

1630

DEUGEN
INC.

ENGINEERS
LEVEL BOOK

No. 410F

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6 For slopes of 1 on 1½ see inside of back cover.

Copyright, 1914, by Eugene Dietzgen Co.

1630

CITY ENGINEER

ENGINEERING DEPARTMENT
CITY OF SAN DIEGO,
CALIFORNIA.

The paper stock of this book is made of a high grade 50% rag paper having a water resisting surface. This book is sewed with Bing Special Enamel Waterproof Thread.

Made in U. S. A.

Chi

H

0
1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40

to be
of ros
exam
30.6

Riley		2-12
Lauretta		13-26
Mildred		27-36
Azusa		37-41
Janicia		42-45
Colusa		46-50
Brunner		51-54
Eureka		55-59
Goshen		60-65
Josephine		66-67
Mildred		68-71

Amended Map Showing

Silver Terrace Map 695

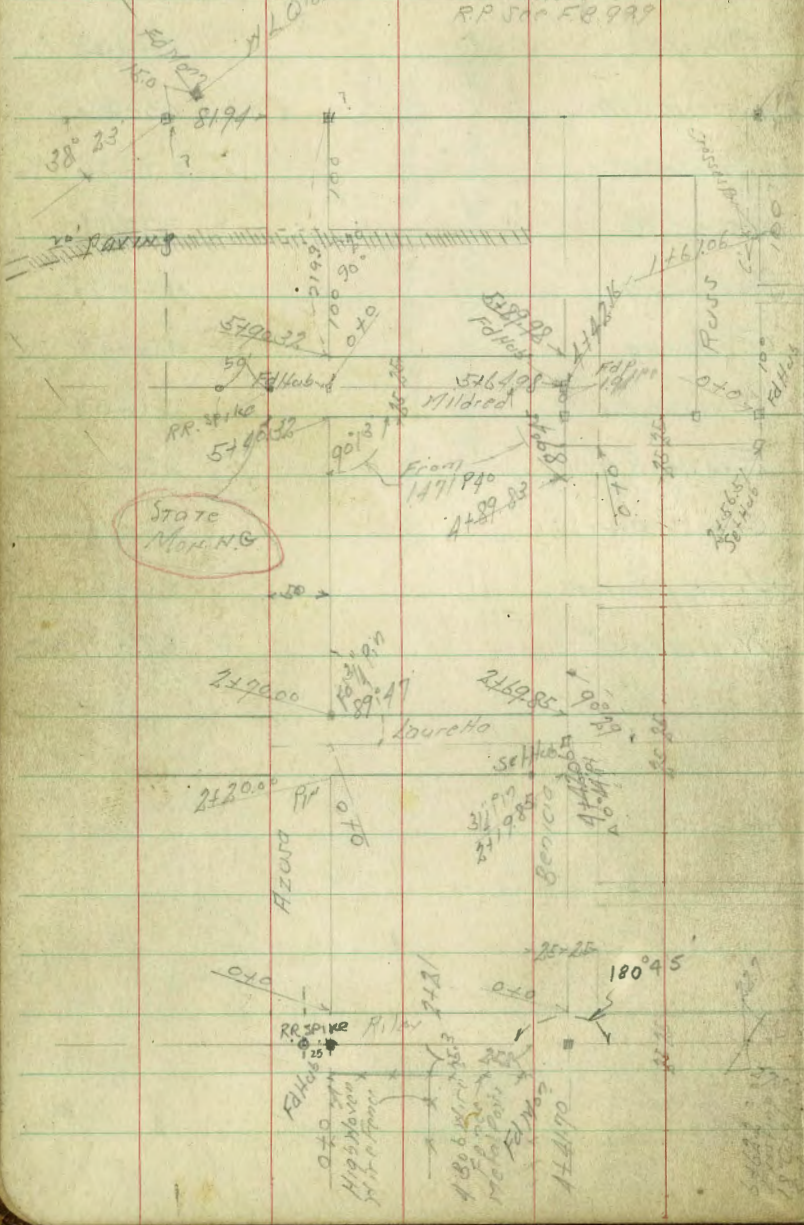
Cross Section Streets in
Silver Terrace

see Book 1471 page 40
for sketch

See R of S 4543

For Lindavista Road
RP See FE 999

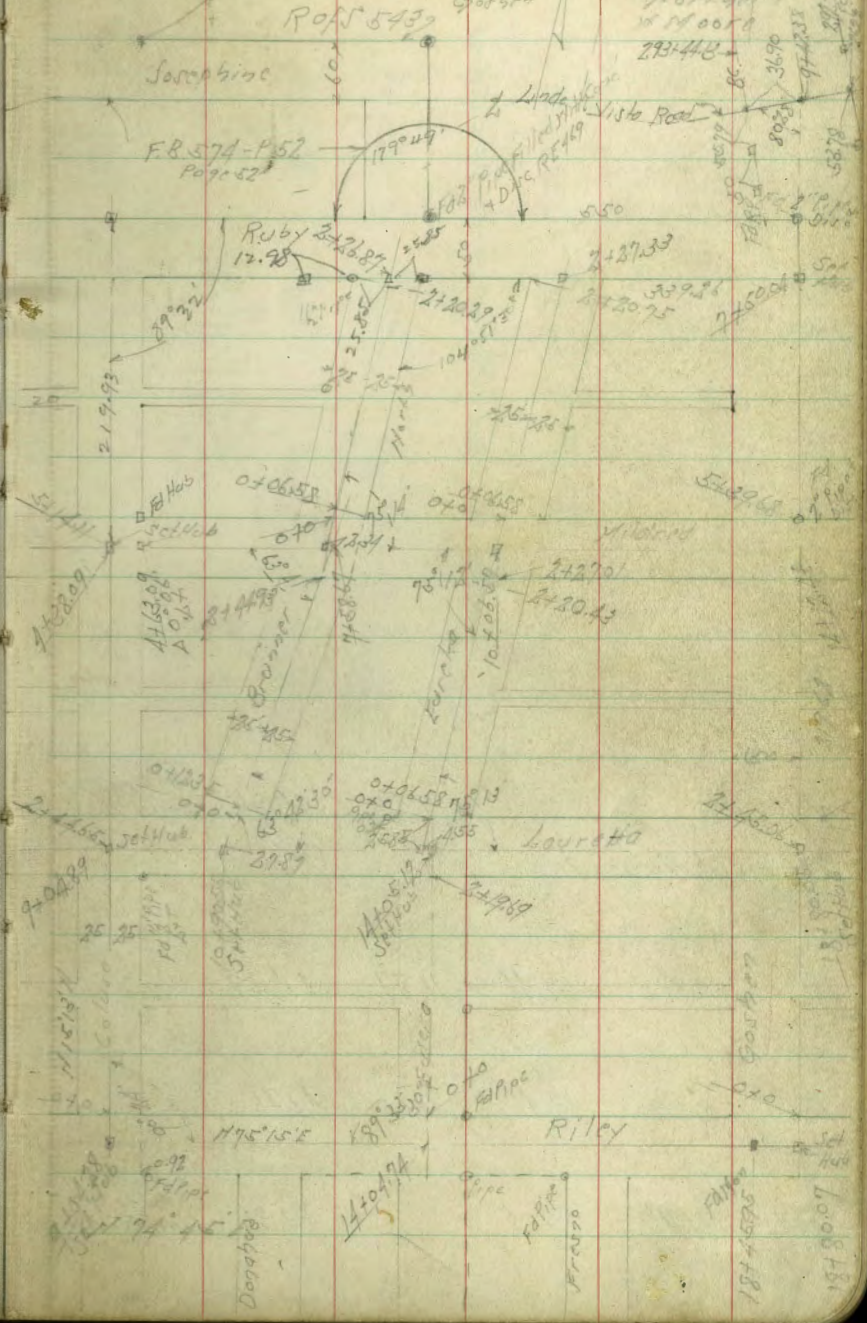
Indexed
c.s.k.



Platted on Tio sheets
2-20-44 c.s.k.

See LAD on Curvants
Lindavista at
Goshen

March 13 1944
J. S. K.
1944-48



Cross Section Pile St.
Azusa to Goshen

Indexed
c.s.k.

Notes Reduced & Plotted 4-23-42 C. K. Hays

1+50

1+0

0+50

0+05

BM

0+0 = EL Azusa St

TP 587 37.46 11.87 31.59

TP 0.00 43.46 11.60 43.46

BM 11.19 55.06 43.87

of Hub
EL Azusa +
2 R. 14

N.E. Top of Hyd.
Mildr at +
Lundqvist Pt.

March 25-42
Sisson
Hortberg
H Moore

LN

8

PL 5

2

36.6	31.0	32.0	31.9	31.4	32.8	31.5	31.5
29 15	65 18	56 15	56	61 11	47 15	49 20	49 25

34.8	30.0	30.0	30.2	30.0	31.7	33.3	33.8
27 15	75 18	75 15	73	75 10	58 15	41 20	40

33.4	29.0	29.0	29.0	28.7	30.7	31.9	32.0
41 25	85 19	85 15	85	88	60 15	56 20	55 25

31.7	28.4	28.4	28.5	28.3	27.0	30.6	30.5
58 25	91 23	91 15	90	92 23	105 25	69 15	70 25

28.2	28.4	28.4	29.0	26.7	28.8	28.7	30.46
92 25	91 15	91	95 8	10.8 15	87 20	88 25	70.0 25

37.46
W

✓
60.0
25

BM

6.8°

40.81

2 Mon
Riley + Service

4+16.70 W.L. Benicia

4+02 224 Rt of 2 - Sky Anchor Pole ✓

4+0

3+50

3+0

2+50

TP 12.04 47.61 1.89 35.57

2+0

37.46

47

47

47

3

43.8

40.0
25

43.5

41.0
25

40.3

37.0
25

40.4

37.0
25

40.6

37.0
25

40.0

37.0
25

41.3

37.0
25

42.7

37.0
25

42.2

37.0
25

43.2

41.0
25

43.2

41.0
25

40.0

37.0
25

39.7

37.0
25

39.9

37.0
25

40.2

37.0
25

39.5

37.0
25

42.2

37.0
25

42.0

37.0
25

42.2

40.0
25

42.2

40.0
25

37.4

35.0
25

37.5

35.0
25

38.4

36.0
25

38.8

36.0
25

38.0

36.0
25

40.4

38.0
25

41.2

38.0
25

41.0

38.0
25

40.8

38.0
25

40.8

38.0
25

36.3

34.0
25

37.0

34.0
25

37.1

34.0
25

36.4

34.0
25

38.6

36.0
25

39.3

36.0
25

39.6

37.0
25

39.6

37.0
25

35.4

33.0
25

35.7

33.0
25

35.6

33.0
25

34.4

32.0
25

37.0

35.0
25

38.2

36.0
25

38.1

36.0
25

38.3

36.0
25

38.3

36.0
25

35.3

33.0
25

39.7

37.0
25

47.61

33.8

31.0
25

33.0

31.0
25

34.4

32.0
25

36.7

34.0
25

36.8

34.0
25

37.46

Wiley St

4750

TP 11.87 5942 0.06 47.55

670

5785 224 Lt of L - Sly Parrot Tree

5750

5718 170 Lt of L = N.Y. 24" Pepper Tree

570

4769 196 Lt of L = N.Y. 18" Pepper Tree

4766.7 = E.L. Benicia 248 Lt of L = N.Y. Wire Fence

4741.7 = L Benicia

4761

L T Rt

487	480	480	476	475	470	477	452	448	447
107/25	111/30	114/35	118/40	119/45	124/50	147/65	142/70	146/75	147/80

5942

474	465	459	460	456	444	433	423	391
0/25	11/30	17/35	14/40	20/45	12/50	10/55	15/60	25/65

463	447	433	425	412	400	386
130/25	219/30	300/35	301/40	314/45	266/50	390/55

432	415	404	388	381	369	357	325	305
144/25	208/30	216/35	180/40	175/45	177/50	139/55	151/60	171/65

454	452	433	422	421	418	426	427
22/25	24/30	43/35	54/40	55/45	58/50	50/55	49/60

423	416	413	413	411	413	415
50/25	60/30	62/35	63/40	65/45	60/50	61/55

4761

8+79.28 = 14.4 Colusa 24.4 Lt of 2 - Fly Lath Fence ✓

8+76 22.5 Rt of 2 - Sky Power Pole ✓

8+50

8+22 22.2 Rt of 2 - Sky Power x Tel. Pole ✓

8+0

7+74 24.0 Lt of 2 - Fly Lath Fence ✓

7+50

7+0

6+73 24.2 Lt of 2 - Fly Wire Fence ✓

6+62.2 - Existing 18" Corrugated Iron Culvert on diagonal ✓

59.4

Lt.

Rt.

Rt.

5

52.4	58.1	54.5	54.3	53.6	53.6	52.3
10	12	14	15	16	16	16
25	19	14	11	10	10	11

57.3	57.0	57.0	53.1	53.2	53.3	55.6	55.1	54.5
11	11	11	12	12	11	12	12	12
25	19	15	12	12	15	18	18	18

55.4	54.8	52.8	51.5	51.9	51.5	53.4	53.2	1.5
10	16	16	17	17	17	18	18	18
25	18	15	13	15	15	18	18	18

52.2	52.0	50.8	50.5	50.6	50.1	51.0	50.9	50.5
7.7	7.4	8.6	8.9	8.8	9.0	8.4	8.6	8.8
25	18	15	12	12	15	17	15	15

5.00	48.7	49.6	49.1	49.1	48.9	49.0	48.7	48.1
9.4	10.7	9.8	10.2	10.3	10.5	10.4	10.7	11.2
25	18	15	10	10	14	15	15	15

26.66
12.76
22.7
11.1
59.42

47.22
15.20
27.7
11.1
59.42

9+70 24.5 41 of 1/2 = 1/4 Picket Fence

9+50

9+29.28 34.1 41 of 1/2 = 1/4 Picket Fence
 EL Colusa From North

9+20

BM 8.25 63.50 4.17 55.25 on Hub Riley + Colusa

9+04.28 = 1/2 Colusa St

8+82

5942

92.9 62.1 60.8 60.1 60.4 59.8 59.2
 0.9 1.4 2.7 3.4 4.1 5.2 6.1
 25 15 15 15 15 25 25

61.7 59.5 60.5 60.0 59.4 59.2 58.6
 1.8 1.9 1.5 1.5 1.5 1.5 1.9
 25 20 15 15 15 15 15

60.9 60.5 58.8 57.5 57.3 56.7 56.8 56.5
 1.6 1.8 1.7 1.2 1.2 1.3 1.7 1.5
 25 18 15 12 12 13 15 15

57.9 56.6 56.3 55.7 55.2
 5.6 6.9 7.2 7.8 8.2
 25 15 15 15 25

55.5 55.0 63.50 54.8 54.2
 2.9 3.4 4.0 4.6 5.1
 25 15 15 15 25

52.5 53.8 53.4
 4.9 5.6 6.0
 15 15 15

5942

11+25

11+0

10+75

TP 1.31 51.98 12.83 50.67

10+50

10+25 22.8 Pt of 2 - Sky Pattern Pale

10+0

63.50

17

2

PT

7

4.2x	4.2x	4.2x	4.2x	4.0x	3.9x	3.7x
6/10	7/10	8/10	9/10	11/10	12.5/25	14.6/60

4.2x	4.2x	4.2x	4.2x	4.1x	4.0x	3.8x	3.6x
7/10	8/10	9/10	9.5/10	10.2/10	11.2/10	12.5/25	13.5/50

4.0x	4.0x	4.0x	4.0x	4.0x	4.0x	4.0x	3.7x
7/10	8/10	9/10	9.5/10	10.1/10	10.8/10	11.2/25	14.5/50

51.98

4.2x	4.2x	4.2x	4.2x	4.2x	4.0x	4.0x
7/10	7.8/10	10.2/15	11.5/10	12.0/15	12.2/25	17.0/45

4.2x	4.2x	4.2x	4.2x	4.2x	4.2x	4.2x	4.2x
8/10	9/10	10/15	11/15	12/10	14/15	15.2/25	17.2/45

4.2x	4.2x	4.2x	4.2x	4.2x	4.2x	4.2x	4.2x
9/10	10/10	11/10	12/10	13/10	14/10	15.2/25	17.2/45

63.50

12+75

TP 12.92 77.10 0.00 64.18

12+50

12+25

12+23 230 Rt of 1/2 sly Power Pole

12+0

TP 12.58 64.18 0.38 51.60

11+75

11+50

57.98

Lt.

Rt

Rt

67.6	67.2	67.6	67.6	67.1	67.4	69.8	59.3
93 25	99 22	125 15	125	130 80	147 15	162 25	178 33.3 HMA House

77.10

62.2	65.3	67.1	67.3	69.9	59.2	57.5	57.3	57.6	61.60
170 25	111 21	115 15	119 18	133	150 15	167 20	169 25	166 33.8 HMA House	154 2.54 2.54 2.54

63.9	63.6	67.1	67.3	69.3	57.1	56.0	57.5	57.1	51.9
83.3 25	86 22	61 15	63 10	69	71 10	82 15	99 20	101 25	123 40

59.5	58.6	57.5	57.7	57.1	57.3	50.9	46.6
47 25	56 19	97 15	95	101 80	119 15	153 25	176 40

64.18

65.0	63.9	62.7	60.0	59.6	58.7	47.7	45.0	38.9
130 35	111 25	107 19	20 15	24	33 10	43 15	70 25	131 30

47.6	45.2	46.5	44.6	43.7	42.5	40.5	36.9
65 30	68 25	65 15	71	82 10	95 15	115 25	151 50

51.98

BM

1.97

87.62

1/2 Prop Pipe
Riley
Furcho

14+15

1410474 = L Furcho

137974 = W L Furcho St.

TP 12.73 89.59 0.24 76.86

13+50

13+25

13+0

7710

81

8

81

9

84.0

83.5

80.8

78.5

76.8

56
25

71
15

88

112

128
25

83.1

81.9

80.2

77.6

76.3

65
25

77
15

91

120
15

135
25

81.2

80.6

79.2

78.4

79.3

78.9

76.9

76.2

73.2

84
25

90
20

104
15

112
12

103

112

127
15

134
20

161
25

89.59

78.4

77.1

78.6

77.6

75.3

75.1

73.0

72.9

71.5

71

103
25

90
20

45
15

15
11

1.8

2.0
10

4.1
15

4.2
20

5.6
25

6.0
35

75.1

74.6

69.9

69.4

72.2

72.1

71.0

69.4

69.0

67.0

66.1

20
25

25
20

72
15

77
9

19

50

61
10

77
15

81
21

101
25

110
35

70.5

70.1

67.8

68.5

68.1

67.6

66.1

64.5

62.1

66
25

70
20

92
15

86
10

90

95
5

110
15

126
20

150
35

7210

TP 1228 113.82 0.24 101.54

15765

15730

15102 245 ft of 1/2 Fly Board Fence ↓

1570

TP 13.01 101.78 0.82 88.77

14790 = 1/2 3.7 Conc Walk on Pt ↓

14750

147974 = FL Fence 245 ft of 1/2 Fly Board
205 ft of 1/2 Fly Par M. Pole ↓

89.59

1001 920 210 1010 2001 916 916 961
7/15 8/15 9/15 10/15 11/15 12/15 1/16 2/16

946 946 946 946 946 946 946 946
12/15 1/16 2/16 3/16 4/16 5/16 6/16 7/16

816 816 816 816 816 816 816 816
8/16 9/16 10/16 11/16 12/16 1/17 2/17 3/17

101.78

926 896 887 890 896 876 853.4 853.5
4/16 5/16 6/16 7/16 8/16 9/16 10/16 11/16

202 568 818 856 862 848 826 816
12/16 1/17 2/17 3/17 4/17 5/17 6/17 7/17

826 826 829 827 824 809 809
8/17 9/17 10/17 11/17 12/17 1/18 2/18

89.59

17+30

17+0

16+80 = E.L. Fresno 214 Rt 0/2 = S/Ly Parker Pole ↓

16+55 = 1/2 Fresno

16+30 = H.L. Fresno 299 Rt 0/2 = S/Ly Parker Pole ↓

BM

925

104.57

S/Ly Prop Pole
Riley + Fresno

16+0

113.82

Lt

2

Rt

11

1073

65
25

109.5

13
18

1080

58
15

1083

55
15

1073

65
15

1052

81
15

103.8

100
25

1026

112
35

1115

22
25

1106

32
18

1091

47
15

1092

46
15

1085

52
15

1065

70
15

1051

87
25

1039

99
35

1120

18
25

1111

27
20

1096

42
15

1094

44
15

1088

50
15

1068

70
15

1053

85
25

1118

20
25

1116

26
20

1097

41
15

1089

49
15

1066

72
15

1049

89
25

1111

27
25

1104

34
18

1089

49
15

1082

56
15

1058

80
15

1045

92
25

1082

56
25

1059

79
17

1054

82
15

1053

85
15

1041

97
15

1024

114
25

1008

120
35

113.82

Riley St.

18+80.09 - E.L. Garber

BM 4.06 108.63

18+30.09 - W.L. Garber

18+0

17+65

113.82

S.W. Prop. Pl.
Riley + Fr. 2100

P.

104.57

41

2

Pl.

12

1070	1011	985	954	922	876
56 25	75 15	101	13.7 15	15.1 25	21.0 50

108.63

1062	1074	1041	1029	1007	992	980
76 25	88 18	97 15	109	131 15	146 25	158 35

1074	1066	1053	1053	1043	1024	1006	994
64 25	72 18	85 15	85 25	95	114 15	132 25	144 35

1087	1078	1064	1065	1056	1042	1026	1018
51 25	60 18	74 15	73 7	82	96 15	118 25	130 35

113.82

Cross Section Lauretto St.
Hjusa to East of Gosh 17

Indexed
c.s.k.

March 30, 11

1+35

140

0+75

0+50

0+25

BM

0+01 16.5 Rt of $\frac{1}{2}$ = Sly Power Pole

0+0 = F.H. Hjusa

BM 895 56.81

Notes Reduced & Plotted. 4-27-42 C.B.H.

502 31.78

H.F. Prop Car
Lauretto +
Hjusa

27.86

Hub
P. 101 +
Hjusa

St. N

L

Rt. S

13

340	33.6	323	322	322	315	310	303
28 40	25 25	25 61.5	46	46 10	53 15	58 25	65 15

328	325	319	312	308	307	304	299
40	25	19 15	56	10	61 15	61 25	79 15

321	317	307	307	304	304	299	294
47 40	25 25	61 15	61	61 15	61 20	74 25	84 15

319	313	308	303	302	294	287	274
49 40	61 25	61 15	65	66 12	71 15	80 25	90 15

318	312	305	308	304	304	287	280
50 40	54 25	61 15	60	64	64	80 15	88 25

319	318	316	314	307	31.65	282
49 25	54 40	52	65.4	61	61 15	86 25

36.81

Prop Car
Hjusa

3729

TP 12.93 61.83 0.39 48.90

340

2170

2135

TP 12.87 49.29 0.29 36.42

210

1770

18.90

17

2

P1

$\frac{94.3}{10}$ $\frac{117}{25}$ $\frac{117}{15}$ $\frac{120}{15}$ $\frac{116}{15}$ $\frac{116}{20}$ $\frac{121}{25}$ $\frac{121}{25}$
 27.40 96.5 105 86.2 205 205 262 262
 9/10/10 11/10/10 11/10/10 11/10/10 11/10/10 11/10/10 11/10/10 11/10/10
 61.83

$\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$
 $\frac{27}{10}$ $\frac{21}{25}$ $\frac{22}{25}$ 19 $\frac{21}{25}$ $\frac{22}{25}$ $\frac{22}{25}$ $\frac{22}{25}$

$\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$
 $\frac{27}{10}$ $\frac{21}{25}$ $\frac{22}{25}$ $\frac{22}{25}$ $\frac{21}{25}$ $\frac{22}{25}$ $\frac{22}{25}$ $\frac{22}{25}$

$\frac{6}{5}$ $\frac{3}{5}$ $\frac{3}{5}$ $\frac{3}{5}$ $\frac{3}{5}$ $\frac{3}{5}$ $\frac{3}{5}$ $\frac{3}{5}$
 $\frac{9}{10}$ $\frac{96}{25}$ $\frac{104}{25}$ 117 $\frac{120}{15}$ $\frac{121}{25}$ $\frac{121}{25}$ $\frac{121}{25}$

49.29

$\frac{8}{10}$ $\frac{9}{25}$ $\frac{3}{5}$ $\frac{3}{5}$ $\frac{3}{5}$ $\frac{3}{5}$ $\frac{3}{5}$ $\frac{3}{5}$
 $\frac{27}{10}$ $\frac{21}{25}$ $\frac{22}{25}$ 09 $\frac{21}{25}$ $\frac{22}{25}$ $\frac{22}{25}$ $\frac{22}{25}$

$\frac{5}{10}$ $\frac{5}{25}$ $\frac{5}{25}$ $\frac{5}{25}$ $\frac{5}{25}$ $\frac{5}{25}$ $\frac{5}{25}$ $\frac{5}{25}$
 $\frac{27}{10}$ $\frac{21}{25}$ $\frac{22}{25}$ $\frac{22}{25}$ $\frac{21}{25}$ $\frac{22}{25}$ $\frac{22}{25}$ $\frac{22}{25}$

36.81

610

631

627

616

609

601

592

94
2598
15

109

116
15124
25133
40

7P 11.20 72.52 0.51 61.32

72.52

5175

618

613

604

600

598

585

98
2595
15

114

118
15126
25130
25

5152

61.95

609

608

594

588

578

578

574

98
2598
2599
25

115

121

120
15130
15140
25144
35

5125

61.25

609

608

585

582

575

572

98
2598
25118
15

125

136
15148
25155
35

5115

61.8

603

609

581

575

567

565

99
25115
15119
15

127

145
15151
25153
25

510

61.2

608

625

625

615

96
25110
15125
15135
15152
25

61.82

Lauretta

7+70

7+85

6+90

6+80

6+67

6+60

6+30

72.52

17

68.3	67.5	66.1	65.3	64.8	63.7
$\frac{12}{25}$	$\frac{50}{15}$	64	$\frac{72}{15}$	$\frac{76}{25}$	$\frac{88}{10}$

67.6	66.9	65.9	64.9	63.5	62.8
$\frac{19}{25}$	$\frac{56}{15}$	71	82	$\frac{90}{25}$	$\frac{100}{40}$

66.3	65.2	64.1	63.9	63.2	62.4	61.3
$\frac{68}{25}$	$\frac{70}{15}$	$\frac{84}{5}$	84	$\frac{95}{15}$	$\frac{101}{25}$	$\frac{112}{40}$

63.1	62.5	62.2	62.5	62.7	61.3
$\frac{91}{25}$	$\frac{100}{15}$	102	$\frac{100}{15}$	$\frac{98}{25}$	$\frac{112}{40}$

65.1	63.6	62.3	62.0	61.3	60.6	60.0
$\frac{68}{25}$	$\frac{89}{15}$	$\frac{102}{10}$	$\frac{105}{10}$	$\frac{113}{15}$	$\frac{119}{25}$	$\frac{125}{40}$

65.5	64.9	63.7	62.6	61.5	60.9	59.4
$\frac{70}{25}$	$\frac{76}{15}$	86	$\frac{99}{15}$	$\frac{110}{15}$	$\frac{116}{25}$	$\frac{131}{40}$

64.6	63.8	62.5	62.1	61.9	61.3	60.1
$\frac{79}{25}$	$\frac{87}{15}$	$\frac{100}{15}$	104	$\frac{106}{15}$	$\frac{112}{25}$	$\frac{124}{40}$

72.52

9+13

9+10

BM

3.06

69.46

on Hub
Laurahay
Colusa

9+104.89 = 1/2 Colusa

8+7989 = 1/2 Colusa

22.5 Lt of 1/2 = Fly of 10 Acacia Trees ✓

25.4 Rt of 1/2 = Fly Board Fence ✓

8+51

254 Rt of 1/2 = Angle Board Fence ✓

8+45

276 Rt of 1/2 = Fly Shed ✓

8+0

9+81

220 Lt of 1/2 = Fly 10 Acacia Trees Big L'D area

9+82

277 Rt of 1/2 = Fly Shed ✓

72.52

Lt.

1/2

Rt.

72.9	72.1	70.7	70.4	69.4	68.5
10.1	9.1	1.8	2.1	1.1	2.0
25	15	10	21	15	25

72.5	70.7	69.9	68.6	67.9
1.0	1.8	2.1	1.9	1.6
25	15	21	15	25

71.6	70.8	69.7	68.5	67.8
9.9	1.7	2.8	1.0	1.7
25	15	21	15	25

70.8	70.1	69.5	68.9	68.1	67.4
1.7	2.1	3.0	3.6	1.1	5.1
25	15	8	3.6	15	25

69.9	69.0	67.7	66.7	66.4	65.4	65.5
2.6	3.5	1.8	5.8	6.1	7.1	3.0
25	15		15	19	25	30

69.9	68.2	66.8	65.7	64.9	63.9	62.5
2.2	4.3	5.7	6.2	7.6	8.6	8.0
25	15		15	21	25	25

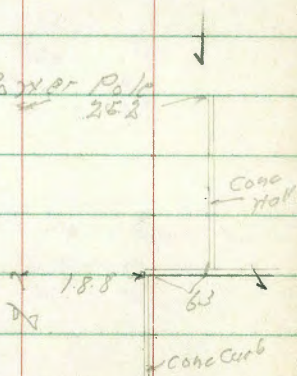
72.52

11+07.89 = L Brunner on N

10+75 = Approx. W. Brunner From N
 247 ft of L. Wire Fence

10+30 171 ft of L. S. P. or Pole
 252

9+98



9+85

191

TP 12.90 84.97 0.45 72.07

9+29.89 = F.L. Colura 246 ft of L. W. Wire Fence

72.52

84.4	83.0	81.0	79.7	78.9	77.5
06	2.0	1.0	5.3	6.1	7.7
25	15	10	15	25	45

83.0	81.7	80.2	79.3	78.9	78.1	77.1
2.0	5.3	1.8	5.7	6.1	6.9	7.9
15	15	18	2	15	25	35

80.7	79.6	78.5	77.5	77.3	76.6	74.7	74.7	73.8
1.3	5.4	6.5	2.7	2.7	8.4	10.3	10.26	11.2
25	15	5	2	2	15	25	25.2	35

78.6	77.6	75.2	75.2	74.2	73.96	74.26	73.2
6.4	7.8	9.8	9.8	10.8	11.01	10.71	11.8
25	15	5	2	15	15	25	35

76.1	75.2	73.2	73.3	72.2	72.43	71.7	71.4
8.9	9.8	11.8	11.7	12.8	12.54	13.2	13.6
25	15	8	17	15	19.1	25	35

84.97

73.5	72.8	71.7	71.3	70.1
1.0	10.3	9.8	1.2	2.4
25	15	9	15	25

72.52

12+30 25 6/10 8 = Fly Wire Floor ✓

12+07

TP 1201 89.84 8.14 76.83

11+90

11+90

11+45

11+30.74 = FL Brugger at H

8197

3-31-42

Lt

Z

Rt

20

79.8	81.8	82.8	84.9	84.9	84.1	81.0	77.5	73.2
10.0	8.0	7.1	4.9	4.9	5.7	8.8	12.3	11.6
5.0	2.5	1.5	1.0	1.0	1.0	1.5	2.5	2.0

76.5	65.5	63.8	63.8	72.2	76.1	76.4	75.8	74.4	64.0	61.8
11.0	24.3	26.0	26.0	17.6	13.7	13.1	14.0	15.4	15.8	22.0
5.0	3.5	2.5	2.0	1.5	1.0	1.0	1.5	1.5	2.0	2.0

89.84

72.0	65.5	64.0	64.9	60.0	59.7	59.1	58.4	57.4
12.0	12.5	21.0	22.1	25.0	25.2	25.1	26.6	27.6
4.5	3.5	2.5	1.5	2.0	1.5	2.5	2.0	1.5

72.0	64.8	63.8	62.6	62.2	60.8	60.0	59.7	65.6
12.0	20.2	21.2	22.4	22.8	24.1	25.0	25.2	19.4
5.2	4.0	2.5	1.5	1.0	1.5	2.5	2.5	1.0

84.7	82.4	80.5	78.7	78.8	76.7
2.2	2.6	1.5	6.3	6.2	2.5
1.5	1.5	1.5	1.5	2.5	1.0

84.7	83.7	82.9	80.7	79.9	78.7
2.2	1.3	3.0	4.0	5.1	6.8
1.5	1.5	1.0	1.5	2.5	1.5

8197

BM 11.77 118.09 6.70 10632

14+05.12 - Eureka From

13+80.12 - W L. Eureka From South

TP 12.64 113.02 0.88 100.38

13+35

13+79 230 Rto of 2 - S/L Anchor Pole ↓

13+0

TP 12.99 101.26 1.57 88.27

12+70

12+43

89.84

2 Hub
2 Court Ho +
Eureka From

14

8

Rt

21

101.80
19
25

107.4
56
15

106.3
67

105.2
28
15

104.4
86
25

102.9
81
25

102.2
86
15

102.5
95

102.3
107
15

101.5
115
25

98.4
29
40

97.8
35
25

97.7
36
25

96.7
46

95.9
54
15

95.2
51
25

94.3
70
40

93.1
87
40

92.7
86
25

92.3
90
15

91.9
94

91.1
101
15

90.3
110
25

89.3
120
40

101.26

90.8
40
50

89.5
35
25

88.8
10
15

87.6
22

87.0
28
15

86.8
30
25

84.3
55
50

84.4
55
50

86.6
32
25

86.6
32
15

85.5
43

84.5
52
9

82.3
75
15

79.4
101
25

77.6
122
50

89.34

1610

TP 1221 14147 0.26 12926

15470

15435

1540

TP 11.72 129.52 0.29 117.80

14165

1443012 = FL Farcho From South

14127 256 pto of $\frac{1}{2}$ = 54 Paper Pole ✓
118.09

22

54

2

PA

1323

 $\frac{22}{25}$

1312

 $\frac{10.2}{15}$

1307

148

1284

 $\frac{13.1}{15}$

1273

 $\frac{14.2}{25}$

1261

 $\frac{15.4}{40}$ 141.47

1282

 $\frac{0.15}{25}$

1282

 $\frac{1.15}{15}$

1271

24

1260

 $\frac{5.5}{15}$

1250

 $\frac{1.5}{25}$

1236

 $\frac{5.9}{40}$

1259

 $\frac{3.6}{25}$

1249

 $\frac{1.6}{15}$

1238

57

1222

 $\frac{7.3}{15}$

1211

 $\frac{8.1}{25}$

1199

 $\frac{9.6}{40}$

1217

 $\frac{7.8}{35}$

1208

 $\frac{8.7}{25}$

1202

 $\frac{9.8}{15}$

1193

102

1181

 $\frac{1.1}{15}$

1172

 $\frac{12.3}{25}$

1159

 $\frac{13.6}{40}$ 129.52

1173

 $\frac{0.8}{40}$

1162

 $\frac{1.9}{25}$

1152

 $\frac{2.9}{15}$

1143

3.8

1131

 $\frac{5.0}{15}$

1122

 $\frac{5.9}{25}$

1112

 $\frac{6.9}{39}$ ✓
RIGHT HOUSE

1117

 $\frac{6.1}{25}$

1107

 $\frac{7.1}{15}$

1099

82

1085

 $\frac{9.1}{15}$

1076

 $\frac{10.5}{25}$ 118.09

Lauretta

17135

17140

16175

16160

16150

16131

224' R to 1st Sky Power Pole

16122

141.47

23

41

2

171

140.9

140.1

138.3

136.8

135.7

134.8

26
25

14
15

22
15

17
15

58
25

28
40

139.2

138.1

136.7

135.2

134.1

132.7

23
25

24
15

18
15

63
15

24
25

88
40

136.0

136.4

135.5

133.9

133.0

131.3

5.5
25

5.1
15

10
15

7.6
15

8.5
25

10.8
40

10:11 F. Collt
14:15

134.4

134.7

133.7

131.0

131.1

130.8

7.1
25

5.8
15

7.8
15

12.5
15

9.6
25

10.7
40

10:11 F. Collt
14:15

130.0

132.5

131.4

132.9

132.5

129.5

128.9

11.5
25

9.0
15

19.1
15

8.6
10

9.0
15

12.0
25

12.6
40

133.7

131.6

130.6

130.1

128.3

127.8

127.8

7.8
25

9.9
15

18.9
10

11.4
15

13.3
15

13.7
25

13.7
40

134.1

132.9

131.7

129.0

128.6

127.9

126.8

24
25

8.6
15

9.8
15

12.1
7

13.9
15

13.4
25

14.7
40

141.47

19+0

18+80.05-EL. Goshco

BM

5.33

141.59

Hub 2
Laurie Ho
EL. Goshco

18+55.05-~~L~~

18+30.05-~~W~~ Goshco

TP

5.91

146.92

0.46

141.01

18+0

17+70

141.47

24

1429

20
25

1415

24
25

1438

23
25

1434

25
25

1429

24
25

1419

20
25

1437

25
25

1432

27
25

1426

25
25

1422

27
25

1419

20
25

1408

27
25

1420

20

1416

25

1412

27

1406

27

1403

27

1393

27

1403

26
25

1398

27
25

1392

27
25

1388

27
25

1387

28
25

1380

25
25

1388

28
25

1385

28
25

1380

28
25

1376

28
25

1377

28
25

1370

25
25

1369

28
20

1385

28
25

1380

28
25

1376

28
25

1359

28
20

1351

28
20

141.47

April 13-42

25

2140

20470

TP 12.07 158.42 0.57 146.35 ^{0.2% Lot 5} 20435

20435

2040

19470

19435

14692

Lt.

S

Pt

156.1
20
25

157.2
12
15

150.9
80

147.8
10.5
15

146.1
123
25

142.8
160
45

153.1
52
25

150.9
75
15

147.9
10.5

145.6
12.8
15

144.0
144
25

141.0
174
45

158.42

148.9
230
25

148.1
15
15

145.5
1.4

143.8
52
15

141.6
52
25

139.8
76
40

147.3
20.4
25

145.7
12
15

143.4
3.5

141.4
5.5
15

139.8
71
25

137.9
97
40

145.2
17
25

143.7
52
15

141.4
5.5

138.4
8.5
15

136.1
10.8
25

133.7
122
40

145.1
18
25

143.9
30
15

142.2
77

140.1
18
15

138.8
81
25

137.1
98
40

14692

23+30 = 44

237

0.09

180.71

NW Prop Stub

23+0

TP

11.77

180.80

1.51

169.03

22+70

22+35

TP

12.12

170.54

0.00

158.42

22+0

21+70

21+35

158.42

180.7

0.1
25

177.7

0.1
25

179.1

0.2
25

175.5

0.5
25

176.6

0.2
25

173.5

0.2
25

174.7

0.6
25

170.8

0.9
25

173.0

0.8
25

169.3

1.1
25

170.2

1.6
25

166.1

1.7
25

26

180.80

172.9

0.9
25

171.2

0.7
25

168.9

1.6

166.5

1.0
25

165.1

0.5
25

162.1

0.4
25

167.3

0.2
25

165.5

0.5
25

163.3

0.7

160.7

0.8
25

159.4

1.1
25

157.6

1.4
25

170.54

163.2

0.8
25

161.7

0.3
25

159.6

0.7

157.3

1.1
25

155.0

0.4
25

150.2

0.8
25

160.4

0.8
25

158.4

0.0
25

155.0

0.4

151.4

0.7
25

148.6

0.8
25

140.2

1.8
25

157.9

0.5
25

156.1

0.2
25

153.4

0.0

150.2

0.2
25

147.6

1.0
25

140.4

1.8
25

158.42

Cross Section Mildred St.
Benicia to Gosport

Indexed
C.S.K.

0+75

TP 11.76 78.15 0.07 66.39

0+50

0+25

0+12

0+0 = F.L. Benicia

Set
BM

BM 11.81 66.46

Red. from page 71 this book

0.07 66.39

7 Pipe
Benicia +
Mildred to W

7 Hub
Laurel to
Benicia
Page 15

April 11-22

St. W

8

91.5

27

64.6	64.9	65.3	66.9	69.0	70.0	69.7
12.6	13.3	12.9	11.3	9.3	8.3	8.5
50	25	15		25	25	20

78.15

80.0	77.4	79.8	79.7	79.5	60.8	62.7	63.8
57	91	6.7	6.8	7.0	57	3.8	2.7
50	25	25	15		15	25	40

57.7	58.5	58.1	58.0	57.4	57.7	57.2	57.2	58.3
6.8	8.0	8.4	10.9	9.1	8.8	9.3	9.3	8.2
70	25	15		25	20	15	25	20

59.0	59.7	54.6	56.7	56.4	56.3	56.7
7.5	8.8	11.9	9.8	10.1	10.2	9.8
25	15		10	15	25	40

60.6	58.7	56.8	56.0	54.4	55.2
5.9	7.8	9.7	10.5	12.1	11.2
25	15		10	15	25

66.46

BM 465 84.59

H. F. Prop
W. L. R. 1/2
M. L. R. 1/2
R. 1/2

27.31.5 = 1/2

27.06.5 = H. L. Russ From D

1475

TP 11.56 89.21 0.47 77.68

1450

1425

1406 12.5 1/2 1/2 = H. L. Parver Pol.

140

78.15

4+

2

pt

28

83.0 82.6 81.3 81.0 80.4 79.4
5.2 6.6 7.9 8.2 8.8 9.8
25 15 15 15 25 40

80.2 79.6 80.5 77.4 79.2 79.0 78.0
9.0 9.6 8.9 11.2 10.0 10.2 11.2
25 15 15 15 20 25 40

80.4 79.1 77.1 77.1 77.3 77.0 76.1 74.0
8.8 9.5 11.5 11.5 11.9 12.2 12.1 15.7
25 15 5 15 15 25 35 45

89.24

79.0 78.8 78.2 77.5 75.7 75.5 74.7
7.8 7.6 9.2 9.7 2.5 2.7 3.5
25 25 15 15 15 25 40

75.8 75.8 76.5 75.9 75.1 74.5 72.8
2.1 2.1 1.9 2.2 3.1 2.7 5.1
10 25 15 15 15 25 20

72.3 71.2 72.3 72.0 73.4 72.8 72.1
5.9 7.0 5.9 5.8 4.8 5.4 6.1
15 25 15 15 15 25 40

78.15

2+50

Δt	2	Δt	2	Δt	2	Δt	2
89.0	88.4	87.0	86.5	80.4	77.6	74.6	74.2
0.2	0.8	2.2	2.7	8.8	11.6	14.1	15.0
25	15		3	15	25	40	50

40-50 Years

2+25

88.1	86.9	85.1	84.8	84.7	84.1	80.6
0.5	2.2	4.1	1.1	1.5	5.1	8.6
25	15		15	25	35	50

40-50 Years

2+13

88.4	87.9	86.8	84.5	83.8	81.9
0.8	1.2	2.1	4.7	5.4	7.2
25	15		15	25	50

2+0

86.0	86.4	87.0	85.0	84.2	82.4
2.2	2.8	2.2	1.5	5.0	1.8
25	15		15	25	40

2+85

86.9	85.6	83.3	83.6	84.3	83.3
2.2	3.6	5.9	5.6	4.2	5.9
25	15		15	25	40

2+75

86.3	85.5	83.8	83.8	79.9	81.7	81.8
2.9	3.7	5.4	5.4	9.2	7.5	7.4
25	15		15	25	32	45

2+58

173 St of L - NY Power Pole

2+56.5 = FL Run

84.6	84.3	83.1	81.8	82.3	81.4
4.6	4.2	6.1	7.4	6.9	7.8
25	15		15	25	45

89.24

89.21

April 13-12

BM 10.97 101.57 ^{2 Nos Mildred} F.L. Caluso

4+63.09 = F.L. Caluso

TP 11.68 112.54 0.14 100.86 ^{Hail H 100} Guard Pond

4+38.09 = F.L. Caluso

4+13.09 = F.L. Caluso

4+0

TP 11.86 101.00 0.10 89.14

4+80

4+70

89.21

61

2

91

101.0 101.5 101.5 101.5 100.5 100.1 100.2
 11.5 11.0 11.0 11.0 12.0 12.4 12.2
 25 15 2 2 5 15 25

112.54

92.9 95.1 97.2 99.1 98.2 97.2
 7.1 5.9 5.2 1.9 2.8 2.5
 25 15 8 13 25

84.0 86.4 89.1 90.6 93.6 94.1 94.3
 12.0 14.4 11.9 10.4 7.4 6.9 6.2
 15.0 = 8.0 wash 15 8 15 25

92.3 83.0 84.0 85.4 87.7 89.6 89.8 91.8 93.15 ✓
 8.7 18.0 17.0 15.6 13.3 11.4 11.2 9.7 28.5
 6.0 35.0 = 8.0 wash 15 15 25 25 8.85 = 11.0 wash Floor

101.00

91.7 81.9 81.2 79.2 82.7 85.3 86.0
 7.3 7.2 8.0 10.0 6.5 5.9 2.2
 15 25 15 15 25 25 38.5 = 11.0 wash

90.0 87.9 85.8 82.3 78.2 77.7 80.5 83.7
 7.0 1.2 2.4 6.9 11.0 11.5 8.4 5.5
 35 25 15 10 15 25 40

89.21

6+29

6+21.5 16.8 1/2 of 1/2 - 1/4 Power Pole ✓

6+0

5+63

35 R of 1/2 - 1/4 Wire Fence ✓
248 1/2 of 1/2 - 1/4 3 Board Fence ✓

TP

1210 124.45 0.19 112.35

5+35

5+22

5+0

4+65

170 1/2 of 1/4 Power Pole

112.54

H

L

R

12.937	12.37	12.29	12.07	11.95	11.98	11.98	11.87	11.62
0.88	0.8	1.6	2.8	5.0	4.7	4.7	5.8	8.0
24.2	24	15	8	5	15	16	35	40

5425
5425
5425
5425

12.10	12.02	11.98	11.74	11.77	11.76	11.59	11.39
5.4	4.4	5.7	7.1	6.8	6.9	8.6	10.6
25	15	15	4	15	19	25	40

11.69	11.61	11.52	11.37	11.37	11.37	11.24	11.08
7.6	8.4	9.1	10.8	10.8	10.8	12.1	13.7
25	15	15	15	15	18	35	40

124.45

11.29	11.27	11.24	11.14	11.08	11.02	11.02	10.95	10.92
7.0	7.02	8.1	10	7.3	9.3	9.2	10.0	10.0
25	25	15	10	15	15	20	25	35

108.41

108.36

106.9

107.4

107.2

106.5

105.4

105.3

104.6

104.7

5.1	5.1	5.2	6.0	7.1	7.2	7.8	8.8
40	25	16	10	15	15	25	40

112.54

1/4 - 1/2
1/5 - 1/2
Cape
Walk

1/8
3500
Walk

TP 0.57 113.27 1175 112.70

870

BM

5.00 119.45

072406
Mildred
Brunner
From South

7+89 137 1/2 of 2 - W4 Anchor Pole

7+5867 - 2 Brunner From South

7+40

7+33 172 1/2 of 2 - W4 Parole Pole

7+185 - W4 Brunner From South

7+0

6+63 248 1/2 of 2 - Fly 2 Board Fence

6+53

124.45

L

S

R

117.8

116.0

114.0

112.7

111.0

106.7

117.8

116.0

114.0

112.7

111.0

106.7

123.9

122.5

121.2

119.5

117.9

116.0

123.9

122.5

121.2

119.5

117.9

116.0

124.4

122.9

122.6

122.6

122.7

119.3

117.7

114.3

124.4

122.9

122.6

122.6

122.7

119.3

117.7

114.3

126.6

125.1

123.9

122.0

122.2

120.1

119.6

115.8

126.6

125.1

123.9

122.0

122.2

120.1

119.6

115.8

126.1

125.3

123.5

121.8

122.9

122.2

119.5

116.9

126.1

125.3

123.5

121.8

122.9

122.2

119.5

116.9

121.9

123.8

124.4

122.5

120.6

120.8

120.9

119.3

116.9

121.9

123.8

124.4

122.5

120.6

120.8

120.9

119.3

116.9

121.9

123.8

124.4

122.5

120.6

120.8

120.9

119.3

116.9

124.45

TP 10.59 122.33 091 111.74

9+25

9+05

TP 11.94 112.65 0.73 100.71

8+85

8+82 25 R¹⁰/₂ = Fly Wire Fence ✓

8+80

8+60

TP 0.15 101.44 11.92 101.29

8+35

112.27

Lt.

R

R1

33

113.3	111.1	111.5	111.7	109.8	109.5	108.6
$\frac{+25}{25}$	$\frac{+1}{25}$	$\frac{+2}{15}$	$\frac{+2}{25}$	$\frac{+29}{15}$	$\frac{+37}{25}$	$\frac{+1}{30}$

102.7	102.3	101.8	101.1	101.3	102.5	104.7
$\frac{+100}{45}$	$\frac{+104}{25}$	$\frac{+109}{15}$	$\frac{+116}{15}$	$\frac{+114}{15}$	$\frac{+102}{25}$	$\frac{+80}{50}$

112.65

97.1	88.3	87.2	86.1	86.6	91.3	93.1	98.1	98.1
$\frac{+37}{50}$	$\frac{+131}{25}$	$\frac{+142}{25}$	$\frac{+150}{25}$	$\frac{+148}{10}$	$\frac{+101}{15}$	$\frac{+22}{25}$	$\frac{+23}{40}$	$\frac{+53}{25}$

98.1	94.3	93.0	93.2	89.9	85.6	84.6	90.7	92.3
$\frac{+27}{45}$	$\frac{+71}{25}$	$\frac{+84}{15}$	$\frac{+82}{15}$	$\frac{+115}{10}$	$\frac{+158}{15}$	$\frac{+168}{25}$	$\frac{+127}{40}$	$\frac{+91}{25}$

105.4	104.9	103.7	101.3	97.8	94.5	91.8	82.4	83.6
$\frac{+70}{45}$	$\frac{+215}{25}$	$\frac{+123}{15}$	$\frac{+01}{15}$	$\frac{+31}{15}$	$\frac{+69}{25}$	$\frac{+91}{35}$	$\frac{+190}{50}$	$\frac{+178}{20}$

101.44

114.1	112.3	111.0	108.6	105.6	103.9	97.7
$\frac{+28}{25}$	$\frac{+18}{15}$	$\frac{+22}{15}$	$\frac{+47}{15}$	$\frac{+22}{15}$	$\frac{+102}{25}$	$\frac{+156}{50}$

112.27

TP 12.18 156.25 0.53 144.07

10+75

10+50

TP 11.04 144.60 0.10 133.56

10+25.82 - E.L. Furcko From South

BM 4.65 129.01

10+0

9+74.11 - W.L. Furcko From South

TP 12.11 133.66 0.98 121.55

9+60

122.33

142.5
2.1
25

142.2
2.1
15

142.0
2.6
25

141.7
2.9
15

141.3
2.3
25

140.6
2.0
25

138.2
4.4
25

138.0
4.4
15

137.8
4.8
25

137.5
2.1
15

137.2
2.4
25

137.0
2.6
25

144.60

133.2
0.5
25

133.2
0.5
15

132.9
0.8
25

132.5
1.2
15

132.2
1.5
25

128.5
5.2
25

128.2
5.2
15

127.6
6.1
25

127.6
6.1
15

127.3
6.4
25

121.7
1.0
25

121.4
1.2
15

121.4
1.2
25

121.6
1.2
15

121.4
1.2
25

133.66

119.5
2.8
10

118.7
3.6
25

118.4
3.9
15

118.1
4.2
25

117.6
4.7
15

117.6
4.7
25

117.1
5.2
10

122.33

Mildred

12+70

12+35

TP 1211 167.30 1.06 155.19

12+0

11+70

11+35

11+0

136.25

Lt.

S

Rt

35

162.4	161.7	160.9	159.9	159.3	158.5
$\frac{4.9}{25}$	$\frac{5.7}{15}$	$\frac{6.1}{15}$	$\frac{7.1}{15}$	$\frac{8.0}{25}$	$\frac{8.8}{25}$

158.4	157.8	156.8	156.0	155.9	155.5
$\frac{8.9}{25}$	$\frac{9.5}{15}$	$\frac{10.5}{15}$	$\frac{11.0}{15}$	$\frac{11.4}{25}$	$\frac{11.8}{25}$

167.30

155.7	155.3	154.6	154.1	153.5	153.1
$\frac{2.6}{25}$	$\frac{1.0}{15}$	$\frac{1.7}{15}$	$\frac{2.2}{15}$	$\frac{2.8}{25}$	$\frac{3.2}{25}$

152.9	152.4	151.7	150.9	150.6	150.1
$\frac{3.1}{25}$	$\frac{3.9}{25}$	$\frac{4.1}{15}$	$\frac{5.1}{15}$	$\frac{5.7}{25}$	$\frac{6.3}{25}$

149.7	149.3	148.7	148.1	147.8	147.6
$\frac{6.6}{25}$	$\frac{7.0}{15}$	$\frac{2.1}{15}$	$\frac{3.2}{15}$	$\frac{3.5}{25}$	$\frac{3.7}{25}$

146.5	146.1	145.4	144.6	144.1	143.6
$\frac{9.8}{25}$	$\frac{10.2}{15}$	$\frac{10.9}{15}$	$\frac{11.7}{15}$	$\frac{12.2}{25}$	$\frac{12.7}{25}$

156.25

At

Z

Rt

BM

292

175.05

HER Ppt
Mildred
Garland

13+6294 = M L Garland

13+35

TP

1134

177.97

0.67

166.62

13+0

167.30

11721
59
25

171.2
68
15

1696
84

168.2
98
15

1674
106
25

14901
79
25

169.1
89
15

167.6
104

1660
120
15

164.7
132
25

1638
142
25

166.1
13
25

155.7
17
15

164.3
3.0

163.1
4.2
15

162.2
5.1
25

161.9
6.3
25

167.30

Cross Section Azusa St
 Riley to Linda Vista Road
 East Line Stationing

indexed
 c.s.k.

1+0

0+75

0+50

0+25

0+07

0+0 = H.L. Riley

BM 7.63 35.49

Reduced 7 Plotted 4-25-42 - C.B.H.

27.86

406 of
 Riley + F.L.
 Azusa
 10922

April 1442

St-N

S

RT-S

37

18.9

156
 50

22.2

133
 25

26.2

63
 5

28.0

65

29.1

64
 11

29.4

62
 5

28.2

72
 25

24.4

111
 32

24.0

115
 45

21.0
 115
 45

23.1
 134
 25

26.8
 77
 5

28.9
 66
 5

24.7
 68

26.5
 70
 11

29.1
 64
 5

25.5
 100
 25

28.4
 71
 40

28.8
 67
 10

30.5
 50
 25

30.5
 50
 19

28.7
 62
 5

24.4
 71

28.2
 78
 10

28.8
 77
 5

22.1
 28
 15

31.0
 45
 20

31.0
 45

31.2
 42
 20

28.4
 71
 5

28.1
 71

28.0
 74
 10

28.7
 68
 15

31.7
 88
 25

30.5
 50
 25

30.7
 48
 25

30.5
 50
 20

27.9
 71
 5

28.0
 76

28.2
 70
 25

28.5
 70
 20

30.7
 88
 25

30.4
 50
 25

30.5
 50
 25

30.2
 50
 20

27.7
 71
 5

28.0
 75

28.1
 74
 15

28.2
 74
 25

35.49

2+40

2+20 = 5L Louetta

2+0

1+25

1+50

1+22 : Existing 24" Corq Iron Cols

1+05

35.49

Lt.

32.47

Rt.

Rt.

30.2

6-13 M.H. Col

29.2
48
15

31.5
40
15

31.7
58
11

31.7
58
11

32.5
50
15

28.2
50
15

25.4
101
45

25.2
90
45

31.5
10
15

31.0
45
15

31.5
48
11

31.2
48
11

31.9
46
15

26.3
92
25

25.9
86
45

29.8
107
45

25.7
98
45

31.2
48
15

30.4
51
15

30.6
49
11

30.4
51
11

31.1
44
15

25.7
98
25

25.5
100
45

24.0
115
45

29.8
107
25

30.1
54
15

30.0
55
15

29.7
58
11

30.4
51
15

24.6
109
25

24.6
109
45

20.3
152
50

20.7
148
25

20.2
141
18

21.2
188
18

29.5
60
15

29.4
61
15

29.4
61
10

29.8
57
15

26.8
87
20

22.1
154
25

22.4
181
25

24.1
144
45

6-13 M.H. Col

6-13 M.H. Col

29.34
61.5
6-13 M.H. Col

35.49

410

3494 27 At. of % = Wly Power Pole ✓

3470

3435

TP 11.37 46.49 0.37 3512

340

2470 = H. Lauretto

B17

372

31.77

2445 = X

3519

N.F. Proppio
Lauretto
Azusa
31.78 Pappo

4

2

Rt

435

20
25

43.3

20
25

418

15
15

402

12
12

407

5
8

409

5
15

438

19
19

427

18
15

425

10
25

401

15
15

382

13
13

384

1
1

385

10
15

401

10
10

393

10
25

306

59
25

315

90
15

358

107
12

359

10.6

318

106
15

375

90
19

366

99
25

350

115
15

4649

357

10
25

342

15
15

340

15
15

339

11
15

344

15
15

337

100
15

332

11
15

327

22
25

330

199
15

331

24
15

330

15
15

325

10
15

318

107
15

318

17
25

323

12
15

323

17
15

325

10
15

316

19
25

3519

5782 255 Rt of $\frac{1}{2}$ = W4 Power Pole ✓

5780

BM

418

5428

* Hub of Mildred
FL HZWA

5765.32 - $\frac{1}{2}$

5740.32 = S-L Mildred

570

4770

TP 12.13 58.46 0.16 46.33

4735

4649

47

2

Rt

828

522

628

155

090

5723

5523

46

32

55

615

525

525

125

425

6623

6023

50

12

23

5120

2121

823

622

222

025

822

422

8825

9725

487

282

112

222

102

82

8025

472

112

471

122

192

122

102

462

452

132

451

426

428

424

424

452

132

14

29

87

81

31

06

06

5846

4649

AZUSA St. 50' wide
8-18-43

Note! Nly. line of this 20' strip Pav.
was proposed E. of the widening
in 1944.

1+00 Sly edge 20' strip Pav. Linda Vista Rd.
(Camp Kearney Rd.)

0+95

0+93

0+75

0+50

0+38 17 Lt. Power Pole Guy

0+15

B.M. Hub 12.88 6716 54.28 Page 40

5+90x32 = 112' Mildred = 0+100

58.46

54.28
0.93
55.21
11.34
43.87 = B.M. Top FH.
NE cor. Mildred
and Linda Vista Rd.
43.87

Lt. 8 PI 41

66.02	61.38	61.84	62.60	63.31	63.97
7.1x 50	5.8 25	5.32 15	4.56	3.85 15	3.39 25
61.3	61.8	62.1	63.3	63.9	
5.9 25	5.4 15	4.5	3.9 15	3.3 25	
62.6	63.2	63.8	65.3	65.2	
4.6 25	4.0 15	3.4	1.8 15	1.0 25	
61.6	62.3	63.1	64.3	65.6	
5.7 25	4.9 15	4.1	2.9 15	1.8 25	
65.5	66.1	66.1	67.1	67.4	
8.2 25	7.5 15	6.5	5.1 15	4.0 25	
56.1	57.8	58.9	59.9	60.1	
10.5 25	9.4 15	8.5	7.3 15	6.5 25	

67.15

1.25
3.4
2.5

55.7
8.8
15

56.0
2.5

57.8
0.9
15

57.5
0.0
25

58.46

Cross Section Benicia
 Riley to Linda Vista Road
 Stationing

Indexed
 C.S.K.

Apr 15 42

Lt=N

Z

Rt=2

42

2+18 217 40/2 = 114 Power Pole

2+0

TP 12.21 64.78 0.44 52.57

1+50

1+0

0+50

0+25

0+0 = N.L. Riley

BM 12.20 53.01

40.81

2 N 00
 Riley
 8401610
 Page 3

Reduced and plotted 4-29-42 G.P.H.

52.9	52.5	53.2	53.5	53.3
11.9	12.3	11.6	11.3	10.5
55	55	55	55	55
50.6	50.3	51.2	51.7	52.11
2.7	1.8	1.3	0.90	0.70
25	25	25	25	25
48.4	48.6	48.1	48.8	49.4
46	44	40	42	42.6
25	25	25	25	25
46.0	46.5	46.2	46.6	46.9
7.0	6.5	6.8	6.1	6.1
25	25	25	25	25
45.3	45.6	45.5	45.1	45.3
7.7	7.4	8.5	7.7	6.6
25	25	25	25	25
43.9	44.0	44.5	43.3	43.6
9.1	9.0	11.5	10.7	10.6
25	25	25	25	25
45.2	45.5	45.2	45.4	45.1
7.8	7.5	7.8	6.6	5.9
15	25	25	25	25

64.78

2507 NOK
 2507 NOK
 2507 NOK

53.01
 N

4125 281 Lt of 2 = W4 Harbor Pole

410

3+94 219 Lt of 2 = W4 Parker Pole

3+75

3+50

3+0

2+6985 = St. Laurette

BM

10.15 54.63

Hub
Laurette
Ben 10.15
54.63

2+1985 = St. Laurette

64.78

516
13.7
50

541 Lt.
10.7
25-El
15

557
9.1
15

589
8.9
15

609
8.9
15

639
8.9
15

522
12.6
50

538
7.3
25

538
5.0
15

608
4.0
10

618
4.0
10

633
1.5
15

639
0.9
25

573
7.5
10

600
4.8
25

613
3.5
15

616
3.2
15

621
2.7
15

629
2.1
25

602
4.6
25

659
4.9
15

606
4.2
15

621
3.7
15

619
3.1
25

571
7.1
25

575
7.3
15

585
6.8
15

628
6.0
15

625
5.5
25

548
9.6
25

558
9.0
15

568
8.0
15

572
7.6
15

570
7.8
25

533
11.4
25

543
11.5
15

574
10.4
15

548
10.0
15

545
10.2
25

6478

5+8998 = H.L. Mildred From West

5+80 28.6 Lt of $\frac{1}{2}$ = My Paper Pole

5+6498 = $\frac{1}{2}$ Mildred From W

BM 10.05 66.35

4 Pipe Mildred to Benicio 8639 Page 27

TP 11.62 76.40 0.00 64.78

5+3983 = H.L. Mildred From East

5+1483 = $\frac{1}{2}$ Mildred From East

4+8983 = S.L. Mildred From East

4+50

64.78

67	64	64	64	64	64	64	64
40	25	25	25	25	25	25	25
69.7	70.0	70.5	71.2	70.6	70.5	69.5	66.1

65.9	66.6	66.7	66.4	65.6	61.0
16.5	9.8	9.7	10.0	10.8	15.4
40	25	25	25	25	50

61.9	62.4	62.2	62.5	61.5	60.7
2.9	2.4	2.6	2.3	2.3	1.6
40	25	25	25	25	25

56.9	57.5	57.7	57.5	57.5	56.9
7.9	7.3	7.1	7.3	7.3	7.9
50	25	25	25	25	25

52.6	53.5	53.6	54.2	53.6	55.1
12.2	11.3	11.2	12.6	11.2	9.7
50	25	25	25	25	25

50.1	51.9	52.2	54.7	56.2	57.4	60.8
14.7	12.9	11.6	10.1	8.6	7.4	7.0
50	25	25	25	25	25	25

64.78

6+88 = S Edge Conc. Paving Linda Vista Road

6+78 21.7 H of E = Wly Poxter Pale

6+75

6+50

6+48.5 = 5 Wire Cross Fence

TP 11.88 88.03 0.26 76.14

6+25

76.40

Lt.

L

Rt.

82.28

5.33
50 on Pav.

84.02

1.00
2.50 on Pav.

84.53

3.49
1.50 on Pav.

85.34

2.68
on Pav.

87.27

1.75
1.50 on Pav.

87.87

1.15
2.50 on Pav.

87.99

0.02
45

83.9

4/10

84.5

3.25
2.5

84.5

3.25
2.5

84.8

3.2

85.0

3.0
2.5

85.1

2.9
2.5

84.3

3.7
40

80.4

7.6
40

80.8

7.2
2.5

80.9

7.5

80.8

7.2

80.2

7.8
1.8

81.0

8.0
2.5

78.8

9.7
40

88.03

75.8

0.6
40

75.9

0.5
2.5

76.1

0.3
1.5

76.4

0.0

76.1

0.3
1.5

76.0

0.4
2.5

74.9

1.5
40

76.40

Cross Section Colusa St
Riley to Linda Vista Road

Indexed
c.s.k.

Reduced
Plotted 4-29-42
C.B.H.

1437			
1408	23.8	Lt of $\frac{1}{2}$ = 5/4 Picket Fence	✓
140	25.2	Rt of $\frac{1}{2}$ = 1 1/4 Lat 4 Fence	✓
0+93			
0+82	22.5	Lt of $\frac{1}{2}$ = 1 1/4 Lat 4 Fence	✓
0+70	25.2	Rt of $\frac{1}{2}$ = 5/4 Lat 4 Fence	✓
0+56			
0+47	25.2	Rt of $\frac{1}{2}$ = 1 1/4 Picket Fence	✓
0+25			
0+02	20.0	Lt of $\frac{1}{2}$ = 1 1/4 Anchor Pole	✓
0+0	23.3	Lt of $\frac{1}{2}$ = 5/4 Lat 4 Fence	✓
	25.2	Rt of $\frac{1}{2}$ = 5/4 Picket Fence	✓
BM	11.71	66.96	55.25

Hub
Riley +
Colusa
Page 6

April 10 42
Sisson
North
W. Moore

Lt: Rt

P=F

46

621	49	43	59	92	638	648	554
40	25	15	15	22	15	15	15
610	51	48	52	629	640	644	
25	15	15	15	15	15	15	
610	51	48	52	615	624	627	672
25	15	15	15	10	15	15	280
595	598	591	593	599	608	617	617
75	77	79	77	70	75	70	75
584	581	582	585	573	605	609	
86	84	108	104	97	65	61	
25	25	15	15	15	20	25	
			66.96				

51
23.8
5/4
Sisson
Diff. File

280
Colusa
Page 6

3+35 20' ht of $\frac{1}{2}$ = $\frac{1}{4}$ 18" Palm Tree ✓

TP 11.58 89.83 0.03 78.25

3+15 21' ht of $\frac{1}{2}$ = $\frac{1}{4}$ 18" Palm Tree ✓

3+0

2+94 18' ht of $\frac{1}{2}$ = $\frac{1}{4}$ 5" Acacia Tree ✓

2+78 18.5' ht of $\frac{1}{2}$ = $\frac{1}{4}$ 4" Acacia Tree ✓

2+69.65 = N.L. Lauretta 24.8 ft of $\frac{1}{2}$ = 5 1/2 Wire Fence ✓

BM 8.85 69.43

2 Hus Lauretta Colusa 69.46 ✓

2+19.65 = N.L. Lauretta 24.3' ht of $\frac{1}{2}$ = $\frac{1}{4}$ Picket Fence ✓

2+19 20' ht of $\frac{1}{2}$ = $\frac{1}{4}$ 1/2" Pencil Pole ✓

TP 11.91 78.28 0.59 66.37

1+75

1+50

66.96

716 718 783 788 790 803 810 881.7
122 120 115 110 108 95 82 88.1
40 25 15 10 5 7 15 25

89.83

785 789 745 746 747 764 770 776
140 141 128 127 126 119 115 107
35 25 15 10 5 7 15 25

788 713 716 716 727 732 737
75 70 67 67 56 51 46
25 15 10 10 15 15 25

674 676 678 679 681 685
109 107 105 104 99 88
25 15 10 10 15 25

78.28

638 646 648 650 650 663 667
32 24 22 20 20 17 16
4000 DIRT 25 15 10 10 15 25

135
09
32.5
32.5 + 9000 DIRT Floor

66.96

5+56

R11

2.90

101.54

2 Hub of Mildred
F.L. Colours
101.57

TP

3.84

104.44

0.05

100.60

4+8911 = S.L. Mildred

4+50

4+44

242 R1 of 2 - My Wire Fence ✓

4+25

TP

11.43

100.65

0.61

89.22

4+0

3+72

23.7 H of 2 = Fly Parrot Pole + My Wire Fence ✓

89.83

898

136

40

885

209

30

844

200

25

889

155

15

901

143

15

931

113

8

961

82

15

985

159

25

1006

150

25

104.44

243

61

25

257

150

25

267

10

10

274

150

25

283

10

10

100.7

10

25

895

112

40

909

120

25

916

91

20

925

82

15

925

72

15

940

67

4

960

47

15

983

24

25

872

125

40

886

121

25

897

110

15

905

102

15

907

100

4

918

89

6

931

76

15

942

65

25

100.65

845

53

40

818

10

25

864

61

15

873

25

15

883

15

15

894

10

15

905

10

25

810

88

40

820

78

25

829

69

15

845

63

15

837

61

4

853

45

6

860

42

15

868

50

25

89.83

TP 12.07 116.21 0.80 10414

6740

6710

670

5786

5775

5764

10444

St

S

pt.

49

92.3 121 40	87.4 170 25	87.4 200 30	86.2 182 15	92.3 121 7	941 103	95.0 9.1 15	95.6 88 15	97.6 68 25	102.5 59 40	92.3 121 7	941 103	95.0 9.1 15	95.6 88 15	97.6 68 25	102.5 59 40
92.8 116 50	93.2 112 30	90.8 132 25	87.8 166 15	85.9 185 10	941 103	95.0 9.1 15	95.6 88 15	97.6 68 25	92.3 121 7	941 103	95.0 9.1 15	95.6 88 15	97.6 68 25	102.5 59 40	
93.5 109	94.0 104 25	94.1 103 15	94.0 101	87.9 185	947 97 10	947 97 15	96.3 81 25	97.6 68 40	93.5 109	94.0 104 25	94.1 103 15	94.0 101	87.9 185	947 97 10	947 97 15
97.0 74 40	96.8 76 25	96.9 75 5	96.9 75 5	944 80	947 97 10	947 97 15	96.3 81 25	97.6 68 40	97.0 74 40	96.8 76 25	96.9 75 5	96.9 75 5	944 80	947 97 10	947 97 15
97.0 74 40	95.8 70 25	95.4 70 25	95.5 70 25	95.7 87 6	92.4 120	96.24 820 15	95.3 91 5	95.6 80 25	97.0 74 40	95.8 70 25	95.4 70 25	95.5 70 25	95.7 87 6	92.4 120	96.24 820 15
97.0 74 40	95.8 70 25	95.4 70 25	95.5 70 25	95.7 87 6	92.4 120	96.24 820 15	95.3 91 5	95.6 80 25	97.0 74 40	95.8 70 25	95.4 70 25	95.5 70 25	95.7 87 6	92.4 120	96.24 820 15

8.11.13
B.1.1.13
C.1.1.13
D.1.1.13

10444

7+21.4 = Sky Conc Paving on Curve Linda Vista Road

7+15

7+0

6+70

116.21

21

2

RT

110.51

5.70
50 on Pav

112.02

4.19
25 on Pav

112.59

3.7
15 on Pav

113.45

2.75
5 on Pav

114.30

1.9
5 on Pav

114.91

1.30
5 on Pav

116.21

0.50
5 on Pav

112.11

1.0
5 on Sky Pav

112.6

2.6
15

112.9

2.8

114.2

2.0
10

113.5

2.7
15

113.6

2.4
25

112.8

2.1
10

108.4

7.0
40

109.0

7.2
35

109.1

7.1
15

110.2

8.0

110.6

5.1
15

110.5

4.7
25

110.9

5.0
40

104.9

11.2
10

104.6

11.6
25

104.8

11.4
15

106.6

9.6
7

106.6

9.7
7

105.1

11.1
15

104.4

11.8
25

114.2

12.0
40

116.21

Cross Section Brunner St.
Lauretta to Ruby

Indexed
C.S.K.

April 8, 48

N-X

Rt-E

51

1+19 24.9 1/2 = 1/4 wire fence ✓

1+0

TP 11.52 10290 0.15 9238

0+70

0+35

0+12.35 = Opp. H. Lauretta on Rt

0+0 = H. Lauretta on 5109000 ✓

TP 11.65 92.53 0.45 80.88

BM 11.87 81.33 69.46

Notes Revised & Plotted
Profile 2934 N-2-42
C.S.K.

0 1/2 Hub
Lauretta +
Brunner

0 1/2 Hub
Lauretta +
Colusa
Page 18

99.6
4.3
25

98.8
4.5
25

97.1
6.8
25

96.7
7.2
25

95.9
8.0
25

95.8
10.1
25

94.0
4.5
25

93.4
4.9
25

92.7
4.2
25

92.3
0.2
25

91.7
0.8
25

90.5
2.0
25

89.4
4.1
25

89.4
3.1
25

88.7
3.6
25

88.7
3.9
25

88.3
4.2
25

87.8
4.7
25

88.7
5.8
25

86.3
1.2
25

86.2
6.3
25

85.8
6.7
25

85.1
7.1
25

84.7
7.8
25

83.0
9.5
27.9

82.7
8.8
26.7

82.6
7.9
25

82.1
7.8
26.7

82.7
7.8
27.9

92.53

070 = H.L. Mildred on Diagonal

B.M.

6.21

119.46

002 Hub
visited 4
Brugger Friends
119.45 R32

274493 = S.L. Mildred on Diagonal

TP

11.29

12567

0.92

114.38

273258 = S.L. Mildred on X

2730

16.11 of 1/2 - 1/4 Harbor Pole ✓

240

1470

TP

11.58

11530

0.18

108.72

1435

103.90

5421
0.8
258

1239
1.3
21

47
1235
15.5

1240
5.7

1228
2.9

1210
4.7
15.5

1194
6.2
258

1151
6.2
27.9

1186
7.1
16.7

1122
8.5

1157
10.0
16.7

1139
11.8
27.9

12367

1196
14.2
25

1184
12.1
15

1158
10.5

1173
2.0
15

1119
3.4
25

1066
8.7
25

1122
10.1
25

1142
11
15

1121
8.2

1102
5.1
15

1086
6.7
25

1036
11.7
46

1025
12.8
53

1116
8.9
25

1106
14.7
15

1083
7.0

1062
9.1
15

1048
12.5
25

1032
12.1
35

992
16.1
50

11530

1057
11.8
25

1051
11.2
15

1038
0.1

1018
2.1
15

1006
2.2
25

967
7.2
50

103.90

1765 26.3 Lt of L = 11/4 Pale Fence ✓
 1749 12.5' Lt of L = 5/4 Pale Fence ✓
 1747 18.0 Rt of L = 5/4 of 11 Small Dec. Trees ✓
 1735

170

0198 20.8 Lt of L = 11/4 Power Pole ✓
 0470

TP 11.10 136.58 0.19 125.48

0425

0406.58 = opp H6 Mildred on Rt

125.67

Lt. Rt. Rt.

131.9	131.9	131.9	131.4	130.0	128.5	125.5
47 25	47 15	47	57	66 15	81 25	111 40
131.7	131.9	131.7	131.3	130.6	129.6	128.3
49 25	47 25	49 15	53 25	58 15	70 15	83 25
132.3		131.6	131.3	128.7	127.3	125.2
43 25		50 15	53 15	79 15	93 25	114 40
132.1	131.6	130.3	130.2	128.4	127.4	126.4
45 25	51 20	63 15	64 15	82 25	92 15	108 25
129.1	128.7	127.5	127.4	127.2	126.2	124.7
43 25	49 25	49 20	47 15	45 15	45 25	49 15
126.7	124.6	124.1	121.4	119.4		
49 25	41 20	41 15	43 15	63 25		
125.67						

LT. 2 PL

BM 2.81 13877

SE 738 P.H. 101
Lindovistafors
+ Brunner St
13887
H 274. P 54

TP 7.27 141.58 2.27 13431

2+26.87 = S-L Ruby on diagonal

2+20.29 = opp S-L Ruby on Lt

2+15 14.5 Pt of 2 = 4/4 of 11 Small Eye Trees ✓

2+0

1491

136.58

8251
151
258
1326
10
155
1320
46
1313
85
1305
61
155

828
1321
3.8
28
1325
11
15
1319
47
1314
62
1305
61
15

1318
18
10
1322
44
25
1322
44
15
1328
48
55
1314
55
1304
67
15
1285
91
25
1245
101
40

151.91
167
44.4
136.58
Carpenter
10.7100

Cross Station Furca St.
Riley to Ruby

Indexed
O.S.K.

April 18/42

Lt-M

Rt-F

55

1470

960
12.5
40

981
104
25

993
92
15

1009
76

1023
62
15

105.2
52
25

1435

937
148
40

951
124
25

962
123
15

981
104

993
92
15

995
90
20

100.5
80
25

TP 11.70 108.50 0.46 96.80

108.50

140

904
69
40

920
52
25

928
75
15

943
80

951
52
15

957
76
15

973
80
25

0+70

870
103
40

890
80
25

910
72
15

917
56

927
46
15

936
40
21

947
26
25

0+35

841
137
40

855
121
25

863
110
15

875
98

884
89
15

893
80
17

907
66
25

0+32 237 Rt of L = Fly Anchor Pole

0+0 - N.L. Riley

873
110
25

885
148
15

895
128
8

927
146
15

930
143

940
132
12

963
110
15

977
96
25

BM 9.64 97.26 87.62

N.E. Prop Pipe
Riley & Furca
Page 9

97.26

Reduced and Plotted
5-2-42 C.B.H.

0+70

109.3	112.4	113.9	115.7	117.8	119.0
8.7	5.8	4.1	2.5	2.2	1.0
40	25	15	25	15	25

0+54 141 Rt 1/2 - Ely Anchor Pole

108.0	109.1	110.4	112.0	113.7	114.6
11.0	8.9	7.6	6.0	4.5	3.4
40	25	15	25	15	25

0+35

104.5	106.4	107.6	109.3	110.6	111.6
13.5	11.6	10.4	8.7	7.4	6.4
40	25	15	27	15	25

0+06.58 = H.L. Lauritto on Rt

104.8	106.1	108.5	110.1	111.6
13.2	11.9	9.5	7.9	6.4
25.8	13.5	15.5	15.5	25.8

0+0: H.L. Lauritto on Diagonal

TP 11.66 117.96 2.20 106.30

on 2 Hops
Lauritto
Ely to So
106.30
Page 21

117.96

2+1968 = S.L. Lauritto

101.6	102.9	104.5	106.4	107.5
6.9	5.6	4.0	2.1	1.0
25	15	40	15	25

2+0

98.4	100.3	101.5	102.8	104.5	106.0
10.1	8.7	4.0	5.9	4.0	2.5
40	25	15	15	15	25

108.50

108.50

TP 12.15 14.13 0.41 12898

on 2 Herb
Mildred y
Eureka
129.01
Page 84

2127.01 - S.L. Mildred on Diagonal

2120.43 - S.L. Mildred on Lt.

210

1470

1435

TP 11.43 129.39 0.00 117.96

140

117.96

121.6	123.4	127.5	130.6	132.1
79	60	19	+12	+27
258	15.5		16.5	258

121.5	123.5	127.0	129.8	131.3
79	59	24	+0.4	+1.9
25.	13		15	25

117.3	120.1	122.0	125.1	127.9	130.0
121	9.2	7.4	12	1.5	+0.6
40	25	15	16	15	25

115.4	118.7	120.5	123.3	126.7	128.1
140	107	89	61	27	1.5
40	25	15		15	25

113.4	116.8	118.4	120.9	123.4	125.4
150	126	110	85	30	40
40	25	15		15	25

		129.39			
116.9	114.2	105.9	118.5	120.7	122.2
7.1	2.8	2.1	+0.5	+2.7	+4.2
40	25	15		15	25

117.96

TP 8.76 149.58 0.81 140.82

1735

133.8

$\frac{20}{10}$

136.1

$\frac{50}{25}$

137.9

$\frac{52}{15}$

140.7

$\frac{04}{15}$

142.8

$\frac{42}{15}$

145.1

$\frac{40}{25}$

170

130.2

$\frac{10.9}{40}$

133.4

$\frac{77}{25}$

135.4

$\frac{52}{15}$

137.9

$\frac{52}{15}$

140.8

$\frac{02}{15}$

142.6

$\frac{15}{25}$

0770

127.2

$\frac{13.9}{40}$

131.0

$\frac{10.1}{25}$

133.2

$\frac{7.9}{15}$

135.6

$\frac{5.5}{15}$

138.7

$\frac{2.1}{15}$

140.7

$\frac{0.9}{25}$

0735

124.7

$\frac{16.1}{40}$

127.8

$\frac{13.2}{25}$

130.4

$\frac{10.7}{15}$

133.7

$\frac{7.4}{15}$

136.2

$\frac{4.9}{15}$

138.2

$\frac{2.9}{25}$

0706.58 = Nk of Mildred on Rt

122.6

$\frac{18.5}{40}$

126.2

$\frac{14.9}{25}$

128.5

$\frac{12.6}{15}$

131.6

$\frac{9.5}{15}$

133.9

$\frac{7.2}{15}$

135.7

$\frac{5.1}{25}$

070 = Nk Mildred on diagonal

125.0

$\frac{16.1}{25.8}$

127.2

$\frac{13.9}{25.5}$

130.9

$\frac{10.2}{15.5}$

133.5

$\frac{7.6}{15.5}$

135.7

$\frac{5.4}{25.8}$

14/13

14/13

BM

734

142.24

on Hub
S.L. Ruby
Z. Furcko

2+2733 = S.L. Ruby on Diagonal

2+20.75 = S.L. Ruby on Lt.

2+0

1+90

149.58

138.0

11.4
25.8

139.8

9.8
25.5

142.3

7.0

145.2

9.1
25.6

146.8

2.0
25.8

138.2

11.4
25

139.9

9.7
15

142.5

7.1

145.4

1.3
15

147.2

2.1
25

134.8

11.8
26

138.1

11.5
25

140.2

9.4
15

142.8

5.8

145.2

1.1
15

146.8

2.8
25

135.0

11.6
26

137.6

12.0
25

139.6

12.0
15

142.6

7.2

145.1

4.5
15

146.2

2.1
25

149.58

Cross Section Goshes St
Riley to Linda Vista Road

indexed
C.S.K.

TP 12.02 143.58 0.02 131.56

1+35

1+0

TP 11.72 131.58 0.11 119.86

0+70

0+35

TP 11.51 119.97 0.47 108.46

0+0 = H.L. Riley

BM 4.36 108.93 104.57

5th Prop. Pt.
Riley & Franco
Page 11

Reduced & Plotted 5-5-92 C.B.H.

April 28 42

60

Lt.

S

Rt.

124.9
5.7
2.5

124.9
5.7
2.5

125.0
5.6
2.5

125.3
5.6
2.5

125.4
5.7
2.5

125.5
5.7
2.5

120.0
4.6
2.5

119.7
4.9
2.5

119.4
4.7
2.5

119.3
4.6
2.5

119.3
4.6
2.5

119.3
4.6
2.5

131.58

115.6
4.4
2.5

114.9
5.1
2.5

114.8
5.2
2.5

114.8
5.2
2.5

114.9
5.1
2.5

114.8
5.2
2.5

111.2
8.8
2.5

110.7
9.3
2.5

109.9
10.1
2.5

109.5
10.5
2.5

109.5
10.5
2.5

109.1
10.9
2.5

119.97

106.3
8.6
2.5

105.9
8.0
2.5

105.3
8.6
2.5

104.5
9.8
2.5

102.9
8.0
2.5

100.9
8.0
2.5

108.93

JP 1234 165.89 0.16 152.55

3735

320

2790.06 = H.L. Lauretta

JP 1215 153.71 2.02 141.56

on 2 Hub
Lauretta
Fl. Gables
14139 P24

272006 = S.L. Lauretta

210

1470

14358

61

8

PT

150.1
56
40

150.8
29
25

151.4
20
15

152.0
17

152.6
14

152.7
10
25

147.0
57
40

146.9
58
25

147.2
55
15

147.9
50

148.2
55
15

148.3
59
25

143.7
100
25

143.9
98
15

144.0
97

144.4
93
15

144.5
92
25

15571

137.8
58
25

137.9
57
15

137.9
57

138.1
54
15

138.4
53
25

135.7
84
25

135.1
85
15

135.7
84

135.3
82
15

135.6
80
25

130.1
120
25

130.6
130
15

130.6
130

130.7
129
15

131.1
125
25

131.2
124
16

14358

5714.68 = $\frac{1}{2}$ Mildred4789.68 = $\frac{1}{2}$ Mildred

4790

TP 1225 178.02 0.12 165.77

4735

470

3770

165.89

LH

R

RH

169.5

 $\frac{83}{25}$

170.2

 $\frac{78}{15}$

170.8

74

171.6

 $\frac{64}{15}$

172.2

 $\frac{58}{25}$

174.1

 $\frac{80}{20}$

176.5

 $\frac{65}{25}$

167.4

 $\frac{106}{25}$

167.8

 $\frac{102}{15}$

168.5

95

169.3

 $\frac{87}{15}$

169.7

 $\frac{82}{25}$

172.9

 $\frac{51}{15}$

176.8

 $\frac{12}{25}$

163.8

 $\frac{142}{20}$

165.0

 $\frac{120}{25}$

165.6

 $\frac{124}{15}$

166.4

116

167.8

 $\frac{102}{15}$

167.7

 $\frac{102}{25}$

178.02

160.5

 $\frac{54}{20}$

161.5

 $\frac{44}{25}$

162.1

 $\frac{38}{15}$

163.1

28

164.2

 $\frac{17}{15}$

164.9

 $\frac{10}{25}$

157.0

 $\frac{89}{20}$

157.9

 $\frac{80}{25}$

158.4

 $\frac{75}{15}$

159.5

64

160.4

 $\frac{55}{15}$

160.9

 $\frac{50}{25}$

153.7

 $\frac{122}{20}$

154.4

 $\frac{145}{25}$

155.0

 $\frac{109}{15}$

155.7

102

156.6

 $\frac{93}{15}$

156.9

 $\frac{90}{25}$

165.89

740
 TP 10.59 200.17 0.19 189.58

6470

6435

640

5470

TP 11.75 189.77 0.00 178.02

B.M 309 175.00

513968 - N.H. Mildred

17802

N.H. Prop. P. 10
 Mildred
 9/5/62
 17305 P36

182.6
 $\frac{176}{25}$

185.4
 $\frac{148}{25}$

187.0
 $\frac{152}{25}$

189.5
 19.7

192.0
 $\frac{82}{25}$

193.9
 $\frac{50}{25}$

200.17

181.1
 $\frac{82}{25}$

183.8
 $\frac{60}{25}$

185.2
 $\frac{46}{25}$

187.4
 2.4

189.4
 $\frac{0.1}{25}$

190.7
 $\frac{+0.9}{25}$

178.8
 $\frac{110}{25}$

180.7
 $\frac{91}{25}$

181.8
 $\frac{80}{25}$

183.3
 6.5

185.2
 $\frac{4.6}{25}$

186.2
 $\frac{2.6}{25}$

175.6
 $\frac{14.2}{25}$

178.1
 $\frac{14.7}{25}$

178.6
 $\frac{11.2}{25}$

179.7
 10.1

181.1
 $\frac{8.2}{25}$

181.8
 $\frac{8.0}{25}$

173.8
 $\frac{16.0}{40}$

174.9
 $\frac{14.9}{25}$

175.7
 $\frac{14.1}{25}$

176.7
 13.1

177.7
 $\frac{12.7}{25}$

178.4
 $\frac{11.4}{25}$

189.77

172.1
 $\frac{5.9}{25}$

172.8
 $\frac{5.2}{25}$

173.7
 4.2

174.4
 $\frac{3.6}{25}$

175.0
 $\frac{3.0}{25}$

177.0
 $\frac{1.0}{25}$

179.3
 $\frac{+1.3}{95}$

182.7
 $\frac{+4.7}{125}$

8750

TP 0.90 189.02 12.05 188.12

8730

8710.04 - NL Ruby

BM

2.48 197.69

NE From Pipe
Ruby +
Gorbes

778204 - Z Ruby

776004 - S6 Ruby

7435

200.17

L

Z

R

64

177.3	177.0	178.7	181.5	184.1	186.1
167	120	193	7.5	12	29
50	25	15		15	25

189.02

175.9	180.9	182.3	185.1	189.6	192.6
243	198	180	151	196	26
50	25	15		15	25

179.2	183.5	185.6	189.2	193.7	197.7
210	167	146	110	65	25
50	25	15		15	25

181.4	185.4	187.8	192.1	197.3	201.8
188	148	121	81	39	76
50	25	15		15	25

181.9	186.4	188.4	191.9	195.8	200.0
183	128	118	80	71	0
50	25	15		15	25

182.8	186.0	188.4	191.5	195.5	197.0
180	142	118	80	72	32
15	25	15		15	25

200.17

BM		7.14	138.71	
TP	0.73	145.85	12.12	145.12
TP	0.82	157.24	11.96	156.42
TP	0.94	168.38	11.97	167.44

9+32.3 = SLY Curve Passing Linda Vista Road Take on at Line of B.

9+25				
TP	2.64	179.41	12.25	176.77

9+15				
9+13		20.4 ft of L - 1/4 Power Pole	✓	

8+90				
------	--	--	--	--

8+75				
------	--	--	--	--

18902

41.

2

PT

65

S TOP OF HWY
Linda Vista Rd.
7.85 runner
138.77
p 54

167.88	170.85	172.38	173.86	176.91
11.53 75 0.7 Curve of 20.1m	8.86 25	7.02	5.55 25	2.50 75

170.8	171.4	172.4	173.4	174.0
8.6 25	8.0 15	7.0	6.0 15	5.1 25

179.41

170.2	173.0	173.3	175.2	177.6	179.5
18.8 30	16.0 25	15.7 15	12.8	11.4 15	9.5 25

172.5	174.2	174.7	176.3	178.3	179.3
16.5 30	14.8 25	14.2 15	12.7	10.2 15	8.7 25

177.8	175.0	176.4	178.0	179.6	181.1
12.2 30	14.0 25	13.6 15	11.0	9.4 15	7.9 25

18902

Cross Section Post St. to Machine St.
H.L. Mildred to Linderoth Road.

Indexed
C.S.K.

April 28, 42

H.M.

Z

R.H.F.

66

TP 10.22 106.42 0.38 96.14

170

0775

0750

0740

0725

070 = H.L. Mildred

BM

11.93

96.52

84.57

Reduced & Plotted Profile 2936
C.B.H. 5-15-1942

H.I. Prop Hub
Mildred's
Post
Page 28

90.1	91.5	92.1	93.5	94.5	95.0
6.4 40	5.0 25	4.4 15	5.0 15	2.0 15	1.5 25

87.6	88.7	89.5	90.5	91.4	92.1	93.3
8.9 40	7.8 25	7.0 15	6.0 15	5.1 15	4.1 25	3.3 40

85.5	86.2	87.0	88.0	89.0	89.7	89.9	88.7
11.0 40	10.2 25	9.5 15	8.5 15	7.5 15	6.8 25	6.6 30	7.8 45

84.4	85.2	85.9	87.1	88.2	87.2	88.8
12.1 40	11.3 25	10.6 15	9.4 15	8.2 15	9.2 25	7.7 40

83.2	83.9	84.7	85.6	84.5	85.6	86.9
12.2 40	12.1 25	11.8 15	10.9 15	12.0 5	10.9 15	9.6 25

80.1	80.7	82.6	83.1	84.0	84.6
16.4 25	15.7 15	13.9 7	13.1 15	12.5 15	11.9 25

96.52

1+6106 = 1/2 Pav 129

1+511 = 1/4 Conc Pav 129 Linda Vista Road

1+45

1+42 50 Lt 2/2 = 1/4 Pav 129 Park

1+85

106.42

102.15
1.27
2.3

97.10

8.72
30

99.39

7.02
35

100.08

6.34
13

101.04

5.38

102.01

4.11
13

102.60

3.82
25

102.06

2.36
30

99.7

7.1
35

99.9

6.5
15

100.8

5.6

101.8

4.6
15

102.3

4.1
25

91.1

16.2
50

94.4

12.0
25

95.2

11.2
15

96.9

9.5

98.5

7.6
15

99.3

7.1
25

106.42

Cross Section Mildred
Azusa. to Bericia

Indexed
C.S.K.

HP

L.H.

A

R.S

68

1+25

559
65
25

549
75
15

537
87

524
100

510
114
15

505
119
25

480.0
144
50

1+0

548
65
25

548
66
15

536
88

523
101
10

518
106
15

508
116
25

491
130
10

TP 983 1239 338 5256

62.39

0+75

603
44
25

583
44
15

571
18

525
34
15

511
48
25

495
64
10

0+50

605
46
25

585
46
15

559
60
10

551
68

545
14
10

530
29
15

531
28
25

489
70
55

0+25

600
44
25

579
40
15

564
45
10

557
68

557
40
10

554
64
25

549
40
25

534
45
10

0+0 = P.L. Azusa

546
47
25

548
61
15

547
12

543
76
10

527
47
15

520
49
25

BM 1207 55.94

43.87

Top of
Hyd.
Mildred
bedrock

55.94

Reduced & Plotted 4-28-42 G.B.H.

Mildred

2163

2145

2125

2110

176 H of L - My Potter Pole

210

175

170

62.39

Lt.

Rt.

Rt.

69

28
22

0 520
25

60.6
58

589
5

554
50

554
25

5708
278

56.11
6.28

598
55

587
55

567
55

542
50

538
50

55.35
209

55.63
6.26

578
55

563
55

546
78

526
98

514
110

511
110

564
60

544
80

528
96

514
110

501
122

496
128

481
148

554
70

541
80

532
92

527
117

491
132

474
150

550
74

541
80

536
88

512
112

496
128

498
136

476
148

62.39

6.28
28
22
Elmer
Platform
M. G. C.
Pound Corn
M. G. C.
Pound Corn
M. G. C.
Pound Corn

Mildred

3790

3765

3731 = Cross Hill Fence

3730

3719

370

TP 9.00 71.10 0.29 62.10

2785

62.89

Lt

A

Rt

68.4

68.1

66.1

68.9

61.7

59.1

65.5

68.0

65.3

68.9

62.4

62.2

59.40

159

68.0

65.8

67.9

62.4

62.4

150
15

61.5

65.3

67.5

62.5

62.4

64.9

64.4

62.5

62.1

61.3

60.1

64.9

64.4

62.5

62.1

61.3

60.1

64.5

62.9

63.9

62.3

60.7

60.6

58.5

58.80

66.0

62.2

62.3

60.7

60.6

58.5

58.80

71.10

62.4

60.3

60.0

58.2

55.3

57.95

60.0

60.3

60.0

58.2

55.3

57.95

62.39

150 = 1/2 Sheds
150 = 1/2 Sheds
150 = 1/2 Sheds
150 = 1/2 Sheds

144 = Top of Foundation

Continued on Page 27
this book

4+67.16 = F.L. Benicio

4+42.16 = J. Benicio

8.74

4.72

66.38

2 pipe
Mildred +
Benicio
82.95 Page 44

4+17.16 = M.L. Benicio

71.10

44

8

84

70.5
26
25

68.7
24
25

66.0
51
25

63.3
78
15

60.9
102
25

71.1
20
25

69.6
24
25

66.8
43
25

64.1
70
15

62.5
86
25

69.7
24
25

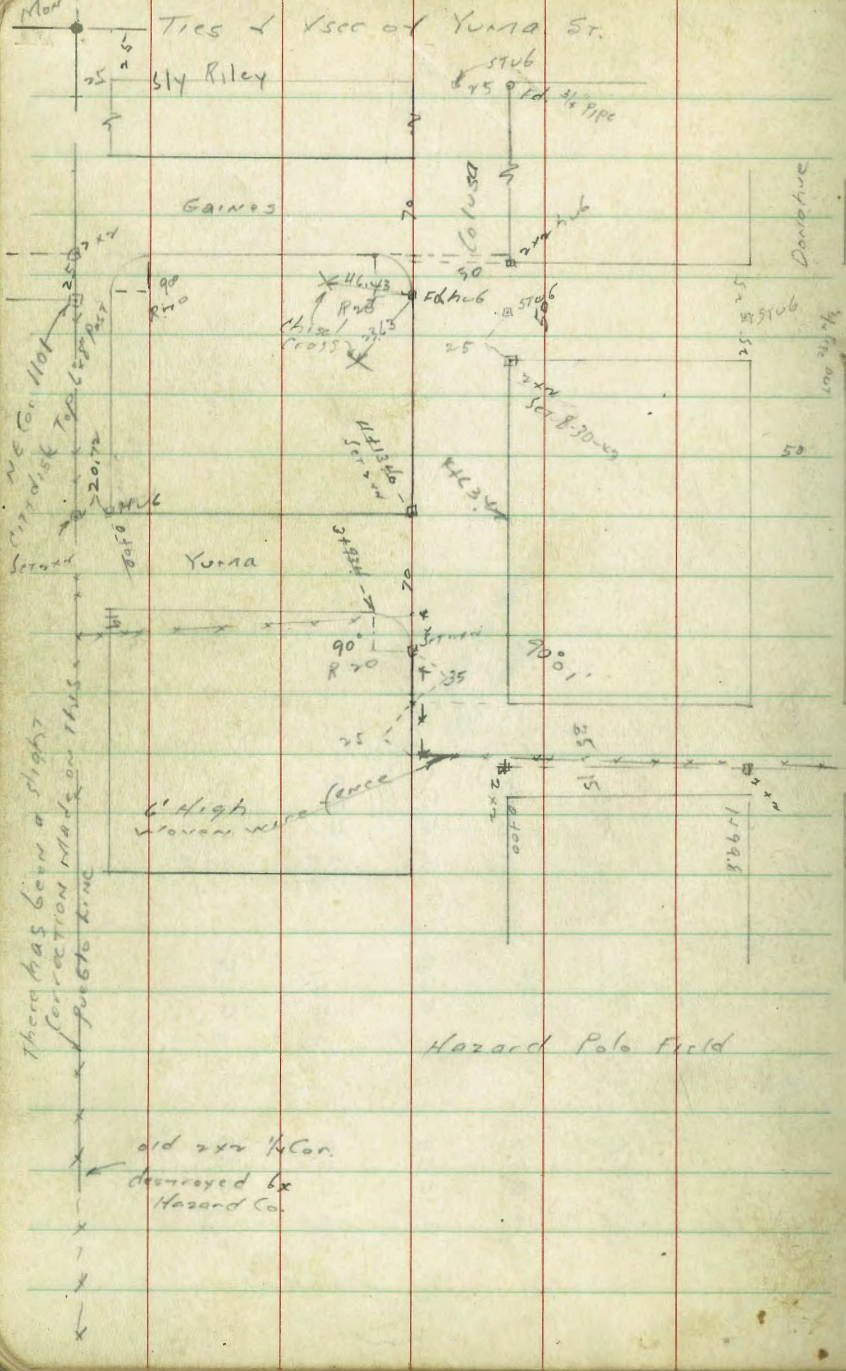
68.7
24
15

66.9
47
25

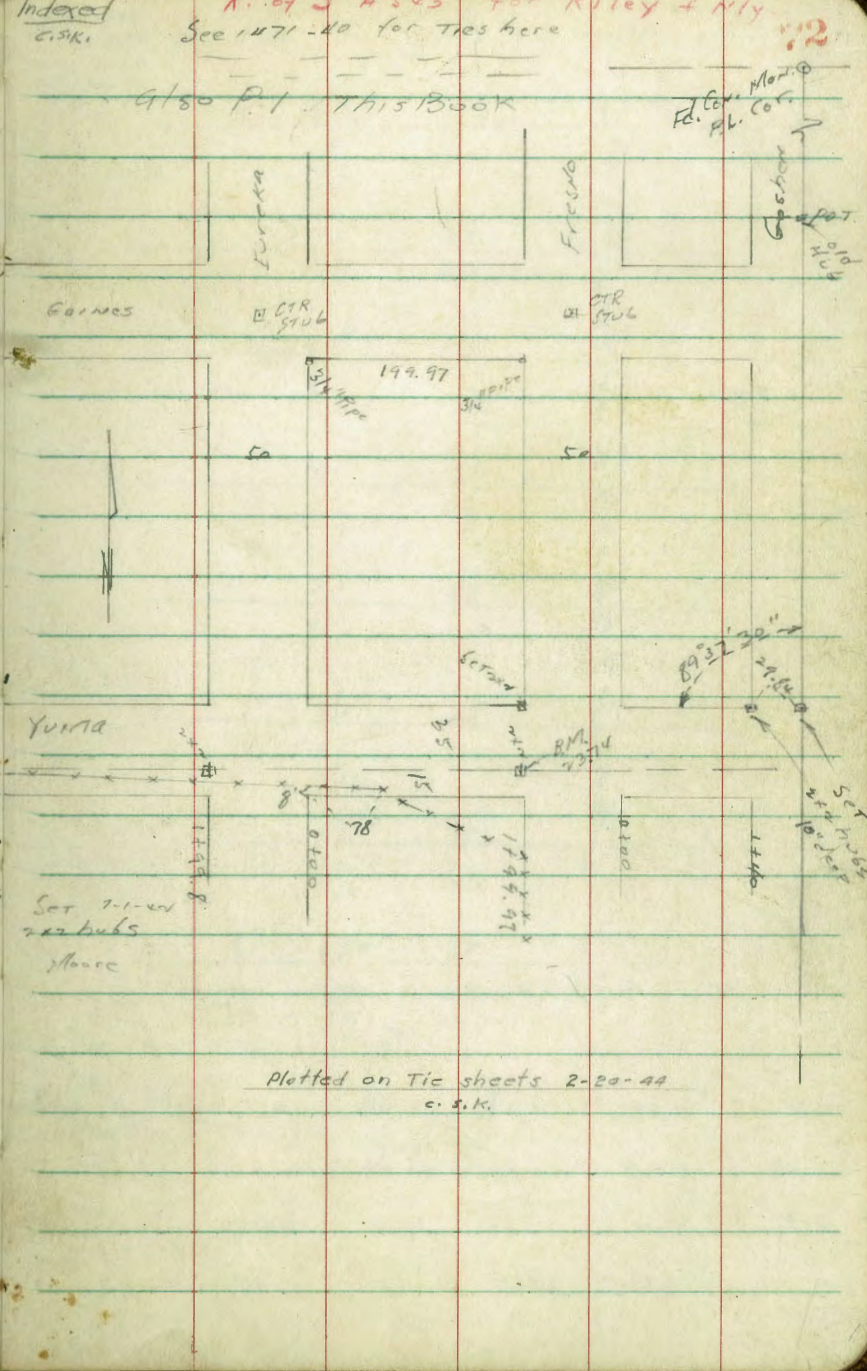
63.8
72
15

62.3
80
25

71.10



There has been a slight contraction marks on this fence line



1 sec of YUMA St. 50' wide

Benicia to Goshen

Howe
Walker
Hardin
Reed
7-1-44

Indexed
C.S.K.

LT

\$

RT

73

150

150

150

0 + 50

0 + 0 EL Benicia

T.P.	11.83	15.48	11.49	10.65
T.P.	00.9	22.14	13.09	22.05
T.P.	11.2	35.11	54.0	33.99
81A 2x2 hub	11.53	39.39		27.86

This - Red
should have
been 13.09

2x2 Hub &
E.C. 2250
& Riley

Reduced & Plotted 7-6-42 S.B.H.

13.7	11.3	9.3
1.8	4.2	6.2
2.5		2.5
11.7	10.2	8.5
3.8	5.3	7.0
2.5		2.5
10.9	9.0	8.1
4.6	6.3	7.4
2.5		2.5
10.1	8.6	7.8
5.2	6.9	7.7
2.5		2.5
9.1	8.0	7.0
6.4	7.5	8.5
2.5		2.5
8.6	7.6	7.2
6.9	7.9	8.3
2.5		2.5
8.5	7.5	7.0
7.0	8.0	8.5
2.5		2.5
8.3	8.36	7.6
7.2	7.09	7.9
2.5	2.5	2.5

gravel
HUB

Please
Correct

15.58
7

Benicia + Gaines

(P. 37)

EL
0+0 Danahoe

1+99.8 WL Danahoe

150

0+50

T.P. SW Cor
Part of
Palasub
Office

361

~~15.57~~

3.57

11.96

11.93 = Conv.

4+63.4 EL Colusa = 0+00 to EAST

4+38.4 E Colusa

4+13.40 WL Colusa

3+93.4

5
15.48

Lr

R

Rr

74

10.7 10.0 9.2

5.8 5.5 1.3
2.5 2.5

10.3 9.5 9.0

5.2 5.0 0.5
2.5 2.5

10.7 9.3 8.8

5.3 4.7 0.7
2.5 2.5

10.7 9.6 8.7

4.8 5.9 1.1
2.5 2.5

11.0 9.1 8.5

4.5 6.0 1.5
2.5 2.5

15.57

15.0 12.3 10.9 10.2 10.1 9.3 8.3

2.5 2.7 4.6 5.3 5.4 6.2 7.2
2.5 4.5 8.0 10.5 13.0

15.0 12.4 11.1 10.3 9.1 8.5 8.4

2.5 2.9 4.4 5.7 6.4 7.0 7.1
2.5 4.5 8.0 10.5 13.0

14.3 12.5 10.4 9.6 8.2 8.2 8.3

1.7 2.0 5.1 5.3 7.3 7.3 7.7
2.5 4.5 8.0 10.5 13.0

13.8 12.0 9.8

1.7 3.5 5.7
2.5 2.5

WL Colusa to EAST

1 + 50

1 + 100

0 + 50

0 + 10 E. L. Furka

IP 12.11 25.39 23.7 23.20

1 + 99.8 W. L. Furka

1 + 50

0 + 50

15.57

34.3	29.6	19.4	18.5	17.4
+ 8.9	+ 4.2	6.0	4.9	8.0
25	24	7		25

26.8	22.4	22.4	16.1	15.5	15.0	12.1
+ 1.4	3.0	3.0	4.3	7.9	10.4	13.3
25	15	9	4		10	15

19.1	18.1	13.0	12.8	11.1	12.8
6.0	7.3	12.0	12.6	13.7	12.6
25	20	10		12	25

14.7	12.4	11.9	11.6	10.5
10.7	13.0	13.5	13.8	14.9
25	15		7	25

39
25.39

14.4	12.1	11.5	9.8	9.7
11	3.4	4.0	5.7	5.8
25	15		10	25

14.0	10.9	10.2	10.1	9.4	9.6
6.5	5.6	5.3	5.4	6.1	5.9
25	15		12	15	25

13.3	10.8	10.3	9.8	9.3	9.4
2.7	5.7	5.2	5.7	6.2	6.1
25	20		12	15	25

10.6	10.2	9.3
6.9	5.3	6.2
25		25

15.57

0 + 80

0 + 50

0 + 0 EL Fresno

W L + 47

W L + 40

W L + 11

W L + 10

T.P. 946 34.36 .33 0.57 24.90

1 + 99.97 W L Fresno

25 39

L

E

R

70

18.5

28.3	28.2	26.3	26.3	27.1	24.8	23.2	21.0	19.8
6.0	6.1	8.0	8.0	7.2	9.5	11.1	13.3	14.5
25	19	15	8.0	8	15	20	25	38

37.0	37.0	28.8	28.1	28.8
+ 2.7	+ 2.7	15.5	6.2	5.5
25	20	5	6.2	5.5

40.9	39.0	28.9	28.2	27.8
+ 6.6	+ 4.7	5.2	6.1	6.5
25	17	14	6.1	25

40.8	38.8
+ 4.5	+ 4.5
25	15

30.1	28.9	27.8
4.2	5.2	6.5
25	15	6.5

30.7	26.1	24.9
3.6	8.2	9.2
	8	

38.6	36.3	29.9	26.9	24.9
+ 4.3	+ 2.0	4.4	8.2	9.4
25	15	13	8	9.4

34.36

35

37.6	36.4	27.4	24.0	23.7	23.74	24.1
+ 12.2	+ 11.0	+ 2.0	4.4	1.7	1.65	1.5
25	17	12	5	1.7	10	15

39

25.42

EM

or HLG

check to BM & Hub

Calusa + Riley P. 6

4.03 55.²⁶~~29~~ 55.25

T.P. 12.21 59.34 2.29 47.11

T.P. 1.82 49.40 12.26 44.59

T.P. 11.64 56.14 2.24 45.00

T.P. 12.29 45.44 1.21 33.15

1+40 = 44.6 Goshen

1+10

33
34.30

LT

2

Pr

77

16!

18✓

25

16!

17.5

55

15!

19✓

16!

17.6

15!

17.3

25

18.9

17.4

18

19.9

20.4

25

34.33
34.34

3036

Azusa St.

0750

E	2.8	27.6
74	4.7	25.7
cb.	5.2	24.2
1/4	5.3	25.1
L	5.4	25.0
1/4	5.9	24.5
cb.	6.2	24.2
TS	4.6	25.8
W	4.8	25.6

0+75

W	6.4	24.0
cb.	6.5	23.9
1/4	6.0	24.4
L	5.6	24.8
1/4	5.3	25.1
cb.	5.0	25.4
E	3.4	27.0

1+00

E	3.3	27.1
cb.	4.7	25.7
1/4	5.1	25.3

3036

79

L	5.4	25.0
1/4	5.7	24.7
cb.	6.3	24.1
W	6.8	23.6
710	8.0	22.4
5' W of 710		
1711 = 8 SDG & Elec. MW	5.15	25.21 on Run
1707.7 on E on end of vial	2.40	27.96
1+25		
-10	6.0	24.4
W	6.0	24.4
cb.	5.8	24.6
1/4	5.3	25.1
L	5.1	25.3
1/4	4.6	25.8
cb.	4.3	26.1
E	2.7	27.7
	1+50	
E	2.2	28.2
cb.	3.7	26.7
1/4	3.9	26.5
L	4.3	26.1
1/4	1.9	25.5
cb.	4.7	25.7
W	4.3	26.1
710	4.6	25.8

Agusa St.
Cont. Back of Book

W	2100	20	28.4
cb.		2.2	28.2
$\frac{1}{4}$		2.2	28.2
$\frac{1}{2}$		2.1	28.3
$\frac{3}{4}$		2.1	28.3
cb.		2.3	28.1
E		1.5	28.9
H75	54.50 + 5016 + E. MH	2.81	27.55 Ritt
	2750		
E		1.8	28.6
cb.		0.9	29.5
$\frac{1}{4}$		0.7	29.7
$\frac{1}{2}$		0.6	29.8
$\frac{3}{4}$		0.6	29.8
cb.		0.7	29.7
W		0.7	29.7
	27935 = N.L. Guinet		
W		+0.6	31.0
cb.		+0.5	30.9
$\frac{1}{4}$		+0.8	31.2
$\frac{1}{2}$		+0.5	30.9
$\frac{3}{4}$		0.3	30.1
cb.		10.1	30.5
E		+0.2	30.6

Profile for Culvert Location #1

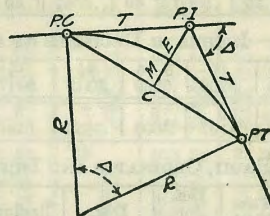
W.L. Agusa			
=0+00		6.67	23.9 on stake
+20		8.6	21.8
+50		10.7	19.7
+75		12.1	18.3
+102.4		12.4	18.0
+108		14.1	16.3
+115		14.2	16.2

Profile for Culvert Location Alternate #2

W.L. Agusa			
=0+00		7.3	23.1
+20		8.1	22.3
+31		8.9	22.1
+45		10.8	19.6
+80		12.4	18.0
+98		12.7	17.7
+99		14.2	16.7
+115		14.3	16.1

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

$$\text{Radius} = R = \frac{50}{\sin \frac{D}{2}} \quad (1) \quad \text{Degree of Curve} = D \text{ and } \sin \frac{D}{2} = \frac{50}{R} \quad (2)$$

$$\text{Tangent} = T = R \tan \frac{\Delta}{2} \quad (3) \quad \text{Length of Curve} = L = 100 \frac{\Delta}{D} \quad (4)$$

$$\text{Middle ordinate} = M = R \left(1 - \cos \frac{\Delta}{2}\right) \quad (5) = R \text{vers} \frac{\Delta}{2} \quad (6)$$

$$\text{External} = E = T \tan \frac{\Delta}{4} \quad (7) = R \div \cos \frac{\Delta}{4} - R \quad (8) = R \text{exsec} \frac{\Delta}{4} \quad (9)$$

$$\text{Long Chord} = C = 2 R \sin \frac{\Delta}{2} \quad (10) \quad \Delta = \text{Central Angle}$$

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta=62^\circ 10'$ $D=8^\circ 20'$. From Table IV for 1° curve $T=3454.1$ and $\div 8\frac{1}{2}=414.49$ ft. From Table V correction=.36 or $T=414.85$ ft. P. C.—Sta. P. I.— $T=157+45.50$. Also from (4) $L=746.00$ and P. T.—Sta. P. C. + $L=164+91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance= 158 —Sta. P. C.=54.50, hence offset= $7.27 (54.50 \div 100)^2=2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26)=2.16$ ft.

Deflections.—Deflection angle= $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft.=(in minutes) $.3 \times C \times D^\circ$ or=defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve=.3 $\times 54.5 \times 8\frac{1}{2}=136.2'$ or $2^\circ 16.2'$, or= $2.50 \times 54.5=136.2'$ from Table III. For Sta. 159 deflection angle= $2^\circ 16.2' + 8^\circ 20' \div 2=6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve $E=960.6$ for $8^\circ 20'=960.6 \div 8\frac{1}{2}=91.27$ and from Table V correction=.10 or $E=91.37$ ft. Or suppose $\Delta=32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E=230.9$ and $\div 42=5.5$ or $D=5^\circ 30'$.

Azusa St.
Cont from P-80

		30.36			
T.P.	6.03	36.25	0.14	30.22	Hub of
cbk starting BM			2.26	33.99	Guinos
				33.99	Benecian
				0.000	

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

90 22 30

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) * 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

MADE IN U.S.A.