

1623

THE  
FIELD



# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

DEC 2 1908

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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1623

ENGINEERING DEPARTMENT,  
CITY OF SAN DIEGO,  
CALIFORNIA.

The paper stock of this book is made of a high grade 50% rag paper having a water resisting surface. This book is sewed with Bing Special Enamel Waterproof Thread.

Made in U. S. A.



Amherst ST.	11 - 39
73 <sup>RD</sup> ✓	40 - 44
Horbison Ave	45 - 48
72 <sup>ND</sup> ST.	49 - 50
Normandie Pl.	51 - 52
71 <sup>ST</sup> ST.	53 - 57
70 <sup>TH</sup> ✓	58 - 59



Bliss-Notes  
 Sommermyer Hch.  
 B899  
 11/19/2

HWY  
 Pacific Sewer Interceptor-Kurtz St  
 from 14+37.53 Moore FB-1395-P24. to 46+89.37 Frontier  
 + Rosecrans via Kurtz St

Street

Frontier

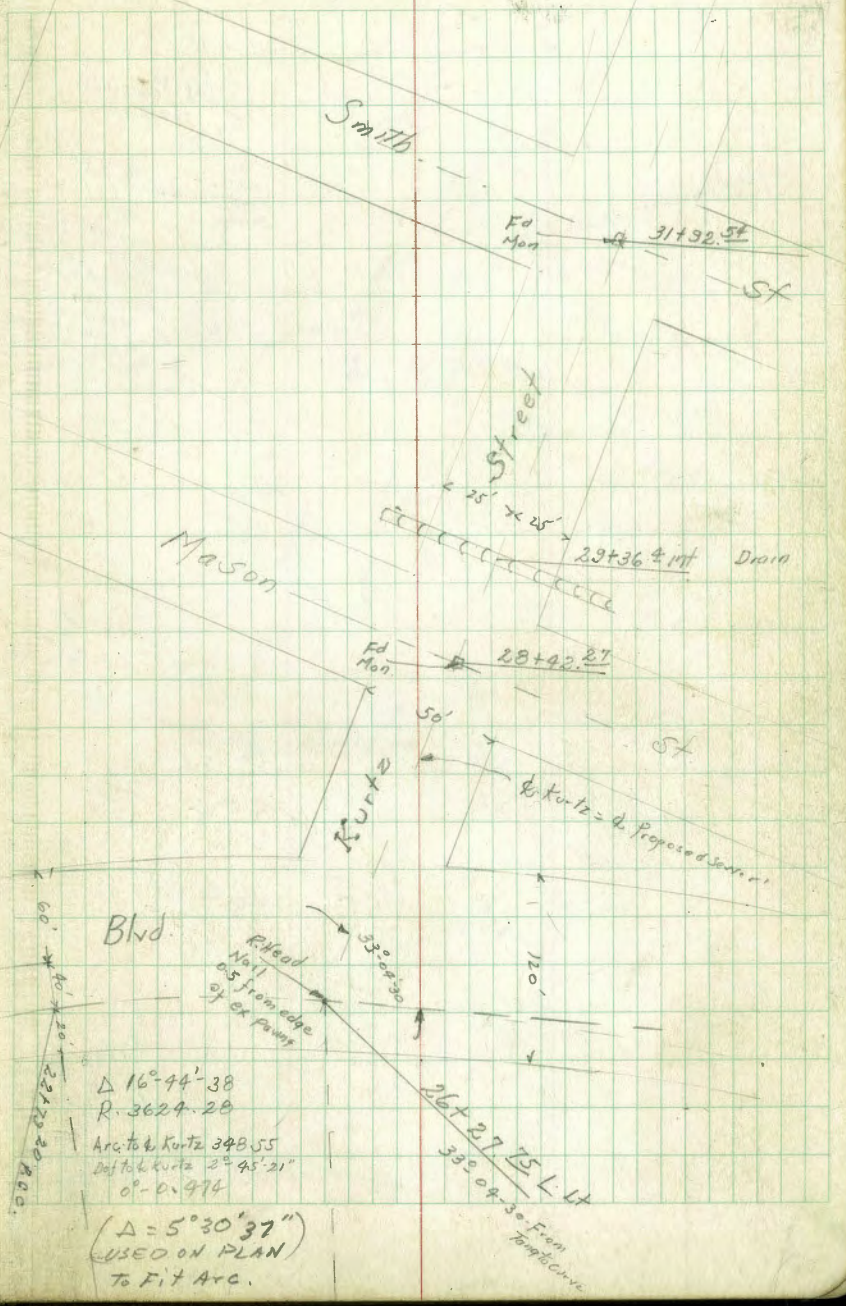


24°  
 22-00-22  
 R. 1460  
 T. 310.58  
 283.87  
 LC 61173

60' x 10' x 20' 2170 20 800

Δ 16°-44'-38"  
 R. 3624.28  
 Arc to Kurtz 348.55  
 Def to Kurtz 3°-45'-21"  
 of - 0.974  
 (Δ = 5°30'37")  
 USED ON PLAN  
 TO FIT ARC.

2-452 2 14  
 5 30 42





Iron pin  
to Midway + Rosecrans  
set by State Survey Eng. Dept

Rosecrans

E. Rosecrans  
see FB 1422

46+84.87 = 41423.89

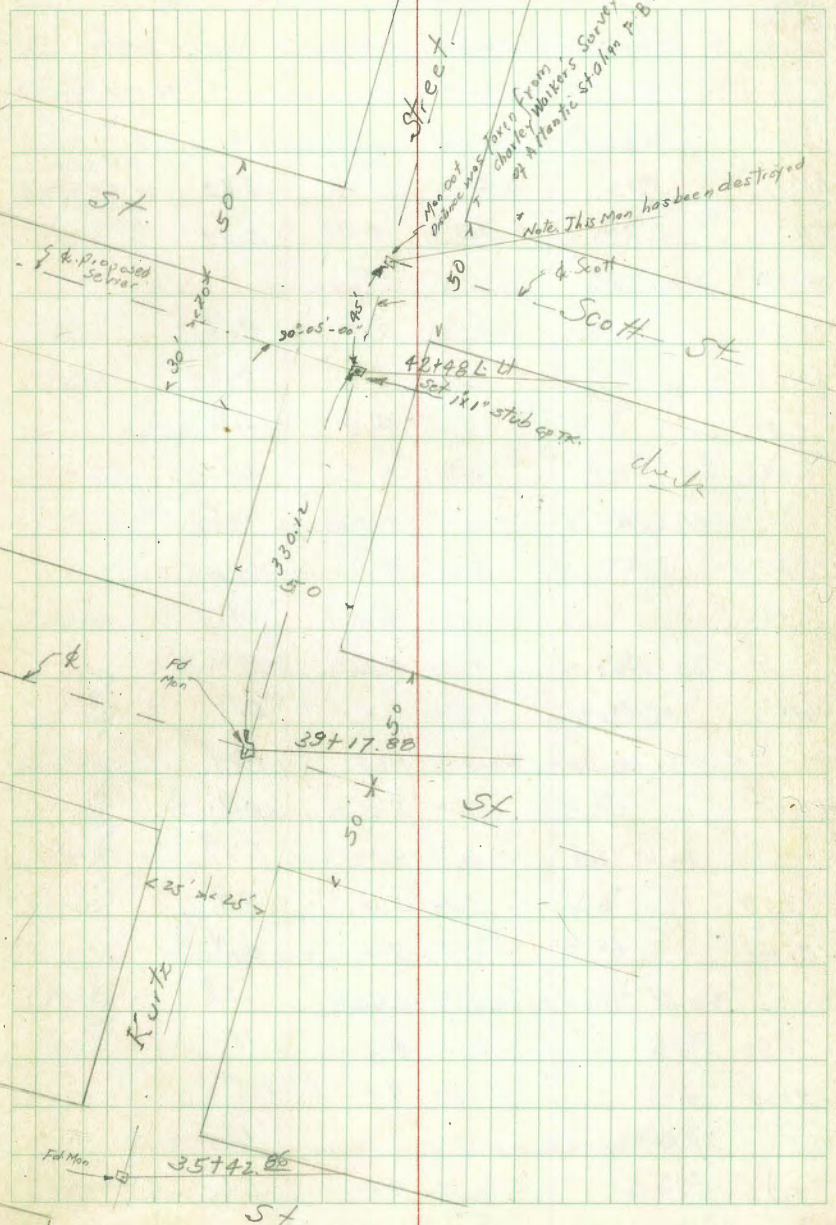
R.H.  
Nail in  
paving

Note Header  
Paving Header  
used to Establish  
N Line Frontier  
N Line Frontier  
Bates says it is set  
exactly 195  
set N Line  
of proposed  
Survey of Frontier

Frontier

Taylor

Wallace



Man out of station was found from Charles Walker's Survey of Atlantic Station P.B. 1822-23

Note. This Mon has been destroyed

42+98.64

set 1x1' stub cap

39+17.80

25' x 25'

Kurtz

35+42.86

Fol Man



Bliss Notes  
Sommerayer T  
Bepps - Rod  
11/2/4

Sewer Profile Levels for Kurtz St.

Alignment Pacific Interceptor Sewer from  
14+37<sup>53</sup> Moore's Frontier alignment to 40+00<sup>37</sup>?

Rosecrans & Frontier

BM.	3.92	6.61	2.69	
TP.	3.79	<u>5.93</u>	4.47	2.14
14+37 <sup>53</sup>	Moore's B.C.		4.9	
+50			5.0	0.9
15+00			5.1	0.8
+50			4.9	1.0
+788			4.8	1.1
" "	7° Rt Top Footing		4.88	1.05
16+00			4.8	1.1
16+36			4.8	1.1
" "	Top Footing		4.91	1.02
16+	B.C. Pt		5.2	0.7
" "	20' Lt. Top ex. Paving		4.69	1.24
17+00			5.0	0.9
" "	20' Lt. Top ex. Paving		4.74	1.19
+50			5.0	0.9
18+00			5.0	0.9
" "	20' Lt. Top ex. Paving		4.65	1.28
+50			4.8	1.1
19+00			4.4	1.5
" "	20' Lt. Top ex. Paving		4.30	1.63
+50			4.4	1.5

R.P. SPIKE  
M.P.P. #371 R  
Set by Stone 10/17  
10/10/4

Red 11/4/4 w.o.

5.93

3

TP.	5.75	<u>7.29</u>	4.39	1.54
20+00			5.3	2.0
" "	20' Lt. Top ex. Paving		5.35	1.94
+50			5.4	1.9
21+00			5.4	1.9
" "	20' Lt. Top ex. Paving		5.10	2.19
+50			5.3	2.0
22+00			5.0	2.3
" "	20' Lt.		4.79	2.50
+50			4.9	2.4
+79	20 p.c.c. on slab		4.85	2.44
" "	20' Lt. Edge ex. Paving		4.56	2.73
23+00			4.9	2.4
" "	19.5' Lt. Edge ex. Paving		4.51	2.78
+50			4.8	2.5
24+00			4.7	2.6
" "	16.9' Lt. Edge ex. Paving		4.49	2.80
+50			4.8	2.5
25+00			4.8	2.5
" "	16' Lt. Edge ex. Paving		4.59	2.70
TP.	4.17	<u>6.81</u>	4.65	2.64
+50			4.3	2.5
26+00			4.2	2.6
" "	1.55' Lt. Edge ex. Paving		4.12	2.69
+23	25' int. edge ex. paving		4.12	2.69
26+27.75	L. Lt		4.11	2.70
" "	0.5' Rt. edge ex. paving		4.12	2.69



T  
6.81

26+61 <sup>1</sup> -	ex. Paying	3.99	2.82
26+93 <sup>8</sup>	N. Edge ex. Paying	4.30	2.51
27+01 <sup>3</sup>	N. Edge Rock & oil berm.	4.5	2.3
27+40		5.8	1.0
+75		6.7	0.1
28+00		6.3	0.5
+42 <sup>47</sup>	Mon. & Mason <sup>on</sup> lead	6.16	0.65
+50		6.0	0.8
29+00		6.3	0.5
+08		6.3	0.5
+14		5.1	1.7
+36 <sup>4</sup>	inf 36" spec. Drain	5.3	1.5
"	Flow Line <small>Pipes open on N. side. Note of grade from State Eng.</small>	9.56	2.75
+50		5.8	1.0
30+00		5.3	1.5
+50		4.8	2.0
T.P.	170	<u>6.53</u>	1.98 4.83
31+00		4.8	1.7
+50		4.9	1.6
+92 <sup>54</sup>	Mon & Smith <sup>on</sup> lead	5.40	1.13
32+00		4.9	1.6
+50		4.6	1.9
33+00		4.4	2.1
+50		4.4	2.1
34+00		4.4	2.1

T  
6.53

4

34+50		4.2	2.3
35+00		4.3	2.2
+42 <sup>86</sup>	Mon. & Wallace on lead	5.31	1.22
36+00		4.1	2.4
T.P.	428	<u>6.81</u>	4.00 2.53
+50		4.4	2.4
37+00		4.5	2.3
+50		4.3	2.5
38+00		4.5	2.3
+50		4.8	2.0
39+00		4.6	2.2
+17 <sup>88</sup>	Mon. & Taylor on lead	5.14	1.67
+50		4.5	2.3
40+00		4.7	2.1
+50		4.5	2.3
41+00		4.5	2.3
+50		4.5	2.3
42+00		4.1	2.7
+48	L. Lt. 1"x1" pipe stub	4.34	2.47
T.P. on L.	496	<u>7.43</u>	4.34 2.47
+98	15 Rt. to edge ex. paying	4.87	2.56
+73	S. line Kutz	5.0	2.4
43+00		5.1	2.3
"	" 2" Rt. edge ex. paying	5.00	2.43
+50		5.0	2.4



44+00			4.8	2.6
44+50	2 <sup>nd</sup> Rt ex. Paving oil	Rock	4.71	2.72
45+00			4.8	2.6
45+50			4.4	3.0
46+00	2 <sup>nd</sup> Rt +- ex paving		4.36	3.07
46+50			4.6	2.8
46+60			4.8	2.8
46+30			4.4	3.0
49+14	inf Rock + oil Paving	Curve from Frontier	3.92	3.51
46+00			3.90	3.53
45+00	on Rock + oil paving		4.02	3.41
48+87 =	S.S. H. line Frontier		3.92	3.51
TP:	2.57	610	3.90	3.53
Check BM:			5:57	0.53
				0.56
				0.03 error







c	Par	8.46	3006
1/4	"	8.44	3008
gvt	"	8.42	3010
cb		7.70	3082
E		7.7	308
0 + 50			
E		4.9	336
+9		5.4	331
cb		6.4	321
+1		7.3	312
1/4		6.6	319
c		6.2	323
1/4		6.4	321
cb		6.4	321
+2		6.0	325
w		6.2	323
0 + 85.7			
w	+0.8 edge cent. walk	4.44	3408 ✓
0 + 93.9			
w	+0.8 edge " "	4.23	3429 ✓
1 + 00			
w		4.0	345
cb		4.4	343
+2		4.7	338
1/4		4.3	342
c		4.1	344

1/4		4.5	340
+3		5.0	335
cb		4.5	340
+1		3.7	348
+8		3.4	351
E		2.4	361
1 + 00			
w	+ 2' cent. walk	3.90	3462 ✓
1 + 35.6			
E	-1.8 2' cent walk	1.53	36.99 ✓
1 + 37.7			
E	+0.1 6" drain outlet	2.37	36.15 ✓
1 + 50			
E		0.8	37.7
+2		1.5	37.0
cb		2.4	36.1
+2		2.8	35.7
1/4		2.3	36.2
c		2.1	36.4
1/4		2.4	36.1
cb		2.4	36.1
w		2.7	35.8
T.P. 7.00		46.13	1.41 37.11



	1+50			
E-7.2	edge Conv. apron	7.29	38.84	
E-29.9	" do. garage	7.08	39.05	
	1+72			
E-7.2	edge apron	7.37	38.76	
E-29.9	" garage	7.07	39.06	
	1+63.6	Line Colthoun		
W		10.1	36.0	
cb		9.7	36.4	
1/4		9.4	36.7	
c		9.1	37.0	
1/4		9.2	36.9	
cb		9.2	36.9	
E		8.2	37.9	
	E	Colthoun		
E		9.6	38.5	
+8		8.0	38.1	
cb		8.7	37.4	
1/4		8.9	37.2	
c		8.5	37.6	
1/4		8.7	37.4	
cb		9.1	37.0	
W		10.1	36.0	
	E + 7			
W		10.2	35.8	
cb		9.6	36.5	

1/4		8.6	37.5	
c		8.4	37.7	
	E + 10			
c		8.3	37.8	
1/4		8.5	37.6	
+3		9.0	37.1	
+5		9.5	36.6	
cb		8.8	37.3	
W		8.3	37.8	
	0+0 = Nly Colthoun		2103.66	
W		7.6	38.5	
+8		7.9	38.2	
cb		8.5	37.6	
+2		9.0	37.1	
1/4		8.4	37.7	
c		8.0	38.1	
1/4		8.3	37.8	
cb		8.2	37.9	
E		6.2	39.9	
	0+50		2153.66	
E-2		4.7	43.4	
E		4.1	42.0	
+2		5.8	40.3	
cb		6.6	39.5	
1/4		6.6	39.5	
c		6.5	39.6	



1/4		6.7	39.2
cb		7.0	39.1
+3		6.7	39.4
w		11.3	41.8
	1+00	3+03.66	
w-3		2.7	43.4
w		3.4	42.7
cb		5.1	41.0
+w		5.5	40.6
1/4		4.8	41.3
c		4.4	41.7
1/4		4.4	41.7
+3		5.1	41.0
cb		4.4	41.0
+4		2.6	43.5
E		2.2	43.9

T.P. 6.88 5095 2.02 44.07

1+50

3+53.66

E		5.6	45.4
+8		5.8	45.2
cb		7.4	43.8
+w		7.9	43.1
1/4		7.1	43.9
c		7.0	44.0

1/4		7.4	43.6
4c		8.6	42.4
cb		7.7	43.3
w		6.9	44.1
+c		4.7	46.3
	2+00	4+03.66	
w		5.4	45.8
+9		5.7	45.3
cb		6.3	44.7
1/4		5.5	45.5
c		5.0	46.0
1/4		5.0	46.0
+5		5.6	45.4
cb		5.0	46.0
+w		3.5	47.5
E		2.8	48.2

2+39

4+37.66

E		1.6	49.4
cb		2.3	48.7
+1		2.7	48.3
1/4		3.4	47.8
c		3.4	47.6
1/4		4.0	47.0
cb		4.0	47.0
w		3.3	47.7



~~4244.91~~

2 + 41.25	Sly	Juan	57.	
W		4.0	470	
+ 9.5 end Top	Curb	3.79	47.16	
gvt	pay	4.14	46.81	
1/4	"	3.80	47.15	
c	"	3.38	47.57	
1/4	"	3.01	47.94	
gvt	"	2.62	48.33	
" + 0.5 end Top	Curb	7.14	48.81	48.81
E		1.6	49.4	

583-37

+ 48.25 Sly cb Juan

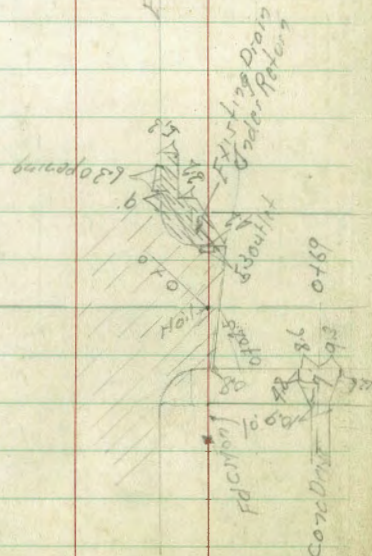
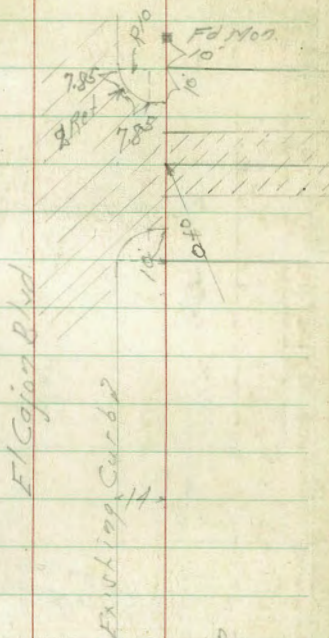
SE	cb	pc.	1.14	49.31
F	gvt.		1.91	49.04
cb	pay		2.53	48.12
1/4	"		2.88	48.07
c	"		3.23	47.72
1/4	"		3.63	47.32
cb	"		3.95	47.00
W	gvt		2.39	46.56
W	cb	pc.	4.04	46.91



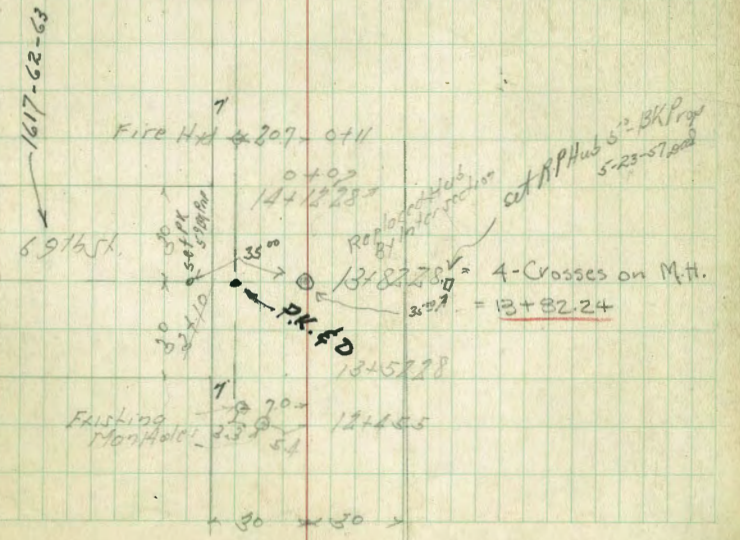
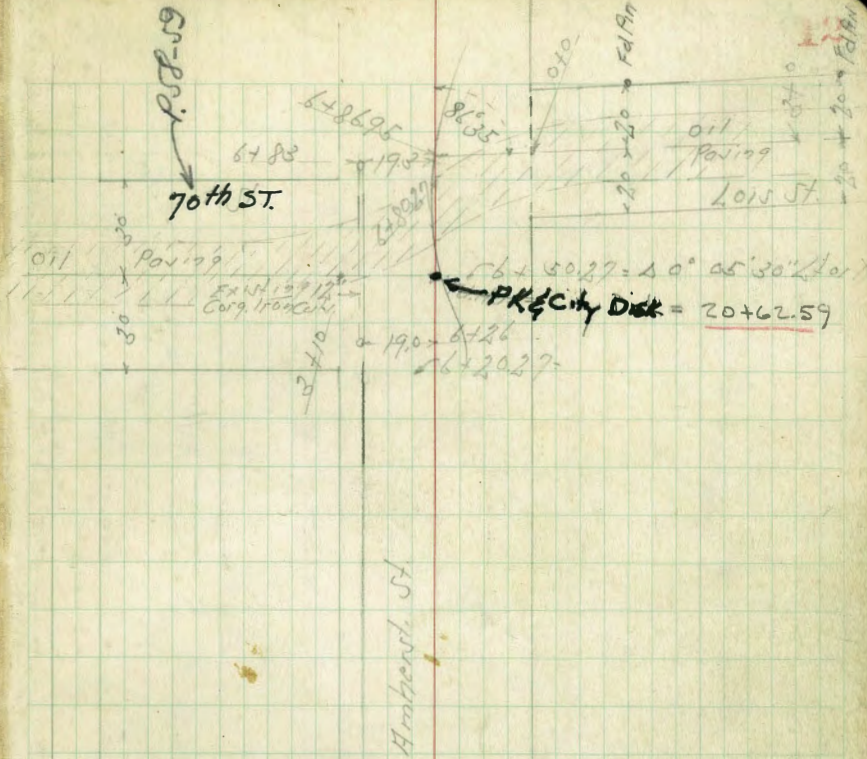




Amherst St.



60-25-1  
70th ST.





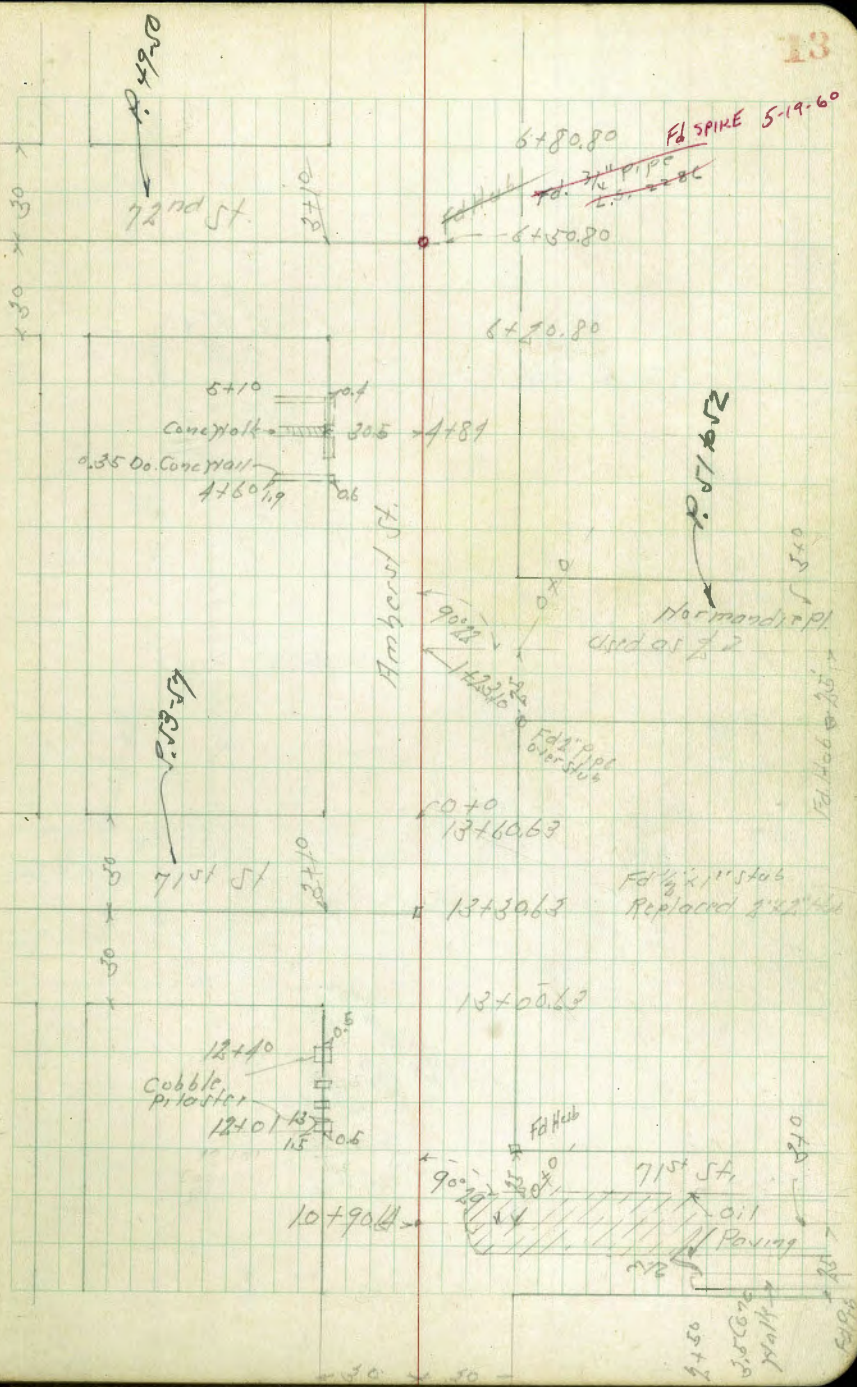
SET CITY disk  
7' PT.  
6-20-46  
C.S.M.

El Cajon Blvd

Frasing Carb 2

Fd. Con. 10' 70'

Fd. Con. 10' 70'









Cross Section from 4th St.  
67th St to 73rd St.

1+0 23.2 Pt of  $\Delta$  - Sky Power Pole ✓

0+79 =  $\Delta$  Double Garage ✓

0+50

0+25

0+0 = E.L. 67th on North

S.C.H. = E.L. of 67th St on Diagonal

B.M. 0.72 454.42

453.70

S.W. B.P.  
E.I. Corp  
67th St

Reduced & Plotted on Profile 2898  
3-4-42 - C.B.H.

Lt = 11

2

Pt. 5

448.9 55 30	448.8 56 20	448.6 58 10	448.0 64 5	448.2 62	448.0 64 17	448.6 58 20	448.8 56 30	
						448.17 ✓ 6.25 88.5 - 11/2 Cont H. Prop.	448.28 ✓ 6.14 70.0 - 2 Bedrock Conc. Fl.	
448.7 57 30	448.4 60 20	448.2 62 13	447.2 72 9	447.6 68	447.3 71 15	448.2 62 20	448.9 66 30	
448.7 57 30	448.1 63 20	448.1 63 14	446.0 81 10	446.6 78	446.6 78	447.5 69 20	448.6 58 26	448.5 59 30
448.8 56 30	448.9 55 20	445.3 91 10	445.5 89	445.3 91	446.3 81 20	448.8 56 27	448.9 55 30	
448.8 56 30.6	449.0 54 20.4	448.8 56 18	445.3 91 14	445.2 92	449.8 96 18	445.8 86 20.4	448.8 56 27	449.1 55 30.6
954.43								



2+13

2+0

1+81 240 Rt of Z = 5/4 Porcel Poll ✓

1+63 = Conc Gutter on Lt.

TP 5.52 454.68 5.26 449.16   
 Nail Panel  
 Pole  
 1+81 on Rt

1+62 30' Lt of Z = Fly 1.0 Rubble Wall ✓

1+50

1+22 300' Lt of Z = Wk 1.0 Rubble Wall ✓

1+17 = Z 84 Conc Drain on Lt ✓

454.42

Lt

Z

Rt

16

449.89 ✓

449.89 ✓

4.79  
30' on Wall

4.79  
16.95/1.03  
Conc Poll

449.4 449.3 449.2 448.9 449.1 449.3 448.9 448.8 448.3  
5.3 5.4 5.5 5.8 5.6 5.4 5.8 5.9 6.4  
30 20 10 5 10 20 30 50

449.129 ✓

449.16 ✓

5.39  
30' on Wall

5.52  
30' on Wall  
Conc

449.09

448.62

449.00 ✓

448.48 ✓

5.59  
30' on Wall

6.06  
30' Gutter

5.68  
10.5' on Wall

6.70  
10.5' Gutter

454.68

448.88

448.8

448.5

448.4

448.5

448.4

448.6

448.7

448.4

5.6  
30' on Wall

5.6  
20'

5.6  
10'

6.0  
6.5

5.9  
1.5

5.8  
20'

5.7  
30'

6.0  
20'

449.02

448.91

5.4  
30' on Wall

5.51  
30' on Wall  
Conc

454.42



2+10 = 3.5 ft of  $\frac{1}{2}$  = NY Con. Glass Hot House ✓

2+82 = 3.0 Conc Walk on Lt. ✓

2+67 = 2.2 on Diag Conc Walk ✓

2+62 = 2.1 Lt of  $\frac{1}{2}$  = Sky Picket Fence ✓

2+57 =  $\frac{1}{2}$  72 Conc Drive on Lt ✓

2+50

2+37 = 3.7 Conc Walk on Lt ✓

454.68

450.5	450.3	450.2	449.7	449.9	450.0	449.7	450.0	450.26
$\frac{1.2}{30}$	$\frac{1.1}{20}$	$\frac{1.5}{15}$	$\frac{5.0}{50}$	1.8	$\frac{1.7}{10}$	$\frac{5.0}{20}$	$\frac{1.7}{36}$	$\frac{1.52}{31.5}$

100 Conc Found Below of 6 last

450.91	450.66
$\frac{5.77}{30}$	$\frac{1.02}{18.8}$

3.0 Conc Walk  
Sky Picket Fence

449.93

$\frac{4.75}{31.0}$   
2.2 Conc Walk

450.78	450.43
--------	--------

$\frac{3.90}{30}$	$\frac{4.25}{17.0}$
-------------------	---------------------

3.0 Conc Drive  
Sky Picket Fence

450.7	450.5	449.8	449.5	449.6	449.7	449.4	449.7	450.0
$\frac{1.30}{30}$	$\frac{1.2}{20}$	$\frac{1.9}{15}$	$\frac{5.2}{50}$	5.1	$\frac{5.0}{10}$	$\frac{5.0}{20}$	$\frac{5.0}{30}$	$\frac{2.0}{20}$

450.39	450.36
--------	--------

$\frac{1.39}{30}$	$\frac{1.39}{18.8}$
-------------------	---------------------

3.0 Conc Walk  
Sky Picket Fence

454.68



4+26 316 - Rt of Lt - H.F. Car Hot House ✓

4+0

3+98 = Lt 70 2 Ribbon Conc Dr. 2 Ribbon ✓

3+53 = Lt 76 Conc Dr. on Lt ✓

3+37 = Lt 25 Conc Walk on Lt ✓

3+30 23.5 Rt of Lt - Sly Power Pole ✓

3+04 = Lt 6.9 - 2 Ribbon Conc Dr. 2 Ribbon ✓

45468

Lt.

Lt.

Rt.

18

450.91

3.77  
3.76

Top Conc Found  
Hot House

451.1

451.0

450.1

450.1

450.4

450.2

450.4

450.5

3.6  
3.6

3.7  
3.6

3.6

3.6

3.8  
3.8

3.5  
3.8

3.3  
3.6

3.2  
3.3

451.11

451.03

3.57  
3.60 on Dr.

3.65  
3.82 - 2 Ribbon  
Conc Dr.

450.80

450.72

450.70

450.0

449.9

449.9

450.4

450.1

450.43

3.88  
3.90 on Dr.

3.91  
3.90 on Dr.

3.98  
3.81 - 2 Ribbon  
Conc Dr.

4.7  
4.8

4.8

4.8  
4.8

4.3  
4.2

4.6  
4.6

4.25  
3.15 on Conc  
Foot of  
Hot House

450.96

450.75

3.71  
3.60 on Walk

3.93  
3.84 - 2.25  
Conc Walk

450.50

450.25

4.18  
4.60 on Dr.

4.13  
4.71 - 2.25  
Conc Dr.

45468



6742 300 Lt of  $\frac{1}{2}$  = Fly Wire Fence Nly Picket Fence ✓

TP 499 455.91 3.76 450.92

6734 26.2 Lt of  $\frac{1}{2}$  = Nly 12" Acacia Tree ✓

670 26.4 Lt of  $\frac{1}{2}$  = Nly 12" Acacia Tree ✓

5775

5763 30.0 Lt of  $\frac{1}{2}$  = Fly Wire Fence ✓

5750

5732 =  $\frac{1}{2}$  1.5 Cone Walk on Pt ✓

5730 22.9 Pt of  $\frac{1}{2}$  = Fly Paper Pole ✓

570

4750

454.68

$\frac{1}{2}$

$\frac{1}{2}$

Pt.

451.6 451.5 451.0 450.5 450.7 450.7 450.7 450.8 449.7 449.5 450.1  
 $\frac{3.7}{40}$   $\frac{3.8}{30}$   $\frac{3.7}{20}$   $\frac{3.8}{15}$   $\frac{4.0}{15}$   $\frac{4.0}{10}$   $\frac{4.0}{10}$   $\frac{3.9}{20}$   $\frac{5.0}{25}$   $\frac{5.1}{30}$   $\frac{4.6}{40}$

451.0 450.9 450.5 450.6 450.5 450.6 450.6 450.4 450.7 449.5 449.5 449.7  
 $\frac{3.7}{40}$   $\frac{3.8}{30}$   $\frac{4.0}{20}$   $\frac{4.1}{10}$   $\frac{3.8}{15}$   $\frac{4.1}{10}$   $\frac{4.1}{10}$   $\frac{4.0}{17}$   $\frac{4.0}{10}$   $\frac{5.2}{25}$   $\frac{5.2}{30}$   $\frac{5.0}{40}$

450.7 450.6 450.3 451.0 450.4 450.3 450.3 450.7 450.1 450.1  
 $\frac{4.0}{40}$   $\frac{4.0}{30}$   $\frac{4.1}{20}$   $\frac{5.2}{15}$   $\frac{4.0}{15}$   $\frac{4.1}{10}$   $\frac{4.1}{10}$   $\frac{4.0}{20}$   $\frac{4.6}{30}$   $\frac{4.6}{35}$

450.68 ✓  
 $\frac{4.0}{40}$   
 $\frac{4.1}{30} = \frac{1.1}{15}$   
 Cone Walk

451.0 451.0 450.7 450.5 450.4 450.3 450.5 450.7 450.6 450.6  
 $\frac{3.7}{40}$   $\frac{3.7}{30}$   $\frac{4.0}{20}$   $\frac{4.2}{15}$   $\frac{4.0}{15}$   $\frac{4.1}{10}$   $\frac{4.2}{10}$   $\frac{4.0}{20}$   $\frac{4.1}{30}$   $\frac{4.1}{40}$

451.2 450.9 450.4 450.4 450.7 450.8 451.0 451.0  
 $\frac{3.5}{30}$   $\frac{3.8}{20}$   $\frac{4.0}{15}$   $\frac{4.0}{10}$   $\frac{4.1}{10}$   $\frac{3.9}{20}$   $\frac{3.7}{30}$   $\frac{3.7}{40}$

454.68

454.68



7+83.21 Approx W.L. Olive St ✓

7+77 22.3 Rt of L = Sly Power Pole ✓

7+32.76 = E.L. 68<sup>th</sup> St

7+11

BM

492

450.99

Hub  
H. Herbert  
88<sup>th</sup> St

7+02.76 - L

6+80 22.5 Rt of L = Sly Power Pole ✓

6+72.76 W.L. 68<sup>th</sup> St 300 Lt of L = Fly Picket Fence ✓

6+52 26.0 Lt of L = 1/4 8" Pecan Tree ✓

6+50

455.91

Lt.

L

Rt

20

451.5	451A	451.0	451.3	450.9	451.0	450.7	450.1	449.9
4.4 30	4.5 30	4.9 30	4.6 30	5.0 30	4.9 30	5.2 30	5.8 30	6.0 30

451.9	451.2	450.9	451.4	451.1	451.2	451.1	450.5	450.8	450.3	450.1
4.9 30	4.7 30	5.0 30	4.5 30	4.8 30	4.7 30	4.8 30	5.1 30	5.1 30	5.6 30	5.8 30

450.88

451.46

5.03

81.5 = H. 1033 Conc Well

4.45

81.5 = H. 1033 Conc Well

451.3

451.3

451.5

451.5

451.2

450.9

450.9

451.1

4.6  
30

4.6  
30

4.4  
30

4.4  
30

4.7  
30

5.0  
30

5.0  
30

4.8  
30

452.1

451.6

451.1

451.3

451.1

451.0

450.0

450.7

5.8  
30

4.9  
30

4.8  
30

4.6  
30

4.8  
30

4.9  
30

5.9  
30

5.7  
30

452.0

451.9

451.3

450.7

450.6

450.9

450.9

451.0

451.0

449.9

449.9

450.3

4.9  
30

4.9  
30

4.6  
30

5.2  
30

5.3  
30

5.0  
30

5.0  
30

4.9  
30

4.9  
30

6.0  
30

6.0  
30

5.6  
30

455.91



9+86 21.8 Rt of  $\frac{1}{2}$  = Sly Porter Pole ✓

9+50

9+0

8+72 = 0.33 Conc Wall on Rt

8+50 22.0 Rt of  $\frac{1}{2}$  = Sly Anchor Pole

8+20

8+0

45591

452.9	452.1	452.1	451A	451.7	451.7	451.2	453.0	452.3	452.0
$\frac{3.0}{2.0}$	$\frac{3.8}{2.0}$	$\frac{3.8}{2.0}$	$\frac{4.5}{2.0}$	$\frac{4.0}{2.0}$	$\frac{4.2}{2.0}$	$\frac{4.2}{2.0}$	$\frac{4.9}{2.0}$	$\frac{3.6}{2.0}$	$\frac{3.9}{2.0}$

452.6	452.1	452.1	451.2	451A	451A	450.8	451.6	451.9	452.1
$\frac{3.0}{2.0}$	$\frac{3.8}{2.0}$	$\frac{3.8}{2.0}$	$\frac{4.7}{2.0}$	$\frac{4.5}{2.0}$	$\frac{4.5}{2.0}$	$\frac{5.1}{2.0}$	$\frac{4.3}{2.0}$	$\frac{4.0}{2.0}$	$\frac{3.8}{2.0}$

451.88 ✓

$\frac{4.03}{3.1} = 1.1033$   
0.33 Conc Wall

452.1	451.7	451.2	451.5	451.0	451.2	451.3	450.8	451.3	451A	451.1
$\frac{3.8}{2.0}$	$\frac{4.2}{2.0}$	$\frac{4.7}{2.0}$	$\frac{4.1}{2.0}$	$\frac{4.9}{2.0}$	$\frac{4.7}{2.0}$	$\frac{4.5}{2.0}$	$\frac{5.1}{2.0}$	$\frac{4.6}{2.0}$	$\frac{4.5}{2.0}$	$\frac{4.8}{2.0}$

451.5	451.6	451.1	451.2	450.8	451.0	451.3	450.6	451.0	450.8
$\frac{4.4}{2.0}$	$\frac{4.0}{2.0}$	$\frac{4.8}{2.0}$	$\frac{4.7}{2.0}$	$\frac{4.7}{2.0}$	$\frac{4.9}{2.0}$	$\frac{4.5}{2.0}$	$\frac{5.3}{2.0}$	$\frac{4.9}{2.0}$	$\frac{5.1}{2.0}$

451.4	451.5	451.0	451.4	451.0	450.9	451.1	451.1	450.8
$\frac{4.5}{2.0}$	$\frac{4.6}{2.0}$	$\frac{4.9}{2.0}$	$\frac{4.5}{2.0}$	$\frac{4.9}{2.0}$	$\frac{5.0}{2.0}$	$\frac{4.8}{2.0}$	$\frac{4.8}{2.0}$	$\frac{5.1}{2.0}$

45591



11+50

11+11 = 1/2 35 Conc Walk on H1 ✓

11+0

10+75 = 1/2 39 Conc Walk on H1 ✓

TP 4.98 457.66 3.23 452.68

Hall Floor  
Polc Pt  
9+86

10+50

10+0

455.91

L1

R1

R1

22

453.1	452.8	452.8	452.6	452.0	452.7	453.2	450.4
4.6 30	4.9 20	4.9 10	5.1	5.2 15	5.0 10	5.5 0	7.0 15

453.16

4.48  
301-5145 Conc  
Walk

453.2	452.8	452.4	452.5	452.5	451.8	452.7	453.3	451.6
4.5 30-8.056 Walk	4.9 10	5.3 10	5.2	5.5 15	5.9 15	5.0 10	6.1 0	6.1 10

453.05

453.05

4.41  
30 on Walk  
4.61  
472-5139  
Conc Walk 457.66

453.1	452.9	452.6	452.3	452.1	451.4	452.2	452.9	451.4
4.8 30-0.17 Walk	4.0 10	3.3 10	3.6	3.8 0	4.5 14	4.7 10	5.0 0	4.5 10

452.9	452.2	452.4	251.9	251.7	251.5	252.3	252.6	252.1
5.0 10	4.7 10	3.5 10	4.0 10	4.2	4.4	5.0 10	5.0 0	4.0 10

455.91











2+32 230 Pt of L = 5/4 14" Acacia Tree ✓  
 3+18 230 = Pt of L = 5/4 12" Acacia Tree ✓  
 3+0

2+90 29' Pt of L = 5/4 8" Acacia Tree ✓  
 2+80 = L 2.8 Conc Walk on Lt ✓  
 2+76 230 Pt of L = 5/4 10" Acacia Tree ✓  
 2+61 283 Lt of L = 5/4 Picket Fence ✓  
 2+54 29.5 Pt of L = 5/4 Picket Pole ✓  
 2+51

2+0

1+69 = L 4.0 Conc Walk on Pt ✓  
 1+61 288 Lt of L = 5/4 Picket Fence ✓  
 1+55 = L 6.6-2 Ribboz Conc Dr. on Lt 2 R. 66oz ✓

460.46

	Lt.	Rt.	Pt.	
	457.5	457.0	456.5	456.7
	3.0	3.5	4.0	3.8
	457.94 ✓			456.6
		457.81 ✓		456.9
	2.52	2.65		456.5
	100' Walk	288 = 5/4 8" Conc		456.2
	458.17 ✓	457.68 ✓	456.7	456.5
	2.39	2.78	3.8	4.0
	700' Walk	28.7	3.0	3.9
	456.7	456.1	456.3	456.6
	3.8	4.1	4.2	4.4
	3.0	3.0	3.0	3.0
	456.7	456.1	456.3	456.3
	3.8	4.1	4.2	4.2
	3.0	3.0	3.0	3.0
	456.7	456.1	456.3	456.4
	3.8	4.1	4.2	4.1
	3.0	3.0	3.0	3.0
	456.7	456.1	456.3	456.0
	3.8	4.1	4.2	4.5
	3.0	3.0	3.0	3.0
	456.7	456.1	456.3	455.9
	3.8	4.1	4.2	4.1
	3.0	3.0	3.0	3.0
	456.7	456.1	456.3	455.6
	3.8	4.1	4.2	4.1
	3.0	3.0	3.0	3.0
	456.7	456.1	456.3	455.78
	3.8	4.1	4.2	4.1
	3.0	3.0	3.0	3.0
	456.7	456.1	456.3	455.78
	3.8	4.1	4.2	4.1
	3.0	3.0	3.0	3.0
	456.7	456.1	456.3	455.7
	3.8	4.1	4.2	4.1
	3.0	3.0	3.0	3.0
	456.7	456.1	456.3	455.2
	3.8	4.1	4.2	4.1
	3.0	3.0	3.0	3.0
	456.7	456.1	456.3	455.8
	3.8	4.1	4.2	4.1
	3.0	3.0	3.0	3.0
	456.7	456.1	456.3	455.7
	3.8	4.1	4.2	4.1
	3.0	3.0	3.0	3.0
	456.7	456.1	456.3	455.5
	3.8	4.1	4.2	4.1
	3.0	3.0	3.0	3.0
	456.7	456.1	456.3	460.46
	3.8	4.1	4.2	4.1
	3.0	3.0	3.0	3.0







Amberst St.

6+80.27 = FL 70<sup>th</sup> St

6+63 256 Rt of 1/2 = Sky Power Tel Pole ✓

6+50.27 = 1/2 70<sup>th</sup> St

BM 836 467.23 3.70 458.87 <sup>2. Hub</sup> <sub>1.70 60<sup>th</sup> St</sub>

6+26 = N End 12" Cong. Culv. 00 Lt ✓

6+20.27 = N.L. 70<sup>th</sup> St.

6+10 254 Rt of 1/2 = Sky Tel Pole ✓

6+0

5+50

462.57

Feb. 19-48

457.4	457.2	457.4	456.0	460.1	460.2	460.2		
7.8 30	8.0 30	7.8 30	7.2	7.1 30	7.0 30	7.0 30		
457.4	457.2	457.3	457.2	458.9	458.4	458.9	457.2	460.3
7.8 30	8.0 30	7.9 30	8.0	8.3 30	8.8 30	8.3 30	8.0 30	8.9 30
				467.23				
				457.65				
				1.93				
				19.0				
				= N End 12"				
				Cong. Culv.				
				Florida				
458.8	458.7	458.2	458.6	458.4	458.2	458.4	458.5	459.6
3.8 30	3.9 30	4.1 30	4.0	4.2 30	4.5 30	4.2 30	4.1 30	4.0 30
458.6	458.3	458.0	458.4	458.3	457.7	458.3	458.1	457.9
6.0 30	4.5 30	4.6 30	4.6	4.3 30	4.7 30	4.3 30	4.5 30	4.7 30
458.8	458.0	457.7	458.2	458.0	457.8	457.7	457.7	458.2
3.8 30	4.6 30	4.9 30	4.4	4.6 30	4.8 30	4.9 30	4.9 30	4.4 30
				462.57				







10+33 = Z 7-7-2 Ribboz Cone Dr. 2' Ribboz on Lt ✓

10+0

9+92 246 Rt of Z - Sly Power Tail Pole ✓

9+80 = Z 8.5 Cone Drive on Rt ✓

9+72 30 Rt of Z - Ely Wire Fence ✓

9+50

9+26 30 Rt of Z - Wly Wire Fence ✓

9+17 = Z of Porch on Lt ✓

9+0

46723

	Lt	Z	Rt
	46413	46427 ✓	
	310 21' 0" Dr. = 21' Hour	296 297' - SH 2 Ribboz Cone Dr.	
	4636	4637	4639
	36 10' 51" Dr. = 10' 51" Hour	35 30	33 20
		4647	4650
		25 10	26
		4649	4643
		29 10	29 20
		4658	4661
		14 25	11 60
		46513 ✓	46617
		210 216.3' - 1/2" 11' 85" Cone Dr. =	139.4 139.4' - 1/2" 11' 85" Grate.
		(Calc. 30' at 46513)	59.2 59.2' - 1/2" 11' 85" Grate.
	4626	4623	4624
	46	49	48
	40	30	20
		4631	4636
		41	21
		4635	4639
		36 10	44 20
		4652	
		42 20	43 30
	46301 ✓	46273 ✓	
	337 341' - Porch Landing	450 444' - Tom Bottom 54' P	
	4620	4616	4618
	52 10	56 30	54 20
		4623	4626
		49 10	46
		4625	4620
		47 10	50 20
		4639	
		54 30	55 30
		46723	



11+92 = 2 3 Conc Walk on Rt ✓

11+50

11+15 24.6 Rt of 2 5/4 Tol Pole ✓

TP 6.77 17312 0.88 466.35

10+91 = Approx 1/2 of 71<sup>st</sup> to South ✓

10+79 = 2 7.7 Conc Dr. N Rib. 30 E Ribber 20 ✓

10+65 24.6 Rt of 2 5/4 Tol Pole ✓

10+50

467.23

LT = 11

8

RT = 5

30

468.79 ✓

469.24 ✓

4.33  
1.30 = 1/4 2.0  
Conc Walk

3.90  
1.90 on Walk

465.6

465.8

466.4

466.3

467.1

467.4

467.1

469.4

7.5  
4.0

7.3  
3.0

6.7  
2.0

6.8  
1.0

6.0

5.7  
1.0

6.0  
2.0

6.7  
3.0

465.4

465.6

465.9

465.9

466.7

466.9

466.8

468.9

7.7  
1.0

7.5  
3.0

7.2  
2.0

7.2  
1.0

6.4

6.2  
1.0

6.0  
2.0

7.2  
3.0

473.12

464.6

464.8

465.0

465.2

466.2

466.8

467.3

467.8

7.6  
4.0

7.4  
3.0

7.2  
2.0

8.0  
1.0

1.0

0.4  
1.0

10.1  
2.0

10.6  
3.0

464.60 ✓

464.70 ✓

2.63

2.53

16.1 = 5 1/4 hr  
Hour

29.7 = 5 1/2 Ribber  
Condrin

464.3

464.9

464.6

465.2

465.7

466.0

465.5

467.4

7.0  
4.0 = 5 1/4 Hour

7.5  
3.0

7.6  
2.0

7.0  
1.0

1.5

1.2  
1.0

1.7  
2.0

10.2  
3.0

467.23







2+60 31.24 of 2 = Fly Resc Trills ✓

2+50

TP 11.42 484.01 0.53 472.59

2+0

1+50

1+49 22.8' 1/2 = Sly Power Hal pole 22.34 of 2 = 1/4 Anchor pole ✓

1+18

1+0 - Approx WL - Normandie Place ✓

0+50

473.12

47

2

PT

32

4716	4714	4715	4720	4726	4727	4732	4737	4737	4739
124/40	136/30	125/20	130/15	114	110/6	108/10	100/20	108/30	101/40

48401

4711	4701	4708	4710	4713	4717	4722	4721	4718	4723
20/40	30/30	23/20	21/10	18	16/10	9/12	10/20	10/30	9/20

4708	4695	4701	4701	4702	4701	4700	4712	4713
23/40	36/30	30/30	30/11	29	30/8	21/10	19/20	18/30

4698	4697	4698	4695	4699	4701	4709	4713
30/40	39/30	30/20	36/12	32/5	27/10	25/20	18/30

4694	4695	4691	4696	4699	4704	4711
37/30	36/20	40/12	35	33/18	27/20	30/30

4691	4686	4684	4687	4692	4697	4707
40/30	45/20	47/10	44	39/15	31/20	31/30

47312







670

5750

5710

224 Rt of 1/2 - Sly Power Pole ✓

570

4787 - 2.6 Conc Walk on H ✓

4760

484.01

L

R

Rt.

34

4787	4792	4797	4793	4800	4799	4804	4799	4804
570/20	578/30	578/20	577/20	570/20	571/20	576/20	571/20	576/20

4790	4797	4794	4795	4791	4801	4800	4802	4801	4800	4811
570/20	573/30	576/27	575/20	579/20	579/20	570/20	578/20	579/20	570/20	579/20

47881 ✓

47892 ✓

570/20 Conc Walk

570/20 Conc Walk

4786

4789

4790

4790

4794

4800

4804

4808

574/20

571/20

570/20

570/20

576

570

576

570

47820 ✓

47840 ✓

578/20 Conc Walk

570/20 Conc Walk

47820 ✓

47899 ✓

578/20 Conc Walk

570/20 Conc Walk

48401



8+0

7+90

39.2 Lt of  $\frac{1}{2}$  = Sky Picket Fence

7+50

7+40

22.5 Lt of  $\frac{1}{2}$  1 1/4" Tree

7+0

6+80.80 = E.L. 72<sup>nd</sup> St.

BM 2.78 482.49 4.30 479.71

on N. Hub St.  
Hamberst  
+ 72<sup>nd</sup> St.

6+50.80 = W.L. 72<sup>nd</sup> St.

6+20.80 = W.L. 72<sup>nd</sup> St.

484.01

477.5 477.4 476.8 476.7 476.6 476.5 476.7 475.6 475.7 475.1 474.5  
 5.0 5.0 5.2 5.8 6.0 6.0 5.8 6.9 6.8 7.4 8.0  
 10 10 10 10 10 10 10 11 10 10 10

478.3 478.0 477.7 477.9 478.1 478.1 478.5 477.1 477.0 476.9 476.6  
 4.2 4.5 4.8 4.6 4.4 4.3 4.0 5.7 5.5 5.6 5.9  
 10 10 10 10 10 10 10 11 10 10 10

478.5 478.7 478.5 479.0 479.1 479.1 479.4 478.7 478.7 478.4 478.0  
 4.0 3.8 4.0 3.5 3.4 3.4 3.1 3.8 3.8 4.1 4.5  
 10 10 10 10 10 10 10 10 10 10 10

479.0 478.8 479.4 479.5 479.9 479.5 479.7 478.6  
 3.5 3.7 3.6 3.0 3.6 3.0 3.0 3.9  
 10 10 10 10 10 10 10 10

478.8 479.2 479.8 480.1 480.0 480.1 479.9  
 5.2 4.8 5.2 3.9 4.0 3.9 3.6  
 10 10 10 10 10 10 10

478.7 479.3 479.5 479.9 479.9 480.1 480.1 480.3  
 5.0 4.7 4.5 3.1 4.1 3.9 3.9 3.7  
 10 10 10 10 10 10 10 10

484.01



9+50

768.3	467.1	466.2	465.7	465.7	464.8	464.0	463.0	463.1	462.1
2.7 40	3.9 30	4.8 25	5.3 20	5.3 10	6.2	7.0	8.0 20	7.9 30	8.9 10

9+25

472.0	470.9	469.2	468.6	468.7	467.5	466.1	465.8	465.4	463.8
1.0 40	0.1 30	1.8 25	2.1 20	2.3 10	3.5	4.9 10	5.1 20	5.6 30	7.2 10

TP 0.52 471.04 11.97 470.52

473.5	473.2	472.6	471.5	471.8	471.04	470.6	468.9	468.6	467.5	466.2
9.0 40	9.3 30	9.9 25	11.0 20	10.7 10	11.9	13.6 10	13.9 20	15.0 30	16.3 10	

9+0

8+75

475.0	474.9	474.7	474.1	474.3	473.6	473.6	472.0	471.4	470.6	468.8
7.5 10	7.6 30	7.8 22	8.4 20	8.2 10	8.9	8.9	10.5 8	11.1 20	11.9 30	13.7 10

8+50

476.2	475.7	475.4	475.5	475.4	475.5	473.7	473.6	472.5	471.1
6.3 40	6.8 30	7.1 20	7.0 10	7.1	7.0	8.8 10	8.9 20	10.0 30	11.4 10

8+40 30.2 H of L - Sly Leds Fence ✓

✓  
477.01

✓  
476.79

8+30 1/2 8 CONDOR on Lt ✓

5.48  
4 CONDOR

5.70  
30-51/8  
CONDOR

482.49

482.49







12+25

12+21

300 Rpt of  $\frac{1}{2}$  = Sly Power Pole ✓

12+17

TP

11.14 481.22 0.96 170.08

12+0

11+65

11+30

11+0

471.04

LT

Z

RT

38

467.6	468.4	469.2	469.9	470.9	471.0	471.0	471.8	472.0
$\frac{13.6}{40}$	$\frac{13.8}{30}$	$\frac{12.0}{20}$	$\frac{11.3}{10}$	$\frac{12.3}{10}$	$\frac{10.2}{10}$	$\frac{10.8}{20}$	$\frac{9.1}{30}$	$\frac{9.1}{40}$

466.2	467.2	468.4	468.8	469.6	469.9	469.9	470.4	468.8
$\frac{15.0}{40}$	$\frac{14.0}{30}$	$\frac{12.8}{20}$	$\frac{12.1}{10}$	$\frac{11.6}{10}$	$\frac{11.3}{10}$	$\frac{11.0}{30}$	$\frac{11.8}{30}$	$\frac{12.1}{40}$

465.1	465.8	465.9	<u>481.32</u>		467.3	467.7	467.6	467.4
$\frac{5.7}{40}$	$\frac{5.8}{30}$	$\frac{5.1}{20}$	$\frac{1.7}{10}$	$\frac{4.2}{10}$	$\frac{5.7}{10}$	$\frac{5.3}{20}$	$\frac{5.4}{30}$	$\frac{5.6}{40}$

461.8	462.3	462.6	462.3	462.5	462.8	462.7	463.3	464.0	463.9
$\frac{9.2}{50}$	$\frac{8.7}{30}$	$\frac{8.4}{20}$	$\frac{8.7}{10}$	$\frac{8.5}{10}$	$\frac{8.2}{10}$	$\frac{8.3}{20}$	$\frac{7.9}{30}$	$\frac{7.0}{40}$	$\frac{7.1}{50}$

460.3	459.9	459.8	460.0	460.0	459.9	460.2	460.2	460.3	460.3	459.6
$\frac{10.7}{50}$	$\frac{11.1}{40}$	$\frac{11.2}{30}$	$\frac{11.0}{20}$	$\frac{11.0}{10}$	$\frac{11.1}{10}$	$\frac{10.8}{10}$	$\frac{10.8}{20}$	$\frac{10.7}{30}$	$\frac{10.7}{40}$	$\frac{11.4}{50}$

459.9	459.5	459.2	458.7	458.4	458.6	458.4	458.1	457.9	457.5
$\frac{11.1}{40}$	$\frac{11.5}{30}$	$\frac{11.8}{20}$	$\frac{12.2}{10}$	$\frac{12.6}{10}$	$\frac{12.4}{10}$	$\frac{12.6}{20}$	$\frac{12.9}{30}$	$\frac{12.1}{40}$	$\frac{12.5}{50}$

471.04



BM

2.75 478.47

072406  
Humboldt St  
473rd

18+00.56 = HL 7<sup>th</sup> dN

12+92

24.6 R/O 1/2 = 5 1/4 4" Tree ✓

Reduced Plotted Profile 2497

3-4-42 G.B.H.

12+75

12+55

22.6 Lt of 1/2 = 11 1/4 8" Pepper Tree ✓  
25.5 R/O 1/2 = 5 1/4 6" Pepper Tree ✓

12+50

481.22

Lt = n

2

Rt = 5

39

476.5

476.8

477.1

476.8

477.0

477.0

476.8

47

41

41

44

42

42

43

474.3

474.7

475.5

475.7

475.6

475.4

475.3

475.8

475.5

5.9

6.5

5.7

5.5

5.6

5.8

6.0

5.3

5.7

380

30

20

10

10

20

20

30

194

476.1

471.6

472.3

473.3

474.0

473.8

473.7

474.3

473.9

10.7

9.6

8.7

7.9

7.2

7.4

7.5

6.9

7.8

481.22















5+50

5+31

5+30

5+18

5+0

4+91

4+87

4+82

4+64

4+47

21.0 Lt of  $\frac{1}{2}$  = Wly 2.0 Cypress Hedge ✓

19.5 Lt of  $\frac{1}{2}$  = Wly 3.0 Conc Walk ✓

19.9 Rt of  $\frac{1}{2}$  = Wly Power Pole ✓

24.5 Rt of  $\frac{1}{2}$  =  $\frac{1}{2}$  + Ely 4.0 Cypress Hedge ✓

21.6 Lt of  $\frac{1}{2}$  =  $\frac{1}{2}$  + Wly 5.0 Cypress Hedge ✓

$\frac{1}{2}$  12" Cong Iron Culvert ✓

481.87

481.6	481.3	480.9	480.1	480.0	479.7	479.4	479.5	479.2
$\frac{0.3}{30}$	$\frac{0.6}{23}$	$\frac{1.9}{20}$	$\frac{1.8}{10}$	$\frac{1.9}{10}$	$\frac{2.8}{28}$	$\frac{2.5}{20}$	$\frac{2.1}{20}$	$\frac{2.7}{20}$

✓  
480.87 ✓  
480.57

$\frac{1.06}{30}$  on Walk  
 $\frac{1.30}{21}$  = Wly 0.5 Conc Walk

479.72 ✓  
479.02

$\frac{2.15}{30}$  on Walk  
 $\frac{2.85}{19.5}$  = Wly 3.0 Conc Walk

478.6	477.9	477.5	477.6	477.3	476.5	475.2	474.8
$\frac{3.3}{30}$	$\frac{4.0}{20}$	$\frac{4.1}{10}$	$\frac{4.3}{10}$	$\frac{4.6}{10}$	$\frac{5.1}{20}$	$\frac{6.7}{20}$	$\frac{7.1}{10}$

478.2 ✓  
477.64 ✓  
476.9  
476.9  
477.9  
476.9  
476.6  
475.5  
472.8  
471.9

$\frac{3.75}{30}$  on Walk  
 $\frac{4.23}{22}$  = Wly 3.0 Conc Walk  
 $\frac{5.0}{20}$   
 $\frac{5.0}{10}$   
4.9  
5.0  
5.3  
6.4  
8.6  
10.0

477.59 ✓

$\frac{7.30}{19.7}$  = Wly 1.0 Conc Walk

473.10 ✓

$\frac{8.77}{21.1}$  = Wly 1.0 Conc Walk

481.87



6420 = Approx N.E. of La Mesita Place From East

TP 4.13 485.90 0.10 481.77

640

5488 = 2 6.8-2-Ribbon Drive 2.0 Ribbons ✓

5456 = 2 7.8 Conc Drive 0.7 RI ✓

481.87

4839	4835	4827	4824	4823	4818	4814	4810	4807
$\frac{20}{30}$	$\frac{24}{35}$	$\frac{37}{20}$	$\frac{35}{10}$	$\frac{36}{10}$	$\frac{41}{10}$	$\frac{45}{20}$	$\frac{49}{30}$	$\frac{52}{10}$

485.90

4836	4819	4817	4817	4818	4815	4813	4811	4809
$\frac{17}{30}$	$\frac{10}{35}$	$\frac{02}{20}$	$\frac{02}{10}$	$\frac{01}{10}$	$\frac{01}{10}$	$\frac{06}{20}$	$\frac{08}{30}$	$\frac{10}{10}$

480.73 ✓

480.46 ✓

1.45  
29.5-Fl 2 Ribbons  
- Conc Dr

1.41  
30.0 Conc  
Drive

479.68 ✓

479.25 ✓

2.19  
29.4-Fl 2 Ribbons  
Conc Drive

2.62  
30.0 Conc  
Drive

481.87



Cross Section Harboron Flc  
 S.L. El Cajon to South of Harbort  
 See sketch page 14

Feb 24-42

indexed  
 C.S.R.

1+59 164 Pl of 1/2 Wly Power Pole + Tel.

1+50

1+41

TP 1.10 470.83 12.08 469.73

1+0

0+50

0+0: S.L. El Cajon

0-14: 506 Line of El Cajon

BM 1+46 481.81

480.35 S.W.B.P.  
 El Cajon  
 7000 ft

Notes Red + Plotted on Profile # 2501

3-C-42 C.B.H.

L.F.

1/2

Rt-24

45

466.0 466.6 467.03 468.2 468.48 468.64 468.48 468.9 467.7 467.5  
 2.8 2.5 2.8 2.6 2.25 2.19 2.25 2.1 2.1 2.25  
 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2  
 18 = 20 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft

468.09 J

2.79  
 2.79 = 2.79 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft

470.83

468.1 470.4 470.8 470.16 470.99 471.11 470.82 470.7 472.9 473.0  
 12.7 11.4 11.0 11.5 10.84 10.70 10.99 11.1 8.9 8.8  
 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5  
 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft

473.4 473.2 473.3 472.72 473.51 473.56 473.14 472.9 475.6 475.6  
 8.4 8.6 8.5 9.09 8.30 8.25 8.47 8.9 6.2 6.2  
 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5  
 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft

476.2 476.11 475.47 475.96 475.87 475.62 475.43 476.11 476.6  
 5.5 5.70 6.34 6.05 5.91 6.19 6.35 5.70 5.8  
 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5  
 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft

476.68 476.04 476.06 475.76 475.76 475.74 475.75 475.75 476.37 476.03 476.66  
 5.13 5.77 5.45 6.07 6.05 6.07 6.06 6.06 5.44 5.78 5.15  
 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5 2.5  
 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2 10.2  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft  
 15 = 15 ft

481.81



3+73.25 = FC.

3+50

3+25

2+91.96 BC RT

2+50

2+0

470.83

H

Z

R1

46

458.7	459.1	459.8	460.6	460.41	460.17	460.0	460.1
$\frac{12}{35}$	$\frac{11}{25}$	$\frac{11}{3}$	$\frac{10.87}{10.7}$	$\frac{10.42}{10.1}$	$\frac{10.66}{9.9}$	$\frac{10.8}{15}$	$\frac{10.9}{25}$

459.5	460.4	460.64	460.81	460.75	460.7	460.9
$\frac{11.2}{25}$	$\frac{10.4}{15}$	$\frac{10.19}{10.1}$	$\frac{10.02}{10.1}$	$\frac{10.08}{9.7}$	$\frac{10.1}{15}$	$\frac{9.9}{25}$

461.0	461.1	461.23	461.46	461.35	461.5	461.5
$\frac{9.8}{25}$	$\frac{9.7}{13}$	$\frac{9.50}{10.1}$	$\frac{9.37}{10.1}$	$\frac{9.48}{9.7}$	$\frac{9.3}{15}$	$\frac{9.3}{25}$

459.6	461.1	462.4	462.0	462.33	462.63	462.47	462.4	462.2	461.5
$\frac{11.2}{35}$	$\frac{9.1}{25}$	$\frac{8.1}{18}$	$\frac{8.8}{13}$	$\frac{8.50}{10}$	$\frac{8.20}{10}$	$\frac{8.21}{9.9}$	$\frac{8.1}{15}$	$\frac{8.6}{25}$	$\frac{8.3}{35}$

461.7	462.9	463.6	464.5	464.4	464.27	464.5	461.6	461.7
$\frac{9.6}{20}$	$\frac{7.9}{25}$	$\frac{7.7}{13}$	$\frac{6.8}{9.7}$	$\frac{6.27}{10.1}$	$\frac{6.53}{10.1}$	$\frac{6.32}{15}$	$\frac{9.2}{25}$	$\frac{9.1}{35}$

463.9	464.1	464.2	465.9	466.3	466.57	466.22	466.1	463.7	463.3	463.2
$\frac{6.9}{10}$	$\frac{6.7}{25}$	$\frac{6.6}{20}$	$\frac{4.9}{15}$	$\frac{4.6}{9.9}$	$\frac{4.26}{10.1}$	$\frac{4.1}{10.1}$	$\frac{4.7}{15}$	$\frac{2.1}{20}$	$\frac{2.5}{25}$	$\frac{2.6}{40}$

470.83



540

4775

4748.37 = B.C.H

4719 = 1/2 Conc Wall o'ht. ✓

TP 4.40 46380 11.43 459.40

4702 = 1/2 Garage + Conc Drive o'ht. ✓

470

470.83

456.3 25 25	456.4 24 25	456.9 69 15	457.43 637 10.5 = WHP	457.67 613	457.41 639 9.5 = WHP	457.9 59 15	459.0 18 25
-------------------	-------------------	-------------------	-----------------------------	---------------	----------------------------	-------------------	-------------------

456.4 24 25	456.6 22 25	457.3 65 15	457.93 587 10.6 = WHP	458.8 562	457.97 583 9.5 = WHP	458.9 57 15	459.1 14 25
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457.0 60 25	457.2 56 25	457.8 60 15	458.44 536 10.5 = WHP	458.75 505	458.50 530 9.6 WHP	458.8 50 15	459.8 40 20	459.9 30 25
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457.70 ✓  
510  
39.6  
3.92 = WHP  
3.15 = Conc Wall

457.73 ✓  
607  
39.7  
3.92 = WHP  
3.15 = Conc Wall

457.71 ✓  
1312  
410 = WHP  
Conc Floor

458.50 ✓  
1233  
36.3 = WHP  
3.15 = Conc Drive

458.5 123 25	459.2 116 15	459.54 1129 105	459.81 1102	459.40 1142 10 = WHP	457.7 111 15	460.1 107 25	460.5 103 25
--------------------	--------------------	-----------------------	----------------	----------------------------	--------------------	--------------------	--------------------

470.83



For Check

10+21.8 on Amberd

2.94

5+4890 = E.C.

5+28

= 2 78 Core Drive on Lt

5+08

= 1/2 3' Core Walk on Lt

463.80

455.1	455.3	456.2	456.63	456.68	456.38	456.4	457.8
8.3	8.5	7.6	7.6	7.12	7.22	7.4	6.8
			7.6 = FH P.		7.2 = WH P.		

455.87	456.01	456.5	456.98	457.09	456.86	457.3	458.3
7.9	7.7	7.3	6.8	6.71	6.9	6.5	5.5
7.5 = WH P.	7.5 = WH P.	7.3 = WH P.	6.8 = FH P.		6.9 = WH P.		

456.201	456.51
7.5	7.2
5.5 = WH P.	2.1 = WH P.
	463.80



Cross Section 72nd St.  
S.W. El Cajon to South 4 of Embury St.  
See Sketch Page 12

Indexed  
C.S.K.

Lt = L

Rt = H

49

1+58 312 Rt of L = W/W Power & Tel Pole ✓  
1+50  
1+38 298 Lt of L = S/W Wire & Lat 4 Fence ✓  
1+0  
0+86 = 2 Garage on Rt ✓  
0+68 291 Rt of L = S/W Wire Fence ✓  
301 Lt of L = W/W Wire Fence ✓  
0+51 340 Lt of L = S/W Cor. Bldg ✓  
0+50  
0+15 227 Lt of L = R/W Tel Pole ✓  
0+14 337 Lt of L = W/W Cor. Bldg ✓  
0+01 227 Rt of L = W/W Power Pole ✓ 301 Rt of L = W/W Wire Fence ✓  
0+0 = South 4 line of El Cajon  
0-14 = South 4 Curb Line of El Cajon  
BM 300 483.46 480.46

Redy Plot Profile # 2502  
3-5-42 C.B.M.

295  
55-6

S.W. RP  
El Cajon  
72nd St

476.5 7.2 30	476.6 6.9 30	477.1 6.9 30	477.2 6.0 30	477.5 6.0 30	477.5 5.5 30	478.0 5.2 30	478.3
478.0 5.5 30	478.0 5.5 30	477.7 5.8 30	478.3 5.2 30	478.4 5.1 30	479.3 4.2 30	479.7 3.8 30	
						480.5 ✓ 3.0 53.0 = Garage Dirt Floor	
479.1 4.4 30	478.7 4.8 30	478.4 5.1 30	478.7 4.8 30	478.7 4.8 30	479.3 4.2 30	480.1 3.4 30	
479.6 3.9 30	479.0 3.6 30	479.4 4.2 30	479.5 3.8 30	479.5 3.6 30	479.5 3.6 30	479.7 3.7 30	480.2 3.7 30
479.8 3.6 30							480.3 3.0 30
478.83 4.6 30	479.77 3.9 30	479.12 4.2 30	479.31 4.5 30	479.55 3.9 30	479.68 3.7 30	479.77 3.6 30	479.79 3.6 30
							479.83 3.6 30
							480.45 3.0 30
							480.5 3.0 30
							480.74 3.0 30
							480.46















Cross Section 71st St.  
 El Cajon to Amber St.  
 See Sketch Page 13

Indexed  
 C.S.R.

Feb. 25-42

Lt = E

2

Pr. 21

53

1+10 =  $\frac{1}{2}$  Dr. Garage on Pt

1+0

0+82 30.7' Pt of  $\frac{1}{2}$  = W/4 12" Pipe Tree ✓

TP 4.45 475.23 6.06 470.78

0+72 31.5' Pt of  $\frac{1}{2}$  = W/4 12" Pipe Tree ✓

0+50

0+25

0+02 228' Pt of  $\frac{1}{2}$  = W/4 Power Pole ✓

0+0 = S.L. El Cajon

0-14 = South Carb Line El Cajon

BM 579 476.84

473.05

S.W. B.P.  
 El Cajon + 71st

Notes Reduced & Plotted on profile # 2563  
 3-5-42 C.B.H.





BM

7.53

467.70

072 Hub  
Hamberst  
7.53  
467.64

3+10 = 11.6

2+70

2+35

2+0

1+70

21.2 Lt of L = 2 Fire Hyd

1+61

22.9 Rt of L = 4 1/2 Porter Pole

1+50

47523

4685

6.7  
30

4685

6.7  
20

4684

6.8  
10

4683

6.9

4683

6.9  
8

4677

7.5  
18

4684

6.8  
20

4685

6.7  
30

4705

6.7  
30

4700

5.2  
20

4696

5.8

4691

5.1  
10

4691

6.1

4694

6.8  
8

4689

6.0  
12

4700

5.2  
20

4702

5.0  
30

4702

5.0  
30

Flow  
Station

4724

7.8  
30

4720

5.2  
20

4717

6.5  
10

4714

6.8

4697

5.5  
15

4698

5.7

4707

5.0  
8

4700

5.2  
12

4714

5.8  
20

4709

5.0  
30

4708

5.1  
10

4728

7.2  
30

4722

5.0  
20

4720

6.2  
20

4702

5.0

4702

5.0

4703

4.9  
18

4702

5.0  
18

4711

4.1  
20

4708

5.0  
30

4708

4.4  
10

4723

5.0  
30

4718

5.1  
10

4712

4.0  
10

4707

6.5  
15

4706

4.6

4705

4.7  
10

4703

4.9  
18

4705

4.7  
20

4699

5.0  
30

4697

5.5  
10

47523



Cross Section 71st St.  
Amherst St South

Indexed  
c.s.K.

1+90 = 251 ft of  $\frac{1}{2}$  = NY Pictet Fence

1+29 =  $\frac{1}{2}$  2.6 Brick Walk on Rt

1+10 =  $\frac{1}{2}$  7.8 Conc Drive on Rt

1+0 = 20.4 ft of  $\frac{1}{2}$  = NY Power Pole

0+50

0+10 =  $\frac{1}{2}$  2.5 Conc Walk on Rt

0+0 = S.L. Amherst

B.V. 6.46 174.10

467.64  $\frac{1}{2}$  Hub  
Amherst  
Street North

Lt: E

$\frac{1}{2}$

Rt: W

55

469.91 ✓

469.74 ✓

4.19  
25 = 51.2  
Brick Walk

4.35  
35 = 51.2  
on Walk

469.68

469.53

4.45  
15 = 51.2  
Conc Dr.

4.57  
35 = 51.2  
on Dr.

470.1

469.9

469.6

469.9

469.5

469.5

469.0

1.10  
25

1.2  
15

1.5  
12 = 51.2  
on Dr.

1.2

1.5  
15 = 51.2  
on Dr.

1.6  
25

1.5  
35

469.5

469.4

469.1

469.2

468.7

468.8

468.5

468.2

1.6  
25

1.7  
15

1.5  
12 = 51.2  
on Dr.

1.9

1.4  
14 = 51.2  
on Dr.

1.5  
15

1.6  
25

1.5  
35

468.25 ✓

468.11 ✓

5.85  
25 = 51.2  
Conc Walk

5.99  
35 = 51.2  
on Walk

468.9

468.4

467.6

467.8

467.2

467.5

467.7

5.2  
25

5.9  
15

6.5  
12 = 51.2  
on Dr.

6.3

6.9  
13 = 51.2  
on Dr.

6.6  
15

6.4  
25

474.10



1+98 = 1/2 1.5 Brick Walk on Rt ✓

1+84 = 1/2 6.6-2 Ribbons Conc Dr. Ribbons 2.0 ✓

1+80 = 25.6 1/2 of 1/2 = 5 1/2 Picket Fence ✓

1+63 = 1/2 3 Conc Walk on Lt ✓

1+60 = 1/2 6.6 Conc Drive on Rt ✓

1+50

1+48 = 1/2 1.5 B ✓

474.10

469.87 ✓

469.63 ✓

4.23  
2.50 = Fill  
Brick Walk

4.47  
3.50 = Walk

471.55 ✓

471.29 ✓

2.55  
2.35 = Conc Drive

2.81  
2.24 = 1/2 1/2 Ribbons  
Conc Drive

471.52 ✓

471.43 ✓

2.56  
2.35 = Conc Walk

2.67  
2.18 = 1/2 Conc  
Walk

470.00 ✓

469.80 ✓

4.10  
2.50 = Fill  
Conc Dr.

4.30  
3.50 = Walk

471.2

470.7

470.3

470.4

470.0

470.1

470.1

469.6

2.9  
2.5

3.4  
1.5

3.8  
3.2 = Fill  
Box

3.7

4.5  
4.0 = 1/2 1/2

4.9

4.0  
3.5

4.5  
3.5

470.12

469.80

3.98  
2.50 = Fill  
1/2 Conc Walk

4.30  
3.50 = Walk

474.10



71st St.

240

2468 = 2 3' Conc Walk on Lt ✓

2450 = 1 1/4 3.5 Conc Walk on Rt ✓

2446 = 2 6.5 2 Ribbed Conc Dr. Ribbed 15' ✓

240 220 Rto/L = 1/2 Wly Parer-Pole

Lt.

Rt.

Rt.

57

472.4

472.1

471.8

472.1

471.8

471.95 ✓

472.00 ✓

1.7  
2.5

2.0  
1.5

2.0  
1.1-1.0  
1.0

2.0

2.2  
1.5-1.0  
1.0

2.15  
2.2-1.0  
1.0

2.10  
2.55-1.0  
1.0

471.83 ✓

471.73 ✓

2.27  
3.00  
1.0

2.37  
2.53-1.0  
1.0

471.7

471.3

471.0

471.3

470.9

470.94 ✓

470.5

2.4  
2.5

2.8  
1.5

3.1  
1.2-1.0  
1.0

2.8

2.2  
1.5-1.0  
1.0

3.16  
2.3-1.0  
1.0

3.6  
3.5

471.98 ✓

471.74 ✓

2.12  
3.50  
1.0

2.36  
2.53-1.0  
1.0

471.2

470.7

470.5

470.7

470.3

470.5

470.0

469.7

2.9  
2.5

3.1  
1.5

3.6  
1.5-1.0  
1.0

3.4

3.8  
1.5-1.0  
1.0

3.6  
1.8

4.1  
3.5

4.1  
3.5







2+10 = H.L. Amberst

2+07 22.6 Pt of Z = H.L. Porro's Tot. Pole ↓

2+65

2+30

2+17 21.0 Pt of Z = S.A.F. 15 Hedge ↓

2+0

466.54

459.4 459.4 459.7 459.4 459.4 458.8 458.4 458.8 458.7

7/30 7/30 6/8 7/1 7/1 7/7 8/1 7/7 7/8  
10-5/10 10-5/10 10-5/10 10-5/10 10-5/10 10-5/10 10-5/10 10-5/10

459.9 459.9 459.8 459.9 460.3 460.1 459.3 460.2 460.0 460.0

6/6 6/6 6/7 6/6 6/2 6/4 7/3 6/3 6/5 6/5  
10-5/10 10-5/10 10-5/10 10-5/10 10-5/10 10-5/10 10-5/10 10-5/10 10-5/10

460.7 461.3 461.4 460.3 461.0 461.2 461.9 459.1 461.0 461.0 461.1

5/8 5/8 5/1 6/2 5/5 5/3 5/5 6/4 5/5 5/5 5/4  
10-5/10 10-5/10 10-5/10 10-5/10 10-5/10 10-5/10 10-5/10 10-5/10 10-5/10 10-5/10

462.1 461.9 461.3 460.9 461.7 462.0 461.7 466.8 461.2 461.5 461.4

4/4 4/6 5/2 5/6 4/8 4/5 4/8 5/7 5/3 5/3 5/1  
10-5/10 10-5/10 10-5/10 10-5/10 10-5/10 10-5/10 10-5/10 10-5/10 10-5/10 10-5/10 10-5/10

466.54



F1 Capco Blvd. Bench Levels  
69th St to 73rd St.

Feb-20-92

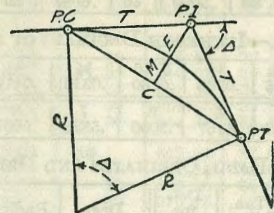
S. 1107  
795th St  
795th St

B.M.	7.83	464.58		456.75	S. 1107 795th St
B.M.	9.70	473.96	0.32	467.26	S. 1107 795th St
B.M.	12.02	485.07	0.91	473.05	S. 1107 795th St
B.M.	2.05	483.51	4.61	480.46	S. 1107 795th St
B.M.			2.16	480.35	S. 1107 795th St

Put in Bench Books 3-2-92  
C.S.R.

## DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



### CURVE FORMULAS

Radius= $R = \frac{50}{\sin \frac{D}{2}}$  (1) Degree of Curve= $D$  and  $\sin \frac{D}{2} = \frac{50}{R}$  (2)

Tangent= $T = R \tan \frac{\Delta}{2}$  (3) Length of Curve= $L = 100 \frac{\Delta}{D}$  (4)

Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2})$  (5)  $= R \text{vers} \frac{\Delta}{2}$  (6)

External= $E = T \tan \frac{\Delta}{4}$  (7)  $= R \div \cos \frac{\Delta}{2} - R$  (8)  $= R \text{exsec} \frac{\Delta}{2}$  (9)

Long Chord= $C = 2 R \sin \frac{\Delta}{2}$  (10)  $\Delta =$  Central Angle

### EXPLANATION AND USE OF TABLES

**Stations.**—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T.  $\Delta = 62^\circ 10'$   $D = 8^\circ 20'$ . From Table IV for  $1^\circ$  curve  $T = 3454.1$  and  $+8\frac{1}{3} = 414.49$  ft. From Table V correction  $= .36$  or  $T = 414.85$  ft. P. C.—Sta. P. I.— $T = 157 + 45.50$ . Also from (4)  $L = 746.00$  and P. T.—Sta. P. C. +  $L = 164 + 91.50$ .

**Offsets.**—Tangent offsets vary (approximately) directly with  $D$  and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.  $= 7.27$  ft. Distance  $= 158 - \text{Sta. P. C.} = 54.50$ , hence offset  $= 7.27 (54.50 \div 100)^2 = 2.16$  ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus  $(54.50)^2 \div (2 \times 688.26) = 2.16$  ft.

**Deflections.**—Deflection angle  $= \frac{1}{2} D$  for 100 ft.,  $\frac{1}{4} D$  for 50 ft., etc. For  $c$  ft.  $= (\text{in minutes}) .3 \times C \times D^\circ$  or  $= \text{defl. for 1 ft. from Table III} \times C$ . For Sta. 158 of above curve  $= .3 \times 54.5 \times 8\frac{1}{3} = 136.2'$  or  $2^\circ 16.2'$ , or  $= 2.50 \times 54.5 = 136.2'$  from Table III. For Sta. 159 deflection angle  $= 2^\circ 16.2' + 8^\circ 20' + 2 = 6^\circ 26.2'$ , etc.

**Externals.**—May be found in similar manner to tangents. Thus  $E$  for curve above is 91.37. For from Table IV for  $1^\circ$  curve  $E = 960.6$  for  $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 91.27$  and from Table V correction  $= .10$  or  $E = 91.37$  ft. Or suppose  $\Delta = 32^\circ$  and  $E$  is measured and found to be 42 ft. What is  $D$ ? From Table IV  $E = 230.9$  and  $+42 = 5.5$  or  $D = 5^\circ 30'$ .



13 30 67  
590.27  
74036  
6-



RRSP P.P. #371R

Elev 2.69 city Datum

2.69	272	269
3.92	372	
2.61	264	272
4.47	447	
2.14	117	

BM #31 227 L.P. N End - 445 + 79.5

Elev 2.27

451.01.

BM #34 3/4" I.P. 55 Lt + 466 + 45 Elev 1.89

15+00 S.E.S. Way

+62.8

+78.0 - Forting

10+36 N.E. Footing

6+51.2 S. End St. Way

16+68 97 N.E. St Way

100+97.10

162 + 51.00

162 = 16.8

Equation  
of Cov.

100 x R.2

R.L

DISTANCES FROM CENTER OF ROADWAY FOR  
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) \* 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

MADE IN U.S.A.