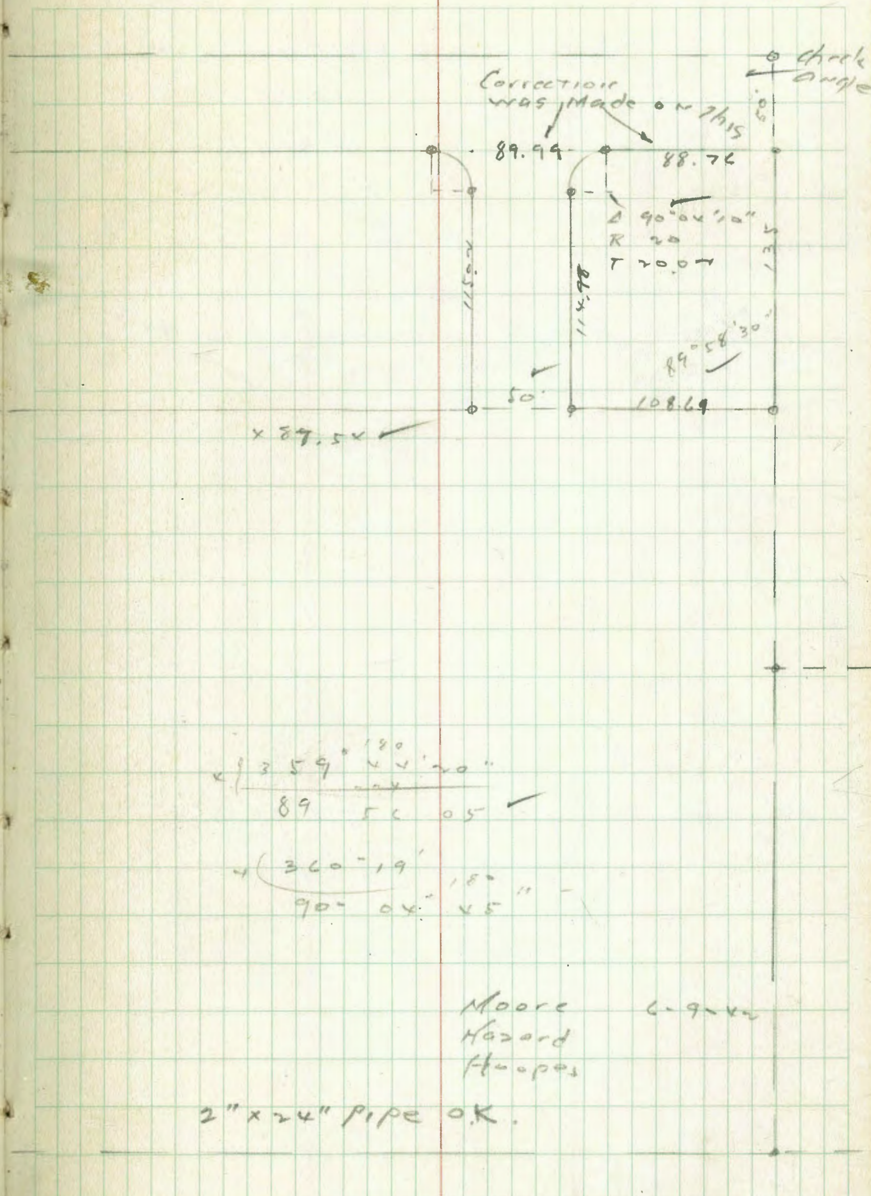
		287.29			
	1+75				
-15			10.1	277.2	
N			6.4	280.9	
C			5.1	282.2	
S			4.3	283.0	
	2+00				
S-3			5.1	282.2	
S-1			5.1	282.2	
S			6.4	280.9	
C			7.7	279.6	
+5			8.1	278.2	
N			12.0	275.3	
+15			15.2	272.1	
	2+07				
S-1.5	End fence ✓				
T.P.	2+60	277.36	12.53	274.76	
	2+75				
-15			11.1	266.3	
N			7.6	269.8	
C			4.7	272.7	
S			4.1	273.3	
	2+49.45 EL. Richmond				
-5			4.3	271.1	
S			8.8	268.6	

277.36

C		10.9	266.5
N		13.3	264.1
	+75	18.9	258.5
	2+57		
-15		14.3	263.1
N		13.6	263.8
C		12.0	265.4
S		9.7	267.7
	+5	7.5	269.9
	2+66 = cm6. on 4.11		
S		7.1	270.3
C		8.0	269.4
N		8.8	268.6
	2+69 = cm6.		
N		8.1	269.3
C		7.7	269.7
S		6.6	270.8
	2+69.45 = E. gut. Richmond		
S	on pav	7.26	270.10
C	" "	8.28	269.07
N	" "	9.22	268.14
T.P.	3.86	281.18	0.04 277.32
check to BM1		1.13	280.05 280.04
SE Cor. Myrtle Richmond			0.01

Check Survey, Lyons Park





Check Survey
Victory Manor

Moore
Hazard
Hoopes
6-10-42.

Indexed
C.S.H.

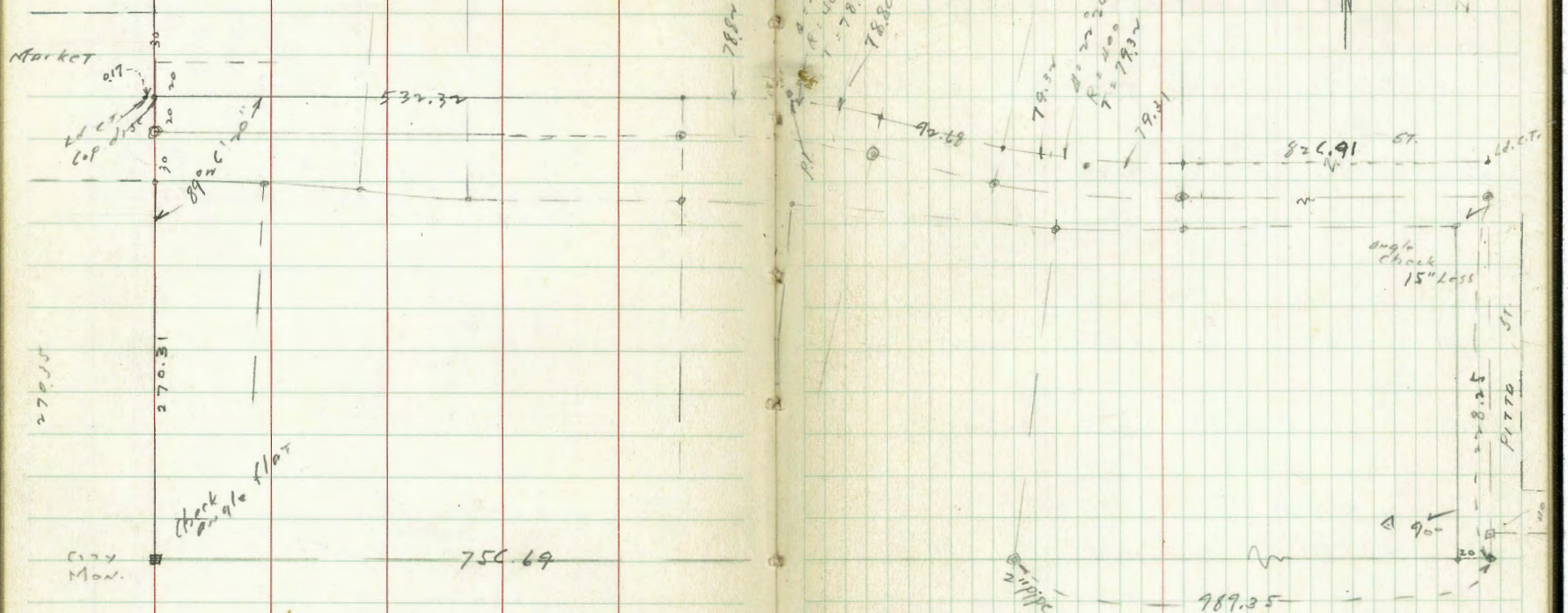
57

⊙ = 2" Pipes ⇒ 4"

• = Fd. Ld. CT.

• 3/4" pipe

Note! Ld. & CT. in pav. will shift during Expansion in course of 15 years



46th = 60' Sdw. 15 - Rdy 30 — C S [illegible] 12-21-45

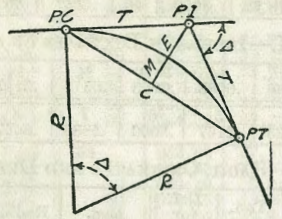
Levels on 46th at Wightman

	3.48	351.41		347.93	Wightman Chamarre
NWEP	5.06	349.06	7.41	344.60	
	NC Wightman = 00				
cb			5.11		
gt			5.62		
	2 + 00				
cb			2.85		
gt			3.36	345.70	✓
	2 + 50				
cb			2.24		
gt			2.83	346.23	
T.P.	5.16	351.15	3.07	345.99	
	2 + 50				
W L 46th			4.91		Con dr
40' W of W L 46th			4.99		" "
80' W " "			5.09		" Sdw
110 W " "			5.19	345.96	" "
110 W " "			4.72		Bot. Step
125 " " "			4.26		alley alley
135 " " "			4.62		Ealley
25' S of 95 W			5.4		
50' " " "			5.6		

351.15

25' N of 70' W of 46th	4.11	347.04	Con
15 N of 68 " "	4.47		
On Stokey	4.7	346.45	
50' N of 68	4.4	346.75	

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES



CURVE FORMULAS

Radius=R=$\frac{50}{\text{sin. } D/2}$ (1) Degree of Curve=D and sin. $\frac{D}{2}=\frac{50}{R}$ (2)

Tangent=T=Rtan$\frac{\Delta}{2}$ (3) Length of Curve=L=100$\frac{\Delta}{D}$ (4)

Middle ordinate=M= R(1—cos. $\frac{\Delta}{2}$) (5) =Rvers $\frac{\Delta}{2}$ (6)

External=E=Ttan$\frac{\Delta}{4}$- (7) =R÷cos.$\frac{\Delta}{2}$—R (8)=Rexsec$\frac{\Delta}{2}$ (9)

Long Chord=C=2 R sin.$\frac{\Delta}{2}$ (10) Δ=Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161 +60.35 to find Sta. of P. C. and P. T. Δ=62° 10′ D=8° 20′. From Table IV for 1° curve T=3454.1 and÷8⅓=414.49 ft. From Table V correction=.36 or T=414.85 ft. P. C.=Sta. P.I.—T=157 +45.50. Also from (4) L=746.00 and P. T.=Sta. P. C. +L=164 +91.50.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset=7.27 (54.50÷100)²=2.16 ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus (54.50)²÷(2 x 688.26)=2.16 ft.

Deflections.—Deflection angle=½ D for 100 ft., ¼ D for 50 ft., etc. For c ft.=(in minutes) .3 x C x D° or=defl. for 1 ft. from Table III x C. For Sta. 158 of above curve=.3 x 54.5 x 8⅓=136.2′ or 2° 16.2′, or=2.50 x 54.5=136.2′ from Table III. For Sta. 159 deflection angle=2° 16.2′ +8° 20′÷2=6° 26.2′, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve E=960.6 for 8° 20′=960.6÷8⅓=91.27 and from Table V correction=.10 or E=91.37 ft. Or suppose Δ=32° and E is measured and found to be 42 ft. What is D? From Table IV E=230.9 and÷42=5.5 or D=5° 30′.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20—16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

MADE IN U.S.A.