

LIETZ



LIBRARY



1872

TRAVERSE TABLE FOR TRANSIT BOOK.

From 1° to 90° for a distance of 100.

Degrees.	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		Degrees.
	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	
0			100 00	0 44	100 00	0 87	99 99	1 31	89
1	99 98	1 75	99 98	2 18	99 97	2 62	99 95	3 05	88
2	99 94	3 49	99 92	3 93	99 91	4 36	99 88	4 80	87
3	99 86	5 23	99 84	5 67	99 81	6 10	99 79	6 54	86
4	99 76	6 98	99 73	7 41	99 69	7 85	99 66	8 28	85
5	99 62	8 72	99 58	9 15	99 54	9 58	99 50	10 02	84
6	99 45	10 45	99 41	10 89	99 36	11 32	99 31	11 75	83
7	99 25	12 19	99 20	12 62	99 14	13 05	99 09	13 49	82
8	99 03	13 92	98 97	14 35	98 90	14 78	98 84	15 21	81
9	98 77	15 64	98 70	16 07	98 63	16 50	98 56	16 93	80
10	98 48	17 36	98 40	17 79	98 33	18 22	98 25	18 65	79
11	98 16	19 08	98 08	19 51	97 99	19 04	97 90	20 36	78
12	97 81	20 79	97 72	21 22	97 63	21 64	97 53	22 07	77
13	97 44	22 50	97 34	22 92	97 24	23 34	97 13	23 77	76
14	97 03	24 19	96 92	24 62	96 81	25 04	96 70	25 46	75
15	96 59	25 88	96 48	25 30	96 36	26 72	96 25	27 14	74
16	96 13	27 56	96 00	27 98	95 88	28 40	95 76	28 82	73
17	95 63	29 24	95 50	29 65	95 37	30 07	95 24	30 49	72
18	95 11	30 90	94 97	31 32	94 83	31 73	94 69	32 14	71
19	94 55	32 56	94 41	32 97	94 26	33 38	94 12	33 79	70
20	93 97	34 20	93 82	34 61	93 67	35 02	93 51	35 43	69
21	93 36	35 84	93 20	36 24	93 04	36 65	92 88	37 06	68
22	92 72	37 46	92 55	37 86	92 39	38 27	92 22	38 67	67
23	92 05	39 07	91 88	39 47	91 77	39 87	91 53	40 27	66
24	91 35	40 67	91 18	41 07	91 00	41 47	90 81	41 87	65
25	90 63	42 26	90 45	42 66	90 26	43 05	90 07	43 44	64
26	89 88	43 84	89 69	44 23	89 49	44 62	89 30	45 01	63
27	89 10	45 40	88 90	45 79	88 70	46 17	88 50	46 56	62
28	88 29	46 95	88 09	47 33	87 88	47 72	87 67	48 10	61
29	87 46	48 48	87 25	48 86	87 04	49 24	86 82	49 62	60
30	86 60	50 00	86 38	50 38	86 16	50 75	85 94	51 13	59
31	85 72	51 50	85 49	51 86	85 26	52 25	85 04	52 62	58
32	84 80	52 99	84 57	53 36	84 34	53 73	84 10	54 10	57
33	83 87	54 46	83 63	54 83	83 39	55 19	83 15	55 56	56
34	82 90	55 92	82 66	56 28	82 41	56 64	82 16	57 00	55
35	81 92	57 36	81 66	57 71	81 41	58 07	81 16	58 42	54
36	80 90	58 78	80 64	59 13	80 39	59 48	80 13	59 83	53
37	79 86	60 18	79 60	60 53	79 34	60 88	79 07	61 22	52
38	78 80	61 57	78 53	61 91	78 26	62 25	77 99	62 59	51
39	77 71	62 93	77 44	63 27	77 16	63 61	76 88	63 94	50
40	76 60	64 28	76 32	64 61	76 04	64 94	75 76	65 28	49
41	75 47	65 61	75 18	65 93	74 90	66 26	74 61	66 59	48
42	74 31	66 91	74 02	67 24	73 73	67 56	73 43	67 88	47
43	73 14	68 20	72 84	68 52	72 54	68 84	72 24	69 15	46
44	71 93	69 47	71 63	69 78	71 33	70 09	71 02	70 40	45
45	70 71	70 71							
Degrees.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Dep.	Lat.	Degrees.
	DEGREES.		¼ DEGREE.		½ DEGREE.		¾ DEGREE.		

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MADE IN
U. S. A.



Quality
Evidenced
Since
1882.

Standard
Tripod
Connection

LIETZ STANDARD ENGINEERS' TRANSIT
With U Shaped Standards

No. 5E with 6¼" limb.

No. 11E with 5" limb.

Furnished with either Internal or External
Focusing Telescope.

TABLE OF STADIA REDUCTIONS.—Continued.

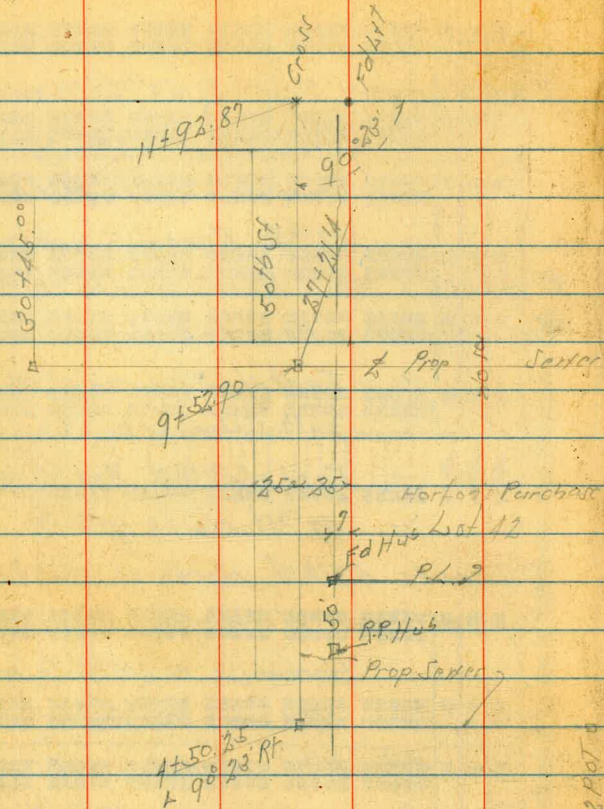
TABLE OF STADIA REDUCTIONS.—Continued.

Min.	24°		25°		26°		27°		28°		29°		30°	
	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.	Hor. Dist.	Diff. Elev.
0	83.46	37.16	82.14	38.30	80.78	39.40	79.39	40.45	77.96	41.45	76.50	42.40	75.00	43.30
2	83.41	37.23	82.09	38.38	80.74	39.44	79.34	40.49	77.91	41.48	76.45	42.43	74.95	43.33
4	83.37	37.27	82.05	38.41	80.69	39.47	79.29	40.52	77.87	41.52	76.40	42.46	74.89	43.36
6	83.33	37.31	82.01	38.45	80.65	39.51	79.25	40.55	77.83	41.55	76.35	42.49	74.85	43.39
8	83.29	37.35	81.96	38.49	80.60	39.55	79.20	40.59	77.78	41.59	76.30	42.53	74.80	43.42
10	83.24	37.39	81.92	38.53	80.55	39.58	79.15	40.62	77.72	41.61	76.25	42.56	74.75	43.45
12	83.20	37.43	81.87	38.56	80.51	39.61	79.11	40.66	77.67	41.65	76.20	42.59	74.70	43.47
14	83.15	37.47	81.83	38.59	80.46	39.64	79.06	40.69	77.62	41.68	76.15	42.62	74.65	43.50
16	83.11	37.51	81.79	38.62	80.41	39.67	79.01	40.72	77.57	41.71	76.10	42.65	74.60	43.53
18	83.07	37.54	81.74	38.65	80.37	39.70	78.96	40.75	77.52	41.74	76.05	42.68	74.55	43.56
20	83.02	37.58	81.69	38.68	80.32	39.73	78.92	40.79	77.48	41.77	76.00	42.71	74.50	43.59
22	82.98	37.62	81.65	38.71	80.28	39.76	78.87	40.82	77.42	41.81	75.95	42.74	74.44	43.62
24	82.93	37.66	81.60	38.75	80.23	39.79	78.82	40.86	77.37	41.84	75.90	42.77	74.39	43.65
26	82.89	37.69	81.56	38.78	80.18	39.82	78.77	40.89	77.31	41.87	75.85	42.80	74.34	43.68
28	82.85	37.73	81.51	38.82	80.14	39.85	78.73	40.93	77.26	41.90	75.80	42.83	74.29	43.71
30	82.80	37.77	81.47	38.86	80.09	39.88	78.68	40.96	77.20	41.93	75.75	42.86	74.24	43.74
32	82.76	37.81	81.42	38.89	80.04	39.91	78.63	40.99	77.15	41.97	75.70	42.89	74.19	43.77
34	82.72	37.85	81.38	38.93	80.00	39.94	78.58	41.02	77.10	42.00	75.65	42.92	74.14	43.80
36	82.67	37.89	81.33	38.97	79.95	40.00	78.54	41.06	77.05	42.03	75.60	42.95	74.09	43.83
38	82.63	37.93	81.29	39.00	79.90	40.07	78.49	41.09	77.00	42.06	75.55	42.98	74.04	43.86
40	82.59	37.97	81.24	39.04	79.86	40.11	78.44	41.12	76.95	42.09	75.50	43.01	73.99	43.89
42	82.54	38.00	81.19	39.08	79.81	40.14	78.39	41.15	76.89	42.12	75.45	43.04	73.93	43.90
44	82.50	38.04	81.15	39.11	79.76	40.18	78.34	41.18	76.84	42.15	75.40	43.07	73.88	43.93
46	82.45	38.08	81.10	39.15	79.72	40.21	78.30	41.22	76.79	42.18	75.35	43.10	73.82	43.96
48	82.41	38.12	81.06	39.19	79.67	40.24	78.25	41.25	76.74	42.22	75.30	43.13	73.77	43.99
50	82.36	38.16	81.01	39.22	79.62	40.28	78.20	41.29	76.69	42.25	75.25	43.16	73.71	44.01
52	82.32	38.20	80.97	39.26	79.57	40.31	78.15	41.32	76.64	42.28	75.20	43.19	73.66	44.04
54	82.27	38.24	80.92	39.29	79.53	40.35	78.10	41.36	76.59	42.31	75.15	43.22	73.60	44.07
56	82.23	38.28	80.87	39.33	79.48	40.38	78.05	41.39	76.54	42.34	75.10	43.25	73.55	44.10
58	82.18	38.32	80.83	39.36	79.44	40.42	78.01	41.42	76.49	42.37	75.05	43.28	73.50	44.13
60	82.14	38.36	80.78	39.39	79.39	40.45	77.96	41.45	76.44	42.40	75.00	43.31	73.45	44.16
c=75...	68	31	68	32	67	33	66	35	66	36	65	37	65	38
c=1.15...	1.05	46	1.04	50	1.03	51	1.02	53	1.01	55	1.00	57	0.99	58
c=1.90...	1.73	79	1.72	82	1.70	85	1.69	88	1.67	91	1.65	94	1.64	95

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Proposed Sewer Ozark St. 50 th St. Nagal St	1-7
" " Blk 22 Estrella + 48 th Glavin + Polk	8
" " Escoto Frank to H + 49 th St	10-14
" " 47 th St Escoto Frank to H + 49 th St	15-19
Proposed 6" Main Roseland Dr Torrey Pines to Spindrift 2026	
Proposed Sewer Federal Blvd. Sub 1 + 2	30-38
" " East of 47 th West of Market	39-42
" " 27 th + Harbor Dr.	43-45
" " East of 47 th St Bet. C + H St.	46
" " 49 th St North of H St.	47-48
Culverts 47 th St North of Market	49
Proposed Sewer Niemyer Tract	50
" " Harbor Dr. + 27 th So. Main St.	51-52
" " Adams Ave East of College Way	53
Cross Sec. Alley Blk C Montclair + 16 City Hts.	54-64
Storm Drain Market St + 47 th St	65-77
" " " " " "	-79

Proposed Sewer Ozark St. Ext/Sewer South to Imperial Ave



11+92.87

9+52.90

25+25

1+50.25
90° 23' R

* Prop Sewer

Horizon Purchase

Ed Hus Lot 12

P.L. 2

R.P. Hus

Prop Sewer

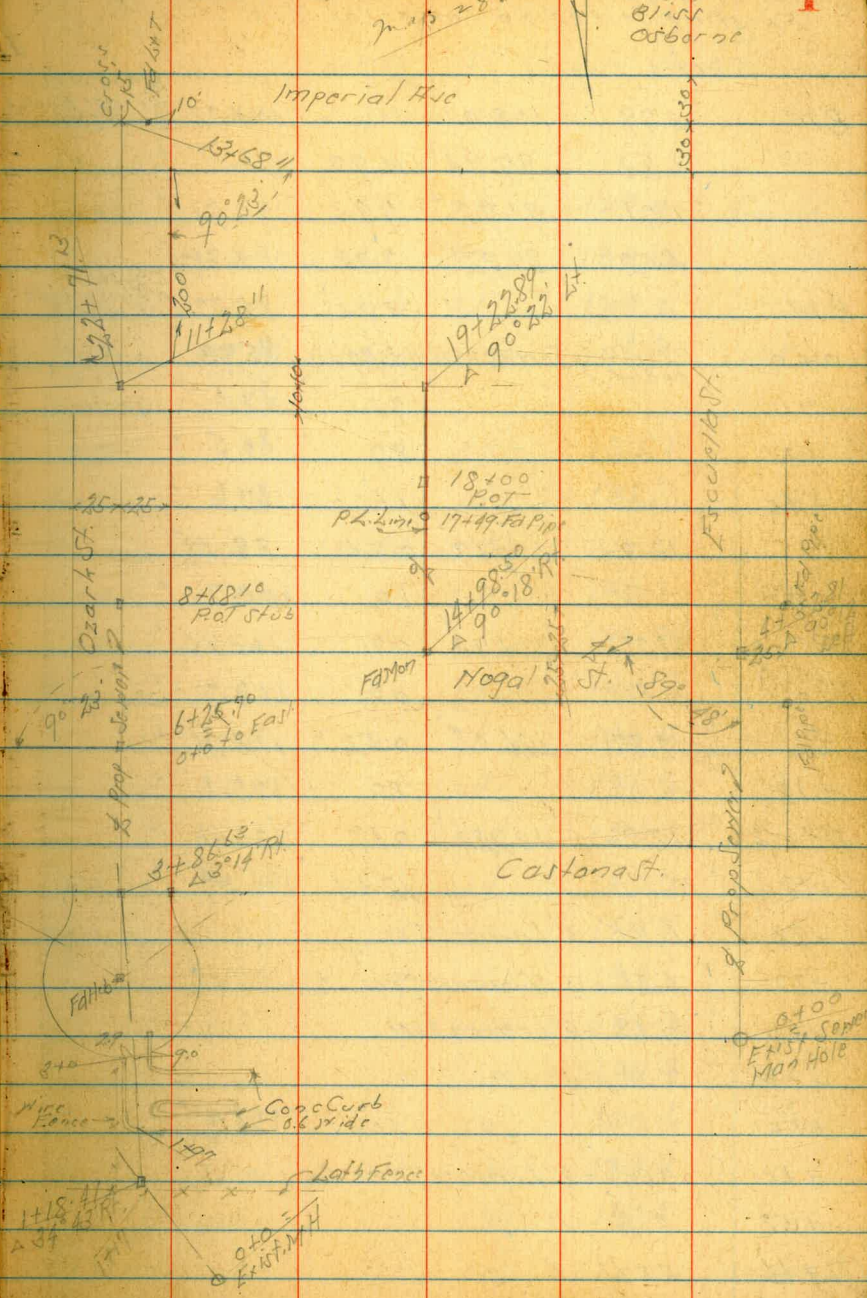
2+33.02 Plot

Indexed
c.s.R.

7+13 29.3

Sept. 11 44
S. 3300
Bliss
Osborn

1



Imperial Ave

12+2+71.13

13+68.11

90° 33' R

1000

11+28.11

19+22.80

90° 26' R

18+00 Pot

P.L. 2 in 9 17+49.70 P.P. 11

8+18.10 Pot St 06

6+26.90 St to Ed

14+90.18 R

90° 10' R

Nogal St. 89

Cartanast

Fence

Conc Curb 0.6 37 etc

Lot's Fence

0+00 East Sewer Man Hole

Frac. 1/2 in

Prop Sewer

0+00 East Sewer Man Hole

13+33.33

11+18.44
37

147

Wire Fence

Levels Proposed Sewer Ozark St.
Existing Sewer to Imperial Ave

Sketch Page 1

BM	3.79	108.01		104.22	BPNW Cor Bridge Foot 200' S of Marked	1+80	4.8 ft - 4" Lemon Tree			
	1.83	97.94	11.90	96.11		"	9' Rt - 3" "			
	1.71	91.72	7.93	90.01		+97		8.8	129.0 Ground	
	4.52	89.22	7.02	84.70		"	Top o.k. Conc Wall	7.70	130.12	
BM			3.95	85.27	Chisel A Fly S Shoulder of M.H.	2+0		8.6	129.2	
0+0 = Existing Sewer M.H. Sealed			3.29	85.93	on Top	" "	115' Rt - N.E. Cor House	11.2	126.6	on Floor
"			7.1	82.1	Ground	+32	4' Rt - Conc Curb			
+35			8.7	80.5		+50	6' Rt - " "			
+45			1.6	87.6		2+0		1.1	136.7	
TP	1219	101.67	0.74	88.48		TP	916	146.64	0.84	137.48
+75			1.0	100.7		+35		6.5	140.1	
TP	1277	113.73	0.71	100.96		+86.62	2 3/4' Rt	6.00	140.62	on Hub
1+0			0.0	113.7		4+0		6.0	140.6	
TP	1287	126.08	0.52	113.21		"	17' Rt of 7	6.2	140.4	
+12			1.0	125.1		"	31' " " "	10.4	136.2	
TP	1221	137.82	0.47	125.61		"	50' " " "	12.5	134.1	
+18.41			12.33	125.49	on Hub	+50		6.4	140.2	
+23.	6' Rt = 3" Lemon Tree					5+0		6.7	139.9	
+27	6' Lt = 2" Jacaranda Tree					"	20' Rt of 7	8.0	138.6	
+37	7' Rt = 8" Lemon Tree					"	50	18.3	133.3	
+38	7' Lt = 8" " "					+50		6.7	139.9	
+50			10.9	126.9		6+0		6.0	140.6	
+51	7.5' Rt = 3" Lemon Tree					"	26' Rt of 7	7.7	138.9	
+52	6' Lt = 3" " "					"	50' " " "	1.7	139.9	
+66	5.5' Lt = 3" " "					+25.70		5.12	141.52	on Hub
+66	8' Rt = 3" " "									

index
c.s.k.

137.82

Sept. 13-44
S. J. 007
81155
Osborne
Hardin

2

146.64

6+50			4.1	142.5	✓
7+0			0.3	146.3	✓
TP	12.72	158.95	0.41	146.23	✓
+50			8.9	150.0	✓
8+0			5.8	153.1	✓
+50			4.5	154.4	✓
+68.10	P.O.T.		4.09	154.86	✓ on slab
9+0			3.8	153.1	✓
+50			2.6	155.3	✓
10+0			2.3	155.6	✓
+50			3.1	155.8	✓
11+0			2.7	156.2	✓
TP	7.53	163.84	2.64	156.31	✓
+22.11	EXHAUST		7.06	156.78	✓ on slab
+50			6.2	157.6	✓
12+0			3.5	160.3	✓
+50			3.0	160.8	✓
13+0			2.8	160.0	✓
+39			4.4	159.4	✓
+59.11	NY Paving		4.40	159.44	✓
+68.11	Imperial		4.38	159.46	✓
B.M.			5.07	158.77	✓ IMPERIAL 116 03044
TP	0.84	152.56	12.12	151.72	✓
TP	3.58	147.57	8.57	148.99	✓
B.M.			9.86	137.71	✓ 1177 IMPERIAL 116 03044 137.87

Proposed Series Across Lot 42, Hartons Purchase
 Ozark St to 50th St. Also 50th St to Imperial Ave

Sketch Page 1

BM	1282	154.34	141.52	07 Hub 6125.70 Ozark P2	410		10.8	152.9	
0+0	= 642570 Ozark St				"	15' Lt of $\frac{1}{2}$	11.0	152.7	
+03		13.2	141.1		"	50' " " "	13.8	149.9	
+25		12.2	142.1		"	25' Rt " "	8.0	155.7	
+50		9.1	145.2		"	50' Rt " "	8.8	154.9	
+70		5.8	148.5		+25		13.1	150.6	
1+0		4.4	149.9		+50.25	$\Delta 90^{\circ} 23'$ Rt	13.91	149.84	02 Hub
+50		3.1	150.9		"	25' Lt of $\frac{1}{2}$	15.8	147.9	
2+0		2.1	152.2		"	50' " " "	16.6	147.1	
TP	9.79	163.75	0.38	153.96	+60		15.8	147.9	
+3302	P.O.T	9.23	154.52	02 Stub	+85		12.8	150.9	
+50		10.2	153.5		5+0		10.7	153.0	
"	25' Lt of $\frac{1}{2}$	10.6	153.1		+50		9.2	154.5	
"	50' " " "	13.6	150.1		6+0		7.2	156.5	
"	25' Rt " "	9.5	154.2		"	50' Lt of $\frac{1}{2}$	8.6	155.1	
"	50' Rt " "	6.6	157.1		+50		4.3	159.4	
3+0		8.9	154.8		7+0		2.6	161.1	
"	25' Lt of $\frac{1}{2}$	8.6	155.1		+50		0.9	162.8	
"	50' " " "	11.3	152.4		TP	11.60	174.59	0.76	162.99
"	25' Rt " "	5.0	158.7		8+0		10.7	163.9	
"	50' Rt " "	5.0	158.7		+50		9.5	165.1	
+50		8.4	155.3		9+0		8.4	166.2	
"	25' Lt of $\frac{1}{2}$	10.1	153.6		+52.90	$\frac{1}{2}$ E + N Alley	6.61	167.98	02 Hub
"	50' Lt " " "	13.4	150.3		10+0		4.2	170.4	
"	Rt " " "	6.4	157.3		+50		1.6	173.0	
"	Rt " " "	4.6	159.1						

indexed
c.s. 16

163.75

4

		174.59		
TP	6.87	181.01	0.45	174.14
1140			5.3	175.7
+50			4.1	176.9
+83.87 - N.Y. Pav.			2.97	178.04
+92.87 - Imperial Ave			2.91	178.10
TP	9.06	187.70	2.37	178.64
BM			2.83	184.87

8 p 5.25
Churchyard
+ Imperial

Levels Proposed Sewer Escuela & Hoyal St ✓
And Alley North of Imperial Ave

Indexed
6.5.16

Sept 14-16
Sisson
8155 T
Osborne
Herdin Rd. **6**

Sketch Page 1

88.93

BM	0.65	112.82	112.17	SEBR Imperial 4 47 43	57.0	90' Lt. Fly House + 2" Soil Pipe	7.26	81.57	07 Floor
	0.47	100.19	12.10	99.72	6+0		5.8	83.1	
	0.26	87.42	12.03	87.16	+5.0		5.9	85.6	
	3.81	79.18	12.05	75.37	+7.5	55' Lt. Fly House	1.10	87.83	07 Floor
0+0	= Existing Man Hole Scale	4.69	74.49	Top	7+0		0.6	88.3	
"		12.0	67.2	Ground	TP	12.07	101.57	0.43	88.50
+12		12.1	67.1		+5.0		11.1	90.5	
+25		9.7	69.5		8+0		7.8	93.8	
+50		6.2	73.0		+5.0		2.5	98.1	
1+0		6.2	73.0		TP	12.92	114.07	0.42	101.15
+50		5.5	73.7		9+0		10.4	103.7	
2+0		5.8	73.4		"	50 ft of 2"	1.40	100.1	
+50		5.7	73.5		+5.0		6.8	107.3	
3+0		5.3	73.9		10+0		4.5	109.6	
+50		4.5	74.7		"	50 ft of 2"	7.8	106.3	
"	100 ft of 2" Fly House	4.80	74.38	07 Floor	+6.0		1.1	113.0	
4+0		3.2	76.0		TP	11.83	125.45	0.45	113.62
+32.81	= 1/2 Hoyal A 90° 12.64	2.30	76.88	07 Hub	7.93	40' Lt. Fly House	11.40	114.05	07 Floor
+48.5	= 2" 20" Steel Culv.	1.2	77.9		11+0		10.5	115.0	
"	9.6 ft = inlet	2.56	76.62	Floor level	+5.0		8.9	116.6	
"	21.5 ft = outlet	3.62	75.56	"	"	50' Lt. Fly House	9.00	116.45	07 Floor
TP	10.32	88.93	0.57	78.61	12+0		7.8	117.7	
5+0		10.0	78.9		+5.0		7.0	118.5	
+50		8.1	80.8		12+0		6.2	119.2	
+70		7.3	81.6		+5.0		5.7	119.8	

Nogol St.

7

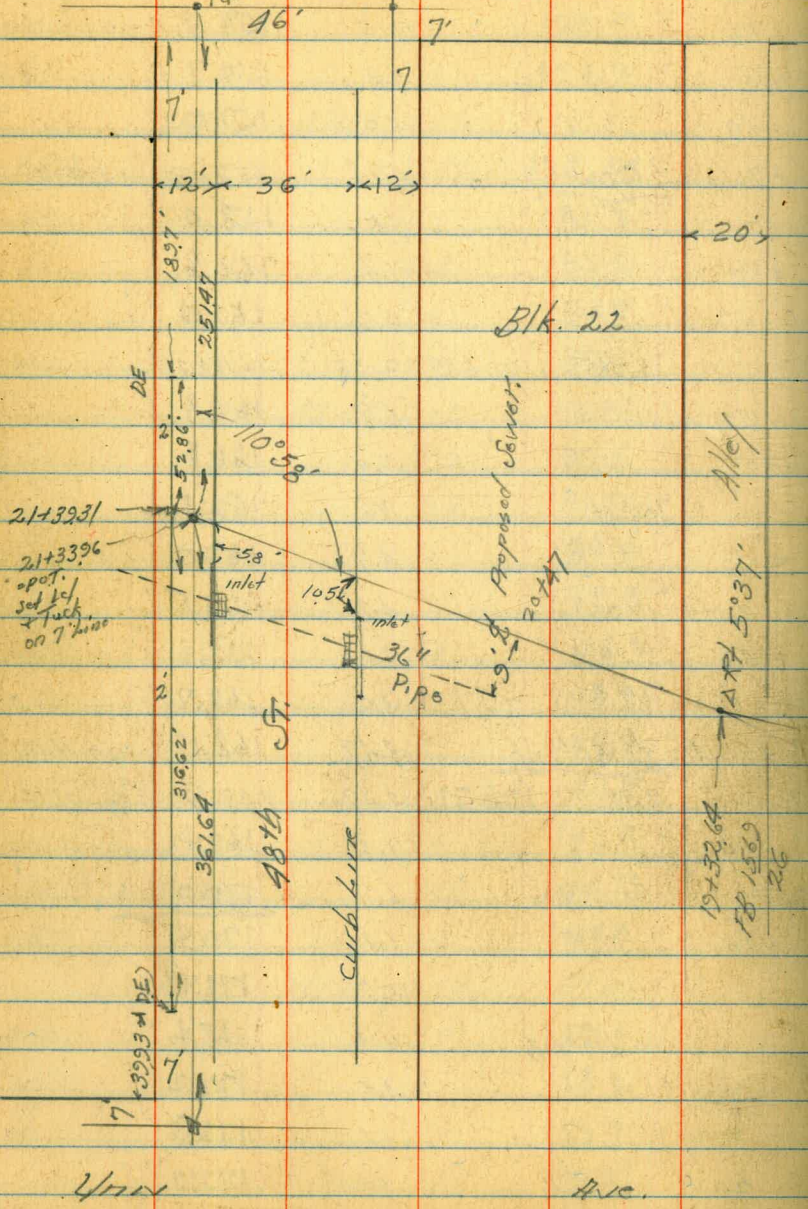
		125.45			
14+0			4.6	120.9	✓
+50			1.3	124.2	✓
TP	12.64	137.51	0.58	124.87	✓
+98.50	<u>Δ 90° 18' R</u>		9.42	128.09	07 Nov
15+50			6.3	131.2	✓
+81			5.3	132.2	✓
16+0			2.6	134.9	✓
"	50 Rt of $\frac{1}{2}$		5.4	132.1	✓
TP	12.57	149.45	0.63	136.88	✓
+50			12.0	137.5	✓
17+0			7.8	141.7	✓
"	50 Rt of $\frac{1}{2}$		10.1	139.4	✓
+20			7.2	142.3	✓
+50			3.3	146.2	✓
18+0	POT		1.10	148.35	07 Nov
+50			4.8	144.7	✓
"	50 Rt of $\frac{1}{2}$		8.0	141.5	✓
19+0			5.6	143.9	✓
+22.89	<u>Δ 90° 22' L</u>		4.72	144.73	07 Nov
+50			0.5	149.0	✓
TP	12.97	161.98	0.44	149.01	✓
20+0			9.9	152.1	✓
+50			8.8	153.2	✓
21+0			9.3	152.7	✓
"	80 Rt. N/Fly House		8.72	153.26	07 Nov

		161.98			
21+50			8.5	153.5	✓
22+0			7.3	157.7	✓
+50			5.0	157.0	✓
+71.13	<u>Δ 0° 30' L</u>		4.98	157.00	07 Nov
22+0			4.0	158.0	✓
+50			1.4	160.6	✓
24+0			0.0	162.0	✓
TP	10.05	171.68	0.35	161.62	✓
+50			6.9	164.8	✓
25+0			5.4	166.3	✓
"	100' L		9.6	162.1	✓
+50			4.7	167.0	✓
26+0			4.2	167.5	✓
+50			3.1	168.6	✓
27+0			3.0	168.7	✓
+21.14	<u>Δ 50° 14' S</u>		3.49	168.19	07 Nov
TP	8.52	176.71	3.49	168.19	07 Nov 27+21.14
+50			7.3	169.4	✓
28+0			6.7	170.0	✓
+50			6.3	170.4	✓
29+0			5.6	171.1	✓
"	100' L of $\frac{1}{2}$		11.3	165.4	✓
+50			4.5	172.2	✓
30+0			4.4	172.3	✓
+45			4.0	172.7	✓
"	100' L		12.9	164.5	✓

POLK

Fd. Ct. W. Pky.

Ave.



Blk. 22

Proposed Sewer

19+32.64
FB 1569
21
AT 5°37' Allev

Union

Ave.

Proposed Change in Line
Preliminary Location Sewer
Blk 22 - Between Estrella & 48th

" Union Ave And Polk

Original Location FB 1569
76

FB 1569-49

810 (316.48)

308.38

19+32.64 AT 5°37'	810	308.38 ✓
+50	71	309.4 ✓
3' W. in ditch	8.2	308.3 ✓
2' AT	5.2	311.3 ✓
19+65	5.1	311.4 ✓
+80	4.5	312.0 ✓
4.5 W = " "	6.3	310.2 ✓
20+00	3.9	312.6 ✓
+25	3.5	313.0 ✓
6' W. "Bottoms"	6.8	309.7 ✓
T.P. 9.06 (323.76)	178 (314.70)	
20+47	9.8	314.0 ✓
(20+47) 9' W = 36" Pipe	10.82	312.94 ✓
20+56 Top Fill	8.1	315.7 ✓
T.P. 9.18 (332.28)	0.66 (323.10)	
20+75.5 on Fill Top Bank	6.3	326.0 ✓
+81.1 = on Edge Walk	5.41	326.81 ✓
+86.3 " W " "	5.60	326.68 ✓
290 on cb	5.41	326.87 ✓
20+90 " Gut	6.14	326.14 ✓
21+09.4 = 48th	5.42	326.86 ✓

DBls. Checked

(332.28)

21+28.8 = W Gut	5.72	326.56	✓
" " cb	5.06	327.22	✓
21+32.5 E. edge Walk	5.13	327.15	✓
21+37.9 W. " "	5.19	327.09	✓
21+39.31 - 2' East of W.L. 48th	5.33	326.95	on stake
chk vi cb 21+21.75 FB 1861-49	4.53	327.75	✓
		327.72	
		0.03 diff.	
chk wharf W end	14.74	317.54	FB 1861
		317.50	P 50
		0.04	

Proposed Sewer To Serve Federal Blvd. Subs.
From Encanto Trunk Sewer to #1st + 49th St
"B" Line

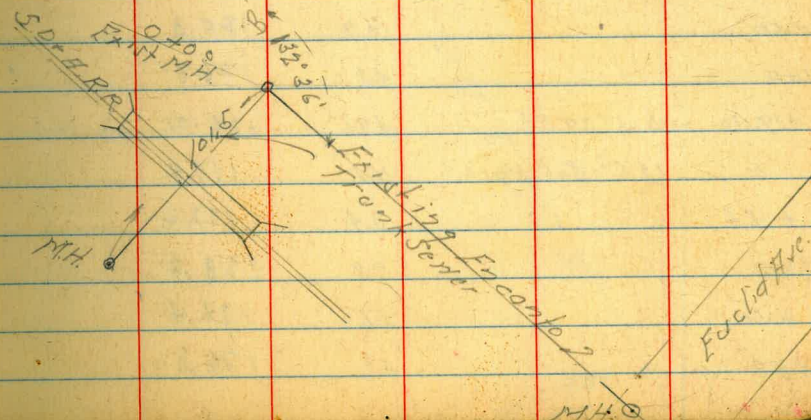
BM	4.12	108.34	109.22	8 p.m. H.C. or Bridge 2.00 So Market on Ferry Rd
0+0	Top Sealed M.H.	12.84	96.00	07 Cross
"	Ground	15.8	92.5	
+25		15.5	92.8	
+50		11.9	96.4	
+65		11.0	97.3	
1+0		15.1	93.2	
+25		15.8	92.5	
+35		11.8	96.5	
+50		11.8	96.5	
2+0		14.4	93.9	
+06		10.9	97.4	
TP	12.57	109.39	11.52	96.82
+50			13.5	95.9
3+0			14.0	95.4
+20			12.7	96.7
+40			10.4	99.0
+50			2.4	106.0
+60.3	= 5/4 Pav. on Market	3.20		106.09
+80.8	= 1/2 " " "	2.51		106.88
+101.3	= 1/4 " " "	2.25		107.14
TP	11.21	119.41	12.9	108.10
+15			11.1	108.3
+25			14.2	105.1
+50			14.2	105.2

Indexed
c.s.m.

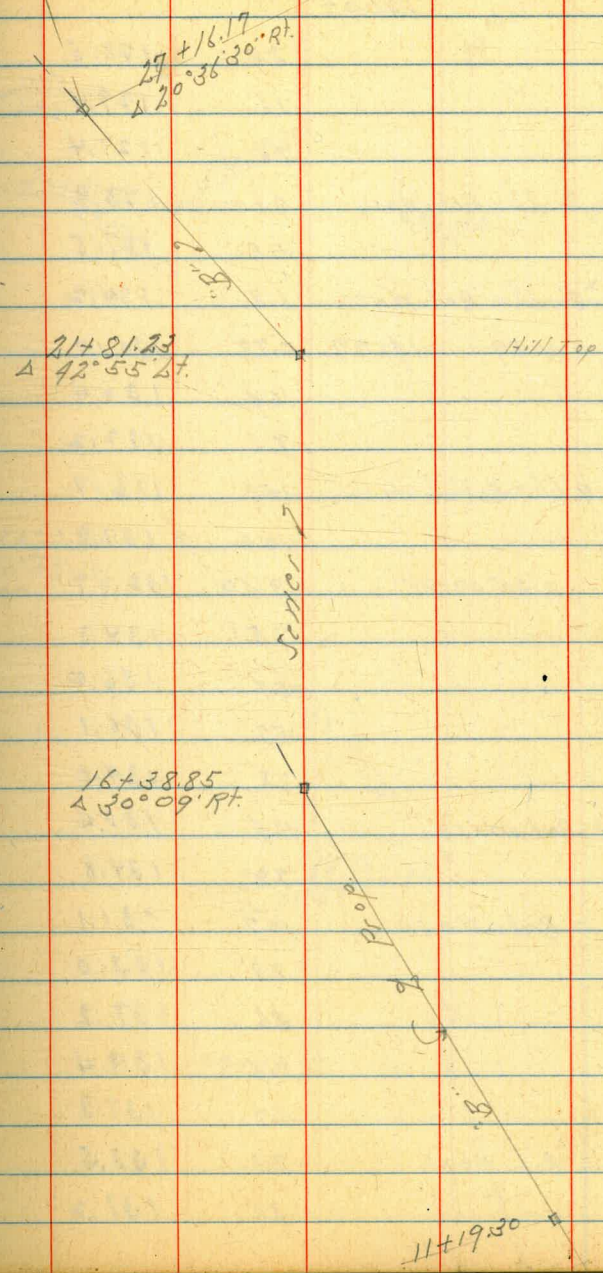
April 24-45
SUNSON
Bliss
Osborn

$\frac{11 \times 1930}{5 \times 29 \text{ Ft}}$

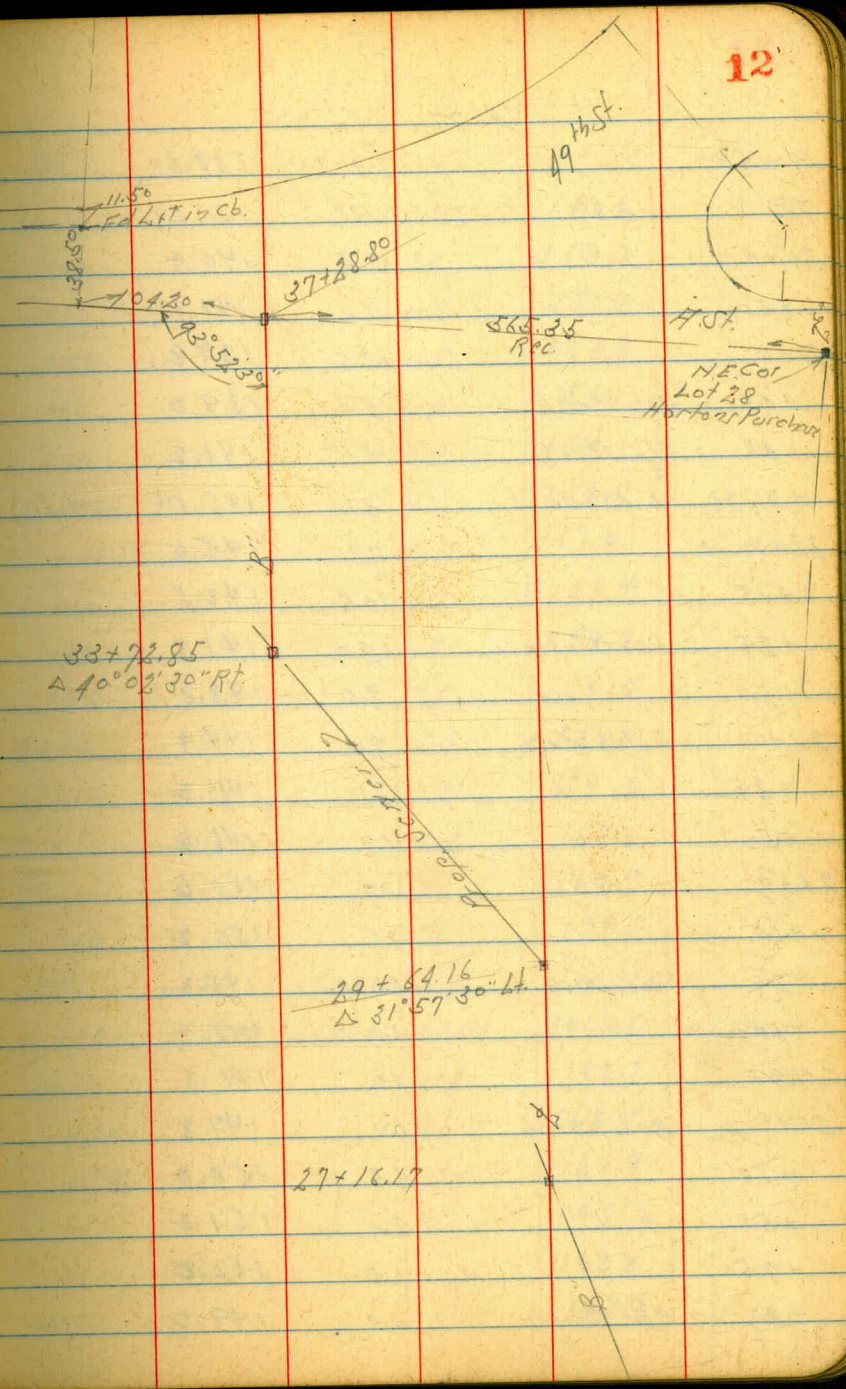
$\frac{64900}{215 \times 54 \times 30 \text{ Ft}}$



		119.41		
5+0		13.4	106.0	
+40	= Bottom Marsh	13.7	105.7	
+50		11.9	107.5	
6+0		10.7	108.7	
+50		7.9	111.5	
+90	= $\Delta 16^{\circ}54'30''$ Rt	59.5	113.46	07 Hnd
7+0.5'		8.6	110.8	
+35	= Bottom Marsh	10.0	109.4	
+50		7.9	111.5	
8+0		7.2	112.2	
+50		6.5	112.9	
9+0		1.7	117.7	
TP	1268	130.97	112	118.29
+50		11.7	119.3	
10+0		11.9	119.1	
+15	= Sly Marsh	13.7	117.3	
+38	= Bottom Marsh	14.1	116.9	
+50		10.7	120.3	
11+0		4.2	126.8	
+19.30	= $\Delta 5^{\circ}29'$ Rt	4.96	126.01	07 Stub
"	13.21: Bot Marsh	11.1	119.9	
+54		8.4	122.6	
12+0		7.8	123.2	
+50		6.1	124.4	
13+0		4.2	126.8	



		130.97		
13+50		2.5	128.5	
+85		1.6	129.4	
14+0		3.6	127.4	
"	8' Lt = Bot. Wash	7.1	123.9	
+50		3.5	127.5	
"	8' Lt = Bot. Wash	6.8	124.2	
TP	11.59	141.77	0.79	130.18
15+0		11.4	130.4	
+50		9.6	132.2	
"	9' Lt = Bottom Wash	15.1	126.7	
16+0		10.0	131.8	
+38.85	$\Delta 130^{\circ}09'91''$	9.40	132.37	on stake
+50		7.5	134.3	
17+0		5.4	136.4	
+30		5.7	136.1	
+50		7.8	134.0	
+60	= Bot. Wash	11.4	130.4	
+85		7.0	134.8	
+95	= Bot. Wash	10.7	131.1	
18+0		8.8	133.0	
+50		4.6	137.2	
+75		2.4	139.4	
19+0		4.0	137.8	
+20	= Bot. Wash	8.3	133.5	
+35		4.6	137.2	



		141.97			
19+50		2.3	139.5		
TP	12.80	153.25	132	140.45	
20+0			12.4	140.9	
+50			11.4	141.9	
21+0			13.5	139.8	
+15 = Bot Wash			14.3	139.0	
+45 = Fly Wash			13.1	140.2	
+81.23 = A 42° 55' Lt.			8.11	145.14	asstus
22+0			7.7	145.6	
+15			10.8	142.5	
+25 = Bot Wash			12.0	141.3	
+50			9.5	143.8	
23+0 = S.W. Wash			8.4	144.9	
+35			8.1	145.2	
+50			6.7	146.6	
24+0			2.7	150.6	
+15			3.1	150.2	
+25 = Bot Wash			8.0	145.3	
+50			5.0	148.3	
+95			4.0	149.3	
25+0 = Bot Wash			6.0	147.3	
+10			3.3	150.0	
+50			2.1	151.2	
+75			1.3	152.0	
+80 = Bot Wash			4.3	149.0	

		153.25			
TP	9.76	162.11	0.90	152.35	
26+0			9.5	152.6	
+12			8.9	153.2	
+22 = Bot Wash			11.2	151.9	
+50 in "			11.3	150.8	
+65 " "			11.0	151.1	
+70			8.0	154.1	
27+0			5.6	156.5	
+16.17 = A			5.10	157.01	asstus
+50			3.7	158.4	
+89			3.8	158.3	
+95 = Bot Wash			7.1	154.0	
28+0			5.3	156.8	
+50			2.8	159.3	
+63 = Bot Wash			5.3	156.8	
29+0			1.6	160.5	
+40			2.6	159.5	
TP	13.06	174.31	0.86	161.25	
+64.16 = A 31° 57' 20" Lt.			13.06	161.25	asstus
30+0			11.2	163.1	
+20			10.8	163.5	
+25 = Bot Wash			12.9	161.9	
+60			9.1	165.2	
+65 = Bot Wash			10.5	163.8	
31+0			7.0	167.3	

	174.31		5.5	168.8	
31+50					8M
32+0			3.9	170.4	
+34			2.2	171.1	
+40	Bot. Wash		5.6	168.7	
+70	"		4.4	169.9	
33+0			0.9	173.4	
TP	12.93	185.31	19.3	172.58	
+30			12.2	173.1	
+35	Bot. Wash		14.6	170.7	
+50			10.9	174.4	
+72.85	A 40°02'30" Rt		8.53	176.78	on Stud
+78			8.5	177.8	
+83	Bot. Wash		11.5	173.8	
34+0	17 "		9.7	175.6	
+50	" "		8.5	176.8	
35+0	" "		3.9	181.4	
TP	13.11	198.12	0.30	185.01	
+50			14.5	183.6	
+70			10.9	187.2	
36+0			7.1	190.7	
+25			6.7	191.4	
+50			1.3	196.8	
TP	12.31	209.19	1.24	196.88	
37+0			7.1	201.8	
+28.80			5.79	203.40	on Hob

209.19

0.90

208.29

✓ NE Top. of Hill
 H St + 49 1/2 ft
 208.29
 1682.14

Proposed Sewer 47th St. A" Line
From Encanto Trunk Sewer to 47th 49th

Indexed
e.s.k.

April 26. 45
Sisson
Bliss
Osborne

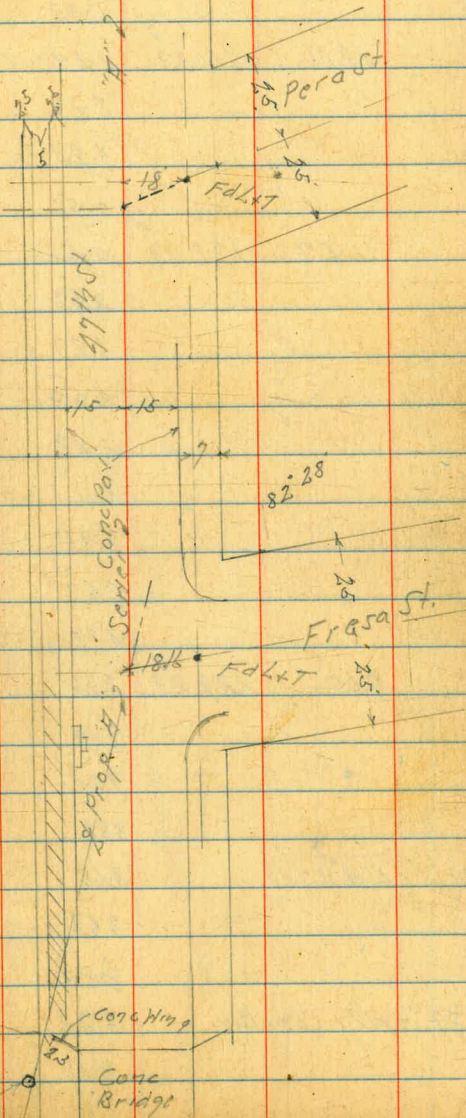
15

BM	4.93	80.50		75.37	Lat 2/10901 E of Line 47th Page 6
0+0	= Top Sealed M.H.	10.20		70.0	
"		14.9		65.4	
+25		11.8		68.5	
+30		5.0		75.3	
+63	= 1/4 Conc Walk	4.83		75.47	
+75	= Fly " "	5.04		75.26	
+98	= W. Cb. of 47th St.	5.09		75.21	
"	Gutter on Conc Pav	5.67		74.63	
+70.80	A 12" Ht	5.59		74.71	Crossed Pav
TP	12.89	88.44	4.75	75.55	
2+0		11.07		75.37	on paving
+50		10.73		77.71	"
3+0		8.48		79.96	"
+50		6.10		82.34	"
+70		5.18		83.26	"
+93.40		4.81		83.63	"
4+0		4.73		83.71	"
+50		4.06		84.38	"
5+0		3.25		85.19	"
+50		2.70		85.74	"
6+0		1.81		86.60	"
+50		1.09		87.35	"
TP	12.93	100.01	1.56	87.08	
7+0		11.31		88.70	

3193.40
3+87.26
Calc. GRH

1+70.80
A 12" Ht

0+89
0+00
Existing M.H.
Conc Wing
Conc Bridge



22 00
17 39 37
4 6063

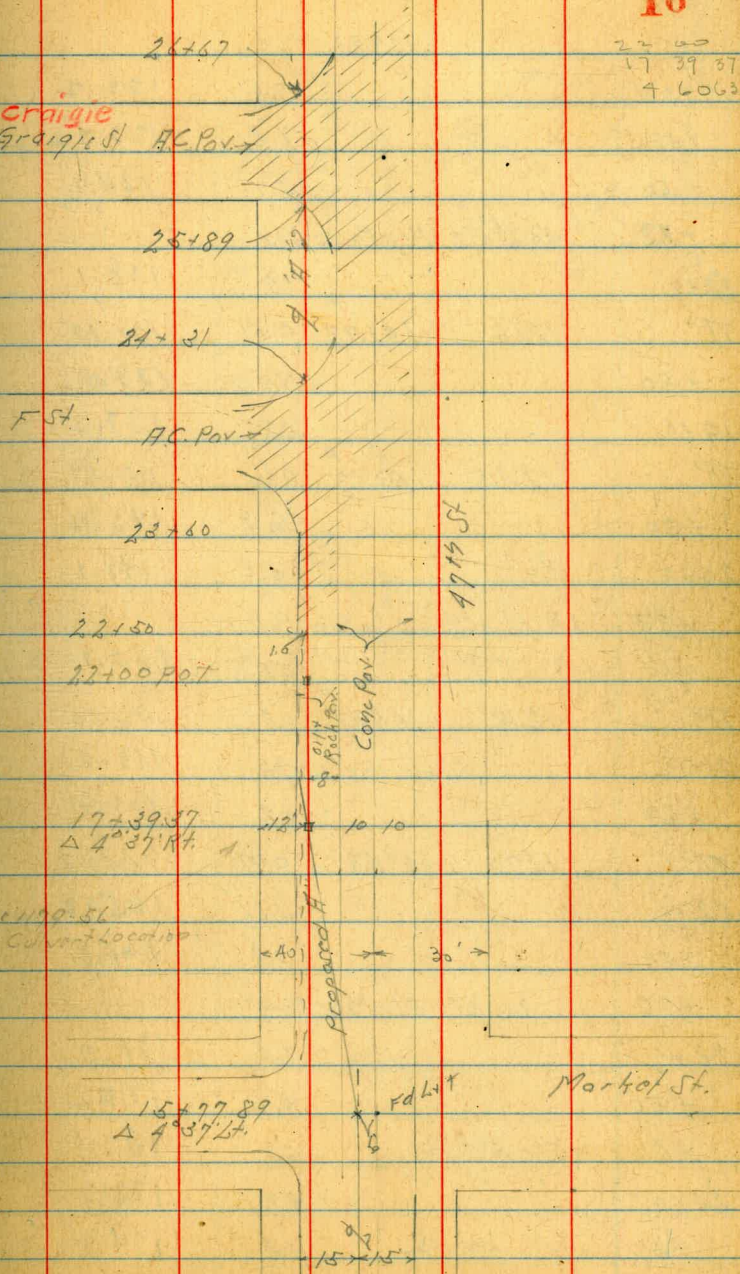
	100.01			
7+50		898	91.03	on Pav 199
8+0		5.44	94.57	" "
+50		1.33	98.68	" "
TP	12.66	111.33	1.34	98.67
9+0		8.37	102.96	on Pav 199
+50		4.23	107.10	" "
10+0		0.51	110.82	" "
TP	11.57	122.39	0.51	110.82
+50		8.61	113.78	
11+0		6.29	116.10	
+50		4.50	117.89	
12+0		3.42	118.97	
+50		3.11	119.28	
13+0		2.86	119.53	
+50		2.60	119.79	
14+0		2.17	120.22	
TP	9.60	129.83	2.16	120.23
+50		9.39	120.44	
15+0		9.01	120.79	
+50		8.82	121.01	
+77.89	-4 9 37 44	8.65	121.18	
BM		8.68	121.15	2 41 7 Mark 11+47 120.95
16+0		8.25	121.48	
+38.89	-w/ly Cond Pav.	8.23	121.60	
+50		8.18	121.65	

Craigie
Craigie St AC Pav

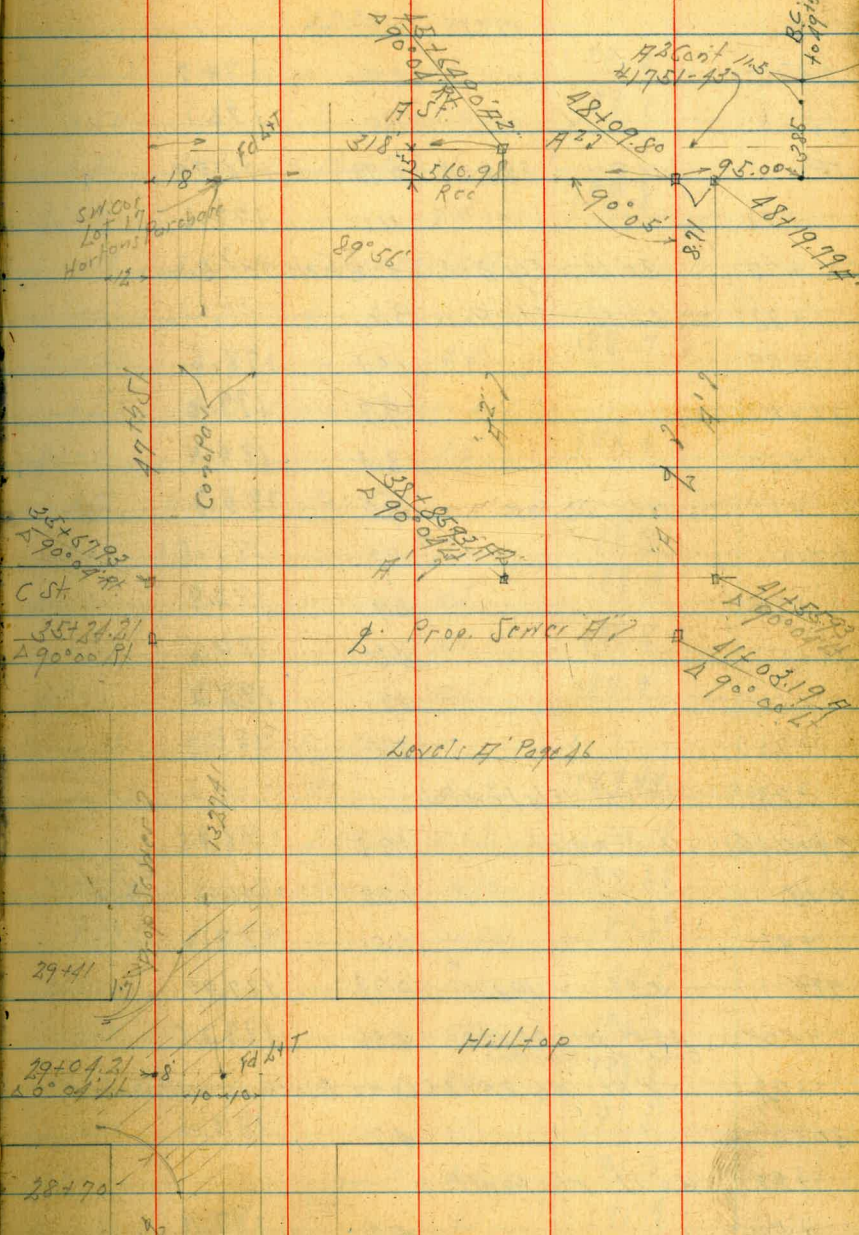
F St.
AC Pav

Sec 1199-56
For Current Location

15+77.89
-4 9 37 24



	12983			
17+0		76	122.2	
+39.87 - A		6.51	123.32	020+0.6
+50		5.7	124.1	
+82	33 Lt of 8 Fly Power Pole			
18+0		1.7	128.1	
TP	12.66	141.98	0.51	129.32
+50		9.0	133.0	
19+0		3.8	137.2	
TP	12.35	153.67	0.66	141.32
+50		10.5	143.2	
20+0		5.6	148.1	
+33	35 Lt of 8 Fly Power Pole			
+50		0.6	153.1	
TP	12.19	165.59	0.27	153.10
21+0		7.6	158.0	
+50		3.2	162.4	
TP	12.70	177.58	0.71	164.88
22+0		11.66	165.92	020+0.6
+50		8.8	168.8	
+82	3-1 Lt Fly Power Pole			
23+0		6.6	171.0	
+50		5.4	172.2	
+60	5-1 Fly Power Pole	5.2	172.4	
24+0		3.9	173.7	
+21	5-1 Fly Power Pole	3.2	174.3	



		197.58		
24+50			2.9	174.7
25+0			1.5	176.1
TP	11.81	188.68	0.71	176.87
+50			11.1	177.6
+77	3.0' Lt = Fly 3' x 3' Conc Block			Tcl. Road
+82	3.2' Lt = Fly Por. Pole			
+89			10.1	178.6
26+0			9.7	179.0
+50			8.3	180.4
+67	W/4 Ac. Pav.		7.9	180.8
27+0			7.2	181.5
+50			5.9	182.8
28+0			4.2	184.5
+50			2.9	185.8
+70			2.4	186.3
+78	3.0' Lt = Fly Por. Pole			
29+0 4.21	- Δ 0° 04' Lt		1.73	186.95
BM			1.72	186.96
+41			1.5	187.2
TP	5.21	193.11	0.78	187.90
+50	3.2' Rt = W/4 2.2' x 2.2' Conc 17' x 17' Hole 9' or		5.86	187.25
+92	0.4' Rt = W/4 2.5' x 2.5' Conc Block School Guard			
30+0			4.7	188.4
+22	3.0' Lt = Fly Por. Pole			
+50			5.2	187.9

		193.11		
31+0			5.1	188.0
+50			5.0	188.1
+83	3.5' Lt = Fly Por. Pole			
32+0			4.3	188.8
+14	2' Lt = Fly 6" Pepper Tree			
+30	2.2' Lt = " " "			
+50			4.4	188.7
+62	1.8' Lt = Fly 6" Pepper Tree			
33+0			4.5	188.6
+42	3.5' Lt = Fly Por. Pole			
+50			4.2	188.9
34+0			4.2	188.9
+50			3.6	189.5
35+0			3.2	189.9
+02	3.5' Lt = Fly Por. Pole			
+24.21	- Δ 90° 00' Rt		3.62	189.49
TP	10.66	200.15	3.62	189.49
+32.21	= W/4 Conc Pav		10.90	189.25
+52.21	= Fly " "		10.86	189.29
36+0			10.1	190.1
+50			9.7	190.5
37+0			9.4	190.8
+50			8.7	191.5
38+0			8.5	191.7
+50			8.5	191.9

		200.15			
39+0			7.9	192.3	
+50			7.4	192.8	
40+0			6.9	193.3	
+20	= Ely Playground		6.2	194.0	
+28			4.0	196.2	
+50			3.8	196.4	
41+03.19	= 290° 00' W		2.69	197.46	02 Stub
+50			2.2	198.0	
TP	9.46	208.71	0.90	199.25	
42+0			9.3	199.4	
+50			8.8	199.9	
43+0			7.6	201.1	
+50			6.7	202.0	
44+0			7.7	201.0	
+50			7.4	201.3	
45+0			7.5	201.2	
+20			7.1	201.6	
+50			8.6	200.1	
46+0			10.1	198.6	
+15			10.5	198.2	
+50			9.5	199.2	
47+0			8.0	200.7	
+50			6.7	202.0	
48+0			4.3	204.4	
+09.80			4.19	204.52	02 Stub

		208.71			
TP	4.70	209.22	4.19	204.52	NETOPANND
BM			0.80	208.42	HST+4915
					208.29 = 0.16

indexed
e.s.k.

C.S.M. Proposed 1" Main on Roseland Dr
C.S. Torrey Pines Rd. to Spindrift,
6-25-45.

E Levels on Roseland Dr.

Torrey Pines Rd
Calle de La Plata

Torrey Rd. to Spindrift

NWBP	11.71	66.40	54.69
TP	6.83	72.44	65.59

0+00 Sedge 30 Strip pav	1.07	71.35
-------------------------	------	-------

0+25 A 22°30' LT = B.C. LT	2.88	69.59
----------------------------	------	-------

+30	3.19	69.23
-----	------	-------

+32	2.9	69.5
-----	-----	------

+64 Flagstone Walk	6.53	65.89
--------------------	------	-------

+64 " "	6.15	66.27
---------	------	-------

0+82.12 F.C. Stub	7.82	69.60
-------------------	------	-------

1+29.42	12.73	59.69
---------	-------	-------

TP	0.23	59.93	12.72	59.70
----	------	-------	-------	-------

1+41.2 Top Con. Wall	0.86	59.07
----------------------	------	-------

1+41.7 IN Drive	2.4	57.5
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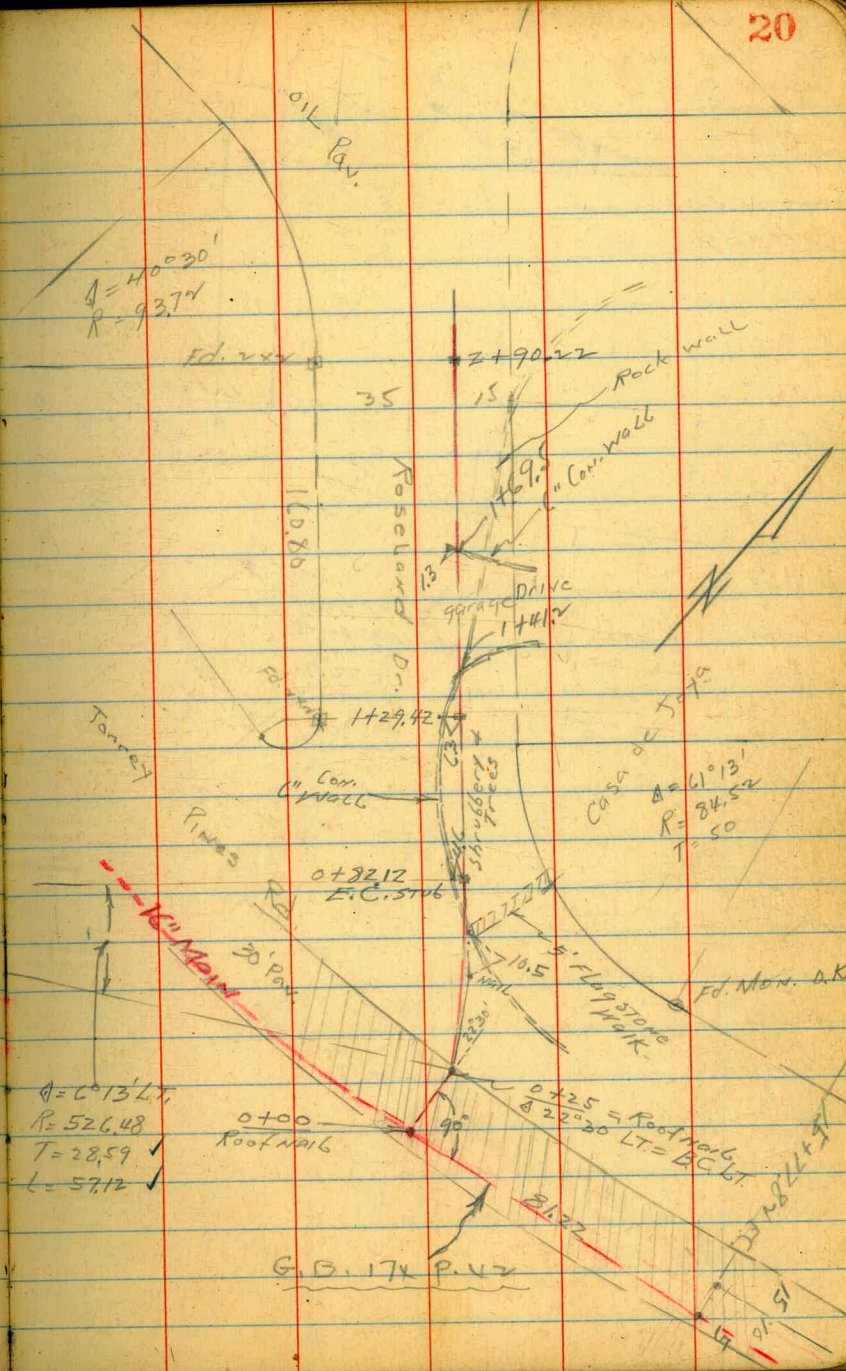
1+69.5 " "	4.3	55.6
------------	-----	------

1+69.5 Top Con Wall	3.73	56.20
---------------------	------	-------

1+73.3 Top Rock wall	3.9	56.0
----------------------	-----	------

"	4.4	55.5
---	-----	------

Cont'd. P. 24



$\Delta = 6^\circ 13' LT$
 $R = 526.48$
 $T = 28.59$
 $L = 57.12$

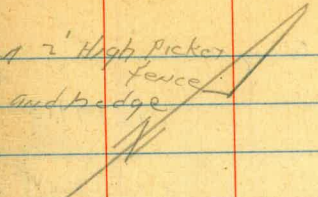
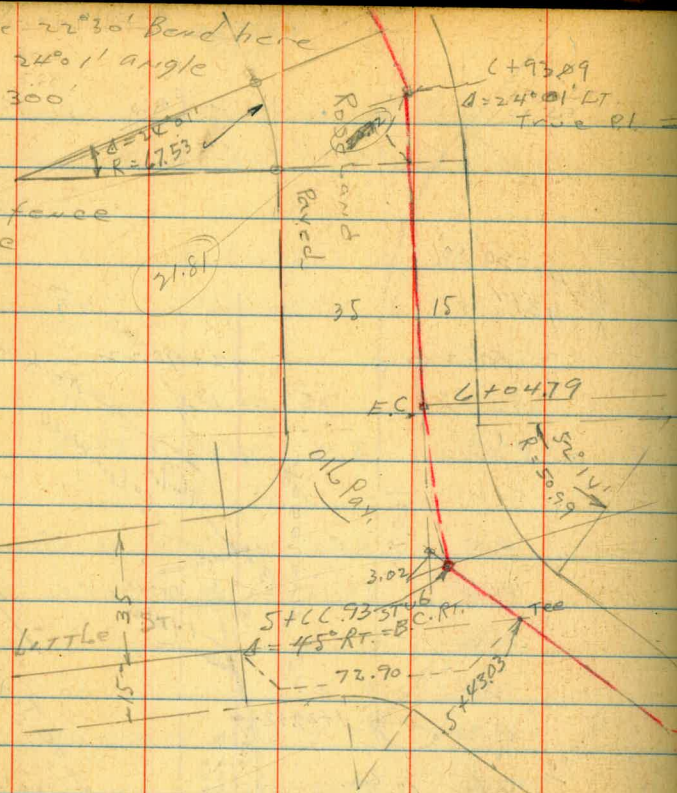
0+00
Rock Wall

0+25 = Rock Wall
 $\Delta = 22^\circ 20' LT = B.C. LT$

G.B. 174 P. 47

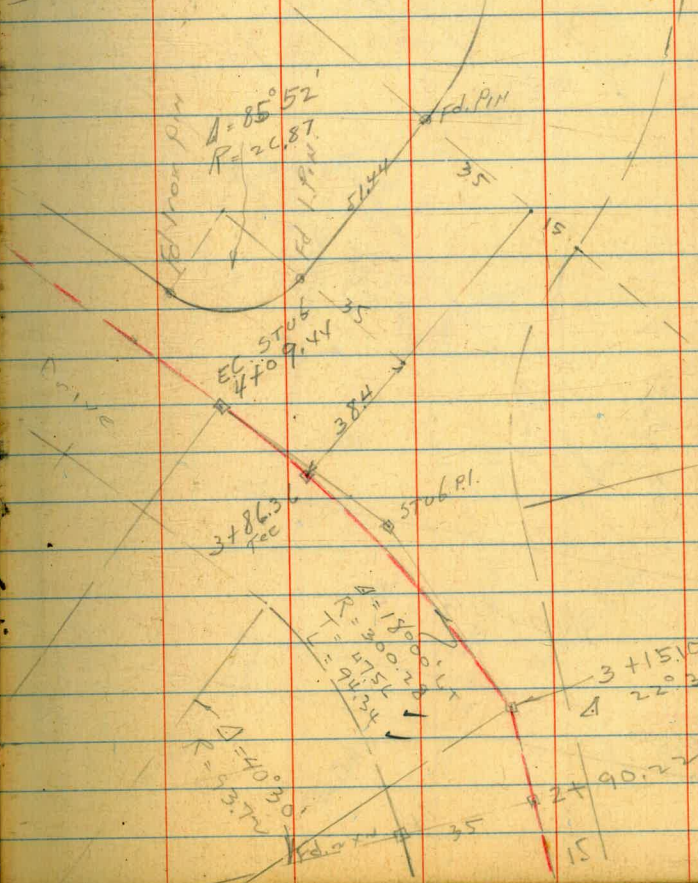
Can use 22°30' bend here
 or use 24°1' angle
 with R. 300

Suggest
 latter
 acct. of fence
 + Hedge

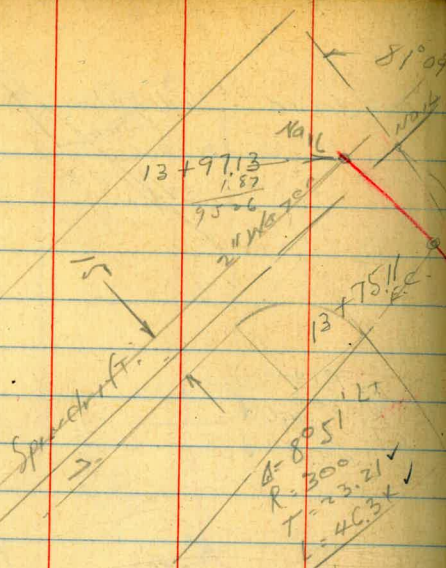


Ave. Alameda

$\Delta = 7°14'$
 $R = 300$
 $T = 1896$
 $L = 37.87$



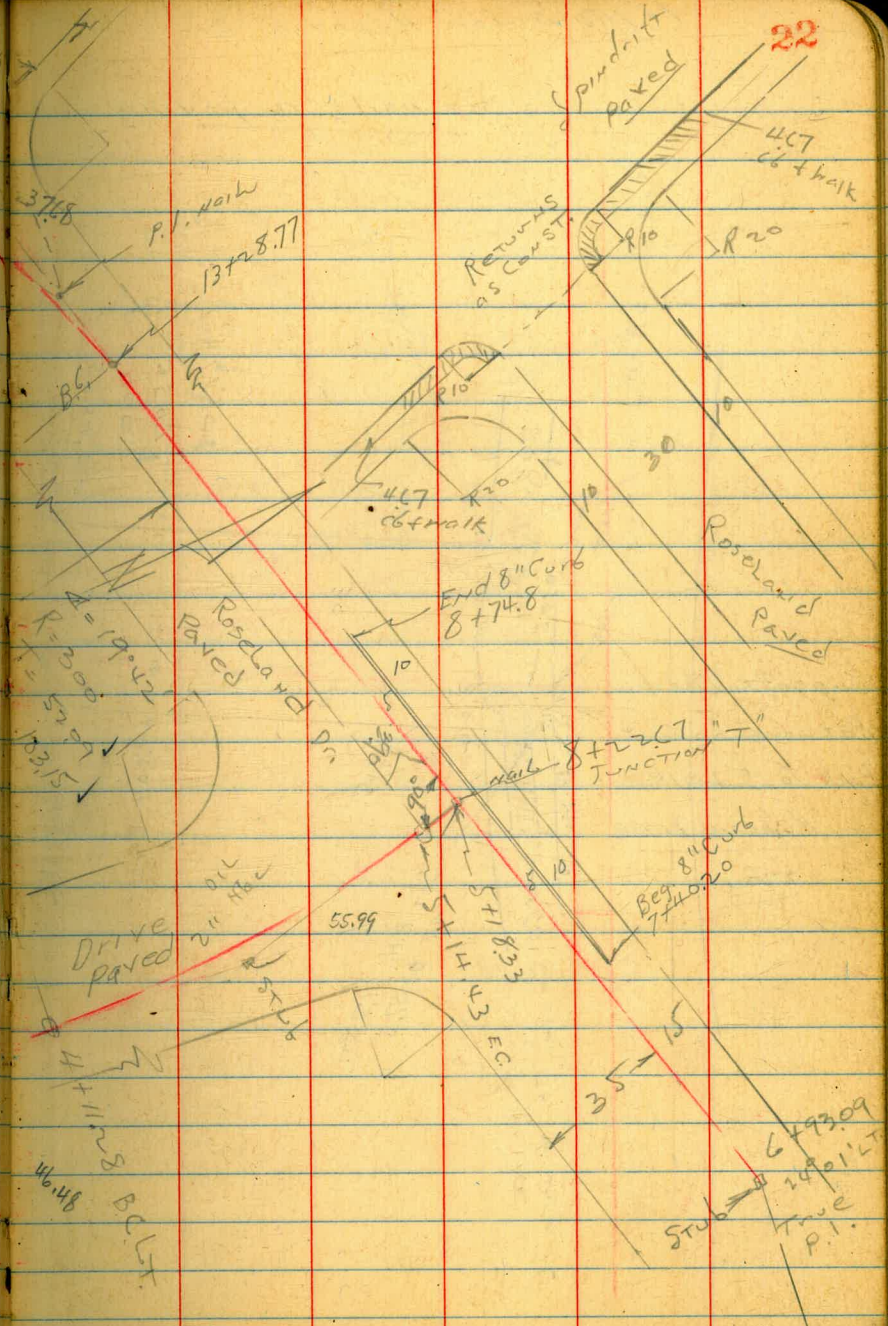
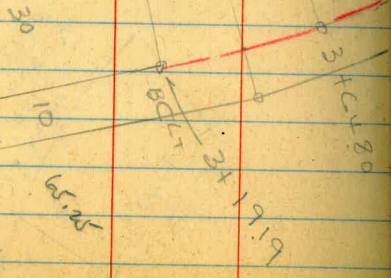
o = nails



$\Delta = 6.33'$
 $R = 400$
 $L = 218.2$
 $L = 56.11$

$\Delta = 15.5' \times 20''$
 $R = 400$

Hypatia
 EC 2
 153.11
 30
 10
 65.25



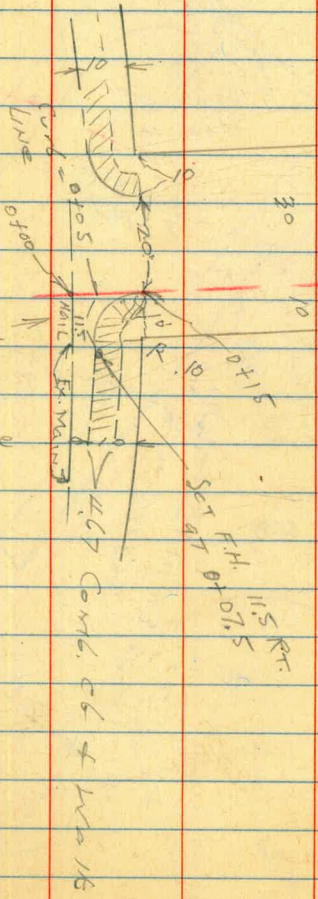
$\Delta = 19.42'$
 $R = 300$
 $L = 57.97$
 $L = 13.15$

Stub
 6493.09
 1461.17
 true P.I.

Main for Hypatia Dr.

D = NAILS IN PAVING

St. Louis Tern



Suggest these
 Return to cut
 back to 5' walk
 on Hypatia Drive
 CSAN

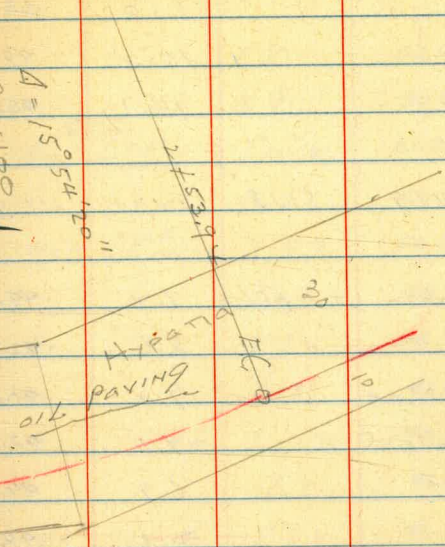
$L = 500.21' 50''$
 $R = 400'$
 $T = 354.7'$
 $T = 17.75'$

$0.678, 0.4 BCLT$

$1 \times 33.57' EQ$

4.39

$A = 15^{\circ} 54' 12''$
 $R = 400'$
 $T = 558.8'$
 $L = 111.9'$



$BCLT 1417.90'$

FRONT P. 110
59.93

5445

2 + 00		6.0	53.9	
+ 50		10.2	49.7	
✓ + 90.22		14.1	45.8	
T.P.	419	5118	12.94	416.99
3 + 15.10 = 22°30' LT = BC LT		7.2	44.0	
+ 50		8.6	42.6	
+ 8(36) = Tee		9.4	41.8	
4 + 109.44 = F.C.		9.1	42.1	
+ 45		6.9	44.3	
+ 90		2.1	49.1	
T.P.	10.19	61.11	0.26	50.92
5 + 10		9.8	51.3	
+ 43.03 Tee		7.3	53.8	
+ 66.93 = 45° R = BC RT		5.65	55.26	STUB
+ 80		5.4	55.7	
6 + 04.79 FC		5.7	55.22	
+ 40		6.8	55.3	
6 + 93.09 = true P.I. 224°21' LT		8.3	52.0	STUB
Note! Can Use 22°30' Bend here.				
SET SPIKE T.P. in Pole # 7951	0.39	54.45	7.05	54.06

7		1.8	52.6	
+ 110.22		3.9	50.6	
" 5' RT	Begin Top curb	3.22	51.23	
+ 50		4.1	50.2	
" 5' RT	TOP CURB	3.59	50.86	
8 + 03		5.7	48.8	
" 5' RT	TOP CURB	5.54	48.91	
8 + 27.67 "Tee"		6.5	48.0	
" 5' RT	TOP CURB	6.42	48.03	
+ 50		7.6	46.8	
" 5' RT	TOP CURB	7.53	46.92	
+ 74.8		8.6	45.8	
" 5' RT	End Top curb	8.56	45.89	
9		9.6	44.8	
+ 50		12.1	42.2	
T.P.	0.50	42.65	12.30	42.15
+ 75		1.7	41.0	
10		3.4	39.2	
+ 25		5.0	37.6	
+ 50		6.6	36.6	
+ 75		8.5	34.2	
11		10.5	32.2	

		42.65 ✓		
T.P.	0.08	<u>30.42</u>	12.31	30.34
11+50			2.4	28.0
12			6.5	23.9
+50			10.0	20.9
13			12.9	17.5

T.P.	0.80	<u>18.36</u>	12.86	17.56
------	------	--------------	-------	-------

13+28.77 BC			2.0	16.9
-------------	--	--	-----	------

CTR Curve			3.0	15.9
-----------	--	--	-----	------

13+75.11 EC			3.9	14.5
-------------	--	--	-----	------

" 10' Rt for F.H.			3.8	14.6	ground
-------------------	--	--	-----	------	--------

+82.2			4.2	14.2
-------	--	--	-----	------

" 9.5 Rt ch end			4.53	13.7
-----------------	--	--	------	------

13+97.13 - approx			4.1	14.3
-------------------	--	--	-----	------

2" line

on Spindrift & Roseland.

SE BC curb		Spindrift & Roseland	12.28	1.08
------------	--	----------------------	-------	------

Please
check
to Profile

		18.36 ✓		
T.P.	12.78	<u>30.57</u>	0.57	17.79
T.P.	12.71	43.17	0.11	30.46
T.P.	12.34	55.50	0.01	43.16

Spoke B.M.	Pole # 7951 75' E of Hypatia S side Roseland		1.44	54.06	54.06
------------	--	--	------	-------	-------

T.P.	12.85	<u>67.24</u>	0.13	54.37
------	-------	--------------	------	-------

T.P.	12.43	<u>79.65</u>	0.00	<u>67.24</u>
------	-------	--------------	------	--------------

T.P.	12.32	<u>91.84</u>	0.13	<u>79.65</u>
------	-------	--------------	------	--------------

check to B.M. BP	xw Little L & Tarnay		7.57	90.17	90.11
------------------	-------------------------	--	------	-------	-------

T.P.	0.09	<u>83.34</u>	9.59	83.25
------	------	--------------	------	-------

T.P.	1.92	<u>72.32</u>	12.94	70.40
------	------	--------------	-------	-------

E Water Levels
 on Hypatia Dn
 St Louis Tean to Roseland

66.93 ✓

		72.32 22	Fnd.	
0 + 00	Pay		7.1	65.2
+ 05			7.4	69.9
"	11.5 Pt Top		5.1x	66.68
+ 15	qut.		7.2x	65.08
"	cb end		6.4x	65.90
+ 50			5.8	66.5
0 + 98.0x	BCLT		3.8	68.5
	ctr Curve		3.0	69.3
1 + 33.5	EC		2.3	70.0
1 + 42.90	BCLT		2.0	70.3
+ 79.71			0.8	71.5
2 + 16.9x			0.3	72.0
2 + 53.9x	EC		0.5	71.8
+ 80			1.3	71.0
3			2.4	69.9
3 + 17.9	BCLT		3.9	68.9
+ 42			5.7	66.6
T.P.	0.29	66.93 22	5.68	66.6x
3 + 64.80	EC		2.5	64.2
4			6.1	60.8

14' ft. of 0 + 05 = M.L. W. Brat Walk
 to HOUSE
 10' ft. = 2 Meters in Walk

4 + 11.28	BCLT	7.4	59.5
+ 45.66		11.5	55.9
T.P.	0.47	54.83	12.57
4 + 80.04		3.8	51.0
+ 96		5.6	49.2
5 + 14.23	EC	6.6	48.2
5 + 18.33	"T" at Roseland	6.9	47.9
check to Spike P.P. # 7951	0.77	54.06	54.06
75' E of Hypatia + Roseland			

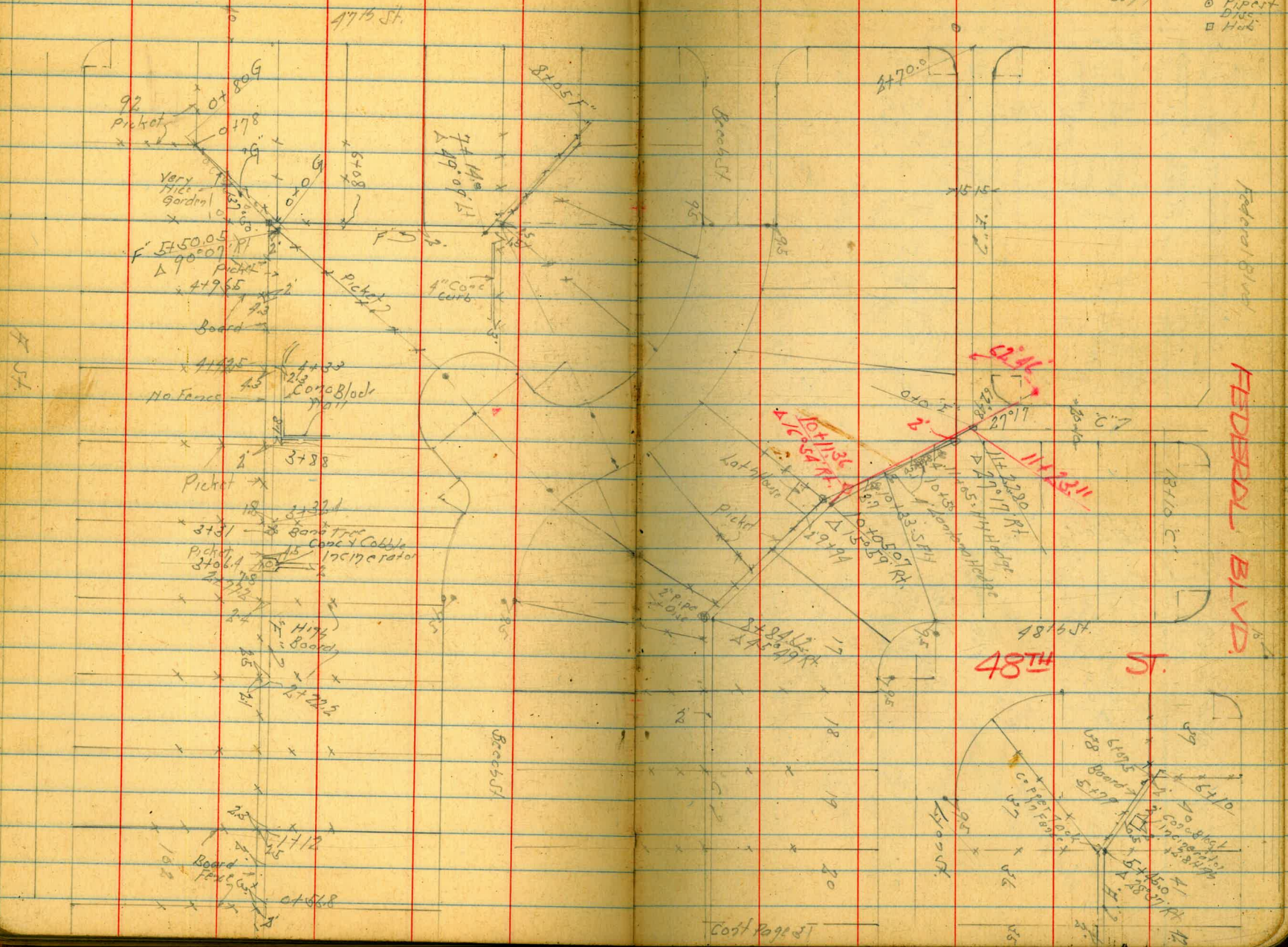
Notes Reduced - 8-2-95

Proposed Sewers Federal Blvd Subs #1 & 2

Indexed
C.S.K.

July 18, 1945
51509
81138
05601.57
8099

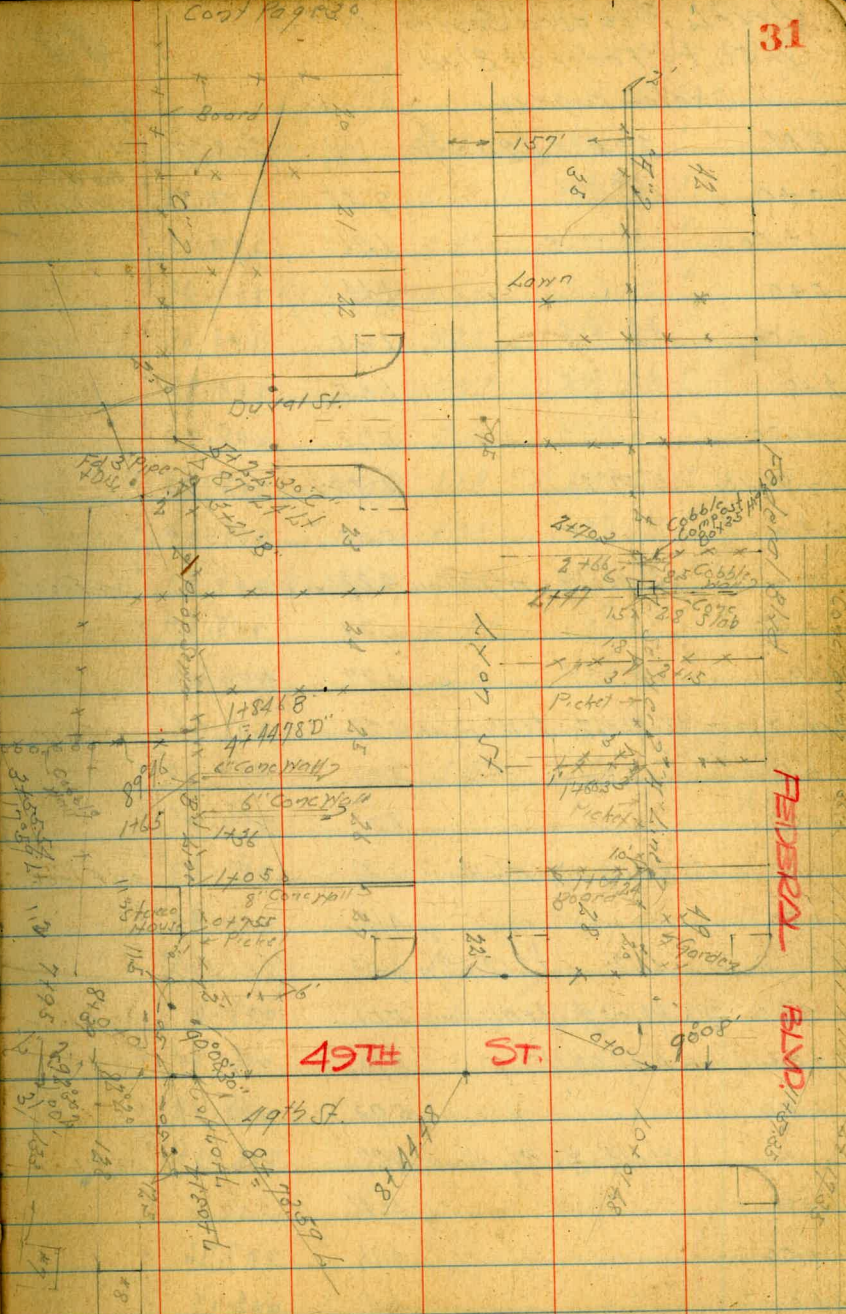
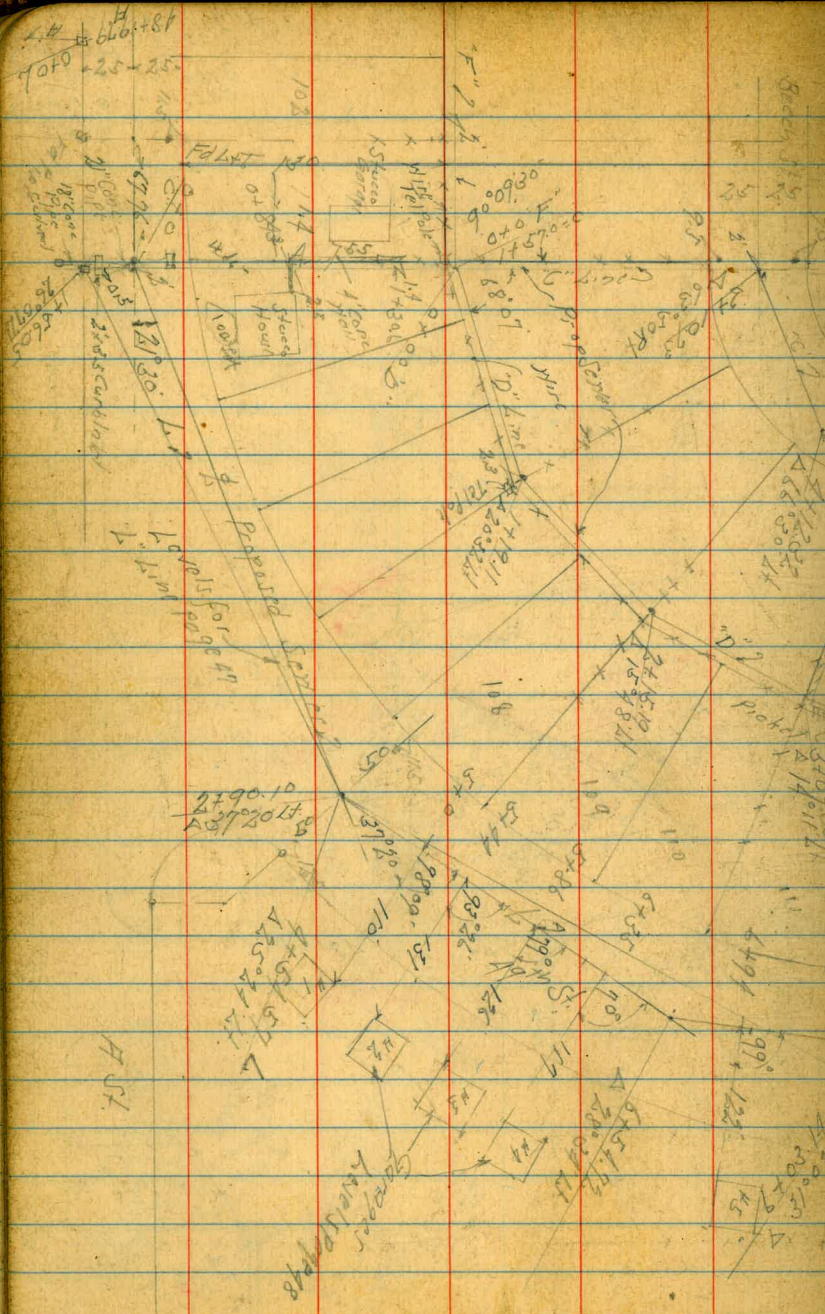
30
Packed Road
Lead
Tack
Pipe
Blind
Hick



FEDERAL BLVD.

48TH ST.

Cost Report



FELDER

BLVD. HARRIS

49TH ST.

Levels Proposed Senior 1974/5

H St. to Federal Blvd.

Sketch Page 81

Sketch on sheet

July 10-45
S. 1107
81' W.
Osborne
8099

BM	3.74	(211.03)	208.29	8+14.48	2 Lyon to West	3.89	208.73	✓
0+0		7.45	203.58	9+0		2.67	209.95	✓
+50		6.96	204.07	+50		0.41	214.21	✓
1+0		6.64	204.39	TP	12.86	(224.89)	212.09	✓
+50		6.35	204.68	10+0	14.8	9.23	215.66	✓
2+0		6.05	204.98	+50		5.73	219.16	✓
+50		5.73	205.30	11+0		2.10	222.79	✓
+90.10 = Δ 87° 20' L		5.38	205.65	TP	6.05	(229.27)	(223.21)	✓
3+0		5.09	205.64	+59.35		4.00	225.26	✓
"	80 Rt of Δ = 1/2 Wly House	4.22	206.81	on Floor	+81.5 = Sky Canopy Federal	3.75	225.51	✓
+50		5.34	205.69		+99.35 = 1/2 " " "	3.41	225.85	✓
4+0		4.97	206.06		12+17.35 = " " "	2.77	225.49	✓
+10	96 Rt of Δ = 1/2 Wly House	3.78	207.25	on Floor				
+50		4.73	206.30		BM	3.89	(225.37)	✓
5+0		4.58	206.45					
+15	88 Rt of Δ = 1/2 Wly House	3.40	209.63	on Floor				
+50		4.63	206.40					
TP	6.12	(212.62)	4.53	(206.50)				
+70	77 Rt of Δ = 1/2 Wly House	5.01	207.61	on Floor				
6+0	Δ 31° 02' L	6.10	206.54					
+50		5.93	206.69					
"	Rt of Δ = 1/2 Wly House	4.27	206.35	on Floor				
7+0		5.46	207.16					
+50		4.86	207.76					
8+0		4.41	208.13					

J.E. Taptin
Federal Blvd
4474 S.
225.32

Levels Prop Server "H" Line
Federal Blvd Sub #1

Sketch Page 31

BM	0.80	1226.17	225.32	✓	SE Top Fire H Federal Blvd #4915 St
0+0	= 1/2 49 1/2 St	10.49	215.63	✓	
+39.5	- Top Rail Typ Curb	11.30	214.82	✓	
+50	2 1/2 1/2 of 1/2 - NY F Board	11.3	214.8	✓	
+51	1/2 - Fly Young Berry Row	10.4	215.7	✓	
+05	2 - NY Young Berry				
+05	5.281 = Sky Tel Pole # 448333H				
+50		96	216.5	✓	
TP	1251	230.06	217.55	✓	
+60.3	- NY S Picket Fence	13.2	216.9	✓	
1+50	78 Lt of 1/2 - 1/2 NY House	130	217.1	✓	on Floor
+61		11.7	218.4	✓	
+97	0.5 Rt of 1/2 - Sky Clothes Post	9.7	220.4	✓	
"	79 Hold - 1/2 NY House	9.0	221.1	✓	on Floor
+15.2	2.8 Rt - Sky Tel Pole # 448334H				
	- NY S Picket Fence	7.7	222.4	✓	
	1.8 Lt of 1/2 - Picket				
+50		6.6	223.5	✓	
"	78 Hold - NY House	6.2	223.9	✓	on Floor
+62	1.3 Rt of 1/2 - Sky 4" x 4" Clothes Post				
+70.3	- NY S Picket Fence	5.4	224.7	✓	
"	1.8 Lt of 1/2 - Fly Picket Fence				
3+0		5.1	225.0	✓	
"	78 Lt of 1/2 - NY House	4.3	225.8	✓	on Floor
+23.2	- NY S Picket Fence				
"	2 Lt of 1/2 - Fly Picket Fence				
+50		5.0	225.1	✓	
"	78 Lt of 1/2 - NY House	4.4	225.7	✓	on Floor
+99	0.7 Lt of 1/2 - NY Tel Pole # 448335H				
+80	- NY S Picket Fence				
4+0	1.9 Lt of 1/2 - Fly Picket Fence	4.4	225.7	✓	
+27	1.3 Lt of 1/2 4"x5" Clothes Post				

		230.06			
4+55.4	- NY S Picket Fence to - Sky Young Berry				
	1.8 Lt of 1/2 - Fly Picket Fence	5.0	225.1	✓	
+50					
+70	78 Lt of 1/2 - NY House	4.0	226.1	✓	on Floor
+83	2 - Sky 4" x 4" Clothes Post				
+90	- NY S Picket Fence				
	2.1 Lt of 1/2 - Fly Picket Fence				
5+0			225.8	✓	
+44.5	0.8 Lt of 1/2 - NY Tel Pole # 448336H				
+45	1.28 37 Rt - NY S Picket	4.3	225.8	✓	
"	2.1 Lt of 1/2 - Fly Picket Fence				
TP	6.56	232.62	4.00	226.06	✓
+45	85 Lt of 1/2 - NY House	5.8	226.8	✓	on Floor
+75	0.2 Lt of 1/2				
6+0	1.8 Lt of 1/2 - Board Fence	6.1	226.5	✓	
6+10		5.5	227.1	✓	
BM	1.78	230.84			SE Top Fire H Federal Blvd #4915 St 230.80
2+81	0.9 Rt of 1/2 - Sky 4" x 4" Clothes Post				
4+37	1 Lt of 1/2 - Fly Flower Bed				
4+66	1 Lt of 1/2 - NY " "				
5+28	1 Rt of 1/2 - 6" x 6" Post				
5+61	0.6 Rt of 1/2 - Cable Dead Man				
6+0	2 Lt of 1/2 - Young Berry				
6+08.5	1 Lt of 1/2 - NY 4" x 4" Clothes Post				

Levels Prop. Saylor B' Line
Federal Blvd. Sec #1 & #2

Sketch Page 31

B.M.	11.07	(218.23)	207.6	✓	9+0 99th St Page 32
0+0	= 2' 19th St.	11.0	207.4	✓	
+39.5	- Top Rail Type Curb	11.10	207.1	✓	
+50		9.6	208.6	✓	
+78.5	= 4" Cobble Wall			✓	
1+0	3' Lt = Nly House	6.7	211.5	✓	
+01	= 5 Fly 1.5 Rubble Gutter N Page = 2.07 Line				
+05	= Nly 2" Conc. Wall = Nly 1.8 Conc. Walk				
+21	2" = Nly 3" x 5" Post				
+21.5	= Nly 5 Cobble Wall Gutter 1.5 East 1.9 West				
+31	= Nly 5 Cobble Wall Also Fly 5" Conc. Walk				
+36.5	= Nly 5 " " Also 4.5 Nly 1.5 Rubble Gutter + Fly 1.8 Conc. Gutter	213.7	✓		
+50		32	215.0	✓	
+61	= Nly 2" Conc. Gutter	13	216.9	✓	
+80					
+82	= Nly 5 Picket Fence			✓	
+84.6		0.3	217.9	✓	
TP	594	(223.77)	0.40	(217.83)	Pin 2' 8"
+88	= Fly Flower Bed 3' South of Fence	6.02	(217.75)	1+826	
2+0		5.5	218.3	✓	
+152	= Nly 5 Picket Fence				
+50		4.3	219.5	✓	
+61	4" Lt = Nly Fly House	2.55	221.44	07 Floor	
+62	= 5.7 Nly 5 Picket Fence				
3+0		4.4	219.4	✓	
+71		4.7	219.1	✓	

Note

1+25 to 3+20 = Lawn

Level Prop Saylor G' Line

219.82 From Page 32

34

Blatted

0+0	= 5 x 50.5 F		213.4	
+50		6.5	213.6	✓
+80		5.9	213.9	✓
House on lot 92		4.9	214.9	07 Floor
0+03.7	= Nly 5 Picket Fence			
+07	1.5 Lt of 2" = 1" Grape Vine			
+09	2' Rt of 2" = Nly Row Grape			
+11.5	2' Lt " = 2" Apricot			
+28	2' Rt of 2" = S Wly Row Grape			
+34	2.5 Lt = 1" Peach Tree			
+37	1.5 Lt of 2" = Nly Black Berry Fox			
+40	1.5 Rt of 2" = Picket Fence			
+71	3.7 Lt " = 1" Peach Tree			
+78	2" = 3 Way Picket Fence			
"	1.4 Lt of 2" = S Wly Black Berry			

May 9-47

S. S. Coy
Johnson

Levels Prop. Section "D" Line
Federal Blvd Sub #2

Sketch Page 31

Plotted

35

<221.39>

BM	187	<210.16>	208.29	NETOP FH. F 8' x 19"	BM
TP	742	<215.27>	2.22	<207.94>	
0+0	= 1+57' C"	7.4	208.0	✓	
+50		6.7	208.7	✓	
1+0		5.1	210.3	✓	
"	72' Rt of 7' = NY House	3.9	211.5	on Floor	
+1911	= A 20°32' Lt	4.8	210.6	✓	
+19.4	= N x S Wire Fence				
+50		3.8	211.6	✓	
TP	8.60	<221.39>	2.57	<212.79>	
+85	71' Rt = NY House	7.5	213.9	on Floor	
2+0		8.3	213.1	✓	
+1519	= A 15°48' Lt	8.2	213.2	✓	
+50		7.7	213.7	✓	
+59.5	35' Rt = NY Tel Pole				
3+0		6.9	214.5	✓	
"	70' Rt = NY House	7.8	213.6	on Floor	
+08	= E x W Picket Fence	6.3	215.1	Top of Concrete Wall	
+0906	= A 14°11' Lt	6.3	215.1	✓	
+53.54	= A 17°59' Lt	5.5	215.9	✓	
+75		5.0	216.4	✓	
"	74' Rt = NY House	8.9	212.5	on Floor	
+917	= E x W Picket Fence				
4+0		4.2	217.2	✓	
+44.78	= 1+84.6 B	2.5	217.9	✓	

3.68

<217.71>

67 P 17 2' Rt
1+82.6 B
217.75
Page 31

Levels Prop Survey "C" Line
Federal Blvd. Subs. #1 & #2

July 12, 15

36

Sketch Page 30 & 31

Sketch

(223.80)

BM	2.08	(210.27)	208.29	NETop Finth H St + 49 1/4	5+0	6.5	217.3	✓	
0-16.7	= Fly Line Conc Box 4' CB Inlet	12.10	198.27	✓	+22.30 = 187° 24' Rt	5.70	218.07	✓	
0+0		6.82	203.55	✓	+377 = Gutter	6.20	217.60	✓	
+15.8	= Fly 34 x 2.2 Conc Box	10.67	199.70	✓	+387 = Cb Top	5.81	217.99	✓	
+18.1	= Gutter	7.1	203.3	✓	+50	5.8	218.0	✓	
+18.1	= Top Curb	6.26	204.11	✓	6+0	6.0	217.8	✓	
+50		5.1	205.3	✓	+09	1 1/2 of 2 = NY Tel Pole			
+80	17' 1/2 = 5' Car Board Fence				+12.5 = NY S Picket Fence 23' 1/2 of 2 = Fly Picket Fence				
+84.3		4.1	206.3	✓	+30	5.8	218.0	✓	
"	Top 4" Concrete	2.98	207.39	✓	"	7 1/2 of 2 = NY House	6.4	217.4	07 Floor
1+0		3.7	206.7	✓	+6.5 = NY S Board Fence 2 1/2 of 2 = Picket Fence Post Board				
+55.3	1 1/2 of 2 = Fly Tel Pole				7+0	5.0	218.8	✓	
+57.0	= 0+0 D"	2.42	207.95	✓	+20.5 = NY S Board Fence 22 1/2 of 2 = " "				
TP	9.40	(217.25)	2.42	(207.95)	07 Hall 1+57	+50	5.1	218.7	✓
2+0		7.5	209.8	✓	"	7 1/2 of 2 = NY House	5.8	218.0	07 Floor
+50		5.5	211.8	✓	+75.2 = NY S Picket Fence 22 1/2 of 2 = Fly Picket "				
+95.9	= Fly Cb Top Beech St	4.67	212.68	✓	+78 = 3' 1" off of Tree	5.2	218.6	✓	
+96.9	= Gutter	5.05	212.30	✓	+80.6 = NY S Picket Fence 21 1/2 of 2 = Fly Picket Fence				
3+0		4.7	212.6	✓	+50	4.9	218.9	✓	
+10.73	= A 68° 50' Rt	4.11	213.24	✓	+60	7 1/2 of 2 = NY House	4.6	219.2	07 Floor
+50		3.8	213.5	✓	+76.6	1 1/2 of 2 = NY Tel Pole			
4+0		2.6	214.7	✓	+84.2 = A 65° 49' Rt 19 1/2 of 2 = Picket Fence 07 Strip	4.9	218.9	✓	
+12.32	= A 66° 30' Lt	2.49	214.86	✓	"	7 1/2 of 2 = Ford Temp - NY Ha	3.6	220.2	07 Floor
+50		1.45	215.90	✓	9+0	4.5	219.3	✓	
TP	7.03	(223.80)	6.58	(216.77)	+50	7.6	221.2	✓	
					"	1.5 1/2 of 2 = Picket Fence			

		222.80		
9+75	5' H of 1/2 - Wly House	+0.3	224.1	02 Floor
+83	0.7' H of 1/2 - Cable Duct			
TP	12.94	(232.53)	4.21	(219.59)
10+0		9.6	222.9	✓
+05.07	-A 15' 59" Pt	9.5	223.0	✓
"	0.8' H of 1/2 - Wly Tel Pole			
+32	18' Pt of 1/2 - SE 1/4 2' Lantana Hedge			
"	0.8' H of 1/2 - Wly House	7.5	225.0	02 Floor
+50		6.7	225.8	✓
11+0		4.6	227.9	✓
+05	3.4' Pt of 1/2 - Wly 2' Lantana Hedge			
	0.4' Pt of 1/2 - Wly Tel Pole			
+228	-A 27' 7" Pt	4.95	227.68	02 Floor
+50		4.8	227.7	✓
"	87' Pt of 1/2 - Wly House	4.0	228.5	02 Floor
12+0		4.6	227.9	✓
+55		3.5	229.0	✓
13+10		2.9	229.6	✓
"	82' Pt of 1/2 - Wly House	0.9	231.6	02 Floor

Levels Prop Survey "E" Line
Federal Blvd Sub 41
Sketch Page 50

		(232.53)	6.76	227.68	02 Stake
0+0	-11+2280C		4.85	227.6	✓
+50			4.9	226.8	02 Floor
+75	83' H - Wly House		5.7	227.3	✓
1+0			5.2	227.5	✓
+50			5.0	226.5	02 Floor
+90	82' H of 1/2 - Wly House		6.0	226.9	✓
2+0			5.6	226.3	✓
+55			6.2	226.0	✓
+70	-FL 47' 30"		6.5	226.25	✓
TP	8.60	(234.85)	6.28	(226.25)	
BM			6.76	228.09	2 Lx7 Federal Blvd 47' 30" 228.05

Levels Prop. Section "F" Line
Federal Blvd. Sub #2

Sketch Page 30 + 31

B.M.	10.38	(218.33)	207.95	09 Nail 17576
0+0			207.9	✓
+02	= 4x5 Wire Fence	10.4	207.9	✓
+50		9.8	208.5	✓
+56.8	= 4x5 Wire Fence		209.8	✓
+90	79' Lt of 1/2 = 1/4 House	8.5	209.8	07 Floor
1+0		9.2	209.1	✓
+13	15' Lt of 1/2 = 1/4 Tail Pole # 458123H		210.2	✓
+50		8.1	210.2	✓
+67.4	= 4x5 Board Fence		209.7	✓
2+0	22' Lt of 1/2 = 1/4 + 1/4 Board Fence	8.6	209.7	✓
"	79' Lt of 1/2 = 1/4 House	7.8	210.5	07 Floor
+07	19' Lt of 1/2 = 1/4 Chicken Coop		210.0	✓
+22.2	= 4x5 High Board Fence	8.3	210.0	✓
+23		7.3	211.0	✓
+50		7.2	211.1	✓
+77.2	= 4x5 High Board Fence	7.0	211.3	✓
+78		5.9	212.4	✓
+79	17' Lt of 1/2 = 1/4 Tail Pole # 458122H		212.7	✓
3+0		5.6	212.7	✓
+10	79' Lt of 1/2 = 1/4 House	6.6	211.7	07 Floor
+11	= 5x4 Grooved Flang Fence 16' Long			
+22.4	= 4x5 Picket Fence		213.7	✓
+50		4.6	213.7	✓
4+0		4.3	214.0	✓
+15	79' Lt = 1/4 House	3.8	214.5	07 Floor
+43	09' Lt of 1/2 = 1/4 Tail Pole # 458121H		212.9	✓
+50		5.1	212.9	✓
5+0		5.5	213.0	✓

May 5-47
Sisson
McCol
Johnson
No. 31375

(218.33)

5+23	79' Lt of 1/2 = 1/4 House	2.3	215.0	07 Floor
5+50.05	= 190° 07' Rt		213.4	✓
+53	2 1/2' Lt of 1/2 = Picket 4x5x4		213.8	✓
6+0		4.5	213.8	✓
TP	5.96	(219.83)	4.46	(218.87)
+50			4.9	214.9
7+0			4.0	215.8
"	83' Lt of 1/2 = Fly House	1.2	218.6	07 Floor
+140	= 199° 09' Lt		216.1	✓
+203	= Exposed Board Fence			
TP	8.98	(225.08)	2.72	(216.10)
+50	1 1/2' Rt = Fence		216.9	✓
8+0	19' Lt of 1/2 = Fly House	5.2	219.9	07 Floor
+05			6.7	218.4
B.M.	9.11	(221.61)	2.61	(222.47)
B.M.			3.53	(228.08)
0+03	24' Lt of 1/2 = 1/4 Post = Fly Grape Vine			228.05
0+35	18' Rt " = 1/4 Grape Vine			
0+53	= 4x5 Young Berries 2 1/2' Lt of 1/2 = 1/4 Berry			
0+88	= 4x5 Wire Fence Chicken Coop			
+15	1' Lt of 1/2 = Fly Small Hedge			
+20	1 1/2' Rt of 1/2 = 3" Spruce Tree			
+28	17' Rt of 1/2 = 1/4 Young Berry Vine			
+33	17' Rt " " " " " " " "			
+39	17' Rt of 1/2 = 1/4 Plum Tree			
+57	1' Lt of 1/2 = 1/4 Small Hedge			

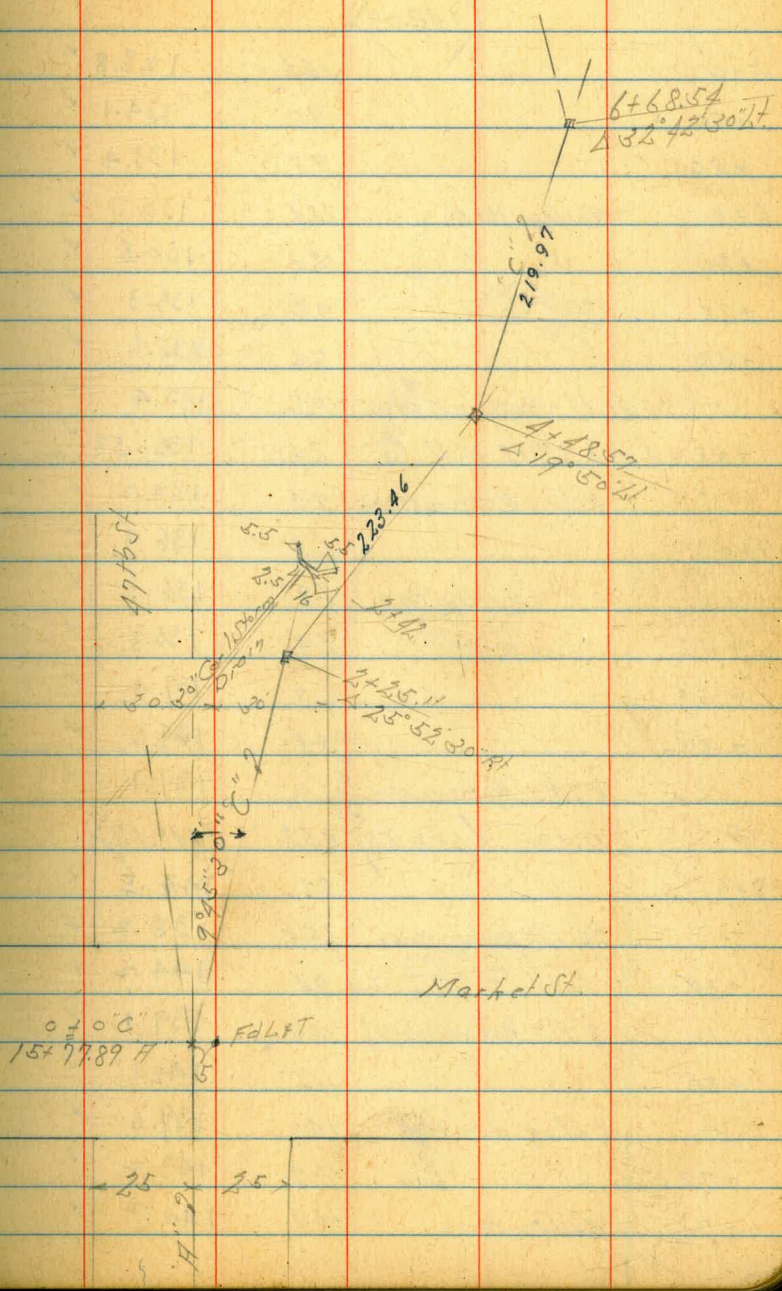
July 13-45
Sisson
Bliss
Ogborne
899

38
related

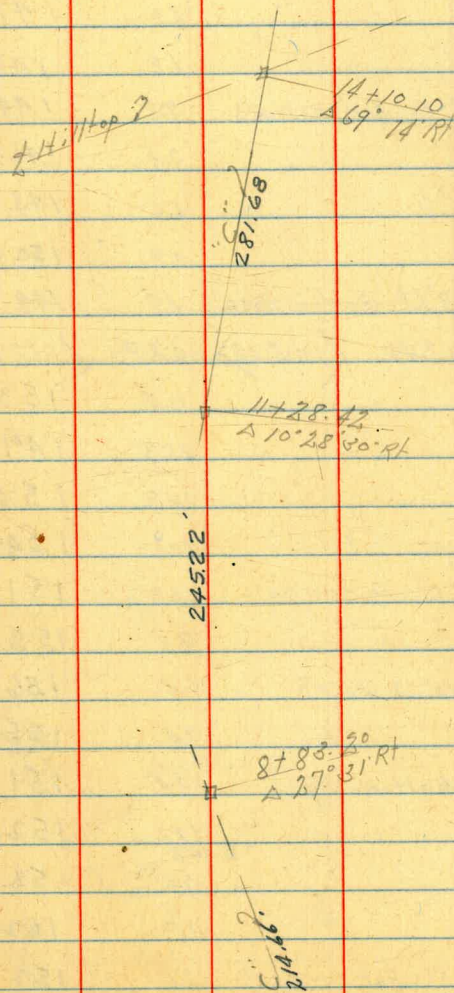
Proposed Sewer East of 47th North of Market 'C' Line

July 14, 1915
S. Wray Osborne
81155 8199

BM	1292 <123.88>	12096	2x1 Market 497 Page 6
0+0	- 15+77.89 H	12.88	121.00 ✓
+50		12.36	121.52 ✓
+91	- Fly Conc Pav 179	11.90	121.98 ✓
1+0		12.0	121.9 ✓
+10		11.5	122.4 ✓
+50		9.6	124.3 ✓
2+0		8.6	125.3 ✓
+25.11	= $\Delta 25^{\circ} 52' 30''$ Rt	9.16	124.72 ✓ on Hub
+42		8.9	125.0 ✓
"	16' H of Fly - 191 at 30'	11.02	122.86 ✓ Top Hood
"	Corp. 1163		
"	- Fly 4.92 at 30' Culv.	15.02	118.86 ✓
+50		8.1	125.8 ✓
+90		4.6	129.3 ✓
2+0		5.3	128.6 ✓
"	2 1/2' of Bottom Wash	12.7	121.2 ✓
+37		8.5	125.4 ✓
+45	= Bottom Wash	11.5	122.4 ✓
+50		8.6	125.3 ✓
TP	12.57 <143.09>	3.36	<130.52>
+10		12.6	129.5 ✓
"	22' Rt Bottom Wash	18.5	124.6 ✓
+48.57	= $\Delta 19^{\circ} 50'$ Lt	15.0	128.1 ✓
+64	= Bottom Wash	16.9	126.2 ✓
+90	= " "	16.3	126.8 ✓

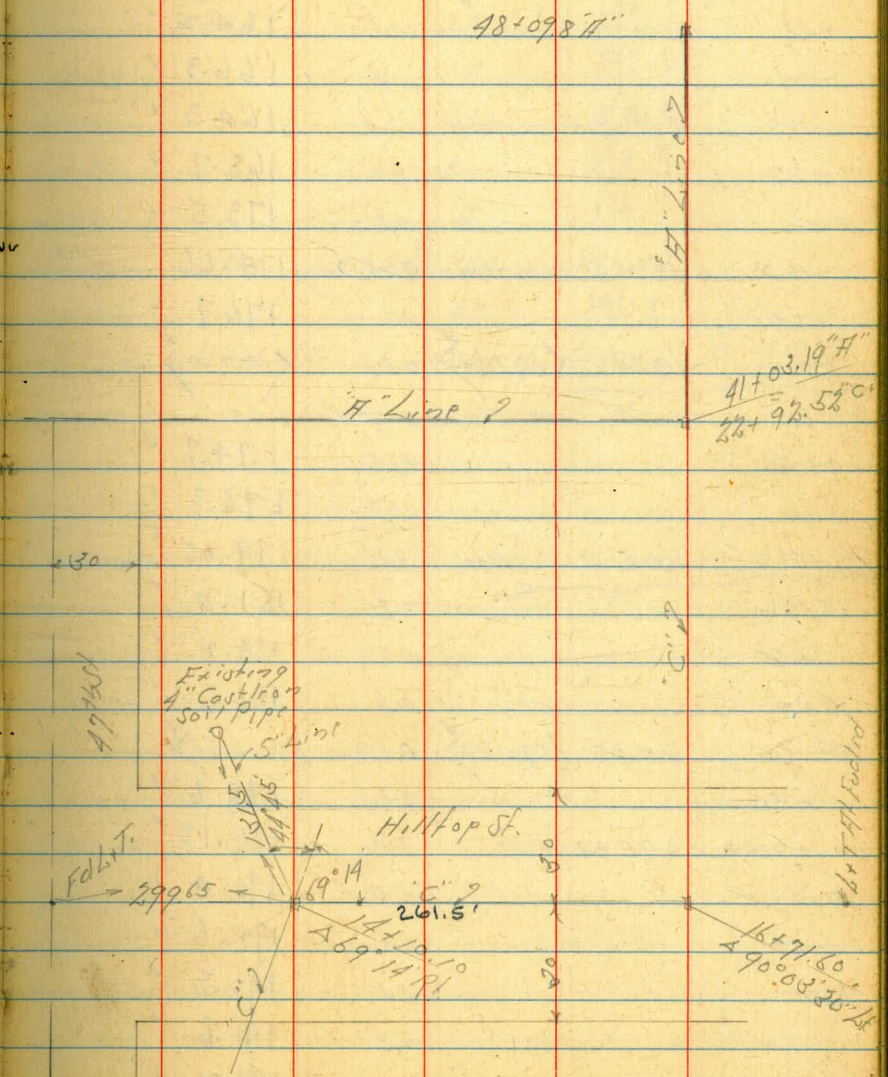


Height	Description	Distance	Sum	Check
5+0		14.3	128.8	✓
+50		9.0	134.1	✓
+80		9.7	133.4	✓
6+0	= Bottom Wash	12.4	130.7	✓
+20	" "	12.3	130.8	✓
+25		9.8	135.3	✓
+50		7.5	135.6	✓
"	3' Lt = Bottom Wash	10.7	132.4	✓
+68.54	- 1 32° 42' 30" Lt	6.51	136.58	on Hub
"	8' Lt = Bottom Wash	8.9	134.2	✓
7+0		6.2	136.9	✓
"	5' Lt = Bottom Wash	6.8	136.3	✓
+32	" "	6.3	136.8	✓
+50	" "	5.9	137.4	✓
+55		3.5	139.6	✓
"	5' Lt = Bottom Wash	6.0	137.1	✓
TP	11.10 $\langle 153.57 \rangle$	0.62	$\langle 142.97 \rangle$	✓
8+0		9.1	144.5	✓
"	25' Lt = Bottom Wash	15.4	138.2	✓
+30		9.4	144.2	✓
"	8' Lt = Bottom Wash	14.5	139.1	✓
+50		11.5	142.1	✓
"	5' Lt = Bottom Wash	14.0	139.6	✓
+72		10.4	143.2	✓
+73	= Bottom Wash	13.4	140.2	✓



152.57

8+83.20	Δ 27° 31' Rt	9.26	144.31	✓	on Hub
9+0		6.9	146.7	✓	
"	9' Pt. Bottom Wash	12.2	141.4	✓	
+50		6.0	147.6	✓	
10+0		6.8	146.8	✓	
"	8' Pt. Bottom Wash	8.8	144.8	✓	
+08'		7.3	146.3	✓	
+38		5.4	148.2	✓	
+50		0.9	152.7	✓	
"	8' Lt. Bottom Wash	4.9	148.7	✓	
TP	12.49	(165.18)	0.88	(152.69)	✓
+63		11.4	153.8	✓	
+75		15.7	149.5	✓	
+90		14.7	150.5	✓	
11+0		11.2	154.0	✓	
"	9' Lt. Bottom Wash	14.0	151.2	✓	
+05'		9.3	155.9	✓	
+28.42	Δ 10° 28' 30" Rt	8.46	156.72	✓	on Hub
+40		9.4	155.8	✓	
+45	= Bottom Wash	12.1	151.8	✓	
+50	"	12.8	152.4	✓	
+65		9.0	158.2	✓	
12+0		3.0	162.2	✓	
"	20' Pt. Bottom Wash	12.6	152.6	✓	
+50		3.2	162.0	✓	



1370	= Bottom Wash	165.18	5.4	159.8	✓
TP	12.71	177.71	0.18	165.00	✓
+42			13.5	164.2	✓
+50			11.4	166.3	✓
"	3' Lt. Bottom Wash		13.4	164.3	✓
+87			9.0	168.7	✓
1470			4.2	173.5	✓
+10.10	= Δ 69° 14' Rt = 1/4 Hill Top		30.5	174.66	on stake
+50			1.0	176.7	✓
TP	9.84	187.21	0.34	177.57	✓
"S" Line For School Tank					
-0750			12.5	174.7	✓
170			10.9	176.3	✓
+31.5	= 8 1/4" C/L Soil Pipe		8.16	179.05	Flashed
1570			6.2	181.0	✓
+50			3.0	184.2	✓
1670			0.6	186.6	✓
TP	10.25	196.89	0.67	186.51	✓
+50			8.3	188.6	✓
+71.60	= 90° 02' 30" Lt		7.76	189.13	on stake
1770			6.5	190.4	✓
+50			4.3	192.6	✓
1870			4.4	192.5	✓
+50			5.3	191.6	✓
1970			5.7	191.2	✓
"	100' Lt		7.2	189.1	✓

19750		196.89	4.6	192.3	✓
2070			3.9	193.0	✓
"	100' Lt		7.4	189.5	✓
+50			3.3	193.6	✓
2170			2.5	194.4	✓
+50			2.0	194.9	✓
2270			1.2	195.1	✓
TP	6.19	200.84	2.24	194.65	✓
+50			4.7	196.1	✓
+92.62	= 41° 02' 19" R		3.60	197.21	✓

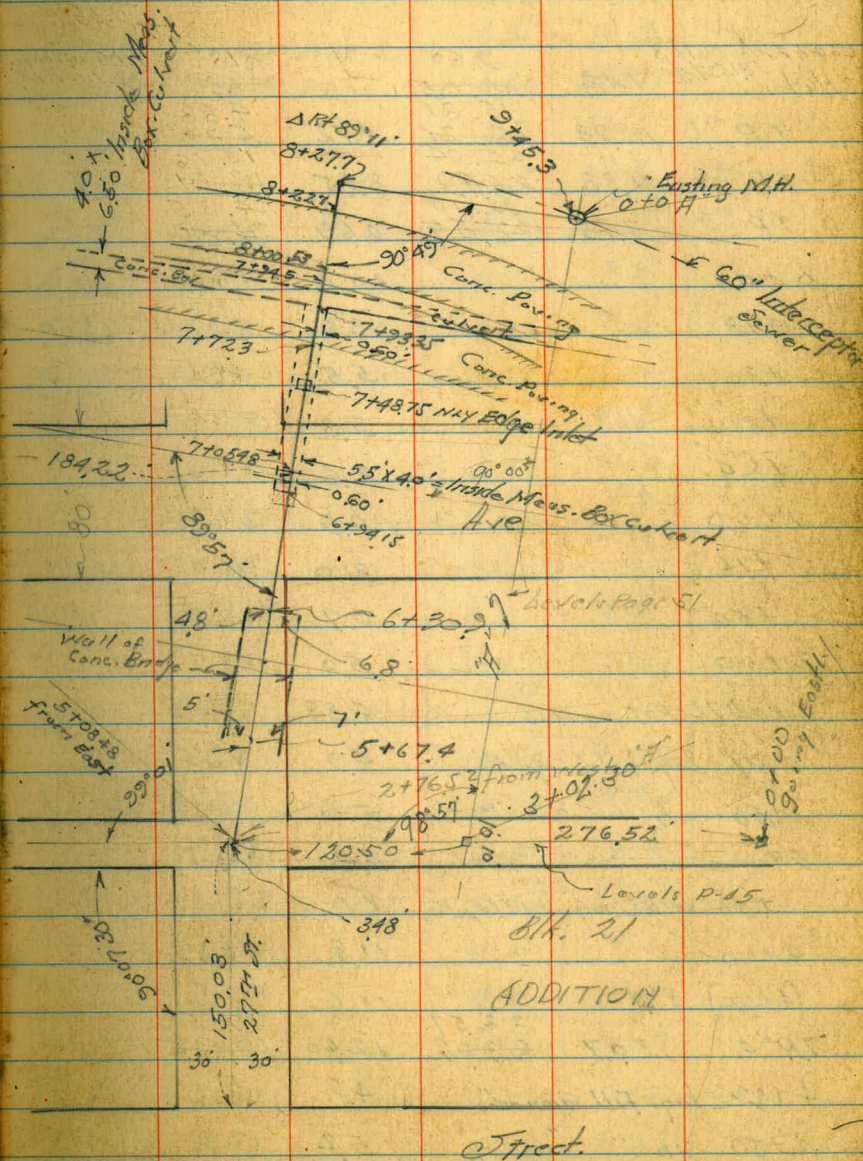
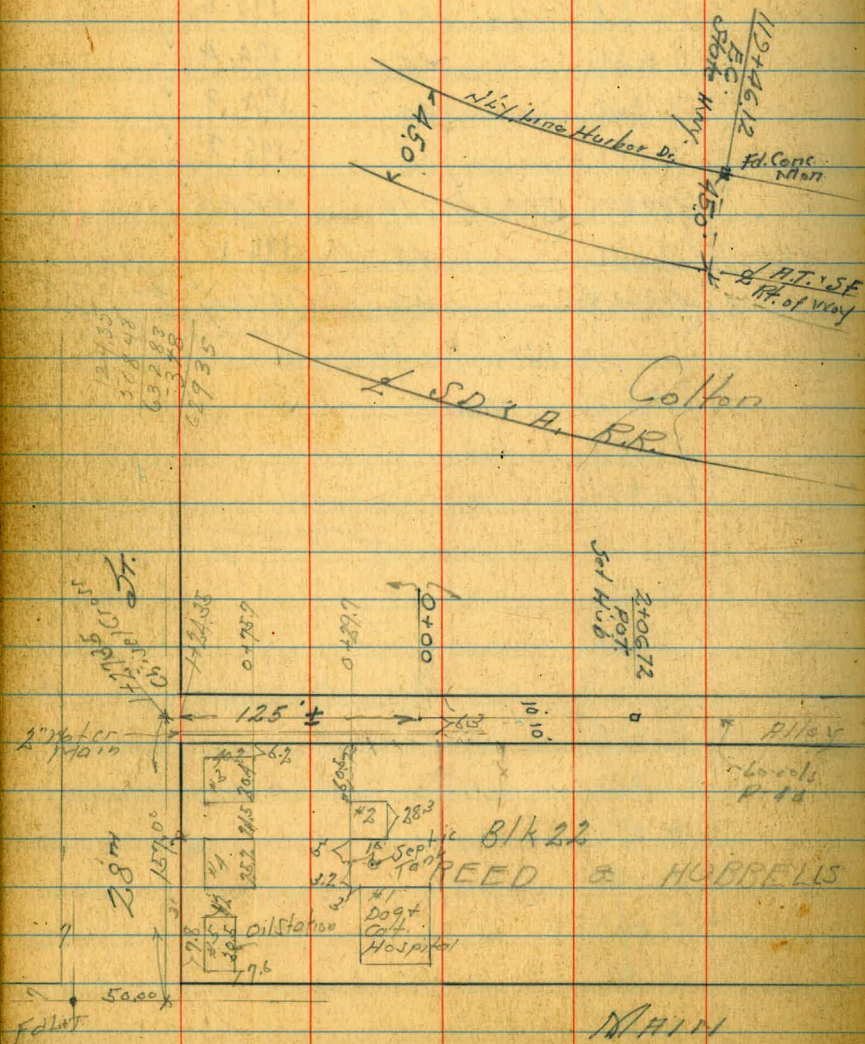
on stake
41+03.19 F
19746
Page 19

Walker
Hurdin
Hunley
11-30-45

Survey - Proposed Sewer in
27th St. And in Harbor Drive
South of Main Street.
And in Alley South of Main st.
between 26th and 28th St.

Indexed
c. S. K.

43



Levels - Proposed Section
Location P. 43

South side Colton
& Harbor
18,157.50

142	9.60	818	
	10.05	863	
TP #1 10.93	15.81	4.88	
	16.26	5.33	
TP #2 11.88	25.04	13.76	
	25.49	13.61	
TP #3 7.75	32.10	24.35	
	32.55	24.80	
0+00		10.0	22.1
+18		8.9	23.2
+30		5.5	26.6
+50		3.8	28.3
+84		2.6	29.5
+100		0.9	31.2
+16		2.0	30.1
+50		3.7	28.4
2+00		5.0	27.1
2+06.72 - POT. on Hub		4.88	27.2
+27 = beg. Cold Lay Pav.		4.9	27.2
+50 on " " "		5.0	27.1
3+00 " " "		5.4	26.7
+50 = NLY edge cold lay Pav.		7.1	25.0
4+00		11.8	20.3
(4+00) 3' Lt. " " "		11.6	20.5
	22.57	19.30	
TP #4 3.07	23.02	19.25	
4+12 = beg. Fill Ground		4.0	18.6
4+50 in " "		5.2	17.4
10' Lt. on N edge 10' cold lay		5.3	17.3

See
P. 45
PM on Hwy
Top. Fire Hdr.

2302
22.57

4+77 on ELY Cold Lay Pav	5.5	17.1	Fill Ground
+91 = NLY " " "	5.7	16.9	" "
5+00 on Hub. Pine in Fill	6.3	16.3	" "
+08.48 = Lt. 30° 55'	6.60	15.97	" "
+29 in	6.5	16.1	" "
+44	11.7	10.9	
TP #5 - 0.95	8.86	9.81	
	9.31	12.76	10.26
5+63	6.1	2.8	
5+67.4 = NLY end Bridge Walls	6.6	2.3	
6+05.5 = 2 SDYA on Rail	+6.2	15.1	Hub. Canal on Bridge
6+00	6.4	2.5	
6+30.7 = Sand Walls	6.9	2.0	
(6+30.7) 4.8 Lt on Bottom slope Conc. Wall	5.3	3.6	
(6+30.7) 6.8 Rt " " "	5.2	3.7	
6+50 in ditch	8.0	0.9	
785 " " "	9.4	-0.5	
	10.67	-1.81	Flora Lirre
6+82.15 = Conc. Lip Box Culvert			
+94.15	10.68	-1.82	
" on Hd. wall	4.82	4.04	
7+00	4.5	4.4	
+03.12 = N Rail AT 1.5F	3.84	5.02	
7+10	4.8	4.1	
+40	4.2	4.7	
	5.56	3.30	
7+48.75 = Edge Inlet Cover			
7+48.75 on Flow Culvert	11.01	-2.15	
7+93.35 on Flow Box Culvert	11.13	-2.27	

Curt. P-15-A

P-45-A	T 9.21 8.86	Cont. from P-44	
7+62 on Asphalt shoulder	5.57	3.29	
7+72.3 on N edge Conc. Pav.	5.10	3.76	N Strip
7+94.5 on Conc. Pav.	4.07	4.79	
8+00.59 " " "	4.02	4.84	
+22.7 " S edge Conc. Pav.	2.99	5.87	
8+27.7 = A Pt 89°11'	3.14	5.72	
+50 on cold lay Pav	3.19	5.67	
9+00 " " " "	3.45	5.41	
+45.3 = 1st Exst. M.H.	3.74	5.12	
9+45.3 on Floor 60" Sewer Hyd.	14.58	-5.72	✓
chk Starting B.M.	0.68	8.63	✓

Walker 11-30-45	Levels - Proposed	Sewer	Block 21
	17' Alley	West of 27th St.	
	Mid South of Main St.	Location P-43	
	x=3		
	32.55 from P-44		
	32.10		
0+00		10.2	21.9
+50		10.1	22.0
+100		10.2	21.9
+50		10.7	21.4
2+00 = bog. Fill Ground		11.4	20.7
+25 in Fill		12.8	19.3
+50 " "		13.5	18.6
		19.58	
TP#4	3.07	22.57	19.50
		23.02	19.95
2+63 in Fill		11.2	11.4
+68 " "		6.6	16.0
2+76.52 on Pine Hub		6.60	15.97

Check Above B.M.

B.M.	4.29	31.77	27.48	SE B.P. Mail
T.P.	1.37	27.34	5.70	26.07
T.P.	0.00	14.41	12.93	14.41
chk Above Hyd. Starting B.M.		6.23	8.18	
			8.63	
			0.45 Error	
	13.2	9.50	8.18	
chk. on S side Harbor Dr. 18 1837 P-39		2.35	7.15	

Fire Hyd. Evidently Moved from orig. Place

6 Sicard St.

25+08.48 P-44

Levels Proposed Section A' Line
East of 47th St. Between C + H Sts.

Sketch Page 19

BM	4.53	20199	197.46	02 Stub 41+03.19 H Page 19
35+67.99 Δ	90°04' R	11.55	190.44	02 Stub
+75.9	= W/4 Conc Pav	11.80	190.19	
+95.6	= E/4 Conc Pav	11.90	190.09	
36+0		12.1	189.9	
+0.6	= W/4 0.1 x Rock Walk	11.1	190.9	
+1.2	= E/4	11.1	190.9	
+1.6	39 1/2' of S-Sly to Pole			
+5.0		11.0	191.0	
37+0		9.7	192.3	
+5.0		9.5	192.5	
38+0		9.1	192.9	
+5.0		8.4	193.6	
39+0		8.8	193.2	
+5.0		7.0	195.0	
40+0		6.4	195.6	
+5.0		6.1	194.9	
41+0		4.7	197.3	
+55.99 Δ	90°04' L	2.77	198.23	02 Stub
42+0		2.9	199.1	
+5.0		1.8	200.2	
43+0		1.0	201.0	
TP	4.66	205.65	1.00	200.99
+5.0		2.6	202.1	
44+0		4.5	201.2	

205.65

44+50

46

201.1

45+0

51

200.6

+3.5

48

200.9

+7.5

69

198.8

46+0

77

198.0

+5.0

71

198.6

47+0

52

200.5

+5.0

37

202.0

48+0

17

204.0

+19.79

114

204.51

02 Stub

For Check

112

204.53

02 Stub
48+09.80 H
204.52
Page 19

See 25-46
S. 33.50
S. 33.50
8099

46

Proposed Sewer 19th St North of H St
L Line

Sketch Page 3

Jan 21. 46
Simon
Osborne
Esq.

47

BM	2.50	210.79		208.29	NE Top of H St H St x 49 th St
0+0	= 48+19.79	H Page 17	6.41	204.38	on Street
+50			7.3	203.5	
1+0			7.7	203.1	
+54.2	6' Lt of 1/2	10' Lt.	7.28	203.51	Tap on
"	6 " "		12.51	198.28	FL 10' Lt
"	18.3' Bl off = Sly 18"		14.73	196.06	Flow line
+56.05	1 26° 07' Lt	Cone Pipe	7.06	203.73	on Street
+78	8 - Sly Right Oil Pan		7.2	203.6	
2+0		on " " "	7.1	203.7	
+50		" " " "	6.0	204.8	
3+0		" " " "	6.0	204.8	
+50		" " " "	5.8	205.0	
4+0		" " " "	5.5	205.3	
+54.57	1 25' 34' Lt.		5.1	205.7	
5+0		" " " "	5.1	205.7	
+50		" " " "	4.8	206.0	
6+0		" " " "	4.4	206.4	
+54.72	1 28' 34' Lt.		4.1	206.7	
7+0		" " " "	4.3	206.5	
+50		" " " "	4.4	206.4	
8+0		" " " "	4.3	206.6	
+50			3.9	206.9	
773.59	1 9° 47' Lt.		3.53	207.24	
7+07.40					

Levels of Garage Floors East Side 1945
 North of 17 St. 2" Linc. Sta.

Sketch pages

Feb 6-46
 S. 5007
 056001
 8099
 Wodde!

48

B.M.	2.67	210.96		208.29	N.E. Top of Hill H.S. 1945
5+0	110' Rl of 2' Sewer = Gar. #1	8.18		202.78	on Conc. Floor
5+44	121' Rl of 2' Sewer = Gar. #2	10.10		200.86	" " "
TP	5.13	211.54	4.55	206.41	
5+86	126' Rl of 2' Sewer = Gar. #3	8.90		202.60	on Conc. Floor
6+35	117' " " " = Gar. #4	8.42		203.12	" " "
TP	4.76	211.60	4.70	206.84	
6+94	122' Rl of 2' Sewer = Gar. #5	7.71		203.89	on Conc. Floor
7+46	131' Rl of " " = #6	7.73		203.87	" " "
TP	4.54	211.88	4.26	207.34	
7+95	133' Rl of 2' Sewer = Gar. #7	6.80		205.08	on Conc. Floor
8+39	128' Rl " " = " #8	4.71		207.17	" " "
8+73.59	2" on 2'		4.65	207.25	on Wall 207.25 Page 47

Location of Culverts 47th St North
of Market St.

See page 72
also

Feb. 18-46
S. S. Co.
0.560 m
8099
Yaddel

49

BM 6.50 129.82 123.82 on St. 17+39.37 1799

Culvert No 1

16+64.58 57.8 H.H. of 18" sewer 10.56 119.26 on Head Wall
38" Cor. Iron Culv.
" " 14.60 115.22 Floor Line

Culvert No 2

17+54.45 197 St. of 18" sewer 10.11 116.71 Floor Line
Outlet 30" Cor. Iron Culvert

" " 81.3 H. of 18" = 6.94 123.08 on Head Wall
Outlet 30" Cor. Iron Culv.

" " 10.82 119.00 Floor Line

Culvert No 3

BM 12.33 178.25 165.92 on St. 22+0.47 1799

21+47 51 H. of 18" sewer = 13.97 164.28 Floor Line
Outlet 18" Cor. Iron Culv.

Inlet Covered

No Culvert at 33+50

17+39.37

15+77.89

16+48

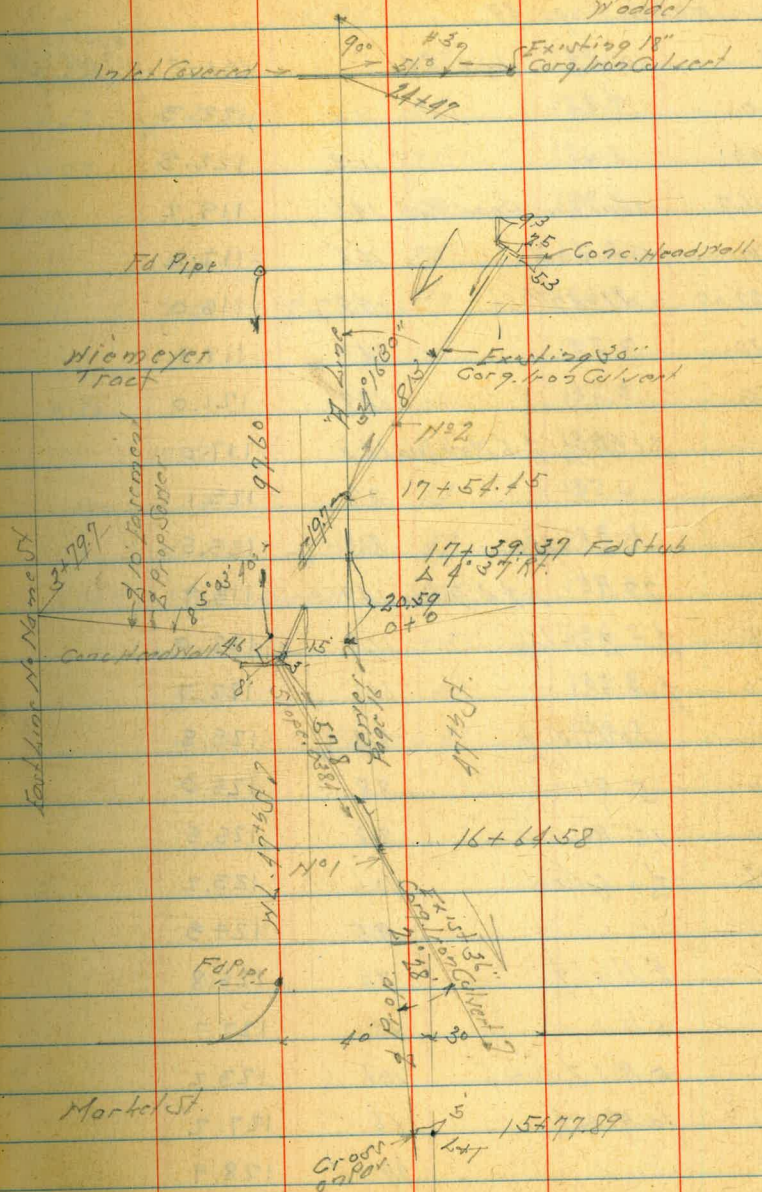
Inlet Covered

Fd Pipe

Hiemeyer
Tract

East line No Name St

Market St.



Proposed Section to Serve Wilmeyer Tract
North of Market St & West of 47th St.

Sketch Page 49

Feb 20 46
S. J. S. 007
Asborne
Model

50

				133.84			
B.M.	10.52	122.84	123.32	21 65		4.7	129.1
0+0		11.3	122.3	+ 68	1/2 5' Ditch	7.9	125.9
+07		11.3	122.3	+ 90	" " "	7.6	126.2
+16.7	Top Conc Head Wall	14.6	119.2	3+0		3.9	129.9
"	Ground	16.6	117.2	"	10' Lt of 1/2	2.5	131.3
+22.08	W. 47th St	17.8	116.0	"	7' Rt " 1/2 5' Ditch	6.9	126.9
+30		14.0	119.8	"	15 " " "	1.8	132.0
+50		12.8	121.0	+50		1.0	132.8
"	23' Rt of 1/2 5' Wide Ditch	16.8	117.0	"	10' Lt of 1/2	+0.3	134.1
1+0		8.7	125.1	"	3 Rt " "	1.2	132.6
"	10' Lt of 1/2	8.3	125.5	"	7 " " 1/2 5' Ditch	4.9	128.9
"	27 Rt " 1/2 4' Ditch	14.9	118.9	+79.7	EL. 11° Namest	+0.5	134.3
+25	1/2 5' Ditch	11.8	122.0	"	10' Lt of 1/2	+2.1	136.2
+50	1/2 " "	11.1	122.7	"	9' Rt " "	0.0	133.8
"	10' Lt of 1/2	8.3	125.5	"	18 Rt " 1/2 4' Ditch	4.1	129.7
"	5' Rt " "	8.8	125.0				
"	15' Rt " "	8.3	125.5				
+92	1/2 Ditch	10.6	123.2				
2+0		9.5	124.3				
"	2' Lt of 1/2	7.0	126.8				
"	10' Lt " "	6.1	127.7				
"	5' Rt = 1/2 Ditch	10.6	123.2				
"	10' Rt of 1/2	6.6	127.2				
+38		9.9	128.9				
"	16' Rt of 1/2 5' Ditch	9.7	124.1				

Proposed Sewer Across Harbor Drive
 Santa Fe + S.D. + H.R.R. to Alley South of
 Main St. East of 27th St "H" Line
 Sketch Page 42

BM	7.83	16.01	8.18	Top Fire Hyd S Side Colton + Harbor page 41
0+0	= Exp. M.H. 60' laterceptor 1/2 Harbor Drive	10.88	5.13	02 Run
+28.5	= 5/4 Conc Strip Paving	9.99	6.02	
+51.2	= 1/4 " " " "	10.64	5.37	
+57.5	= 5/4 " " " "	10.67	5.34	
+80	= 1/4 " " " "	11.42	4.58	
+89	= 1/4 Oil Shoulder	11.6	4.4	
140		12.8	3.2	
+11		13.1	2.9	
+23.85	= 1/2 Santa Fe R.R.	10.64	5.37	Top Rail
+25		12.8	3.2	
+45		12.0	3.0	
+48		10.0	6.0	
+63		0.8	15.2	
TP	10.08	25.18	0.91	15.10
2+0		10.9	14.3	
+06'		12.1	13.1	
+24.30	= 1/2 S.D. + H.R.R.	9.10	16.1	Top Rail
+43		11.3	13.9	
+45		9.0	16.2	
+57		9.2	15.9	
+73		6.5	18.7	
+77	= F&W Lath Fence	2.3	21.9	
3+02.3	= 1/2 Alley	2.75	21.43	on stub 5+08.48 Page 41
5+08.48	Walker	9.46	15.72	

Feb. 26-46
 S. S. 107
 Osborn
 8099
 Waddel

TP	11.03	31.69	4.52	20.66	
2+06.72	Walker		4.41	27.28	on stub 27.22 Page
Elevation 4x5.5 Conc Box Culvert Harbor Dr. + 27th St					
BM	1.47	9.65		8.18	Top Fire Hyd S Side Colton + Harbor Dr
7+18.78	= 1/4 Edge Lot	11.79	-2.14		Flow Line
7+99.83	= 5/4 4x5.5 Conc Box Culvert	11.92	-2.27		Flow Line

Proposed Section 2 Along Souths of
Main Street of 28th St.

Sketch Page 48

March 12-46
S. S. 117
O'Brien
Begg
Waddel

52

B.M.	8.72	35.64		27.22	07 Hub 2+106.72 Page 44
0+0			14.1	21.5	
"	15' S of 1/2 - Sky Fill Top		14.3	21.3	
Bldg #1	Dept Cal Hospital	9.32		26.32	07 Floor
" #2		9.96		25.68	" "
Septic Tank		18.12		17.52	Bottom Tank
TP	265	25.80	12.49	23.15	
0+30			12.2	13.6	
0+50			7.9	17.9	
"	24' S of 1/2 = Sky Bottom		21.7	4.1	
"	6' N of 1/2 = Sky Top Fill		4.6	21.2	
"	28' " " "		4.0	21.8	
0+75.7			5.4	20.4	
"	17' S of 1/2 - Sky Bot. Fill		15.9	9.9	
Bldg #3			3.71	22.09	07 Floor
Bldg #4	SW Cor = Toilet		2.41	23.39	" "
0+96.5	= NW H.C. Pav		7.2	18.5	
"	10' S of 1/2 on NW Pav		7.9	17.9	
1+21.35	W.L. = 28th St		7.95	17.85	
TP	11.98	30.57	7.21	18.59	
Bldg #5	= Oil Station		5.17	25.40	07 Floor
TP	9.85	39.72	0.70	29.87	
B.M.			1.73	27.99	SW B.P. Main St 29.38.00

Sept. 2-17
5.0.07

Walker
Horsbracks
Huntley
Carey
5-21-46
Proposed Sewer in Adams Ave
East of College Way

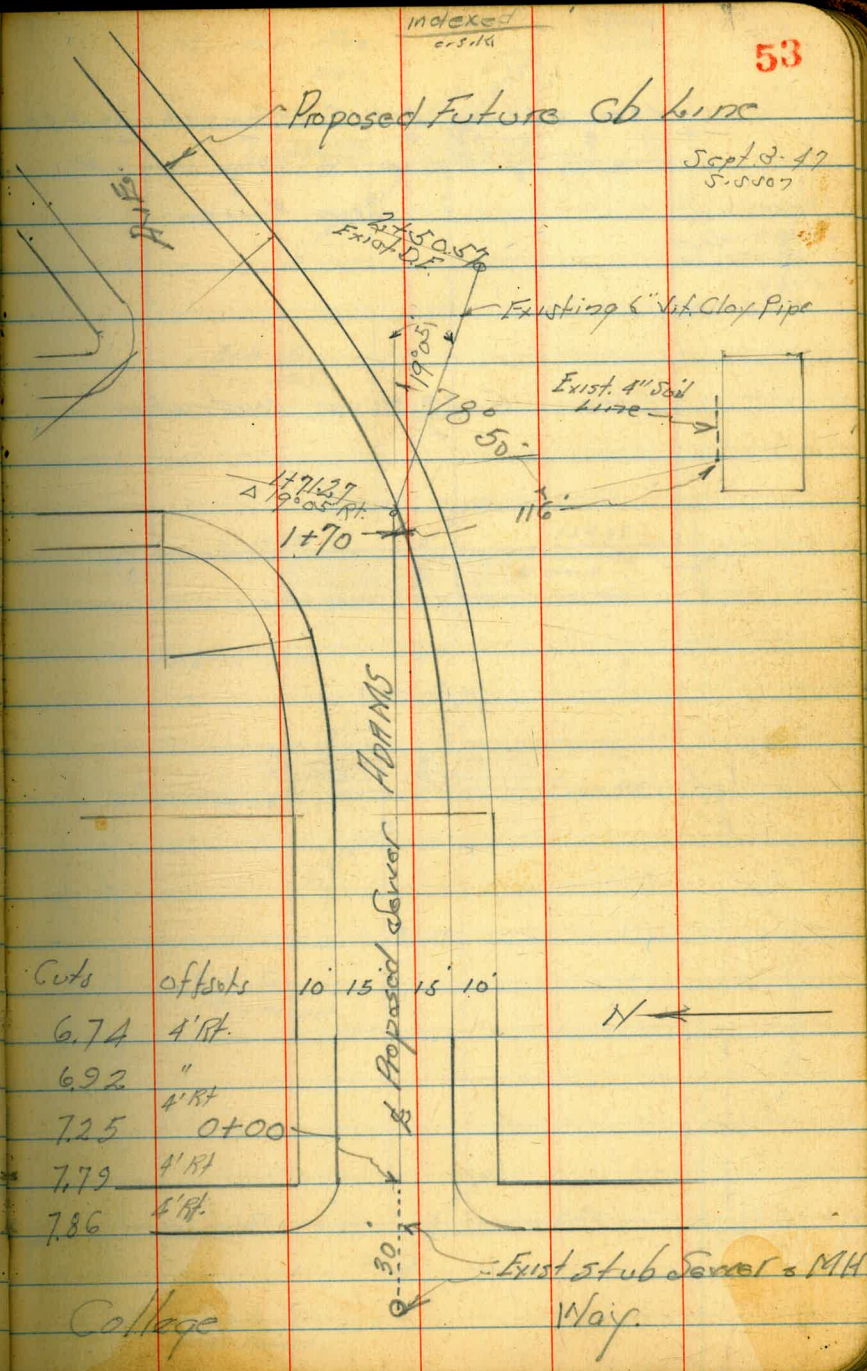
BM	347	468.74	465.27	DE N.M. BP E/Capn + College
1+71.27	$\Delta 19^{\circ}05'$ Rt.	10.36	458.38	Top 6" Bell V.C. Pipe
2+50.57	= Dead End	9.17	459.57	Top 6" Bell V.C. Pipe

Profile Ground Line

2.67	467.94	465.27	B.M. N.M. E/Capn + College Way
0+30' on MH	4.95	462.99	
" " Flow Line MH	11.81	456.13	
0+00	4.8	456.37	
+425	4.4	463.5	
+85	3.7	464.2	
1+27.5	2.9	465.0	
+70	2.5	465.4	

Const. Notes Above Sewer

Const. Notes Above Sewer	Elev.	Flow Line	Cuts	Offsets	10' 15' 15' 10'
0+00	4.83	463.11	456.37	6.74	4' Rt.
+425	4.35	463.59	456.67	6.92	"
+85	3.72	464.22	456.97	7.25	4' Rt.
1+27.5	2.89	465.05	457.26	7.79	4' Rt.
+70	2.52	465.42	457.56	7.86	4' Rt.
116' South East on 4" Soil Line Flow	7.74	461.83			
TP	3.38	468.39	456	465.01	
chk. Starting B.M.	3.12	465.37			



x sec alley Blk. C Montclair, P. 55

" " " 16 City Hts. P.

W.O. # 1190

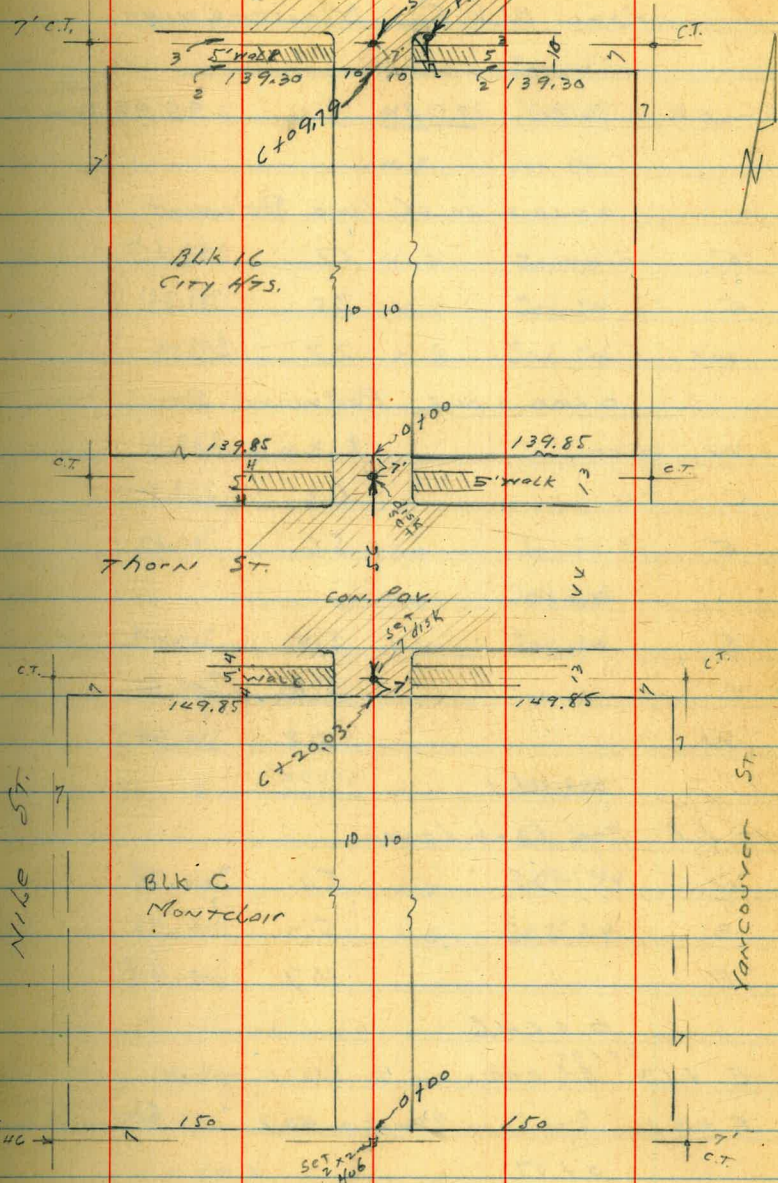
C. Moore
J. Meyer
W. Moore
2099
C-C-VL

sec. G 229 for construction
47

Myrtle Ave.
Con. Pav.

Indexed
C.S.R.

54



Redwood St.
Not Paved.

Xsec BLK C Mantzland

SweBP 5.86 305.8x 299.98 Redwood
Kasauer

0-10 = 1x cb. line Redwood

E dirt 6.7 299.4

C " 7.5 298.34

W " 7.7 298.14

0+100 = N.L. Redwood St.

W dirt 6.3 299.54

C " 6.3 299.54

E " 5.0 300.24

0+110

E 5.8 300.44

C 5.8 300.04

W 5.8 300.04

0+411

- 1.8 Beg. Lath fence

W 5.1 300.74

C 5.2 300.64

E 4.9 300.99

0+446

E + 1.2 ^{S edge} Bd. addition to Wash room 12' Alley

E - 2.1 SW Cor. STUCCO 428 301.56 Wash room
can clean

0+77

E + 0.6 N edge Bd. addition to wash room

305.84

55

0+80

E 4.4 301.44

C 4.5 301.34

W 4.8 301.04

1+00

W 4.7 301.14

C 4.5 301.34

E 4.3 301.54

1+10

W+1 & 12' P.P.

1+20

E 4.0 301.84

C 4.2 301.64

W 4.4 301.44

+1 end Lath fence

1+60

W - 0.1 Beg. Corn. ^{Cobble} wall 4.0 301.84

W 4.0 301.84

C 3.4 302.44

E 3.0 302.24

1+83

W+0.1 ^{Cor} end Cobble wall

1+85

W - 0.1 SE Cor. Sted

1+89.7

C Run in H. 2.99 302.85

305.84

1+94

W + 0.2 H.S. Cor. Shed + Beg. wire fence

2+00

- 20

E

C

W

+ 20

2+09

E + 0.8 Beg. picket fence

2+10

W - 0.1 end wire fence

2+11

W + 1.5 ϕ 12" P.P.

2+49.5

- 20

W

C

+ 9 end picket fence

E Ed. Pipe Cor.

+ 10

2+85

- 10

E

C

+ 5

2.7

303.14

3.0

302.84

3.0

302.84

3.3

302.54

3.8

302.04

3.2

302.64

2.7

303.14

2.6

303.24

2.4

303.44

2.3

303.54

2.0

303.84

1.9

303.94

2.2

303.64

1.8

304.04

305.84

56

W

2.1

303.74

+ 0.2 beg. Bd. fence

+ 20

2.3

303.54

T.P.

C.C.I

310.64

1.83

304.01

3+10

W - 15

7.3

303.32

W

6.9

303.72

+ 6.2 ϕ 12" P.P.

C

6.7

303.92

E

6.4

304.22

+ 15

6.4

304.22

3+50

- 15

5.8

304.82

E

5.9

304.72

C

6.4

304.22

W

6.3

304.32

+ 15

6.8

303.82

3+60

W + 0.3 End Bd. + beg. catch fence

3+64.8

W - 2.7 S. end + E.L. 6.04 304.58 of 15 Cor. walk

3+82

W - 2.3 N. end + E.L. 5.98 304.64

of 15 Cor. walk

4+00

-15	5.9	304.72
W	5.8	304.82
C	5.7	304.92
E	5.5	305.12
+15	5.2	305.42

4+10

W-02 end last fence

W+0.8 Φ 10" P.P.

4+50

-15	4.3	306.32
E	4.3	306.32
+4	5.1	305.52
C	5.1	305.52
W	5.1	305.52
+15	5.3	305.32

4+68

W-20.7 Φ Sim. gar.	4.99	305.63	CON. FL.
-15.5 Φ Con. apron	5.08	305.54	
W	4.0	306.02	
C	4.8	305.82	
E	4.4	306.22	
+15	4.4	306.22	

4+70

E-3' S.L. 4 Con. gar.	3.69	306.93	CON. FL.
-----------------------	------	--------	----------

4+89.3

C	M.H. Rim	4.25	306.37	
5+06				
E-3	S.L. 4 Con. gar.	3.69	306.93	CON. FL.
E		4.2	306.42	
C		4.2	306.42	
W		4.1	306.52	
+15		4.6	306.02	

5+10

W+0.6 Φ 10" P.P.

5+24

W-31.7 Φ Sim. gar.	4.77	305.85	CON. FL.
W-25.3 Φ Con. apron	4.74	305.88	
W	4.3	306.32	
C	4.2	306.42	
E	4.0	306.62	
+15	4.0	306.62	

5+39

E-04 S.W. Con. Bathroom add. to House

5+48

E-04 NW Con. " " " "

5+50

-15	3.5	307.12
E	3.8	306.82
C	3.7	306.92
W	3.9	306.72
+15	4.3	306.32

310.62

5+75

-15		4.1	306.52
W		3.5	307.12
C		3.7	306.92
E		3.5	307.02
+15		3.4	307.22
	C+00		
-10		3.3	307.32
E		3.5	307.02
+5		4.1	306.52
C		4.0	306.62
W		3.4	307.22
+15		4.0	306.62

C+10

W+06 E 14" PP

C+11

-15		K.0	306.62
W		3.5	307.12
+5		K.C	306.02
C		K.8	305.82
+5		K.C	306.02
E		3.9	306.72
+10		3.7	306.92

C+20.03 S.L. THORN ST.

E	Top cb.	5.10	305.46
E	Con. Pav.	5.38	305.24

310.62

58

C	Con. Pav.	5.66	304.96
W	" Pav	5.42	305.20
W	Top cb.	5.24	305.38
	C+33.03	5.06	Line of THORN
W	on Pav.	6.00	304.62
C	" "	5.86	304.76
E	" "	5.65	304.97

T.P.	3.46	309.61	4.47	306.15
------	------	--------	------	--------

check to NEBP	THORN + 10.60	5.89	303.72	303.69
				0.03

xsec alley Blk 16 CITY HTS.

Sketch P. 54

P. 58
N.E.B.P.

8.50 312.19

303.69 Thorn
+ Nile

0-13 - N. cb. Line Thorn

W on Pav 6.90 305.29

C " " 6.74 305.45

F " " 6.60 305.59

0+00 - N.L. Thorn St.

E Top cb. 5.90 306.29

E Pav 6.19 306.00

C " 6.49 305.70

W " 6.25 305.94

W Top cb. 6.08 306.11

0+01

W - 0.9 beg. picket fence

0+07

E + 0.7 beg. Cobble wall 4.3 307.89 Top

E + 1.5 ground 5.3 306.89

0+10

W 5.0 307.19

C 5.4 306.79

+ 7.5 ground 5.2 306.99

+ 7.6 A Top cobble wall 4.1 308.09

E 4.0 308.19

0+30

E ground 3.7 308.49

+ 2.7 Top end Cobble wall 3.3 308.89

+ 2.5 ground 3.9 308.29

C 4.0 308.19

W 4.1 308.09

0+34

E - 0.1 beg. picket fence

0+45.5

W - 3.4 S.E. Cor. Sim. gate South entrance 3.58 308.61 Cor. FL.

W - 0.4 E. 7' Cor. slab 3.57 308.62 garbage
STAND

W 3.6 308.59

C 3.6 308.59

E 3.5 308.69

+ 1.0 Lawn 3.4 308.79

0+70

- 1.0 in yard 2.9 309.29

E 3.3 308.89

C 3.2 308.99

W 3.1 309.09

+ 1.0 in yard 3.4 308.79 drain riser

1+00

- 1.5 3.4 308.79

W - 0.3 end picket fence

W 3.0 309.19

C 2.7 309.49

312.19

1700

E 2.6 309.59

+10 2.8 309.29

1701

E to y end picket and beg. last fence ^{04 in alley}

W +17 15" P.P.

T.P. nail
in P.P.
1701 on W

4.95 314.68 2.46 309.73

1702

W - 13.25 h. do. gar. ^{CON. FL.} 5.38 309.30 ^{5 1/2 = NO APRON}

1724

-15 5.2 309.48

E 5.2 309.48

+5 5.4 309.28

C 5.2 309.48

W 5.2 309.48

+12.6 N. edge CON. apron 5.42 309.26

+13.7 N.L. do. gar. ^{CON. FL.} 5.42 309.26

1750

-15 5.4 309.28

W 5.0 309.68

C 5.3 309.28

+5 5.3 309.28

+9.4 End last + Beg. of Picket fence

E 5.1 309.58

+15 5.1

314.68

60

1775

-15 in yard 5.0 309.68

E 5.1 309.58

C 5.2 309.48

W 4.9 309.78

+15 5.0 309.68

2700

-15 4.8 309.88

W Beg. Bd. fence 4.6 310.08 on line

C 5.0 309.68

+9.5 picket fence

E 5.0 309.68

+15 in yard 5.0 309.68

2725

-15 out apron 4.5 310.18

E 4.7 309.98

C 4.5 310.18

W 4.5 310.18

+15 in yard 4.5 310.18

2748

E end picket + Beg. wire fence on line

2750

-15 4.5 310.18

W end Bd. fence 4.4 310.28 on line

C 4.6 310.08

E 4.5 310.08

+15 4.4 310.28

314.68

2 + 51

W + 1.7 @ 12" P.P.

2 + 75

E - 1.5 on 2' con. walk 4.4 310.54

E - 0.1 end " " " 4.0 310.58

E 4.3 310.38

C 4.4 310.28

W 4.2 310.48

+ 1.5 4.3 310.38

2 + 99.5

- 1.5 4.3 310.38

W 4.3 310.38

+ 1.4 @ 12" P.P.

C 4.2 310.48

+ 9.7 wire fence

E 4.2 310.48

+ 1.5 yard 4.0 310.68

3 + 25

- 1.5 3.8 310.88

E 4.1 310.58

C 3.8 310.88

W 3.7 310.98

+ 1.5 3.8 310.88

3 + 48

E + 0.5 end wire and beg. Lark fence
in alley

314.68

3 + 50

- 1.5 3.4 311.28

- 2 Beg. green hedge

W 3.1 311.58

C 3.5 311.18

E 3.6 311.08

+ 1.5 3.8 310.88

T.P. 5.9 316.52 3.35 311.33

3 + 81

- 1.5 5.4 311.12

E end Lark fence 5.2 311.32 on line

C 5.4 311.12

W 4.9 311.62

+ 2 hedge

+ 1.5 yard lawn 4.9 311.62

3 + 82

E - 5.5 S.L. do. gar. 5.08 311.44 con. EC

3 + 98

E - 5.6 W.L. do. gar. 4.97 311.55 " "

W - 2 end hedge

4 + 00

- 1.5 5.0 311.52

W 4.6 311.92

C 5.2 311.32

61

316.52

E		5.2	311.32
+15		5.1	311.42
	4+08		
W+09	E 1x" P.P.		
	4+25		
-15		4.9	311.62
E		5.2	311.32
C		5.1	311.42
W		4.6	311.92
+15		4.8	311.72
	4+50		
-15		4.4	312.12
W		4.3	312.22
C		4.8	311.72
F		4.8	311.72
+15		4.5	312.12
	4+75		
-15		4.1	312.42
-1'	Req. back fence		
F		4.7	311.82
C		4.6	311.92
W		4.1	312.42
+15		4.1	312.42

316.52

62

	4+97		
E-8	on Cor. walk	4.0	312.52
F-07	Req. 1.5 ^{Com.} W. L. walk	4.00	312.52
	5+00		
-15	ground	3.9	312.62
-15	S.E. Cor Top Cor. wall	2.94	313.58
-0.9	" " "	3.23	313.29
-0.9	ground	3.9	312.62
W		3.9	312.62
C		4.1	312.42
F		4.3	312.22
+0.7	W.L. 1.5 ^{Com.} walk	3.97	312.52
+10	ground	4.2	312.32
	5+08		
W+0.8	E 1x" P.P.		
	5+12		
W-1'	end ^{Com.} wall	3.00	313.52
"	" " "	3.5	313.02
	5+20		
E-15	yard	4.0	312.52
F-07	wedge 1.5 ^{Com.} walk	3.78	312.74
F		4.2	312.32
C		4.0	312.52
W		3.6	312.92
+1'	ground	3.6	312.92
+1	Top Req. ^{Com.} wall	3.10	313.42
W+15	yard	3.4	313.12

316.57
T.P. 5.55 318.63 3.54 312.98

5+50

W-1.5 5.0 313.63

W-1.3 end picket 489. Rd. fence

W-1' end top Con. wall 4.57 314.06

W 5.0 313.63

C 5.7 312.93

E 5.8 312.83

E +0.7 wedge 1.5 Con. walk 5.52 313.11

+1.5 ground 5.0 313.03

5+60

E +0.7 E 7' Con. apron 5.48 313.15

E-1.6 " " " 5.18 313.45 + 9 garage

5+85

E 0.7 = wedge 1.5 Con. walk 5.02 313.61

E 5.2 313.43

C 5.1 313.53

W 4.8 313.83

C +0.2

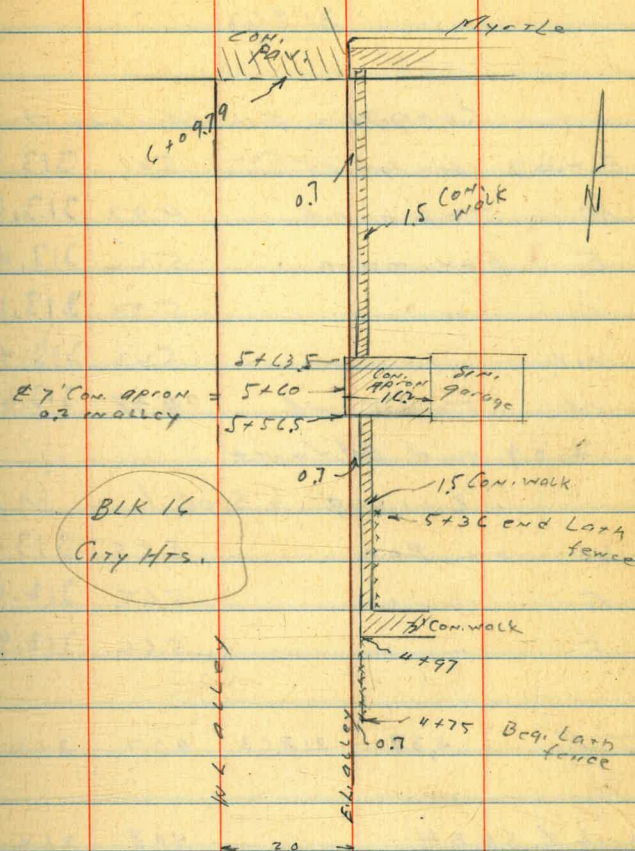
W 4.5 314.13

+4 5.0 313.63

C 5.2 313.43

E 4.8 313.83

E +0.7 wedge 1.5 Con. walk 4.74 313.89



318.63

6109.79 = S.W. Myrtle Ave.

E-07 W. edge 15' ^{com.} walk 5.01 313.62

E Top curb 4.97 313.66

E Pav. edge 5.22 313.41

C " " 5.50 313.12

W " " 5.23 312.40

W Top curb 4.98 313.65

+ 0.9 end distance

6114.79 = S. 66' Line Myrtle

W on Pav. 5.55 313.08

C " " 5.65 312.98

E " " 5.66 312.97

T.P. 4.37 318.63 4.37 314.26

check to S.E.B.P. 4.08 314.55 314.56

Side of Myrtle 0.01

Location & Levels of
Storm drains at
47th & Market

EM. P.I.C
E.L. C.T.
47th and
Market 4.56 125.52 120.96

E.L. inlet of Ex. 36" 10.50 115.02

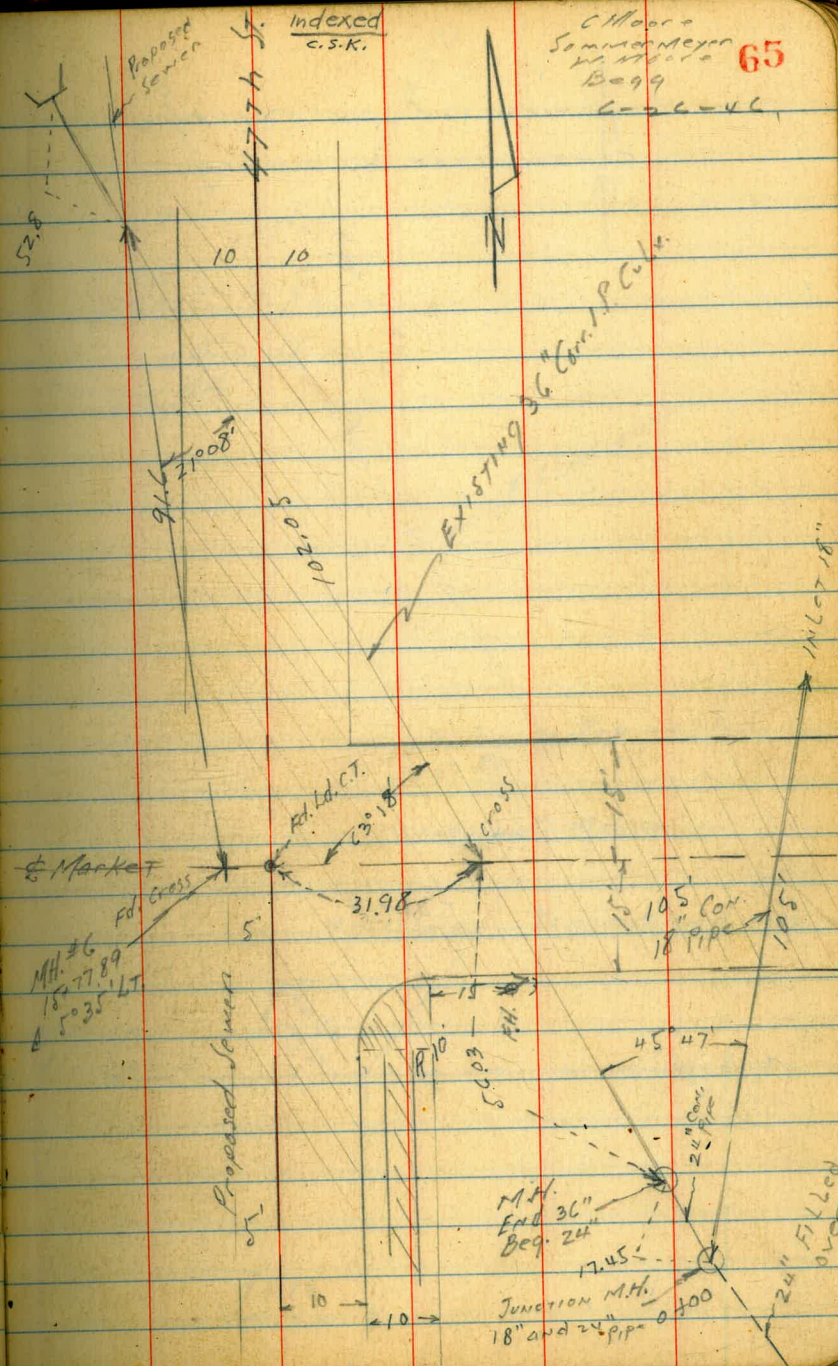
E.L. of M.H. End of 36"
Beg. 24" 17.00 108.52

Rise and ground " " 4.4 121.1

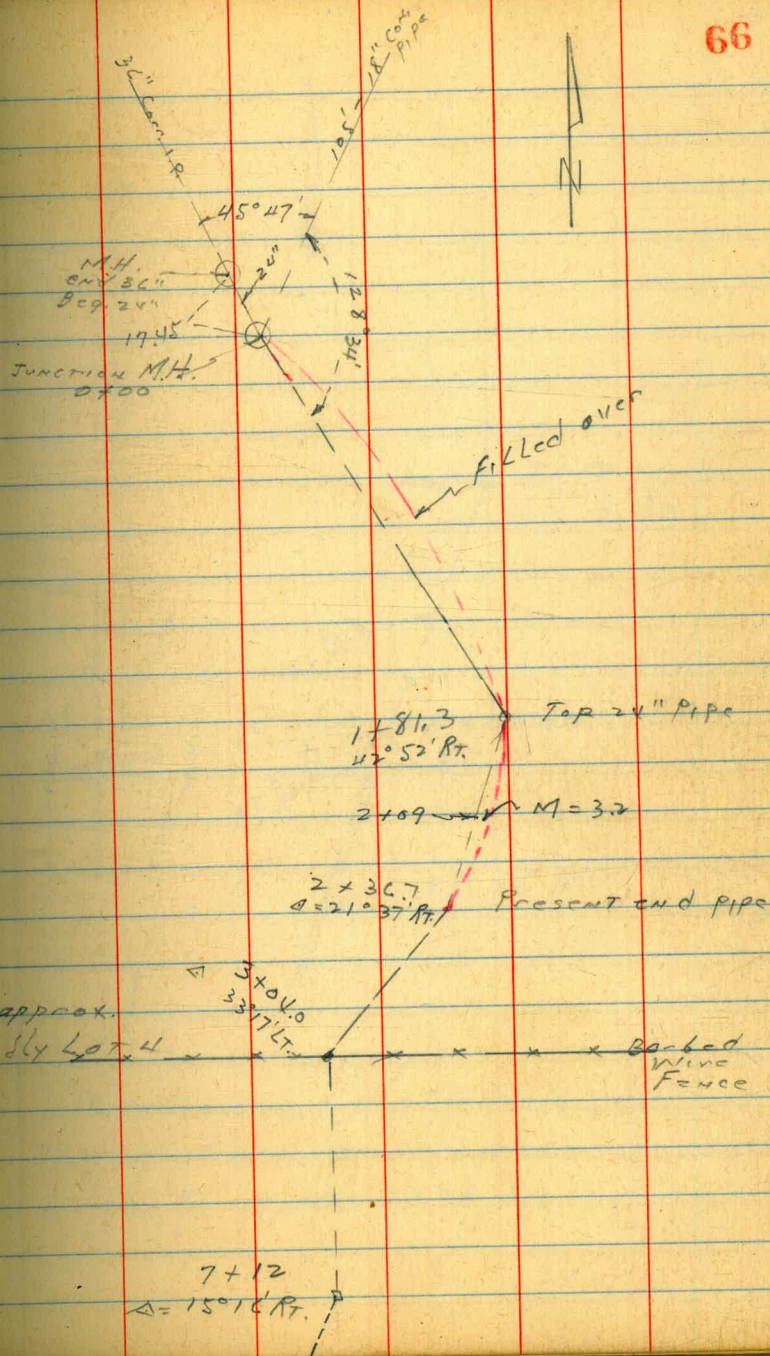
E.L. of inlet of 18" pipe 11.83 113.69 N. Side
Market

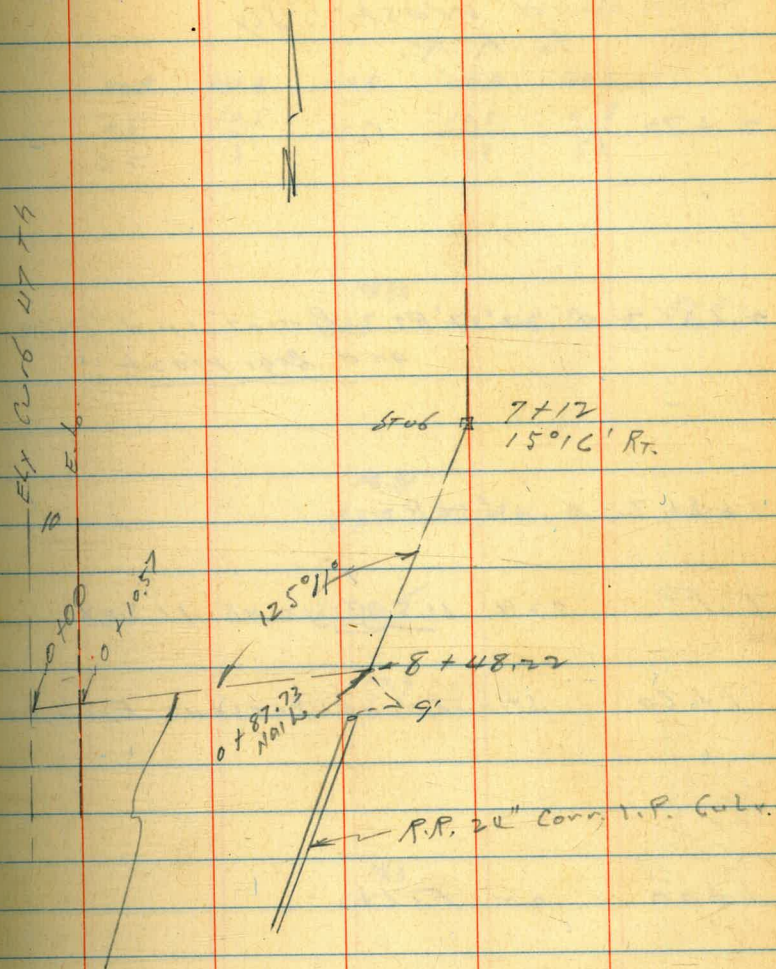
JUNCTION M.H.
18" and 24" 17.55 107.97

Rise & ground " " " 4.6 120.9



Location of 24" Con. Pipe
constructed by owner.





See Recent Survey
to standardize this R.R. Curb
and const. curb outlet
on to E of 47th St.

Levels of Ex. 24" Con. Pipe
and Wash Sly
to R.R.

2+70

2+34.7 Δ 21° 37' RT Present end pipe
and beg. Wash

1+81.3 Δ 42° 52' RT

T.P. 039 115.33 10.48 11.50x

1+60 shoulder present fill

1+00 on fill

0+00 = Junction M.H.
Fl. 24" and 18" 17.55 107.97

125.52 \downarrow from P. 65

LT = TO EAST $\frac{1}{2}$

R₂ = 68
TO WEST

110.8	109.8	109.8	109.8	108.5
<u>4.5</u>	<u>10.5</u>	10.5	<u>10.5</u>	<u>6.8</u>
25	3		33	50

103.95
11.38 = Fl. 24" ^{END} PIPE

106.99
8.34 = Top 24" Con. Pipe

115.33 \checkmark

117.9
7.6

119.3
6.7

17.55 = Fl. 107.97

125.52 \checkmark

5+00

4+50

T.P.

5.14 107.94 12.53 102.80

4+00

3+50

3+25

3+04 Δ 33° 17' LT. Sec. on SPLIT.

115.33

102.8	100.5	100.3	100.3	102.9
<u>4.1</u>	<u>7.4</u>	7.6	<u>7.6</u>	<u>3.5</u>
75	44		14	35

103.5	101.9	101.7	100.6	105.9
<u>4.4</u>	<u>6.5</u>	6.7	<u>7.3</u>	<u>2.0</u>
75	44		20	40

107.94 ✓

105.6	109.9	102.7	102.1	105.9
<u>9.7</u>	<u>10.4</u>	12.6	<u>13.2</u>	<u>9.4</u>
25	15		33	50

111.5	110.3	106.8	103.5	103.2	108.2
<u>3.8</u>	<u>5.0</u>	8.9	<u>11.8</u>	<u>12.1</u>	<u>7.1</u>
25	15		21	55	65

110.6	106.8	103.9	103.7	108.8
<u>4.7</u>	8.5	<u>11.4</u>	<u>11.6</u>	<u>6.9</u>
25		15	49	60

109.9	107.3	109.5	107.5	109.6	109.6
<u>5.9</u>	<u>8.0</u>	<u>10.8</u>	10.8	<u>10.7</u>	<u>5.7</u>
25	7	5		44	55

115.33 ✓

7+50

T.P. 3.80 99.12 12.62 95.32

7+12 A 15.6 R

6+75

6+50

6+00

5+50

107.94 ✓

Lr

R

R

70

97.5	93.5	99.2	96.3
16	56	4.9	2.8
15		3	19

99.12 ✓

101.8	95.6	95.3	95.4	99.7
61	12.3	12.6	12.7	8.2
30	5		6	18

101.6	99.9	96.1	95.7	96.3	99.8
6.3	8.0	11.8	12.2	11.6	8.1
30	15		2	11	22

101.2	97.3	97.3	97.9	105.3
6.7	10.6	10.6	10.5	2.6
35	25		17	36

102.2	98.2	98.3	98.5	103.9
5.7	9.5	9.6	9.4	4.0
50	32		8	20

102.3	99.6	99.3	99.3	103.6
5.6	8.3	8.6	8.6	4.3
50	25		18	35

107.94 ✓

at top E. ch of 47th 11.15 87.97 ✓
 check me in other
 Book
 Proposed 8 Curb
 gutter

8 + 57.22 = E.L. 24" under Ex. RR Curb

8 + 48.22

8 + 25

8 + 00

7 + 80

99.12 ✓

87.91

11.71 = E.L. 24"

91.3	88.2	88.2	88.2	92.3
7.8	10.9	10.9	10.9	6.8
5	2		2	7

93.6	90.8	90.8	89.8	92.2	97.1
5.5	8.3	8.3	9.3	6.9	2.0
41	24		6	15	23

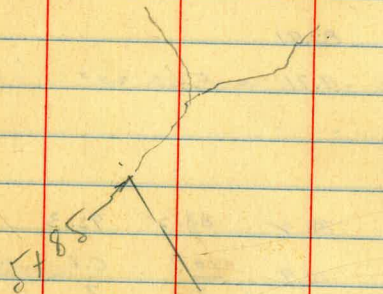
99.1	90.7	93.6
5.9	8.4	5.5
21		17

97.0	93.9	91.6	91.7	92.1	94.2	95.1
2.1	5.2	7.5	7.4	7.0	4.9	4.0
20	6	4		7	10	20

99.12 ✓

Levels for drain
 N.W. Cor. of 47th and Market

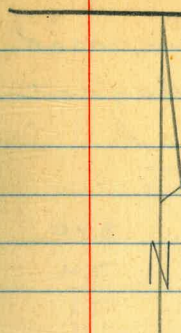
C.S.M.
 C.S.
 W.M.
 E.B.
 C-28-4C.



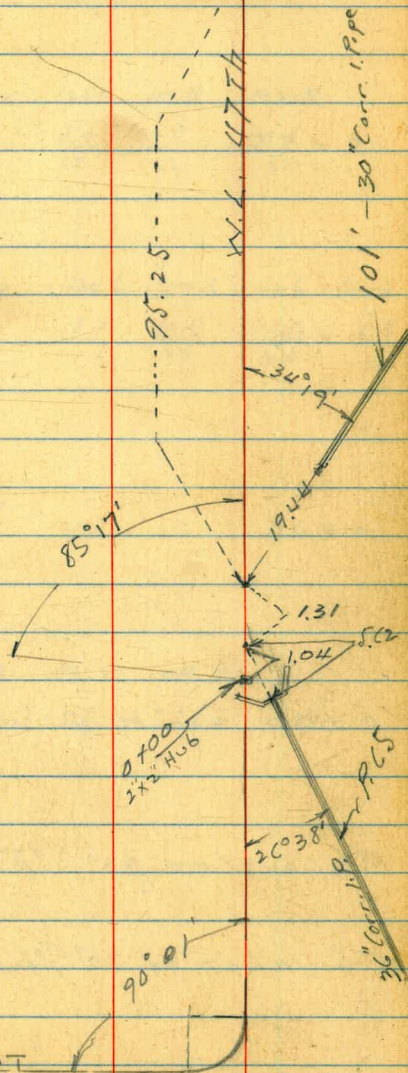
3 + 50.10
 Δ = 53.13 Rt.

SEE PAGE 49

72



Ed. R.E. 2718 3/4" Pipe



Baseline
 For Wash
 Levels

N.W. Market

Levels for proposed drain
NW 47th + Market
up Wash

0 + 55

0 + 30

0 + 06

0 + 00 2x2 Hub w/ 47th St.

F.L. outlet 30" ^{Corr} P.P. 12.74 116.59

F.L. inlet of 30" ^{Corr} P.P. 10.54 118.81

Ld. C.T. &
47th and
Market

837

129.33 ✓

120.96

LT to South \$

RT

73

124.8	123.2	121.3	117.8	121.5
<u>4.5</u>	6.1	8.0	<u>11.5</u>	7.8
15		15	23	31

122.1	121.2	120.6	117.8	117.6	121.4
<u>7.2</u>	8.1	<u>8.7</u>	<u>11.5</u>	<u>11.7</u>	<u>7.9</u>
25		12	20	24	31

119.3
100

119.27	115.3	116.4	118.7
<u>10.05</u>	14.0	<u>13.1</u>	<u>10.6</u>
5		7	14

Top Admt

129.33 ✓

1+66

1+25

1+05

0+95

0+86

0+70

129.33 ✓

LT

£

RT

74

126.3	123.3	122.2	126.2	127.9
$\frac{3.0}{15}$	$\frac{6.0}{5}$	6.1	$\frac{3.1}{4}$	$\frac{1.4}{25}$

125.3	125.1	122.9	122.5	122.8	124.7	125.2
$\frac{4.0}{15}$	$\frac{4.2}{10}$	$\frac{6.4}{6}$	6.8	$\frac{6.5}{2}$	$\frac{4.6}{7}$	$\frac{4.1}{20}$

125.7	123.6	121.9	121.9	123.5	122.2
$\frac{3.6}{15}$	$\frac{5.7}{3}$	7.4	$\frac{7.4}{4}$	$\frac{5.8}{8}$	$\frac{5.1}{28}$

125.9	123.8	120.9	122.8	123.2	120.8	123.8
$\frac{3.4}{15}$	5.9	8.9	$\frac{6.5}{14}$	$\frac{6.1}{33}$	$\frac{8.5}{39}$	$\frac{5.5}{40}$

125.7	124.1	121.9	118.9	119.4	122.8
$\frac{3.6}{15}$	5.2	7.4	$\frac{10.4}{16}$	$\frac{9.8}{22}$	$\frac{6.5}{37}$

125.6	123.9	121.8	118.2	121.9
$\frac{3.7}{15}$	4.4	$\frac{7.5}{20}$	$\frac{11.1}{25}$	$\frac{7.4}{31}$

129.33 ✓

2 + 70

2 + 45

2 + 30

2 + 20

2 + 10

1 + 84

T.P.

911

136.29

2.15

127.18

129.32

Lt

¢

Rt

75

131.5	130.0	126.1	126.1	130.8	132.9
4.8	6.3	10.7	10.7	5.5	3.4
15	6		3	10	25

130.6	129.3	125.8	125.8	125.7	129.3	131.7
5.7	7.0	10.5	10.5	10.6	7.0	4.6
15	6	1		3	9	25

130.7	129.0	128.9	125.0	125.0	129.3	130.7
5.6	7.3	7.9	11.3	11.3	7.0	5.6
15		3	8	11	15	25

130.2	129.5	126.7	124.3	128.9	130.9
6.1	6.8	9.6	12.0	7.4	5.9
15	5		14	19	30

129.6	128.5	127.5	123.9	123.9	128.7	130.5
6.7	7.8	8.8	12.4	12.4	7.6	5.8
15		8	12	16	20	30

129.0	126.6	123.9	123.9	127.2	127.7
7.3	9.7	12.9	12.9	9.1	8.6
15		4	10	14	20

136.29 ✓

4 + 45

4 + 10

3 + 85

T.P.

9.33 143.22 2.40 123.89

3 + 50.10 Δ = 53° 13' Rt Sec. an SPLIT

3 + 70

2 + 90

136.29 ✓

Lt

E

Rt

137.2	135.9	132.2	132.2	135.5	137.6
<u>6.0</u>	<u>7.3</u>	11.0	<u>11.0</u>	<u>7.7</u>	<u>5.6</u>
15	2		3	7	20

136.6	134.1	130.7	130.7	132.9	136.2
<u>6.6</u>	9.1	<u>12.5</u>	<u>12.5</u>	<u>8.3</u>	<u>7.0</u>
15		4	7	13	20

136.4	133.6	130.2	130.2	133.1	134.3
<u>6.8</u>	9.0	<u>13.0</u>	<u>13.0</u>	<u>10.1</u>	<u>8.9</u>
15		4	8	11	20

143.22 ✓

136.0	133.9	133.5	129.1	129.1	132.0	134.0
<u>6.3</u>	2.4	<u>2.8</u>	<u>7.7</u>	<u>7.2</u>	<u>4.3</u>	<u>2.3</u>
10		3	8	17	16	30

134.0	132.4	131.5	130.6	130.6	132.1	134.7
<u>2.3</u>	3.9	<u>4.8</u>	<u>5.7</u>	<u>5.7</u>	<u>3.0</u>	<u>1.6</u>
15		7	12	16	21	30

132.0	130.6	126.9	126.9	128.3	132.2	133.9
<u>4.2</u>	5.7	<u>9.4</u>	<u>9.4</u>	<u>8.0</u>	<u>4.1</u>	<u>2.4</u>
15		5	8	11	18	25

136.29 ✓

check to orig B1A 10.91 170.97 120.96 ✓

T.P. 1.66 131.88 13.00 130.22 ✓

5 + 85 env? ✓

5 + 30

5 + 00

4 + 70

143.22 ✓

Notes Reduced 7-9-96

LT

S

F₂

77

142.9	138.9	139.0	139.6	141.8
<u>0.8</u>	<u>4.3</u>	<u>4.2</u>	<u>3.6</u>	<u>1.4</u>
15	4		4	14

141.5	140.1	136.5	136.5	136.5	139.5	142.1
<u>1.7</u>	<u>3.1</u>	<u>6.7</u>	<u>6.7</u>	<u>6.7</u>	<u>3.7</u>	<u>1.1</u>
15	9	1		2	8	25

140.8	139.0	136.0	136.9	139.0	140.9
<u>2.4</u>	<u>4.2</u>	<u>7.2</u>	<u>6.8</u>	<u>4.2</u>	<u>2.3</u>
15		8	12	17	25

138.9	137.3	139.5	139.5	138.0	139.9
<u>4.3</u>	<u>5.9</u>	<u>8.7</u>	<u>8.7</u>	<u>5.2</u>	<u>3.3</u>
15		11	14	20	25

143.22 ✓

Additional Notes F Line
Proposed Sewer Federal Blvd. Sub #2

78

- 5+53 $\frac{1}{2}$ = S W/4 Young Berry Rt. Ford Page 38
5+56 $\frac{1}{2}$ = S/4 Strawberry East of Fence
+66 35 Rt of $\frac{1}{2}$ = 3" Lemon Tree
+79 35 Rt of $\frac{1}{2}$ = 1" Plum "
+93 18 Rt of $\frac{1}{2}$ = 2" Orange Tree
+97 1.8 Lt of $\frac{1}{2}$ = Picket Fence
6+08 35 Rt of $\frac{1}{2}$ = 2" Orange Tree
+19.5 32 Rt of $\frac{1}{2}$ = " "
+36 $\frac{1}{2}$ = S/4 2.5 Hedge
+37 2 Lt of $\frac{1}{2}$ = W/4 Picket Fence
7+0 1 Lt of $\frac{1}{2}$ = $\frac{1}{2}$ 2.5 Hedge
7+8 0.2 Rt of $\frac{1}{2}$ = S/4 Tol Pole # 477539 H
+20.3 = E + W Board Fence
+26 16 Rt of $\frac{1}{2}$ = Board Fence Also Fly Flower Bed
+55 2.5 Lt of $\frac{1}{2}$ = 1/2" Tree
" 0.8 Rt of $\frac{1}{2}$ = Board Fence
+58 2 Lt of $\frac{1}{2}$ = Bird Bath Portable
+63.5 2.9 Lt of $\frac{1}{2}$ = S E/4 10 Rose Bushes
+88 $\frac{1}{2}$ = Board Fence
8+02.6 $\frac{1}{2}$ = N + S Picket Fence Also 2 Lt of $\frac{1}{2}$ = N W/4 10 Rose Bushes
8+05 0.8 Lt of $\frac{1}{2}$ = Angle of Board Fence

Walker
Hendricks
Becker
Williams
2-27-48

Location Existing 24" steel Culvert
in Sunshine Gardens Subdv.
South of Market St
And East of 47th St.

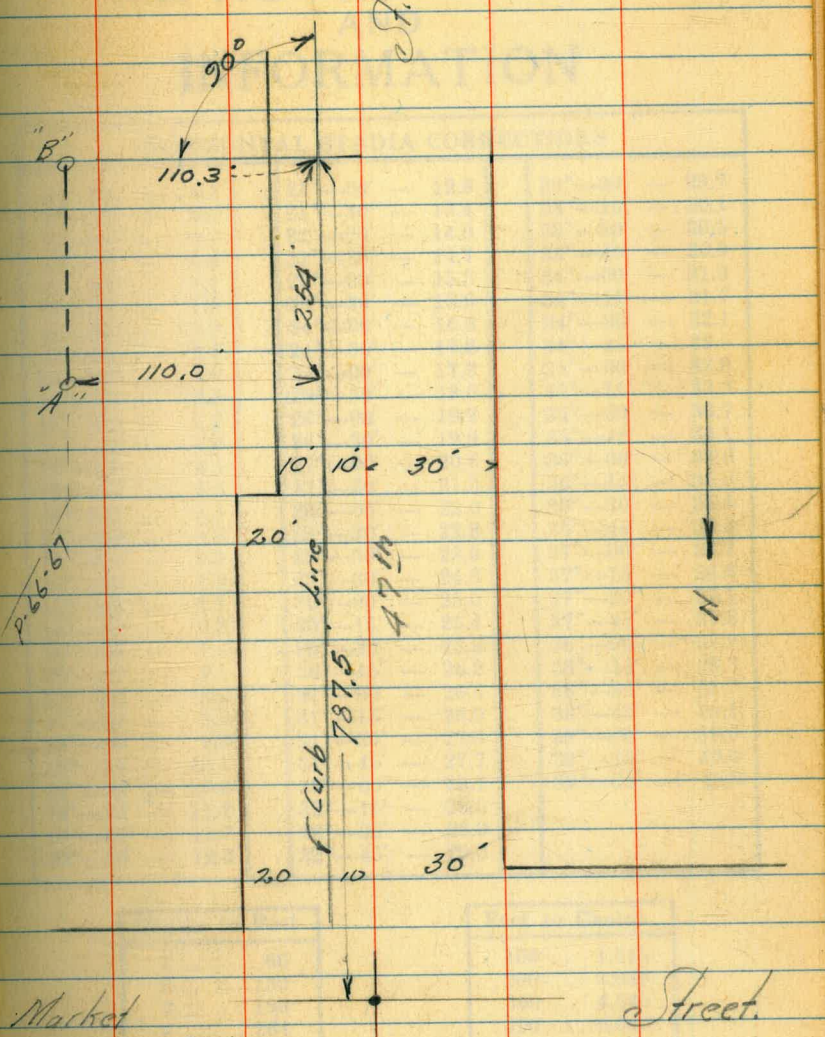
Sta + H.I - Elev
Top of Pipe

110-21001

INDEXED
MAR 2 1948

"B" on Top 24" Steel Pipe	6.42	98.56
"A" on Top 24" Cons. Pipe	1.28	102.70
B.M	16.57	104.98

87.41
87.91



F.L. 24" Pipe under R.R. track From P-71
8-57-22 - this Book

IMPROVED TABLES AND INFORMATION

149
62

HORIZONTAL STADIA CORRECTIONS

2°-00' — 0.1	21°-00' — 12.8	33°-00' — 29.7
3°-00' — 0.3	21°-30' — 13.4	33°-15' — 30.1
4°-00' — 0.5	22°-00' — 14.0	33°-30' — 30.5
5°-00' — 0.8	22°-30' — 14.7	33°-45' — 30.9
6°-00' — 1.1	23°-00' — 15.3	34°-00' — 31.3
7°-00' — 1.5	23°-30' — 15.9	34°-15' — 31.7
8°-00' — 1.9	24°-00' — 16.5	34°-30' — 32.1
9°-00' — 2.5	24°-30' — 17.2	34°-45' — 32.5
10°-00' — 3.0	25°-00' — 17.9	35°-00' — 32.9
10°-30' — 3.3	25°-30' — 18.6	35°-15' — 33.3
11°-00' — 3.6	26°-00' — 19.2	35°-30' — 33.7
11°-30' — 4.0	26°-30' — 19.9	35°-45' — 34.1
12°-00' — 4.3	27°-00' — 20.6	36°-00' — 34.6
12°-30' — 4.7	27°-30' — 21.3	36°-15' — 35.0
13°-00' — 5.1	28°-00' — 22.0	36°-30' — 35.4
13°-30' — 5.5	28°-30' — 22.8	36°-45' — 35.8
14°-00' — 5.9	29°-00' — 23.5	37°-00' — 36.2
14°-30' — 6.3	29°-30' — 24.3	37°-15' — 36.6
15°-00' — 6.7	30°-00' — 25.0	37°-30' — 37.1
15°-30' — 7.2	30°-15' — 25.4	37°-45' — 37.5
16°-00' — 7.6	30°-30' — 25.8	38°-00' — 37.9
16°-30' — 8.1	30°-45' — 26.2	38°-15' — 38.3
17°-00' — 8.5	31°-00' — 26.5	38°-30' — 38.7
17°-30' — 9.0	31°-15' — 26.9	38°-45' — 39.1
18°-00' — 9.5	31°-30' — 27.3	39°-00' — 39.6
18°-30' — 10.1	31°-45' — 27.7	39°-15' — 40.0
19°-00' — 10.6	32°-00' — 28.1	39°-30' — 40.5
19°-30' — 11.2	32°-15' — 28.5	
20°-00' — 11.7	32°-30' — 28.9	
20°-30' — 12.3	32°-45' — 29.3	

Chains to Feet

1	66
2	132
3	198
4	264
5	330
6	396
7	462
8	528
9	594
10	660

Feet to Chains

100	1.515
200	3.030
300	4.545
400	6.060
500	7.575
600	9.090
700	10.606
800	12.121
900	13.636
1,000	15.151

814
46527 NWE/Cujon + Gilcher

51.85 E/W

91.2 N/H

22

17 + 39.37
4.6063

787.5
533
25 x 5

35 = 455
485
5.15
29.74 = M/H

62.55 = Prop

63 = Line

64 = stake

5+44.74

0+32

+64 = DE.

RE 2718

116
68
48
147127
29.30
275057

9290
3425

865
36
122.5

170.8
39
131.8

LS
2236