1629

HETZ

TRAVERSE TABLE FOR TRANSIT BOOK.

From 1 to 100 for a distance of 100.

Degrees	DEGREES.		¼ DEGREE.		⅓ DEGREE.		½ DEGREE.		Degrees
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100 00	0 44	100.00	0 87	99.99	1.31	90
1	99.98	1 75	99 98	2 18	99 97	2.62	99 95	3.05	89
2	99.94	3.49	99 93	3.93	99 91	4 36	99.88	4.80	88
3	99.86	5.23	99 84	5 67	99 81	6.10	99.79	6.54	87
4	99 76	6.98	99 73	7.41	99.69	7.85	99.66	8.28	86
5	99 62	8.72	99.58	9.15	99 54	9.58	99.50	10 02	85
6	99.45	10.46	99.41	10 89	99.36	11.33	99.31	11.75	84
7	99 25	12.19	99 20	12.62	99.14	13.05	99.00	13.49	83
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16 50	98 56	16.93	80
10	98 48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98 16	19.08	98 08	19 51	97.99	19 94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21 64	97.53	22.07	77
13	97.44	22.50	97.34	22.93	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.93	24 62	96.81	25 04	96 70	25.46	75
15	96.59	25 88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27 98	95.88	28 40	95 76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30 07	95.24	30.49	72
18	95.11	30 90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35 43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38 67	67
23	92.06	39.07	91.88	39 47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89 69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87 67	48.10	61
29	87.46	48.48	87.25	48 86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	53 00	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.48	83.63	54.85	83.39	55.19	83.15	55.56	56
34	82.90	55.93	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60 53	79.34	60.88	79.07	61 22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.19	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.06	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.69	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							
Degrees	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees
	DEGREES.		¼ DEGREE.		⅓ DEGREE.		½ DEGREE.		

Published by the A. Lietz Co., San Francisco, Cal.

MADE IN U. S. A.

Quality Evidenced Since 1882.

Standard Tripod Connection

LIETZ STANDARD ENGINEERS' TRANSIT

With U Shaped Standards

No. 5E with 6¼″ limb. No. 11E with 5″ limb.

Furnished with either Internal or External Focusing Telescope.

Table of Stadia Reductions.—Continued.

Min	8°	9°	10°	11°	Min.	12°	13°	14°	15°

Table of Stadia Reductions.—Continued.

Min.	24° Hor. Dist.	24° Diff. Elev.	25° Hor. Dist.	25° Diff Elev.	26° Hor. Dirt.	26° Diff. Elev.	27° Hor. Dist.	27° Diff.. Elev.
0′	83.46	37.16	82.14	38.30	80.78	39.40	79.39	40.45
2	83.41	37.20	82.09	38.34	80 74	39.44	79.34	40.49
4	83.37	37.23	82.05	38.38	80.69	39.47	79.30	40.52
6	83.33	37.27	82.01	38.41	80.65	39.51	79.25	40.55
8	83.28	37.31	81.96	38 45	80 60	39.54	79.20	40.59
10	83.24	37.35	81.92	38.49	80 55	39.58	79.15	40.62
12	83.20	37.39	81.87	38.53	80.51	39.61	79.11	40.66
14	83.15	37.43	81.83	38.56	80.46	39.65	79.06	40.69
16	83.11	37.47	81.78	38.60	80.41	39.69	79.01	40.72
18	83.07	37.51	81.74	38.64	80.37	39.72	78.96	40.76
20	83.02	37.54	81.69	38.67	80.32	39.76	78 92	40.79
22	82.98	37.58	81.65	38.71	80.28	39.79	78.87	40.82
24	82.93	37.62	81.60	38.75	80.23	39.83	78.82	40.86
26	82.89	37.66	81.56	38.78	80.18	39.86	78.77	40.89
28	82.85	37.70	81.51	38.82	80.14	39.90	78.73	40.92
30	82.80	37 74	81.47	38 86	80.09	39.93	78.68	40.96
32	82.76	37.77	81.42	38.89	80 04	39.97	78.63	40.99
34	82.72	37.81	81.38	38.93	80.00	40.00	78.58	41.02
36	82.67	37.85	81 33	38.97	79.95	40.04	78.54	41 06
38	82.63	37.89	81 28	39.00	79.90	40.07	78.49	41.09
40	82.58	37.93	81 24	39 04	79.86	40.11	78 44	41.12
42	82.54	37.96	81.19	39 08	79 81	40.14	78.39	41.16
44	82.49	38.00	81.15	39 11	79.76	40.18	78.34	41.19
46	82 45	38.04	81.10	39.15	79 72	40.21	78.30	41.22
48	82 41	38 08	81 06	39.18	79.67	40.24	78.25	41.26
50	82.36	38.11	81.01	39.22	79.62	40.28	78 20	41.29
52	82.32	38.15	80 97	39.26	79.58	40.31	78 15	41.32
54	82.27	38.19	80.92	39.29	79.53	40 35	78.10	41.35
56	82.23	38.23	80.87	39.33	79.48	40.38	78 06	41.39
58	82.18	38.26	80.83	39.36	79.44	40.42	78.01	41.42
60	82 14	38.30	80.78	39.40	79 39	40.45	77 96	41 45
c= 75	68	31	.68	32	67	.33	.66	.35
c=1.15	1.05	48	1.04	50	1.03	.51	1 02	.53
c=1 90	1.73	79	1.72	82	1.70	85	1 69	.88

Min.	28° Hor. Dist	28° Diff. Elev.	29° Hor. Dist	29° Diff Elev.	30° Hor. Dist.	30° Diff. Elev.
0′	77 96	41 45	76.50	42 40	75.00	43 30
2	77.91	41.48	76.45	42.43	74.95	43.33
4	77.86	41 52	76.40	42.46	74.90	43.36
6	77.81	41.55	76 35	42.49	74.85	43 39
8	77.77	41 58	76.30	42.53	74 80	43.42
10	77.72	41.61	76.25	42.56	74.75	43.45
12	77.67	41.65	76.20	42.59	74.70	43.47
14	77.62	41.68	76.15	42.62	74.65	43.50
16	77.57	41.71	76.10	42.65	74.60	43 53
18	77.52	41.74	76.05	42 68	74.55	43 56
20	77.48	41.77	76.00	42.71	74.49	43.59
22	77.42	41.81	75.95	42 74	74.44	43 62
24	77.38	41.84	75.90	42.77	74.39	43 65
26	77.33	41.87	75.85	42.80	74.34	43.67
28	77.28	41.90	75.80	42.83	74.29	43 70
30	77.23	41.93	75.75	42.86	74.24	43 73
32	77.18	41 97	75.70	42.89	74.19	43.76
34	77.13	42 00	75.65	42.92	74.14	43 79
36	77.09	42.03	75.60	42.95	74.09	43.82
38	77.04	42.06	75.55	42 98	74.04	43 84
40	76.99	42.09	75.50	43.01	73.99	43.87
42	76.94	42.12	75 45	43 04	73.93	43 90
44	76.89	42.15	75.40	43 07	73 88	43.93
46	76.84	42.19	75.35	43.10	73 83	43 95
48	76.79	42 22	75.30	43.13	73.78	43.98
50	76.74	42.25	75 25	43.16	73.73	44 01
52	76.69	42.28	75 20	43.18	73.68	44.04
54	76.64	42.31	75.15	43.21	73.33	44 07
56	76.59	42.34	75.10	43.24	73.58	44.09
58	76.55	42.37	75.05	43 27	73.52	44.12
60	76.50	42.40	75.00	43 30	73.47	44.15
c= .75	.66	.36	.65	.37	.65	38
c=1.15	1 01	55	1.00	.57	0.99	.58
c=1.90	1.67	91	1.65	.94	1 64	.95

Published by the A. Lietz Co, San Francisco, Cal.

1629

CITY ENGINEER

Bench Levels Mission Valley
Trunk Sewer
For Final line See 2040

Also F.B 1631
1703
1873
2003
2054

Bench Levels Mission Valley Trunk Sewer #3

BM #1A	5.89	6.45 ✓		0.56
T.P.	5.92	8.67 ✓	3.70	2.75 ✓
T.P.	3.42	6.27 ✓	5.82	2.85 ✓
Set BM #1B (See Profile Levels)	2.63	5.86 ✓	3.04	3.23 ✓
Check BM #2	3.29	6.79 ✓	2.36	3.50 ✓
T.P.	5.28	7.57 ✓	4.50	2.29 ✓
Check BM #3	2.74	8.47 ✓	1.84	5.73 ✓
T.P.	5.39	9.42 ✓	4.44	4.03 ✓
Set BM #4	0.37	7.20 ✓	2.59	6.83 ✓
T.P.	3.28	7.31 ✓	3.17	4.03 ✓
T.P.	3.86	9.72 ✓	1.45	5.86 ✓
			5.09	4.63 ✓
Set B.M. #5	7.39	14.28 ✓	2.83	6.89 ✓
T.P.	4.54 ~~8.81~~	8.81 ✓	10.01	4.27 ✓
Set BM #6	5.09	11.01 ✓	2.89	5.92 ✓

B.P. in Cb. S.W. Rosecrans + Midway or Causeway

40 penny Spike in Gas Lt Pole # 3001 S.W. Kurtz + Rosecrans

See Profile Levels
R.R. spike in Gas + Lt Pole #3155. F.B. 1526-P
20' Lt. of 5+70

Mon. & Hancock + Riley

N.E. Top Fire Hy. Riley + Moore

40 penny Spike in Gas + Lt Pole # P 3201. S.W. Congress + Riley

40' S. of S. Diego Ave.
R.H. Nail in Pole carrying both Phone + Power on W. side. Pole # 75761 H
G+LT # J.P. 3988

Mon. & Juan St. to East

S.W. Juan St. to East
40 penny Spike in Gas + Lt Pole # 4033. 20' Lt 30+00

R.R. Spike in Gas + Lt Pole # P 4230 S.W. Riley + Whitman

Station	+S	H.I.	−S	Elev.	Description
		⊼ 11.01			
T.P.	4.60	11.44	4.17	6.84	R.H. Nail in G+Lt Pole # P3049
Set BM #7	2.37	11.38	2.43	9.01	S.W. Top Fire Hydrant Whitman + Taylor
T.P.	8.31	16.07	3.62	7.76	
T.P.	8.16	22.79	1.44	14.63	
Check BM #8	2.58	22.58	2.79	20.00	S.W.B.P. Old Town Bridge South End * Note See Levels Run to verify Elev of This BM P.79
T.P.	4.94	20.12	7.40	15.18	
T.P.	7.11	21.06	6.17	13.95	
Check BM #9	6.69	20.42	7.33	13.73	Top city Mon 90' Rt ± 66+00 in Park.
Check BM #10	10.37	21.09	9.70	10.72	Top 1" pipe 10' Lt 72+26 ²⁶
T.P.	4.98	21.16	4.91	16.18	
Check BM #11	6.10	16.40	10.86	10.30	Conc Mon ℄ Harney St. N.E.ly line of Old S.D.
Set B.M. #12	4.93	19.37	1.96	14.44	40 penny Spike Top Eucalyptus Stump 12' Lt 84+06 +−
T.P.	9.23	27.24	1.36	18.01	

		T 27.24		
T.P.	9.26	34.73	1.77	25.47
Check BM #13	10.43	43.94	1.22	33.51
T.P.	5.46	44.96	4.44	39.50
Check BM #14	3.31	42.95	5.32	39.64
T.P.	5.17	40.61	7.51	35.44
Set BM #15	3.84	32.30	12.15	28.46
T.P.	2.64	25.74	9.20	23.10
Check BM #16	6.96	21.28	11.42	14.32
Check BM #17	8.42	18.56	11.14	10.14
T.P.	5.40	19.11	4.85	13.71
Check BM #18	11.83	25.79	5.15	13.96
T.P.	5.90	26.60	5.09	20.70
Set BM #19	8.97	26.47	9.10	17.50

Bench Mon. 20' Lt 92+50 +- 4' S. of North Line of Hiway R.O.W. 20' West of Entrance to Bernards Nursery

Top 1" pipe 16' Lt of East of Bernards Nursery

R.R. Spike in Eucalyptus Tree 65' Lt +- 104+20

L.P. in city Mon. 10' Lt 108+03.88

2" Pipe 10' Lt. B.C. 113+58.16

2" pipe 10' Lt. E.C. 118+76.21

Set BM. 86' Rt 125+70 Gas Lt. Pole #79050 40 penny Spike

		26.47			
Check BM #20	3.83	20.33	9.97	16.50	2" pipe on R.O.W. 10' Lt 130+78 +- 73+39 Minor Sta.
T.P.	9.55	26.11	3.77	16.56	
Set BM #21	6.12	27.35	4.88	21.23	40 penny spike in G.+Lte Pole #79056 80+- Rt of 140+10
Check BM #22	8.18	27.71	7.82	19.53	2" pipe 10' Lt 147+06.02 to R.O.W. Camino Del Rio = 6+66.89 Minor
T.P.	5.12	30.00	2.83	24.88	
Check BM #23	8.12	29.07	9.05	20.95	R.O.W. Mon 90' Rt 151+76.56 = 94+57.09 Camino Del Rio.
T.P.	6.78	31.40	4.45	24.62	
Check BM #24	7.09	31.77	6.72	24.68	C.P. TK L.P. Top Headwall N End Triple Box culvert W Line 6.15 15' Rt 157+85 +-
T.P.	4.41	31.31	4.87	26.90	
Set BM #25	9.15	31.62	8.84	22.47	R.O.W. Mon 90' Rt 164+49 on L.C. produced South.
Check BM #26	6.72	32.68	5.66	25.96	L.P. Cap Tab. Top Headwall 60+- Rt 171+03.95
T.P.	5.23	32.77	5.14	27.54	
Set BM #27	7.70	34.13	6.34	26.43	40 penny spike Gas + Lt Transformer Pole #79080 85' Rt 179+85

	+	H.I. 34.13	-	Elev.	
Check BM #28	6.37	34.17	6.33	27.80	40 penny Spike 6' Lt. Pole # 79083 35' Lt. +- 189+28
TP.	0.98	31.31	3.84	30.33	
Check BM #29	8.54	35.91	3.94	27.37	2" pipe 10' Lt. 190+25. 44
T.P.	4.11	36.21	3.81	32.10	
Check BM #30	7.47	37.93	5.75	30.46	BP. Top culvert Headwall 60' Rt +- 197+70
TP	5.18	37.71	5.40	32.53	
Check BM #31	5.95	37.81	5.85	31.86	40 penny Spike in Tel-phone pole # 87891 H 15' Rt 204+03
TP.	6.40	38.87	5.34	32.47	
Check BM #32	6.97	40.73	5.11	33.76	3 Nails in Gas Lt. Pole #79127 80' Rt 212+70
TP.	4.33	40.24	4.82	35.91	
Check BM #33	10.87	41.85	9.26	30.98	Top 2" pipe 10' Lt. 218+50. 51 B.C.
T.P.	5.46	43.36	4.15	37.70	
Check BM #34	8.83	42.21	9.98	33.38	Top 2" pipe 10' Lt 223+07. 93

		42.21		
T.P.	5.91	43.42	4.70	37.51
Set BM #35	8.42	47.39	4.45	38.97
T.P.	7.38	52.71	2.06	45.33
Check BM #36			5.11	47.60
Check BM #37	7.49	50.51	9.69	43.02
Check BM #38	8.29	45.82	12.98	37.53
T.P.	11.32	50.10	7.04	38.78
Check BM #39	11.53	50.10	11.53	38.57
Set BM #40	5.95	54.65	1.40	48.70
T.P.	5.12	52.71	7.06	47.59
Check BM #41	12.88	57.03	8.56	44.15
" BM #42	2.22	56.89	2.36	54.67
T.P. L	6.28	51.87	11.30	45.59

40 Penny Spike S. Side G. Lt Pole # P79136 60' Rt 230+40+ -

Spike in Trunk Cypress Tree S East Texas & Camino Del Rio

cp. Tab Tie out for P.I. Curve on Dbl box culvert 11' Lt 237+81

2" pipe 10' Lt 241+99.91

2" pipe 10' Lt 245+93.83 Hiway EC Sewer ℄ Sta.

40 penny Spike G&Lt Pole # 79147 85' Rt 248+50+ -

2" pipe on N Line of R.O.W. 10' Lt 257+88.72 Sewer Sta

R.P. Hub 35' Lt 202+21.32 Hiway Sta

		⊼ 51.87	169 L	
Set BM #43	4.18	50.39	5.66	46.21
T.P.	6.25	48.94	7.70	42.69
T.P. L263+14.89	0.42	46.06	3.30	45.64
Set B.M. #44	3.92	47.11	2.87	43.19
TP	5.43	50.52	2.02	45.09
T.P. on L	7.20	55.94	1.78	48.74
Set BM #45	2.85	57.23	1.56	54.38
T.P.	1.45	54.11	4.57	52.66
Set BM #46	2.63	54.66	2.08	52.03
T.P.	4.53	53.69	5.50	49.16
T.P. on L 296+92.29	4.57	55.95	2.31	51.38
Set B.M. #47	2.78	53.68	5.05	50.90
TP	4.26	56.34	1.60	52.08

46.06 47 10.3 7

B.P. in Culvert spillway wall 20'+- Rt 263+40+-

Bolt in Top of P. Ricards Well 10' Rt 273+70+- W. Bolt Directly over Ricards Name on Well
water

B.P. in Culvert Spillway wall 250' East of L on Production back tank

Top 90° Bend set on 2½" Galvanized pipe 8'+- Lt 289+32

40 penny spike in G+Lt Pole # 175889 35' Lt 301+00

		56.34 ✓			
T.P.	12.71	65.18 ✓	3.87	52.47 ✓	
T.P	11.59	70.00 ✓	6.77	58.41 ✓	
Set BM #48	1.47	70.58 ✓	0.89	69.11 ✓	40 penny Spike Telephone pole #939303 45'Rt 312+10
T.P	6.69	65.31 ✓	11.96	58.62 ✓	
T.P	3.62	61.48 ✓	7.45	57.86 ✓	
T.P 316+12 39L	5.92	61.88 ✓	5.52	55.96 ✓	
T.P	3.20	62.86 ✓	2.22	59.66 ✓	
Set BM #49	4.90	65.30 ✓	2.46	60.40 ✓	40 penny Spike G.Lt Pole # 79198 20'Lt 322+75
T.P.	4.04	65.35 ✓	3.99	61.31 ✓	
Set BM #50	0.36	64.24 ✓	1.47	63.88 ✓	40 penny Spike Tel pole # 'D' 35147T 45'Lt 329+30T
T.P	5.72	65.17 ✓	4.79	59.45 ✓	
Set BM #51	9.93	73.08 ✓	2.02	63.15 ✓	40 penny Spike G.Lt pole # 79680 15'Lt 334+75 +-
T.P.	6.12	77.67 ✓	1.53	71.55 ✓	

8		77.67 ✓		
Set BM #52	2.89	78.91 ✓	1.65	76.02 ✓
TP	3.83	76.57 ✓	6.17	72.74 ✓
Set BM #53	4.90	80.34 ✓	1.13	75.44 ✓
TP	6.34	84.12 ✓	2.56	77.78 ✓
Set BM #54	3.70	87.67 ✓	0.15	83.97 ✓
TP	8.60	95.40 ✓	0.87	86.80 ✓
Set BM #55	2.46	96.36 ✓	1.50	93.90 ✓
TP	7.86	95.88 ✓	8.34	88.02 ✓
Set BM #56	0.86	90.90 ✓	5.84	90.04 ✓
TP	1.57	81.58 ✓	10.89	80.01 ✓
Set BM #57	4.96	78.24 ✓	8.30	73.28 ✓
Set BM #58	2.90	80.76 ✓	0.38	77.86 ✓
TP	2.78	79.58 ✓	3.96	76.80 ✓

in Daley's Backyard
40 penny spike G & Elec pole Private Pole 27' Rt 338+78

40 penny Spike G & Lt Pole # 79761 45' Rt 344+95

40 penny Spike G & Lt Pole # 79763 45' Rt 351+70 ✓

40 penny Spike G & Lt pole # 79765 45' Rt 358+00

Con Mon 12' Lt 361+96.22

Sq cut West End South Head wall Culvert under Camino Del Rio

40 penny Spike G & Lt pole # 79875 45' Rt 370+00

		T 79.58 ✓		
			4.41	75.17 ✓
Set BM #59	5.24	76.34 ✓	8.48	71.10 ✓
T.P.	6.04	81.54 ✓	0.84	75.50 ✓
Set B.M. #60	0.62	81.24 ✓	0.92	80.62 ✓
T.P. on L. Sta	11.74	89.94 ✓	3.04	78.20 ✓
TP	7.47	90.87 ✓	6.54	83.40 ✓
Set BM #61	3.~~30~~ 29	90.97 ✓	3.13	87.68 ✓
T.P.	5.22	93.60 ✓	2.59	88.38 ✓
T.P.	4.31	96.23 ✓	1.68	91.92 ✓
Set BM #62	0.07	94.57 ✓	1.73	94.50 ✓
TP	0.30	83.75 ✓	11.12	83.45 ✓
Set BM #63	6.78	77.56 ✓	12.97	70.78 ✓
TP	7.37	81.67 ✓	3.26	74.30 ✓

check BM? Spike in Pond Pole # Marked 81 to BM #61

B.P. S.E. Cor. Culvert Kingwell 400' N. Commabel Row East Side Fairmount (Powers St.)

40 penny spike Tel. pole # 82380H 40' Rt. Sta. 381+50

40 penny Spike Gr. Lt. Pole # 79959 60' t - Rt. 389+10

Iron Pin 1" square Rod. 27 t - Rt 393+66 E. End of Dairy Milk Barn

40 penny Spike Top of Willow Stump 200' t - Lt 395+20

		T 81.67 ✓			
TP on ℄ 401+88 77	12.87	92.20 ✓	2.34	79.33	✓
Set BM #64	3.24	86.60 ✓	8.84	83.36	✓
TP	5.46	83.93 ✓	8.13	78.47	✓
TP	4.99	85.33 ✓	3.59	80.34	✓
Set BM #65	6.55	87.60 ✓	4.28	81.05	✓
TP	6.12	90.17 ✓	3.55	84.05	✓
Set BM #66	5.79	90.16 ✓	5.80	84.37	✓
TP	5.54	92.48 ✓	3.22	86.94	✓
Set BM #67	0.09	92.25 ✓	0.22	92.26	✓ ←
TP	7.80	94.89 ✓	5.26	87.09	✓
TP	9.40	100.11 ✓	4.18	90.71	✓
Set BM #68	4.60	100.53 ✓	4.18	95.93	✓
Check BM			6.17	94.36	✓

92.48
5.2
97.3

Top of 1½" Galvanized Pipe 55'+- Lt 408+00

B.P. Top of Blowoff valve #42 Concrete Box on El. Capitan Pipe Line 200'+- Lt 415+00

40 penny Spike in 20" Dia Sycamore 50' Lt 419+10

40 penny Spike in 16" Dia Sycamore 35'+- Rt 422+90

40 penny Spike 16" Sycamore 55'+- Lt 430+20

20 Penny Spike Base of 12" Sycamore 70'+- Lt 430+20

Did Not Discover ord B.M until New one had been Set. Probably Set by Yeager

10445
7 5
97 10 2 00' down ll

		HI 100.53 ✓			
T.P.	7.37	104.45 ✓	3.45	97.08 ✓	
T.P.	5.53	104.57 ✓	5.41	99.04 ✓	
Set BM #69	2.32	105.23 ✓	1.66	102.91 ✓	40 penny Spike 16" Sycamore 160' Rt ± 436+50
T.P.	7.01	108.70 ✓	3.54	101.69 ✓	
Set BM #70	4.27	110.67 ✓	2.30	106.40 ✓	40 penny Spike 22" Sycamore 60' Rt 441+50
TP	6.32	115.40 ✓	1.59	109.08 ✓	
Set BM #71	4.70	117.86 ✓	2.24	113.16 ✓	40 Penny Spk in Base of large Scrub Oak 12 ± Lt 448+70
TP	5.48	119.62 ✓	3.72	114.14 ✓	
TP	7.81	123.50 ✓	3.93	115.69 ✓	
Set BM #72	12.05	131.33 ✓	4.22	119.28 ✓	40 penny Spike Base of Small Sycamore 100' Lt ± 453+75 ±
T.P.	13.00	143.01 ✓	1.32	130.01 ✓	
TP	12.10	152.37 ✓	2.74	140.27 ✓	
Set BM #73	12.95	163.84 ✓	1.48	150.89 ✓	Nail in Redwood Hub 90' ± Rt 457+10.25 P.O.T.

		163.80 ✓			
TP on L 459+19	12.92	167.63 ✓	9.13	154.71 ✓	
TP	12.66	179.92 ✓	0.37	167.26 ✓	
TP	6.62	184.80 ✓	1.74	178.18 ✓	
Set BM #74	13.09	194.77 ✓	3.12	181.68 ✓	R.W. 2'x2" Hub Nail in ctr 80± Lt 461+40
TP	12.60	206.16 ✓	1.21	193.56 ✓	
TP	12.34	217.68 ✓	0.82	205.34 ✓	
T.P.	12.87	229.75 ✓	0.80	216.88 ✓	
			2.93	219.82 ✓	POT. 463+41.83 on 1"x1" Stake
TP	11.81	241.14 ✓	0.42	229.33 ✓	
TP	12.33	252.86 ✓	0.61	240.53 ✓	
			7.44	245.42 ✓ = 245.05	Checked on County TR Hickey Survey Missed 0.37
TP	10.18	261.47 ✓	1.57	251.29 ✓	
Set BM #75	12.54	266.63 ✓	7.38	254.09 ✓	2"x2" R.W. H.6 130± Lt 464+20
TP	12.80	278.84 ✓	0.59	266.04 ✓	

		T 278.84 ✓		
TP.	12.72	290.94 ✓	062	278.22 ✓
TP	12.20	302.18 ✓	0.96	289.98 ✓
Set BM #76	10.20	310.51 ✓	1.87	300.31 ✓
TP	6.21	313.96 ✓	2.76	307.75 ✓
T.P	10.18	319.82 ✓	4.32	309.64 ✓
Set BM #77	11.67	323.61 ✓	7.88	311.94 ✓
TP	12.46	335.88 ✓	0.19	323.42 ✓
T.P.	12.45	348.13 ✓	0.20	335.68 ✓
T.P.	10.48	358.40 ✓	0.21	347.92 ✓
T.P.	11.72	367.85 ✓	2.27	356.13 ✓
TP	12.53	380.02 ✓	0.36	367.49 ✓
TP	12.77	392.69 ✓	0.10	379.92 ✓
T.P.	12.80	405.39 ✓	0.10	392.59 ✓

2"x2" RW Hub 35 ± Δ+ 466+09 75

L. 467+15.74 on 1"x1" stake

L. 468+95.24 on 1"x1" stake

B.P. Top Rubble concrete wall 2' S. of the So end of Receiving Tank.

		BM 405.39 ✓			
T.P.	12.79	417.91 ✓	0.27	405.12	✓
T.P.	12.09	429.59 ✓	0.41	417.50	✓
T.P.	6.25	432.49 ✓	3.35	426.24	✓
TP	5.32	432.57 ✓	5.24	427.25	✓
TP	10.31	442.79 ✓	0.09	432.48	✓
check BM			2.14	440.65	✓ City Datum
		U.S.G.S. Datum →		446.60	✓
				5.95 diff	

1" ford axle 5'-5" West Flagpole adjacent to "Aztec" Business office on State College grounds

Mission Valley Line Revision
East of Fairmount
Sketch Page 17

BM #57	7.35	⟨80.63⟩		73.28	
use other 366+00 ~~366+0~~	Page 20 Forward		~~0.9~~	~~79.7~~	or 3/30/43
+50			1.8	78.8	✓
367+0			3.1	77.5	✓
+50			4.4	76.2	✓
368+0			6.2	74.4	✓
+22			6.9	73.7	✓
+27			9.0	71.6	✓
+33			10.4	70.2	✓ on Conc Rubble
+36.4	Wly Culvert Fairmount		17.0	63.6	✓ Flow Line Culvert
+36.4			11.00	69.6	✓ Top Inside Culvert
+68.46				61.7	Approach below curb
+72.8	Ely Culvert		16.9	63.7	Flow Line Culv
+72.8			10.95	69.68	✓ Top Inside Culvert
+75			9.8	70.8	✓
+85			7.8	72.8	✓
+85	10' Lt of ℄		13.5	67.1	✓
369+0			7.6	73.0	✓
369+0	8' Lt of ℄		7.6	73.0	✓
369+0	16' Lt of ℄		12.9	67.7	✓
+50			7.6	73.0	✓
370+0			7.2	73.4	✓
370+0	5' Lt of ℄		7.1	73.5	✓
+50			6.9	73.7	✓
371+0			6.4	74.2	✓

March 30-43 16
Sisson
Bliss
Begg
Newcomb

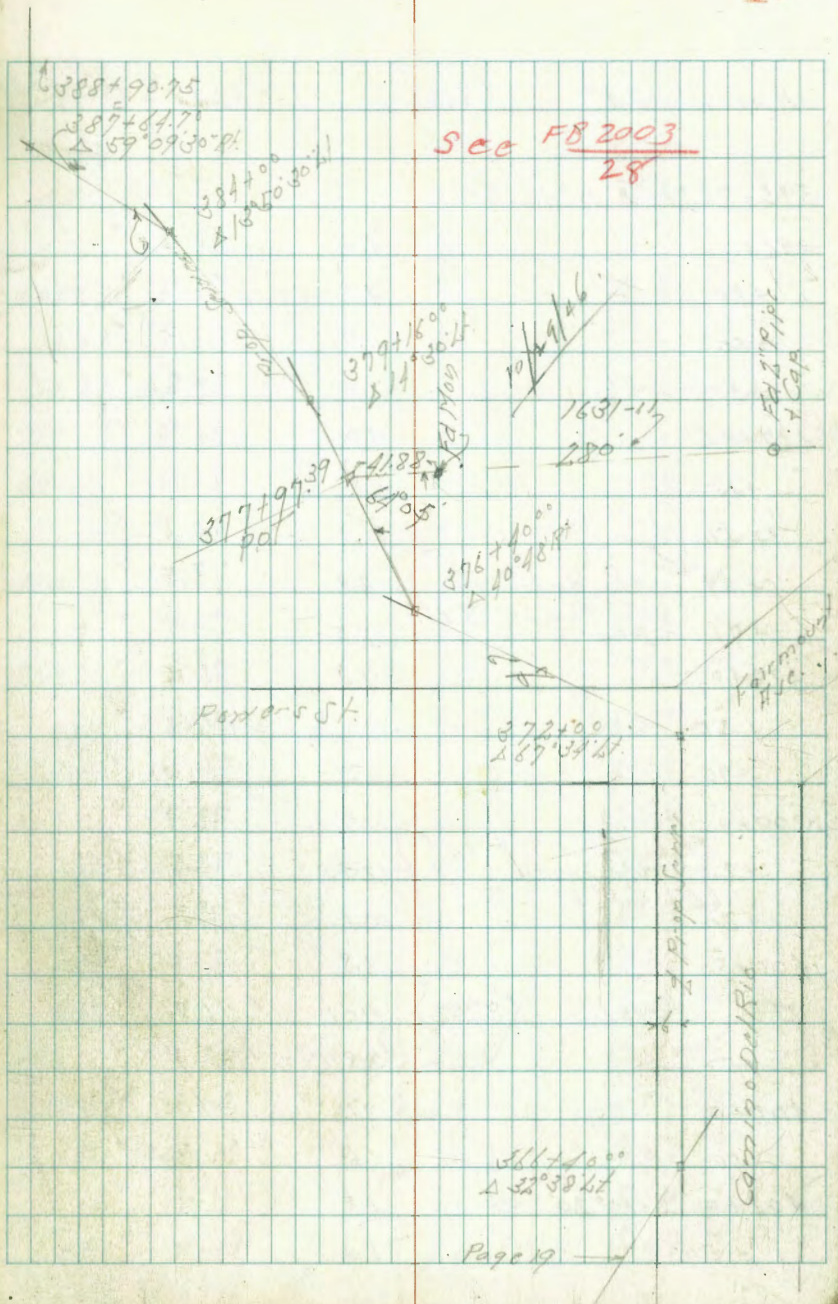
76.39
6.6
83.99
3.6

6.6

⟨80.63⟩

371+0	8' Lt of ℄		5.4	75.2	✓
+30	P.I. Paving		5.8	74.8	✓
+70.4	" "		4.6	76.0	✓
372+0	= Δ 67°34' Lt. ℄ Fairmount + Mission Valley Road		4.0	76.6	✓
TP	7.19	⟨83.86⟩	7.96	⟨76.67⟩	✓
+29	Edge Pav		7.5	76.4	✓
+57			8.0	75.9	✓
373+0			7.5	76.4	✓
+50			6.7	77.2	✓
374+0			5.8	78.1	✓
+50			5.7	78.2	✓
375+0			6.9	77.0	✓
+50			7.5	76.4	✓
+88			7.3	76.6	✓
376+0			5.6	78.3	✓
+09			0.5	83.4	✓
+40	Δ 40°48' Rt.		4.7	79.2	✓
+70			5.2	78.7	✓
377+0			5.4	78.5	✓
+50			6.2	77.7	✓
378+0			6.9	77.0	✓
+30			5.1	78.8	✓
+60			5.7	78.2	✓
379+0			6.0	77.9	✓
TP	11.24	⟨87.63⟩	7.47	⟨76.39⟩	

		(87.63)		
379+16.0	Δ 14°30' Lt.		9.9	77.7
+50			10.4	77.2
380+0			9.4	78.2
BM #60			7.00	(80.63)
+50			9.3	78.3
381+0			9.6	78.0
+50			8.8	78.8
382+0			8.8	78.8
+50			8.1	79.5
383+0			9.5	78.1
+43			12.0	75.6
384+0	Δ 13°50'30" Lt.		6.7	80.9
+24			6.1	81.2
TP	8.90	(84.90)	11.63	(76.00)
+60			4.7	80.2
+74			5.2	79.7
385+0			7.5	77.4
+70			8.7	76.2
386+0			8.3	76.6
+50			5.9	79.0
387+0			3.8	81.1
+34			4.8	80.1
+64.70	Δ 59°09'30" Rt.		7.72	(77.18)
388+90.75				

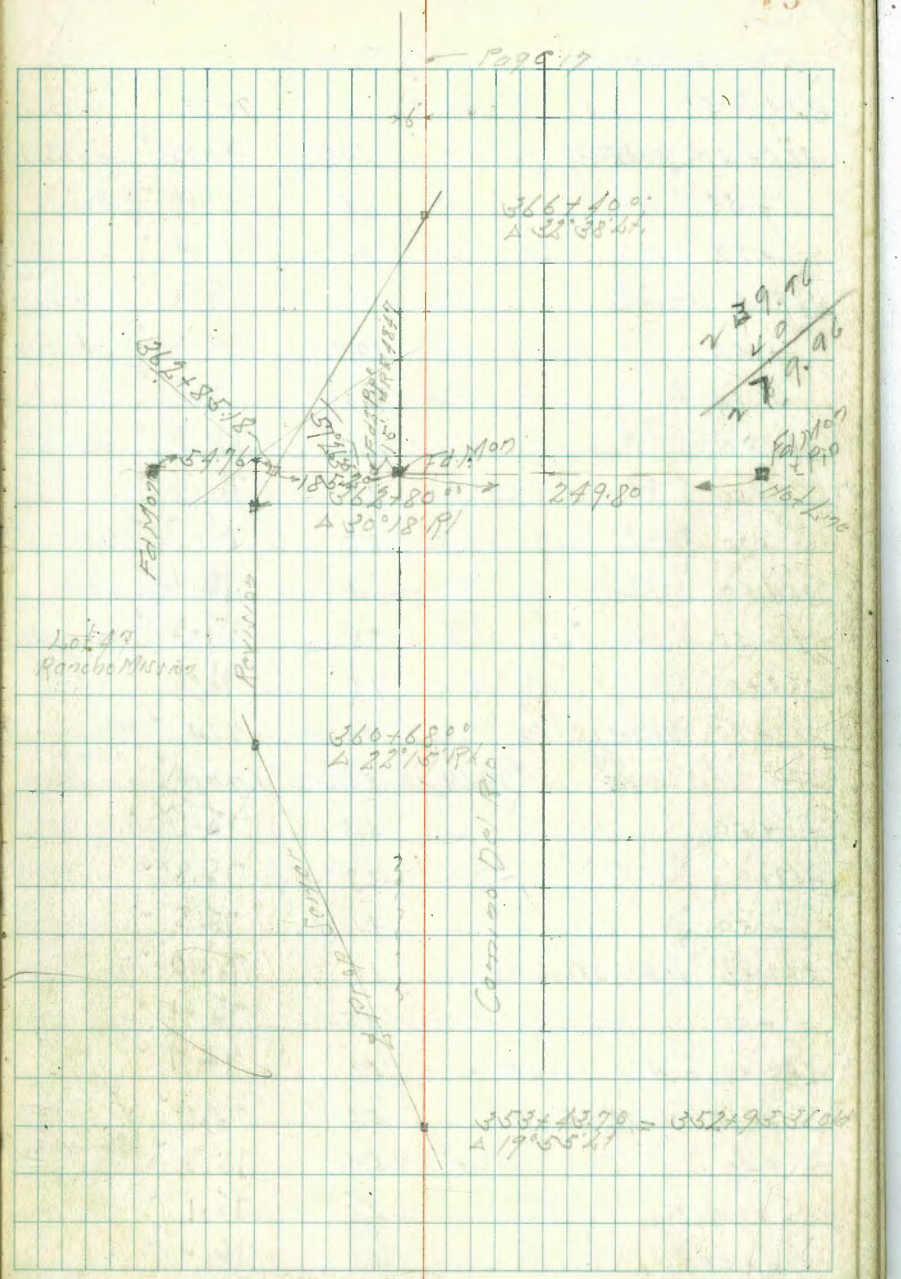


BM	2.37	[85.82]	[83.45]	Offsets 896+80.23	
395+86.21	Δ 11°40' Rt				
396+0		4.5	81.3		
+20		4.1	81.7		
+50		1.9	83.9		
+80		2.0	83.8		
397+0		3.9	81.9		
+15		4.8	81.0		
+50	25' Rt. = EL. = 76.2	11.3	74.5		
+59	W/y Wash	12.3	73.5		
+71	25' Lt. EL. = 71.9 — Ely "	12.5	73.3		
398+0		9.4	76.4		
+50		9.0	76.8		
+70		9.8	76.0		
399+0		11.9	73.9		
+25	EL. 25' Rt. = 76.5 W/y Wash EL 25' Lt. = 71.3	12.3	73.5		
+50		10.1	75.7		
400+0		8.8	77.0		
TP	11.11	[87.92]	90.1	[76.81]	
+50		8.8	79.1		
401+0		7.1	80.8		
+50		6.6	81.3		
402+0	Δ 10°20' Rt	6.8	81.1		
+50		5.3	82.6		

[87.92]

403+0		5.4	82.5	
+50		7.9	80.0	
+93		9.3	78.6	
+95		9.2	78.7	
404+0		8.1	79.8	
+40		6.3	81.6	
+70	Δ 29°10' Lt.	5.74	[87.18]	Offset Hub 404+70
TP	7.86 90.04	5.74	[82.18]	
405+0		10.1	79.9	
+50		8.7	81.3	
406+0		6.3	83.7	
+50		6.2	83.8	
407+0		6.7	83.3	
+29	Δ 61°06' Rt.	7.3	82.7	
+50		6.1	83.9	
408+0		4.6	85.4	
+50		3.1	86.9	
+50 : W/y Road		3.7	86.3	
+81		3.2	86.8	
+87		6.0	84.0	
TP	6.97 [92.19]	4.82	[85.22]	
409+0		6.4	85.8	
+04		9.5	82.7	
+28		7.2	85.0	
+45		7.4	84.8	

		(92.19) ✓		
409+70	POT	0.9	91.3 ✓	
410+0	Ground	9.1	83.1 ✓	
410+0	Top E/Capilano Pipe Line	10.25	81.94 ✓	
+07		9.0	83.2 ✓	
+15		5.8	86.4 ✓	
+35	Δ 29°00' Lt	4.85	87.34 ✓	on Hub
+60		9.2	83.0 ✓	
+85		11.1	81.1 ✓	
411+0		11.1	81.1 ✓	
+50		10.5	81.7 ✓	
412+0		9.2	83.0 ✓	
+50		10.9	81.3 ✓	
+90.03	Δ 20°02'30" Lt.	10.5	81.7 ✓	
TP	8.40	(92.62) ✓	7.97	(84.22) ✓
413+0			10.9	81.7 ✓
+35			11.9	80.7 ✓
+50			11.7	80.9 ✓
414+0			9.0	83.6 ✓
+48.25	Δ 14°09' Rt		6.92	(85.70) ✓ on Hub
413+99.77	old Line			
BM "65"			11.52	(81.10) ✓ 81.05 Page 11



Revision Mission Mission Valley Trunk
West of Fairmount.
Sketch Page 19

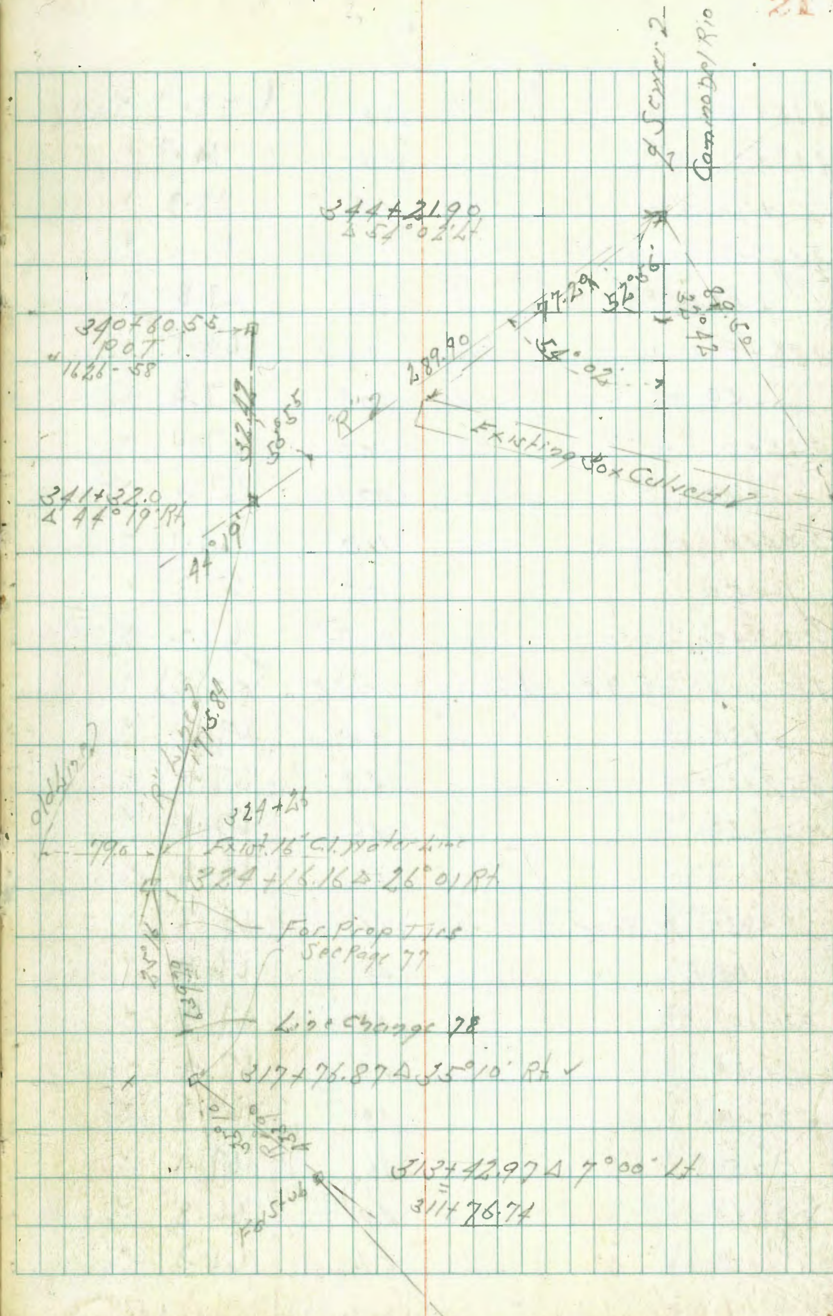
B.M.# 57	11.61	⟨84.89⟩		73.28	
366+40	Δ 32°38' Lt.		6.16	78.73	on Hub
+33			6.5	78.4	
+22			9.5	75.4	
366+0			9.6	75.3	
+50			10.9	74.0	
+14			11.6	73.3	
365+0			11.0	73.9	
+50			9.2	75.7	
+25			8.2	76.7	
364+0			8.3	76.6	
+55			7.6	77.3	
363+0			9.8	75.1	
362+80	Δ 30°18' Rt.		10.5	74.4	
TP	4.35	⟨79.63⟩	9.61	⟨75.28⟩	on Peg 3' Rt 362+85
+50			4.5	75.1	
362+0			3.8	75.8	
+50			4.1	75.5	
361+0	= Ely Stock Pile		4.6	75.0	
+50			4.5	75.1	
360+0	= Wly Stock Pile		4.9	74.7	
+68.0	Δ 22°15' Rt.		5.4	74.2	359+72 35' Lt = S.Wly Cor. 16×18' Frame Garage
+40			6.3	73.3	
359+0			4.5	75.1	
+50			3.2	76.4	

April 5-43
Sisson
Bliss
Begg
Newcomb

		⟨79.63⟩			
358+0			1.0	78.6	
TP	12.41	⟨91.88⟩	0.16	⟨79.47⟩	
+50			9.2	82.7	
357+0			6.9	85.0	
+50			5.3	86.6	
356+0 P.O.T.			4.9	87.0	
+50			5.3	86.6	
355+0			7.0	84.9	
+55			7.2	84.7	
+40			9.5	82.4	
+35			7.8	84.1	
354+0			9.2	82.7	
+85			9.8	82.1	
+70			8.7	83.2	
353+13.70	Δ 19°55' Lt.		9.07	⟨82.81⟩	on Hub
352+92.36 Old					
TP	7.20	⟨96.96⟩	2.12	⟨89.76⟩	
BM# 55			3.06	⟨93.90⟩	93.90

Mission Valley Line
Revision At Hard Road
"R" Line

BM # 53	0.62	⟨76.06⟩		⟨75.44⟩	Spk 35 ft 344+95 0.6 ft
344+21.90 Δ 54°02' Lt.			2.2	73.9	✓
344+0			3.6	72.5	✓
+85			4.7	71.4	✓
+65			4.2	71.9	✓
+44.7			6.8	69.3	✓
+44.0 = Nly Conc Top Wing			7.30	68.76	✓
+44.0 Ground			16.7	59.4	✓
+33.0 = Sly Conc Top Wing			7.70	68.36	✓
+33.0 Ground			16.7	59.4	✓
+15			5.1	71.0	✓
343+0			6.3	69.8	✓
+80			6.5	69.6	✓
+72			7.2	68.9	✓
+67.5 = Ely Paving			7.00	69.06	✓
+21.0 = Wly "			8.13	67.93	✓
342+0			5.8	70.3	✓
+75			1.0	75.1	✓
+32.0			0.9	75.2	✓
TP	2.74	⟨78.13⟩	0.67	⟨75.39⟩	✓
341+0			2.6	75.5	✓
+50			1.9	76.2	✓
340+0			2.7	75.4	✓
+50			2.8	75.3	✓
339+0			2.9	75.2	✓



		(78.13)		
338+50		2.8	75.3	✓
338+0		3.4	74.7	✓
+75		4.8	73.3	✓
337+0		6.1	72.0	✓
+50		8.3	69.8	✓
336+0		10.0	68.1	✓
+50		10.8	67.3	✓
335+0		10.7	67.4	✓
+50		10.9	67.2	✓
334+0		11.0	67.1	✓
+50		10.8	67.3	✓
333+0		10.9	67.2	✓
TP	8.75	(71.66)	10.22	(67.91) ✓
+50			4.4	67.3 ✓
332+0			4.5	67.2 ✓
+50			4.6	67.1 ✓
331+0			5.1	66.6 ✓
+83 = ℄ Road			6.0	65.7 ✓
+50			4.8	66.9 ✓
330+0			4.4	67.3 ✓
+50			4.3	67.4 ✓
329+0			4.2	67.5 ✓
+50			4.6	67.1 ✓
328+0			4.9	66.8 ✓
+50			5.4	66.3 ✓

		(71.66)		
327+0			6.8	65.9 ✓
+50			6.2	65.4 ✓
326+0			6.9	64.8 ✓
+50			7.6	64.1 ✓
325+0			8.3	63.4 ✓
+50			9.1	62.6 ✓
+35 = Natural Ground			9.53	62.13 ✓
+16.16 ∆ 25°16'Rt			9.4	62.3 ✓
BM #19 6.87		(64.28) ✓	11.25	(60.41) ✓
324+26 : Top 16" C.I. Water Pipe 79.0 Lt = old Line			8.10	(59.18) ✓
BM #19 6.42		(64.82) ✓		(60.40) ✓
324+0			2.3	61.5 ✓
+50			2.1	61.7 ✓
323+0			2.2	61.6 ✓
+50			2.5	61.3 ✓
322+0			3.4	60.6 ✓
+50			4.1	59.7 ✓
321+0			4.8	59.0 ✓
+50			5.1	58.7 ✓
320+0			5.3	58.5 ✓
+70			4.4	59.4 ✓
+50			4.8	59.0 ✓
319+0			5.1	58.7 ✓
+75			5.8	58.0 ✓

		〈63.82〉 ✓			
318+60			7.5	56.3	
+30			8.3	55.5	
318+0			8.3	55.5	
+76.87	Δ 35°10' Rt		8.3	55.5	
TP	9.25	〈64.78〉 ✓	8.29	〈55.53〉 ✓	on Hub 318+76.87
+76.87	6' Lt of ℄		10.7	54.1	
+50			8.6	56.2	
317+0			7.9	56.9	
"	12' Lt of ℄		8.9	55.9	
"	22 " " "		12.2	52.6	
+50			7.7	57.1	
316+0			7.0	57.8	
"	Lt of ℄		7.0	57.8	
+50			5.6	59.2	
+17	= N'ly Farm Road		4.6	60.2	
315+0			4.3	60.5	
+70			5.1	59.7	
+60			7.1	57.7	
+50			6.0	58.8	
+40			6.5	58.3	
314+0			6.9	57.9	
"	5' Lt of ℄		6.9	57.9	
"	12' Lt of ℄		8.8	56.0	
313+42.97 = 311+76.74 old	Δ 7°00' Lt		8.27	〈56.51〉 ✓	

see 162/60

		〈64.78〉 ✓			
TP	9.60	〈73.46〉 ✓	0.92	〈63.86〉 ✓	
BM*18			4.34	〈69.12〉 ✓	69.11 P8

April 19 46
5:55 [illegible]

Elev. Water Main 324+26

BM	5.78	68.08		62.3	on Hub 324+16.16 Page 22

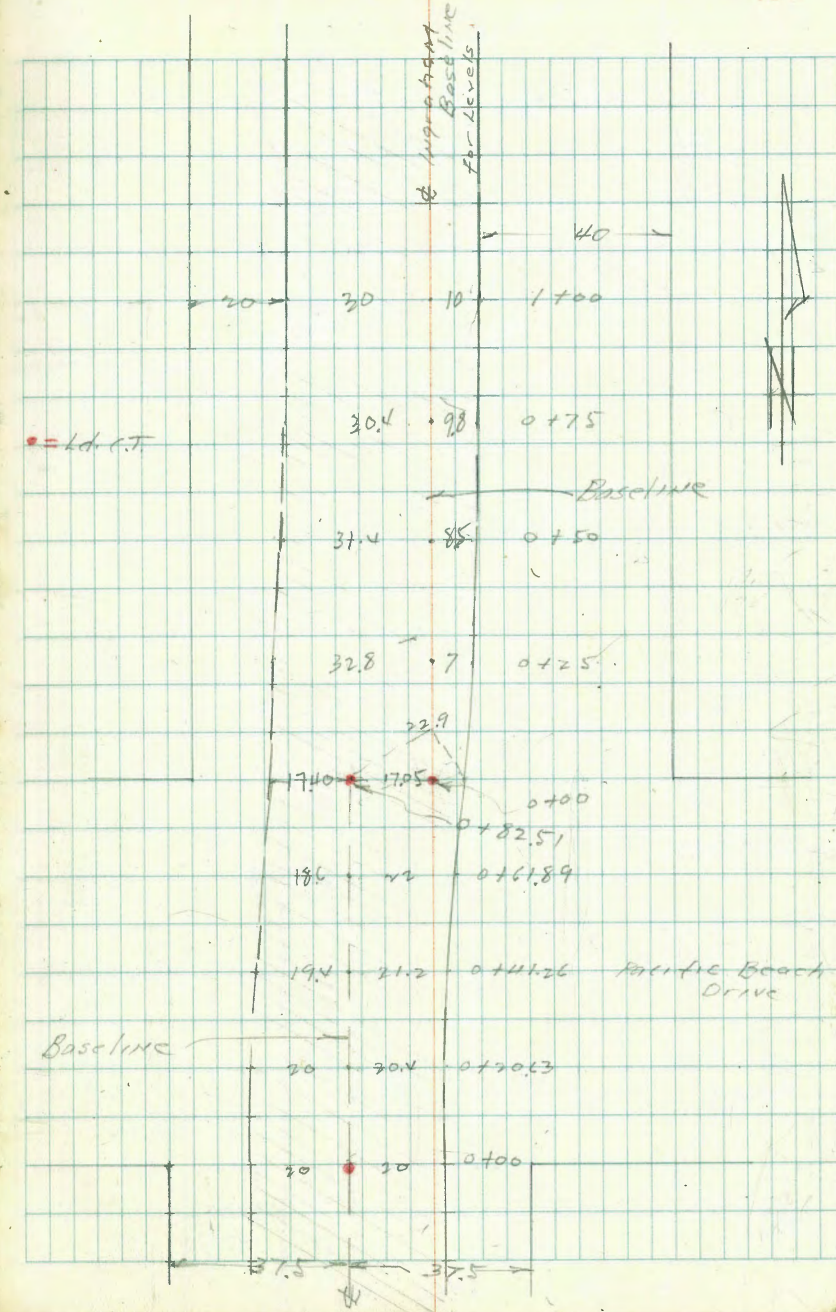
Location shown on Page ~~22~~ page 18

26' S of Sewer Top 16" C.I. Water Main 7.96 60.12

Indexed
P.D.K.

Levels on Paving on
Ingraham St.
Pacific Beach Dr. to Thomas

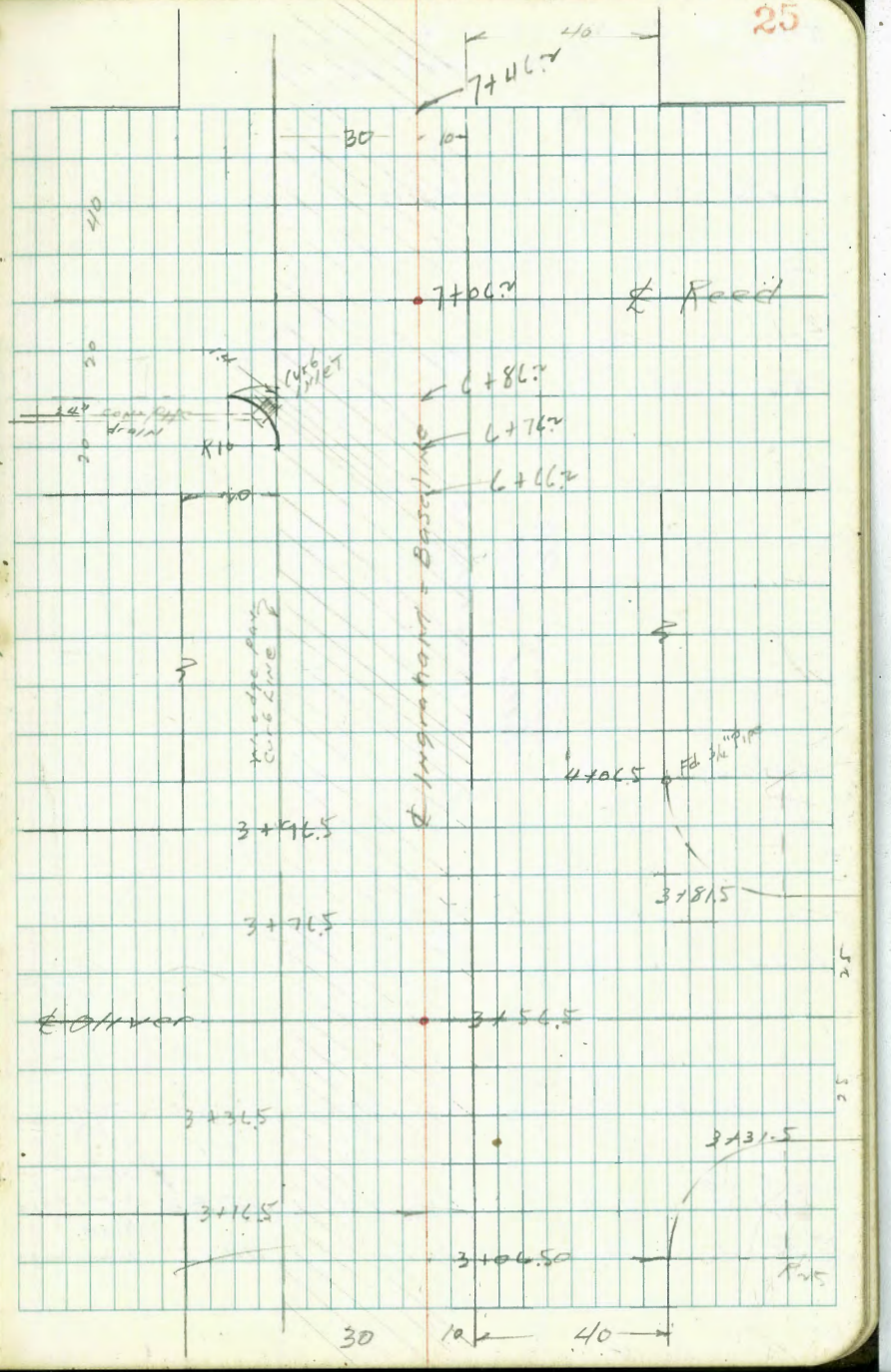
C. Moore
Sommermeyer
W. Moore
12-13-43



S.L. Thomas = 10+15.75

E " = 10+55.75

N.L. " = 10+95.75



Indexed P.D.K.

Ingraham St. 6" Pav. (Conc.) Levels

Pacific to Thomas

0+82.51 = N.L. Pacific = 0+00 to North

0+61.89

0+41.26

0+20.63

0+00 = S.L. Pacific

Reduced AEB
Plotted OBH
Profiles 1202-3

check to BM Ld CT	N.L. Pacific Beach Dr ℄ Ingraham to S.		5.39	46.24	46.11 / 0.13
T.P. ℄ Ld. C.T.	3.65	51.63	3.19	47.98	Oliver Ingraham
℄ Ld. C.T.	7.02	51.17		44.15	Reed Ingraham

Lt	℄ Baseline	Rt
45.67 / 5.96 / 17.4	46.24 / 5.39	46.09 / 5.54 / 22.9
45.59 (46.59) / 6.04 / 18.6	46.21 / 5.42	45.58 / 5.65 / 22
45.57 (46.57) / 6.11 / 19.4	46.11 / 5.52	45.79 / 5.84 / 21.2
45.61 / 6.02 / 20	46.03 / 5.60	45.68 / 5.95 / 20.4
45.61 / 6.02 / 20	46.00 / 5.63	45.65 / 5.98 / 20
	51.63	

This is on ℄ of Paved Strip LT → | ℄ of St. Not Paving RT — ℄ Baseline

Station				℄ Baseline	
+50	46.93 / 4.70 / 30	47.32 / 4.31 / 20	47.48 / 4.15 / 10	47.57 / 4.06	47.47 / 4.16 / 10
2+00	46.61 / 5.02 / 30	46.99 / 4.64 / 20	47.20 / 4.43 / 10	47.29 / 4.34	47.15 / 4.48 / 10
+50	46.31 / 5.32 / 30	46.68 / 4.95 / 20	46.90 / 4.73 / 10	46.97 / 4.66	46.85 / 4.78 / 10
1+00	46.04 / 5.59 / 30	46.43 / 5.20 / 20	46.64 / 4.99 / 10	46.69 / 4.94	46.55 / 5.08 / 10
0+75	45.88 46.88 / 5.75 / 30.4	46.30 / 5.33 / 20	46.49 / 5.14 / 10	46.55 / 5.08	46.44 / 5.19 / 9.8
0+50	45.77 / 5.86 / 31.4	46.21 / 5.42 / 21.5	46.42 / 5.21 / 11.5		46.29 / 5.34 / 8.5
0+25	45.71 / 5.92 / 32.8	46.19 / 5.46 / 33	46.33 / 5.30 / 13		46.18 / 5.45 / 7

51.63

3+81.5 S.L. Oliver to East

3+76.5

3+56.5 ℄ Oliver

3+36.5

3+31.5 S.L. Oliver to East

3+10.5 S.L. Oliver to West

3+06.50 Prop B.C. on Rt.

L ℄ Rt

42.32	42.70	42.88	42.93	42.85
4.31	3.93	3.75	3.68	3.78
30	20	10		10
42.31	42.71	42.90	42.96	42.82
4.32	3.94	3.73	3.67	3.76
30	20	10		10
42.32	42.70	42.93	42.95	42.82
4.31	3.93	3.70	3.65	3.78
30	20	10		10
42.37	42.69	42.90	42.96	42.84
4.36	3.94	3.73	3.67	3.79
30	20	10		10
42.27	42.68	42.89	42.94	42.83
4.34	3.95	3.74	3.69	3.80
30	20	10		10
42.23	42.63	42.87	42.96	42.84
4.40	3.98	3.76	3.67	3.79
30	20	10		10
42.19	42.60	42.78	42.91	42.71
4.44	4.03	3.81	3.72	3.84
30	20	10		10

51.63

6 + 50

6

+ 50

5

4 + 50

Ld. ct. E
T.P. Oliver 2.16 50.14 3.65 47.98

4 + 06.5 Prop. B.C. on Rt.

3 + 96.5 N.L. Oliver to West

51.63

	Lt		℄	Rt
43.60 / 6.54 / 30	44.04 / 6.10 / 20	44.27 / 5.87 / 10	44.46 / 5.68	44.45 / 5.69 / 10
44.50 / 5.64 / 30	44.93 / 5.21 / 20	45.19 / 4.95 / 10	45.36 / 4.78	45.34 / 4.80 / 10
45.22 / 4.92 / 30	45.62 / 4.52 / 20	45.87 / 4.27 / 10	45.98 / 4.16	45.94 / 4.20 / 10
45.94 / 4.20 / 30	46.35 / 3.79 / 20	46.54 / 3.60 / 10	46.65 / 3.49	46.54 / 3.60 / 10
46.67 / 3.47 / 30	47.03 / 3.11 / 20	47.24 / 2.90 / 10	47.31 / 2.83	47.17 / 2.97 / 10

50.14

47.74 / 4.39 / 30	47.61 / 4.02 / 20	47.81 / 3.82 / 10	47.86 / 3.77	47.71 / 3.92 / 10
47.30 / 4.33 / 30	47.68 / 3.95 / 20	47.91 / 3.72 / 1.0	47.97 / 3.66	47.83 / 3.80 / 10

51.63

Station	Description	Other shots	Lt 30	Lt 20	Lt 10	℄	Rt 10	Remarks
8+00			44.98 / 5.16 / 30	45.36 / 4.78 / 20	45.54 / 4.60 / 10	45.62 / 4.52	45.52 / 4.62 / 10	
7+46.2	N.L. Reed		44.18 / 5.96 / 30	44.59 / 5.55 / 20	44.85 / 5.29 / 10	44.97 / 5.17	44.89 / 5.25 / 10	
7+26.2			43.88 / 6.26 / 30	44.23 / 5.91 / 20	44.38 / 5.76 / 10	44.51 / 5.63	44.50 / 5.64 / 10	
7+06.2	℄ Reed		43.57 / 6.57 / 30	44.87 / 6.27 / 20	44.01 / 6.13 / 10	44.02 / 5.99	44.10 / 6.04 / 10	
6+86.2	S. cb. Reed	43.95 / 6.19 / 40 / cb.; 43.22 / 6.92 / 40 / gut; 40.36 / 9.78 / F.L. Box; 43.99 / 6.15 / ℄ Return curb; 43.20 (~~45.20~~) / 6.94 / grate	43.27 / 6.87 / 30	43.58 / 6.56 / 20	43.65 / 6.49 / 10	43.83 / 6.31	43.81 / 6.33 / 10	← Valley Gutter
6+76.2		43.96 / 6.18 / 30 / cb	43.21 / 6.93 / 30 / gut	43.55 / 6.59 / 20	43.73 / 6.41 / 10	43.95 / 6.19	43.92 / 6.22 / 10	
6+66.2	S.L. Reed		43.29 / 6.85 / 30	43.70 / 6.44 / 20	43.93 / 6.21 / 10	44.11 / 6.03	44.09 / 6.05 / 10	

Headings on the grid page: Lt, ℄, Rt

50.14

10 + 35.75

10 + 15.75 · S.L. Thomas

10

+ 50

9

8 + 50

T.P.	L x C	51.81	4.59	45.55
		50.14		

Lt Baseline Rt

48.17	48.48	48.28	48.25	48.49
3.44	3.33	3.03	3.04	3.34
30	20	10		10
48.27	48.38	48.54	48.45	48.15
3.59	3.47	3.27	3.34	3.06
30	20	10		10
42.21	48.14	48.33	48.30	48.04
4.10	3.67	3.48	3.51	3.77
30	20	10		10
42.14	42.42	42.63	42.64	42.41
4.31	4.34	4.18	4.17	4.40
30	20	10		10
46.38	46.21	46.41	46.93	46.76
5.43	5.64	4.90	4.88	5.05
30	20	10		10
45.68	46.05	46.24	46.31	46.19
6.13	5.76	5.57	5.50	5.64
30	20	10		10

51.81

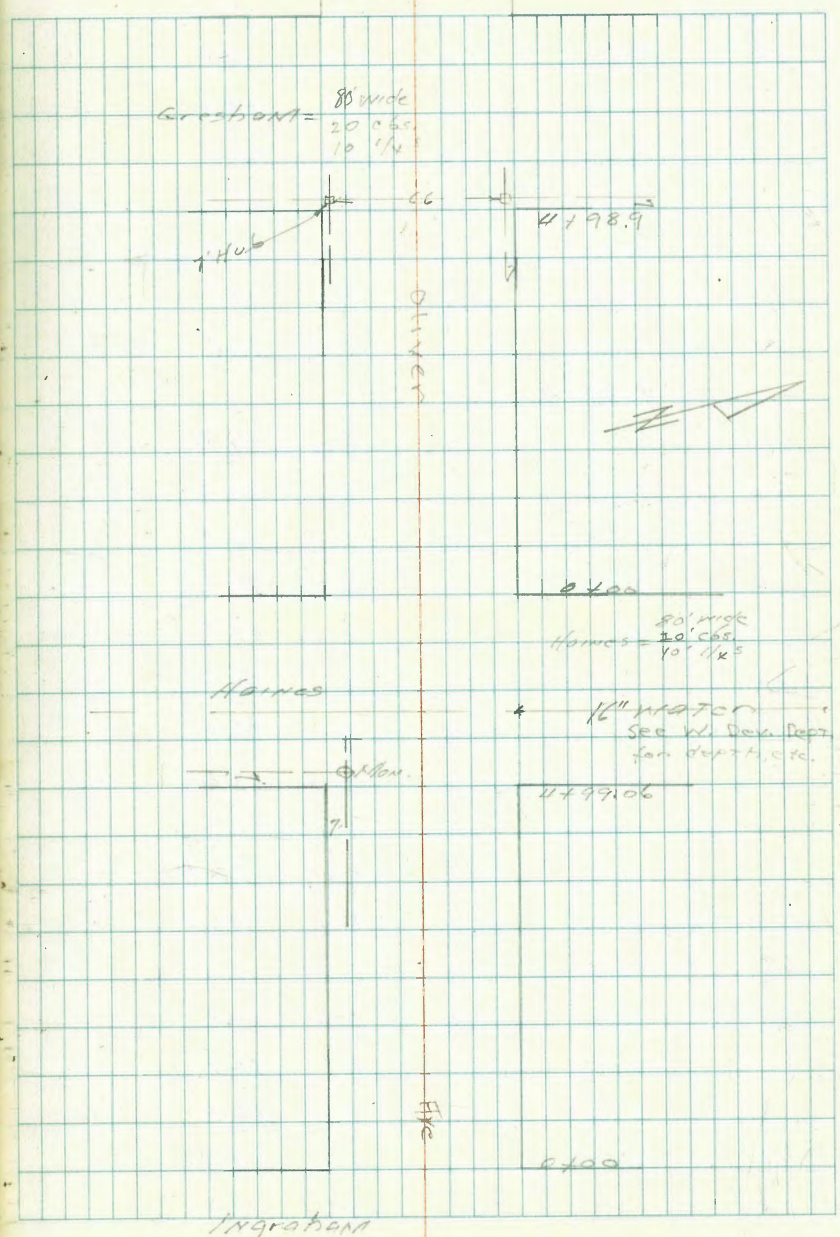
N.E. B.P. in Curb Check to Grand & Ingraham			1.87	55.85	55.85 0.00
T.P.	7.82	57.72	1.91	49.90	
10 + 95.75 N. L. Thomas					
10 + 75.75					
10 + 55.75 ℄ Thomas					

Lt		Baseline		Rt
		℄ 40' Pav. Strip		
48.09 2.72 30	48.45 2.36 20	48.61 2.20 10	48.55 2.26	48.30 2.51 10
48.72 3.09 30	48.12 2.69 20	48.33 2.48 10	48.25 2.56	48.01 2.80 10
48.49 3.32 30	48.86 2.95 20	48.05 2.76 10	48.02 2.79	48.78 3.03 10

Xsec Oliver Ave. = 80' – 20' cbs. 10' 1/4s
Ingraham to Gresham Moore 12-14-43

P.2.C ℄ Ld. C.T.	9.17	57.15		47.98	Oliver Ingraham
	0 – 5				
5			9.2	48.0	
+10			9.3	47.9	
c6			9.2	48.0	
1/4			9.3	47.9	
℄			9.1	48.1	
1/4			9.3	47.9	
c6			9.5	47.7	
N			9.6	47.6	
	0+00 W.L. Ingraham				
N			6.4	50.8	
+15			7.4	49.8	
c6			8.1	49.1	
1/4			8.8	48.4	
℄			8.9	48.3	
1/4			9.1	48.1	
c6			8.6	48.6	
+5			6.9	50.3	
S			5.7	51.5	
	0+02				
S			4.5	52.7	

Reduced OEB & CRH
Plotted 1-7-44 CRH
Profiles 2343 of unnumbered



5 + 15	5.1	52.1
c6	8.2	49.0
1/4	8.8	48.4
c	8.8	48.4
1/4	8.6	48.6
c6	8.4	47.8 48.8
+ 5	5.3	51.9
N	5.6	51.6
0 + 25		
N	5.4	51.8
c6	5.2	52.0
1/4	6.5	50.7
c	7.1	50.1
1/4	6.8	50.4
c6	6.6	50.6
+ 4	4.2	53.0
5	4.0	53.2
0 + 50		
5	3.9	53.3
+ 16	4.2	53.0
c6	5.1	52.1
1/4	5.2	52.0
c	5.5	51.7
1/4	5.0	52.2
c6	4.9	52.3
N	5.5	51.7

0 + 75		
N	5.5	51.7
c6	5.1	52.1
1/4	4.6	52.6
c	4.9	52.3
1/4	4.8	52.4
c6	4.3	52.9
+ 5	3.8	53.4
5	3.6	53.6
1 + 00		
5	3.7	53.5
c6	3.9	53.3
1/4	4.8	52.4
c	4.8	52.4
1/4	5.0	52.2
c6	5.3	51.9
N	5.6	51.6
1 + 50		
N	6.6	50.6
c6	6.2	51.0
1/4	5.6	51.6
c	5.2	52.0
1/4	5.2	52.0
c6	4.6	52.6
5	4.2	53.0

	2 + 00		
S		5.3	51.9
C6		5.8	51.4
1/4		6.5	50.7
C		6.6	50.6
1/4		6.9	50.3
C6		7.3	49.9
N		7.9	49.3
	2 + 50		
N		9.8	47.4
C6		9.6	47.6
1/4		9.0	48.2
C		8.6	48.6
1/4		8.7	48.5
C6		7.9	49.3
S		6.9	50.3
	2 + 7.2		
S + 2	Beg. 4" Con wall	8.0	49.2 ✓ Top
	3 + 00		
S	ex walk	9.06	48.09 ✓
+ 1.2	E 3' con. walk	9.1	48.04
C6		9.9	47.3
1/4		10.6	46.6
C		10.6	46.6
1/4		10.9	46.3
C6		11.3	45.9
N		11.3	45.9

	3 + 2.6		
S + 1.7	ex'd 4" Con wall	9.6	47.6 ✓ Top
	3 + 50		
N		12.4	44.8
C6		12.5	44.7
1/4		12.2	45.0
C		12.0	45.2
1/4		12.0	45.2
C6		11.6	45.6
S		10.8	46.4
S + 0.1	E 3' Con walk	10.58	46.62 ✓
T.P	3.91	49.63 ✓	11.43	45.72 ✓
	4 + 00		
S - 3.2	Beg. 6" Con. Ret. wall	3.91	45.72 Top ✓
S		4.1	45.5
C6		5.1	44.5
1/4		5.3	44.3
C		5.2	44.4
1/4		5.3	44.3
C6		5.4	44.2
N		5.2	44.4
	4 + 50		
N		5.3	44.3
C6		5.4	44.2

49.63

1/4		5.7	43.9
c		5.4	44.2
1/4		5.5	44.1
cb		5.6	44.0
s		4.8	44.8
	4+54.4		
S – 3.4	End C" Con. Ret Wall 4.45		45.38 Top ✓
	4+99.06 E.L. Haines =	80' wide 20' cbs 10' 1/4s	
s		5.0	44.6
cb		5.7	43.9
1/4		6.0	43.6
c		5.3	44.3
1/4		5.7	43.9
cb		5.9	43.7
N		5.6	44.0
	E curb		
N		4.5	45.1
cb		5.4	44.4
1/4		5.3	44.3
c		5.9	43.7
1/4		5.7	43.9
cb		5.5	54.1
s		5.9	43.7
	E 1/4		
s		6.4	43.4
cb		6.4	43.2

49.63

1/4		6.4	43.2
c		6.3	43.3
1/4		6.3	43.3
cb		6.4	43.4
N		5.9	43.7
	E Haines		
N		6.0	43.6
cb		6.3	43.3
1/4		6.4	43.2
c		6.5	43.1
1/4		6.5	43.1
cb		6.5	43.1
s		6.3	43.3
	W 1/4		
s		6.5	43.1
cb		6.5	43.1
1/4		6.7	42.9
c		6.6	43.0
1/4		6.6	43.0
cb		6.4	43.2
N		6.2	43.4
	W curb		
N		5.8	43.8
cb		5.8	43.8
1/4		6.3	43.3
c		6.3	43.3

		49.63			
c +4			6.6	43.0	
1/4			7.1	42.5	
+4			6.5	43.1	
c6			6.4	43.2	
S			6.1	43.5	
	0+00 W L Haines				
S			6.7	42.9	
c6			6.4	43.2	
+7			6.4	43.2	
1/4			7.0	42.6	
+4			7.4	42.2	
C			6.7	42.9	
1/4			6.4	43.2	
c6			6.1	43.5	
N			5.9	43.7	
Nail T.P. in P.P.	0.77	44.82	5.58	44.05	Swecon Oliver Haines
	0+50				
N			2.0	42.8	
+10			2.0	42.8	
c6			2.8	42.0	
1/4			2.6	42.2	
C			3.2	41.6	
+5			3.7	41.1	
1/4			2.8	42.0	

	44.82		
c6		3.0	41.8
S		3.0	41.8
	1+00		
S		4.8	40.0
c6		4.8	40.0
1/4		4.7	40.1
+4		5.3	39.5
C		5.1	39.7
1/4		4.5	40.3
c6		4.5	40.3
+10		3.6	41.2
N		3.7	41.1
	1+50		
N		6.5	38.3
+10		6.1	38.7
c6		6.6	38.2
1/4		6.8	38.0
C		7.0	37.8
1/4		7.9	36.9
+4		6.9	37.9
c6		7.0	37.8
S		7.2	37.6
	2+00		
S		10.4	34.4
c6		10.4	34.4
+6		10.1	34.7

44.82

1/4		11.1	33.7
C		10.3	34.5
1/4		9.8	35.0
C6		10.2	34.6
+10		9.6	35.2
N		9.6	35.2
	2+50		
-10		13.5	31.3 ✓
N		13.6	31.2
C6		14.1	30.7
1/4		13.8	31.0
C		14.2	30.6
1/4		14.4	30.4
C6		14.0	30.8
S		14.2	30.6
+10		14.4	30.4 ✓
T.P	0.83	32.95 ✓	12.70 32.12
	3+00		
-10		5.4	27.6 ✓
S		5.1	27.9
C6		5.0	28.0
1/4		4.7	28.3
C		4.7	28.3
1/4		4.9	28.1

32.95

33

C6		5.1	27.9
+10		4.6	28.4
N		4.3	28.7
+10		4.3	28.7 ✓
	3+50		
-10		6.1	26.9 ✓
N		6.2	26.8
C6		6.4	26.6
1/4		6.4	26.6
C		6.2	26.8
1/4		6.5	26.5
C6		7.1	25.9
S		7.0	26.0
+10		7.1	25.9 ✓
	4+00		
-10		7.7	25.3 ✓
S		7.7	25.3
C6		7.5	25.5
1/4		7.3	25.7
C		6.8	26.2
1/4		6.9	26.1
C6		7.2	25.8
N		6.9	26.1
+10		6.8	26.2 ✓
	4+50		
N-10		6.8	26.2 ✓

N		6.8	26.2
c6		7.2	25.8
1/4		7.1	25.9
C		7.0	26.0
1/4		7.4	25.6
c6		7.5	25.5
S		7.9	25.1
+10		7.9	25.1
	4+98.9 E.L. Gresham =		80 wide 20' c6s 10' 1/4s
S		7.8	25.2
c6		7.3	25.7
1/4		7.2	25.8
C		7.0	26.0
1/4		6.8	26.2
c6		6.6	26.4
N		6.6	26.4
	E c6		
N		6.5	26.5
c6		6.6	26.4
1/4		6.8	26.2
C		7.2	25.8
1/4		7.2	25.8
c6		7.1	25.9
S		7.4	25.6
	E c6 + 5		
S		8.4	24.6

c6		8.3	24.7
1/4		8.3	24.7
C		8.2	24.8
1/4		8.0	25.0
c6		7.9	25.1
S		7.2	25.8
	E 1/4		
N		6.8	26.2
c6		7.1	25.9
1/4		7.1	25.9
C		7.2	25.8
1/4		7.4	25.6
c6		7.6	25.4
S		7.8	25.2
	E Gresham		
S		7.7	25.3
c6		7.3	25.7
1/4		7.2	25.8
C		7.1	25.9
1/4		7.0	26.0
c6		6.8	26.2
N		6.5	26.5
	W 1/4		
N		6.7	26.3
c6		7.1	25.9
1/4		7.2	25.8

32.95

c	7.4	256
1/4	7.5	255
c6	7.7	253
S	8.0	250
W c6		
S	7.3	257
c6	7.0	260
1/4	7.3	257
c	7.0	260
1/4	7.0	260
c6	6.8	262
+7	5.9	271
N	5.7	273
W.L. Gresham		
N	5.7	27.3
+15	6.0	270
c6	6.8	262
1/4	6.4	266
c	6.5	265
1/4	6.7	263
c6	6.9	261
+3	6.6	264
S	7.1	259

32.95

T.P. 400 = 8.71 BM = 24.71

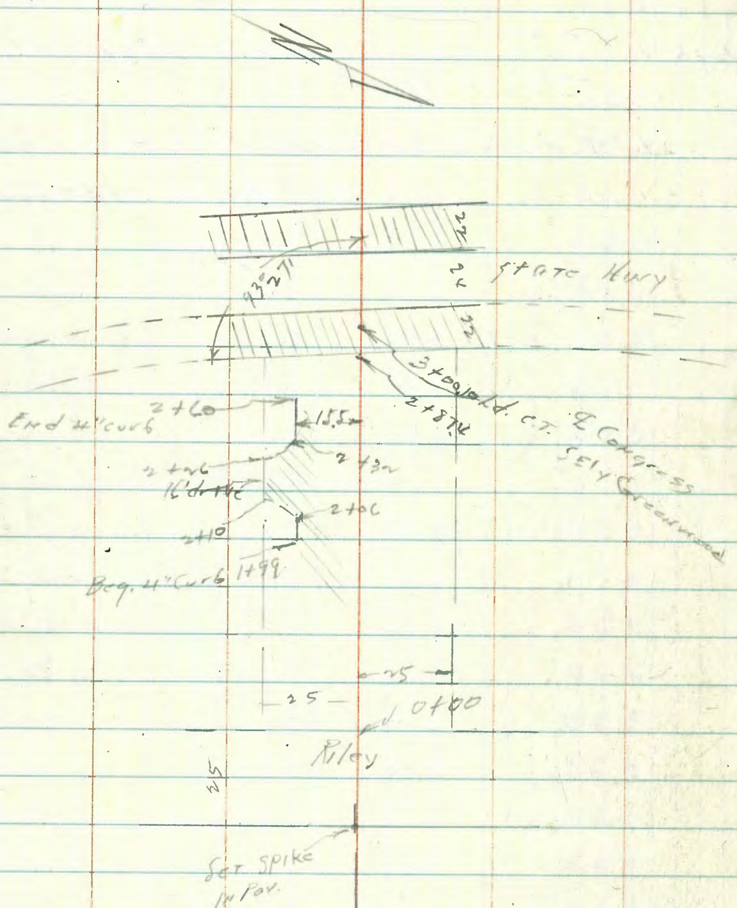
check to NW BP Pac. Beach Drive and Gresham 7.62 = 21.09

27.19 derive from Walker USC&G

21.10 " " U.S. from Old Town

Indexed
C.S.K.

Levels on Pav. on
Congress, Pacific to Greenwood
W.E.M.
1-31-44



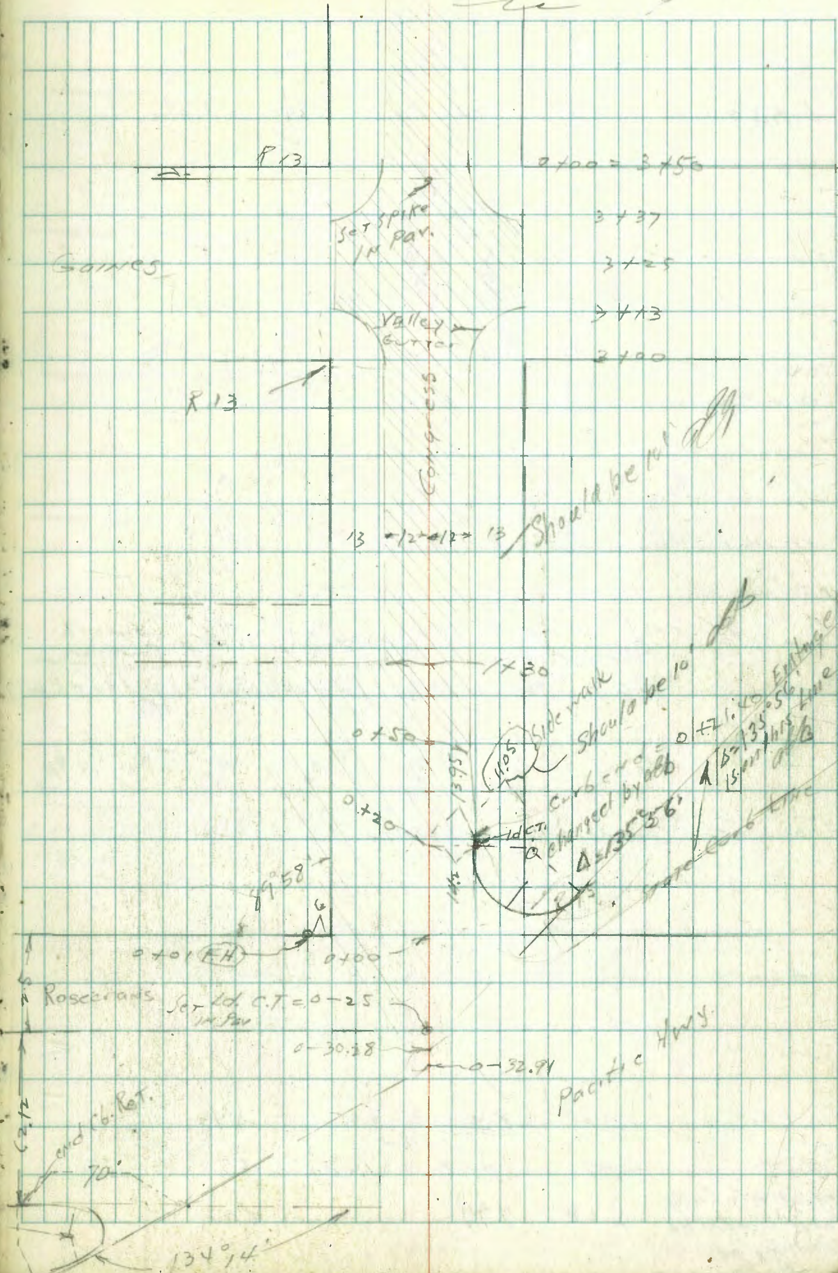
Note! the Boss will be interested on the Sdwalk width

12.88 Sidewalk

Double Compound Return

Curb Line Sty

Riley same as Gaines
except no Valley gutter



Pav Levels on Congress

1+30 end Extra Pav on Lt. = Ely 20' alley

1+00

Reduced 2/2/44 CBH

0+50

0+21.x end curb Ret. to Rt.

Note! 0+0 to 1+30 on Sly side = Comm'l. Gutter

0+00 Nwly Rosecrans (and diagonal cb Ret to cb Ret)

0-05 Comm'l. Gutter to S/y

0-25

T.P.	4.77	8.49	3.96	4.72	
T.P.	4.97	10.68	4.28	5.71	
BMBF Wly Curb Pacific approx 800' Sly of Rosecrans	5.68	9.99		4.31	

Swly = Lt ℄ Rt

Lt	Lt	Lt	Lt	℄	Rt	Rt	Rt	Rt
		3.70 / 4.79 / 25	3.31 / 5.18 / 12	3.55 / 4.94	3.32 / 5.17 / 12			
		3.79 / 4.70 / 25	3.39 / 5.10 / 12	3.66 / 4.83	3.37 / 5.12 / 12			
		4.06 / 4.43 / 25	3.54 / 4.95 / 12	3.83 / 4.66	3.55 / 4.94 / 12			
		4.17 / 4.32 / 25	3.73 / 4.76 / 12	3.82 / 4.63	3.71 / 4.78 / 13.95 / 94T	4.28 / 4.21 / 13.95		
		3.84 / 4.65 / 25	3.58 / 4.71 / 12	3.72 / 4.77	3.82 / 4.67 / 12	3.90 / 4.59 / 25	3.88 / 4.61 / 35 / 94T	4.53 / 3.96 / 35 / cb
3.94 / 4.55 / 120	3.72 / 4.77 / 70	3.64 / 4.85 / 25	3.59 / 4.90 / 12	3.69 / 4.80	3.81 / 4.68 / 12	3.91 / 4.58 / 25		
		4.35 / 4.14 / 25		4.31 / 4.18	4.21 / 4.27 / 25			

Top end Ret.

Pt of 90° Plot this

8.49

Congress

3+13

3+05 Valley Quizzen

T.P. 5.43 8.16 5.76 2.73

3+00 Ely Gaines

2+95

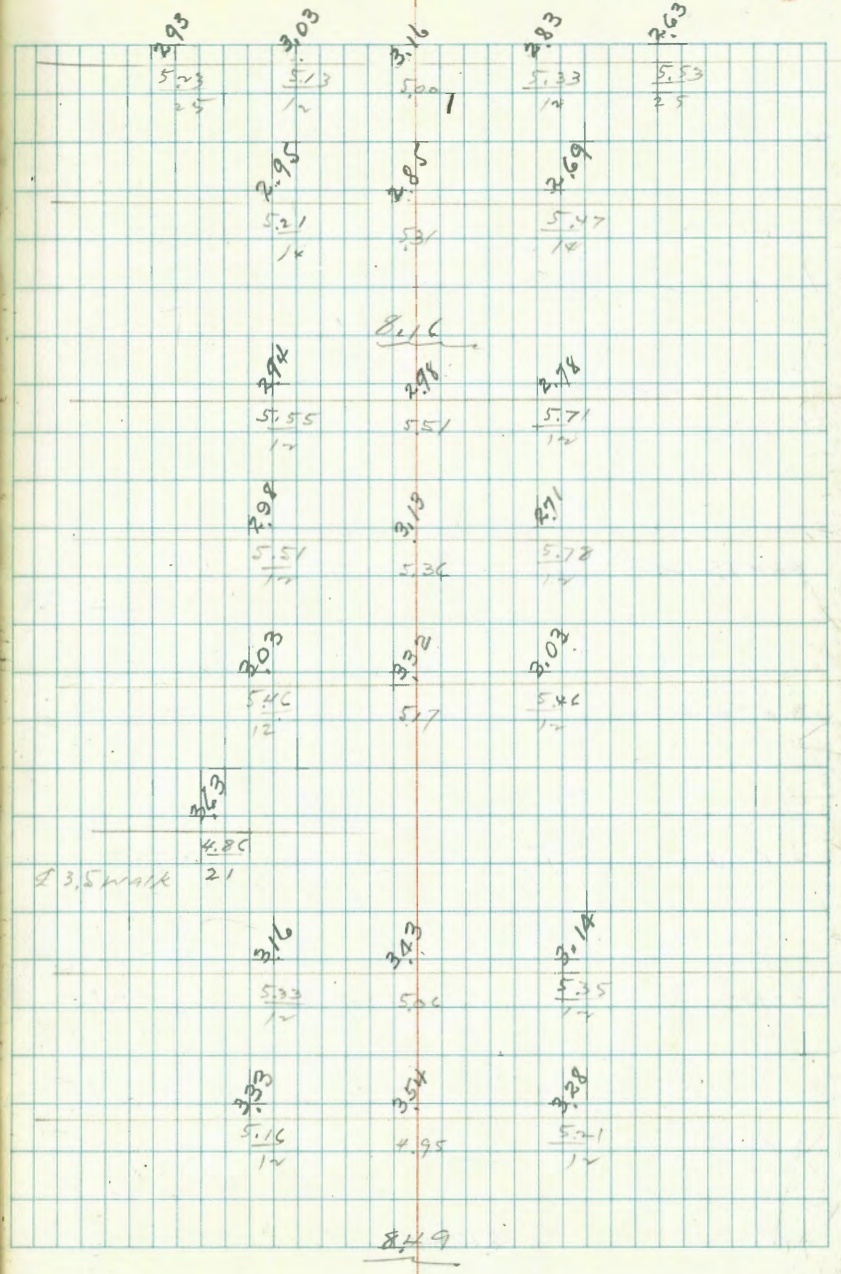
2+50

2+05

2+00

1+50 : Wly alley

8.49



Congress

Station		Lt	℄	Rt	
✓		3.76 / 4.40 / 12	4.04 / 4.12	3.74 / 4.42 / 12	
+50		3.52 / 4.64 / 12	3.80 / 4.36	3.56 / 4.60 / 12	
1		3.42 / 4.74 / 12	3.68 / 4.48	3.40 / 4.76 / 12	
0+47.5 ←	3.66 / 4.53 / 25 (4.35 Walk)	3.22 / 4.94 / 12	3.41 / 4.75	3.18 / 4.98 / 12	
3+50 = 0+00 Wly Gaines		3.08 / 5.08 / 12	3.28 / 4.88	3.00 / 5.16 / 12	
3+37	2.89 / 5.27 / 25	3.00 / 5.16 / 12	5.44	3.01 / 5.15 / 12	2.36 / 5.80 / 25
3+25 ℄ Gaines	2.82 / 5.34 / 25	2.97 / 5.19 / 12	3.22 / 4.94 MH Rim	2.87 / 5.29 / 12	2.32 / 5.84 / 25
3+15	2.92 / 5.24 / 25	3.04 / 5.12 / 12	3.18 / 4.98	2.83 / 5.33 / 12	2.59 / 5.57 / 25

8.16

8.16

Congress

0+50

T.P. 4.88 10.17 2.87 5.29

3+50 = 0+00 W/y Riley

3+37

3+25 E Riley

3+13

3+00 Ely Riley

2+50

2+15

8.16

Lt ℄ Rt 45

4.44 4.41 4.42
5.73 5.46 5.75
1.2 1.2

10.17

4.29 4.33 4.38
3.87 3.63 3.88
1.2 1.2

4.12 4.19 4.26 4.35 4.19
4.04 3.97 3.70 3.71 3.97
2.5 1.2 1.2 2.5

4.10 4.17 4.39 4.38 4.05
4.06 3.99 3.77 3.83 4.11
2.5 1.2 2.5

3.95 4.10 4.24 4.14 3.91
4.21 4.06 3.87 4.03 4.25
2.5 1.2 1.2 2.5

4.03 4.28 4.01
4.13 3.88 4.15
1.2 1.2

3.96 4.16 3.89
4.24 4.00 4.17
1.2

4.11
3.65
2.5.5

℄ 4.5
Tile walk
Sett'n Com.

8.16

Congress

check to R.R. Rail Cor.	Sly Hancock Greenwood	3.19	4.52	4.50	
T.P.	5.32	7.71	9.07	2.39	
T.P.	4.46	11.26	3.17	7.00	

2 + 87.40 ℄ Sta on Ely edge of Ely 22' Lane of State Job

2 + 65

2 + 50

2 + 16 Session on ℄ drive

2

150

1

10.17

46

Lt 1 ℄ Rt

N.G.

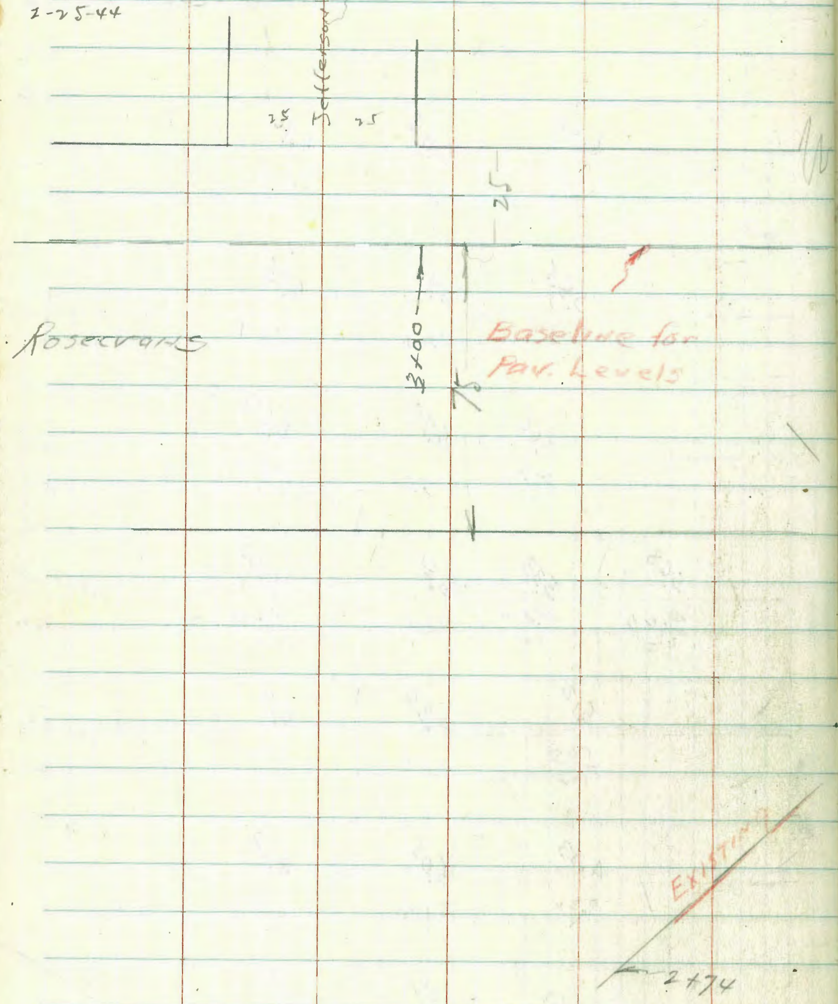
This B.M. has been knocked over about (" 3)

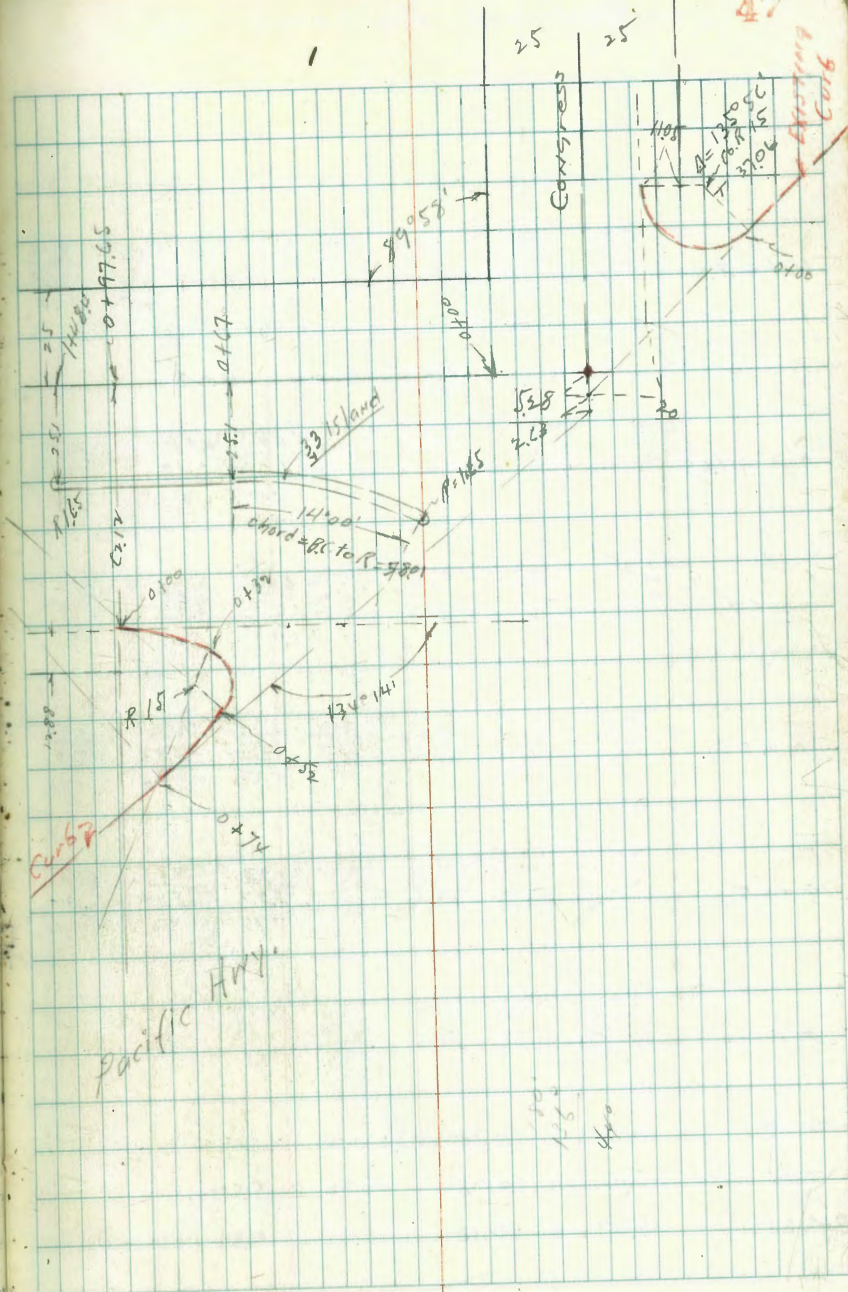
Lt		℄	Rt
	6.84 / 3.33 / 25	6.86 / 3.31	6.90 / 3.27 / 25
	5.85 / 4.32 / 12	5.94 / 4.23	5.95 / 4.22 / 12
	5.66 / 4.51 / 12	5.77 / 4.40	5.62 / 4.55 / 12
5.68 / 4.49 / 25	5.33 / 4.84 / 12	5.50 / 4.67	5.25 / 4.92 / 12
	5.12 / 5.05 / 12	5.36 / 4.81	5.13 / 5.04 / 12
	4.83 / 5.34	5.05 / 5.12	4.82 / 5.35 / 12
	4.61 / 5.56 / 12	4.92 / 5.25	4.65 / 5.52 / 12

10.17

C. Moore
Smi Mgr.
W.E.M.
Beggs
2-25-44

Levels on Rosecrans
at Pacific Hwy.





Rosecrans Pav. Levels

1 + 48.4	Sly end Curbed Island on 1.65 R					4.28 / 5.51 / 52 (edge oil pav.)	5.13 / 5.17 / 37	
T.P. Top cb. Nwly Cor. end	6.02	10.30	6.02	4.28				
0 + 97.65				4.64 / 5.66 / 62 gut	4.85 / 5.45 / 50	5.30 / 5.00 / 27.1		
0 + 67				4.64 / 5.66 / 58	4.73 / 5.57 / 50	5.15 / 5.15 / 27.1		
0 + 50				4.65 / 5.65 / 60	4.77 / 5.53 / 50	5.11 / 5.19 / 27.7		
0 + 25				4.73 / 5.57 / 75	4.86 / 5.44 / 50	5.07 / 5.23 / 31.2		
0 + 00	Sly Congress							
T.P.	4.74	10.30	5.22	5.56				
T.P.	5.16	10.78	11.56	5.62				
B.M. B.P.	5.87	10.18		4.31	Wly cb.			

Lt. B.L. Rt. = Wly

5.23 / 5.07 / 27.1 — 5.74 / 4.56 / 26.8 — 5.74 / 4.56 / 23.6 — 5.31 / 4.99 / 23.4 — 5.08 / 5.22 / 15 — 4.40 / 5.90 — 4.02 / 6.28 / 19 — 4.20 / 6.10 / 25 (cb)

10.30

5.73 / 4.57 / 26.8 — 5.75 / 4.55 / 23.6 — 5.33 / 4.97 / 23.4 — 5.21 / 5.09 / 15 — 4.75 / 5.55 — 3.98 / 6.32 / 19 — 4.28 / 6.02 / 25 (cb)

5.58 / 4.72 / 26.8 — 5.62 / 4.68 / 23.6 — 5.19 / 5.11 / 23.4 — 5.11 / 5.19 / 15 — 4.70 / 5.60 — 3.90 / 6.40 / 21 — 4.16 / 6.14 / 25 (cb)

Concrete gut along here

5.50 / 4.80 / 27.5 cb — 5.56 / 4.74 / 24.7 cb — 5.12 / 5.18 / 23.9 — 5.03 / 5.27 / 15 — 4.63 / 5.68 — 3.82 / 6.48 / 22 — 3.95 / 6.35 / 25

5.42 / 4.88 / 30.9 — 5.42 / 4.88 / 27.3 cb — 5.05 / 5.25 / 27 — 4.75 / 5.55 / 15 — 4.42 / 5.88 — 3.67 / 6.63 / 23 — 3.78 / 6.52 / 25 (cb Island)

4.84 / 5.46 / 38 — 4.67 / 5.63 / 21 — 4.35 / 5.95 — 3.66 / 6.64 / 21 — 3.83 / 6.47 / 25

10.30

on Pac. Hwy approx 800' S. of Rosecrans

Rosecrans

3 N/y of Jefferson St

+50

√

10.30 Fwd

Lt | BL | Rt

4.65 / 5.65 / 49	4.90 / 5.40 / 35	4.97 / 5.33 / 25	4.66 / 5.64 / 15	3.88 / 6.42	3.38 / 6.92 / 18	3.74 / 6.56 / 25
4.61 / 5.69 / 46	4.92 / 5.38 / 37	4.97 / 5.33 / 25	4.67 / 5.63 / 15	4.08 / 6.22	3.73 / 6.57 / 18	4.00 / 6.30 / 25
4.76 / 5.54 / 50	5.07 / 5.23 / 37	5.08 / 5.22 / 25	4.82 / 5.48 / 15	4.31 / 5.99	3.88 / 6.42 / 17	4.05 / 6.25 / 25

Conc'd gut

+ Edge of Pav

℄ Rosecrans

10.30

Levels on SWly Compounded Return Rac. & Reference

10.30 End

0+00 = C6 end on Reference = BC

C6 in drive 4.76 / 5.54

out 4.63 / 5.47

0+16

C6 in drive 4.77 / 5.53

out 4.68 / 5.47

0+32 PCC

C6 in drive 4.92 / 5.38

out 4.81 / 5.49

0+48

Top C6 5.48 / 4.82

out 4.79 / 5.51

0+52 PCC

Top C6 5.52 / 4.78

out 4.86 / 5.44

0+63

Top C6 5.52 / 4.78

out 4.90 / 5.40

0+74 EC

C6 in drive 5.06 / 5.24

out 4.93 / 5.37

1+14

Top C6 5.36 / 4.54

out 5.08 / 5.32

1+74

Top C6 5.82 / 4.48

out 5.14 / 5.16

2+24

C6 in drive 5.18 / 4.11

out 5.04 / 5.32

2+74

Top C6 5.21 / 4.59

out 5.06 / 5.24

N.W'ly Ret. Pac. & Congress

10.30 Fnd.

Return Pl. on pav.		4.06 / 6.24
	Middle Ret.	
cb		4.45 / 5.85
gut		3.88 / 6.42
	E.C. Ret. 0+00	
cb		4.53 / 5.77
gut		3.90 / 6.40
	0+52	
cb		4.30 / 6.00
gut		3.61 / 6.69
	1+00	
cb		4.05 / 6.25
gut		3.40 / 6.90
	1+57	
cb		3.83 / 6.47
gut		3.10 / 7.20
	2+00	
cb		3.50 / 6.80
gut		2.85 / 7.45

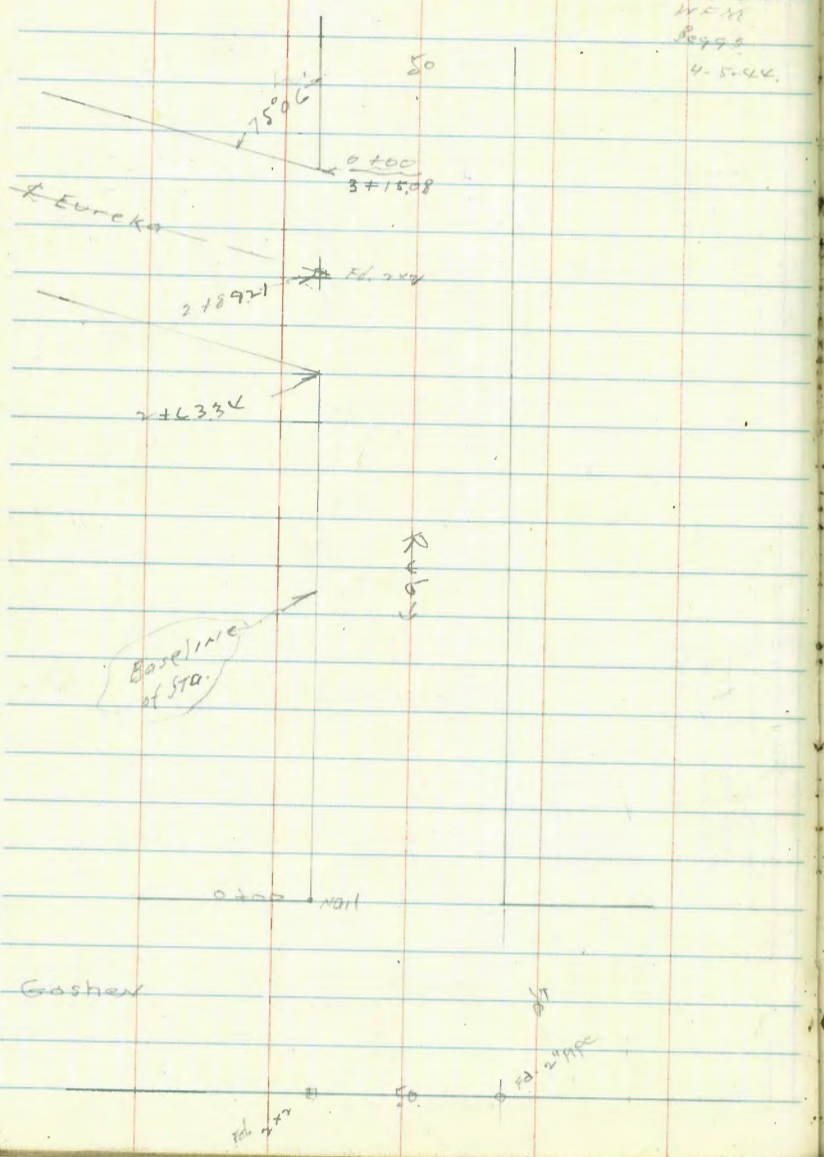
10.30

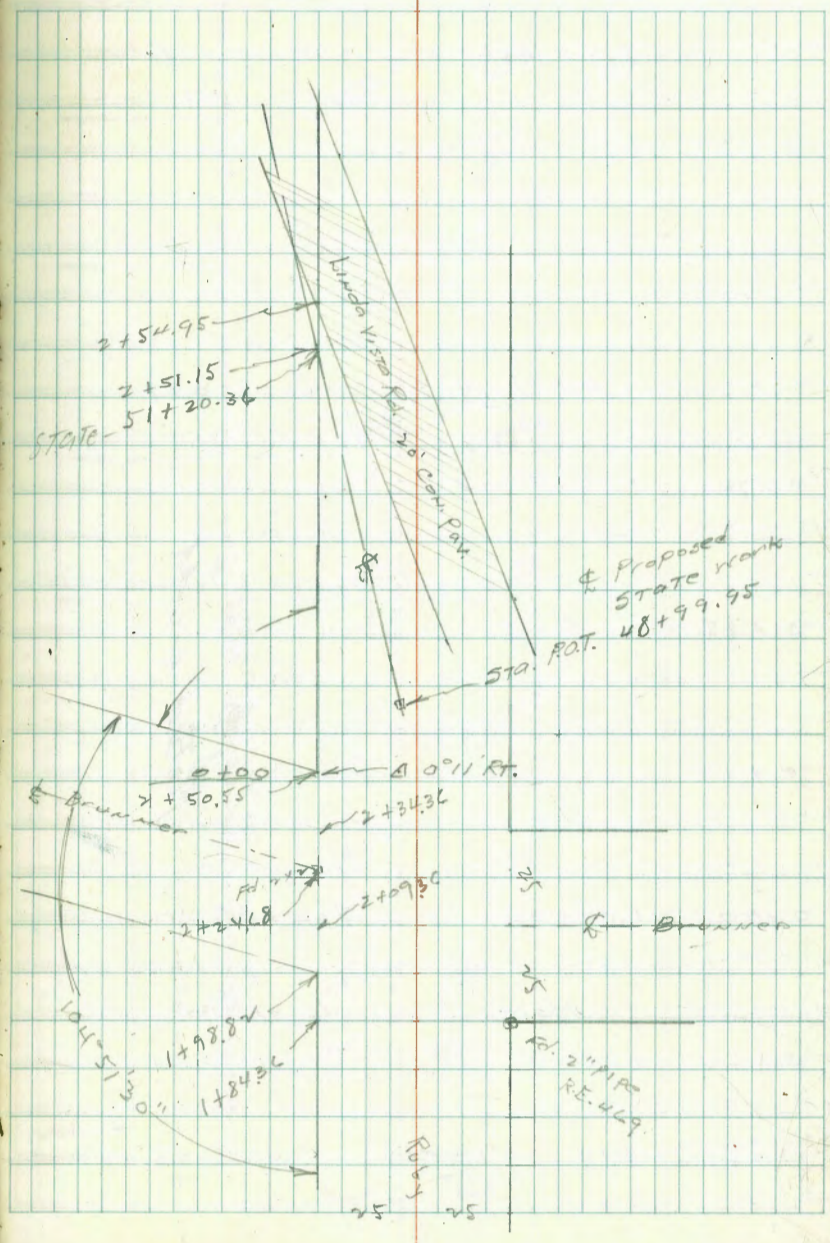
E'ly Gaines &

E'ly Ret. at Intersec. of Pac. Hwy

Top cb. & cb inlet	2.50 / 7.80
gut grating	1.42 / 8.83

Xsec of Ruby ST.
Goshen to Linda Vista Rd.





Roby

T.P.	0.07	161.22	12.92	161.15	
1+35					
1+00					
T.P.	0.64	174.07	12.79	173.43	
0+70					
0+35					
0+12					
0+00	Wly Goshen St.		Top of Cut		
0-6					
B.M. NE Cor 2" Pipe	11.17	186.22		175.05	Goshen Mildred

Note! Sections at 90°
S.L. = Baseline

Profile Never Plotted 4-6-44

LT. S.L. RT

S.L.			
164.3 / 9.8	162.4 / 11.7 / 25	160.3 / 13.8 / 50	158.5 / 15.6 / 70
168.9 / 5.2	168.0 / 6.1 / 25	165.9 / 8.2 / 50	
174.1 / 12.1	172.6 / 13.6 / 25	172.0 / 14.2 / 50	
179.4 / 6.8	178.8 / 7.4 / 25	177.4 / 8.8 / 50	
184.0 / 2.2	183.1 / 3.1 / 25	181.0 / 5.2 / 50	
185.0 / 1.2	184.0 / 2.2 / 25	182.2 / 4.0 / 50	
180.5 / 5.7	179.5 / 6.7 / 25	178.6 / 7.6 / 50	

174.07

186.22

Ruby

0+34

0+25

3+15.08 = 0+00 W/y Eureka

T.P. 0.24 136.38 12.81 136.14

2+89.21 E Eureka

2+63.24 Ely Eureka

T.P. 0.46 148.95 12.73 148.49

2+35

2+00

1+60

161.22

LT 130.6 130.1 125.9 123.4 RT. 118.5 127.7

5.8 6.3/10 10.5/25 13.0/35 17.9/50 8.7/65

132.2 131.7 128.1 124.2 119.8 125.2

4.2 4.7/13 8.3/25 12.0/50 16.6/55 8.2/70

138.5 137.7 133.1 129.0 128.0 129.9 128.7

+2.1 +0.8/8 3.3/25 7.4/50 8.4/63 13.5/68 7.7/78

136.38

142.3 140.4 134.6 132.5 127.2 131.3

dry ditch 6.66 8.6/25 14.4/50 16.5/65 21.4/80 17.7/90

147.2 145.7 143.2 139.8 139.3 130.5 139.8

4.8 3.7/25 5.8/40 9.2/50 15.7/70 18.5/75 15.7/85

148.95

150.8 149.2 144.9 138.6

10.4 12.0/25 16.3/50 22.6/75

155.4 153.5 150.9 145.1

5.8 7.7/25 10.9/50 16.1/70

159.7 158.4 154.0 153.7

1.5 2.8/25 5.2/50 7.5/70

161.22

Ruby

	109.2	104.7	104.9	105.2
1+20	17.0	21.5	21.3	21.0
	35	20	20	20
		110.1	110.7	105.8
1+16		16.1	15.5	20.4
		35	20	18
		115.9	115.6	108.9
0+93		10.3	10.6	17.3
		25	17	13
		117.0	117.0	113.9
0+88		9.2	9.2	12.3
		25	17	13
0+80				
0+63				
T.P.	0.64	124.15	10.87	125.51
0+50				
0+40				
		136.38		

	LT		SH			RT	
	111.2	109.9	113.2	116.4	121.4	126.5	128.0
	15.0	16.3	13.0	9.8	4.8	+0.3	+1.8
	13	7		6	25	50	60
	110.1	109.0	115.0		121.1	126.8	128.2
	16.1	17.2	11.2		5.1	+0.6	+2.0
	13	7			25	50	60
	112.3	112.9	114.2		117.0	121.6	127.0	129.5
	13.9	13.3	12.0		9.2	4.6	+0.8	+3.3
	7				10	25	50	60
	112.4	110.9	111.0		111.7	121.3	126.9	129.3
	13.8	15.2	15.2		14.5	4.9	+0.7	+3.1
	7	5			10	25	50	60
	118.7	116.0	115.6	112.9	118.0	124.3	127.3	129.2
	7.5	10.2	10.6	13.3	8.2	3.9	+1.1	+3.0
	15		12	15	25	35	50	60
	122.9	121.3		119.4	114.2	120.8	126.7	128.6
	3.3	4.9		6.8	11.9	5.4	+0.5	+2.4
	10			18	25	35	50	60
	125.9	125.5	121.8	124.5	119.9	119.9	120.5	125.2	128.6
	10.3	10.9	15.4	10.5	20.5	15.9	11.2	7.8
	10		25	37	34	40	50	60
		128.9	127.6	124.2	122.9	118.1	123.5	129.3
		7.5	8.8	12.2	13.5	18.3	12.9	7.1
			12	25	30	41	50	65
					131.38			

Ruby

Δ = 0° 11' Rt. to Sisson Hub at Russ St.

2+50.55 = 0+00 Wly Brunner to South

2+34.36

2+24.68 ℄ Brunner to South

2+09.36

1+98.82 Ely Brunner to South

1+84.36

T.P. 11.89 137.87 0.17 125.98

1+50

1+25 103.8 22.4/37 104.9 21.3/25

126.15

Lt		Sh.	Rt		
		132.8 / 5.1	133.8 / 4.1 / 25	135.1 / 2.8 / 40	136.6 / 1.3 / 50
		132.4 / 5.5	133.7 / 4.2 / 25	134.6 / 3.3 / 30	135.9 / 2.0 / 50
		132.2 / 5.7	133.7 / 4.2 / 25	135.5 / 2.4 / 50	
		130.6 / 7.3	132.2 / 5.7 / 25	133.8 / 4.1 / 40	135.5 / 2.4 / 50
129.0 / 8.9 / 10		129.5 / 8.4	131.2 / 6.7 / 25	133.4 / 4.5 / 50	
126.4 / 11.5 / 10		127.4 / 10.5	129.8 / 8.1 / 25	132.5 / 5.4 / 50	
			137.87		
117.8 / 8.4 / 30		121.1 / 5.1	125.2 / 1.0 / 25	129.2 / +3.0 / 50	131.2 / +5.0 / 60
112.0 / 14.2 / 17		116.4 / 9.8	121.3 / 4.5 / 25	126.9 / +0.7 / 50	128.2 / +2.0 / 60

126.15

		Ruby			
1+35					
1+10					
T.P.	1.22	129.91	11.25	128.69	
0+86					
0+80					
0+67					
0+50					
Check to B.M.	Top F.H. Linda Vista Rd. & Brunner		1.16	138.78	138.87 / 0.09
T.P.	7.90	139.94	5.83	132.04	
0+35					

137.87

Lt S.L. Rt.

114.5 15.4/20 — 120.4 9.5/8 — 121.9 8.0 — 124.8 5.1/22 — 126.1 3.8/25 — 127.2 2.7/30 — 126.5 3.4/32 — 127.3 2.6/44.2 edge pav.

120.7 9.2/23 — 117.4 12.5/14 — 122.3 7.6 — 127.2 2.7/25 — 129.5 0.4/43 — 128.0 1.9/45 — 128.7 1.2/50 — 129.0 0.9/54.4 pav. edge

129.91

120.8 19.1/15 — 120.5 19.4/7 — 123.7 16.2 — 126.9 13.0/15 — 127.9 12.0/25 — 130.4 9.5/40 — 130.7 9.2/50

123.1 16.8/13 — 120.9 19.0/7 — 122.4 17.5 — 127.5 12.4/15 — 129.4 10.5/25 — 131.8 8.1/40 — 133.6 6.3/50

126.2 13.7/11 — 124.2 15.7/8 — 124.2 15.7 — 124.1 15.8/5 — 126.9 13.0/10 — 130.9 9.0/25 — 134.0 5.9/50

128.7 11.2 — 126.7 13.2/12 — 131.6 8.3/25 — 135.3 4.6/50

139.94

132.7 7.2 — 128.9 9.0/12 — 130.0 7.9/25 — 135.5 4.4/50

137.87

Ruby

1+54.95

2+25

2+00

1+84

1+60

129.91

53

Lt. Sh. Rt.

		119.8				
		10.1	edge Pav.			
116.2	119.1	120.8		121.7		
13.7 / 20	10.8 / 10	9.1		8.2 / 11.5		edge Pav.
116.1		120.3	122.9	123.1	123.3	
13.8 / 20		9.6	7.0 / 10	6.8 / 10	6.6 / 20.8	edge Pav.
116.8		120.7	123.4	123.3	124.3	
13.1 / 20		9.2	6.5 / 12	6.6 / 17	5.6 / 25.6	edge Pav.
117.9		121.0	125.4	124.5	124.7	124.6
12.0 / 18		8.9	4.5 / 20	5.4 / 23	5.2 / 25	5.3 / 34.6 edge Pav.

129.91

Cross Section Ash St.
50' West of W.L. 7th St to E.L. 7th St.

Indexed
C.S.K.

0+77					
TP	6.24	136.90	3.36	130.66	
0+64 = N Curb Line					
0+50 = W.L. 7th St					
0+25					
0+00 = 50' W of West Line of 7th St					
TP	13.97	134.02	0.45	121.05	
TP	12.93	121.50	0.96	108.57	
BM	12.59	109.53		96.94	S.W. B.P. Ash + 6th St.

Reduced Plot on #60
Also Section 1 large Scale
5-10-44

May 9-44
Sisson
Bliss
Osborne

Lt = N ℄ Rt = S

133.21 — 3.69 / 40
132.62 — 4.28 / 26
132.03 — 4.87 / 13
131.41 — 5.49
130.85 — 6.05 / 13
130.28 — 6.62 / 26
129.64 — 7.26 / 40

136.90

132.13 — 1.89 / 40 = Cb
131.81 — 2.21 / 40 Gutter
131.40 — 2.62 / 26
130.83 — 3.19 / 13
130.16 — 3.86
129.51 — 4.51 / 13
128.80 — 5.22 / 26
128.37 — 5.65 / 40 Gutter
128.97 — 5.05 / 40 = Cb

132.24 — 1.78 / 26 = Cb
131.39 — 2.63 / 26 Gutter
130.82 — 3.20 / 13
130.24 — 3.78
129.28 — 4.74 / 13
128.49 — 5.53 / 26 Gutter
128.88 — 5.14 / 26 = Cb

128.45 — 5.57 / 26
127.67 — 6.35 / 26
127.52 — 6.50 / 13
126.97 — 7.05
126.10 — 7.92 / 13
124.95 — 9.07 / 26
125.30 — 8.72 / 26

124.96 — 9.06 / 26 = Cb
124.10 — 9.92 / 26 Gutter
124.02 — 10.00 / 13
123.48 — 10.54
122.64 — 11.38 / 13
121.40 — 12.62 / 26 Gutter
121.77 — 12.25 / 26 Top Curb

134.02

45th St

BM			7.81	129.09	45th+7th
1+50 = E.L. of 7th St.					
1+16 = E Cb of 7th St					
1+03					
0+90 = ℄ 7th St.					
		13690			

Lt. ℄ Rt.

135.42	134.57	134.25	133.71		132.70	131.63	131.83	
1.48 / 26 = Cb	2.33 / 26 = Gutter	2.65 / 13	3.19		4.20 / 13	5.27 / 26 Gutter	5.07 / 26 = Cb	
135.32	134.57	134.11	133.47	132.90	132.17	131.45	131.10	131.78
1.58 / 40 = Cb	2.33 / 40 = Gutter	2.79 / 26	3.43 / 13	4.00	4.73 / 13	5.45 / 26	5.80 / 40 Gutter	5.12 / 40 = Cb
134.63	134.04	133.45	132.91		132.20	131.70	131.02	
2.27 / 40	2.86 / 26	3.45 / 13	3.99		4.70 / 13	5.20 / 26	5.88 / 40	
134.17	133.56	132.95	132.40		131.83	131.42	130.60	
2.73 / 40	3.34 / 26	3.95 / 13	4.50		5.07 / 13	5.50 / 26	6.30 / 40	

136.90

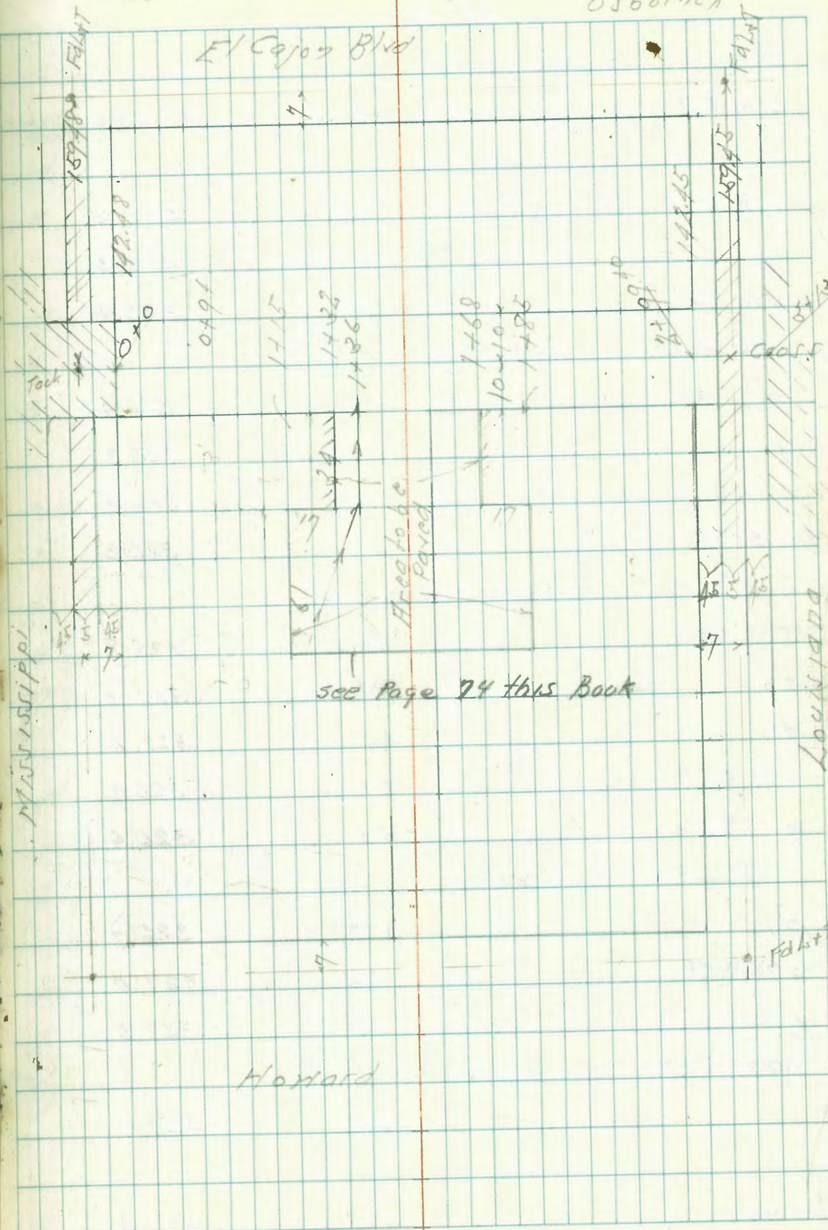
Cross Section East & West Alley
Block 127 University Heights
From Mississippi to Louisiana
Between El Cajon Blvd & Howard

BM	6.42	332.41		325.99	N.E.B.P. El Cajon & Louisiana
	0-14' E Cb of Mississippi				
N	on Paving		12.22	320.19	
℄	" "		12.39	320.02	
S			12.44	319.97	
	0+0 : E.L. Mississippi				
S	Top Cb		11.62	320.79	
S	Gutter on Pav.		11.86	320.55	
℄	" "		12.01	320.40	
N	Gutter "		11.65	320.75	
N	Top Cb		11.31	321.10	
	0+02'				
N			10.7	321.7	
℄			11.3	321.1	
S			10.8	321.6	
	0+18				
S			9.3	323.1	
℄			9.4	323.0	
N			9.2	323.2	
	0+50				
N			8.5	323.9	
℄			8.5	323.9	
S			8.3	324.1	

Reduced & Plotted Profile # 2985
6-17-1944 CBH

Indexed
C.S.K.
Check Heade Grade Page 74

June 16-44
Sisson
Bliss
Osborne



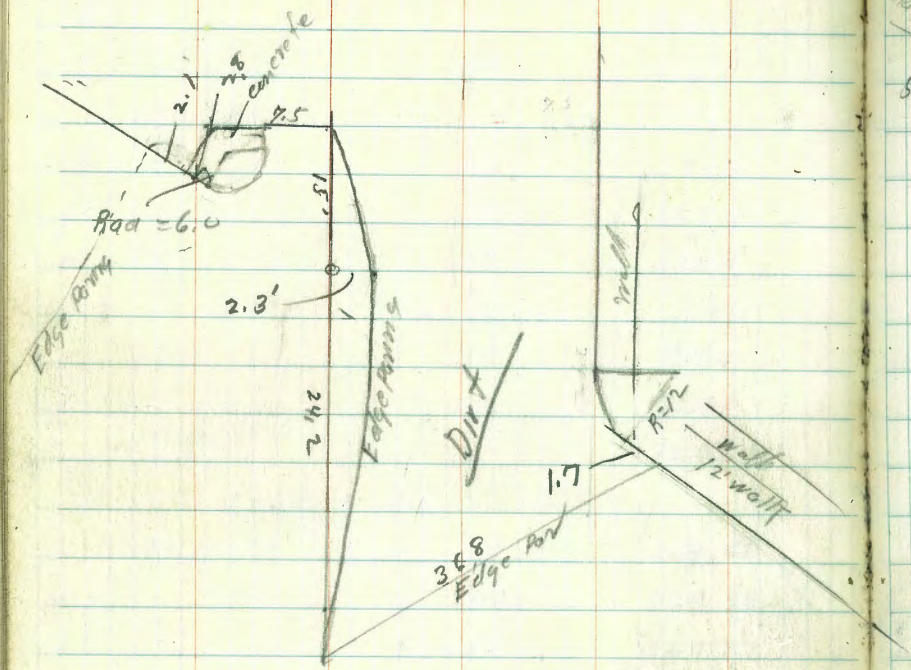
	332.41			
	0+94			
S + 53' = W'ly Garage Under Const.			5.18	327.23 on Forms = Floor
	1+0			
S			7.2	325.2
℄			7.0	325.4
N			7.0	325.4
	1+25			
N			6.0	326.4
℄			6.1	326.3
S			5.9	326.5
+50			6.2	326.2
	1+33 = ℄ Local Hump			
S			3.6	328.8
+5			4.1	328.3
℄			5.2	327.2
+2			5.7	326.7
N			5.8	326.6
	1+40			
N			5.7	326.7
+7			5.4	327.0
℄			4.9	327.5
+9.7 = S'ly Power Pole				
S			4.5	327.9
	1+50			
-50			5.0	327.4
		332.41		
S			4.8	327.6
+7			4.9	327.5
℄			5.3	327.1
N			5.5	326.9
	1+60			
N			5.0	327.4
℄			4.8	327.6
S			4.9	327.5
	1+80			
-50			4.3	328.1
S			4.0	328.4
℄			4.0	328.4
N			4.3	328.1
TP	7.30	(335.74)	3.97	328.44
		2+0		
N			7.0	328.7
℄			7.0	328.7
S			7.0	328.7
		2+25		
S			5.9	329.8
℄			6.1	329.6
N			6.4	329.3

		335.74			
	2+50				
N			5.6	330.1	
L			5.4	330.3	
S			5.2	330.5	
	2+85				
S			4.7	331.0	
L			4.8	330.9	
N			4.8	330.9	
	2+99.40 = W/L Louisiana				
N			5.8	329.9	
L			5.9	329.8	
S			6.1	329.6	
	3+08.90 = W/L Conc Walk				
S	on Walk		6.32	329.42	
L	" "		6.42	329.32	
N	" "		6.52	329.22	
	3+18.4 = W CL of Louisiana				
N	Top Cb		6.72	329.02	
N	Gutter on Pav		7.32	328.42	
L	" " "		7.22	328.52	
S	Top Cb		6.55	329.19	
S	Gutter on Pav.		7.13	328.62	
BM			9.73	326.01	MAG Bolt E/Cajon + Louisiana 325.99

Cross Section 38th St.
Edna Place to Ward Road

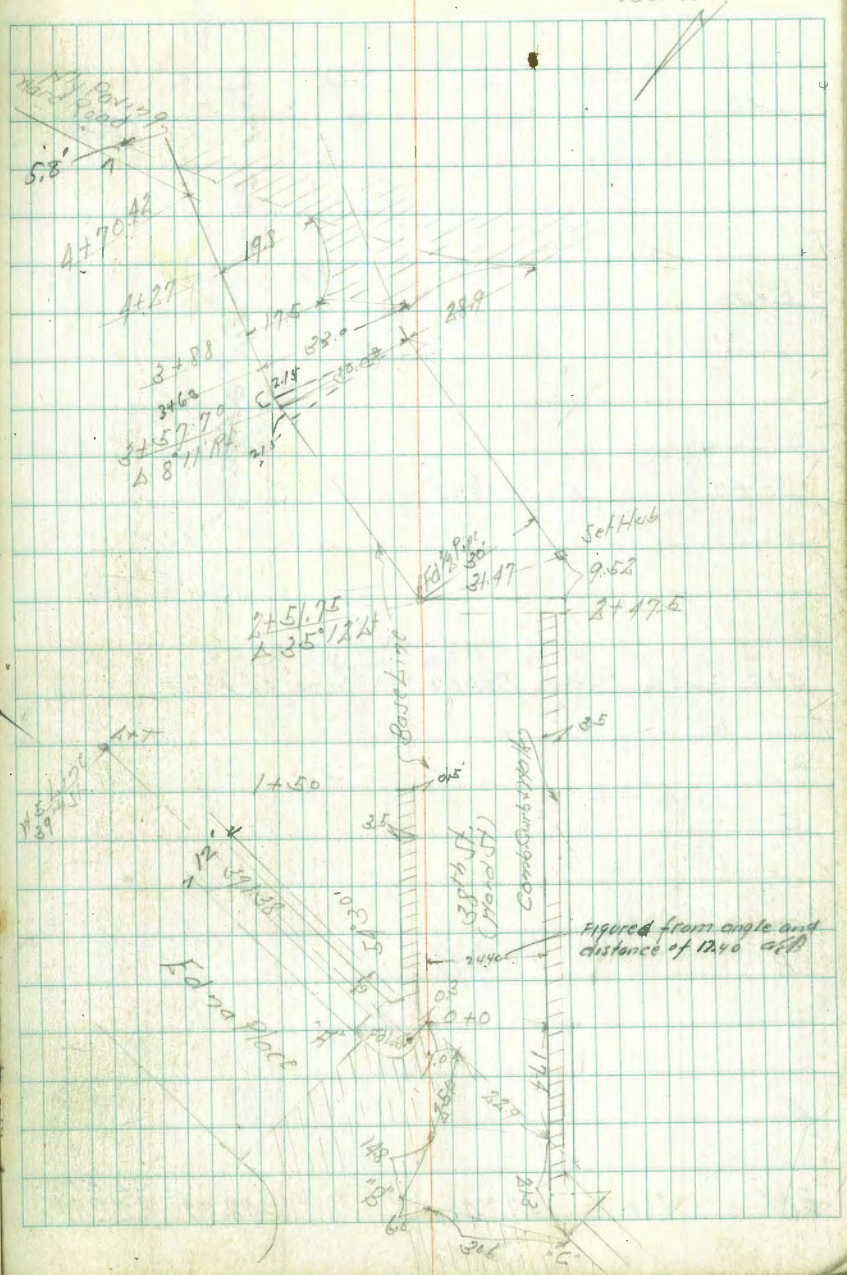
Levels Next Page

Indexed
C.S.K.



July 12 44
Sisson
Bliss
Osborne

64



Yardage Fig. 7-28-1944

Base Line = F

Sta.										
1+0				367.10 / 5.30 / 0.35 = Cb	366.5 / 5.9	366.7 / 5.7 / 12	366.3 / 6.1 / 24.5	367.07 / 5.33 / 24.5 = Cb		
0+50				367.93 / 4.47 / 0.3	367.2 / 5.2	367.4 / 5.0 / 12	367.0 / 5.4 / 24.4	367.81 / 4.59 / 24.4		
0+0	At Right Angle						368.3 / 4.1 / 12	367.7 / 4.7 / 24.4	368.53 / 3.87 / 24.4 = Cb	
0+0 = S.L. Edna Taken on Line of Edna				368.77 / 3.63 / 0.3 = Cb	367.85 / 4.55 / on Bx	368.41 / 3.99 / 7.8	368.40 / 4.00 / 16	367.96 / 4.44 / 29.9 = Gutter	368.85 / 3.55 / 29.9 = Cb	
C								368.26 / 4.14 = Gutter	368.90 / 3.50 = Cb Top	
B							368.59 / 3.81 / on Bx			
A				368.78 / 3.62 / Top Cb	368.17 / 4.23 / Gutter					
BM	3.63	372.40	368.77	SERP Edna at Mountain View	372.40					

2+81.2	= ℄ 3' Walk Conc. on Lt				
2+67.5					
TP	2.04	366.33	8.11	364.29	on 1/2 Pipe 2+51.75 Base Line
2+51.75	= ℄ 35° 12 Lt		Taken on Spht		
2+47.5	= Sly Cb + Walk on West				
2+0					
1+50	= End Cb + Walk on East				

37240

B

Rt = W

365.06 / 1.27 — 0.2 = Top Conc Strip; 363.41 / 2.92 — 2.8 = Bot Step; 363.1 / 15; 362.8 / 25; 363.4 / 29; 363.3 / 30; 363.6 / 40

365.25 / 1.08 — Top 5" Rock Wall; 363.7 / 2.6 / 0.5; 364.2 / 2.1 / 15; 363.6 / 2.7 / 26; 364.5 / 1.8 / 30; 365.3 / 1.0 / 34; 364.4 / 1.9 / 40

366.33

364.6 / 7.8; 364.5 / 7.7 / 16; 364.4 / 8.0 / 22; 364.6 / 7.8 / 31.5

366.80 / 5.60 — 0.1 = Sly Masonry Wall Top; 364.6 / 7.8; 365.1 / 7.3 / 12; 364.7 / 7.7 / 24.4; 364.85 / 7.55 / 24.4 = Sly Cb + Walk

367.39 / 4.81 — 0.3 = Nly Masonry Wall Top; 365.7 / 6.7; 365.7 / 6.7 / 12; 365.0 / 7.4 / 24.4; 365.07 / 7.33 / 24.4 = Cb in Drive

366.38 / 6.02 — 0 = ℄; 366.0 / 6.4; 366.3 / 6.1 / 12; 365.7 / 6.7 / 24.4; 366.35 / 6.05 / 24.4 = Cb

37240

B Rt

3+63

355.5 / 6.8 — 358.4 / 6.9 / 2 — 357.1 / 9.2 / 3 — 353.9 / 10.4 / 12 — 355.5 / 10.8 / 30 — 355.23 / 11.10 / 33: Hwy Pav — 355.0 / 11.0 / 40 — 355.22 / 10.11 / 50: Hwy Pav. Hard Rd.

3+57.70 ∠ 8° 11' Rt = E/y Dry Rock Wall Taken on Spl.

363.32 / 3.1 / 3: Hwy Rock Wall — 360.8 / 5.5 — 357.4 / 8.9 / 5: E/y Wall Rock — 356.5 / 9.8 / 15 — 356.0 / 10.3 / 30.08 — 355.6 / 10.7 / 34 — 356.2 / 10.1 / 38 — 356.0 / 10.3 / 50 — 357.13 / 9.20 / 59: Hwy Pav. Hard Road.

3+20

364.1 / 2.2: Hwy Cobble Wall — 361.29 / 5.04: S/y Conc. Dr. & Bot. Wall — 360.4 / 5.9 / 10 — 360.3 / 6.0 / 15 — 360.2 / 6.1 / 25 — 359.8 / 6.5 / 30 — 361.2 / 5.1 / 35 — 359.6 / 6.7 / 40

3+13.5 = ∠ 8. Conc Drive on Lt

363.80 / 2.53 / 5 on Drive — 362.77 / 3.56 / 6.0: Ed. Conc Drive — 361.74 / 4.59 / 3.9: S/y Conc Drive — 360.9 / 5.4 / 10 — 361.0 / 5.3 / 15 — 361.8 / 5.5 / 25 — 360.4 / 5.9 / 30 — 361.7 / 4.6 / 35 — 360.3 / 6.0 / 40

3+05.6 = Conc Wall 5"

364.56 / 1.77 / 6.0: Top Conc Wall — 364.49 / 1.84 / 1.7: S/y Conc Wall — 364.6 / 1.7 / 3.4: Rock Wall Top

3+0

364.7 / 1.6 — 364.81 / 1.52 / 3.3: Top Rock Wall — 361.8 / 4.5 / 4.2: Bot Wall — 362.0 / 4.3 / 15 — 362.0 / 4.3 / 24 — 361.7 / 4.6 / 28 — 362.0 / 4.3 / 30 — 363.4 / 2.9 / 36 — 362.8 / 3.5 / 40

366.33 366.33

BM			4.59	368.78	S.F.B.P. Edway Mt View 368.77
TP	6.53	373.37	2.95	366.84	
TP	12.03	370.79	0.78	358.76	
4+70.42	Δ				
4+45					
4+27					
TP	6.14	359.54	12.93	353.40	
4+04	6' Rt of Base Line = N'ly Power Pole				
4+0					
3+88					
		366.83			

Reduced + Plotted A.F.B. July 20th 1944

349.85

347.3 / 12.2 / 3=Bot. Wash	348.6 / 9.9	348.85 / 9.69 / 5.5=N'ly Pole	350.01 / 9.53 / 15	350.18 / 9.36 / 28=S'ly Pav. Hard Road

353.1 / 6.4	350.5 / 9.0 / 4	351.1 / 8.4 / 8	351.05 / 8.49 / 14=N'ly Pav	351.04 / 8.50 / 15	351.52 / 8.02 / 30

356.0 / 3.5	352.6 / 6.9 / 6	351.4 / 8.1 / 10	351.7 / 7.8 / 15	352.03 / 7.51 / 19.8=N'ly Pav	352.47 / 7.07 / 30

359.54

358.9 / 7.4	357.4 / 8.9 / 2	354.2 / 12.1 / 5	353.0 / 13.3 / 15	352.94 / 13.39 / 18=N'ly Pav	353.71 / 12.62 / 30	353.86 / 12.47 / 31=N'ly Pav Hard Rd

361.5 / 6.4	354.6 / 11.7 / 6	353.8 / 12.5 / 15	353.83 / 12.50 / 17.5=N'ly Pav	353.72 / 12.61 / 33	354.09 / 12.24 / 30	354.78 / 11.55 / 39=N'ly Pav Hard Rd

366.83

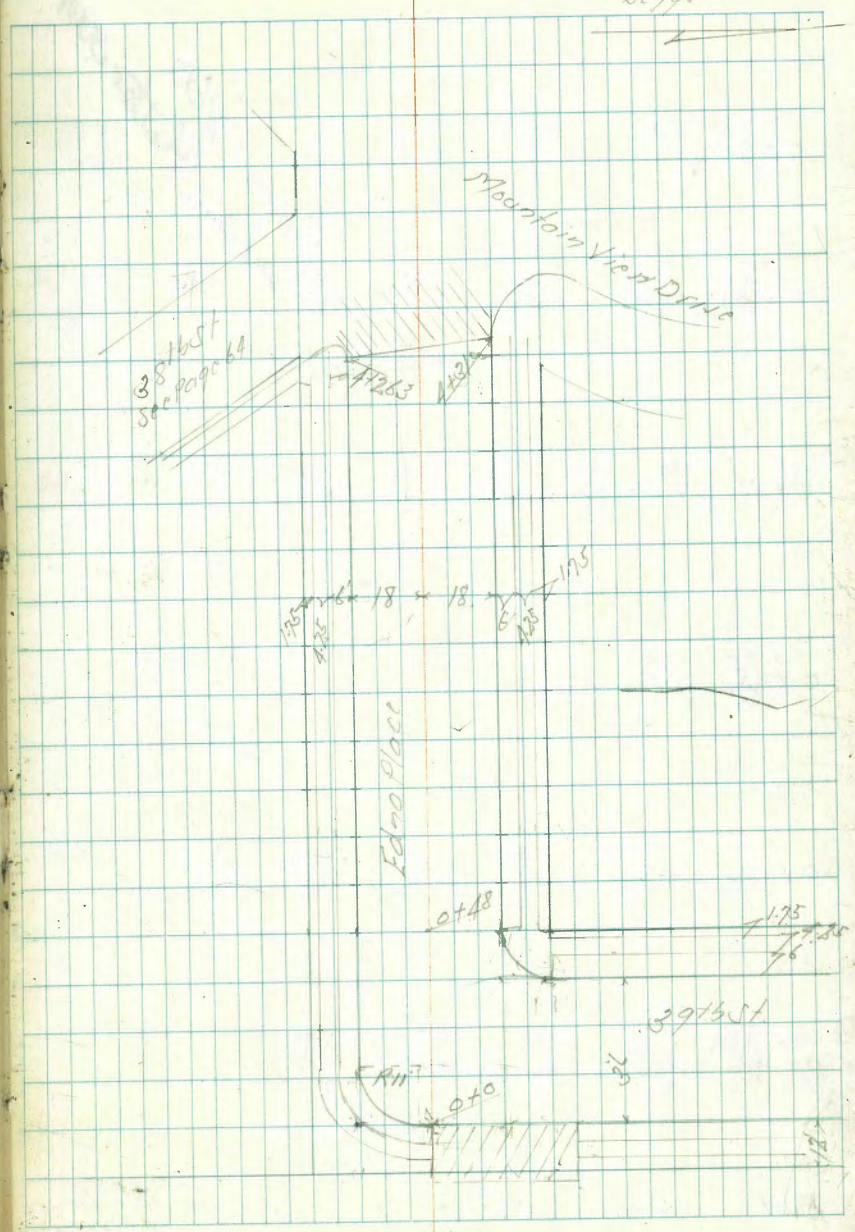
Cross Section Edna Place
39th St to Mountain View Dr.

Indexed
O.S.K.

Levels Next Page

Aug 25-44
S. Sloan
Bliss
Beggs

69



Cross Section Edna Place

Reduced AEB
Section Plotter CBH

Lt: S ℄ Rt: N

Station								
0+75	369.74 / 3.99 / 18=Cb	369.4 / 4.3 / 18	369.6 / 4.1 / 9	369.9 / 3.8	369.6 / 4.1 / 9	369.4 / 4.3 / 18	369.85 / 3.88 / 18	
0+48 = W L	369.81 / 3.92 / 18=Cb	369.5 / 4.2 / 18	369.9 / 3.8 / 9	370.2 / 3.5	369.9 / 3.8 / 9	369.4 / 4.3 / 18	369.92 / 3.81 / 18=Cb	
0+36 = W Cb Line 39th St to North	369.86 / 3.87 / 18=Cb	369.5 / 4.2 / 18	369.9 / 3.8 / 9	370.3 / 3.4	370.3 / 3.4 / 9	369.8 / 3.9 / 18	369.5 / 4.2 / 30 Gutter	370.01 / 3.72 / 30=Cb
0+18 = ℄	369.91 / 3.82 / 18=Cb+Gr.	370.0 / 3.7 / 9	370.3 / 3.4	370.4 / 3.3 / 9	370.4 / 3.3 / 18	370.3 / 3.4 / 30		
0+11	369.95 / 3.78 / 18=Cb+Ground	370.0 / 3.7 / 9	370.2 / 3.5	370.4 / 3.3 / 9	370.4 / 3.3 / 18	370.2 / 3.5 / 30		
0+0 = East Curb Line 39th St.	369.92 / 3.81 / 8=W.Wlk	370.1 / 3.6	370.3 / 3.4 / 9	370.2 / 3.5 / 18	369.8 / 3.9 / 30	370.12 / 3.61 / 38=S.Wlk	369.8 / 3.9 / 38 ground	

373.73

BM 4.96 373.73 368.77 S.E.B.P. Edna Place & Mountain View Dr.

Station	Lt			℄			Rt.
+50	369.18 / 4.55 / 18: Cb	368.8 / 4.9 / 18	369.1 / 4.6 / 9	369.3 / 4.4	369.2 / 4.5 / 9	369.0 / 4.7 / 18	369.32 / 4.41 / 18: Cb
+25	369.38 / 4.38 / 18	368.8 / 4.9 / 18	369.2 / 4.5 / 9	369.4 / 4.3	369.3 / 4.4 / 9	369.0 / 4.7 / 18	369.41 / 4.32 / 18
2+0	369.34 / 4.39 / 18	368.9 / 4.8 / 18	369.2 / 4.5 / 9	369.4 / 4.3	369.3 / 4.4 / 9	369.0 / 4.7 / 18	369.5 / 4.20 / 18
+75	369.42 / 4.31 / 18	368.9 / 4.8 / 18	369.3 / 4.4 / 9	369.6 / 4.1	369.3 / 4.4 / 9	369.0 / 4.7 / 18	369.63 / 4.10 / 18
+50	369.50 / 4.23 / 18	369.0 / 4.7 / 18	369.4 / 4.3 / 9	369.7 / 4.0	369.4 / 4.3 / 9	369.1 / 4.6 / 18	369.75 / 3.98 / 18
+25	369.49 / 4.24 / 18	369.0 / 4.7 / 18	369.4 / 4.3 / 9	369.7 / 4.0	369.5 / 4.2 / 9	369.3 / 4.4 / 18	369.74 / 3.99 / 18
1+0	369.65 / 4.08 / 18: Cb	369.2 / 4.5 / 18	369.5 / 4.2 / 9	369.7 / 4.0	369.5 / 4.2 / 9	369.3 / 4.4 / 18	369.79 / 3.94 / 18: Cb

373.73

373.73

Station	Lt.			℄			Rt.
4+0	368.84 / 4.89 / 18:Cb	368.3 / 5.4 / 18	368.8 / 4.9 / 9	369.2 / 4.5	368.9 / 4.8 / 9	368.6 / 5.1 / 18	369.13 / 4.60 / 18:Cb
+75	368.91 / 4.82 / 18	368.4 / 5.3 / 18	368.9 / 4.8 / 9	369.2 / 4.5	369.1 / 4.6 / 9	368.7 / 5.0 / 18	369.16 / 4.57 / 18
+50	368.96 / 4.77 / 18	368.4 / 5.3 / 18	369.0 / 4.7 / 9	369.2 / 4.5	369.1 / 4.6 / 9	368.8 / 4.9 / 18	369.28 / 4.45 / 18
+25	369.02 / 4.71 / 18	368.5 / 5.2 / 18	369.0 / 4.7 / 9	369.2 / 4.5	369.1 / 4.6 / 9	368.8 / 4.9 / 18	369.27 / 4.46 / 18
3+0	369.11 / 4.62 / 18	368.6 / 5.1 / 18	369.0 / 4.7 / 9	369.2 / 4.5	369.1 / 4.6 / 9	368.9 / 4.8 / 18	369.28 / 4.45 / 18
2+75	369.16 / 4.57 / 18:Cb	368.9 / 4.8 / 18	369.0 / 4.7 / 9	369.4 / 4.3	369.2 / 4.5 / 9	368.9 / 4.8 / 18	369.31 / 4.42 / 18:Cb

87373

4+37.3 on S Cb Line 4+43.5 on N Cb Line = Valley Gutter

4+26.3 on S Cb 4+31.0 N Cb = Fly Paving

368.04 / 5.69 / 18	368.12 / 5.56 / 9		368.29 / 5.44	368.42 / 5.31 / 9		368.92 / 5.36 / 18
368.78 / 4.95 / 18: Cb	368.18 / 5.55 / 18: Gutter paving	368.55 / 5.18 / 9	368.75 / 4.98	368.80 / 4.93 / 9	368.49 / 5.24 / 18: Pav	369.01 / 4.72 / 18: Cb

East + West Alley Block 127 University Hts
Check Header Grades
See Sketch Page 61

Station					
1+32					
1+15					
1+0					
0+80					
0+60					
0+40					
0+20					
0+0 = E.L. Mississippi					
BM	12.26	333.05 ✓		320.79	E.L. Miss. So C B Top Page 61

Sept. 6-44
Sisson
Bligh
Osborne

Lt = N ℄ 326.53 Rt = S

4" Asphalt Conc

Station						
1+32	326.82 / 6.23 / 10: Header	326.2 / 6.9	327.01 / 6.04 / 11.0 Conc Floor	327.00 / 6.05 / 38.0 Conc Floor	326.7 / 6.4 / 75.0 V.L.S. Grade	327.43 / 5.62 / 105.0 on Conc Floor
1+15				327.23 / 5.82 / 44 on Conc Wall	326.98 / 6.07 / 76.4 on Conc Floor	326.98 / 6.07 / 105 on Conc Floor
1+0	325.78 / 7.27 / 10	325.3 / 7.8	325.97 / 7.28 / 10			
0+80	325.22 / 7.83 / 10	324.7 / 8.4	325.25 / 7.80 / 10			
0+60	324.68 / 8.37 / 10	324.1 / 9.0	324.66 / 8.39 / 10			
0+40	324.05 / 9.00 / 10	323.4 / 9.7	323.98 / 9.07 / 10			
0+20	322.76 / 10.29 / 10: Header	322.4 / 10.7	322.78 / 10.27 / 10: Header			

333.05

Station	Lt. H	℄	Rt. S				
2+60	330.94 / 2.11 / 10 = Header	330.5 / 2.6	330.94 / 2.11 / 10				
2+40	330.46 / 2.59 / 10	330.0 / 3.1	330.50 / 2.55 / 10				
2+20	329.78 / 3.27 / 10	329.3 / 3.8	329.81 / 3.24 / 10				
2+0	329.14 / 3.91 / 10	328.6 / 4.5	329.15 / 3.90 / 10 = Header				
1+85			328.75 / 4.30 / 44 = Conc F	329.15 / 3.90 / 57 = Conc Walk	329.43 / 3.62 / 75 = Conc Floor	329.13 / 3.92 / 105 = Conc Floor	
1+68	328.08 / 4.98 / 10	327.6 / 5.5	327.8 / 5.3 / 10 = SG	328.65 / 4.40 / 115 = Conc Floor	328.64 / 4.41 / 38 = Conc Floor	327.9 / 5.2 / 75 = SG	329.12 / 3.93 / 105 = Conc Floor
1+55	327.61 / 5.44 / 10	327.1 / 6.0	327.2 / 5.9 / 10 = SG	327.2 / 5.9 / 44 = SG	327.4 / 5.7 / 75 = SG	327.93 / 5.12 / 105	
1+36 = Gutter to South	326.93 / 6.12 / 10 = Header	326.3 / 6.8 = SG	326.3 / 6.8 / 10 Subgrade	326.5 / 6.6 / 44 = SG	326.8 / 6.3 / 75 = SG	327.43 / 5.62 / 105 = Conc Floor	

2+0 = N. Louisiana - New Alley Returns

2+80

329.15
3.90
10: Header

329.38
3.67
10: Cb

329.4
3.7

329.54
3.51
10: Cb

329.29
header

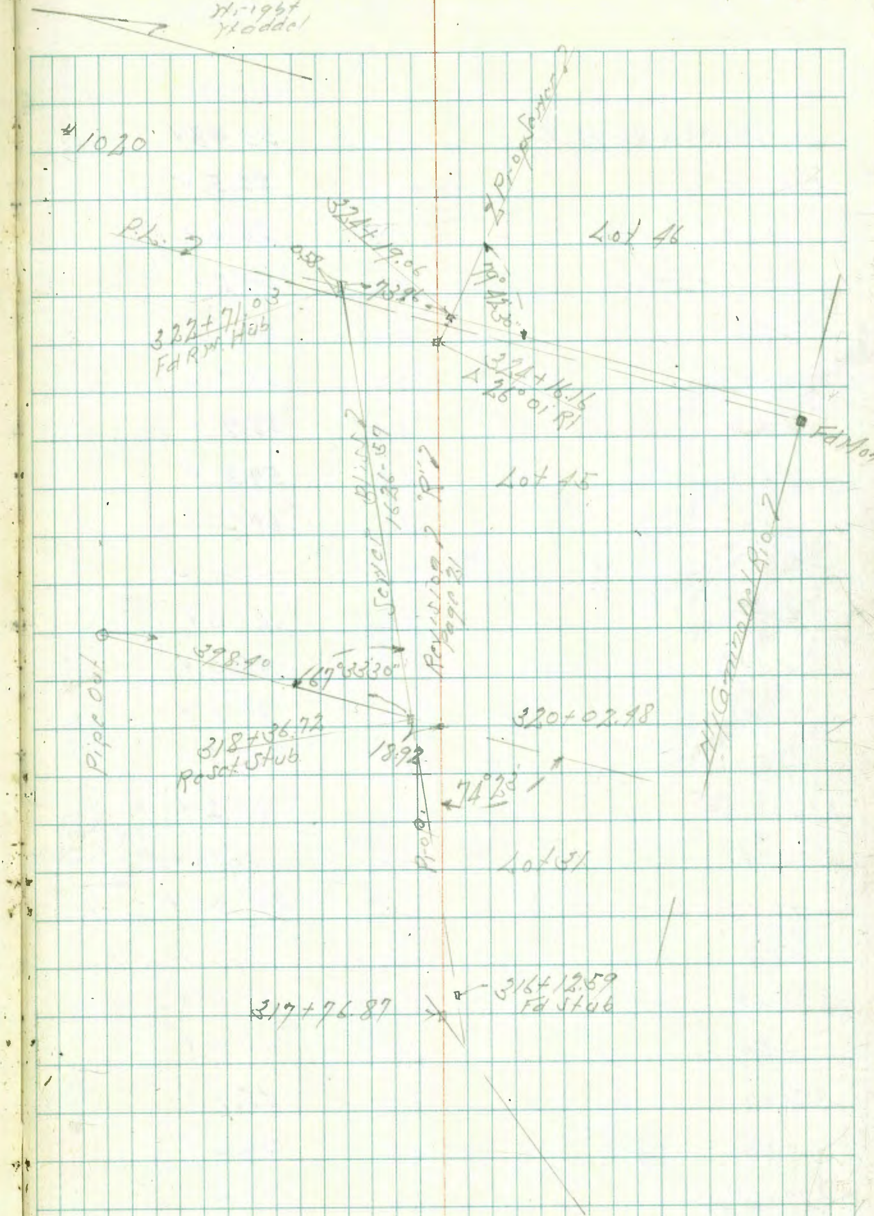
330.86
2.19
10: Header

330.4
2.7
Subgrade

330.85
2.20
10: Header

Property Ties Mission Valley Trunk Sewer
Lots 31-45-46 Rancho Mission of San Diego

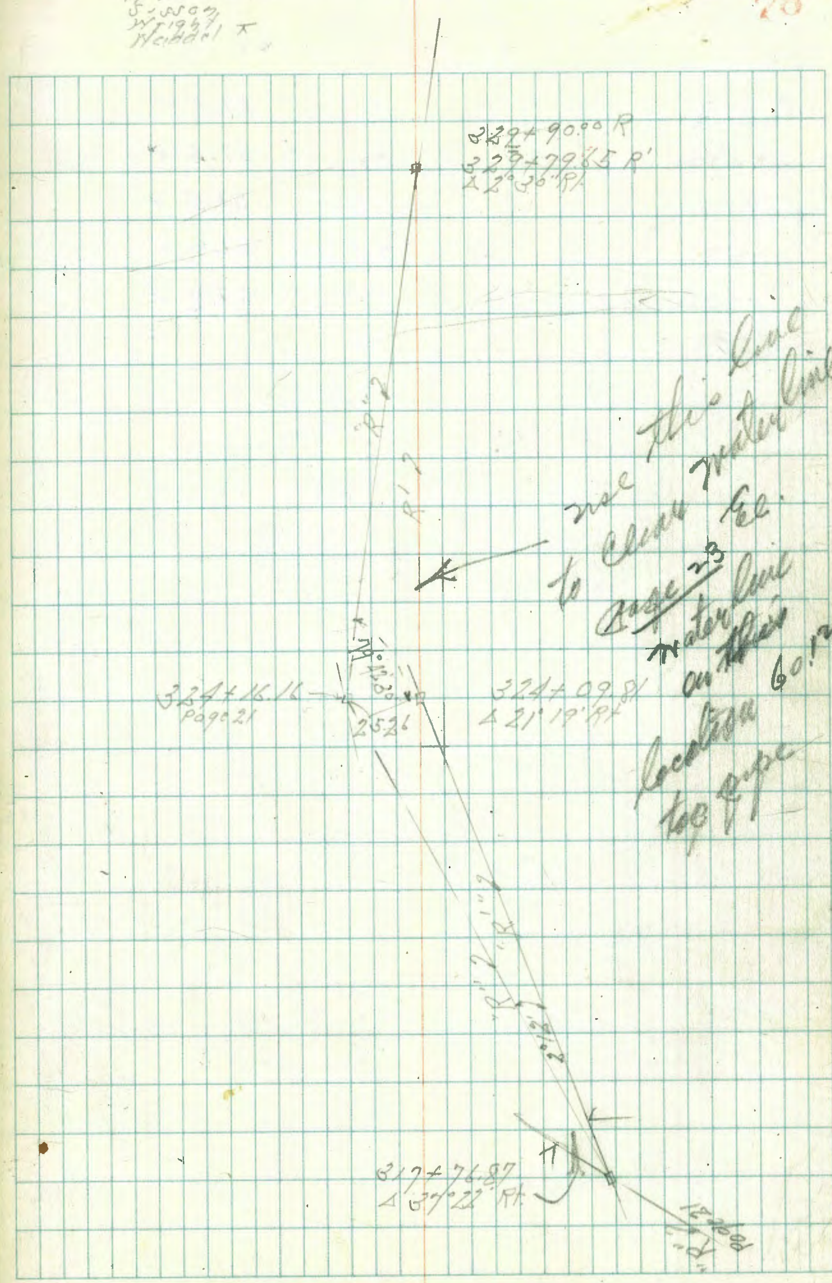
April 16. 46
Sisson
Wright
Moddel



Proposed Sewer Mission Valley Trunk
"R'" Line Line Change West of Daley's

BM	8.52	64.43		55.91	
317+76.87 Δ 37°22' Rt.			8.95	55.48 ✓	on stub
318+0			8.9	55.5 ✓	
+50			7.8	56.6 ✓	
319+0			4.9	59.5 ✓	
+50			4.4	60.0 ✓	
320+0			5.7	58.7 ✓	
+50			5.5	58.9 ✓	
321+0			5.1	59.3 ✓	
+50			4.1	60.3 ✓	
TP	9.11	70.04 ✓	5.50	60.93 ✓	
322+0			8.4	61.6 ✓	
+50			7.0	63.0 ✓	
323+0			7.2	62.8 ✓	
+50			7.2	62.8 ✓	
324+0			6.8	63.2 ✓	
BM #49			9.64	60.40 ✓	Spk Pole 20' Lt 322+75 old Page 8
+09.81 = Δ			6.62	63.42 ✓	on stub
+18			7.4	62.6 ✓	
+50			6.1	63.9 ✓	
325+0			5.5	64.5 ✓	
+50			4.9	65.1 ✓	
326+0			4.3	65.7 ✓	
+50			3.8	66.2 ✓	
327+0			3.4	66.6 ✓	
+50			2.8	67.2 ✓	

April 25-46



R' Line

		70.04.		
328+0			2.5	67.5 ✓
+50			2.4	67.6 ✓
329+0			2.5	67.5 ✓
+50			2.4	67.6 ✓
+79.65 = Δ 2°30' Rt.			2.8	67.2 ✓
329+90				

Camino Del Rio East of Ward Road

79

Nov 13-46
Sisson
McCoy
Thies

R² Line

343+76.97	65' Rt of ℄ =	Approx ℄ Camino Del Rio
348+96.86	33.2 " " " =	" " " "
354+00	34.2 Rt of ℄ =	" " " "
" "	73.3 Rt " " =	Sly Fence
" "	30.4 Rt " " =	Nail Line
362+ on P.L.	27.5 Rt of Mon =	℄ Paving
"	24.3 " " " =	Nail Line
365+65.72	62.6 Rt of ℄ =	Approx ℄ Pav
"	59.3 " " " =	Nail Line
368+52	41.8 Rt of ℄ =	Nly Conc Culvert
"	62.5 " " " =	Approx ℄ Paving
"	60.0 " " " =	Nail Line
"	69 " " =	℄ Culvert
370+70	60.7 Rt of ℄ =	Nail Line
" "	62.6 Rt " " =	Approx ℄ Paving

IMPROVED TABLES AND INFORMATION

HORIZONTAL STADIA CORRECTIONS

2°—00′ — 0.1	21°—00′ — 12.8	33°—00′ — 29.7
3°—00′ — 0.3	21°—30′ — 13.4	33°—15′ — 30.1
4°—00′ — 0.5	22°—00′ — 14.0	33°—30′ — 30.5
5°—00′ — 0.8	22°—30′ — 14.7	33°—45′ — 30.9
6°—00′ — 1.1	23°—00′ — 15.3	34°—00′ — 31.3
7°—00′ — 1.5	23°—30′ — 15.9	34°—15′ — 31.7
8°—00′ — 1.9	24°—00′ — 16.5	34°—30′ — 32.1
9°—00′ — 2.5	24°—30′ — 17.2	34°—45′ — 32.5
10°—00′ — 3.0	25°—00′ — 17.9	35°—00′ — 32.9
10°—30′ — 3.3	25°—30′ — 18.6	35°—15′ — 33.3
11°—00′ — 3.6	26°—00′ — 19.2	35°—30′ — 33.7
11°—30′ — 4.0	26°—30′ — 19.9	35°—45′ — 34.1
12°—00′ — 4.3	27°—00′ — 20.6	36°—00′ — 34.6
12°—30′ — 4.7	27°—30′ — 21.3	36°—15′ — 35.0
13°—00′ — 5.1	28°—00′ — 22.0	36°—30′ — 35.4
13°—30′ — 5.5	28°—30′ — 22.8	36°—45′ — 35.8
14°—00′ — 5.9	29°—00′ — 23.5	37°—00′ — 36.2
14°—30′ — 6.3	29°—30′ — 24.3	37°—15′ — 36.6
15°—00′ — 6.7	30°—00′ — 25.0	37°—30′ — 37.1
15°—30′ — 7.2	30°—15′ — 25.4	37°—45′ — 37.5
16°—00′ — 7.6	30°—30′ — 25.8	38°—00′ — 37.9
16°—30′ — 8.1	30°—45′ — 26.2	38°—15′ — 38.3
17°—00′ — 8.5	31°—00′ — 26.5	38°—30′ — 38.7
17°—30′ — 9.0	31°—15′ — 26.9	38°—45′ — 39.1
18°—00′ — 9.5	31°—30′ — 27.3	39°—00′ — 39.6
18°—30′ — 10.1	31°—45′ — 27.7	39°—15′ — 40.0
19°—00′ — 10.6	32°—00′ — 28.1	39°—30′ — 40.5
19°—30′ — 11.2	32°—15′ — 28.5	
20°—00′ — 11.7	32°—30′ — 28.9	
20°—30′ — 12.3	32°—45′ — 29.3	

Chains to Feet	
1	66
2	132
3	198
4	264
5	330
6	396
7	462
8	528
9	594
10	660

Feet to Chains	
100	1.515
200	3.030
300	4.545
400	6.060
500	7.575
600	9.090
700	10.606
800	12.121
900	13.636
1,000	15.151

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1½ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent lenth divided by twice the radius.

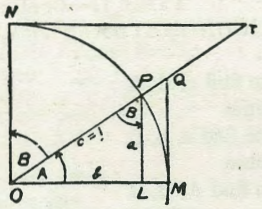


TABLE II

TRIGONOMETRIC FORMULÆ.

$\angle A = \angle MOP \qquad \angle B = \angle PON = \angle OPL$

$R = OB = c = 1$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \tfrac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \qquad \cos \tfrac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

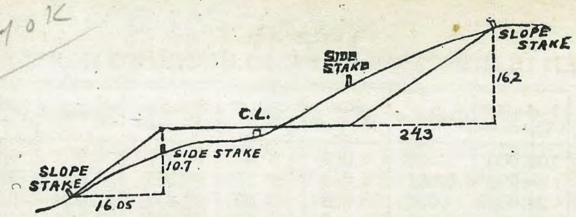
$$\sin 2A = 2 \sin A \cos A \qquad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \tfrac{1}{2}(A+B)}{\tan \tfrac{1}{2}(A-B)}$$

298.91 OK



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

M.H. Kurtz
5+03.6
3' E of ℄ Kurtz

0+67 = BC Is. = Δ 14°
chord 58'
0+97.65
67

28.1 offset to Island

50.75 T 330 wide 1.65 R
97.65
1+48.40

195+95.27 Pot Road Sur
W of Fairmount + Poway

379 16.0
377+97.4
1+1.86

5.80
4.66

54.11
46
49.51 289+00

58'
4.66
2)1.15
.57

4.92
1.15
3.77

54.66
46
50.56
293
597
63
48.4

73.28
14.5

4.92
.57
4.35
16" pipe
16" ½ shell
22½ Bell

58
39.58

379+16.00
377+97.39
1+18.61