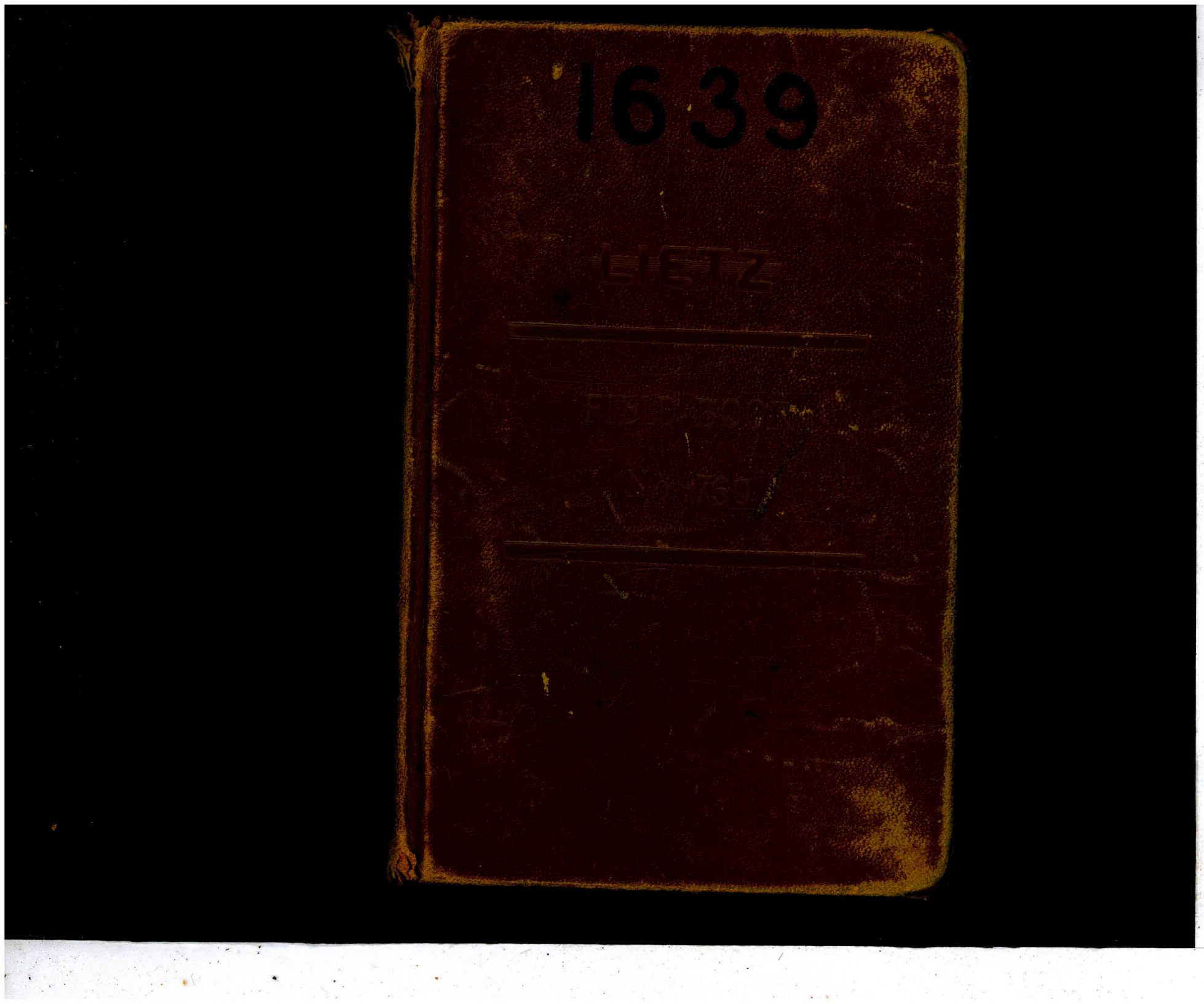
1639
METZ

TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		⅛ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100.00	0 44	100.00	0.87	99.99	1.31	89
1	99.98	1 75	99.99	2 18	99 97	2.62	99 95	3.05	88
2	99.94	3.49	99 92	3.93	99 91	4 36	99.88	4.80	87
3	99.86	5.23	99 84	5 67	99 81	6.10	99.79	6.54	86
4	99 76	6.98	99 73	7.41	99.69	7.85	99.66	8.28	85
5	99 62	8.72	99.58	9.15	99 54	9.58	99.50	10 02	84
6	99.45	10.45	99.41	10 89	99.36	11.32	99.31	11.75	83
7	99 25	12.19	99 20	12.62	99.14	13.05	99.09	13.49	82
8	99.03	13.92	98.97	14.35	98.90	14.78	98.84	15.21	81
9	98.77	15.64	98.70	16.07	98.63	16 50	98 56	16.93	80
10	98 48	17.36	98.40	17.79	98.33	18.22	98.25	18.65	79
11	98 16	19.08	98 08	19 51	97.99	19 94	97.90	20.36	78
12	97.81	20.79	97.72	21.22	97.63	21 64	97.53	22.07	77
13	97.44	22.50	97.34	22.92	97.24	23.34	97.13	23.77	76
14	97.03	24.19	96.92	24 62	96.81	25 04	96 70	25.46	75
15	96.59	25 88	96.48	26.30	96.36	26.72	96.25	27.14	74
16	96.13	27.56	96.00	27 98	95.88	28 40	95 76	28.82	73
17	95.63	29.24	95.50	29.65	95.37	30 07	95.24	30.49	72
18	95.11	30 90	94.97	31.32	94.83	31.73	94.69	32.14	71
19	94.55	32.56	94.41	32.97	94.26	33.38	94.12	33.79	70
20	93.97	34.20	93.82	34.61	93.67	35.02	93.51	35 43	69
21	93.36	35.84	93.20	36.24	93.04	36.65	92.88	37.06	68
22	92.72	37.46	92.55	37.86	92.39	38.27	92.22	38 67	67
23	92.05	39.07	91.88	39 47	91.71	39.87	91.53	40.27	66
24	91.35	40.67	91.18	41.07	91.00	41.47	90.81	41.87	65
25	90.63	42.26	90.45	42.66	90.26	43.05	90.07	43.44	64
26	89.88	43.84	89 69	44.23	89.49	44.62	89.30	45.01	63
27	89.10	45.40	88.90	45.79	88.70	46.17	88.50	46.56	62
28	88.29	46.95	88.09	47.33	87.88	47.72	87 67	48.10	61
29	87.46	48.48	87.25	48 86	87.04	49.24	86.82	49.62	60
30	86.60	50.00	86.38	50.38	86.16	50.75	85.94	51.13	59
31	85.72	51.50	85.49	51.88	85.26	52.25	85.04	52.62	58
32	84.80	52 99	84.57	53.36	84.34	53.73	84.10	54.10	57
33	83.87	54.46	83.63	54.83	83.39	55.19	83.15	55.56	56
34	82.90	55.92	82.66	56.28	82.41	56.64	82.16	57.00	55
35	81.92	57.36	81.66	57.71	81.41	58.07	81.16	58.42	54
36	80.90	58.78	80.64	59.13	80.39	59.48	80.13	59.83	53
37	79.86	60.18	79.60	60 53	79.34	60.88	79.07	61 22	52
38	78.80	61.57	78.53	61.91	78.26	62.25	77.99	62.59	51
39	77.71	62.93	77.44	63.27	77.16	63.61	76.88	63.94	50
40	76.60	64.28	76.32	64.61	76.04	64.94	75.76	65.28	49
41	75.47	65.61	75.18	65.93	74.90	66.26	74.61	66.59	48
42	74.31	66.91	74.02	67.24	73.73	67.56	73.43	67.88	47
43	73.14	68.20	72.84	68.52	72.54	68.84	72.24	69.15	46
44	71.93	69.47	71.63	69.78	71.33	70.09	71.02	70.40	45
45	70.71	70.71							
Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees.
	DEGREES.		¾ DEGREE.		⅛ DEGREE.		¼ DEGREE.		

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MADE IN
U. S. A.

TABLE OF STADIA REDUCTIONS

For a Constant of 100.

ROD VERTICAL.

Min.	0°		1°		2°		3°	
	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff Elev.	Hor Dist.	Diff. Elev.
0'	100.00	.00	99.97	1.74	99.88	3.49	99.73	5.23
2	100.00	.06	99.97	1.80	99.87	3.55	99.72	5.26
4	100.00	.12	99.97	1.86	99.87	3.60	99.71	5.34
6	100.00	.17	99.96	1.92	99.87	3.66	99.71	5.40
8	100.00	.23	99.96	1.98	99.86	3.72	99.70	5.46
10	100.00	.29	99.96	2.04	99.86	3.78	99.69	5.52
12	100.00	35	99.96	2.09	99.85	3.84	99.69	5.57
14	100.00	.41	99.95	2.15	99.85	3.90	99.68	5.63
16	100.00	.47	99.95	2.21	99.84	3.95	99.68	5.69
18	100.00	.52	99.95	2.27	99.84	4.01	99.67	5.75
20	100.00	.58	99.95	2.33	99.83	4.07	99.66	5.80
22	100.00	.64	99.94	2.38	99.83	4.13	99.66	5.86
24	100.00	.70	99.94	2.44	99.82	4.18	99.65	5.92
26	99.99	.76	99.94	2.50	99.82	4.24	99.64	5.98
28	99.99	.81	99.93	2.56	99.81	4.30	99.63	6.04
30	99.99	.87	99.93	2.62	99.81	4.36	99.63	6.09
32	99.99	.93	99.93	2.67	99.80	4.42	99.62	6.15
34	99.99	.99	99.93	2.73	99.80	4.48	99.62	6.21
36	99.99	1.05	99.92	2.79	99.79	4.53	99.61	6.27
38	99.99	1.11	99.92	2.85	99.79	4 59	99.60	6.33
40	99.99	1.16	99.92	2.91	99.78	4.65	99.59	6.38
42	99.99	1.22	99.91	2.97	99.78	4.71	99.59	6.44
44	99.98	1.28	99.91	3.02	99.77	4.76	99.58	6.50
46	99.98	1.34	99.90	3.08	99.77	4.82	99.57	6.56
48	99.98	1.40	99.90	3.14	99.76	4.88	99.56	6.61
50	99.98	1.45	99.90	3.20	99.76	4.94	99.56	6.67
52	99.98	1.51	99.89	3.26	99.75	4.99	99.55	6.73
54	99.98	1.57	99.89	3.31	99.74	5.05	99.54	6.78
56	99.97	1.63	99.89	3.37	99.74	5:11	99.53	6.84
58	99.97	1.69	99.88	3.43	99.73	5.17	99.52	6.90
60	99.97	1.74	99.88	3.49	99.73	5.23	99.51	6.96
c= .75	.75	.01	.75	.02	.75	.03	.75	.05
c=1.15	1.15	.01	1.15	.03	1.15	.05	1.15	.07
c=1.90	1.90	.02	1.90	.05	1.90	.08	1.90	.12

Min.	4°		5°		6°		7°	
	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist	Diff. Elev.	Hor Dist.	Diff. Elev.
0'	99.51	6.96	99.24	8.68	98.91	10.40	98.51	12.10
2	99.51	7.02	99.23	8.74	98.90	10.45	98.50	12.15
4	99.50	7.07	99.22	8.80	98.88	10.51	98.48	12.21
6	99.49	7.13	99.21	8.85	98.87	10.57	98.47	12.26
8	99.48	7.19	99.20	8.91	98.96	10.62	98.46	12.32
10	99.47	7.25	99.19	8.97	98.85	10.68	98.44	12.38
12	99.46	7.30	99.18	9.03	98.83	10.74	98.43	12.43
14	99.46	7.36	99.17	9.08	98.82	10.79	98.41	12.49
16	99.45	7.42	99.16	9.14	98.81	10.85	98.40	12.55
18	99.44	7.48	99.15	9.20	98.80	10.91	98.39	12.60
20	99.43	7.53	99.14	9.25	98.78	10.96	98.37	12.66
22	99.42	7.59	99.13	9.31	98.77	11.02	98.36	12.72
24	99.41	7.65	99.11	9.37	98.76	11.08	98.34	12.77
26	99.40	7.71	99.10	9.43	98.74	11.13	98.33	12.83
28	99.39	7.76	99.09	9.48	98.73	11.19	98.31	12.88
30	99.38	7.82	99.08	9.54	98.72	11.25	98.29	12.94
32	99.38	7.88	99.07	9.60	98.71	11.30	98.28	13.00
34	99.37	7.94	99.06	9.65	98.69	11.36	98.27	13.05
36	99.36	7.99	99.05	9.71	98.68	11.42	98.25	13.11
38	99.35	8.05	99.04	9.77	98.67	11.47	98.24	13.17
40	99.34	8.11	99.03	9.83	98.65	11.53	98.22	13.22
42	99.33	8.17	99.01	9.38	98.64	11.59	98.20	13.28
44	99.32	8.22	99.00	9.94	98.63	11.64	98.19	13.33
46	99.31	8.28	98.99	10.00	98.61	11.70	98.17	13.39
48	99.30	8.34	98.98	10.05	98.60	11.76	98.16	13.45
50	99.29	8.40	98.97	10.11	98.58	11.81	98.14	13.50
52	99.28	8.45	98.96	10.17	98.57	11.87	98.13	13.56
54	99.27	8.51	98.94	10.22	98.56	11.93	98.11	13.61
56	99.26	8.57	98.93	10.28	98.54	11.98	98.10	13.67
58	99.25	8.63	98.92	10.34	98.53	12.04	98.08	13.73
60	99.24	8.68	98.91	10.40	98.51	12.10	98.06	13.78
c= .75	.75	.06	.75	.07	.75	.08	.74	.10
c=1.15	1.15	.09	1.14	.11	1.14	.13	1.14	.15
c=1.90	1.89	.15	1.89	.18	1.89	.21	1.88	.25

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Indexed
E.S.K.

Re-align. of Linda Vista Rd. Wly of Linda Vista Housing Project.

10+68.84 EC 2 x 2 hub

7+61 ℄ of Proposed Culv. 18" in Main Cañon

Δ = 51°02' Rt

R = 1200

T = 577.80

L = 1068.84

1.4324

1° 11.47 = 50'

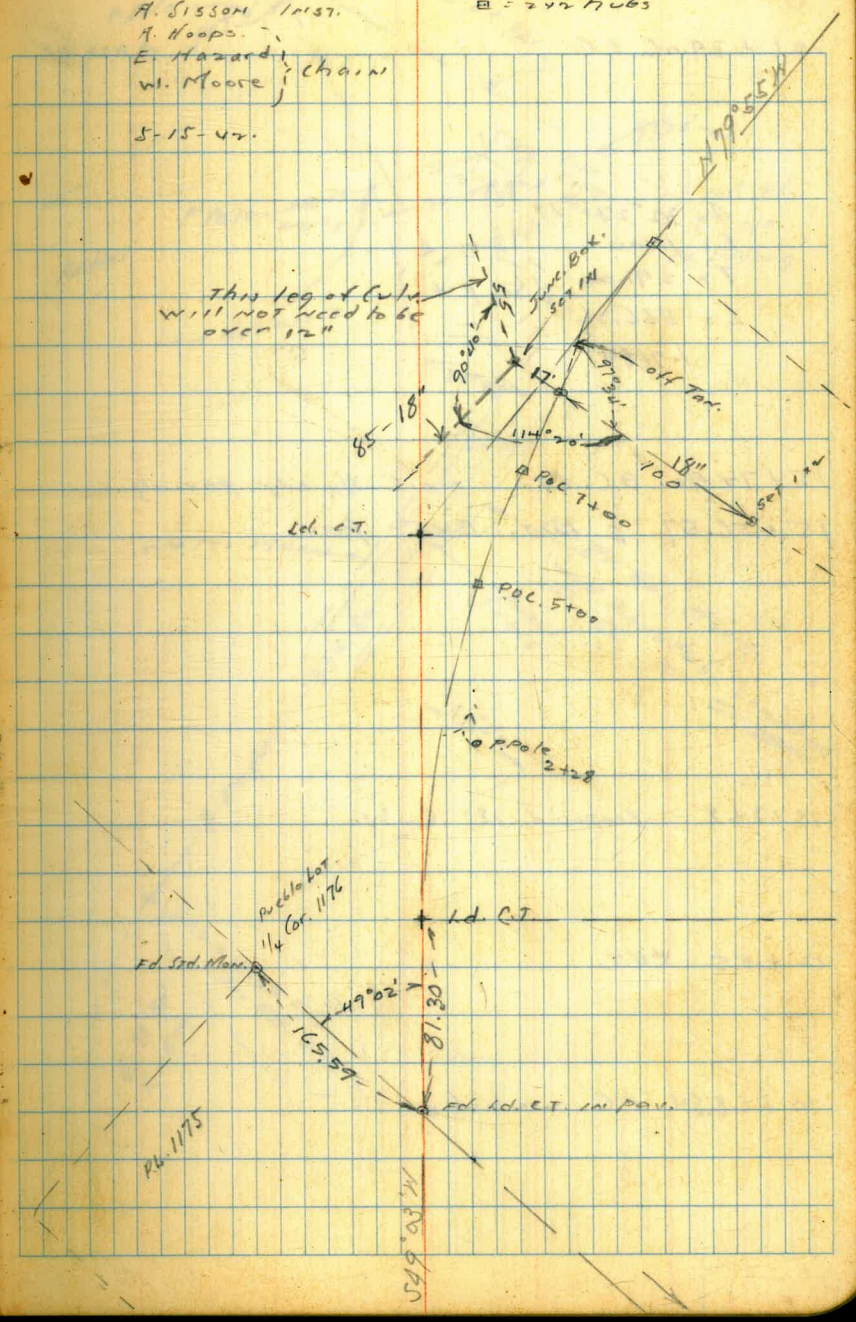
0+00 BC Rt. Ld. C.T.

J.W. Williams, Adm. Engr.
C. Moore Notes
A. Sisson Instr.
A. Hoops.
E. Hazard
W. Moore } Chain

5-15-42.

2

□ = 2 x 2 hubs



Int. & Ex. paving —

21 + 39.46 E.C.

Δ = 32°27' Lt
R = 1000
T = 291.00
L = 566.36
1.7189

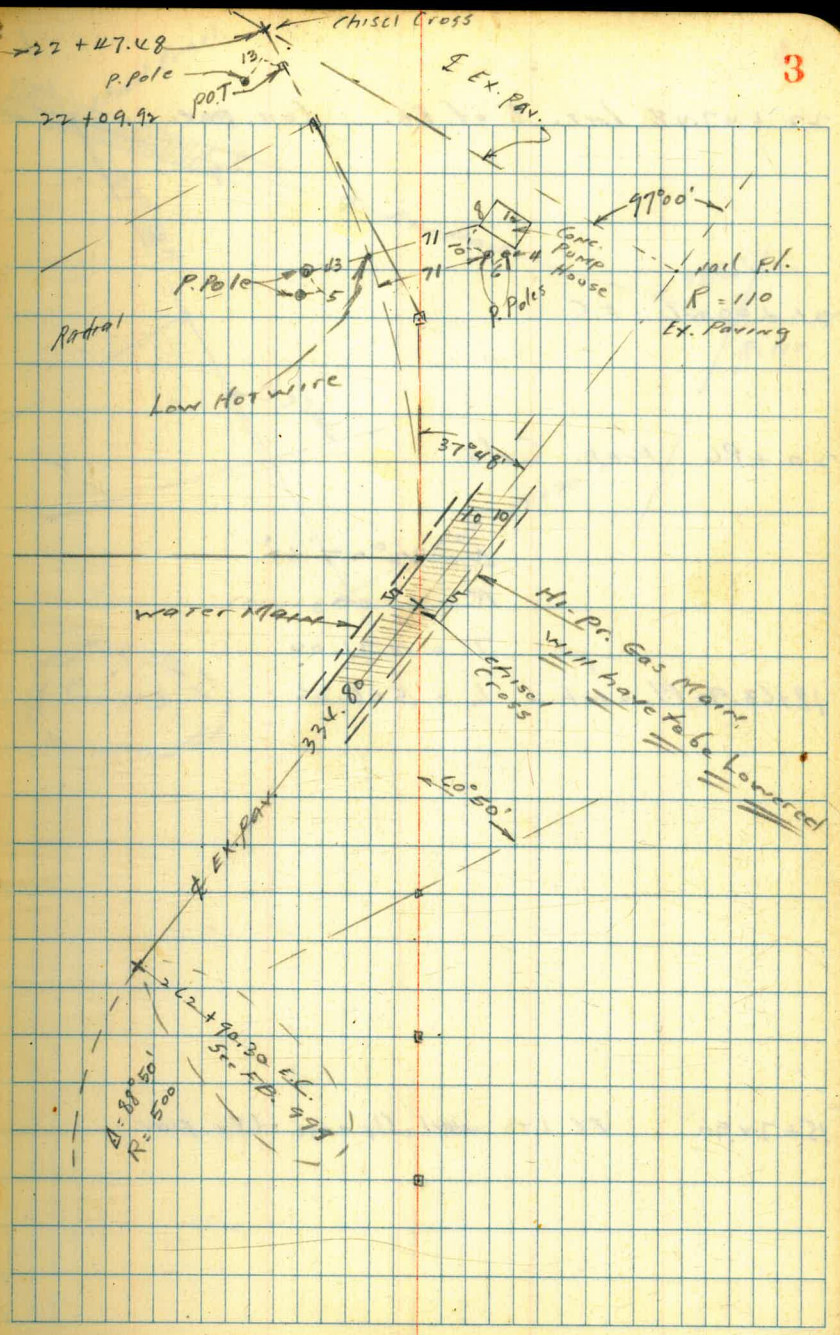
15 + 74.90 B.C. Lt. nail s/y edge paving

15 + 56.57 & Int. Ex. pav.

13 + 34.8 proposed 18" Culv.

12 + 55 P.O.T.

10 + 68.84 E.C. ±



22+47.48 Intr. ℄ of Ex. Con. pav.

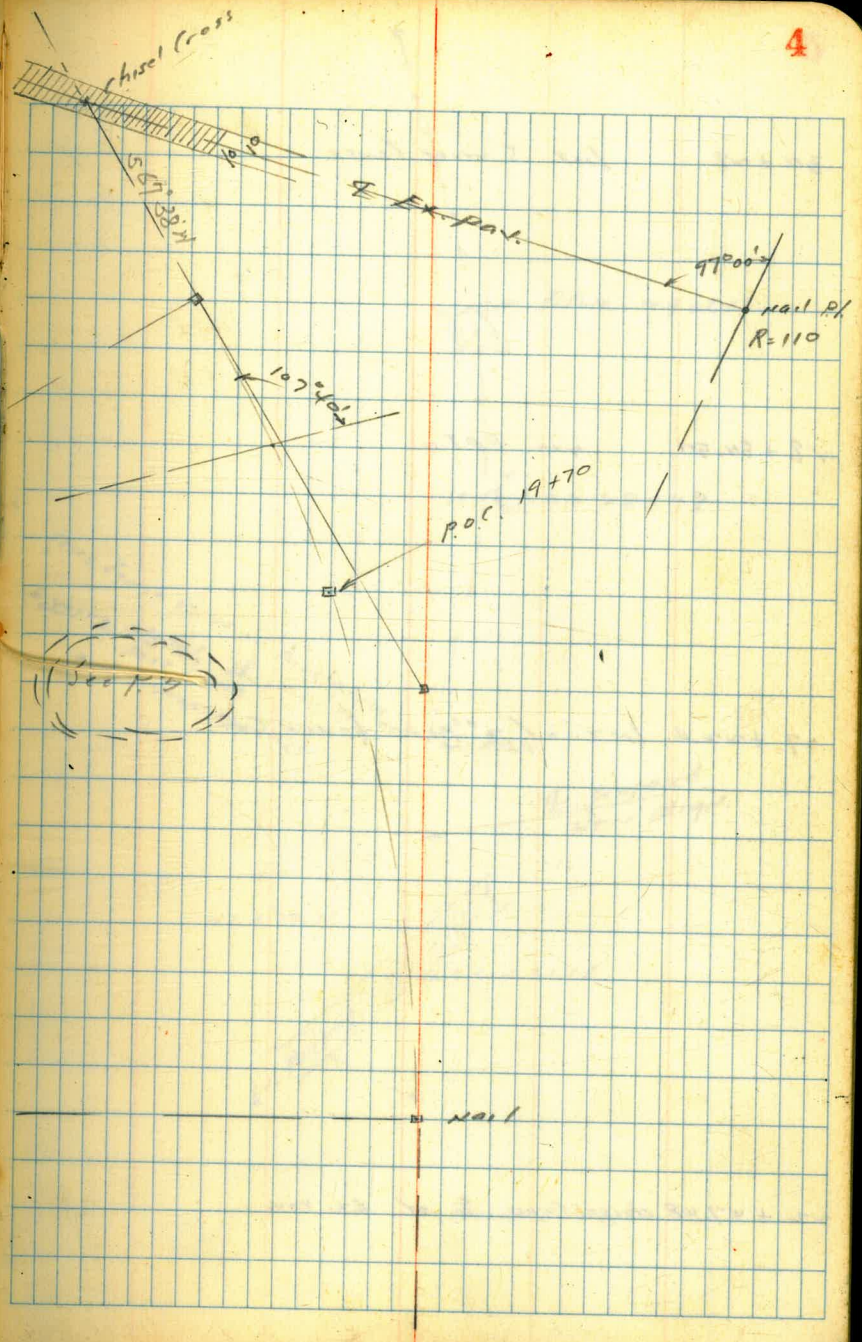
21+39.46 E.C.

20+86 Prop. Curv.

Δ = 32°47'LT
R = 1000
T = 291.00

18+63.90 P.I. Curve L = 566.36

15+72.90 RC LT Nail Sly edge of Ex. pav.

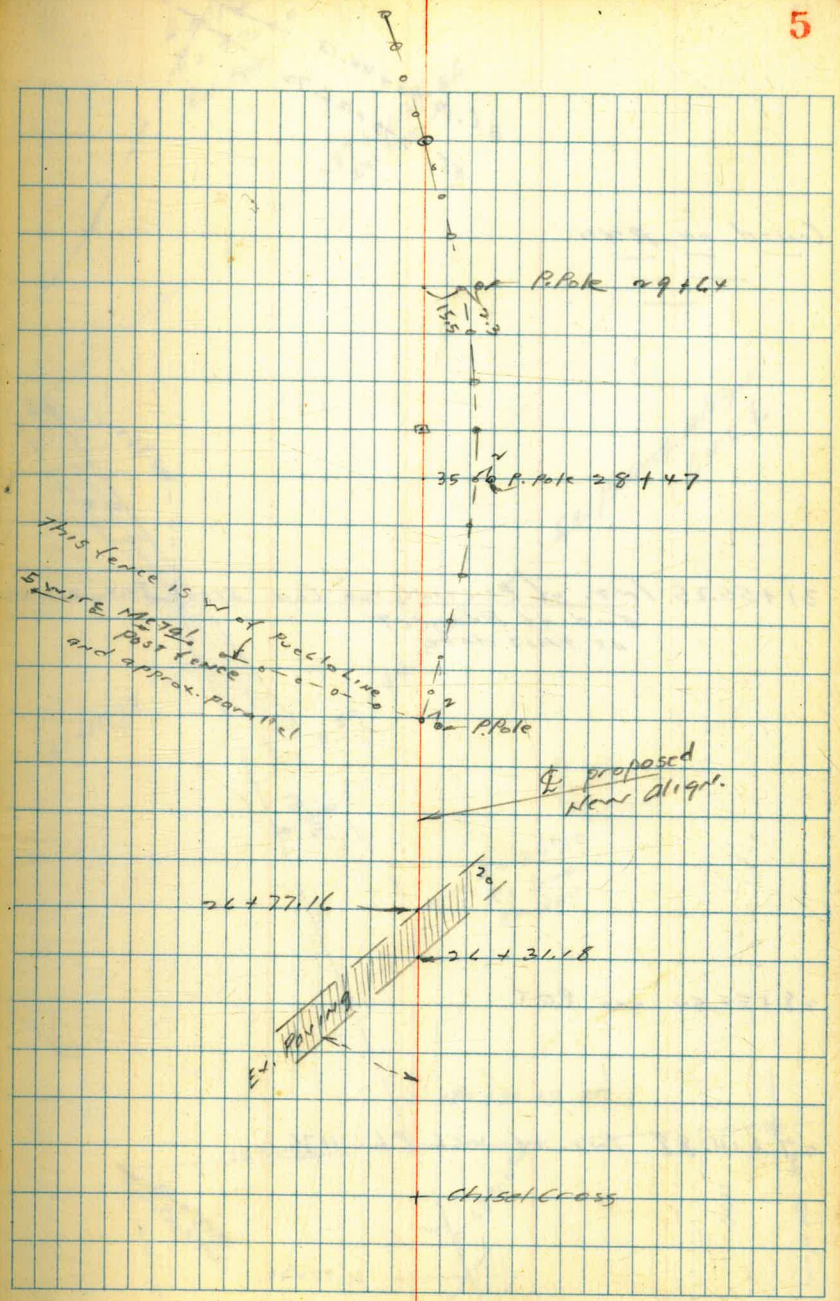


30+28 Int. 5 wire fence

28+54.57 xxx P.O.T.

27+22.4 Int. of 2" Pipe fence Cor.

22+47.48 chisel Cross ℄ of Ex. pav.



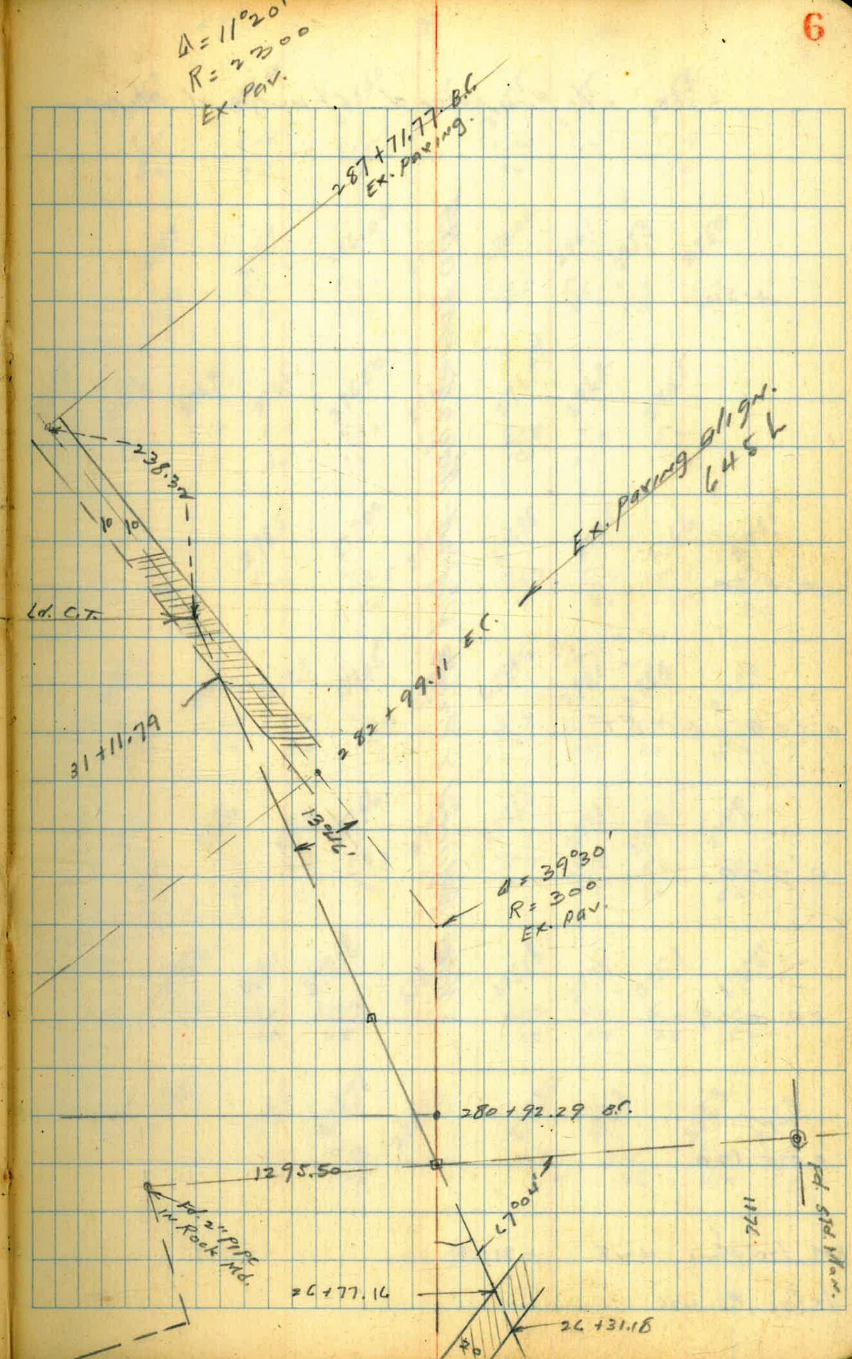
B.C. 293+44.13
E.C. 292+26.72

Contd. on p. 20

31+55.25 Int. of Existing 20' Con. Strip Pav.
End of Project
at this date

28+52.52 P.O.T.

27+14.88 Int. of W.L. P.L. 1176



x sec of Proposed change of align.

Notes Reduced x Profile Plotted May 26 - 1948 ABS

+ 50

0 + 50

0 + 00 BC RT

0 - 20

00 - 49

00 - 120

B.M. Std. Mon. 4-18 2816.5 277.37

1/4 Cor. Pl. 1176

LT. ℄ RT.

275.3 / 6.4 / 50	275.49 / 6.6 / 27	275.50 / 6.5 / 7	275.5 / 6.2	275.5 / 6.2 / 14	275.5 / 6.2 / 30	275.8 / 5.9 / 50
275.7 / 6.0 / 50	275.5 / 6.2 / 35	276.04 / 5.6 / 19	276.00 / 5.6.5	276.00 / 5.6.5 / 1	276.1 / 5.6 / 8	275.3 / 6.4 / 14	275.0 / 6.7 / 50
275.5 / 6.7 / 50	275.6 / 6.1 / 43	276.0 / 5.7 / 39	276.5 / 5.7 / 30	276.50 / 5.5 / 14	276.58 / 5.7	276.47 / 5.8 / 6	276.4 / 5.8 / 14	276.5 / 5.7 / 50
		276.5 / 5.7 / 50	277.00 / 5.6.5 / 11	277.05 / 5.6.0	276.98 / 5.6.7 / 9	276.5 / 5.7 / 20	276.6 / 5.7 / 30	276.5 / 5.7 / 50
275.6 / 6.1 / 50	275.5 / 6.2 / 34	277.3 / 5.4 / 30	277.45 / 5.2.0 / 10	277.58 / 5.0.7	277.46 / 5.1.9 / 10	277.1 / 5.1.6 / 25	275.9 / 5.3 / 30	275.9 / 5.1.8 / 50
275.1 / 6.0 / 50	275.6 / 6.1 / 36	277.6 / 5.1 / 31	277.66 / 3.99 / 10	277.76 / 3.89	277.63 / 4.0.2 / 10	277.1 / 5.1.2 / 25	275.9 / 5.3 / 30	275.8 / 5.9 / 50
276.2 / 5.5 / 50	278.1 / 3.6 / 38	278.18 / 3.4.7 / 28	278.45 / 3.2.0	278.18 / 3.4.7 / 22	277.7 / 5.0 / 30	275.7 / 6.0 / 36	275.5 / 6.2 / 50
277.4 / 4.3 / 50	278.1 / 3.7 / 38	278.75 / 2.9.0 / 28	278.93 / 2.7.2	278.80 / 2.8.5 / 22	278.3 / 3.4 / 32	275.3 / 6.4 / 22	275.3 / 6.4 / 50

281.65

5

+ 50

4

+ 75

+ 70

+ 50

T.P. 3.15 277.71 7.09 270.56

3

+ 50

2 81.65

LT

270.5 7.2 50

270.3 7.4 34

271.5 6.2 21

271.4 6.3

271.2 6.5 20

RT

271.7 6.0 34

273.1 4.6 50

271.5 6.2 50

271.9 5.8 25

272.1 5.6

272.5 5.2 18

273.7 4.0 29

273.0 4.6 50

271.5 6.2 52

272.9 4.8 48

273.0 4.7 27

273.1 4.6

273.6 4.1 13

274.4 3.3 19

273.7 4.0 31

273.8 3.9 50

273.56 4.15 51

274.0 3.7 41

273.7 4.0 20

273.5 4.2

273.7 4.0 36

273.9 3.8 50

273.52 4.15 51 Ins & Pav.

273.5 4.2 45

274.2 3.5 42

273.9 3.8 17

274.8 2.9

274.1 3.6 12

273.5 4.2 23

274.0 3.7 50

273.78 3.43 50

273.78 3.73 49

273.9 3.8 40

274.5 3.7 36

274.0 3.7 20

274.5 3.7

274.5 3.7 20

274.0 3.7 25

274.3 3.4 42

274.7 3.0 50

277.71

274.37 7.28 51

274.40 7.45 30

274.7 7.0 25

275.8 5.9 16

276.0 5.7

276.1 5.6 18

275.7 6.0 32

275.3 6.4 41

276.3 5.4 50

275.4 6.3 50

274.95 6.70 37

274.95 6.70 17

275.2 6.5 7

276.4 5.3 6

276.2 5.5

276.7 5.0 13

276.4 5.3 21

275.7 6.0 50

281.65

T.P	0.06	240.58	12.59	240.52
7				
T.P.	0.37	253.11	12.87	252.74
+ 75				
+ 50				
+ 25				
T.P.	0.55	265.61	12.65	265.06
6				
+ 90				
5 + 50				
		277.71		

LT ℄ RT

240.6 — 12.5 / 75

233.9 — 19.2 / 40 — Bot Canon

240.2 — 12.9 / 39

245.9 — 7.2 / 18

247.8 — 5.3

246.4 — 6.7 / 31

243.8 — 9.3 / 50

251.3 — 11.8 / 65

253.11 ℄

238.4 — 27.2 / 75 — Bot Canon

246.3 — 19.3 / 50

252.8 — 12.8 / 27

255.1 — 10.5

255.2 — 10.4 / 25

253.1 — 12.5 / 50

249.6 — 16.0 / 70

255.5 — 10.1 / 50

258.1 — 7.5 / 40

259.7 — 5.9 / 24

259.9 — 5.7

259.3 — 6.3 / 37

259.2 — 4.4 / 50

263.1 — 2.5 / 55

263.8 — 1.8 / 24

263.8 — 1.8

264.3 — 1.3 / 14

264.6 — 1.0 / 26

263.5 — 2.1 / 41

263.6 — 2.0 / 50

265.61 ℄

264.3 — 13.4 / 65

264.5 — 12.2 / 50

267.4 — 10.3 / 24

267.3 — 10.4

266.9 — 10.8 / 25

266.4 — 11.3 / 50

269.2 — 10.5 / 50

268.1 — 9.6 / 30

268.9 — 8.8 / 10

269.0 — 8.7

268.7 — 9.0 / 17

268.5 — 9.2 / 50

268.6 — 9.1 / 50

269.3 — 8.4 / 23

269.3 — 8.4

269.9 — 7.8 / 17

270.2 — 7.5 / 37

269.8 — 7.9 / 50

277.71 ℄

+50

T.P. 11.99 ≈23.87 0.44 251.88

+≈5

T.P. 11.8≈ ≈5≈.3≈ 0.08 ≈40.50

8

7+61 Sec. at 90°

7+61 Proposed Culv.

+50

7+≈5

≈40.58

Lt. 2519 12.0 / 60 | 2525 11.≈ / 50 | 253.7 10.≈ / 45 | ℄ 255.3 8.6 | 255.6 8.3 / 25 | PT 253.3 8.C / 50 | 254.8 5.1 / 2≈

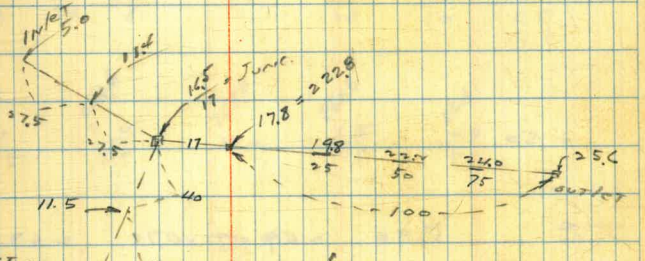
≈23.87

2450 7.3 / 70 | 244.8 7.5 / 50 | 246.2 6.1 / 25 | 248.2 4.1 | 249.7 ≈.6 / 25 | 248.6 3.7 / 50 | 248.6 3.7 / 60

≈5≈.3≈

238.4 2.≈ / 65 | 237.7 2.9 / 50 | 236.5 4.1 / 2≈ | 238.2 2.4 / 10 | 237.8 2.8 | 237.6 3.0 / 29 | 238.0 2.6 / 50 | 237.2 3.≈ / 65

239.9 0.7 / 25 | 235.2 5.≈ / 50 | 228.8 11.8 / 32 | 234.5 16.1 / 18 | 222.8 17.8 | 220.9 19.7 / 25 | 221.4 19.≈ / 43 | 219.≈ 21.≈ / 70 | 218.8 ≈1.8 / 85



228.3 2.3 / 60 | 233.9 6.7 / 50 | Inlet 4.3 227.6 12.9 / 30 | 226.0 14.6 / 21 | 226.6 14.0 / 11 | 226.9 13.7 | 223.5 17.1 / 24 | 221.2 19.≈ / 36 | 218.4 2≈.≈ / 50 | 216.9 ≈3.7 / 75

45

238.9 1.7 / 67 | 228.8 11.8 / 40 | Bot. Culvert 234.2 6.≈ / 20 | 23.78 ≈.3 | 236.8 3.8 / 25 | 233.6 7.0 / 40 | 230.1 10.5 / 60 | 228.4 ≈≈.≈ / ≈5

≈40.58

+ 50

11

10 + 18.84 E.C.

+ 50

10

+ 50

T.P. 5.90 269.07 0.70 263.17

9

8 + 75

263.87

LT

259.7 | 9.3 | 55

259.7 | 9.3 | 25

260.4 | 8.6

261.1 | 7.9 | 25

262.4 | 6.6 | 55

260.9 | 8.1 | 55

262.1 | 6.9 | 35

262.4 | 6.6 | 20

262.0 | 7.0

263.4 | 5.6 | 17

262.6 | 6.4 | 38

262.6 | 6.4 | 55

262.9 | 6.1 | 55

263.0 | 6.0 | 35

262.8 | 6.4 | 15

262.7 | 6.30

HUB

262.9 | 6.1 | 20

263.1 | 5.9 | 40

264.0 | 5.0 | 55

263.2 | 5.8 | 55

263.2 | 5.8 | 25

263.2 | 5.8

263.5 | 4.5 | 15

263.2 | 4.8 | 30

263.3 | 5.7 | 55

264.4 | 4.6 | 55

264.4 | 4.6 | 44

263.7 | 3.3 | 24

264.4 | 4.4 | 8

263.9 | 5.1

264.4 | 4.6 | 28

265.1 | 3.9 | 50

264.8 | 4.2 | 55

264.9 | 4.1 | 55

264.6 | 4.4 | 25

263.0 | 4.0

264.5 | 4.5 | 15

264.1 | 4.9 | 55

269.07

261.8 | 2.1 | 55

263.5 | 1.4 | 25

262.5 | 1.4 | 15

262.4 | 1.5

262.7 | 1.2 | 25

262.2 | 1.7 | 55

258.7 | 8.2 | 60

256.5 | 7.4 | 50

258.5 | 5.4 | 24

260.3 | 3.6

260.1 | 3.8 | 25

259.5 | 4.4 | 50

259.6 | 4.3 | 60

263.87

13 + 34.8 prop. Culy.

+ 76

13

T.P. 0.08 244.75 12.83 244.67

+ 77

17 + 55 P.O.T.

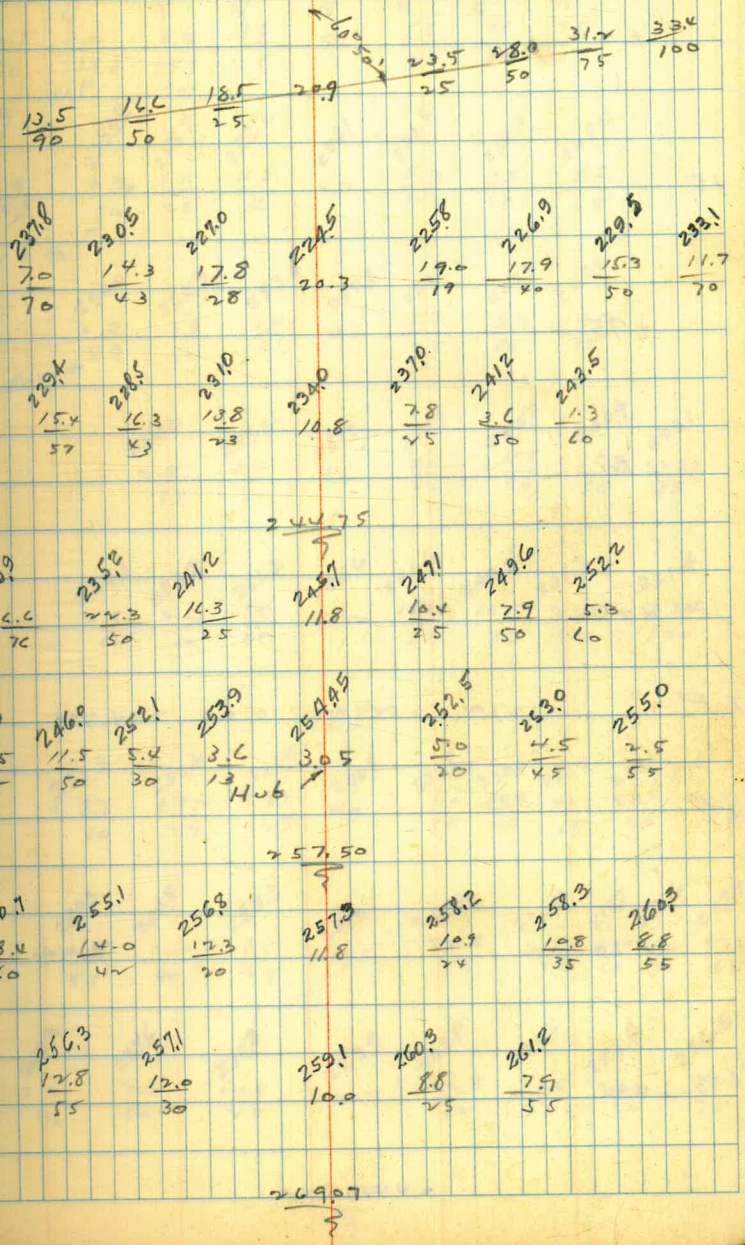
T.P. 0.06 257.50 11.63 257.44

+ 25

17

269.07

LT ℄ RT



+21

15

+75

+50

+25

T.P. 12.10 256.87 0.03 244.77

14

+70

13 +44

244.75

LT RT

251.5 253.3 253.8 253.8 253.2 251.2 251.2 249.7 249.3

5.3 3.5 3.0 3.0 3.6 5.6 5.6 7.1 7.5

5.5 50 39.8 15.7 5 50 25 50 65

S.L.P.

N.L.P.

253.9 253.92 253.7 252.2 252.1 251.5 250.3 248.2

2.9 7.90 4.7 4.6 4.7 5.9 6.5 8.4

56.5 32 23 12 25 50 65

S.L.P.

N.L.P.

254.0 252.9 253.4 252.8 251.1 247.9 244.2

2.8 3.9 3.4 4.0 5.7 8.9 14.6

50 34 21 25 50 75

N.L.P.

254.0 253.4 251.7 248.7 245.3 240.9 233.1

2.8 4.4 5.2 8.1 11.5 15.9 23.7

55 32 22 40 56 85

254.3 254.2 251.2 246.6 241.6 240.3 231.3 221.4

2.5 3.6 5.6 10.2 15.2 16.5 25.5 35.2

60 50 21 25 36 64 100

256.87

253.5 252.0 245.9 240.8 238.8 230.0 221.7 216.1 210.1

8.7 7.2 11.1 4.0 4.0 14.8 23.1 28.7 34.7

60 47 25 13 38 68 90 108

249.3 248.8 239.3 231.3 224.4 221.5 217.7 218.6 217.7

4.5 1.0 5.5 13.5 20.6 23.3 27.1 31.2 27.1

55 40 25 25 45 60 70 85

242.3 237.6 230.3 223.9 222.0 221.2 223.8 226.5

7.5 7.2 14.5 20.9 22.8 23.6 21.0 18.3

70 50 25 12 27 50 70

244.75

+50

T.P 12.51 +56.96 1+.37 244.45

+30

16

+85

15 +7+.90 B.C. L.T. Sec at 90°

+56.57 Sec. on ℄ Ex. Pav

+56.57 Int. ℄ of Ex. Pav. Sec at 90°

15+79

+56.87

Lt ℄ Rt

2403 16.7 60

2397.5 19.5 45

2378 19.2 33

2398 17.2 18

2437 13.3

2464 10.6 15

2490 8.0 50

2532 3.8 60

+56.96

2469 8.9 60

2454 11.4 38

2464 10.4 18

2475 9.3

2490 7.8 32

2530 3.8 42

2534 3.4 64

2483 8.5 60

2482 8.6 50

2481 8.7 25

2486 8.2

2531 8.7 12

2532 3.6 48

2490 7.8 60

2481 8.7 70

2492 7.6 60

2490 7.8 40

2494 7.6 16

2497 7.1 10

2531 3.7 5.5 Hor. Ber.

2533 3.5 48

2501 6.7 42

2487 8.1 71

2500 6.8 65

2498 7.0 50

2494 7.4 25

2499 6.9 18

2533 3.5 10

2536 5.18 5L Pav.

2532 3.6 35

2500 6.8 44

2488 8.0 55

2468 10.0 85

2553.7 1.45 200 Pav.

2538.0 3.07 Pav.

2533.2 3.50 150 Pav.

2503 6.5 60

2501 6.7 31

2535 3.2 27

2538.0 3.07 Pav.

2535 3.3 20

2531 3.7 24

2503 6.5 31

2496 7.2 57

2481 7.7 70

2510 5.8 60

2509 5.9 53

2534 3.4 46

2538.2 3.00 5L Pav.

2537.2 3.10 45 Pr. H L

2534 3.4

2541 5.7 6

2512 5.6 25

2497 7.1 50

2495 7.3 65

2538.7

20+00

T.P. 0.59 = 44.81 12.74 = 44.21

+70 P.O.C

Suggest 2 or 3 to 1 slope cut on North side for borrow and on South cut out to canon slope to grade

19

+50

70.1 / 200 Bot. canon 23.4 / 187

Set B.M. P.I. Hub 18+63.90 Δ = 32°27' Lt. 2.65 54.31

18

541 / 137 576 / 123

+50

17

56.96

22.5	23.6	24.9	24.6	24.8	24.4	24.1	23.1
17.3	8.1	2.9	1.2	2.0	1.4	1.7	2.7
80	50	30		35	70	90	97

44.81 / 5

22.3	24.4	25.6	25.7	25.3	25.4	25.6	25.2	25.1
3.7	14.6	4.5	1.3	1.7	2.1	3.4	1.8	1.9
100	60	36	20		42	56	69	100

22.5	24.2	25.4	25.6	25.7.0	25.5	25.6.9
31.4	12.8	2.7	0.8	0.0	0.5	0.1
100	60	33		30	60	100

23.6	24.3	25.8	25.4.8	25.5.0	25.5.3	25.5.5
33.4	15.7	4.2	2.2	2.0	1.7	1.5
100	60	33		35	70	100

20.5	21.7	22.4	23.3	25.0.9	25.2.7	25.3.2	25.4.6	25.5.0
5.5	4.3	3.6	1.7	0.1	0.3	3.8	2.4	2.0
150	120	90	60	30		30	60	100

20.6.7	21.9.8	22.9.7	23.6.7	24.2.7	24.8.8	25.2.5	25.3.5	25.4.5
50.3	37.2	27.3	20.3	14.3	8.2	4.5	2.5	2.5
111	72	48	34	17		24	40	100

21.5.8	21.2.9	22.1.3	23.1.0	24.1.2	25.0.0	25.3.0	25.3.6
41.2	44.1	35.7	26.0	15.8	7.0	4.0	3.4
100	75	50	25		29	20	100

22.1.8	22.1.0	23.0.6	23.6.8	23.6.4	24.7.1	24.9.9	25.2.3
35.2	36.0	36.4	30.2	20.6	8.9	2.1	4.7
80	71	47	21		26	52	80

56.96

22 + 10

+ 9C

+ 5C

21 + 29.26 E.C.

21

See P4

20 + 8C Sec. on prop. Line of Culv

+ 7r Rod of 3.7 Con & Hotwire Span
229.7 overhead

20 + 50

T.P. 1.07 r32.9C 17.9r r31.89
r44.81

L+ & RT

206.4	215.1	219.3	222.7	222.8	223.3	223.3	222.1	222.2
24.6	17.9	13.7	10.3	10r	9.7	9.7	10.9	10.8
70	30	7		7 St Pav.	30 N.L Pav.	40	44	55

205.1	212.4	217.9	221.0	223.7	223.7	224.1	223.0	
27.9	20.4	15.1	12.0	9.3	9.3	8.9	10.0	
80	50	25		6	14 St Pav.	36 N.L Pav.	64	

205.4	211.9	218.0	220.7	223.1	226.2	226.4	226.9	
27.6	21.1	15.0	12.3	9.9	6.8	6.6	6.1	
80	55	25		20	29	35 St Pav.	57 N.L Pav.	

204.3	209.3	213.7	217.0	221.5	221.3	222.5	
28.7	23.7	19.3	16.0	11.5	5.7	5.5	
80	50	25		26	38	43	= Scobe Pav.

181.6	197.1	203.5	207.9	211.9	219.0	219.9	230.3	
57.4	35.9	29.1	24.1	21.1	16.0	15.1	2.7	Shoulder of old Alignr.
100	80	40	17		30	21	64	

191.8	196.4	202.6	208.3	211.7	217.2	220.8	220.4	223.3	227.0
41.2	36.6	30.x	24.7	21.3	15.8	12.2	12.6	9.7	6.0
80	50	34	27		30	47	50	54	65

202.3	208.9	210.9	214.3	216.3	222.5	227.5	231.6	
30.7	24.1	22.1	18.7	16.7	10.5	5.5	1.4	
100	60	30		30	50	63	70	

218.8	219.2	220.5	220.0	221.6	224.3	226.4	230.0	
21.2	13.8	12.5	13.0	11.4	8.7	2.6	3.0	
100	50	25		30	50	66	75	

r32.9C
5

25+04 Could be C&G or could be filled south to old Ex. pav.

109.2 / 1.9 / 57 — 209.2 / 2.0 / 49 — N.L. Pav.

+91

+71

+50

24

T.P. 0.90 211.16 12.69 210.26

+50

23

22+47.48 Int. & of Ex. Pav.

T.P. P.O.T.
22+09.92 0.35 222.95 10.36 222.60
23.96

Lt — ℄ — Rt

209.21 / 1.95 / 57 — 208.7 / 2.5 / 40 — 201.01 / 10.1 / 28 — 199.6 / 11.6 — 198.8 / 13.4 / 30 — 194.1 / 17.1 / 60
N.L Pav. 54

206.1 / 5.1 / 44 — 203.3 / 7.9 / 35 — 202.4 / 8.8 / 28 — 204.4 / 6.8 / 18 — 200.6 / 10.6 / 9 — 202.5 / 8.7 — 204.7 / 6.5 / 3 — 203.3 / 7.9 / 30 — 201.4 / 9.8 / 60

209.2 / 2.0 / 55 — 206.6 / 4.6 / 34 — 205.9 / 5.3 / 15 — 202.7 / 8.5 / 6 — 204.9 / 6.3 — 204.2 / 7.0 / 30 — 201.7 / 9.5 / 60

210.53 / 1.63 / 60 — 208.2 / 3.80 / 42 — 207.4 / 4.0 / 22 — 206.4 / 11.8 — 205.5 / 5.7 / 30 — 203.9 / 7.3 / 60
N.L Pav.

210.7 / 0.5 / 58 — 210.3 / 0.9 / 28 — 209.4 / 1.8 — 209.3 / 1.9 / 30 — 208.5 / 2.7 / 55

211.16

213.87 / 9.08 / 63 — 213.50 / 9.45 / 41 — 219.5 / 9.5 — 212.6 / 10.4 / 30 — 213.4 / 9.6 / 55
Super. Here → 5L Pav. — N.L Pav.

215.3 / 7.7 / 60 — 216.1 / 6.9 / 49 — 216.87 / 6.08 / 38 — 217.05 / 5.90 / 15 — 216.6 / 6.4 — 216.7 / 6.3 / 30 — 216.1 / 6.9 / 55
5L Pav. — N.L Pav.

207.7 / 15.3 / 70 — 210.3 / 12.7 / 58 — 214.7 / 8.3 / 30 — 219.7 / 3.3 / 21 — 220.20 / 2.75 / 11.4 / 5L Pav. — 220.59 / 2.36 — 220.78 / 2.17 / 11.5 / N.L Pav. — 220.3 / 2.7 / 23 — 219.3 / 3.7 / 27 — 221.0 / 2.0 / 55

222.95

LT ℄ RT

27 + 08

27

+ 77.16 SL. Pav.

+ 31.18 Int. N.L. Pav.

+ 07

26

T.P 11.23 218.83 3.56 207.60

+ 50

Super El.

25 + 17

211.16

LT			℄					RT	
212.8	211.5	211.7	209.0	208.27	208.89	208.9	207.5		
6.0	7.3	7.1	9.8	10.58	9.94	9.9	11.3	206.7	
55	30		8	16 SL P	39	50	54	12.1 60	
213.0	211.9	211.0	210.7	209.7	208.35	208.91	208.7	207.3	206.8
5.8	6.9	7.8	8.1	10.1	10.48	9.97	10.1	11.5	12.0
55	48	30	6		12 SL Pav.	35 NL Pav.	47	51	60
215	212.5	211.0	210.2	209.1	208.63	208.96	208.8	207.2	206.3
5.3	6.3	7.8	8.6	9.7	10.20	9.87	10.0	11.6	13.5
60	50	44	15	11		24 NL Pav.	36	41	67
211.2	209.3	208.9	209.8	209.17	208.99	208.7	207.7	207.4	208.4	206.1
7.6	9.5	9.9	9.0	9.44	9.84	10.1	11.1	11.4	10.4	12.7
60	48	39	35	23 SL P		11	13	26	38	60
209.4	210.3	209.43	208.98	209.0	207.3	207.0	207.8	207.0	205.5
9.4	8.5	9.40	9.85	9.8	11.5	11.8	11.0	11.8	13.3
60	47	37 SL P	13 NL P		4	22	40	50	60
209.2	210.2	209.51	209.00	209.0	207.1	207.1	204.2		
9.6	8.6	9.32	9.83	9.8	11.7	11.7	14.6		
60	50	40 SL Pav.	16 NL Pav.	5		30	60		
			218.83						
210.04	208.99	208.9	205.1	205.2	203.4	200.7			
1.12	2.17	7.3	5.5	6.9	7.8	10.5			
56 SL Pav.	37 NL Pav.	28	22		30	60			
209.1	205.5	201.3	204.0	202.7	204.4	203.6	202.9	200.7	198.7
2.1	5.7	9.9	7.2	8.5	6.6	7.6	8.3	10.5	12.5
44 Top of old Pav.	38 Shoulder	25	17	13		30	40	50	60
			214.16						

Levels cont'd. Parr

Moore
Hoopes
5-23-47.

28+88.98 B.C.L.T.					
28+50					
27+00 B.M.	9.14	221.49		212.35	Spike in pole

See Grade Bk. for Elev. on Const. of Parr.

R.P. Hub	74.09 Rt.	Ex. Parr. align.	2.25	257.72	
R.P. Hub	33.79 Rt. of B.C.	249+47.67	2.06	257.91	
B.M. Pk. Hub 18+63.90 P 15	5.66	259.97		254.31	
28+0					
27+50					
27+00	Fd. B.M. spike in P.P. 2' Rt. of E		6.48	212.35	212.45

0.10

218.83

218.9 LT	216.9	E	214.3	210.9	210.4 R	207.4	207.3
2.6	4.6		7.2	10.6	11.1	14.1	14.2
50	25			30	35	40	50 Parr

219.6	218.2	216.3	212.2	211.7	208.0	208.1
1.9	6.3	5.2	9.3	9.8	13.5	13.9 S.L.
50	25		30	38	42	58 Parr

221.49

216.5	216.1	214.5	211.6	207.6	207.70	208.68
2.6	2.7	4.3	7.3	11.7	11.3	10.15
55	30		30	37	50 S.L. Parr	90 N.L. Parr

214.7	214.9	213.4	212.0	201.2	208.1	207.85	208.8
4.1	3.9	5.4	6.8	7.6	10.7	10.98	10.0
55	44	30		17	27	52 R	58 N.L.P.

218.83

Contd. from P. 6

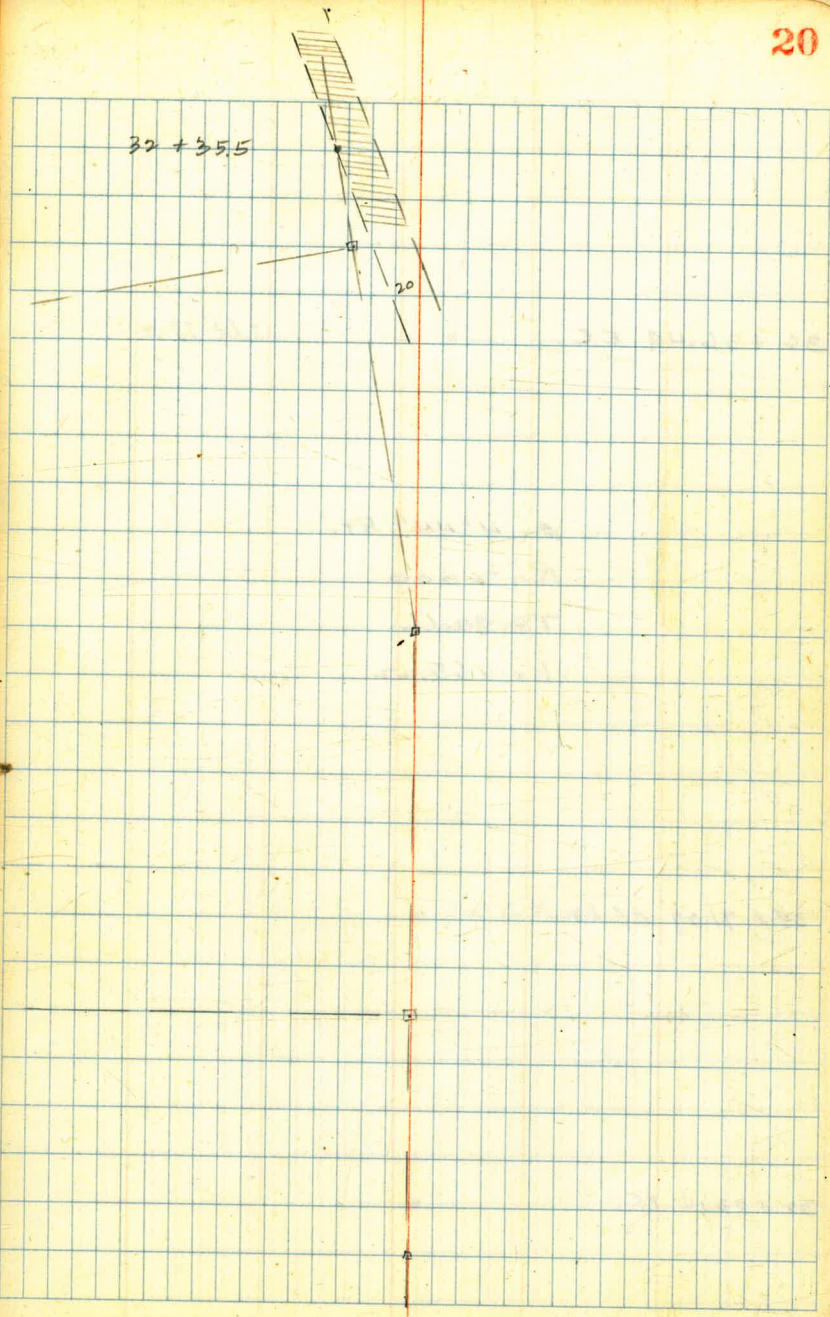
This align. has NOT yet been approved (34 Who)

32 + 03.14 EC S 58°38 W

Δ = 9°00' LT.
R = 2000
P.I. 30+46.38 T = 157.40
L = 314.16
0.859 = 1'
0°42.97 = 50'

28 + 88.98 BC LT.

28 + 52.52 POT

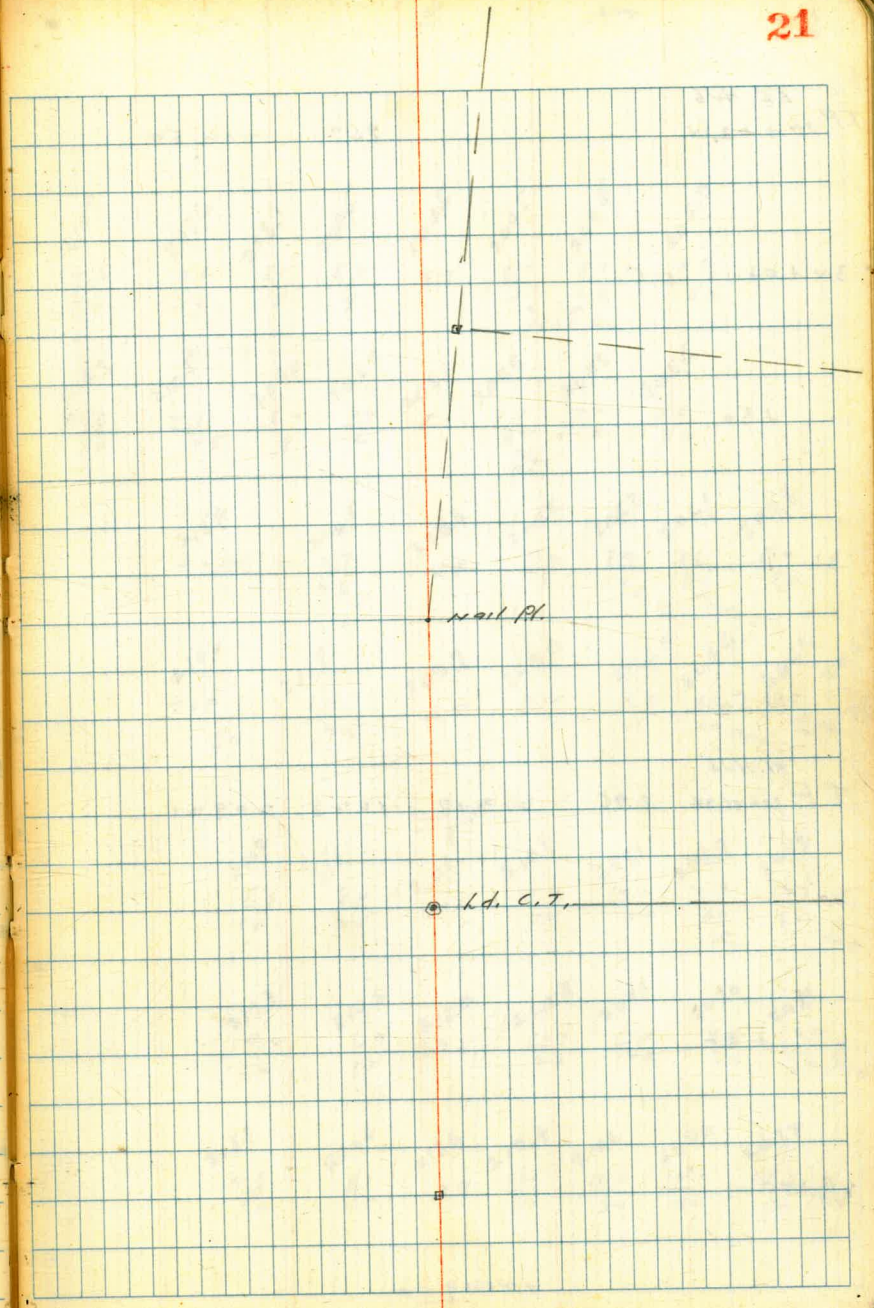


36 + 36.49 E.C. S 63° 22' W

Δ = 4° 44' Rt.
R = 2000
T = 82.66
L = 165.22

34 + 71.27 BC Rt.

32 + 03.14 EC.



E.C. Hub
T.P. 3N + 03.14 8.67 204.50

3N + 03.14 E.C.

+50

31

+50

R.I. Hub
T.P. 30+46.38 3.96 213.17 12.78 209.21

30

+50

N9+00

XX1.49

LT ℄ RT

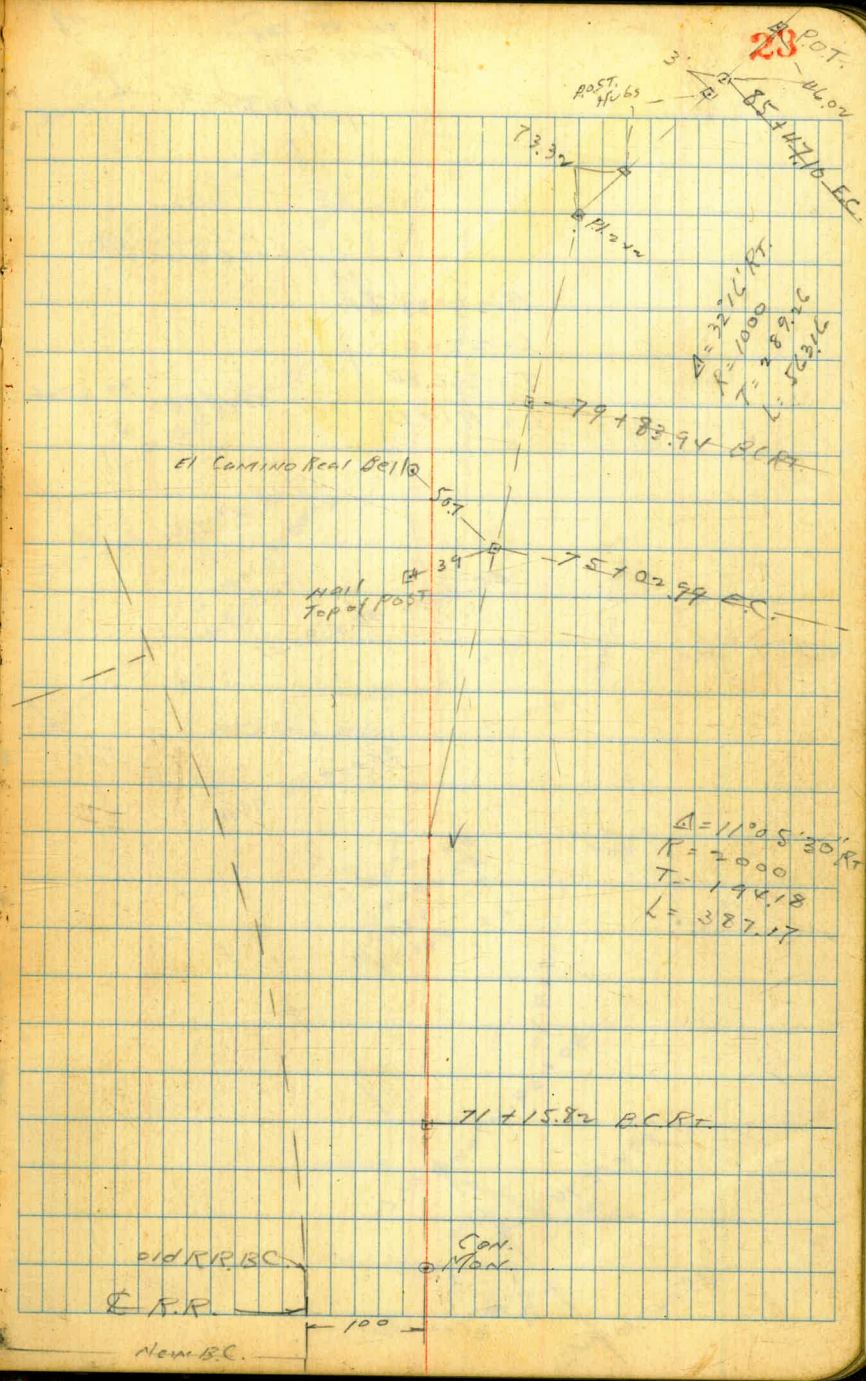
210.7	207.6	208.1	204.5	204.5	204.5	204.5	205.3
4.5	5.6	5.1	8.7	8.7	8.7	8.7	7.3
50	25	15	9		3	23	50
					20+40 P&V		
213.8	210.5	208.0	206.0	205.1	205.5	205.5	205.6
+0.6	2.7	5.2	7.2	8.1	7.7	7.7	7.6
50	25	9	6		8	28	50
					24 RAV		
215.4	210.5	208.3	206.2		206.2	206.1	204.8
+2.2	2.7	4.9	7.0		7.0	7.1	8.4
	25		1		14	32	50
					52 P&V	42 RAV	
214.2	211.8	209.7	209.0		206.5	206.6	206.6	206.2
+1.0	1.4	3.5	4.2		6.7	6.6	6.6	7.0
50	25		7		11	20	40	50
						P&V	P&V	
		213.17						
		5						
216.2	213.1	210.9	210.1		207.1	208.9	207.2
5.3	8.4	10.6	11.4		14.4	12.5	14.3
50	25		15		20	30	50
						P&V	P&V
217.3	214.6	212.0	210.8		207.3	207.0	207.3
4.2	6.9	9.5	10.7		14.2	14.5	14.2
50	25		23		28	40	50
							P&V
218.7	214.4	213.6	210.4		210.1	207.4	207.2
2.8	5.1	7.9	11.1		11.4	14.1	14.3
50	25		30		34	40	50
							P&V
		XX1.49					
		S					

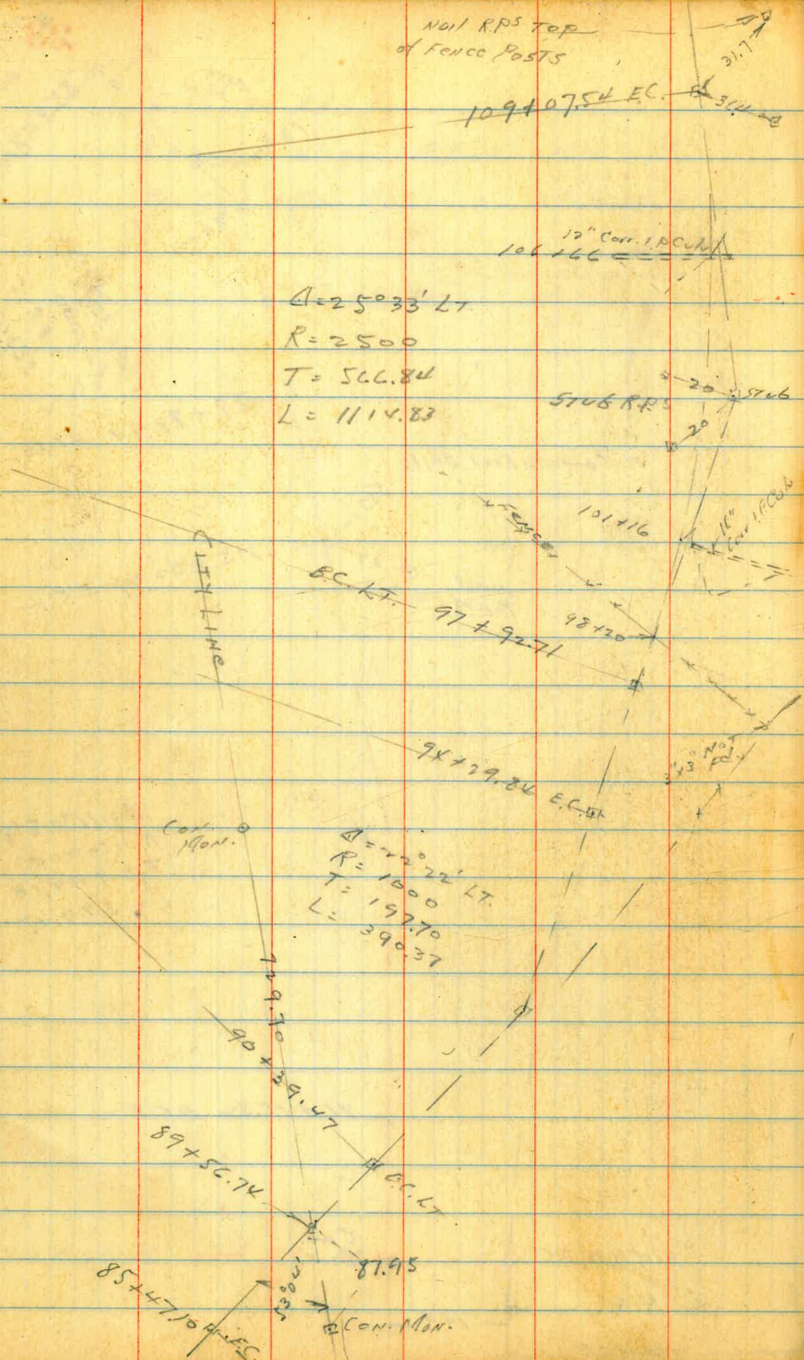
Sorrento Rd. Survey, Proposed 100' ROW
Change Align. PLAT 1367 M/y
to Del Mar Terrace Map 1547

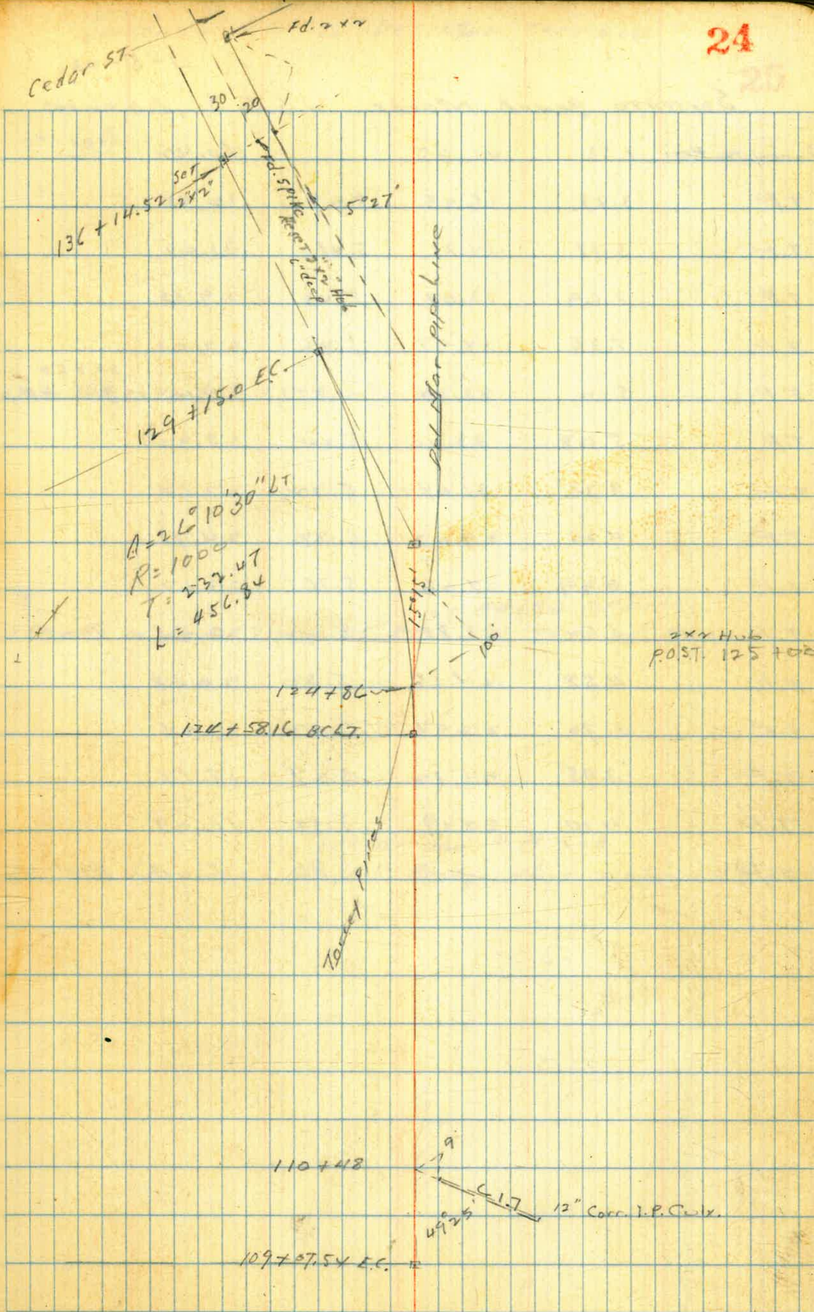
C. Moore
Southerneyer
W. Moore
11-1-43

3"x3" Hubs set

70+25.46 old B.C. F.B. 1498-16




Nail R.P.s Top of Fence Posts
109+07.54 E.C.
31.7
12" Corr. I.P. Culv.
106+66
Δ=25°33' Lt.
R=2500
T=566.84
L=1114.83
Stub R.P.s
20
Stub
101+16
Fence
11" Corr. I.P. Culv.
E.C. Lt.
97+92.71
98+20
City Line
94+39.84 E.C. Lt.
Con. Mon.
Δ=22°22' Lt.
R=1000
T=197.70
L=390.37
79.70
90+39.47
E.C. Lt.
89+56.74
87.95
85+47.10 E.C.
Con. Mon.


Fd. 2x4
Cedar St.
30
20
136+14.52
5°27'
129+15.0 E.C.
Δ=26°10'30" Lt.
R=1000
T=232.47
L=456.84
2x4 Hub
POST. 125+00
124+86
124+58.16 B.C. Lt.
110+48
12" Corr. I.P. Culv.
109+07.54 E.C.

11-5-43.

Sorrento Bench Marks U.S.G.S. Datum

Sorrento P.O.	1.53	41.95		40.42	Granite Mon.
T.P.	3.47	36.45	8.97	32.98	
T.P.	3.77	34.81	5.41	31.04	
T.P.	3.69	33.07	5.43	29.38	
T.P.	7.36	34.97	5.46	27.61	
T.P.	5.62	33.72	6.87	28.10	22+50 B.M. R.R.: Spike S.E. end of S. R.P. Bridge about
T.P.	5.08	33.40	5.40	28.32	
T.P.	3.36	31.04	5.72	27.68	
T.P.	4.32	29.03	6.33	24.71	
T.P.	3.99	27.26	5.76	23.27	
T.P.	3.62	25.88	5.00	22.26	B.M. RR Spike in Eucal. Tree 25' Rt. of 44+50 approx. S/y Tree of Row.
T.P.	4.58	24.66	5.80	20.08	
T.P.	3.70	22.98	5.42	19.24	
T.P.	3.95	21.62	5.27	17.67	
T.P.	4.10	20.19	5.53	16.09	
T.P.			3.86	15.00	B.M. RR Spike S.E. end of S. Fe Bridge # A 248 S. RR. Bridge about approx 69+20

Cross Section Chalcedony St.
Noyes St + Academy St.

Indexed
C.S.H.C.

26

June 22-44
Sisson
Bliss
Osborne

F.B. 2080
GL

Noyes St

Academy St (P 37)

Lamont St

Chalcedony St (P 27)

Noyes St (P 33)

Set Mon.

Fd Pipe

Board Fence

House

Open Ditch

Fd Pipe Capped

Lamont

Cross Section Chalcedony St.
Lamont to Hayes

1+20	✓ 20.5 Rt of ℄ = N 44½ Fence				
1+0	✓ 20' Rt = ℄ = S½ Power Pole				
0+50					
0+20	✓ 21.5 Lt of ℄ = N½ Tel Pole				
0+05					
0+0	= E.L. Lamont				
0-20	= E Curb Line Lamont				
BM			5.18	126.21	S.E. ℄ & ℄ Chalcedony & Lamont 126.03 CBH
TP	6.14	131.39	0.28	125.25	
TP	9.73	125.53	0.57	115.80	
BM	10.84	116.37		106.03	S.W. B.P. Diamond & Lamont

Reduced & Plotted
6-28-1944

June 22-44
Sisson
Bliss
Osborne

Lt = N ℄ Rt = S

27

126.9	126.1		125.3	125.2	124.2	123.7	123.2	
5.3 / 1.0	5.1 / 2.0		5.9	6.0 / 2.0	7.0 / 2.5	7.5 / 1.0	8.0 / 6.5	
128.1	127.7	126.0	126.2	126.1	125.6		124.9	
8.1 / 4.0	6.5 / 2.0	5.2 / 1.5	5.0	5.7 / 1.5	6.6 / 2.0		6.2 / 4.0	
129.7	128.6	126.3	126.1	126.3		125.8		
7.5 / 4.0	7.6 / 3.3	4.9 / 1.5	5.1	4.9 / 2.0		5.1 / 4.0		
129.5	126.94	127.27	126.14	125.33		125.88		126.1
5.7 / 4.0	4.39 / 2.0 - CB	4.91 / 2.0 Gutter	5.09	5.88 / 2.0 - Gutter		5.33 / 2.0 - CB		5.1 / 4.0
127.00	126.42	126.19	125.90	125.42		125.13		125.86
4.91 / 4.0 - CB	4.79 / 4.0 - Gutter	5.03 / 2.0	5.21	5.79 / 2.0		6.08 / 4.0 - Gutter		5.35 / 4.0 - CB

Bench Book.

131.21 used per AEB
131.39

4+0

3+50

+14 ✓16.7 Lt o/l - Hy Tel Pole

3+0

+95 ✓18.5 Rt o/l - Sly Pow Pole

TP 3.35 129.19 5.55 125.84

2+50

2+25 ✓19.8 Rt o/l - N Fly Fence

2+0

1+50 ✓19.5 Lt o/l - N/y Tel Pole

131.89

Lt. Z Rt

125.1	124.6	123.3	122.5	120.6	120.0
3.9 4.0	4.4 5.0	5.7	6.5 6.0	8.4 4.0	9.0 5.0
125.2	124.0	123.8	123.6	123.1	122.9
3.8 4.0	5.0 2.0	5.2	5.4 2.0	5.9 4.0	6.1 5.0
125.2	125.9	125.4	125.1	124.0	124.0	124.9	124.3
3.8 4.0	3.1 2.0	3.6 4.0	3.9 1.0	4.0 1.5	4.0 2.0	4.1 4.0	4.7 5.0
			129.19				
			129.01				
126.2	126.2	125.6	125.7	125.2	125.0
5.0 4.0	5.0 2.0	5.6	5.5 2.0	6.0 4.0	6.3 5.0
125.5	125.5	124.9	125.1	125.3	124.1	123.8
5.9 4.0	5.7 2.0	6.3 1.0	6.1	5.9 2.0	7.1 4.0	7.4 5.0
126.3	125.2	125.5	125.0	125.0	124.2	123.3	122.9	122.5
4.9 4.0	6.0 2.0	5.7 1.5	6.1 1.0	6.3	7.0 2.0	7.9 2.9	8.3 4.0	8.7 5.0
				131.21				
				131.39				

Chalcedony St

5+80				
TP	4.09	121.11	12.17	117.02
5+50				
5+0				
4+75				
4+50				
4+11				

129.19

Lt. | ℄ | Rt.

+5.19 / 114.99

11.6.2 | 11.3.2 | 11.2.1 | 111.4 | 110.4 | 110.1

1.7/50 | 5.9.4 Conc Pipe | 7.7/20 | 8.8 | 9.5/20 | 10.5/40 | 10.8/50

121.11 / 120.93

118.1 | 116.3 | 114.0 | 112.5 | 111.5 | 111.3

10.9/40 | 12.7/20 | 150 | 16.5/20 | 17.5/40 | 17.7/50

120.2 | 118.9 | 118.3 | 118.9 | 116.7 | 116.4

8.8/40 | 10.1/20 | 10.7 | 11.0/20 | 12.3/40 | 12.6/50

121.8 | 121.3 | 121.2 | 120.5 | 119.0 | 118.6

7.2/40 | 7.7/20 | 7.8 | 8.5/20 | 10.0/40 | 10.4/50

123.3 | 123.0 | 123.0 | 122.3 | 120.4 | 119.8

5.7/40 | 6.0/20 | 6.0 | 6.7/20 | 8.6/40 | 9.2/50

125.90

8.1/20 = 4.05 Conc Pipe

129.01

129.19

7+64.9 = BC on Lt.

7+53

7+50 = ℄ open Ditch Taken on Diagonal

7+45

7+0

6+50

6+0

121.11

Lt. ℄ Rt

	112.5	112.2	111.5	109.2	104.7	104.1
	8.4 / 40	8.7 / 20	9.4	11.7 / 20	16.2 / 40	16.8 / 50
			9.2			
108.6	108.3	107.9	107.3	105.6	104.8	104.2
13.2 / 45	12.6 / 42.8	13.0 / 21.4	13.6 (8.4 to Ditch)	15.3 / 21.4	16.1 / 42.8	16.7 / 65
112.7	112.5	112.4	111.7	111.9	109.4	107.8	107.8
8.2 / 50	8.4 / 40	8.5 / 20	9.2	9.0 / 15	11.5 / 20	13.1 / 40	13.1 / 50
112.6	112.5	112.2	112.1	112.3	109.4	108.6	108.4
8.3 / 50	8.4 / 40	8.7 / 20	8.8	8.6 / 15	11.5 / 20	12.3 / 40	12.5 / 50
112.7	112.6	112.6	112.5	112.5	109.9	109.5	109.2
8.2 / 50	8.3 / 40	8.3 / 20	8.4	8.4 / 15	11.0 / 20	11.4 / 40	11.7 / 50
113.2	112.5	112.3	112.2	111.8	110.3	109.6	109.4
7.7 / 50	8.4 / 40	8.6 / 20	8.7	9.1 / 15	10.6 / 20	11.3 / 40	11.5 / 50

121.11 (1209.3)

Chalcedony St.

9+00				
TP	12.44	155.75	0.73	143.31
8+75				
TP	12.41	144.04	0.89	131.63
8+649 = BC of Lt				
TP	11.91	132.52	0.50	120.61
8+25				
8+149 = ℄ of Academy St.				
7+899 = WL of Academy St to North				
		121.11		

Lt ℄ Rt.

139.7	140.6	142.4	147.1	145.3	143.2	142.4
1.59 50	1.50 40	1.45 30	8.5	10.3 20	12.4 40	13.3 50
			155.75	(155.57)		
127.6	128.7	133.7	136.7	139.5	140.4	140.2	139.7
1.63 50	1.52 40	10.2 20	7.2	4.4 20	5.5 30	6.7 40	4.3 50
			144.04	(143.86)		
122.8	123.3	128.2	131.8	134.3	138.2	138.3
9.55 50	9.0 40	4.1 30	0.5	+2.0 20	+5.9 10	+6.0 50
			132.52	(132.34)		
114.9	115.6	116.1	116.9	118.7	119.2
6.0 40	5.3 30	4.8	4.0 20	2.2 40	1.7 50
113.9	113.9	114.1	114.4	113.8	113.1
7.0 40	7.0 30	6.8	6.5 20	8.1 40	8.8 50
112.4	112.2	111.8	111.3	109.8	109.2
8.5 40	8.7 30	9.1	9.6 20	11.1 40	11.7 50
		121.11	(120.93)		

BM		234	158.74	2.81	New Point to Consider Chalcedon Arroyo
10+55.21 = BC of L1					
TP	757	161.08	2.24	158.51	
713	28.6 Rt = Sly Power Pole				
10+0					
9+50					
9+20					
9					

155.75

Lt. 4 Rt.

158.6	156.0	153.9	150.8	148.5	146.8	
2.3 / 40	4.9 / 20	7.0	10.1 / 20	13.1 / 40	14.1 / 60	
		161.08	(160.90)			
156.7	156.0	153.8	152.1	150.3	148.7	147.4
+1.1 / 60	+0.4 / 40	4.8 / 20	3.5	5.3 / 20	6.9 / 40	8.3 / 60
154.3	153.8	150.7	149.8	149.2	148.89	
5.3 / 60	4.8 / 40	4.9 / 20	5.8	6.4 / 20	6.68 / 8/15 = N/40	
150.0	151.0	149.4	148.5	147.5	146.1	145.4
5.6 / 60	4.6 / 40	5.2 / 20	7.1	8.1 / 20	9.5 / 40	10.3 / 60

155.75 (155.57)

Cross Section Noyes St.
N.L. Missouri to North of Chalcedony

Sta.					
+69 ✓	23.0 Lt of ℄ = Wly Anchor Pole				
1+50					
+25 ✓	23.3 Lt of ℄ = Wly of Power Pole				
TP	12.21	138.79	0.46	126.58	
+13 ✓	30.4 Rt of ℄ = Nly Lots				
+03 ✓	= ℄ 2.4 Conc Walk on Rt				
1+0					
+60 ✓	31.0 Rt of ℄ = Sly Lots Fence				
0+50					
0+0	= N.L. Missouri				
TP	12.88	127.04	0.25	114.16 (114.09 / 112.86)	
BM			1.46	112.95	Mon S.T.L. Missouri & Noyes
TP	12.92	114.41	0.30	101.49 — 101.40	
BM	10.42	101.79		91.37 (91.28)	SE Top Hyd Diamond & Noyes

F.B. 2080 / 62

Reduced & used (HI) 6-28-44
Plotted

Indexed

Lt = W ℄ Rt = E

June 24-44 **33**
Sisson
Bliss
Osborne Rod

Sta.								
1+50	130.7 8.0/40	131.0 7.7/20	129.5 9.2/17	130.2 8.5	129.7 9.0/5	131.3 7.4/10	131.0 7.7/20	130.6 8.1/40
1+0	125.7 1.3/40	126.8 0.2/23	124.7 2.3/16	124.8 2.2	124.8 2.2/20	125.3 1.7/40		
0+50	120.3 6.7/40	122.3 4.7/25	120.1 6.9/19	120.6 6.4	120.7 6.3/20	120.6 6.4/40		
0+0	117.2 9.8/40	118.5 8.5/22	116.9 10.1/18	117.2 9.8	117.1 9.9/20	117.7 9.3/40		

+03: 125.73 1.33 30.8 Rt Conc Walk; 125.60 1.35 40 on Walk

138.79 (138.70)

127.04 (126.95)

Note. These "BM" Not in Bench Books

Noyes

				use 158.56	
BM			1.77	158.65	N.W. Point Chalkdown & Noyes
TP	9.86	160.42	0.33	150.56	
2+94	✓ Sly 24" steel Culvert on Lt				
2+80					
2+67	= N'ly Pav on Rt.				
2+58	= E Pav on Rt.				
+46	23.5 Lt of ℄ = N'ly Power Pole				
2+43	= Sly Paving on Rt.				
TP	12.62	150.89	0.52	138.27	
2+0					
		138.79			

Lt. ℄ Rt.

149.38

1.42
20 = Sly 24" Steel Culvert

149.5	149.7	148.8	148.8	149.7	149.8
1.3 / 10	1.1 / 24	1.0 / 20	2.0	1.1 / 20	1.0 / 10

147.3	147.8	146.9	146.3	145.2	144.07	143.03
3.5 / 10	3.0 / 25	1.8 / 20	1.5	5.6 / 20	6.73 / 10 = N'ly Pav	7.77 / 90 = N'ly Pav

142.61

7.19
10 = N'ly Pav

143.7	144.1	142.2	142.5	144.3	144.14	143.14
7.1 / 40	6.7 / 24	8.6 / 18	8.3	6.5 / 20	6.66 / 10 = Sly Pav	7.66 / 90 = Sly Pav

150.89 (150.80)

136.9	137.4	135.6	136.3	135.7	136.8	137.3	136.1
1.8 / 10	1.3 / 23	3.1 / 17	2.4	4.6 / 5	1.9 / 7	1.4 / 20	2.6 / 10

138.79 (138.70)

Noyes St

1+50				
TP	12.44	182.87	0.75	171.43
1+0				
0+52.19	= BC Rt.			
TP	12.55	172.18	0.79	159.63
0+0	= N/L Chalcedony	Taken on Line Chalcedony		
3+20 ✓	= N/y 24" Steel Pipe on Lt			
3+07.62	= ℄ Chalcedony to West			

160.42

Lt. ℄ Rt.

172.7 172.5 172.8 172.8 172.2 172.6 172.4 172.2 173.1

11.1 11.6 11.0 11.0 11.6 11.3 11.4 11.6 10.7

183.78

167.6 167.7 167.3 167.7 167.5 169.0

4.5 4.4 4.8 4.5 4.6 6.1

163.12 163.5 163.5 163.1 163.3 162.6 164.9

8.97 8.6 9.6 9.0 8.8 9.5 7.7

25' Top of Pipe 25' Top of Pipe

172.18 (172.09)

159.1 159.1 159.0 157.8 157.5 158.3 158.3 158.1

1.2 1.2 1.3 2.5 2.8 2.0 2.0 2.4

152.91

7.47

Steel Pipe

154.0 153.5 152.8 153.7 153.3

6.3 6.8 7.5 6.6 7.0

160.42 (160.33)

Noyes St.

4+05.11 = BC				
3+68				
3+31.44 = E.C.				
TP	557	189.14	0.30	188.57
2+0				
2+50				
2+0				

188.87

St. St. PT

186.4	186.0	185.3	184.7	183.5
2.2 / 25	3.1 / 15	5.8	4.7 / 15	5.6 / 25
185.2	184.9	184.5	183.5	182.7
3.9 / 25	4.3 / 15	4.6	5.6 / 15	6.4 / 25
184.5	184.0	183.4	182.7	182.1
4.6 / 25	5.1 / 15	5.7	6.4 / 15	7.0 / 25
		189.05		
183.6	183.2	182.5	181.9	181.2
0.5 / 25	0.6 / 15	1.3	1.9 / 15	2.6 / 25
181.2	180.9	179.7	180.4	179.8
2.6 / 25	2.9 / 15	4.1	3.4 / 10	4.0 / 25
177.4	177.6	176.7	176.2	176.7
6.4 / 25	6.3 / 15	7.1	7.6 / 19	7.1 / 25

188.87 183.78

Cross Section Academy St.
Chalcedony to North of Law St.

indexed
E.J.R.

TP	10.79	134.37	2.56	123.58	
1+25					
1+0					
0+75					
0+50					
0+25					
0+0	: E.C. 25 N of N L Chalcedony				
BM	10.97	126.14		115.17	On Pipe 40' Lt 5+80 Chalcedony Page 29
				114.99	

Reduced Plotted 6-29-44

Lt: W — ℄ — Rt: E

June 26-44
Sisson
Bliss
Osborne

37

Sta.	Lt: W			℄	Rt: E			
1+25	116.4 9.6/50	117.8 8.2/25	119.6 6.4/15	122.3 3.7	125.0 1.0/15	128.5 +2.5/25 : W/ Level Area		
1+0	115.8 10.2/50	116.7 9.3/25	118.2 7.8/15	120.6 5.4	122.5 3.5/15	128.0 +2.0/25	128.4 +2.4/30	
0+75	115.3 10.7/50	116.1 9.9/25	117.2 8.8/15	118.7 7.3	121.1 4.9/15	126.0 0.0/25	127.6 +1.6/30 : W/ Level Area	
0+50	114.4 11.6/50	115.2 10.8/25	115.8 10.2/15	116.8 9.2	118.8 7.2/15	124.7 1.3/25	127.1 +1.1/30	
0+25	113.5 12.5/50	114.0 12.0/25	114.4 11.6/15	115.5 10.5	116.9 9.1/12	119.1 6.6/20	122.9 3.1/25	126.9 +0.9/30 : W/ Level Area
0+0	112.8 13.2/50	112.9 13.1/25	113.1 12.9/15	114.2 11.8	115.9 10.1/15	120.2 5.8/25	125.7 0.3/35 : W/ Fence	

126.14 (125.96)

Lt. Rt.

2+70

122.2 120.1
120 / 100 14.1 / 45

2+45

120.2 120.0
14.0 / 100 14.2 / 60

2+25

119.2 119.0 116.4
15.0 / 90 15.2 / 60 17.8 / 69

1+94.71 = B.C on Lt

118.3 116.6
15.9 / 60 17.6 / 69

1+75

1+50

134.37

Lt.						Rt.			
119.7	119.3	119.6	120.9	121.1	122.4	123.8	124.9	126.7	128.2
14.5 / 50	18.9 / 45 Bot Hash	14.6 / 69	13.2 / 25	13.1 / 15	11.8	10.4 / 15	9.3 / 25	7.5 / 25	6.0 / 30
114.1	118.3	119.6	120.3	121.8	124.5	125.1	126.8	128.4	
20.1 / 47 Bot Hash	15.9 / 33	14.6 / 25	13.9 / 15	12.4	9.7 / 15	9.1 / 25	7.4 / 25	5.8 / 30	
113.6	117.5	119.2	119.9	122.1		126.2	127.2	128.8	
20.6 / 37 Bot Hash	16.7 / 37	15.0 / 25	14.3 / 15	12.1		8.0 / 25	7.0 / 25	5.4 / 30	
113.9	117.9	118.7	120.4	122.8		127.2	129.1	130.2	
20.3 / 36 Bot Hash	16.3 / 31	15.5 / 25	13.8 / 15	11.4		7.0 / 20	5.1 / 25	4.0 / 30	
114.1	113.2	117.4	119.9	121.7	124.2	126.9	129.5	130.2	130.4
20.1 / 50	21.0 / 45 Bot Hash	16.8 / 38	14.3 / 25	12.5 / 15	10.0 / 0.0	7.3 / 15	6.7 / 20	4.0 / 25	3.8 / 30
114.7	119.7	121.1	123.7	126.9		128.9	130.0		
17.5 / 50	14.5 / 25	13.1 / 15	10.5	7.8 / 15		5.3 / 25	4.2 / 30		

134.37 (134.19)

BM			9.06	115.18	on pipe 10+47 51.86 Englewood Page 29
TP	0.67	124.24	10.80	123.57	
3+75					
3+50					
3+25					
3+0					

115.0

114.99

118.2	124.9	125.1	124.9	125.9	132.9	134.5	139.0
1.0 / 50	10.2 / 35	9.1 / 25	9.3 / 15	8.3	7.3 / 15	7.3 / 25	1.8 / 30
124.2	123.9	124.2	126.2	126.7	129.6	133.0	134.8
1.0 / 50	10.3 / 25	10.0 / 10	8.0	7.5 / 5	4.6 / 15	1.7 / 25	0.6 / 30
122.7	122.9	123.5	124.6	127.0	128.4	131.2	
1.5 / 50	11.3 / 25	10.7 / 15	9.6	7.2 / 15	5.8 / 25	3.0 / 30	
121.6	122.0	122.3	123.6	125.7	128.4	129.2	
1.4 / 50	1.2 / 25	1.9 / 15	1.0.6	8.5 / 20	5.8 / 25	5.0 / 30	

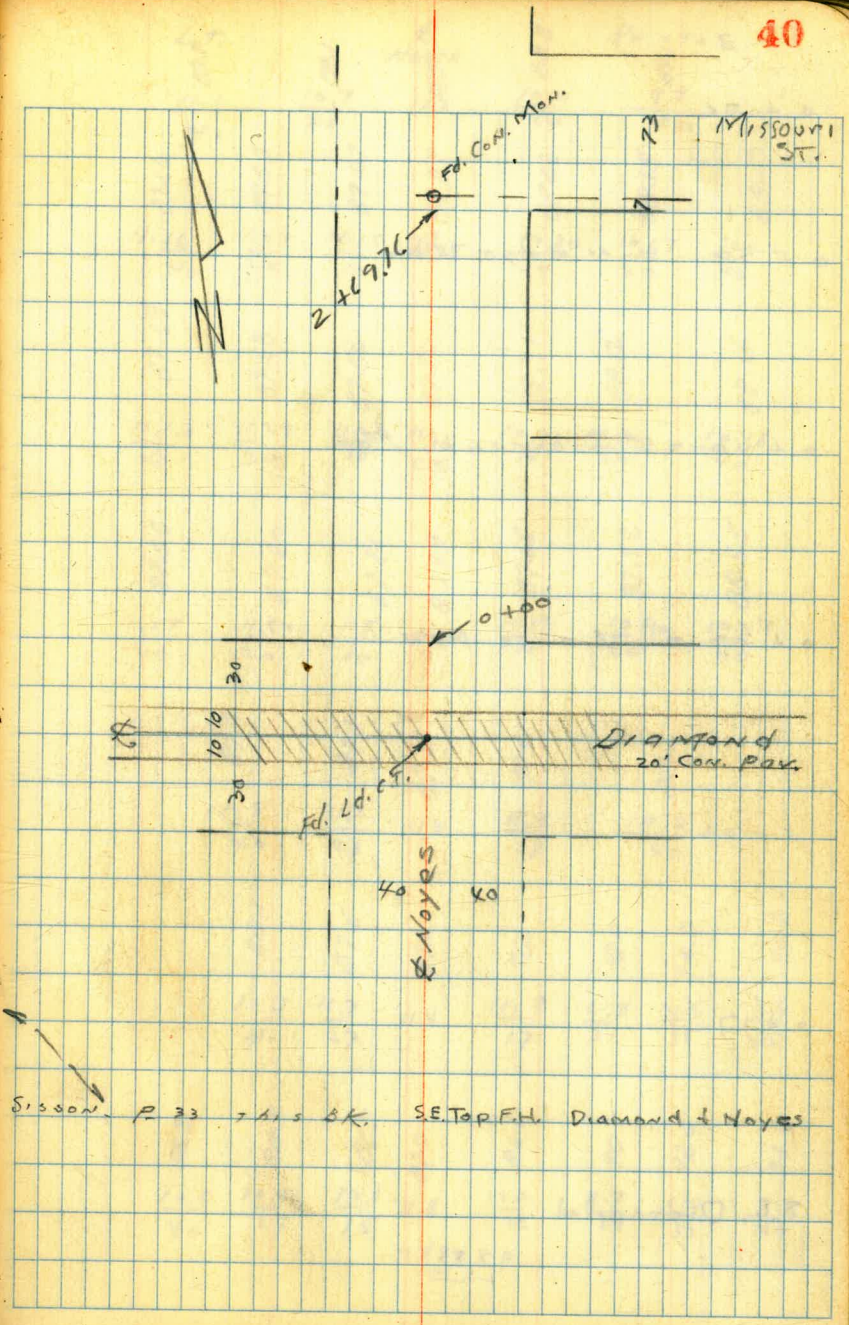
134.37

(134.19)

C.H. Moore
Sommermeyer

Indexed
C.S.K.

X sec Noyes St. 80' wide
Bagg.
4-11-46 Diamond to Missouri St.



	7.45	98.82		91.37	used Sisson
T.P.			3.49	91.39	91.37 = 0.02
T.P.	2.35	94.88	9.55	92.53	
T.P.	0.54	102.08	8.53	101.54	
old City B.M. SW BP	4.12	110.07		105.95	LaMont Diamond.

decified from USC+G = 106.03

Sisson P 33 7 41 5 B.K. S.E. Top F.H. Diamond & Noyes

LT. — ℄ Noyes — RT. = to E

Station								
0 + 56	11.1 / 40 — 87.7	10.7 / 20 — 88.1	10.1 — 88.7	10.0 / 20 — 88.8	9.7 / 40 — 89.1			
0 + 50 = N edge Pav.	11.16 / 40 — 87.66	11.27 / 20 — 87.55	11.15 / 10 — 87.67	10.95 — 87.87	10.80 / 10 — 88.02	10.67 / 20 — 88.15	10.22 / 40 — 88.60	
0 + 40 = ℄ Diamond Pav.	11.13 / 40 — 87.69	11.29 / 20 — 87.53	11.26 / 10 — 87.56	11.06 C.T. — 87.76	10.91 / 10 — 87.91	10.70 / 20 — 88.12	10.18 / 40 — 88.64	
0 + 30 = S. edge Pav.	11.27 / 40 — 87.55	11.52 / 20 — 87.30	11.51 / 10 — 87.31	11.33 — 87.49	11.17 / 10 — 87.65	10.90 / 20 — 87.92	10.27 / 40 — 88.55	
0 + 20	11.5 / 40 — 87.3	11.7 / 23 — 87.1	11.3 — 87.5	11.4 / 18 — 97.4	10.6 / 40 — 88.2			
0 + 17	10.7 / 40 — 88.1	11.3 / 22 — 87.5	11.4 — 87.4	11.9 / 17 — 76.9	6.8 / 21 — 92.0	4.5 / 31 — 94.3	3.6 / 40 — 95.2	
S.L. Diamond	10.6 / 40 — 88.2	10.5 / 25 — 88.3	12.1 / 15 — 86.7	11.8 — 87.0	12.2 / 16 — 86.6	8.7 / 17 — 90.1	6.2 / 31 — 92.6	5.6 / 40 — 93.2

98.82

98.82

2+00

10.32 118.13

T.P. — 108.82 1.01 107.81

1+34.98 = ℄ Alley

+24 21° Lt = ctr. 14" P. Pole

1+19 45° Rt = ℄ door. 20' wide house

1+05 = 40 Rt = End batt fence

1+00 30° Rt. = double pepper tree

+75 30° Rt = ctr. 1' Pepper tree

+64 30° Rt = ctr. 1' Acacia tree.

0+51 - start batting fence - 40' Rt.

T.P. 11.20 108.82 1.20 97.42

N L Diamond = 0+00

+63

98.8±

09.0 L+ 10.4 09.0 09.4 08.9 09.9 10.0

9.1/40 7.7/17 9/14 8.7 9.2/14 8.7/19 8.1/40

05.3 06.5 05.2 05.8 05.6 06.3 06.4

3.5/40 2.3/17 3.6/13 3.0 3.2/13 2.5/18 2.4/40

04.2 05.5 04.3 04.2 04.4 05.6 05.6 05.77

4.6/40 3.3/17 4.5/13 4.1 4.4/12 3.2/30 3.2/40 3.05/45

03.6 05.2 02.8 03.2 03.0 04.4 05.3

5.2/40 3.6/17 6.0/12 5.6 5.8/12 4.4/16 3.5/40

01.5 02.5 01.1 97.8 97.6 97.8 00.7 02.4 02.3 02.8

7.3/40 6.3/31 7.7/24 11.0/9 11.2 11.6/12 8.1/16 6.4/22 6.5/40 6.00/45

Start asphalt walk

108.82

95.8 97.5 97.7 91.4 91.4 98.5 99.3

3.0/40 1.3/10 7.1/13 7.4 7.1/16 0.3/23 +0.5/40

94.2 95.3 89.5 89.5 89.8 97.3 97.9

1.6/40 3.5/10 9.3/13 9.3 9.0/17 1.5/27 0.9/40

98.8±

Mon. ₵ Noyes Sou'th Line Missouri
See page 33. 5.17 112.96

118.13

S. Line + 60

S. Line + 40 = ₵ Missouri St.

S. Line + 20

2+67.76 S. Line Missouri St

2+35

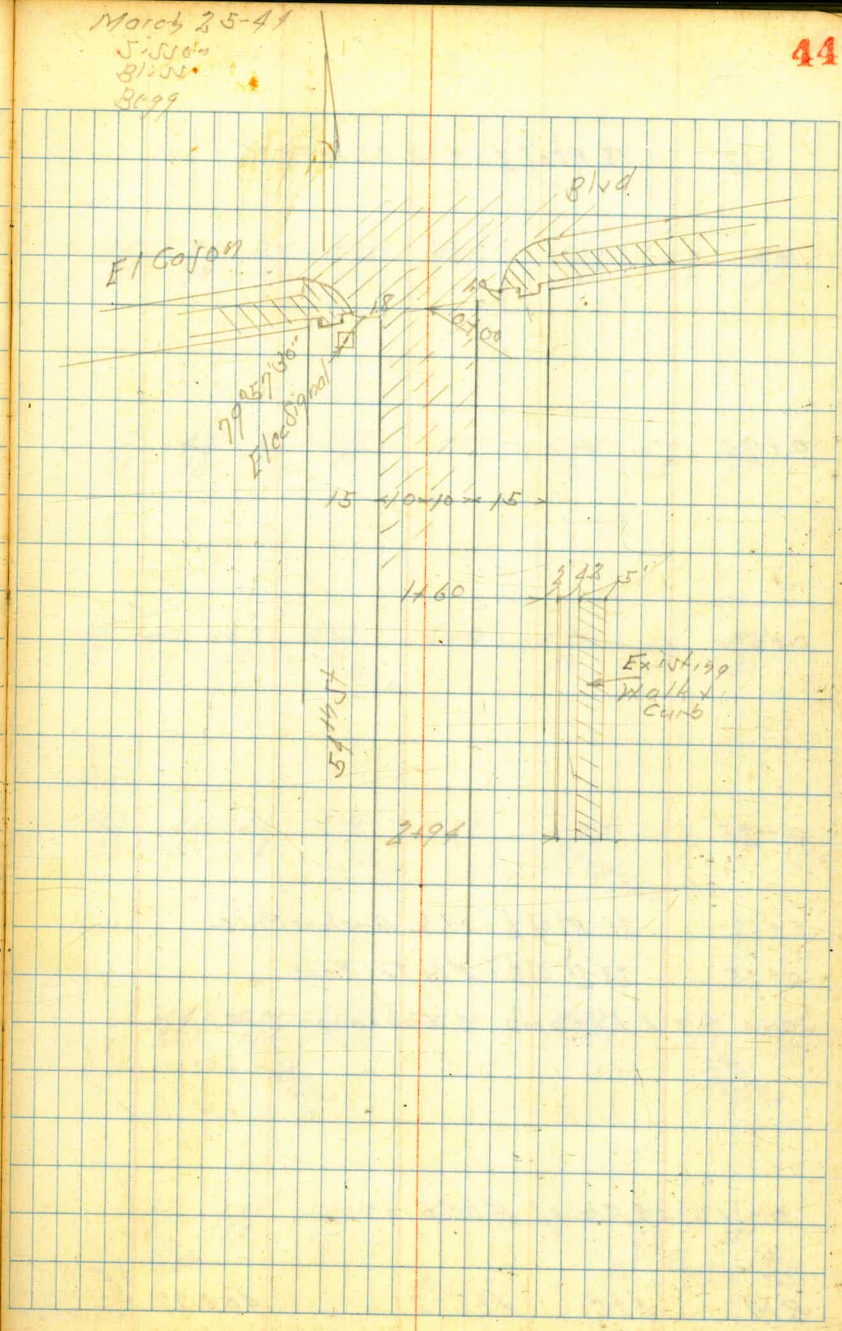
118.13

S. Line + 60			2.3/40 (15.8)		2.3/20 (15.8)	2.1 (16.0)		2.1/20 (16.0)	2.2/40 (15.9)
S. Line + 40			3.3/40 (14.8)		3.3/20 (14.8)	3.3 (14.8)		3.3/20 (14.8)	3.4/40 (14.7)
S. Line + 20			5.0/40 (13.1)		4.5/20 (13.6)	4.3 (13.8)	4.4/20 (13.7)	4.1/40 (14.0)	
2+67.76	6.1/40 (12.0)	5.5/30 (12.6)	Ctr 12" R.P. 22	4.4/17 (13.7)	5.3/17 (12.8)	5.3 (12.8)	5.7/13 (12.4)	4.9/20 (13.2)	4.9/40 (13.2)
2+35	7.5/40 (10.6)	7.0/30 (11.1)	5.5/18 (12.6)	7.1/15 (11.0)	7.0 (11.1)	7.4/13 (10.7)	6.0/19 (12.1)	6.2/40 (11.9)	

Cross Section Sta 455
300' South of El Cajon Blvd
Level next Page

Indexed
C.S.K.

March 25-44
5355 Blvd Bridge



1+12 18 Rt of ℄ = 2 12" Olive Tree

1+0

0+75

0+50

0+25

6+18 21' Rt of ℄ = W.L. Anchor Pole

0+15 28' Lt of ℄ = E.L. Tel Pole

0+0 = S L E/Cajon Taken on Diag

0-10 = S C6 of E/Cajon

BM 425 408.02 403.77 SE B.P. E/C 4107 +5 ft S.

Lt = E ℄ Rt = W

4.5 / 2.5	4.5 / 1.9	5.0 / 1.7	5.22 / 1.0	5.65	5.72 / 1.0	5.7 / 1.5	5.8 / 2.5
4.6 / 2.5	4.8 / 1.8	5.5 / 1.7	5.48 / 1.0	5.31	5.44 / 1.0	5.7 / 1.5	6.2 / 2.5
4.3 / 2.5	4.7 / 1.7	5.7 / 1.6	5.62 / 1.0 = E¼ Pav	5.49	5.66 / 1.0 =	5.6 / 1.5	5.8 / 2.5
4.3 / 2.5	4.3 / 1.6	5.6 / 1.5	5.79 / 1.0 = E¼ Pav	5.82	5.92 / 1.0 = W¼ Pav	5.9 / 1.5	5.7 / 1.6	5.3 / 2.5
4.4 / 2.5.3	5.17 / 1.5.5	5.63 / 1.5.5	5.70	6.22 / 1.5.6	5.75 / 1.5.6 = C6 5.5a	6.2 / 2.5.3
4.36 / 2.1 - C6.8c 7.0p	5.00 / 4.4	5.54 / 1.5	5.97	6.51 / 1.6	7.14 / 2.7 - Gully c.	6.51 / 2.7 - C6.8c 7.0p

408.02

1

1+25

1+50

1+75

2+00

2+25

+43 23' Rt of ℄ = Wly Power Pole

+87 19' Rt = ℄ = 29" Oliver Tree

408.02

℄ ℄ Rt

403.26
4.76 5.38 5.52 5.61 5.47 5.55 5.9 4.7 4.9
27 27 25 10 10 16 18 25
27-Cb

403.97
4.05 4.7 4.6 5.02 4.81 4.87 5.2 3.7 4.0
27 27 25 10 10 15 20 25
27-Cb

404.18
3.84 4.4 4.4 4.81 4.71 4.85 5.2 4.7 4.8
27 27 25 10 10 15 20 25
27-Cb

404.10
3.74 3.92 4.3 4.78 4.72
3.64 27 27 10
3.54 27-Wly Top
Wall Conc Cb

3.5 3.7 4.4 4.87 4.77 4.90 5.3 4.7 4.9
25 23 22 10 10 15 19 25

4.4 4.7 5.01 4.90 5.65 5.9 5.7
25 19 10-Ely Rev 10-Wly Rev 18 25

408.02

2+00

2+94 = Sly Cb y Walk on Lt

2+75

+58 185Rt of Z = L 8" Olive Tree

2+50

408.02

Lt Z Rt

9.0 8.80 8.68 8.79 9.3 6.1
25 10 10 19 25

400 16
9.86 8.6 8.6 8.44 8.84 8.47 9.1 5.7
27=Cb Trd 27 25 10 10 19 25

401 19
6.83 7.4 7.5 7.54 7.43 7.58 8.1 5.3
27=Cb 27 25 10 10 17 25

402 30
5.72 6.3 6.4 6.54 6.41 6.53 7.0 4.3 4.2
27=Cb 27 25 16=Fir 10=White 16 17 25

408.02

Levels on curb & paving on Via Del Norte at old R R Xing

Moore
Walker
Hazard
Reed
6-22-42

NWBP	10.69	90.56		City datum 79.87 La Jolla Blvd & del Norte
	0 to Ely Comm'l.		Sly curb = Sta. baseline	
S cb			4.93	85.63
gut			5.20	85.36
c			4.67	85.89
gut			4.90	85.66
N cb			4.57	85.99
	0+15			
N cb			3.93	86.63
gut			4.46	86.10
c			4.18	86.38
gut			4.69	85.87
S cb			4.37	86.19
	0+30			
S cb			2.77	87.79
gut			3.30	87.26
c			2.91	87.65
gut			3.35	87.21
N cb			2.84	87.72
T.P.	11.85	101.98	0.43	90.13

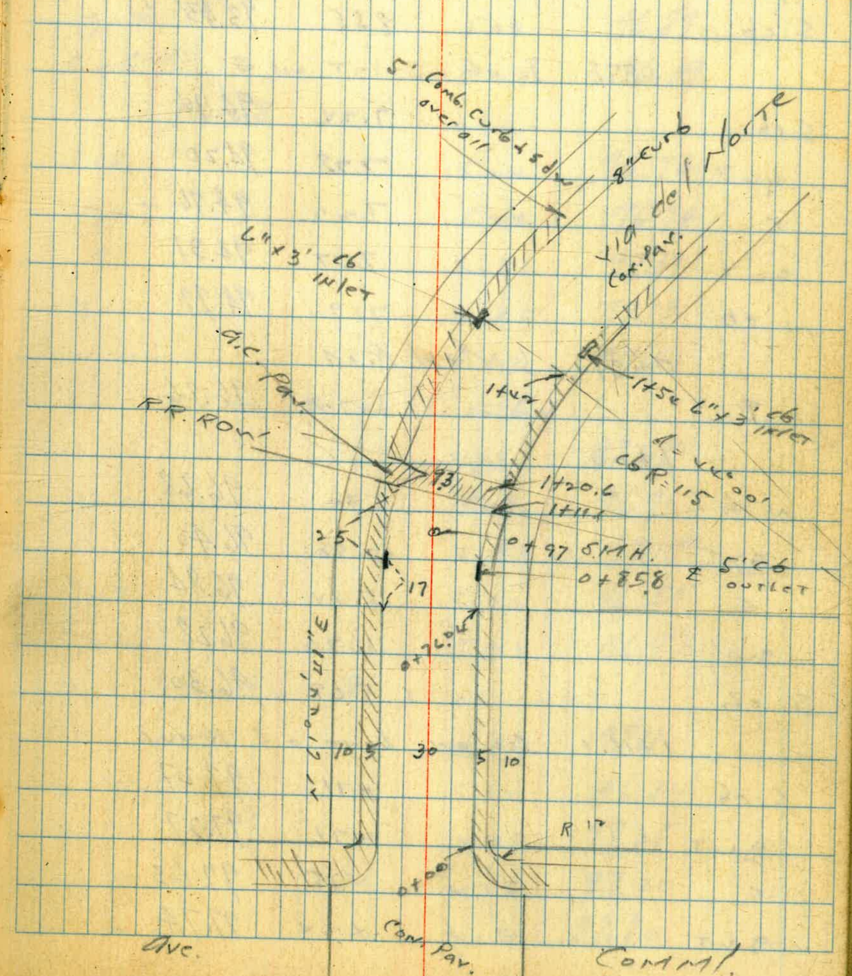
Green Profile B-28-1942 C.B.Hough

Red. & Plotted (onion skin) 6/26/42 (W)

Indexed
C.S.K.

Note! See Tel & power Conduit

This El. from USC&G Circ approx. 0.34 dif. from old



0+760 v P.C.		
N c6	8.55	93.43
gut	9.14	92.86
c	8.67	93.31
gut	9.11	92.87
S c6	8.55	93.43
0+858 ℄ c6 outlet on S		
S c6	7.24	94.74
gut	7.78	94.20
c	7.22	94.76
gut	7.67	94.31
N c6	7.19	94.79
0+97 S.M.H. Rim		
℄	5.74	96.26
1+00		
N c6	5.30	96.68
gut	5.58	96.40
c	5.14	96.84
gut	5.70	96.28
S c6	5.68	96.30
1+11.1 Sec on Line of Row		
S c6	4.71	97.27
gut	4.71	97.27
c	4.35	97.63
gut	4.24	97.74

N c6	4.24	97.74
1+20.6 Sec of Line of Row		
N c6	4.56	97.42
gut	4.56	97.42
c	4.71	97.27
gut	5.09	96.89
S c6	5.09	96.89
1+28		
S c6	5.24	96.74
gut	5.24	96.74
c	4.81	97.17
gut	4.85	97.13
N c6	4.47	97.51
1+42 ℄ 3' c6 outlet		
N c6	4.33	97.65
gut	5.07	96.91
c	4.83	97.15
gut	5.40	96.58
S c6	5.01	96.97
1+52 ℄ 3' c6 inlet		
S c6	4.87	97.11
gut	5.64	96.34
c	4.73	97.25
gut	4.78	97.20
N c6	4.18	97.80

10.1.98

1464.35 EC

N ob			3.93	98.05
gut			4.53	97.45
C			4.55	97.43
gut			5.35	96.63
S ob			4.84	97.14
	2400			
S ob			3.57	98.41
gut			4.19	97.79
C			3.50	98.48
gut			3.55	98.43
N ob			2.96	99.02
T.P.	3.89	97.12	8.35	93.63
TP	4.91	96.73	5.30	91.82
T.P			3.84	92.87

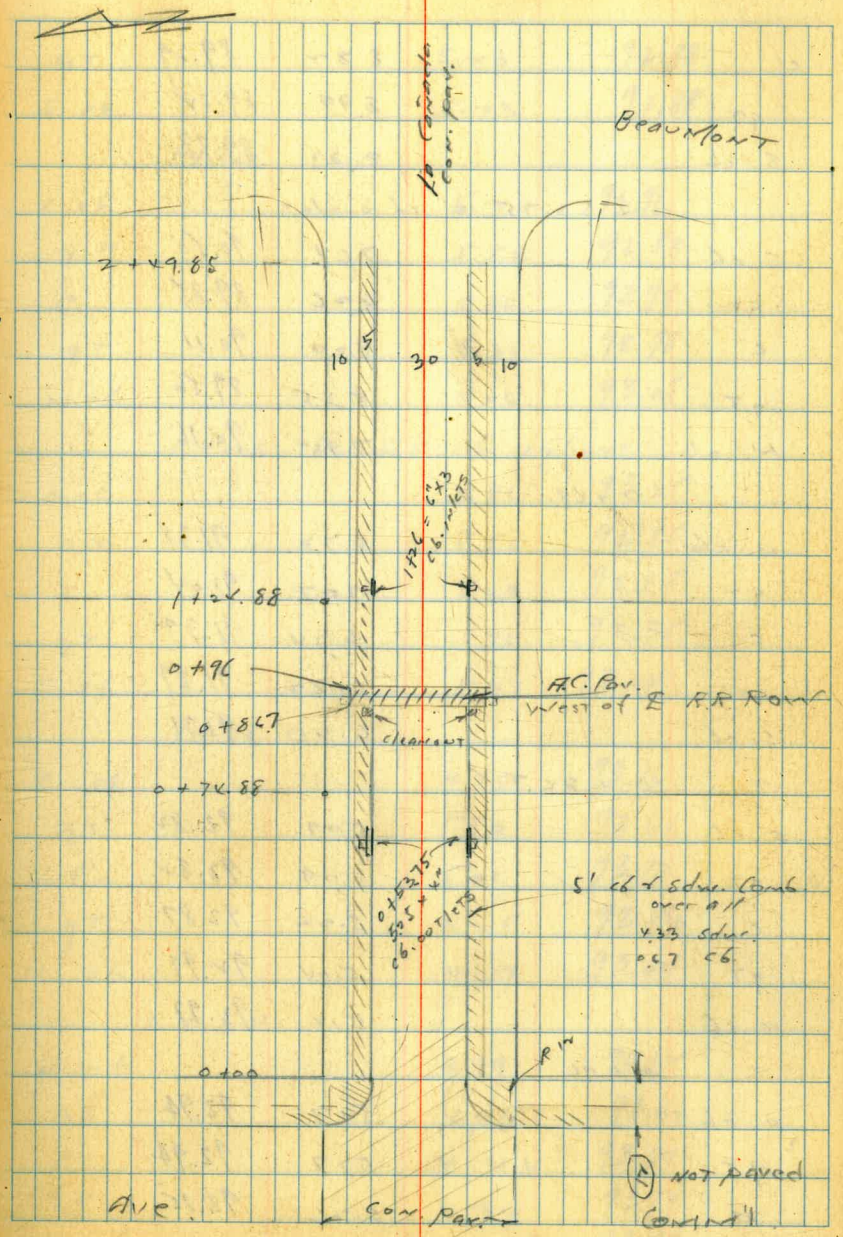
Levels on Curbs at old
R.R. Xing on La Cañada
NL = Sta. Baseline.

T.P. PSI	5.24	98.11	92.87
0+00 EL Comm'l.			
S c6		12.27	85.84
gT		12.71	85.40
C		12.67	85.44
gT		13.28	84.83
N c6		12.87	85.24
0+10			
N c6		12.00	86.11
gT		12.64	85.47
C		12.01	86.10
gT		12.07	86.04
S c6		11.41	86.70
0+35			
S c6		10.07	88.04
gT		10.76	87.35
C		10.64	87.49
gT		11.23	86.88
N c6		10.57	87.54
0+45			
N c6		8.74	89.37
gT		9.42	88.69

Green Profile 1"=40' 9-3-1941 C.D.H.

Indexed
C.S.K.

52



c	8.8~	89.29
gT	8.99	89.12
S c6	8.33	89.78
0+53.75 = c6 outlet		
S c6	7.61	90.50
gT	8.06	89.85
c	8.00	90.11
gT	8.55	89.56
N c6	7.95	90.16
0+68		
N c6	6.73	91.38
gT	7.07	91.04
c	6.74	91.37
gT	6.8~	91.29
S c6	6.40	91.71
0+86.7		
S c6	5.79	92.82
gT	5.79	92.82
c	5.84	92.87
gT	5.1~	92.97
N c6	5.1~	92.97
0+96		
N c6	5.17	92.94
gT	5.17	92.94
c	5.26	92.85

gT	5.~3	92.88
S c6	5.~3	92.88
1+10		
S c6	5.~0	92.91
gT	5.58	92.53
c	5.36	92.75
gT	5.33	92.78
N c6	5.06	93.05
1+26 & 5.5 c6 inlets		
N c6	4.86	93.25
gT	5.56	92.55
c	5.~3	92.88
gT	5.76	92.35
S c6	5.07	93.04
1+36		
S c6	4.95	93.16
gT	5.50	92.61
c	5.01	93.10
gT	5.~5	92.86
N c6	4.67	93.44
1+50		
N c6	3.99	94.1~
gT	4.45	93.46
c	4.44	93.67
gT	4.9~	93.19
S c6	4.35	93.76

98.11

	1+60			
S c6			3.70	94.41
QT			4.3x	93.79
C			3.90	94.21
QT			4.07	94.04
N c6			3.4x	94.70
	1+77			
N c6			x.xo	95.91
QT			x.87	95.24
C			x.cx	95.49
QT			3.10	95.01
S c6			x.x9	95.6x
	2+00			
S c6			0.7x	97.37
QT			1.37	96.74
C			0.9x	97.17
QT			1.x3	96.88
N c6			0.53	97.58
T.P.	10.39	108.10	0.40	97.71
	2+x5			
N ck			8.78	99.3x
QT			9.39	98.71
C			9.09	99.01

108.10

QT			9.5x	98.54
S c6			8.9o	98.xx
	2+x6 approx PC Curb Beginning			
S c6			7.39	100.71
QT			7.89	100.21
C			7.6x	100.48
QT			7.93	100.17
N c6			7.87	100.73
	2+x9.85 = Prop PC or			
N c6			7.1x	100.99
QT			7.7x	100.36
C			7.8	100.7x
QT			7.6x	100.46
S c6			7.10	101.00
T.P.	o.c6	104.93	3.x3	10x.87
T.P.	o.03	9x.89	10.37	9x.5c
T.P.	o.99	8x.96	1x.cx	81.97 = T.P. for Camino Costa
check to Ext. B.P. w c6 of La Jolla Blvd. 1x5' S. of Camino de la Costa			6.7x	7c.xx
				75.84 = ohc7x El.
Reduced from USC&G				76.18

Indexed
C.S.K.

55

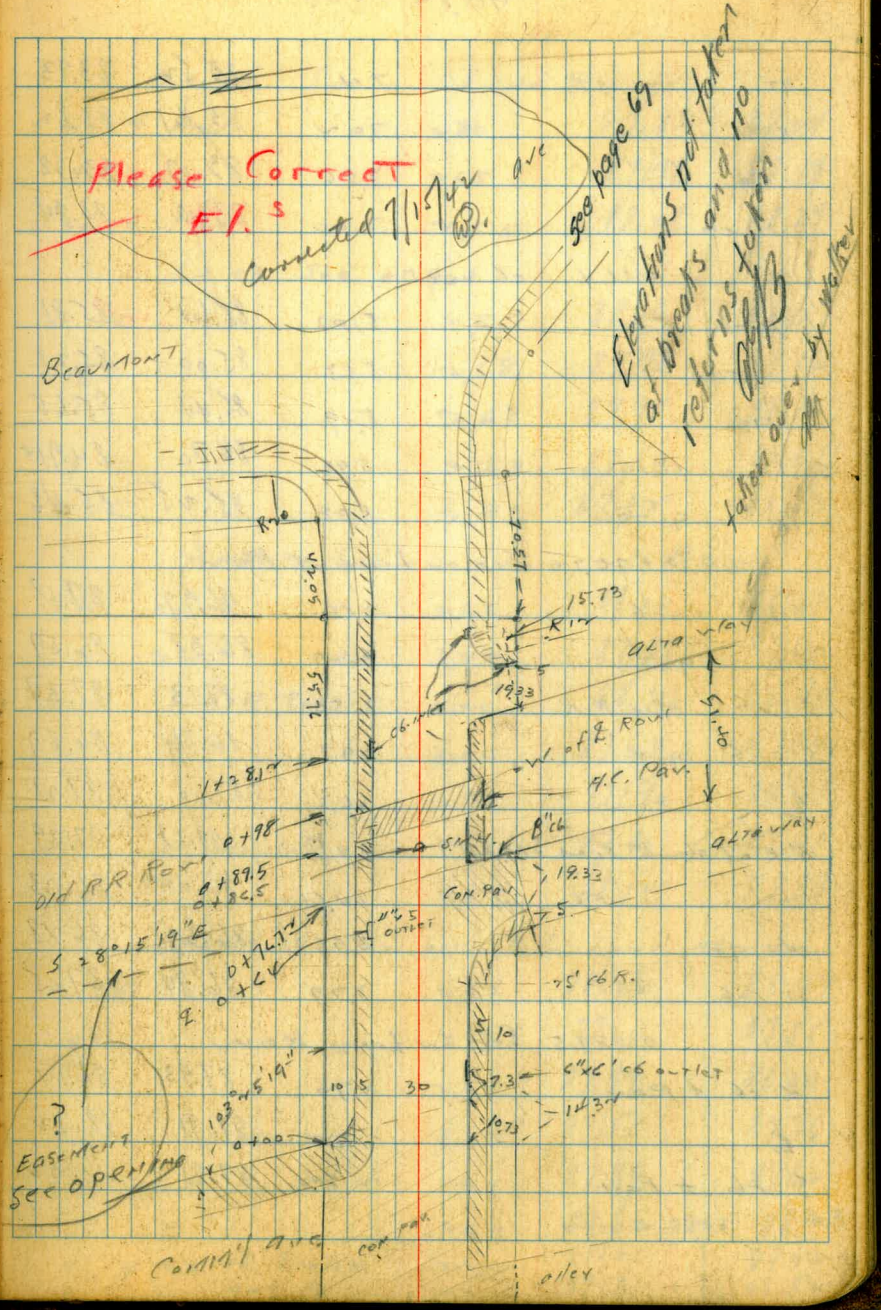
Cerritos de la Costa

Levels, Contrl. to Beaumont

for change of grade at R.R. Xing

N.L. = Sta. Baseline

T.P. p. 54	8.87	90.8x ~~90.63~~	Fly Contrl Over	81.97 ~~81.76~~ ← N.G.	
	0+00	Sec at 90°			
N c6			11.03	79.60	79.81
gT			11.49	79.14	79.35
c			11.01	79.57	79.78
gT			11.0x	79.61	79.8x
S c6			10.3x (Comm)	80.29	80.50
	0+00	Sec. on Line			
S c6			9.80	80.83	81.04
gT			10.43	80.20	80.41
c			10.66	79.97	80.18
gT			11.49	79.14	79.35
N c6			11.03	79.60	79.81
	0+19	at 90°			
N c6			9.52	81.11	81.32
gT			10.14	80.49	80.70
c			9.65	80.98	81.19
gT			9.83	80.80	81.01
S c6			9.1x	81.49	81.70
	0+42	Sec			
S c6	approx. PC. Curb		6.45	84.18	84.39



~~90.63~~
90.84

QT	7.11	83.52	83.73
C	7.02	83.61	83.82
QT	7.56	83.07	83.28
N c6	7.00	83.63	83.84
0+64 : c6 outlet			
N c6	5.03	85.60	85.81
QT	5.63	85.00	85.21
C	5.19	85.44	85.65
So. Line curb	5.93	84.70	84.91
" QUT	5.38	85.25	85.46
0+76.72 Sec on Line of Row			
SL curb	3.66	86.97	87.18
SL QUT	4.15	86.38	86.59
S c6 Mid. 3'R	3.50	87.13	87.34
S c6 QUT	3.97	86.66	86.87
℄	3.63	87.00	87.21
3' E of above R in SMH	3.45	87.18	87.39
" " " FL "	14.61	86.02	86.23
N QT	3.96	86.67	86.88
N c6	3.79	86.84	87.05
0+89.5 Sec on Line Row			
N c6 + Pav	2.70	87.93	88.14
℄	2.72	87.91	88.12
S c6 + Pav	2.82	87.81	88.02

~~90.63~~
90.84

56

0+98 Sec on Line Row			
S c6 + Pav	2.80	87.83	88.04
℄	2.65	87.98	88.19
N c6 + Pav	2.55	88.08	88.29
1+13 Sec at 96			
N c6	2.57	88.06	88.27
QT	2.68	87.95	88.16
C	2.68	87.95	88.16
QT	2.83	87.80	88.01
S c6	2.81	87.82	88.03
1+41.17 Sec on Line of Row			
SL curb	2.63	88.00	88.21
SL QUT	3.24	87.39	87.60
S c6 E 3' R Rot.	2.40	88.23	88.44
" QUT	3.00	87.63	87.84
C	2.73	87.90	88.11
QT E.L. INLET	3.23	87.40	87.61
N c6	2.51	88.12	88.33
1+48.48 Sec on E/L Line 4Th Way			
N c6	2.37	88.26	88.47
QT	2.99	87.64	87.85
C	2.64	87.99	88.20
S QUT in Valley	3.08	87.55	87.76
SL QUT	3.24	87.39	87.60
" c6	2.61	~~88.02~~ 88.03	88.23
" + 2.3 c6. E INLET	2.60	88.01	88.22
" " QUT FL "	3.32	87.31	87.52

~~90 C3~~
90.8 ℄

57.

1+77.5 at 90°

S C6	2.30	88.33	88.54
S QT & 3 C6 inlet	3.10	87.53	87.74
C	2.40	88.23	88.44
QT	2.72	87.91	88.12
N C6	2.15	88.48	88.69

1+83.88 PC, at 90°

N C6	2.03	88.60	88.81
QT	2.64	87.99	88.20
C	2.53	88.40	88.61
QT	2.72	87.91	88.12
S C6	2.14	88.49	88.70

2+25.93 PCC on M.L. at 90°

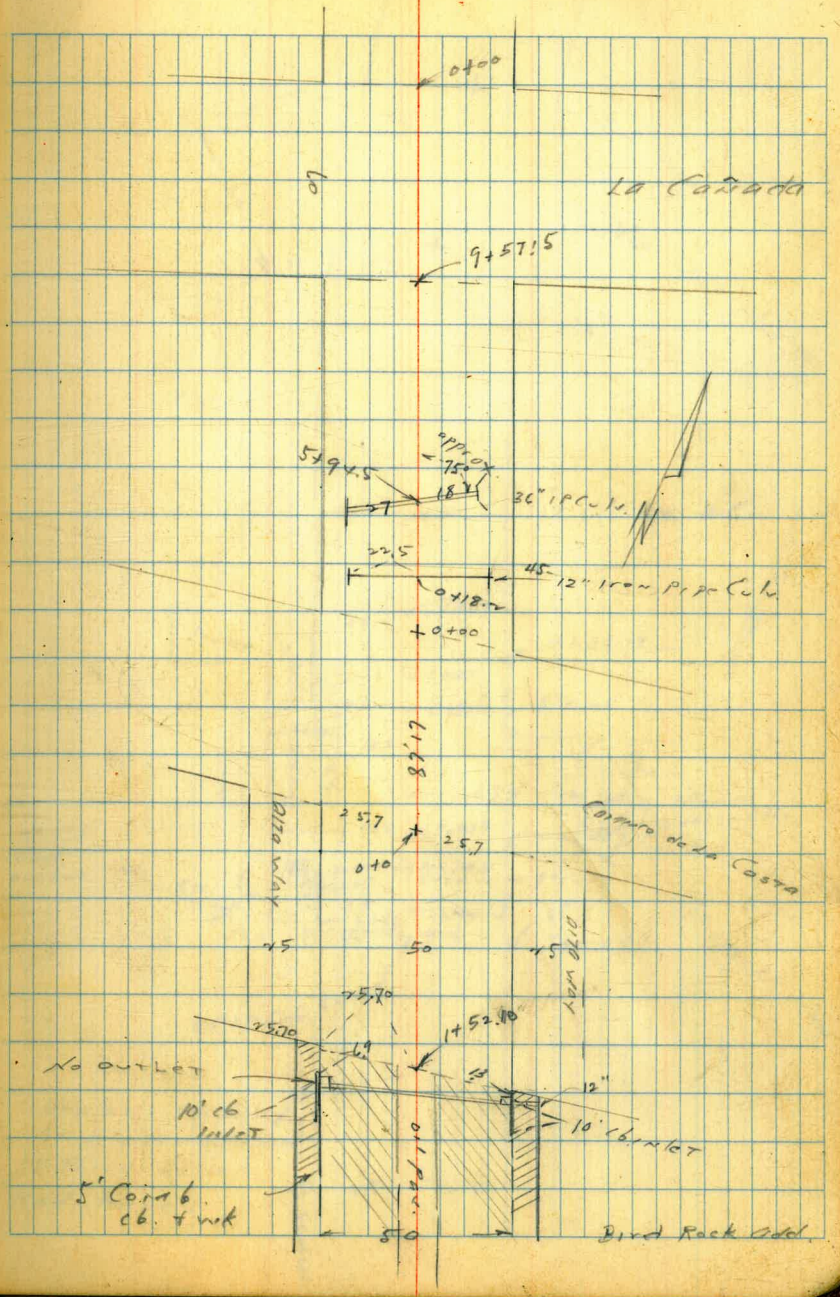
S C6	0.99	89.64	89.85
QT	1.67	88.96	89.17
C	1.26	89.37	89.58
QT	1.46	89.17	89.38
N	0.90	89.73	89.94

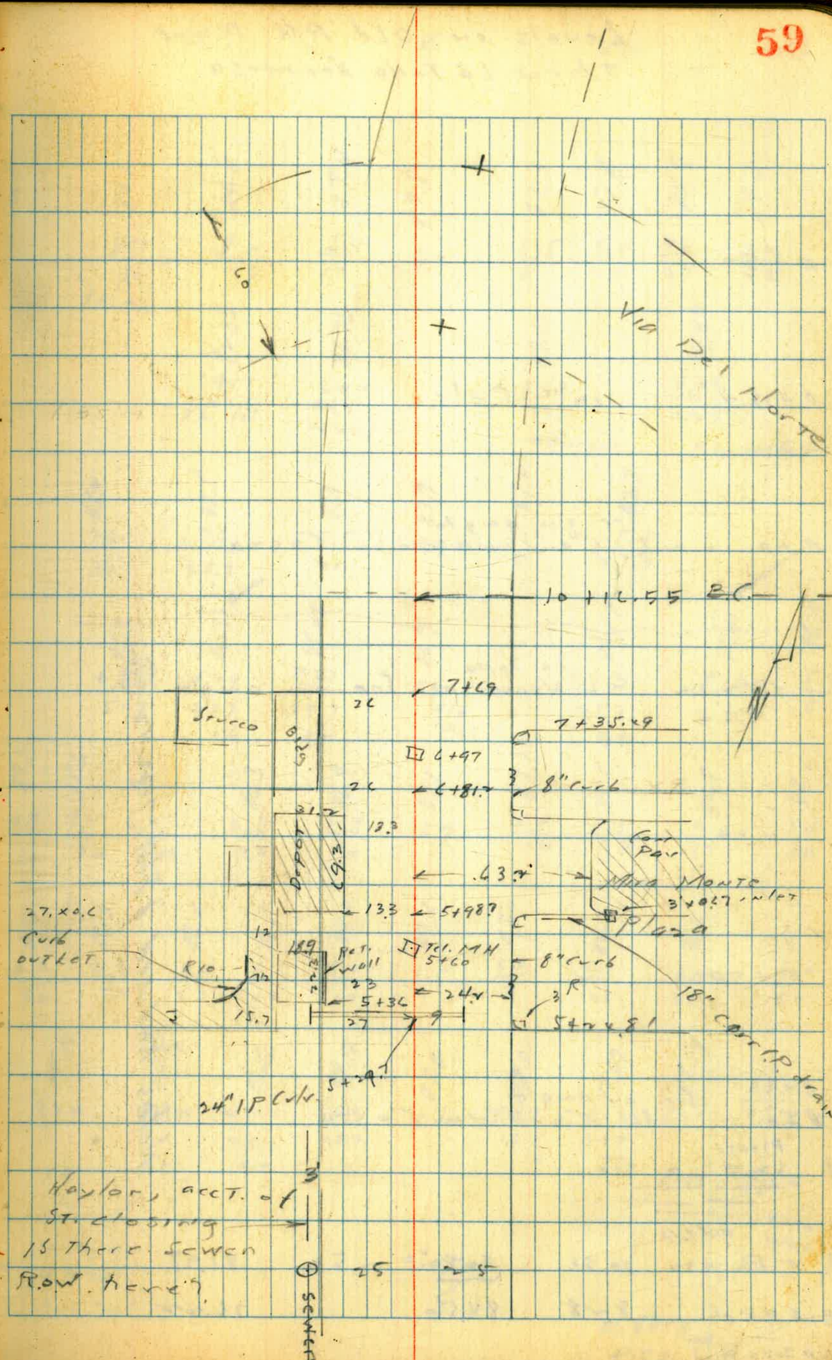
Indexed
C.S.K.

50

X sec old R.R. Road thru
La Jolla Hermosa

Note! Power Line Poles
on E of old Road
approx 145 ctrs




60
Via Del Monte
10+16.55 B.C.
7+69
Stucco
Bldg.
26
7+35.49
6+97
26
6+81.7
8" Curb
31.7
Depot
69.3
13.3
Conc.
Pav.
.43.7
Mira Monte
3'x0.67 inlet
Plaza
13.3
5+98.7
27.x0.6
Curb
outlet
12
18.9
Ret.
wall
Tel. MH
5+60
8" Curb
R10.
12
23
5+36
24.7
3R
15.7
27
9
5+74.81
18" Conc. P. drain
5+29.7
24" I.P. Culv.
3
Haylor, acct. of
St. closing
Is there sewer
R.O.W. here?
25
25
sewer

Levels on Old RR Row Thru La Jolla Hermosa

0+50

0+18.2 — 12" Culv

0+0 — N. Camino de la Costa (Sec. on angle)

1+52.10 — S. La Jolla Hermosa (Sec. on angle)

1+00

0+50

0+0 — S. Camino Costa (Sec. on angle)

Please back up sta.

old T.P.

T.P. p54	10.83	92.80	2.53	81.97
BM B.P.c6	8.28	84.50		76.22

La Jolla Blvd 105' S Camino Costa

Notes Reduced & Plot 7-22-42 [illegible]

LT ℄ RT

0+50: 84.1 8.7/30 fence | 84.8 8.0/25 | 87.4 5.4/17 | 87.8 5.0 | 87.3 5.5/8 | 87.8 5.0/25 | 85.8 7.0/35 | 89.4 3.4/45

0+18.2: 84.33 9.47/22.5 F.L. 12" | 86.76 6.04/22.5 Hd wall | 87.17 5.63/22.5 Hd wall | 84.87 7.93/22.5 FL inlet

0+0: 85.2 7.6/30 | 85.5 7.3/25.7 | 87.3 5.5/20 | 87.9 4.9 | 87.2 5.6/5 | 87.3 5.5/25.7

1+52.10: 85.9 6.9/51.7 | 86.31 6.49/25.7 c6 | 85.43 7.37/25.7 9T | 86.9 5.9 old rail | 86.57 6.23/25.7 9T | 87.41 5.39/25.7 | 86.9 5.9/51.7

1+00: 83.1 9.7/70 | 85.6 7.2/50 | 86.4 6.4/40 | 86.3 6.5/25 | 86.9 5.9/10 | 87.1 5.7 | 87.1 5.7/10 | 86.5 6.3/25 | 86.8 6.0/35 | 87.0 5.8/50

0+50: 84.1 8.7/50 | 86.3 6.5/40 | 86.4 6.4/25 | 86.5 6.3/18 | 87.4 5.4/10 | 87.3 5.5 | 87.0 5.8/8 | 86.7 6.1/25 | 86.6 6.2/35 | 86.8 6.0/50

0+0: 85.46 7.34 c6 | 84.90 7.90 9T | 86.56 6.24/25.7 9T | 87.18 5.62/25.7 c6 | 87.8 5.0 | 88.31 4.49/25.7 c6 | 87.67 5.13/25.7 9T | 87.59 5.21 E 9T | 88.23 4.57 c6 E

W side g to on W

92.80

[illegible] way on E

El. 88.23 P.56

Station				
+50				
↓				
3+50				
T.P.	6.69	95.87	3.62	89.18
3+00				
+50				
2+00				
+50				
1+00				

92 80

Lt			℄		Rt			
88.5 7.2/35	88.3 7.6/25	89.1 6.2/20	89.9 6.0	90.1 5.8/11	92.4 3.5/18	93.2 2.7/25	93.7 2.2/35	
86.5 9.4/35	87.1 8.8/25	89.0 6.9/18	89.5 6.4	89.4 6.4/12	91.7 4.2/25	92.7 3.2/26 ← Fence		
87.2 8.7/35	87.5 8.2/25	88.8 7.1/20	89.7 6.2	89.7 6.2/12	91.2 4.7/20	89.9 6.0/25	92.1 3.8/35	
			95.87					
89.1 6.7/35	86.3 6.5/25	88.4 4.4/17	88.9 3.9	88.8 4.0/12	89.2 3.6/25	89.2 3.6/35	81.2 1.6/40	
83.8 9.0/35	84.1 8.7/25	87.9 4.9/17	88.5 4.3	88.6 4.2/15	88.9 3.9/25	88.8 4.0/38	89.6 3.2/45	
82.9 9.9/35	83.5 9.3/25	87.7 5.1/17	88.3 4.5	88.6 4.2/20	87.9 4.9/25	87.9 4.9/38	89.2 3.6/45	
83.6 9.2/35	84.6 8.2/25	87.4 5.4/18	88.0 4.8	88.8 4.0/20	87.4 5.4/25	87.4 5.4/38	89.3 3.5/44	
84.1 8.7/35	84.3 8.5/25	87.8 5.0/17	87.1 4.9	87.6 5.2/8	88.3 4.5/20	86.7 6.1/25	86.7 6.1/37	88.8 4.0/47

92 80

7+00

+50

6+75

+98.8

+89

+80

+50

5+00

95.87

Lt

Rt

95.87

1

0 + 50

0 to = N/y Cañada

T.P. P.51 3.90 96.75 6.35 9v.85 9v.87

+ 57.15 = S.y. La Cañada

9

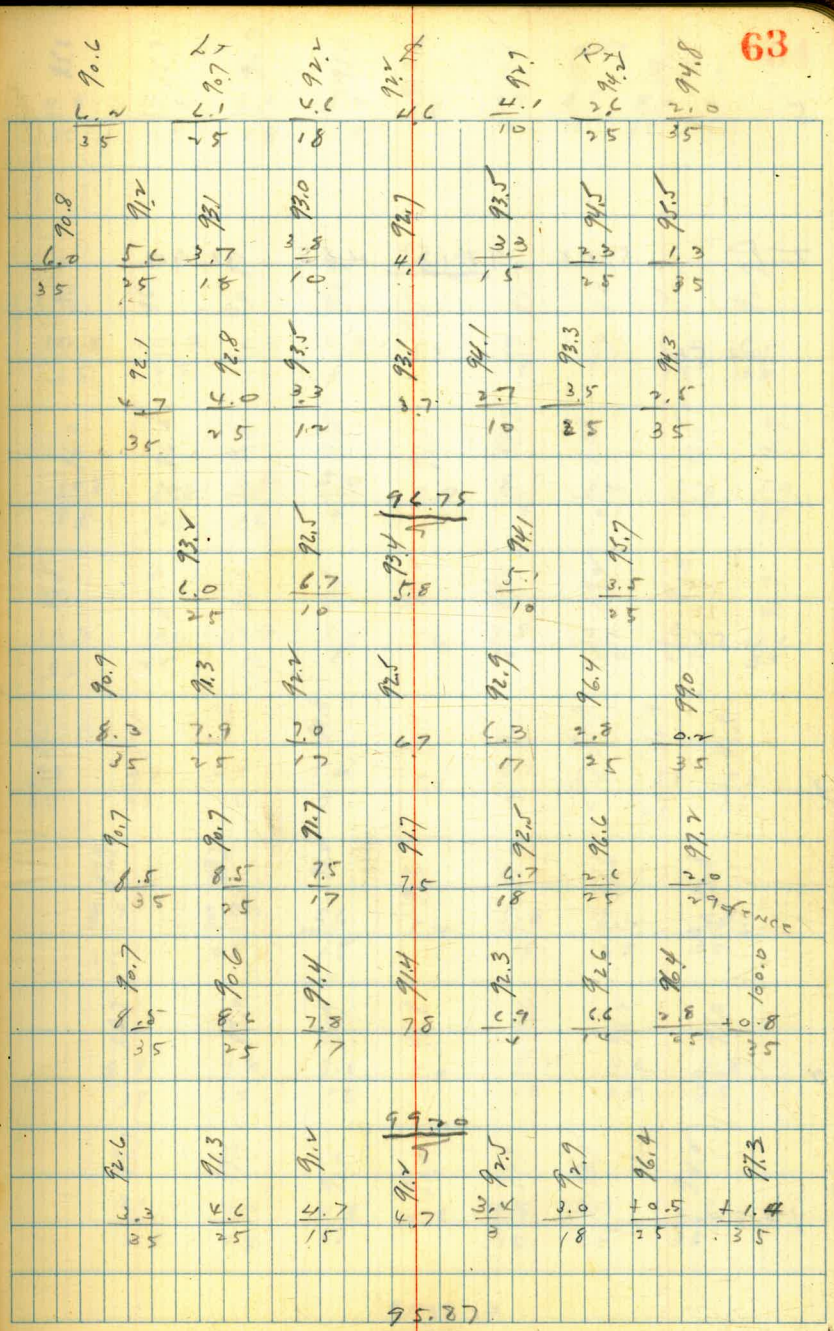
+ 50

8

T.P. 7cN 99.20 4.9 91.58

7 + 50

95.87



T.P.	5+3	97.13	4.85	91.90
	+50			
H				
	+50			
3				
	+50			
4				
	1+50			

96.75

96.75

7+50

7+35.49

7+00

+68

6+50

5+987

+58.3

5+36

5+19.7 24" I.P. Curb

97.13

11

+50 Here ROW is wider
See Map

10+16.55 B.C. Rt.

10

+50

9

+50

8+00

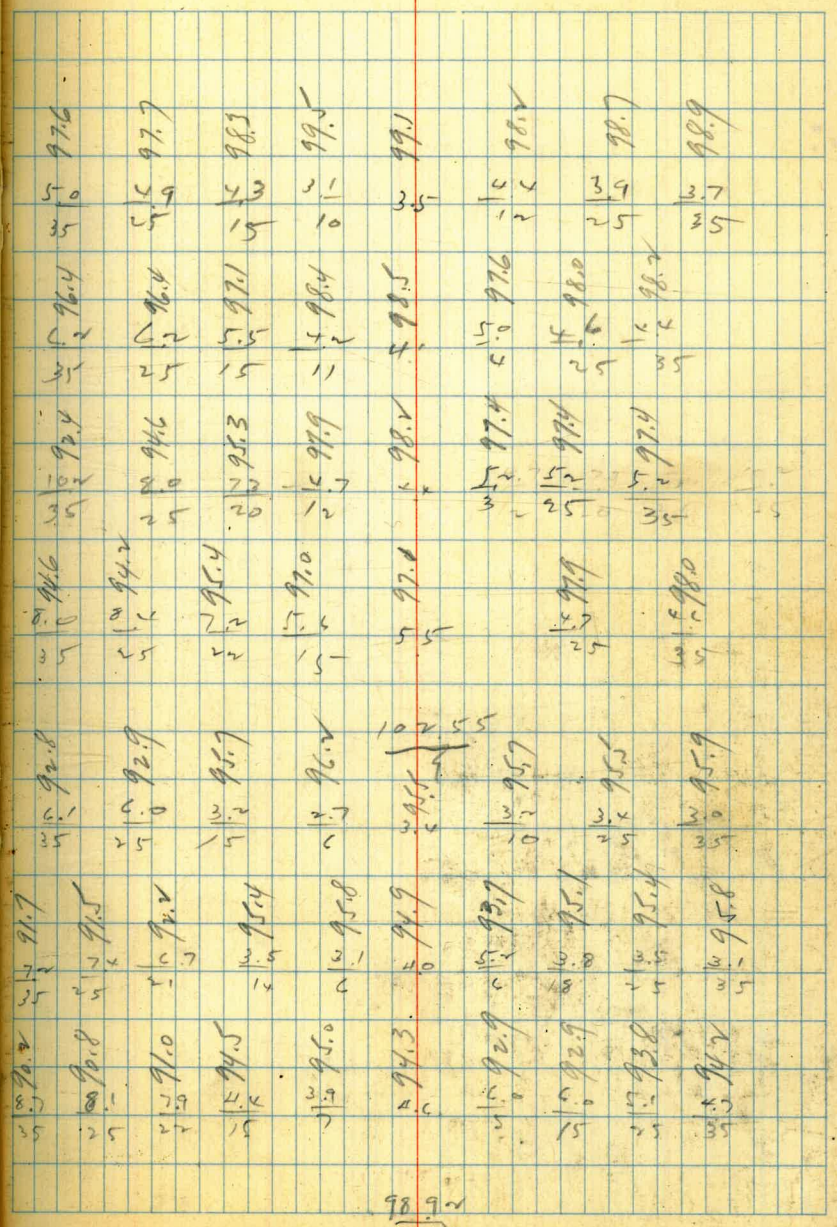
T.P.	6.56	98.92	4.77	92.36
		97.13		

Width Row ← 25' →

Lt					℄	Rt		
89.1 / 9.8 / 40	89.7 / 9.2 / 25	90.2 / 8.7 / 23	93.6 / 5.3 / 16	94.2 / 4.7 / 9	93.5 / 5.4	91.9 / 7.0 / 6	92.4 / 6.5 / 25	92.9 / 6.0 / 35
87.9 / 11.0 / 40	88.6 / 10.3 / 25		92.9 / 6.0 / 17	93.6 / 5.3 / 10	92.6 / 6.3	91.2 / 7.7 / 5	90.8 / 8.1 / 25	91.6 / 7.3 / 35
87.2 / 11.7 / 40	87.4 / 11.5 / 25		92.5 / 6.4 / 17	93.2 / 5.7 / 10	92.2 / 6.7	89.4 / 9.5 / 7	90.1 / 8.8 / 25	90.6 / 8.3 / 35
87.0 / 11.9 / 40	87.3 / 11.6 / 25		92.5 / 6.4 / 17	93.1 / 5.8 / 10	91.9 / 7.0	89.2 / 9.7 / 7	89.7 / 9.2 / 25	90.4 / 8.5 / 35
86.3 / 12.6 / 40	86.8 / 12.1 / 25		92.0 / 6.9 / 18	92.5 / 6.4 / 10	91.6 / 7.3	88.8 / 10.1 / 10	88.9 / 10.0 / 25	89.4 / 9.5 / 35
85.6 / 13.3 / 40	86.3 / 12.6 / 25		92.0 / 6.9 / 17	92.5 / 6.4 / 9	91.6 / 7.3	87.9 / 11.0 / 11	88.1 / 10.8 / 25	88.5 / 10.4 / 35
85.0 / 13.9 / 40	85.6 / 13.3 / 25		91.4 / 7.5 / 17	92.3 / 6.6 / 9	91.5 / 7.4	87.7 / 11.2 / 10	87.7 / 11.2 / 25	88.5 / 10.4 / 35
85.3 / 13.6 / 40	86.5 / 12.4 / 25		91.9 / 7.0 / 17	92.2 / 6.7 / 9	91.6 / 7.3	87.5 / 11.4 / 6	88.3 / 10.6 / 25	88.4 / 10.5 / 35

98.92
℄

1+50						
1+						
13 +50						
1+80	Mly del Norte					
TP 5.06						
2 inlet 1+54	5.4 ↓	164.55	1.81	97.4	97.11	
P. 50						
12 +25.5	Sly del Norte on Curve					
1+						
11+50						
		98.9-r				



Walker
Hardin
Wirt
8-24-42

Levels on curb and Paving

CAMINO DE LA COSTA

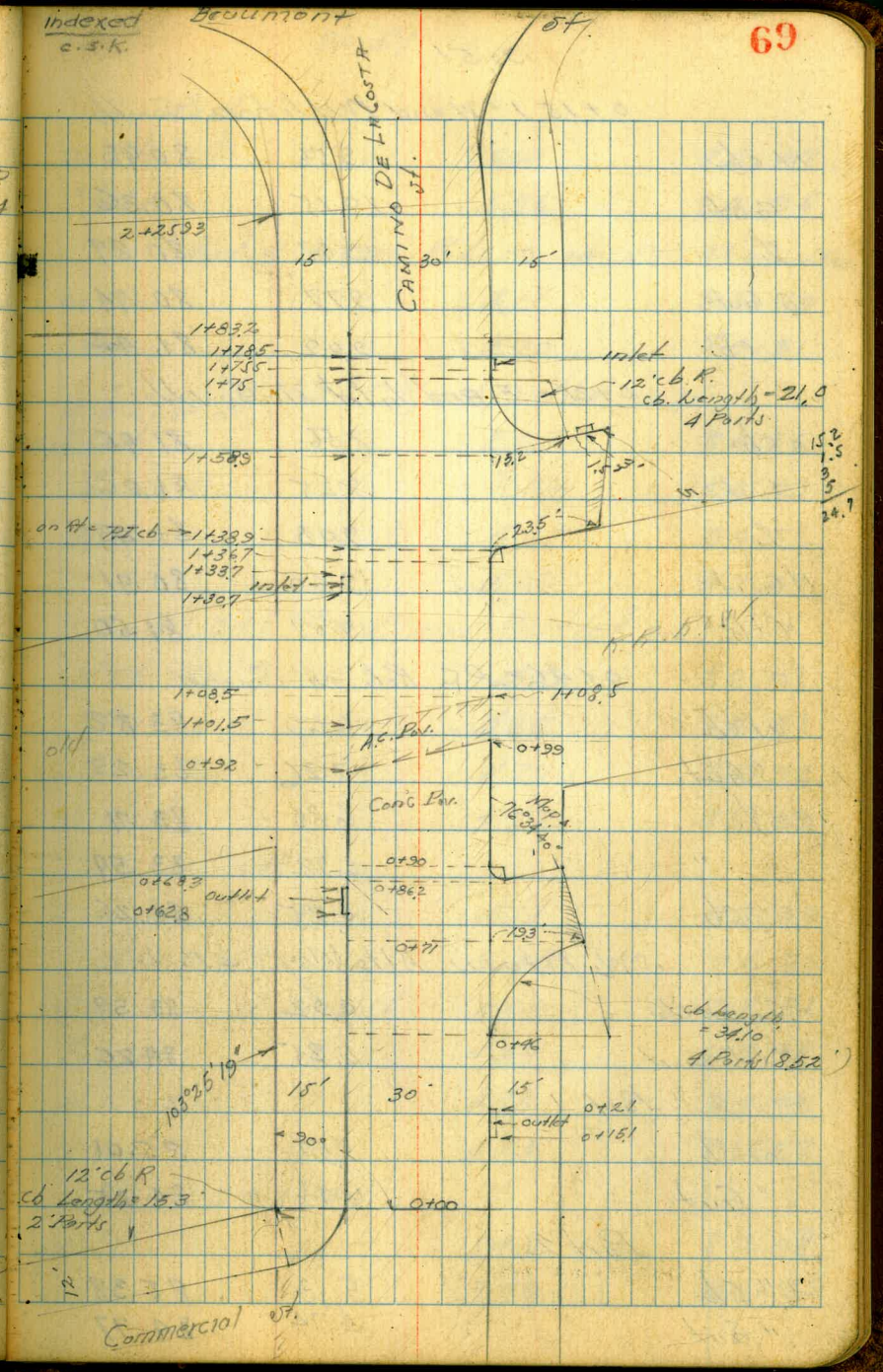
from Commercial St. 2+25.93 North East

Filed: TP
Page 54

8.54	90.51	81.97
0-30'		
Scb.	11.29	79 22
" Gut.	11.91	78.60
L on Pav.	11.53	78 97
N cb " "	11.64	78 87
N.E. Ref.		
P.C. on cb.	10.93	79 58
Gut.	11 44	79 07
L Ref. on cb.	10 91	79 60
" Gut	11.45	79 06
E.C. on cb.	10.93	79 58
" " Gut.	11 35	79 16
0+00		
E.C. on cb. } same Place as Above.	10.93	79.58
" " Gut.	11.35	79 16
L on Pav.	10.73	79.78
S G.L.	10.70	79 81
S Top cb.	10.02	80.49
0+07.3		
S cb.	9.47	81.04
" Gut.	10 12	80.39
L	10 03	80 48
N Gut.	10.57	79 94
N cb.	9.98	80 53

Green Profile 1"=40' 9-2-1942 C.O.H.

#466



0+15.1 = W end Outlet on South

N cb.	9.56	80.95
Gut.	10.15	80.36
℄	9.62	80.89
S Gut.	9.77	80.74
" cb.	9.09	81.42

0+21 = E end Inlet on South

S cb.	8.56	81.95
S Gut.	9.25	81.26
℄	9.08	81.43
N Gut.	9.60	80.91
N cb.	9.01	81.50

0+46 = PC Ret. on South

N cb.	6.69	83.82
" Gut.	7.26	83.25
℄	6.80	83.71
S "	6.92	83.59
" cb.	6.25	84.26

S.W. Return Alta Wall 4 Pcts.

P.C. on cb.	6.92	83.59
" " Gut.	6.25	84.26

Part 1

on cb.	5.50	85.01
" Gut.	6.26	84.25

Part 2

" Cb.	5.13	85.38
" Gut.	5.74	84.77

Part 3

on cb.	5.04	85.47
" Gut.	5.56	84.95

Part 4 = end Return on S.W. 4.3' beyond line

on cb.	5.11	85.40
" Gut.	5.70	84.81

0+62.8 = W end Outlet on N

S cb. Line St.		
on S. Gut.	5.65	84.86
℄ on Ret.	5.30	85.21
N Gut.	5.65	84.86
" cb.	5.02	85.49

0+68.3 = E end Outlet on N

N cb.	4.50	86.01
" Gut.	5.10	85.41
℄ on Ret.	4.79	85.72
S Gut.	5.22	85.29

0+71

S cb. at end Ret.	5.11	85.40
" Gut " "	5.70	84.81
S cb. Gut. cb Line St.	5.00	85.51
℄	4.53	85.98
N Gut.	4.78	85.73
N cb.	4.23	86.28

0+80.4

N cb.	3.43	87.08
" Gut.	3.56	86.95

℄	3.63	86.88
S Gut.	4.24	86.27
0+86.18		
SL on cb = 15.2' from PI.	3.34	87.17
" " Gut " " "	3.93	86.58
S Gut. = cb Line St. = PI. cb.	3.79	86.72
℄ on Rim MH	3.15	87.36
" " Pan	3.10	87.41
N Gut.	2.88	87.63
" cb.	2.77	87.74
0+89 on N = Bk in cb. on N		
N cb.	2.48	88.03
" Gut.	2.63	87.88
0+90 = EC. 3 Rad on South		
N cb.	2.42	88.09
"Gut.	2.55	87.96
℄	2.72	87.79
S Gut.	3.37	87.14
" Top cb. EC. Rd.	3.07	87.44
0+92 on N cb. and 0+99 on S cb. ℄ on diag. these sta.		
S cb.	2.59	87.92
S Gut.	2.57	87.94
℄	2.43	88.08
N "	2.44	88.07
N cb.	2.41	88.10

1+01.5 on N and 1+08.5 on South

N cb.	2.25	88.26
" Gut.	2.27	88.24
℄ on diag. of stations	2.33	88.18
S Gut.	2.49	88.02
S Top cb.	2.50	88.01
1+20		
S cb.	2.36	88.15
" Gut.	2.55	87.96
℄	2.37	88.14
N "	2.52	87.99
N cb.	2.24	88.27
1+30.7 = W end Inlet on N		
N cb.	2.20	88.31
" Gut.	2.87	87.67
℄	2.41	88.10
S "	2.61	87.90
" cb.	2.20	88.31
1+33.7 = E end Inlet on N		
S cb.	2.14	88.37
"Gut.	2.62	87.89
℄	2.41	88.10
N "	2.88	87.63
N cb.	2.14	88.37

1+36.7 = PC. 3' Rod. on South.

N Cb.	2.14	88.37
" Gut.	2.83	87.68
℄ on ℘	2.41	88.10
S Gut.	2.66	87.85
" Cb.	2.09	88.42
1+38.9		
23.5 South of PI. on Cb.	2.30	88.21
" " " " " Gut	2.90	87.61
38' South of PI. on PC Rot	2.07	88.44 3' Rod.
PI. Cbs. on Gut	2.67	87.84
℄ on Pav.	2.42	88.09
N Gut.	2.80	87.71
" Cb.	2.15	88.36
1+58.9		
N Cb.	2.00	88.51
" Gut.	2.63	87.88
℄	2.29	88.22
S Gut. = PI Cbs.	2.76	87.75
15.2' Rt. of PI. on PC. 12'R.	2.27	88.24 on Cb
" " " " " "	2.91	87.60 " Gut.
16.7 Rt of PI. = N end Inlet	2.30	88.21 on Cb
16.7 " "	2.99	87.52 " Inlet
19.7 " " = S " "	2.30	88.21 on Cb.
" " " " "	2.99	87.52 " Inlet
24.7' Rt. of PI. = End Cb.	2.33	88.18 on Cb.
" " " " " "	2.93	87.58 " Gut

S.E. Rot 12' Cb Rod. 4 Parts.

PC. on Cb	2.27	88.24
" " Gut	2.91	87.60
Part 1		
on Cb	2.22	88.29
" Gut.	2.82	87.69
Part 2		
on Cb.	2.15	88.36
" Gut.	2.76	87.75
Part 3		
" Cb.	2.08	88.43
" Gut.	2.78	87.73
Part 4 = E.C. 1+75		
Cb.	2.04	88.47
Gut.	2.77	87.74
1+75.5 = N end Inlet on South		
S Cb.	2.01	88.50
" Gut	2.76	87.75
℄	2.08	88.43
N Gut	2.93	88.08
N Cb.	1.84	88.67
1+78.5 = E. end Inlet on South		
N Cb	1.79	88.72
" Gut.	2.38	88.13
℄	2.01	88.46
S "	2.68	87.83
" Cb.	1.93	88.58

90.51

1+83.2 = PC. Cb & Prop.

S Cb.	1.83	88.68
" Gut.	2.44	88.07
L	1.95	88.56
N Gut	2.32	88.19
N Cb.	1.71	88.80
2+00		
N Cb.	1.37	89.14
" Gut.	2.03	88.48
L	1.60	88.91
S "	2.03	88.48
S Cb	1.40	89.11
2+25.93		
S Cb.	0.70	89.81
" Gut.	1.37	89.14
L	0.96	89.55
N "	1.16	89.35
N Cb	0.59	89.92
		89.94 = Moore C 0.02 P-59
Chk. Gut.	5.07	85.44 W Side
Chk. Cb 1+52.1 P-60	4.20	86.31 = Top Cb.
" " " "	3.10	87.41 = Top C. E. Side
" Gut. " "	3.93	" "

Reg Levels Linda Vista Road
Sta. 0+00 to

BM #4	1.84	258.69	0.865	256.85	#1 256.8 #2 256.8
	3.735	257.715	1.565	253.98	
	1.16	255.545	13.00	254.385	
BM #3	5.245	267.385	6.09	262.14	#1 262.1 #2 262.1
	6.93	268.23	0.78	261.30	
	12.45	262.08	0.64	249.63	
	0.36	250.27	12.585	249.91	
	0.51	262.495	12.62	261.985	
BM #2	1.58	274.605	1.58	273.025	#1 273.005 #2 273.01
	0.925	274.605	6.77	273.68	
	3.66	280.45	7.90	276.79	
BM #1	3.445	284.69		281.245	

Nov. 28. 43
Peebles
Sunset
Blue Tape
Begg Rod.

74

60d Spike in Power Pole # 178424 185' Rt 20+80

Chisel X Top Curb W/M Con Stone Bkg 125 Lt. 13+20

Chisel Cross N orth Edge Side Walk 60 Lt 7+65

Chisel X Top Curb 21' Rt 0+00 A Linc

	0.57	169.19	12.895	168.62	
BM #7	0.265	181.515	5.515	181.25	#1 #2 181.24
	9.005	186.765	12.94		
	0.36	190.70	11.09	190.34	
	0.20	201.43	12.72	201.23	
BM 6	6.99	213.95	13.055	206.95	
TP	2655	220.015	2.01	217.36	
	10.31	219.37	4.75	209.06	
	1.68	213.81	11.03	212.13	
	1.70	223.16	11.62	221.46	
BM #5	0.94	232.08	4.02	232.14	#1 232.03 #2 232.11
	1.27	236.16	12.965	234.89	
	0.875	247.856 258.69	11.21	247.48	

RR Spike in Power Pole 40' Lt. 43+47

Drill Hole 36+50

RR Spike in Pole #450566 H 91 Rt 33+53

Drill Hole 31+50 Rt

Chisel X Set on Conc Pump House 40 Rt 23+82

			11.67	60.12	
	0.215	71.79	11.84	71.575	
BM #9	2.98	83.415	12.17	80.425	#1 80.38 #2 80.29
	0.40	92.605	12.62	92.21	
	0.58	104.83	12.51	104.25	
	0.805	116.76	12.81	115.955	
	0.19	128.765	12.665	128.575	
BM #8	3.48	141.24	9.275	137.76	#1 #2 137.795
	0.935	147.035	12.51	146.10	
	1.845	158.61	12.425	156.765	
		169.19			

¾" Galv. Pipe 60' Lt. 57+19

Chisel D. Top S.D. Gas + Elec. Manhole 29' Rt. 47+60

University Heights Reservoir
Elevation of High Water

indexed
c.s.k.

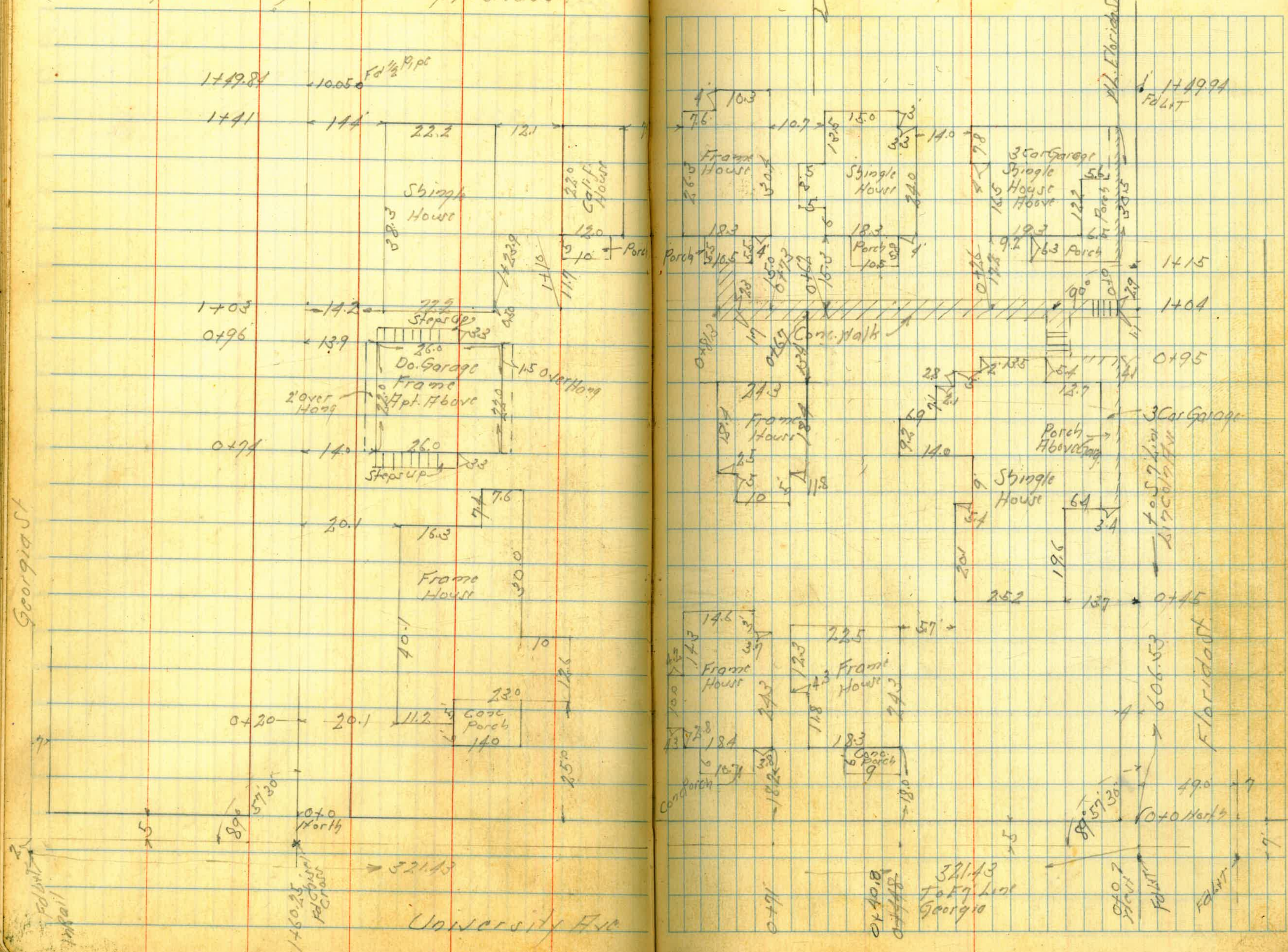
BM	12.50	385.51		372.01	SEBP Howard & Idaho
TP	7.05	391.75	0.81	384.70	
Elev. High Water = 12' on Gauge			5.94	385.81	

March 25-44
Sisson
Bliss
Bogg

Location of Houses Lots 25 to 30 Inclusive
Block 195 University Heights
North of University Ave. West of Florida St.

March 1-46
Sisson
Osborne
Waddel

indexed
C.S.K.



IMPROVED TABLES AND INFORMATION

HORIZONTAL STADIA CORRECTIONS

2°—00′	— 0.1	21°—00′	— 12.8	33°—00′	— 29.7
3°—00′	— 0.3	21°—30′	— 13.4	33°—15′	— 30.1
4°—00′	— 0.5	22°—00′	— 14.0	33°—30′	— 30.5
5°—00′	— 0.8	22°—30′	— 14.7	33°—45′	— 30.9
6°—00′	— 1.1	23°—00′	— 15.3	34°—00′	— 31.3
7°—00′	— 1.5	23°—30′	— 15.9	34°—15′	— 31.7
8°—00′	— 1.9	24°—00′	— 16.5	34°—30′	— 32.1
9°—00′	— 2.5	24°—30′	— 17.2	34°—45′	— 32.5
10°—00′	— 3.0	25°—00′	— 17.9	35°—00′	— 32.9
10°—30′	— 3.3	25°—30′	— 18.6	35°—15′	— 33.3
11°—00′	— 3.6	26°—00′	— 19.2	35°—30′	— 33.7
11°—30′	— 4.0	26°—30′	— 19.9	35°—45′	— 34.1
12°—00′	— 4.3	27°—00′	— 20.6	36°—00′	— 34.6
12°—30′	— 4.7	27°—30′	— 21.3	36°—15′	— 35.0
13°—00′	— 5.1	28°—00′	— 22.0	36°—30′	— 35.4
13°—30′	— 5.5	28°—30′	— 22.8	36°—45′	— 35.8
14°—00′	— 5.9	29°—00′	— 23.5	37°—00′	— 36.2
14°—30′	— 6.3	29°—30′	— 24.3	37°—15′	— 36.6
15°—00′	— 6.7	30°—00′	— 25.0	37°—30′	— 37.1
15°—30′	— 7.2	30°—15′	— 25.4	37°—45′	— 37.5
16°—00′	— 7.6	30°—30′	— 25.8	38°—00′	— 37.9
16°—30′	— 8.1	30°—45′	— 26.2	38°—15′	— 38.3
17°—00′	— 8.5	31°—00′	— 26.5	38°—30′	— 38.7
17°—30′	— 9.0	31°—15′	— 26.9	38°—45′	— 39.1
18°—00′	— 9.5	31°—30′	— 27.3	39°—00′	— 39.6
18°—30′	— 10.1	31°—45′	— 27.7	39°—15′	— 40.0
19°—00′	— 10.6	32°—00′	— 28.1	39°—30′	— 40.5
19°—30′	— 11.2	32°—15′	— 28.5		
20°—00′	— 11.7	32°—30′	— 28.9		
20°—30′	— 12.3	32°—45′	— 29.3		

Chains to Feet	
1	66
2	132
3	198
4	264
5	330
6	396
7	462
8	528
9	594
10	660

Feet to Chains	
100	1.515
200	3.030
300	4.545
400	6.060
500	7.575
600	9.090
700	10.606
800	12.121
900	13.636
1,000	15.151

ENGINEERING DEPARTMENT.
CITY OF SAN DIEGO,
CALIFORNIA.

341
73
268

2055
1810
2086

7.27
1.50
3.20
11.37

9.92
2.65
5.27
3.95
1.50
11.92
11.9

8.77

12.4
1.5
10.9
4
6.9
8.7
12.0
1.5

729.70
590.64
139.06

767.30
590.64
176.66

590.64
178.77
769.41

817.65
769.41
48.24