1633

LIETZ

LEVEL BOOK

No. 772

TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		⅛ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100 00	0 44	100.00	0.87	99.99	1.31	89
1	99.98	1 75	99 98	2 18	99 97	2.62	99 95	3.05	88
2	99.94	3.49	99 92	3.93	99 91	4 36	99.88	4.80	87
3	99.86	5.23	99 84	5 67	99 81	6.10	99.79	6.54	86
4	99 76	6.98	99 73	7.41	99.69	7.85	99.66	8.28	85
5	99 62	8.72	99.58	9.15	99 54	9.58	99.50	10 02	84
6	99.45	10.45	99.41	10 89	99.36	11.32	99.31	11.75	83
7	99 25	12.19	99 20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16 50	98 56	16.93	80
10	98 48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98 16	19.08	98 08	19 51	97.99	19 94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21 64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24 62	96.81	25 04	96 70	25.46	75
15	96.59	25 88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27 98	95.88	28 40	95 76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30 07	95.24	30.49	72
18	95.11	30 90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93,97	34.20	93.82	34.61	93.67	35.02	93.51	35 43	69
21	93,36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38 67	67
23	92.05	39.07	91.88	39 47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89 69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87 67	48.10	61
29	87.46	48.48	87.25	48 86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52 99	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60 53	79.34	60.88	79.07	61 22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							
Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees.
	DEGREES.		¾ DEGREE.		⅛ DEGREE.		¼ DEGREE.		

Published by the A. Lietz Co., San Francisco, Cal.

MADE IN
U. S. A.

TABLE OF STADIA REDUCTIONS

For a Constant of 100.

ROD VERTICAL.

Min.	0°		1°		2°		3°	
	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff Elev.	Hor Dist.	Diff. Elev.
0'	100.00	.00	99.97	1.74	99.88	3.49	99.73	5.23
2	100.00	.06	99.97	1.80	99.87	3 55	99.72	5.28
4	100.00	.12	99.97	1.86	99.87	3.60	99.71	5.34
6	100.00	.17	99.96	1.92	99.87	3.66	99.71	5.40
8	100.00	.23	99.96	1.98	99.86	3.72	99.70	5.46
10	100.00	.29	99.96	2.04	99.86	3.78	99.69	5.52
12	100.00	.35	99.96	2.09	99.85	3.84	99.69	5.57
14	100.00	.41	99.95	2.15	99.85	3.90	99.68	5.63
16	100.00	.47	99.95	2.21	99.84	3.95	99.68	5.69
18	100.00	.52	99.95	2.27	99.84	4.01	99.67	5.75
20	100.00	.58	99.95	2.33	99.83	4.07	99.66	5.80
22	100.00	.64	99.94	2.38	99.83	4.13	99.66	5.86
24	100.00	.70	99.94	2.44	99.82	4.18	99.65	5.92
26	99.99	.76	99.94	2.50	99.82	4.24	99.64	5.98
28	99.99	.81	99.93	2.56	99.81	4.30	99.63	6.04
30	99.99	.87	99.93	2.62	99.81	4.36	99.63	6.09
32	99.99	.93	99.93	2.67	99.80	4.42	99.62	6.15
34	99.99	.99	99.93	2.73	99.80	4.48	99.62	6.21
36	99.99	1.05	99.92	2.79	99.79	4.53	99.61	6.27
38	99.99	1.11	99.92	2.85	99.79	4 59	99.60	6.33
40	99.99	1.16	99.92	2.91	99.78	4.65	99.59	6.38
42	99.99	1.22	99.91	2.97	99.78	4.71	99.59	6.44
44	99.98	1.28	99.91	3.02	99.77	4.76	99.58	6.50
46	99.98	1.34	99.90	3.08	99.77	4.82	99.57	6.56
48	99.98	1.40	99.90	3.14	99.76	4.88	99.56	6.61
50	99.98	1.45	99.90	3.20	99.76	4.94	99.56	6.67
52	99.98	1.51	99.89	3.26	99.75	4.99	99.55	6.73
54	99.98	1.57	99.89	3.31	99.74	5.05	99.54	6.78
56	99.97	1.63	99.89	3.37	99.74	5:11	99.53	6.84
58	99.97	1.69	99.88	3.43	99.73	5.17	99.52	6.90
60	99.97	1.74	99.88	3.49	99.73	5.23	99.51	6.96
c= .75	.75	.01	.75	.02	.75	.03	.75	.05
c=1.15	1.15	.01	1.15	.03	1.15	.05	1.15	.07
c=1.90	1.90	.02	1.90	.05	1.90	.08	1.90	.12

Min.	4°		5°		6°		7°	
	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor Dist.	Diff. Elev.
0'	99.81	6.96	99.24	8.68	98.91	10.40	98.51	12.10
2	99.51	7.02	99.23	8.74	98.90	10.45	98.50	12.15
4	99.50	7.07	99.22	8.80	98.88	10.51	98.48	12.21
6	99.49	7.13	99.21	8.85	98.87	10.57	98.47	12.26
8	99.48	7.19	99.20	8.91	98.96	10.62	98.46	12.32
10	99.47	7.25	99.19	8.97	98.85	10.68	98.44	12.36
12	99.46	7.30	99.18	9.03	98.83	10.74	98.43	12.43
14	99.46	7.36	99.17	9.08	98.82	10.79	98.41	12.49
16	99.45	7.42	99.16	9.14	98.81	10.85	98.40	12.55
18	99.44	7.48	99.15	9.20	98.80	10.91	98.39	12.60
20	99.43	7.53	99.14	9.25	98.78	10.96	98.37	12.66
22	99.42	7.59	99.13	9.31	98.77	11.02	98.36	12.72
24	99.41	7.65	99.11	9.37	98.76	11.08	98.34	12.77
26	99.40	7.71	99.10	9.43	98.74	11.13	98.33	12.83
28	99.39	7.76	99.09	9.48	98.73	11.19	98.31	12.88
30	99.38	7.82	99.08	9.54	98.72	11.25	98.29	12.94
32	99.38	7.88	99.07	9.60	98.71	11.30	98.28	13.00
34	99.37	7.94	99.06	9.65	98.69	11.36	98.27	13.05
36	99.36	7.99	99.05	9.71	98.68	11.42	98.25	13.11
38	99.35	8.05	99.04	9.77	98.67	11.47	98.24	13.17
40	99.34	8.11	99.03	9.83	98.65	11.53	98.22	13.22
42	99.33	8.17	99.01	9.88	98.64	11.59	98.20	13.28
44	99.32	8.22	99.00	9.94	98.63	11.64	98.19	13.33
46	99.31	8.28	98.99	10.00	98.61	11.70	98.17	13.39
48	99.30	8.34	98.98	10.05	98.60	11.76	98.16	13.45
50	99.29	8.40	98.97	10.11	98.58	11.81	98.14	13.50
52	99.28	8.45	98.96	10.17	98.57	11.87	98.13	13.56
54	99.27	8.51	98.94	10.22	98.56	11.93	98.11	13.61
56	99.26	8.57	98.93	10.28	98.54	11.98	98.10	13.67
58	99.25	8.63	98.92	10.34	98.53	12.04	98.08	13.73
60	99.24	8.68	98.91	10.40	98.51	12.10	98.06	13.78
c= .75	.75	.06	.75	.07	.75	.08	.74	.10
c=1.15	1.15	.09	1.14	.11	1.14	.13	1.14	.15
c=1.90	1.89	.15	1.89	.18	1.89	.21	1.88	.25

Published by the A. LIETZ Co., San Francisco, Cal.

Table of Stadia Reductions.—Continued.

Min	8°		9°		10°		11°	
	Hor Dist.	Diff. Elev	Hor Dist.	Diff. Elev	Hor Dist.	Diff Elev	Hor Dist.	Diff Elev.
0'.....	98.06	13.78	97.55	15.45	96 98	17.10	96 36	18.73
2.....	98.05	13.84	97 53	15.51	96.96	17.16	96.34	18 78
4.....	98.03	13.89	97.52	15.56	96 94	17.21	96 32	18 84
6.....	98.01	13.95	97.50	15.62	96.92	17 26	96.29	18.89
8.....	98.00	14.01	97.48	15.67	96 90	17.32	96 27	18.95
10.....	97.98	14 06	97.46	15.73	96 88	17.37	96.25	19.00
12.....	97 97	14.12	97.44	15.78	96 86	17.43	96 23	19 05
14.....	97 95	14.17	97.43	15.84	96 84	17.48	96 21	19.11
16.....	97 93	14 23	97.41	15.89	96.82	17.54	96.18	19.16
18.....	97.92	14.28	97.39	15.95	96.80	17 59	96.16	19.21
20.....	97.90	14.34	97.37	16.00	96 78	17.65	96.14	19.27
22.....	97.88	14.40	97.35	16 06	96.76	17.70	96.12	19.32
24.....	97.87	14.45	97.33	16.11	96.74	17.76	96.09	19.38
26.....	97.85	14.51	97.31	16 17	96.72	17.81	96.07	19.43
28.....	97.83	14.56	97.29	16.22	96.70	17 86	96.05	19.48
30.....	97.82	14.62	97.28	16.28	96.68	17.92	96.03	19.54.
32.....	97.80	14.67	97.26	16 33	96 66	17 97	96.00	19.59
34.....	97.78	14.73	97 24	16.39	96.64	18 03	95 98	19.64
36.....	97.76	14.79	97.22	16.44	96 62	18 08	95 96	19 70
38.....	97.75	14.84	97.20	16.50	96.60	18.14	95 93	19.75
40.....	97 73	14.90	97.19	16.56	96 57	18 19	95.91	19.80
42.....	97.71	14.95	97.16	16 61	96.55	18.24	95.89	19 86
44.....	97.69	15.01	97.14	16 66	96 53	18.30	95 86	19 91
46.....	97.68	15 06	97.12	16 72	96.51	18 35	95.84	19.96
48.....	97.66	15.12	97.10	16.77	96 49	18.41	95.82	20 02
50.....	97.64	15.17	97 08	16.83	96 47	18.46	95.79	20 07
52.....	97.62	15.23	97.06	16.88	96 45	18.51	95 77	20.12
54.....	97.61	15 23	97.04	16 94	96 42	18.57	95 75	20.18
56.....	97 59	15.34	97 02	16 99	96 40	18 62	95.72	20.23
58.....	97.57	15.40	97.00	17.05	96.38	18 68	95.70	20.28
60.....	97.55	15.45	96.98	17 10	96.36	18.73	95.68	20.34
c= .75.	74	11	74	12	.74	14	.73	15
c=1.15...	1.14	.17	1.13	.19	1 13	21	1 13	.23
c=1.90.	1.88	.28	1.87	.31	1 87	35	1 86	.38

Min.	12°		13°		14°		15°	
	Hor. Dist.	Diff Elev	Hor Dist.	Diff. Elev	Hor Dist.	Diff Elev	Hor. Dist.	Diff. Elev.
0'.....	95.68	20.34	94.94	21.92	94.15	23.47	93.30	25.00
2.....	95.65	20.39	94.91	21.97	94 12	23.52	93.27	25.05
4.....	95 63	20.44	94.89	22.02	94.09	23.58	93.24	25.10
6.....	95.61	20 50	94.86	22.08	94.07	23.63	93.21	25.15.
8.....	95 58	20.55	94.84	22.13	94.04	23.68	93.18	25 20
10.....	95.56	20.60	94.81	22.18	94.01	23.73	93.16	25.25
12.....	95.53	20 66	94 79	22 23	93.98	23.78	93.13	25.30
14.....	95.51	20 71	94.76	22.28	93.95	23.83	93.10	25.35
16.....	95.49	20.76	94.73	22.34	93.93	23.88	93 07	25 40
18.....	95.46	20.81	94.71	22.39	93.90	23.93	93.04	25.45
20.....	95.44	20.87	94.68	22.44	93.87	23.99	93.01	25.50
22.....	95 41	20.92	94.66	22.49	93.84	24.04	92.98	25.55
24.....	95.39	20.97	94.63	22.54	93 81	24.09	92.95	25.60
26.....	95.36	21.03	94.60	22.60	93.79	24.14	92.92	25.65
28.....	95.34	21.08	94.58	22.65	93.76	24.19	92.89	25.70
30.....	95.32	21.13	94.55	22.70	93.73	24.24	92.86	25.75
32.....	95 29	21.18	94.52	22.75	93.70	24.29	92.83	25.80
34.....	95.27	21.24	94.50	22 80	93.67	24.34	92.80	25.85
36.....	95.24	21.29	94 47	22.85	93.65	24.39	92.77	25.90
38.....	95.22	21.34	94 44	22 91	93.62	24.44	92.74	25.95
40.....	95.19	21.39	94.42	22 96	93.59	24.49	92.71	26.00
42.....	95.17	21.45	94 39	23 01	93 56	24.55	92.68	26 05
44	95 14	21.50	94.36	23.06	93.53	24 60	92 65	26 10
46.....	95 12	21.55	94.34	23 11	93.50	24.65	92.62	26.15
48.....	95.09	21.60	94.31	23.16	93.47	24 70	92.59	26.20
50.....	95.07	21.66	94.28	23.22	93.45	24.75	92.56	26 25
52.....	95.04	21.71	94.26	23.27	93.42	24.80	92.53	26.30
54.....	95.02	21.76	94 23	23.32	93.39	24.85	92.49	26.35
56.....	94.99	21 81	94.20	23.37	93.36	24.90	92.46	26 40
58.....	94.97	21.87	94.17	23.42	93 33	24.95	92.43	26.45
60.....	94 94	21.92	94 15	23.47	93.30	25.00	92.40	26 50
c= .75...	73	16	.73	17	.73	19	.72	20
c=1.15. ..	1.12	.25	1.12	.27	1 11	29	1.11	.31
c1.90 .	1.85	.41	1.85	44	1.84	48	1.83	.58

Published by the A. Lietz Co., San Francisco, Cal.

Table of Stadia Reductions.—Continued.

Min	16°		17°		18°		19°	
	Hor. Dist.	Diff Elev	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.
0'.....	92.40	26 50	91.45	27.96	90.45	29.39	89.40	30.78
2.....	92.37	26.55	91.42	28.01	90.42	29.44	89.36	30.83
4.....	92.34	26.59	91.39	28.06	90.38	29.48	89.33	30.87
6.....	92.31	26.64	91.35	28.10	90.35	29.53	89.29	30 92
8	92.28	26 69	91.32	28.15	90.31	29.58	89.26	30.97
10.....	92.25	26.74	91 29	28.20	90 28	29.62	89.22	31.01
12.....	92.22	26.79	91.26	28.25	90.24	29.67	89.18	31.06
14.....	92.19	26.84	91.22	28.30	90.21	29.72	89.15	31.10
16.. . ..	92.15	26 89	91.19	28.34	90.18	29.76	89 11	31.15
18.....	92.12	26.94	91.16	28.39	90.14	29.81	89.08	31.19
20.....	92.09	26.99	91 12	28.44	90 11	29.86	89.04	31.24
22.....	92 06	27.04	91.09	28.49	90 07	29.90	89.00	31.28
24	92 03	27 09	91.06	28.54	90 04	29.95	88.96	31.33
26	92.00	27.13	91.02	28 58	90.00	30.00	88.93	31.38
28.....	91 97	27.18	90.99	28.63	89 97	30 04	88.89	31.42
30.....	91.93	27 23	90.96	28.68	89.93	30.09	88.86	31.47
32.....	91.90	27.28	90 92	28.73	89 90	30.14	88 82	31.51
34.....	91 87	27.33	90.89	28.77	89 86	30.19	88.78	31.56
36.....	91.84	27.38	90 86	28 82	89 83	30.23	88 75	31.60
38.....	91.81	27 43	90 82	28.87	89.79	30.28	88.71	31.65
40.....	91.77	27 48	90.79	28.92	89.76	30.32	88.67	31.69
42.....	91.74	27.52	90.76	28.96	89.72	30.37	88.64	31.74
44.....	91 71	27 57	90.72	29 01	89 69	30.41	88.60	31.78
46.....	91.68	27 62	90 69	29 06	89.65	30.46	88.56	31.83
48.....	91.65	27.67	90.66	29 11	89.61	30.51	88.53	31.87
50.	91.61	27 72	90.62	29 15	89 58	30.55	88.49	31.92
52.....	91 58	27.77	90.59	29.20	89.54	30.60	88.45	31.96
54.....	91.55	27.81	90.55	29 25	89.51	30.65	88.41	32 01
56.....	91 52	27 86	90 52	29.30	89 47	30 69	88.38	32.05
58	91.48	27.91	90.48	29.34	89.44	30 74	88.34	32.09
60.....	91 45	27.96	90.45	29.39	89.40	30.78	88 30	32.14
c= .75. ..	.72	.21	72	.23	.71	.24.	.71	.25
c=1.15.	1 10	33	1 10	.35	1.09	.37	1.08	.38
c=1 90.	1 82	.54	1.81	57	1.80	60	1.79	.63

Min.	20°		21°		22°		23°	
	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dis.	Diff. Elev.	Hor. Dist.	Diff Elev
0'.....	88.30	32.14	87.16	33.46	85.97	34 73	84.73	35.97
2.....	88.26	32.18	87.12	33.50	85.93	34.77	84.69	36.01
4.....	88.23	32.23	87.08	33.54	85.89	34.82	84.65	36 05
6.....	88.19	32.27	87.04	33.59	85.85	34.86	84.61	36 09
8.....	88.15	32.32	87.00	33.63	85.80	34.90	84 57	36.13
10.....	88.11	32.36	86.96	33.67	85.76	34.94	84.52	36.17
12.....	88.08	32.41	86.92	33.72	85.72	34.98	84.48	36.21
14.....	88 04	32.45	86.88	33.76	85.68	35 02	84.44	36.25
16.....	88.00	32.49	86.84	33.80	85.64	35.07	84.40	36.29
18	87.96	32.54	86.80	33.84	85.60	35.11	84.35	36.33
20.....	87.93	32.58	86.77	33.89	85.56	35.15	84.31	36 37
22.....	87.89	32.63	86.73	33.93	85.52	35.19	84.27	36.41
24.....	87.85	32.67	86.69	33.97	85.48	35.23	84.23	36.45
26.....	87.81	32.72	86.65	34.01	85.44	35.27	84.18	36.49
28.....	87.77	32.76	86.61	34.06	85.40	35 31	84.14	36.53
30.....	87.74	32.80	86.57	34.10	85.36	35.36	84.10	36.57
32.....	87.70	32.85	86.53	34.14	85.31	35.40	84.06	36 61
34.....	87.66	32.89	86.49	34.18	85.27	35.44	84.01	36.65
36.....	87.62	32.93	86 45	34 83	85.23	35.48	83 97	36.69
38.....	87.58	32 98	86.41	34.27	85.19	35.52	83.93	36.73
40.....	87.54	33.02	86.37	34.31	85.15	35.56	83.89	36.77
42.....	87.51	33.07	86.33	34.35	85.11	35.60	83.84	36 80
44.....	87.47	33.11	86.29	34.40	85.07	35.64	83.80	36.84
46.....	87.43	33.15	86.25	34.44	85.02	35.68	83.76	36.88
48.....	87.39	33.20	86.21	34.48	84.98	35.72	83 72	36.92
50.....	87.35	33.24	86.17	34.52	84.94	35.76	83 67	36.96
52.....	87.31	33.28	86.13	34.57	84.90	35.80	83.63	37.00
54	87 27	33.33	86.09	34.61	84.86	35.85	83.59	37.04
56.....	87 24	33.37	86.05	34.65	84.82	35 89	83.54	37 08
58.....	87 20	33.41	86.01	34.69	84.77	35.93	83.50	37.12
60.....	87.16	33.46	85.97	34.73	84.73	35.97	83.46	37.16
c= .75....	.70	.26	.70	.27	.69	.29	.69	.30
c=1.15....	1.06	.40	1.07	.42	1.06	.44	1.05	.46
c=1.90....	1.78	.66	1.77	70	1.76	.73	1.74	.76

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Table of Stadia Reductions.—Continued.

Min.	24°		25°		26°		27°	
	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff Elev.	Hor. Dirt.	Diff. Elev.	Hor. Dist.	Diff.. Elev.
0'	83.46	37.16	82.14	38.30	80.78	39.40	79.39	40.45
2	83.41	37.20	82.09	38.34	80 74	39.44	79.34	40.49
4	83.37	37 23	82.05	38.38	80.69	39.47	79.30	40.52
6	83.33	37.27	82.01	38.41	80.65	39.51	79.25	40.55
8	83.28	37.31	81.96	38 45	80 60	39.54	79.20	40.59
10	83.24	37.35	81.92	38.49	80 55	39.58	79.15	40.62
12	83.20	37.39	81.87	38.53	80.51	39.61	79.11	40.66
14	83.15	37.43	81.83	38.56	80.46	39.65	79.06	40.69
16	83.11	37.47	81.78	38.60	80.41	39.69	79.01	40.72
18	83.07	37.51	81.74	38.64	80.37	39.72	78.96	40.76
20	83.02	37.54	81.69	38.67	80.32	39.76	78 92	40.79
22	82.98	37.58	81.65	38.71	80.28	39.79	78.87	40.82
24	82.93	37.62	81.60	38 75	80.23	39.83	78.82	40.86
26	82.89	37.66	81.56	38.78	80.18	39.86	78.77	40.89
28	82.85	37.70	81.51	38.82	80.14	39.90	78.73	40.92
30	82.80	37 74	81.47	38 86	80.09	39.93	78.68	40.96
32	82.76	37.77	81.42	38.89	80 04	39.97	78.63	40.99
34	82.72	37.81	81.38	38.93	80.00	40.00	78.58	41.02
36	82.67	37.85	81 33	38.97	79.95	40.04	78.54	41 06
38	82.63	37.89	81 28	39.00	79.90	40.07	78.49	41.09
40	82.58	37.93	81 24	39 04	79.86	40.11	78 44	41.12
42	82 54	37.96	81.19	39 08	79 81	40.14	78.39	41.16
44	82.49	38.00	81.15	39 11	79.76	40.18	78.34	41.19
46	82 45	38.04	81.10	39.15	79 72	40.21	78.30	41.22
48	82 41	38 08	81 06	39.18	79.67	40.24	78.25	41.26
50	82.36	38.11	81.01	39.22	79.62	40.28	78 20	41.29
52	82.32	38.15	80 97	39.26	79.58	40.31	78 15	41.32
54	82.27	38.19	80.92	39.29	79.53	40 35	78.10	41.35
56	82.23	38.23	80 87	39.33	79.48	40.38	78 06	41.39
58	82.18	38.26	80.83	39.36	79.44	40.42	78.01	41.42
60	82 14	38.30	80.78	39.40	79 39	40.45	77 96	41 45
c= 75	68	31	.68	32	67	.33	.66	.35
c=1.15	1.05	48	1.04	50	1.03	51	1 02	.53
c=1 90	1.73	79	1.72	82	1.70	85	1 69	.88

Min.	28°		29°		30°	
	Hor. Dist	Diff Elev.	Hor. Dist	Diff Elev.	Hor. Dist.	Diff. Elev.
0'	77 96	41 45	76.50	42 40	75.00	43 30
2	77.91	41.48	76.45	42.43	74.95	43.33
4	77.86	41 52	76.40	42.46	74.90	43.36
6	77.81	41.55	76 35	42.49	74.85	43 39
8	77.77	41 58	76.30	42.53	74 80	43.42
10	77.72	41.61	76.25	42.56	74.75	43.45
12	77.67	41.65	76.20	42.59	74.70	43 47
14	77.62	41.68	76.15	42.62	74.65	43.50
16	77.57	41.71	76.10	42.65	74.60	43 53
18	77.52	41.74	76.05	42 68	74.55	43 56
20	77.48	41.77	76.00	42.71	74.49	43.59
22	77.42	41.81	75.95	42 74	74.44	43 62
24	77.38	41.84	75.90	42.77	74.39	43 65
26	77.33	41.87	75.85	42.80	74.34	43.67
28	77.28	41.90	75.80	42,83	74.29	43 70
30	77.23	41.93	75.75	42.86	74.24	43 73
32	77.18	41 97	75.70	42.89	74.19	43.76
34	77.13	42 00	75.65	42.92	74.14	43 79
36	77.09	42.03	75.60	42.95	74.09	43.82
38	77.04	42.06	75.55	42 98	74.04	43 84
40	76.99	42.09	75.50	43.01	73.99	43.87
42	76.94	42.12	75 45	43 04	73.93	43 90
44	76.89	42.15	75.40	43 07	73 88	43.93
46	76.84	42.19	75.35	43.10	73 83	43 95
48	76.79	42 22	75.30	43.13	73.78	43.98
50	76.74	42.25	75 25	43.16	73.73	44 01
52	76.69	42.28	75 20	43.18	73.68	44.04
54	76.64	42.31	75.15	43.21	73.33	44 07
56	76.59	42.34	75.10	43 24	73 58	44.09
58	76.55	42.37	75.05	43 27	73.52	44.12
60	76.50	42.40	75.00	43 30	73.47	44.15
c= .75	.66	.36	.65	.37	.65	38
c=1.15	1 01	55	1.00	.57	0.99	.58
c=1.90	1.67	91	1.65	.94	1 64	.95

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46 7th St. Thorn to Myrtle 52 - 56

Myrtle E. to Alley & W. to Alley 57 - 59

Indexed
C.S.K.

C.S.M. 4-Ka

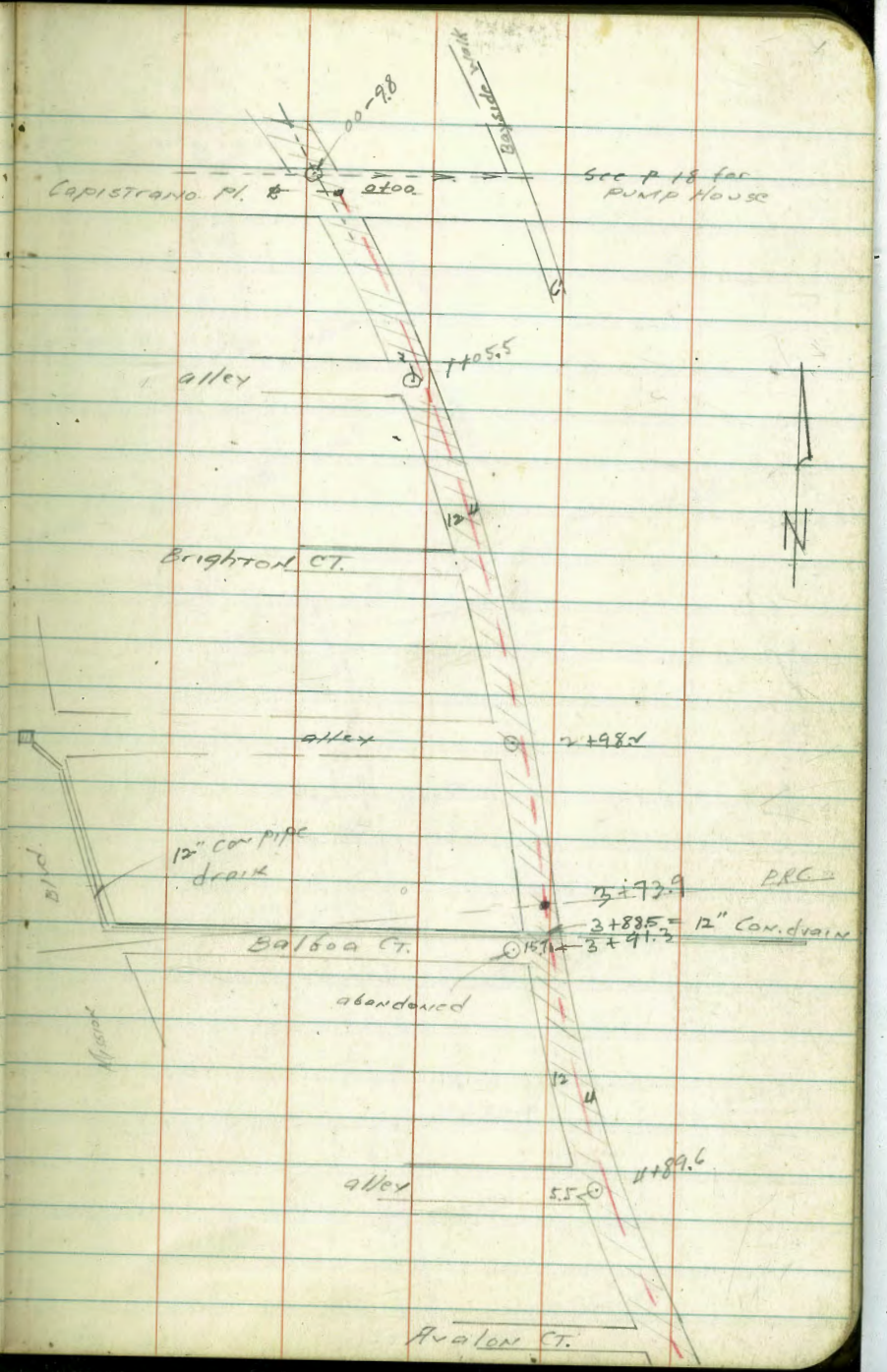
Mission Beach Trunk Sewer on Bayside Lane, Capistrano St to Ocean Beach.

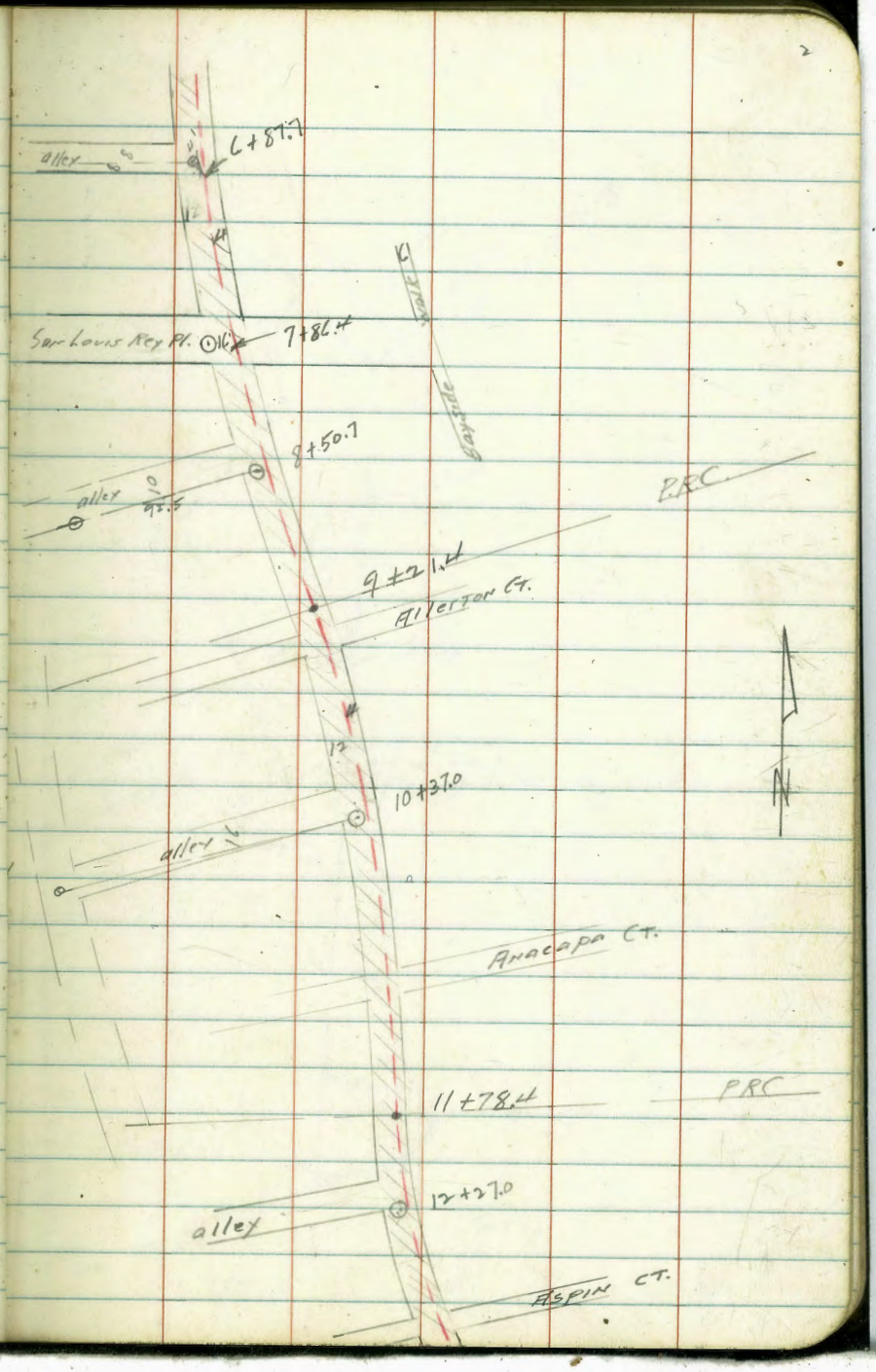
Con. Pav. on Bayside Lane

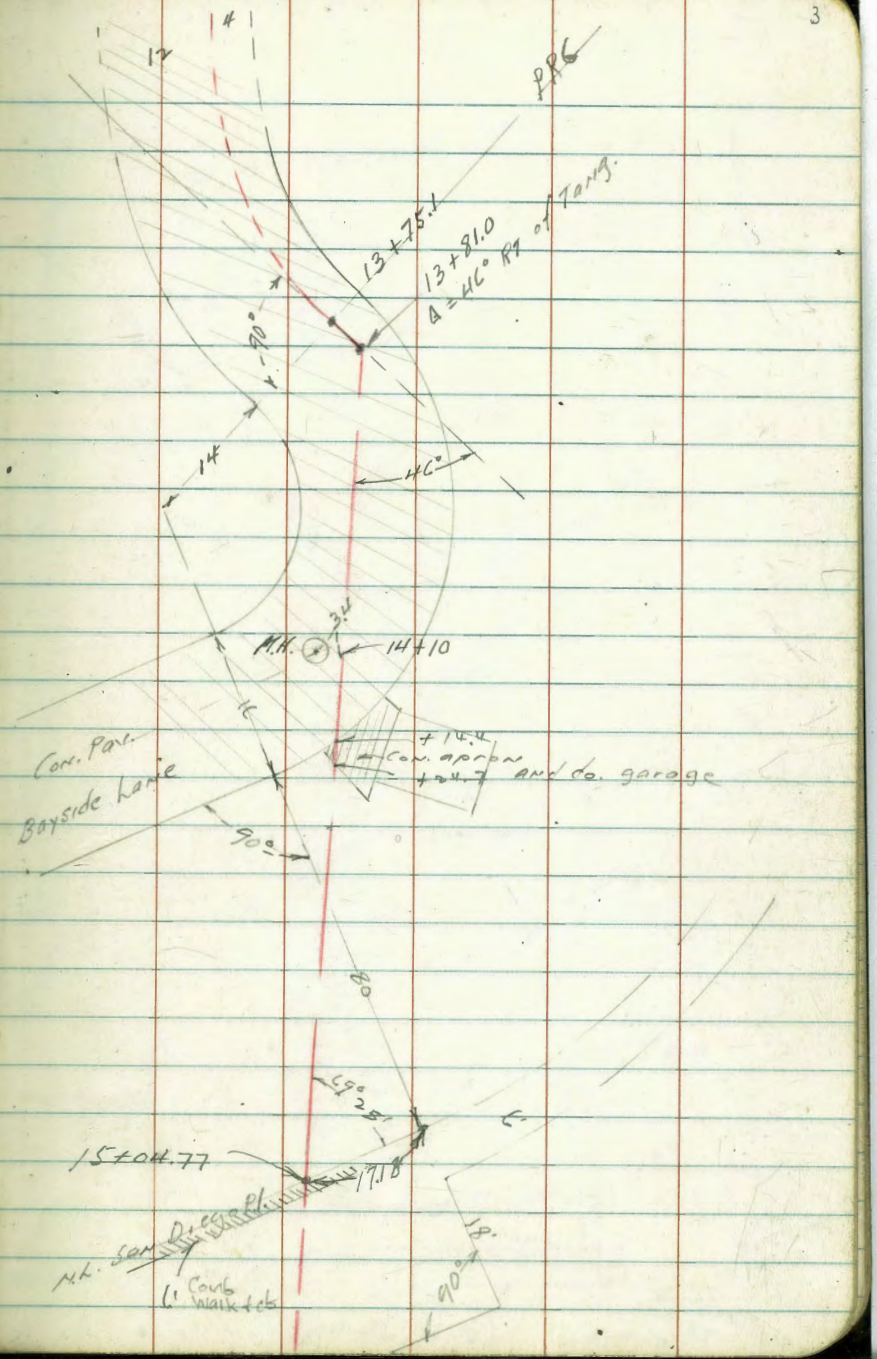
High Line

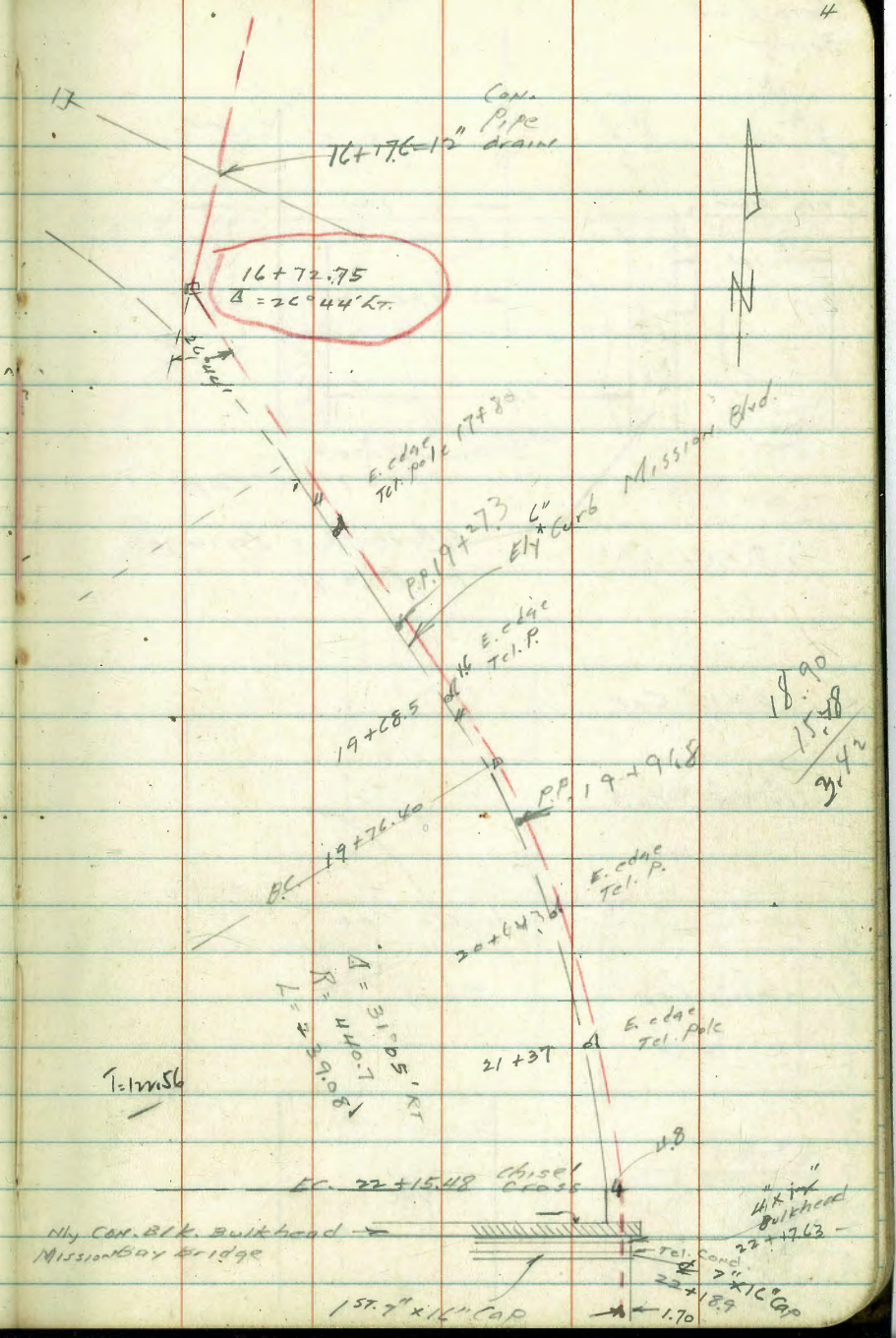
Ex. Sewer on ℄ Bayside Lane, also Sewer
4" ± C.I. water 4' E of ℄ will have
to be high lined unless sewer could
be constructed 2' N of Ex. of Lane

Ex. Hi-pres. gas Line 4' N of ℄ Lane

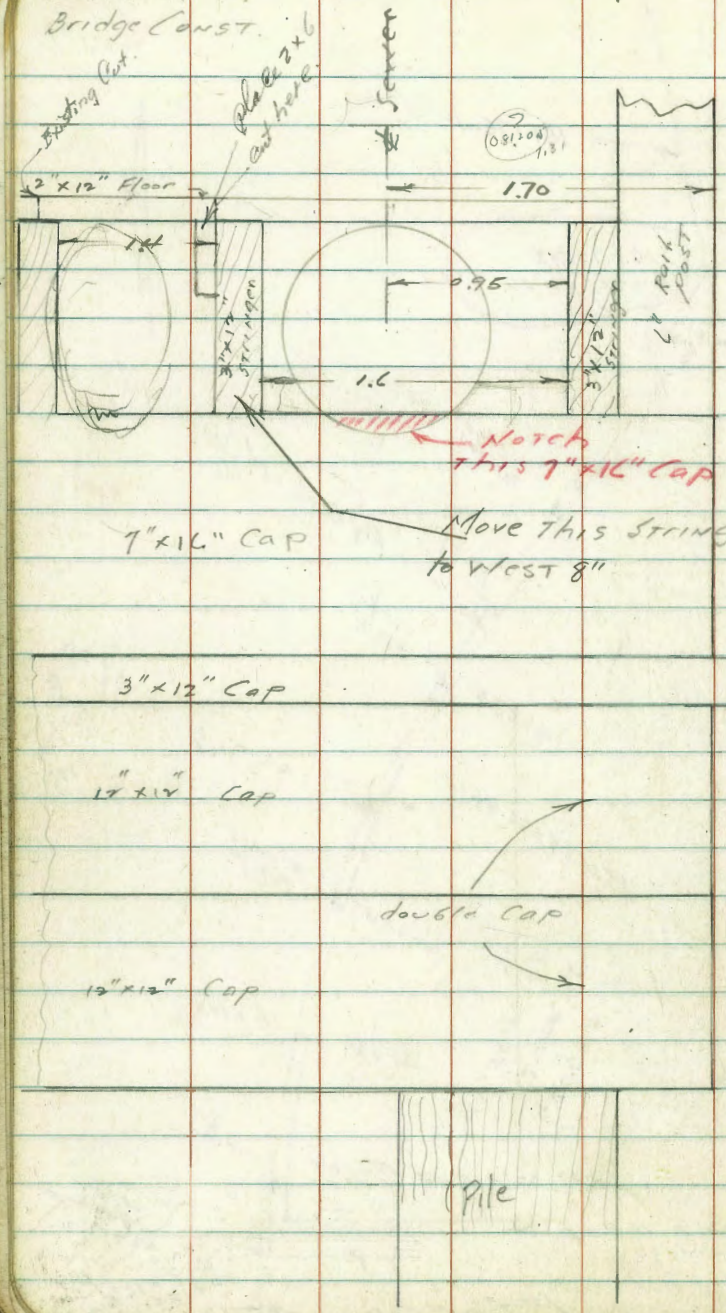


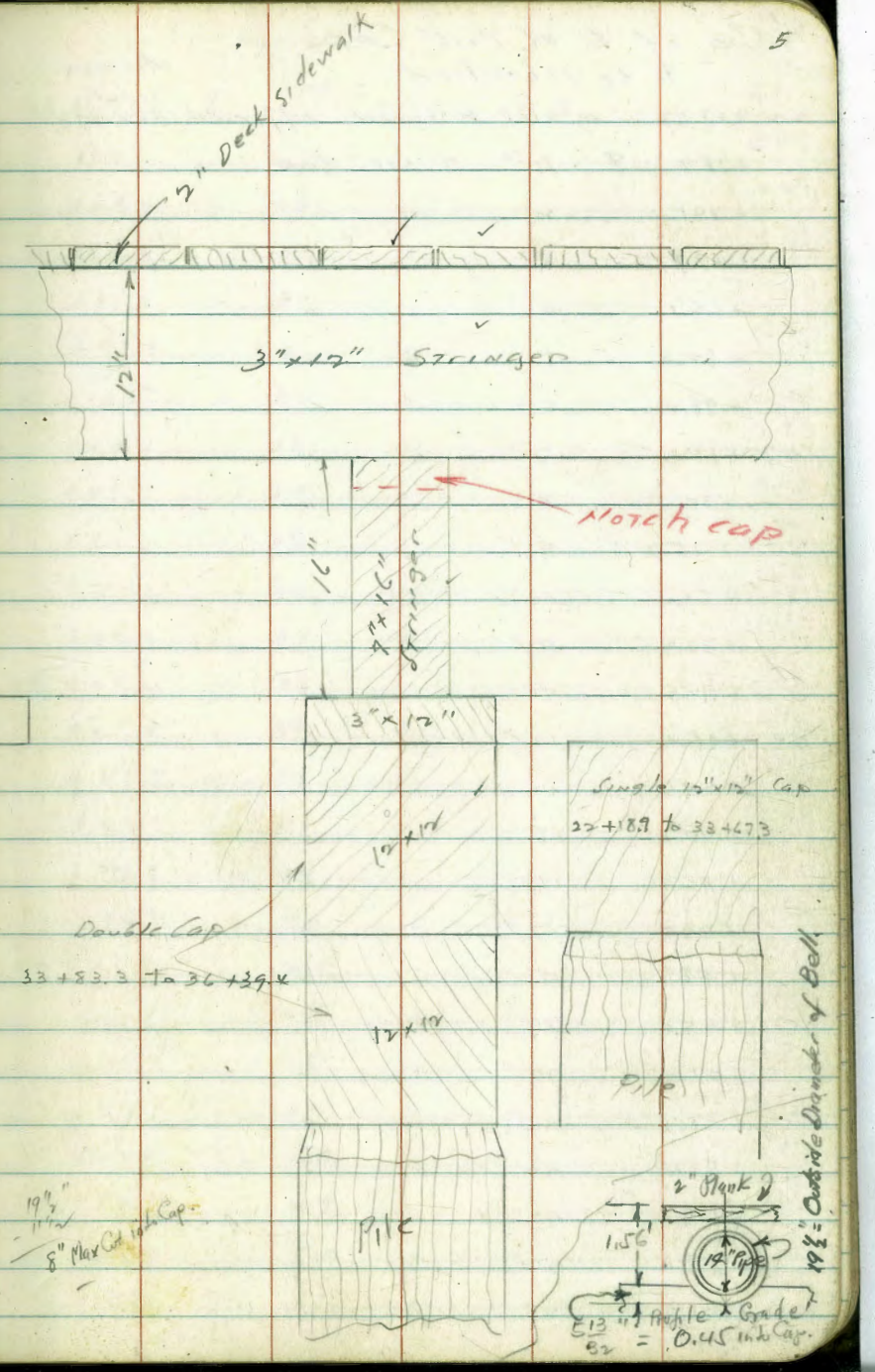

alley
6+87.7
San Louis Rey Pl.
7+86.4
8+50.7
alley
9+21.4
Allerton Ct.
10+37.0
alley
Anacapa Ct.
11+78.4
12+27.0
alley
Aspin Ct.
PRC
PRC
N


PRC
13+75.1
13+81.0
Δ=46° Rt of Tang.
90°
14
46°
M.H.
14+10
16
Con. Pav.
Bayside Lane
+14.4
Con. apron
+14.7
and do. garage
90°
80
59° 28'
15+04.77
17.18
N.L. San. Dr. Easement
4' Conc. walk to cb
18.
90°


Con. Pipe drains
16+19.6-12"
16+72.75
Δ = 2C°44'Lt.
E. edge Tel. pole 17+80
Mission Blvd.
6" Curb
P.P. 19+23
Elev
E. edge Tel. P.
19+28.5
P.P. 19+94.8
19+76.40
B.C.
E. edge Tel. P.
20+64.36
E. edge Tel. pole
21+37
T=1m56
R=
L=
Δ = 31°05'-Rt
Chisel Cross
E.C. 22+15.48
Mly Conc. Blk. Bulkhead
Mission Bay Bridge
"H" inf. Bulkhead
22+17.63
Tel. Conc.
22+18.9
1.70
157.7" x 14" Cap
18.90
15.48
91.4'

Detail of Bridge Const.





Sta. of ℄ of 7"x16" Caps
to be Notched

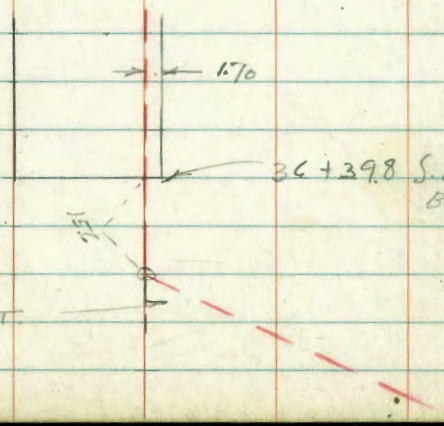
Mission Beach

22	+17.63	4"x12" Bulkhead	Nly end Bridge	
1.27	+18.9	℄ 1ST	7"x16" Cap	
15.7	+34.1	" 2	"	"
15.8	+49.9	" 3	"	"
16.2	+66.1	" 4	"	"
15.9	+80.0	" 5	"	"
16.0	+98.0	" 6	"	"
15.3	23 +13.3	" 7	"	"
16.7	+30	" 8	"	"
15.7	+45.7	" 9	"	"
15.7	+61.4	" 10	"	"
15.9	+77.3	" 11	"	"
15.2	+92.5	" 12	"	"
15.9	24 +08.4	" 13	"	"
16.2	+24.6	" 14	"	"
16.1	+40.7	" 15	"	"
16.2	+56.9	" 16	"	"
16.1	+73.0	" 17	"	"
15.9	+88.9	" 18	"	"
16.1	25 +05.0	" 19	"	"
16.2	+21.2	" 20	"	"
16.1	+37.3	" 21	"	"
15.9	+53.2	" 22	"	"
15.8	+69.0	" 23	"	"
16.1	+85.1	" 24	"	"
16.2	26 +01.3	" 25	"	"

15.9	26 +17.2	℄ 26th	7"x16" Cap	
15.9	+33.1	" 27	"	"
16.2	+49.3	" 28	"	"
16.0	+65.3	" 29	"	"
16.0	+81.3	" 30	"	"
16.0	+97.3	" 31	"	"
16.2	27 +13.5	" 32	"	"
16.1	+29.6	" 33	"	"
16.1	+45.7	" 34	"	"
15.9	+61.6	" 35	"	"
16.0	+77.6	" 36	"	"
15.7	+93.3	" 37	"	"
16.1	28 +09.4	" 38	"	"
16.0	+25.4	" 39	"	"
16.1	+41.5	" 40	"	"
16.2	+57.7	" 41	"	"
16.1	+73.8	" 42	"	"
15.9	+89.7	" 43	"	"
16.0	29 +05.7	" 44	"	"
15.9	+21.6	" 45	"	"
16.0	+37.6	" 46	"	"
16.1	+53.7	" 47	"	"
16.1	+69.8	" 48	"	"
15.9	+85.7	" 49	"	"
16.0	30 +01.7	" 50	"	"
16.1	+17.8	" 51	"	"

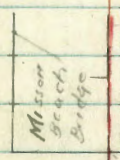
16					
30 + 33.8	℄	52	7"×16" Cap		
15.9 + 49.7	"	53	"	"	
16.1 + 65.8	"	54	"	"	
16.0 + 81.8	"	55	"	"	
16.0 + 97.8	"	56	"	"	= N. end Steel Span
0.7 + 98.5	"	False	"	"	7"×16" Caps rest
14.9 31 + 13.4			"	"	on Top of 1'×3'
13.5 + 26.9	"	"	"	"	Steel Girder
15.2 + 42.1	"	"	"	"	and overhang
1.0 + 43.1	"	57	"	"	4 feet but are
14.1 + 59.2	"	58	"	"	in some relative
15.9 + 75.1	"	59	"	"	position as others
16.0 + 91.1	"	60	"	"	= S. end " "
15.9 32 + 07.0	"	61 ✓	"	"	
16.2 + 23.2	"	62	"	"	
15.8 + 39.0	"	63	"	"	
16.0 + 55.0	"	64	"	"	
16.0 + 71.0	"	65	"	"	
16.1 + 87.1	"	66	"	"	
16.1 33 + 03.2	"	67	"	"	
16.1 + 19.3	"	68	"	"	
15.9 + 35.2	"	69	"	"	
16.3 + 51.5	"	70	"	"	
15.8 + 67.3	"	71	"	"	
16.0 + 83.3	"	72	"	"	
15.7 + 99.0	"	73	"	"	

16.2					
34 + 15.2	℄	74th	7"×16" Cap.		
16.1 + 31.3	"	75	"	"	"
16.0 + 47.3	"	76	"	"	"
15.9 + 63.2	"	77	"	"	"
16.1 + 79.3	"	78	"	"	"
15.9 + 95.2	"	79	"	"	"
16.1 35 + 11.3	"	80	"	"	"
15.9 + 27.2	"	81	"	"	"
16.0 + 43.2	"	82	"	"	"
15.7 + 58.9	"	83	"	"	"
16.4 + 75.3	"	84	"	"	"
15.8 + 91.1	"	85	"	"	"
16.2 36 + 07.3	"	86	"	"	"
16.4 + 23.7	"	87	"	"	"
15.7 + 39.4	"	88	"	"	"
0.4 + 39.8 South end Bridge Bulkhead					



36 + 55.40
Δ = 49° 36' LT

Junction of Mission Beach and Ocean Beach Sewers



1.70

15.6

36+55.40 P.T.
Δ = 49°36' Lt.

Correction P. 21

26.95

38+80.75

Ln. Pt. Loma Blvd

100

B.M. 103 Ocean Bay Beach

142.52

100

80'

1:1.50

Bacon

5T.

Hor. 03.56
5°39'30" Lt

+19.05

5°39'30"

Old ~~line~~ Front Ocean Beach
F.B. 1634-32

Line change

P. 15

162.50
26.95
135.55

Correction
1634-32

this change not used

Sewer 30" RCP

Change

5°39'30"

42+53.73
Junction of Mission Beach and Ocean Beach trunk sewers

30°39'30"

43+26.10
New Junction

28°54' Rt.

Old 133+72.32
New 133+55.37

Δ = 28°54' Rt.

Old Junction

Δ = 30°39'30" Rt.

137+49.60

Sewer 30" RCP

135+05.31

New 24" RCP

New 24" RCP

100 ft. Nom.

Ex. 100' Row

63.85

Levels, Mission Beach Trunk Sewer

Via Bayside Lane, Beg. at Capistrano P.

BM. BP S end Seawall	0.99	8.17 ✓		7.13	Mission Beach
T.P.	4.81	3.53 ✓	9.40	-1.28 ✓	
T.P.	4.82	6.57 ✓	1.78	1.75 ✓	
00 - 98			6.04	0.53 ✓	RIM
" " FL. outlet of MH. to pump			14.58	-8.01 ✓	F.L.
0+00	Pav		6.0	0.6 ✓	
+50	"		5.7	0.9 ✓	
/	"		5.3	1.3 ✓	
+05.5	"		5.3	1.3 ✓	
"	H'w = M.H.		5.28	1.29 ✓	RIM
"	"		14.47	-7.85 ✓	F.L.
+50	Pav.		5.4	1.8 ✓	
"	"		5.0	1.6 ✓	
+50	"		4.9	1.7 ✓	
+98.4	"		4.5	2.1 ✓	
"	H'w = MH		4.53	2.02 ✓	RIM
"	"	"	13.90	-7.33 ✓	F.L.
3	Pav		4.6	2.0 ✓	
+50	"		4.9	1.7 ✓	
3+73.90	P.R.C.		5.1	1.5 ✓	
+88.5	Pav		5.4	1.9 ✓	
"	Top of 12" Con. pipe drain		10.90	-4.33 ✓	
T.P.	4.35	6.10 ✓	4.87	1.75 ✓	

Notes Reduced - 9/25/42

6.10 ✓

3+91.3	Pav				
"	15.7 W = M.H.			- abandoned	RIM
"	"	"			F.L.
H+00	Pav		4.6	1.5 ✓	
+50	"		4.8	1.3 ✓	
+89.6	"		4.9	1.2 ✓	
"	H'w = M.H.		4.86	1.28 ✓	RIM
"	"	"	13.14	-7.08 ✓	F.L.
5+00	Pav		5.0	1.1 ✓	
+50	"		5.2	0.9 ✓	
C	"		5.6	0.5 ✓	
+50	"		5.9	0.2 ✓	
+87.7	"		5.9	0.2 ✓	
"	H'w = MH		5.87	0.23 ✓	RIM
"	"	"	12.58	-6.48 ✓	F.L.
7+00			6.1	0.0 ✓	
T.P.	4.52	4.52 ✓	6.10	0.00 ✓	
7+50	Pav		4.6	-0.1 ✓	
+86.4	10 W = MH		4.55	-0.03 ✓	RIM
"	"	"	Flush Tank?		Full of water
8	Pav		4.5	0.0 ✓	
+50.7	"		5.1	-0.6 ✓	

		4.57		
8+50.7	4'W = M.H.	5.18	-0.66	RIM
"	" "	10.56	-6.02	F.L.
9	Pav	5.0	-0.5	
9 +21.4	" PRC	4.8	-0.3	
9 +50	"	4.7	-0.2	
10	"	4.4	0.1	
+37	"	4.2	0.3	
"	4'W = M.H.	4.14	0.38	RIM
"	" "	9.87	-5.30	F.L.
+50	Pav.	4.2	0.3	
"		3.9	0.6	
		6.59		
T.P.	5.47			
		3.40	4.12	
+50	Pav	5.6	1.0	
+78.4	" PRC	5.5	1.1	
11 +00	"	5.3	1.3	
+27	"	5.3	1.3	
"	4'W = M.H.	5.15	1.32	RIM
"	" " Corner soiled			F.L.
+50	Pav	5.2	1.4	
13	"	5.0	1.6	
+50	"	4.7	1.9	
+75.1	" PRC	4.6	2.0	
+81	" Δ 41°00' Rt. of T.	4.6	2.0	
14	"	4.5	2.1	

		6.59		
14 +10	Pav	4.5	2.1	
"	3.4'W = M.H.	4.42	2.17	RIM
"	" "	11.15	-4.56	F.L.
14 +14.4	edge Con apron	4.6	2.0	
+24.7	" " "	4.5	2.1	Beg. of sand
+50		4.9	1.7	
15		6.6	0	
+04.77	N/y San Diego Pl. and C—Comb walk & Curb	6.34	0.26	
T.P.	4.76	4.96	6.39	0.20
15 +11	c6	4.8	0.2	
+11		5.3	-0.3	
+30		5.3	-0.3	
+50		5.0	0	
+75		5.6	-0.6	
16		6.9	-1.9	
+17.4	Intr. 12" Con. Pipe drain	7.5	-2.5	Sand
"		9.13	-4.17	Top pipe
+28		7.6	-2.6	
+38		5.2	-0.2	
+50		4.5	0.5	
16 +72.75	Δ 21°44' Lt	4.68	0.28	on "X" Hub
17		4.6	0.4	
+50		4.6	0.4	
"	4' Rt. Top Curb	4.17	0.79	

		4.96 ✓			
17+50	8' LT		4.6	0.4	✓
"	17 "		10.4	-5.28	✓
18			3.8	1.2	✓
"	4' RT	Top Curb	3.85	1.11	✓
"	5' LT		3.7	1.3	✓
"	16 "		10.4	-5.2	✓
+50			3.3	1.7	✓
"	4' RT	Top Curb	3.51	1.45	✓
"	6 LT		3.3	1.7	✓
"	15 LT		11.6	-6.6	✓
19			7.9	8.1	✓
"	4' RT	Top Curb	3.0	2.0	✓
"	3 LT		3.0	2.0	✓
"	9 LT		9.5	-4.5	✓
+50			7.7	2.8	✓
"	4 RT	Top Curb	7.47	2.49	✓
"	8 LT		7.3	2.7	✓
"	16 "		11.0	-6.0	✓
T.P.	856	11.36 ✓	2.16	2.80	✓
19+76.40	BC RT		9.1	2.3	✓
"	4 RT	Top Curb	8.33	3.03	✓
"	2 LT		9.1	2.3	✓
"	8 LT		16.7	-5.3	✓

		11.36 ✓			
20+00			8.0	3.9	✓
"	4 RT	Top Curb	7.91	3.95	✓
"	3 LT		8.4	3.2	✓
"	14 LT		17.0	-5.6	✓
+50			6.8	9.6	✓
"	3.5 RT	Top Curb	6.90	4.46	✓
"	3 LT		6.8	9.6	✓
"	15 LT		16.7	-5.3	✓
21+00			6.1	5.3	✓
"	3.4 RT	Top Curb	6.0	5.4	✓
"	4 LT		6.3	5.1	✓
"	16 LT		15.8	-4.8	✓
+50			5.4	6.0	✓
"	3.7 RT	Top Curb	5.31	6.05	✓
"	7.5 LT		5.6	5.8	✓
"	17 LT		16.1	-4.7	✓
22+00			4.7	6.7	✓
"	4.7 RT	Top Curb	4.70	6.66	✓
"	2.5 LT		4.7	6.7	✓
"	10 LT		9.1	2.3	✓
22+15.48 = E.C.			5.1	6.3	✓
+17.63	N. end	Mission Beach Bridge	4.98	6.38	✓ Top 2" Bd. walk
+18.9	22+18.9 to		4.98	6.38	✓
+34.1	S. side		4.96	6.40	✓ all rods.
+49.9	Cap	33 x 7.3 = 12'-1"	4.97	6.42	✓ Top Bd. walk
+66.1			4.94	6.42	✓

		11.30 ✓					12.70 ✓				17
22 + 87			4.91	6.95 ✓	26 + 49.2			5.55	7.15 ✓
+ 98			4.85	6.51 ✓	+ 65.3			5.49	7.21 ✓
23 + 12.3			4.83	6.53 ✓	+ 81.3			5.47	7.28 ✓
+ 30			4.81	6.55 ✓	+ 97.3			5.39	7.31 ✓
+ 45.7			4.79	6.57 ✓	27 + 13.5			5.30	7.80 ✓
+ 61.4			4.73	6.63 ✓	+ 29.6			5.20	7.89 ✓
+ 77.3			4.69	6.67 ✓	+ 45.7			5.24	7.86 ✓
+ 93.5			4.67	6.69 ✓	+ 61.6			5.24	7.86 ✓
24 + 08.4			4.67	6.69 ✓	+ 77.6			5.16	7.52 ✓
+ 24.6			4.66	6.70 ✓	+ 93.3			5.05	7.65 ✓
+ 40.7			4.67	6.69 ✓	28 + 09.4			5.01	7.69 ✓
+ 56.9			4.66	6.70 ✓	+ 25.4			4.98	7.72 ✓
+ 73			4.65	6.71 ✓	+ 41.5			4.96	7.74 ✓
+ 88.9			4.64	6.72 ✓	+ 57.7			4.91	7.79 ✓
25 + 05			4.63	6.73 ✓	+ 73.8			4.88	7.82 ✓
					+ 89.7			4.92	7.73 ✓
T.P.	5.49	12.70 ✓	3.95	7.41 ✓	29 + 05.7			5.01	7.69 ✓
					+ 21.6			5.01	7.69 ✓
25 + 21.2			5.93	6.77 ✓	+ 37.6			4.96	7.74 ✓
+ 37.3			5.88	6.82 ✓	+ 53.7			4.95	7.75 ✓
+ 53.2			5.86	6.84 ✓	+ 69.8			4.96	7.74 ✓
+ 69			5.80	6.90 ✓	+ 85.7			5.01	7.69 ✓
+ 85.1			5.79	6.91 ✓	30 + 01.7			5.00	7.70 ✓
26 + 01.3			5.79	6.91 ✓	+ 17.8			4.97	7.73 ✓
+ 17.2			5.75	6.95 ✓	30 + 33.8			4.94	7.76 ✓
+ 33.1			5.65	7.05 ✓	T.P.	3.43	11.60 ✓	4.23	8.47 ✓

30 + 49.7		3.80	7.80
+ 65.8		3.77	7.83
+ 81.8		3.83	7.77
+ 97.8		3.81	7.79
+ 98.5	Beg Steel Span	3.83	7.77
31 + 13.4		3.84	7.76
+ 26.9		3.88	7.72
+ 41.1	End " "	3.76	7.84
+ 43.1		3.8	7.78
+ 59.2		3.72	7.88
+ 75.1		3.75	7.85
+ 91.1		3.75	7.85
32 + 07.0		3.76	7.84
+ 23.2		3.82	7.78
+ 39.0		3.92	7.68
+ 55.0		4.05	7.55
+ 71.0		4.14	7.46
+ 87.1		4.21	7.39
33 + 03.2		4.41	7.19
+ 19.3		4.61	6.99
+ 35.2		4.85	6.75
+ 51.5		5.07	6.53
+ 67.3	End Single 12"x12" Cap	5.17	6.43
+ 83.3	Beg da. 12"x12" Cap	5.32	6.28
+ 99.0		5.50	6.10
34 + 15.2		5.70	5.90

11.Co

34 + 31.3		5.80	5.80
+ 47.3		6.04	5.56
+ 63.2		6.28	5.82
+ 79.3		6.44	5.66
+ 95.2		6.56	5.08
35 + 11.3		6.77	4.88
+ 27.2		6.97	4.63
+ 43.2		7.13	4.47
+ 58.9		7.27	4.33
+ 75.3		7.50	4.10
+ 91.1		7.64	3.96
36 + 07.3		7.87	3.73
+ 23.7		8.12	3.48
+ 39.4	End da. 12"x12" Cap	8.15	3.45
+ 39.8	S/y end Bridge	8.15	3.45
36 + 55.40 = Δ 49°36' LT		8.7	2.9 ground
T.P. BRG 6 Second Bridge	3.95	7.15	8.40 3.70 Walker 3.72 0.02
37 + 00		3.4	3.8
" 4' LT		3.5	3.7
" 10' LT		9.0	-1.8
37 + 10		8.8	-1.6
" 8 RT		4.1	3.1
" 10 LT		9.0	-1.8
+ 50		8.5	-1.3

7.15

37+50	7' RT	6.2	1.0	✓
"	10 RT	5.2	2.0	✓
"	10 LT	8.6	-1.2	✓
+60		6.2	1.0	✓
"	3' LT	8.5	-1.3	✓
"	10' LT	8.6	-1.2	✓
"	7 RT	5.5	1.7	✓
38+00		5.2	2.0	✓
"	6' LT	8.7	-1.5	✓
"	10 LT	8.8	-1.6	✓
"	10 RT	4.9	2.3	✓
+12		5.0	2.2	✓
"	2 LT	8.7	-1.5	✓
"	10 LT	8.8	-1.6	✓
"	10 RT	4.7	2.5	✓
+30		4.8	2.2	✓
"	5' LT	4.9	2.3	✓
"	7 LT	8.7	-1.5	✓
"	12 LT	8.9	-1.7	✓
"	10 RT	4.6	2.6	✓
+50		4.4	2.8	✓
39		4.3	2.9	✓
+50		4.5	2.7	✓
40	Line change	4.4	2.8	✓
~~40+02.56 Δ 5°39'30"~~	See P. 8			
+50		4.2	3.0	✓
41		3.6	3.6	✓

7.15

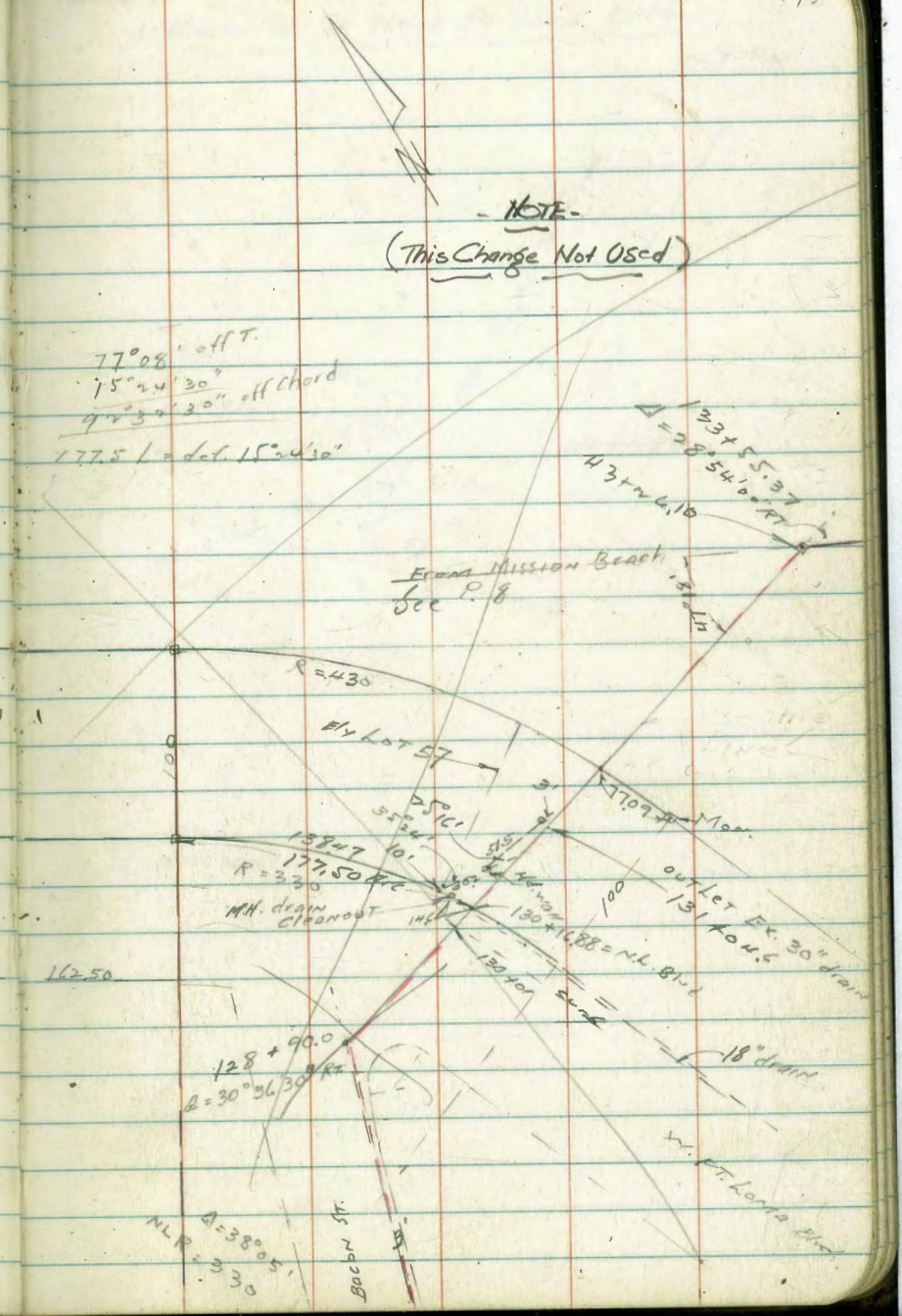
14

41+50		3.2	4.0
42		4.3	2.9
+25		4.4	2.8
42+53.73 = Junction MH 132+94.60		3.35	3.87 on 2nd Hub
811 F c6 Q13			
Second Bridge 4.48	7.68 ✓		3.20 ✓
40+02.56 Δ = 5°39'30" Lt.		4.9	2.8 ✓
+50		4.8	2.9 ✓
41		4.7	3.0 ✓
+50		4.4	3.3 ✓
42		4.7	3.0 ✓
+50		4.8	2.9 ✓
+90		4.8	2.9 ✓
43		3.2	4.9 ✓
+26.10 New Junction		3.6	4.1 ✓
T.P	5.83	10.20 ✓	3.31	4.37 ✓

P-7-9r

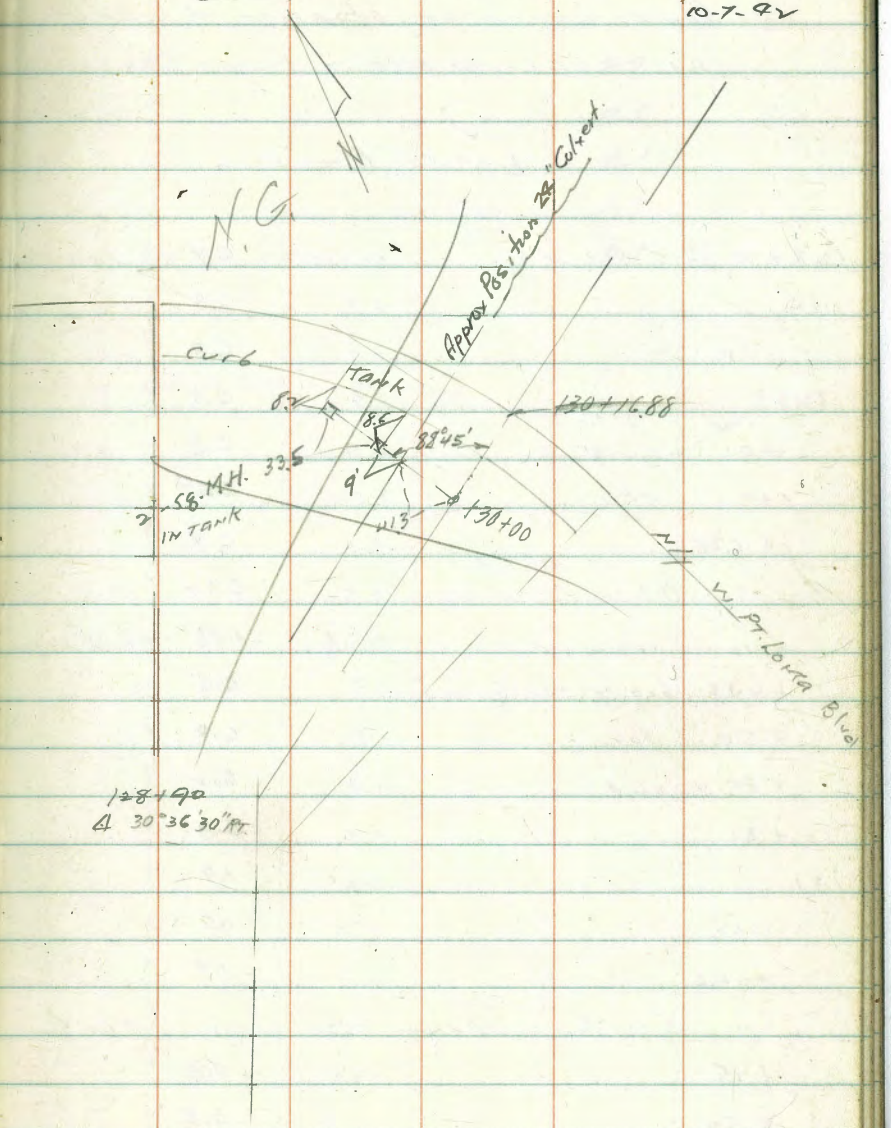
Sewer line change at
W. Pt. Loma Blvd. and Bacon St.
Acct. of Storm drains, etc.

- NOTE -
(This Change Not Used)



Locate Storm Drain & Settling Tank.
Bacon St & West Pt Loma Blvd.

10-7-92



Sewer Levels on change of line

at W. Pt. Loma Blvd. & Bacon St.

P. 15

10.20 H.I. from P. 14

128+90	Δ = 30°36'30" Rt.	3.3	6.9	
129		3.4	6.8	
+50		3.4	6.8	
130		3.9	6.3	
+01	gut	3.9	6.3	
+01	ab	3.63	6.57	
+16.88		3.5	6.7	
"	14C W Clermont MH. Colv.	3.53	6.67	Rim
"	" "	17.08	-1.88	F.L. 18" pipe
+44.6	beg. 8" pav. (Glenns)	3.7	6.5	
+50	pav.	3.8	6.4	
+80.4	end " "	4.0	6.2	
+86		4.4	5.8	
131		8.3	1.9	
+03		8.7	1.5	
+04.6		11.6	-1.4	
"	3' W. to OUTLET of 30" down	13.90	-3.70	F.L. ✓
+75		13.0	-2.8	
+50		12.7	-2.5	
+75		11.8	-1.6	
132		8.5	1.7	

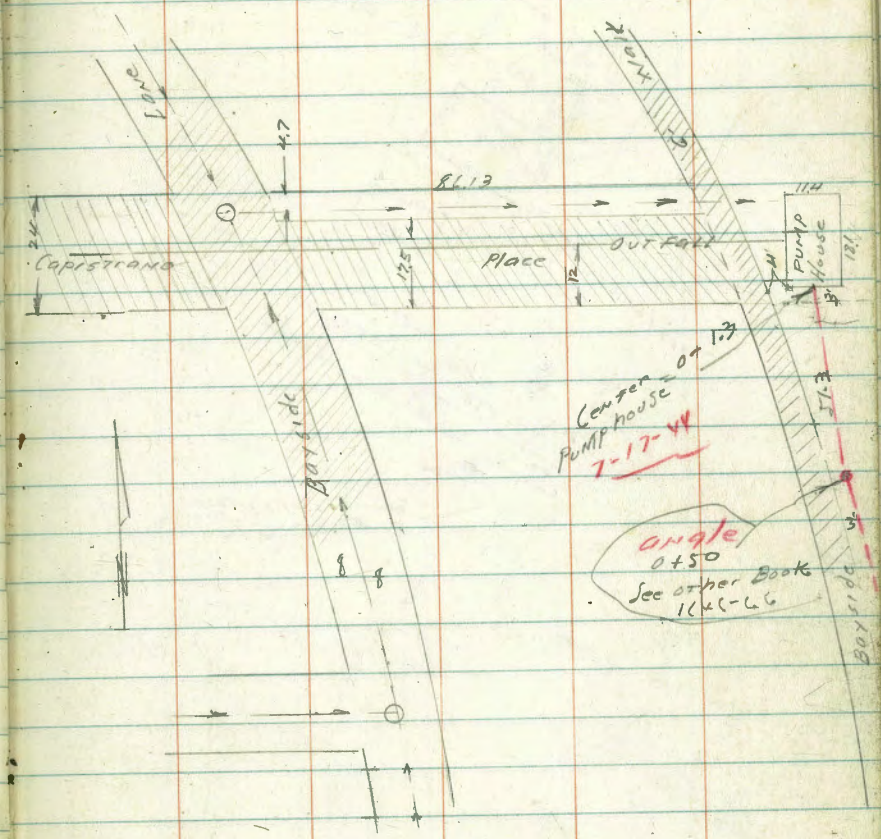
10.20

132+30	5.8	4.9	
+50	5.7	4.5	
133	6.1	4.1	
+25	6.2	3.9	
133+55.37 Δ = 28°54' Rt.	6.1	4.1	New Junction
T.P. on old Junction MH 132+94.60	6.36	3.84 (changed)	(3.82)
F.B. 1634 How does this check?			

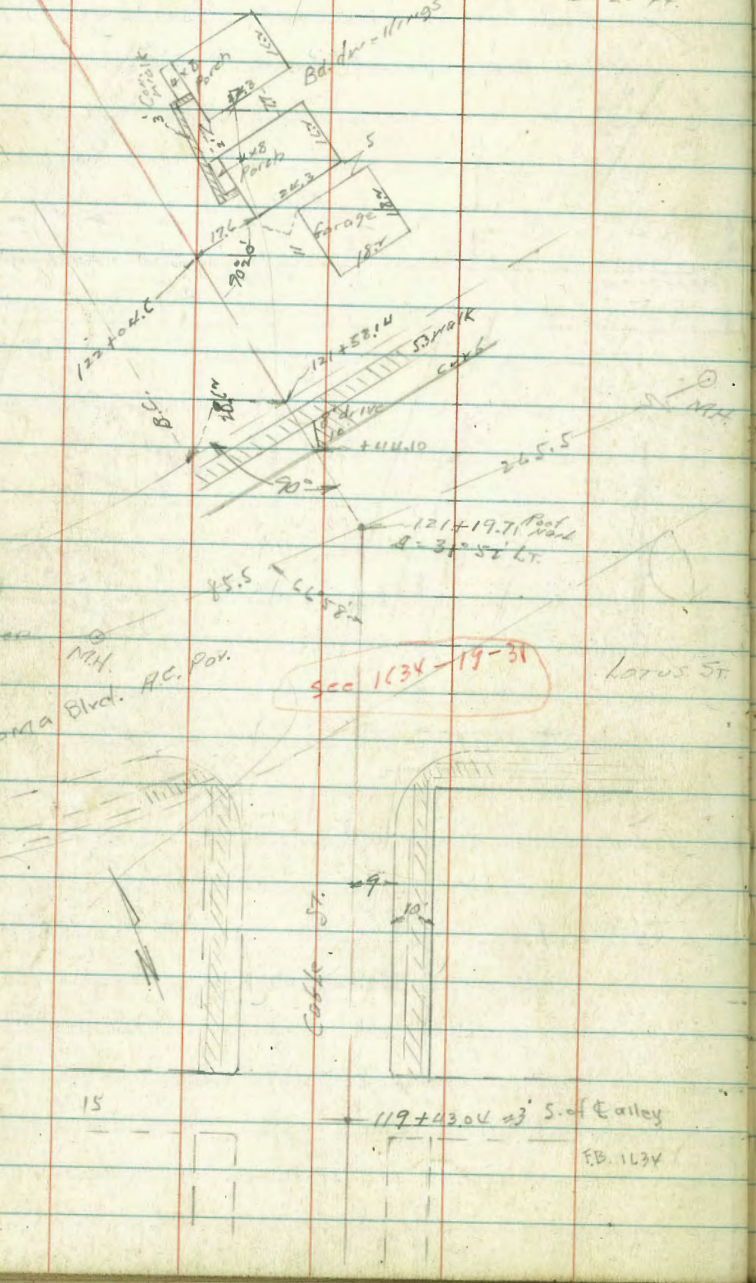
Existing Pump House

Capistrano Pl. and Bayside Walk

Moore
10-7-42.



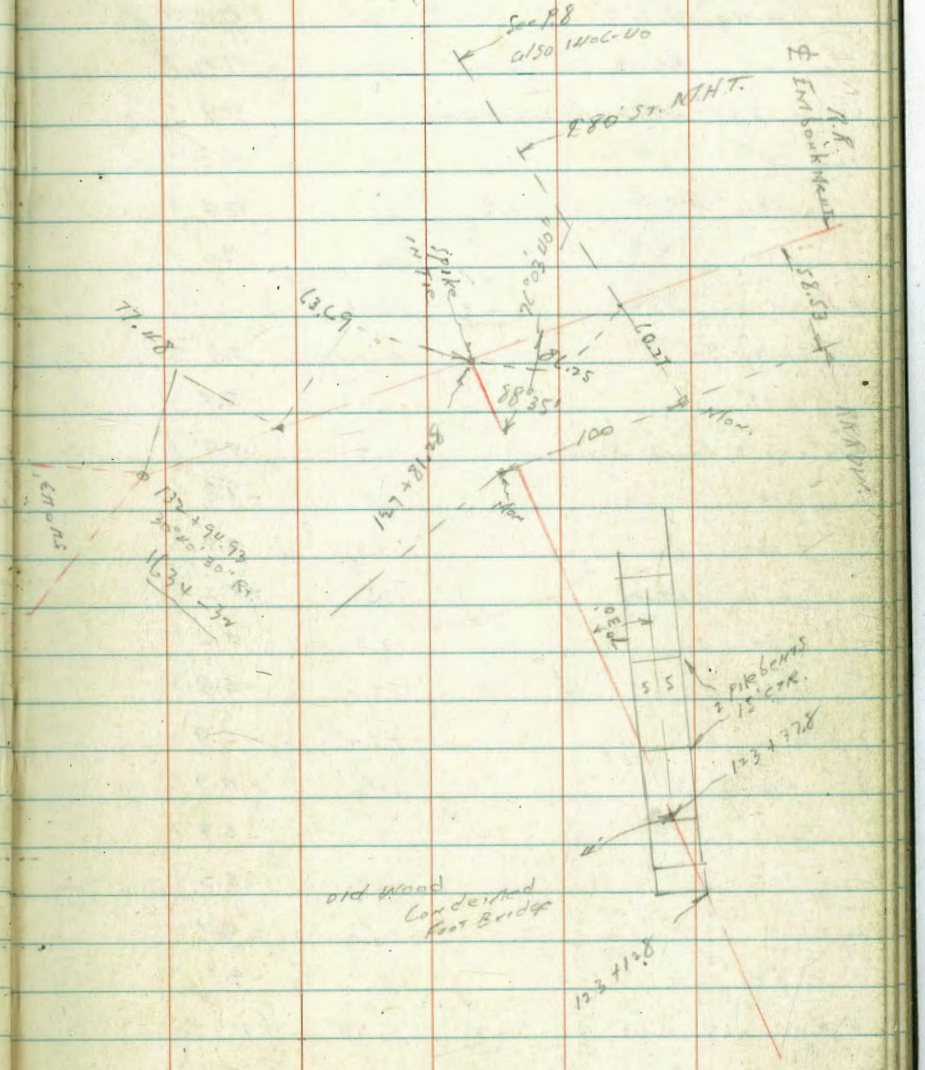
Proposed change of Ocean Beach Sewer at Cable & W. Ft. Loma Blvd. 6-2-44.



19

77.48
63.69
13.79
27.47

149.94
77.48
27.47



Levels Prop. Sewer change csme 6-2-44.
W. Pt. Lomb & Cable to R.R. R.O.W

					Datum &
N6BP	1.50	20.98		19.48	W. Pt. Lomb Blvd
121 + 19.7	⊄ 31°52' Lt		2.81	18.17 ✓	pav.
+ 44.10	gut.		3.85	17.12 ✓	
"	Top Curb		3.75	17.73 ✓	
+ 58.14	N6 W. Pt Lomb Blvd		3.1	17.9 ✓	
122			5.2	15.8 ✓	
+ 50			8.6	12.4 ✓	
+ 75			12.0	9.0 ✓	
T.P.	1.06	9.06	12.78	8.20 ✓	
+ 90			2.0	7.3 ✓	
+ 97			3.2	5.8 ✓	
123 + 12.8	deck Bridge		4.9	4.4 ✓	
+ 13			11.1	-1.8 ✓	
+ 40	"	"	4.9	4.4 ✓	
"	Mud		13.5	-4.2 ✓	
+ 50	"		13.9	-4.6 ✓	
+ 75	"		15.1	-5.8 ✓	
124	"	"	15.2	-5.9 ✓	
+ 15	"		14.0	-4.7 ✓	
+ 27	"		15.2	-5.9 ✓	
+ 35	"		14.3	-5.0 ✓	
125	"		14.0	-4.7 ✓	
+ 50	"		14.0	-4.7 ✓	
T.P.	5.67	9.43	5.58	3.76 ✓	
+ 58			14.4	-5.0 ✓	

9.43

20

+ 61	Mud	15.5	-6.1 ✓	
+ 65	"	14.4	-5.0 ✓	
126	"	14.3	-4.9 ✓	
+ 50		13.3	-3.9 ✓	
127		12.6	-3.2 ✓	
+ 40		12.4	-3.0 ✓	
+ 54		5.3	+4.1 ✓	
+ 60		5.1	4.3 ✓	
+ 66		5.5	3.9 ✓	
+ 71		5.0	4.4 ✓	
127 + 81.8	Junction	5.22	4.21 ✓	Spike in Tie
check to Mu6 P.17		5.33	4.10 ✓	4.10

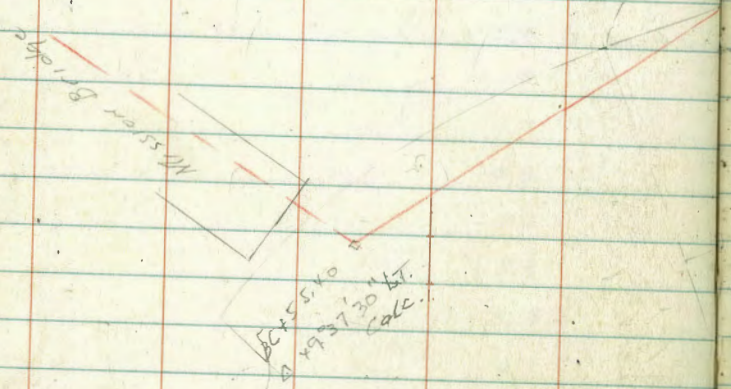
c Srvc

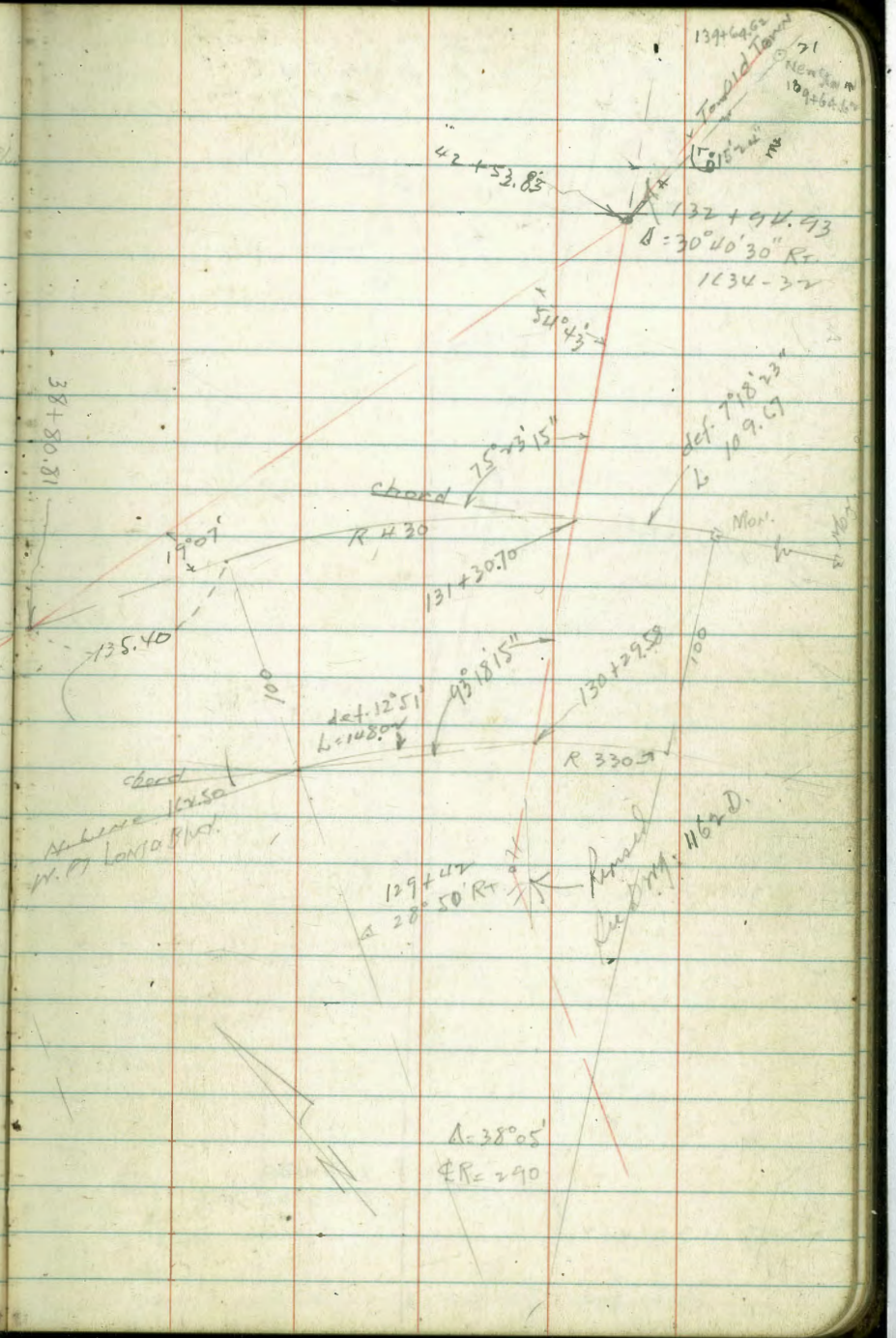
6-12-44

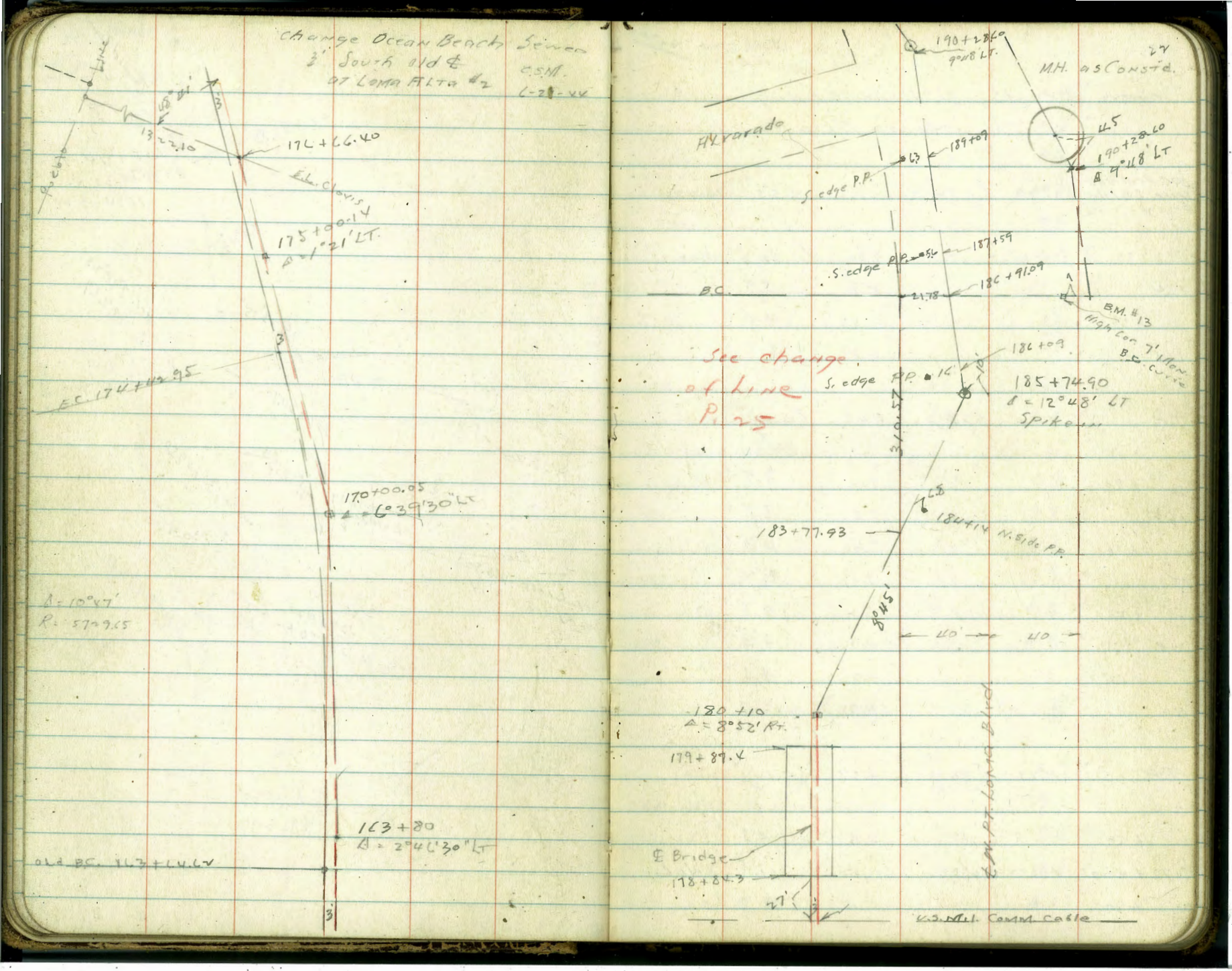
Ocean Beach Trunk Sewer

Prop. Ties at Bacon & W. Pt Loma Blvd

Correction from A P. 8






Change Ocean Beach Sewer
3' South old ℄
of Loma Alta ℄
C.S.M.
L-28-44
17L+66.40
℄ Closes
175+00.00
Δ = 1°21' LT.
EC 174+12.95
170+00.05
Δ = 6°39'30" LT
Δ = 10°47'
R = 5729.65
163+80
Δ = 2°46'30" LT
Old BC 163+44.64
190+28.60
9°48' LT.
M.H. as Constd.
Alvarado
189+09
℄ 5
190+28.60
Δ 9°48' LT
S. edge P.P.
187+59
S. edge P.P.
186+91.09
B.C.
21.78
B.M. #13
High Con 7' West
B.C. Curve
See change of Line P. 25
186+09
S. edge P.P. ℄
185+74.90
Δ = 12°48' LT
Spike
310.57
184+14 N. Side P.P.
183+77.93
80.45'
40'
40'
180+10
Δ = 8°52' Rt.
179+89.4
℄ Bridge
178+84.3
27'
S.D.G.&E. Comm. Cable
S.D.G.&E. Power Lines Blvd.

June 1944

Sewer Levels, 3' Line Change
Tierra Santa Alta #2

BM. Drilled Spike S.E. Pile Bridge	3.99	(8.54)		4.55	1634-44 160+81
163+80	2°46'30" LT.		4.72	(3.82)	4.6
164			0.6	3.9	
+50			4.5	4.0	
165			4.8	3.7	
TP	5.xx	(9.31)	4.45	(4.09)	
+50			5.x	3.9	
166			5.5	3.8	
+50			5.3	4.0	
167			5.1	4.x	
+50			5.0	4.3	
168			4.9	4.4	
+50			4.7	4.6	
169			4.9	4.4	
T.P.	4.77	(9.41)	4.67	(4.64)	
+50			4.9	4.5	
170+00.05	Δ 1°39'30" LT.		4.50	4.91	Hub
+50			5.x	4.x	
171		(9.41)		5.0	4.4
+50				4.9	4.5
172				4.8	4.6
+50				4.8	4.6
173				4.8	4.6
+50				4.7	4.7
TP	3.89	(9.17)		4.13	(5.28)
174				4.6	4.6
+50				4.8	4.4
175+00.14	Δ 1°21' LT.			5.15	(4.07) Hub
+50				5.5	3.7
176				5.x	3.8
+50				5.6	3.6
177				5.3	3.9
+50				4.9	4.3
178				4.7	4.5
T.P.	4.9x	(9.51)		4.58	(4.59)
+50				4.8	4.7
178+84.3	Top Tie Wrench Bridge			4.4	5.1
179+87.4	" " " " "			4.4	5.1
+88				5.0	4.5
180+10	Δ 8°57' RT.			5.03	4.48 Hub

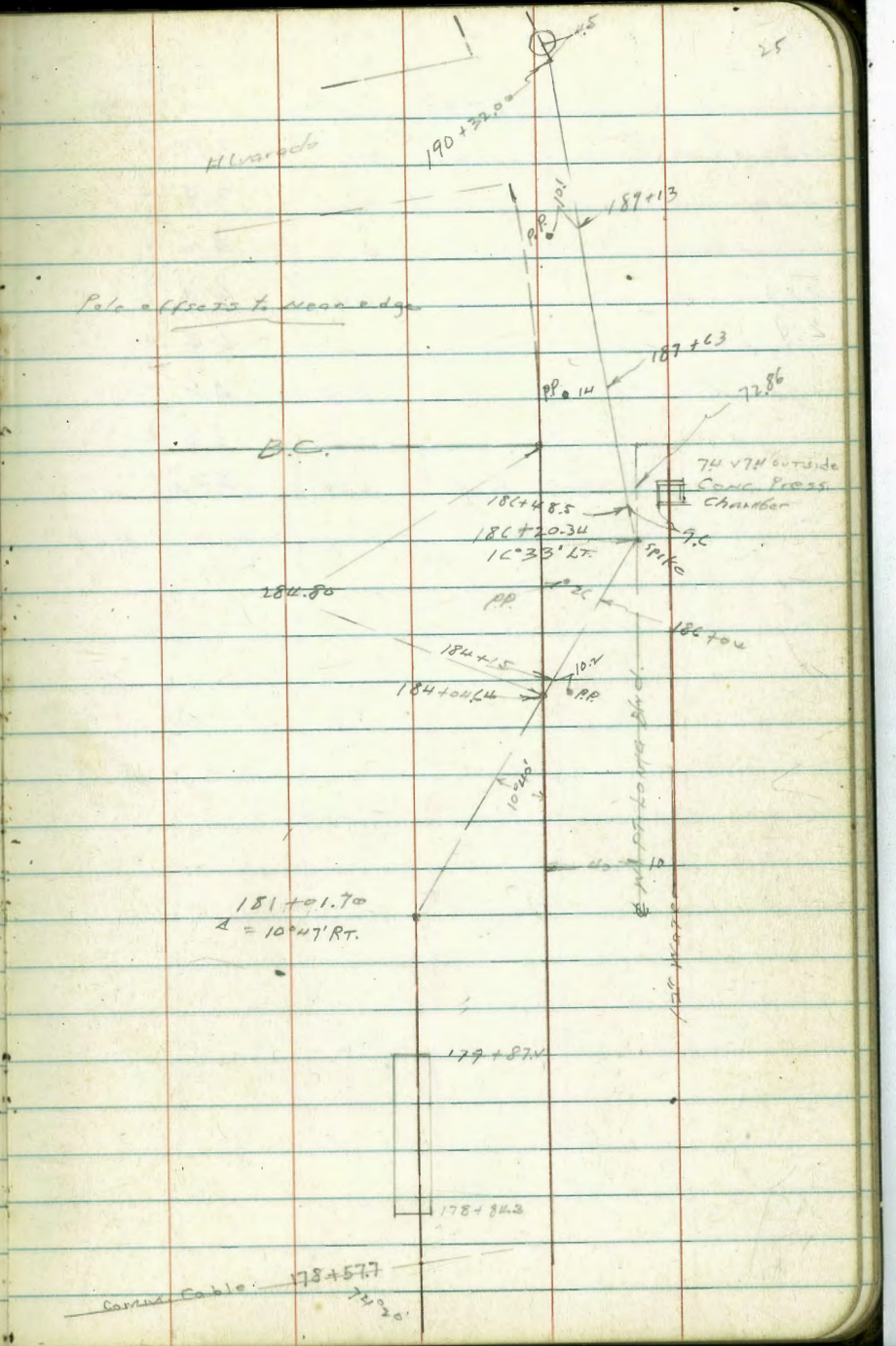
		(9.51) ✓			
180+30			5.6	3.9 ✓	
+48			5.7	3.8 ✓	
181+03			11.7	−1.7 ✓	
+50			12.4	−2.9 ✓	
182			12.5	−3.0 ✓	
T.P.	4.50	(6.87) ✓	7.19	(2.32) ✓	
+50			9.9	−3.1 ✓	
183			9.5	−2.7 ✓	
+35			9.7	−2.4 ✓	
+78			5.8	1.0 ✓	
+83			5.3	1.5 ✓	
184			5.5	1.3 ✓	
+50			4.7	2.1 ✓	
+75			4.5	2.3 ✓	
+92 N edge oil Pav			5.1	1.7 ✓	
185 oil "			4.9	1.9 ✓	
+50 " "			4.1	2.7 ✓	
185+74.90 A 12°48' LT.			3.8	3.0 ✓	Spike in Pav. 0.1
186 oil pav			3.7	3.1 ✓	
+50 " "			3.6	3.2 ✓	
T.P.	6.08	(9.09) ✓	3.81	(3.01) ✓	
187 oil pav			5.7	3.4 ✓	

		(9.09) ✓			24
187+50 N. edge oil Pav.			5.6	3.5	
188 dirt			5.0	4.1	
+50 "			4.7	4.4	
189 "			4.6	4.5	
+50 N edge oil Pav.			4.8	4.3	
190			4.6	4.5	
190+78.6 = Stub end			4.1	5.0	
Check to B.M. #3 on B.C.		4/3 S. 7' Mon.	5.69	(3.40) ✓	3.46 / 0.06
B.M. #12. R.R. Spike in Pole 8.2.3		2.84	(9.16) ✓	6.32	5.66 M.P. Long Stub 190+00
Ex. N.H. R.M.		West end Culvert Job	4/3	5.03 ✓	
" " Feb. 1		" "	15.45	−6.79 ✓	

C.S.M.
C-27-4x

Sewer line change from p. 22

				180+50 Hub p. 23
	1.97	C.L.S. ✓	4.48 ✓	
180+50		2.3	4.1 ✓	
181+01.7	∠ 10°47' RT.	2.70	3.75 ✓	Hub
+32		3.1	3.3 ✓	
+50		4.7	1.7 ✓	
+68		7.6	−1.1 ✓	
182		9.0	−2.6 ✓	
+50		9.5	−3.1 ✓	
183		9.5	−3.1 ✓	
+50		9.2	−2.8 ✓	
+75		8.8	−2.4 ✓	
184+14		4.9	1.5 ✓	
+50		4.4	2.0 ✓	
TP	C.L.X	(8.79) ✓	4.30	(2.15) ✓
+73		6.5	2.3 ✓	
185	edge oil Pav	6.9	1.9 ✓	
+50	Pav	6.1	2.7 ✓	
186	Pav	5.4	3.4 ✓	
186+20.34	∠ 1C°33' LT.	5.25	3.54 ✓	Spike in Pav.
+48.5		5.2	3.6 ✓	
"	9.6 RT	Bot. Con. Box	12.68	−3.89
187		5.1	3.7 ✓	



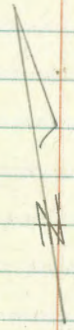
(8.79) ✓

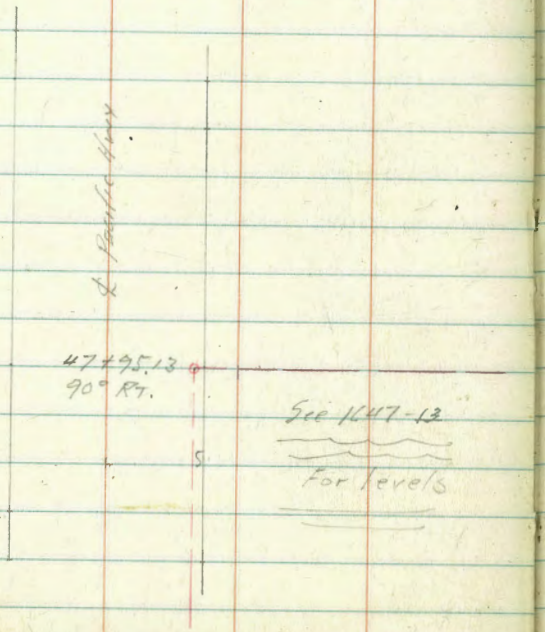
187 + 50	5.1	3.7	✓
188	5.0	3.8	✓
+ 50	4.6	4.2	✓
189	4.4	4.4	✓
+ 50	4.4	4.4	✓
190	4.3	4.5	✓
+ 32	3.8	5.0	✓
+ 36.5 E N.H. R.M.	3.85	4.94	✓
EL.		-6.79	P.V.

Old Town to Pacific Beach
Trunk Sewer
Proposed change of line from
Linda Vista Sewer Junction
to Jellette St.

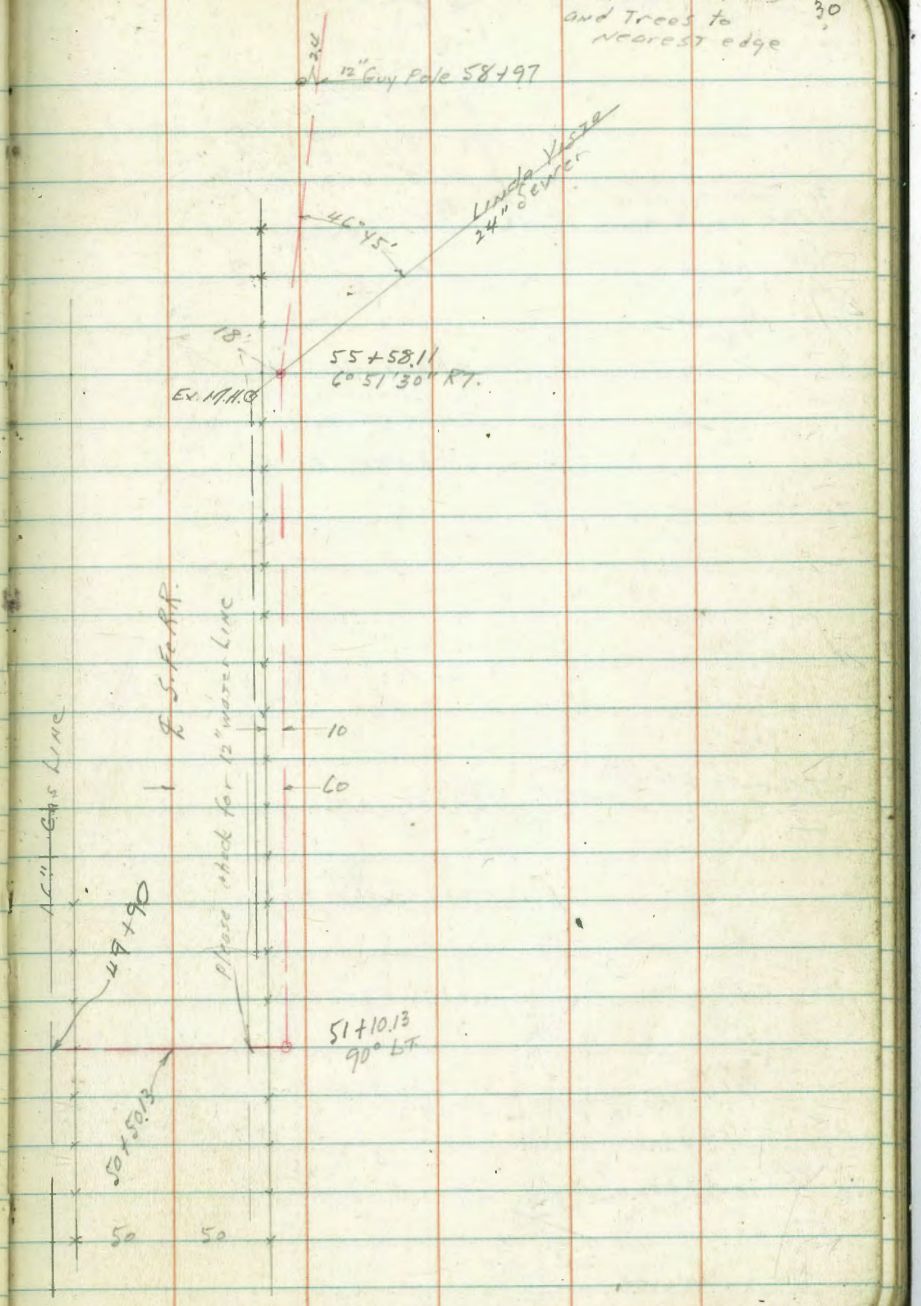
E. Moore
Sanitary Engr.
W. Moore
11-43

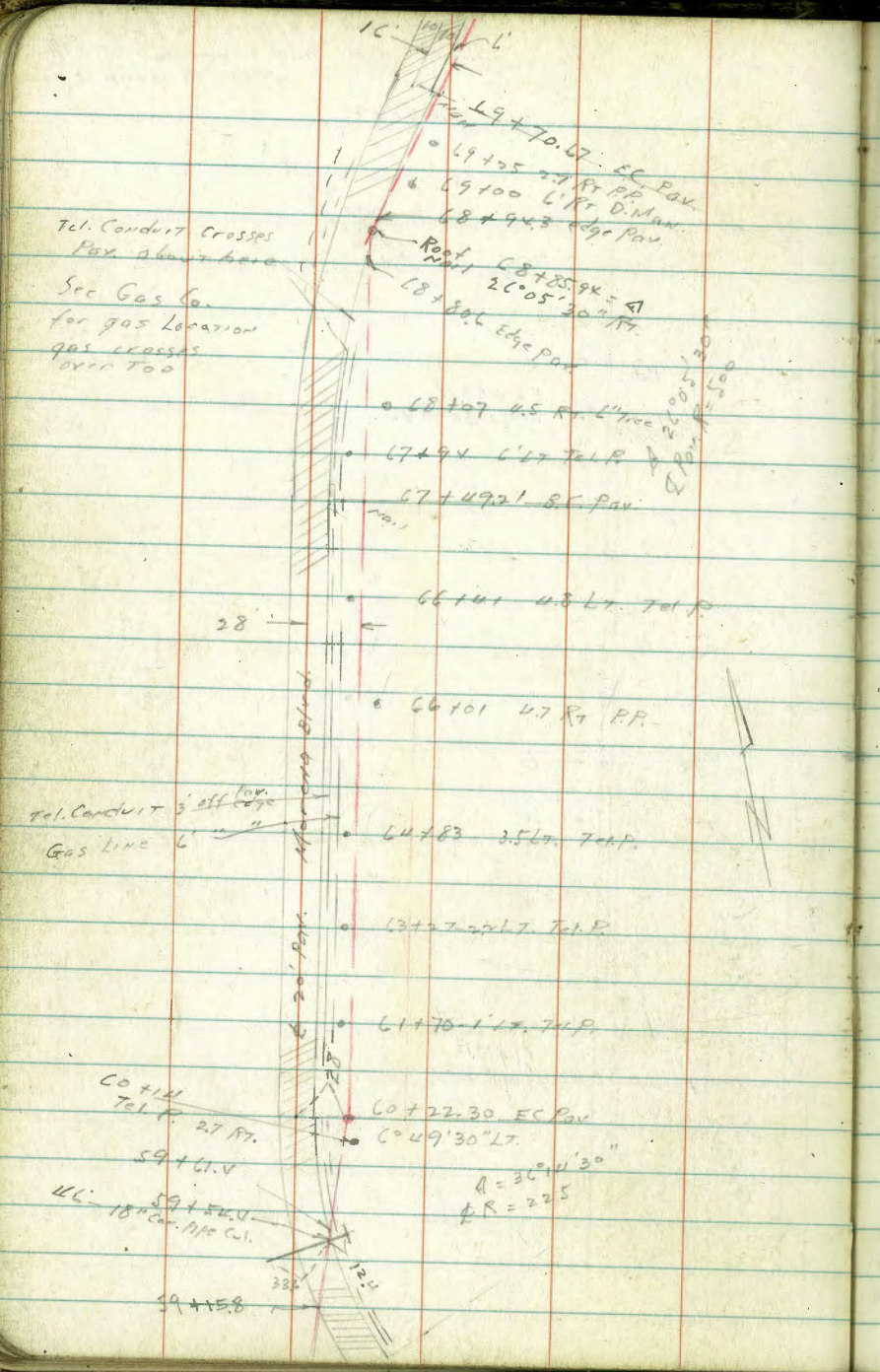
Via Morena Blvd.

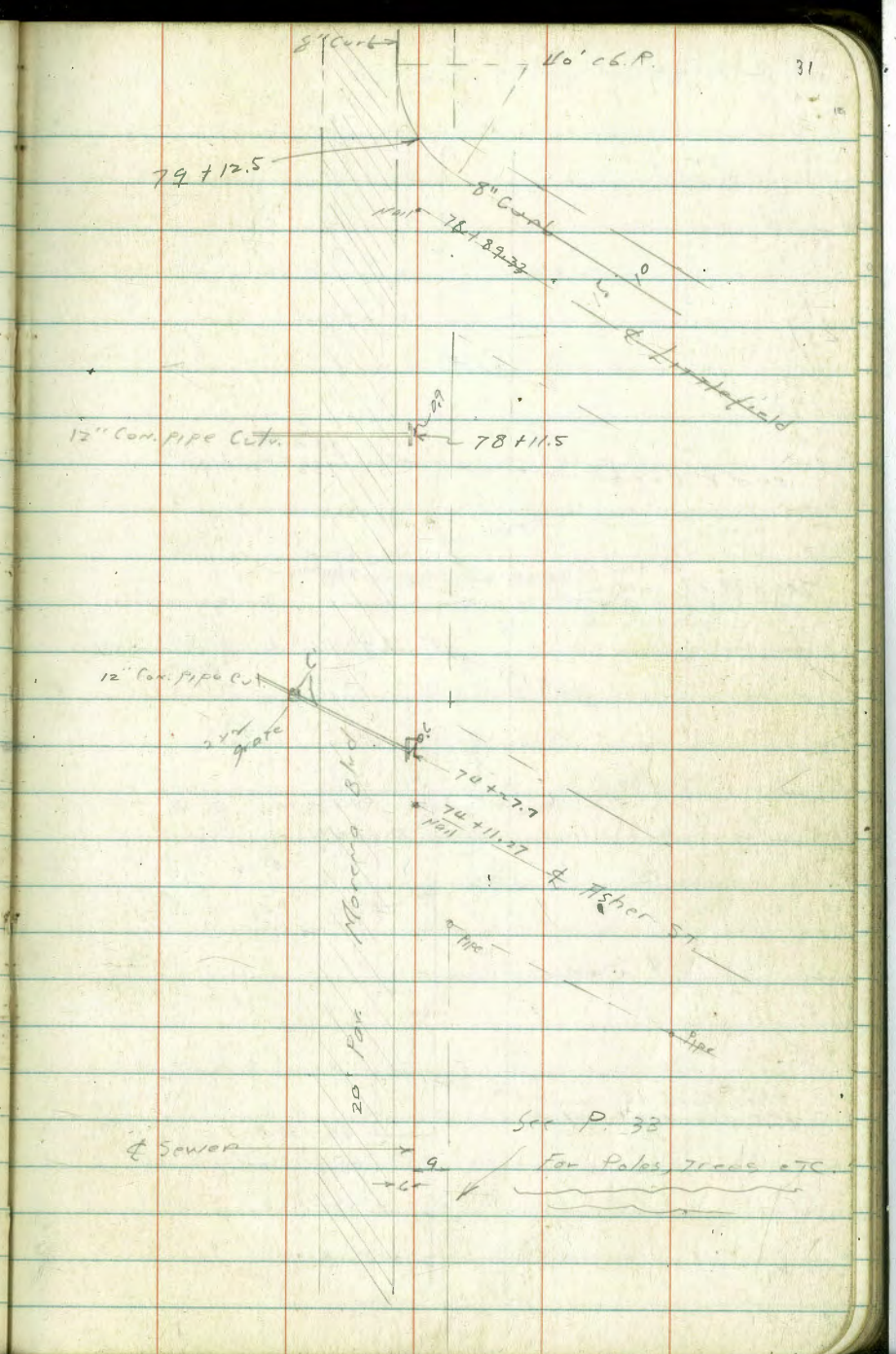


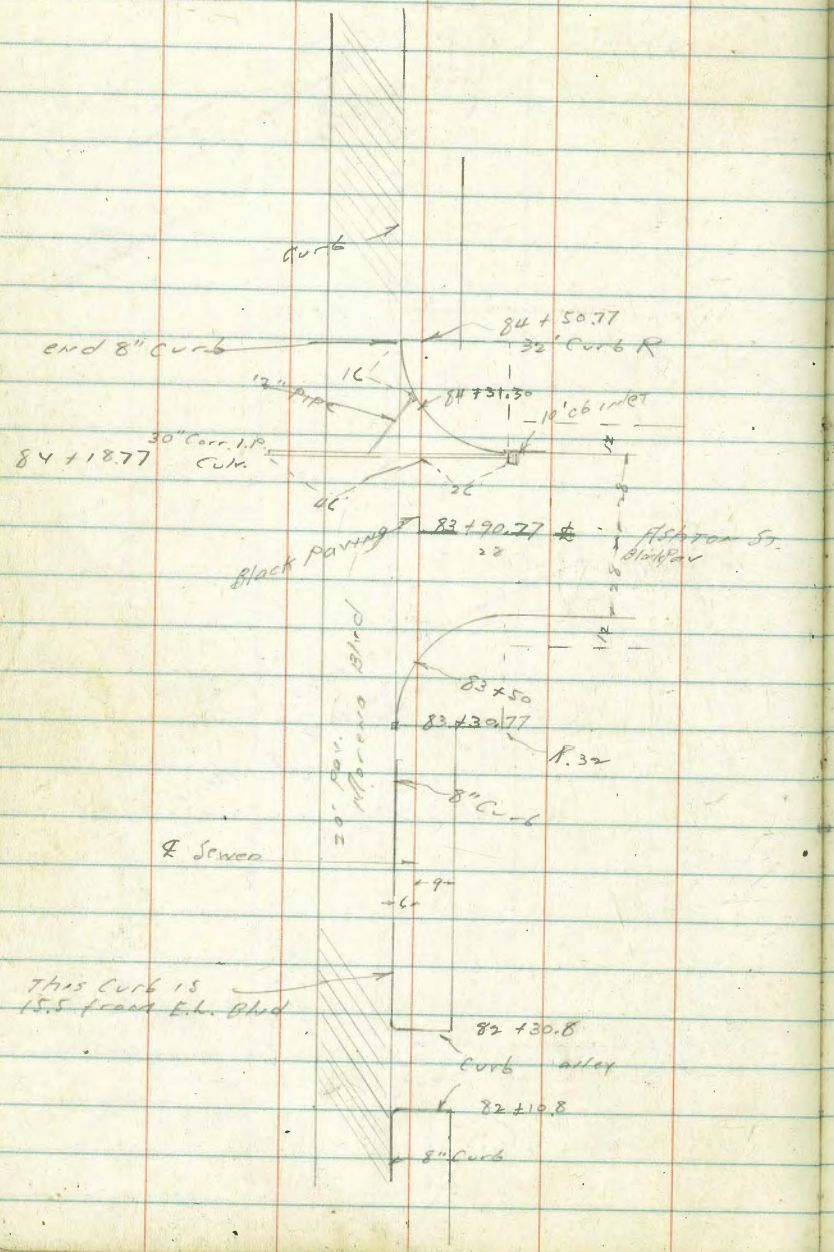


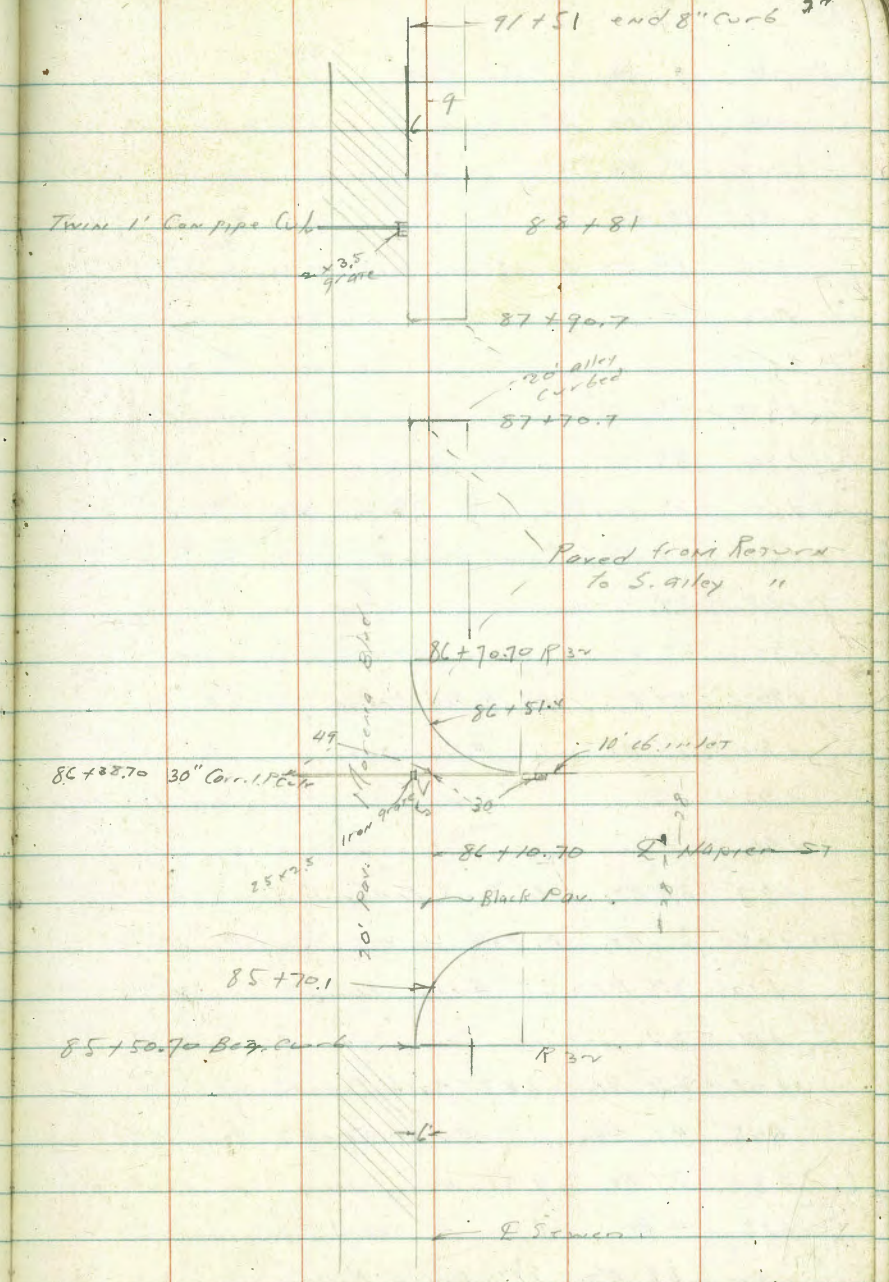
Offsets to Poles and Trees to nearest edge




Tel. Conduit crosses Pav. about here
See Gas Co. for gas Location gas crosses over Too
Tel. 49+70.67 EC Pav.
49+25 2.7 Rt P.P.
49+00 6' Rt D. Man.
68+94.3 Edge Pav.
Road 68+85.94 = 20°05'30" Rt.
68+80± Edge Pav.
68+07 4.5 Rt. 6" Tree
67+94 6' Rt Tel. P.
67+49.2 EC Pav.
66+41 4.8 Lt. Tel P.
66+01 4.7 Rt P.P.
Tel. Conduit 3' off Pav. Edge
Gas Line 6'
64+83 3.5 Lt. Tel P.
63+27 2.7 Lt. Tel P.
61+78 1' Lt. Tel P.
60+41 Tel P. 2.7 Rt.
60+22.30 EC Pav.
6°49'30" Lt.
Δ = 36°41'30"
R = 225
59+61.4
59+54.0
18" Con. Pipe Cul.
33.2'
12.4
59+15.8
28'


8" Curb
40' C.R.
79+12.5
8" Curb
Wall 78+89.33
℄ Intersection
12" Con. Pipe Cul.
78+11.5
12" Con. Pipe Cul.
24" Gate
74+7.7
Wall 74+11.27
℄ Fisher St.
Fire
Fire
Fire
20' Pav
℄ Sewer
See P. 32
For Poles, Trees etc.


curb
84 + 50.77
32' curb R
end 8" curb
12" pipe
84 + 31.50
10' cb inlet
84 + 18.77
30" Corr. I.P. Culv.
46'
26'
83 + 90.27
Alsaton St.
Black Pav't
83 + 50
83 + 30.77
R. 32
8" C-6
℄ Sewer
This Curb is 15.5 from E.L. Blvd
82 + 30.6
curb alley
82 + 10.8
8" Curb


91 + 51 end 8" Curb
Twin 1' Con. pipe Culv.
88 + 81
87 + 90.7
120' alley curbed
87 + 70.7
Paved from Rotary to S. alley
86 + 70.70 R 32
86 + 51.4
10' cb. inlet
86 + 38.70 30" Corr. I.P. Culv.
86 + 10.70
℄ Napier St
Black Pav.
85 + 70.1
85 + 50.70 Beg. Curb
R 32
℄ Sewer

70 +31	9' Rt	10" Pine Tree
+40	11 Rt	7" " "
+47	8.5 Rt	6" " "
+56	13 Rt	8" " "
+66	8.4 Rt	To 18" Sq. Brick Pillar with log rail Beg. of Brick Pillar
+82	" "	" " " "
71 +17.5	" "	" " " "
+35	8.5 "	" " "
+47	8.5 "	" " "
+61	8.5 "	" " "
+67	3.9 Rt	6" Eucal Tree
+68	3.9 "	" "
+75	3.5 "	" "
+80	8.7 Rt	18" Brick Pillar
+87	3.6 Rt	6" Eucal Tree
+90	3.5 "	" "
+96	" "	" "
+99	8.8 Rt	18" Brick Pillar
72 +05	3' Rt	P. Pole
+10	3.7 Rt	5" Eucal Tree
+17	3.7 "	" "
+21	8.9 Rt	18" Brick Pillar
+25	4.1 Rt	8" Eucal Tree
+30	3.7 Rt	9" " "
+38	4 Rt	6" " "
+42	8.8 Rt	18" Brick Pillar
72 +47	8.9 Rt	18" Brick Pillar
+53	" "	" " "
+73	" "	" " "
+77	9 "	" " "
+85	" "	" " "
73 +07	" "	" " "
+31	9.1 "	" " "
+53	9.1 "	" " "
+74	3' Rt	Power P.
+78	9.2 Rt	18" Brick Pillar
75 +34	3.3 Rt	Power P.
77 +09	3.6 "	" "
+21	2.6 "	8" Acacia Tree
78 +60	4 Rt	Power P.
79 +31	4.7 "	Guy P.
+38	" "	D. Main
82 +10.8	66 alley	
+30.8	" "	
+32	4.1 Lt	Power P.
+60	4 Rt	16" Eucal Tree
83 +30	1 "	Lt " "
+48	0.2 Rt	Power Pole Acc Lt
84 +55	16 Lt	40" Eucal Tree
85 +01	1.5 "	" " "
+55	2.7 "	30" " "
87 +60	2.0 "	" " "

88+10	2.5 Lt	30" Excel Trace
+60	1.9 "	" " "
100+75.5	on Line "	" "
102+24.5	" "	" " "
103+25.5	1.5 Lt	36" " "
104+50	2.5 "	24" " "
105	2 "	30" " "
+50	4 Rt	9" " "
106	1 "	24" " "
+51	4.5 "	" " "
107	8 "	30" " "
109+75	3.5 Lt	R.R. wig wag Sig. will be removed
110+04.5	1.5 Rt	Sta. R.R. X Sign

Pgx B.C. 102+17.61

104+00.5± ℄ K&NE

103+58 2' Rt Water gate
See Water Dept.

24" Con. Pipe Culv 101+99 37 1N107 on Line

℄ Prop. Sewer

99+60.5± ℄ Historic

20' Pgx. 1N6 Conc Bldg

6 9

95+30.5± ℄ Milton

Spike

℄ Sewer

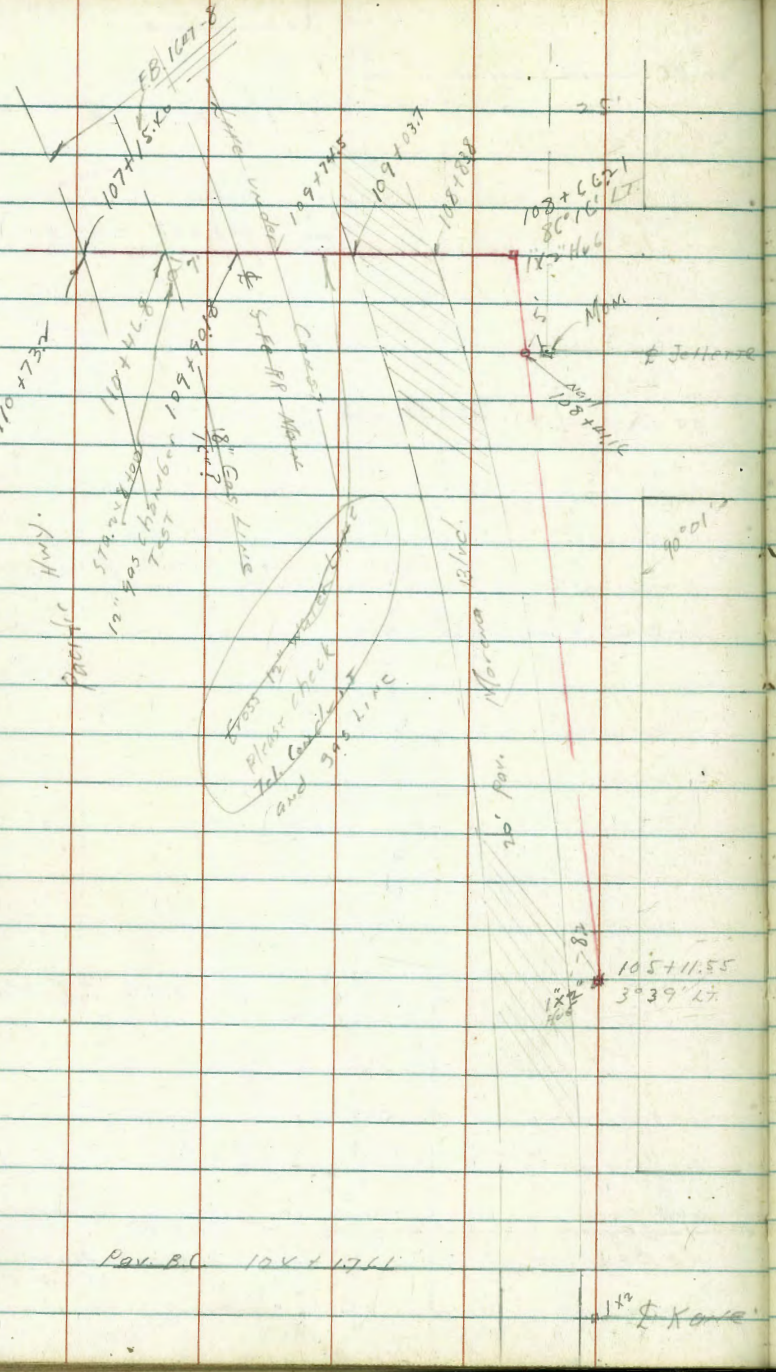
4" Sewer To Bay

92+40

Flank Bay Shore Motor Court

about 4' deep

6 9


FB. 1607-8
107+45.6
107+44.8
110+73.2
109+90.8
109+74.5
109+03.7
108+88.8
108+62.7
8°16' LT
108+44.6
Mon.
℄ Jellette
108+41.6
90°01'
Pavement
Sta. 109+90.8
10" 90° Hydrant
Test
Gross Check
Ick Coal Co.
and Gas Line
Marcum
Island
20' Road
105+11.55
3°39' LT
1"x2"
Pav. B.C. 104+17.66
1"x2" ℄ Kane

℄ Sewer levels, sketch p30

Table of elevations, 11-4-43, mv, Platted

BM chisel x S w. Edward	4.53	(10.18)		5.65	1647-12
T.P.	5.05	(11.53)	3.70	6.48	
50+92			10.2	1.3	
51+00			8.0	3.5	
51+10.12	Δ 90° Lt		6.9	4.6	
+12			9.6	1.9	
+25	cross Tecolote Creek		10.5	1.0	
+40			6.6	4.9	
+50			6.0	5.5	
52			6.8	4.7	
+50			7.3	4.2	
53			7.5	4.0	
+50			7.6	3.9	
TP	3.30	(7.77)	7.96	(4.47)	
54			4.0	3.8	
+50			4.5	3.3	
55			4.8	3.0	
+50			4.6	3.2	

Levels 1647 / 13 to #7+95 / 50+92

(7.77)

55+58.11	Δ 6° 51' 30" Rt		4.7	3.1	
"	18 Lt MH Rim		2.79	4.98	Sealed Cover
56			5.1	2.7	
+50			5.0	2.8	
+60			4.5	3.3	
+80			4.6	3.2	
57			5.0	2.6	
+50			5.0	2.8	
58			5.0	2.8	
+50			4.9	2.9	
T.P.	11.04	(14.51)	4.30	(3.47)	
+91			11.5	3.0	
59			9.4	5.1	
+15.8	edge Pav.		9.72	4.79	
+54.4	Int. Cr/v.		10.96	3.55	Pav.
"	12.4 Rt F.L. inlet		14.88	- 0.37	18" Cr/v.
"	33.6 Lt " outlet		15.59	- 1.08	" "
+61.4	edge pav		11.24	3.30	
60			10.8	3.7	
+23.3	Δ 6° 49' 30" Lt		10.6	3.9	
+50			10.3	4.2	
61			8.4	6.1	
+30			7.5	7.0	
+40			5.8	8.7	
"	9 Rt		5.0	9.5	
"	7 Lt		9.1	5.4	

		(14.51)			
1+60			4.2	10.3	✓
"	9 RT		3.5	11.0	✓
"	7 LT		9.3	5.2	✓
Cr 1+00			3.2	11.3	✓
"	7 LT		8.9	5.6	✓
"	9 RT		1.7	12.8	✓
1+50			2.6	11.9	✓
"	7 RT		1.7	12.8	✓
"	9 RT		0.5	14.0	✓
"	9 LT		8.6	5.9	✓
63			1.5	13.0	✓
"	9 RT		0.3	14.2	✓
"	7 LT		1.7	12.8	✓
"	11 LT		7.9	6.6	✓
1+40			1.0	13.5	✓
"	9 RT		1+0.3	14.8	✓
"	12 LT		7.2	7.1	✓
T.P	8.32	(19.83) ✓	3.00	(11.51) ✓	Spike West Side Tel. Pole 63+27
1+50			7.3	12.5	✓
"	10 RT		10.5	9.3	✓
"	11 LT		11.6	8.2	✓
1+60			10.3	9.5	✓
"	10 RT		9.1	10.7	✓
"	10 LT		11.2	8.4	✓
64			8.8	11.0	✓
"	6 RT		9.7	10.1	✓
"	11 LT		11.7	8.1	✓

		(19.83) ✓		
1+50			9.3	10.5 ✓
"	9 RT		10.1	9.7 ✓
"	6 LT		9.2	10.6 ✓
"	11 LT		11.3	8.5 ✓
1+75			6.1	13.7 ✓
"	10 RT		8.5	11.3 ✓
"	11 LT		11.0	8.8 ✓
65			4.2	15.4 ✓
"	10 RT		7.2	12.1 ✓
"	11 LT		10.2	9.4 ✓
1+25			3.3	16.5 ✓
"	10 RT		7.2	12.4 ✓
"	7 LT		8.7	11.1 ✓
"	13 LT		9.9	9.9 ✓
1+50			4.6	15.2 ✓
"	6 LT		8.2	11.4 ✓
"	11 LT		9.2	10.6 ✓
"	6 RT		6.0	13.8 ✓
1+60			4.1	15.7 ✓
"	10 RT		6.3	13.5 ✓
"	9 LT		8.0	11.8 ✓
1+70			4.5	15.3 ✓
"	7 LT		1.2	18.6 ✓
"	6 LT		7.3	12.5 ✓
66			5.6	14.2 ✓
"	6 RT		2.7	17.1 ✓
"	6 LT		6.6	13.2 ✓

		(19.83)							(27.61)		
CC +15			4.3	15.5			+50			9.6	18.0
"	6 RT		3.2	16.6			72			10.3	17.3
"	7 LT		5.7	14.1			+50			10.7	16.9
+50			3.2	16.6			T.P.	1.92	(19.09)	10.51	(17.19)
"	6 RT		1.7	18.1			73			3.C	15.4
"	10 LT		5.2	14.6			+50			4.0	15.0
67			1.3	18.5			74			4.4	14.6
T.P.	8.45	(27.61)	0.67	(19.6)			+11.27			4.5	14.5
67 +49.21			8.1	19.5			+20			4.C	14.4
+90			6.8	20.8			+27.7	F.L. 12" Conc. Pipe Cul.		7.44	11.58 0.6 LT
68			3.8	23.8			+30			4.4	14.6
+10			5.1	22.5			+50			4.5	14.5
+25			6.1	21.5			75			4.5	14.5
+45			5.8	21.8			+50			4.7	14.3
+55			6.2	21.4			76			5.0	14.0
+85.94	A 26° 05' 30" RT.		5.38	22.23	pav.		+50			5.0	14.0
69			5.47	22.14			77			5.2	13.8
+50			6.2	21.4			+50			5.3	13.7
" 2	RT		6.0	21.6			78			5.5	13.5
" 5	RT		+2.3	29.9			+05			5.8	13.2
70			7.3	20.3			+11.5	F.L. 12" Conc. Pipe Cul.		8.15	10.87 0.7 LT
" 1	RT		7.2	20.4			+20			5.C	13 4
" 5	RT		1.4	26.2			T.P.	3.81	(17.67)	5.C	(13.8C)
+50			2.9	19.7			+50			4.2	13..5
" 3	RT		4.5	23.1			+89.33			3.7	14.0
71			8.5	19.1			79			3.8	13.9
3 RT			7.5	20.1							

79 +12.5			3.7	14.0	✓
"	Top Cvr 6		3.10	14.57	✓
+50			2.6	15.1	✓
Set BM Spike 7ct			3.2	(14.43) ✓	NW Cor Manning Shut Lizzie field
+50			3.8	13.9	✓
80			4.0	13.7	✓
+50			4.1	13.6	✓
81			4.2	13.5	✓
+50			4.5	13.2	✓
82			4.5	13.2	✓
+10.8	Top Cvr 6		4.76	(12.91) ✓	
"			5.3	12.4	✓
+30.8			5.3	12.4	✓
"	Top Cvr 6		4.88	(12.79)	
+50			5.1	12.6	✓
83			5.2	12.3	✓
+30.77	Hub 6		5.42	12.05	✓
+50	Top Cvr 6		5.60	12.07	✓
"	Gut Pav.		6.27	11.40	✓
+90.77	Pav	& Ashton	6.40	11.27	✓
TP	537	(11.44) ✓	6.40	(11.27) ✓	
84	Pav		5.45	11.19	✓
+18.77	Int 30" Culv.		5.70	10.94	✓ on Pav
"	24' Rt El Inlet		8.91	7.73	✓
"	48 Lt " outlet		13.20	3.44	✓
+31.3	Gut Pav		5.62	11.02	✓
"	Top Cvr 6		4.88	11.76	✓

		(10.64)			
+50			5.7	10.9	✓
85			5.6	11.0	✓
+50.7			5.6	11.0	✓
+70.12	Top 66		5.21	11.43	✓
"	Gut Pav		5.66	10.98	✓
86	Pav		5.68	1095	✓
+10.7	E Napier		5.66	11.00	✓
+32.7	Int 30" Culv.		5.69	10.98	✓ Pav
"	30 Rt El Inlet		9.19	7.45	✓
"	48 Lt " outlet		12.89	3.75	✓
+51.4	Gut Pav		5.58	11.06	✓
"	Top Cvr 6		4.94	11.70	✓
87	Pav.		4.73	11.91	✓
+50	"		4.85	11.79	✓
+70.7	Top 66 in drive		4.63	12.01	✓
"	Gut Pav		5.2	11.4	✓
+90.7	"		5.2	11.4	✓
"	Top Cvr 6		4.63	12.01	✓
88			4.8	11.8	✓
+50			4.8	11.8	✓
+81	E Lt El	Twin 6' Pipes	8.11	8.53	✓ Culv Inlet
TP	4.84	(12.15) ✓	4.33	(12.31) ✓	
89			5.5	11.6	✓
+50			5.6	11.5	✓
90			5.3	11.8	✓
+50			5.0	12.1	✓

				⟨17.15⟩				
91			5.0	12.1				
+50			5.0	12.1				
92			5.0	12.1				
+50			5.0	12.1				
93			5.0	12.0				
+50			5.3	11.8				
94			5.3	11.8				
+50			5.5	11.6				
95			5.9	11.2				
+30.5m	E Milton		5.9	11.2				
+50			6.1	11.0				
T.P. spike Tel pole	28	⟨14.77⟩	5.25	⟨11.90⟩	SW Cor Milton Nursing Home			
96			4.4	10.3				
+50			4.6	10.1				
97			4.8	9.9				
+50			4.8	9.9				
98			5.1	9.6				
+50			5.3	9.4				
99			5.3	9.4				
+50			5.3	9.4				
+60.5m	E Linton St		5.3	9.4				
100			5.5	9.2				
+50			5.8	8.9				
101			5.8	8.9				
T.P.	516	⟨14.06⟩	5.8	⟨8.90⟩				
+50			5.7	8.4				

				⟨14.06⟩				
+94			5.8	8.3				
+99	El. inlet 24" ppc Culv.		7.73	6.33				
102 +0.5			5.7	8.4				
+50			5.6	8.5				
103			5.5	8.6				
+50			5.2	8.9				
104 +00.5m	E Kane, Hib		4.71	9.35				
+50			4.6	9.5				
105			4.7	9.4				
+11.55	Δ 3°39' LT		4.9	9.2				
+25			4.6	9.5				
"	4 RT		1.5	12.6				
+50			1.2	12.9				
"	4 LT		4.5	9.6				
"	3 RT		1.1	13.0				
106			0.8	13.3				
"	4 LT		3.7	10.4				
"	3 RT		0.1	14.0				
+25			3.4	10.7				
	3 RT		0.6	13.5				
+50			3.0	11.1				
"	4 RT		0.0	14.1				
107			2.4	11.7				
"	1 RT		2.4	11.7				
"	4 RT		0.0	14.1				
T.P.	619	⟨18.27⟩	1.98	⟨12.08⟩				

(18°37')

107+50			6.1	12.2	
108			4.7	13.6	
+41.6	E Jellette		4.1	14.2	
+66.1	Δ 86°16'27"		4.20	14.07	1x4 Hub
+83.8	pav. edge		4.06	14.01	
109+03.7	" "		4.23	14.04	
+50			5.4	12.9	
+75			7.0	11.3	
	E rail Mainline		5.61	12.66	
+90.8	E on Tie		6.3	12.0	
	W rail Mainline		5.90	12.37	
110			6.8	11.5	
+07			7.2	11.1	
+46.8	In 2, 16" or 18" Nat. gas Line		10.6	8.2	ground
+65			12.2	6.1	
110+73.2	FB 1647-8		13.5	4.8	
check to City BM Mon. SW Cor Marcha Blvd & Jellette			6.85	(11.4)	11.31 / 1647-2.2

El. 16" Gas Line at Jellette St.

BM Mon.	2.56	13.97		11.41
Top of 16" Gas Line at Jellette			9.92	11.05
				1.40
				12.45 El Bot outside

El. Gas Line at Linda Vista Junction

	4.61	11.59	6.98	Top rail
Top RR Bridge Signal		3.33		
" Sign to Top Pipe		7.22		
Top 16" gas Line		10.55	1.04	
		1.04		
		1.40		
		−0.36 El. Bot. 16" gas		

El. 16" Gas Line opp. Sta 55+58.11

M.H. R.M.	4.13	9.11	4.98	18' Lt. of Sta. A-55+58.11
118.5 West of A Sta. 55+58.11		9.85	−0.74	Top 16" Gas

41+17.9

El. 16" gas Line opp S. end Tecolote Bridge

BM. Bolt SW Curb	2.83	10.66	7.83	Tecolote Bridge
Top 16" gas Line 12' E of W L RR. Row.		12.68	−2.02	

Cudahy Plant

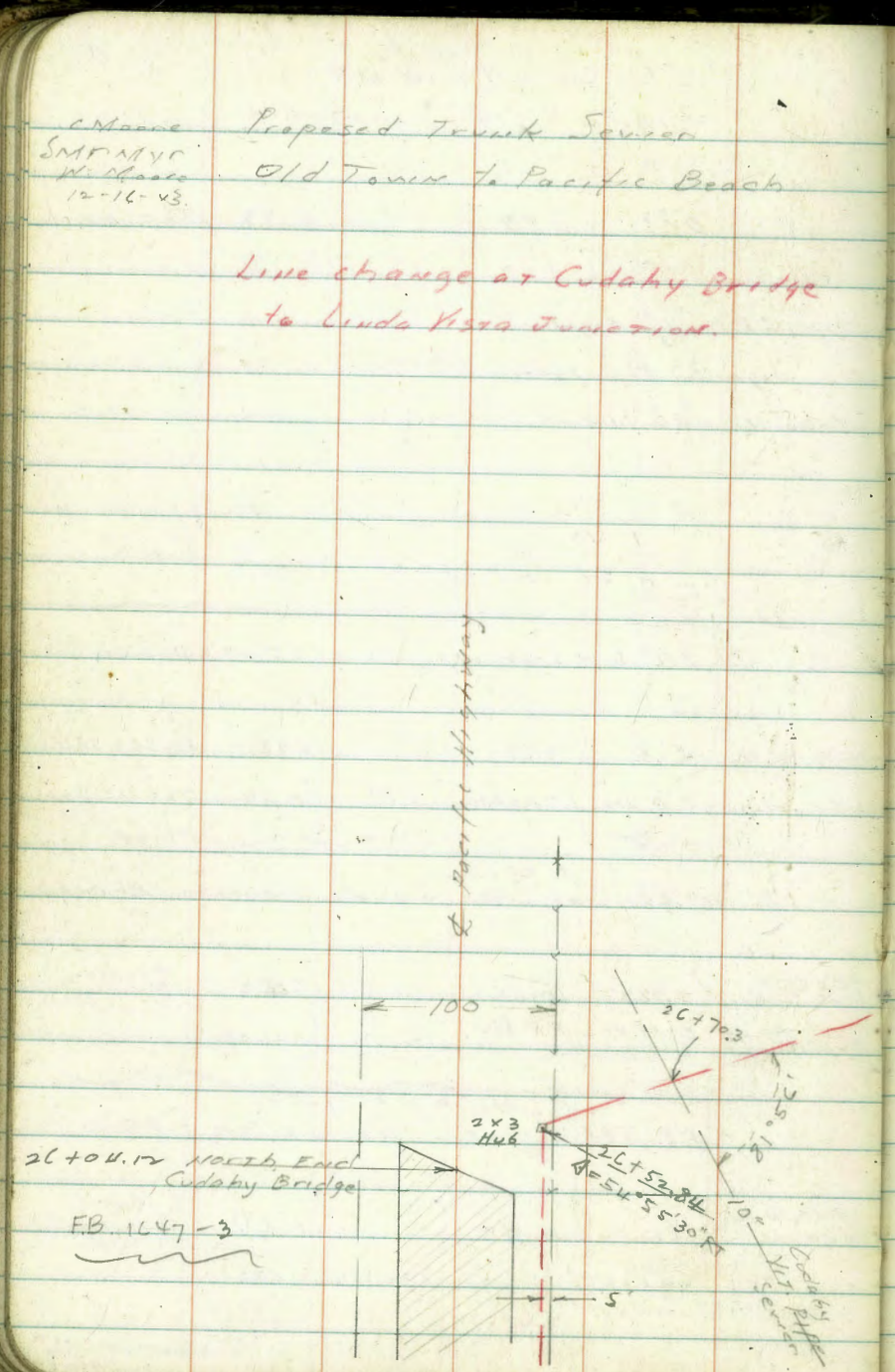
El. 16" gas Line at 29+18.5

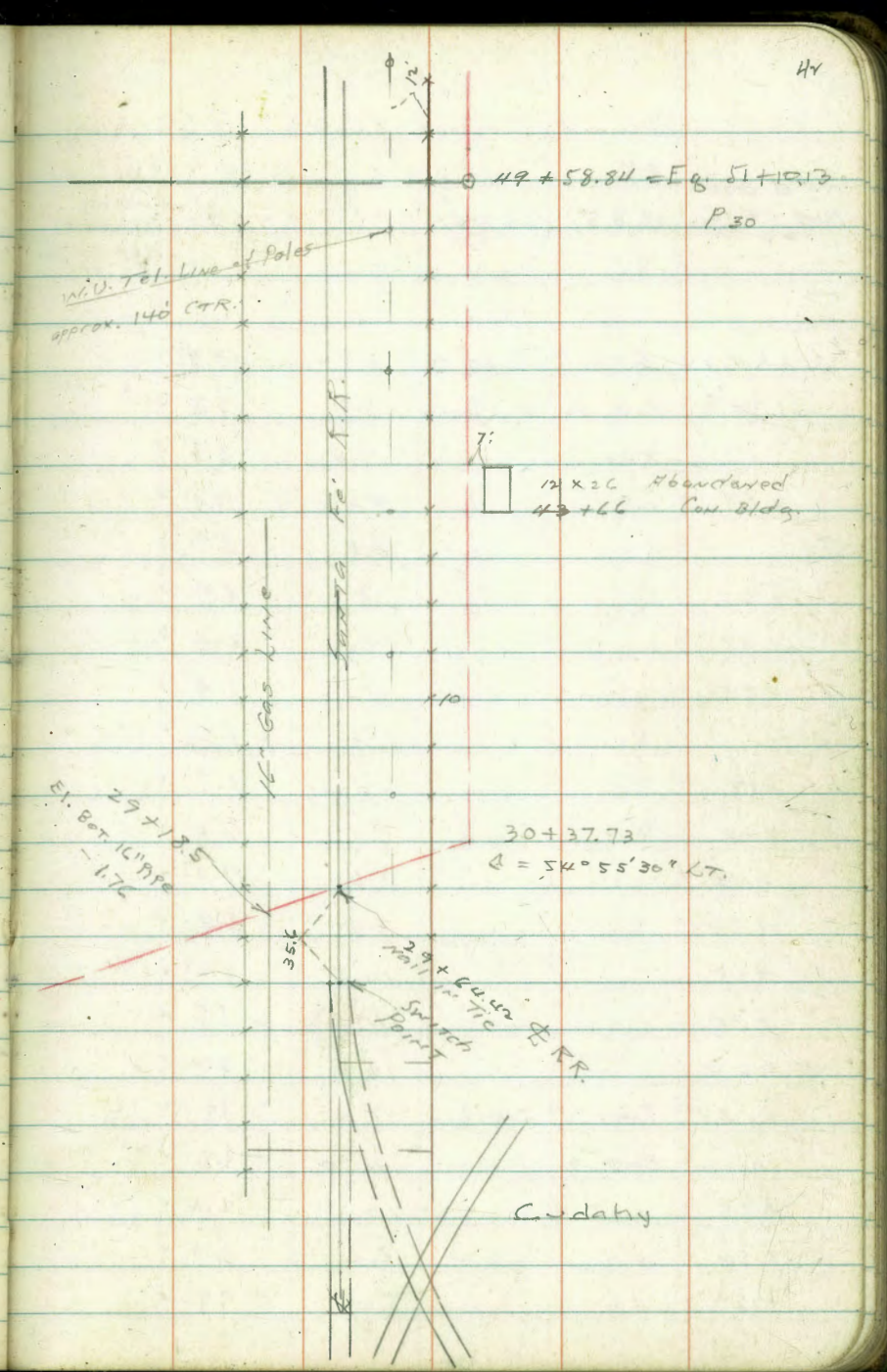
Id. 7/8 Hd Bolt NE Curb	1.20	12.91	11.09	Cudahy Bridge
Top 11" Gas 29+18.5		13.27	−0.36	
			1.40	
			−1.76 =	Bottom 16" pipe

C.M. Moore
SMF MWC
W. Moore
12-16-43.

Proposed Trunk Sewer
Old Town to Pacific Beach

Line change at Cudahy Bridge to Linda Vista Junction.





Trunk Sewer Levels Sketch p 44

□ Bolt BM NE. cor. #8	1.05	⟨12.74⟩ ✓		⟨11.69⟩ ✓	Cudahy Bridge 1647-65 +49
26 +54.84		A 54°55'30" Rt	8.8	3.9 ✓	
+70.3		Int. 10" Vit. Sewer	8.9	3.8 ✓	
"		Top " " "	9.4	3.3 ✓	
+85			9.3	3.4 ✓	
27			8.8	3.9 ✓	
+25			7.8	4.9 ✓	
+37			10.3	2.4 ✓	
+55			11.3	1.4 ✓	
28			11.5	1.2 ✓	
+17			11.0	1.7 ✓	
+28			6.5	6.2 ✓	
+40			5.6	7.1 ✓	
+56			6.8	5.9 ✓	
+68			10.5	2.2 ✓	
+80			11.2	1.5 ✓	
29 +04			10.5	2.2 ✓	
+18.5		Int. 16" Gas Line	11.0	1.7 ✓	
"		Bot. " " "	14.50	−1.8 ✓	
+35			10.3	2.4 ✓	
+50			6.6	6.1 ✓	
+59			5.0	7.7 ✓	

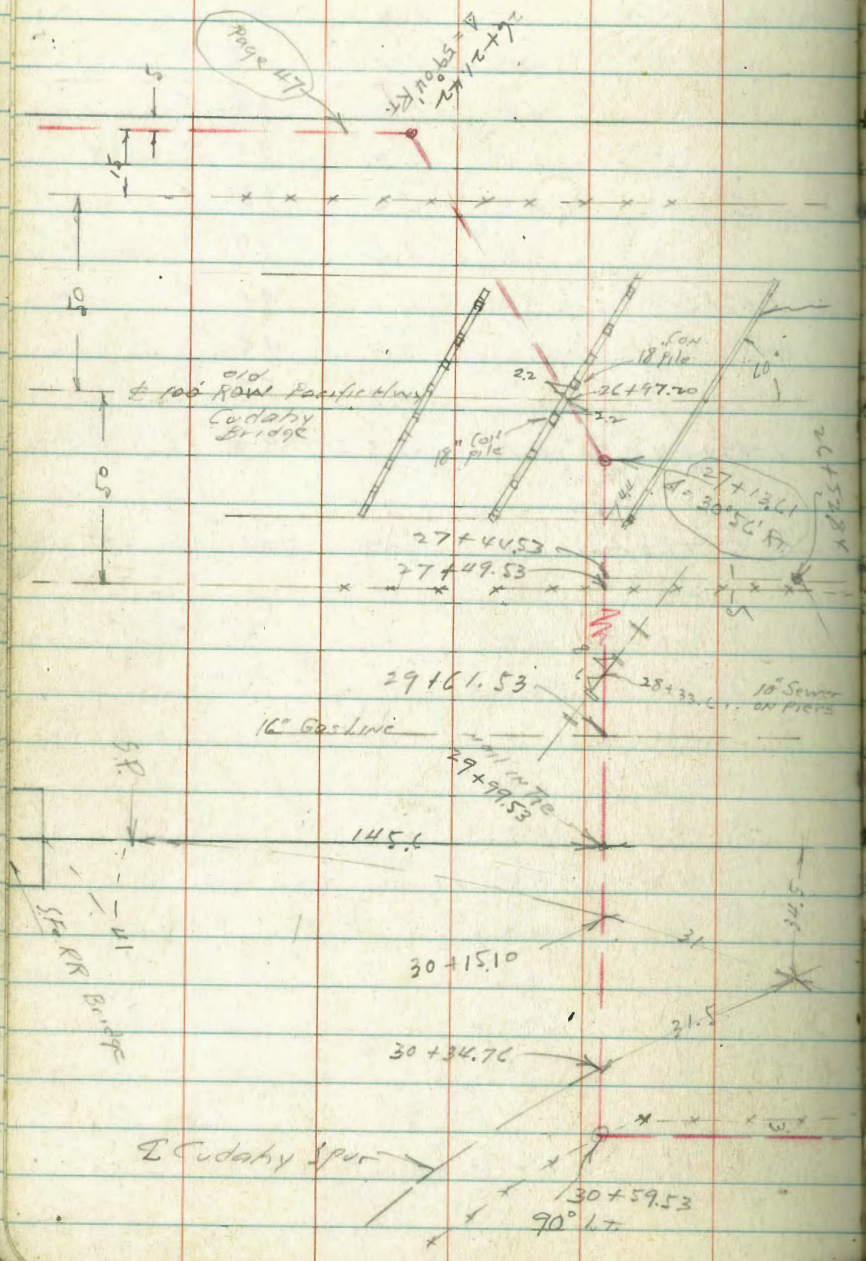
⟨12.74⟩ ✓

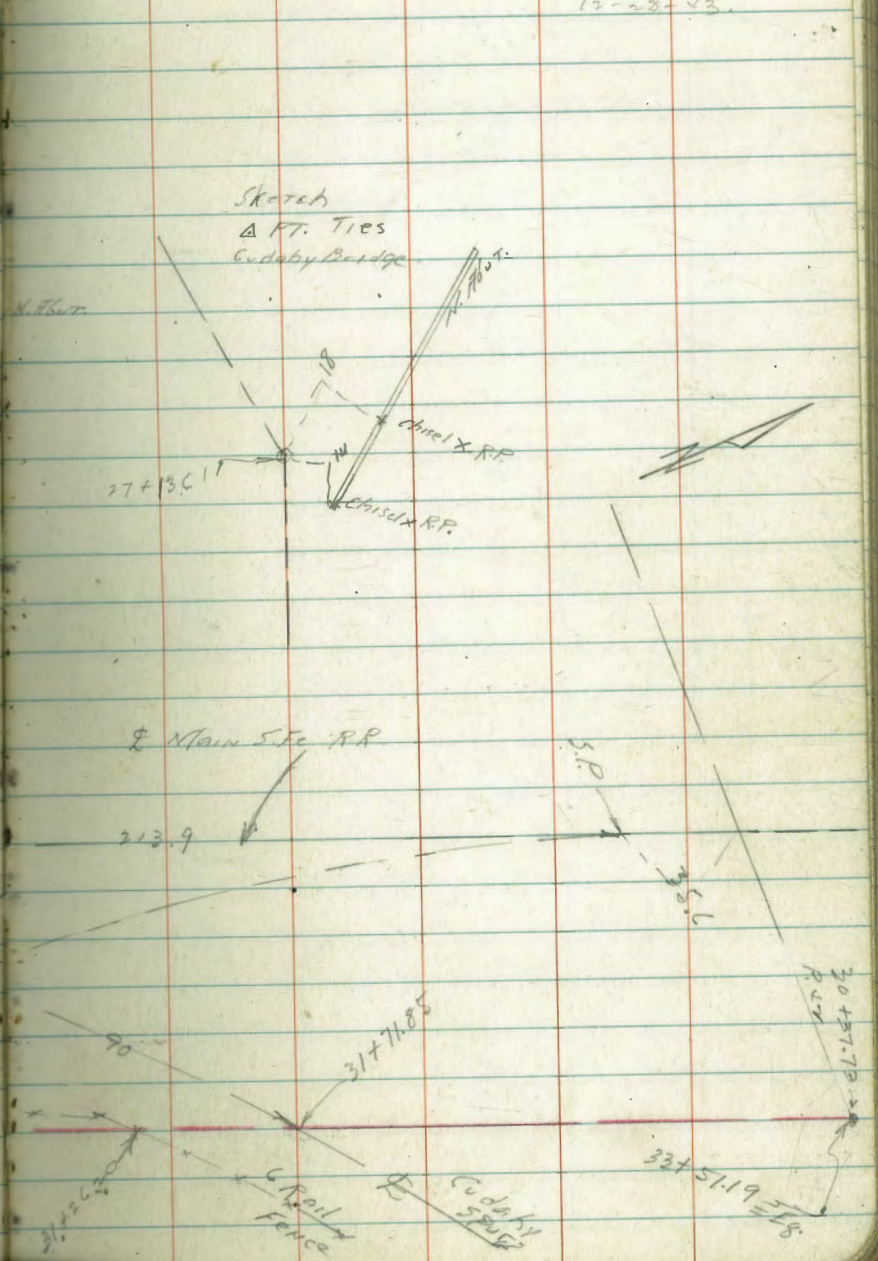
29 +64.42		& Santa Fe RR	4.8	7.9 ✓	Top of Tie
			4.21	8.53 ✓	Top rail
+71			4.9	7.8 ✓	
+77			5.8	6.9 ✓	
+90			5.9	6.8 ✓	
30 +12			7.3	5.4 ✓	
+25			11.3	1.4 ✓	
+30			11.7	1.0 ✓	
30 +37.73		A 54°5	9.4	3.3 ✓	
+50			9.8	2.9 ✓	
+75			10.7	2.0 ✓	
31			11.6	1.1 ✓	
+25		Beg. Salt Marsh	11.2	1.5 ✓	
+50			12.0	0.7 ✓	
32			11.8	0.9 ✓	
+50			11.6	1.1 ✓	
33			12.0	0.7 ✓	
T.P	4.67	⟨9.43⟩ ✓	7.98	⟨4.76⟩ ✓	
+50			8.7	0.7 ✓	
34			8.9	0.5 ✓	
+50			9.4	0.0 ✓	
35			9.6	−0.2 ✓	
+50			9.2	0.2 ✓	

		⟨9.63⟩				⟨10.08⟩		
36			9.6	-0.2	✓	45+50	8.8	2.1 ✓
+50			9.6	-0.2	✓	46	7.7	2.9 ✓
37			9.4	0.0	✓	+50	7.3	2.8 ✓
+50			10.1	-0.7	✓	47	6.9	3.2 ✓
38			9.9	-0.5	✓	+50	6.6	3.5 ✓
+50			9.8	-0.4	✓	48	6.2	3.9 ✓
39			9.7	-0.3	✓	+50	6.1	4.0 ✓
+50			10.0	-0.6	✓	49	5.6	4.5 ✓
						+50	5.8	5.3 ✓
TP	8.71	⟨9.54⟩ ✓	8.60	⟨0.83⟩ ✓		49+58.84 = Eq 51 +10.13 old Δ	5.5	4.6 ✓
40			9.4	0.1	✓	check to Topcall 1647-13	3.97	7.01 ✓ 6.98 .03
+50			9.5	0.0	✓			
41			9.8	-0.3	✓			
+50			9.5	0.0	✓			
42			9.3	0.2	✓			
+50			9.1	0.4	✓			
43			9.4	0.1	✓			
+50	End of	Salt Marsh	9.1	0.4	✓			
+65			8.2	1.3	✓			
44			8.3	1.2	✓			
+50			7.7	1.8	✓			
45			7.5	2.0	✓			
TP	7.26	⟨10.08⟩ ✓	6.72	⟨2.87⟩ ✓				

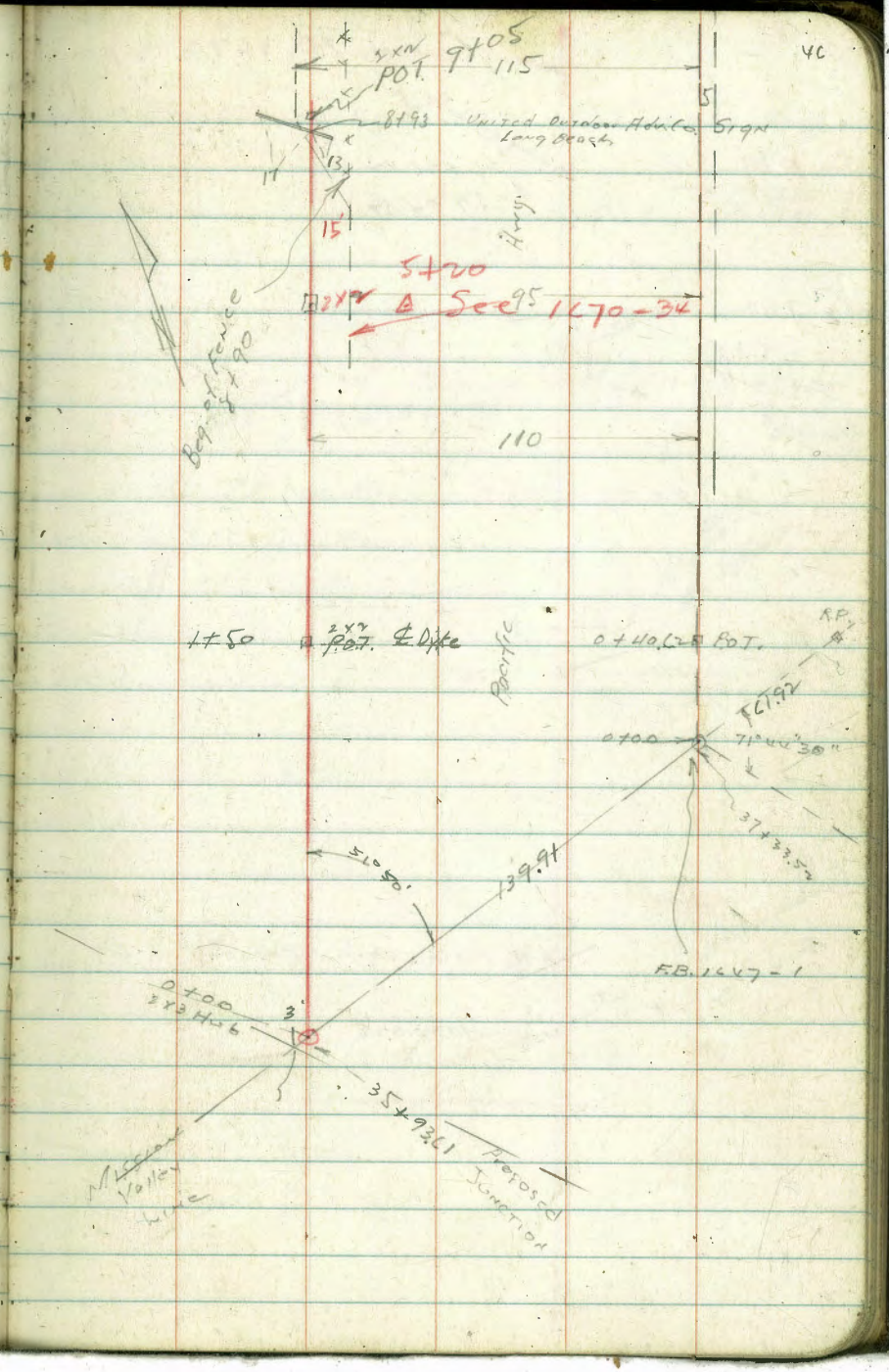
C. Moore
Sometimes Wages
W. Moore
12-28-43.

Old Town to Pacific Beach Trunk Sewer
Via West Side Pacific Hwy





Old Town to Pacific Beach Sewer
Via West Side Pacific Hwy
to Cudahy Bridge, thence to
E side S.Fe R.R. see P. 45



← Contd. FB. 1670-27

See P. 45 →

26+21.42
Δ = 59°04' Rt.

22+20
Foster & Kl. Sign

21+85.73 P.O.T.

115
5

Foster & Kleiser Sign 20' long

17+87

Pebble Lane

Elm St.

14+06 United Outdoor Sign

18

14+00.78

Elev. Top 16" Gas Main at Cudahy Plant

BM. P41

14.69

Cudahy Bridge

29+14.53

P. 45

Location of Power Poles N. of Pac. Highway

See FB. 1670-27.

11+00 23.5 Rt PP

13+25 PP 14' Rt.

14+22 PP 18' Rt.

17+18 PP 18' Rt.

18+67 " " "

19+76 " " "

22+27 " " "

27+15 " 19 "

30+13 " " "

P. 78 THIS BK.

for R.O.W. Ties

12-43

12/44 Kuhn & Ch. nv.

Sewer Levels Sketch p. 46

ENGR	80C	(20.76) ✓	12.70	Sm. Con. RR. Abut.	
0+00 = 35+93.61	Mission Valley Line		8.9	11.9	✓
+30			12.1	8.7	✓
+50			13.4	7.4	✓
1			14.0	6.8	✓
+10			13.0	7.8	✓
+36			6.7	14.1	✓
+50	P.O.T. on 46		6.1x	14.6x	✓
+57			6.x	14.6	✓
+60			9.1	11.7	✓
+70			10.7	10.1	✓
T.P.	0.09	(80x) ✓	12.81	(795) ✓	
+77			2.x	5.6	✓
+9x			5.6	x.4	✓
x			6.1	1.9	✓
+25			5.x	x.8	✓
+40			5.x	x.8	✓
+45			6.5	1.6	✓
+65			6.x	1.6	✓
+88			8.6	- 0.4	✓
3			9.0	- 1.0	✓

(8.04) ✓

v8

3+15			9.x	-1.x	✓
+30			9.8	-1.8	✓
+40			9.7	-1.7	✓
+41			10.8	-2.8	✓
+50	S.O. Struct.		12.8	-4.8	✓
+65	" "		12.7	-4.7	✓
+7x			10.8	-2.8	✓
+75			10.0	-2.0	✓
4			9.8	-1.8	✓
+08			8.0	-1.0	✓
+35			9.x	-1.x	✓
+47			8.5	-0.5	✓
+68			9.4	-1.4	✓
+75			6.4	1.6	✓
+95			6.8	1.x	✓
5+03			4.9	3.1	✓
+50			3.7	4.3	✓
6			4.x	3.8	✓
+30			4.0	4.0	✓
T.P.	8.xx	(13.16) ✓	3.10	4.9x	✓
+55			11.3	1.9	✓
+75			12.1	1.1	✓
+8x			11.1	2.1	✓
7			11.4	1.8	✓

7 + 11		(13.16)	11.C	1.6	✓
+ 20			10.C	2.6	✓
+ 45			11.0	2.2	✓
+ 70			8.8	4.4	✓
8			8.3	4.9	✓
+ 50			7.8	5.4	✓
+ 76			7.4	5.8	✓
+ 84			6.4	6.8	✓
+ 94	Alma Ramp		1.5	11.7	✓
9 + 08			0.9	12.3	✓
+ 20			7.4	5.8	✓
+ 50			7.4	5.8	✓
10			7.C	5.6	✓
+ 50			7.7	5.5	✓
11			7.C	5.6	✓
+ 25			7.8	5.4	✓
+ 43			7.3	5.9	✓
+ 55			5.9	7.3	✓
+ 90			5.1	8.1	✓
12			5.C	7.6	✓
T.P.	4.9 +	(11.37)	6.7C	(6.40)	✓
+ 15			5.4	5.9	✓
+ 50			5.6	5.7	✓
13			6.4	4.9	✓

13 + 21		(11.37)	5.6	5.7	✓
+ 47			7.2	9.1	✓
+ 50			0.7	10.6	✓
+ 58			1.8	9.5	✓
+ 70	Alma St. Ramp		0.8	10.5	✓
14	"	"	2.5	8.8	✓
+ 15	"	"	2.6	8.7	✓
+ 20			5.5	5.8	✓
+ 27	(P.P. 8' RT. = 18 on Range A9)				?
+ 25			6.0	5.3	✓
+ 50			6.2	5.1	✓
15			6.7	4.6	✓
T.P.	6.88	(11.57)	6.63	(4.69)	✓
+ 50			6.7	4.9	✓
16			7.0	4.6	✓
+ 50			7.2	4.4	✓
+ 95			7.1	4.5	✓
17			6.4	5.2	✓
+ 05	Ramp		4.5	7.1	✓
+ 28	"		2.7	8.9	✓
+ 38			6.3	5.3	✓
+ 50			7.2	4.4	✓
18			7.2	4.4	✓
+ 50			7.3	4.3	✓

		(11.57)				
19			8.0	3.6		
+50			7.9	3.7		
20			8.2	3.4		
T.P.	6.07	(9.85)	7.79	(3.78)		
+50			5.6	4.2		
21			5.5	4.3		
+50			6.3	3.5		
22			7.3	2.5		
+15			7.0	2.8		
+25			5.6	4.2		
+50			4.8	5.0		
+75			5.2	4.6		
+90			7.1	2.7		
23			7.8	2.0		
+15			7.1	2.7		
+25			6.5	3.3		
+50			6.5	3.3		
+56			6.6	3.2		
+65			9.8	0.0		
+72			9.3	0.5		
+80			7.6	2.2		
24			7.6	2.2		
+20			8.6	1.2		
+44			9.0	0.8		

		(9.85)				
24 +50			9.9	0.0		
+93			9.8	0.0		
25 +03			9.4	0.4		
+27			9.2	0.6		
+32			9.6	0.2		
+50			10.0	−0.2		
26			9.7	0.1		
26 +21.4	∠ 59°04'R		9.5	0.3		
+50			9.8	0.0		
27			10.0	−0.2		
27 +13.6	∠ 30°56'R		7.3	2.5		Under Cudahy Bridge
T.P.	5.02	(6.94)	8.33	(1.52)		
+30			0.7	6.2		
+40			1.0	5.9		
+45			3.2	3.7		
+55			5.2	1.7		
+72			5.4	1.5		
+79			2.6	4.3		
+95			1.8	5.1		
T.P.	7.04	(1.29)	1.69	(5.25)		
28 +03			10.2	0.1		
+25			10.8	1.5		

12-29

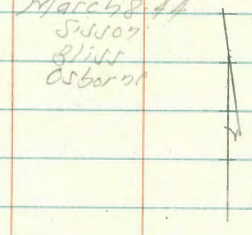
28 + 32.6	ground	11.5	0.8	✓
"	Top 10" CI. Sewer Pipe	7.56	4.73	✓
+47		13.0	- 0.7	✓
+50		14.7	- 2.4	✓
+60		14.6	- 2.3	✓
+66		9.7	2.6	✓
+82		8.7	3.6	✓
+90		5.5	6.8	✓
29		4.0	8.3	✓
+08		5.0	7.3	✓
+17		10.4	2.2	✓
+25		9.6	2.7	✓
+50		9.1	3.2	✓
+61.53	ground	8.5	3.8	✓ 7.43 3.05
"	Top 16" Gas Line	10.48	1.81	✓
+78		6.6	5.7	✓
+85		4.4	7.9	✓
+92		3.8	8.5	✓
+95		3.0	9.3	✓
29 + 99.53	Top rail	2.38	9.91	✓ Main Line
"	on Tie	2.95	9.34	✓
30 + 15.10	Top rail	2.44	9.85	✓ Spur
"	on Tie	2.93	9.36	✓
30 + 34.76	Top rail	2.79	9.50	✓ Spur
"	on Tie	3.30	8.99	✓
+24		2.4	9.9	✓

12-29

30 + 59.53	∠ 90° Lt.	+ 2.8	15.1	✓
31 + 26		1.4	10.9	✓
+31		3.0	9.3	✓
+71.85	Top rail	2.37	8.9 2	✓ Spur
"	ground	3.5	8.8	✓
32		3.6	8.7	✓
+50		3.8	8.5	✓
33		5.2	7.1	✓
+51.9 - 30 + 37.73		9.0	3.3	✓
check to BM. Cudahy Bridge		o.k.	11.17 ✓	16.47 / 4.9 = 11.59 o.k.

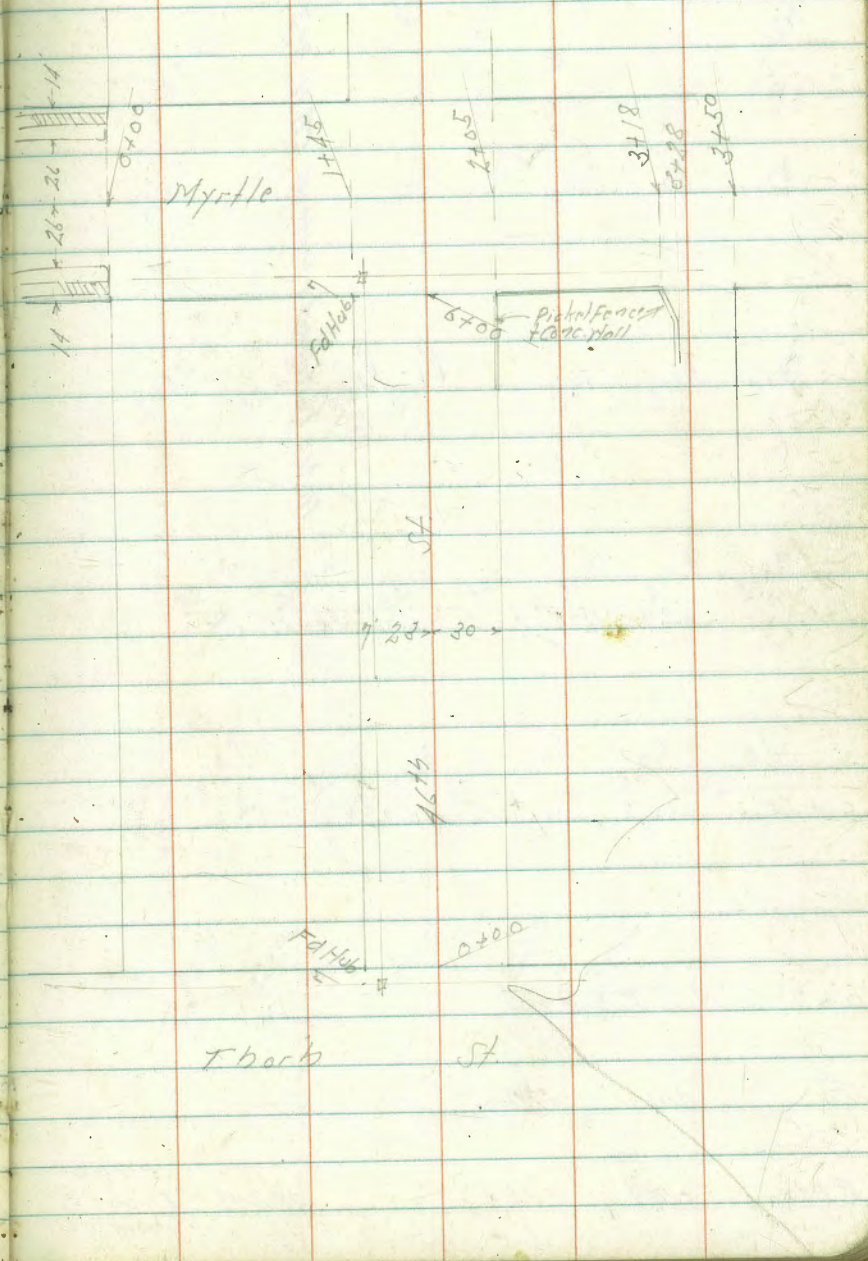
Cross Section 46th St. Thorn to Myrtle
Myrtle From Alley West of 46th St
to Alley East of 46th St.

March 8 44
Sisson
Bliss
Osborn



Indexed
C.S.K.

5



Cross Section 46th St.
Thorn to Myrtle

Notes Reduced & Plotted CBK 3-8-1944

2+50					
2+0					
1+50					
1+0	29.5 Lt o/℄ = N.L. Lath Fence ✓				
0+50	30.5 Lt o/℄ = S.L. Lath Fence ✓				
0+0 = N.L. Thorn St					
TP	4.01	327.06	11.42	323.05	
BM	.49	334.47		332.98	NWBP Thorn & Chamount

Lt=W ℄ Rt=E

320.8	320.2	318.9	317.9	317.1	316.7	315.4
6.4	6.9	8.2	9.3	10.0	10.4	11.7
30	20		5	20	30	45
322.8	321.8	320.2	320.6	318.1	317.1	315.8
4.3	5.3	6.9	6.5	9.0	10.0	11.3
30	20		5	20	30	45
323.2	322.3	321.4	321.9	319.1	318.9	316.5
3.9	4.8	5.7	5.2	8.0	8.2	10.5
30	20		1	20	30	45
323.6	322.4	321.4	321.7	320.1	319.1	316.0
3.5	4.7	5.7	5.4	7.0	8.0	11.1
30	20		3	20	30	45
323.7	322.7	321.8	321.9	320.5	319.7	317.1
3.4	4.4	5.3	5.2	6.6	7.4	10.0
30	20		5	20	30	45
324.1	323.0	321.4		320.0	319.6	
3.0	4.1	5.7		7.1	7.5	
30	20			20	30	

327.06

4+95 — 22.5 Rt of ℄ = 2.24 Palm ✓

4+67

4+61 — 22' Rt of ℄ = 2.30 Palm ✓

4+50

4+0

3+80

3+50

3+0

327.06

Lt ℄ Rt

321.79
5.27
30.5 WIT 8.56 WOTK

320.3 319.5 319.8 320.3 320.6
6.8 7.6 7.3 6.8 6.5
30 20 20 30

319.7 319.1 318.7 318.3 318.1
7.4 8.0 8.4 8.8 9.0
30 20 30 30

321.6 319.7 318.9 318.8 318.2 317.2 318.7 318.9
5.5 7.1 8.2 8.4 8.9 9.9 9.4 8.2
35 30 20 20 30 45 87.5

321.7 319.6 319.0 318.2 316.4 315.1 310.5 305.5
5.4 7.5 8.1 8.9 10.7 13.0 16.6 20.6
35 30 20 20 30 40 50

321.7 319.5 319.3 318.4 315.8 315.3 310.1 305.1
5.4 7.3 7.8 8.7 11.3 11.8 17.0 22.0
35 30 30 20 30 45 55

327.06

5+50					
5+48					
5+38	23' Rt of ℄ = 2 24" Palm				✓
5+32					
5+24	23' Rt of ℄ = 2 24" Palm				✓
5+13					
5+06					
5+0					
TP	849	831.09	4.46	822.60	
		827.06			

Lt ℄ Rt

324.3 324.2 324.7 325.2 325.52 324.9

6.8 6.9 6.1 5.9 5.57 6.1

30 20 20 29.6 = 24 Pocket Face

Conc Wall

32493

6.76

29.5 = W 1.5

Conc Walk

32413

6.95

33 = E 4 3 Conc Walk

32439

6.70

34 = W 1.25

Conc Walk

32.88

8.41

34 = E 4 3 Conc Walk

32436

6.73

28.8 = E 4 W 1.5

Conc Ck 29.6

32189 32212 32218 32222 32236 3241

9.20 9.9 9.2 8.9 9.5 9.5

30 20 20 10 10 30

33.09

BM			0.55	335.83	MAG SP Nail Chiseled mound 335.89
TP	6.72	336.38	1.43	329.66	
6+0 = SL Myrtle					
54.85					

331.09

Lt. | ℄ | Rt.

332.38

326.8	326.4	326.3	326.3	325.0	328.4	323.56
4.3 / 30	4.7 / 20	4.8	4.8 / 5	6.1 / 20	7.7 / 30	7.53 / 80 = Top of Wall

326.77	326.1	325.9	326.1	326.2	325.6	324.9	325.2
4.27 / 34 = Top of Concrete	5.0 / 30	5.7 / 20	5.0	4.9 / 10	5.5 / 20	6.2 / 30	5.9 / 36 = Top of Wall at ℄

331.09

Cross Section Myrtle From Alley West of 46th St to Alley East of 46th St.

Reduced & plotted Profile 9-8-44 CBH

Lt: N

Indexed E.J.K.

Rt: S

5C

0+87

0+64

0+51.7 — 39.2 Rt of Σ - Elv Picket Fence ✓

0+50

0+41

0+30 — 39.1 Rt of Σ = Elv Picket Fence ✓ (0+21.7 For Fence)

0+0 = W/ Alley

336.88 Ft. Fore

336.38

329.15
7.93
38 = 4 Cars Walk

328.53 328.58
7.85 7.80
42.9 Rt. 46.1 Rt
Corner Porch Corner Floor

329.9 329.2 328.9 328.7 328.5 328.1 328.6 328.5
6.5 7.5 7.5 7.7 7.9 8.3 7.8 7.9
40 26 13 13 21 26 40

330.73
6.66
39.5 Lt of Cen. Walk

330.8 330.3 329.6 330.0 329.8 329.5 329.0 329.6 329.5
5.6 6.1 6.8 6.4 6.6 6.9 7.4 6.8 6.9
40 27 24 13 13 23 26 40

330.94 330.63 330.2 330.2 330.3 329.8 329.4 329.67 329.99
5.44 5.25 6.2 6.2 6.1 6.6 7.0 6.71 6.39
40 = W/ Alley 46.26 46 13 13 46 26 To Pole 40 = Elev. Alley

TP	0.90	318.79	11.82	317.89
2+50				
2+07	29' Rt of ℄ - Sly Anchor Pole ✓			
2+05 = EL Myrtle				
1+75 = ℄ Myrtle				
TP	2.84	329.71	9.51	326.87
1+45 = W. Arthur	28' Rt of ℄ - Sly Power Pole ✓			
1+27				
1+00				

386.38

Lt ℄ Rt

311.7	312.0	313.3	315.8	316.7	318.6	318.7	318.0	319.1
18.0	17.7	16.4	13.9	13.0	11.1	11.0	11.9	10.6
50	40	25	13		4	13	25	40

318.7	318.6	319.0	320.2	320.6	322.5	323.6	323.2
11.0	11.1	10.7	9.5	9.1	7.2	7.1	6.5
50	40	25	13		13	25	40

322.7	327.8	323.7	324.9	326.2	325.9	326.3
7.0	6.7	6.0	4.8	2.5	3.8	3.4
40	25	13		13	25	40

329.71

326.3	326.0	326.8	327.1	327.1	326.7	327.4	327.2
11.1	10.4	9.6	9.3	9.3	9.7	9.8	9.3
40	25	13		13	22	25	40

327.20
9.18
38.5 - 24" Conc
Mon. ℄

328.7	328.5	328.2	327.8	327.4	327.7	327.4
7.7	7.9	8.4	8.6	9.0	8.7	9.0
40	25	13		13	25	40

336.38

3+50 = ℄ Line of Alley 23 Rt of ℄ - Sly Tel Pole

3+30 29.5 Rt of ℄ - Sly Power Pole ✓

3+28

3+18 = Δ Conc Wall on Rt ✓

2+0

1+86

818.79

Lt ℄ Rt

2908 2953 3022 3082 3107
2.80 2.35 1.66 1.06 .81
13 26 40 50

2973 3072 3135 3134 3137 3155.9
2.15 1.16 .53 .54 .51 3.20
00 13 21 40 54 54: Δ Conc Wall

3158.4
2.95
59.2 Δ Top Conc Wall

3025 3036 3068 3148 3143 3158 3162.6
1.62 1.58 1.20 .40 .45 .36 2.53
13 7 13 26 39 39: Top Conc Wall

3162.3 3167.8
2.56 2.01
35 Δ Conc Wall 39.5 ℄ Conc Wall

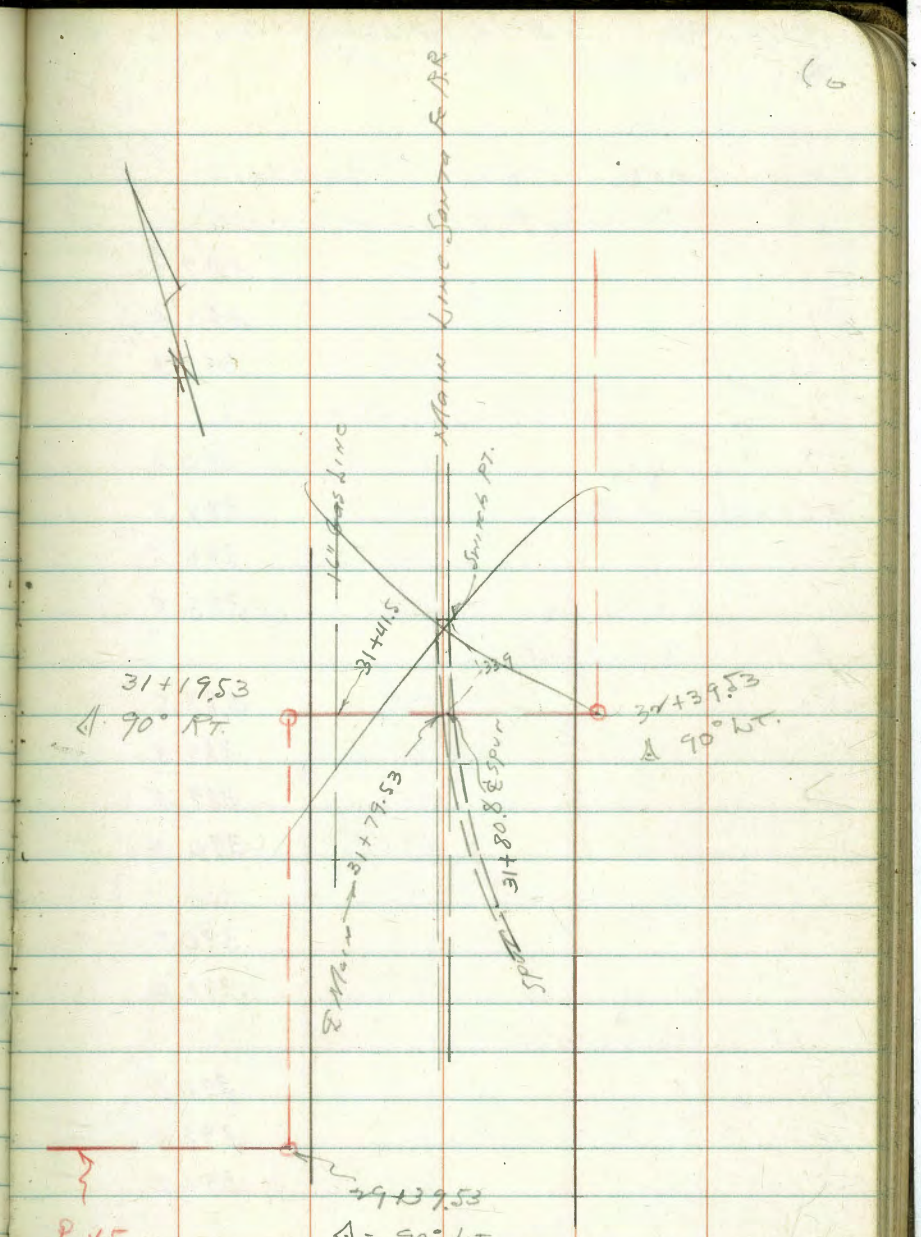
818.79

C5m
3-21-44

Sewer Line Change to avoid R.R. Spurs at Cudahy Plant.

From p. 45

BM ⊡ Bolt	0.7	(12.43)		11.69	Nec. on Cudahy Bridge
29+39.53	Δ = 90° Lt.		9.5	2.9	✓
+50			9.8	2.6	✓
30			10.1	2.3	✓
+50			10.2	2.2	✓
31			10.4	1.8	✓
31+19.53	Δ 90° Rt.		10.8	1.6	✓
+41.5	ground		10.5	1.9	✓
"	Top 12" Gas Line		12.24	-0.21	✓
+50			10.5	1.9	✓
+68			5.9	6.5	✓
+72			4.2	8.2	✓
+79.53	℄ Main Track		4.1	8.3	Top Tie
	Top Rail Main "		3.51	8.92	✓
+80.8	℄ Spur		4.1	8.3	" "
	Top rail on Spur		3.48	8.95	✓
+86			4.4	8.0	✓
+89			5.2	7.2	✓
32+30			5.7	6.7	✓
32+39.53	Δ 90° Lt.		4.0	8.4	✓



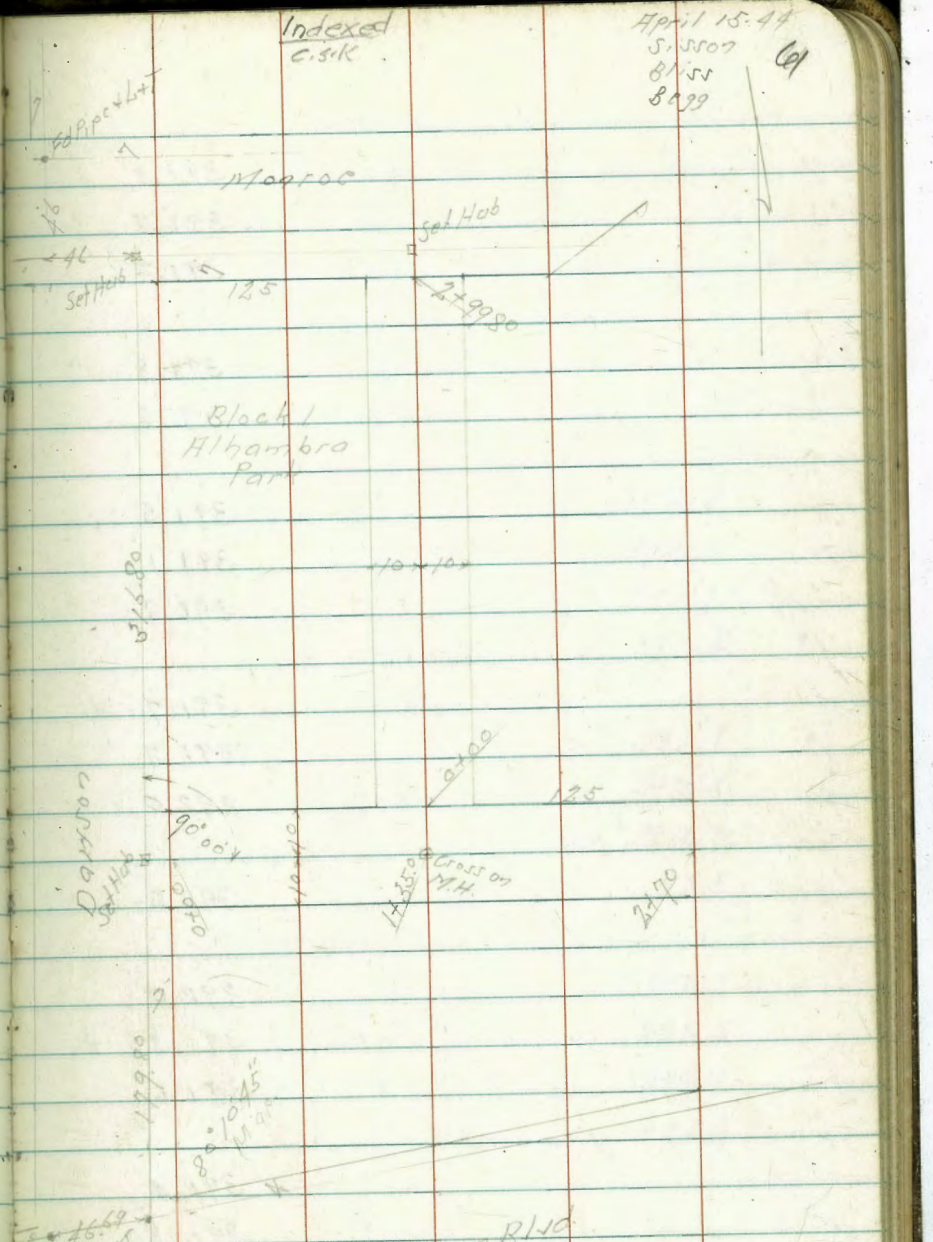
Cross Section Alleys Block 1 Alhambra Park
East & West Alley

B.M.	308	396.96		393.88	S.W. BP El Cajon Blvd.
		0-12 = EC & Line Dawson			
N			95	387.5	
℄			96	387.4	
S			97	387.3	
		0+10 = EL Dawson			
S			68	390.2	
+26 = Wh Wire Fence			77	389.3	
℄			85	388.5	
N			90	388.0	
		0+15			
N			83	388.8	
℄			77	389.3	
+8			75	389.5	
S			66	390.4	
		0+50			
-15			63	390.7	
S			60	391.0	
+16		= Wire Fence			
℄			65	390.5	
N			66	390.4	
+15			68	390.2	
		0+75			
-15			65	390.5	
N			62	390.8	

Indexed
C.S.K.

April 15.44
S. 1550?
81 55
8499

69



396.96

℄	5.9	391.1
S	5.3	391.7
+15	5.8	391.2
1+00		
-15	5.4	391.8
S	5.4	391.8
+ 4.0 = Wire Fence		
℄	5.5	3915
N	5.9	391.1
+15	6.1	390.9
1+25 = ℄ N & S Alley		
N	5.3	391.7
℄	5.3	391.7
S	5.0	3920
+0.3 = Wire Fence		
+15	4.5	3925
1+35 = ℄ N & S Alley		
S	5.0	3920
℄ on Man Hole Rim	5.08	391.88
N	5.1	391.6
1+45 = ℄ N & S Alley		
N	5.6	391.4
℄	5.2	391.8
S	5.1	391.9
+0.8 = Wire Fence		
+15	4.1	392.6

396.96

1+47

N - 0.6 = S.W. Cor. Bldg

1+65

N - 0.7 = S.E. Cor. Bldg

1+67

S - 0.7 = N.W. Cor. S Bldgs Auto Court

1+75

S	4.8	392.2
℄	5.0	392.0
N	5.3	391.7
+15	5.5	391.5
2+0		
-15	5.3	391.7
N	4.9	3921
℄	4.7	392.3
S	4.5	392.5
2+35		
S	4.3	392.7
℄	4.5	392.5
N	4.7	392.3
+15	4.9	3921

2+68

S - 0.9 = N.E. Cor. S Bldgs ✓

		396.96			
	2+70				
-15			4.7	392.3	
N			4.5	392.5	
℄			4.4	392.6	
S			4.3	392.7	

North & South Alley

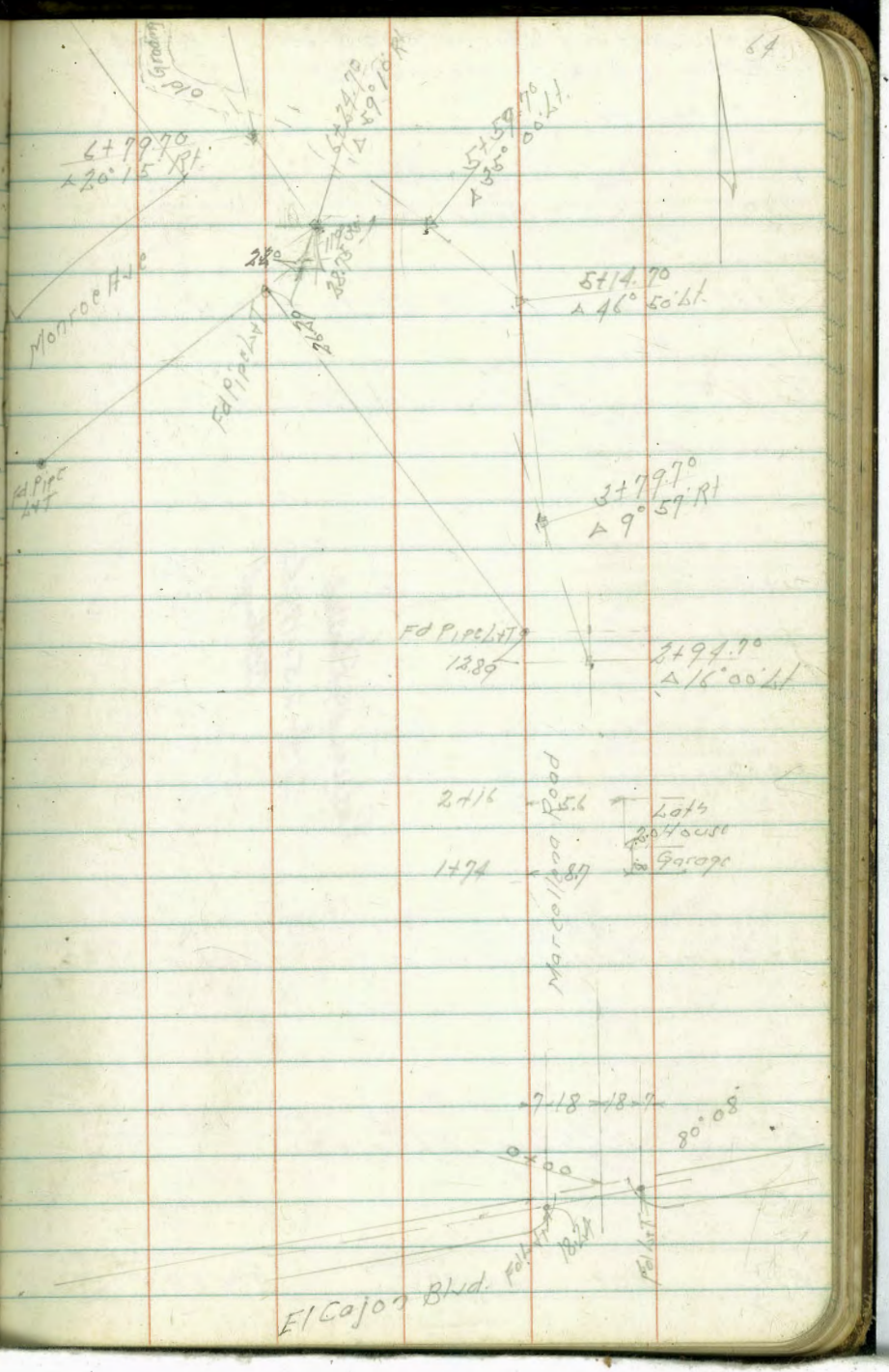
63

396.96

6+40 = N.L. E & W Alley

E			5.6	391.4	✓
℄			5.4	391.6	
W			5.4	391.6	
	6+45				
W			6.3	390.7	
℄			6.1	390.9	
E			6.2	390.8	
	6+50				
-15			6.3	390.7	
E			6.6	390.4	
℄			6.4	390.6	
W			6.8	390.2	
+1.1 = S'ly Fence ✓					
+15			6.9	390.1	
	1+00				
-0.8 = Fence ✓					
-0.3 = W'ly Power Pole ✓					
W			7.0	390.0	
℄			6.8	390.2	
E			7.0	390.0	
+15			6.8	390.2	
	1+50				
-15			6.8	390.7	
E			6.9	390.1	

	396.96	
Z	67	390.3
W	72	389.8
+0.4 = Fence		
+1.5	75	389.5
Z+0		
-1.5	91	389.9
W = Fence	67	390.3
+0.9 = W/L Power Pole		
Z	65	390.5
E	65	390.5
+1.5	62	390.8
Z+50		
-1.5	58	391.2
E	61	390.9
Z	61	390.9
W = Fence	63	390.7
Z+90		
W+0.7 = W/L Anchor Pole		
Z+99.80 = ℄		
W = Fence	59	391.1
Z	55	391.5
E	55	391.5
BM	55.0	391.46



Cross Section Marcellena Road
El Cajon Blvd to Monroe Ave.

Indexed
c. S.R.

Sketch Page 64

1+0				
0+81	23' Rt of ℄ - ℄ 36" Palm			✓
0+65	= ℄ Dbl Ribbon Conc Drive on Rt.			
0+50				
0+10				
0+0	24' Rt of ℄ = Rt ℄ Bridge = N.L. El Cajon = Taken on Line of El Cajon			
0-10	= NCb Line El Cajon			
BM	6.09	39997	39988	

Relieved of Station
4-25-1944
C.E. Kemp

Sta	℄	Rt = E
394.8	395.1	395.5
5.3	4.9	4.5
25	15	
394.7	395.0	395.6
5.2	5.0	4.4
25	15	
395.0	395.5	395.4
5.0	4.5	4.6
25	15	
395.2	395.09	394.13
4.8	4.68	5.34
25	15.4 = Gutter	15.4 = Gutter
395.29	394.42	394.67
4.68	5.35	5.30
23.6 = Gutter	23.6 = Gutter	15

Sta	℄	Rt = E
395.7	395.6	
4.3	4.4	
15	25	
395.9.0	396.26	✓
4.09	3.71	
25 = N.L. 2nd Ave. Dr.	15 = Curb	
395.8	396.1	
4.5	3.9	
15	25	
395.6	395.4	
4.4	4.6	
15	25	
395.05	394.78	395.40
4.92	5.19	4.59
	15.5 = Gutter	15.5 = Curb
394.80	394.90	394.91
5.17	5.09	5.08
	15	29.3 = Gutter

Sta	℄	Rt = E
395.54		
4.6		
25.4		
395.50		
4.47		
27.3 = Curb		

39997

April 19, 44
Sisson
Bliss
Osborn

65

3+50

2+94.7° Δ 16°00'Lt Taken on Spike

TP 2.54 396.88 5.63 394.34

2+50

2+24 14.5 Rt of Σ = Σ 24" Tree

2+0

1+74

1+50

1+38 20 Rt of Σ = Σ 8" Locust Tree
24 Lt of Σ = NE ½ of Hedge
399.97

Lt		Σ		Rt	
393.5	392.6	391.2	389.3	386.9	384.1
5.4 / 25	4.3 / 15	5.7	7.6 / 15	10.0 / 25	12.8 / 35
395.1	394.2	393.0	388.9	385.7	381.6
1.8 / 25	2.7 / 15	3.9	8.0 / 15	11.2 / 25.2	15.3 / 35
		396.88			
394.8	395.0	394.4	391.3	388.8	384.8
5.2 / 25	5.0 / 15	5.6	8.7 / 15	11.2 / 25	15.2 / 35
395.5	395.2	395.1	394.9		
4.5 / 25	4.8 / 15	4.9	5.1 / 8.5	W½ South House	
			395.0		
			5.0 / 8.7	S½ Garage Dr. Floor	
395.7	395.3	395.3	395.2	394.9	
4.3 / 25	4.7 / 15	4.7	4.8 / 15	5.1 / 25	
		399.97			

Marcellena Road

5+59.70	Δ 35°00' Lt	Take on Spk		
5+14.70	Δ 11°50' Lt	Take on Spk		
TP	7.19	391.39	12.68	384.20
5+0				
4+50				
4+0				
3+79.70	Δ 9°57'Rt	Take on Spk		

396.88

67

Lt.		Rt	
386.9	385.3	383.2	381.2	378.6	374.2
4.5	6.1	8.2	10.2	12.8	17.2
25	15		15	25	15
386.4	384.5	383.2	381.5	380.0	376.1
5.0	5.9	8.22	9.9	11.4	15.3
27.2	15	07 5+06	15	27.2	15
		391.39			
386.6	385.2	384.0	382.0	380.4	375.0
14.3	11.7	12.0	14.0	16.5	21.9
25	15		15	25	15
388.9	387.6	385.7	384.1	378.0	373.6
8.0	9.3	11.2	12.8	18.9	23.3
25	15		15	25	20
			383.0 / 25		
391.4	390.3	388.5	387.1	381.0	376.5
5.5	4.6	8.4	9.8	15.9	20.4
25	15		15	20	10
392.6	391.5	389.8	388.6	385.5	382.3
4.3	5.4	7.09	8.3	11.4	14.6
25.1	15	07 5+06	15	25.1	15

396.88

BM			4.39	391.44	Pipe L47 5' Left of SL Monrd p 64
TP	6.81	395.83	1.87	389.52	
7+25					
7+00					
6+79.70	Δ 20°15' Rt	Take on spl t			
6+50					
6+21.70	Δ 59°10' Rt	Take on spl t			
6+00					

69/139

Lt		Δ		Rt		68
372.6	370.1	369.8	369.4	369.8	369.4	369.6
18.8	21.3	21.6	22.0	21.6	22.0	21.8
40	25	15		15	25	40
		Ditch Road				
377.3	377.1	376.8	376.8	376.8	376.4	375.4
14.1	14.3	14.6	14.6	14.6	15.0	16.0
30	25	15		15	25	40
385.9	382.9	382.4	381.0	379.4	378.4	376.7
6.4	8.5	9.0	10.40	12.0	13.0	14.7
60	25.4	15		15	25.4	50
387.8	386.0	385.8	384.7	383.5	382.9	379.9
5.6	5.4	5.6	6.7	7.9	9.0	11.5
57	25	15		15	25	40
390.8	388.6	387.8	386.6	385.0	383.2	381.7
0.6	3.8	3.6	4.8	6.4	8.7	9.7
58	28.8	17		17	28.2	40
	388.4	387.3	385.8	383.6	382.2	380.9
	3.9	4.1	5.6	7.8	9.2	11.5
	25	15		15	25	40

39/139

Marcellena Road

TP	12.04	372.55	5.61	360.51
8+64.70	Δ 32°22'Lt		Taken on spl't	
8+25				
8+0				
TP	7.64	376.12	10.79	368.48
7+79.70	Δ 20°06'Lt		Taken on spl't	
7+50				
TP	0.31	369.27	12.62	368.96
BM	0.59	381.58		380.99

69

Lt				Rt			
368.8	362.2	360.4	357.2	353.8	351.5	343.6	338.6
+2.7	3.9	5.7	8.98	12.3	14.6	22.5	27.5
50 = Elwood Road	20.0	15	Ditch	15	20.0	55	70
370.1	362.7	358.8	356.6	353.1	349.8	346.1	341.6	340.6
+4.0	3.9	7.3	9.5	13.0	17.1	20.1	24.5	25.5
55 = Elwood Road	25	25	15		15	25	45	65
370.1	354.1	355.0	351.3	346.1	346.6	345.8	344.8
+4.0	9.0	11.1	14.8	20.0	19.5	20.2	24.3
55 = Elwood Road	25	15		17	25	50	60
			366.12				
363.3	358.1	353.9	353.3	354.4	355.9	356.3	357.1
6.0	12.2	15.4	16.0	14.9	13.4	13.0	12.2
50	35.4	15	10		20	25.4	50
371.3	367.8	358.9	360.0	362.9	363.9	364.1	364.8
+2.0	1.5	10.4	9.3	6.4	5.4	5.2	4.5
60 = Elwood Road	45	20	15		15	25	45
				369.27			

10+83.70	Δ			Taken 90° off Back Tang
10+44.70	Δ	37°25' Rt		Taken on Spir
10+0				
9+79.7	Δ	14°47' Lt		Taken on Spir
9+50				
TP	6.50	378.25	0.80	377.75
9+25				
9+0				

378.25

372.55

Lt. 2 Rt.

377.6	374.9	371.9	369.4	368.3	360.8	360.8	359.4	358.3
0.7	3.1	6.1	8.8	10.0	17.5	17.5	18.9	21.0
25	13	8		6	20	25	31	50
								04-Field Road
379.0	378.3	376.5	372.9	370.1	368.3	363.6	359.9	358.3
+0.7	0.0	1.8	5.4	7.6	10.0	14.7	18.4	20.0
40	26.4	15	07-Shed	15	26.1	39	45	58
								04-Field Road
378.4	375.9	374.2	371.6	367.9	364.1	359.9	359.9	
0.3	2.4	4.1	6.9	10.4	14.2	18.4	18.4	
36	25	15		15	25	32		13-Field Road
378.3	375.7	373.8	371.4	367.3	363.6	361.7		
0.0	2.6	4.5	6.90	12.0	15.7	16.6		
40	25.6	15	07-Shed	15	22	36		04-Field Road
377.7	376.6	374.5	371.2	368.3	363.8	363.8	364.0	
0.6	1.7	3.8	7.1	10.0	14.5	14.5	14.3	
40	25	15		11	20	25	32	04-Field Road
377.4	374.0	370.9	366.9	366.0	363.2	355.3		
+3.3	+1.4	1.7	5.9	6.6	9.4	17.3		
40	25	10		15	25	50		
			07-Shed	04-Field Road				
368.7	367.6	367.5	365.3	361.0	358.6	357.1		
8.9	9.0	9.1	11.3	15.6	18.0	19.5		
86	50	25		15	25	50		
04-Field Road		13-Field Road						

Sewer line change at
Cable and Voltaire
From Eb. 1634-20

C-10-44
Revised Lee Dwg 1162D

129+42
28°50' Rt.

St.

gas line
Ex Sewer
& alley

125+87.60
+78.
P. Pole
Lt. Edge

135+00.4
Army Ref.

125+66.1 Gas drive In
125+32.4

5' Con. walk

10
3

125+02.5
125+00

Cross gasoline intake lines to STD.

5' Rt. East edge Pole +87.7

124+91.6

+81.4

5.5' Rt. Flood Lite

54
6.5

+66.4

124+40.16
90° Rt.

2 yr. storm
8" drain
Shallow

Garage

Cable St.

AC pav.

117+98.60
90° Lt.

Voltaire

41

19

Levels on Line Change on Voltaire

Cable to Bacon ± Lance

Wly to Alley ± Bear See 163K

SE Top FH	0.10	20.38		20.28	Cable & Voltaire 163K-31.
117 + 88.6	90° Lt. & Voltaire		7.85		
118 + 50			3.63		
+ 9			4.32		
+ 50			4.93		
120			5.65		
+ 50			6.33		
121			6.9K		
+ 50			7.55		
122			8.20		
TP	2.51	1501	7.88	12.50	
+ 50			3.50		
123			4.19		
+ 50			4.85		
124			5.3K		
124 + 40.16	& 90° Rt.		5.49		
+ 50			5.89		
+ 66.4	Gutter		6.27		
"	Top curb		5.52		
125	Con. Sdw.		5.47		

1501

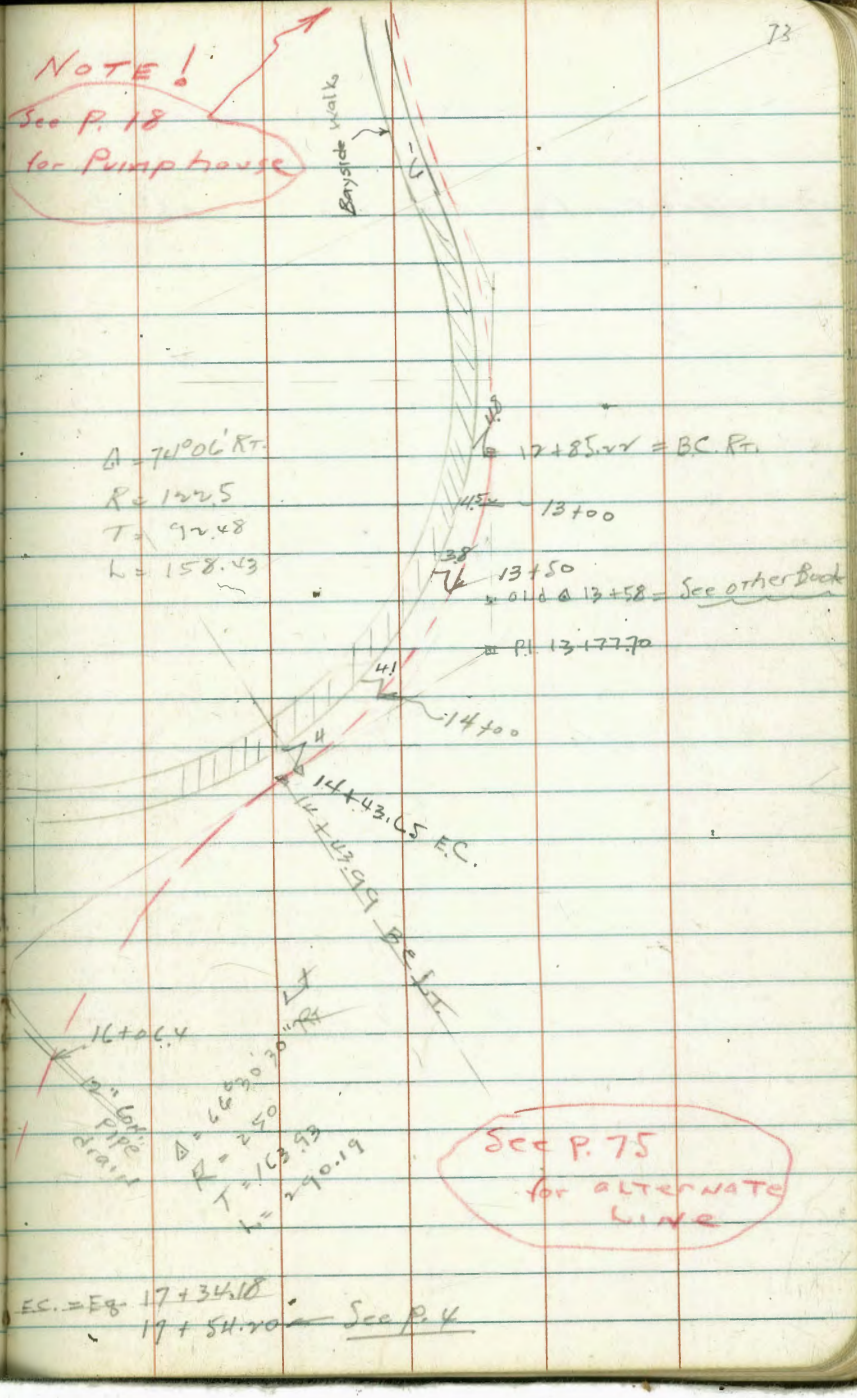
TP	4.75	14.31	5.45	9.56	
125 + 37.4	Con'd. Ive		4.80		
+ 50			5.09		
+ 66.1			4.8C		
+ 80.4			4.92		
"			5.33		
125 + 87.6	& Alley		5.56		Ex. Sewer
check to BM. BP in C.L. NE Bacon & W. Pr. Loma Blvd.			7.82	6.49	6.48 163K-4W

C.S.M.C.

7-17-44, Sewer Change on Bayside Walk

N.E.Pt.	6.1 W	(4.95)		= 1.19	S.O.Pl. Mission Blvd
12 + 85.22 = P.C. Rt.			4.4	0.6	
"	4.8 W = edge Walk		4.02	.93	
13			3.4	1.5	
"	4.5 W	" "	4.01	.94	
+ 50			3.7	1.2	
"	3.8 W	" "	4.00	.95	
13 + 60			sand = 2.5	2.4	
14			4.0	.9	
"	4.1 W	edge walk	4.01	.91	
14 + 43.65 = E.C.			4.0	1.0	
" "	4' W	" "	4.00	.95	
14 + 43.99 = B.C. L.T.			4.0	.9	S.D.P.L.
+ 50			4.1	.8	
15			4.9	.0	
+ 50			6.3	- 1.3	
16			7.3	- 2.3	
+ 06.4	Cross 12" Con Pipe drain		7.4 Sand	- 2.4	
"	Top 12" Pipe		9.26	- 4.31	
+ 20			7.7	- 2.7	
+ 36			4.5	.4	
+ 50			4.0	.9	
17			4.6	.3	

NOTE! See P. 18 for Pumphouse



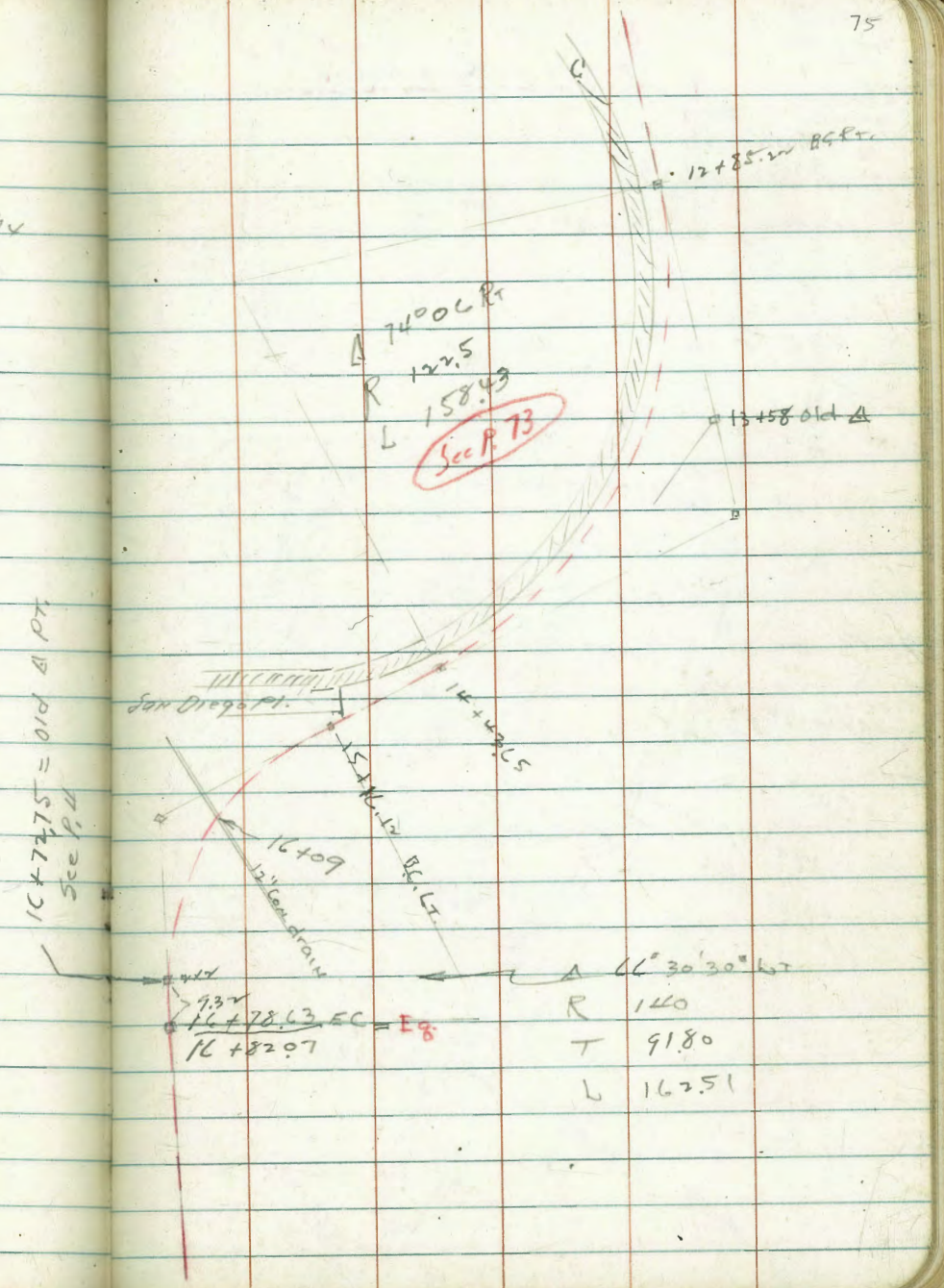
4.95 ✓

17+34.18 = E.C.₁ = Eq 17+54.70 4.3 0.6 ✓

Levels on Aqueduct Line
7-17-44 Pressure Sewer

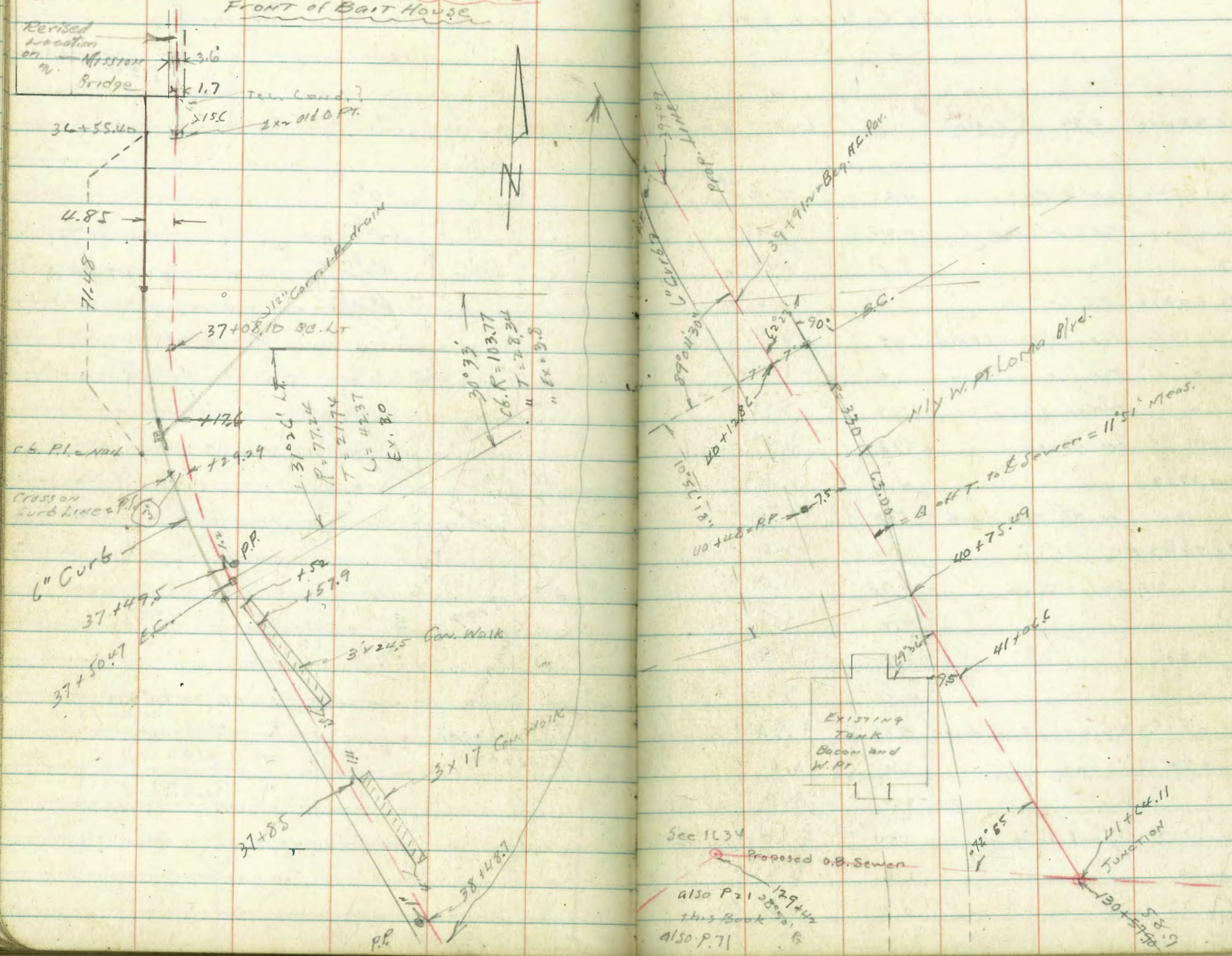
4.95 Ht. Fwd. from P.74

15+16.14 BC Lt.	4.1
+50	5.4
16	6.5
+04	6.4
16+09 12" drain ox	5.4
" Top 12" drain	8.91 Calc.
+15	4.6
+50	4.7
16+78.63 = E.C.	4.9
16+82.07 = Eq.	



CSTM

7-18-40 Sewer Line change from P.S. Front of Bait House



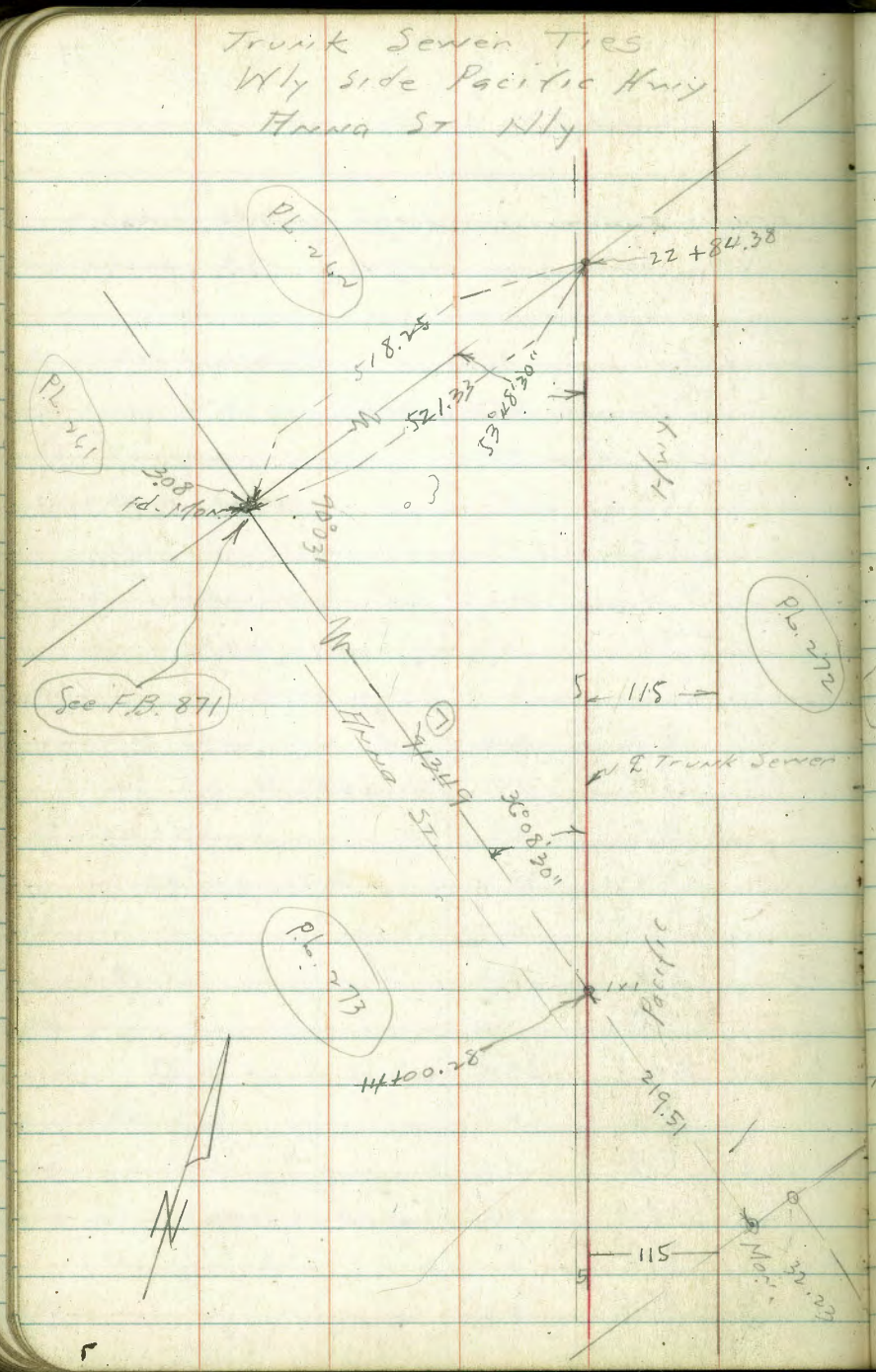
Sewer Levels Sketch p 76

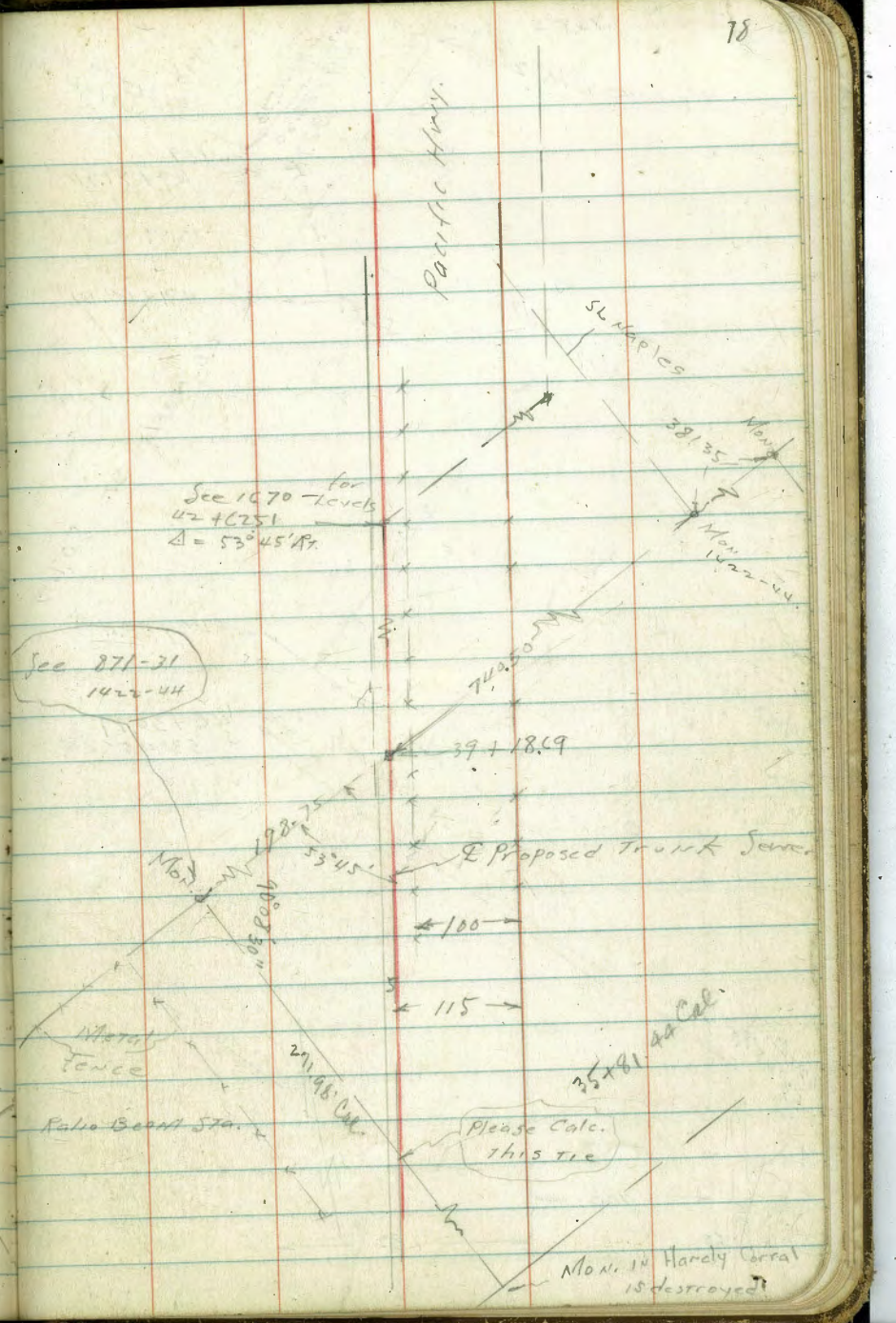
N.E.B.R.W.ch	0.92	(7.40)	6.48	Bacon + K. Pt Loma Blvd
36 + 55.40 = old ⊕ Pt		4.6	7.8	ground
" " 4.85 W Top ch		4.32	3.08	
37		5.4	7.0	
37 + 08.10 P.C. Lt.		5.0	2.4	
+ 17.6 Inv. 12" Conc. I.P. diam		4.9	7.5	ground
" Top " " "		6.2	1.7	
" Top ch		5.19	2.21	
" on grate		6.18	1.77	
+ 29.29		4.8	2.6	
" 3'W P.I. Top Curb		5.08	2.32	
37 + 50.47 E.C.		5.0	2.4	
" 2.9 S.W. ly = Curb		4.98	2.42	
38		4.7	2.7	
+ 50		3.9	3.5	
39		4.1	3.3	
" 5.3 S.ly = curb in drive		3.86	3.54	gutter
+ 50		3.4	4.0	
40		2.4	5.0	on Pav
" 71 S.ly = ch in gutter		2.54	4.86	in drive
+ 50		1.6	5.8	
41		0.8	6.6	

(7.40)

41 + C.L. Junction 1.0 6.40 Pav

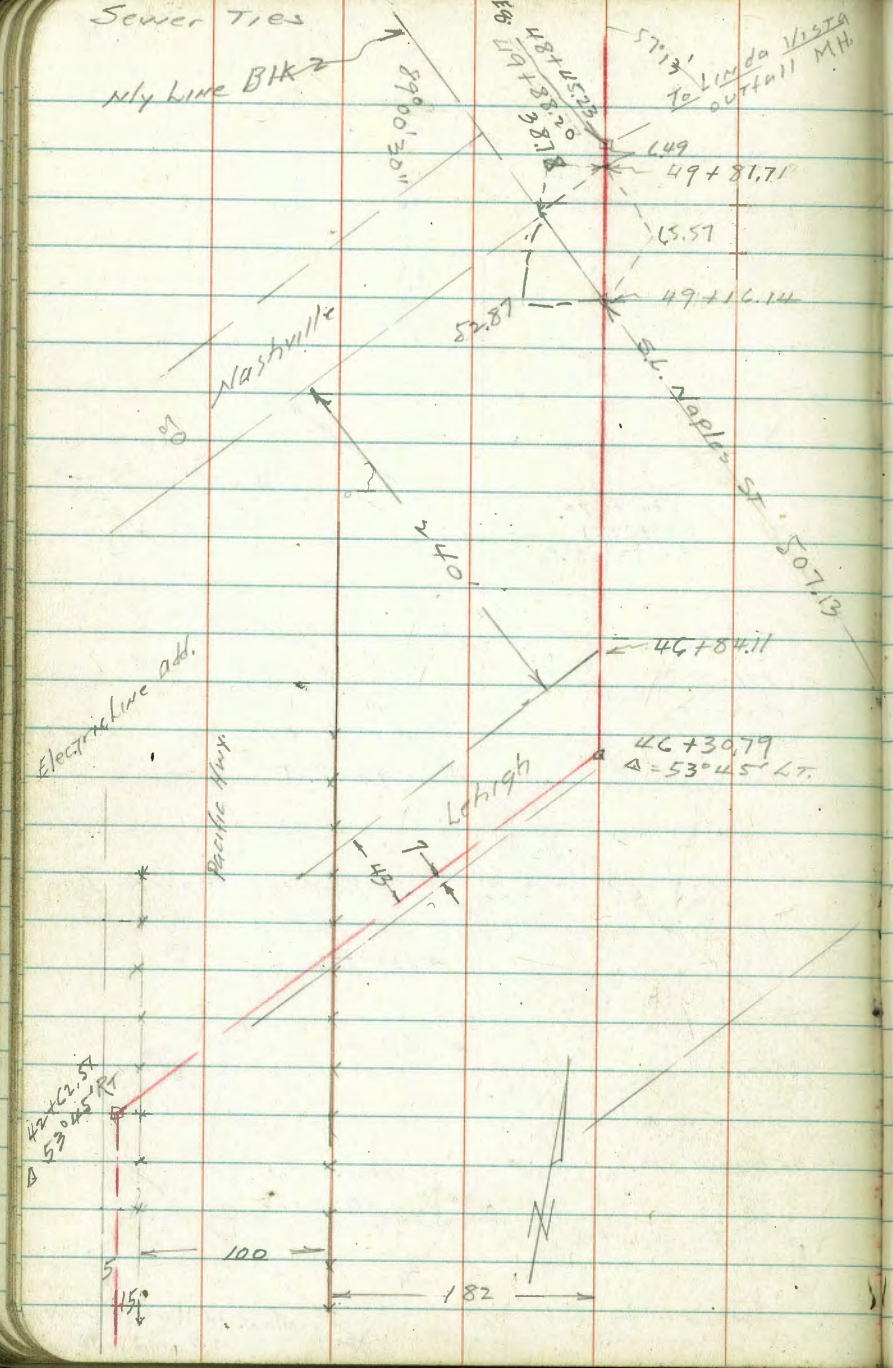
Trunk Sewer Ties
Wly side Pacific Hwy
Hawa St Wly





Sewer Ties

Nly Line Blk 2



Capstan Head

Floor Level to Seat of El on Discharge = 12.0

Disch 2.5' above floor.

Seat of L to 4.6 floor Sel - top 2" limit

1.5/8" on gauge = 100 Sel - W.

Rebuilt M.H.

BM	5.50	11.98	6.48	NE cor BM B P C6 Bacon + W. Pt. Lomo Blvd
Bacon + W. Pt. Lomo Blvd	M.H. Rim	5.75	6.73	
	F.L.	12.00	-0.02 ✓	

IMPROVED TABLES AND INFORMATION

HORIZONTAL STADIA CORRECTIONS

2°—00′	0.1	21°—00′	12.8	33°—00′	29.7
3°—00′	0.3	21°—30′	13.4	33°—15′	30.1
4°—00′	0.5	22°—00′	14.0	33°—30′	30.5
5°—00′	0.8	22°—30′	14.7	33°—45′	30.9
6°—00′	1.1	23°—00′	15.3	34°—00′	31.3
7°—00′	1.5	23°—30′	15.9	34°—15′	31.7
8°—00′	1.9	24°—00′	16.5	34°—30′	32.1
9°—00′	2.5	24°—30′	17.2	34°—45′	32.5
10°—00′	3.0	25°—00′	17.9	35°—00′	32.9
10°—30′	3.3	25°—30′	18.6	35°—15′	33.3
11°—00′	3.6	26°—00′	19.2	35°—30′	33.7
11°—30′	4.0	26°—30′	19.9	35°—45′	34.1
12°—00′	4.3	27°—00′	20.6	36°—00′	34.6
12°—30′	4.7	27°—30′	21.3	36°—15′	35.0
13°—00′	5.1	28°—00′	22.0	36°—30′	35.4
13°—30′	5.5	28°—30′	22.8	36°—45′	35.8
14°—00′	5.9	29°—00′	23.5	37°—00′	36.2
14°—30′	6.3	29°—30′	24.3	37°—15′	36.6
15°—00′	6.7	30°—00′	25.0	37°—30′	37.1
15°—30′	7.2	30°—15′	25.4	37°—45′	37.5
16°—00′	7.6	30°—30′	25.8	38°—00′	37.9
16°—30′	8.1	30°—45′	26.2	38°—15′	38.3
17°—00′	8.5	31°—00′	26.5	38°—30′	38.7
17°—30′	9.0	31°—15′	26.9	38°—45′	39.1
18°—00′	9.5	31°—30′	27.3	39°—00′	39.6
18°—30′	10.1	31°—45′	27.7	39°—15′	40.0
19°—00′	10.6	32°—00′	28.1	39°—30′	40.5
19°—30′	11.2	32°—15′	28.5		
20°—00′	11.7	32°—30′	28.9		
20°—30′	12.3	32°—45′	29.3		

Chains to Feet	
1	66
2	132
3	198
4	264
5	330
6	396
7	462
8	528
9	594
10	660

Feet to Chains	
100	1.515
200	3.030
300	4.545
400	6.060
500	7.575
600	9.090
700	10.606
800	12.121
900	13.636
1,000	15.151

861

6-79

587
+
6-79

Nat. Gas Main 16".

" 1.40 outside

16 13/16 "

120 + 51.8

end Con 120 + 74.7

2.2

84.3
57.7
26.6

121 19.7
78.44
121 58.14 = PC

121 + 19.70 = 38° 5' Lt

66° 58' 5W

127 + 81.88 = N Strad. Nail
Co

127 + 81.28

180 10
91.7

181 + 01.7

178 57.7

310.57
25.77
284.80