

1617

WATER

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EXHIBITS

LEVEL BOOK

No. 413

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# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and

**MICROFORMING INSTRUMENTS**

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 10 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

# 1617

| H  | 0    | .1   | .2   | .3   | .4   | .5   | .6   | .7   | .8   | .9   | H  |
|----|------|------|------|------|------|------|------|------|------|------|----|
| 0  | 8.0  | 8.1  | 8.2  | 8.3  | 8.4  | 8.5  | 8.6  | 8.7  | 8.8  | 8.9  | 0  |
| 1  | 9.0  | 9.1  | 9.2  | 9.3  | 9.4  | 9.5  | 9.6  | 9.7  | 9.8  | 9.9  | 1  |
| 2  | 10.0 | 10.1 | 10.2 | 10.3 | 10.4 | 10.5 | 10.6 | 10.7 | 10.8 | 10.9 | 2  |
| 3  | 11.0 | 11.1 | 11.2 | 11.3 | 11.4 | 11.5 | 11.6 | 11.7 | 11.8 | 11.9 | 3  |
| 4  | 12.0 | 12.1 | 12.2 | 12.3 | 12.4 | 12.5 | 12.6 | 12.7 | 12.8 | 12.9 | 4  |
| 5  | 13.0 | 13.1 | 13.2 | 13.3 | 13.4 | 13.5 | 13.6 | 13.7 | 13.8 | 13.9 | 5  |
| 6  | 14.0 | 14.1 | 14.2 | 14.3 | 14.4 | 14.5 | 14.6 | 14.7 | 14.8 | 14.9 | 6  |
| 7  | 15.0 | 15.1 | 15.2 | 15.3 | 15.4 | 15.5 | 15.6 | 15.7 | 15.8 | 15.9 | 7  |
| 8  | 16.0 | 16.1 | 16.2 | 16.3 | 16.4 | 16.5 | 16.6 | 16.7 | 16.8 | 16.9 | 8  |
| 9  | 17.0 | 17.1 | 17.2 | 17.3 | 17.4 | 17.5 | 17.6 | 17.7 | 17.8 | 17.9 | 9  |
| 10 | 18.0 | 18.1 | 18.2 | 18.3 | 18.4 | 18.5 | 18.6 | 18.7 | 18.8 | 18.9 | 10 |
| 11 | 19.0 | 19.1 | 19.2 | 19.3 | 19.4 | 19.5 | 19.6 | 19.7 | 19.8 | 19.9 | 11 |
| 12 | 20.0 | 20.1 | 20.2 | 20.3 | 20.4 | 20.5 | 20.6 | 20.7 | 20.8 | 20.9 | 12 |
| 13 | 21.0 | 21.1 | 21.2 | 21.3 | 21.4 | 21.5 | 21.6 | 21.7 | 21.8 | 21.9 | 13 |
| 14 | 22.0 | 22.1 | 22.2 | 22.3 | 22.4 | 22.5 | 22.6 | 22.7 | 22.8 | 22.9 | 14 |
| 15 | 23.0 | 23.1 | 23.2 | 23.3 | 23.4 | 23.5 | 23.6 | 23.7 | 23.8 | 23.9 | 15 |
| 16 | 24.0 | 24.1 | 24.2 | 24.3 | 24.4 | 24.5 | 24.6 | 24.7 | 24.8 | 24.9 | 16 |
| 17 | 25.0 | 25.1 | 25.2 | 25.3 | 25.4 | 25.5 | 25.6 | 25.7 | 25.8 | 25.9 | 17 |
| 18 | 26.0 | 26.1 | 26.2 | 26.3 | 26.4 | 26.5 | 26.6 | 26.7 | 26.8 | 26.9 | 18 |
| 19 | 27.0 | 27.1 | 27.2 | 27.3 | 27.4 | 27.5 | 27.6 | 27.7 | 27.8 | 27.9 | 19 |
| 20 | 28.0 | 28.1 | 28.2 | 28.3 | 28.4 | 28.5 | 28.6 | 28.7 | 28.8 | 28.9 | 20 |
| 21 | 29.0 | 29.1 | 29.2 | 29.3 | 29.4 | 29.5 | 29.6 | 29.7 | 29.8 | 29.9 | 21 |
| 22 | 30.0 | 30.1 | 30.2 | 30.3 | 30.4 | 30.5 | 30.6 | 30.7 | 30.8 | 30.9 | 22 |
| 23 | 31.0 | 31.1 | 31.2 | 31.3 | 31.4 | 31.5 | 31.6 | 31.7 | 31.8 | 31.9 | 23 |
| 24 | 32.0 | 32.1 | 32.2 | 32.3 | 32.4 | 32.5 | 32.6 | 32.7 | 32.8 | 32.9 | 24 |
| 25 | 33.0 | 33.1 | 33.2 | 33.3 | 33.4 | 33.5 | 33.6 | 33.7 | 33.8 | 33.9 | 25 |
| 26 | 34.0 | 34.1 | 34.2 | 34.3 | 34.4 | 34.5 | 34.6 | 34.7 | 34.8 | 34.9 | 26 |
| 27 | 35.0 | 35.1 | 35.2 | 35.3 | 35.4 | 35.5 | 35.6 | 35.7 | 35.8 | 35.9 | 27 |
| 28 | 36.0 | 36.1 | 36.2 | 36.3 | 36.4 | 36.5 | 36.6 | 36.7 | 36.8 | 36.9 | 28 |
| 29 | 37.0 | 37.1 | 37.2 | 37.3 | 37.4 | 37.5 | 37.6 | 37.7 | 37.8 | 37.9 | 29 |
| 30 | 38.0 | 38.1 | 38.2 | 38.3 | 38.4 | 38.5 | 38.6 | 38.7 | 38.8 | 38.9 | 30 |
| 31 | 39.0 | 39.1 | 39.2 | 39.3 | 39.4 | 39.5 | 39.6 | 39.7 | 39.8 | 39.9 | 31 |
| 32 | 40.0 | 40.1 | 40.2 | 40.3 | 40.4 | 40.5 | 40.6 | 40.7 | 40.8 | 40.9 | 32 |
| 33 | 41.0 | 41.1 | 41.2 | 41.3 | 41.4 | 41.5 | 41.6 | 41.7 | 41.8 | 41.9 | 33 |
| 34 | 42.0 | 42.1 | 42.2 | 42.3 | 42.4 | 42.5 | 42.6 | 42.7 | 42.8 | 42.9 | 34 |
| 35 | 43.0 | 43.1 | 43.2 | 43.3 | 43.4 | 43.5 | 43.6 | 43.7 | 43.8 | 43.9 | 35 |
| 36 | 44.0 | 44.1 | 44.2 | 44.3 | 44.4 | 44.5 | 44.6 | 44.7 | 44.8 | 44.9 | 36 |
| 37 | 45.0 | 45.1 | 45.2 | 45.3 | 45.4 | 45.5 | 45.6 | 45.7 | 45.8 | 45.9 | 37 |
| 38 | 46.0 | 46.1 | 46.2 | 46.3 | 46.4 | 46.5 | 46.6 | 46.7 | 46.8 | 46.9 | 38 |
| 39 | 47.0 | 47.1 | 47.2 | 47.3 | 47.4 | 47.5 | 47.6 | 47.7 | 47.8 | 47.9 | 39 |
| 40 | 48.0 | 48.1 | 48.2 | 48.3 | 48.4 | 48.5 | 48.6 | 48.7 | 48.8 | 48.9 | 40 |

## CITY ENGINEER

The paper stock of this book is made of a high grade 50% rag paper having a water resisting surface and is sewed with Bing Special Enamel Waterproof Thread.

Made in U. S. A.

ENGINEERING DEPARTMENT,  
CITY OF SAN DIEGO,  
CALIFORNIA.

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \times 2$  or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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|                  |                      |         |
|------------------|----------------------|---------|
| Roswell ST.      | Market - Hilltop     | 3 - 20  |
| 51 <sup>ST</sup> | Roswell - North -    | 21 - 23 |
| Melrose          | r - South            | 24 - 28 |
| Hilltop          | r - 51 <sup>ST</sup> | 30 - 49 |

|                      |                   |         |
|----------------------|-------------------|---------|
| 70 <sup>TH</sup> ST. | fwd. from 1623-59 | 60 - 61 |
| 69 <sup>TH</sup> ST. |                   | 62 - 63 |
| 68 <sup>TH</sup> ST. |                   | 64 - 65 |
| Olive                |                   | 66 - 67 |
| 67 <sup>TH</sup>     |                   | 68 - 71 |

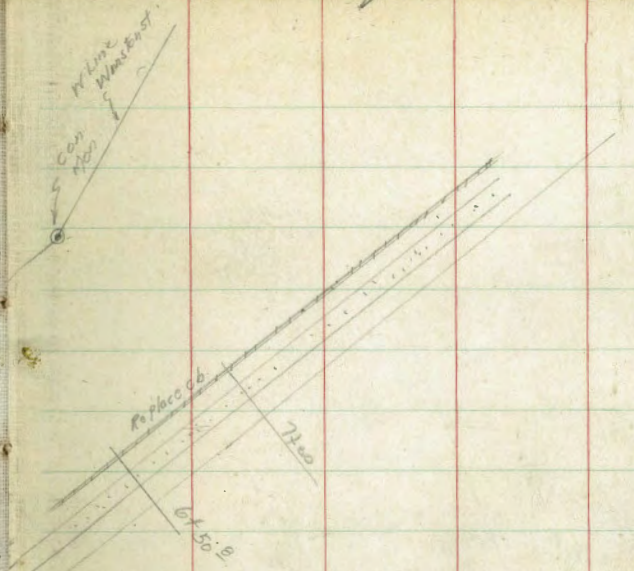
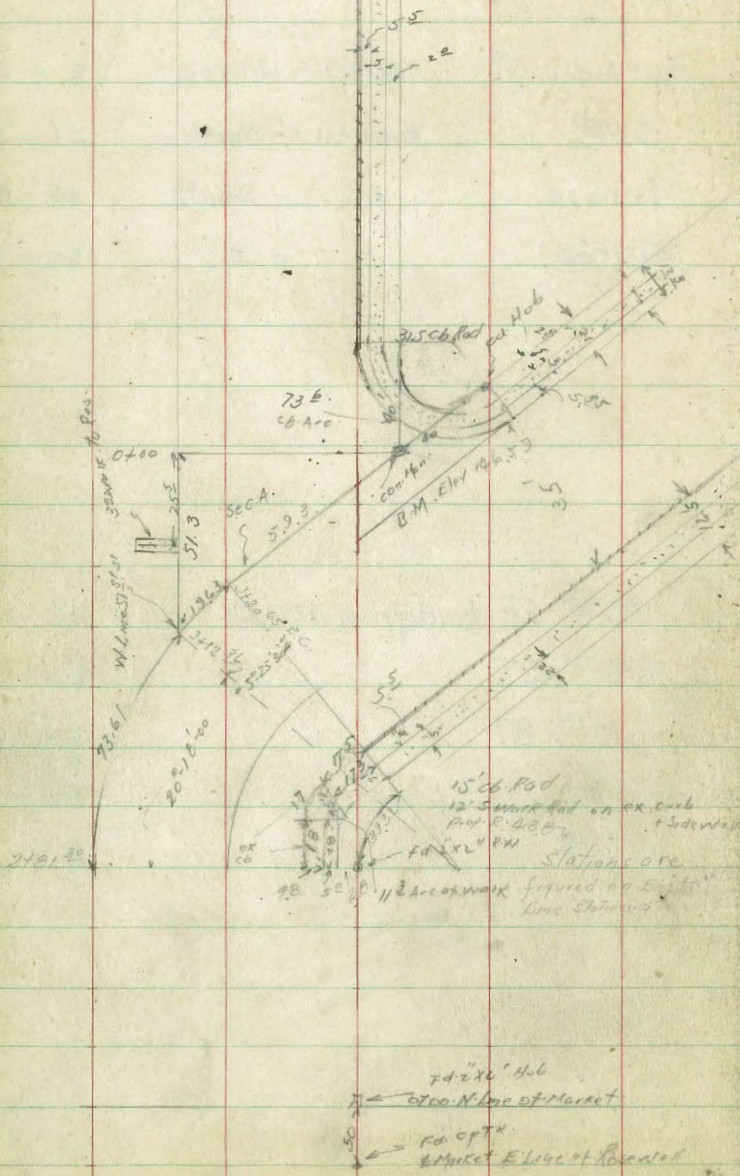
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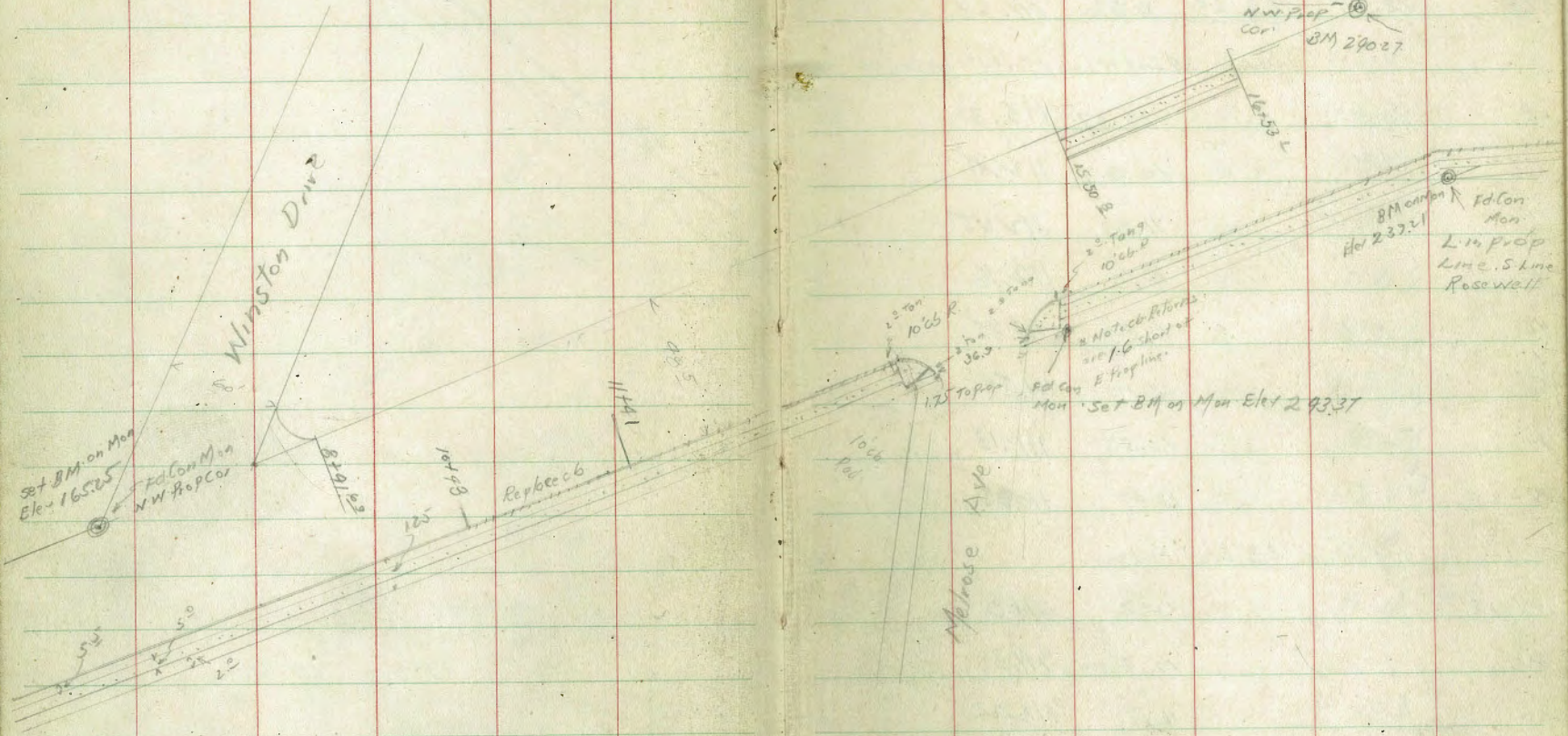
to be  
of roa  
exami  
30.6 =

78

1753 End C6

1769<sup>2</sup>  
Edmark





X Section Reswell St. from N. Line of

Market to W. Line of Hilltop Drive

B.M. 7.97 112.19 109.22

TP 12.95 123.68 0.56 111.63

Sec 35.5 of N. Line Market on Parking

E 10.37 113.31

cb 10.87 112.81

1/4 11.23 112.45

E 11.52 112.16

1/4 11.83 111.85

cb 12.10 111.58

N 12.55 111.13

N+25 13.43 110.25

Red. 10-31-41

28 S. of N. Line

W-25 12.7 111.0

W 12.4 111.3

cb 11.5 112.2

1/4 11.5 112.2

41 Note This Culvert runs 90°-00-00 to the E. of Marker

E Top culvert head wall 1097 112.71

Flow Line 18" pipe 14.47 109.21

1/4 10.7 113.0

60' St  
12 1/2 cbs  
5 1/4 1/4's  
B.P. N.W.  
Cor. Bldg 200'  
S. of Market on Field

Indexed  
LM

T  
123.68

cb 40 112.7

E 104 113.3

24'S

E 8.3 115.4

cb 9.7 114.0

1/4 10.3 113.4

+7 10.3 113.4

E 12.7 111.0

+2 12.7 111.0

+4 10.3 113.4

1/4 11.2 112.5

cb 11.3 112.4

N 12.2 111.5

+25 12.3 111.4

0+00 N. Line of Market

-25 11.4 112.3

N 10.5 113.2

+2 11.2 112.5

cb 10.6 113.1

1/4 9.9 113.8

T  
123.68

|                          |      |        |
|--------------------------|------|--------|
| +6                       | 10.7 | 113.0  |
| ±                        | 9.0  | 114.7  |
| 1/4                      | 7.6  | 116.1  |
| cb                       | 6.9  | 116.8  |
| E on 2 <sup>nd</sup> Hub | 7.83 | 118.85 |
| 0+25                     |      |        |
| E                        | 1.9  | 121.8  |
| cb                       | 4.5  | 119.2  |
| 1/4                      | 5.0  | 118.7  |
| 1/4                      | 5.5  | 118.2  |
| ±                        | 8.5  | 115.2  |
| 1/4                      | 8.7  | 115.0  |
| cb                       | 9.0  | 114.7  |
| +9                       | 9.8  | 113.9  |
| W                        | 9.0  | 114.7  |
| +5                       | 10.8 | 112.9  |
| +25                      | 10.2 | 113.5  |
| 0+50                     |      |        |
| -25                      | 8.3  | 114.8  |
| W                        | 7.3  | 116.4  |
| +4                       | 8.0  | 115.7  |

T  
123.68

4

|                                   |       |        |
|-----------------------------------|-------|--------|
| cb                                | 7.4   | 116.3  |
| 1/4                               | 7.2   | 116.5  |
| ±                                 | 7.0   | 116.7  |
| +4                                | 5.7   | 118.0  |
| 1/4                               | 5.1   | 118.6  |
| cb                                | 3.4   | 120.3  |
| E                                 | 1.3   | 122.4  |
| TP                                | 12.10 | 131.52 |
| 0+62 Telephone pole 17 W. E. line |       |        |
| 0+70                              |       |        |
| E                                 | 7.8   | 123.7  |
| +5                                | 8.8   | 122.7  |
| cb                                | 10.3  | 121.2  |
| +6                                | 12.8  | 118.7  |
| 1/4                               | 13.2  | 119.3  |
| ±                                 | 13.6  | 117.9  |
| 1/4                               | 13.3  | 118.2  |
| cb                                | 13.7  | 117.8  |
| +6                                | 14.0  | 117.5  |
| +7                                | 13.5  | 118.0  |
| W                                 | 13.5  | 118.0  |

T  
13152

0770

W+25 195 117.0

0785 T. pole Dead Man 17 W of E.L.M.

W-25 13.4 118.1

W 12.2 119.3

cb 12.6 118.9

1/4 12.3 119.2

2 12.4 119.1

+2 12.2 119.3

1/4 12.1 119.4

cb 11.7 119.8

E 8.4 122.1

1700

E 7.6 123.9

cb 10.6 120.9

+3 11.3 120.2

1/4 10.9 120.6

+3 10.6 120.9

+5 11.6 119.9

2 11.4 120.1

1/4 10.9 120.6

T  
13152

1700

cb 11.1

W 11.3 120.2

+25 9.6 121.9  
# Note Lot on West has  
been a barrel pit for 100 ft  
No more out on West

1725

W 8.8 122.7

cb 8.8 122.7

1/4 8.7 122.8

2 9.3 122.2

+5 9.7 121.8

+7 9.0 122.5

1/4 9.1 122.4

+5 8.6 122.9

cb 7.5 124.0

E 9.2 127.3

1750

E 0.8 130.7

cb 9.2 127.3

1/4 6.4 125.1

+6 7.9 123.6

2 7.4 124.1

5



T  
131.52

1750

|     |     |       |
|-----|-----|-------|
| 1/4 | 6.7 | 124.8 |
| cb  | 6.6 | 124.9 |
| W   | 6.6 | 124.9 |

1790

|      |       |                    |        |
|------|-------|--------------------|--------|
| W    | 3.2   | 128.3              |        |
| cb   | 3.0   | 128.5              |        |
| 1/4  | 3.4   | 128.1              |        |
| £    | 3.9   | 127.6              |        |
| +6   | 4.4   | 127.1              |        |
| 1/4  | 2.2   | 129.3              |        |
| T.P. | 12.61 | <u>144.03</u> 0.10 | 131.42 |
| cb   | 12.5  | 131.5              |        |
| E    | 8.3   | 135.7              |        |

2115

|     |      |       |
|-----|------|-------|
| E   | 6.3  | 137.7 |
| cb  | 10.0 | 134.0 |
| +7  | 11.0 | 133.0 |
| 1/4 | 13.5 | 130.5 |
| +1  | 14.2 | 129.8 |
| £   | 13.4 | 130.6 |

T  
144.03

6

|     |      |       |
|-----|------|-------|
| 1/4 | 13.3 | 130.7 |
| cb  | 13.2 | 130.8 |
| W   | 13.4 | 130.6 |

2187 Telephone Pole 2128327 20' W of E Line

2196 " D. Mon 20' W. + E Line

2150

|     |      |            |
|-----|------|------------|
| W   | 10.4 | 133.6      |
| cb  | 9.8  | 134.2      |
| 1/4 | 9.8  | 134.2      |
| £   | 10.3 | 133.7      |
| 1/4 | 11.0 | 133.0      |
| +5  | 8.3  | 135.7      |
| cb  | 7.7  | 136.3      |
| E   | 4.0  | 140.0      |
| E   | 7.04 | 2165 140.7 |
| cb  | 5.7  | 138.3      |
| +4  | 6.5  | 137.5      |
| +1  | 8.6  | 135.4      |
| 1/4 | 8.8  | 135.2      |

144.03

|     |     |       |
|-----|-----|-------|
| 8   | 8.3 | 135.7 |
| 1/4 | 8.1 | 135.9 |
| cb  | 8.2 | 135.8 |
| W   | 8.8 | 135.2 |

2+72<sup>E</sup> East Pokon West #7654 7' East Walk

2+91<sup>30</sup> 80' See sketch page 1

|                     |      |        |
|---------------------|------|--------|
| W                   | 6.3  | 137.7  |
| +5                  | 7.2  | 136.8  |
| cb                  | 6.8  | 137.2  |
| 1/4                 | 6.3  | 137.7  |
| 8                   | 6.7  | 137.3  |
| 1/4                 | 6.6  | 137.4  |
| +3                  | 6.4  | 137.6  |
| +5                  | 4.4  | 139.6  |
| Top cb              | 3.76 | 140.27 |
| cb on Sid           | 3.5  | 140.5  |
| +48 Edge ex walk    | 3.65 | 140.37 |
| " Ground            | 2.8  | 141.2  |
| +2.7 East Edge walk | 3.47 | 140.56 |
| " " Ground          | 3.2  | 140.8  |
| E on Top 2x 1/2     | 2.81 | 141.21 |

144.03

2+84 L Pok DM on 7' W of E Line

2+90

|                           |      |        |
|---------------------------|------|--------|
| E                         | 2.1  | 141.9  |
| +4                        | 3.0  | 141.0  |
| cb                        | 3.2  | 140.8  |
| Top Ex cb 1/4 W of E line | 3.28 | 140.75 |
| excb + 6                  | 5.2  | 138.8  |

1/4 5.3 138.7

8 4.9 139.1

1/4 4.6 139.4

cb 4.5 139.5

+9 4.9 139.1

W 3.3 140.7

3+00

W 0.8 143.2

+6 2.1 141.9

cb 3.2 140.8

+4 2.3 141.7

1/4 2.8 141.2

8 3.1 140.9

1/4 3.5 140.5

+4 ~ Gutter 3.5 140.5

" Top ex curb 2.50 141.53

cb 1/4 ex curb 2.0 142.0

T  
144.03

Theor/ro of +0.85 ex Sidewalk 2.48 141.55

ex cb 2.25 141.78

E 1.6 142.4

3112 36 See sketch

E +0.1 144.1

+2.6 edge work 1.25 142.78

+7.7 " " 1.93 142.60

+12 1.0 143.0

7.13<sup>2</sup> ex cb 1.51 142.52

Gutter 2.0 142.0

1/4 1.7 142.3

1/4 1.3 142.7

1/4 0.8 143.5

T.P 11.68 155.15 0.56 143.47

cb 11.2 144.0

W 10.6 144.6

3120 25. E C See sketch page 1

W 10.5 144.7

cb 11.2 144.0

1/4 10.9 144.3

T  
155.15

8

1/4 1.4 143.8

1/4 1.8 143.4

Gutter 12.4 142.8

Top cb 11.88 143.27

+5.5 w. edge walk 11.89 143.26

+10.5 E 11.82 143.33

E 10.3 144.9

3150

E 9.7 145.5

Top cb 9.93 145.22

Gutter 10.4 144.8

1/4 9.9 145.3

1/4 10.0 145.2

1/4 9.7 145.5

cb 9.7 145.5

W 9.7 145.5

4100

W 6.6 148.6

77<sup>2</sup> int of cb 6.57 148.58

+10 7.1 148.1

15515

|               |      |        |
|---------------|------|--------|
| cb.           | 7.1  | 148.1  |
| 1/4           | 7.2  | 148.0  |
| 1/2           | 7.2  | 148.0  |
| 1/4           | 7.1  | 148.1  |
| Gutter        | 7.5  | 147.7  |
| E Topcb       | 6.77 | 148.38 |
| E             | 6.3  | 148.9  |
| 4+20          |      |        |
| E             | 5.0  | 150.2  |
| +0.5          | 5.29 | 149.86 |
| +5.5          | 5.36 | 149.79 |
| cb            | 5.47 | 149.68 |
| E             | 6.3  | 148.9  |
| 1/4           | 6.0  | 149.2  |
| 1/2           | 5.9  | 149.3  |
| 1/4           | 6.1  | 149.1  |
| +7.5 W Gutter | 6.1  | 149.1  |
| " Topcb       | 5.58 | 149.57 |
| S Edge Walk   | 5.55 | 149.60 |
| N "           | 5.51 | 149.64 |

149.68  
 149.57  
 ---  
 149.11

15515

9

|                                   |      |        |
|-----------------------------------|------|--------|
| W                                 | 6.3  | 148.9  |
| Set B.M. 11/20. N.E. 51° Rosewell | 8.56 | 146.59 |
| 4+50                              |      |        |
| W                                 | 4.1  | 151.1  |
| +13.3 Topex cb                    | 3.72 | 151.43 |
| " Gutter                          | 4.7  | 150.5  |
| 1/4                               | 4.5  | 150.7  |
| 1/2                               | 4.1  | 151.1  |
| 1/4                               | 4.1  | 151.1  |
| Gutter                            | 4.4  | 150.8  |
| Topcb                             | 3.42 | 151.73 |
| E                                 | 3.0  | 152.2  |
| 4+89 Endcb on W                   |      |        |
| E                                 | 0.4  | 154.8  |
| +1.0 E edge walk                  | 0.48 | 154.67 |
| +5.5 W " "                        | 0.64 | 154.51 |
| Topcb                             | 0.81 | 154.34 |
| Gutter                            | 1.4  | 153.8  |
| 1/4                               | 1.3  | 153.9  |
| 1/2                               | 1.8  | 153.4  |

mm  
 151.4  
 151.1  
 151.1  
 151.1

T  
155.15

|                   |       |        |  |        |
|-------------------|-------|--------|--|--------|
| 1/4               |       |        | 2.2                                      | 153.0  |
| +7.7 Gutter       |       |        | 2.4                                      | 152.8  |
| " " Top ex cb     |       |        | 1.00                                     | 154.15 |
| +5.6 S. Edge walk |       |        | 0.91                                     | 154.24 |
| +10.6 N " "       |       |        | 0.96                                     | 154.19 |
| W                 |       |        | 1.2                                      | 154.0  |
| T.P.              | 11.37 | 165.61 | 0.91                                     | 154.24 |
| W + 10            |       |        | 13.5                                     | 152.1  |
|                   |       |        | 5148 <sup>2</sup> Box in Cb and Walkways |        |
| W-10              |       |        | 10.3                                     | 155.3  |
| W-4               |       |        | 7.4                                      | 158.2  |
| W                 |       |        | 7.4                                      | 158.2  |
| +10               |       |        | 7.5                                      | 158.1  |
| cb                |       |        | 7.9                                      | 157.7  |
| +4                |       |        | 8.7                                      | 156.9  |
| 1/4               |       |        | 8.2                                      | 157.4  |
| E                 |       |        | 7.8                                      | 157.8  |
| 1/4               |       |        | 7.8                                      | 157.8  |
| G                 |       |        | 7.8                                      | 157.8  |
| Top cb            |       |        | 7.20                                     | 158.41 |
| +5.5              |       |        | 7.10                                     | 158.51 |
| +10.5             |       |        | 7.02                                     | 158.59 |

10

T  
165.61

|                  |       |                         |            |        |
|------------------|-------|-------------------------|------------|--------|
| E                |       |                         | 6.7        | 158.9  |
|                  |       |                         | 6+00       |        |
| E                |       |                         | 2.7        | 162.9  |
| Edge walk +20    |       |                         | 2.82       | 162.79 |
| W edge walk +5.5 |       |                         | 2.89       | 162.72 |
| E Top cb         |       |                         | 3.12       | 162.49 |
| G                |       |                         | 3.9        | 161.7  |
| 1/4              |       |                         | 3.9        | 161.7  |
| E                |       |                         | 4.0        | 161.6  |
| 1/4              |       |                         | 4.6        | 161.0  |
| +6               |       |                         | 5.1        | 160.5  |
| cb               |       |                         | 4.2        | 161.4  |
| W                |       |                         | 3.8        | 161.8  |
| +2               |       |                         | 3.8        | 161.8  |
| +10              |       |                         | 7.9        | 157.7  |
| T.P.             | 12.49 | <sup>50</sup><br>177.46 | 0.65       | 164.96 |
|                  |       | 6+50 <sup>8</sup>       | Replace cb |        |
| W-10             |       |                         | 16.0       | 161.5  |
| W-2              |       |                         | 11.7       | 165.8  |
| W                |       |                         | 11.6       | 165.9  |
| +8               |       |                         | 11.6       | 165.9  |

T  
177.46

|  |       |        |
|--|-------|--------|
| cb                                       | 12.3  | 165.2  |
| +4                                       | 13.0  | 164.5  |
| 1/4                                      | 12.6  | 164.9  |
| 2  | 12.0  | 165.5  |
| 1/4                                      | 11.7  | 165.8  |
| G  | 11.7  | 165.8  |
| E Topcb                                  | 10.81 | 166.65 |
| +5.5 WEDGEWALK                           | 10.58 | 166.88 |
| +10.5 E " "                              | 10.99 | 166.97 |
| E  | 10.4  | 167.1  |
| 6+71 <sup>33</sup> W. line Winston Drive |       |        |
| E  | 8.1   | 169.4  |
| +2.0                                     | 8.75  | 168.71 |
| +5.5                                     | 8.85  | 168.61 |
| cb                                       | 8.4   | 168.9  |
| Gutter                                   | 10.0  | 167.5  |
| 1/4                                      | 9.9   | 167.6  |
| 2  | 10.2  | 167.3  |
| 1/4                                      | 11.0  | 166.5  |
| +6                                       | 11.4  | 166.1  |

T  
177.46

11

|   |       |        |
|---|-------|--------|
| +8  | 10.5  | 167.0  |
| cb  | 10.6  | 166.9  |
| W   | 10.0  | 167.5  |
| Sat B.M. <sup>Mar</sup> 314 Winston Paswell | 10.21 | 167.25 |
| +2  | 10.2  | 167.3  |
| +10   | 13.9  | 163.6  |
| 7+00  |       |        |
| W-10  | 8.5   | 169.0  |
| W   | 7.7   | 169.8  |
| cb  | 8.4   | 169.1  |
| +2  | 8.6   | 168.9  |
| +3  | 9.7   | 167.8  |
| 1/4   | 8.5   | 169.0  |
| 2   | 7.7   | 169.8  |
| 1/4   | 7.5   | 170.0  |
| Gutter                                      | 7.4   | 170.1  |
| Topcb                                       | 6.65  | 170.81 |
| WedgeWalk +5.5                              | 6.39  | 171.07 |
| E " " +10.5                                 | 6.29  | 171.17 |
| E   | 5.7   | 171.8  |

177.96

7+31<sup>51</sup> ♀ Winston Drive

|       |       |        |
|-------|-------|--------|
| E     | 3.0   | 174.5  |
| Topcb | 3.98  | 173.48 |
| G     | 4.9   | 172.6  |
| 1/4   | 5.0   | 172.5  |
| ♀     | 5.0   | 172.5  |
| 1/4   | 5.6   | 171.9  |
| cb    | 5.8   | 171.7  |
| W     | 5.5   | 172.0  |
| +10   | 5.9   | 171.6  |
| TP    | 11.51 | 186.73 |
|       | 2.24  | 175.22 |

Nail in pole  
approx Winston  
Drive on S.7+91<sup>69</sup> E Line Winston Drive

|                 |      |        |
|-----------------|------|--------|
| N-5             | 10.8 | 175.9  |
| W               | 10.4 | 176.3  |
| cb              | 10.3 | 176.4  |
| 1/4             | 10.2 | 176.5  |
| ♀               | 9.6  | 177.1  |
| 1/4             | 9.3  | 177.4  |
| G               | 9.1  | 177.6  |
| Topcb           | 8.24 | 178.49 |
| W Edge walk +55 | 8.10 | 178.63 |

186.73

12

|                  |                    |                              |
|------------------|--------------------|------------------------------|
| E edge walk +105 | 8.02               | 178.71                       |
| E                | 7.0                | 179.73                       |
|                  | 8+41 <sup>69</sup> | PC-N.E. Cor Winston Drive    |
| E                | 3.2                | 183.5                        |
| E edge walk +20  | 3.83               | 182.90                       |
| W " " +75        | 3.93               | 182.80                       |
| Topcb            | 4.08               | 182.65                       |
| G                | 4.6                | 182.1                        |
| 1/4              | 4.7                | 182.0                        |
| ♀                | 5.2                | 181.5                        |
| 1/4              | 6.2                | 180.5                        |
| +3               | 5.9                | 180.8                        |
| cb               | 6.3                | 180.4                        |
| W                | 6.6                | 180.1                        |
| +5               | 6.4                | 180.4                        |
|                  | 8+52               | Break in x Sidewalk rd. on S |
| N-5              | 5.1                | 181.6                        |
| W                | 5.5                | 181.2                        |
| cb               | 5.0                | 181.7                        |
| +6               | 4.7                | 182.0                        |
| 1/4              | 5.3                | 181.4                        |

T  
186.23

|                |  |      |        |
|----------------|--|------|--------|
| ¢              |  | 4.5  | 182.2  |
| 1/4            |  | 4.0  | 182.7  |
| G              |  | 3.6  | 183.1  |
| Topcb          |  | 3.23 | 183.50 |
| +5.5 Edge work |  | 3.10 | 183.63 |
| +10.5 " "      |  | 2.98 | 183.75 |
| E              |  | 1.0  | 185.7  |

T.P. 12.58 198.09 1.22 185.51

9400

|                   |  |      |        |
|-------------------|--|------|--------|
| W-5               |  | 10.6 | 187.5  |
| W                 |  | 11.4 | 186.7  |
| cb                |  | 11.6 | 186.5  |
| 1/4               |  | 11.9 | 186.2  |
| ¢                 |  | 11.1 | 187.0  |
| 1/4               |  | 10.5 | 187.6  |
| G                 |  | 10.0 | 188.1  |
| cb                |  | 9.49 | 188.60 |
| W Edge work + 5.5 |  | 9.29 | 188.80 |
| E " " + 10.5      |  | 9.14 | 188.95 |
| E                 |  | 7.0  | 191.1  |

T  
198.09

9750

13

|       |  |      |        |
|-------|--|------|--------|
| E     |  | 2.6  | 195.5  |
| Topcb |  | 4.29 | 193.80 |
| ¢     |  | 5.3  | 192.8  |
| 1/4   |  | 5.6  | 192.5  |
| ¢     |  | 5.8  | 192.3  |
| 1/4   |  | 6.6  | 191.5  |

|    |  |     |       |
|----|--|-----|-------|
| cb |  | 6.3 | 191.8 |
| +7 |  | 6.6 | 191.5 |
| W  |  | 5.7 | 192.4 |
| +5 |  | 5.3 | 192.8 |

10400

|      |       |               |             |
|------|-------|---------------|-------------|
| W-5  |       | 0.2           | 197.9       |
| W    |       | 0.7           | 197.4       |
| cb   |       | 0.9           | 197.4       |
| +4   |       | 1.6           | 196.5       |
| 1/4  |       | 1.7           | 196.4       |
| ¢    |       | 1.0           | 197.1       |
| 1/4  |       | 0.4           | 197.7       |
| G    |       | 0.2           | 197.9       |
| T.P. | 12.91 | <u>210.50</u> | 0.50 197.59 |



T  
210.50

|             |       |        |
|-------------|-------|--------|
| cb          | 11.42 | 199.08 |
| +55         |       |        |
| W Edge walk | 11.19 | 199.31 |
| +10.5       |       |        |
| E " "       | 11.10 | 199.40 |
| E           | 8.3   | 202.2  |

10+43 Replace cb See sketch page 2

|             |       |        |
|-------------|-------|--------|
| E           | 4.8   | 205.7  |
| +2.0        |       |        |
| E edge walk | 6.42  | 204.08 |
| +7.5        |       |        |
| W " "       | 6.50  | 204.00 |
| Top cb      | 6.54  | 203.96 |
| G           | 7.7   | 202.8  |
| 1/4         | 8.2   | 202.3  |
| 2           | 8.6   | 201.9  |
| 1/4         | 9.3   | 201.2  |
| +5          | 9.2   | 201.3  |
| cb          | 8.5   | 202.0  |
| +6          | 8.0   | 202.5  |
| W           | 7.9   | 202.6  |
| +5          | 7.8   | 202.7  |
|             | 11+00 |        |
| -5          | 17    | 208.8  |

T  
210.50

14

|             |       |        |                                 |
|-------------|-------|--------|---------------------------------|
| W           |       | 2.6    | 207.9                           |
| +3          |       | 2.2    | 208.3                           |
| cb          |       | 3.0    | 207.5                           |
| +5          |       | 2.5    | 208.0                           |
| 1/4         |       | 3.5    | 207.0                           |
| 2           |       | 2.4    | 208.1                           |
| 1/4         |       | 2.0    | 208.5                           |
| G           |       | 1.6    | 208.9                           |
| Top cb      |       | 0.9    | 209.6                           |
| +55         |       |        |                                 |
| W Edge walk |       | 0.52   | 209.98                          |
| +10.5       |       |        |                                 |
| E " "       |       | 0.37   | 209.13                          |
| E           |       | +1.4   | 211.9                           |
| T.P.        | 13.03 | 223.07 | 0.46 210.04                     |
|             |       | 11+41  | End Broken cb See sketch page 2 |
| E           |       | 6.3    | 216.8                           |
| Top cb      |       | 8.75   | 214.32                          |
| G           |       | 9.7    | 213.4                           |
| 1/4         |       | 9.8    | 213.3                           |
| 2           |       | 10.2   | 212.9                           |
| 1/4         |       | 11.2   | 211.9                           |

T  
223.07

|            |       |        |
|------------|-------|--------|
| +4         | 10.9  | 212.2  |
| cb         | 11.0  | 212.1  |
| +4         | 10.3  | 212.8  |
| W          | 10.3  | 212.8  |
| +5         | 10.1  | 213.0  |
|            | 12+00 |        |
| W-10       | 3.6   | 219.5  |
| -5         | 4.5   | 218.6  |
| W          | 3.8   | 219.3  |
| +7         | 3.6   | 219.5  |
| +9         | 4.3   | 218.8  |
| cb         | 4.5   | 218.6  |
| 1/4        | 4.7   | 218.4  |
| 4          | 3.9   | 219.2  |
| 1/4        | 3.6   | 219.5  |
| G          | 3.5   | 219.6  |
| Top cb     | 2.60  | 220.47 |
| Wedge walk | 2.46  | 220.61 |
| E " "      | 2.38  | 220.69 |
| E          | 1.4   | 221.7  |

15

T  
223.07

|        |       |        |       |        |
|--------|-------|--------|-------|--------|
| Top    | 13.03 | 235.94 | 0.16  | 222.91 |
|        |       | 12+50  |       |        |
| E      |       |        | 7.9   | 228.0  |
| Top cb |       |        | 10.20 | 225.74 |
| G      |       |        | 11.2  | 224.7  |
| 1/4    |       |        | 11.4  | 224.5  |
| 4      |       |        | 11.7  | 224.2  |
| 1/4    |       |        | 12.4  | 223.5  |
| +6     |       |        | 12.7  | 223.2  |
| cb     |       |        | 12.3  | 223.6  |
| +3     |       |        | 12.6  | 223.3  |
| +4     |       |        | 11.2  | 224.7  |
| W      |       |        | 11.3  | 224.6  |
| W+10   |       |        | 11.2  | 224.7  |
|        |       | 12+98  |       |        |
| W-10   |       |        | 4.7   | 231.2  |
| W      |       |        | 5.7   | 230.2  |
| +6     |       |        | 5.7   | 230.2  |
| +8     |       |        | 6.5   | 229.4  |
| cb     |       |        | 7.2   | 228.7  |

T  
235.94

|             |       |               |             |
|-------------|-------|---------------|-------------|
| 1/4         |       | 7.0           | 228.9       |
| 1/2         |       | 6.4           | 229.5       |
| 1/4         |       | 6.0           | 229.9       |
| G           |       | 5.6           | 230.3       |
| Topcb       |       | 4.81          | 231.13      |
| W Edge walk |       | 4.65          | 231.29      |
| E           | "     | 4.59          | 231.35      |
| E           |       | 3.1           | 232.8       |
| T.P.        | 11.17 | <u>246.94</u> | 0.17 235.77 |
|             |       | 13.48         |             |
| E           |       | 9.8           | 237.1       |
| Topcb       |       | 10.60         | 236.34      |
| G           |       | 11.3          | 235.6       |
| 1/4         |       | 11.6          | 235.3       |
| 1/2         |       | 11.8          | 235.1       |
| 1/4         |       | 12.4          | 234.5       |
| cb          |       | 13.1          | 233.8       |
| +1          |       | 13.1          | 233.8       |
| +2          |       | 12.2          | 234.7       |
| W           |       | 11.3          | 235.6       |
| +10         |       | 10.2          | 236.7       |

T  
246.94

16

13.78

|           |  |       |          |
|-----------|--|-------|----------|
| W-10      |  | 7.0   | 239.9    |
| W         |  | 8.8   | 238.1    |
| +8        |  | 9.0   | 237.9    |
| +9        |  | 10.5  | 236.4    |
| cb        |  | 10.5  | 236.4    |
| 1/4       |  | 9.6   | 237.3    |
| 1/2       |  | 9.0   | 237.9    |
| 1/4       |  | 8.6   | 238.3    |
| G         |  | 8.1   | 238.8    |
| Topcb     |  | 7.46  | 239.48 ✓ |
| E         |  | 6.4   | 240.5    |
|           |  | 14.01 | 23       |
| E         |  | 4.3   | 242.6    |
| Edge walk |  | 4.64  | 242.30   |
| W a "     |  | 4.76  | 242.18   |
| Topcb     |  | 4.98  | 241.96 ✓ |
| E         |  | 6.1   | 240.8    |
| 1/4       |  | 6.6   | 240.3    |
| 1/2       |  | 6.8   | 240.1    |
| 1/4       |  | 7.2   | 239.7    |

6209 on  
Ange

Wlime Malrose

246.94

|                       |      |        |
|-----------------------|------|--------|
| cb                    | 7.3  | 239.6  |
| +6                    | 6.2  | 240.7  |
| N                     | 6.1  | 240.8  |
| +5                    | 5.7  | 241.2  |
| 1413.7 W.C.B.         |      |        |
| -5                    | 4.8  | 242.1  |
| N                     | 5.1  | 241.8  |
| cb                    | 5.6  | 241.3  |
| +3                    | 6.3  | 240.6  |
| 1/4                   | 6.2  | 240.7  |
| 2                     | 6.0  | 240.9  |
| 1/2                   | 5.8  | 241.1  |
| cb                    | 5.3  | 241.6  |
| +2.5                  | 4.5  | 242.4  |
| +10 on Ground         | 3.7  | 243.2  |
| +10 Top cb end Return | 4.92 | 242.02 |
| E                     | 3.3  | 243.3  |
| 2 14132.37            |      |        |
| E                     | 3.7  | 243.2  |
| cb                    | 4.3  | 242.6  |

246.94

17

|                         |      |        |
|-------------------------|------|--------|
| 1/4                     | 4.8  | 242.1  |
| 2                       | 5.2  | 241.7  |
| 1/4                     | 5.3  | 241.6  |
| +6                      | 5.6  | 241.3  |
| cb                      | 5.2  | 241.7  |
| N                       | 4.5  | 242.4  |
| +5                      | 4.2  | 242.7  |
| 14151 E.C.B. Melrose    |      |        |
| N-5                     | 4.2  | 242.7  |
| N                       | 4.2  | 242.7  |
| cb                      | 4.9  | 242.0  |
| +5                      | 5.5  | 241.4  |
| 1/4                     | 5.3  | 241.6  |
| 2                       | 5.0  | 241.9  |
| 1/4                     | 4.7  | 242.2  |
| cb                      | 4.4  | 242.5  |
| +10 Top cb end Return   | 3.77 | 243.17 |
| N Grd                   | 3.3  | 243.6  |
| E                       | 3.1  | 243.8  |
| Set B.M. S.E. Prop. Mos | 3.57 | 243.37 |

Melrose  
Rosewell

T  
24694

14+63.9<sup>2</sup> E Line Mcrose.

|              |      |        |
|--------------|------|--------|
| E            | 31   | 243.8  |
| E. Edge walk | 3.54 | 243.40 |
| cb           | 3.72 | 243.22 |
| G            | 4.6  | 242.3  |
| 1/4          | 4.9  | 242.0  |
| 2            | 5.1  | 241.8  |
| 1/4          | 5.2  | 241.7  |
| +6           | 5.5  | 241.4  |
| cb           | 5.0  | 241.9  |
| W            | 4.6  | 242.3  |

14+97

|             |      |        |
|-------------|------|--------|
| W           | 5.9  | 241.5  |
| cb          | 5.4  | 241.5  |
| +1          | 6.1  | 240.8  |
| 1/4         | 5.8  | 241.1  |
| 2           | 5.7  | 241.2  |
| 1/4         | 5.6  | 241.3  |
| G           | 5.4  | 241.5  |
| Topcb       | 4.64 | 242.30 |
| W Edge walk | 4.44 | 242.50 |

24694

18

|             |       |                                      |
|-------------|-------|--------------------------------------|
| E edge walk | 4.40  | 242.54                               |
| E           | 4.6   | 242.3                                |
|             | 15+50 | 3 Begin cb on W. Sec 34 E1<br>page 2 |
| E           | 5.6   | 241.3                                |
| Topcb       | 5.63  | 241.31                               |
| G           | 6.4   | 240.5                                |
| 1/4         | 6.4   | 240.5                                |
| 2           | 6.5   | 240.4                                |
| 1/4         | 6.5   | 240.4                                |
| G           | 6.7   | 240.2                                |

|                |      |        |
|----------------|------|--------|
| Topcb          | 6.17 | 240.77 |
| +5.5 edge walk | 5.96 | 240.98 |
| +10.5 W. "     | 5.93 | 241.01 |
| W              | 6.0  | 240.9  |

15+97

|             |      |        |
|-------------|------|--------|
| W           | 6.7  | 240.2  |
| W edge walk | 6.67 | 240.27 |
| E "         | 6.73 | 240.21 |
| Topcb       | 6.84 | 240.10 |
| G           | 7.3  | 239.6  |

π  
246.94

1/4 6.9 240.0

⊕ 6.9 240.0

1/4 6.9 240.0

⊖ 7.1 239.8

Topcb 6.41 240.53

+5.5 Wedge 6.28 240.66

+10.5 edge walk 6.23 240.71

E 6.4 240.54

TP 4.58 295.11 6.91 240.53

16+53<sup>L</sup> find cb on West page <sup>see sketch</sup>

E 5.0 240.1

cb 19 driveway Grd. 5.2 239.9

G 5.4 239.7

1/4 5.2 239.9

⊕ 5.3 239.8

1/4 5.2 239.9

⊖ 5.7 239.4

Topcb 5.93 239.68

+5.5 edge walk 5.79 239.92

+10.5 " 5.13 239.98

π  
245.11

19

W 5.2 239.9

17+00

W 4.7 240.4

cb 5.3 239.8

+4 5.3 239.8

+5 5.7 239.4

1/4 5.4 239.7

⊕ 5.2 239.9

1/4 5.5 239.6

G 6.0 239.1

Topcb 5.20 239.91

+5.5 5.10 240.01

+10.5 5.00 240.11

E 4.9 240.2

+5 5.0 240.1

17+23<sup>L</sup> See from L on cb on South

Set BM. L Mon on Shore Pavilion 5.90 239.21

S 5.7 239.4

Topcb 5.46 239.65

G 6.5 238.6

|                           |      |        |
|---------------------------|------|--------|
| 1/4                       | 6.2  | 238.9  |
| £                         | 5.7  | 239.4  |
| 1/4                       | 5.7  | 239.4  |
| +9                        | 6.0  | 239.1  |
| cb                        | 5.6  | 239.5  |
| +9                        | 4.9  | 240.2  |
| +1 W                      | 3.6  | 241.5  |
| 17+33.5 From N. Prop line |      |        |
| W on Ground               | 4.6  | 240.5  |
| W on Prop Measurement     | 4.84 | 240.27 |
| +10                       | 5.5  | 239.6  |
| cb                        | 5.8  | 239.3  |
| 1/4                       | 5.8  | 239.3  |
| £                         | 5.8  | 239.3  |
| 1/4                       | 6.2  | 238.9  |
| G                         | 6.5  | 238.6  |
| Top cb                    | 5.97 | 239.64 |
| +5.5                      | 5.31 | 239.80 |
| +10.5                     | 5.27 | 239.84 |
| E                         | 5.7  | 239.4  |
| +10                       | 6.9  | 238.2  |

To Angle on South  
 Line Roswell

To Angle  
 41.00  
 50.00  
 10.00  
 Roswell

|                                   |      |        |              |            |
|-----------------------------------|------|--------|--------------|------------|
| T.P.                              | 0.78 | 244.15 | 1.74         | 243.37     |
| T.P.                              | 0.04 | 231.20 | 12.99        | 231.16     |
| T.P.                              | 0.35 | 219.19 | 12.36        | 218.84     |
| T.P.                              | 0.21 | 206.32 | 13.08        | 206.11     |
| T.P.                              | 0.35 | 193.85 | 12.82        | 193.50     |
| T.P.                              | 0.16 | 181.03 | 12.98        | 180.87     |
| T.P.                              | 0.65 | 168.80 | 12.88        | 168.15     |
| check BM                          |      |        | 1.53         | 165.27     |
| T.P.                              | 0.22 | 156.43 | 12.59        | 156.21     |
| check BM NE Prop Man              |      |        | 9.82         | 146.61     |
| T.P.                              | 1.45 | 145.06 | 12.82        | 143.61     |
| T.P.                              | 0.66 | 132.71 | 13.01        | 132.25     |
| T.P.                              | 0.40 | 120.11 | 13.00        | 119.71     |
| T.P.                              | 2.08 | 112.09 | 10.10        | 110.01     |
| check starting BM NW Cor. E. side |      |        | 7.82         | 104.27     |
|                                   |      |        | 8.00         | 104.22     |
|                                   |      |        | 200 S of Man | 0.05 error |

Mon. N.W.  
 Winston Drive  
 Roswell

165.25 error  
 0.02

X Section 51<sup>st</sup> from the N Line of

Posewell to 200' North

3M 4.25 150.84 146.59

Lerek Around Return on N.E. Cor. Posewell + 51<sup>st</sup>

Arc 73.6 Divided into 5 parts 14.72

Oteo P.C. 40 E. of Prop Man 1.27 149.57

Gutter 1.9 148.9

#1 1.98 148.86

Gutter 2.5 148.3

#1 Sidewalk 5.5 N 1.91 148.93

" 10.5 " 1.84 149.00

#2 2.97 148.37

Gutter 3.1 147.7

" Sidewalk 5.5 N 2.98 148.36

" " 10.5 " 2.39 148.50

#3 2.95 147.89

Gutter 3.6 147.2

" Sidewalk 5.5 N 2.86 147.98

" " 10.5 " 2.78 148.06

#4 3.27 147.57

Gutter 4.0 146.8

" Sidewalk 5.5 N 3.21 147.63

" " 10.5 " 3.14 147.4

#5 F.C. 3.54 147.30

Sec A See sketch page 1

E Line 3.8 147.0

Indexed  
RM

Red. 10/31/41 (W)

15089

10' Lt 4.9 146.4

20 " 4.9 145.9

30 " 5.4 145.4

40 " 5.8 145.0

50 " 6.3 144.5

60 " 6.2 144.6

70 " 6.3 144.5

80' W.L.M. 51<sup>st</sup>

Sidewalk 25.5 S of Oteo See sketch page 1

2.9 W.L.M. 4.58 146.26

0400

W 9.3 146.5

cb 5.0 145.8

1/4 5.2 145.6

1/2 4.9 145.9

1/4 4.7 146.1

cb 4.3 146.5

E 3.8 147.0

0440 F.C. Ch. Ret on East

E 3.4 147.4



|        |             |      |        |
|--------|-------------|------|--------|
| +2.5   | E Edge walk | 3.33 | 147.51 |
| +7.5   |             | 3.45 | 147.39 |
| Top cb |             | 3.53 | 147.31 |
| G      |             | 4.2  | 146.6  |
| 1/4    |             | 4.2  | 146.6  |
| E      |             | 4.3  | 146.5  |
| 1/4    |             | 4.4  | 146.4  |
| cb     |             | 4.1  | 146.7  |
| W      |             | 3.2  | 147.6  |

0170

|        |           |      |        |
|--------|-----------|------|--------|
| W      |           | 2.8  | 148.0  |
| +5     |           | 3.1  | 147.7  |
| cb     |           | 4.3  | 146.5  |
| 1/4    |           | 4.5  | 146.3  |
| E      |           | 4.2  | 146.6  |
| 1/4    |           | 3.8  | 147.0  |
| G      |           | 3.7  | 147.1  |
| Top cb |           | 3.23 | 147.61 |
| + 5.5  | Edge walk | 3.18 | 147.68 |
| + 10.5 | " "       | 3.13 | 147.71 |
| E      |           | 3.4  | 147.4  |

1400

|        |      |      |        |
|--------|------|------|--------|
| E      |      | 3.2  | 147.6  |
| +2.5   | walk | 3.17 | 147.67 |
| +7.5   | " "  | 3.25 | 147.59 |
| Top cb |      | 3.40 | 147.44 |
| E      |      | 4.1  | 146.7  |
| 1/4    |      | 4.4  | 146.4  |
| E      |      | 4.3  | 146.5  |
| 1/4    |      | 3.6  | 147.2  |
| cb     |      | 3.5  | 147.3  |
| W      |      | 2.8  | 148.0  |

1414 Telephone Pole G. E. of W. line

1420

|     |  |     |       |
|-----|--|-----|-------|
| W-3 |  | 2.7 | 148.1 |
| W   |  | 2.8 | 148.0 |
| cb  |  | 2.8 | 148.0 |
| +2  |  | 2.8 | 148.0 |
| +4  |  | 4.1 | 146.7 |
| 1/4 |  | 4.3 | 146.5 |
| E   |  | 4.3 | 146.5 |
| 1/4 |  | 4.7 | 146.1 |
| G   |  | 4.3 | 146.5 |

T  
15084

|       |      |        |
|-------|------|--------|
| cb    | 3.79 | 147.05 |
| +5.5  | 3.77 | 147.07 |
| +10.5 | 3.68 | 147.16 |
| E     | 3.5  | 147.3  |
| 1+40  |      |        |
| E     | 4.0  | 146.8  |
| +2    | 4.99 | 145.85 |
| +7    | 5.06 | 145.78 |
| cb    | 5.11 | 145.73 |
| C     | 5.3  | 145.5  |
| +5    | 5.5  | 145.3  |
| 1/4   | 6.6  | 144.2  |
| E     | 7.0  | 143.8  |
| 1/4   | 6.9  | 143.9  |
| +4    | 6.6  | 144.2  |
| +8    | 4.5  | 146.3  |
| cb    | 4.4  | 146.4  |
| +1    | 4.4  | 146.4  |
| +8    | 6.4  | 144.4  |
| W     | 7.6  | 143.2  |
| +10   | 10.5 | 140.3  |

23

T  
15084

+69<sup>2</sup> End of Kon East

|        |        |        |
|--------|--------|--------|
| E      | 8.76   | 142.08 |
| W      | 8.86   | 141.98 |
| Topcb  | 8.93   | 141.91 |
| 1475.3 | End cb |        |
| W-20   | 22.0   | 148.64 |
| W      | 17.6   | 133.2  |
| cb     | 13.7   | 137.1  |
| 1/4    | 11.9   | 138.9  |
| E      | 12.1   | 138.7  |
| 1/4    | 11.5   | 139.3  |
| C      | 10.4   | 140.4  |
| Topcb  | 9.86   | 140.98 |
| +2     | 11.7   | 139.1  |
| +6     | 9.9    | 140.9  |
| E      | 6.8    | 144.0  |
| 2+00   |        |        |
| E      | 11.8   | 139.0  |
| cb     | 15.6   | 135.2  |
| 1/4    | 15.7   | 135.1  |
| E      | 16.6   | 134.2  |
| 1/2    | 16.2   | 134.6  |
| cb     | 20.8   | 130.0  |
| W      | 24.5   | 126.3  |
| W+25   | 30.9   | 119.9  |

4/7/41  
Bliss  
Sommer Myer  
Beegs

### X Section Melrose Place From the S. Line of Rosewell to Dead End 400 S.

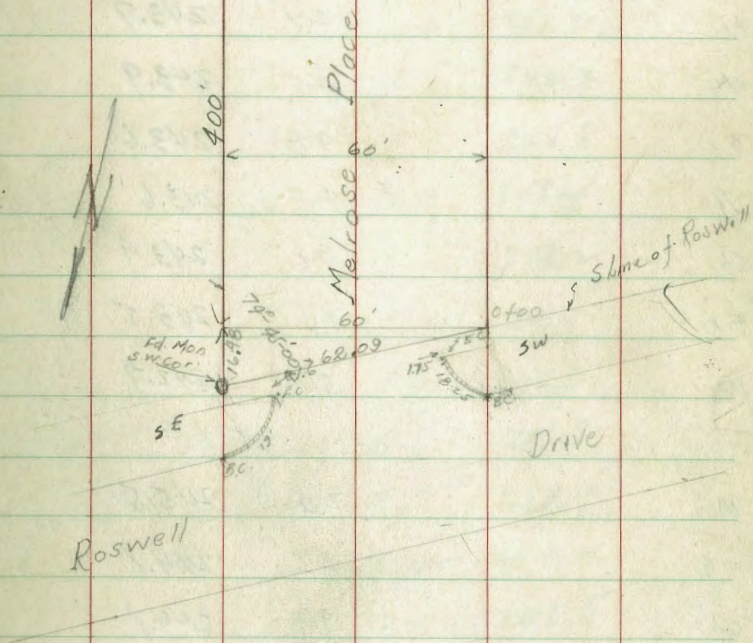
| BM                      | 5.06 | <u>248.43</u> | 243.37               |
|-------------------------|------|---------------|----------------------|
| Levels around SE Return |      |               |                      |
| EC S Line Rosewell      | 5.27 | 243.16        |                      |
| #1                      | 5.24 | 243.19        |                      |
| #2                      | 5.23 | 243.20        |                      |
| #3                      | 5.22 | 243.21        |                      |
| #4 C                    | 5.22 | 243.21        |                      |
| Levels around SW Return |      |               |                      |
| EC S Line Rosewell      | 6.42 | 242.01        | 18.25 Arc<br>4 parts |
| #1                      | 6.35 | 242.08        |                      |
| #2                      | 6.38 | 242.05        |                      |
| #3                      | 6.42 | 242.01        |                      |
| #4 EC                   | 6.47 | 241.96        | ✓                    |
|                         |      | 62.03         |                      |
| Sec A                   |      |               |                      |
| W Line                  | 5.7  | 242.7         |                      |
| #6                      | 5.0  | 243.4         |                      |
| 1/4                     | 5.2  | 243.2         |                      |
| 1/4                     | 5.2  | 243.2         |                      |
| 1/4                     | 5.1  | 243.3         |                      |

Plotted 11-13-41  
Okey

Indexed  
LM



See page No. 2



248.43

|      |      |       |
|------|------|-------|
| cb   | 7.8  | 243.6 |
| E    | 4.6  | 243.8 |
|      | 0+00 |       |
| E-10 | 5.4  | 243.0 |
| E    | 4.8  | 243.6 |
| cb   | 4.7  | 243.7 |
| 1/4  | 4.5  | 243.9 |
| E    | 4.8  | 243.6 |
| 1/4  | 4.8  | 243.6 |
| cb   | 4.5  | 243.9 |
| +10  | 4.9  | 243.5 |
| W    | 5.7  | 242.7 |
|      | 0+50 |       |
| W    | 2.9  | 245.5 |
| +2   | 3.6  | 244.8 |
| cb   | 4.3  | 244.1 |
| 1/4  | 4.5  | 243.9 |
| E    | 4.4  | 244.0 |
| 1/4  | 4.6  | 243.8 |
| cb   | 5.2  | 243.2 |
| E    | 5.2  | 243.2 |

248.43

25

|      |      |       |
|------|------|-------|
| +5   | 6.0  | 242.4 |
| +10  | 6.2  | 242.2 |
|      | 1+00 |       |
| E-15 | 7.6  | 240.8 |
| -5   | 7.1  | 241.3 |
| E    | 6.2  | 242.2 |
| cb   | 6.2  | 242.2 |
| 1/4  | 5.6  | 242.8 |
| +4   | 5.0  | 243.4 |
| E    | 5.2  | 243.2 |
| 1/4  | 5.3  | 243.1 |
| +6   | 5.6  | 242.8 |
| +7   | 4.5  | 243.9 |
| cb   | 4.5  | 243.9 |
| +10  | 4.2  | 244.2 |
| W    | 2.9  | 245.5 |
|      | 1+50 |       |
| W    | 4.8  | 243.6 |
| +2   | 5.3  | 243.1 |
| cb   | 5.6  | 242.8 |

T  
248.43

|      |      |      |       |
|------|------|------|-------|
| +2   |      | 6.4  | 242.0 |
| 1/4  |      | 6.3  | 242.1 |
| 1/2  |      | 6.3  | 242.1 |
| +4   |      | 6.2  | 242.2 |
| 1/4  |      | 6.7  | 241.7 |
| cb   |      | 7.2  | 241.2 |
| E    |      | 7.6  | 240.8 |
| +15  |      | 9.4  | 239.0 |
|      | 2+00 |      |       |
| E-20 |      | 11.8 | 236.6 |
| -8   |      | 10.8 | 237.6 |
| E    |      | 8.9  | 239.5 |
| cb   |      | 9.2  | 239.2 |
| 1/4  |      | 8.1  | 240.3 |
| +9   |      | 7.5  | 240.9 |
| 1/2  |      | 7.6  | 240.8 |
| 1/4  |      | 7.6  | 240.8 |
| +6   |      | 7.8  | 240.8 |
| cb   |      | 7.0  | 241.4 |
| +10  |      | 6.6  | 241.8 |

T  
248.43

26

|  |      |      |       |
|--|------|------|-------|
| W  |      | 5.7  | 242.7 |
|  | 2+09 |      |       |
| Gas Lt. Pole, West Face 12' from W Line 12" dia. |      |      |       |
|  | 2+28 |      |       |
| Dead Man Guy for above pole 12' from West Line   |      |      |       |
|  | 2+50 |      |       |
| W  |      | 7.6  | 240.8 |
| cb   |      | 8.8  | 239.6 |
| +6   |      | 9.4  | 239.0 |
| 1/4  |      | 9.4  | 239.0 |
| 1/2  |      | 9.6  | 238.8 |
| +6   |      | 9.8  | 238.6 |
| 1/4  |      | 10.3 | 238.1 |
| cb   |      | 10.6 | 237.8 |
| E  |      | 10.7 | 237.7 |
| +7   |      | 13.0 | 235.4 |
| +12  |      | 13.2 | 235.2 |
| +20  |      | 13.6 | 234.8 |
|  | 3+00 |      |       |
| E-20   |      | 15.5 | 232.9 |

|      |      |        |       |        |
|------|------|--------|-------|--------|
| E-10 |      |        | 14.7  | 232.7  |
| E    |      |        | 13.0  | 235.4  |
| +2   |      |        | 12.5  | 235.9  |
| cb   |      |        | 12.3  | 236.1  |
| 1/4  |      |        | 11.5  | 236.9  |
| ϕ    |      |        | 10.8  | 237.6  |
| 1/4  |      |        | 10.7  | 237.7  |
| +6   |      |        | 10.6  | 237.8  |
| cb   |      |        | 9.9   | 238.5  |
| +11  |      |        | 8.9   | 239.5  |
| W    |      |        | 8.1   | 240.3  |
| T.P. | 2.17 | 239.87 | 10.73 | 237.70 |
| W    |      |        | 0.8   | 239.1  |
| +2   |      |        | 2.0   | 237.9  |
| cb   |      |        | 3.0   | 236.9  |
| +2   |      |        | 3.7   | 236.2  |
| 1/4  |      |        | 4.0   | 235.9  |
| ϕ    |      |        | 4.4   | 235.5  |
| +2   |      |        | 4.3   | 235.6  |

|                   |  |      |      |        |
|-------------------|--|------|------|--------|
| 1/4               |  |      | 5.2  | 234.7  |
| +6                |  |      | 6.1  | 233.8  |
| cb                |  |      | 5.6  | 234.3  |
| +8                |  |      | 5.7  | 234.2  |
| E.                |  |      | 6.4  | 233.5  |
| +4                |  |      | 7.5  | 232.4  |
| +20               |  |      | 8.8  | 231.1  |
|                   |  | 9+00 |      |        |
| E-20              |  |      | 11.1 | 228.8  |
| -10               |  |      | 10.2 | 229.7  |
| E on 2x2 prop Hub |  |      | 8.63 | 231.24 |
| +3                |  |      | 7.6  | 232.3  |
| +10               |  |      | 7.7  | 232.2  |
| cb                |  |      | 8.0  | 231.9  |
| 1/4               |  |      | 7.5  | 232.4  |
| ϕ                 |  |      | 6.56 | 233.31 |
| 1/4               |  |      | 6.5  | 233.4  |
| cb                |  |      | 6.0  | 233.9  |
| +8                |  |      | 4.9  | 235.0  |
| W                 |  |      | 3.7  | 236.2  |

7  
233.87

Sec A <sup>10</sup> See sketch

|               |     |       |
|---------------|-----|-------|
| Rad           | 6.6 | 233.3 |
| +10           | 6.7 | 233.2 |
| +20           | 6.9 | 233.5 |
| +30 Prop line | 5.6 | 234.3 |
| +34           | 3.3 | 236.6 |
| +40           | 2.9 | 237.0 |
| R             | 6.6 | 233.3 |
| +10           | 6.9 | 233.0 |
| +20           | 7.1 | 232.8 |
| +30 Prop line | 6.8 | 233.1 |
| +40           | 6.5 | 233.4 |

Sec B <sup>13.54</sup>

|          |     |       |
|----------|-----|-------|
| Rad      | 6.6 | 233.3 |
| +10      | 7.4 | 232.5 |
| +20      | 8.1 | 231.8 |
| +30 Prop | 8.7 | 231.2 |
| +40      | 9.5 | 230.4 |

Sec C <sup>17.56</sup>

|     |     |       |
|-----|-----|-------|
| R   | 6.6 | 233.3 |
| +10 | 7.8 | 232.1 |
| +20 | 8.6 | 231.3 |

7  
232.87

28

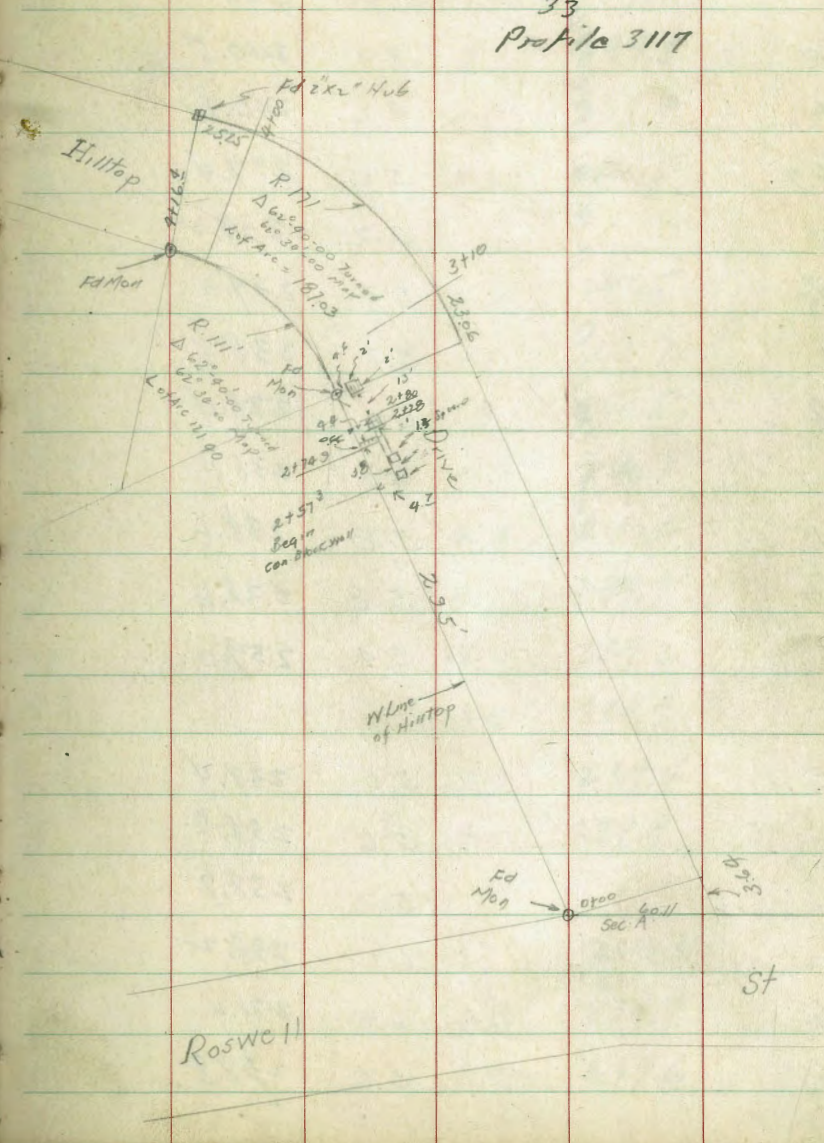
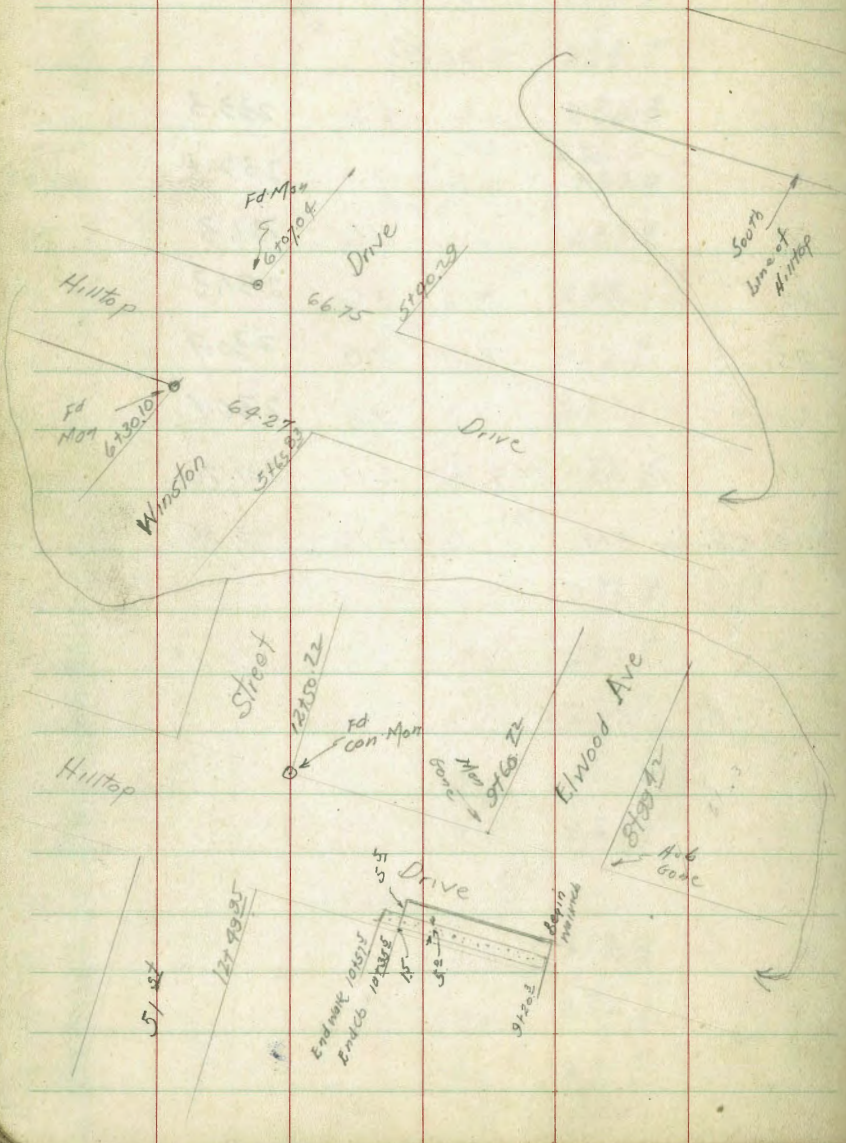
|                     |     |       |
|---------------------|-----|-------|
| +30                 | 9.4 | 230.5 |
| +40                 | 9.4 | 230.5 |
| Sec E <sup>6'</sup> |     |       |
| R                   | 6.6 | 233.3 |
| +10                 | 7.8 | 232.1 |
| +20                 | 8.6 | 231.3 |
| +30                 | 8.6 | 231.3 |
| +35                 | 9.0 | 230.9 |
| +40                 | 9.8 | 230.1 |

|                   |      |        |      |        |
|-------------------|------|--------|------|--------|
| T.P.              | 1076 | 248.46 | 2.17 | 237.70 |
| check starting BM |      |        | 5.10 | 243.36 |

Indexed  
LM

X-Section. Hilltop St. Beverly. Roswell  
to the East Line of 51st.

Also F.B.  $\frac{1612}{16}$   
 $\frac{259}{33}$   
Profile 3117





11/2/41  
Bliss  
Sommermyer  
8995

X. Section Hilltop Roswell to  
W. line 51st

60' st  
12' cbs  
9' 1/4'

X Secs are stationed to W line Distances

NW Prop  
Mon. Roswell  
Hilltop

BM 4.12 244.39 240.27

Sec. A See. Sketch

|     |     |       |
|-----|-----|-------|
| W   | 3.9 | 240.5 |
| t6  | 4.2 | 240.2 |
| t9  | 5.0 | 239.4 |
| cb  | 5.2 | 239.2 |
| 1/4 | 5.4 | 239.0 |
| 2   | 5.7 | 238.7 |
| 1/4 | 6.0 | 238.4 |
| t7  | 6.3 | 238.1 |
| cb  | 5.8 | 238.6 |
| t7  | 5.8 | 238.6 |
| E   | 5.4 | 239.0 |

Red. W.L.O. 11-14-41 (PROP. PLOTTED)

0+00

|     |     |       |
|-----|-----|-------|
| E   | 5.0 | 239.4 |
| t3  | 5.6 | 238.8 |
| cb  | 5.7 | 238.7 |
| t2  | 6.2 | 238.2 |
| 1/4 | 6.0 | 238.4 |
| 2   | 5.6 | 238.8 |

π  
244.39

30

|      |     |       |
|------|-----|-------|
| 1/4  | 5.4 | 239.0 |
| cb   | 5.2 | 239.2 |
| t3   | 4.9 | 239.5 |
| t5   | 4.5 | 239.9 |
| W    | 3.9 | 240.5 |
| 0+25 |     |       |
| W    | 2.9 | 241.5 |
| t5   | 3.7 | 240.7 |
| cb   | 3.8 | 240.5 |
| t3   | 4.3 | 240.1 |
| 1/4  | 4.4 | 240.0 |
| 2    | 4.7 | 239.7 |
| 1/4  | 5.2 | 239.2 |
| t6   | 5.5 | 238.9 |
| cb   | 5.0 | 239.4 |
| E    | 4.5 | 239.9 |
| 0+50 |     |       |
| E    | 4.1 | 240.3 |
| cb   | 4.5 | 239.9 |
| t3   | 4.8 | 239.6 |

244.39

|     |     |       |
|-----|-----|-------|
| 1/4 | 4.6 | 239.8 |
| ¢   | 4.3 | 240.1 |
| 1/4 | 4.3 | 240.1 |
| cb  | 4.0 | 240.4 |
| +10 | 4.0 | 240.4 |
| W   | 3.5 | 240.9 |

1100

|     |     |       |
|-----|-----|-------|
| W   | 4.5 | 239.9 |
| cb  | 4.3 | 240.1 |
| 1/4 | 4.5 | 239.9 |
| ¢   | 4.5 | 239.9 |
| 1/4 | 4.5 | 239.9 |
| cb  | 4.7 | 239.7 |
| E   | 4.0 | 240.4 |

1125

G. & Lt. Pole Wedge 11.5 from W line

1130

|     |     |       |
|-----|-----|-------|
| E   | 3.9 | 240.5 |
| cb  | 5.0 | 239.4 |
| 1/4 | 5.0 | 239.4 |

244.39

31

|     |     |       |
|-----|-----|-------|
| ¢   | 4.8 | 239.6 |
| 1/4 | 4.8 | 239.6 |
| cb  | 5.0 | 239.4 |
| W   | 5.3 | 239.1 |
| +10 | 5.8 | 238.6 |

1144 2' concrete walk on West

ct

6.05 238.34

1160

|      |     |       |
|------|-----|-------|
| W-10 | 7.1 | 237.3 |
| W    | 6.4 | 238.0 |
| cb   | 5.6 | 238.8 |
| 1/4  | 5.4 | 239.0 |
| ¢    | 5.2 | 239.2 |
| 1/4  | 5.4 | 239.0 |
| +8   | 5.3 | 239.1 |
| cb   | 4.8 | 239.6 |
| E    | 4.2 | 240.2 |

1176 Single Garage on West E.

10.5 Back D. Floor Opening 7.3 237.1

1186 4' 2" Dia Cypress Trees 1' to 4' in street  
Trees are RTL 5' to E.

T  
24439

2700

|      |      |       |
|------|------|-------|
| E    | 4.9  | 239.5 |
| +10  | 5.4  | 239.0 |
| cb   | 6.2  | 238.2 |
| 1/4  | 6.2  | 238.2 |
| 2    | 6.2  | 238.2 |
| 1/4  | 6.7  | 237.7 |
| cb   | 6.8  | 237.6 |
| +10  | 6.9  | 237.5 |
| W    | 7.1  | 237.3 |
| +7   | 9.1  | 235.3 |
| +20  | 10.8 | 233.6 |
| 2725 |      |       |
| -20  | 12.2 | 232.2 |
| -6   | 10.5 | 233.9 |
| W    | 8.8  | 235.6 |
| +5   | 7.7  | 236.7 |
| cb   | 7.6  | 236.8 |
| 1/4  | 7.7  | 236.7 |
| 2    | 7.2  | 237.2 |
| 1/4  | 7.0  | 237.4 |

T  
24439

32

|      |      |       |
|------|------|-------|
| cb   | 7.0  | 237.4 |
| +6   | 6.2  | 238.2 |
| E    | 5.7  | 238.7 |
| 2745 |      |       |
| E    | 6.7  | 237.7 |
| cb   | 8.0  | 236.4 |
| 1/4  | 8.0  | 236.4 |
| 2    | 8.2  | 236.2 |
| 1/4  | 8.8  | 235.6 |
| +3   | 8.4  | 236.0 |
| cb   | 8.8  | 235.6 |
| +5   | 9.0  | 235.4 |
| W    | 10.3 | 234.1 |
| +7   | 11.5 | 232.9 |
| +20  | 13.0 | 231.4 |
| 2750 |      |       |
| -20  | 13.0 | 231.4 |
| W    | 11.6 | 232.8 |
| +4   | 11.6 | 232.8 |
| +7   | 8.9  | 235.5 |

24439

|     |     |       |
|-----|-----|-------|
| cb  | 9.1 | 235.3 |
| +7  | 8.6 | 235.8 |
| 1/4 | 9.0 | 235.4 |
| ϕ   | 8.5 | 235.9 |
| 1/4 | 8.4 | 236.0 |
| cb  | 8.0 | 236.0 |
| E   | 6.8 | 237.6 |

2451<sup>3</sup> Top of Wall

Top 67 Wall 10.07 234.32

2470

|     |      |       |
|-----|------|-------|
| E   | 8.2  | 236.2 |
| cb  | 9.5  | 234.9 |
| 1/4 | 9.7  | 234.7 |
| ϕ   | 9.8  | 234.6 |
| 1/4 | 10.0 | 234.4 |
| cb  | 10.5 | 233.9 |
| +   | 10.4 | 234.0 |
| +   | 11.9 | 232.5 |
| W   | 11.9 | 232.5 |
| +10 | 12.2 | 232.2 |
| +20 | 14.5 | 229.9 |

8.20  
10.30

24739

33

2479<sup>2</sup> See sketch

|                      |       |        |
|----------------------|-------|--------|
| Top Wall on Pop Line | 10.30 | 234.05 |
| " " 47 E of Pop      | 8.20  | 236.19 |

2480

|                       |      |        |
|-----------------------|------|--------|
| Ground at Base Pillar | 12.2 | 232.2  |
| Top 2x2 pillar        | 5.39 | 239.00 |

2482

|      |      |       |
|------|------|-------|
| W-20 | 16.1 | 228.3 |
| W-10 | 13.2 | 231.2 |
| K1   | 12.7 | 231.7 |
| cb   | 11.0 | 233.4 |
| 1/4  | 10.6 | 233.8 |
| ϕ    | 10.5 | 233.9 |
| 1/4  | 10.3 | 234.1 |
| cb   | 10.0 | 234.4 |
| E    | 8.8  | 235.6 |

2493 Gilt Plate Edge 15' from Mine

2495 B.C.

|      |      |       |
|------|------|-------|
| E-10 | 10.4 | 234.0 |
| E    | 10.3 | 234.1 |
| cb   | 10.4 | 234.0 |

T  
24439

|      |      |               |             |
|------|------|---------------|-------------|
| 1/2  |      | 10.8          | 233.6       |
| 2    |      | 11.2          | 233.2       |
| 1/4  |      | 11.5          | 232.9       |
| cb   |      | 12.1          | 232.3       |
| +11  |      | 12.7          | 231.7       |
| W    |      | 13.4          | 231.0       |
| +10  |      | 15.1          | 229.3       |
| +20  |      | 16.7          | 227.7       |
| T.P. | 1.80 | <u>233.55</u> | 1264 231.75 |
|      |      | 3+10          |             |
| W-20 |      | 7.4           | 226.2       |
| -6   |      | 5.4           | 228.2       |
| W    |      | 4.1           | 229.5       |
| +3   |      | 3.1           | 230.5       |
| cb   |      | 2.9           | 230.7       |
| 1/4  |      | 2.2           | 231.4       |
| 2    |      | 1.9           | 231.7       |
| 1/4  |      | 1.7           | 231.9       |
| cb   |      | 1.2           | 232.4       |
| E    |      | 0.5           | 233.1       |
| +10  |      | 0.7           | 232.9       |

cb+5  
3+12 D.M.

T  
23355

34

3+12 G+LT D.M.

|      |  |                 |       |
|------|--|-----------------|-------|
|      |  | 17' from W Line |       |
|      |  | 3+25            |       |
| E-10 |  | 2.6             | 231.0 |
| F    |  | 2.8             | 230.8 |
| cb   |  | 3.3             | 230.3 |
| 1/4  |  | 3.9             | 229.7 |
| 2    |  | 4.2             | 229.4 |
| 1/4  |  | 4.3             | 229.3 |
| cb   |  | 4.3             | 229.3 |
| +7   |  | 4.6             | 229.0 |
| W    |  | 6.2             | 227.4 |
| +20  |  | 7.8             | 225.8 |
|      |  | 3+40            |       |
| -20  |  | 9.9             | 223.7 |
| W    |  | 8.0             | 225.6 |
| +9   |  | 6.6             | 227.0 |
| cb   |  | 6.4             | 227.2 |
| 1/4  |  | 6.6             | 227.0 |
| 2    |  | 6.5             | 227.1 |
| 1/4  |  | 6.3             | 227.3 |

T  
223.55

|     |     |       |
|-----|-----|-------|
| cb  | 6.0 | 227.6 |
| E   | 6.1 | 227.5 |
| +10 | 6.4 | 227.2 |

3+55

|     |      |       |
|-----|------|-------|
| -10 | 9.2  | 224.4 |
| E   | 8.7  | 224.9 |
| cb  | 8.9  | 224.7 |
| 1/4 | 8.9  | 224.7 |
| £   | 9.1  | 224.5 |
| 1/4 | 9.2  | 224.4 |
| cb  | 9.2  | 224.4 |
| W   | 10.4 | 223.2 |
| +10 | 11.0 | 222.6 |

3+70

|      |      |       |
|------|------|-------|
| W-10 | 13.0 | 220.6 |
| W    | 12.8 | 220.8 |
| cb   | 12.4 | 221.2 |
| 1/4  | 12.2 | 221.4 |
| £    | 12.1 | 221.5 |
| 1/4  | 11.8 | 221.8 |

T  
223.55

35

|     |  |      |       |
|-----|--|------|-------|
| cb  |  | 12.0 | 221.6 |
| E   |  | 11.7 | 221.9 |
| +10 |  | 12.3 | 221.3 |

|    |      |        |      |        |
|----|------|--------|------|--------|
| JP | 0.28 | 221.23 | 1260 | 220.95 |
|    |      | 3+85   |      |        |

|      |  |     |       |
|------|--|-----|-------|
| E-10 |  | 3.2 | 218.0 |
| E    |  | 3.0 | 218.2 |
| +6   |  | 2.3 | 218.9 |
| cb   |  | 2.7 | 218.5 |
| 1/4  |  | 2.3 | 218.9 |
| £    |  | 2.6 | 218.6 |
| 1/4  |  | 2.9 | 218.3 |
| cb   |  | 2.9 | 218.3 |
| +7   |  | 2.6 | 218.6 |
| W    |  | 2.7 | 218.5 |
| +10  |  | 2.8 | 218.4 |

3+91 Gold D. Man 3' E. of W line

|      |  |      |       |  |
|------|--|------|-------|--|
|      |  | 4+00 |       |  |
| W-10 |  | 4.4  | 216.8 |  |
| W    |  | 4.9  | 216.3 |  |

T  
221.23

|               |      |                                      |
|---------------|------|--------------------------------------|
| cb            | 5.3  | 215.9                                |
| 1/4           | 5.5  | 215.7                                |
| 2             | 5.6  | 215.6                                |
| 1/4           | 5.6  | 215.6                                |
| cb            | 5.3  | 215.9                                |
| E             | 5.9  | 215.8                                |
| +10           | 6.0  | 215.2                                |
|               | 4+16 | 4 E.C. 7.25 N of Skins, inside E.C.  |
| N-10          | 9.1  | 212.1                                |
| N             | 8.4  | 212.8                                |
| cb            | 8.0  | 213.2                                |
| 1/4           | 8.0  | 213.2                                |
| 2             | 7.9  | 213.3                                |
| 1/4           | 7.9  | 213.3                                |
| cb            | 7.6  | 213.6                                |
| +5            | 6.8  | 214.4                                |
| S on Cor. Mon | 6.63 | 214.60                               |
| +10           | 6.0  | 215.2                                |
|               | 4+24 | Single Garage on South<br>8' opening |
| 2             | 5.79 | 215.44                               |

T  
221.23

36

4+31

|      |                      |                                  |
|------|----------------------|----------------------------------|
| 5-5  | 7.5                  | 213.7                            |
| 5    | 8.1                  | 213.1                            |
| cb   | 9.4                  | 211.8                            |
| 1/4  | 9.8                  | 211.4                            |
| 2    | 9.5                  | 211.7                            |
| +5   | 8.8                  | 212.4                            |
| 1/4  | 9.1                  | 212.1                            |
| cb   | 9.5                  | 211.7                            |
| N    | 10.3                 | 210.9                            |
| +10  | 11.4                 | 209.8                            |
| +20  | 12.6                 | 208.6                            |
|      | 4+97                 | Stairway to Res. on South. 6.95. |
|      | Ground. 69. South    | 9.2 212.0                        |
|      | Concrete Bottom Step | 8.65 212.58                      |
|      | 4+50                 |                                  |
| N-20 | 15.6                 | 205.6                            |
| N    | 13.3                 | 207.9                            |
| cb   | 12.4                 | 208.8                            |
| 1/4  | 12.1                 | 209.1                            |
| 2    | 12.2                 | 209.0                            |
| 1/4  | 12.1                 | 209.1                            |

π  
221.23

|      |      |               |       |        |
|------|------|---------------|-------|--------|
| +3   |      |               | 12.0  | 209.2  |
| +6   |      |               | 11.5  | 209.7  |
| cb   |      |               | 11.3  | 209.9  |
| S    |      |               | 10.6  | 210.6  |
| +5   |      |               | 10.0  | 211.2  |
| TP   | 0.08 | <u>208.35</u> | 12.96 | 200.27 |
|      |      | 475           |       |        |
| S-10 |      |               | 1.5   | 206.9  |
| S    |      |               | 2.1   | 206.3  |
| cb   |      |               | 3.0   | 205.4  |
| +4   |      |               | 3.0   | 205.4  |
| 1/4  |      |               | 3.9   | 204.5  |
| £    |      |               | 4.2   | 204.2  |
| 1/4  |      |               | 4.6   | 203.8  |
| cb   |      |               | 4.4   | 204.0  |
| N    |      |               | 4.6   | 203.8  |
| +20  |      |               | 6.6   | 201.8  |
|      |      | 5100          |       |        |
| N-20 |      |               | 10.1  | 198.3  |

π  
20835

37

|     |      |               |       |        |
|-----|------|---------------|-------|--------|
| N   |      |               | 9.3   | 199.1  |
| cb  |      |               | 9.1   | 199.3  |
| 1/4 |      |               | 8.7   | 199.7  |
| £   |      |               | 8.7   | 199.7  |
| 1/4 |      |               | 8.6   | 199.8  |
| cb  |      |               | 7.6   | 200.8  |
| S   |      |               | 6.7   | 201.7  |
| +5  |      |               | 6.5   | 201.9  |
|     |      | 5130          |       |        |
| -5  |      |               | 11.3  | 197.1  |
| S   |      |               | 11.8  | 196.6  |
| cb  |      |               | 12.8  | 195.6  |
| 1/4 |      |               | 13.8  | 194.6  |
| £   |      |               | 14.0  | 194.4  |
| 1/4 |      |               | 14.2  | 194.2  |
| +2  |      |               | 13.4  | 195.0  |
| cb  |      |               | 13.5  | 194.9  |
| N   |      |               | 13.9  | 194.5  |
| +20 |      |               | 14.4  | 194.0  |
| TP  | 0.27 | <u>195.99</u> | 12.63 | 195.72 |



195.99

5755 to 5740<sup>3</sup> on N

See  
Sketch

|     |     |       |
|-----|-----|-------|
| N   | 4.6 | 191.4 |
| cb  | 4.5 | 191.5 |
| +8  | 3.8 | 192.2 |
| 1/4 | 3.9 | 192.1 |
| ¢   | 4.0 | 192.0 |
| 1/4 | 4.3 | 191.7 |
| cb  | 4.3 | 191.7 |
| S   | 3.4 | 192.6 |
| +2  | 2.2 | 193.8 |
| +5  | 2.2 | 193.8 |

E line of Winsby place 5765<sup>83</sup> to 5740<sup>3</sup> on N

# Note  
sections  
taken Disg.

|      |     |       |
|------|-----|-------|
| S-10 | 6.1 | 189.9 |
| S    | 5.2 | 190.8 |
| cb   | 5.9 | 190.1 |
| +3   | 6.1 | 189.9 |
| 1/4  | 5.4 | 190.6 |
| ¢    | 4.6 | 191.4 |
| 1/4  | 4.6 | 191.4 |
| cb   | 5.2 | 190.8 |
| N    | 4.6 | 191.4 |

195.99

5778<sup>6</sup> = 5753<sup>7</sup>

38

|     |      |       |
|-----|------|-------|
| N   | 6.2  | 189.8 |
| cb  | 6.0  | 190.0 |
| 1/4 | 5.6  | 190.4 |
| ¢   | 6.6  | 190.0 |
| 1/4 | 6.7  | 189.3 |
| cb  | 7.5  | 188.5 |
| S   | 8.3  | 187.7 |
| +10 | 10.0 | 186.0 |

5797.765 = 5773<sup>7</sup> N

|      |      |       |
|------|------|-------|
| S-10 | 11.5 | 184.5 |
| S    | 10.0 | 186.0 |
| +6   | 8.5  | 187.4 |
| cb   | 8.1  | 187.9 |
| 1/4  | 7.7  | 188.3 |
| ¢    | 7.3  | 188.7 |
| 1/4  | 7.2  | 188.8 |
| cb   | 7.2  | 188.8 |
| N    | 7.3  | 188.7 |
| +10  | 7.3  | 188.7 |

195.99

WCB  
6+10.55 = 5187.1N

|      |      |       |
|------|------|-------|
| -10  | 8.5  | 187.5 |
| N    | 8.8  | 187.2 |
| cb   | 8.3  | 187.7 |
| 1/4  | 8.3  | 187.7 |
| 2    | 8.6  | 187.4 |
| 1/4  | 9.1  | 186.9 |
| cb   | 9.5  | 186.5 |
| S    | 11.2 | 184.8 |
| +10  | 12.9 | 183.1 |
| S-10 | 13.3 | 182.7 |
| S    | 12.6 | 183.4 |
| +5   | 11.2 | 184.8 |
| cb   | 10.4 | 185.6 |
| 1/4  | 9.8  | 186.2 |
| 2    | 9.4  | 186.6 |
| 1/4  | 9.2  | 186.8 |
| cb   | 8.9  | 187.1 |
| N    | 9.1  | 186.9 |
| +10  | 9.3  | 186.7 |

6+27<sup>10</sup> S = 6+04 North

39

195.99

W Prop Line  
6+30.5 = 6+07 04N

|        |      |        |
|--------|------|--------|
| N-10   | 11.4 | 184.6  |
| N      | 11.7 | 184.3  |
| cb     | 11.0 | 185.0  |
| 1/4    | 11.2 | 184.8  |
| 2      | 11.5 | 184.5  |
| 1/4    | 11.2 | 184.8  |
| cb     | 11.6 | 184.4  |
| +8     | 12.0 | 184.0  |
| S      | 13.3 | 182.7  |
| +10    | 13.9 | 182.1  |
| Set BM | 0.42 | 184.68 |
| S      | 2.0  | 182.7  |
| +8     | 1.3  | 183.4  |
| cb     | 2.2  | 182.5  |
| 1/4    | 2.9  | 181.8  |
| 2      | 2.9  | 181.8  |
| 1/4    | 3.0  | 181.7  |
| cb     | 3.4  | 181.3  |
| N      | 3.8  | 180.9  |
| +20    | 3.9  | 180.8  |

184.68  
6+30.10  
N-W Proj  
Mon Wins By  
+ Hut Top Line  
G. Lt Pole 7' from S. Line  
At angle to S Prop. Line

T  
18468

6+48

|      |     |       |
|------|-----|-------|
| N-20 | 5.8 | 178.9 |
| N    | 5.6 | 179.1 |
| cb   | 5.1 | 179.6 |
| 1/4  | 5.1 | 179.6 |
| £    | 5.9 | 178.8 |
| 1/4  | 5.8 | 178.9 |
| cb   | 4.7 | 180.0 |
| +7   | 3.3 | 181.4 |
| S    | 3.0 | 181.7 |
| +10  | 3.0 | 181.7 |
| +20  | 4.5 | 180.2 |
| 6+65 |     |       |
| S-20 | 7.4 | 177.3 |
| S    | 6.5 | 178.2 |
| cb   | 7.4 | 177.3 |
| 1/4  | 8.5 | 176.2 |
| £    | 8.4 | 176.3 |
| 1/4  | 7.6 | 177.1 |
| cb   | 7.4 | 177.3 |
| N    | 7.9 | 176.8 |

T  
18468

40

|      |      |       |
|------|------|-------|
| +20  | 8.8  | 175.9 |
| 6+71 |      |       |
| N-20 | 9.6  | 175.1 |
| N    | 8.8  | 175.9 |
| cb   | 8.9  | 175.8 |
| 1/4  | 9.3  | 175.4 |
| £    | 9.8  | 174.9 |
| 1/4  | 9.3  | 175.4 |
| cb   | 8.0  | 176.7 |
| S    | 6.8  | 177.9 |
| +20  | 9.0  | 175.7 |
| 6+85 |      |       |
| -20  | 11.7 | 173.0 |
| S    | 11.1 | 173.6 |
| cb   | 11.9 | 172.8 |
| 1/4  | 13.2 | 171.5 |
| £    | 13.7 | 171.0 |
| 1/4  | 13.5 | 171.2 |
| cb   | 12.9 | 171.8 |
| N    | 11.1 | 173.6 |
| +6   | 10.2 | 174.5 |

$\pi$   
184.68

6+85

|        |      |        |       |        |
|--------|------|--------|-------|--------|
| N+20   |      |        | 10.6  | 174.1  |
| T.P.   | 0.43 | 172.29 | 12.82 | 171.86 |
| N+20   |      | 7+00   | 0.1   | 172.2  |
| N.     |      |        | 1.5   | 170.8  |
| cb     |      |        | 5.6   | 166.7  |
| +9     |      |        | 6.5   | 165.8  |
| 1/4    |      |        | 6.9   | 165.4  |
| $\phi$ |      |        | 7.0   | 165.3  |
| 1/4    |      |        | 6.1   | 166.2  |
| cb     |      |        | 5.0   | 167.3  |
| S      |      |        | 4.6   | 167.7  |
| +20    |      |        | 2.2   | 170.1  |

7+15

|        |  |  |      |       |
|--------|--|--|------|-------|
| S-20   |  |  | 6.9  | 165.4 |
| S      |  |  | 10.3 | 162.0 |
| cb     |  |  | 11.7 | 160.6 |
| 1/4    |  |  | 13.0 | 159.3 |
| $\phi$ |  |  | 14.2 | 158.1 |
| 1/4    |  |  | 14.4 | 157.9 |
| cb     |  |  | 10.5 | 161.8 |

$\pi$   
172.29

41

|        |      |        |       |        |
|--------|------|--------|-------|--------|
| N      |      |        | 7.6   | 164.7  |
| +10    |      |        | 5.9   | 166.4  |
| +20    |      |        | 5.4   | 166.9  |
| JP     | 0.70 | 159.90 | 13.09 | 159.20 |
|        |      | 7+40   |       |        |
| N-20   |      |        | 2.9   | 157.0  |
| N      |      |        | 5.1   | 154.8  |
| cb     |      |        | 6.6   | 153.3  |
| 1/4    |      |        | 7.8   | 152.1  |
| $\phi$ |      |        | 8.6   | 151.3  |
| 1/4    |      |        | 8.8   | 151.1  |
| cb     |      |        | 7.8   | 152.1  |
| S      |      |        | 6.1   | 153.8  |
| +20    |      |        | 5.1   | 154.8  |
|        |      | 7+50   |       |        |
| -20    |      |        | 9.0   | 150.9  |
| S      |      |        | 9.8   | 150.1  |
| +4     |      |        | 10.8  | 149.1  |
| cb     |      |        | 11.6  | 148.3  |
| 1/4    |      |        | 12.0  | 147.9  |

139.90

|     |      |       |
|-----|------|-------|
| £   | 11.8 | 148.1 |
| 1/4 | 11.2 | 148.7 |
| cb  | 10.2 | 149.7 |
| N   | 8.5  | 151.4 |
| +20 | 7.0  | 152.9 |

7+70

|     |      |       |
|-----|------|-------|
| -20 | 16.5 | 143.4 |
| N   | 17.6 | 142.3 |
| cb  | 17.4 | 142.5 |
| 1/4 | 17.1 | 142.8 |
| £   | 17.3 | 142.6 |
| 1/4 | 18.9 | 141.0 |
| cb  | 18.9 | 141.0 |
| S   | 18.3 | 141.6 |
| +20 | 16.9 | 143.0 |

|    |      |               |       |        |
|----|------|---------------|-------|--------|
| TP | 0.50 | <u>147.51</u> | 12.89 | 147.01 |
|----|------|---------------|-------|--------|

7+85

|      |      |       |
|------|------|-------|
| S-20 | 9.2  | 138.3 |
| S    | 9.6  | 137.9 |
| cb   | 10.5 | 137.0 |

147.51

42

|     |      |       |
|-----|------|-------|
| 1/4 | 10.2 | 137.3 |
| £   | 10.3 | 137.2 |
| 1/4 | 10.4 | 137.1 |
| cb  | 11.4 | 136.1 |
| N   | 11.1 | 136.4 |
| +20 | 11.8 | 135.7 |

|    |      |               |       |        |
|----|------|---------------|-------|--------|
| TP | 0.37 | <u>136.80</u> | 11.08 | 136.93 |
|----|------|---------------|-------|--------|

8+00

|     |     |       |
|-----|-----|-------|
| -20 | 3.8 | 133.0 |
| N   | 3.6 | 133.2 |
| cb  | 3.3 | 133.5 |
| 1/4 | 2.5 | 134.3 |
| £   | 2.1 | 134.7 |
| 1/4 | 2.3 | 134.5 |
| cb  | 2.0 | 134.8 |
| S   | 1.5 | 135.3 |
| +20 | 1.0 | 135.8 |

8+30

|      |     |       |
|------|-----|-------|
| S-20 | 2.4 | 134.4 |
| S    | 3.4 | 133.4 |
| cb   | 4.5 | 132.3 |

T  
136.80

|     |     |       |
|-----|-----|-------|
| 1/4 | 5.5 | 131.3 |
| £   | 5.0 | 131.8 |
| 1/4 | 5.2 | 131.6 |
| cb  | 5.5 | 131.3 |
| N   | 5.7 | 131.1 |
| +20 | 5.7 | 131.1 |

8+50

|     |     |       |
|-----|-----|-------|
| -20 | 6.1 | 130.7 |
| N   | 6.1 | 130.7 |
| cb  | 6.1 | 130.7 |
| 1/4 | 6.0 | 130.8 |
| £   | 5.8 | 131.0 |
| 1/4 | 5.9 | 130.9 |
| cb  | 5.1 | 131.7 |
| S   | 4.4 | 132.4 |
| +20 | 3.3 | 133.5 |

8+60 Gas + LI Pole

8.2 N of Skine

8+88 Gas Lt D Man

8.2 N of S Line

T  
136.80

43

8+89<sup>2</sup> E Line of Elwood on North

|     |     |       |
|-----|-----|-------|
| -10 | 6.3 | 130.5 |
| S   | 6.5 | 130.3 |
| cb  | 6.9 | 129.9 |
| 1/4 | 7.3 | 129.5 |
| £   | 7.0 | 129.8 |
| 1/4 | 7.0 | 129.8 |
| cb  | 6.9 | 129.9 |
| N   | 7.0 | 129.8 |
| +10 | 7.0 | 129.8 |

TP. 3.99 134.51 6.28 130.52

see sketch

9+20<sup>3</sup> Begin Walk Road cb of South

|          |      |        |
|----------|------|--------|
| -10      | 4.7  | 129.8  |
| N        | 4.7  | 129.8  |
| cb       | 4.8  | 129.7  |
| 1/4      | 5.1  | 129.4  |
| £        | 5.0  | 129.5  |
| 1/4      | 5.3  | 129.2  |
| S        | 5.2  | 129.3  |
| Topex cb | 5.24 | 129.27 |

T  
134.57

|       |  |        |
|-------|--|--------|
| +6.5  | 520                                      | 129.31 |
| +10.5 | 509                                      | 129.42 |
| S     | 50                                       | 129.5  |
| +5    | 50                                       | 129.5  |
|       | 3+60 <sup>24</sup> W line of Elwood on N |        |
| S-5   | 5.5                                      | 129.0  |
| S     | 55                                       | 129.0  |
| +15   | 561                                      | 128.90 |
| +65   | 576                                      | 128.75 |
| cb    | 576                                      | 128.75 |
| G     | 58                                       | 128.7  |
| 14    | 5.8                                      | 128.7  |
| ¢     | 5.5                                      | 129.0  |
| 14    | 5.3                                      | 129.2  |
| cb    | 5.1                                      | 129.4  |
| N     | 50                                       | 129.5  |
| +5    | 4.8                                      | 129.7  |
|       | 3+76                                     |        |
| -10   | 50                                       | 129.5  |
| N     | 5.1                                      | 129.4  |

T  
134.51

44

|           |      |        |
|-----------|------|--------|
| cb        | 5.4  | 129.1  |
| 14        | 5.4  | 129.1  |
| +7        | 52   | 129.3  |
|           | 59   | 128.6  |
| 14        | 62   | 128.3  |
| +6        | 5.8  | 128.7  |
| G         | 58   | 128.7  |
| Top ex cb | 6.03 | 128.48 |
| +5.5      | 575  | 128.76 |
| +10.5     | 585  | 128.66 |
| S         | 59   | 128.6  |
| +5        | 5.8  | 128.7  |
|           | 3+78 |        |
| S-5       | 5.8  | 128.7  |
| S         | 59   | 128.6  |
| cb        | 5.8  | 128.7  |
| +4        | 5.8  | 128.7  |
| 14        | 62   | 128.3  |
| ¢         | 59   | 128.6  |
| +7        | 5.4  | 129.1  |

T  
134.51

|        |     |              |      |        |
|--------|-----|--------------|------|--------|
| 1/4    |     |              | 54   | 129.1  |
| cb     |     |              | 54   | 129.1  |
| +9     |     |              | 54   | 129.1  |
| N      |     |              | 7.9  | 126.6  |
| T.P.   | 686 | <u>13451</u> | 6.86 | 127.65 |
|        |     | 9490         |      |        |
| N-20   |     |              | 7.6  | 126.9  |
| N      |     |              | 7.9  | 126.6  |
| cb     |     |              | 7.9  | 126.6  |
| 1/4    |     |              | 7.2  | 127.3  |
| +4     |     |              | 5.6  | 128.9  |
| +7     |     |              | 5.6  | 128.9  |
| £      |     |              | 6.5  | 128.0  |
| 1/4    |     |              | 6.6  | 127.9  |
| +5     |     |              | 5.9  | 128.6  |
| cb Grd |     |              | 6.1  | 128.4  |
| S      |     |              | 6.0  | 128.5  |
| +5     |     |              | 6.0  | 128.5  |
|        |     | 10+00        |      |        |
| S-5    |     |              | 6.2  | 128.3  |

T  
13451

45

|           |  |                    |              |        |
|-----------|--|--------------------|--------------|--------|
| S         |  |                    | 6.2          | 128.3  |
| +1.5      |  |                    | 6.21         | 128.30 |
| +6.5      |  |                    | 6.35         | 128.16 |
| cb on Grd |  |                    | 6.3          | 128.2  |
| Topex cb  |  |                    | 6.52         | 127.99 |
| +6        |  |                    | 6.2          | 128.3  |
| 1/4       |  |                    | 6.8          | 127.7  |
| £         |  |                    | 7.3          | 127.2  |
| 1/4       |  |                    | 7.9          | 126.6  |
| cb        |  |                    | 7.9          | 126.6  |
| N         |  |                    | 7.6          | 126.9  |
| +20       |  |                    | 7.2          | 127.3  |
|           |  | 10+25 <sup>5</sup> | End cb on S. |        |
| +20       |  |                    | 7.6          | 126.9  |
| N         |  |                    | 7.3          | 127.2  |
| cb        |  |                    | 8.2          | 126.3  |
| 1/4       |  |                    | 8.1          | 126.4  |
| £         |  |                    | 7.9          | 126.6  |
| 1/4       |  |                    | 8.2          | 126.3  |
| +6        |  |                    | 8.2          | 126.3  |



π  
13951

|              |      |        |
|--------------|------|--------|
| C6 9rd       | 6.9  | 127.6  |
| Top ex cb    | 7.07 | 127.44 |
| +55 Edgewalk | 6.78 | 127.73 |
| +10.5 " "    | 6.65 | 127.86 |
| S            | 6.6  | 127.9  |
| +5           | 6.5  | 128.0  |

10 +57<sup>5</sup> End walk on Scott

|               |      |        |
|---------------|------|--------|
| S-5           | 7.5  | 127.0  |
| S             | 7.0  | 127.5  |
| +1.5 Edgewalk | 6.86 | 127.65 |
| +6.5 " "      | 7.08 | 127.43 |
| cb            | 8.5  | 126.0  |
| 1/4           | 8.7  | 125.8  |
| ⊕             | 8.7  | 125.8  |
| 1/4           | 8.4  | 126.1  |
| cb            | 8.2  | 126.3  |
| N             | 7.9  | 126.6  |
| +20           | 8.1  | 126.4  |

10 +65

|      |     |       |
|------|-----|-------|
| N-20 | 8.1 | 126.4 |
|------|-----|-------|

π  
13951

10.2  
1100

46

|     |       |       |
|-----|-------|-------|
| N   | 8.5   | 126.0 |
| cb  | 8.6   | 125.9 |
| 1/4 | 8.5   | 125.9 |
| ⊕   | 8.9   | 125.6 |
| 1/4 | 8.8   | 125.7 |
| cb  | 8.2   | 126.3 |
| S   | 8.3   | 126.2 |
| +10 | 7.3   | 127.2 |
|     | 11+00 |       |
| -10 | 8.2   | 126.3 |
| S   | 8.9   | 125.6 |
| cb  | 8.8   | 133.7 |
| 1/4 | 9.1   | 125.4 |
| ⊕   | 9.2   | 125.3 |
| 1/4 | 9.7   | 124.8 |
| +6  | 8.6   | 125.9 |
| cb  | 8.3   | 126.2 |
| N   | 8.2   | 126.3 |
| +20 | 7.4   | 127.1 |

1101 Gas + Lite Pole

102 N of S Line

T  
134.51

11+03

|      |       |       |
|------|-------|-------|
| N-20 | 9.4   | 125.1 |
| N    | 9.4   | 125.1 |
| cb   | 9.6   | 124.9 |
| 1/4  | 9.8   | 124.7 |
| ϕ    | 9.2   | 125.3 |
| 1/4  | 9.1   | 125.4 |
| t-2  | 9.9   | 124.6 |
| cb   | 9.8   | 124.7 |
| t-1  | 8.8   | 125.7 |
| S    | 8.7   | 125.8 |
| t-20 | 9.0   | 125.5 |
|      | 11+20 |       |
| S-20 | 9.1   | 125.4 |
| -10  | 8.7   | 125.8 |
| S    | 10.1  | 124.4 |
| t-3  | 10.8  | 123.7 |
| cb   | 10.3  | 124.2 |
| 1/4  | 9.1   | 125.4 |
| ϕ    | 9.4   | 125.1 |
| 1/4  | 9.6   | 124.9 |

T  
134.51

47

|      |       |       |
|------|-------|-------|
| cb   | 8.9   | 125.6 |
| N    | 8.9   | 125.6 |
| t-10 | 8.6   | 125.9 |
| t-20 | 8.5   | 126.0 |
|      | 11+50 |       |
| N-20 | 8.5   | 126.0 |
| N    | 8.9   | 125.6 |
| cb   | 9.2   | 125.3 |
| 1/4  | 9.4   | 125.1 |
| ϕ    | 8.9   | 125.6 |
| 1/4  | 8.7   | 125.8 |
| t-5  | 10.6  | 123.9 |
| cb   | 10.6  | 123.9 |
| S    | 10.7  | 123.8 |
| t-10 | 10.3  | 124.2 |
| t-20 | 10.8  | 123.7 |
|      | 11+74 |       |
| -20  | 10.7  | 123.8 |
| -7   | 10.3  | 124.2 |
| S    | 10.3  | 124.2 |

T  
13451

|     |       |       |
|-----|-------|-------|
| cb  | 10.1  | 124.4 |
| +6  | 7.5   | 127.0 |
| 1/4 | 7.7   | 126.8 |
| ±   | 8.1   | 126.4 |
| 1/4 | 8.6   | 125.9 |
| cb  | 8.9   | 125.6 |
| N   | 9.1   | 125.4 |
| +20 | 9.0   | 125.5 |
|     | 11+77 |       |
| -20 | 6.9   | 127.6 |
| N   | 7.0   | 127.5 |
| cb  | 7.2   | 127.3 |
| 1/4 | 7.3   | 127.2 |
| ±   | 7.8   | 126.7 |
| 1/4 | 7.4   | 127.1 |
| +5  | 7.3   | 127.2 |
| cb  | 8.9   | 125.6 |
| +8  | 10.2  | 124.3 |
| S   | 10.4  | 124.1 |
| +20 | 10.7  | 123.8 |

T  
13451

48

11+82

|     |       |       |
|-----|-------|-------|
| -20 | 10.9  | 123.6 |
| -12 | 10.2  | 124.3 |
| -3  | 10.5  | 124.0 |
| ±   | 8.2   | 126.3 |
| cb  | 7.0   | 127.5 |
| +4  | 6.4   | 128.1 |
| 1/4 | 6.7   | 127.8 |
| ±   | 6.7   | 127.8 |
| 1/4 | 7.4   | 127.1 |
| cb  | 7.2   | 127.3 |
| N   | 7.1   | 127.4 |
| +20 | 7.1   | 127.4 |
|     | 12+00 |       |
| -20 | 3.2   | 131.3 |
| -12 | 5.3   | 129.2 |
| N   | 7.2   | 127.3 |
| cb  | 6.9   | 127.6 |
| 1/4 | 7.0   | 127.5 |
| +4  | 4.6   | 129.9 |
| ±   | 4.4   | 130.1 |
| 1/4 | 4.8   | 129.7 |

T  
134.51

|      |       |               |             |
|------|-------|---------------|-------------|
| +5   |       | 4.9           | 129.6       |
| cb   |       | 6.8           | 127.7       |
| +3   |       | 7.3           | 127.2       |
| S    |       | 7.9           | 126.6       |
| +20  |       | 8.6           | 125.9       |
|      | 12+38 |               |             |
| S-20 |       | 8.0           | 126.5       |
| S    |       | 7.3           | 127.2       |
| +7   |       | 6.5           | 128.0       |
| cb   |       | 3.4           | 131.1       |
| +6   |       | 0.6           | 133.9       |
| T.P. | 7.01  | <u>140.95</u> | 0.57 133.94 |
| 1/4  |       | 6.6           | 134.4       |
| ¢    |       | 6.3           | 134.7       |
| +8   |       | 6.5           | 134.5       |
| 1/4  |       | 6.9           | 134.1       |
| cb   |       | 10.9          | 130.1       |
| N    |       | 9.1           | 131.9       |
| +13  |       | 7.8           | 133.2       |
| +20  |       | 6.9           | 134.1       |

T  
140.95

49

12+49 <sup>95 on 5 =</sup> 12+50.72 on N.

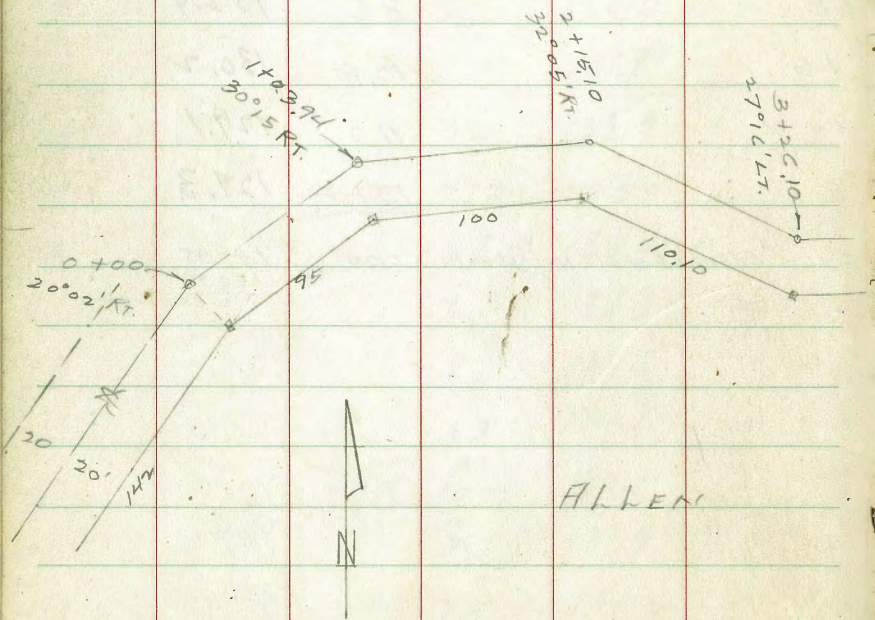
|  |             |      |                                       |
|--|-------------|------|---------------------------------------|
| N-20   |             | 3.8  | 137.2                                 |
| Set BM   | Ground Same |      |                                       |
| N.E. on con. Prop. Mon                             |             | 6.35 | 134.60                                |
| cb   |             | 7.4  | 133.6                                 |
| 1/4  |             | 4.6  | 136.4                                 |
| +2   |             | 4.1  | 136.9                                 |
| ¢  |             | 4.5  | 136.5                                 |
| 1/4  |             | 4.6  | 136.4                                 |
| +3   |             | 4.5  | 136.5                                 |
| cb   |             | 8.6  | 132.4                                 |
| +6   |             | 10.8 | 130.2                                 |
| +11  |             | 11.9 | 129.1                                 |
| S  |             | 13.7 | 129.3                                 |
| check End of cb. on 51 <sup>st</sup> N of Roswell. | 0.00        |      | <u>140.95</u><br>140.98<br>0.03 error |

Prelim Survey of Carriere Rd.  
thru Allen's Dairy to Camino del Rio

Moore  
Road  
Evel Moore  
12-15-41.

SEE MAP 5500

Save to p 60



BDRY MAP 1620

ALLEN

TERRACE

#1620

Save to P Co.

The image shows an open notebook with two facing pages. Both pages are cream-colored and feature horizontal blue lines for writing. Vertical red lines create margins on both sides of each page. The right page is numbered '52' in the upper right corner. The notebook is bound in the center, and the pages appear slightly aged with some minor blemishes. The notebook is placed on a white surface.





The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. Each page has a red vertical margin line on the left side (for the left page) and a red vertical margin line on the right side (for the right page). The pages are numbered '53' in the top left corner and '54' in the top right corner. The notebook is bound in the center, and the pages are otherwise blank.







The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. Vertical red lines create margins on both sides of each page. The right page has the number '58' printed in red in the top right corner. The notebook is placed on a white surface, and a portion of another notebook is visible at the bottom edge.



Cross Section 706 N  
 Amberst St South 300  
 See Sketch # 1623 Page 12

Indexed  
 C.S.N.

Feb 26-43  
 Sisson  
 Workman  
 H Moore

E  
 Lt

Δ

W

Rt

60

170

0+97 = 70' 2 Ribbar Core Drive ext N Ribbar 30 S Ribbar 20

0+76 = 30 Core Walk of H ↓

TP 9.83 468.75 7.62 458.97

2 Feb  
 Amberst  
 702254  
 45227

0+50

0+02 204 Rt of S = NY Mill Ford ↓

0+0 = S.L. Amberst

466.54 Rt Ford From # 1623 Page 12

Reduced & Plotted on Profile  
 2505 3-4-42 C.B.H.

461.9 461.8 461.6 461.7 462.1 261.6 461.0 460.8  
 6.9 7.0 7.2 6.9 6.7 7.2 7.8 8.0  
 30 20 15 10-11-10.1 10-11-10.1 20 30

461.05 461.73  
 6.70 7.22  
 30-11-10.1 10-11-10.1

461.91 461.81  
 6.78 6.74  
 30-11-10.1 10-11-10.1

468.75

461.5 461.3 460.8 461.0 461.2 460.5 460.7 460.7 460.3  
 5.0 5.2 5.7 5.5 5.3 6.0 5.8 5.8 6.8  
 30 20 15 8-11-10.1 11-11-10.1 13 20 30

460.4 460.1 460.5 460.5 459.8 459.8 459.5  
 6.1 6.4 6.0 6.0 6.7 6.7 7.0  
 30 13 5-11-10.1 17-11-10.1 20 30

466.54

2+0

2+74 190 Rt of  $\frac{1}{2}$  = NY Power Pole

2+50

2+0

1+55 197 Rt of  $\frac{1}{2}$  = NY Power + Tail Pole ✓

1+50

1+48 192 Lt of  $\frac{1}{2}$  = NY 12 Foot Tree = NY Row ✓1+05 215 Lt of  $\frac{1}{2}$  = NY Row Elec Tree ✓

468.75

Lt

R

Rt

61

|      |      |      |           |      |            |      |      |      |      |
|------|------|------|-----------|------|------------|------|------|------|------|
| 4688 | 4673 | 4659 | 4660      | 4660 | 4656       | 4653 | 4678 | 4670 | 4664 |
| 20   | 15   | 29   | 28        | 28   | 32         | 35   | 10   | 18   | 31   |
|      |      | 12   | 9 = F/Oil |      | 10 = F/Oil | 12   | 16   | 20   | 30   |

|      |      |      |           |      |            |      |      |      |      |
|------|------|------|-----------|------|------------|------|------|------|------|
| 4668 | 4664 | 4649 | 4651      | 4653 | 4648       | 4647 | 4658 | 4659 | 4653 |
| 20   | 24   | 32   | 37        | 35   | 40         | 41   | 30   | 29   | 35   |
| 20   | 14   | 12   | 9 = F/Oil |      | 10 = F/Oil | 12   | 16   | 20   | 30   |

|      |      |      |      |           |      |            |      |      |      |      |
|------|------|------|------|-----------|------|------------|------|------|------|------|
| 4647 | 4643 | 4640 | 4635 | 4640      | 4642 | 4639       | 4636 | 4640 | 4637 | 4635 |
| 41   | 45   | 48   | 53   | 48        | 46   | 49         | 52   | 48   | 51   | 50   |
| 30   | 20   | 14   | 12   | 9 = F/Oil |      | 10 = F/Oil | 13   | 15   | 20   | 30   |

|      |      |      |           |      |            |      |      |      |
|------|------|------|-----------|------|------------|------|------|------|
| 4630 | 4638 | 4625 | 4628      | 4631 | 4626       | 4621 | 4617 | 4615 |
| 58   | 53   | 63   | 60        | 57   | 67         | 67   | 71   | 72   |
| 30   | 20   | 15   | 9 = F/Oil |      | 10 = F/Oil | 13   | 20   | 30   |

468.75



Cross Section 6516 St.  
 E/Cajon to Amberst St

indexed  
 C.S.R.

See Sketch #1623 Page 12

1+59 277 Rt of L = Nly Power Pole ✓

1+40 = Sly Curb on Rt

1+0

0+50

0+06 232 Lt of L = Ely T&I Pole ✓  
 228 Rt of L = Nly Power Pole ✓

0+0 = S.L. E/Cajon

0-14 = South Curb Line E/Cajon

BM 310 459.85 456.75

Reduced & Plotted Profile # R506 C.B.H.

456.81  
 456.808  
 3.04 3.82  
 65-cb 65-guth

548P  
 E/Cajon #  
 69757

L.F

Rt. W

F2

|           |                 |              |            |           |            |                   |                  |                 |               |        |         |        |
|-----------|-----------------|--------------|------------|-----------|------------|-------------------|------------------|-----------------|---------------|--------|---------|--------|
| 454.7     | 454.8           | 454.6        | 454.6      | 454.9     | 454.7      | 454.4             | 454.87           | 455.9           | 455.00        |        |         |        |
| 5.2<br>10 | 5.0<br>10       | 5.0<br>20    | 5.0<br>10  | 5.0       | 5.2<br>10  | 5.5<br>20-guth    | 4.98<br>20-cb    | 4.9<br>30       | 4.85<br>30-cb |        |         |        |
| 454.9     | 454.7           | 454.9        | 454.7      | 454.8     | 455.1      | 455.0             | 454.6            | 455.23 ✓        | 455.2         |        |         |        |
| 5.0<br>10 | 5.2<br>30       | 5.0<br>20    | 5.2<br>17  | 5.0<br>10 | 4.8        | 4.9<br>10         | 5.3<br>20-guth   | 4.62<br>20-cb   | 4.7<br>30     |        |         |        |
| 455.4     | 455.2           | 455.4        | 455.0      | 455.0     | 455.5      | 455.5             | 455.1            | 455.78 ✓        | 455.8         |        |         |        |
| 4.5<br>10 | 4.7<br>30       | 4.5<br>20    | 4.9<br>17  | 4.9<br>17 | 4.4        | 4.1<br>10         | 4.8<br>19.9-guth | 4.07<br>19.9-cb | 4.1<br>30     |        |         |        |
| 456.7     | 456.99 ✓        | 455.02 ✓     | 455.66     | 455.93 ✓  | 455.88     | 455.66 ✓          | 456.33 ✓         | 456.6           |               |        |         |        |
| 3.2<br>30 | 3.36<br>20.8-cb | 4.83<br>20.8 | 4.19<br>10 | 3.92      | 3.97<br>10 | 4.19<br>19.8-guth | 3.52<br>19.8-cb  | 3.3<br>30       |               |        |         |        |
| 456.54    |                 |              |            |           |            |                   | 456.55           |                 |               |        |         |        |
| 3.31      |                 |              |            |           |            |                   | 3.30             |                 |               |        |         |        |
| Return    |                 |              |            |           |            |                   | Return           |                 |               |        |         |        |
| 456.71    | 456.91          | 456.68       | 456.33     | 456.29    | 456.18     | 455.23            | 456.16           | 456.10          | 456.08        | 456.74 | 456.10  | 456.77 |
| 3.10      | 4.55            | 3.17         | 3.52       | 3.56      | 3.69       | 3.62              | 3.69             | 3.75            | 3.77          | 3.11   | 3.75    | 3.08   |
| 40-cb     | 42.5            | 30-guth      | 30-guth    | 20        | 10         | 10                | 10               | 10              | 30-guth       | 30-cb  | 53-guth | 55-cb  |

459.85

BJM

5.98

453.87

072 Hub  
Amherst St  
467th St  
453.85

2+10 = 1/2 Amherst St

2+70 = 1/2 27 Conc Walk of Lt.

2+38 = 1/2 Garage Conc Floor of Lt

2+0

1+65 = 246 1/2 of 1/2 Fly Tel Pole

1+60 = S.L. Hwy

459.85

Lt.

S

Rt

63

|           |           |           |           |       |           |           |           |           |
|-----------|-----------|-----------|-----------|-------|-----------|-----------|-----------|-----------|
| 455.5     | 455.3     | 459.7     | 453.7     | 453.8 | 453.6     | 453.4     | 453.9     | 454.3     |
| 1.4<br>30 | 1.6<br>25 | 6.2<br>20 | 5.2<br>20 | 6.1   | 6.3<br>10 | 6.5<br>18 | 6.0<br>20 | 5.6<br>30 |

|            |            |           |           |           |       |           |           |           |           |           |
|------------|------------|-----------|-----------|-----------|-------|-----------|-----------|-----------|-----------|-----------|
| 455.62     | 455.66     | 454.0     | 453.9     | 454.1     | 454.2 | 453.9     | 453.4     | 454.1     | 454.4     | 453.6     |
| 4.23<br>40 | 4.19<br>27 | 5.9<br>20 | 6.0<br>20 | 5.8<br>18 | 5.7   | 6.0<br>10 | 6.5<br>17 | 5.8<br>20 | 5.5<br>30 | 5.3<br>40 |

|            |           |           |           |           |       |           |           |           |           |           |
|------------|-----------|-----------|-----------|-----------|-------|-----------|-----------|-----------|-----------|-----------|
| 454.6      | 455.1     | 454.9     | 454.1     | 454.2     | 454.5 | 454.1     | 453.7     | 454.5     | 454.5     | 453.8     |
| 4.09<br>57 | 4.8<br>40 | 5.0<br>30 | 5.8<br>20 | 5.7<br>10 | 5.4   | 5.8<br>10 | 6.2<br>18 | 5.4<br>20 | 5.4<br>30 | 6.1<br>40 |

|           |           |           |           |       |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-------|-----------|-----------|-----------|-----------|-----------|
| 454.5     | 454.2     | 454.3     | 454.0     | 454.6 | 454.3     | 453.9     | 454.5     | 454.7     | 454.4     |
| 5.4<br>10 | 5.7<br>30 | 5.6<br>20 | 5.6<br>12 | 5.3   | 5.6<br>10 | 5.0<br>17 | 5.4<br>20 | 5.7<br>30 | 5.5<br>40 |

|           |           |           |           |       |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-------|-----------|-----------|-----------|-----------|-----------|
| 454.7     | 454.6     | 454.8     | 454.4     | 454.8 | 454.6     | 454.4     | 455.0     | 455.2     | 454.8     |
| 5.2<br>10 | 5.3<br>30 | 5.1<br>20 | 5.5<br>12 | 5.1   | 5.3<br>10 | 5.5<br>18 | 5.7<br>20 | 5.7<br>30 | 5.1<br>40 |

459.85

Cross Section 6876 F/Cajon Blvd to  
Amberst St

Indexed  
C.S.K.

1735

1720

170

0750

0702

226 Pt of Is: w/ly Porcel Pale ✓

070 = SL F/Cajon

0-19 = SCB 121 of F/Cajon

BM

3.70

461.10

157.40

S.M. & P.  
F/Cajon 4  
68451

H-1

Δ

Pt-W

64

|          |          |          |         |         |      |          |          |          |          |          |      |      |
|----------|----------|----------|---------|---------|------|----------|----------|----------|----------|----------|------|------|
| A583     | A584     | A585     | A586    | A587    | A588 | A589     | A590     | A591     | A592     | A593     | A594 | A595 |
| 58<br>40 | 57<br>30 | 56<br>20 | 57<br>8 | 55<br>5 | 64   | 64<br>10 | 66<br>17 | 62<br>20 | 62<br>30 | 64<br>40 |      |      |

|          |          |          |         |         |      |          |          |          |          |          |
|----------|----------|----------|---------|---------|------|----------|----------|----------|----------|----------|
| A585     | A586     | A587     | A588    | A589    | A590 | A591     | A592     | A593     | A594     | A595     |
| 56<br>40 | 56<br>30 | 57<br>20 | 57<br>8 | 62<br>5 | 61   | 62<br>10 | 64<br>17 | 56<br>20 | 49<br>30 | 55<br>40 |

|          |          |          |         |         |      |          |          |          |          |          |
|----------|----------|----------|---------|---------|------|----------|----------|----------|----------|----------|
| A586     | A587     | A588     | A589    | A590    | A591 | A592     | A593     | A594     | A595     | A596     |
| 55<br>40 | 54<br>30 | 55<br>20 | 57<br>8 | 62<br>5 | 59   | 60<br>10 | 62<br>17 | 55<br>20 | 54<br>30 | 55<br>40 |

|          |          |          |          |          |      |          |          |          |          |
|----------|----------|----------|----------|----------|------|----------|----------|----------|----------|
| A589     | A586     | A583     | A580     | A585     | A586 | A586     | A588     | A589     | A589     |
| 42<br>40 | 45<br>30 | 48<br>20 | 61<br>12 | 56<br>10 | 55   | 55<br>15 | 53<br>20 | 52<br>30 | 52<br>40 |

|          |           |           |           |       |           |           |           |          |
|----------|-----------|-----------|-----------|-------|-----------|-----------|-----------|----------|
| A577     | A5716     | A5650     | A5680     | A5690 | A5674     | A5647     | A5707     | A571     |
| 34<br>30 | 374<br>20 | 460<br>20 | 430<br>10 | 420   | 436<br>10 | 463<br>20 | 403<br>20 | 40<br>30 |

|           |           |           |           |           |           |           |           |           |           |           |           |           |           |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|
| A5736     | A5715     | A5716     | A5705     | A5702     | A5701     | A5709     | A5708     | A5703     | A5688     | A5676     | A5741     | A5668     | A5733     |
| 374<br>20 | 374<br>20 | 374<br>20 | 408<br>30 | 409<br>20 | 401<br>10 | 402<br>10 | 402<br>10 | 407<br>10 | 422<br>20 | 435<br>30 | 369<br>30 | 444<br>30 | 377<br>55 |

461.15

3+10 - N. 2 Amberst St 28.0 Rt of L - S+ Fly 3' Hedge ✓

2+90

2+84 22.1 Rt of L - Wly Power Pole ✓

2+50 28.0 Rt of L - N+ Fly 20' Cypress Hedge ✓

2+42 20.0 Rt of L - S+ Fly 2' Hedge ✓

2+20 L 1.9 Conc Walk on Rt

2+0

1+91 20.3 Rt of L - N+ Fly 2' Hedge ✓

1+69 21.3 Rt of L - L Fire Hyd ✓

1+62 22.3 Rt of L - Wly Power 10' Pole ✓

1+60 - S. 2 Alley

46110

|  | Lt          |             | Rt       |          |
|--|-------------|-------------|----------|----------|
|  | 4520        | 4517        | 4517     | 4514     |
|  | 91<br>30    | 91<br>20    | 91<br>8  | 91<br>6  |
|  | 4518        | 4518        | 4520     | 4519     |
|  | 92<br>10    | 92<br>30    | 91<br>20 | 91<br>4  |
|  | 4526        | 4528        | 4528     | 4531     |
|  | 85<br>10    | 83<br>30    | 83<br>20 | 82<br>6  |
|  | 4528        | 4528        | 4525     | 4526     |
|  | 83<br>10    | 83<br>15    | 82<br>20 | 81<br>5  |
|  | 4539.4 ✓    | 454.00 ✓    |          |          |
|  | 716<br>22.5 | 710<br>36.0 |          |          |
|  | 4541        | 4543        | 4541     | 4542     |
|  | 70<br>10    | 68<br>30    | 70<br>20 | 69<br>6  |
|  | 4536        | 4539        | 4536     | 4541     |
|  | 72<br>10    | 72<br>18    | 71<br>20 | 70<br>30 |
|  | 4549        | 4551        | 4550     | 4551     |
|  | 62<br>10    | 60<br>30    | 61<br>20 | 60<br>8  |
|  | 4543        | 4543        | 4543     | 4548     |
|  | 68<br>10    | 68<br>18    | 68<br>20 | 67<br>30 |
|  | 4547        | 4546        |          |          |
|  | 64<br>10    | 65<br>10    |          |          |

46110  
W

Cross Section Olivest  
 Amberst St. to 300' South

Indexed  
 C.S.K.

1780

1750

170

0+60 = 7. Garage on 1st Conc Floor

0+50

0+29 19.8 ft of 2: My Porch + Tel. Pole

0+0 = 5L Amberst St 20 ft of 2: My High Fence

BM 2.60 453.63 10.07 451.03  
 161.10

Notes Red. Plot on Profile \* 2499 C.S.K.

2 Hubs  
 Amberst St  
 68' East  
 450.99

| Station | 4457     | 4457     | 4453              | 4455                            | 4456              | 4452             | 4455              | 4447     | 4446     |
|---------|----------|----------|-------------------|---------------------------------|-------------------|------------------|-------------------|----------|----------|
| 1780    | 79<br>30 | 79<br>20 | 83<br>12          | 81<br>9 = F Hole                | 80                | 84<br>9 = W Hole | 81<br>12          | 89<br>20 | 90<br>30 |
| 1750    | 4467     | 4461     | 4457              | 4456                            | 4459              | 4455             | 4458              | 4456     | 4459     |
|         | 69<br>30 | 75<br>20 | 81<br>15          | 80<br>9 = F Hole                | 77                | 81<br>9 = W Hole | 78<br>12          | 80<br>20 | 77<br>30 |
| 170     | 4480     | 4479     | 4460              | 4471                            | 4473              | 4471             | 4466              | 4474     | 4485     |
|         | 56<br>30 | 57<br>30 | 76<br>14          | 65<br>8 = F Hole                | 63                | 65<br>9 = W Hole | 70<br>16          | 62<br>20 | 51<br>30 |
|         |          |          |                   | V<br>450.02                     |                   |                  |                   |          |          |
|         |          |          |                   | 3.61<br>30 = 1.60<br>Conc Floor |                   |                  |                   |          |          |
| 0+50    | 449.5    | 449.1    | 449.1             | 4477                            | 4489              | 449.1            | 4487              | 4482     | 449.2    |
|         | 46<br>20 | 45<br>17 | 45<br>14          | 59<br>14                        | 47<br>8 = F Hole  | 45               | 49<br>10 = W Hole | 54<br>17 | 44<br>20 |
| 0+29    | 450.9    | 450.2    | 450.6             | 450.8                           | 450.9             | 4497             | 4498              |          |          |
|         | 27<br>20 | 34<br>12 | 30<br>10 = F Hole | 28                              | 36<br>12 = W Hole | 39<br>15         | 38<br>20          |          |          |
|         |          |          |                   | 453.63                          |                   |                  |                   |          |          |

370

2750

2725

2718.3 = Existing Double 24" Corrugated Culvert

2712 20.8 Rt of 1/2 wly Power Pole ✓

2710

453.63

Lt

Z

Rt

|          |          |          |                |       |                |          |          |          |          |
|----------|----------|----------|----------------|-------|----------------|----------|----------|----------|----------|
| 444.6    | 445.3    | 446.1    | 445.8          | 445.8 | 445.5          | 445.3    | 445.8    | 445.0    | 444.8    |
| 90<br>85 | 81<br>70 | 75<br>15 | 78<br>8-EH/101 | 78    | 81<br>10-w/101 | 83<br>13 | 78<br>15 | 86<br>20 | 88<br>30 |

|          |          |          |          |                |       |               |          |           |           |
|----------|----------|----------|----------|----------------|-------|---------------|----------|-----------|-----------|
| 444.6    | 445.4    | 445.3    | 445.5    | 445.6          | 445.4 | 444.9         | 445.1    | 442.1     | 440.6     |
| 90<br>85 | 82<br>70 | 77<br>15 | 81<br>12 | 80<br>8-EH/101 | 87    | 87<br>9-w/101 | 85<br>14 | 115<br>20 | 130<br>30 |

|          |          |          |          |                |       |               |          |           |           |
|----------|----------|----------|----------|----------------|-------|---------------|----------|-----------|-----------|
| 443.9    | 445.4    | 445.8    | 445.4    | 445.5          | 445.3 | 445.0         | 445.0    | 443.5     | 442.6     |
| 97<br>85 | 82<br>70 | 78<br>15 | 82<br>12 | 81<br>8-EH/101 | 83    | 86<br>9-w/101 | 85<br>12 | 101<br>20 | 110<br>30 |

↓ 442.36

↓ 440.80

1427  
27 = total  
Flux

1983  
199 = total  
Flux

|          |          |          |          |                |       |               |          |          |          |
|----------|----------|----------|----------|----------------|-------|---------------|----------|----------|----------|
| 443.9    | 444.8    | 445.7    | 445.3    | 445.5          | 445.5 | 445.1         | 445.4    | 444.0    | 444.0    |
| 97<br>80 | 88<br>70 | 79<br>15 | 83<br>12 | 81<br>0-EH/101 | 81    | 85<br>9-w/101 | 82<br>15 | 96<br>20 | 96<br>30 |

153.63

Cross Section 67th St  
 El Cajon Blvd to South of Amberst  
 See Sketch #1623 Page 11

Indexed  
 C.S.K.

0+85 22.6 ft of  $\frac{1}{2}$ " = 11 ft 12" Pepper Tree ✓  
 0+60  
 0+50  
 0+0 = 5' El Cajon on West  
 0-10.5 = 5 ft Full Width Paving Taken on Ground  
 0-29.4 = Line of Curb From West  
 0-37.36 = 5' El Cajon to East  
 BM 335 457.05 453.70

Notes Red. Plot 3-7-92 G.B.H.

J.M.B.P.  
 El Cajon  
 4-5-76

Feb 28 1942 Lt-E 2 Rt-W 68

|                                 |  |                     |                                 |                                 |                                 |                                    |                     |                     |                     |                                 |                                 |
|---------------------------------|--|---------------------|---------------------------------|---------------------------------|---------------------------------|------------------------------------|---------------------|---------------------|---------------------|---------------------------------|---------------------------------|
| 4510<br>60<br>40                | 4511 <sup>3</sup><br>58<br>30                | 452.5<br>45<br>30   | 452.0<br>50<br>12               | 452.17<br>488<br>7.5-54         | 4524.3<br>463                   | 452.21<br>484<br>7.4-54<br>12' Pav | 451.9<br>51<br>30   | 452.5<br>45<br>30   | 452.7<br>48<br>40   |                                 |                                 |
| 452.4<br>44<br>30               | 452.5<br>42<br>30                            | 452.1<br>49<br>11   | 452.32<br>472<br>7.6-54<br>Curb | 452.55<br>450                   | 452.35<br>470<br>7.4-54<br>Pav  | 451.9<br>51<br>30                  | 452.1<br>49<br>30   | 452.6<br>44<br>30   |                     |                                 |                                 |
| 454.50<br>255<br>30             | 453.6 <sup>7</sup><br>40<br>20               | 453.1<br>40<br>14   | 453.02<br>400<br>7.6-54<br>Pav  | 453.20<br>325                   | 452.98<br>407<br>7.4-54<br>Pav  | 452.7<br>412<br>16                 | 453.3<br>37<br>20   | 453.6<br>34<br>30   |                     |                                 |                                 |
| 453.34<br>391<br>19.2-54<br>Pav | 453.40<br>375<br>10                          | 453.43<br>362<br>10 | 453.30<br>375<br>10             | 452.84<br>411<br>19.2-54<br>Pav | 453.31<br>374<br>19.2-54<br>Pav | 453.68<br>327<br>10                | 453.61<br>344<br>20 | 453.45<br>360<br>20 | 453.24<br>381<br>20 | 453.09<br>376<br>40.5-54<br>Pav | 453.68<br>337<br>40.5-54<br>Pav |
| 454.13<br>493<br>50.2-54<br>Pav | 453.55 <sup>✓</sup><br>350<br>21.5-54<br>Pav | 453.81<br>321<br>20 | 453.89<br>316<br>10             | 453.91<br>314                   | 457.05                          |                                    |                     |                     |                     |                                 |                                 |

217278 = 11.4 Ambered on 11

2164 21.2 ft of 2 = 2 Fire Hyd. ✓

2151 23.2 ft of 2 = 11/4 1.5 Pepper Tree ✓

2150

2118 22.5 ft of 2 = 11/4 1.0 Pepper Tree ✓

210

1483 22.0 ft of 2 = 11/4 1.0 Pepper Tree ✓

1450 23.2 ft of 2 = 11/4 0.8 Pepper Tree ✓

TP 2.42 452.81 6.66 450.39

1429 22.6 ft of 2 = 11/4 1.0 or 1.0 ✓

1415 23.6 ft of 2 = 11/4 1.2 Pepper Tree ✓

140

457.05

L.

S.

Rt.

69

448.8

448.8

448.7

446.2

446.10

444.23

446.25

446.0

448.0

448.9

448.9

5.0

5.0

5.1

7.6

7.7

7.38

7.56

7.8

5.8

4.9

4.9

448.8

448.8

448.8

444.99

447.28

447.06

444.9

449.3

449.5

449.3

449.1

449.5

448.7

448.81

449.10

448.91

448.6

449.3

450.3

450.2

450.0

450.1

450.6

450.37

450.64

450.46

450.3

450.5

451.1

450.7

450.8

451.2

451.9

451.60

451.88

451.68

451.6

451.7

451.7

6.2

6.2

5.8

5.1

5.45

5.17

5.37

5.4

5.2

5.2

455.81

457.05



3758

3750

3743 230 Pt of  $\frac{1}{2}$  - WY 0.7 Pepper Tree ✓

37396 - SL Amberst on W

3722

3720 233 Pt of  $\frac{1}{2}$  - WY 1.0 Pepper Tree ✓

3790

3785 230 Pt of  $\frac{1}{2}$  - WY 0.8 Pepper Tree ✓

453.81

|  | 4         | 8      | R         |           |
|--|-----------|--------|-----------|-----------|
|  |           |        |           | 443.19    |
|  |           |        |           | 442.95    |
|  |           |        |           | 443.8     |
|  |           |        |           | 444.2     |
|  |           |        |           | 10.62     |
|  |           |        |           | 10.86     |
|  |           |        |           | 7.3-11/10 |
|  |           |        |           | 20        |
|  |           |        |           | 96        |
|  |           |        |           | 50        |
|  | 4490      | 4489   | 4483      | 4434      |
|  | 44324     | 44347  | 44332     | 4434      |
|  | 4495      | 4470   |           |           |
|  | 10.57     | 10.34  | 10.49     | 10.4      |
|  | 7.7-11/10 |        | 7.3-11/10 | 17        |
|  | 10.51     |        | 10.1      | 9.3       |
|  | 50        |        | 50        | 50        |
|  | 4491      | 4491   | 446.7     | 444.0     |
|  | 44380     | 444.09 | 44394     | 4442      |
|  | 4474      | 4476   |           |           |
|  | 10.01     | 9.72   | 9.87      | 9.6       |
|  | 7.7-11/10 |        | 7.3-11/10 | 17        |
|  | 10.01     |        | 9.6       | 6.4       |
|  | 50        |        | 50        | 50        |
|  | 4448      | 4444   | 4441      | 44421     |
|  | 44451     | 44434  | 444.5     | 448.3     |
|  | 448.1     |        |           |           |
|  | 9.0       | 9.1    | 9.2       | 9.6       |
|  | 7.7-11/10 |        | 7.7-11/10 | 9.20      |
|  | 9.0       |        | 9.49      | 9.3       |
|  | 50        |        | 7.3-11/10 | 16        |
|  |           |        | 5.5       | 5.5       |
|  |           |        | 50        | 57        |
|  |           |        | 50        | 50        |
|  | 4452      | 4452   | 445.43    | 445.72    |
|  | 445.53    | 445.6  | 448.8     | 448.7     |
|  | 8.8       | 8.6    | 8.38      | 8.28      |
|  | 7.7-11/10 |        | 7.3-11/10 | 8.2       |
|  | 8.8       |        | 8.2       | 5.0       |
|  | 50        |        | 5.0       | 5.0       |
|  |           |        | 5.0       | 5.0       |
|  | 4490      | 4488   | 445.4     | 445.64    |
|  | 44590     | 445.75 | 445.7     | 448.6     |
|  | 448.7     |        |           |           |
|  | 8.8       | 8.1    | 8.1       | 8.1       |
|  | 7.7-11/10 |        | 7.3-11/10 | 5.0       |
|  | 8.8       |        | 8.1       | 5.0       |
|  | 50        |        | 5.0       | 5.0       |
|  |           |        | 5.0       | 5.0       |
|  |           |        | 153.81    |           |

BM

11.01

on BC Mon  
on HCV  
478532

4785.32 = Poxing BC Rt.

47.50

47.15

TP 209 448.86 704 446.77

3785 234 Rt of L: 14 05 Pepperc Tree

3772

453.81

47

2

Rt

71

444.8 444.2 443.6 439.0 439.9 438.11 437.9 437.7 437.4

86 97 50 109 110 1075 1100 112 115  
30 20 18 11 7.3 7.3 20 50  
7.3 = 11/12  
7.3 = 11/12

446.4 446.2 439.5 439.26 439.48 439.20 439.2 439.8 439.8

25 27 91 96 938 966 97 91 96  
30 20 14 10 7.7 7.3 17 20 36  
7.7 = 11/12  
7.3 = 11/12

447.9 447.6 446.7 440.9 440.71 440.16 440.16 440.8 442.6 443.4

10 13 27 80 815 790 810 815 53 55  
30 20 18 10 7.7 7.3 15 20 30  
7.7 = 11/12  
7.3 = 11/12

448.86

448.2 447.9 447.9 442.0 441.89 442.16 441.94 442.0 441.7 445.0

56 59 52 110 112 1165 1187 118 91 85  
30 20 18 14 7.7 7.3 15 20 30  
7.7 = 11/12  
7.3 = 11/12

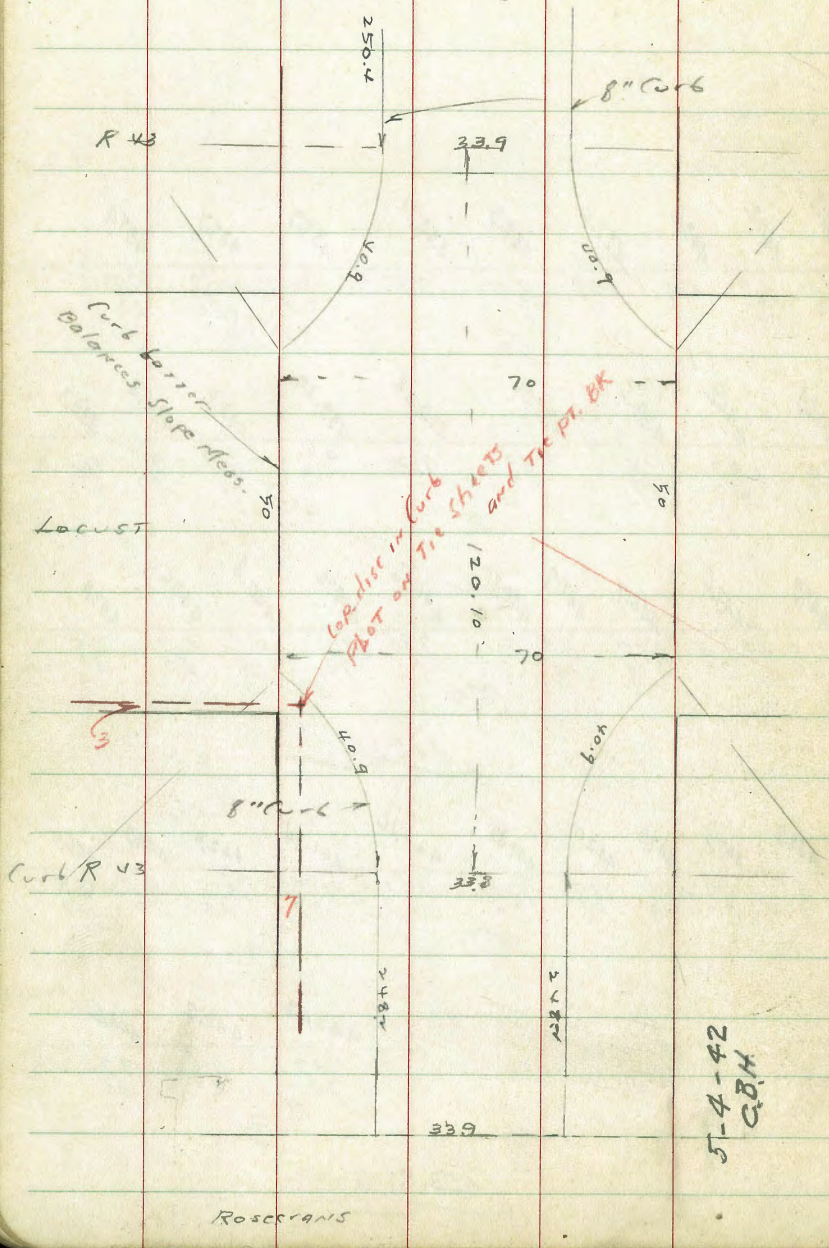
442.44 443.2 444.6

1187 10.6 92  
7.3 = 11/12 20 30

453.81

Final Meas. on Ingelow St.

Moore  
Hazard  
Hoopes  
4-30-44

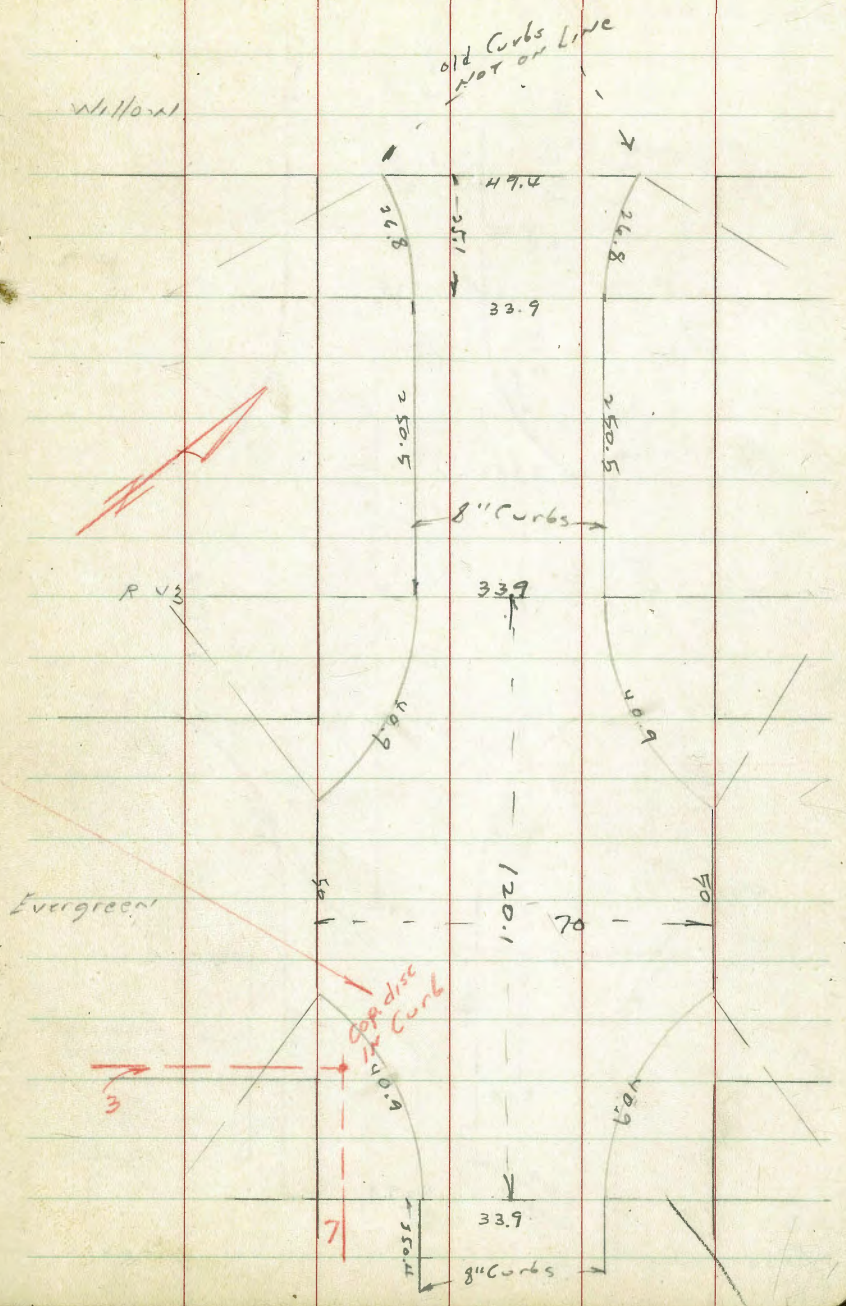


5-4-42  
C.B.H.

Rosecrans

Indexed  
C.B.H.

72



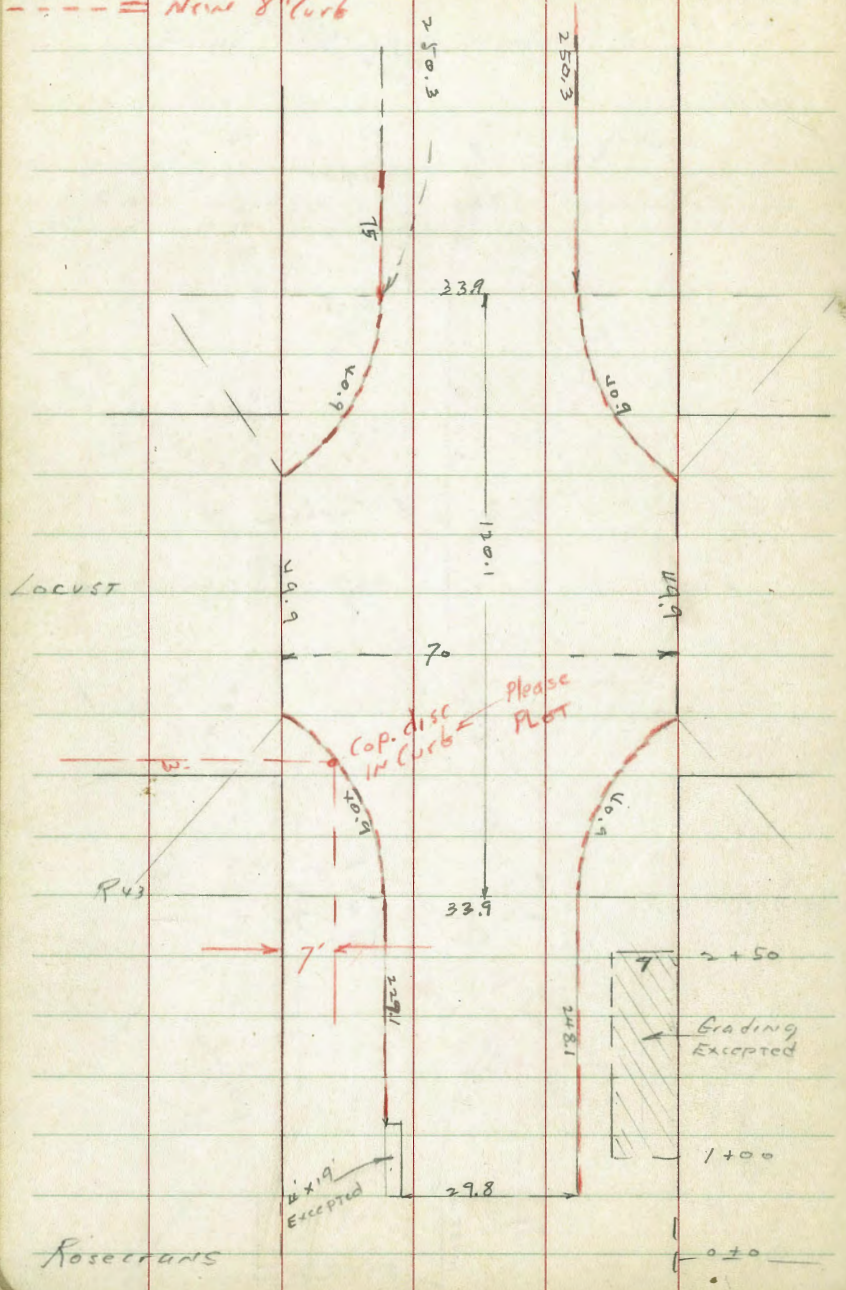
old Curbs  
Not on Line

Willow

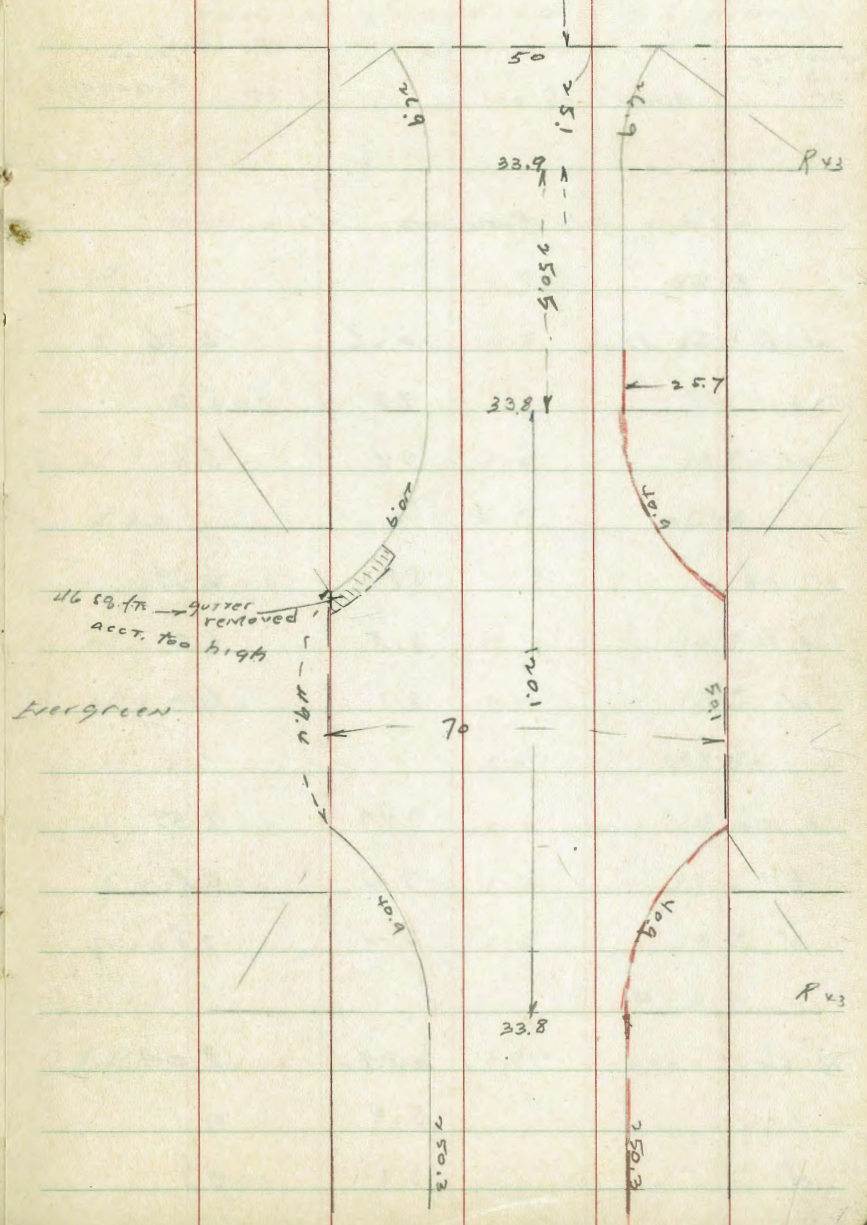
Evergreen

opp. disc  
for curb

--- = New 8" Curb



Willow



X sec Hugo St.  
to deduct Excepted ydge.  
on Griffiths Contract

Indexed  
C.S.K.

NW Top  
Curb at  
PC.

14.22 15.02

3.80

Hugo  
Rosscians

0+0 = w/ly Rosscians

1+00

N cb in drive

10.26

4.76

+11

9.8

5.2

N

9.4

5.6

1+50

N cb

8.83

6.19

+11

8.8

6.2

N

8.1

6.9

2+00

N cb

7.49

7.53

+11

7.4

7.8

N

7.2

7.8

2+50

N cb

5.98

9.04

+11

5.9

9.1

N

5.9

9.1

Indexed  
C.S.K.

X sec on Hugo  
bet. Locust & Evergreen  
to show area graded out from  
natural ground on N + S lines  
to Point 5.67 from curb.

74

15.02

0+0 = w/ly Locust

N

2.7

12.3

S

2.7

12.1

0+03

N

1.2

13.8

N 13

2.6

12.4

0+25

N

0.2

14.8

N + 17.33

1.4

13.6

N cb

1.47

13.55

S

0.4

14.6

S + 17.33

1.4

13.6

S cb

1.8

13.2

T.P.

11.24

25.44

0.67

14.40

|               |      |       |       |
|---------------|------|-------|-------|
|               | 0+50 |       |       |
| N             |      | 9.8   | 15.8  |
| +12.33        |      | 11.0  | 14.6  |
| N cb          |      | 11.05 | 14.59 |
| S             |      | 10.1  | 15.5  |
| +12.33        |      | 11.0  | 14.6  |
| S cb          |      | 11.4  | 14.2  |
|               | 1+00 |       |       |
| N             |      | 7.5   | 18.1  |
| +12.33        |      | 9.0   | 16.6  |
| N cb          |      | 9.07  | 16.62 |
| S             |      | 8.0   | 17.6  |
| +10           |      | 8.5   | 17.1  |
| +12.33        |      | 9.2   | 16.4  |
| S cb in drive |      | 9.72  | 15.92 |
|               | 1+50 |       |       |
| N             |      | 5.7   | 19.9  |
| +12.33        |      | 6.8   | 18.8  |
| N cb          |      | 6.92  | 18.72 |
|               | 2+00 |       |       |
| N             |      | 3.5   | 22.1  |

|        |                     |       |      |       |
|--------|---------------------|-------|------|-------|
| N      | +12.33              |       | 4.8  | 20.8  |
| N      | cb                  |       | 4.8  | 20.8  |
|        | 2+50                |       |      |       |
| N      |                     |       | 1.9  | 23.7  |
| +12.33 |                     |       | 2.7  | 22.9  |
| N cb   |                     |       | 2.7  | 22.9  |
|        | 2+75                |       |      |       |
| N      |                     |       | 0.6  | 25.0  |
| +12.33 |                     |       | 1.6  | 24.0  |
| N cb   |                     |       | 1.7  | 13.9  |
|        |                     |       |      |       |
| T.P.   | 8.04                | 32.09 | 1.57 | 24.07 |
|        |                     |       |      |       |
|        | 3+00 = EL Evergreen |       |      |       |
| N      |                     |       | 6.1  | 26.0  |
| +10    |                     |       | 7.0  | 25.1  |
|        | 3+09                |       |      |       |
| N      |                     |       | 5.9  | 26.2  |
| +3     |                     |       | 6.7  | 25.4  |
|        | 3+10                |       |      |       |
| N      |                     |       | 6.5  | 25.6  |

37.09

0 + 00 W/L EVERGREEN

0 - 5

N 4.7 27.4

0 - 4

N 3.2 28.5

+ 2 4.7 27.4

0 + 00

N 3.5 28.6

+ 2 3.5 28.6

+ 3 4.5 27.6

0 + 45

N 2.3 29.8

+ 12 33 3.4 28.7

N c 6 3.5 28.6

0 + 50

N 1.8 30.3

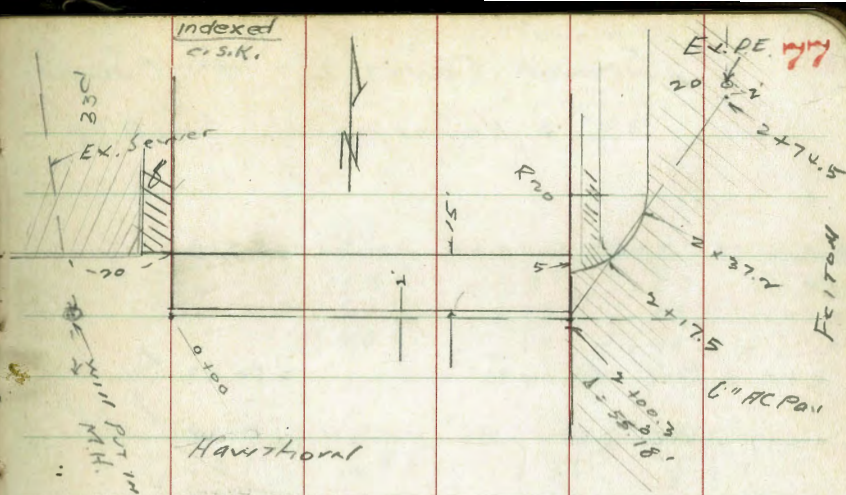
+ 11 2.0 30.1

+ 12.33 4.5 29.6

N c 6 4.6 29.5

7-10-47 Sewer Levels on Hawthorn 64

| BM B.P.N.G                     | 33d to Felton   |        | 33d & Hawthorn |
|--------------------------------|-----------------|--------|----------------|
| car walk                       | 10.41           | 268.57 | 458.10         |
|                                | N of            |        |                |
| F.L. Ex. M.H. on 33d, Hawthorn | 9.02            | 259.55 |                |
| R.M.                           | 0.13            | 268.44 |                |
|                                | Hawthorn        |        |                |
| Pav. El. 20' W of N.E. Cor 33d | 10.79           | 257.78 |                |
| 0+00                           | grove           | 12.6   | 256.0          |
| T.P.                           | 0.00            | 455.87 | 12.75          |
|                                |                 |        | 455.87         |
| 0+35                           |                 | 2.8    | 253.0          |
| 0+70                           |                 | 5.1    | 250.7          |
| 0+96                           | top of fill     | 7.5    | 248.3          |
| 1+07                           | Top             | 3.4    | 252.6          |
| 1+40                           |                 | 4.0    | 251.8          |
| 1+70                           |                 | 4.4    | 251.4          |
| 1+00.3                         | Δ pav to ground | 4.41   | 251.41         |
| 2+17.5                         | gut             | 4.25   | 251.37         |
| "                              | Top curb        | 3.89   | 251.93         |
| 2+37.7                         | "               | 3.77   | 252.05         |
| "                              | gut Pav         | 4.33   | 251.49         |
| 2+74.5                         | Pav 2' S of Cap | 3.29   | 252.13         |
| "                              | F.L. Ex. D.E.   | 8.13   | 249.69         |



ok Moen will ring up when he has  
 Ex. Sewer Exposed at proposed  
 M.H. Location on 33d & Hawthorn  
 at low spot on Hawthorn, the plans  
 con. pieces with con. slab to lay con.  
 pipe on, instead of C.I. pipe and only pieces.

CSM

For construction notes see page 78



Sewer Const. Dept. of Sewers

33<sup>d</sup> + Hawthorne. See P. 77

|                                       |     |        |          |
|---------------------------------------|-----|--------|----------|
| B.M. P. 77                            | 326 | 261.42 | 25816    |
| 0 + 0 = Prop. M.H. on 33 <sup>d</sup> |     |        | 250.63 ✓ |
| 0 + 17.2 E.L. 33 <sup>d</sup>         |     |        | 250.46 ✓ |
| 0 + 52.2                              |     |        | 250.10 ✓ |
| 0 + 87.2                              |     |        | 249.75 ✓ |
| 1 + 13.2                              |     |        | 249.49 ✓ |
| 1 + 22.2                              |     |        | OUT      |
| 1 + 57.2                              |     |        | 249.05 ✓ |
| 2 + 17.5 A LT M.H.                    |     |        | 248.44 ✓ |
| 2 + 54.4                              |     |        | 248.07 ✓ |
| 2 + 91.7 M.H. re DE.                  |     |        | 247.69 ✓ |

Moore  
7-14-42

78

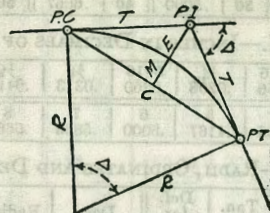
|        |        |        |        |        |
|--------|--------|--------|--------|--------|
| 50.63  | 50.46  | 50.10  | 49.75  | 49.49  |
| ✓      | 10.96  | 11.32  | 11.67  | 11.93  |
|        | 6.15   | 9.18   | 11.58  | 14.13  |
|        | C 481  | C 4.14 | C 0.09 | F 2.20 |
| 49.05  | 48.44  | 48.07  | 47.69  |        |
| 12.37  | 12.98  | 13.35  | 8.97   |        |
| 9.69   | 10.09  | 9.37   | 4.51   |        |
| C 2.68 | C 2.89 | C 3.98 | C 4.46 |        |
|        |        | Top 6. |        |        |

T.P. 261.42  
9.37  
254.05 ✓  
4.14  
256.66



# DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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## CURVE FORMULAS

Radius= $R = \frac{50}{\sin \frac{D}{2}}$  (1) Degree of Curve= $D$  and  $\sin \frac{D}{2} = \frac{50}{R}$  (2)

Tangent= $T = R \tan \frac{\Delta}{2}$  (3) Length of Curve= $L = 100 \frac{\Delta}{D}$  (4)

Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2}) = R \text{vers} \frac{\Delta}{2}$  (6)

External= $E = T \tan \frac{\Delta}{4} = R \div \cos \frac{\Delta}{2} - R$  (8)  $= R \text{exsec} \frac{\Delta}{2}$  (9)

Long Chord= $C = 2 R \sin \frac{\Delta}{2}$  (10)  $\Delta = \text{Central Angle}$

## EXPLANATION AND USE OF TABLES

**Stations.**—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T.  $\Delta = 62^\circ 10'$   $D = 8^\circ 20'$ . From Table IV for  $1^\circ$  curve  $T = 3454.1$  and  $\div 8\frac{1}{3} = 414.49$  ft. From Table V correction = .36 or  $T = 414.85$  ft. P. C.—Sta. P.I.— $T = 157 + 45.50$ . Also from (4)  $L = 746.00$  and P. T.—Sta. P. C. +  $L = 164 + 91.50$ .

**Offsets.**—Tangent offsets vary (approximately) directly with  $D$  and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = 158—Sta. P. C. = 54.50, hence offset =  $7.27 (54.50 \div 100)^2 = 2.16$  ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus  $(54.50)^2 \div (2 \times 688.26) = 2.16$  ft.

**Deflections.**—Deflection angle =  $\frac{1}{2} D$  for 100 ft.,  $\frac{1}{4} D$  for 50 ft., etc. For  $c$  ft. = (in minutes)  $.3 \times C \times D^\circ$  or = defl. for 1 ft. from Table III  $\times C$ . For Sta. 158 of above curve =  $.3 \times 54.5 \times 8\frac{1}{3} = 136.2'$  or  $2^\circ 16.2'$ , or =  $2.50 \times 54.5 = 136.2'$  from Table III. For Sta. 159 deflection angle =  $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$ , etc.

**Externals.**—May be found in similar manner to tangents. Thus  $E$  for curve above is 91.37. For from Table IV for  $1^\circ$  curve  $E = 960.6$  for  $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 91.27$  and from Table V correction = .10 or  $E = 91.37$  ft. Or suppose  $\Delta = 32^\circ$  and  $E$  is measured and found to be 42 ft. What is  $D$ ? From Table IV  $E = 230.9$  and  $\div 42 = 5.5$  or  $D = 5^\circ 30'$ .

TABLE I.—MINUTES IN DECIMALS OF A DEGREE.

Table with 11 columns and 11 rows showing minutes in decimals of a degree. Columns are labeled 1' through 11' and rows are labeled 1 through 11.

TABLE II.—INCHES IN DECIMALS OF A FOOT.

Table with 11 columns and 11 rows showing inches in decimals of a foot. Columns are labeled 1-16 through 11 and rows are labeled 1 through 11.

TABLE III.—RADI, ORDINATES AND DEFLECTIONS.

Table with 10 columns and 30 rows showing radi, ordinates and deflections. Columns are labeled Deg., Radius, Mid. Ord., Tan. Offset, Def. for 1 Foot, and then repeated for 7°, 8°, 9°, 10°, 11°, 12°, 13°, 14°, 15°, 16°, 17°, 18°, 19°, 20°, 21°, 22°, 23°, 24°, 25°, 26°, 27°, 28°, 29°, 30°.

Note. Chord Deflection=2 times tangent deflection.

133  
7.75  
5.55

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Table with 9 columns and 30 rows showing tangents and externals to a 1° curve. Columns are labeled Central Angle, Tangent, External, and then repeated for angles 1° through 30°.

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

| Central Angle | Tangent | External | Central Angle | Tangent | External | Central Angle | Tangent | External |
|---------------|---------|----------|---------------|---------|----------|---------------|---------|----------|
| 31°           | 1589.0  | 216.3    | 41°           | 2142.2  | 387.4    | 51°           | 2732.9  | 618.4    |
| 10'           | 1598.0  | 218.7    | 10'           | 2151.7  | 390.7    | 10'           | 2743.1  | 622.8    |
| 20            | 1606.9  | 221.1    | 20            | 2161.2  | 394.1    | 20            | 2753.4  | 627.2    |
| 30            | 1615.9  | 223.5    | 30            | 2170.8  | 397.4    | 30            | 2763.7  | 631.7    |
| 40            | 1624.9  | 226.0    | 40            | 2180.3  | 400.8    | 40            | 2773.9  | 636.2    |
| 50            | 1633.9  | 228.4    | 50            | 2189.9  | 404.2    | 50            | 2784.2  | 640.7    |
| 32°           | 1643.0  | 230.9    | 42°           | 2199.4  | 407.6    | 52°           | 2794.5  | 645.2    |
| 10            | 1652.0  | 233.4    | 10            | 2209.0  | 411.1    | 10            | 2804.9  | 649.7    |
| 20            | 1661.0  | 235.9    | 20            | 2218.6  | 414.5    | 20            | 2815.2  | 654.3    |
| 30            | 1670.0  | 238.4    | 30            | 2228.1  | 418.0    | 30            | 2825.6  | 658.8    |
| 40            | 1679.1  | 241.0    | 40            | 2237.7  | 421.4    | 40            | 2835.9  | 663.4    |
| 50            | 1688.1  | 243.5    | 50            | 2247.3  | 425.0    | 50            | 2846.3  | 668.0    |
| 33°           | 1697.2  | 246.1    | 43°           | 2257.0  | 428.5    | 53°           | 2856.7  | 672.7    |
| 10            | 1706.3  | 248.7    | 10            | 2266.6  | 432.0    | 10            | 2867.1  | 677.3    |
| 20            | 1715.3  | 251.3    | 20            | 2276.2  | 435.6    | 20            | 2877.5  | 682.0    |
| 30            | 1724.4  | 253.9    | 30            | 2285.9  | 439.2    | 30            | 2888.0  | 686.7    |
| 40            | 1733.5  | 256.5    | 40            | 2295.6  | 442.8    | 40            | 2898.4  | 691.4    |
| 50            | 1742.6  | 259.1    | 50            | 2305.2  | 446.4    | 50            | 2908.9  | 696.1    |
| 34°           | 1751.7  | 261.8    | 44°           | 2314.9  | 450.0    | 54°           | 2919.4  | 700.9    |
| 10            | 1760.8  | 264.5    | 10            | 2324.6  | 453.6    | 10            | 2929.9  | 705.7    |
| 20            | 1770.0  | 267.2    | 20            | 2334.3  | 457.3    | 20            | 2940.4  | 710.5    |
| 30            | 1779.1  | 269.9    | 30            | 2344.1  | 461.0    | 30            | 2951.0  | 715.3    |
| 40            | 1788.2  | 272.6    | 40            | 2353.8  | 464.6    | 40            | 2961.5  | 720.1    |
| 50            | 1797.4  | 275.3    | 50            | 2363.5  | 468.4    | 50            | 2972.1  | 725.0    |
| 35°           | 1806.6  | 278.1    | 45°           | 2373.3  | 472.1    | 55°           | 2982.7  | 729.9    |
| 10            | 1815.7  | 280.8    | 10            | 2383.1  | 475.8    | 10            | 2993.3  | 734.8    |
| 20            | 1824.9  | 283.6    | 20            | 2392.8  | 479.6    | 20            | 3003.9  | 739.7    |
| 30            | 1834.1  | 286.4    | 30            | 2402.6  | 483.3    | 30            | 3014.5  | 744.6    |
| 40            | 1843.3  | 289.2    | 40            | 2412.4  | 487.2    | 40            | 3025.2  | 749.6    |
| 50            | 1852.5  | 292.0    | 50            | 2422.3  | 491.0    | 50            | 3035.8  | 754.6    |
| 36°           | 1861.7  | 294.9    | 46°           | 2432.1  | 494.8    | 56°           | 3046.5  | 759.6    |
| 10            | 1870.9  | 297.7    | 10            | 2441.9  | 498.7    | 10            | 3057.2  | 764.6    |
| 20            | 1880.1  | 300.6    | 20            | 2451.8  | 502.5    | 20            | 3067.9  | 769.7    |
| 30            | 1889.4  | 303.5    | 30            | 2461.7  | 506.4    | 30            | 3078.7  | 774.7    |
| 40            | 1898.6  | 306.4    | 40            | 2471.5  | 510.3    | 40            | 3089.4  | 779.8    |
| 50            | 1907.9  | 309.3    | 50            | 2481.4  | 514.3    | 50            | 3100.2  | 784.9    |
| 37°           | 1917.1  | 312.2    | 47°           | 2491.3  | 518.2    | 57°           | 3110.9  | 790.1    |
| 10            | 1926.4  | 315.2    | 10            | 2501.2  | 522.2    | 10            | 3121.7  | 795.2    |
| 20            | 1935.7  | 318.1    | 20            | 2511.2  | 526.1    | 20            | 3132.6  | 800.4    |
| 30            | 1945.0  | 321.1    | 30            | 2521.1  | 530.1    | 30            | 3143.4  | 805.6    |
| 40            | 1954.3  | 324.1    | 40            | 2531.1  | 534.2    | 40            | 3154.2  | 810.9    |
| 50            | 1963.6  | 327.1    | 50            | 2541.0  | 538.2    | 50            | 3165.1  | 816.1    |
| 38°           | 1972.9  | 330.2    | 48°           | 2551.0  | 542.2    | 58°           | 3176.0  | 821.4    |
| 10            | 1982.2  | 333.2    | 10            | 2561.0  | 546.3    | 10            | 3186.9  | 826.7    |
| 20            | 1991.5  | 336.3    | 20            | 2571.0  | 550.4    | 20            | 3197.8  | 832.0    |
| 30            | 2000.9  | 339.3    | 30            | 2581.0  | 554.5    | 30            | 3208.8  | 837.3    |
| 40            | 2010.2  | 342.4    | 40            | 2591.0  | 558.6    | 40            | 3219.7  | 842.7    |
| 50            | 2019.6  | 345.5    | 50            | 2601.1  | 562.8    | 50            | 3230.7  | 848.1    |
| 39°           | 2029.0  | 348.6    | 49°           | 2611.2  | 566.9    | 59°           | 3241.7  | 853.5    |
| 10            | 2038.4  | 351.8    | 10            | 2621.2  | 571.1    | 10            | 3252.7  | 858.9    |
| 20            | 2047.8  | 354.9    | 20            | 2631.3  | 575.3    | 20            | 3263.7  | 864.3    |
| 30            | 2057.2  | 358.1    | 30            | 2641.4  | 579.5    | 30            | 3274.8  | 869.8    |
| 40            | 2066.6  | 361.3    | 40            | 2651.5  | 583.8    | 40            | 3285.8  | 875.3    |
| 50            | 2076.0  | 364.5    | 50            | 2661.6  | 588.0    | 50            | 3296.9  | 880.8    |
| 40°           | 2085.4  | 367.7    | 50°           | 2671.8  | 592.3    | 60°           | 3308.0  | 886.4    |
| 10            | 2094.9  | 371.0    | 10            | 2681.9  | 596.6    | 10            | 3319.1  | 892.0    |
| 20            | 2104.3  | 374.2    | 20            | 2692.1  | 600.9    | 20            | 3330.3  | 897.5    |
| 30            | 2113.8  | 377.5    | 30            | 2702.3  | 605.3    | 30            | 3341.4  | 903.2    |
| 40            | 2123.3  | 380.8    | 40            | 2712.5  | 609.6    | 40            | 3352.6  | 908.8    |
| 50            | 2132.7  | 384.1    | 50            | 2722.7  | 614.0    | 50            | 3363.8  | 914.5    |

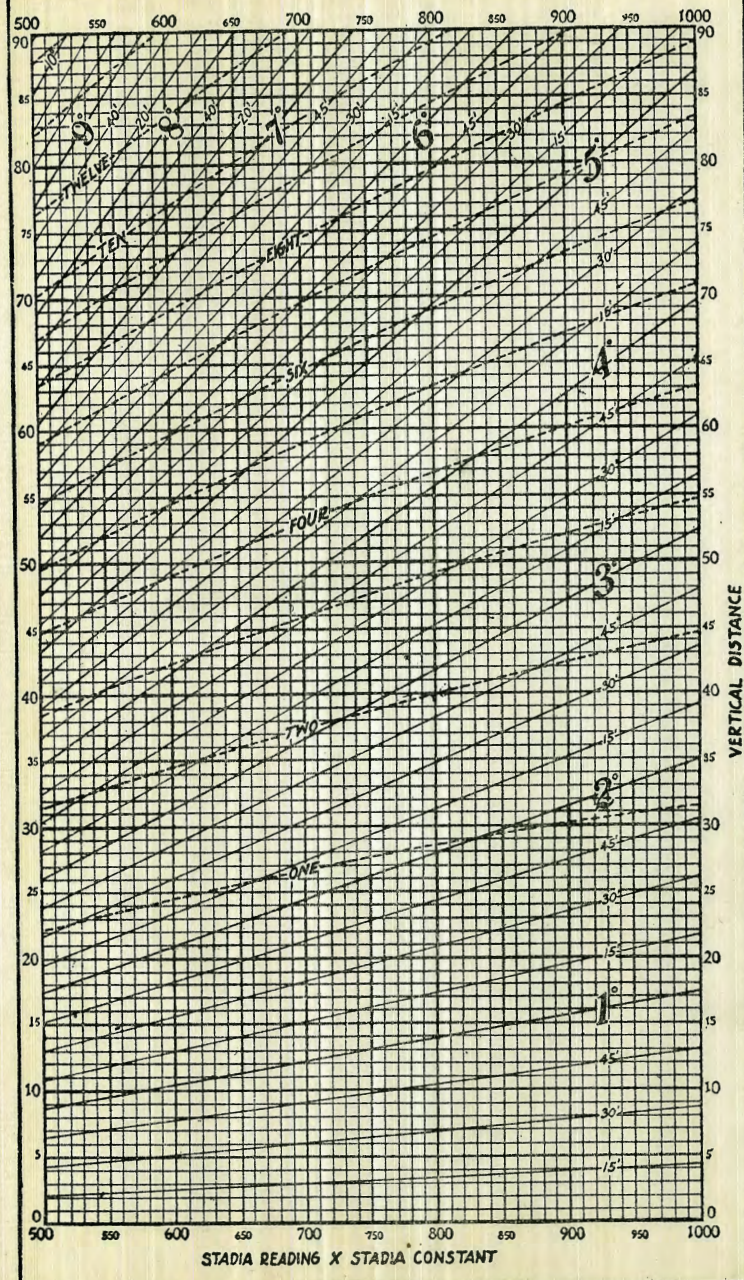
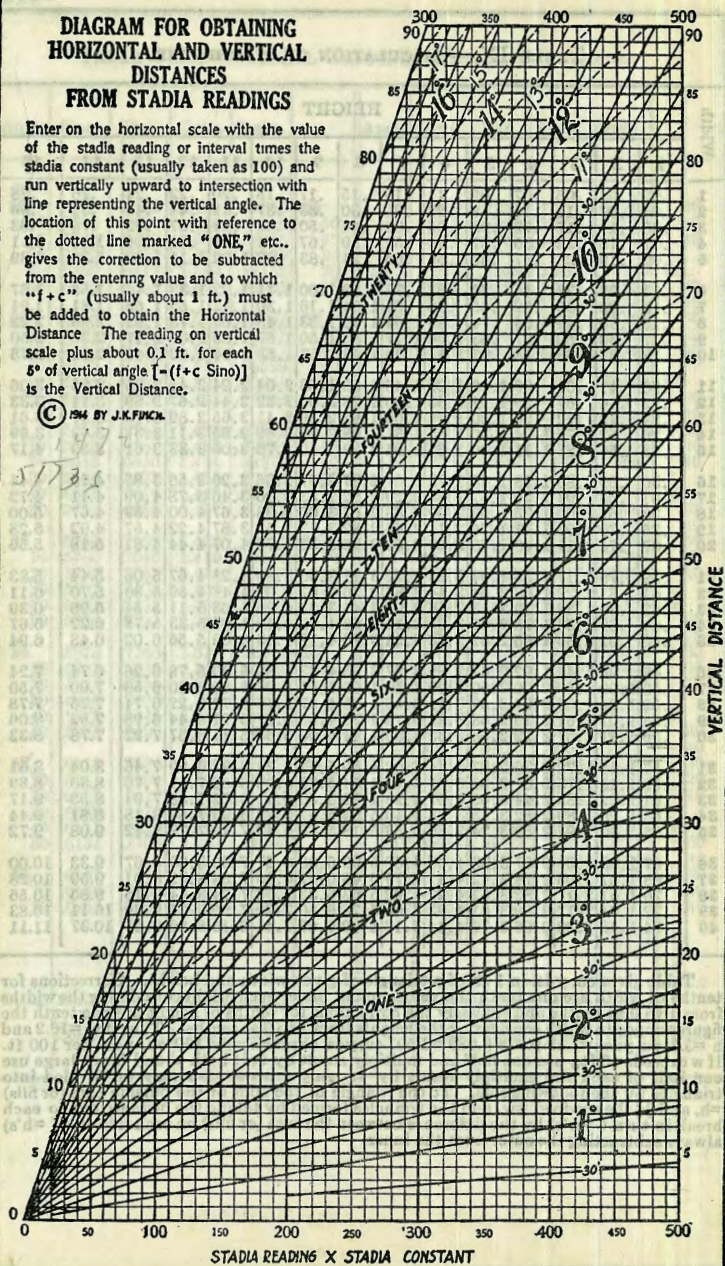
TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

| Central Angle | Tangent | External | Central Angle | Tangent | External | Central Angle | Tangent | External |
|---------------|---------|----------|---------------|---------|----------|---------------|---------|----------|
| 61°           | 3375.0  | 920.2    | 71°           | 4086.9  | 1308.2   | 81°           | 4893.6  | 1805.3   |
| 10'           | 3386.3  | 925.9    | 10'           | 4099.5  | 1315.6   | 10'           | 4908.0  | 1814.7   |
| 20            | 3397.5  | 931.6    | 20            | 4112.1  | 1322.9   | 20            | 4922.5  | 1824.1   |
| 30            | 3408.8  | 937.3    | 30            | 4124.8  | 1330.3   | 30            | 4937.0  | 1833.6   |
| 40            | 3420.1  | 943.1    | 40            | 4137.4  | 1337.7   | 40            | 4951.5  | 1843.1   |
| 50            | 3431.4  | 948.9    | 50            | 4150.1  | 1345.1   | 50            | 4966.1  | 1852.6   |
| 62°           | 3442.7  | 954.8    | 72°           | 4162.8  | 1352.6   | 82°           | 4980.7  | 1862.2   |
| 10            | 3454.1  | 960.6    | 10            | 4175.6  | 1360.1   | 10            | 4995.4  | 1871.8   |
| 20            | 3465.4  | 966.5    | 20            | 4188.5  | 1367.6   | 20            | 5010.0  | 1881.5   |
| 30            | 3476.8  | 972.4    | 30            | 4201.2  | 1375.2   | 30            | 5024.8  | 1891.2   |
| 40            | 3488.3  | 978.3    | 40            | 4214.0  | 1382.8   | 40            | 5039.5  | 1900.9   |
| 50            | 3499.7  | 984.3    | 50            | 4226.8  | 1390.4   | 50            | 5054.3  | 1910.7   |
| 63°           | 3511.1  | 990.2    | 73°           | 4239.7  | 1398.0   | 83°           | 5069.2  | 1920.5   |
| 10            | 3522.6  | 996.2    | 10            | 4252.6  | 1405.7   | 10            | 5084.0  | 1930.4   |
| 20            | 3534.1  | 1002.3   | 20            | 4265.6  | 1413.5   | 20            | 5099.0  | 1940.3   |
| 30            | 3545.6  | 1008.3   | 30            | 4278.5  | 1421.2   | 30            | 5113.9  | 1950.3   |
| 40            | 3557.2  | 1014.4   | 40            | 4291.5  | 1429.0   | 40            | 5128.0  | 1960.2   |
| 50            | 3568.7  | 1020.5   | 50            | 4304.6  | 1436.8   | 50            | 5143.9  | 1970.3   |
| 64°           | 3580.3  | 1026.6   | 74°           | 4317.6  | 1444.6   | 84°           | 5159.0  | 1980.4   |
| 10            | 3591.9  | 1032.8   | 10            | 4330.7  | 1452.5   | 10            | 5174.1  | 1990.5   |
| 20            | 3603.5  | 1039.0   | 20            | 4343.8  | 1460.4   | 20            | 5189.3  | 2000.6   |
| 30            | 3615.1  | 1045.2   | 30            | 4356.9  | 1468.4   | 30            | 5204.4  | 2010.8   |
| 40            | 3626.8  | 1051.4   | 40            | 4370.1  | 1476.4   | 40            | 5219.7  | 2021.1   |
| 50            | 3638.5  | 1057.7   | 50            | 4383.3  | 1484.4   | 50            | 5234.9  | 2031.4   |
| 65°           | 3650.2  | 1063.9   | 75°           | 4396.5  | 1492.4   | 85°           | 5250.3  | 2041.7   |
| 10            | 3661.9  | 1070.2   | 10            | 4409.8  | 1500.5   | 10            | 5265.6  | 2052.1   |
| 20            | 3673.7  | 1076.6   | 20            | 4423.1  | 1508.6   | 20            | 5281.0  | 2062.5   |
| 30            | 3685.4  | 1082.9   | 30            | 4436.4  | 1516.7   | 30            | 5296.4  | 2073.0   |
| 40            | 3697.2  | 1089.3   | 40            | 4449.7  | 1524.9   | 40            | 5311.9  | 2083.5   |
| 50            | 3709.0  | 1095.7   | 50            | 4463.1  | 1533.1   | 50            | 5327.4  | 2094.1   |
| 66°           | 3720.9  | 1102.2   | 76°           | 4476.5  | 1541.4   | 86°           | 5343.0  | 2104.7   |
| 10            | 3732.7  | 1108.6   | 10            | 4489.9  | 1549.7   | 10            | 5358.6  | 2115.3   |
| 20            | 3744.6  | 1115.1   | 20            | 4503.4  | 1558.0   | 20            | 5374.2  | 2126.0   |
| 30            | 3756.5  | 1121.7   | 30            | 4516.9  | 1566.3   | 30            | 5389.9  | 2136.7   |
| 40            | 3768.5  | 1128.2   | 40            | 4530.4  | 1574.7   | 40            | 5405.6  | 2147.5   |
| 50            | 3780.4  | 1134.8   | 50            | 4544.0  | 1583.1   | 50            | 5421.4  | 2158.4   |
| 67°           | 3792.4  | 1141.4   | 77°           | 4557.6  | 1591.6   | 87°           | 5437.2  | 2169.2   |
| 10            | 3804.4  | 1148.0   | 10            | 4571.2  | 1600.1   | 10            | 5453.1  | 2180.2   |
| 20            | 3816.4  | 1154.7   | 20            | 4584.8  | 1608.6   | 20            | 5469.0  | 2191.1   |
| 30            | 3828.4  | 1161.3   | 30            | 4598.5  | 1617.1   | 30            | 5484.9  | 2202.2   |
| 40            | 3840.5  | 1168.1   | 40            | 4612.2  | 1625.7   | 40            | 5500.9  | 2213.2   |
| 50            | 3852.6  | 1174.8   | 50            | 4626.0  | 1634.4   | 50            | 5517.0  | 2224.3   |
| 68°           | 3864.7  | 1181.6   | 78°           | 4639.8  | 1643.0   | 88°           | 5533.1  | 2235.5   |
| 10            | 3876.8  | 1188.4   | 10            | 4653.6  | 1651.7   | 10            | 5549.2  | 2246.7   |
| 20            | 3889.0  | 1195.2   | 20            | 4667.4  | 1660.5   | 20            | 5565.4  | 2258.0   |
| 30            | 3901.2  | 1202.0   | 30            | 4681.3  | 1669.2   | 30            | 5581.6  | 2269.3   |
| 40            | 3913.4  | 1208.9   | 40            | 4695.2  | 1678.1   | 40            | 5597.8  | 2280.6   |
| 50            | 3925.6  | 1215.8   | 50            | 4709.2  | 1686.9   | 50            | 5614.2  | 2292.0   |
| 69°           | 3937.9  | 1222.7   | 79°           | 4723.2  | 1695.8   | 89°           | 5630.5  | 2303.5   |
| 10            | 3950.2  | 1229.7   | 10            | 4737.2  | 1704.7   | 10            | 5646.9  | 2315.0   |
| 20            | 3962.5  | 1236.7   | 20            | 4751.2  | 1713.7   | 20            | 5663.4  | 2326.6   |
| 30            | 3974.8  | 1243.7   | 30            | 4765.3  | 1722.7   | 30            | 5679.9  | 2338.2   |
| 40            | 3987.2  | 1250.8   | 40            | 4779.4  | 1731.7   | 40            | 5696.4  | 2349.8   |
| 50            | 3999.5  | 1257.9   | 50            | 4793.6  | 1740.8   | 50            | 5713.0  | 2361.5   |
| 70°           | 4011.9  | 1265.0   | 80°           | 4807.7  | 1749.9   | 90°           | 5729.7  | 2373.3   |
| 10            | 4024.4  | 1272.1   | 10            | 4822.0  | 1759.0   | 10            | 5746.3  | 2385.1   |
| 20            | 4036.8  | 1279.3   | 20            | 4836.2  | 1768.2   | 20            | 5763.1  | 2397.0   |
| 30            | 4049.3  | 1286.5   | 30            | 4850.5  | 1777.4   | 30            | 5779.9  | 2408.9   |
| 40            | 4061.8  | 1293.6   | 40            | 4864.8  | 1786.7   | 40            | 5796.7  | 2420.9   |
| 50            | 4074.4  | 1300.9   | 50            | 4879.2  | 1796.0   | 50            | 5813.6  | 2432.9   |

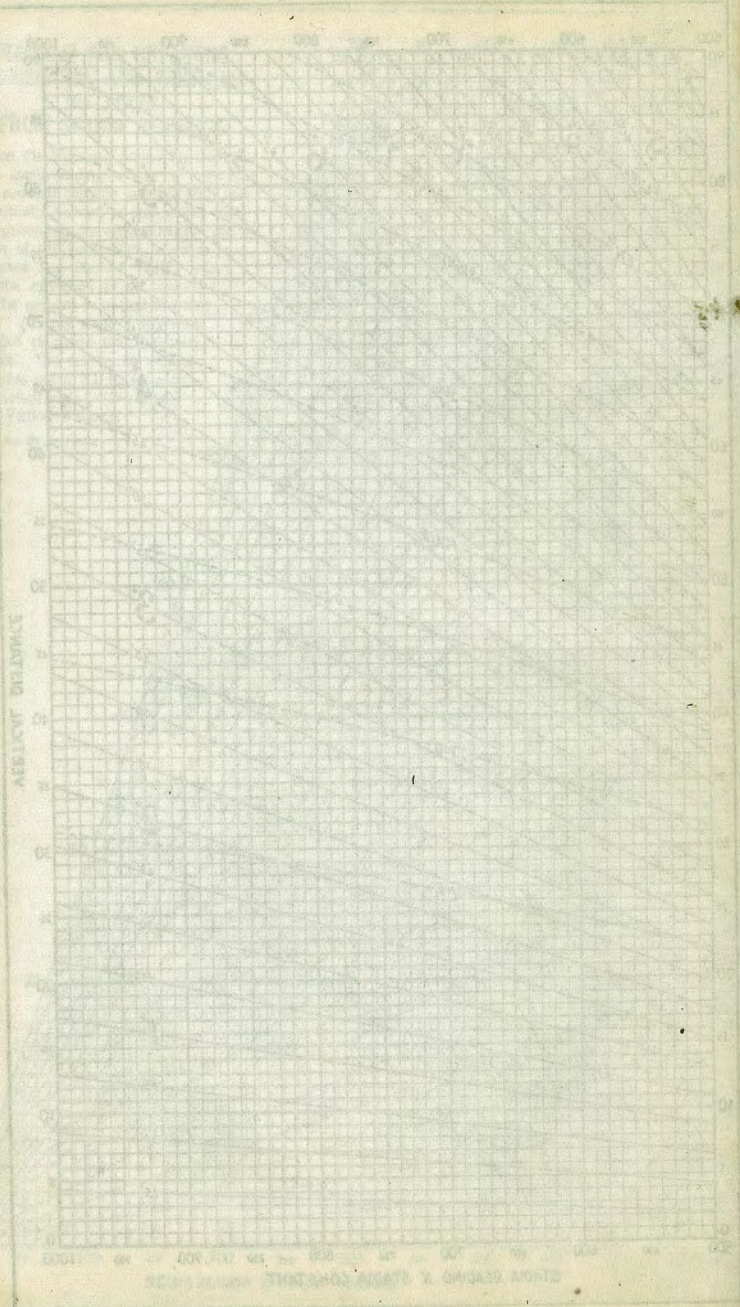
### DIAGRAM FOR OBTAINING HORIZONTAL AND VERTICAL DISTANCES FROM STADIA READINGS

Enter on the horizontal scale with the value of the stadia reading or interval times the stadia constant (usually taken as 100) and run vertically upward to intersection with line representing the vertical angle. The location of this point with reference to the dotted line marked "ONE," etc., gives the correction to be subtracted from the entering value and to which "f+c" (usually about 1 ft.) must be added to obtain the Horizontal Distance. The reading on vertical scale plus about 0.1 ft. for each 5° of vertical angle [ $-(f+c \sin \alpha)$ ] is the Vertical Distance.

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12.52

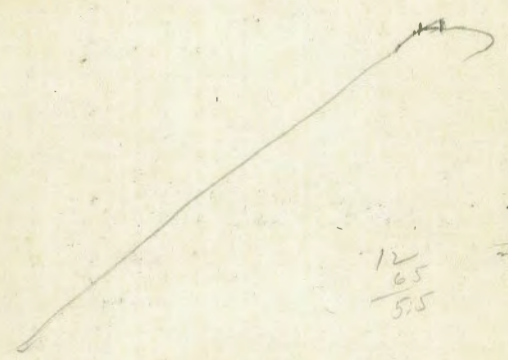


1.5  
6.5  
12.1

9720 3 Begin Walk  
1. Ch. on Hilltop N of Washoe

10735 5 End  
10757 5

1522-62



248.1  
19  
229.1

12  
65  
55

338  
4  
298

2.5  
2.5  
5.0  
6.25

2.5  
16  
15.0  
40.0

49.95

2 9130  
5132  
60.02

4720  
2 5120  
671.30

29134

DISTANCES FROM CENTER OF ROADWAY FOR  
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½  
For Single Track Embankment.

| H  | 0    | .1   | .2   | .3   | .4   | .5   | .6   | .7   | .8   | .9   | H  |
|----|------|------|------|------|------|------|------|------|------|------|----|
| 0  | 8.0  | 8.2  | 8.3  | 8.5  | 8.6  | 8.8  | 8.9  | 9.1  | 9.2  | 9.4  | 0  |
| 1  | 9.5  | 9.7  | 9.8  | 10.0 | 10.1 | 10.3 | 10.4 | 10.6 | 10.7 | 10.9 | 1  |
| 2  | 11.0 | 11.2 | 11.3 | 11.5 | 11.6 | 11.8 | 11.9 | 12.1 | 12.2 | 12.4 | 2  |
| 3  | 12.5 | 12.7 | 12.8 | 13.0 | 13.1 | 13.3 | 13.4 | 13.6 | 13.7 | 13.9 | 3  |
| 4  | 14.0 | 14.2 | 14.3 | 14.5 | 14.6 | 14.8 | 14.9 | 15.1 | 15.2 | 15.4 | 4  |
| 5  | 15.5 | 15.7 | 15.8 | 16.0 | 16.1 | 16.3 | 16.4 | 16.6 | 16.7 | 16.9 | 5  |
| 6  | 17.0 | 17.2 | 17.3 | 17.5 | 17.6 | 17.8 | 17.9 | 18.1 | 18.2 | 18.4 | 6  |
| 7  | 18.5 | 18.7 | 18.8 | 19.0 | 19.1 | 19.3 | 19.4 | 19.6 | 19.7 | 19.9 | 7  |
| 8  | 20.0 | 20.2 | 20.3 | 20.5 | 20.6 | 20.8 | 20.9 | 21.1 | 21.2 | 21.4 | 8  |
| 9  | 21.5 | 21.7 | 21.8 | 22.0 | 22.1 | 22.3 | 22.4 | 22.6 | 22.7 | 22.9 | 9  |
| 10 | 23.0 | 23.2 | 23.3 | 23.5 | 23.6 | 23.8 | 23.9 | 24.1 | 24.2 | 24.4 | 10 |
| 11 | 24.5 | 24.7 | 24.8 | 25.0 | 25.1 | 25.3 | 25.4 | 25.6 | 25.7 | 25.9 | 11 |
| 12 | 26.0 | 26.2 | 26.3 | 26.5 | 26.6 | 26.8 | 26.9 | 27.1 | 27.2 | 27.4 | 12 |
| 13 | 27.5 | 27.7 | 27.8 | 28.0 | 28.1 | 28.3 | 28.4 | 28.6 | 28.7 | 28.9 | 13 |
| 14 | 29.0 | 29.2 | 29.3 | 29.5 | 29.6 | 29.8 | 29.9 | 30.1 | 30.2 | 30.4 | 14 |
| 15 | 30.5 | 30.7 | 30.8 | 31.0 | 31.1 | 31.3 | 31.4 | 31.6 | 31.7 | 31.9 | 15 |
| 16 | 32.0 | 32.2 | 32.3 | 32.5 | 32.6 | 32.8 | 32.9 | 33.1 | 33.2 | 33.4 | 16 |
| 17 | 33.5 | 33.7 | 33.8 | 34.0 | 34.1 | 34.3 | 34.4 | 34.6 | 34.7 | 34.9 | 17 |
| 18 | 35.0 | 35.2 | 35.3 | 35.5 | 35.6 | 35.8 | 35.9 | 36.1 | 36.2 | 36.4 | 18 |
| 19 | 36.5 | 36.7 | 36.8 | 37.0 | 37.1 | 37.3 | 37.4 | 37.6 | 37.7 | 37.9 | 19 |
| 20 | 38.0 | 38.2 | 38.3 | 38.5 | 38.6 | 38.8 | 38.9 | 39.1 | 39.2 | 39.4 | 20 |
| 21 | 39.5 | 39.7 | 39.8 | 40.0 | 40.1 | 40.3 | 40.4 | 40.6 | 40.7 | 40.9 | 21 |
| 22 | 41.0 | 41.2 | 41.3 | 41.5 | 41.6 | 41.8 | 41.9 | 42.1 | 42.2 | 42.4 | 22 |
| 23 | 42.5 | 42.7 | 42.8 | 43.0 | 43.1 | 43.3 | 43.4 | 43.6 | 43.7 | 43.9 | 23 |
| 24 | 44.0 | 44.2 | 44.3 | 44.5 | 44.6 | 44.8 | 44.9 | 45.1 | 45.2 | 45.4 | 24 |
| 25 | 45.5 | 45.7 | 45.8 | 46.0 | 46.1 | 46.3 | 46.4 | 46.6 | 46.7 | 46.9 | 25 |
| 26 | 47.0 | 47.2 | 47.3 | 47.5 | 47.6 | 47.8 | 47.9 | 48.1 | 48.2 | 48.4 | 26 |
| 27 | 48.5 | 48.7 | 48.8 | 49.0 | 49.1 | 49.3 | 49.4 | 49.6 | 49.7 | 49.9 | 27 |
| 28 | 50.0 | 50.2 | 50.3 | 50.5 | 50.6 | 50.8 | 50.9 | 51.1 | 51.2 | 51.4 | 28 |
| 29 | 51.5 | 51.7 | 51.8 | 52.0 | 52.1 | 52.3 | 52.4 | 52.6 | 52.7 | 52.9 | 29 |
| 30 | 53.0 | 53.2 | 53.3 | 53.5 | 53.6 | 53.8 | 53.9 | 54.1 | 54.2 | 54.4 | 30 |
| 31 | 54.5 | 54.7 | 54.8 | 55.0 | 55.1 | 55.3 | 55.4 | 55.6 | 55.7 | 55.9 | 31 |
| 32 | 56.0 | 56.2 | 56.3 | 56.5 | 56.6 | 56.8 | 56.9 | 57.1 | 57.2 | 57.4 | 32 |
| 33 | 57.5 | 57.7 | 57.8 | 58.0 | 58.1 | 58.3 | 58.4 | 58.6 | 58.7 | 58.9 | 33 |
| 34 | 59.0 | 59.2 | 59.3 | 59.5 | 59.6 | 59.8 | 59.9 | 60.1 | 60.2 | 60.4 | 34 |
| 35 | 60.5 | 60.7 | 60.8 | 61.0 | 61.1 | 61.3 | 61.4 | 61.6 | 61.7 | 61.9 | 35 |
| 36 | 62.0 | 62.2 | 62.3 | 62.5 | 62.6 | 62.8 | 62.9 | 63.1 | 63.2 | 63.4 | 36 |
| 37 | 63.5 | 63.7 | 63.8 | 64.0 | 64.1 | 64.3 | 64.4 | 64.6 | 64.7 | 64.9 | 37 |
| 38 | 65.0 | 65.2 | 65.3 | 65.5 | 65.6 | 65.8 | 65.9 | 66.1 | 66.2 | 66.4 | 38 |
| 39 | 66.5 | 66.7 | 66.8 | 67.0 | 67.1 | 67.3 | 67.4 | 67.6 | 67.7 | 67.9 | 39 |
| 40 | 68.0 | 68.2 | 68.3 | 68.5 | 68.6 | 68.8 | 68.9 | 69.1 | 69.2 | 69.4 | 40 |

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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