1636

LIETZ

FIELD BOOK

No. 60

TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0 44	100.00	0.87	99.99	1.31	89
1	99.98	1 75	99.98	2 18	99 97	2.62	99 95	3.05	88
2	99.94	3.49	99 92	3.93	99 91	4 36	99.88	4.80	87
3	99.86	5.23	99 84	5 67	99 81	6.10	99.79	6.54	86
4	99 76	6.98	99 73	7.41	99.69	7.85	99.66	8.28	85
5	99 62	8.72	99.58	9.15	99 54	9.58	99.50	10 02	84
6	99.45	10.45	99.41	10 89	99.36	11.32	99.31	11.75	83
7	99 25	12.19	99 20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16 50	98 56	16.93	80
10	98 48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98 16	19.08	98 08	19 51	97.99	19 94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21 64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24 62	96.81	25 04	96 70	25.46	75
15	96.59	25 88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27 98	95.88	28 40	95 76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30 07	95.24	30.49	72
18	95.11	30 90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35 43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38 67	67
23	92.05	39.07	91.88	39 47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89 69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87 67	48.10	61
29	87.46	48.48	87.25	48 86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52 99	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60 53	79.34	60.88	79.07	61 22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							
Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees.
	DEGREES.		¾ DEGREE.		½ DEGREE.		¼ DEGREE.		

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MADE IN
U. S. A.

Quality Evidenced Since 1882.

Standard Tripod Connection

LIETZ STANDARD ENGINEERS' TRANSIT

With U Shaped Standards

No. 5E with 6¼" limb. No. 11E with 5" limb.

Furnished with either Internal or External Focusing Telescope.

1636

CITY ENGINEER

TABLE OF STADIA REDUCTIONS

For a Constant of 100.

ROD VERTICAL.

Min.	0° Hor. Dist.	0° Diff. Elev.	1° Hor. Dist.	1° Diff. Elev.	2° Hor. Dist.	2° Diff. Elev.	3° Hor. Dist.	3° Diff. Elev.	4° Hor. Dist.	4° Diff. Elev.	5° Hor. Dist.	5° Diff. Elev.	6° Hor. Dist.	6° Diff. Elev.	7° Hor. Dist.	7° Diff. Elev.
0'	100.00	.00	99.97	1.74	99.88	3.49	99.73	5.23	99.51	6.96	99.24	8.68	98.91	10.40	98.51	12.10
2	100.00	.00	99.97	1.86	99.87	3.50	99.72	5.24	99.51	7.02	99.23	8.74	98.90	10.45	98.50	12.15
4	100.00	.00	99.97	1.86	99.87	3.50	99.72	5.24	99.50	7.07	99.23	8.80	98.88	10.51	98.48	12.21
6	100.00	.12	99.96	1.92	99.87	3.66	99.71	5.49	99.49	7.13	99.21	8.85	98.87	10.57	98.47	12.28
8	100.00	.17	99.96	1.98	99.86	3.72	99.70	5.46	99.48	7.19	99.20	8.91	98.86	10.63	98.46	12.32
10	100.00	.23	99.96	2.01	99.86	3.78	99.69	5.53	99.47	7.25	99.19	8.97	98.85	10.68	98.44	12.35
12	100.00	.33	99.96	2.09	99.85	3.84	99.69	5.57	99.46	7.30	99.18	9.03	98.83	10.74	98.43	12.43
14	100.00	.47	99.95	2.11	99.85	3.90	99.68	5.63	99.46	7.36	99.17	9.08	98.82	10.79	98.41	12.49
16	100.00	.47	99.95	2.11	99.84	3.90	99.68	5.69	99.45	7.43	99.16	9.14	98.81	10.85	98.40	12.55
18	100.00	.52	99.95	2.27	99.84	4.01	99.67	5.75	99.44	7.48	99.15	9.20	98.80	10.91	98.39	12.60
20	100.00	.53	99.95	2.33	99.83	4.07	99.66	5.80	99.43	7.53	99.14	9.25	98.78	10.96	98.37	12.66
22	100.00	.64	99.94	2.38	99.83	4.13	99.66	5.86	99.42	7.59	99.13	9.31	98.77	11.02	98.36	12.72
24	100.00	.70	99.94	2.44	99.82	4.19	99.65	5.92	99.41	7.65	99.11	9.37	98.76	11.08	98.34	12.77
26	99.99	.81	99.93	2.50	99.81	4.30	99.63	6.04	99.40	7.71	99.10	9.43	98.74	11.13	98.33	12.83
28	99.99	.87	99.93	2.62	99.81	4.36	99.63	6.09	99.39	7.76	99.09	9.48	98.73	11.19	98.31	12.88
30	99.99		99.93		99.81		99.63		99.38	7.82	99.08	9.54	98.72	11.25	98.29	12.94
32	99.99	.93	99.93	2.67	99.80	4.42	99.62	6.15	99.36	7.86	99.07	9.60	98.71	11.30	98.28	13.00
34	99.99	.99	99.93	2.73	99.80	4.48	99.62	6.21	99.36	7.94	99.06	9.66	98.69	11.36	98.27	13.06
36	99.99	1.05	99.93	2.79	99.79	4.53	99.61	6.27	99.35	7.99	99.04	9.71	98.68	11.42	98.24	13.11
38	99.99	1.11	99.92	2.85	99.79	4.59	99.60	6.33	99.34	8.05	99.03	9.77	98.67	11.47	98.23	13.17
40	99.99	1.16	99.92	2.91	99.78	4.65	99.59	6.38	99.34	8.11	99.03	9.83	98.65	11.53	98.22	13.22
42	99.99	1.22	99.91	2.97	99.78	4.71	99.59	6.44	99.33	8.17	99.01	9.88	98.64	11.59	98.20	13.28
44	99.98	1.28	99.91	3.02	99.77	4.76	99.58	6.50	99.32	8.23	99.00	9.94	98.63	11.64	98.19	13.33
46	99.98	1.34	99.90	3.08	99.77	4.82	99.57	6.56	99.31	8.34	98.99	10.00	98.61	11.70	98.17	13.45
48	99.98	1.40	99.90	3.14	99.76	4.88	99.56	6.61	99.30	8.34	98.98	10.06	98.60	11.76	98.16	13.45
50	99.98	1.45	99.90	3.20	99.76	4.94	99.56	6.67	99.29	8.40	98.97	10.11	98.58	11.81	98.14	13.50
52	99.98	1.51	99.89	3.26	99.75	4.99	99.55	6.73	99.28	8.45	98.96	10.17	98.57	11.87	98.13	13.56
54	99.98	1.57	99.89	3.31	99.74	5.03	99.54	6.78	99.27	8.51	98.94	10.23	98.56	11.93	98.11	13.61
56	99.97	1.63	99.89	3.37	99.74	5.11	99.53	6.84	99.26	8.57	98.93	10.28	98.54	11.98	98.10	13.67
58	99.97	1.63	99.88	3.43	99.73	5.17	99.52	6.90	99.25	8.63	98.92	10.34	98.53	12.04	98.08	13.73
60	99.97	1.74	99.88	3.49	99.73	5.23	99.51	6.96	99.24	8.68	98.91	10.40	98.51	12.10	98.06	13.79
c= .75	.75	.01	.75	.02	.75	.03	.75	.05	.75	.06	.75	.07	.75	.09	.74	.10
c=1.15	1.15	.01	1.15	.03	1.15	.05	1.15	.07	1.15	.09	1.14	.11	1.14	.13	1.14	.15
c=1.90	1.90	.02	1.90	.05	1.90	.08	1.90	.12	1.89	.15	1.89	.18	1.89	.21	1.88	.25

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Table of Stadia Reductions.—Continued.

Min	8°		9°		10°		11°	
	Hor Dist.	Diff. Elev	Hor Dist	Diff. Elev	Hor Dist.	Diff Elev	Hor Dist	Diff Elev.
0'	98.06	13.78	97.55	15.45	96 98	17.10	96 36	18.73
2	98.05	13.84	97 53	15.51	96.96	17.16	96.34	18 78
4	98.03	13.89	97.52	15.56	96 94	17.21	96 32	18 84
6	98.01	13.95	97.50	15.62	96.92	17 26	96.29	18.89
8	98.00	14.01	97.48	15.67	96 90	17.32	96 27	18.95
10	97.98	14 06	97.46	15.73	96 88	17.37	96.25	19,00
12	97 97	14.12	97.44	15.78	96 86	17.43	96 23	19.05
14	97.95	14.17	97.43	15.84	96 84	17.48	96 21	19 11
16	97.93	14 23	97.41	15.89	96.82	17.54	96.18	19.16
18	97.92	14.28	97.39	15.95	96.80	17 59	96.16	19.21
20	97.90	14.34	97.37	16.00	96 78	17.65	96.14	19.27
22	97 88	14.40	97.35	16 06	96.76	17.70	96.12	19.32
24	97.87	14.45	97.33	16.11	96.74	17.76	96.09	19.38
26	97.85	14.51	97.31	16 17	96.72	17.81	96.07	19.43
28	97.83	14.56	97.29	16.22	96 70	17.86	96.05	19.48
30	97.82	14.62	97.28	16.28	96.68	17.92	96.03	19.54.
32	97.80	14.67	97.26	16 33	96 66	17 97	96.00	19.59
34	97.78	14.73	97 24	16.39	96.64	18 03	95 98	19.64
36	97.76	14.79	97.22	16.44	96 62	18 08	95 96	19 70
38	97.75	14.84	97.20	16.50	96.60	18.14	95.93	19.75
40	97 73	14.90	97.18	16.56	96 57	18 19	95.91	19.80
42	97.71	14.95	97.16	16 61	96.55	18.24	95.89	19 86
44	97.69	15.01	97.14	16 66	96 53	18 30	95 86	19 91
46	97.68	15 06	97.12	16 72	96.51	18 35	95.84	19.96
48	97.66	15.12	97.10	16.77	96 49	18 41	95.82	20 02
50	97.64	15.17	97 08	16.83	96 47	18.46	95.79	20 07
52	97.62	15.23	97.06	16.88	96 45	18.51	95 77	20.12
54	97.61	15 28	97.04	16 94	96 42	18.57	95 75	20.18
56	97 59	15.34	97 02	16 99	96 40	18 62	95.72	20.23
58	97.57	15.40	97.00	17.05	96.38	18 68	95.70	20.28
60	97.55	15.45	96.98	17 10	96.36	18.73	95.68	20.34
c= .75.	74	11	74	12	74	14	.73	15
c=1.15	1.14	.17	1.13	.19	1 13	21	1 13	.23
c=1.90.	1.88	.28	1.87	.31	1 87	35	1 86	.38

Min.	12°		13°		14°		15°	
	Hor. Dist.	Diff Elev	Hor Dist.	Diff. Elev	Hor Dist.	Diff Elev	Hor. Dist.	Diff. Elev.
0'	95.68	20.34	94 94	21.92	94.15	23.47	93.30	25.00
2	95.65	20.39	94.91	21.97	94 12	23.52	93.27	25.05
4	95.63	20.44	94.89	22 02	94.09	23.58	93.24	25.10
6	95.61	20 50	94.86	22.08	94.07	23.63	93.21	25.15.
8	95 58	20.55	94.84	22.13	94.04	23.68	93.18	25 20
10	95.56	20.60	94.81	22.18	94.01	23.73	93.16	25.25
12	95.53	20 66	94 79	22 23	93.98	23.78	93.13	25.30
14	95 51	20 71	94.76	22.28	93.95	23.83	93.10	25.35
16	95.49	20.76	94.73	22.34	93.93	23.88	93 07	25 40
18	95.46	20.81	94.71	22.39	93.90	23.93	93.04	25.45
20	95.44	20.87	94.68	22.44	93.87	23.99	93.01	25.50
22	95 41	20.92	94.66	22.49	93.84	24.04	92.98	25.55
24	95.39	20.97	94.63	22.54	93 81	24.09	92.95	25.60
26	95.36	21.03	94.60	22.60	93.79	24.14	92.92	25.65
28	95.34	21.08	94.58	22.65	93.76	24.19	92.89	25.70
30	95.32	21.13	94.55	22.70	93.73	24.24	92.86	25.75
32	95.29	21.18	94.52	22.75	93.70	24.29	92.83	25.80
34	95.27	21.24	94.50	22.80	93.67	24.34	92.80	25.85
36	95.24	21.29	94.47	22.85	93.65	24.39	92.77	25.90
38	95.22	21.34	94.44	22.91	93.62	24.44	92.74	25.95
40	95.19	21.39	94.42	22 96	93.59	24.49	92.71	26.00
42	95.17	21.45	94 39	23 01	93 56	24.55	92.68	26 05
44	95 14	21.50	94.36	23.06	93.53	24 60	92 65	26 10
46	95 12	21.55	94.34	23 11	93.50	24.65	92.62	26.15
48	95.09	21.60	94.31	23.16	93.47	24.70	92.59	26.20
50	95.07	21.66	94.28	23.22	93.45	24.75	92.56	26 25
52	95.04	21.71	94.26	23.27	93.42	24.80	92.53	26.30
54	95.02	21.76	94 23	23.32	93.39	24.85	92.49	26.35
56	94.99	21.81	94 20	23.37	93.36	24.90	92.46	26 40
58	94.97	21.87	94.17	23.42	93.33	24.95	92.43	26.45
60	94.94	21.92	94 15	23.47	93.30	25.00	92.40	26 50
c= .75..	73	16	.73	17	.73	19	.72	20
c=1.15. .	1.12	.25	1.12	.27	1 11	29	1.11	.31
c1.90	1.85	.41	1.85	44	1.84	48	1.83	.53

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Table of Stadia Reductions.—Continued.

Min	16°		17°		18°		19°	
	Hor. Dist.	Diff Elev	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.
0'	92.40	26 50	91.45	27.96	90.45	29.39	89.40	30.78
2	92.37	26.55	91.42	28.01	90.42	29.44	89.36	30.83
4	92.34	26.59	91.39	28.06	90.38	29.48	89.33	30.87
6	92.31	26.64	91.35	28.10	90.35	29.53	89.29	30 92
8	92.28	26 69	91.32	28.15	90.31	29.58	89.26	30.97
10	92.25	26.74	91 29	28.20	90 28	29.62	89.22	31.01
12	92.22	26.79	91.26	28.25	90.24	29.67	89.18	31.06
14	92.19	26.84	91.22	28.30	90.21	29.72	89.15	31.10
16	92.15	26 89	91.19	28.34	90.18	29.76	89 11	31.15
18	92.12	26.94	91.16	28.39	90.14	29.81	89.08	31.19
20	92.09	26.99	91 12	28.44	90 11	29.86	89.04	31.24
22	92 06	27 04	91.09	28.49	90 07	29.90	89.00	31.28
24	92.03	27 09	91.06	28.54	90 04	29.95	88.96	31.33
26	92.00	27.13	91 02	28 58	90.00	30.00	88.93	31.38
28	91 97	27.18	90.99	28.63	89.97	30 04	88.89	31.42
30	91.93	27 23	90.96	28.68	89.93	30.09	88.86	31.47
32	91.90	27 28	90 92	28.73	89 90	30.14	88 82	31.51
34	91 87	27 33	90 89	28.77	89.86	30.19	88.78	31.56
36	91.84	27.38	90.86	28 82	89 83	30.23	88 75	31.60
38	91.81	27 43	90 82	28.87	89.79	30.28	88.71	31.65
40	91.77	27 48	90.79	28.92	89.76	30.32	88.67	31.69
42	91.74	27.52	90.76	28 96	89.72	30.37	88.64	31.74
44	91 71	27 57	90 72	29 01	89 69	30.41	88.60	31.78
46	91.68	27 62	90 69	29 06	89.65	30.46	88.56	31.83
48	91.65	27.67	90.66	29 11	89.61	30.51	88.53	31.87
50	91.61	27 72	90.62	29 15	89 58	30.55	88.49	31.92
52	91 58	27.77	90.59	29.20	89.54	30.60	88.45	31.96
54	91.55	27.81	90.55	29 25	89.51	30.65	88.41	32 01
56	91 52	27 86	90 52	29.30	89.47	30.69	88.38	32.05
58	91.48	27.91	90.48	29.34	89.44	30 74	88.34	32.09
60	91 45	27.96	90.45	29.39	89.40	30.78	88 30	32.14
c= .75..	.72	.21	72	.23	.71	.24	.71	.25
c=1.15.	1 10	33	1 10	35	1.09	.37	1.08	.38
c=1 90.	1 82	.54	1.81	57	1.80	60	1.79	.63

Min.	20°		21°		22°		23°	
	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dis.	Diff. Elev.	Hor. Dist.	Diff. Elev.
0'	88.30	32.14	87.16	33.46	85.97	34 73	84.73	35.97
2	88.26	32.18	87.12	33.50	85.93	34.77	84.69	36.01
4	88.23	32.23	87.08	33.54	85.89	34.82	84.65	36 05
6	88.19	32.27	87.04	33.59	85.85	34 86	84.61	36 09
8	88.15	32.32	87.00	33.63	85.80	34.90	84 57	36.13
10	88.11	32.36	86.96	33.67	85.76	34.94	84.52	36.17
12	88.08	32.41	86.92	33.72	85.72	34.98	84.48	36.21
14	88 04	32.45	86.88	33.76	85.68	35 02	84.44	36.25
16	88.00	32.49	86.84	33.80	85.64	35.07	84.40	36.29
18	87.96	32.54	86.80	33.84	85.60	35.11	84.35	36.33
20	87.93	32.58	86.77	33.89	85.56	35.15	84.31	36 37
22	87.89	32.63	86.73	33.93	85.52	35.19	84.27	36.41
24	87.85	32.67	86.69	33.97	85.48	35.23	84.23	36.45
26	87.81	32.72	86.65	34.01	85.44	35.27	84.18	36.49
28	87.77	32.76	86.61	34.06	85.40	35 31	84.14	36.53
30	87.74	32.80	86.57	34.10	85.36	35.36	84.10	36.57
32	87.70	32.85	86.53	34.14	85.31	35.40	84.06	36 61
34	87.66	32.89	86.49	34.18	85.27	35.44	84.01	36.65
36	87.62	32.93	86 45	34 23	85.23	35.48	83 97	36.69
38	87.58	32 98	86.41	34.27	85.19	35.52	83.93	36.73
40	87.54	33.02	86.37	34.31	85.15	35.56	83.89	36.77
42	87.51	33.07	86.33	34.35	85.11	35.60	83.84	36 80
44	87.47	33.11	86.29	34.40	85 07	35 64	83.80	36.84
46	87.43	33.15	86.25	34.44	85.02	35.68	83.76	36.88
48	87.39	33.20	86.21	34.48	84.98	35.72	83 72	36.92
50	87.35	33.24	86.17	34.52	84.94	35.76	83 67	36.96
52	87.31	33.28	86.13	34.57	84.90	35.80	83.63	37.00
54	87 27	33.33	86.09	34.61	84.86	35.85	83.59	37.04
56	87 24	33.37	86.05	34.65	84.82	35 89	83.54	37 08
58	87 20	33.41	86.01	34.69	84.77	35.93	83.50	37.12
60	87.16	33.46	85.97	34.73	84.73	35.97	83.46	37.16
c= .75..	.70	.26	.70	.27	.69	.29	.69	.30
c=1.15.	1.08	.40	1.07	.42	1.06	.44	1.05	.46
c=1.90.	1.78	.66	1.77	70	1.76	.73	1.74	.76

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TABLE OF STADIA REDUCTIONS.—Continued.

Min.	24°		25°		26°		27°	
	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.
0'.....	83.46	37.16	82.14	38.30	80.78	39.40	79.39	40.45
2.....	83.41	37.20	82.09	38.34	80 74	39.44	79.34	40.49
4.....	83.37	37.23	82.05	38.38	80.69	39.47	79.30	40.52
6.....	83.33	37.27	82.01	38.41	80.65	39.51	79.25	40.55
8.....	83.28	37.31	81.96	38 45	80 60	39.54	79.20	40.59
10.....	83.24	37.35	81.92	38.49	80 55	39.58	79.15	40.62
12.....	83.20	37.39	81.87	38.53	80.51	39.61	79.11	40.66
14.....	83.15	37.43	81.83	38.56	80.46	39.65	79.06	40.69
16.....	83.11	37.47	81.78	38.60	80.41	39.69	79.01	40.72
18.....	83.07	37.51	81.74	38.64	80.37	39.72	78.96	40.76
20.....	83.02	37.54	81.69	38.67	80.32	39.76	78 92	40.79
22.....	82.98	37.58	81.65	38.71	80.28	39.79	78.87	40.82
24.....	82.93	37.62	81.60	38.75	80.23	39.83	78.82	40.86
26.....	82.89	37.66	81.56	38.78	80.18	39.86	78.77	40.89
28.....	82.85	37.70	81.51	38.82	80.14	39.90	78.73	40.92
30.....	82.80	37 74	81.47	38 86	80.09	39.93	78.68	40.96
32.....	82.76	37.77	81.42	38.89	80 04	39.97	78.63	40.99
34.....	82.72	37.81	81.38	38.93	80.00	40.00	78.58	41.02
36.....	82.67	37.85	81 33	38.97	79.95	40.04	78.54	41 06
38	82.63	37.89	81 28	39.00	79.90	40.07	78.49	41.09
40.....	82.58	37.93	81 24	39 04	79.86	40.11	78 44	41.12
42.....	82 54	37.96	81.19	39 08	79 81	40.14	78.39	41.16
44	82.49	38.00	81.15	39 11	79.76	40.18	78.34	41.19
46.....	82 45	38.04	81.10	39.15	79 72	40.21	78.30	41.22
48.....	82 41	38 08	81 06	39.18	79.67	40.24	78.25	41.26
50.....	82.36	38.11	81.01	39.22	79.62	40.28	78 20	41.29
52.....	82.32	38.15	80 97	39.26	79.58	40.31	78 15	41.32
54.....	82.27	38.19	80.92	39.29	79.53	40 35	78.10	41.35
56.....	82.23	38.23	80.87	39.33	79.48	40.38	78 06	41.39
58.....	82.18	38.26	80.83	39.36	79.44	40.42	78.01	41.42
60.....	82 14	38.30	80.78	39.40	79 39	40.45	77 96	41 45
c= 75...	68	31	.68	32	67	.33	.66	.35
c=1.15....	1.05	48	1.04	50	1.03	51	1 02	.53
c=1 90....	1.73	79	1.72	82	1.70	85	1 69	.88

Min.	28°		29°		30°	
	Hor. Dist	Diff Elev.	Hor. Dist	Diff Elev.	Hor. Dist.	Diff. Elev.
0'.....	77 96	41 45	76.50	42 40	75.00	43 30
2.....	77.91	41.48	76.45	42.43	74.95	43.33
4.....	77.86	41 52	76.40	42.46	74.90	43.36
6.....	77.81	41.55	76 35	42.49	74.85	43 39
8.....	77.77	41 58	76.30	42.53	74 80	43.42
10.....	77.72	41.61	76.25	42.56	74.75	43.45
12.....	77.67	41.65	76.20	42.59	74.70	43 47
14.....	77.62	41.68	76.15	42.62	74.65	43.50
16.....	77.57	41.71	76.10	42.65	74.60	43 53
18.....	77.52	41.74	76.05	42 68	74.55	43 56
20.....	77.48	41.77	76.00	42.71	74.49	43 50
22.....	77.42	41.81	75.95	42 74	74.44	43 62
24.....	77 38	41.84	75.90	42.77	74.39	43 65
26.....	77.33	41.87	75.85	42.80	74.34	43.67
28.....	77.28	41.90	75.80	42.83	74.29	43 70
30.....	77.23	41.93	75.75	42.86	74.24	43 73
32.....	77.18	41 97	75.70	42.89	74.19	43.76
34.....	77.13	42 00	75.65	42.92	74.14	43 79
36.....	77.09	42.03	75.60	42.95	74.09	43.82
38.....	77.04	42.06	75.55	42 98	74.04	43 84
40.....	76.99	42.09	75.50	43.01	73.99	43.87
42.....	76.94	42.12	75 45	43 04	73.93	43 90
44.....	76.89	42.15	75.40	43 07	73 88	43.93
46.....	76.84	42.19	75.35	43.10	73 83	43 95
48.....	76.79	42 22	75 30	43.13	73.78	43.98
50.....	76.74	42.25	75 25	43.16	73.73	44 01
52.....	76.69	42.28	75 20	43.18	73.68	44 04
54.....	76.64	42.31	75.15	43.21	73.33	44 07
56.....	76.59	42.34	75.10	43.24	73.58	44.09
58.....	76.55	42.37	75.05	43 27	73.52	44.12
60.....	76.50	42.40	75.00	43 30	73.47	44.15
c= .75..	.66	.36	.65	.37	.65	38
c=1.15....	1 01	55	1.00	.57	0.99	.58
c=1.90..	1.67	91	1.65	.94	1 64	.95

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Federal Blvd Subdivision 1 + 12
Market Street Knolls 3-
W.P.L. Blvd. Midway Dr. Fontera St. 4-12
Normal St. paving levels 13 + 15
Greely Ave 16 - 21
Payne St. 22 - 23
Bancroft St 24 - 25
Montemar Ridge Unit #3 26.
Alignment Waterline Midway Dr. Moreno Blvd. 27-39
Wyon St 41 - 44
Sunset St 45 - 48
Whitman St Highway Rte 40 49 - 51
Chestnut St State Hy 52 - 53
Rosecrans 54 - 58
Gaines 59 - 60
Sketch Lena - Brooklyn - Spr. Marin 61 - 62
Kenwood St. 63 - 67
Brooklyn Ave. 68 - 73
Storm Drain along Santa Fe. RR Rosecrans 74 - 75
Waterline US Gov. Dykes (Pt Rest) 76 - 77
" " Haines + La Playa 79.

Federal Boulevard Subdivision
Unit No 2

Indexed
C.S.K.

Notes

• = Lead + Tack

□ = 2" x 2" Hubs

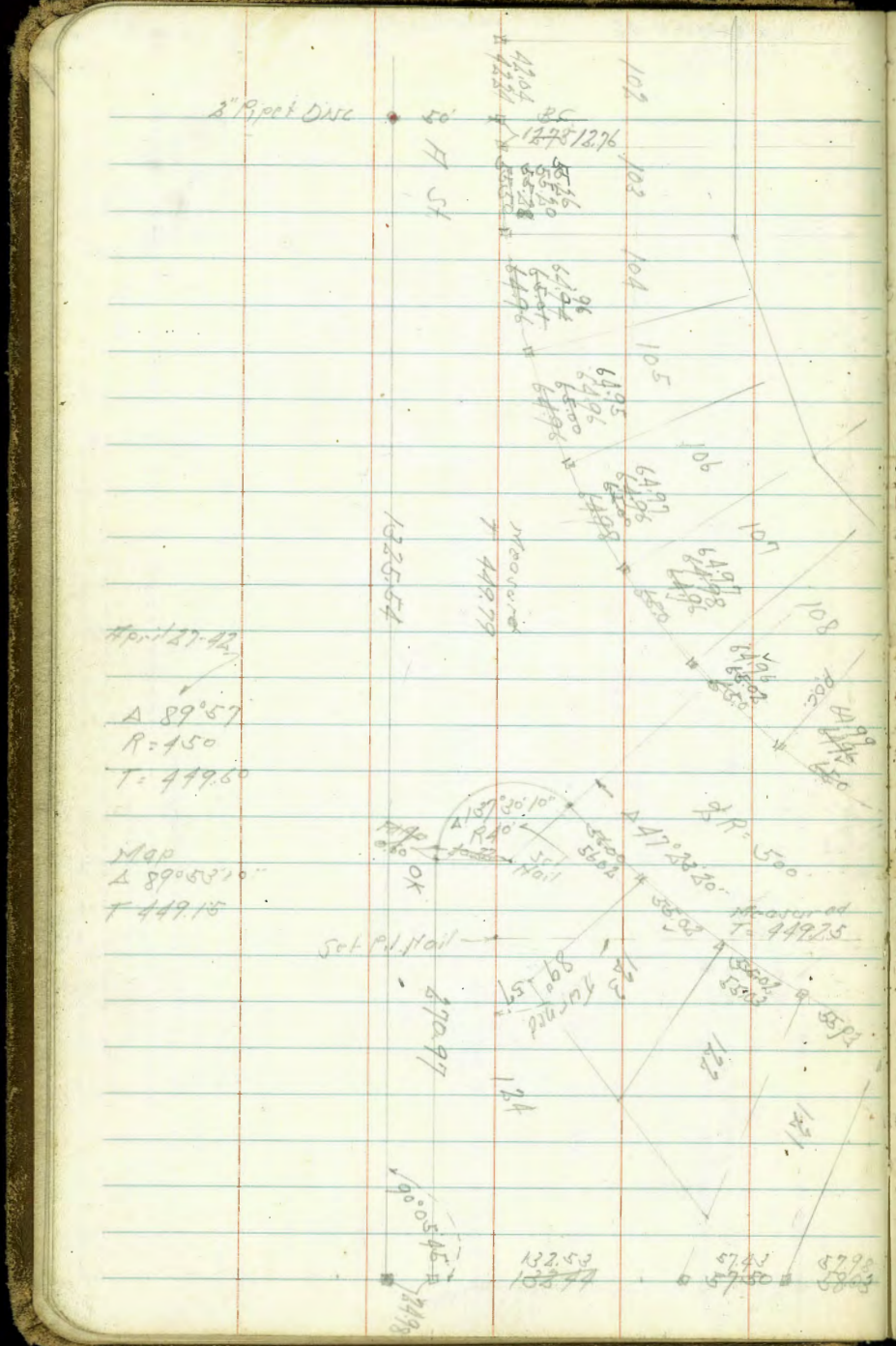
○ 2" Pipe + Disc

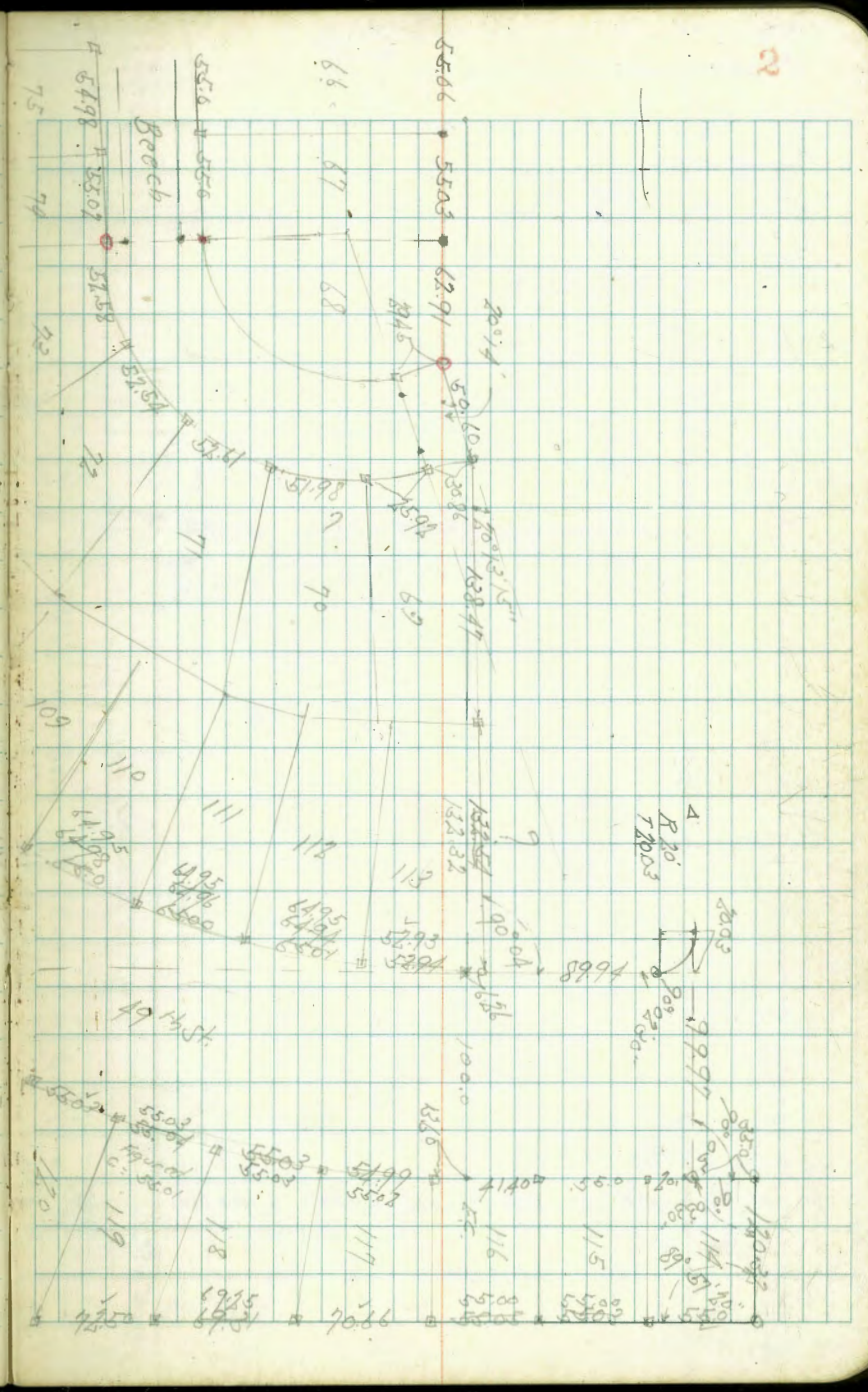
▣ Conc Mon

April 7-42
Sisson
Harbers
& Moore

2nd Check
April 24-42

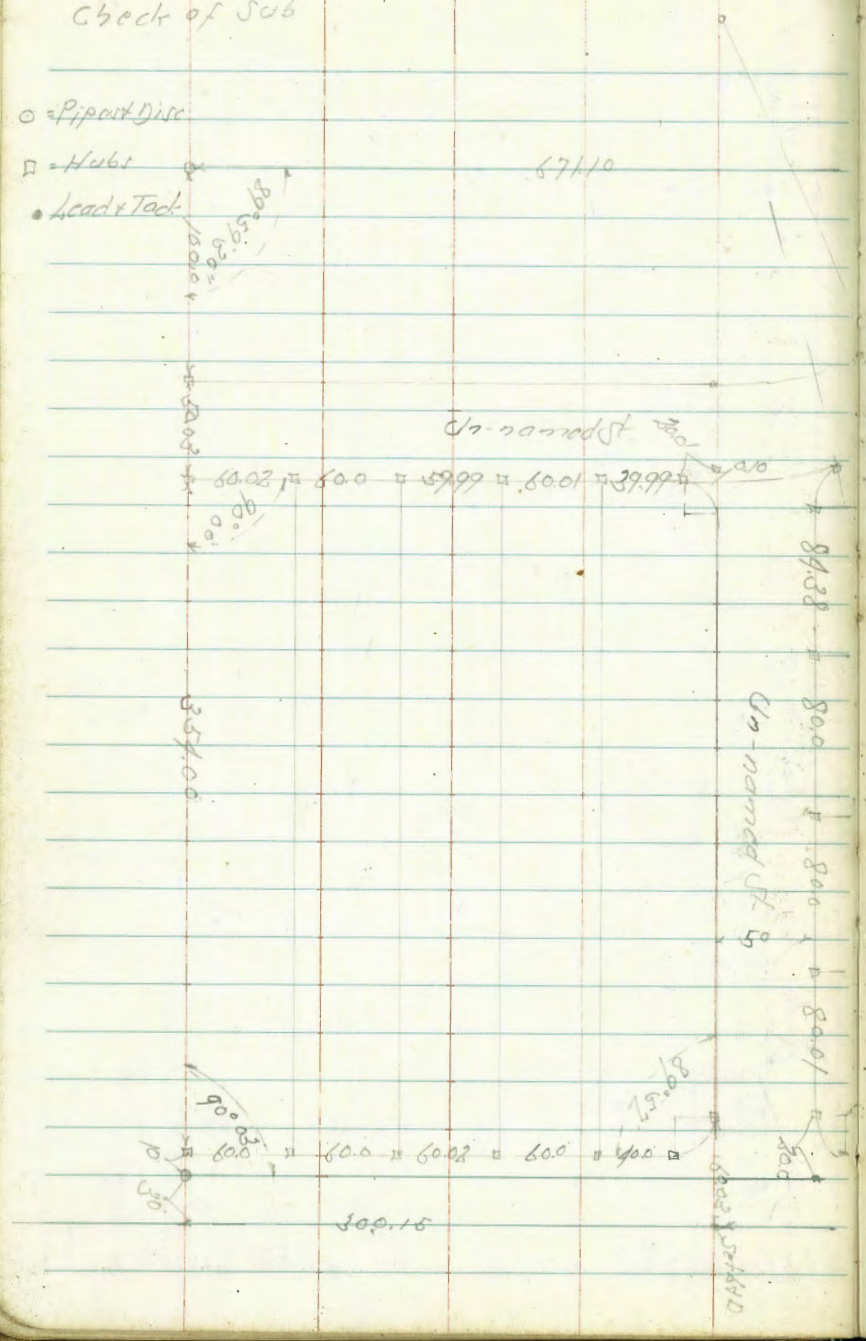
1


2" Pipe Disc
Sct. Pl. Nail
Measured
T. 449.75
Map
Δ 89°53'10"
T 449.15
Apx. 127-12
Δ 89°57
R = 450
T = 449.60
R = 500
Δ 47°28'30"


Beech
Δ
R 20.
T 20.03
89.94

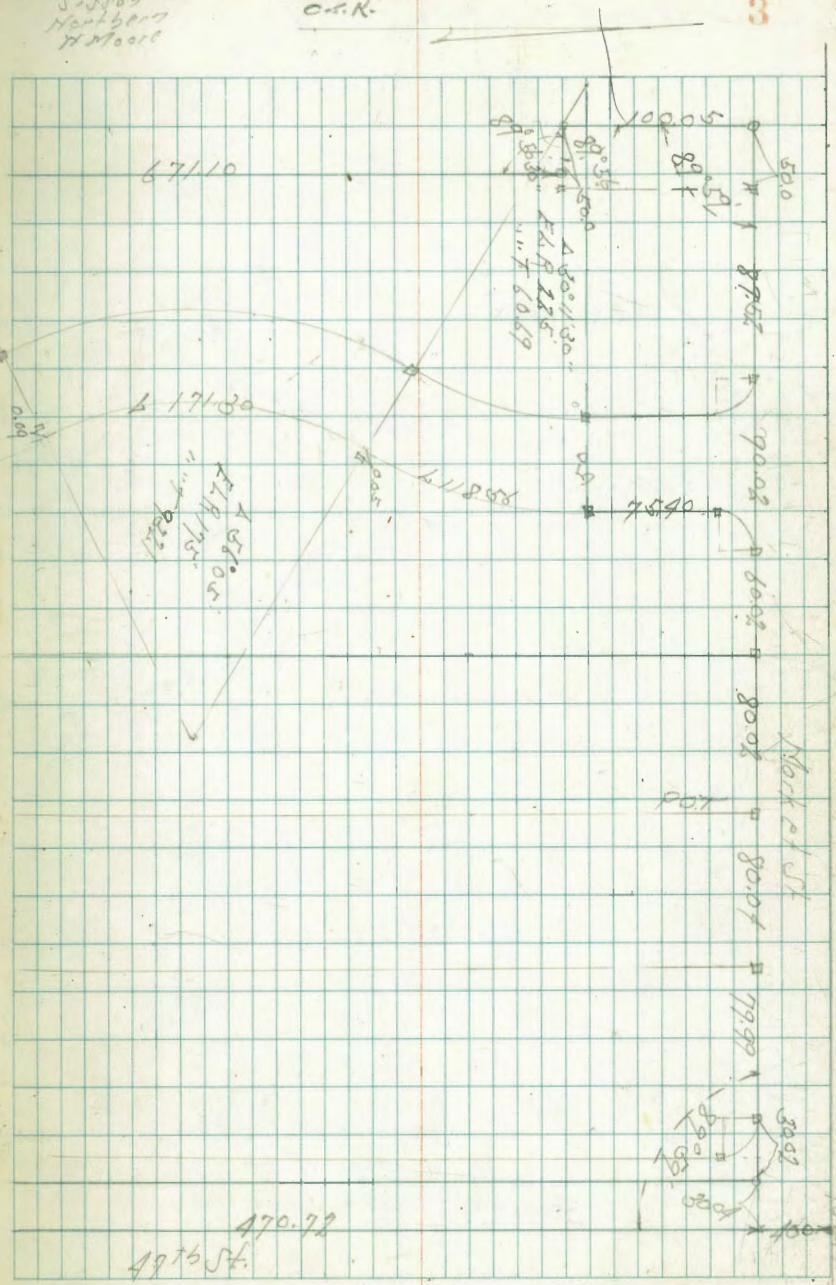
Market Street Knolls
Check of Sub

⊙ = Pipe + Disc
□ = Hubs
• Lead + Tack

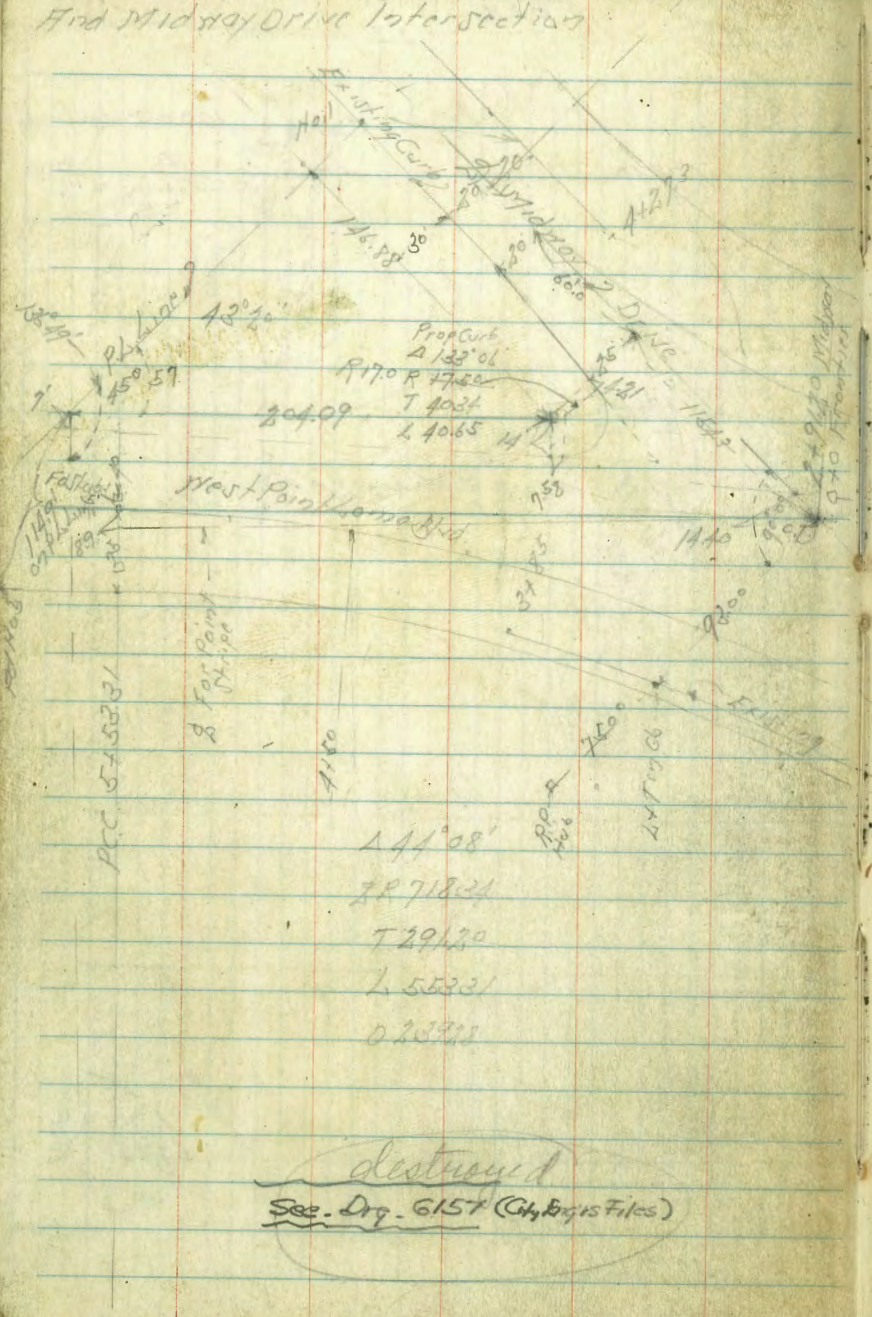


April 19-42
Sisson
Northern
W Moore

Indexed
O.S.K.

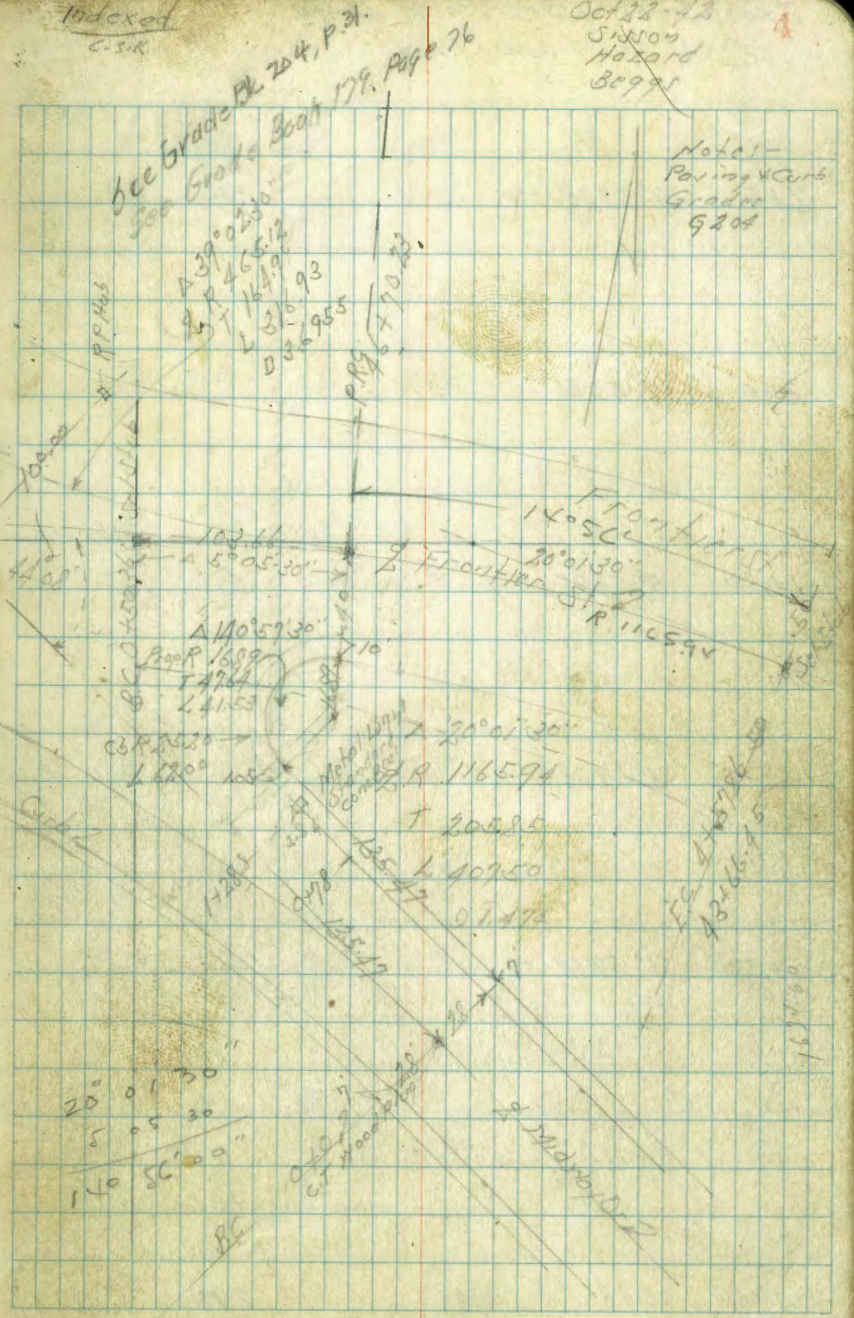


West Point Loma Blvd – Frontier St.
Find Midway Drive Intersection



Indexed
C.S.K.

Oct 22-23
Sisson
Hazard
Book



Cross Section West Point Loma
West of Midway Drive

10-26-1942

Reduced & Plotted on Grade Profile

2+50	9°58.20'	-		
2+0	7°58.58'	-		
1+50	5°58.92'	-		
1+0	3°59.28'	-		
0+50	1°59.64'	+		
0+0	= B.M.			
B.M.	8.48	11.38	2.90	B.P. 5 in N. Midway North of St. Pt. Loma

Oct 23-42
Sisson
Sims
Hazard
B6985

Lt = 5 ℄ Rt. N 5

4.96	4.33	5.26	5.96	6.38		
6.42	7.05	6.12	5.43	5.00		
28	28	14		14		
	Gutter					
4.45	3.79	4.76	5.43			
6.93	7.59	6.62	5.95			
28	28	14				
3.73	3.07	3.98	4.43			
7.65	8.31	7.40	6.95			
28	28	14				
2.94	2.30	3.03	3.33			
8.44	9.08	8.35	8.05			
28	28	14				
2.28	1.66	2.21	2.47			
9.10	9.72	9.17	8.91			
28-CL	28-Gut	14				
1.67	1.00	1.48	1.90	1.61	1.44	2.00
9.71	10.38	9.90	9.68	9.77	9.94	9.28
28-CL	28-Gutter	14		14	28-Gutter	28-CL
			11.58			

West Point Loma

4+50	17°56.76' – sta
4+0	15°57.12' –
2+85	= Wy End Curb on Lt
3+50	13°57.48' –
3+0	11°57.84' –
2+76.65	11°02

11.38

Lt Rt

6

5.41	6.03	6.38	6.38	6.35
5.97	5.35	5.00	5.00	5.13
30-SWPan	14		14	30-SWPan
5.52	5.88	6.42	6.61	6.41	6.08
5.86	5.50	4.96	4.77	4.97	5.36
25-SWPan	14		14	28	43-SWPan
5.73	5.08				
5.65	6.30				
28-Curb	28-Gutter				
5.65	5.02	5.83	6.35	6.66	6.89	6.76	6.12	5.48
5.73	6.36	5.55	5.03	4.77	4.47	4.61	5.26	5.90
28	28	14		14	28	42	56	72
5.54	4.90	5.71	6.30	6.71	6.99
5.84	6.18	5.67	5.08	4.67	4.39
28	28	14		14	28
4.75	4.61	5.51	6.18	6.67
6.13	6.27	5.89	5.20	4.71
28-Curb	28-Gutter	14		14

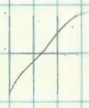
11.38

5+52.31 P.C.C. 22°04'

540 19°56.40'

11.38

Lt. Rt.



5.78 6.28 6.31 6.13
5.60 5.71 5.07 5.75
52-SH/Bx 14 15-HH-Dx

5.61 6.17 6.34 6.20 6.17
5.97 5.31 5.84 5.18 5.31
51-SH/Bx-Dx 14 14 20-HH/Bx

11.38

Cross Sections Midway

2+00

1+50

1+28.8 = Metal Light Standard Conc. Base

1+00

0+78 = End Curb on Rt.

0+50

0+00 = 0+00 on West Point Loop
11+38 Bal Ford

Reduced & Plotted on Quiver Profile
10-26-1942 C.B.H.

Lt. 8 - Rt. 8

5.85	5.99	5.90	5.65	5.84
5.53	5.39	5.48	5.72	5.44
14		14	26	28
4.52	4.51	4.22	4.55	5.02
6.86	6.87	7.16	6.82	6.36
	14	28	42	56

4.38
7.0
27.8=Metal Standard
4.38

3.38	3.38	3.38	
8.00	8.00	8.00	
	14	28	
3.00	3.67		
8.38	7.71		
28=Curb	28=CL		
2.48	2.48	2.48	3.15
8.90	8.90	8.90	8.73
	14	28=Curb	28=CL

11.38

Midway

4+34 = Sly End Curb on Lt

4+27.3 = End Curb on Rt

3+94

3+50

3+0

2+50

11.38

Lt. Rt. 9

6.46 5.62 5.62 5.48 5.32 4.93 5.58
5.13 5.76 5.76 5.90 6.16 6.45 5.80
203-Sly End 203-Sly Cut 10 203-Cut 203-Cb

4.96 5.61
6.42 5.97
203-Cut 203-Cb End

5.88 5.23 5.51 5.58 5.70 5.42
5.50 6.15 5.89 5.80 5.68 5.96
14 14=Gutter 14 10 Rt End

6.33 6.13 5.96 5.57 5.90 5.88
5.05 5.25 5.47 5.51 5.48 5.50
28 14 14 28 38: Rt Curve

7.00 6.87 6.60 5.30 6.25 6.45 6.36
4.38 4.51 4.78 5.08 5.13 4.93 5.07
28 14 14 28 42 56

6.94 6.96 6.89 6.68 6.66 6.59
4.44 4.43 4.51 4.70 4.74 4.79
14 14 28 42 56

11.38

Lt. ☆ Rt.

5+50

5+0

1+50

4.64	3.96	4.16	4.23	4.15	3.90	4.60
6.74	7.42	7.32	7.15	7.33	7.48	6.78
19.9-Cb	19.9-Gyt	10		10	20-Gyt	20-Cb
5.16	4.50	4.70	4.80	4.62	4.32	5.00
6.27	6.88	6.68	6.58	6.76	7.06	6.38
20-Cb	20-Gyt Hr	10		10	20-Gyt	20-Cb
5.99	5.31	5.38	5.21	5.04	4.17	5.43
5.39	6.09	6.00	6.11	6.34	6.61	5.95
20-Cb	20-Gyt	10		10	20.1	

11.38

11.38

Cross Section Frontier St
Midway Drive to 457.86' Fwd.

3+0 — 6°08' ✓

2+50 — 4°54.27' ✓

2+0 — 3°40.57' ✓

1+54.02 PRC 3°32.75

1+50 — 2°26.87'

1+0 — 1° 12.17'

0+50.36 B.C. PT

0+0 = 2+91.20 Mid

Reduced + Plotted on Orion Profile 10-26-72 CBH

11.38 Ft Fwd

Lt						
4.45	4.69	4.78	4.78	4.67	4.33	4.21
6.93	6.89	6.60	6.60	6.71	7.05	7.12
.50=Mid Pt.	30	15		15	30	50
4.88	5.10	5.98	5.24	5.14	4.96	4.63
6.50	6.38	6.10	6.14	6.24	6.42	6.75
50=Mid Pt.	30	15		15	30	50
5.54	5.66	5.73	5.74	6.68	5.45	5.04
5.91	5.93	5.65	5.64	5.70	5.92	6.24
49=Mid Pt.	30	15		15	30	50.5
6.08	6.10	6.25	6.11	5.98	5.68	5.35
5.36	5.22	5.13	5.21	5.40	5.70	6.03
50=Mid Pt.	30	15		15	30	52
5.96	6.33	6.46	6.36	6.11	5.90	5.31
5.42	5.05	4.92	5.02	5.22	5.48	6.07
51=Mid Pt.	30	15		15	30	48
6.08	6.17	6.68	6.74	6.68		
5.30	4.91	4.70	4.64	4.70		
54.5=Mid Pt.	30	15		15		

11.38

Frontier St

4+57.86 = E.C. 10°00.25'

4+0 8°35.37' ✓

3+50 7°21.67' ✓

11.38

Lt. ℄ Rt.

2.81	3.38	3.43	3.54	3.45	3.24	2.98
8.57	8.00	7.95	7.84	7.93	8.14	8.40
50	30	15		15	30	50
3.50	3.78	3.85	3.85	3.78	3.61	3.43
7.88	7.60	7.53	7.53	7.60	7.77	7.95
50=Rt/Rt	30	15		15	30	50
3.90	4.23	4.33	4.33	4.11	3.91	3.76
7.48	7.15	7.05	7.05	7.27	7.47	7.62
50=Rt/Rt	30	15		15	30	50

11.38

Indexed
C.S.K.

Normal St. Pav. Levels

Lincoln to Blaine & Blaine to Univ.

2 + 00

+ 35

N

+ 50

1

0 + 50

0 + 00 = R 13'

0 - 13 = 2' So. of St. Lincoln

Top F.H. J.E. Coon — 0.17 — 315.67 — 315.50

Lincoln Normal

Notes Reduced 3-10-43

E. Lane & W. Lane

308.32	308.79	308.82			308.63	308.50	308.03
7.33	6.88	6.83			7.04	7.17	7.64
55	42.5	30			30	42.5	55
308.63	309.10	309.18			308.92	308.80	308.92
7.04	6.57	6.49			6.75	6.87	7.21
55	42.5	30			30	42.5	55
309.02	309.58	309.67			309.32	309.12	308.86
6.45	6.09	6.00			6.35	6.53	6.84
55	42.5	30			30	42.5	55
309.88	310.30	310.37			310.01	309.86	309.89
5.79	5.37	5.30			5.66	5.81	5.18
55	42.5	30			30	42.5	55
310.70	310.99	311.01			310.66	310.48	310.09
4.97	4.68	4.66			5.01	5.19	5.58
55	42.5	30			30	42.5	55
311.91	311.69	311.69			311.35	311.08	310.68
4.26	3.98	3.98			4.32	4.59	4.99
55	42.5	30			30	42.5	55
312.17	312.32	312.43	312.59		312.13	311.97	311.67	311.25
3.50	3.35	3.24	3.13		2.5 #	3.70	4.00	4.42
55	42.5	30	25		25	30	42.5	55
312.70	312.87	312.97		312.60		312.03	311.84	311.92
3.27	3.70	3.16		3.07		3.64	3.83	4.25
55	42.5	30		Pav.		30	42.5	55

315.67 ✓

5+72 = R 13'

5+36

5+00

4+50

4+00

T.P. 5.13 311.92 8.88 306.79 ✓

3+60

3+42.5

2+85

315.67

E Lane

305.98	305.80	306.05	306.10
6.44	6.12	5.87	5.82
55	42.5	30	25
305.74	306.14	306.13	
6.16	5.80	5.79	
55	42.5	30	
306.11	306.41	306.45	
5.81	5.51	5.47	
55	42.5	30	
306.54	306.77	306.79	
5.38	5.15	5.13	
55	42.5	30	
306.99	307.15	307.16	
4.93	4.77	4.76	
55	42.5	30	
307.35	307.48	307.46	
8.32	8.19	8.21	
55	42.5	30	
307.62	307.93	307.93	
8.05	7.74	7.74	
55	42.5	30	
307.99	308.96	308.51	
7.68	7.21	7.16	
55	42.5	30	

W. Lane

305.99	305.97	305.79	305.92
5.93	5.95	6.13	6.00
25	30	42.5	55
	306.18	305.99	305.69
	5.78	5.93	6.23
	30	42.5	55
	306.38	306.28	305.91
	5.54	5.69	6.01
	30	42.5	55
	306.73	306.60	306.38
	5.19	5.32	5.54
	30	42.5	55
	307.18	307.02	306.80
	4.74	4.90	5.12
	30	42.5	55

311.92 ✓

	307.35	307.31	307.01
	8.32	8.36	8.66
	30	42.5	55
	307.87	307.71	307.33
	7.80	7.96	8.34
	30	42.5	55
	308.39	308.17	307.67
	7.33	7.55	8.00
	30	42.5	55

315.67 ✓

E. Lane & W. Lane 15

302.55	302.75	302.88	303.13	307.77	302.86	307.99
9.38	9.27	9.04	8.79 Pav.	9.15	9.06	9.93
55	42.5	30		30	42.5	55
302.63	302.85	303.07	303.09	302.90	302.81	302.69	302.08
9.29	9.07	8.90	8.83	9.02	9.11	9.28	9.84
55	42.5	30	25	25	30	42.5	55
302.99	303.18	303.25			303.08	302.93	302.88
8.98	8.74	8.67			8.82	8.99	9.42
55	42.5	30			30	42.5	55
303.38	303.59	303.72			303.55	303.40	303.13
8.58	8.33	8.20			8.37	8.54	8.79
55	42.5	30			30	42.5	55
303.65	304.06	304.25			304.10	303.93	303.56
8.27	7.86	7.67			7.82	7.99	8.36
55	42.5	30			30	42.5	55
304.05	304.51	304.67	304.73	304.70	304.65	304.50	304.15
7.87	7.41	7.25	7.18	7.22	7.27	7.42	7.77
55	42.5	30	25	25	30	42.5	55
304.21	304.63	304.80	305.07	304.88	304.67	304.29
7.71	7.29	7.12	6.85 Pav.	7.04	7.25	7.63
55	42.5	30		30	42.5	55
305.36	305.69	305.97	306.11	305.93	305.66	305.29
6.56	6.23	5.95	5.81 Pav.	5.99	6.26	6.63
55	42.5	30		30	42.5	55

3 11.9 N

2 + 03.7 at Univ. Ave.

1 + 90.7 = R 13'

+50

3 15.28
3.28
308.64
.45
315.59
.09
315.50 3155 BM

+50

0 + 00 = R 13'

0 - 13 = 2' So. of Sh. Blaine

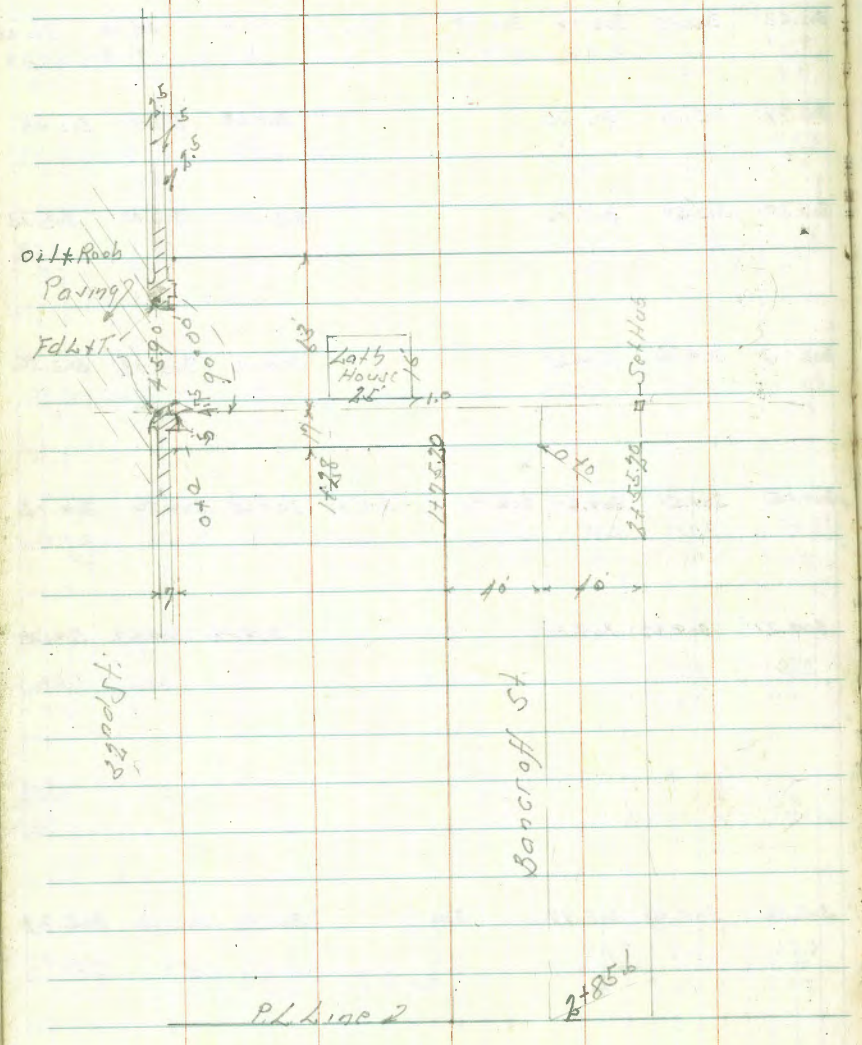
Set
BM. Top
F.H. SECon 4.75 307.17 Blaine Normal

5 + 85 = N. L. Blaine

311.9 N

Cross Section Greeley Ave
32nd St to 33rd St.

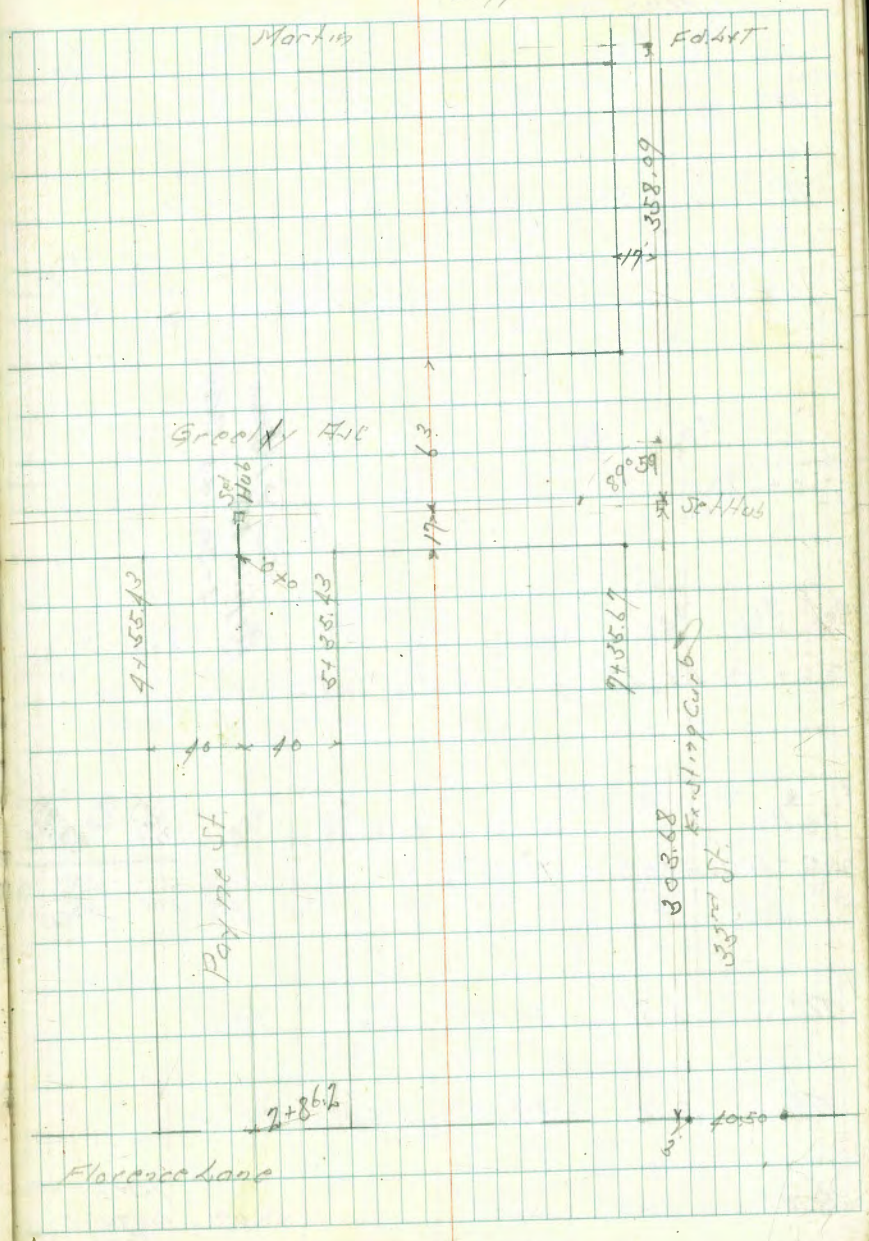
Levels Next Page



Indexed
C.S.K.

March 26-43
Sisson
Bliss
Bragg

16



Cross Section Grade w/ H.C.
32nd St to 33rd St.

Sketch Page 16

1+0		3' Lt of ℄ = Fence		
TP	8.27	42.87	2.56	34.60
0+50		3' Lt: Board Fence		
0+04				
0+0 = EL 32nd St.		4' Lt of ℄ = 5' Wh Board Fence		
0-10 = EC b Line 32nd St.				
TP	8.86	37.16	10.89	28.30
TP	0.14	39.19	12.58	39.05
BM	0.56	51.63		51.07

Red'd Reported Profile 388 3-30-43 CBH

32.7 / .45 60 — 33.39 / 2.77 b=c

NW BP Logan + 32nd St

Lt: N ℄ Rt: S 17

38.7 / 1.3 40 — 38.0 / 1.9 20 — 37.5 / 2.5 40 — 36.2 / 3.7 60 — 36.2 / 3.7 60 — 35.6 / 4.3 20 — 34.5 / 5.4 40 — 32.9 / 7.0 80

42.87

37.0 / 0.7 40 — 36.7 / 0.5 20 — 35.4 / 1.7 60 — 35.2 / 1.9 20 — 35.2 / 1.9 20 — 33.7 / 3.5 20 — 32.3 / 4.9 40 — 30.4 / 6.8 60

36.4 / 0.8 40 — 35.5 / 1.7 20 — 34.9 / 2.3 20 — 33.1 / 4.1 — 32.2 / 5.0 20 — 31.4 / 5.8 40 — 29.7 / 7.5 60

33.4 / 3.8 40 — 33.8 / 3.7 20 — 32.69 / 4.47 20-cb — 32.6 / 4.6 — 32.1 / 5.1 20 — 32.01 / 5.15 20-cb — 31.6 / 5.6 40 — 30.4 / 6.8 60

33.3 / 1.9 40 — 32.57 / 2.29 40-cb — 32.1 / 5.1 30 — 32.52 / 4.54 30-cb — 31.91 / 5.25 20 — 31.42 / 5.74 — 31.0 / 6.7 30 — 30.7 / 7.5 30 — 31.31 / 6.25 30-cb — 31.31 / 6.25 30-cb — 30.4 / 6.8 40 — 30.18 / 6.98 40-cb

37.16

2+55.20 = ℄ Bancroft

2+52 38'Lt of ℄ = SE Fence

2+25

2+15.20 = ℄ Bancroft · 38'Lt of ℄ = Fence

TP	0.41	20.39	12.26	19.98
2+10		38'Lt of ℄ = Board Fence		
TP	2.07	32.24	12.70	30.17
BM			7.52	35.35

PK@ 1+75.00 Rt

1+75.20 = WL Bancroft 3'Lt of ℄ = Wire Fence

1+50 3'Lt of ℄ Wire Fence

42.87

Lt ℄ Rt

8.7	8.4	8.1	7.9	7.9	8.2
11.7	12.0	12.3	12.5	12.5	12.5
60	40	20		20	40
11.5	10.2	8.9	9.6	8.3	7.9
8.9	10.2	11.5	10.8	12.1	12.5
60	40	20		20	40
14.2	13.8	12.1	10.8	11.5	11.9
6.2	6.6	8.3	9.6	8.9	8.5
60	40	20		20	40
			20.39		
21.2	21.0	18.4	18.4	18.3	22.6
11.0	11.2	13.8	13.8	13.9	9.6
60	40	20		20	40
			32.24		
36.8	36.1		36.2	36.0	35.8
6.1	6.8		6.7	6.9	7.1
38.5 Ft Bldg	40			20	40
38.0	37.7	37.6	37.4	36.8	36.3	35.5
4.9	5.2	5.3	5.5	6.1	6.6	7.4
35.5 Ft Bldg Conc Found	40	4		20	40	60

42.87

3+93					
3+83	-Z + Bottom of Creek				
3+70					
3+61					
3+50					
3+40					
TP	7.16	14.96 20.89	12.59	7.80	⊙ Hub 2+55.2 E.L. Bancroft 5172 Greek

4+ Z R+ 3-29-43

19

3.5	3.2	4.0	4.1	3.7	3.4	3.4
11.5 60	11.8 40	11.0 20	10.9	11.3 20	11.6 40	11.6 60
2.7	2.7	3.3	1.9	1.5	0.6	1.4
12.3 60	12.3 40	11.7 20	13.1	13.5 20	14.4 40	13.6 60
3.1	3.1	3.7	2.9	3.3	3.1	3.1
11.9 60	11.9 40	11.3 20	12.1	11.7 20	11.9 40	11.9 60
13.8	12.4	11.6	10.2	12.1	12.2	11.5
2.2 60	2.6 40	3.4 20	4.8	2.9 20	2.8 40	3.6 60
9.5	8.3	9.1	9.9	8.9	9.2	8.8
5.5 60	5.0 40	5.9 20	6.0	6.1 20	5.8 40	6.2 60
8.5	9.0	8.8	8.7	8.4	8.5	8.9
6.5 60	6.0 40	6.2 20	6.2	6.6 20	6.5 40	6.5 60

14.96

5+70

5+35.43 - E.L. Payne

BM	5.10	13.87	6.19	8.77	Hub Z of Payne So. 17 Zinc Spike

4+95.43

4+55.43 - W.L. Payne

4+10

4+02

1496

Z

9.4	9.1	9.4	9.6	8.4	8.6	8.6
4.5 / 60	4.8 / 40	4.5 / 20	4.3	5.5 / 20	5.3 / 40	5.3 / 60
9.3	9.4	9.5	9.7	8.2	8.2	
4.6 / 60	4.5 / 40	4.4 / 20	4.2	5.7 / 20	5.7 / 40	
			13.87			
9.3	9.3	9.5	9.2	8.8	8.7	
5.7 / 60	5.7 / 40	5.5 / 20	5.8	6.2 / 20	6.3 / 40	
9.0	8.9	8.9	8.8	8.2	8.3	
6.0 / 60	6.1 / 40	6.1 / 20	6.2	6.8 / 20	6.7 / 40	
9.4	9.3	9.5	9.4	8.8	8.7	8.2
5.6 / 60	5.7 / 40	5.5 / 20	5.6	6.2 / 20	6.3 / 40	6.8 / 60
11.7	11.1	11.0	10.3	10.3	10.3	10.0
4.3 / 60	3.9 / 40	4.0 / 20	4.7	4.7 / 40	4.7 / 40	5.0 / 60

1496

For Check
Sly W Cb of 33rd
At Fletcher Lane

6.96 6.91

FB 1439
Page 67
6.93

7+55.67 = W Cb Line 33rd St.

7+35.67 = W L. 33rd St.

7+0

6+50

6+0

N.87

Lt. Rt

8.45 8.38 8.39 8.17 8.15 8.07 8.02

5.42 5.49 5.56 5.70 5.72 5.80 5.85
60 40 40 40 40 40 60 Trees

9.3 9.2 9.3 9.5 8.8 8.6 8.4

4.5 4.7 4.6 4.4 5.1 5.3 5.5
60 40 20 40 60

9.3 9.2 9.2 9.5 9.1 9.1 8.9

4.6 4.7 4.7 4.4 4.8 4.8 5.0
60 40 20 20 40 40 60

9.3 9.1 9.1 9.0 9.1 9.2 9.3

4.6 4.8 4.8 4.9 4.9 4.7 4.5
60 40 20 40 60

8.9 9.1 9.4 9.6 8.8 8.7 8.5

5.0 4.8 4.5 4.3 5.1 5.2 5.4
60 40 20 40 60

1487

Cross Section Payne St.
Greeley to Florence Lane

Sketch Page 16

Reduced & Plotted 3-30-43 G.B.H.

2+35					
2+18					
2+0					
1+50					
1+0					
0+50	= 50 Sot S.L. Greeley				
BM	2.30	11.07	8.77	Hub & Payne Sta by W.L. Greeley Page 20	

Lt = E ℄ Rt = W 22

5.7	5.5	1.4	1.4	1.4	1.6		5.2
5.1 60	5.6 40	9.5 40	9.7	9.7 20	9.5 40 - W/L Creek		5.9 60
6.2	5.8	5.6	5.8	7.4	1.5	1.5	1.8	7.6
4.9 60	5.3 40	5.5 20	5.3	8.7 5	9.6 20	9.6 40 - Bot	9.3 60	6.5 60
5.8	6.4	6.3	6.4	5.5	8.7	7.7		1.6
4.3 60	4.7 40	4.8 20	4.7	5.6 10	8.4 20	8.4 40		9.5 60 - Bot Creek
6.5	6.3	6.9	7.3		7.4	7.3	7.6	
4.6 60	4.8 40	4.2 20	3.8		5.7 20	5.8 40	5.5 60	
8.0	7.3	7.0	7.1		7.2	7.6		8.0
3.1 60	3.8 40	4.1 20	4.0		3.9 20	3.5 40		3.1 60
8.2	8.3	7.6	7.9		7.8	7.7	7.8	
2.9 60	2.8 40	3.5 20	3.7		3.3 20	3.4 40	3.3 60	

11.07

LT Z RK

2+86.2 = NL Florence Lane

2+73

2+56

1.4	2.4	6.6	5.9	7.3	5.4	5.9	
9.7	8.7	4.5	5.2	3.8	3.7	3.2	
60	40	20		20	40	50	

60 = ½ Creek

1.3	1.4	1.4	4.5	5.5	5.3	5.5	9.0
9.8	9.7	9.7	6.6	5.6	5.6	5.6	4.4
60	40	30	20		20	40	60

2.6	1.5	1.5	1.5	4.8	4.9	6.1	9.8
8.5	9.6	9.6	9.4	6.3	6.2	5.0	1.3
50	40	20		20	40	50	50

11.07

11.07

Cross Section Bancroft Grade to Florence Lane

Sketch Page 16

Rec'd Plot 3-30-43 CBH.

1+50				
1+25				
1+0				
0+75				
TP	0.24	26.01 ✓	12.75	25.77 ✓
0+50				
0+25 = 35'50/54 Grade/				
BM	2.17	38.52		35.35

Pos 1+75 0'RT Grade Page 18

Lt. E ℄ Rt. W

9.5	11.9	17.9	17.9	16.6	15.5	14.4	13.2	13.7
16.5 60	14.1 47	8.1 46	8.1 40	9.4 30	10.5	11.6 30	15.8 40	13.3 60
8.4	19.9	19.9	19.4	20.0	19.5		18.8	17.6
12.6 63	6.1 48	6.1 40	6.6 20	6.0	6.5 20		7.3 40	8.1 60
8.0	7.9	9.8	19.8	20.3	20.4	21.7	22.3	22.6
18.0 60	18.1 45	16.2 40	6.2 30	5.7 20	5.6	4.3 20	5.7 40	6.1 60
8.3	7.4	8.6	13.5	21.2	20.6	21.8	22.7	
17.7 60	18.6 40	17.4 31	12.5 20	4.8 17	5.4	4.3 20	5.2 40	
					26.01			
8.0	7.3	7.7	8.5	16.5	19.2	21.2	23.9	30.4	33.7
30.5 60	31.2 40	30.8 25	30.0 20	22.0	19.3 15	17.3 20	14.6 30	8.1 35	4.8 25
7.7	8.0	8.0	8.0	13.3	26.9	32.8	34.9		
30.8 60	30.5 40	30.5 20	30.5 12	25.2	11.6 30	5.7 32	3.6 40		
				38.52					

2+85.6	=N.2 Florence Lane			
2+73				
2+50				
2+0				
1+75				
TP	270	17.81	11.90	14.11
		26.01		

11.2 11.8 16.1 21.8 26.8 32.6

6.6 6.0 1.7 +4.0 +9.0 +14.8
60 40 30 30

12.0 12.1 12.6 14.4 23.0 26.3 30.6

5.8 5.7 5.2 3.4 +5.2 +8.5 +12.8
60 40 20 35 40

11.8 9.8 9.9 10.3 11.8 12.9 14.3 14.7

9.5 8.0 2.9 2.5 6.0 4.9 5.5 3.1
60 40 30 5 20 40 50

13.4 18.2 10.3 10.6 11.0 11.1 11.3

4.1 7.6 2.5 2.3 6.8 6.7 6.5
60 40 30 20 40 50

16.8 10.5 9.9 12.8 12.0 10.8 11.2 11.2 11.5

1.0 7.3 7.9 5.0 5.8 7.0 6.6 6.6 6.6
60 55 40 36 20 20 40 40 60

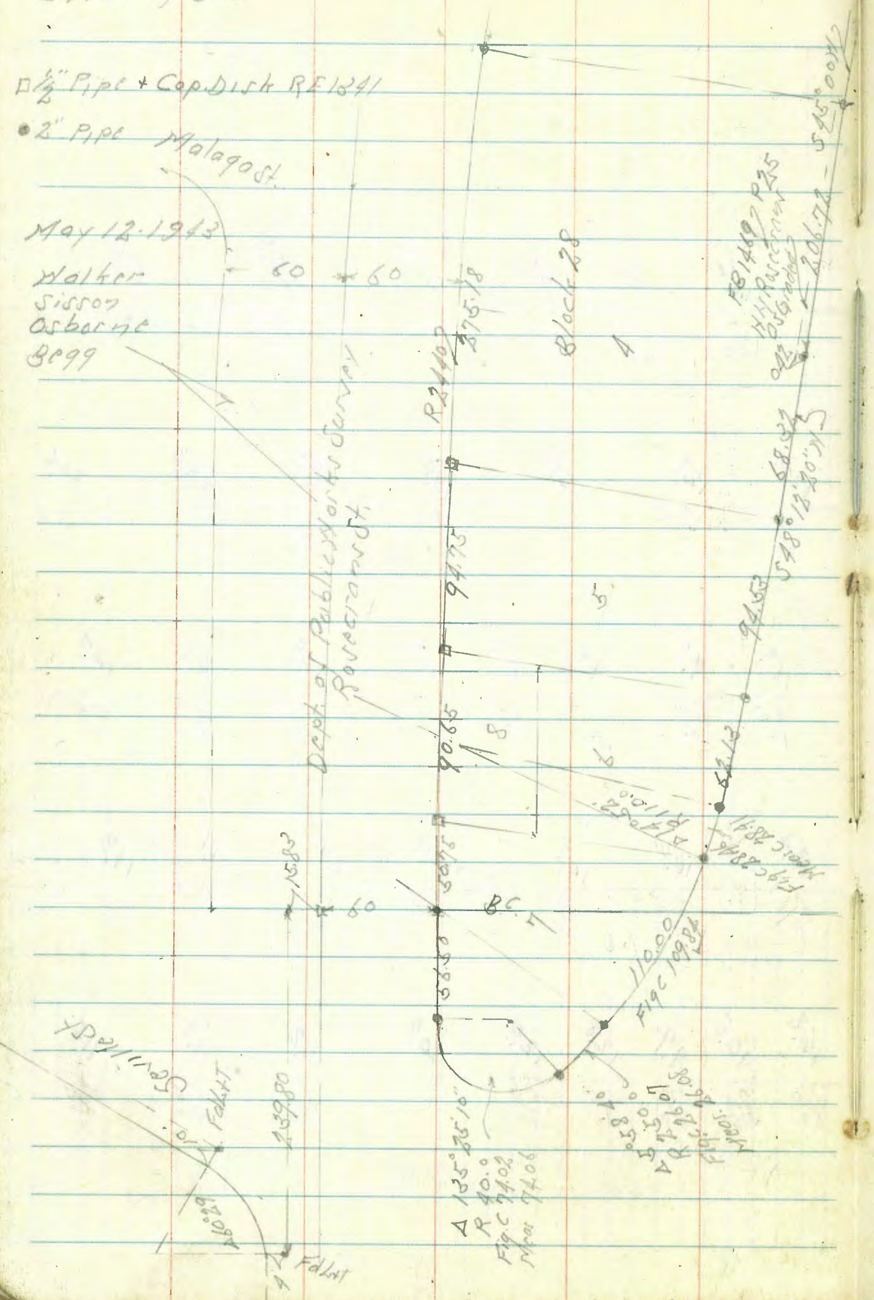
17.81

Montemar Ridge Unit No 3
Check of Sub

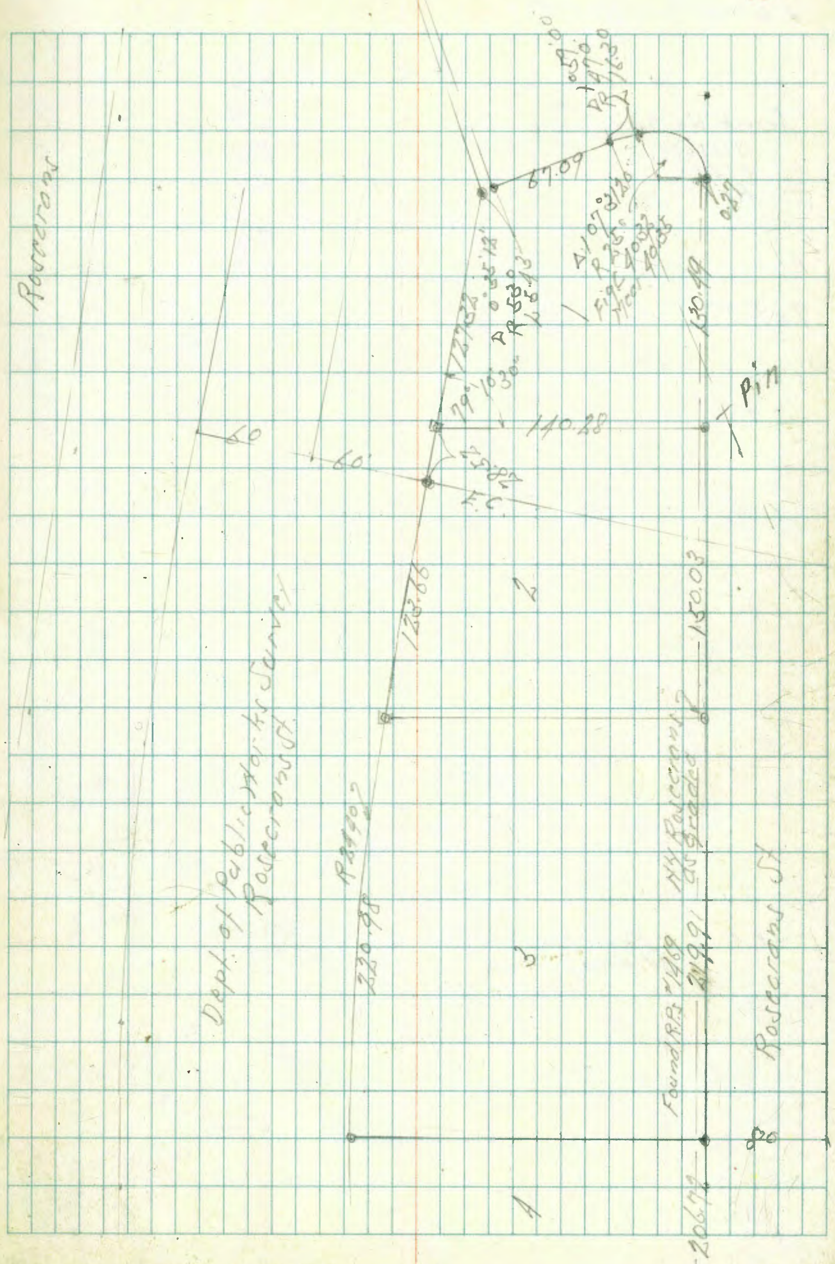
□ 1/2" Pipe + Cop. Disk RE1341
● 2" Pipe

May 12-1943

Walker
Sisson
Osborne
Begg



Indexed
C.S.K



Proposed Water Line Alignment
Midway Dr. & Frontier St. to Moreno Blvd.
& Camino Del Rio

Levels Page 34

June 4-1943
S 1550
B 15.5
B 99

9+91.97 △

0+00 = Existing 18" Water Line
Midway Drive

Midway Dr.

Indexed
C.S.K.

27

Sea book 1634
pages 57, 58 & 71

Frontier St.

Existing 18" Water Line

Midway Dr.

Page 4

Fd RP
Hdo

Equation. 29+28.18
29+28.03 EC =

R= 1000' T= 53.18

L= 106.17

28+75.00 Δ 1°05' Rt 28+21.86 BC

28+03 16.7 Lt of ℄ = Ely Power Pole Angle

26+61 16.5' Lt of ℄ = Ely Power Pole

26+34.88 P.O.T.

22+03.

Equation 10+85.69
10+85.59 EC =

R= 1000' T= 53.72

9+91.97 Δ 1°09' Rt L= 107.38

9+38.25 BC

28+75.00
Δ 1°05' Rt

28+05.09

Fd Mon

#1.

Fd Pipe

26+34.88

#2 26+35.06
See Page 76

Power Pole #1665

Sly Elec Gen Dist Pole
Proposed Line

See Book 1634
pages 51, 52, 271

Fd. Mon + Pipe

9+91.97

47+56.65 P.O.T

Equation → 43+51.82 ←
43+51.79 EC =

R= 1000' T= 51.82
L= 103.56

43+00 Δ 5°56' Rt

42+98.18 BC

Equation → 35+78.89 ←
35+78.79 EC =

R= 1000' T= 41.09
L= 82.03

34+96.76 BC

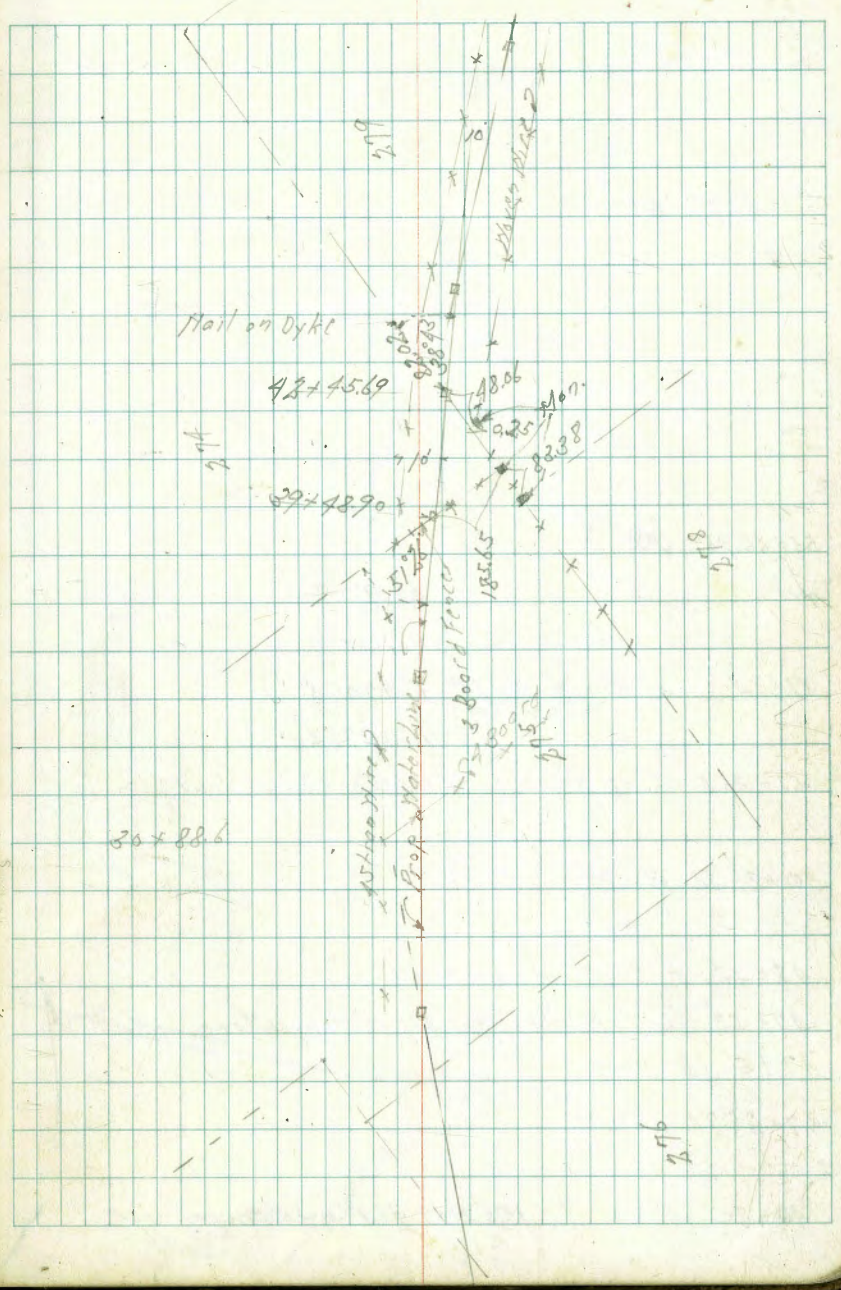
35+37.80 Δ 4°42' Rt

35+19 10.3' Rt of ℄ = Fly Power Pole

32+81 9.8' Lt of ℄ = Fly Power Pole

30+40 9.6' Lt of ℄ = Fly Power Pole

28+75.00 Δ 6°05' Rt



57+41.77 BC Lt

53+66.96 E.C.

Δ 19°19' This Curve Changed Page 77

R 1000.0

51+74 56 Rt of ℄ = N 44 34" T 170.18

Pepper Tree L 337.14

51+35.5 42 Rt of ℄ : N W ly Cor. Calif. House

50+29.83 B.C. Rt

48+48 = S ly Gordon Plot

47+52 18.5 Lt of ℄ = E 4.36" Pepper Tree

47+56.65 P.O.T

47+25.76 P.O.T

46+83 18.5 Lt of ℄ = E ly 30" Pepper Tree

90.98

B.C. Santa Fe R.R.

59+41.77

5.57 40.69 Cl. Link Fence Cor. Island

Pacific Highway

35.63 # Fd Mon 64+28.50

159.36

6.42

5.04 Fd Mon

53+79.98 E.C. New Page 79

E.C. 53+66.96

Fd Mon 21.15

6.82

Δ 13°57'

B.C. 50+29.83

Fd Mon (Bent)

Fd Mon

10.20

Fd Mon

Fd Hub & Tack FB. 15-25-23

69+54.87 P.O.T.

69+15.63 opp Sta.

Equation GC+97.52

GC+97.51 EC

66+42.51 Δ 4°55'45"

66+09.20 Δ 4°23'30" Lt.

R=1000' T=38.38

L=76.65

65+70.86 BC

60+36.11 E.C.

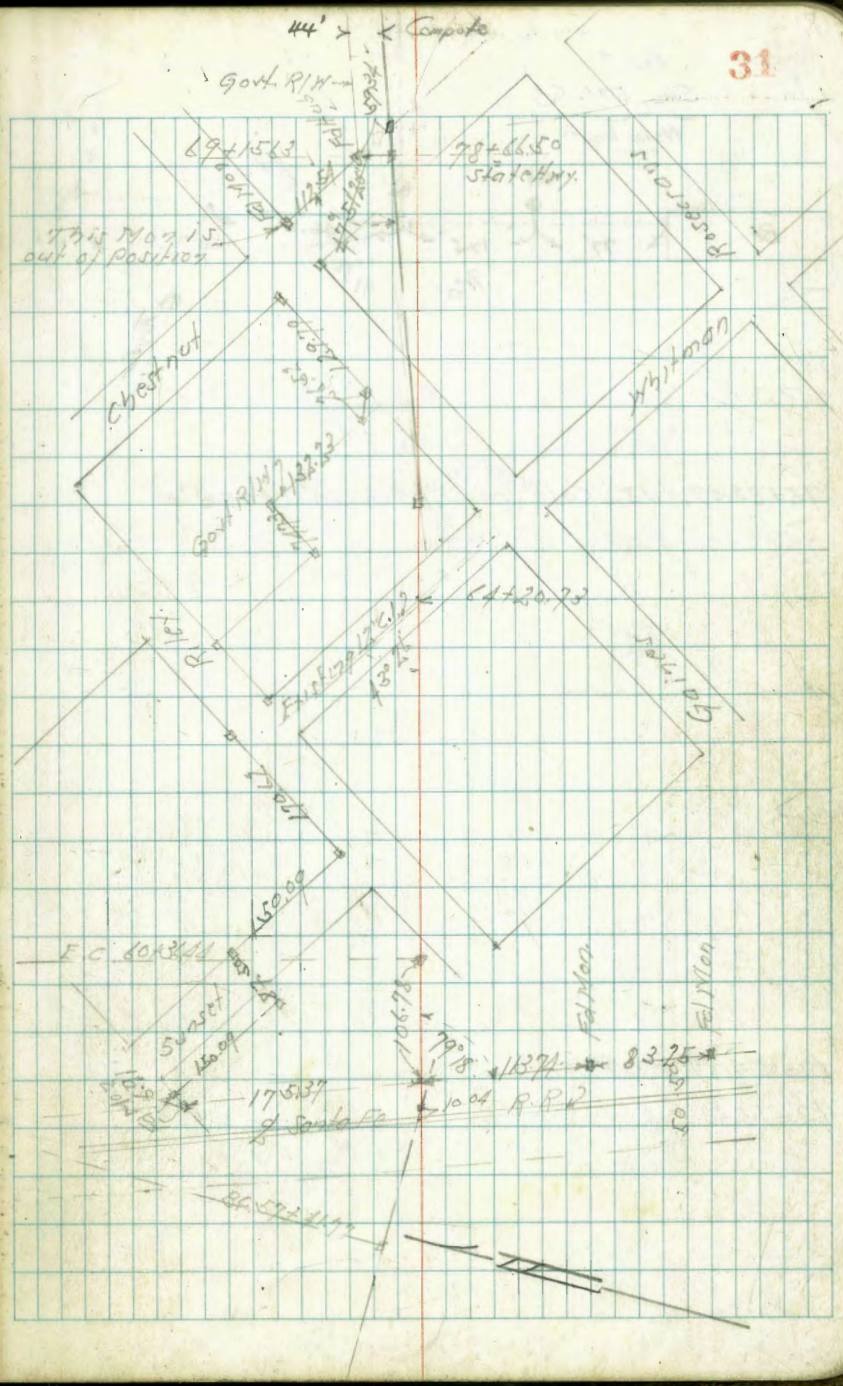
Δ 16°53'

R 1000.0'

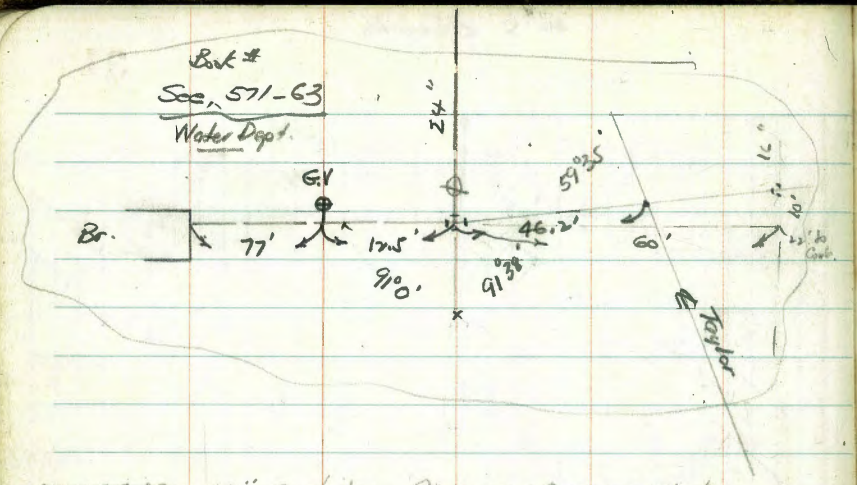
T 148.41'

L 294.67'

57+41.77 BC Lt



Book #
Sec. 571-63
Water Dept.

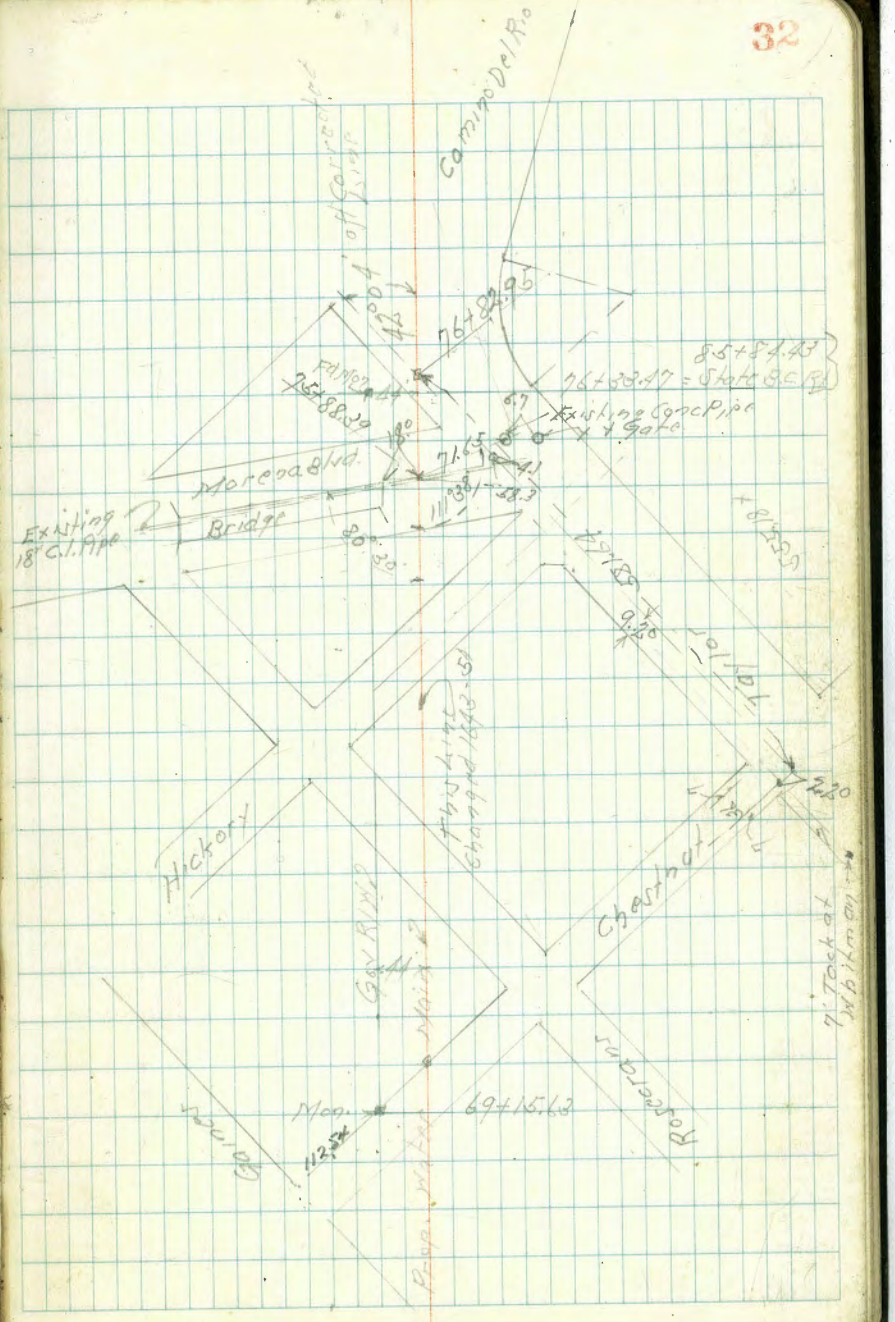


~~75+88.89~~ = 18" Cast Iron Pipe on Morena Blvd.

75+53.06 P.O.T.

~~69+54.89 P.O.T.~~

69+15.63



Levels Proposed Water Line
Midway Dr & Frontier St. to Moreno Blvd
& Camino Del Rio Alignment 27-32

B.M	7.64	10.54		2.90	BP 50' Rt of Cl Midway at 360 Point from
0+0	0' Paving		5.00	5.58	
+25	" "		5.2	5.3	
+50	" "		5.2	5.3	
+60	" "		5.0	5.5	
1+0	" "		5.0	5.5	
+50	" "		5.2	5.3	
2+0	" "		5.6	4.9	
+39	= N Ely Pav.		6.1	4.9	
+42			6.2	4.3	
+53			9.9	0.6	
+64			7.4	3.1	
3+0			7.7	2.8	
"	12 Lt of ℄ = N Ely Fill		8.3	2.2	
"	30' " " "		11.2	- 0.7	
+50			7.5	3.0	
TP	4.46	7.80	7.20	3.34	
4+0			4.8	3.0	
+50			4.7	3.1	
5+0			5.3	2.5	
"	11 Lt of ℄ = N Ely Fill		5.8	2.0	
"	17 Lt " "		8.9	-1.1	
+50			5.8	2.0	
6+0			5.5	2.3	
+50			4.8	3.0	

June 16-43
SISSON
BLISS
BC99

34

7.80

7+0			4.9		2.9
"	6' Lt of ℄ = N Ely Fill		4.9		2.9
"	11' " " "		8.2		-0.4
+50			5.2		2.6
8+0			5.3		2.5
+50			5.1		2.7
9+0			6.4		1.4
"	14' Lt of ℄		7.6		1.2
"	1 Rt " " = N Ely Fill		5.1		2.7
+50			7.4		0.4
+91.99 AL 09 Rt			7.4		0.4
TP	7.21	7.60	7.41	0.39	9+91.99
10+0			7.3		0.4
+50			7.4		0.2
11+0			7.4		0.2
+50			7.2		0.4
12+0			7.4		0.2
"	9' Rt of ℄		7.4		0.2
"	12 Rt of ℄ = N Ely Fill		5.2		2.4
+50			7.2		0.4
13+0			7.2		0.4
+50			7.2		0.4
14+0			7.2		0.4
"	3' Rt of ℄		7.2		0.4
"	7' Rt " " = N Ely Fill		4.3		3.3

		7.60 ✓		
14+50			7.2	0.8
15+0			7.0	0.6
+50			6.9	0.7
16+0			6.8	0.8
"	4' Rt of ℄ = NY Fill		4.2	3.8
+50			6.9	0.7
TP	4.69	7.83 ✓	4.46	3.14
17+0	= NY Fill		5.1	2.7
+50			4.8	3.0
18+0			5.5	2.3
"	2' Lt of ℄ = NY Fill		5.5	2.3
"	5' " "		6.5	1.3
+50			5.1	2.7
19+0			5.0	2.8
+50			4.8	3.0
20+0			5.2	2.6
" "	8' Lt of ℄ = NY Fill		5.0	2.8
" "	11' Lt of ℄		6.2	1.5
+50			5.6	2.2
21+0			5.7	2.1
+50			5.5	2.3
22+0			5.9	1.9
"	11' Lt of ℄ = NY		5.8	2.0
"	15' " "		7.0	0.8
TP	4.58	6.60 ✓	5.76	2.07

		6.60 ✓		
22+50			4.6	2.0
23+0			4.9	1.7
+50			5.1	1.2
24+0			4.8	1.8
"	14' Lt of ℄ = NY Fill		3.8	2.8
"	17' " "		5.2	1.4
+50			4.5	2.1
25+0			4.6	2.0
+50			4.2	2.4
26+0			4.1	2.5
" "	8' Lt of ℄ = NY Fill		4.0	2.6
" "	16' " "		4.8	1.8
+34.88 POT			4.37	2.23 on Stub Nail Pole 1635+28+N
TP	4.12	6.80 ✓	3.92	2.68 ✓
+50			4.9	1.9
27+0			4.9	1.9
+50			4.8	2.0
28+0			4.8	2.0
+50			5.0	1.8
+75.00 A			5.10	1.70 on Stub
29+0			4.9	1.9
+50			5.1	1.7
30+0			4.9	1.9
+30			5.3	1.5
31+0			5.4	1.4

		6.80 ✓			
31+30			4.0	2.8	
+60			5.3	1.5	
32+0			5.2	1.6	
TP	4.32	6.85 ✓	4.27	2.53	
+50			4.7	2.2	
33+0			4.7	2.2	
+50			4.8	2.1	
34+0			4.6	2.3	
+50			4.6	2.3	
35+0			4.7	2.2	
+37.80	Δ		4.65	2.20	on Stub
+50			4.6	2.3	
36+0			4.5	2.8	
+50		✓	4.4	2.5	
TP	5.62	8.09	4.38	2.47	
37+0			5.3	2.8	
+50			5.1	3.0	
38+0			4.9	3.2	
+50			4.9	3.2	
39+0			5.4	2.9	
+50			5.2	2.9	
40+0			5.3	2.8	
+50		✓	5.2	2.9	
TP	5.41	7.70	3.80	4.29	
41+0			4.9	2.8	

		7.70 ✓			
41+50			4.7	3.0	
42+0			4.9	2.8	
+50			4.8	2.9	
43+0	Δ		4.74	2.96	on Stub
+50			4.7	3.0	
44+0			4.6	3.1	
+50			4.6	3.1 ✓	
TP	5.77	8.95 ✓	4.57	3.18	
45+0			5.7	3.3	
+50			5.5	3.5	
46+0			5.0	4.0	
+50			4.7	4.3	
47+0			4.7	4.3	
+25			4.3	4.7	
+56.65 P.O.T.			2.61	6.32	on Stub
+70			4.6	4.7	
48+0			5.2	5.8	
+20			5.5	5.5	
+45			4.4	4.6	
TP	5.32	10.39 ✓	2.78	5.17	
+50			5.6	4.8	
49+0			5.9	4.5	
+50			5.7	4.7	
50+0			5.9	4.5	
+29.88 BC Rt			5.8	4.6	

		10.39 ✓			
50+50			5.5	4.9	
51+0	= Nly Garden Plot		5.8	4.6	
+30			5.4	5.0	
+35			6.5	3.9	
+50			6.3	4.1	
+87			6.2	4.2	
+92			7.3	3.1	
52+0			7.2	3.2	
+50		✓	7.8	2.6	
TP	11.37	14.33	7.43	2.96	
53+0			11.3	3.0	
+50			11.0	3.3	
+66.96	E.C.		10.85	3.48	0.05 Stub
54+0			10.7	3.6	
+50	= Toe Slope		10.2	4.1	
+60			6.9	7.8	
+71		✓	0.8	13.5	
TP	5.23	18.93	0.63	13.70	
+96			4.8	14.1	
55+02			1.5	17.4	
+05	: Sly Pac. Pacific		1.80	17.1	
+40.9	Approx Pacific Conc.		1.76	17.17	
"	Top 2' Conc. Island		1.28	17.65	
+66	= Nly Pac. Pacific		2.80	16.63	
+72			2.7	16.2	

		18.93 ✓			
55+80			5.8	13.1	
+94			6.5	12.4	
56+14	= Toe Slope		12.1	5.8	
+50			12.5	5.4	
57+0			13.4	5.5	
+41.77	85 Lt.		15.9	3.0	
+78			15.55	3.4	
+93			9.5	9.4	
+95	Top Conc. Storm Drain		10.51	8.42	
58+0			11.8	7.1	
+49			13.9	5.0	
+70			13.4	5.5	
+79			10.8	8.1	
+32			10.3	8.6	
+50			7.8	11.1	
+76	Top Rail Santa Fe		5.30	13.63	
+80			6.1	12.8	
+89			7.8	11.1	
59+0		✓	13.3	5.6	
TP	1.51	13.03	7.41	11.52	
+10			9.6	3.8	
+25			9.4	3.6	
+30			7.4	5.6	
+50			7.1	5.9	
60+0			7.3	5.7	

		13.03 ✓			
60+38.44	E.C.		7.55	5.88	on Stub
+50			6.6	6.8	
61+0			6.7	6.3	
" "	18' Rt = Toe Fill Slope		6.2	6.8	
+50	4' Rt of ℄ = W½ Pow Pole		6.9	6.1	
62+0			7.2	5.8	
" "	3' Rt = Toe Fill Slope		7.0	6.0	
+50			7.4	5.6	
+75	116' Lt of ℄ SPK Car U.S. Gov. Bldg				
+97	116' Lt Car of ℄ Same Bldg				
63+0			8.0	5.0	
" "	3' Rt = Toe Fill Slope		7.5	5.5	
+30			5.9	7.1	
+60		✓	7.0	6.0.	
TP	4.56	11.55	6.04	6.99	
64+0			5.7	5.9	
" "	5 Rt = Toe Fill Slope		5.5	6.1	
+13	4' Rt = W ℄ Pow Pole				
+50			5.5	6.1	
65+0			5.4	6.2	
+50			5.3	6.3	
66+0			5.1	6.5	
" "	6 Rt = Toe Fill Slope		5.1	6.5	
+09.20	A		5.26	6.29	on Stub
+44			5.0	6.6	

	11.55 ✓			
66+66 on Ext Ramp		5.2		8.8
+75		4.3		7.3
67+0		4.7		6.9
" " 12' Rt = Toe Fill Slope		4.5		7.1
+50		4.8		6.8
+70 1' Lt SPK Bldg. to be moved				
68+0		4.9		6.7
" " 14' Rt = Toe Fill Slope		4.6		7.0
+50	✓	5.5		6.1
TP 7.78	15.09	4.24		7.31
69+0		10.2		4.9
" " 12' Rt = Toe Fill Slope		9.6		5.5
+40		10.0		5.1
+54.85		7.7		7.8
69+89 12' Rt = Outlet 24" Conc. Storm Drain Flow Line		8.52		6.57
70+0		7.2		7.9
+50		7.4		7.7
71+0		7.5		7.6
" " 7.5 Rt = Toe Fill Slope		7.6		7.6
+50		7.7		7.4
72+0 = Toe Fill Slope		7.0		8.1
+50		5.6		9.5
73+0 on Fill		2.9		12.2
" " 7 Lt = Toe Fill Slope		6.8		8.3
TP 8.43	22.26 ✓	1.26		13.83

		22.26		
78+50	on Fill	9.0	13.3	
79+0	" "	7.6	15.7	
" "	7' Lt = Top Fill Slope 12.6 = 5 Ft Dyke			
" "	4.5 Rt = Shoulder	5.3	17.0	
+50		7.1	15.2	Notes Revised 6/17/93
"	3' Lt = Top Slope	8.1	19.2	
+87	= Dyke & Shoulder	4.5	17.8	
79+0		3.8	18.5	
+50		3.2	19.1	
79+56	= Edge Paving on Morena Blvd.	3.26	19.00	
+88.39		2.8	19.5	
BM		2.16	20.10	SW BP Taylor & Bridge 26.07

Levels Top Conc Pipe & Valve
Taylor & Morena Blvd
Sketch Page 38

July 16-93
Sisson Blvd
Bridge

39

BM	4.28	24.35 Alt.	20.07	SW BP Taylor & Bridge
Top Conc Pipe		10.08	14.27	
Top Valve Stem		9.74	14.61	

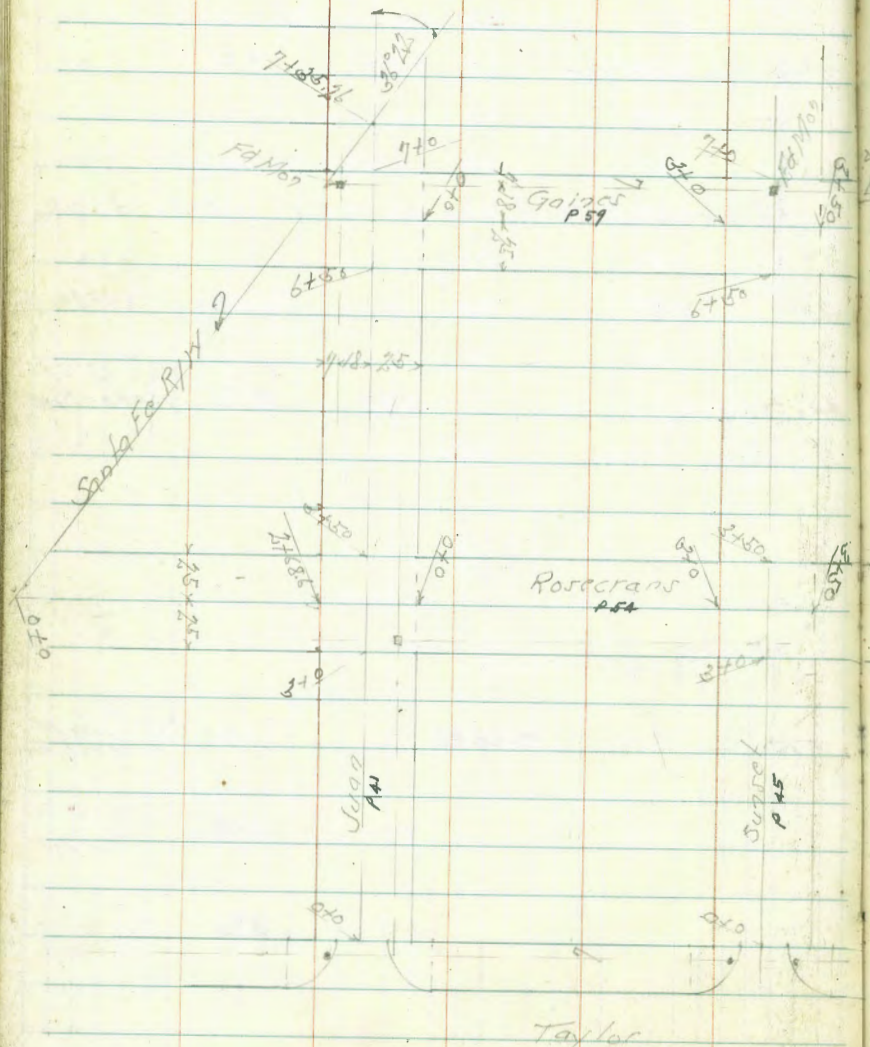
Existing 12" Cast Iron Water Pipe 64+20.73

BM	4.41	10.70	6.29	on Stub 64+82.0
64+20.73		5.97	4.73	Top 12" CI Water Pipe

Levels Top 18" CI Pipe & Valve
Midway West Point Loma Blvd & Frontier St
Sketch page 39

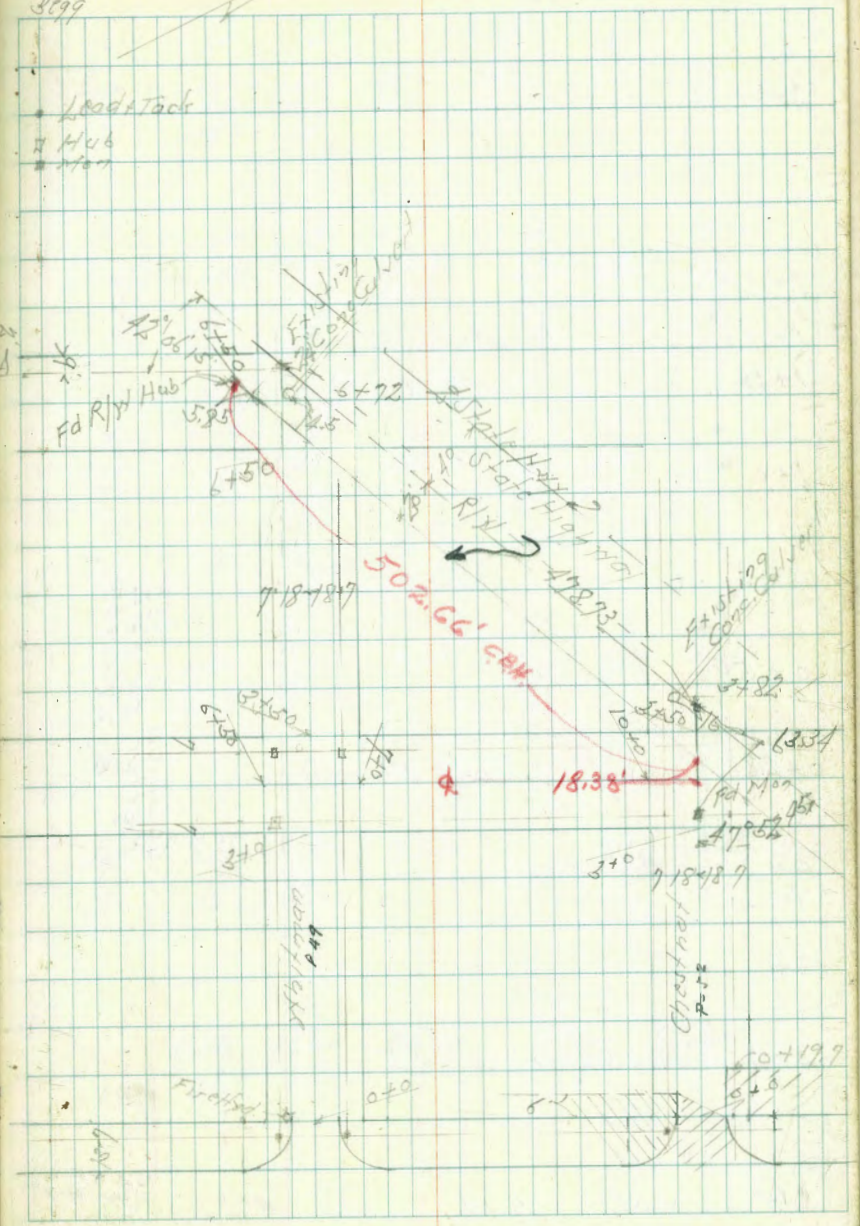
BM	7.78	10.68 Alt.	3.90	SW BP Top Curb Midway N of W Pt Loma
		7+50	3.18	Top 18" CI Pipe in Midway
		6+78	3.90	Top Valve Stem

Cross Section Juan St. Sunset - Whitman
Chestnut - Rosecrans - Gaines



Aug. 23. 43
Sisson Walker
Bliss Hazard
Begg

40



Cross Section of Juanita
Taylor to Gaines

Indexed
C.S.K.

2+00					
1+50					
1+48	17' Lt of Σ - Sly Pole				
1+40	21' Rt of Σ - Nly Power Pole				
1+00					
0+50					
0+28	18' Rt of Σ Nly Pole				
0+00	= W.L. Taylor				
0+20	= W. C & L. Co Taylor				
BM	5.02	9.74		4.72	SET BP Taylor & Juan

Reduced By AEB
Plotted By GBH
8-27-1943

Lt of Σ

RH-N 41

5.7 / 4.0 / 25	5.5 / 4.2 / 15	4.3 / 5.1 / 14	4.7 / 5.0	4.4 / 5.3 / 15	4.2 / 5.0 / 17	4.8 / 4.9 / 26
5.2 / 4.0 / 25	5.4 / 4.2 / 15	4.2 / 5.5 / 14	4.4 / 5.3	3.5 / 5.8 / 15	4.4 / 5.3 / 16	4.5 / 5.3 / 26
5.7 / 4.0 / 24	5.6 / 4.2 / 15	3.9 / 4.5 / 13	4.3 / 5.4	3.9 / 5.8 / 15	4.3 / 5.1 / 15	4.3 / 5.1 / 26
5.4 / 4.3 / 25	5.1 / 4.4 / 15	3.9 / 5.0 / 14	4.3 / 5.1	4.6 / 5.3 / 15	5.6 / 4.7 / 16	4.9 / 3.7 / 26
5.0 / 4.1 / 25	4.93 / 4.90 / 15-CL	4.17 / 5.12 / 15-Slope	4.42 / 5.22		4.19 / 5.55 / 15 Slope	4.28 / 4.94 / 15-26	5.16 / 5.12 / 26
		3.958 / 5.02 / 15	3.59 / 5.75 / 15	4.12 / 5.42	4.16 / 5.58 / 15	4.17 / 5.52 / 26

Swan St.

4+88 24' Rt of ℄ - ℄ 18" Peppercress ✓

4+68 22.5 Rt of ℄ - ℄ 24" Peppercress ✓

4+50

4+0

3+50 = ℄ Rosecrans

3+25 = ℄ Rosecrans

3+0 = ℄ Rosecrans

2+98 17' Rt of ℄ - St. Power Pole ✓

2+50

9.74

42

9.74

Swan St.

7+00 = 3/4 Gainer

6+75 = 3/4 Gainer 18.44 of 7 = 5½ Power Pole

TP	7.41	12.65	4.53	5.21

6+50 = EL Gainer

6+0

5+50

5+0 16.44 of 7 = 5½ Power Pole

9.74

41 7 pt. 43

5.3	5.4	4.9						4.4	4.8		
7.4	7.9	7.8						8.3	7.9		
2.5	1.5							1.5	2.5		
4.5	5.0	5.7	4.9	5.0	5.1						
7.0	7.7	7.3	7.8	7.7	7.6						
2.5	1.5		1.5	1.5	2.5						
		12.55									
5.1	5.1	5.1	4.7	5.2	5.0	5.4					
4.6	4.6	4.6	5.0	4.5	4.7	4.9					
2.5	1.5	1.5		1.5	2.2	2.5					
4.9	5.1	5.0	4.8	5.4		5.3	5.1	5.4	5.1		
4.9	4.6	4.7	4.9	4.3		4.4	4.6	4.3	4.2		
5.0	2.5	1.5	1.3			1.5	2.0	2.1	2.5		
5.1	5.1	5.3	4.9	5.1		4.5	4.6	5.4	5.5		
4.9	4.6	4.9	4.8	4.6		4.8	4.7	4.3	4.3		
5.0	2.5	1.5	1.3			1.5	1.9	2.0	2.5		
5.0	4.8	5.0	4.1	4.9		4.5	4.3	4.2	4.7		
4.9	4.9	4.7	5.1	4.8		5.3	5.3	5.3	5.3		
	5.0	1.5	1.3			1.5	1.5	1.9	2.5		

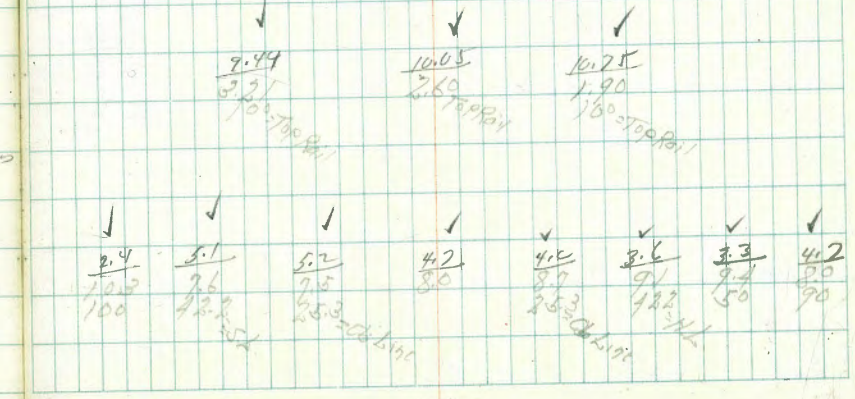
9.74

8+04 = East Rail of Santa Fe RR on Diag

BM 7.88 4.77 SE Corner Juan St Gainer

7+85.21 = Ely RR R/W Taken on Diagonal

1265



1265

Cross Section Sunset St.
Taylor to Gaines

Indexed C.S.R.

2+34	17.5' Rt of ℄ - Hly Tel Pole			✓
2+20	24 Lt of ℄ = ℄ 24" C'tonwood Tree			✓
2+0				
1+50				
1+28	19' Lt of ℄ - Sly Power Pole			
1+0	17' Rt of ℄ - Hly Tel Pole			✓
0+50				
0+185	163 Rt of ℄ = Hly Tel Pole			✓
0+0	W.L. Taylor			
0-20	WC6 Line Taylor			
BM	5.62	10.34	4.72	S.E.B.P. Taylor & Juan

Reduced by AEB
Plotted by CBH

Lt=S ℄ Rt=N 45

✓ 5.3 / 5.0 / 25	✓ 5.3 / 5.0 / 15	✓ 5.4 / 4.7	✓ 5.4 / 4.9 / 15	✓ 5.4 / 4.6 / 25
✓ 5.5 / 4.8 / 25	✓ 5.4 / 5.2 / 15	✓ 5.6 / 4.7	✓ 5.2 / 5.1 / 15	✓ 5.1 / 4.4 / 25
✓ 5.6 / 4.7 / 25	✓ 5.5 / 4.8 / 15	✓ 5.7 / 4.6	✓ 5.5 / 4.8 / 14	✓ 5.2 / 4.6 / 15	✓ 5.0 / 4.6 / 25
✓ 5.6 / 4.7 / 25	✓ 5.4 / 4.9 / 13	✓ 5.7 / 4.6	✓ 5.3 / 5.0 / 16	✓ 5.2 / 4.6 / 15	✓ 5.4 / 4.7 / 25
✓ 5.8 / 4.5 / 30	✓ 5.8.3 / 4.5 / 15-C6	✓ 5.2.9 / 5.0.5 / 15-Sunset	✓ 5.4.6 / 4.8.8	✓ 5.1.9 / 5.1.5 / 15-Sunset	✓ 5.8.6 / 4.4.8 / 15-C6	✓ 5.9 / 4.4 / 25
✓ 5.0.6 / 5.3.8 / 25	✓ 5.0.2 / 5.3.7 / 16	✓ 5.1.3 / 5.2.1	✓ 5.1.5 / 5.1.9 / 14	✓ 5.2.0 / 5.1.4 / 25

10.34

Sunset

4+275 = ℄ 15' Paving Strip on Lt ✓

4+0

3+50 = W.L. Rosecrans

3+25 = ℄ Rosecrans

TP 6.15 10.92 5.57 4.77 52.7 Hwy Rosecrans ℄ Sunset

3+0 = E.L. Rosecrans

2+70 25' Lt of ℄ = ℄ 30" Cottonwood tree ✓

2+50

10.84

Lt ℄ Rt 46

5.74 / 5.8 / 25
5.25 / 5.7 / 25
5.1 / 5.4
5.5 / 5.4 / 15
5.8 / 5.0 / 25

✓ 6.2 / 5.7 / 25
✓ 6.3 / 4.6 / 15
✓ 5.4 / 5.5 / 13
✓ 5.3 / 5.9
✓ 5.3 / 5.6 / 15
✓ 5.6 / 5.3 / 25

✓ 5.4 / 5.5 / 25
✓ 5.2 / 5.2 / 15
✓ 5.7 / 5.8
✓ 5.5 / 5.9 / 15
✓ 5.2 / 5.6 / 25

✓ 5.7 / 5.9 / 25
✓ 5.1 / 5.9 / 15
✓ 5.5 / 5.4
✓ 5.4 / 5.5 / 15
✓ 5.5 / 5.4 / 25

10.92

✓ 5.4 / 4.9 / 25
✓ 5.3 / 6.0 / 15
✓ 5.9 / 5.3 / 13
✓ 5.3 / 5.0
✓ 5.2 / 5.1 / 15
✓ 5.3 / 4.9 / 25

✓ 5.3 / 5.0 / 25
✓ 5.7 / 4.9 / 16
✓ 5.3 / 6.3 / 15
✓ 5.5 / 4.8
✓ 5.5 / 4.8 / 15
✓ 5.4 / 4.7 / 25

10.84

Sunset

RN 6.00 4.92 Sunset N. of Gaines

6+75 = L Gaines

6+50 = FL Gaines

6+0

5+50

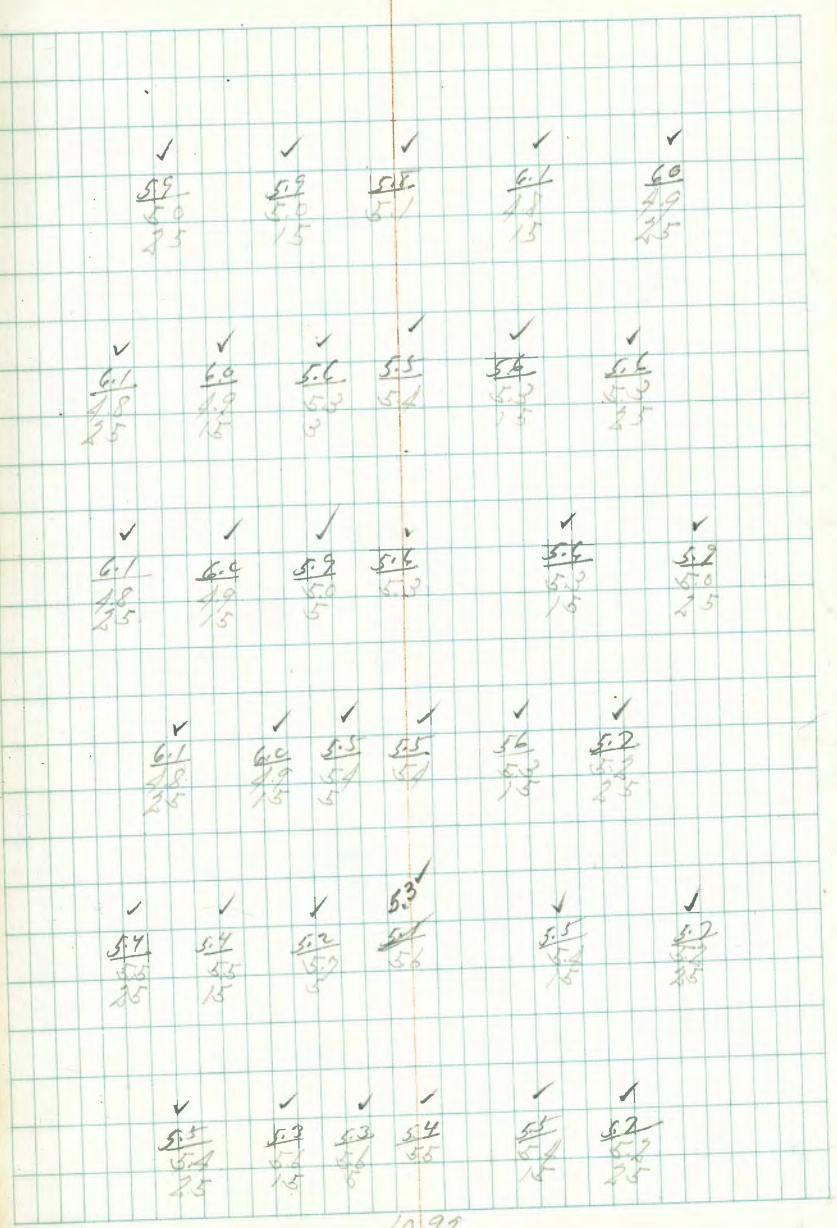
5+17 2456' N of L = Sly Power Pole

5+0

4+50 24' N of L = Sly Power Pole

1092

L R



10+92

Sunset

8+85

8+50

8+0

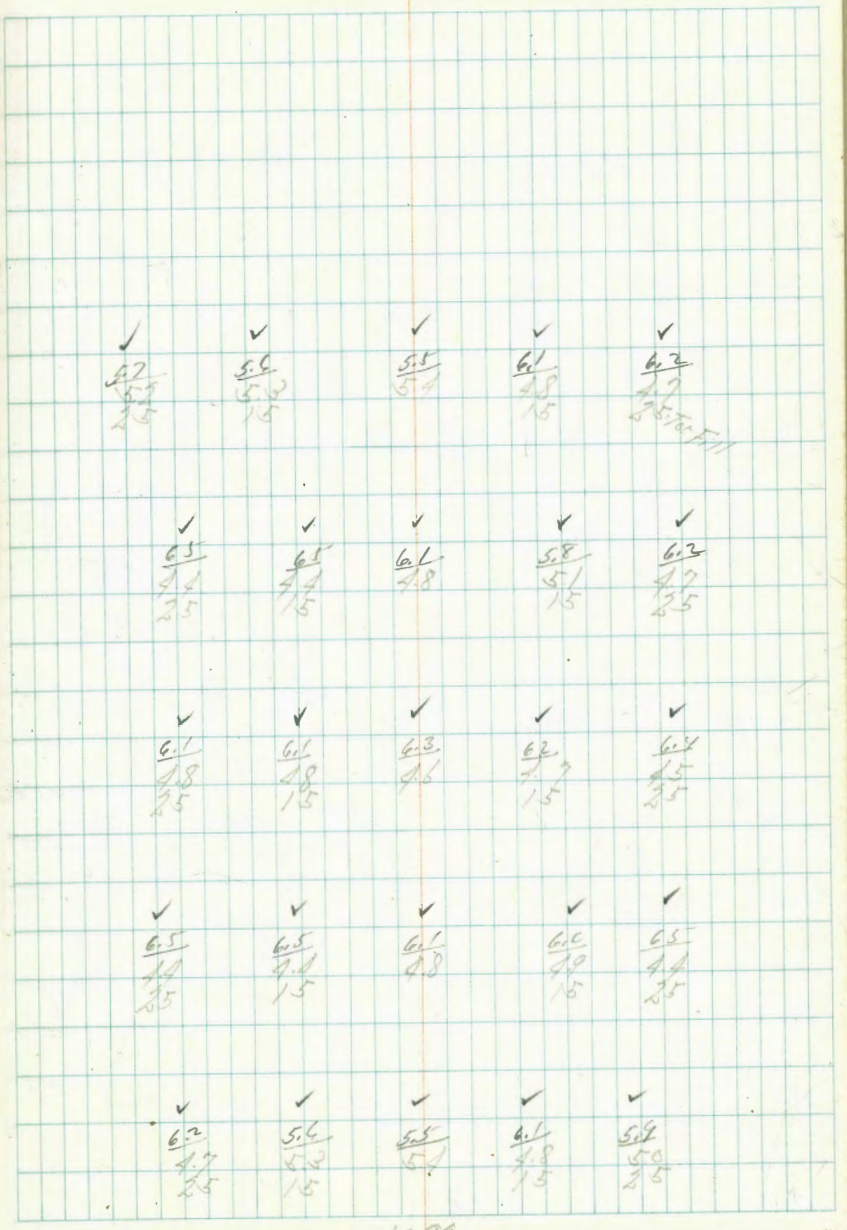
7+50

7+01 25 Lt o/ Z = Sl/ Pow Pole ✓

7+0 = H.L. Gaines.

10.92

LT RT 48



Cross Section. Whitman
Taylor to Gaines

Indexed
C.S.I.R.

1+01	16'Lt of ℄ = Sly Pow Pole				
1+0					
0+50					
0+04	16.9 Lt of ℄ = Sly Tel Pole				
0+0	= W.L. Taylor				
0-20	= W Cb Taylor				
BM			1.94	9.09	SW Top Flgd Tail of + Whitman 8.83
TP	8.66	11.03	6.34	7.37	
BM			5.96	7.75	SW Lgt Taylor + Gaines
TP	4.07	13.71	12.61	9.64	
BM	2.18	22.25		20.07	SW. BP Taylor + S.D. River Bridge

Red. By AE3
Plot. By GBH.

Aug 24 43
45

49

62 4.8 25	62 4.8 15	64 4.6	66 4.4 15	67 4.3 25	
63 4.7 25	64 4.6 15	66 4.4	66 4.4 15	61 4.5 25	
62 4.8 25	620 4.83 15-Cb	6.48 4.84 15-Gulf	6.43 4.60	620 4.83 15-Gulf	681 4.82 15-Cb	6.7 4.8 25
	603 5.01 25	600 5.03 15	604 4.99	614 4.89 15	617 4.81 25

11.03

Whitman

TP	4.25	11.18	4.10	6.93
3+56		18' Lt of ℄ = My Power Pole		
3+55	= W.L. Rosecrans			
3+25	= ℄ Rosecrans			
3+0	= E.L. Rosecrans			
2+60		19.5' Lt of ℄ = ℄ 18" Cottonwood Tree		
2+50				
2+49		19' Lt of ℄ = Sky Power Pole		
2+0		18' Rt of ℄ = ℄ Cottonwood Tree		
1+79		19' Rt of ℄ = ℄ 24" Cottonwood		
1+50				

11.03

Lt. ℄ Rt. 50

63 / 4.7 / 25	63 / 4.8 / 15	63 / 4.6	63 / 4.5 / 15	63 / 4.3 / 25
64 / 4.7 / 25	64 / 4.9 / 15	64 / 4.1	64 / 4.2 / 15	64 / 4.3 / 25
65 / 4.5 / 25	65 / 4.5 / 15	65 / 4.1	65 / 4.5 / 25	65 / 4.4 / 25
67 / 4.3 / 25	67 / 4.3 / 15	67 / 4.1	67 / 4.5 / 25	67 / 4.4 / 25
67 / 4.3 / 25	65 / 4.5 / 15	66 / 4.1	67 / 4.8 / 15	65 / 4.5 / 25
63 / 4.7 / 25	64 / 4.9 / 15	64 / 4.6	64 / 4.6 / 15	62 / 4.3 / 25
62 / 4.8 / 25	61 / 4.9 / 15	63 / 4.7	64 / 4.6 / 15	64 / 4.4 / 25

11.03

Whitman

6+72 = Opp Culv on State Hwy.

6+50 - E.L. Gaines

6+0 19.5 Lt. of ℄ = Sly Pow Pole ✓

5+50

5+0 18.4 Lt of ℄ = Sly Pow Pole ✓

4+50

4+0

118

Lt. ℄ Rt. 51

6.26 ✓
4.26
4.93
4.5 Flow Line Concrete

6.3 ✓ 6.3 ✓ 6.1 ✓ 6.5 ✓ 7.0 ✓
4.9 4.9 4.7 4.7 4.9
1.5 1.5 1.5 4.2 Toe Fill

6.9 ✓ 6.9 ✓ 6.7 ✓ 6.4 ✓ 6.2 ✓ 6.7 ✓
4.3 4.5 4.5 4.8 4.5 4.5
1.5 1.5 1.5 1.5 1.0 2.5

6.7 ✓ 6.7 ✓ 6.7 ✓ 6.5 ✓ 6.7 ✓
4.5 4.5 4.5 4.7 4.5
2.5 1.5 1.5 2.5

6.4 ✓ 6.4 ✓ 6.2 ✓ 6.5 ✓ 6.3 ✓ 6.6 ✓ 6.8 ✓
4.8 4.8 5.0 4.7 4.9 4.6 4.4
1.5 1.5 1.0 1.5 1.4 1.5 2.5

6.5 ✓ 6.8 ✓ 6.5 ✓ 6.9 ✓ 6.7 ✓
4.7 4.8 4.7 4.8 4.6
2.5 1.5 1.5 2.5

6.7 ✓ 6.5 ✓ 6.7 ✓ 6.5 ✓ 6.7 ✓
4.5 4.7 4.5 4.5 4.5
2.5 1.5 1.5 3.5

11.18

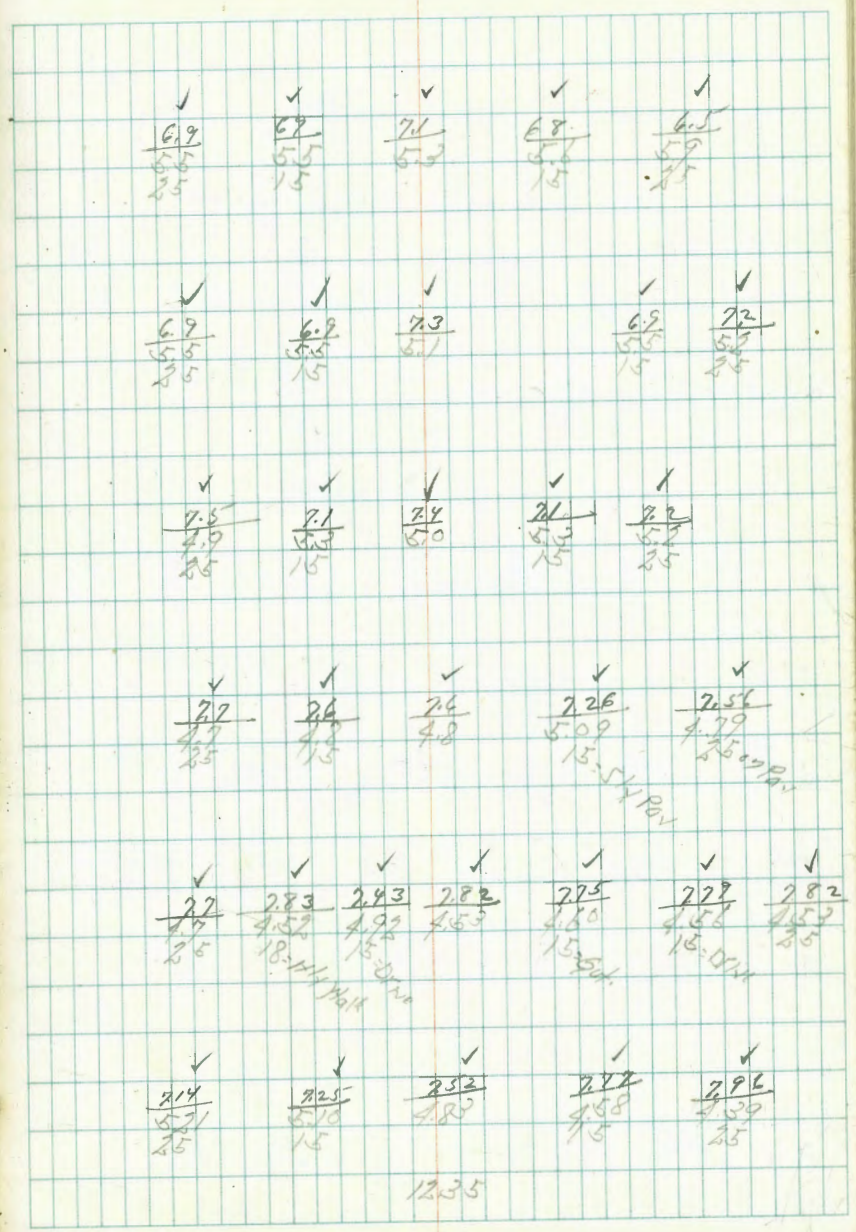
Cross Section - Chestnut St
Taylor - to Rosecrans

Indexed
C.S.K.

1+72	17' Rt of ℄ : NL Anchor Pole	✓
1+50		
1+19	18' Lt of ℄ : SL Power Pole	✓
1+15	18.7 Rt of ℄ = ± 12" Tree	✓
1+07	22' Rt of ℄ = ± 8" "	✓
1+0		✓ ✓
0+94	21.2 Rt of ℄ = ± 10" Tree 23.5' Rt = 12" Tree	
0+68	24.5' Rt of ℄ = ± 8" Tree	✓
0+56	21.0 Rt of ℄ = ± 8" Tree	✓
0+50		
0+30.5	18.3 Lt of ℄ = SL Tel Pole	✓
0+19.7	= WL Paving at Rt	✓
0+0	= NL Taylor	
0-20	= W CL Line Taylor	
BM	4.60	1235	7.75

Notes Reduced by FSB
Plotted by CBH 8-30-43

S.W. 7th & Taylor & Chestnut Page 49



Chestnut

3+82	Opp Culv. on State Hwy.			✓	
3+54	17.8 Lt of Z = W.L. Power Pole			✓	
3+50	W.L. Rascrans				
3+25	℄ Rascrans				
3+08.5	17 Rt of Z = W.L. Power Pole			✓	
3+0	E.L. Rascrans				
TP	4.83	12.03	5.15	7.20	Nail/Pole NE Rascrans & Chestnut
2+50					
2+0					
		12.35			

Lt. Z Rt 53

10.9 ✓

7.4 ✓ 6.7 ✓ 7.3 ✓ 7.5 ✓ 7.5 ✓

7.8 ✓ 7.3 ✓ 7.1 ✓ 7.1 ✓ 7.2 ✓ 7.8 ✓

6.8 ✓ 6.6 ✓ 7.1 ✓ 6.7 ✓ 7.3 ✓ 7.6 ✓

12.03

7.3 ✓ 8.3 ✓ 7.2 ✓ 7.0 ✓ 7.5 ✓

6.9 ✓ 8.2 ✓ 7.3 ✓ 7.6 ✓ 7.3 ✓

12.35

Cross Section Rosecrans
Santa Fe R/W to Chestnut

Indexed
C.S.K.

2+00

1+63.5 24.5 Rt of ℄ = ℄ 21" Palm Tree ✓

1+55 21.3 & 24.7 Rt of ℄ = ℄ 24" Palm ✓

1+50

1+27 17 Rt of ℄ = Ely Tel Pole ✓

1+18 17' Rt of ℄ = Ely Pow Pole ✓

1+0

0+50

0+30

0+0 = Santa Fe R/W Taken Diagonal

0-9 17.5 Rt of ℄ = Ely Power Pole ✓

BM 5.01 10.03 5.02

Reduced By MEB.
Plotted By CBH

Lt: W ℄ Rt: E 54

5.3 5.3 5.4 5.7 5.6 5.4
4.8 4.8 4.6 4.3 4.39 4.5
2.5 1.5 1.5 Rt 5.5 Rt 1.5

4.3 4.3 4.5 5.4 5.8
5.7 5.8 5.5 4.6 4.5
2.5 1.5 2.5

4.3 4.3 4.2 4.2 4.8 6.3
5.7 5.7 5.8 5.8 5.7 5.8
2.5 1.5 1.2 1.5 2.5

4.6 4.8 4.7 4.4 5.9 6.3
5.4 5.4 5.8 5.6 5.0 3.7
2.5 1.5 1.2 1.5 2.5

4.7 4.6 4.6 4.2 5.1 6.2 5.8.3
5.8 5.4 5.4 5.3 4.9 3.8 4.20
2.5 1.5 2.5 1.2 1.5 2.5 Rt 5.5 Rt 1.5 Left

4.4 2.7 4.2 2.4 4.4 4.8 5.4 5.8 5.7
2.0 7.3 8.3 0.6 5.6 5.2 4.5 4.3 4.3
8.0 5.0 5.5 2.0 1.0 1.5 3.2 5.0

10.03

On M.H. Rim
℄ Rosecrans
& Santa Fe
Page 42

Rosecrans

2+70				
1+82				
1+51	17' Rt of ℄ - Fly Power Pole ✓			
1+50				
1+34				
1+04	152 Rt of ℄ - Fly Tel Pole			
1+0				
TP	5.98	10.95	5.06	4.97
0+50	=50' No. of ℄ Jean			
2+68	16.8 Rt of ℄ - Fly Power Pole ✓			
2+50				
		10.03		

55

10.95

10.03

Rosecrans

4+50

4+0

2+98.5 175 Rt of ℄ - Ely Power Pole ✓

2+77

2+50

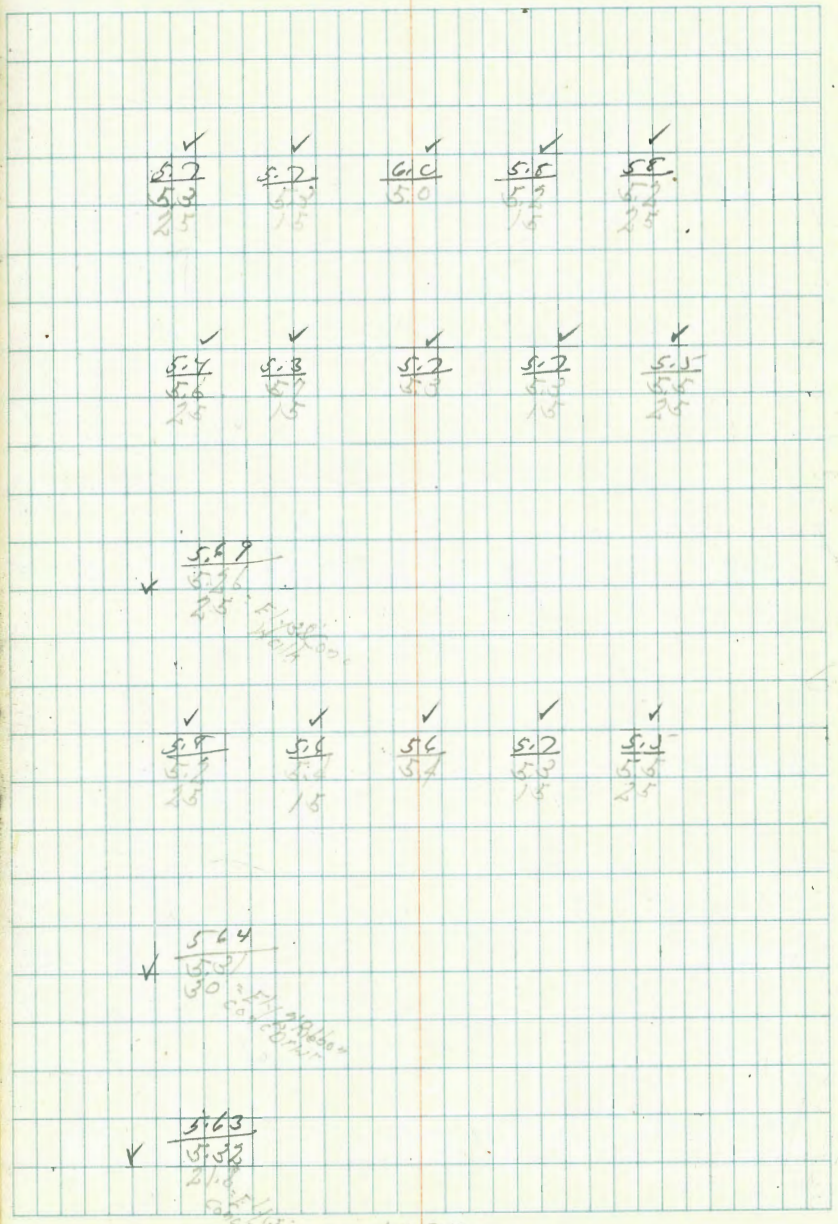
2+47 148 Rt of ℄ Ely Tel. Pole ✓

2+43 = ℄ 2-18" Conc Ribbon Drain

2+18

10.95

4. ℄ Rt 56



10.95

Rosecrans

7+50

6+70 17' Rt of ℄ = E℄ Power Pole ✓

6+70

5+50 238' Rt of ℄ = W℄ Tel℄ Power Pole ✓

5+42

5+45

5+0 17' Rt of ℄ = E℄ Pow Pole ✓ 239' Rt = W℄ Tel Pole ✓

1095

Lt ℄ Rt 57

2.0 / 1.0 / 25 ✓ — 6.8 / 4.1 / 15 ✓ — 7.0 / 4.0 ✓ — 7.2 / 5.0 / 15 ✓ — 8.0 / 4.0 / 25 ✓

6.6 / 4.5 / 25 ✓ — 6.4 / 4.1 / 15 ✓ — 7.0 / 4.0 ✓ — 6.8 / 4.5 / 15 ✓ — 6.7 / 4.3 / 25 ✓

6.7 / 4.6 / 25 ✓ — 6.3 / 4.5 / 15 ✓ — 6.2 / 4.3 ✓ — 6.7 / 4.3 / 15 ✓ — 6.5 / 4.5 / 25 ✓

6.45 / 4.50 ✓ 204' Rt 17' Conc

6.48 / 4.47 ✓ 235' Rt 17' Conc

6.1 / 4.9 / 25 ✓ — 6.1 / 4.9 / 15 ✓ — 6.4 / 4.6 ✓ — 6.2 / 4.8 / 15 ✓ — 6.2 / 4.8 / 25 ✓

1095

Rosecrans

BM		3.68	7.22	Nail & tag RE Rosecrans Exhibit 7.20
9+50				
9+0				
8+50	18" RCP to N - Ely Power Pole			✓
8+39				
8+21				
TP				
8+14	20.5 Lt of ℄ - Wk Tel. Pole			✓
8+0				

1095

47 2 Rt 58

7.4 / 3.6 / 25 ✓	7.4 / 3.6 / 15 ✓	7.6 / 3.4 ✓	7.3 / 3.7 / 15 ✓	7.3 / 3.7 / 25 ✓
7.2 / 3.8 / 25 ✓	7.2 / 3.8 / 15 ✓	7.3 / 3.7 ✓	7.1 / 3.9 / 15 ✓	7.4 / 3.6 / 25 ✓
7.2 / 3.8 / 25 ✓	7.2 / 3.8 / 15 ✓	7.2 / 3.8 ✓	7.0 / 4.0 / 15 ✓	7.0 / 4.0 / 25 ✓
				7.17 / 3.78 / 25 = Rt 37 Conc to Lt ✓
✓ 7.20 / 3.75 / 27.5 = Rt 37.5 Conc to Lt				
				7.17 / 3.78 / 25 = Rt 37 Conc to Lt ✓
7.3 / 3.7 / 25 ✓	7.2 / 3.8 / 15 ✓	7.1 / 3.9 ✓	7.2 / 3.8 / 15 ✓	7.0 / 4.0 / 25 ✓

1095

Cross Section Gainer St
Juan to Whitman.

Indexed
C.S.K.

2+50

2+00

1+50

1+00

0+50

0+47 47' Rt. & Juan ✓

BM 6.13 10.90 4.77 S.F.9. Mon Juan & Gainer Page 21

Reduced By AFB
Plotted By C.B.K.

5.0 / 4.9 / 4.5	5.5 / 5.1 / 4.5	5.2 / 5.3	6.2 / 5.7 / 4.5	6.1 / 5.8 / 4.5
5.8 / 5.7 / 4.5	5.6 / 5.3 / 4.5	5.2 / 6.2	6.0 / 5.9 / 4.5	6.0 / 5.9 / 4.5
5.9 / 5.9 / 4.5	5.7 / 5.3 / 4.5	5.5 / 5.4	5.6 / 5.3 / 4.5	5.2 / 5.3 / 4.5
5.9 / 5.9 / 4.5	5.2 / 5.3 / 4.5	5.5 / 5.4	6.0 / 5.9 / 4.5	5.7 / 5.3 / 4.5
5.1 / 5.3 / 4.5	5.2 / 5.3 / 4.5	5.3 / 5.6	5.2 / 5.3 / 4.5	5.8 / 5.1 / 4.5

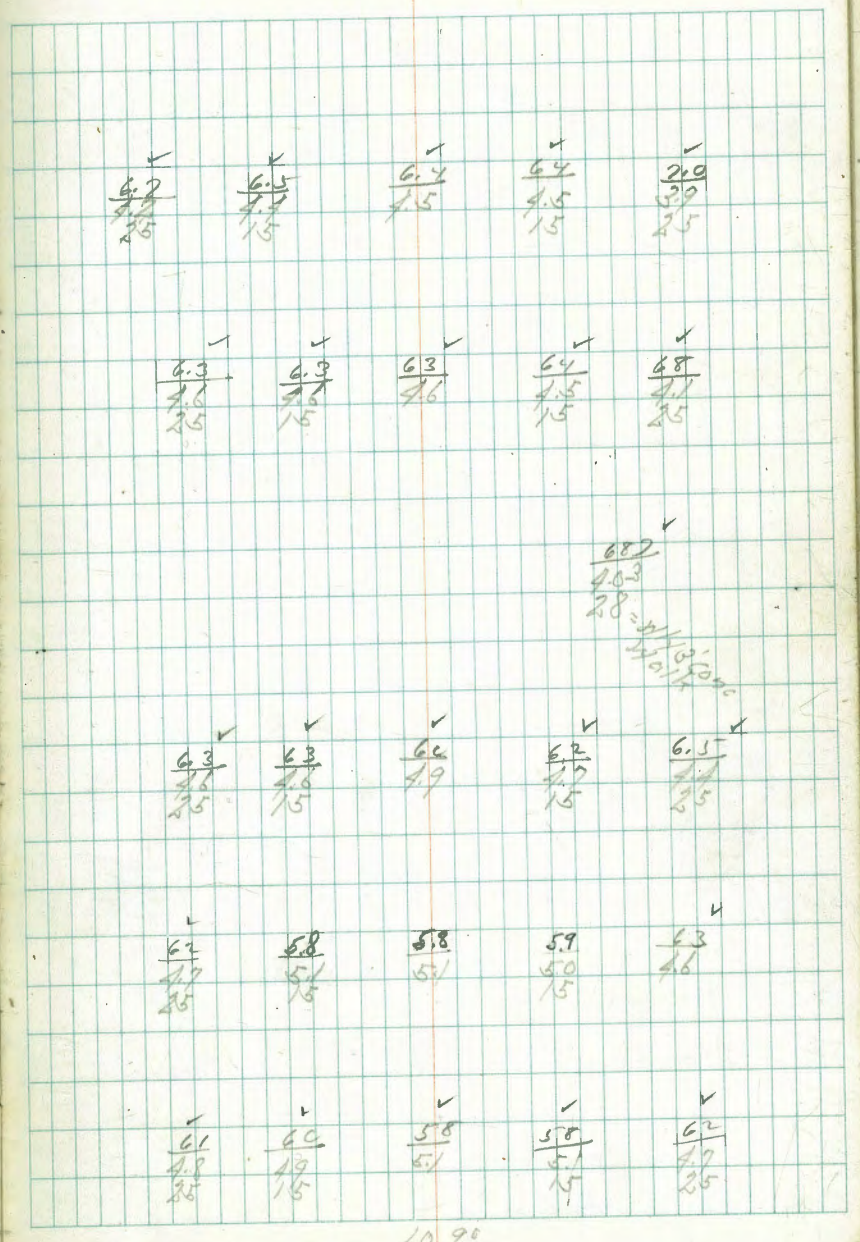
5.63 / 5.9 / 4.5

Rt. 5.4 x 10.90

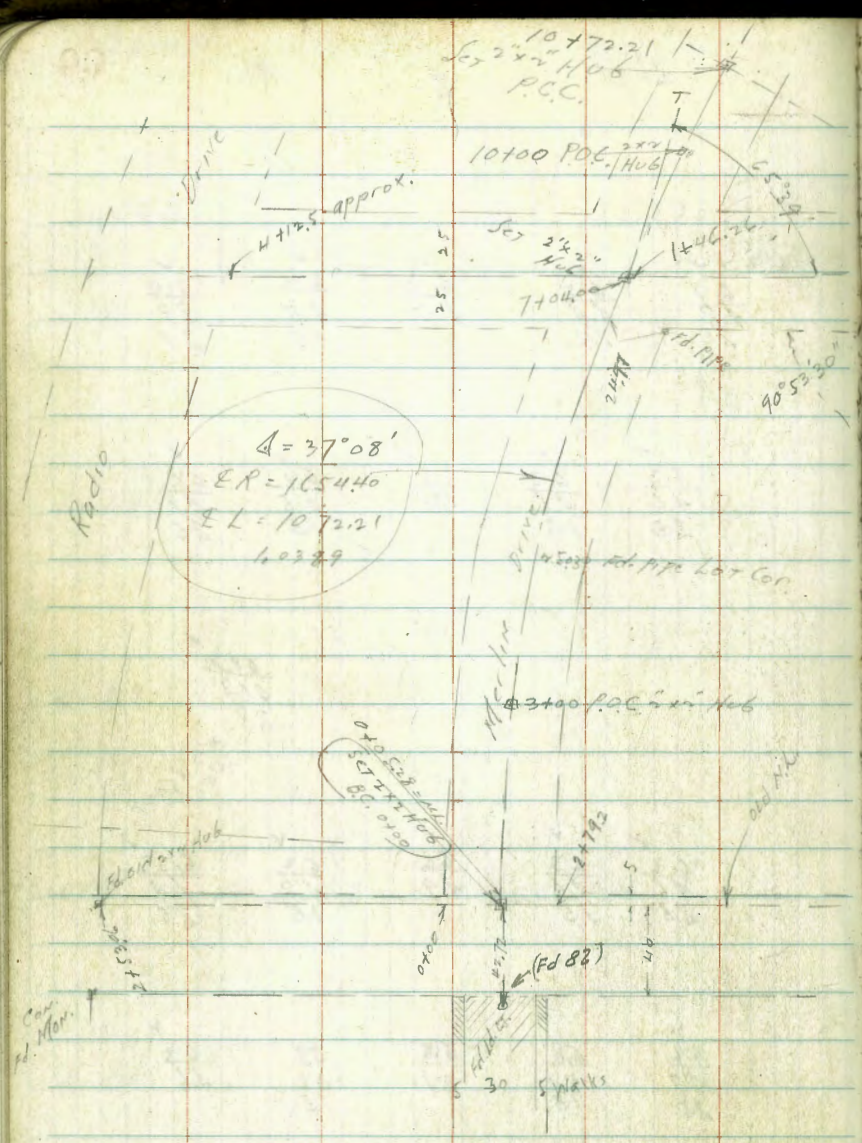
Gain 4

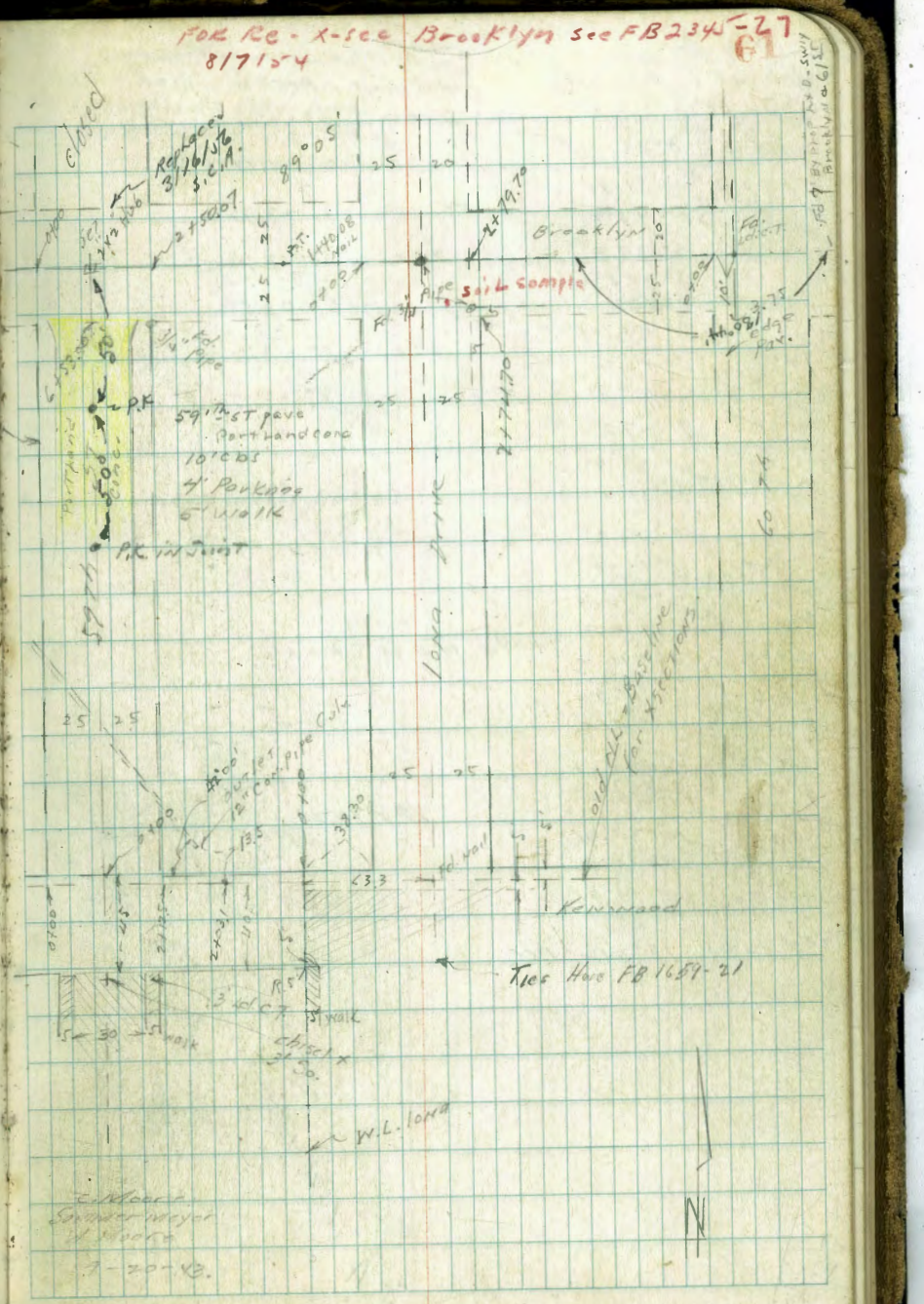
For Check		4.63	6.27	Flow Lines Colton 6472 Whitman Page 51
6+0				
5+50				
5+27				
5+0	18 Lt of ℄ : W/ Power Pole ✓			
4+55				
4+0				
	10.90			

Lt ℄ Rt 60



10.90


10+72.21
Sec 2"x2"x24" Hub
P.C.C.
10+00 P.O.C. 2"x2" Hub
drive
approx.
H+12.5
Sec 2"x2" Hub
1+46.26
7+04.00
25
Rd. Pipe
2"x24"
90°53'30"
Δ = 37°08'
ER = 1654.40
EL = 1072.21
L 0.2.89
Radio
Witness Rd. Pipe Lot Cor.
Witness Rd. Pipe Lot Cor.
Mon. Line
0+34.00 P.O.C. 2"x24" Hub
Sec 2"x2"x24" Hub
B.C. 0+00.0
Edge of Road
Old Mon.
2+39.2
2+79.3
0+00
(Fd 82)
Cor. Rd. Mon.
5
30
5 walks
Xsec of 59th Kenwood to Brooklyn
" Brooklyn 60th to Radio
" Kenwood " " "
" Medina Kenwood " 60th


FOR RE-X-SEC Brooklyn see FB 234-27
8/7/54
61
Closed
Replaced 3/26/54 S.C.I.A.
89°05'
2+50.7
Brooklyn
Fd. Iron Pipe
Rail Road Spike
Fd. Nail
soil sample
59th St pave
Portland conc
10 cbs
4' Parking
6' walk
P.I.
P.C.
P.T.
Radius 500.00'
Tangent 59.71'
Ext. 3.46'
Mid. Ord. 3.37'
Chord 119.22'
Delta 13°40'
Iowa Drive
Old CL = Base line for sections
Kenwood
Ties Here FB 1684-21
Fd. Wall
Curb
Gutter
W.L. Iowa
C. Moore
Sewer Insp.
1-20-54.

1 St Curve
dc per foot = 1.039°

0+00 BC	
0+05.8	0° 05.4
+50	0° 51.95
1	1° 42.9
+50	2° 35.8
2	3° 27.8
+50	4° 19.7
3	5° 11.67 POC
+50	6° 03.6
4	6° 55.6
+50	7° 47.5
5	8° 39.5
+50	9° 31.4
6	10° 23.3
+50	11° 15.3
7	12° 07.23
+03	12° 10.3
+05	12° 12.4
+50	13° 59.2
8	13° 51.1
+50	14° 43.1
9	15° 35.0
+50	16° 26.96
10	17° 18.9
+50	18° 10.9
10+72.21	18° 34.0 PCC

2nd Curve

10+72.21 = PCC	
11+00	0° 44.35
+50	2° 04.14
12	3° 23.93
+50	4° 43.72
13	6° 03.51
+50	7° 23.30
E.C. 13+93.99	8° 33.51

77° 50' 30" Set on B.C. 0°00
12° 11' 23"
C.S. 39' = 2 T. 7+04 Pt. to E Brookline

7+04.0 12° 11.28 E Brookline

Set 7+72 Hub

10+72.21 P.C.C.

Set 7+65.40 Hub

C/L R 165'

Cross Sections
Merlin Dr. from Iona
to 60th FB 1795-19-26

Edge Conc. Elev. = 18+14.08

5' Walk

Bk. Ld. St. & Back

Body

Set Hub C.T.

Elev. 13.7

Set Hub

Elev. 13.14

Set Hub

Elev. 13.30

Set Hub

Elev. 13.23

Set Hub

Elev. 13.36

Set Hub

Elev. 13.49

Set Hub

Elev. 13.62

Set Hub

Elev. 13.75

Set Hub

Elev. 13.88

Set Hub

Elev. 14.01

Set Hub

Elev. 14.14

Set Hub

Elev. 14.27

Set Hub

Elev. 14.40

Set Hub

Elev.

Indexed
C.S.K.

X Sec. Kenwood St. Iona to Radio Rd.

1+50				
1+00				
T.P.	5.75	209.36	3.33	203.61
0+75				
0+44				
0+25				
0+03				
0+0 W L Iona to So.				
0-5 W C6 Iona to S.				

Reduced to Profile Sept 1949

N.G. T# 1659 p. 3
please change
My T.S. yrs Sept

206.94
T.P. Hall in Hole 410 — 206.94 — 202.54 NW Iona & Kenwood

Lt

Baseline 63
old N.L.

Rt

1980 200.8 202.2 200.7 201.1 204.1
11.4 8.6 7.5 8.7 8.3 5.3
48 40 27 20 15 5

1997 1996 202.1 204.5 204.8
11.9 11.8 7.3 4.9 2.6
10 45 48 20 5

209.36

1969 200.60 202.3 204.3 207.4
10.0 6.34 4.6 2.6 1.5
45 44 40 20 5

end Top wall

1968 1968 200.2 200.7 202.1 202.7 204.3
10.1 10.1 6.7 6.7 4.8 4.2 2.6
47 47 40 35 20 5

NW Cor. of 47 House

beg Top Rock wall

1964 1964 1988 200.6 209.3
10.5 10.5 8.0 5.3 3.4
45 40 38 20 5

old CR

1962 1983 1989 200.5 200.7
10.7 8.6 8.0 6.2 6.2
40 35 20 6 5

1995.98 1996.18 1995.52 196.28 196.85 199.1 1995
10.96 10.76 10.38 10.66 10.11 7.8 7.6
40 35 27 20 5 5

Corr pav.

1995.91 1995.30 1995.52 196.20 196.71 199.8 198.4
10.97 11.64 11.42 10.78 10.73 9.1 8.5
40 40 35 20 5 5

94.7 pav. pav. edge

206.9x

Kenwood

0+40

0+00

0+00 on N to 20-5 on S diag sec.

W c6 sq'd to Se. of Kenwood

E sq'd

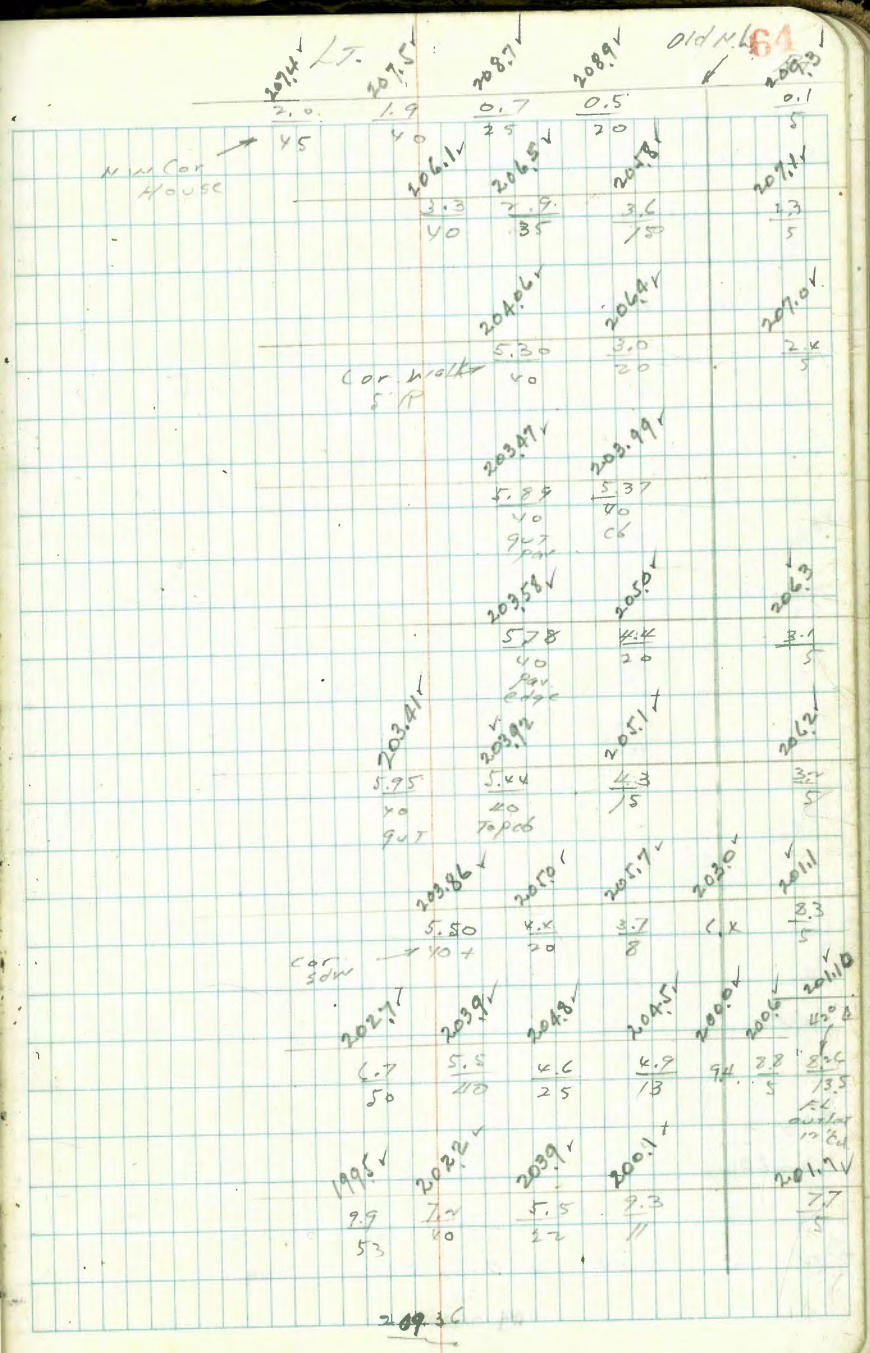
E c6 sq'd So. of Kenwood

2+10.5 on N to 2+17.5 on S Sec on diag = EL sq'd

2+03.1

1+80

209.36



Kenwood

1+84.0 E.L. Merlin to S

2+79.0 E.L. Merlin to N

2+40

2+00

1+65

1+35

1+00

0+80

T.P. 11.4 x 209.37 0.13 209.23

209.36

LT

Old N.L.

65

RT

209.95 / 10.1 / 40

215.7 / 6.7 / 20

217.5 / 2.8 / 5

Cart walk

214.8 / 5.6 / 40

215.9 / 2.5 / 20

217.6 / 2.8 / 5

214.5 / 5.9 / 40 / 42.5

214.5 / 5.9 / 40

215.2 / 5.2 / 20

215.9 / 5.0 / 5

To house

213.2 / 7.5 / 40

214.3 / 6.4 / 20

214.8 / 5.6 / 5

212.0 / 8.7 / 40

213.3 / 8.1 / 20

213.4 / 7.0 / 5

211.2 / 9.7 / 40

211.6 / 8.8 / 20

213.2 / 7.2 / 5

210.6 / 9.8 / 40

210.7 / 9.7 / 20

211.0 / 9.4 / 5

210.2 / 10.1 / 40

210.2 / 10.1 / 20

210.8 / 9.6 / 5

210.37

Kenwood

T.P.	0.11	x09.38	13.10	209.27
0+50				
0+10				
Set T.P. B.C. Hub	Kenwood Merlin	x.8 N	x17.55	For Xsec Merlin
Set B.M. C.T.	Lt. & Merlin and 3' So. of St.	Kenwood	11.13	209.24

0+00 W.L. Merlin to N.

W.L. Merlin to So.

W.C.B. Merlin to So.

& Merlin

E.C.B. Merlin to So.

x x 0.37

Lt.

old p.L. 66

2086 / 11.8 / 20

2091 / 11.3 / 20

2106 / 9.8 / 5

2124 / 7.8 / 40

2136 / 6.8 / 35

2150 / 5.4 / 20

2161 / 4.3 / 5

2112.5 / 7.9 / 40

2114.2 / 6.7 / 35

2125.7 / 4.7 / 20

2169 / 3.5 / 5

2110A / 9.33

2100.4 / 10.33 / 40

2113.5 / 6.9 / 35

2126.1 / 4.3 / 20

2179 / 3.K / 5

Topend to Rockwall

For sdw →

209.99 / 10.38 / 40 / Topcb

209.37 / 11.00 / 40 / Swt

2144 / 6.0 / 30

216.1 / 4.3 / 20

217.K / 3.0

209.49 / 10.88 / 40

2156 / 4.8 / 25

2167 / 3.7 / 15

2180 / 2.K / 5

209.37 / 11.00 / 40 / Swt

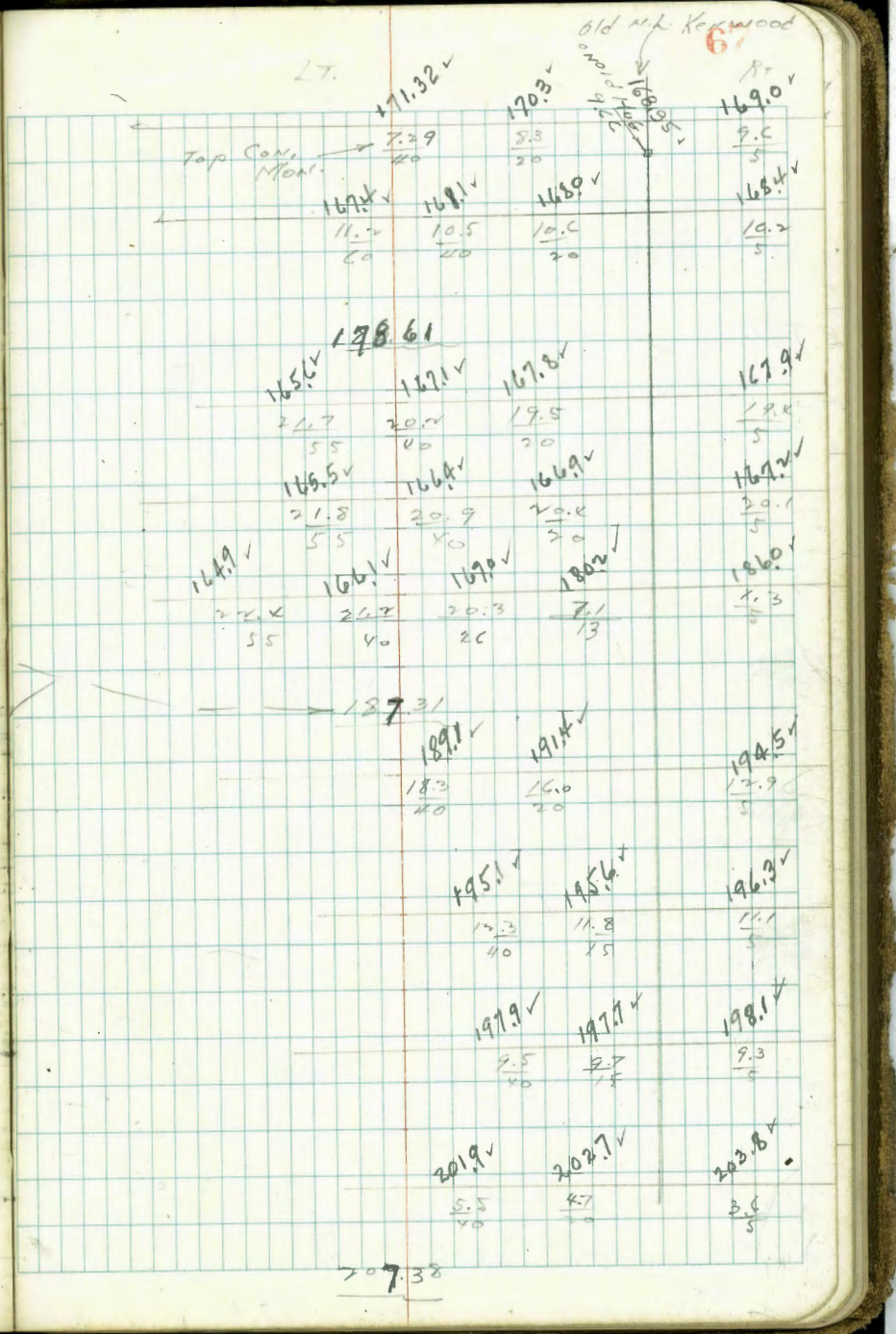
209.90 / 10.47 / CB / 40

x x 0.37

Kenwood

2+53.6	= old "x" Hub	E.L. Radio Drive		
2+40				
T.P.	3.79	178.61	12.49	1748
2+15				
2+08				
1+93				
T.P.	513	187.31	12.83	1824
T.P.	0.3	191.01	12.69	1946
1+76				
1+65				
1+50				
1+00				
		207.38		

Rock 100'N of 1+76.



Sec = Sketch Page 61 for width of Street — Indexed C.S.K.

Cross Sec. Brooklyn Court to Radio Drive

Reduced to Profile #2990 Sept 1943

1+40				
T.P.	12.79	255.95	0.39	243.16
1+00				
0+90				
0+50				
0+30				
0+0	W.L. Court St.			
0=6.25	Wedge Pav.			
T.P. Brooklyn	0.39	243.55	12.87	243.16
N.E. Long	1.68	256.03		254.35 Top Wall

1659/96

Lt — Old ℄ — Rt.

RT. 68

255.95 ✓

244.29 ✓ — 245.39 ✓

11.4 C. — 10.6 C.
2.8 — 2.8
Edge Wide Conc. dr. — dr.

236.7 ✓ — 237.1 ✓ — 238.3 ✓ — 239.1 ✓ — 239.7 ✓ — 240.4 ✓ — 241.4 ✓ — 243.6 ✓

6.9 — 6.5 — 5.3 — 4.5 — 3.9 — 3.4 — 2.2 — 0.0
25 — 20 — 9 — 12 — 15 — 25 — 26

241.8 / 20 Top Loose Cobble Wall

241.55 ✓
4.0 ℄ C. Conc. dr.
25.3

234.8 ✓ — 235.7 ✓ — 236.8 ✓ — 236.7 ✓ — 237.5 ✓ — 237.5 ✓ — 237.2 ✓ — 240.2 ✓ — 238.8 / 20

8.8 — 7.9 — 6.8 — 6.9 — 6.1 — 6.1 — 4.4 — 3.4
25 — 20 — 14 — 9 — 9 — 13 — 25

234.7 ✓ — 234.9 ✓ — 235.7 ✓ — 236.4 ✓ — 238.2 ✓ — 239.5 ✓ — 239.0 / 20

9.9 — 8.7 — 6.7 — 7.4 — 5.4 — 4.1
25 — 20 — 8 — 13 — 25

234.0 ✓ — 234.1 ✓ — 234.8 ✓ — 235.0 ✓ — 237.5 ✓ — 238.6 ✓ — 237.3 / 20

9.6 — 8.5 — 8.8 — 8.6 — 6.1 — 5.0
25 — 20 — 10 — 18 — 25

233.56 ✓ — 234.35 ✓ — 236.17 ✓ — 235.39 ✓

9.99 — 9.20 — 8.38 — 8.16
20 — 20 — 20 — 25

243.55 ✓

Fd. Blue Mark 2.6 N of Con. Wall

Brooklyn

255.95
1.60
254.35 = BM.

2+79.7 E.L. Iowa to N.

2+79.7 E.L. Iowa to S.

2+76.00

2+50

2+45.5

2+41

2+25

2+00

1+75

1+50

255.95

61d E.

LT

Rr 2.528/20

2.6 N. of Cor wall = BM. 1 blue chalk

251.1 4.3

251.9 4.4 1M

253.3 4.7 24.5

254.19 1.70 25 Top wall

250.4 5.6/20

250.7 5.3/10

251.3 4.7

247.9 8.1/25

248.2 7.8/20

248.9 7.1/14

248.7 7.3/12

248.9 7.1

249.0 7.0/C

250.0 6.0/17

2512/20 251.9 4.1/24

254.02 1.93 24.5 Top wall

241.4 8.6/25

247.6 8.4/20

248.3 7.7/15

248.2 7.8/12

248.4 7.6

248.4 7.6/C

249.7 6.3/20

251.5 4.5/24

254.18 1.77 24.5 Top Sky. wall

249.62 6.33/20

250.53 5.42/24

E. Cor. Sky. wall

245.2 10.8/25

245.4 10.6/20

246.3 9.7/13

246.0 10.0/12

246.4 9.6

246.5 9.5/C

247.9 8.1/17

249.5 6.5/25

2486/20

242.0 14.0/25

242.7 13.3/20

244.0 13.0/13

243.8 13.2/11

244.9 11.6

240.5 15.5/25

240.9 15.1/20

242.6 13.4/13

242.5 13.5/11

242.9 13.1

243.2 12.8/11

244.6 11.4/14

2445/21 245.5 10.5/21

247.4 7.9/25

239.0 17.0/25

239.5 16.5/20

240.9 15.1/14

240.7 15.3/11

241.3 14.7

241.6 14.4/7

2443/20 244.9 12.0/21.4 Hor. Con. wall

244.83 11.13/21.4 Top Cor. wall

246.52 9.43/25 Top wall

243.7/20

255.95

Brooklyn

1+50

1+38.7

1+15.5

1+05

1+00

0+75

0+50

0+44

T.P. 960 265.53 0.07 255.93

0+00 Now at Iona Dr.

255.95

Lt Rt

258.2 7.3 / 25

260.0 5.5 / 12

260.4 5.1

260.6 4.9 / 7

261.9 3.4 / 11

262.8 2.7 / 25

261.64 3' r. 166 on ℄ do. 2' wide R46. Dr. 3.89 / 8.1

262.42 3.1 / 25 on dr.

261.03 ℄ do. 2' r. 46, 7.1 Drive 3' r. 166 on 4.50

262.16 3.37 / 25 on dr.

257.44 7.1 3' wide. Can walk 2.9

258.1 7.1 / 25

259.1 6.4 / 12

259.4 6.1

260.0 5.5 / 8

261.0 6.5 / 10

261.8 3.7 / 25

257.21 8.3 / 25

257.77 ℄ 2' R166 on 6.6 wide do. R46.0n 7.7 / 17.6

255.2 10.3 / 35

256.8 9.7 / 25

257.4 8.1 / 11

257.8 7.7

257.8 7.7 / 8

259.0 6.5 / 10

259.6 5.9 / 19

260.7 4.8 / 25

260.46 5.07 23.8 2' r. 3' wide Can walk

265.53

253.4 2.15 / 25

254.4 1.6 / 8

254.7 1.8

254.8 1.2 / 8

255.8 0.7 / 11

255.9 0.1 / 17

259.0 ± 3.0 / 25

255.95

Brooklyn

0+50

0+07

0+0 New W.L 59-45

℄ 59-45 ST

2+50.07 New EL 59-45 ST

2+40

2+24.5

1+96.6

1+73

265.53

Lt ℄ Rt 71

253.4 12.1/25 254.5 11.0/12 255.2 10.3 255.5 10.0/9 256.4 9.1/10 257.5 8.0/25

258.95

6.58 ℄ 24" 3' wide Con. pipe

253.6 11.9/25 255.8 10.0/10 256.4 9.1 256.7 8.8/10 257.8 7.7/15 258.9 6.6/25

255.2 10.3/25 257.9 8.5/10 257.3 8.0 257.5 8.0/10 258.5 7.0/15 259.4 6.1/21 260.6 4.9/25

262.3 9.2/25 257.9 7.6/10 258.1 7.4 258.3 7.2/10 259.5 6.0/15 260.4 5.1/25

on 3" pipe Con.

260.9 4.58/25.5 ℄ 6.6 wide Con. Drive

257.73 7.80/25.

℄ 3' con. walk

258.12 7.41/24.7 259.6 5.9/12 259.8 5.7 260.9 5.5/10 260.9 4.6/14 261.5 4.0/25

℄ 6.6 double Drive 2 sidewalks

263.44 3.99/26.5 ℄ 3' Con. walk

265.53

Brooklyn

T.P	0.25	224.60	12.9	224.35
1+70				
T.P	0.63	247.27	12.80	246.59
1+35				
1+00				
0+75				
T.P	0.80	254.39	11.9	253.59
0+46.21				
0+00				

℄ Hub

Merlin ± Brooklyn

℄ Merlin Drive

245.53

L.T ℄ R.T

P12

235.8	234.6	233.5	232.7	231.2
6.5 / 25	7.7 / 12	8.8	9.6 / 12	11.1 / 25
245.3	244.5	243.7	243.2	242.6
9.1 / 25	9.9 / 12	10.7	11.2 / 12	11.8 / 25
250.9	250.9	250.5	250.2	249.8
3.5 / 25	3.5 / 12	3.9	4.2 / 12	4.6 / 25
252.4	252.8	252.6	252.5	252.3
2.0 / 25	1.6 / 12	1.8	1.9 / 12	2.1 / 25
254.39				
153.1	153.8	154.1	154.4	154.7
12.4 / 25	11.7 / 12	11.4	11.1 / 12	10.8 / 25
153.0	153.9	154.6	155.1	155.8
12.5 / 25	11.6 / 12	10.9	10.4 / 12	9.7 / 25
252.9	253.8	254.7	255.5	256.5
12.6 / 25	11.7 / 12	10.8	10.0 / 12	9.0 / 25

215.53

Brooklyn

check to T.P Rock	P.67		10.71	194.71	196.69 / 1.98 error
T.P.	3.06	201.54	4.90	206.36	
4+12.5 approx.		E.S. Radio			
T.P.	0.99	207.26	10.57	206.27	
4+00					
3+70					
T.P.	0.16	216.84	12.9	216.78	
3+35					
3+00					
		209.60			

27 4 JP7 73

201.2 ✓ 6.1 / 25
201.7 ✓ 5.6 / 1N
202.1 ✓ 5.2
201.7 ✓ 5.6 / 1N
201.5 ✓ 5.8 / 25

205.9 ✓ 10.9 / 25
205.3 ✓ 11.5 / 1N
204.4 ✓ 12.4
203.2 ✓ 13.6 / 1N
202.0 ✓ 14.8 / 25

211.4 ✓ 5.4 / 25
210.5 ✓ 6.3 / 1N
209.5 ✓ 7.3
208.9 ✓ 7.9 / 1N
208.3 ✓ 8.5 / 25

216.84 ✓
219.6 ✓ 10.0 / 25
218.1 ✓ 11.5 / 1N
216.7 ✓ 12.9
215.6 ✓ 14.0 / 1N
214.8 ✓ 14.8 / 25

229.1 ✓ 0.5 / 25
227.2 ✓ 2.4 / 1N
226.6 ✓ 4.0
224.2 ✓ 5.4 / 1N
223.9 ✓ 6.7 / 25

209.60 ✓

Proposed Storm Drain Along Santa Fe R.R.
Right of Way From Rosecrans to Rosecrans

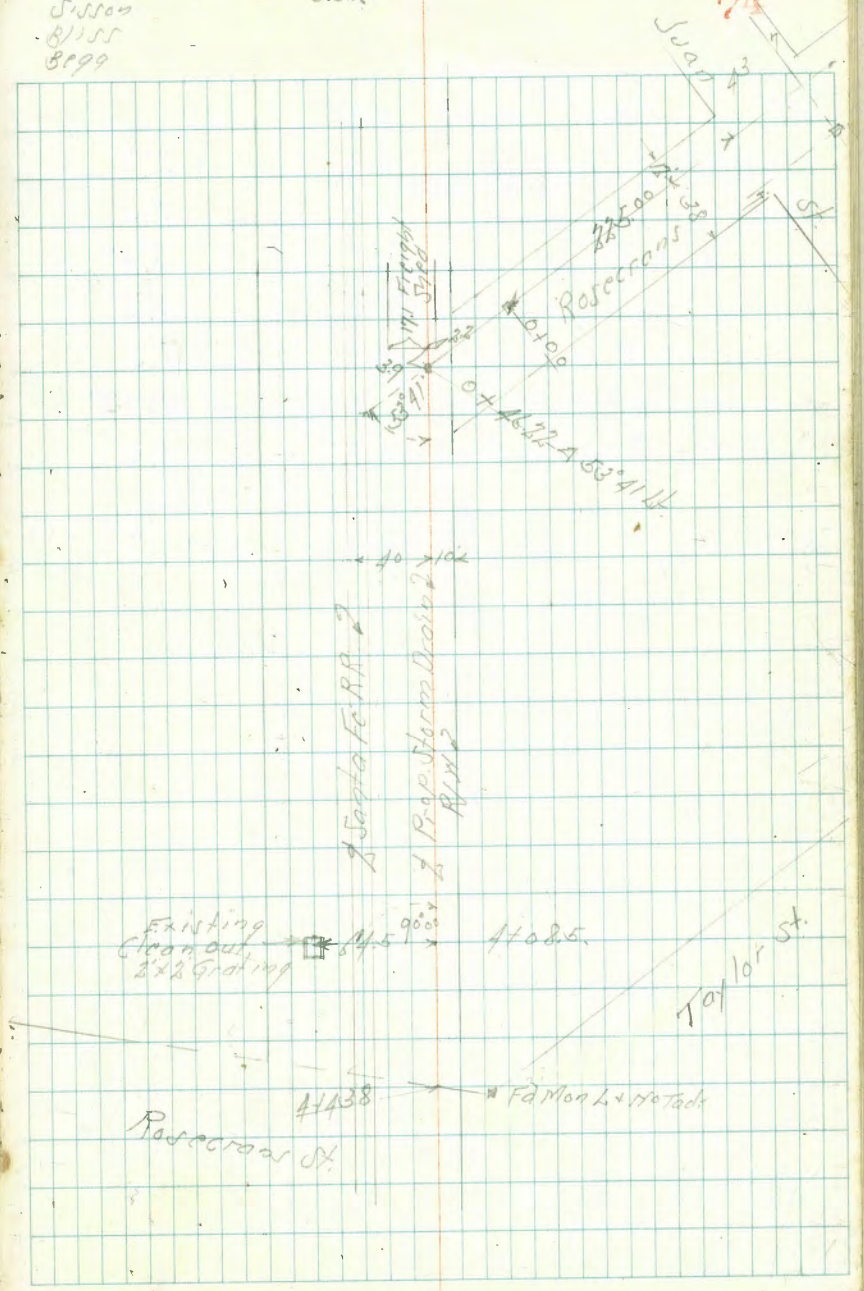
Oct 16-13
Sisson
Bliss
8099

Indexed
C.S.K.

74

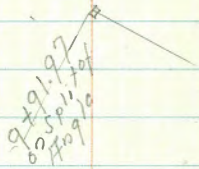
BM	5.50	10.12		4.62	SE BP 2 Curve San Diego & Rosecrans
TP	4.86	10.33	4.65	5.47	
0+0			5.5		4.8
+30			5.8		4.5
+35			7.3		3.0
+43			3.9		6.6
+46.22	Δ 53°41 Lt.		4.10		6.2 on Stab
+64			4.7		5.6
"	10' Rt		4.4		5.9
"	10 Lt.		5.1		5.2
1+0			4.6		5.7
"	10' Rt		4.6		5.7
"	8' Lt		4.6		5.7
	10' W = Wire Fence		3.9		6.4
+50.			4.5		5.8
2+0			4.6		5.7
"	10' Rt		4.6		5.7
"	7' Lt.		5.2		5.1
"	10' Lt.		4.0		6.3
+28	6.3 Lt of ℄ = 2.2 Tel Pole				
+50			4.8		5.5
3+0			5.0		5.3
"	10' Rt		5.0		5.3
"	7' Lt		5.7		4.6
"	10 Lt.		4.8		5.5

Plat + Sketch

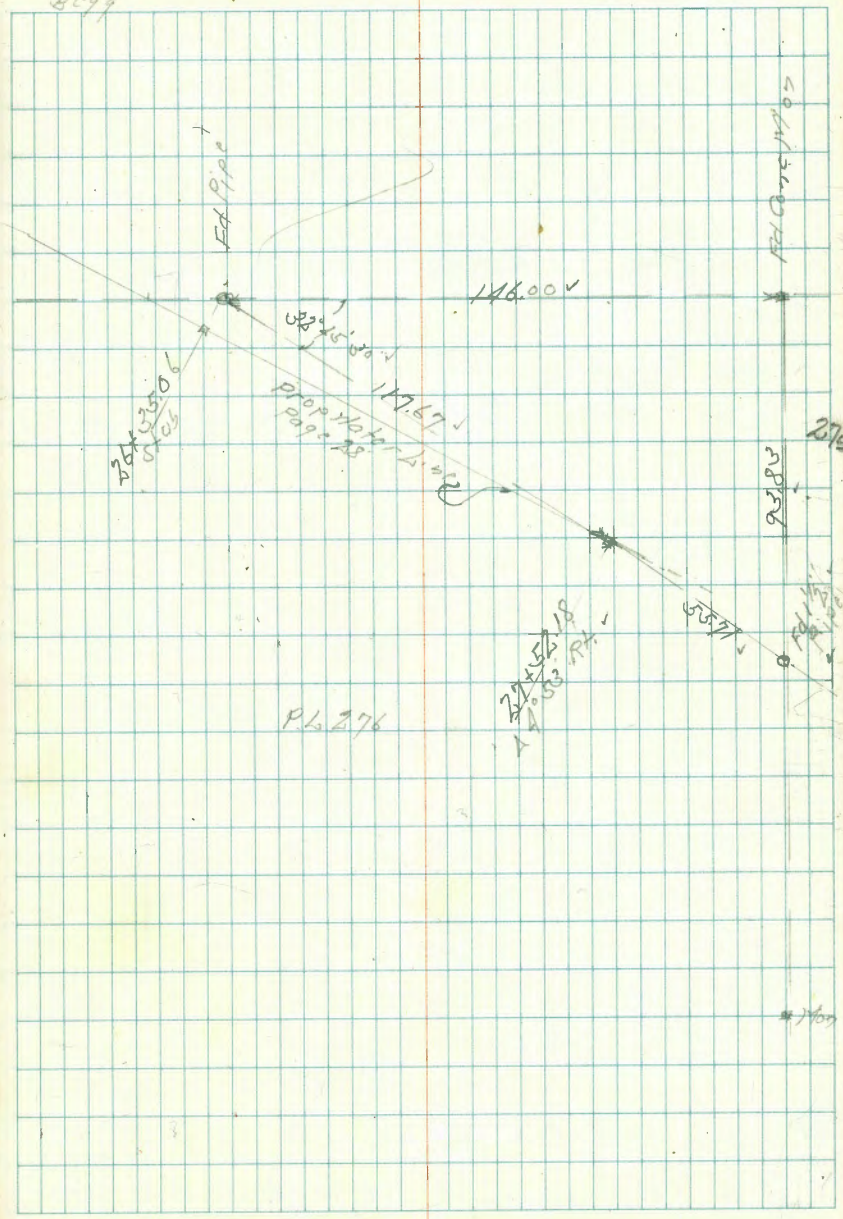


		10.23			
TP	4.78	10.25	4.86	5.47	
3+50			5.0		5.3
+65	6.2 Lt of P.I.	2.0 Tel Pole			
4+0			4.8		5.5
"	10 Rt		4.8		5.5
	7 Lt		4.8		5.5
	10 Lt		4.8		5.5
4+08.5	64 Rt. F.L. Existing		16.40	-	5.15
4+43.8	Approx Loc Rock		4.7		5.6
					Starting
BM			5.63	4.67	

Proposed Water Line Across PL. 276
U.S. Gov. Dyke

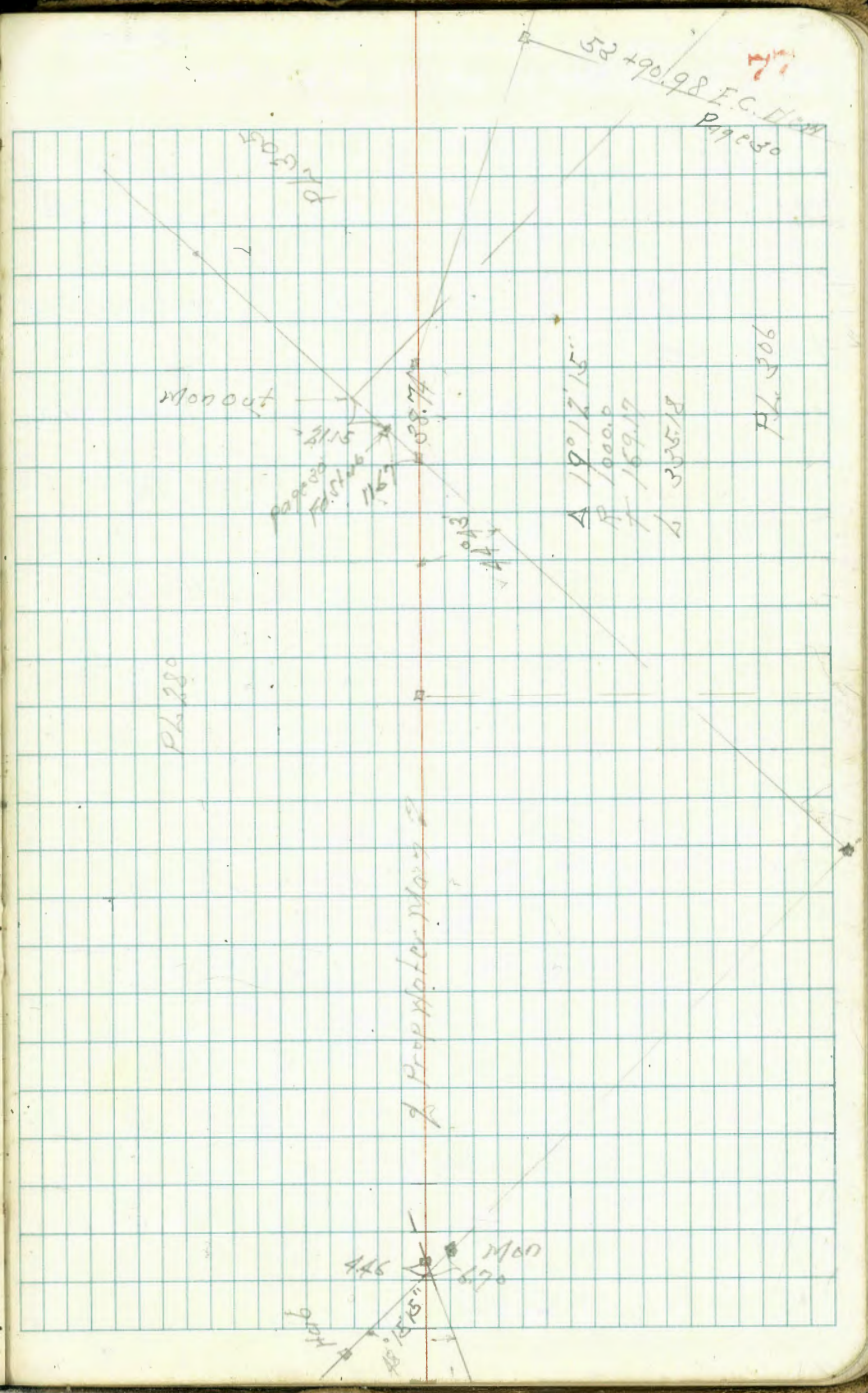


Dec 6-40
S. Sloan
Bliss
Osborn
Bragg

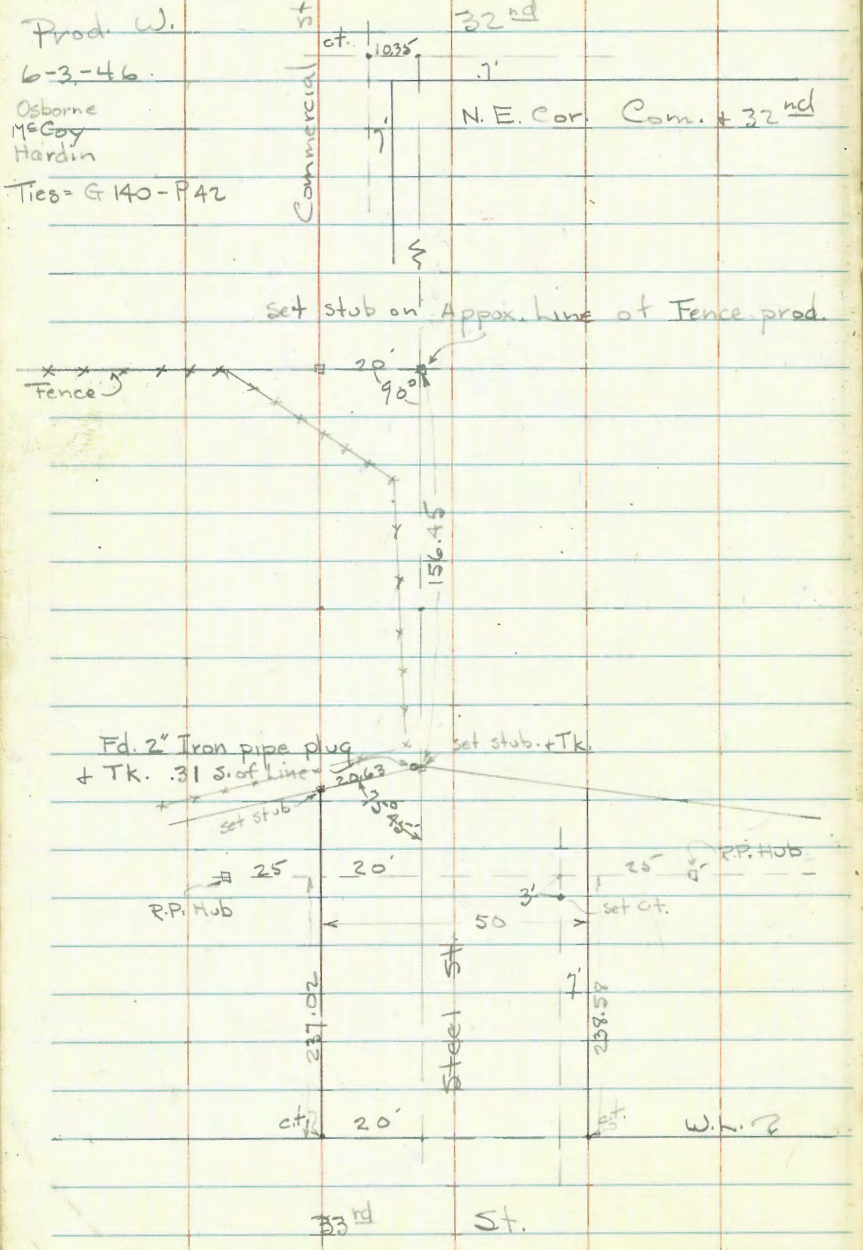


San Diego River Dyke Water Main

Dec 19.43
Sisson
Bush
BC99



Preliminary location of 20' Easement
Thru. Por. of SW 1/4 of P.L. 1152 S.L. Steel
Prod. W.
6-3-46
Osborne
McCoy
Hardin
Ties = G 140 - P 42



Indexed
o.s.K.

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Water line Grades Haines + La Playa. 16" Main as lowered

Sommermeyer
W. Moore
L. Melton. 4-7-47 W.O. 1031

Stationing same as on 6865L

N.E.B.P. Frontera + La Playa.	12.87	32.32	—	19.45
294+87 E			6.76	
295+12 E			6.91	
+37 E			7.08	
+62 E			7.21	
+87 E			7.22	
296+12 E			7.35	
+37 E			7.59	
+50			7.62	
+81.25			7.17	
297+12 E			6.68	
+37 E			6.22	
+57 E			5.59	
+77 E			5.07	

0+45 To1 Polo Iona 2045 ℄ 1619-3
Top Wall NE Brooklyn & Iona ~~2535~~ 2535 " -6
1/2 "Pipe S.W. Marlin 25390 " -11
SW Bk. 60th & Beech 25205 " 11

1414
25
7070
25218
35350

0+44 To 5

146.26
20
71 26

14+48.64
13+93.99
54,65

3085
1205
1561

3085
83

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.