

1678



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DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

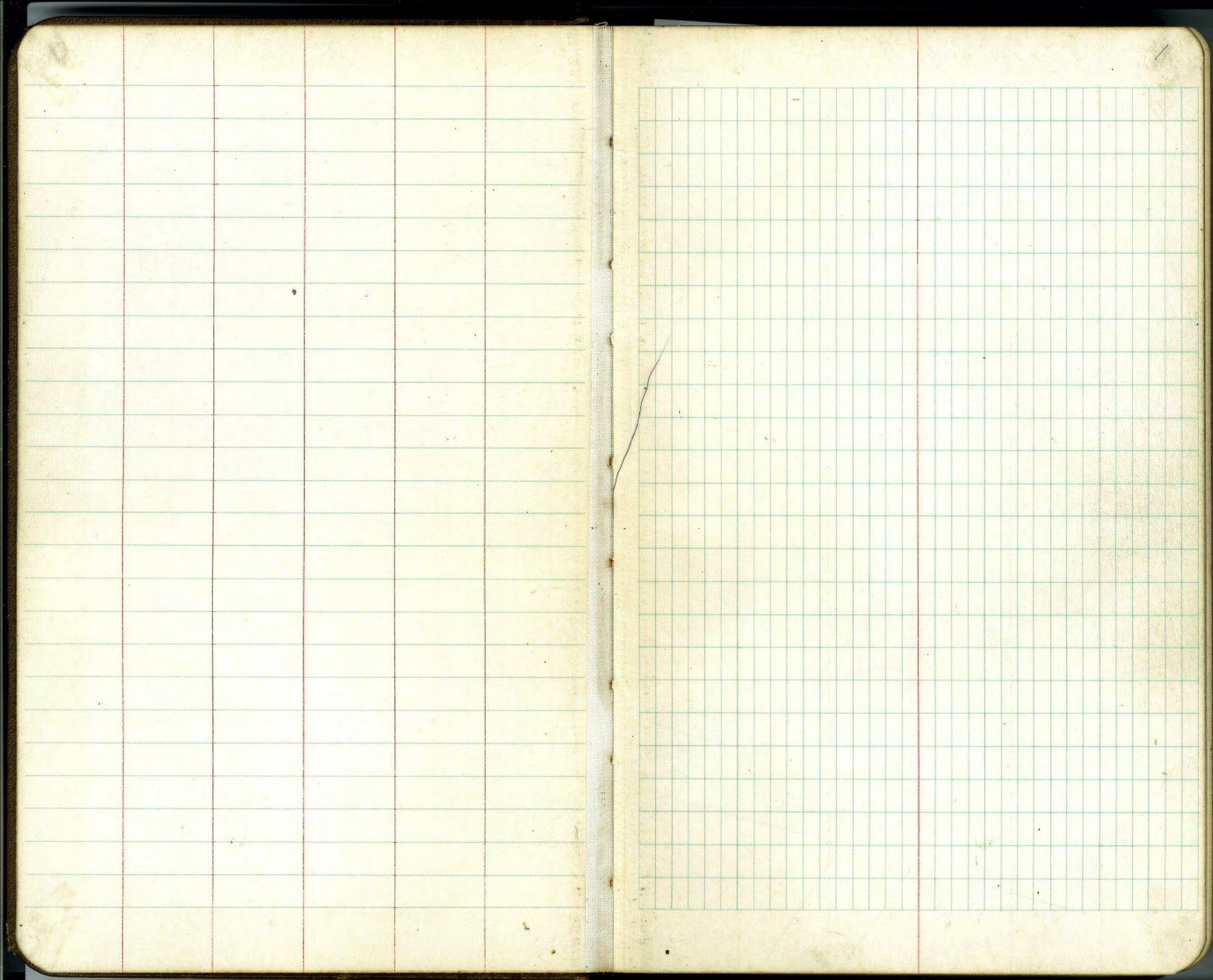
Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.  
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1678

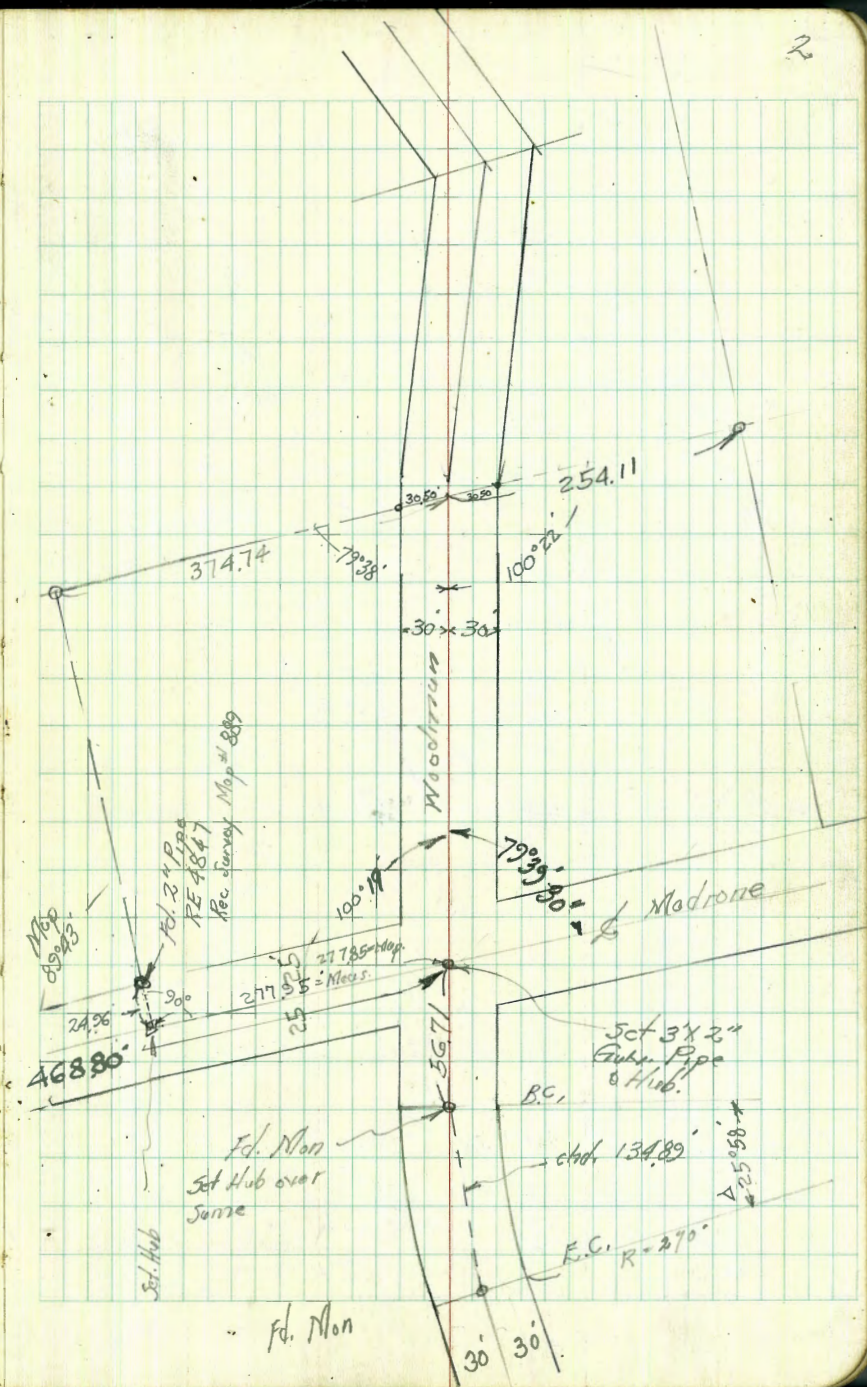
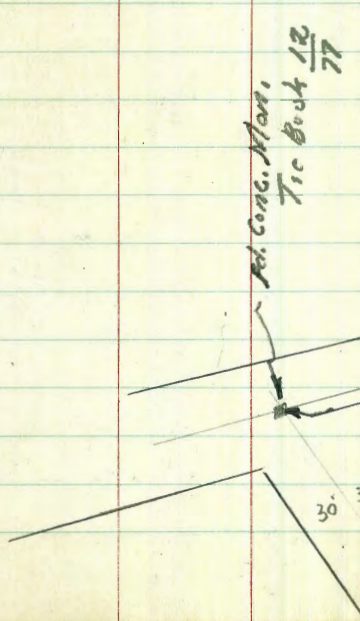
CITY ENGINEER'S OFFICE

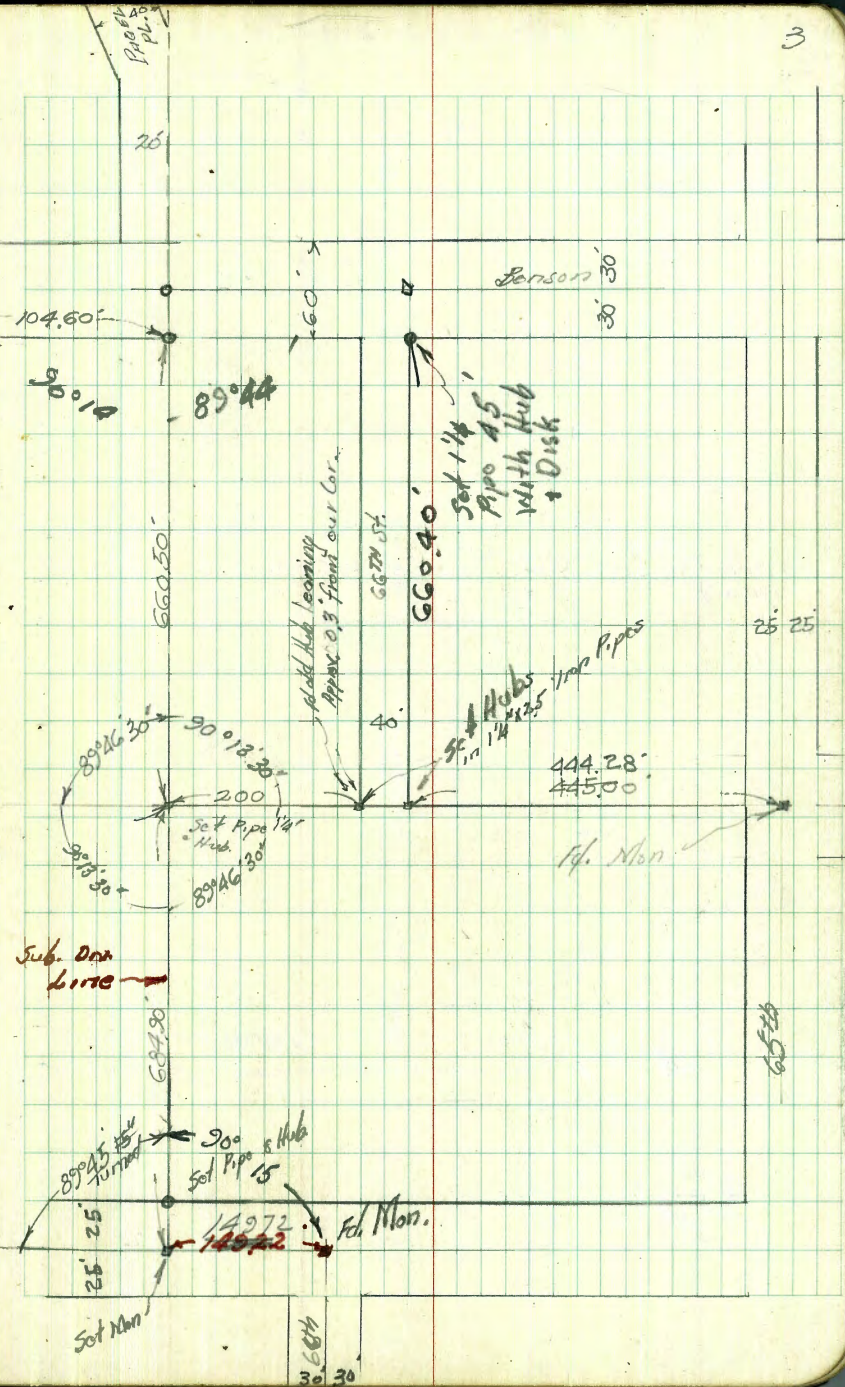
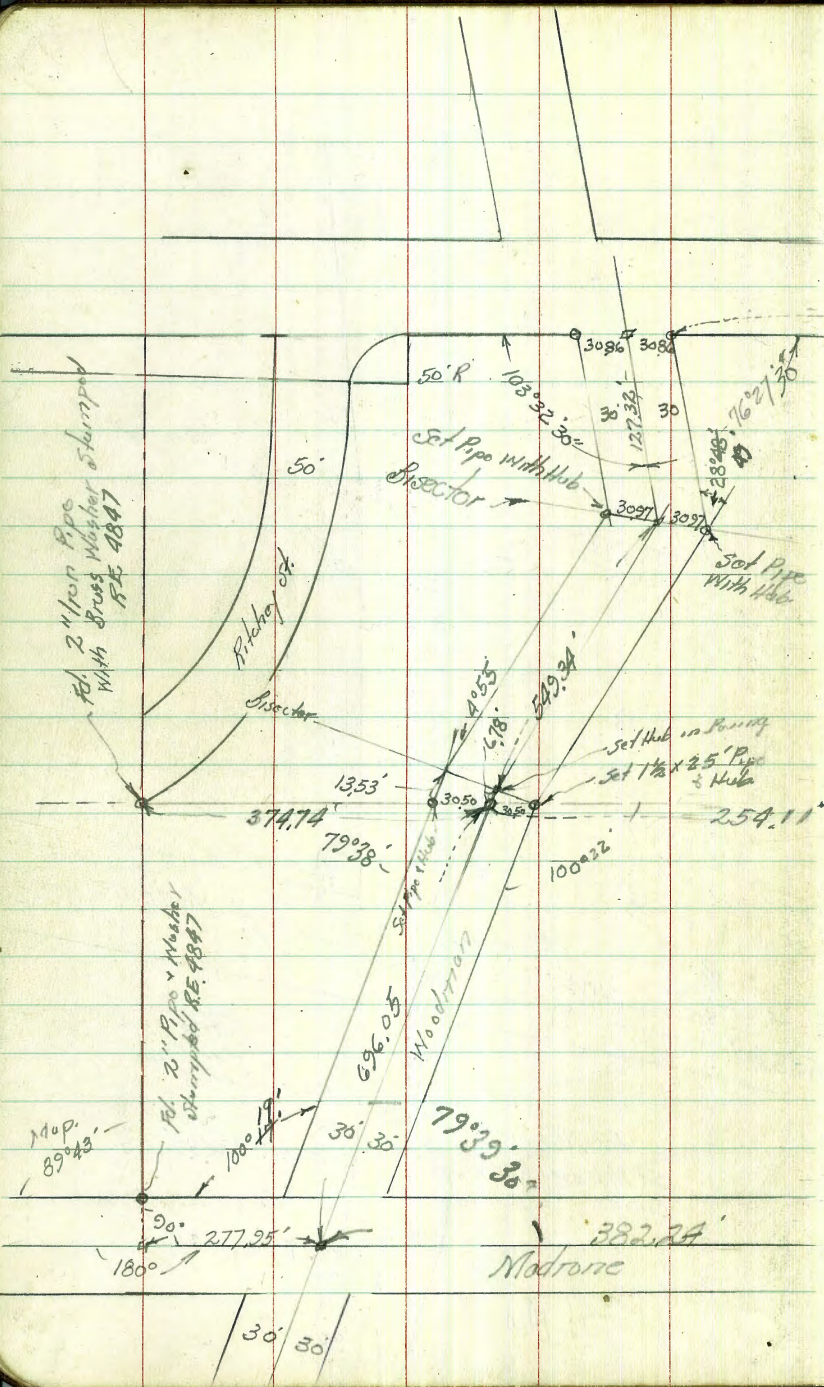
This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

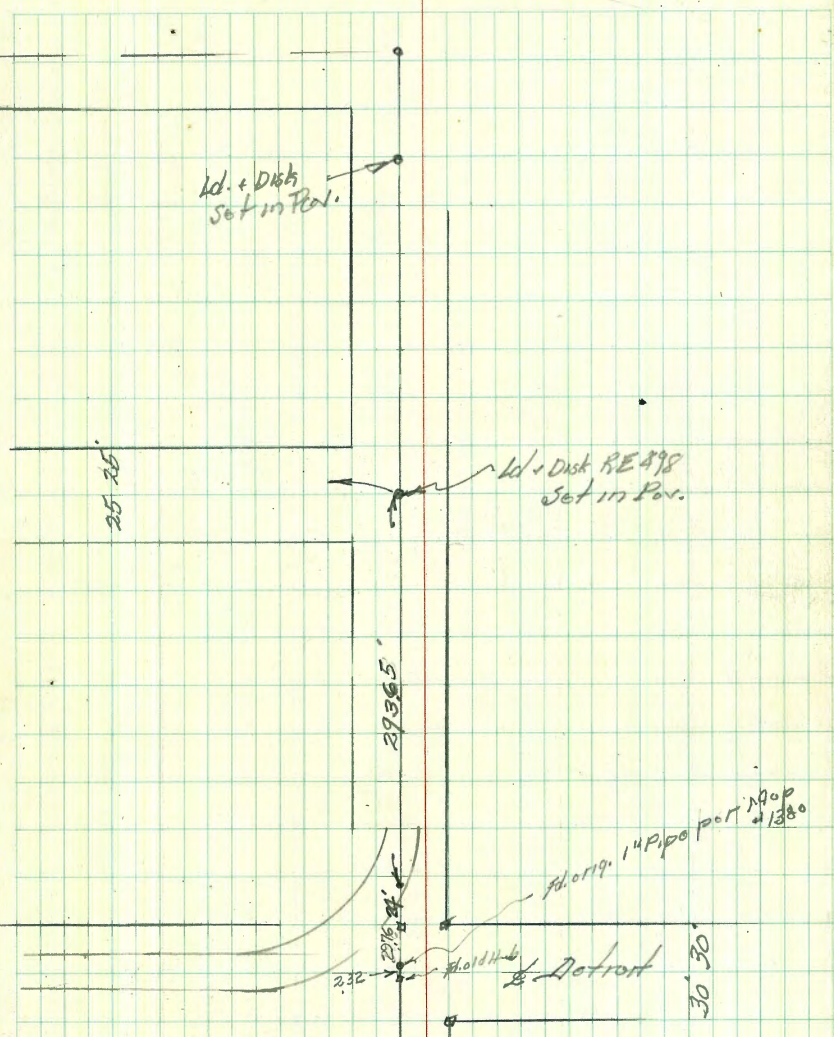
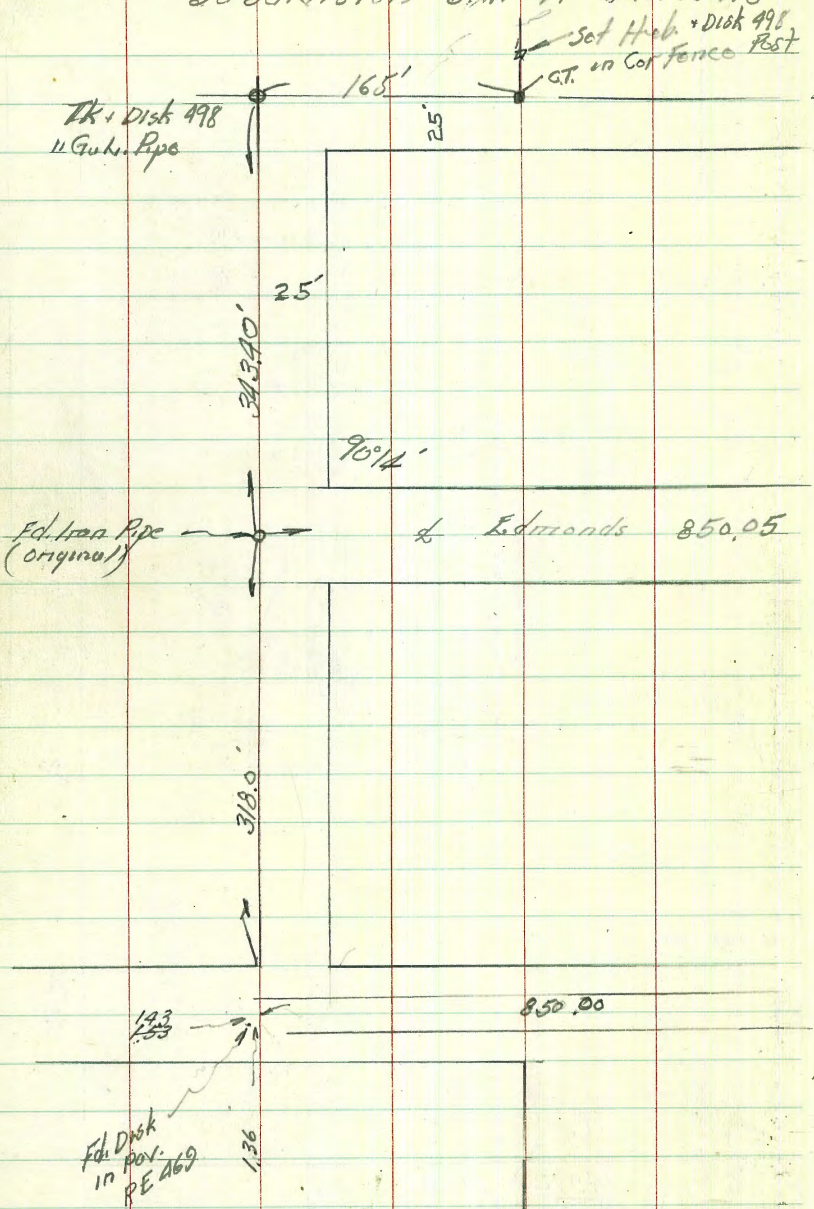


Walker, Hazard, Hardin  
 ~ Fort Comto Ties ~  
 Preliminaries for Tie Point Work  
 Page 1 to 5  
 July 27-1944 This Book Not supposed to be  
 used as a permanent record.  
 For final Ties see Tie Book #24

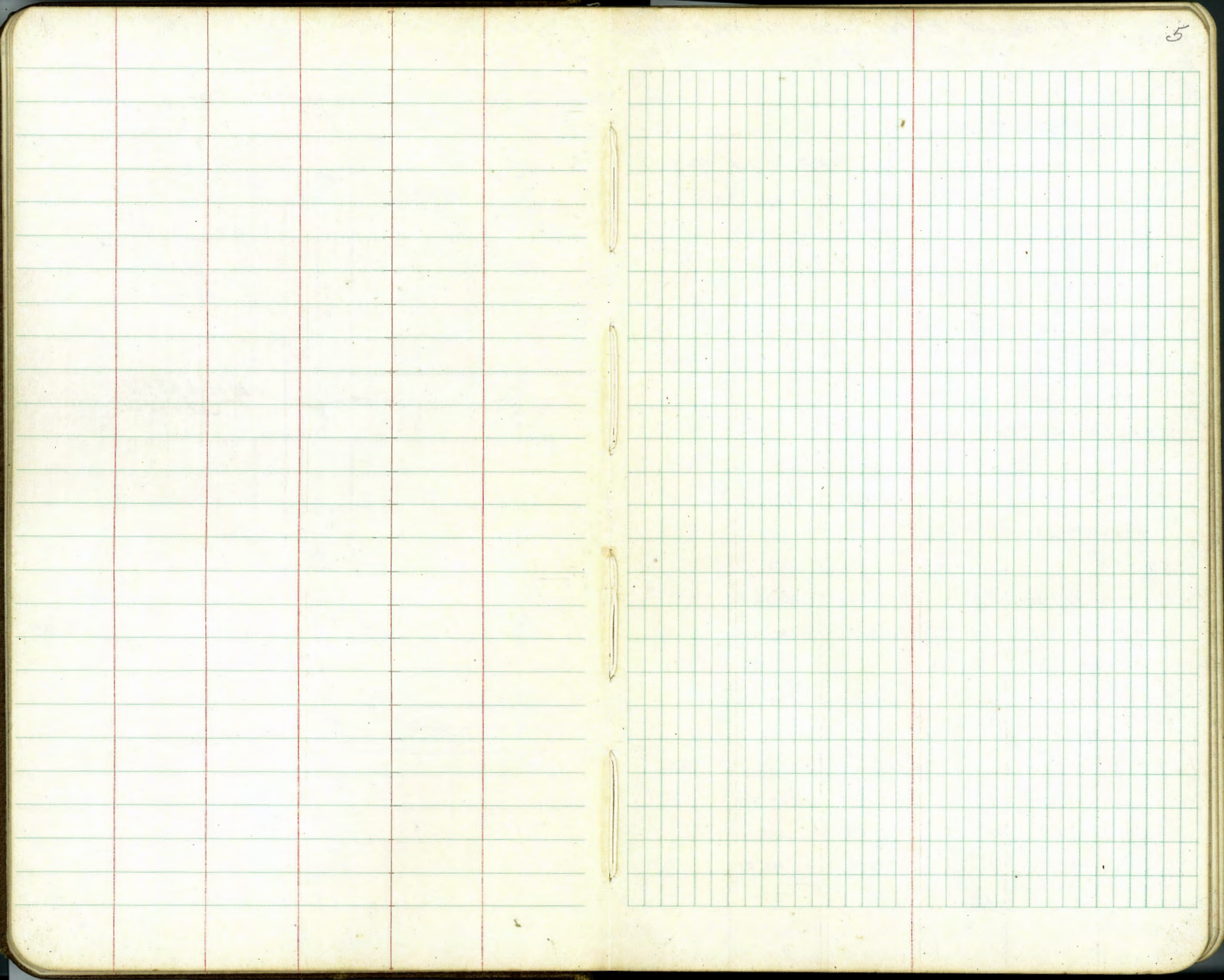




Subdivision Sht. "H" Lincoln



5398  
 232  
 5430  
 232  
 5376



Walker  
Hazard  
Begg  
1-11-05

Proposed Extension - WATER MAIN  
from 28th and Thorin  
to 7th & Laurel  
Locations FB 1674  
And Levels

Levels Cont. from FB 1674 P-1  
156.13 = from P-1 FB 1674

68+10.62 = RC-Rt	1.66	159.97
7' Rt = cb		
55' Lt = cb		
68+50	3.11	153.02
68 Rt = cb		
55 Lt = "		
(68+62) 58 Rt = cb		
60' Lt = cb. RC. 2' R		
68+75	3.24	152.19
+90 29' Rt = cb		4.3' Rt = cb
69+00	4.66	151.97
+21 = End Paving	5.46	150.67
+50	7.1	149.0
12.7' Lt = cb		
69+62.53 = E.C.	7.55	148.58
12' Lt = cb		
(69+68) 25' Rt = End 2.5' x 2.5' Concr. Box Culvert		Beginnng creek
" Top Box	8.43	147.70
" Flow	11.93	144.20
150' NE Turn Int on Sewer	6.22	149.91
Flow =		

156.13

69+83.66 = RC. Lt	8.82	147.31
70+00	9.0	147.1
+50	10.2	145.9
2.2' Lt Cobble Wall		
70+62 = Int of Cobble Wall on Wall.	10.7	145.9
	9.45	146.68
70+94 = Int. "	10.68	145.25
" Cut. Ground	11.9	144.2
71+00	12.1	144.0
T.P. 153	145.56	12.10 144.03
71+50	2.4	143.2
7.7' Lt = Cobble Wall		
71+85 N edge dirt Road	2.7	142.9
72+00	3.1	142.5
12.6' Lt = Cobble Wall		
(72+09) 6' Rt 10" Cy. Ties		
72+14 = End Cobble Wall	14.5' Lt	
+39.79 = E.C.	4.9	140.7
5.3' Rt 5' Bank Creek	5.8	139.8
" "	7' width	
" "	7.7	138.6 <sup>37.9</sup>
+51 3' Rt. Cy. Ties	12"	
(72+70) 8' Rt = Sand 8.5' wide 10' Long Bridge w/ bdy.		
+91.5 Int. Fence	5.8	139.8 <sup>300</sup>
T.P. 9.02	148.12	6.46 139.10



## Proposed Water Main

148.12

72+93		10.1	138.0
73+26		10.8	137.3
+82	E edge Stream	12.9	135.2
+89	W " "	13.2	139.9
+91		11.7	136.9
+85		10.7	137.9
+67		11.5	136.6
+77	Int. E edge N Branch <sup>crack</sup>	12.8	135.3
+88	" W " "	12.6	135.5
73+97		11.3	136.8
74+38.92	Man	10.6	137.5
+47		10.8	137.3
+51		9.6	138.5
+56	E edge Pav.	9.29	138.83
+80	W " "	8.78	139.34
+87		8.4	139.7
+90		5.0	143.1
+92	10" Oak on line		
+83	5" " 7' Lt.		
+95	6' Rt. 14" cyp.		
+98	on line 18" "		
(75+00)	7.3' Lt. 18" "		
+06	on line 14" "		
+10	9' Rt. " "		
+11	6' Lt. 3 1/4" Hyd.		
12	7.6' Lt. 12" "		

7.5 Lt.  
36" Cyp. T.

148.12

7

(75+17)	on line 14" cyp.		
(74+95)	10' Lt 8" Drain <sup>Flow</sup>	7.01	141.11 Steel Pipe
75+30		2.5	145.6
	2.7' Lt. on Top 8" Drain	2.56	145.56
(75+35)	1.5' Lt. <sup>Flow</sup>	2.16	145.96 <sup>Cobbles Stone</sup> <sup>Valley Gut.</sup>
	1.5' Lt. 12" cyp.		
(75+39)	3' Rt. 14" cyp.		
+40	12.5' Lt. 24" "		
T.P.	11.63	159.67	0.08 148.04
(75+43)	11' Lt. 14" cyp.		
75+58		10.7	149.0 <sup>5.5' Lt.</sup> <sup>14" cyp.</sup>
	6' Rt. & 3' Cob. Gut	4.2	148.5 <sup>2" cyp.</sup>
+65		8.1	151.6 <sup>on line</sup>
	7.7' Lt. 14" cyp.		
(75+75)	2.5' Lt. 10" cyp.	6.4	153.3
	3' Rt.	9.6	150.1
	8' Rt.		
75+75	E	3.4	156.3
	10' Lt.	0.2	159.5
	20' Rt. & Cob. Gut	10.4	149.3
(75+68)	13' Lt. 16" cyp.		
T.P.	11.87	171.42	0.12 159.55
(75+86)	1' Rt. 14" cyp.		
75+90	7.7' Lt. 20" cyp.		
75+90		8.8	162.6
	6' Rt.	10.5	160.9
	10' Rt.	13.2	158.7
	10' Lt.	11.8	159.6

Cont. P. 11

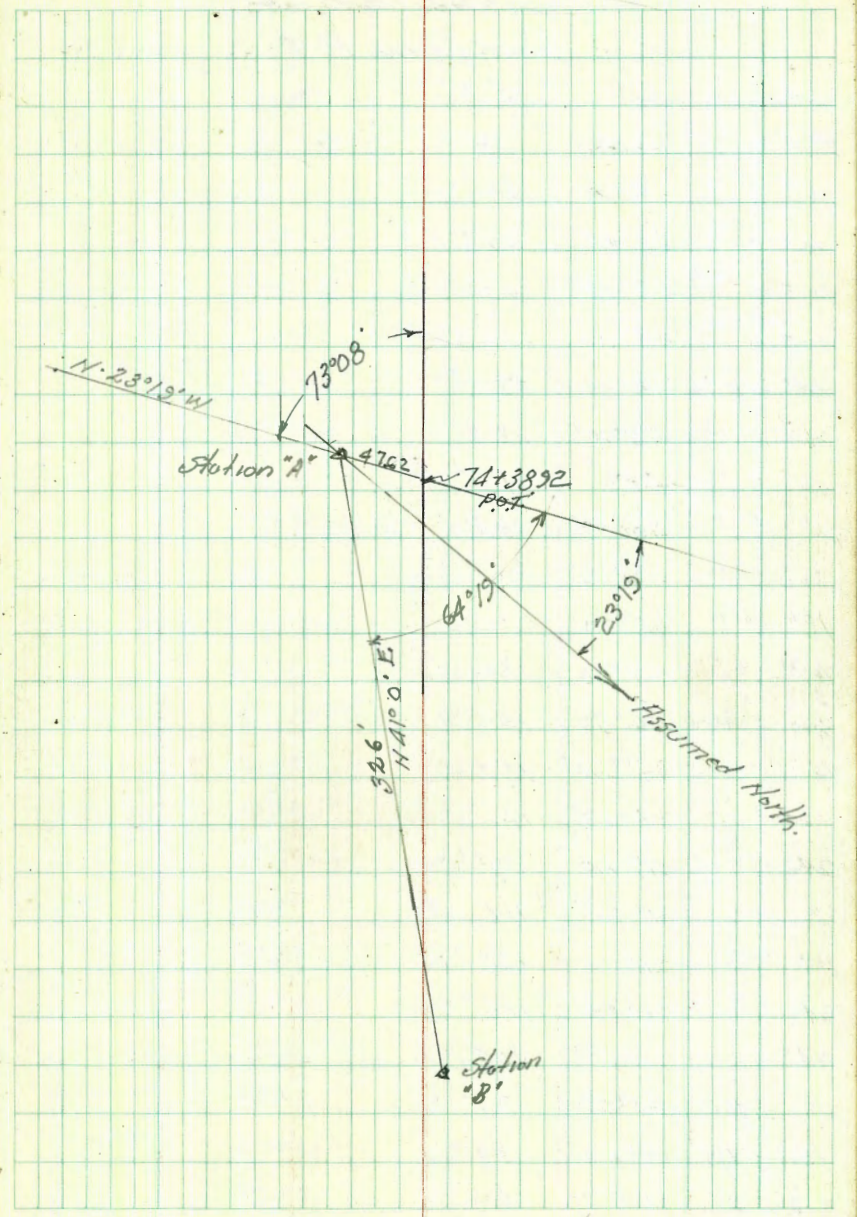
Stadia location Trees etc  
for Water Main Data Near 11th St  
Canyon.

Azimuths Clockwise from Assumed North  
Readings from Station "A"

Station	Azimuth	Stadia
18" Palm	147°36'	63'
" "	142°20'	51'
30" cyp.T.	202°10'	76'
28" " "	229°35'	68'
" " "	231°40'	69'
20" " "	208°20'	85'
" " "	215°15'	112'
28" " "	221°10'	107'
16" " "	227°05'	92'
30" " "	240°40'	46'
24" " "	265°44'	52'
16" " "	268°15'	59'
30" Data "	345°20'	34'
24" cyp.T	4°	37'
18" Syl'	334°	85'
New Sower M.H.	24°40'	58'
old Sower M.H.	23°	66'
conc. Bridge	34°30'	68'
NVI Cor	38°50'	82'
SE "	49°	79'
SW "	48°	58'

Served to Zoo from here

Cont. P. 9



READINGS from sta. "A"

Cont. from P. 8

Station	Ag.	Stadia
30" sp. T	26°30'	93'
24" " "	37°	132'
16" " "	39°45'	137'
N. End Gate to Zoo	42°18'	160'
S. End Gate to Zoo	48°30'	159'
24" cyp. T	51°30'	138'
24" " "	55°14'	123'
" " "	58°	113'
" " "	56°20'	134'
20" " "	62°12'	120'
18" " "	66°20'	111'
14" " "	67°30'	120'
S. V. Cap Zoo fence	66°30'	140'
14" cyp.	69°20'	132'
16" "	67°30'	122'
24" "	71°20'	99'
" "	71°25'	111'
12" "	71°	122'
24" "	76°30'	116'
24" "	77°37'	104'
" Syc.	50°50'	90'
20" cyp.	27°40'	58'
36" Syc.	105°10'	63'

READINGS from "A" Cont.

Station	Ag.	Stadia	
7' wide E. Stream	104°	78'	
Wedge "	32°50'	122'	8' wide
" " "	11°	90'	" "
24' wide E. Post	318°45'	107'	11th Ave Canyon
" "	300°55'	48'	25' wide
" "	196°	29'	" "
" "	162°40'	74'	" "
" "	155°25'	118'	" "

READINGS from Sta "B"

Station	Ag.	Stadia	
S. edge Rd.	217°20'	120'	
4' E. Wall	217°10'	101'	S. side Road
cob. "	216°35'	82'	" "
36" Date T	247°36'	34'	
30" Cyp.	198°10'	89'	
" "	183°50'	44'	
24" "	144°	30'	
" "	132°	46'	
Cob. wall	70°35'	44'	" "
18" E. Tree	49°30'	19'	
18" E "	47°30'	39'	
" " "	49°40'	52'	
" " "	52°30'	72'	

## READINGS from "B" Cont.

Station	Az.	Stadia	
24" E. Tree	52°30'	77'	
30" 18" E. "	54°45'	111'	
24" Cob. Wall	67°10'	57'	S. side Road.
" "	66°30'	66'	" "
16" " "	67°40'	128'	" "
N.E. 3/4	5 End		Cont.
5 E. 2.5 x 2.5'	55°40'	166'	Box Culvert
SE 1/4 N edge Road	56°50'		Send.
24" Box Culvert	56°50'	222'	at Cob. Wall. Stone Pond.
24" on E. S. side	53°12'	107'	" S. edge Creek.
" 30" cyp.	91°30'	45'	
" 36" "	76°45'	93'	
20" SE Cor House	313°47'	36'	22' wide
18" NE " "	330°15'	65'	
14" "			
14" "			
16" "			
24" "			
" "			
12" "			
24" "			
24" "			
" "			
20" "			

		171.42	Cont. from P-7	
76+00		5.1	166.3	6" Ac. (Dead) 7.3' Lt
10' Lt.		4.8	166.6	
10' Rt.		7.2	164.2	
(76+11)	2' Lt 4" Ac. Dead			
T.P.	12.60 183.70	0.32	171.10	
(76+17)	5.5' Rt. 16" Ac.			
+25	5.5' Lt 12" Ac. (Dead)			
76+27	87 - P.O.T.	7.90	175.80	Pen. stub
10' Rt.		9.0	172.7	
10' Lt.		6.5	177.2	
76+35	15' W 18" Ac. 50% Dead			
+38	8' Rt. 6" Ac. " "			
76+46	4" Ac. on line (Dead)			
T.P.	11.39 194.98	0.11	133.59	
76+50		10.9	189.1	
10' Lt.		10.0	185.0	
10' Rt.		12.0	183.0	
76+65		7.2	187.8	
+80		1.3	193.7	
T.P.	10.37 205.03	0.32	194.66	
	Stubs			
	Note: from station 75+50 to 78+25			
77+00		4.7	200.3	
10' Lt.		2.7	202.3	
10' Rt.		6.0	199.0	
T.P.	13.07 216.74	1.36	203.67	
(76+32)	6" Tree on line			

		216.74	
77+25		9.2	207.5
77+33	3/8" Meter Valve		
77+43		3.0	213.7
T.P.	10.50 227.11	0.13	216.61
77+62		10.5	216.6
(77+69)	5' Rt. 8" Ac.		
77+80	27' Rt. 8"		
77+80		5.1	222.0
10' Rt.		6.4	220.7
10' Lt.		4.7	222.4
T.P.	11.61 238.56	0.22	226.89
(78+12)	2.3' Lt. 10" Ac.		
(78+14)	5' Rt. 10" Ac.		
(78+22)	1' Rt. 6" "		
+31	9.3' Lt. 6" "		
78+17		9.3	229.2
10' Rt.		10.4	228.1
10' Lt.		8.1	230.8
(78+36)	4' Rt. 14" Ac.		
+47	24' Lt. 14" Tree		
78+47		1.8	236.7
10' Lt.		1.5	237.0
10' Rt.		3.5	235.0
78+51	15' Rt. 6" Tree		
+58	5' Rt. 6" "		
(78+62)	4' Rt. 12"		

238.50 / Proposed Motor Main Levels

(78+66)	12" Tica on line			
+70	7.7' H 14" T			
(78+82)	1' H 24"			
TP	7.18	243.98	1.70	236.80
78+85			3.1	240.9
+89	1' Rt. 7' on 10" T			
+98	0.3' H 10" "			
+93	12' H 12" "			
79+02	9' H 6" "			
"	12" 12" "			
79+67	10' = B.C. Rt.		2.4	241.6
+110	10' Rt. 16" T.			
+117	4.5' 10" "			
+123	10' Rt. 6" "			
+128	1' Rt. 6" "			
+129	10' H 6" "			
+133	11' H 18" " Ac.			
+134	12' H 16" "			
79+50			0.5	243.5
+152	2' Rt. 3" Ac.			
+154	10.5' H 16" T.			
+168	4.4' Lt. 6" "			
+185	1' Lt. 12" "			
+195	7' Lt. 5" "			
+199	9.4' Lt. 5" "			
"	10.4' Rt. 12" "			

243.98 / 12

TP	6.43	250.13	0.22	243.76
80+00			5.8	244.9
+110	3' H 5" T			
+115	8' H 18" Ac.			
+125	0.2' H 12" T			
+130	1' Lt. 18" "			
+133	3.3' Rt. 20" T.			
+140	9' Rt. 3/4" Hyd.			
+149	11" 18" T.			
+150			5.2	245.0
+153	10.3' Rt. 5" T.			
+158	11.8" 10" T.			
+162	11.8" 16" T.			
+168	8.6' Rt. 12" T			
+169	6.5' Lt. Lamp std.			
+176	10.5' Rt. 18" T.			
+185	3' Rt. 12" T.			
81+00			4.9	245.3
+109			4.9	"
+109' on Wall			2.22	247.97
+110' on Pav. Sidewalk			4.92	245.27
+150			5.00	245.19
81+87.75 = E.C.			4.91	245.28
TP	6.55	251.75	4.99	245.20

Cont. P-123

Proposed Water Main  
Levels.

251.75

82+00	6.38	295.37
+50	5.87	295.88
83+00	5.40	296.35
+50	4.90	296.85
+62.68 = 7°41' H.	4.79	296.96
+99.7 ± 1st cb. on cb.	4.34	297.91
" " Cent.	4.81	296.99
84+23	4.38	297.37
+52.78 = 5 7°41' H.	4.11	297.69
84+62.78 =	4.00	297.75 ✓
= 96+22 FB 1674 - 40		297.76
		0.01

13

Walker  
Hogurd  
8099  
1-13-45

Supplementary Topog.  
WATER LINE SURVEY - THRU 300.

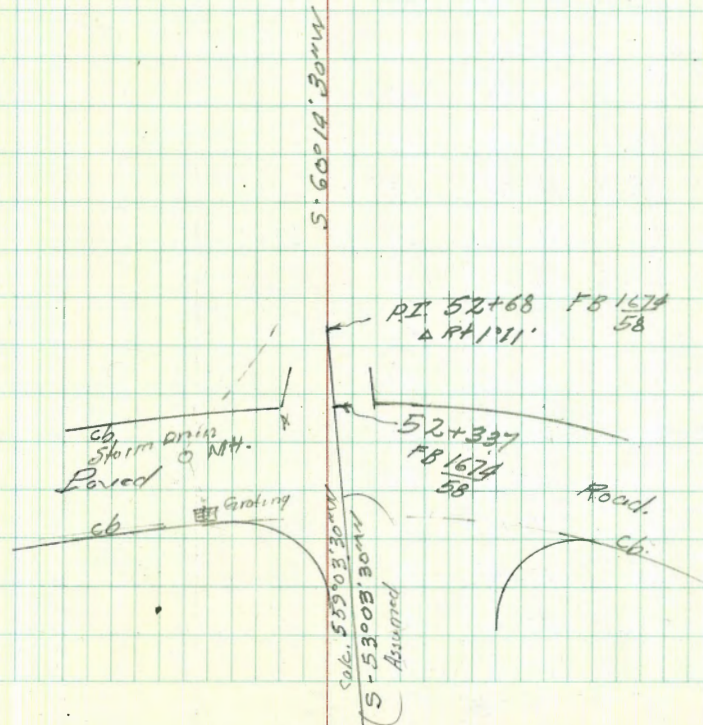
FB 1674-47

READINGS from 52+33.7 Elev 284.97

Assumed  
Az from North Clockwise

Station	Azimuth	Stadia	Vert Δ	Horizontal Dist.	Diff Elev.
Es. cb.	346°50'	166			
" "	353°05'	100'			
" "	0°28'	70			
" " Ret. " " PC	15°10'	49'			
Lump Std.	16°46'	51'			
Approv Ret. cb.	21°10'	47'			
E. C. cb. Ret.	28°25'	52'			
N side Road					
End cb.	33°50'	62'			
S side Ret.					
End cb.	57°45'	57'			
PC Ret.	59°20'	45'			
Approv Ret. cb.	64°37'	38'			
EC. cb. Ret.	75°50'	37'			
Lump Std.	77°37'	40'			
22' x 35' Grading	81°40'	36'			
E. cb. Road	101°50'	49'			
" "	122°55'	87'			
VI " "	146°30'	82'			
" " "	147°15'	49'			
PS. cb. A	148°25'	12'			
End cb. of walk.	183°30'	12'			
N side					
End cb. at walk.	280°	9'			

C-117 D-13





Readings from 52+327

Station	Bearing	Station
PJ. cb.	326°	75
W. cb. Road	329°50'	39
W " "	331°45'	79
Cocos Palm		
E 8"	325°20'	45
" "	322°	30
" " "	312°	14
Iron Sign		
E 4" Post	305°	10
E 10" Palm	162°	17
" 8" "	155°	32
E " "	152°20'	47
E 1.2 x 2' Grading		
qt cb W side Rd	146°	22
E 4" Palm	176°40'	44
E 8" "	189°45'	31
E " "	215°44'	23
E 6" "	256°45'	22
E 3" "	285°0'	30
" " "	300°	43
" " "	308°06'	56
NE. Cor		
Wire Fence	303°15'	58
W Cor		
Above fence	282°53'	80
East End cb		
qt Fence	279°12'	35
Apple in		
Above cb.	262°10'	75
W End		
Above cb.	249°30'	158
Wire Fence	171°38'	67
" "	159°23'	112

Station	Azimuth	Stadia	V Δ	Horiz.	Diff Elev
READINGS FROM station 5475					Elev 279.0
SE end					
conc. Ret. Wall	303°15'	16'			
in " " "	308°45'	21'			
(Wall curves)					
on Wall	354°50'	27'			
" "	9°45'	43'			
sharp curve					
on Wall	12°40'	64'			
" "	11°05'	76'			
End of Wall	7°25'	89'			
on Cobble					
Wall W Side Road	348°	91'			
on Cob. W	350°05'	75'			
" " "	340°30'	56'			
" " "	310°45'	50'			
" " "	301°	53'			
" " "	294°55'	57'			
" " "	278°55'	86'			
N. end					
Dunn	291°40'	97'			
30" E Tree	26°45'	59'			
24" E "	23°05'	62'			
30" " "	20°55'	64'			
18" " "	19°45'	58'			
24" " "	20°15'	52'			
8" Palm	24°25'	34'			
" "	18°15'	21'			
" "	337°40'	10'			

Top  
Wall has 3,3' Wire Fence

This is also Sand Conc. Dunn 97' <sup>Top</sup> High

READINGS from 5475 cont.

Station	As.	Stadia
8" Palm	270°45'	14'
" "	258°25'	26'
" "	255°45'	40'
" "	253°55'	57'
" "	252°35'	75'
" "	249°40'	92'
" "	246°30'	111'
" "	242°40'	129'
" "	238°35'	146'
W edge Pav. 16' Road	235°55'	150'
" " "	239°35'	134'
" " "	245°	109'
N side Road	248°30'	85'
" "	250°	62'
" "	250°50'	34'
Po. Cob. Ret. N side Road	255°25'	16'
E Cob. Ret. N edge Bluff	275°35'	12'
" "	293°05'	18'
" "	268°20'	32'
" "	257°	56'
" "	254°25'	75'
" "	253°30'	100'
" "	252°10'	122'
Cob. c6. P.S.	226°	39'
EQ.	215°55'	37'

16'  
S side Road  
8' Poth.

Readings from 54175

Station	Az.	Stadia
End 8' Path of arcade	198°40	46'
End 8' Path of Arcade	191°05	40'
PC. Cob. Ref. E' Path E side Cob. Ref.	210°55	30
" S side 16' 24"	218°05	26'
" " Road Cob. Ref.	199°45	23'
" Ref.	175°05	30'
" "	171°35	35'
" "	176°10	39'
" "	189°20	42'
" "	178°25	48'
" "	172°35	46'
W side Road	168°25	49'
" " "	160°50	94'
" "	158°20	136'
E " "	150°25	134'
" " " PC. Pav.	148°25	72'
E side Road	138°40	50'
"	108°15	37'
"	73°55	43'
"	54°25	59'
E 64' Turnstile	51°15	71'
End Pav	57°30	61'
" "	49°50	74'
Edge "	38°15	78'

W side Road

W side 8' Path  
W side of arcade  
S " 8' Path of "  
" " " "

Cob. cb.

Wire Fence S'E

" " "  
" " "  
" " "  
" " "

Angle in Pav

at Gate

N and Turnstile

Station	Azimuth	Distance
Edge Post	30°40'	86'
" "	23°45'	97'
" "	21°40'	106'
" "	24°0'	119'
" "	21°55'	125'
" "	16°05'	121'
" "	13°15'	126'
" "	9°05'	144'
" "	5°30'	169'
W edge Road	258°15'	150'
N side Road	359°25'	137'
"	357°55'	121'
"	350°40'	120'
16' wide	334°10'	132'
N "	330°10'	116'
24" E Tree	33°45'	86'
24" " "	32°55'	98'
" " "	29°20'	92'
" " "	28°35'	100'
" " "	" "	109'
28" " "	23°	98'

at wire fence

" cob. Ret.

" " "

" " 46.

## Readings from 56+11.85

Station	Bearing	Distance
W edge Pav	197°45'	28
" " "	190°25'	75
" " "	183°30'	106
" " "	182°05'	129
E " "	169°05'	128
" " "	172°30'	84
E " "	174°45'	65
Island N edge	169°05'	47
" " Island	157°15'	51
N edge Path	152°20'	44
" " "	165°45'	36
E " Pav.	167°30'	31
S " "	101°25'	20
Brown Hill	347°15'	25
" " "	239°05'	10
" " "	209°	30
" " "	205°35'	56

on curve

P.R.C. at

W Edge

Island

W E

Edge

Path

"

Top

Loc.

at Wall

"

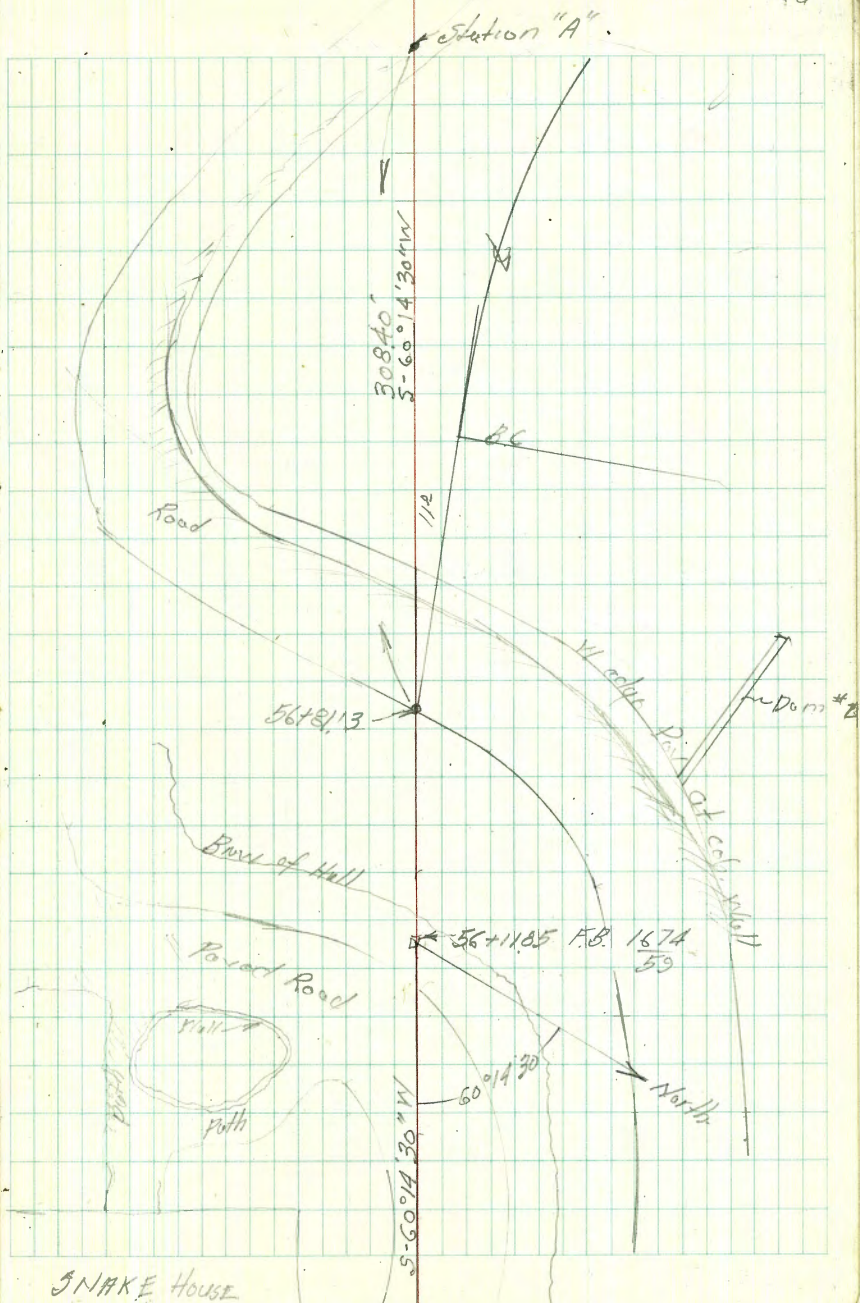
"

"

## READINGS FROM 56+81.13

NW edge Pav.	24°05'	109
" " Pav	18°45'	91
W edge "	6°25'	74
at Wall	309°25'	21
" "	236°10'	42
" "	224°	84

Cont. P-21



READINGS from 56781.13

Station	Azimuth	Stadia	
at W edge Road	223°45'	121'	
E edge	223°	171'	
W edge	214°40'	121'	
" " "	209°35'	70'	
" " "	209°35'	18'	
" " "	18°50'	18'	
" " "	21°15'	57'	
" " "	24°40'	76'	
SE End			2' wide
Dum #2	10°10'	85'	(Top)
NW			
End Dum #2	338°	160'	
L Creek	344°45'	126'	at Dum #2
" "	317°05'	71'	
6' Spillway			L Creek
Dum #3	282°20'	48'	
NW End	248°30'	133'	
Dum #4			85 ELY
" "	240°15'	132'	27' Spillway
8' E of			
End Dum #4	223°05'	133'	

## READINGS from Station "A"

Station	Az.	Stadia	
E. Edge Pav	83°20'	108'	
" " "	27°30'	46'	Approx BC. Rt
" " "	129°45'	19'	
" " "	228°25'	20'	EC.
" " "	263°30'	89'	BC. Lt.
" " "	264°56'	121'	EC.
" " "	267°30'	175'	
" " "	259°55'	188'	Branch to S.E.
North Side Road RC. Cobble Wall	274°40'	154'	N side Road
PRC. " "	273°56'	124'	" "
EC. " "	275°25'	98'	" "
BC. " "	281°	32'	" "
N side Road on curve	291°15'	15'	S. end Dum #5
Cob Wall	58°20'	12'	N side Road
" "	72°10'	33'	
EC. "			
N side Road	72°55'	50'	
" "	73°	90'	
BC. " "			
Cob Wall	72°40'	123'	
EC.	72°05'	158'	
on curve Serial Dum #4	71°	184'	
2 Creek	56°15'	132'	
" "	47°	92'	
" "	31°10'	54'	
N end Dum #5	356°55'	58'	
2. 8' Spillway Dum #5	343°50'	32'	2 Creek



Station	Azimuth	Stadia	
	300°30'	76'	
Cobb wall	Reading from 60+98.83		
cob. "	203°15'	54'	
E edge Path	207°	25'	d. Wall
" " "	81°40'	6'	" "
" " "	43°	35'	on curve " "
" " "	40°45'	56'	" " " "
SE " " "	45°30'	78'	" " " "
E.C. "	51°10'	87'	" " " "
S edge Path	66°	110'	7' N = Sand Bird Cage
Bay. Steps			Steps 7' wide
W edge Path	43°	105'	
on curve	35°20'	80'	
W edge Path	29°40'	55'	
E.C.			
W edge Path	11°55'	12'	
P.C.			
W edge Path	241°05'	14'	
E.C. " "	232°50'	40'	
NW " "	235°	68'	
" " " "	237°30'	95'	
E.C.			
N " Road	247°00'	122'	
S Side "	243°05'		
= N. Side Duck Pond		135'	
P.C.			
S side Road	231°15'	120'	= N.E. side Duck Ponds
E.C. " "			" " " "
N.E. Cor Duck Pond	225°10'	120'	
S.W. edge Road	204°50'	152'	
E side			
Abaco Road	193°40'	160'	

N 88°13' W

60+98.83

E.C. FB 1674

60

Readings from 60+98.83 Cont.

Station	Az.	Feet	
B.C.			
E edge Road	197°50'	140	
N Edge			
Parish Road	164°30'	80	
N edge Pav.	184°45'	78'	
" " "	211°25'	85	
" " "	226°15'	90'	= Int E edge Parcel Path
E edge Path	227°35'	81'	
" " "	226°15'	71'	
" " "	221°45'	53'	
" " "	208°15'	27'	Path Int. with Lab. Hall Adjacent
			Concrete Steps 7' wide
S. end			
E N x S. Axis	65°45'	122	
SW end cage			
on Curve	49°20'	108'	
W Side. Cage			
E.C.	39°20'	128'	
on E.C.			
S.E. end Cage	62°55'	177	
Wire Fence			
on Conc. Wall	37°45'	117	at W edge Conc Steps
Wire Fence	21°10'	75'	Δ in Fence - End Conc. Wall
" "	359°40'	33'	
B.C.			
Wire Fence	265°40'	23'	
Δ in "	253°20'	30'	
B.C. "	248°	82'	
" "	251°45'	109'	

Readings from 63750.89

Station Azimuth Station

Wire Fence 103°10' 114'

Δ " " 63°35' 33'

Δ " " 3°45' 21'

Δ " " 286°35' 115'

" " " 277° 222'

N-side Road EG 102°25' 66'

Δ in Road S-side 116° 51'

Δ in Road S-side 127°30' 8'

Fence Δ to Rt approx 80°

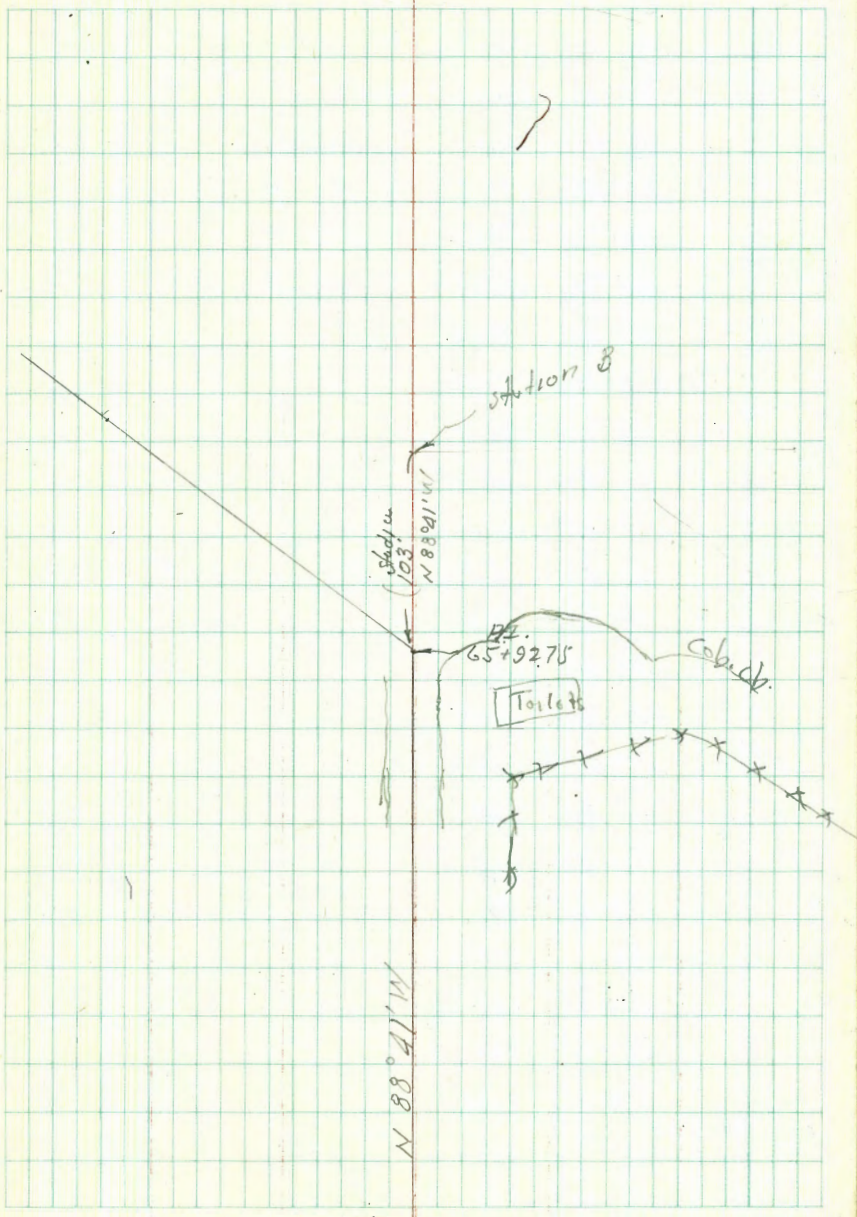
- N Side Duck Ponds

63750.89

N 88°41'W

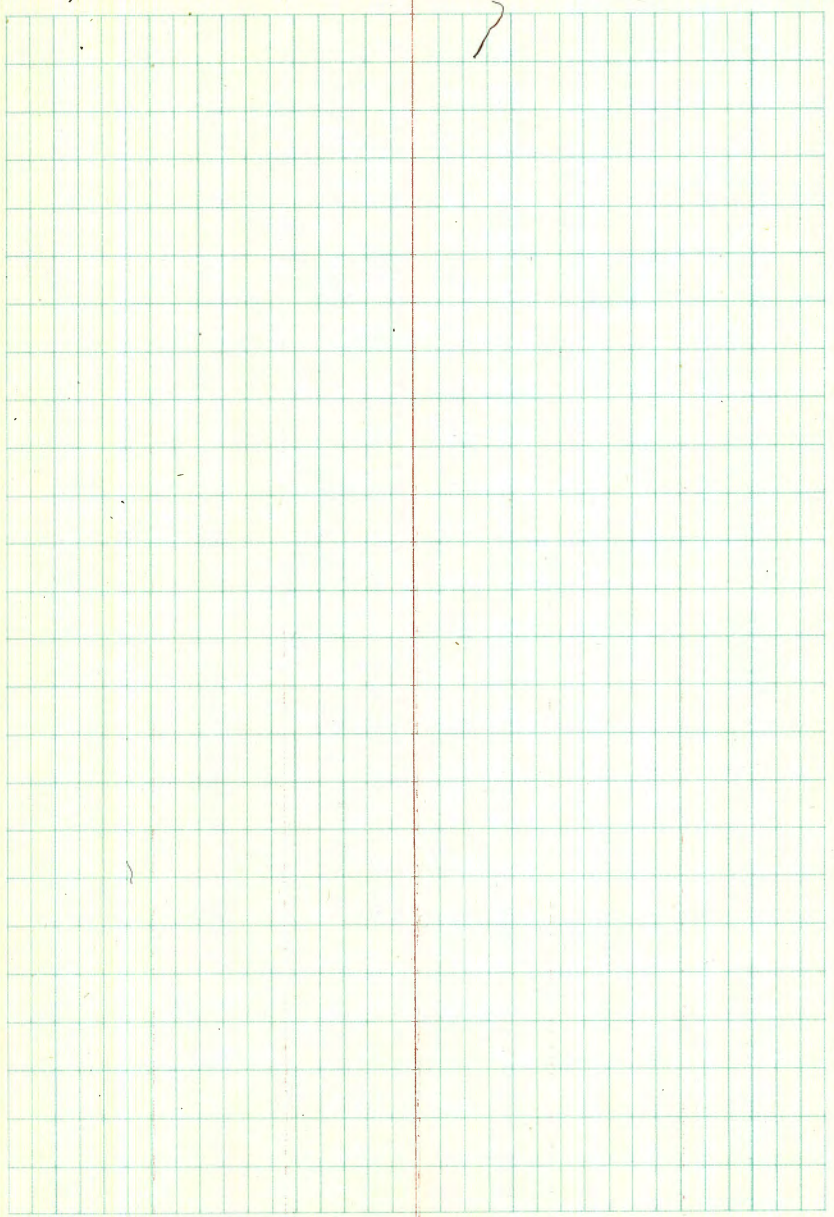
Readings from PI. 65+92.75

Station	Azimuth		
NW Cor			
5' Gate	117°40'	19'	
20" E Tree	121°40'	27.5'	
S.W. Cor			
Gate	134°	19'	at Wall - fog in Pav.
Δ in Cob Wall	207°	16'	E edge Road
Δ in V/Wall	212°	21'	
W edge			
Concr. slab.	203°30'	22'	
NE Cor			
Concr. slab.	189°50'	24'	
SE " "	195°05'	29'	
S.W. End			
Concr. slab.	206°	28'	
Δ in Wall	213°15'	27'	E side Road
	199°40'	25'	Δ Drinking Fountain
	214'	57'	E side Road
	226°45'	66°	W " " PC.
on Curve	241°25'	46'	" " "
" "	261°55'	47'	" " "
" "	268°	59'	S " "
FC	267°10'	69'	
PC			
N-side Road	42°05'	9'	
" " "	332°30'	17'	on curve
	331°50'	24'	" "
	335°20'	39'	" "
NW Cor			
Brick Toilets	345°40'	33'	
SW "	10°15'	13'	
SE "	104' across sly end		



Readings from station "B"

Station	Az.	Stadia	
Δ in cb.			1674
E side Road	65°	105'	= Point "C" 61
" " "	58°40'	114'	on Curve
" " "	55°45'	129'	" "
" " "	54°20'	176'	E.C. "
" " "	54°30'	224'	= P.C. N
W " "	50°20'	228'	} straight
" " "	46°20'	187'	
3 and Emu Pen	53°25'	50'	
Δ in Emu "	20°45'	50'	
Δ " " "	7°15'	116'	
Δ in Fence P.C. cb.	61°40'	128'	East Side Road
Alley Way	58°35'	38'	
" "	47°40'	35'	
" "	35°40'	29'	
at Cob cb.	49°50'	19'	
W side Road.	58°55'	14'	
" "	254°50'	5'	
" "	239°05'	39'	Δ in Cob. cb.
" "	233°	20'	
" "	228°15'	106'	
" "	222°25'	149'	
" "	218°15'	204'	
E side Road P.I.	219°	66'	
White Fence APPROX N			
E side Road	57°45'	214'	



41677

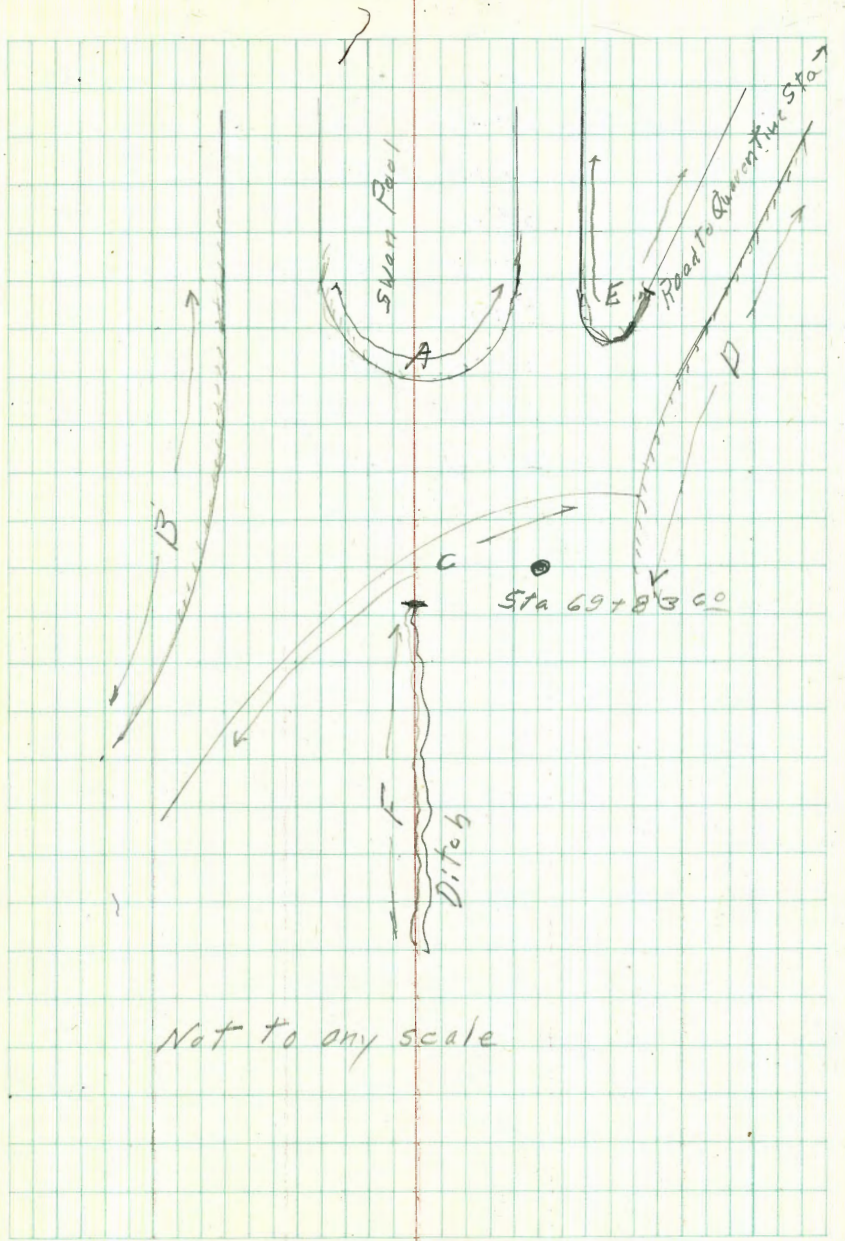
Readings from Sta 69+83.66

Station	Azi	Stadia	
Wire Fence Swm Pool (18c)	57°50'	98	A
" " " "	56°50'	88	
" " " "	50°50'	79	
" " " "	38°50'	76	
" " " "	32°10'	82	
" " " " EC	29°05'	91	B
N side Road Rubble Wall 16' Wide	22°40'	127	
" " "	20°25'	101	
" " "	14°40'	76	
" " "	3°25'	61	
" " "	341°50'	55	C
" " "	323°45'	59	
" " "	309°55'	70	
" " "	289°00'	123	
" " "	282°20'	115	
S edge Rd oil paving	326°15'	42	D
" " "	35°20'	57	
" " "	63°50'	65	
S edge Rd - dirt Rubble wall	89°55'	29	
" " " " "	70°45'	75	
" " oil " "	68°50'	92	E
" " " " "	67°30'	182	
N " " " (No wall)	63°00'	183	
N " " " Wall Begins	62°40'	159	

W side Culvert opening 3' Wide

oil paving begins

Rd 14' Wide



Station	Azi. <sup>s</sup>	St. dia	
Nedge Rd. oil Pump	61° 45'	124	} E
edge " " " "	60° 15'	123	
" " " " " "	58° 05'	140	
Sedge A Ditch	7° 15'	27	} end of drain from <sup>Swan</sup> Pool
"	274° 55'	27	
"	262° 20'	95	} F
"	254° 26'	115	
"	248° 50'	161	

A ledger page with 6 vertical red lines and 20 horizontal green lines. The lines create a grid of 5 columns and 20 rows. The columns are of varying widths, with the first column being the widest and the last being the narrowest.

A ledger page with 12 vertical green lines and 20 horizontal green lines. The lines create a grid of 11 columns and 20 rows. The columns are of varying widths, with the first column being the widest and the last being the narrowest.



Walker  
Hazard  
Hardin

PROPOSED CHANGE IN LINE.

36" WATER LINE SURVEY

2-1-45 from station 42+08.29 to station 72+39.79

FB 1674

Locals this line Pages 39

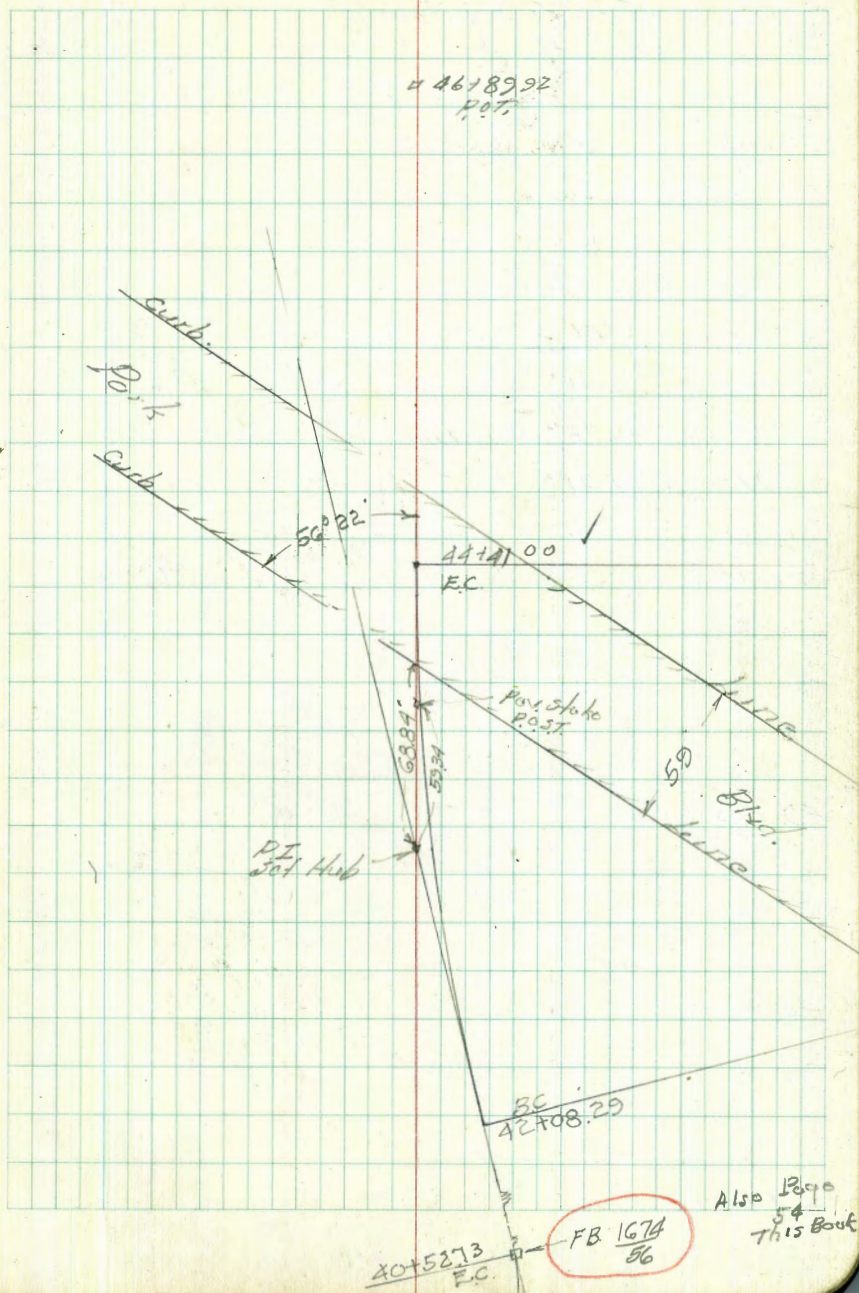
46+00

45+00

44+41.00 = E.C.

$\Delta = 13^{\circ}20'$   
 $R = 1000'$   
 $L = 232.7'$   
 $T = 116.88'$

42+08.29 = B.C. RT



52+29 5.5'lt 8" Cocos Palm  
 8.8'lt 5" " "  
 9.4'lt 1" " " 8" " "  
 +10.4 5'lt parallel to cb. 8" Cocos Palm

Mixed  
 Parallel Park

52+00

51+88.9 1st. corner

702 8'lt Two 4" Trees

51+01 6.5'lt 36" Euc. Tree

51+00

50+98 0.5'lt 16" Euc. Tree

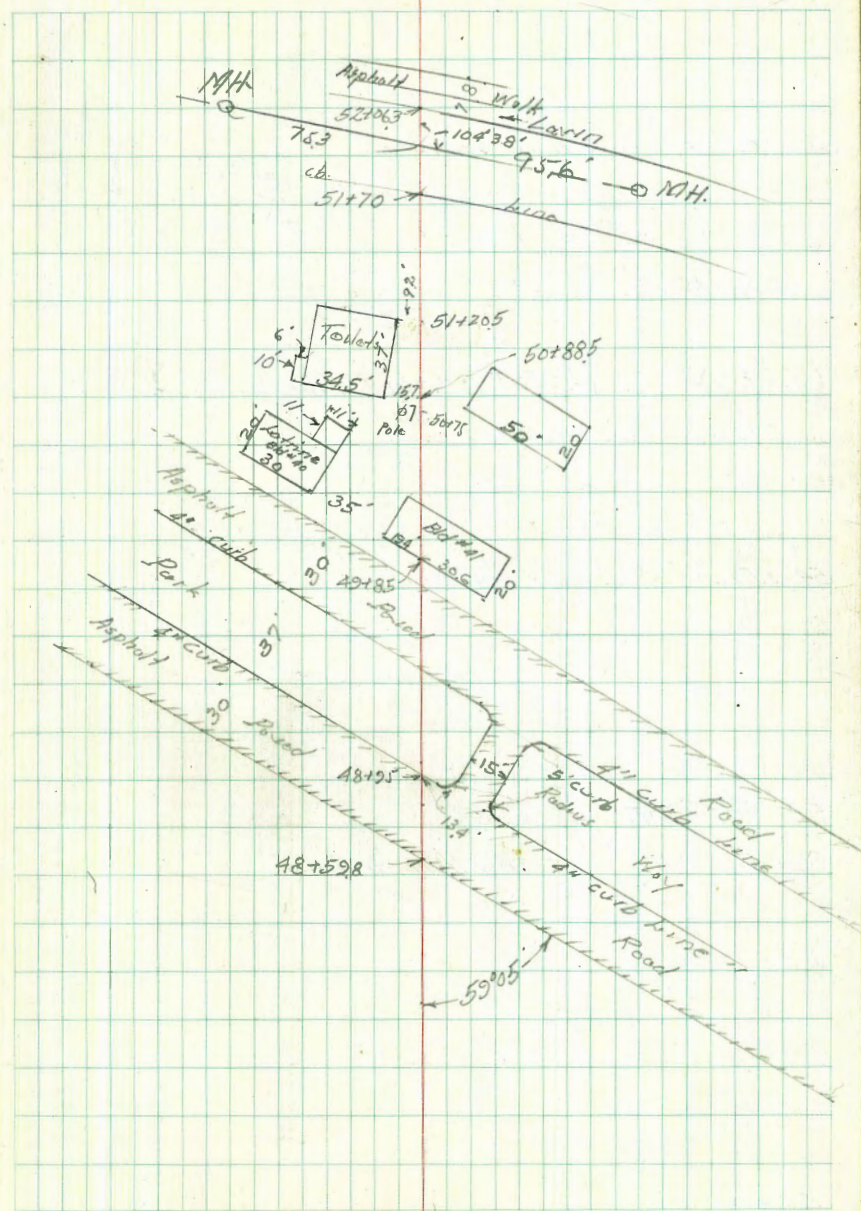
797 5'lt 28" " "

50+00

49+00

48+00

47+00



56+35.01 = EG. Set Nail in Pav.

$\Delta = 29^{\circ}50'$   
 $R = 90'$   
 $T = 23.98'$   
 $L = 16.86'$

P.I. set " " "

55+88.15 = B.C. Lt. " " " "

(55+31.7) 6.7' R.L. = End 10" Steel Pipe Culvert

55+24.2 = Int. West Face Drip  
Cone.

54+51.71 = P.O.T. Set Pine Stub.

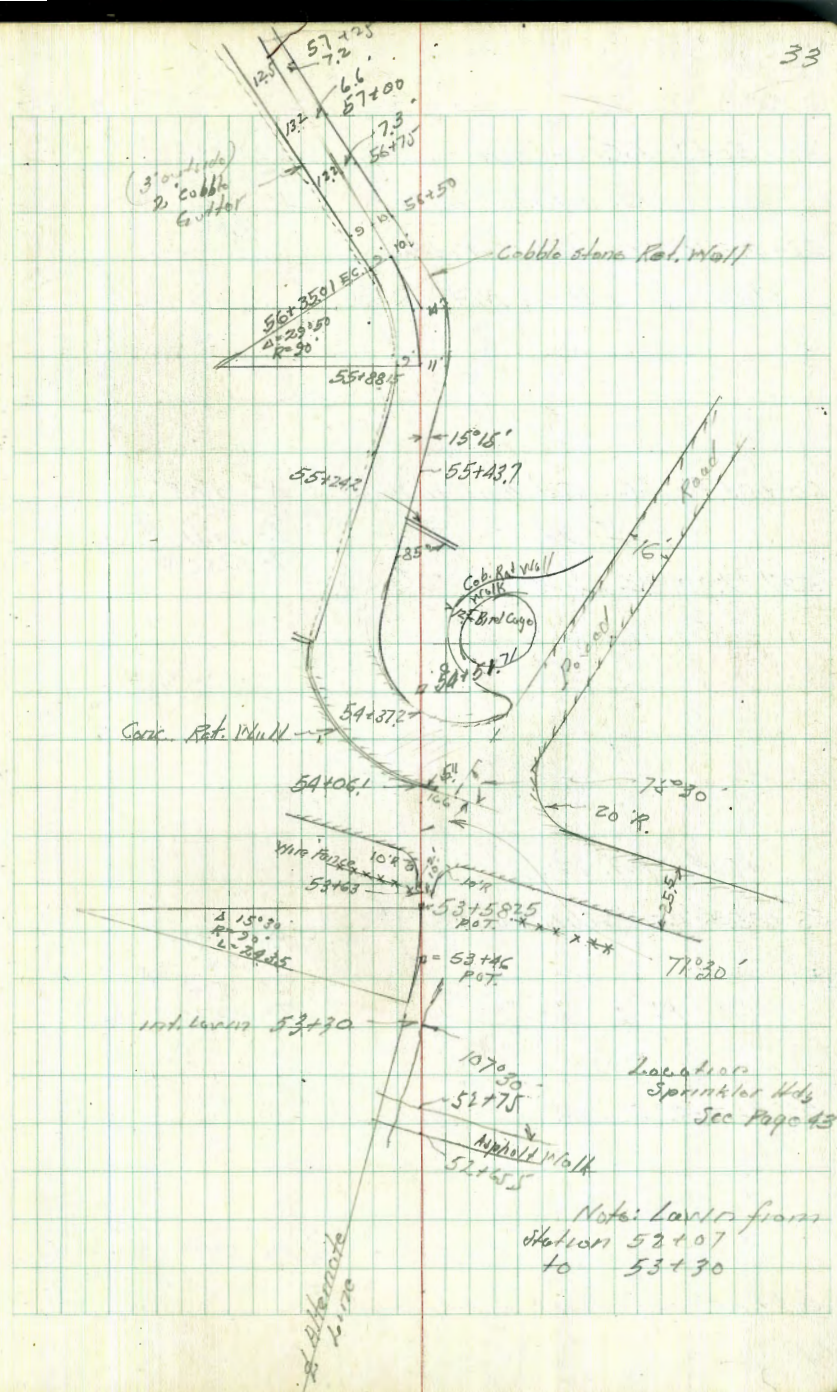
53+58.25 = P.O.T.

53+46 = P.O.T. = P.I. on Alternate Line

53+00

52+65.5 = Int. E. edge Asphalt Walk.

52+00



61+50.57 = E.C. Set Hub.

$\Delta = 17^{\circ}29'$

P.I. Set Hub in Pav

$R = 90'$

$L = 27.46'$

$T = 13.83'$

61+23.11 = B.C. Set Hub in Pav

(61+27.5) 13' 4" = 2' MH

60+05.41 = E.C. Set Hub in Pav

$\Delta = 18^{\circ}05'$

$R = 90'$

P.I. Set " " "

$L = 28.41'$

$T = 14.32'$

59+77.00 = B.C. Pt " " "

+52.46 = Int. Center

58+35.36 = E.C. Set Hub in Pav

$\Delta = 46^{\circ}30'$

$R = 90'$

$L = 73.04'$

$T = 38.76'$

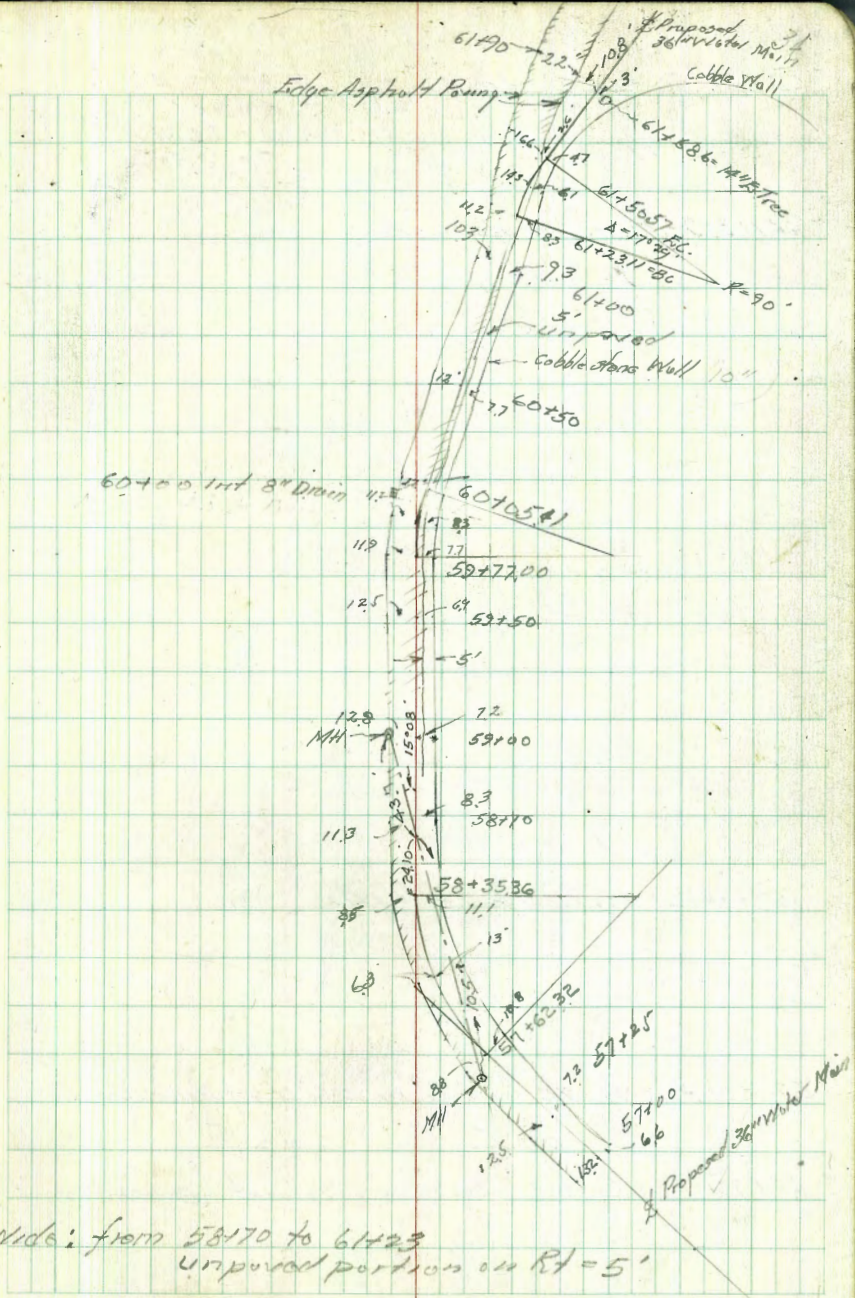
P.I. " " " "

38.67

57+62.32 = B.C. Pt " " "

Unimproved Portion  
from 57+15 to 58+170 on Rt. from 4 to 5'

57+15 Find Full width Pav



64+30.50 = E.C. Set Nail in Pav.

$\Delta = 17^{\circ}04'$   
 $R = 90'$   
 $L = 26.81'$   
 $T = 13.50'$

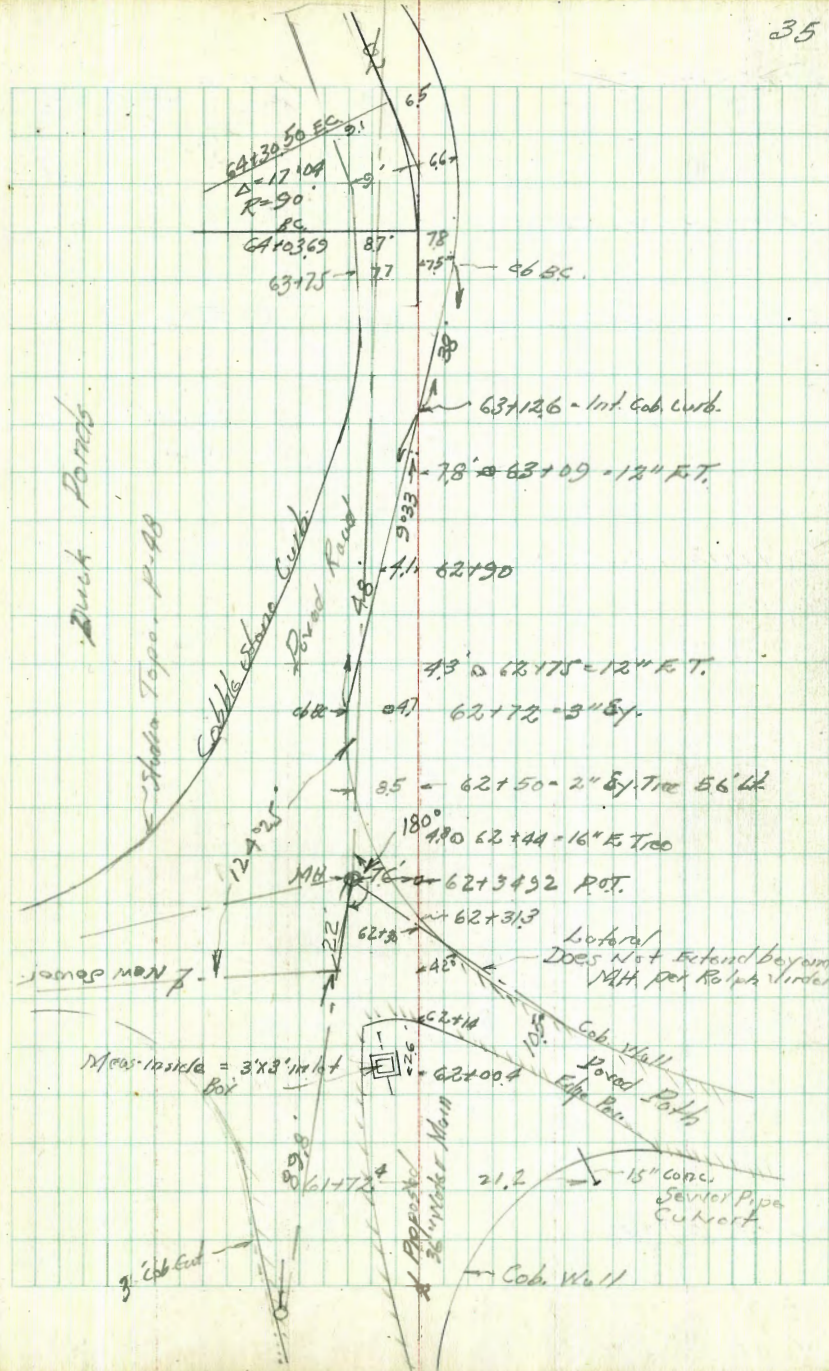
P.T. Set Nail in Pav.

64+03.69 = P.C. Lt. Set Nail in Pav.

62+34.92 = P.O.T. 7.6' Lt = 12" H

62+00.4 = opp NE Cor Inlet Box 2.6' Lt = outside Cor. Box

(61+72) 21.2' Lt = 15" Conc. Culvert (sewer Pipe)



67+98.24 = E.C.

$\Delta = 9^{\circ}24'$   
 $R = 90'$   
 $L = 14.77'$   
 $T = 740'$

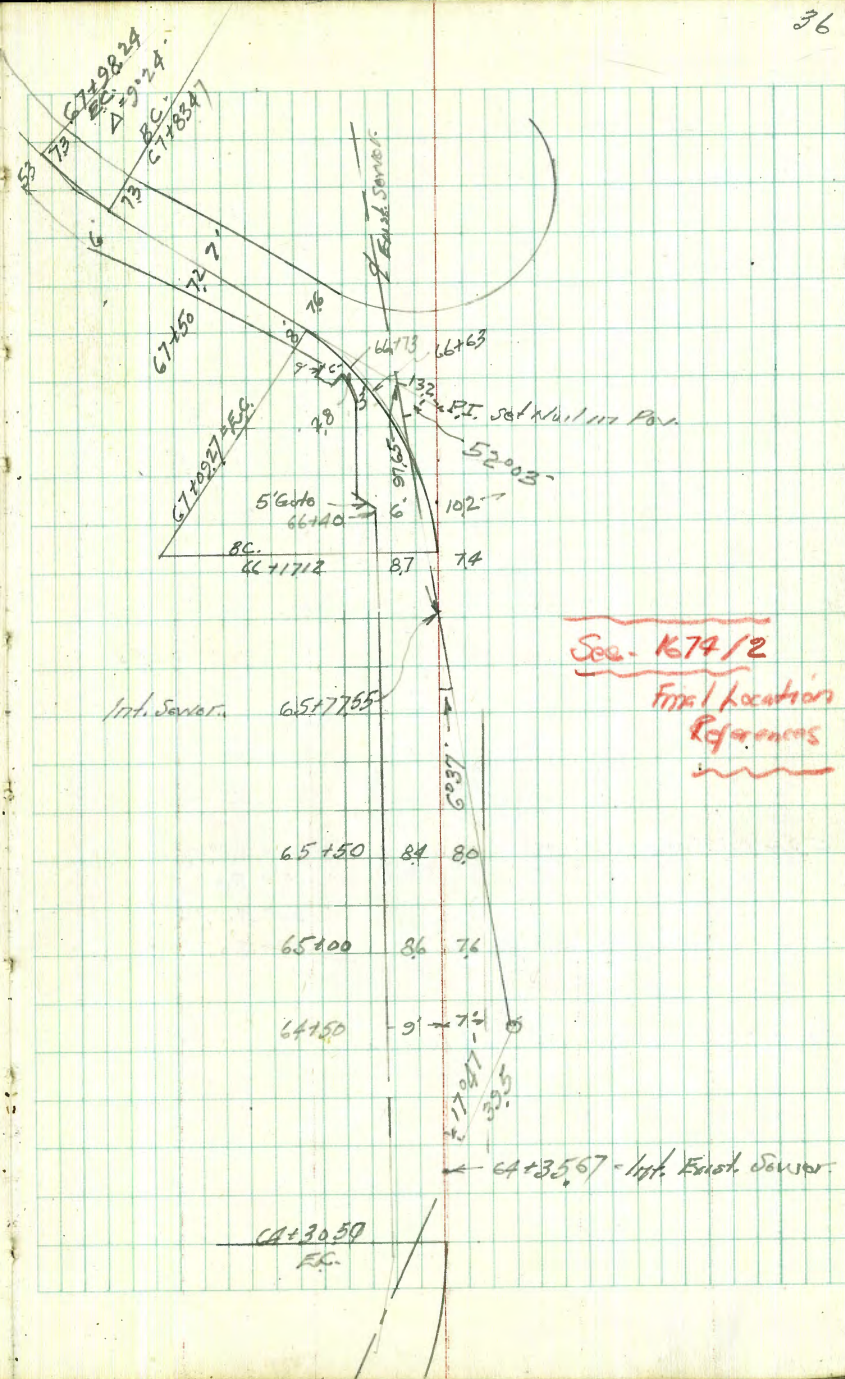
67+83.47 = B.C. RL

67+09.27 = E.C. Set Nail in Pav.

$\Delta = 58^{\circ}40'$   
 $R = 90'$   
 $L = 32.15'$   
 $T = 50.57'$   
 $Ext. = 13.24'$

66+17.12 = B.C. Set Nail in Pav.

50  
67+30.57 = E.C.



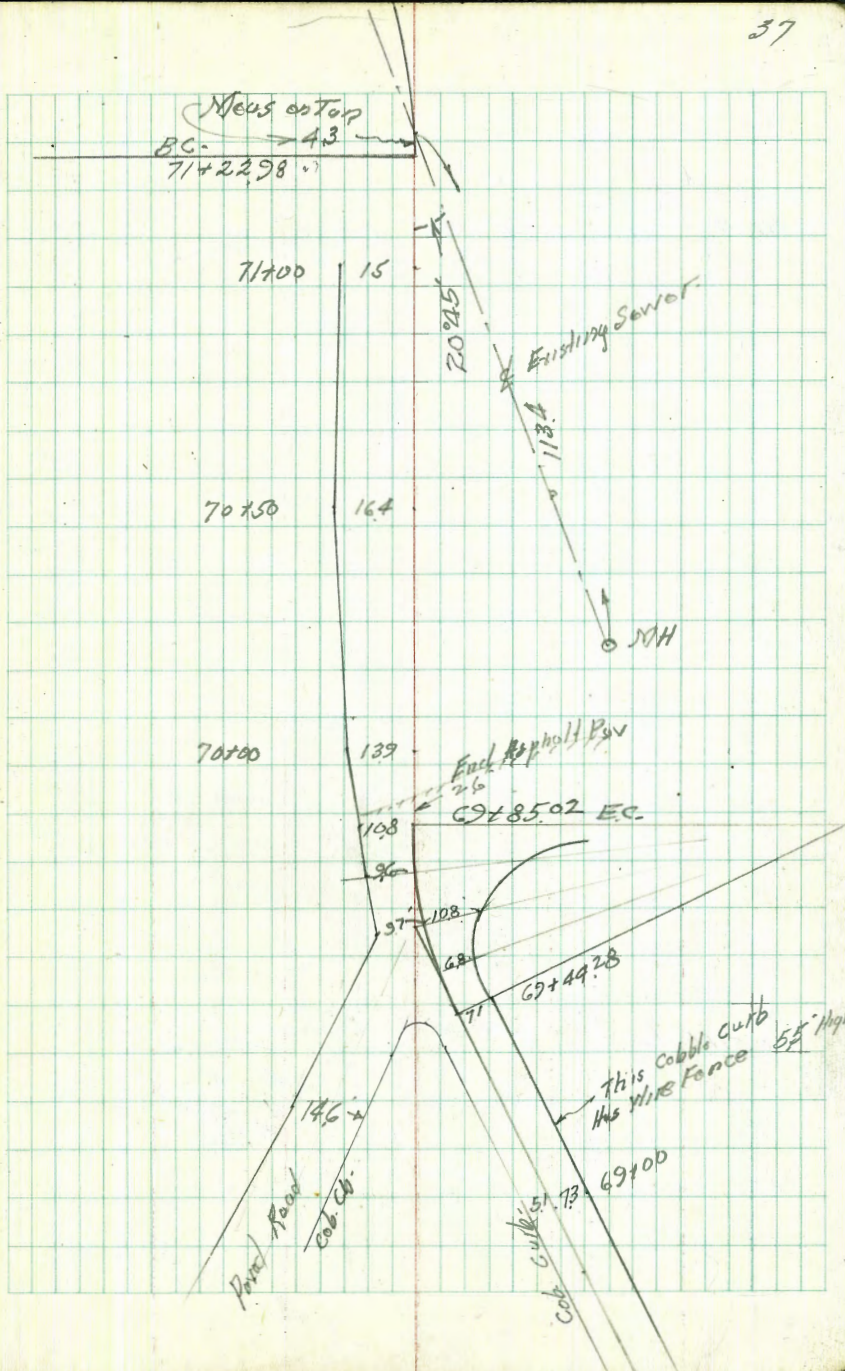
71+22.98 = B.C. Lt.

69+85.02 = E.C. Set Nail in Pav.

P.L. Set Nail in Pav.

$\Delta = 25.56^\circ$   
 $R = 90'$   
 $L = 40.74'$   
 $T = 20.72'$

69+44.28 = B.C. Set Nail in Pav.

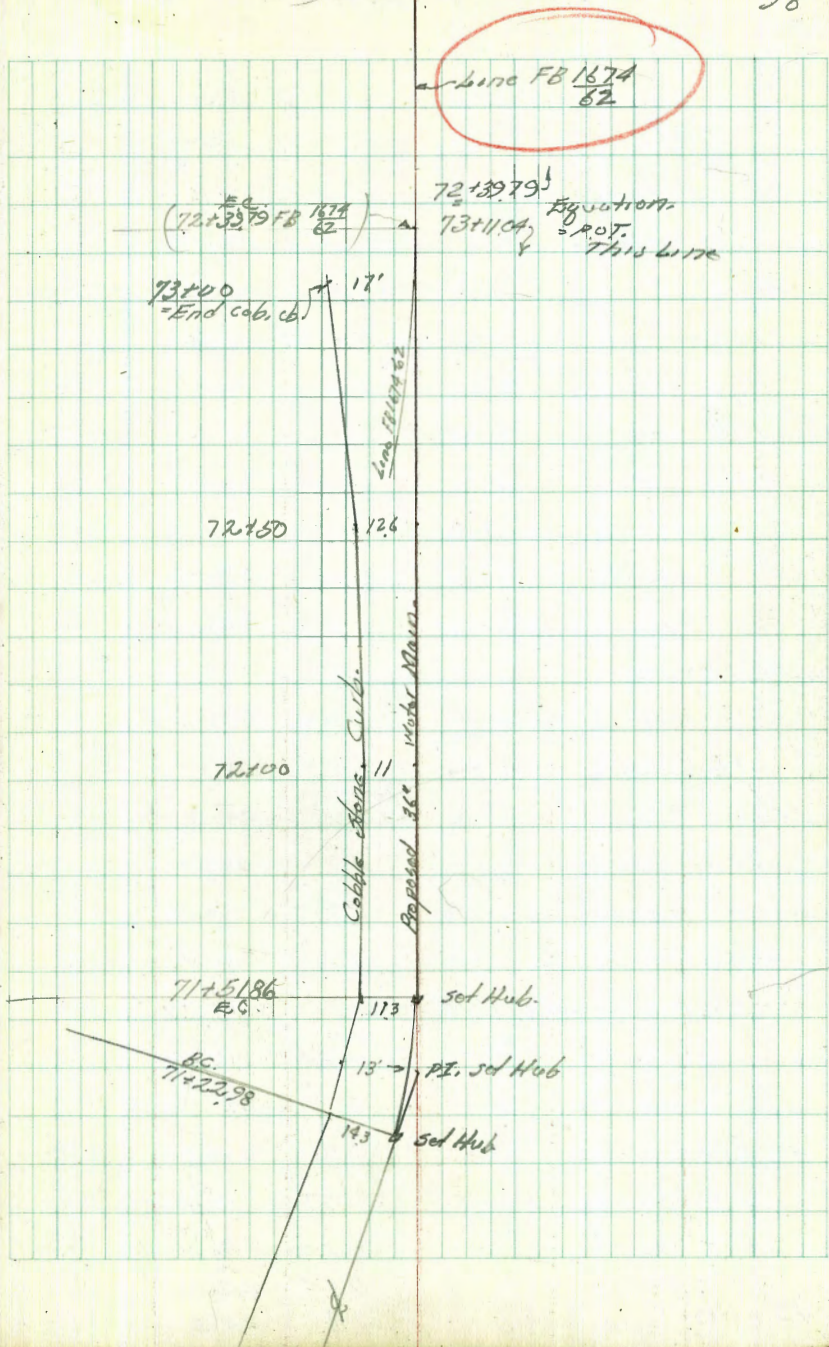


72+3979 Equation  
 73+1164 = P.O.T. This Line Nail

71+5186 = E.C.

$\Delta = 18^{\circ} 23'$   
 $R = 96'$   
 $L = 2888'$   
 $T = 1456'$

71+2298 = B.C.



Line FB 1674  
 62

72+3979 Equation  
 73+1164 = P.O.T. This Line

73+1164  
 End cob. curb

72+50 126

72+100 11

71+5186 E.C. 113 set Hub.

B.C. 71+2298 13' pt. set Hub

143 set Hub



Walker  
Hogart  
Hogart  
2-6-45

Sarals for Proposed Line Change

36" Water thru Zoo

Location Pages 31-38

	1.06	289.12	288.06	811-1017 44-3925 FR1174-44
42+08.29 - BC. Rd on Hub	12.32		276.80	
+50	11.1		278.0	
43+00	9.6		279.5	
+50	7.0		282.1	
+67	5.8		283.3	
+80	1.1		288.0	
E. cb. Park Blvd	1.15		287.97	
Gut. on Porling	1.72		287.90	
Approx 2' Part Blvd	0.92		288.20	
44+11.00 - EC.	0.92		"	
W. Gut. No cb.	1.99		287.63	
TP 12.06 300.93	0.25		288.87	
45+00	11.51		289.9	
+50	8.2		292.7	
46+00	6.2		292.7	
+50	4.6		296.3	
+82.92 - POT. Hub	4.66		296.27	
47+00	4.6		296.3	
+50	5.2		295.7	
48+00	6.2		294.7	
+59.8 - E edge Pav.	7.75		293.18	
+95 Gut	8.22		292.71	
" on cb	7.64		293.29	
49+00	8.4		292.5	

30093

39

49+30	8.5		292.9
49+38.13 on cb	8.94		291.99
" " Gut	9.42		291.51
49+78.10 = W edge Porling	9.58		291.37
+85 on Burruck's Blvd	10.2		290.7
TP 0.30 291.36	9.87		291.06
50+12 = W side Burruck Blvd	1.1		290.3
+75	3.3		288.1
+90	4.0		287.9
51+00	5.2		286.2
+50	6.5		289.9
+70 E cb. (Roadway)	6.89		284.47
" Gut. on Pav.	7.27		289.09
+88 ± 2 Road	7.01		289.26
52+06.3 W Gut	7.36		289.00
" " cb	7.03		289.33
+134 = E edge Side Walk	7.75		283.61
21.5 W " " "	7.76		283.60
+65.5 on E " " "	8.71		282.65
+75 W " " "	8.89		282.97
53+00	9.6		281.8
746 - POT. - PE alternate	10.55		280.81
+58.75 - POT. - EC.	10.69		280.72
	10.74		280.62
TP 0.53 280.98	10.91		280.45
53+63 = E edge Appholt Pav.	0.41		280.57
54+00 on " "	0.96		280.02

		280.98		
54+05	at Well on Pav.	119	279.79	
+06.1	on "	0.61	280.37	
+06.1	on Pav. Branch Road	2.38	278.60	
+37.2	" " " "	5.29	275.69	
"	" cb.	4.71	276.27	
+51.7	-POT. Sub.	3.40	277.58	✓
+61		5.3	275.7	
+72		10.5	270.5	
+85		12.7	268.3	
T.P.	0.16	268.37	12.77	268.21
55+24.2	on Duff	3.76	269.61	
"	" Ground	6.9	261.5	
(55+31.7)	7' Rt. <sup>End</sup> 10" curb cut	12.9	255.5	
55+42		7.2	261.2	
+43.7	on cb. Cobble	5.48	262.89	
"	" Pav.	6.29	262.08	
+75		8.55	259.82	
+88.25	=B.C.W.	2.96	258.91	
56+11.68	Curve	12.73	255.69	
T.P.	0.42	256.06	12.73	255.64
56+35.01	=E.C.	3.18	252.88	
+75		8.97	247.09	
57+00		12.50	243.56	
T.P.	0.39	243.57	12.88	243.18
+25		3.66	239.91	

		243.57		
57+62.32	=B.C.	8.87	234.70	
T.P.	0.48	230.99	13.01	230.56
+93.84	=Curve	0.96	230.03	
58+35.36	=E.C.	4.90	226.09	
+59.46	on Pav. (with drain)	7.40	223.60	
+70		8.66	222.33	
59+00		11.95	219.08	
T.P.	1.14	219.41	12.72	218.27
47	on Run M.H.	1.33	218.08	
"	" Flow "	5.68	213.73	
59+50		6.11	213.20	
+77.40	=B.C.	2.10	210.22	
60+05.41	=E.C.	12.12	207.39	
T.P.	0.99	207.40	12.96	206.45
(60+10)	13' H on Grading	0.20	207.29	
"	" " Flow	2.20	205.29	
60+23.7		2.11	205.33	
158	on Flow outlet <sup>8" drain</sup>	5.59	201.85	
60+50		4.94	202.50	
61+00		10.76	196.68	
T.P.	0.59	195.05	12.98	194.46
61+23.11	=B.C.	1.72	193.83	
(61+27)	on Run M.H. <sup>13' LK</sup>	3.11	191.94	
"	" Flow "	8.32	186.73	
+37	on Pav.	3.17	191.88	
742	Edge Pav.	3.69	191.36	

	195.05		✓
61+50.57 = FC. on Hub	5.00	190.05	2.6 Lt N 2490 660
+90	26	185.9	
(61+77.5) 21,2' ft on Flow 15" dia	2.92	185.13	
62+00.9	10.2	189.8	
2.6' Lt. Grating	11.20	183.8	
on Flow inlet	16.50	178.55	
T.P.	3.24	186.70	12.29
62+14 on E. edge Parung.	2.71	183.99	
62+31.3 on Gut. of Cob. Cb.	3.78	182.92	
" " Cb.	3.07	183.63	
62+34.92 P.O.T. stake	2.27	183.73	
7.6' Lt. on Run MH	4.49	182.21	
" Flow	8.79	177.91	
+44	0.5	186.65	
+50	2.2	186.5	
+44	4.2	182.5	
+77	11	185.6	
2' Lt.	5.2	181.5	
+87	2.9	183.8	
+93	5.9	180.8	
63+12.6 on Cb.	6.25	180.95	
" " Pav.	7.19	179.51	
63+50 " "	7.91	178.79	
64+03.69 B.C.	9.30	177.90	
64+30.50	10.27	176.93	

	196.70		✓
T.P.	0.59	177.86	943 177.27
64+50		1.90	175.96
64+91		3.59	174.27
65+00		4.15	173.71
+50		7.32	170.53
+66		8.35	169.51
65+77.55 on Pav. (Int. Sewer)		9.18	168.68
66+17.12 = B.C.		12.45	165.91
T.P.	1.07	166.32	12.51 165.25
66+40		2.70	163.62
+63 3' Lt. = Cb.		4.57	161.75
+68 1.5' Lt. = Cb.			
+73 2.8 " "			
+86		4.41	159.71
67+09.27 = EC.		7.53	158.79
+50		8.61	157.71
+83.47 = B.C. ft.		9.38	156.92
+98.24 = EC.		9.77	156.55
T.P.	1.47	157.83	10.16 156.16
68+50		2.58	155.25
69+00		4.21	153.62
+44.78 = B.C. ft.		5.53	152.30
+64.65		6.10	151.73
+85.02 = E.C.		6.89	150.92
+87.6 = Edge Pav.		7.08	150.75
70+00		7.9	149.9

157.83

70+50		9.8	148.0
+80		10.9	147.9
5' #		11.6	146.2
7' Rt. S edge	6' Creek	15.5	142.3
71+00		11.3	146.5
(70+94)	8.6' #, 18" E Tree		
T.P.	11.5	148.31	10.67 147.16
71+2298	B.G.	2.06	146.25
+29	3' Rt. 18" K Tree		
	12' R 30" E "		
	17' Rt. S edge 5' creek		
71+49	4' Rt. 16" E Tree		
71+57.86	= E.C. on Hwy	2.17	145.69
+63	5' # = 18" E Tree		
	15' Rt S edge 5' creek		
71+82.28	P.O.T.	2.86	142.85
	6' Rt 19" E Tree		
72+00		4.3	149.0
+08	7.5' Rt 16" E Tree		
+50		5.7	142.6
73+00		7.2	141.1
73+11.04	Equation	7.5	140.8
= 72+39.79	P-6		

10' Rt.  
S' Edge 4' h.

42

148.31

T.P.	5.24	148.64	0.91	147.40
chk.	67+62.53	P-6	4.02	148.62 ✓
				148.58
				0.04 Error

## Location Sprinkler Hds.

from Proposed 3.36" Water Line P-33

52+12 5.5' Rt. Sprinkler Hd.

115 7.2' Lt. " "

119 10' Rt. " "

124 3' Lt. " "

135 6' Rt. " "

138 7.4' Lt. " "

153 8.8' Lt. " "

160 5.3' Rt. " "

173 10.6' Rt. " "

186 4' Lt. " "

188 1.9' Rt. " "

53+00 5.7' Rt. " "

" 7.6' Lt. " "

111 8' Rt. " "

113 4.2' Lt. " "

125 10.8' Lt. " "

127 0.5' Lt. " "

138 13' Rt. " "

140 3.6' Rt. " "

153 7.5' Rt. " "

## Location Sprinkler Hds.

from Alternate Line P46

52+65 2.4' Rt. Sprinkler Hd.

168 7' Rt. " "

180 6.5' Rt. " "

53+08 5' Rt. " "



Walker  
Hoyan  
Hurdin  
2-6-45  
Stations

Alternate Location  
for Proposed 36" Water Main  
from station 46+22.97 to 53+81.4

48+50 6°10.9  
Levels - P-50

48+00 4°44.9

47+50 3°18.2

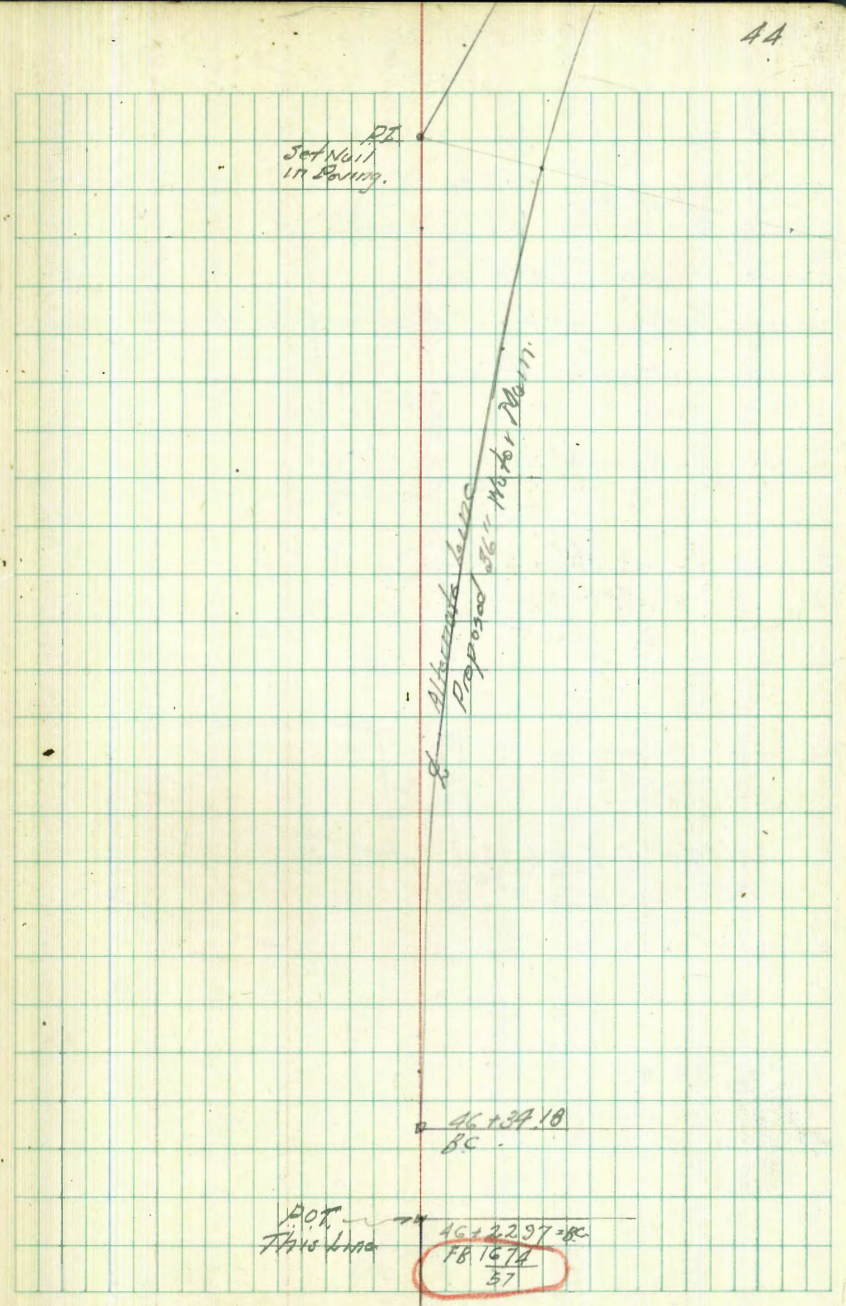
47+00 1°52.9

46+50 0°26.9

46+34.8 BC Pt. set Hub

46+22.97 - P.O.T. Fd Hub

$\Delta = 285030'$   
 $R = 1000'$   
 $L = 50338'$   
 $T = 257.4'$



P.O.T. Fd Hub  
46+22.97 - RC  
FB 1674  
57

Alternate Line  
Cont. from p-44

Stations

51+50 1.3' Rt 5" Tree  
 51+37.56 = E.C. 0.3' Lt 3" E Tree  
 51+24.5 6' Rt = 30" E Tree  
 51+07 3' Rt = 10" E Tree 5' Rt 10" 7' Rt 12" E Trees  
 51+00 13' 20.9

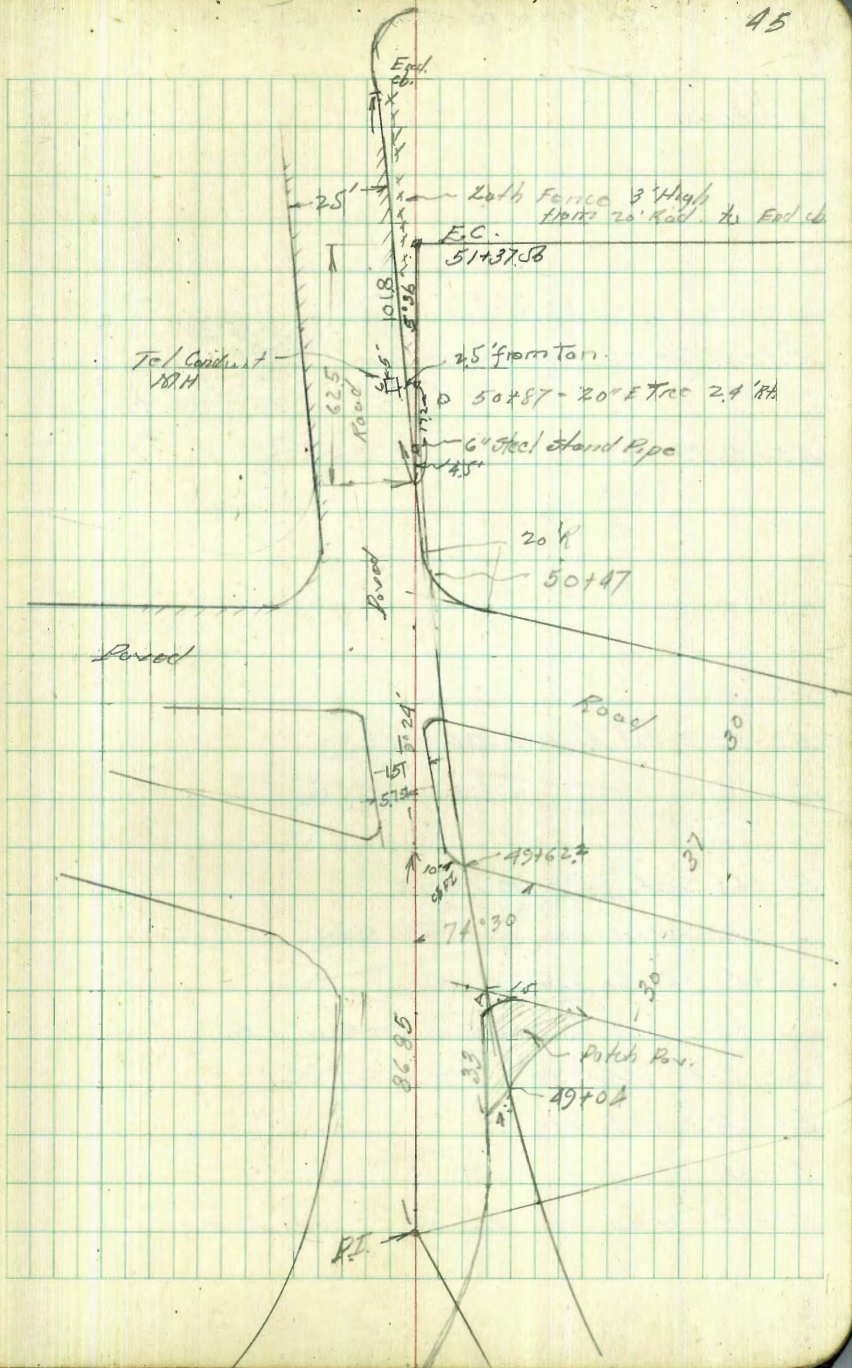
50+50 11° 54.9

50+00 10° 28.9

+71 = 8" Tel Pole 0.2' Lt = N side  
 +62.2 = Int. 4" curb

49+50 9° 02.9

49+00 7° 36.9



Stations

53+58.25 = P-33

53+81.17 = E.C. - End Alternate Line

$\Delta = 15^\circ 30'$   
 $R = 90'$   
 $L = 29.38$   
 $T = 12.25$

53+56.79 = B.C.

52+92.3 - Int Asphalt Side Walk

52+60 - Int 6.5' Wire Fence

+48 - West edge walk

52+40 - Edge Asphalt Walk

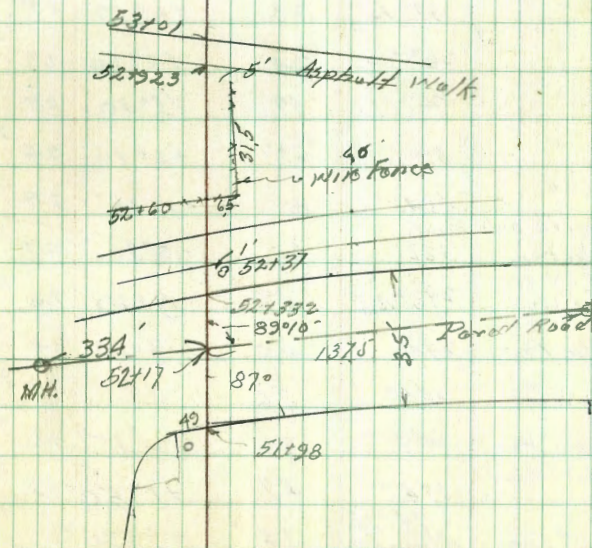
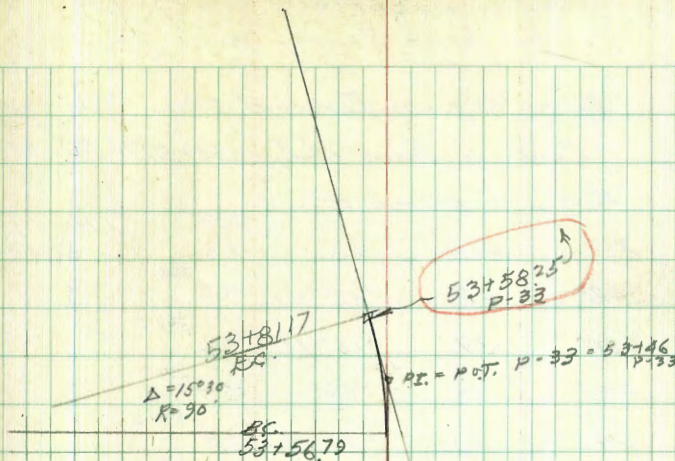
+37 8" Lucas Plumosa 15" High 1' Rt.

52+33.2 = Int Walk

52+17 = Int Jarvis

51+98

51+95 Lamp Stk. 2.5' H. - N edge Base





Walker  
Hazard  
Hazard  
2-7-45

Stadia Location Topography  
Water Level Survey thru Zoo

Azimuths from Forward Zn. Clockwise

Readings from Station 541517 E1 = 277.58

Horiz Δ to nearest 15'

Station	Az	Stadia	VΔ	Diff Elev.	Horiz. Dist.
Roadway 30 N. Cb.	322°	46'	-12°10'	9.5	268.1
" "	332°	37'	-13°10'	8.2	269.9
" "	211°	20'	-18°	5.9	271.7
" "	246°	10'	-21°50'	3.9	274.2
" "	171°15'	17'	-2°30'	0.7	276.9
" "	148°15'	25'	+3°30'	1.1	278.7
on wall Ground Bird Cg	22°	31'	15°	2.7	280.3
on Wall "	61°30'	22'	+6°50'	2.6	280.7
" "	37°15'	23'	+6°10'	2.9	280.0
" "	26°30'	24'	+4°20'	1.8	279.9
" "	26°45'	49'	+3°10'	2.7	280.3
" "	30°	69'	+2°10'	2.6	280.2
" "	35°45'	81'	+1°40'	2.9	280.0
South side Edge Pav.	322°	60'	-10°30'	10.7	266.9
SWLY Cr Rot. Wall	293°45'	47'	-9°40'	7.8	269.8
" "	270°	40'	-9°10'	6.3	271.3
" "	241°	36'	-7°	4.9	273.2
" "	207°	39'	-2°15'	1.5	276.1
End Wall	174°	47'	+1°50'	1.5	276.1
12" Cocos Plumosa	74°15'	14'	+9°30'	2.3	275.3

Ground outside  
3.5' below

5.6' below

5.3 "

4.3 "

Edge Pav

48

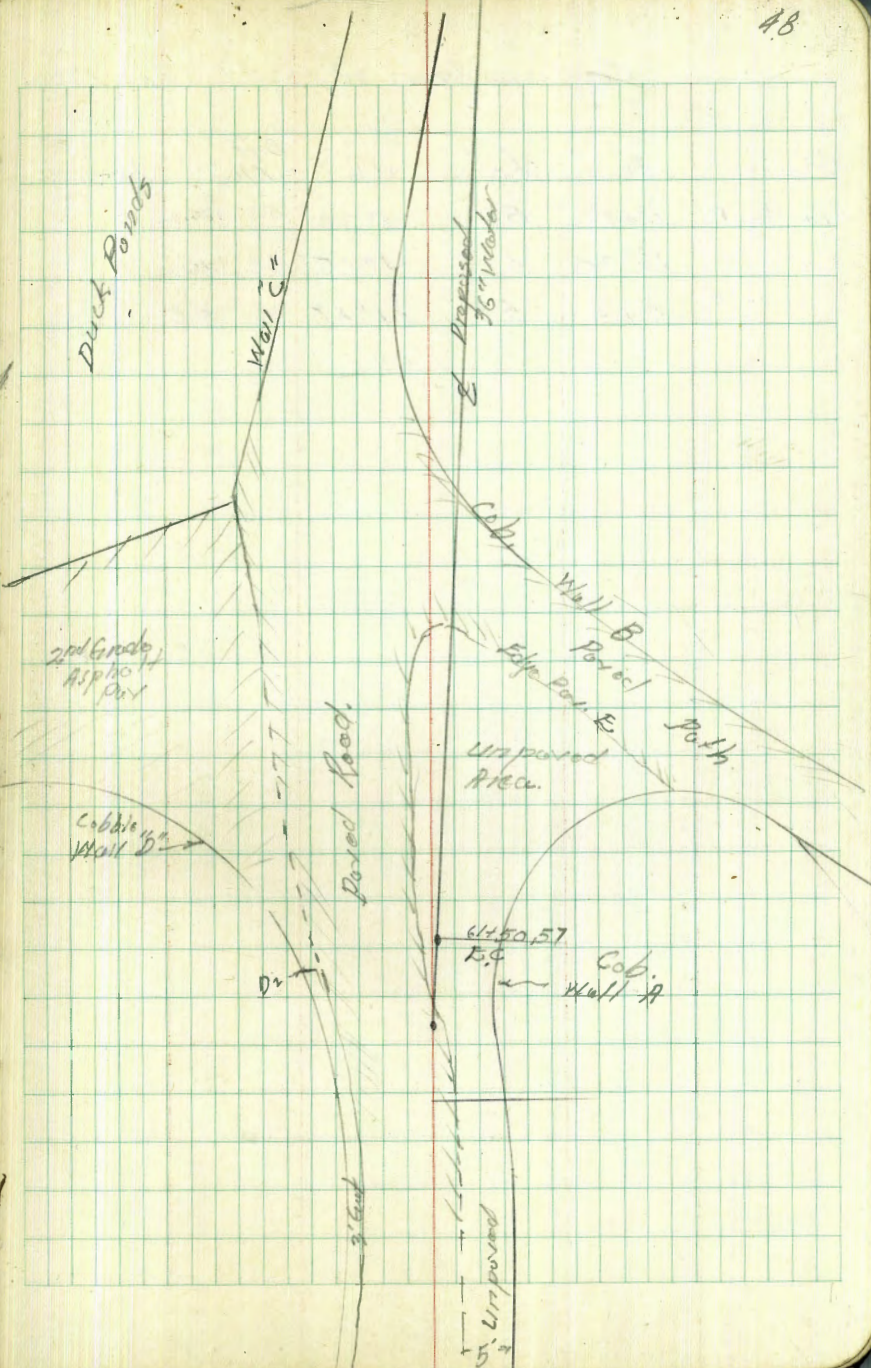
Stadia Readings - p. 39

From 61+50.57 = E.C. = Elev = 190.05

Ag. from Forward Turn Clockwise

Station	Ag.	Stadia	VA	Diff Elev	Horiz. dist.
Wall "A"	156°	45'	+9°10'	7.1	197.1
Wall A	150°30'	12'	+13°15'	2.7	192.7
" "	19°30'	14'	+0°25'	0.1	190.2
" "	34°	33'	+0°15'	0.1	190.2
" "	60°	54'	+2°50'	2.7	192.8
" "	74°	72'	+5°40'	7.1	197.2
Wall "B"	63°30'	72'	+4°20'	5.9	195.4
" "	44°30'	61'	+0°30'	0.5	190.6
" "	19°30'	64'	-3°10'	3.5	186.6
" "	2°15'	78'	-4°30'	6.1	189.0
Wall "C"	347°15'	116'	-3°50'	7.7	182.2
" "	342°15'	96'	-4°10'	7.0	183.0
" "	337°	86'	-4°15'	6.4	183.6
" "	319°30'	84'	-1°30'	6.6	183.4
" "	292°45'	92'	-4°05'	6.5	183.6
Wall D	288°15'	74'	-3°10'	2.1	186.0
" "	295°30'	61'	-3°50'	2.1	186.0
" " " "	302°	40'	-4°45'	3.3	186.8
South Edge Pav.	201°	30'	+6°25'	3.3	193.4
Edge Pav. E	163°	51'	+7°30'	6.6	196.6
" "	270°	26'	0°	0	190.0
" "	335°	23'	-8°10'	3.2	186.8
" "	351°	58'	-6°20'	6.4	183.6

Cont. p. 49



Readings from 6115057 Elev 190.05

Station	Az.	Stadia	V.A	Diff. Elev	Horiz.
Edge Pav. E	1°45'	53	-5°20'	5.8	189.2
" " "	19°30'	52	-4°15'	3.8	186.2
" " "	57°	53	+1°55'	1.8	191.8

at Walk #4

Walker Levels - Alternate Line  
 Hazard proposed 36" Water Main  
 Hardin

1-7-45 Resolution P-40

Station	192	298.19	22627	↓ 877. on slab 4618292 P 39
46+22.97 = POT.		4.18	299.01	
+34.18 = B.C. RT.		3.60	299.59	
+50		3.1	295.1	
47+00		1.2	296.3	
+50		2.0	296.2	
48+00		2.6	295.6	
+50		3.5	299.7	
49+00		5.0	293.2	
+04 on Pav.		5.16	292.03	
+50 " "		6.62	291.57	
+62.2 " " at cb.		6.86	291.33	
" on cb		6.30	291.89	
49+63		6.6	291.6	
50+00		7.7	290.3	
+05 on cb		7.90	290.29	
" Gut.		8.49	289.75	
50+47 Edge Box		8.76	289.93	
T.P.	181	289.88	10.12	288.07
51+00		2.1	287.8	
+37.56 = E.C. on Hub		3.74	286.19	
+50		4.5	285.9	
+98 on cb		5.32	284.56	
" Gut. Porosity		5.77	284.11	

289.88

50

52+17	5.50	289.38
137.5 Rte on MH	5.68	289.20
" " " Floor	12.32	277.58
52+32.2 K. Ch. Gut.	5.85	289.03
" on "	5.47	289.94
+40 on Asphalt West	5.99	283.89
+48 " " "	6.00	283.88
+60	6.5	288.9
+92.3 " " "	7.32	282.56
53+01 " " "	7.46	282.42
+53.79 = B.C. LK	8.95	280.93
+81.17 = E.C.	9.18	280.70
		280.72
		0.02
44+53+46.0 P-33	9.25	280.83
		280.81
		0.02
chk cb 51+17 - P-39	5.40	284.48
		284.47
		0.01

Walker  
Hazard  
Hudson  
3-5-45

PROPOSED CHANGE<sup>IN</sup> ALIGNMENT  
of Preliminary Survey 36" Water Main  
Across Balboa Park  
For original location see FB 1674-6  
Profile boards P-55

Stations

20+42.1° = E.S. ✓

20+00

+50

19+00

+75 = P.I.

+50

18+00

+50

17+04.67 = E.S. ✓

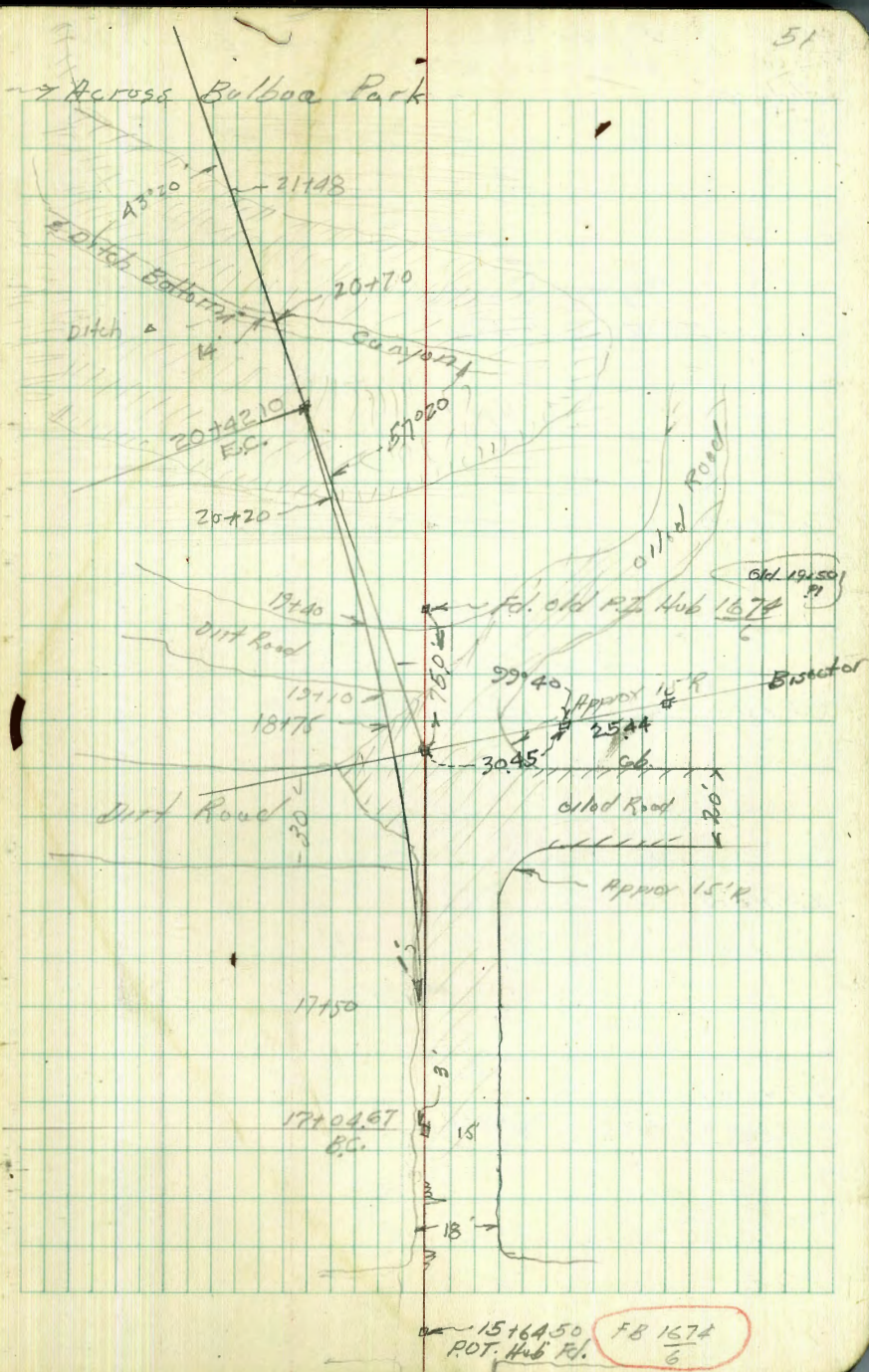
$$\Delta = 129.20$$

$$R = 1000$$

$$T = 170.33 \checkmark$$

$$L = 337.42 \checkmark$$

$$Ext. = 14.40$$



Proposed Change in Line 36" Water  
Main Across Solboa Park  
Cont. from P-51

Stations

27+00

26+50

26+00 - POT Set Hub

25+00

24+00

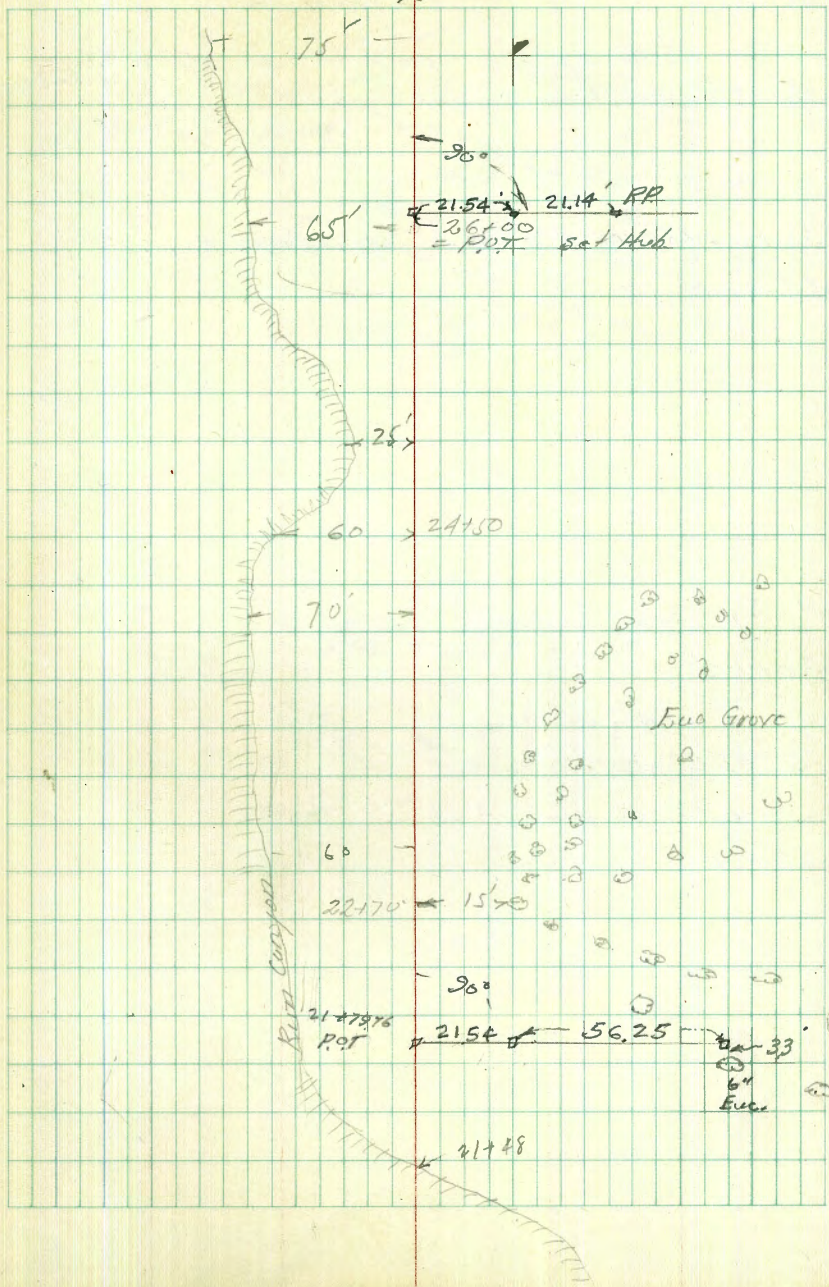
23+00

22+00

+7276 = POT

21+00

52



Proposed Change in line  
of 36" Water Main  
Cont. from p. 52

(10H. 27 Lt.) Rings & Cover to be set by  
Sewer Dept.  
32+82.5 - Int. Abandoned Trunk Sewer

32+04.38 = POT of Powder Canyon Lined Road

32+00

31+00

+15 = POT. Set Hub

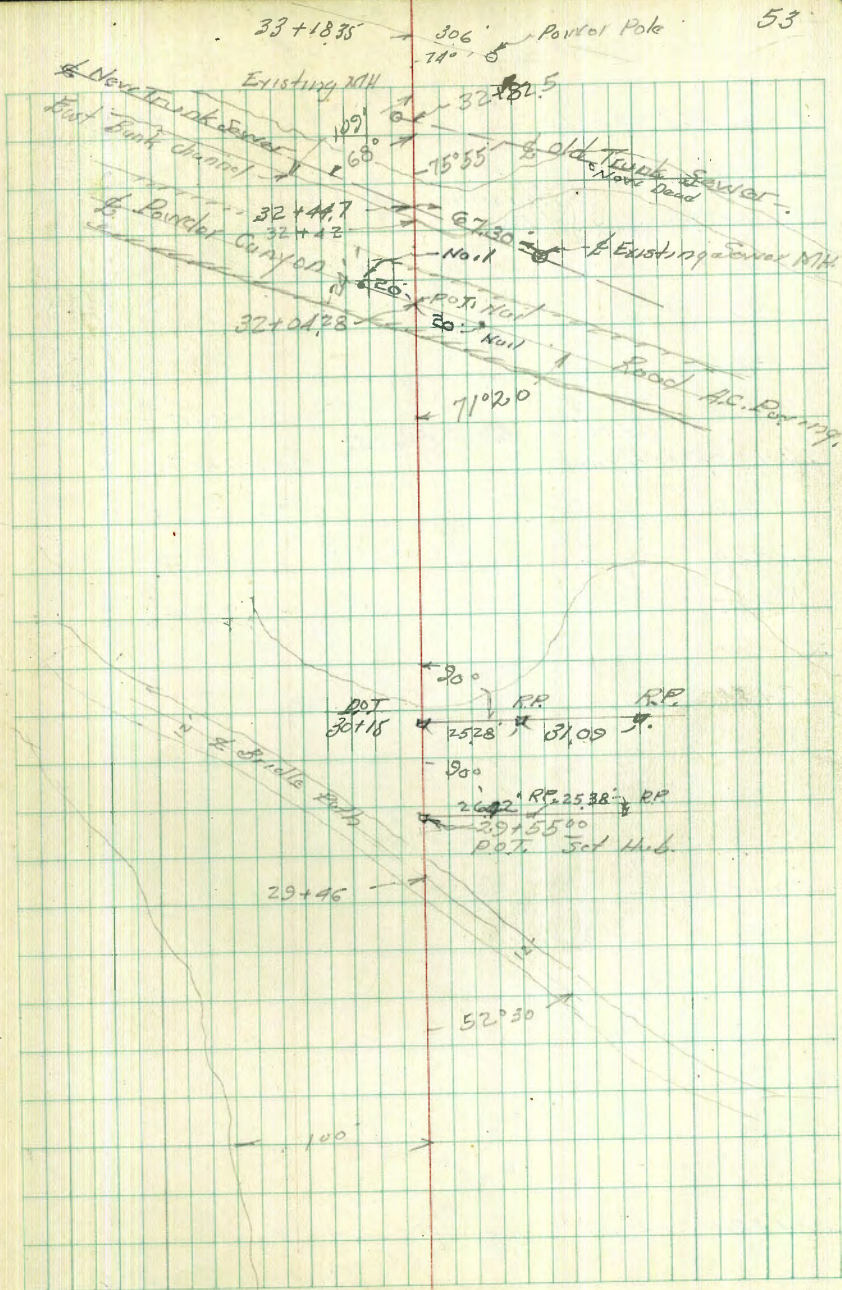
30+00

29+55.00 = POT. Set Hub

+45 = E. 12' Biville Path

29+00

28+00



38+64.67 = B.C. Lt

FB 1674  
56

FB 1674  
56

38+63.79 Ahead

Equation  
B.C.

38+12.56 Back

38+00

+75

+50

37+25

Set POC on Bisector To P.I.

$\Delta = 17^\circ 41'$

36+96.82 = ctr. curve

$R = 750'$

+75

$T = 116.66'$

+50

$L = 231.47'$

+25

$Ect. = 204'$

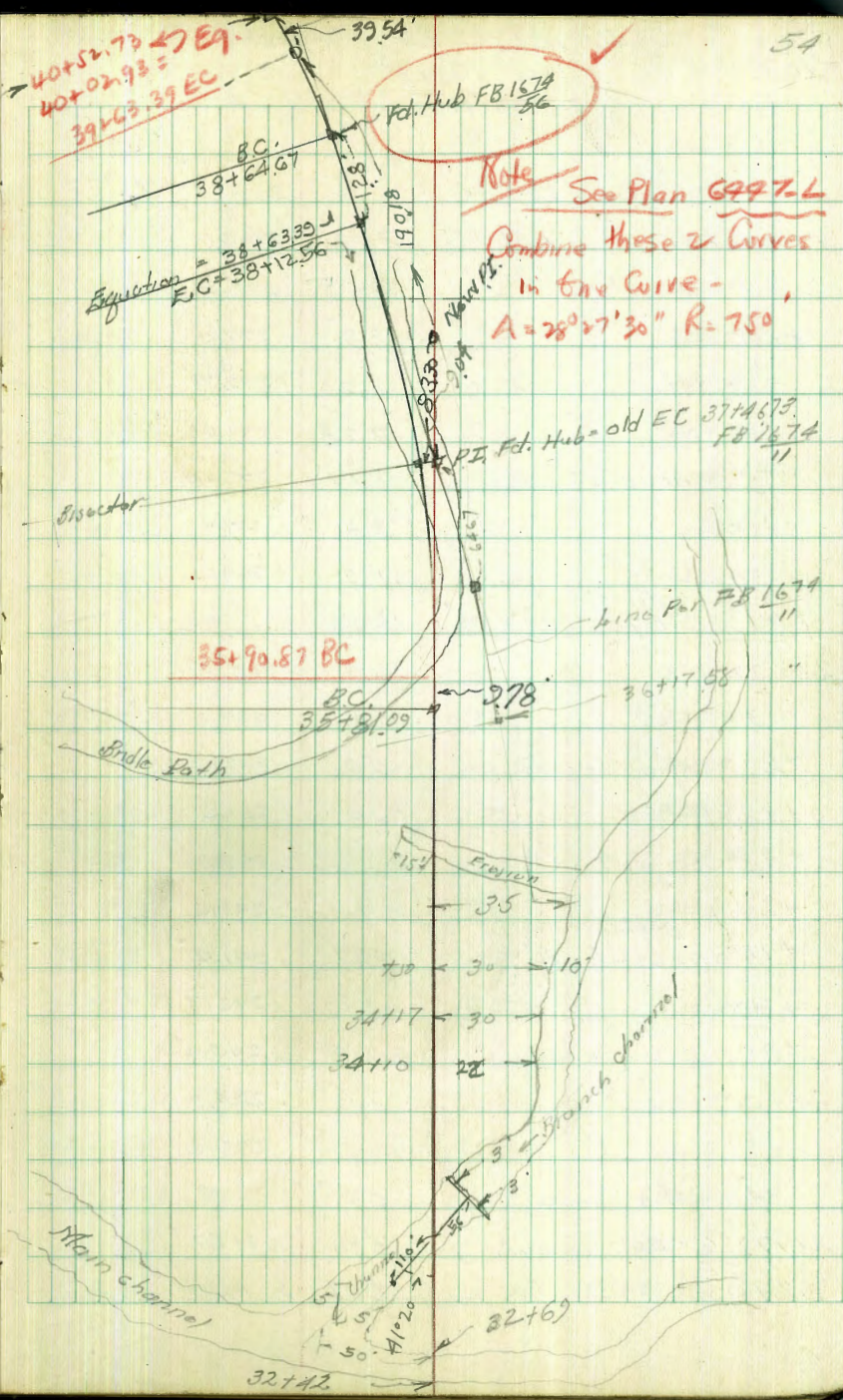
36+00

35+81.9 = B.C. Lt

35+00

34+00

33+32.6 = lot 12" Corrugated culvert (Plugged up)   
 Not in use





LEVELS - for Proposed Change  
 in 17172 36" Water Main  
 Location P-51-54

Station	Offset	Level	Height	Point
	11.20	272.91	268.71	BM + 19750 P.T. Hub FS 1874-22
17+04.67	2.60	276.91		
+50	4.60	275.31		
18+00	5.9	274.0		
+20	6.20	273.71		
+50	7.28	272.63		
175	8.51	271.40		
19+00	9.8	270.1		
+50	11.7	268.2		
TP	0.70	267.52	266.82	
20+00	2.0	265.5		
+13	3.3	264.2		
+20	5.0	262.5		
20+42.10	16.0	251.5		
+53	20.2	247.3		
+60	24.0	243.5		
+70	26.1	241.4		
+80	23.8	243.7		
+90	22.5	245.0		
21+00	17.6	249.9		
+31	12.2	255.3		
+48	6.7	260.8		
21+79.76	5.88	261.67		
TP	18.4	263.29	261.45	on Route

2.6329 ✓

22+50	3.0	260.3	
23+00	4.2	259.1	
+50	5.5	257.8	
+80	6.7	256.6	
24+00	8.1	255.2	
+10	8.8	254.5	
+50	9.2	254.1	
+60	8.6	254.7	
25+00	9.4	253.9	
+50	10.3	253.0	
TP	1.02	251.91	250.89 ✓
26+00	12.40	250.89	
+60	4.9	247.0	
27+00	7.5	244.4	
+50	10.5	241.4	
28+00	13.2	238.7	
TP	0.94	239.82	238.88 ✓
+50	2.9	236.9	
29+00	4.8	235.0	
+25	6.4	233.4	
+39	7.7	232.1	
+40	8.3	231.5	
29+52	8.9	230.9	
29+55	9.52	230.30	
+72	12.5	227.3	
TP	0.16	227.22	227.06 ✓

29+98			4.4	222.8
30+10			6.9	220.3
30+15	POT. on Hub		7.26	219.96
+20	River Canyon		8.4	218.8
+25			10.8	216.9
+27			13.7	213.5
TP	0.13	214.31	13.04	214.18
30+37			7.5	206.81
+44			11.6	202.7
+45			12.1	202.2
TP	0.23	201.81	12.73	201.58
+56			5.9	195.9
+65			3.7	195.1
+71			11.4	190.9
TP	0.19	189.14	12.86	188.95
+80			1.1	185.0
31+05			12.5	176.6
+20			14.3	172.2
+35			15.5	173.6
+50			16.3	172.2
TP	12.1	178.32	12.03	177.11
+76			6.6	171.7
+81			5.0	173.3
+91.16	E side Road Border Canyon		4.31	172.01
32+04.28	Paved Road		4.17	172.15
+16.35	W side		4.34	173.98

32+30			5.0	173.3
+42	on Bank channel		6.9	171.9
+43			10.0	168.3
32+44.7	Trunk Int. Sewer		10.1	168.2 Ground
+58	in channel		9.9	168.9
+62			3.7	172.6
+70			0.1	178.2
chk 32+07.14	Nail in Paving FB 1674-74		1.95	176.37 ✓
				176.34 Nail 5.03 Error
TP	13.61	190.63	0.30	178.02 ✓
32+82.5	int. Abandoned Trunk Sewer		12.4	178.2
27	ft. on River MH		12.14	178.99
"	on Floor North		23.21	167.93
"	" " South		25.12	165.51
32+92			11.2	179.9
33+23			10.1	180.5
+30			11.7	178.9
+31	in channel		14.5	176.1
+32.6	on 12" Pipe Culvert		12.60	178.03 Use
+40	in channel		15.2	175.9
+41			9.9	180.7
(33+37.6)	5.6 ft. on Rubble Dam		10.6	180.0
+45			9.0	181.6
+50			8.5	182.1
+55			7.5	183.1
+75			5.1	185.5

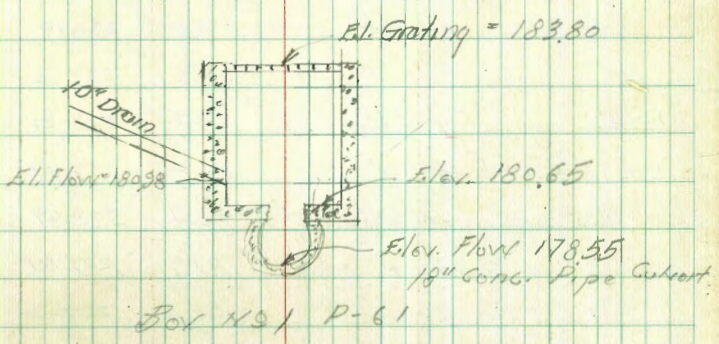
		✓		
		190.63		
33+92			1.3	189.3
T.P. 1	12.59	202.86	0.26	190.27
34+30			8.9	198.0
+50			6.1	196.8
+78			1.8	201.1
+78	erosion		2.6	200.3
+98			0.6	202.3
T.P.	12.14	214.74	0.26	202.60
35+19			2.5	205.2
+20	Erosion		10.9	203.8
+23	"		10.7	204.0
+25			8.6	206.1
+32			6.8	207.9
+50			4.1	210.6
T.P.	10.57	225.02	0.29	214.45 ✓
35+81.09	-B.C. Lt		9.33	215.69
+94	E edge Bridle Path		4.7	220.3
36+00	in Bridle Path		4.9	220.1
+25	W edge " "		4.3	220.7
T.P.	11.85	236.54	0.33	224.69 ✓
(36+25)	5' Rt		15.6	220.9
	1' Lt on Bank		12.9	223.6
	6' Lt		11.0	225.5
36+05			12.3 ✓	224.2
	1' Rt in Path		15.7	220.8

		236.54		57
36+50			10.1 ✓	226.9
	1' Rt		10.5	226.0
	2' in Path		13.6	222.9
	5' Lt		8.8	227.7
36+50	<sup>75</sup>		4.4 ✓	232.1
	5' Lt		3.0	233.5
	1' Rt. S edge Path		10.5	226.0
36+55	<sup>80</sup> " "		10.0 ✓	226.5
	1' Lt on Bank		4.0	232.5
	5' Lt S. edge Path		2.0	239.5
36+96.82	-P.O.C. in Hub		7.89	228.65
	2' Lt		2.5	239.0
	5' Lt		1.5	235.0
37+25			6.3	230.2
	8' Lt at Bank in Path		6.3	230.2
	12' Rt		5.8	230.7
37+50			4.2	232.3
	6' Lt at Bank "		4.2	232.3
	10' Rt. N edge "		3.8	232.7
37+75			2.2	239.3
	6' Lt S edge "		2.2	239.3
	7' Lt on Bank		4.0	240.5
	2' Rt		2.0	239.5
38+00			0.7	235.8
	7' Lt S edge Path		0.7	235.8
	6.5' Rt. N Bank		0.3	236.2 ✓

		236.54			
T.P.	3.24	242.77	2.01	234.53	
38+128 = EC					
= 38+63.39	Equation		6.34	236.43	
38+66.7 = BC Lt.			6.39	236.38	✓
Cont.					
chk E. Elev			6.86	235.91	
T.P.	12.90	255.55	0.12	242.65	✓
chk Hub	40+5273-EC Hub		1.49	254.06	✓
	FB 1674			254.05	
	66			0.01	

Proposed Sewer Levels Cont. from P-59

		211.03			
3+00			8.40	202.63	Edge Pav. 4.3 Lt.
T.P.	0.73	198.96	12.80	198.23	✓
3+46 = Int. Edge Gut. - Edge Pav			1.97	196.99	
+50 in Gut. Line			2.89	196.07	
3+81.68 on Riser Exist. M.H.			6.98	191.98	
Flow M.H. Page 40 =				186.73	
T.P.	3.54	189.88	12.62	186.34	✓
					x chkd out P-61



Box No. 1 P-61

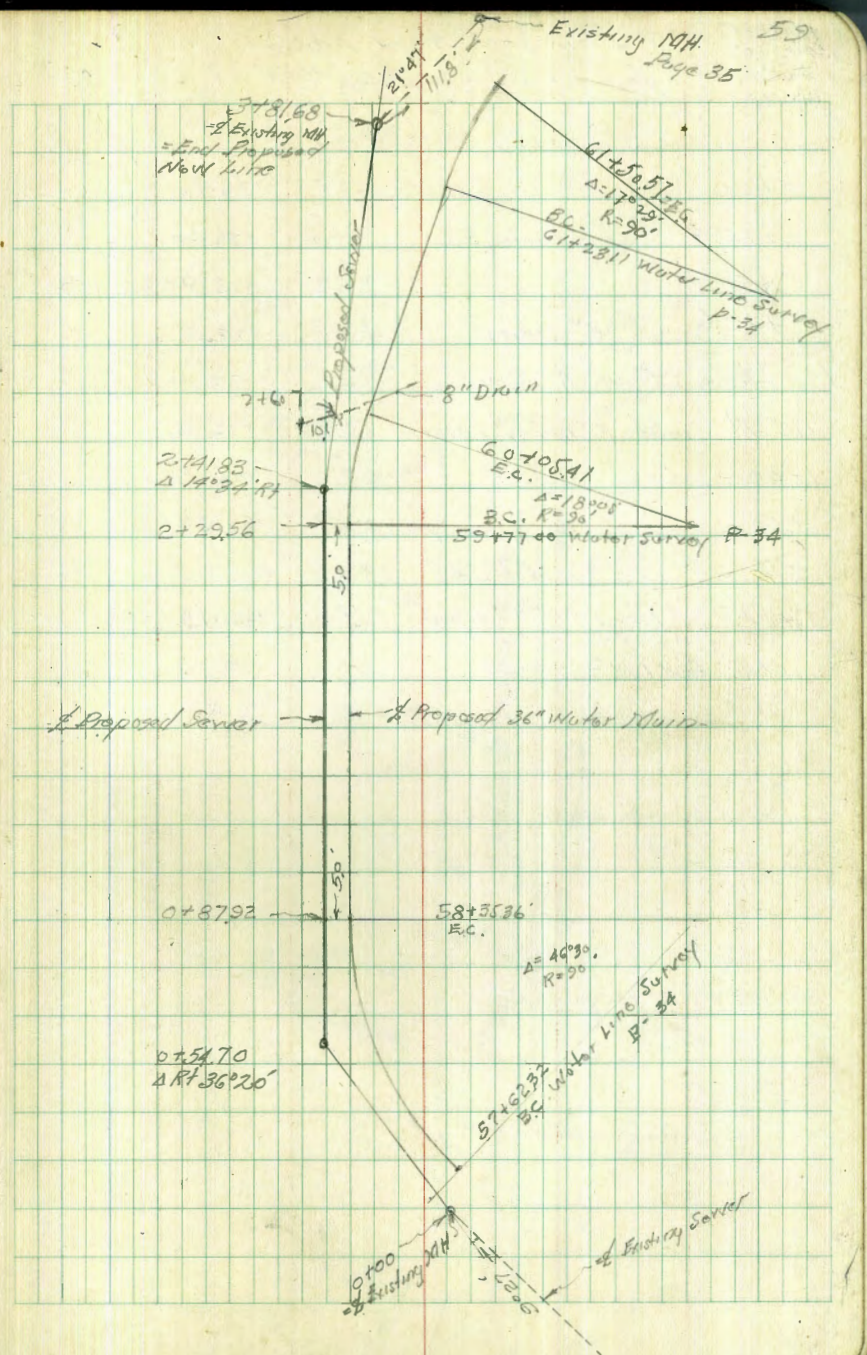
Walker  
Hazard  
Hardin

Alignment for Proposed Change  
of location and Construction of

3-7-45 Existing Sewer to give clearance  
of Proposed 36" Water Main - Zoo Grounds

Line "A"	BM Elev. Point 57+62.32 P-40		
1.24	2.35.94	234.70	
0+00 on Run MH	0.58	235.36	at 36" 8848
Flow		230.55	FB1674-LB
West edge cobble cut = 1.0' Lt.			
0+31.5 - Int. Wedge "	4.55	231.39	
+44 - " "	5.75	230.19	
+47 on " "	6.58	229.36	
+48 on Top Cobble wall	5.73	230.21	
0+54.7 - A RT 36" 20'	5.95	229.99	
+62 Int. E edge Wall	7.27	228.67	
63 Int. East E. edge	8.10	227.89	
767 " " W "	8.64	227.30	
770 on Pavng E "	8.35	227.59	
+87.92 5' Lt. of Water Survey	10.15	225.79	Edge Pav 3' Lt.
1+00 on Pav.	11.42	229.52	Edge Pav 5' Lt.
T.P. 0.23	223.13	13.04	222.90
1+50	3.95	219.18	7' Lt.
2+00	2.70	213.93	Edge Pav 7.3' Lt.
T.P. 0.76	211.03	12.86	210.27
2+41.83 - A RT 14' 34"	1.97	209.06	Edge Pav 5' Lt.
2+60.7 - Int 8" Drain	4.07	206.96	
10.1' Lt. on Grading	3.84	207.19	

Cont. P-58

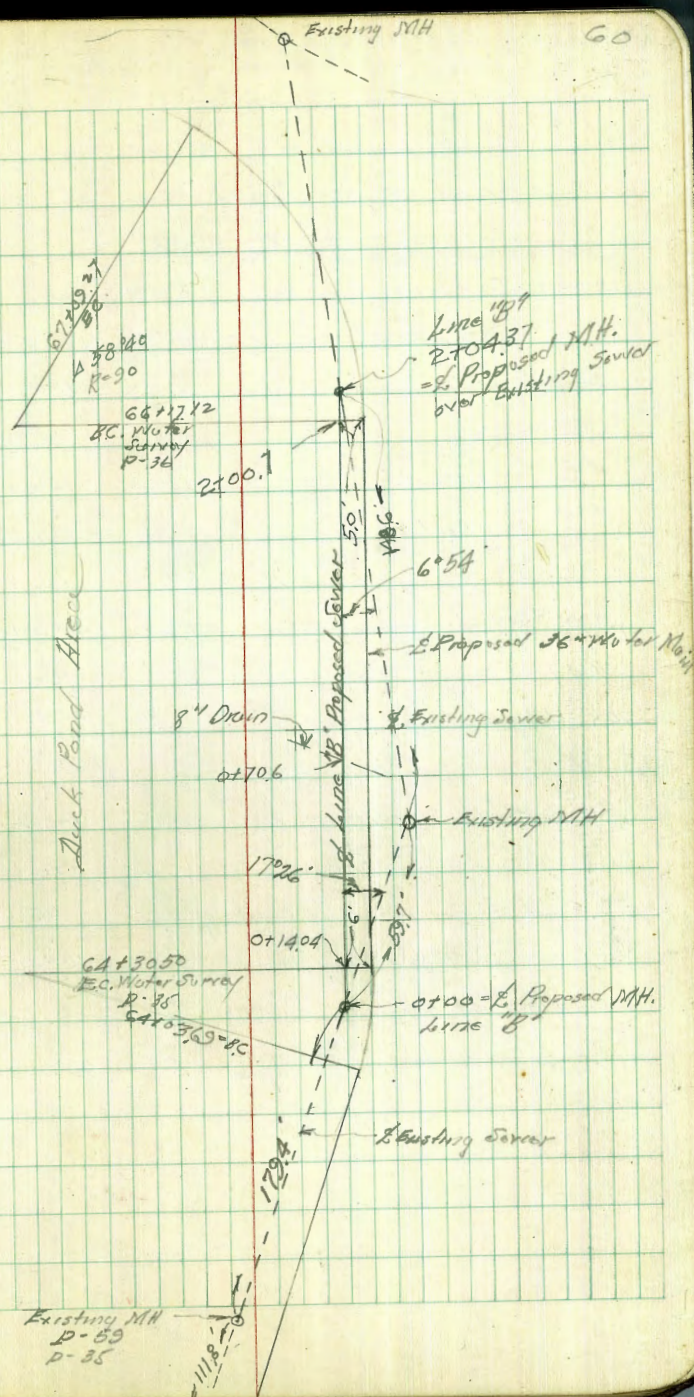


Walker  
Hazard  
Hordin  
3-7-45

Proposed New Location  
for Sewer Line "B"

179.09 = X P-61

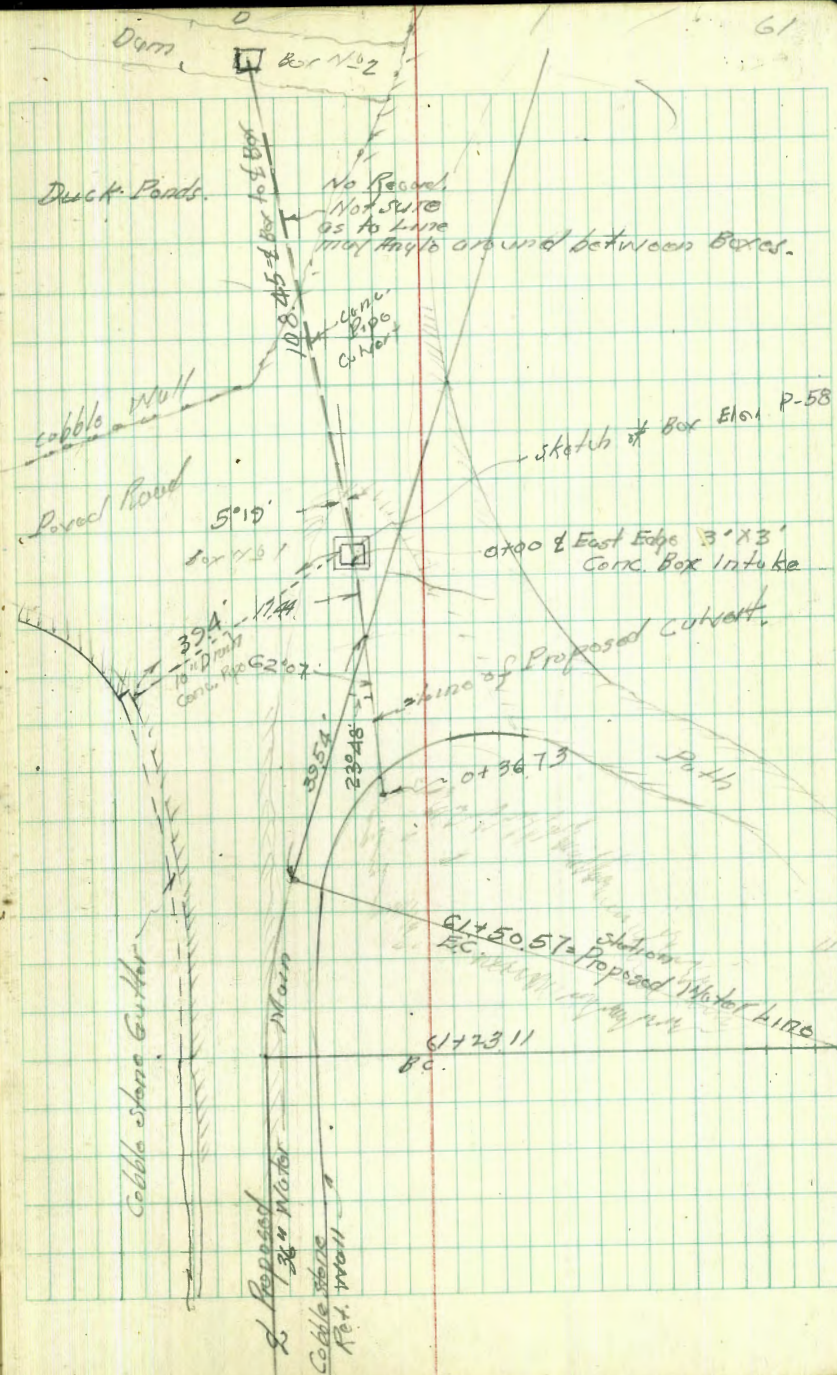
0+00		2.17	176.92	4.2' Lt. = cobble ch.
0+14.04 = 6' Lt of Water EC		2.49	176.60	3.1' Lt
+50		3.62	175.97	3' Lt. = cob. ch.
+70.6	10ft. 8" Drain	4.57	174.52	
12.8 Lt	Flow 8" Drain	8.39	170.70	
13.5 Rt	inlet 8" Drain Flow	7.03	172.06	opp. 0766
1+00		6.32	172.77	3' Lt. cob. wall
+50		9.51	169.58	3.2' Lt
TR	143	167.47	13.05	166.04
2+10(3) = 1/2 Proposed MH=Int. Exst. Sewer		2.34	165.13	3.7' Lt = Wall
cbk. 66+17.12 P-41		2.09	165.38	
			165.41	
			003	



Walker. Location - for Proposed  
Change in Existing Culvert  
account of interfering with grade  
of Proposed 26" Water Main  
Near Duck Pond in 300.

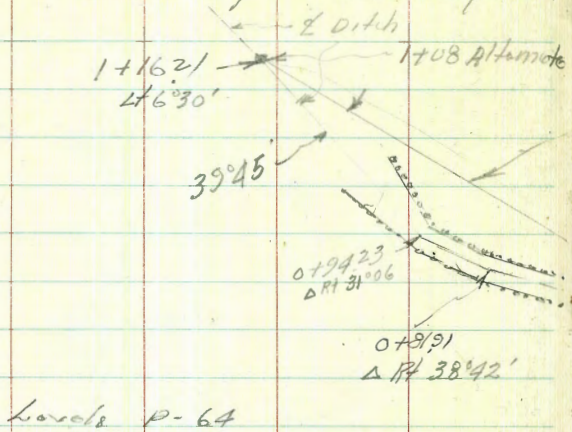
18988 P-58			
0+00	on Grating.	6.08	183.80 ✓
"	on Flow	11.23	178.55 ✓
0+05		5.2	189.7
+22		3.1	186.8
+32.7	at Wall	2.0	187.9
"	on Wall	0.29	189.59
+34	on Stake	3.9	186.0
+36.7	End Proposed W.C.	3.72	186.16
+47	P.O.T.	3.7	186.2
chk stake	62734.92 P-41	6.18	183.70 ✓
			183.73
			0.03
Box No 2	on Grating.	10.81	179.07
"	" " Flow	12.22	170.66
39.4' Lt. of Box No 1	on Grating	4.25	185.63
" " "	on Flow 10" Drain	5.80	184.08
on Flow at Box No 1	10" Drain	8.90	180.98 ✓
T.P.	0.71	122.09	11.50 178.38 ✓

Notes Reduced.



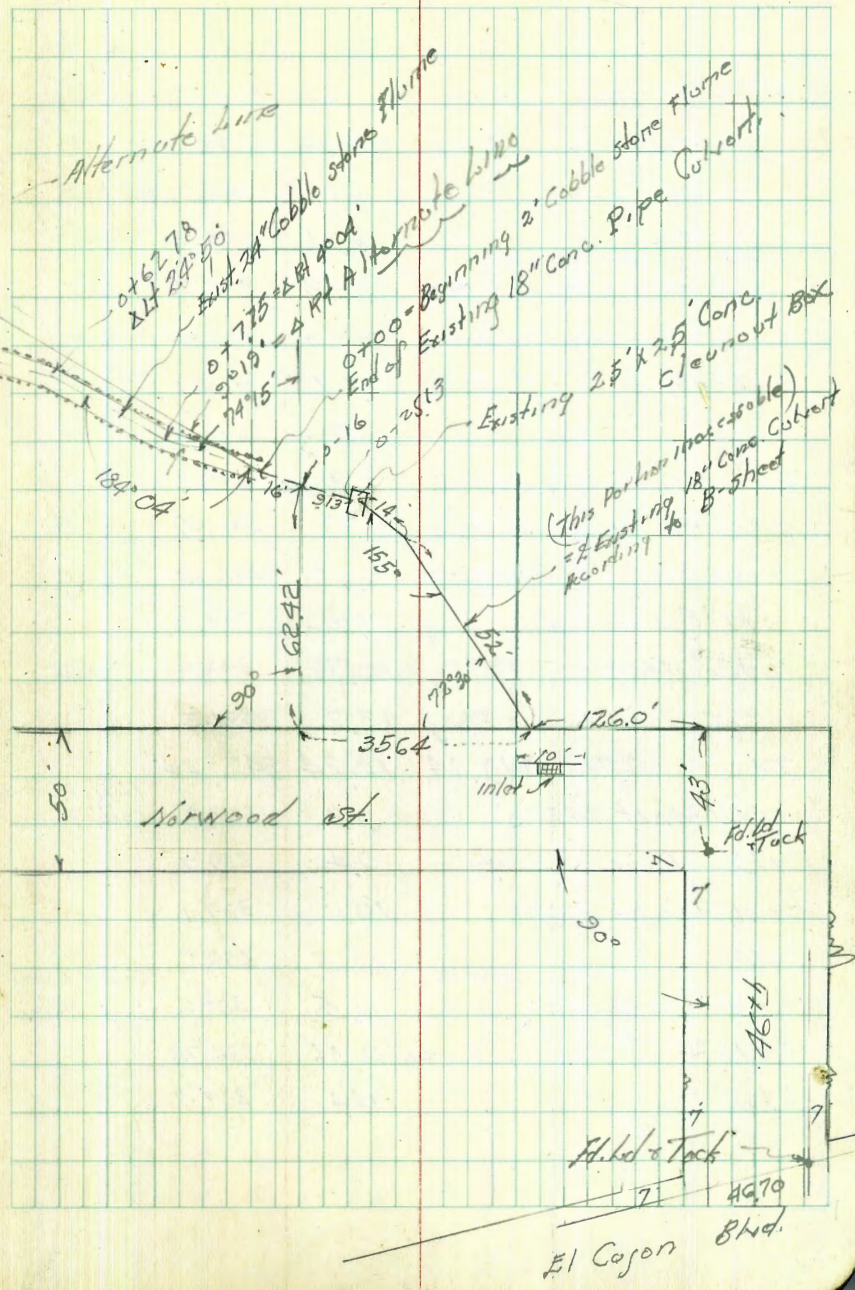
Walker  
Hazard  
Hazard  
7-12-45

Location Existing Culvert  
And Cobble Stone Flume And Line  
for Proposed Culvert Extension  
Across Lots 3 And 4 Edgemont Sub. Map # 129A.



Indexed  
C.S.M.

63





## Flume Line

B.M.					
FB 1372-15	1.56	354.68	353.12		sw. BP Chumma 170 & New Wood
on cb. & lat.	5.13	399.55			
" Grating	6.16	398.52			
" Flow	8.91	398.77			
0-25.13 = West inside edge on Grating Cleanout Box	7.03	397.65			
0-16 = East edge Conn. Drive	7.00	397.68			
0-7.7 = W " " "	7.17	397.51			
0-3	7.3	397.4			
0+00 on Rubble Hd Wall	8.7	396.0			
0+00 on Flow 18" Pipe	11.29	393.39			
0+00 " " Cobble Flume	11.55	393.13			
0+7.75 = Δ Rt 4°04' " "	11.92	392.76			
0+20 Flow " " "	12.7	392.0	2' wide		
+25 " " "	13.2	391.5			
TP 6.70	399.14	12.74	392.44		
0+62.78 = Δ Lt 24°50'	9.3	339.8		Flow 2.5' wide Cobble Flume	
0+79 Flow 3' wide	9.4	339.7			
0+81.91 = Δ Rt 38°42'	10.0	339.1			
+83 on Flow 4' wide	10.5	338.5		Cobble Flow	
0+94.23 = Δ Rt 31°06'	11.5	337.6		Ends here	
1+16.2 / Δ Lt 6°30'	12.36	336.78			
+65 on Flow Ditch on slope	14.4	339.7			

## Alternate Line

6A

349.14

0+00 same as opp Page				
0+09 N edge Flume 6.4	6.4	392.7		
+10 on Flume Wall	5.8	393.3		
0+20	6.1	393.0		
+35	7.2	391.9		
+60	7.8	391.3		
+70	7.0	392.1		
+87	7.5	391.6		
6' Lt = 2" Lime Tree				
6.5' Rt = 2" Orange				
0+95	9.4	339.7		
1+08 Alternate = 1+16.21 Flume Line	12.36	336.78		
TP 12.17	354.58	6.73	342.41	
chk. starting B.M.	4.47	353.11	353.12	✓
		353.12	341	

Cross Section Saratoga St. South by 30'  
70th St to 300 West.

0+80

TP 7.06 478.06 1.17 471.00

0+90

0+0 = N.L. 70th St

0-10 = N.C. of 70th St.

BM 11.83 460.34 <sup>2 LIT</sup> Saratoga St 70th

TP 2.98 472.17 6.36 469.59

BM 11.79 476.05 464.26 <sup>5th St</sup> ETC 90th 70th

Aug. 29-45

S. 500-  
8th St Rd  
at 60th St  
8099 Lt. 5

indexed  
C.S.K.

65

535  
26  
30  
50  
72  
72

478.06

Est. total  
425 Cu. yds

0 715  
500  
299  
56

Final total  
439 Cu. yds

20' width  
8" curb

299  
50  
10.38  
20-66  
11.01  
20-64

Vertical banks

519  
10.38  
30-13  
519  
10.38  
30-64  
519  
11.01  
20  
509  
11.01 ground

Plotted & computed  
Aug. 29, '45  
McKee

472.17

2+0

750

2+0

1+60

1+20

478.06

478.06

66

<del>6.1</del> 0.0	<del>7.1</del> 0.0	<del>6.9</del> 1.0	<del>6.8</del> 0.0
<del>6.5</del> 0.0	<del>7.2</del> 0.0	<del>6.9</del> 1.0	<del>6.8</del> 0.0
<del>6.6</del> 0.0	<del>7.3</del> 0.0	<del>6.9</del> 1.0	<del>6.8</del> 0.0
<del>6.1</del> 0.0	<del>7.3</del> 0.0	<del>6.9</del> 1.0	<del>6.8</del> 0.0
<del>6.1</del> 0.0	<del>7.3</del> 0.0	<del>6.9</del> 1.0	<del>6.8</del> 0.0
<del>6.1</del> 0.0	<del>7.3</del> 0.0	<del>6.9</del> 1.0	<del>6.8</del> 0.0

478.06

Re Cross Section Saranac St South 40°  
70th St to 300' Mark  
For Final Yardage  
Indexed  
c.s.k.

1+60				
1+20				
0+80				
TP	8.36	476.13	2.82	467.77
0+10				
0+0 = W.L. 70th St.				
0+10 = W.C. Line 70th St				
BM	10.25	470.59		460.34 <sup>\$ 2+1</sup> Saranac + 70th

Sept. 25-45 67  
S. 107  
B. 11.5  
A. 5.00 + 1.0

4.5

61.92 86.7 30-1b	61.38 9.21 30-1b	61.1 9.5 20	60.65 9.91 7-13 = 50' Cut	60.3 10.2
41.49 41 30	41.78 8.81 20-1b	41.22 9.37 20-1b	41.22 9.37 20-1b	40.9 9.7
30.74 30 0.8	31.5 30	31.1 30	31.1 30	30.9 30
22.4 20 2.4	22.3 20	22.3 20	22.3 20	22.3 20
13.9 12 1.9	13.5 12	13.6 12	13.6 12	13.5 12
7.1 6.5 0.6	7.8 6.5 1.3	7.3 6.5 0.8	7.3 6.5 0.8	7.1 6.5 0.6
2.3 2.0 0.3	2.3 2.0	2.3 2.0	2.3 2.0	2.3 2.0
2.3 2.0 0.3	2.3 2.0	2.3 2.0	2.3 2.0	2.3 2.0
5.9 5.0 0.9	5.8 5.0	5.8 5.0	5.8 5.0	5.8 5.0
5.9 5.0 0.9	5.8 5.0	5.8 5.0	5.8 5.0	5.9 5.0 0.9

Total  
439 Cu. yds  
Computed by:-  
A. McKee

170.59

370

2750

270

476.13

71.6	71.4	70.9	70.9
4.5	4.7	5.2	5.2
30	21	20	

72.2	71.7	70.5	71.1
3.9	4.4	5.6	5.0
30	23-Top Men Col.	20	

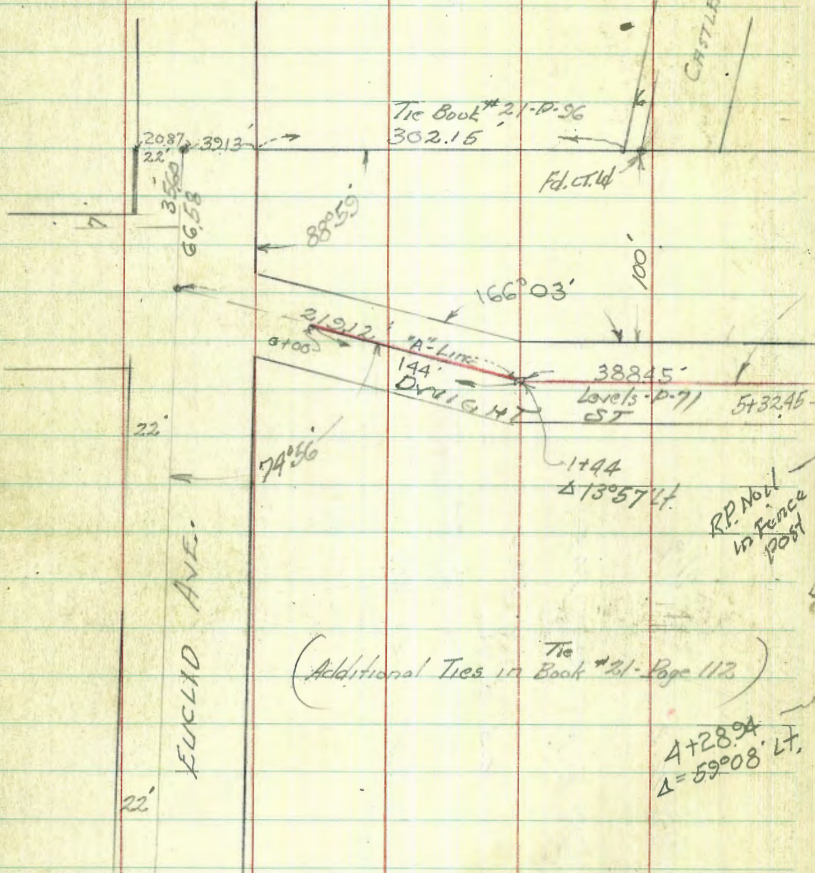
73.1	72.9	70.7	71.2
5.0	5.2	5.4	4.9
30	20-Top Men Col.	20	

476.13

Walker  
Hazard  
Hordin  
Begg  
10-23-45

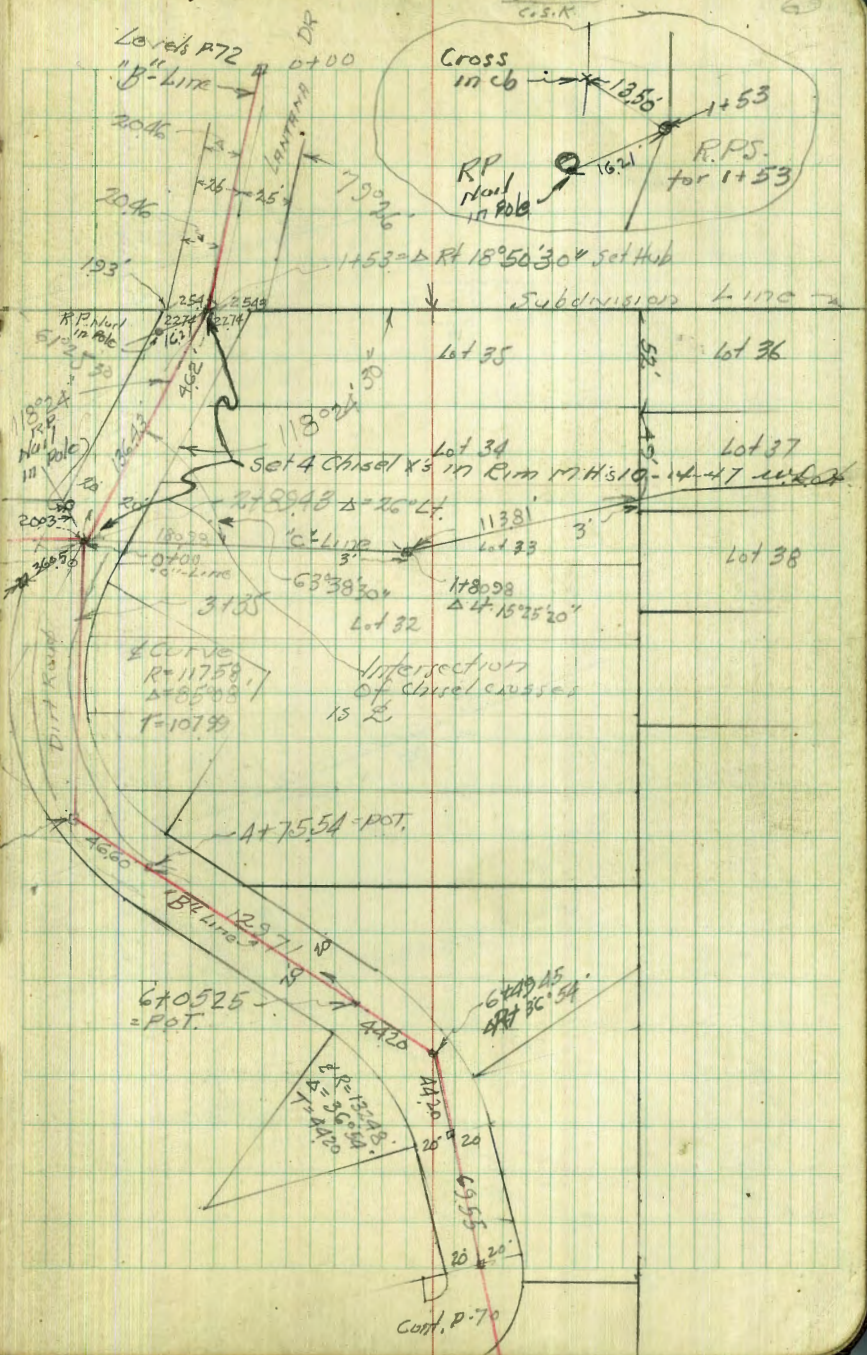
LOCATION - PROPOSED SEWER  
IN DWIGHT ST. - LANTANA DRIVE.

— Proposed Sewer  
Levels P-71

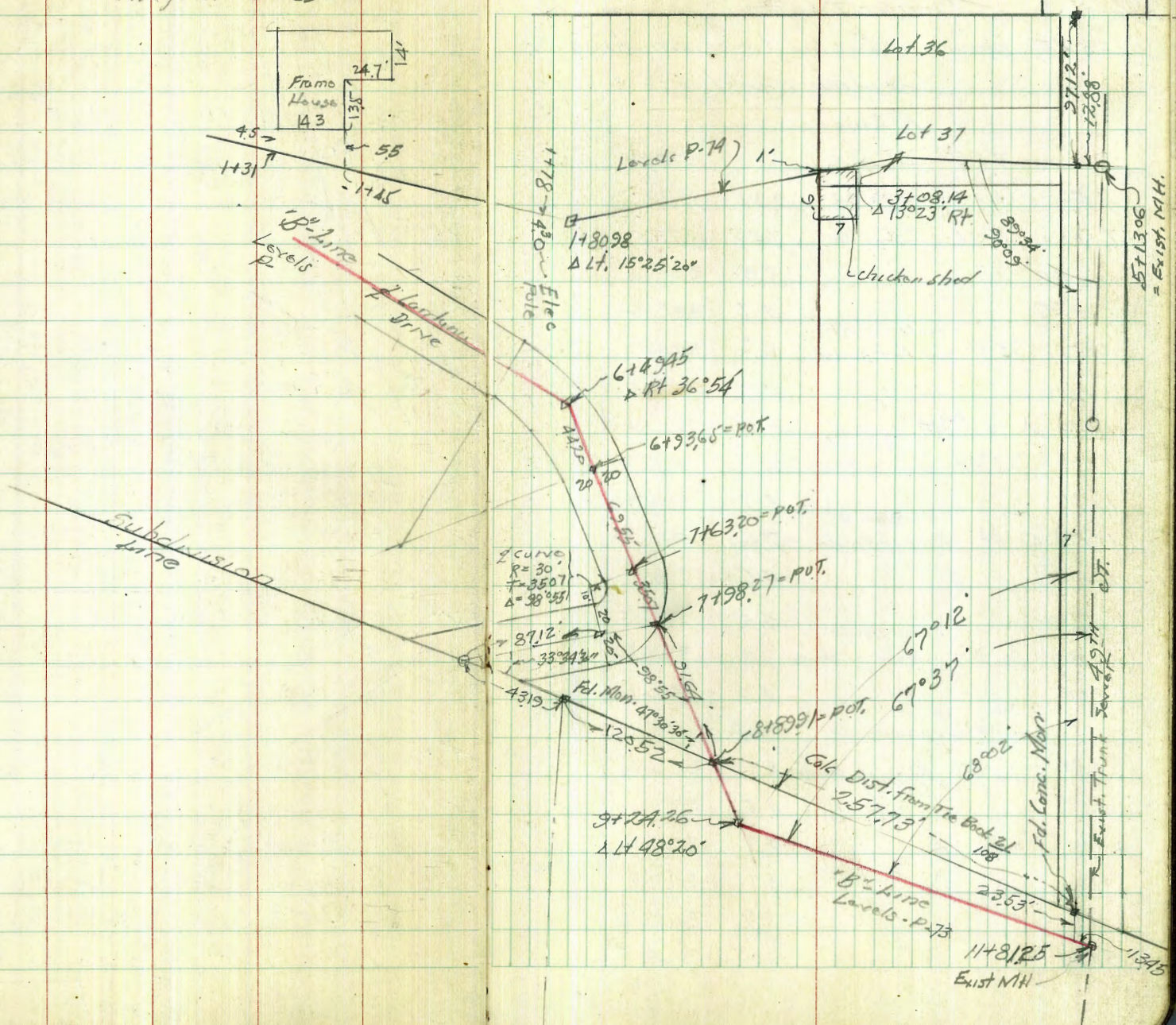


Construction Notes for  
Partion Above Line  
117 Grade Book 229

indexed  
C.S.R.



Proposed Sewer  
Cont. from P. 69



Walker  
Hazard  
Hurdin

LEVELS - PROPOSED SEWER

D NIGHT ST

10-23-45 between Euclid Ave <sup>and</sup> Lantana Dr.

Location Sketch P-69

"A" line

B.M.  
N.E. B.P. Euclid  
Lantana

	7.87	348.33		340.46
T.P.	1.11	339.93	2.51	338.82
T.P.	4.01	336.54	7.40	332.53
0+00			3.9	332.6
+50			4.1	332.4
(0+50)	75' Rt	on Ground opp Rear House	6.2	330.3
1+00			4.5	332.0
1+44	Δ 13° 59' H	up Hub on Ground	4.91	331.63
(1+19)	75' Rt.	Rear of House	7.1	329.4
1+70			4.7	331.8
(1+70)	60' Rt	on ground Rear of House	7.6	328.9
2+00			4.6	331.9
+50			4.1	332.4
(2+50)	90' Rt	on ground Rear of House	7.3	329.2
3+00			4.0	332.5
		Storm Drain on R. in 10 ft.	2.95	
(3+35)	90' Rt	Rear of House	6.1	330.4
3+50			4.4	332.1
4+00	(outs - House E)		4.9	331.6
+50	( " " )		6.7	329.8
+63			7.3	329.2
5+15			12.4	324.1

336.54

71

T.P. 12.09 336.04 12.59 323.25

5+32.45 on Hub 12.85 323.19

for, check out see Cont. Levels P-72



LEVELS SEWER PRELIM.  
IN LANTANA DYNE.  
= "B"-LINE Location 62,70

		N P. 71 336.04			
T.P.	2.44	338.02	0.46	335.58	
0+00	on stub		0.70	337.3	
0+26	70' Lt. Rear of House		1.2	336.8	plumbing
(0+26)	= Conc. Basement House	7.9		330.1	1.0' below floor.
0+50			1.9	336.1	
0+78	on Conc. Basement		2.9	335.1	plumbing
(0+78)	86' Lt. Rear of House	9.3		328.7	1.0' below floor.
1+00			3.9	334.1	
+53	= A 18° 50' 30" RT on Hub	6.20		331.8	plumbing
(1+55)	Parallel to Conc. Basement to 67' Lt. = North Side House	13.4		324.6	1.0' below floor.
T.P.	0.73	332.55	6.20	331.82	on Hub
2+00			1.7	330.9	
+25			2.8	329.8	
+33			5.2	327.4	
+78			7.9	324.7	
2+89.93	(S 132° 45' P 71)	9.36		323.12	SW cor House
(2+95)	13° Lt. Parallel to Lot line = Front of House	18.1		314.5	on Ground.
3+00			9.8	322.8	
+35	in Fill Ground		11.3	321.3	
T.P.	2.40	323.07	11.88	320.67	
3+50			5.0	318.1	
5' Rt.	= E edge Dirt Road		2.1	321.0	
5' Lt.			7.1	316.0	
10' Lt.	= Natural Ground		9.0	314.1	

"B"-Line Cont.

72

323.07

3+75	in Fill Ground	5.1		318.0	
10' Lt.	= Nat. "	8.6		314.5	
5' Rt.	= East Edge dirt Rd	2.6		320.5	
3+90	" " " "	2.7		320.4	
4+00		2.6		320.5	
+28	Δ Lt. 59° 08'	2.6		320.5	
4+28.94	on Hub	2.85		320.2	
+80		4.9		318.2	
5+00		7.0		316.1	
10' Lt.	Nat. Ground	9.5		322.0	
30' Lt.		12.3		310.8	
5+50		12.4		310.7	
40' Lt.		17.7		305.4	
T.P.	0.15	310.64	12.58	310.49	
6+00		7.3		303.3	
50' Lt.		12.6		298.0	
T.P.	0.09	297.63	13.10	297.54	
6+49.45	= Δ Rt 32° 54' on Hub	1.34		296.3	
20' Lt.		6.8		290.8	
55' Lt.		15.7		281.9	
6+93	N-Side House	6.8		290.8	NW cor House
26' Lt.	Soil Pipe	14.7		282.9	7' in St
7+00		7.7		289.9	
+50		13.7		281.9	
T.P.	0.53	285.25	12.91	284.72	

"B" - Line Cont. from p 72

285.25

7+98.27		7.01	278.3	7' RT
8+04		7.1	278.2	Elec Pkt
8+30		13.5	271.8	
T.P.	0.47	273.01	12.71	272.54
8+60		10.3	262.71	
T.P.	0.29	260.44	12.86	260.15
8+90		6.3	254.1	
9+00		8.1	252.3	
+17		10.8	249.6	
9+24.26	△ Lt 48° 20'			
T.P.	2.98	250.10	13.32	247.12
3' RT - 2' ditch		4.1	246.0	
9+50		3.3	246.8	
2' RT " "		4.7	245.4	
9+90 ± " "		4.9	245.2	
10+00		4.1	246.0	
+15		5.2	244.9	
+22 2' 3' "		7.3	242.8	
+30		6.2	243.9	
10+50		7.1	243.0	
5' RT - 2' 3' ditch		8.8	241.3	
10+80		7.7	242.4	
12' RT " 4' "		9.6	240.5	
11+00		8.8	241.3	
+10		9.8	240.3	
750		10.8	239.3	

"B" - Line

73

250.10

T.P.	3.25	242.23	11.12	238.98
11+81.25	±	East. M.H. on Run	3.70	238.5
"		on Floor M.H.	12.49	229.70 = P1011
Set		Sub. line for Korean Acres	4.69	229.74
B.M. 1912		N. on W. Line 49th	2.53	237.54
3		Nails in Pole 16 ft 14475		232.70 ✓
		FB 1561-46		

Walker  
Hazard  
Hurdin  
8999  
10-30-45

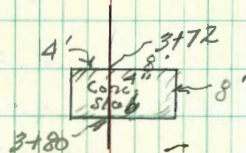
LEVELS PROPOSED SEWER  
"C" Line - Location P-69

Station	Offset	Level	Station	Level
	2.39	325.58	323.19	5132.45
0+00			2.1	323.5
+12			2.5	323.1
+28			6.5	319.1
+41	45' Rt = 5" Poplar Tree			
0+53	4' Rt " " "			
0+58			7.9	317.7
1+00			2.9	315.7
T.P.	0.13	314.18	11.53	314.05
1+50			1.7	312.5
1+80.98	on Hub. = Δ Lt 15°25'20"		6.98	307.2
+86			7.7	306.5
T.P.	0.64	301.72	13.10	301.08
2+00			3.1	298.6
+04			6.2	295.5
+08			7.1	294.6
2+23			16.3	285.4
T.P.	0.59	289.07	13.34	288.38
T.P.	0.12	276.37	12.72	276.25
T.P.	0.49	263.84	13.02	263.35
2+55			+4.0	259.8
+75			2.0	261.8
2+95			7.2	256.6
3+08.14	on Redwood Stub. = Δ Rt 13°23'		9.68	254.2

26384

"C" Line 74

3+25		13.7	250.1
T.P.	3.85	254.66	13.03
3+34		7.1	247.6
+38	in channel	12.3	242.4
+47	" "	12.1	242.6
+49		11.0	243.7
+53		11.0	243.7
+57		10.3	244.4
+68		9.9	244.8
	3' Lt 4' Rt = Pomegranate Trees		
3+72	on Conc. Stub	9.72	244.94



4+00		9.5	245.2
3+85	13' Lt = Quince Tree Bush		
3+98	12.7 Lt = Plum " 4"		
"	15' Rt = 6" Apricot Tree		
4+11	12.7 Lt = 3" Plum "		
"	15' Rt = 8" Apricot "		
4+15	1st chicken wire fence 3' high at Rt a 10'		
4+25	13' Lt 6" Apricot		
4+20	10.7' Rt 2" Peach		
+37	15' Rt 5" Pecan		
4+38	13' Lt 6" Apricot		

25466

"C" Line.

75

4+50 8.7 246.0

" 13' Lt. - 6" Apricot,

4+78 13' Lt " "

+89 " " 5" "

4+15  Chicken wire Fence

2 2' Board

Fence

5-1" x 2" Boards

4+92  10.7

4+94 7.6 247.1

4+99 6.6 248.1

5+13.06 2' MIN on Rim 6.44 248.22

" on Flow 15.25 239.41

239.23 = Plus  
0.18 diff.15' Lt 190+75 Page 71  
chk. 3 Nails in Pole

14.95 239.71

239.70

0.01 Error.

Check of Pamela Park

Final Check  
Feb 23 46

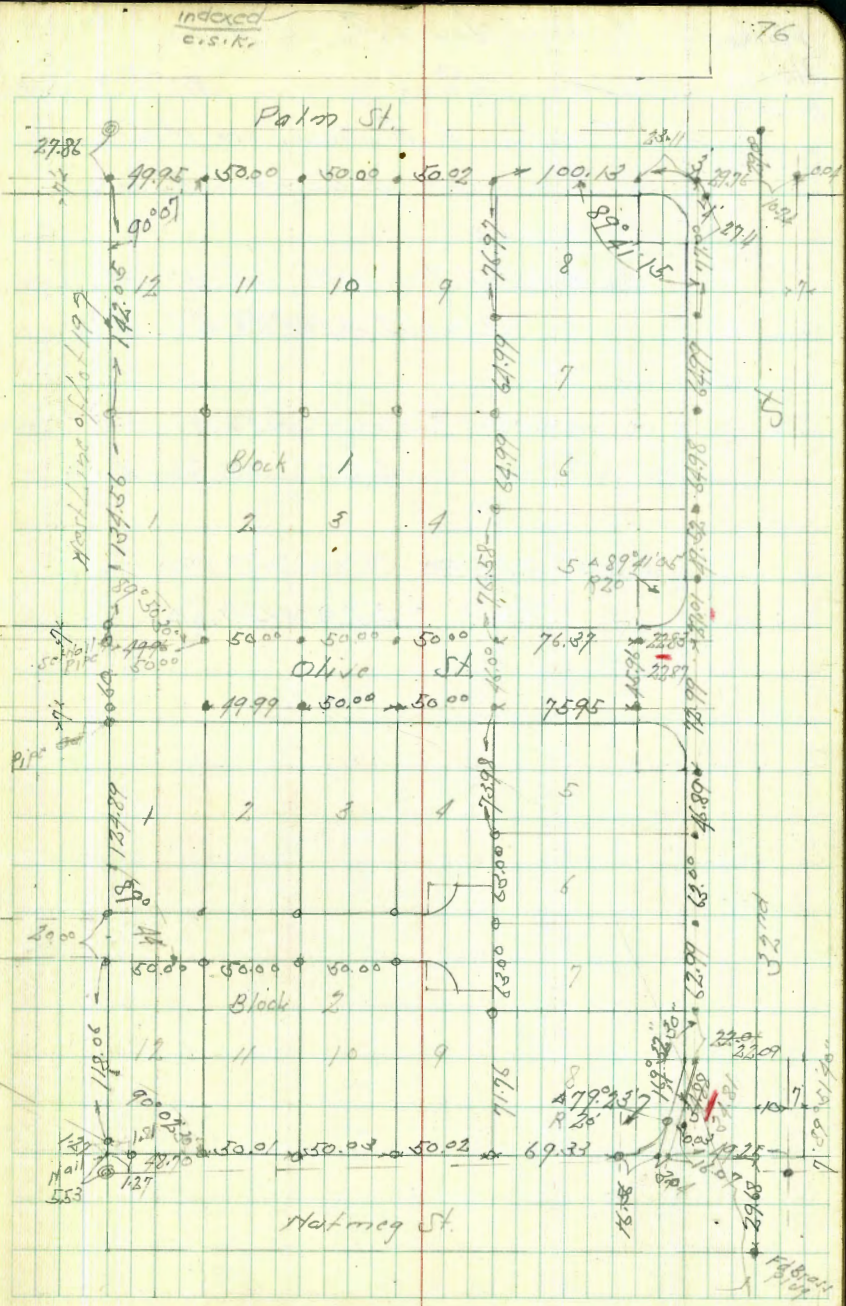
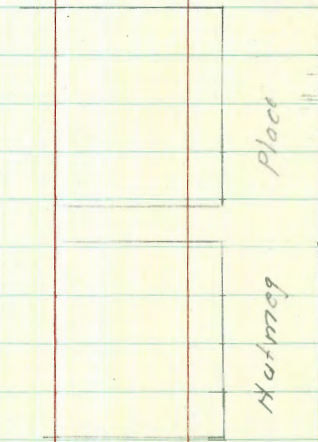
Feb. 19 46

S. 5500  
O. 8000  
W. 6000

- Lead + Tack Found
- ⊙ 3" Pipe Lead + Tack
- ⊙ 2" Pipe "

Surveyed By John F. Covert

R.E. # 2718



Walker  
Hurdin  
Hurley  
12-12-48

36" Water Main Across  
Belboa Park from 30<sup>th</sup> & Thom St.  
Transfer of 3 Elev. on Hubs  
To Reference Hubs - for Const.  
Purposes

4.67 256.07      251.40 B.M.

2.51 253.56 B.M.

5.22 282.13      276.91 B.M.

6.22 275.84 B.M.

3.00 233.30      230.30 B.M.

3.70 229.60

77

on E Hub B.C. 8+41.28 FB 1674-48

" Stake 55' Rt. of 8+41.28

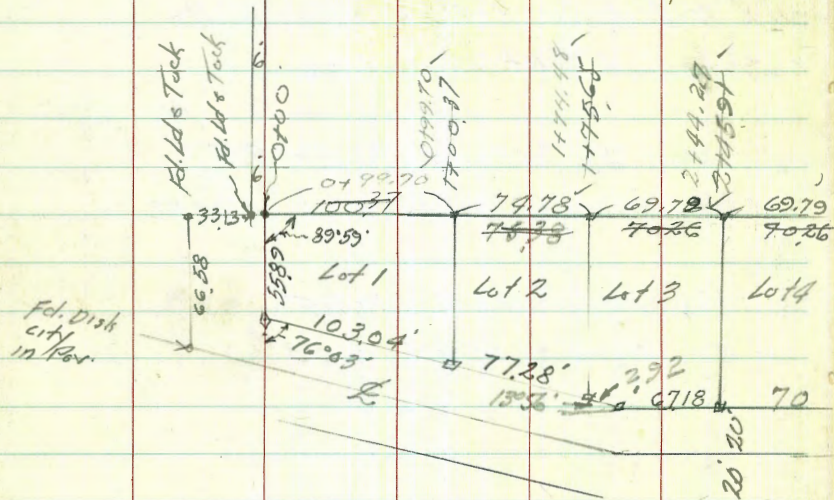
on S Hub B.C. 17+04.67 P-55

on Chisled cross East end cb <sup>on Rt</sup> 17+52

on E Hub - P.O.T. 29+55 P-55

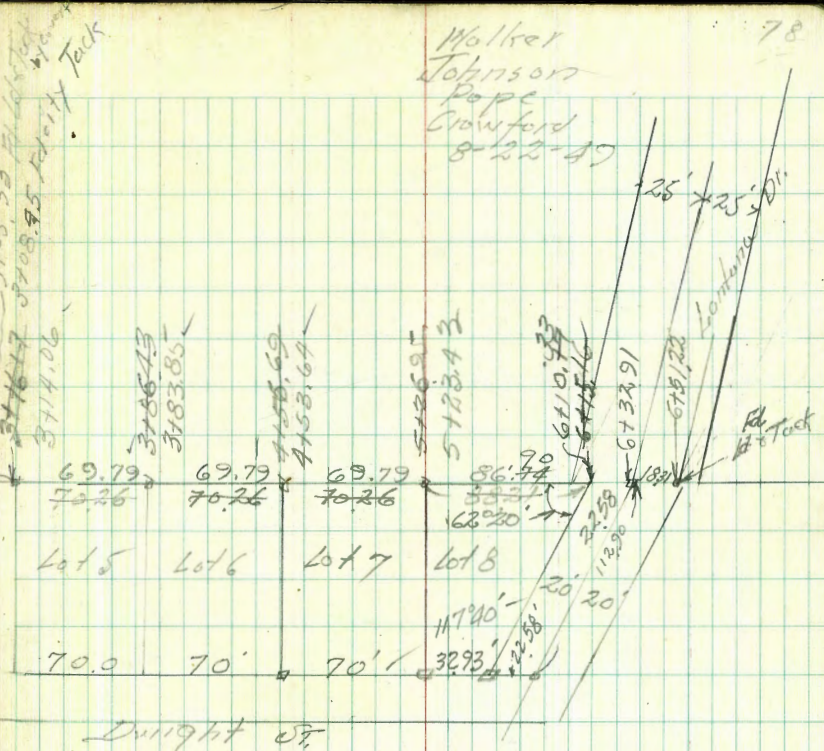
on RP 51.80 RA 29+55 P-53

Set Preliminary Stubs  
 Along North line Subdivision  
 Four-Hundred Acres  
 Between Euclid & Lorain  
 = Proposed Adjustment Lot Lines

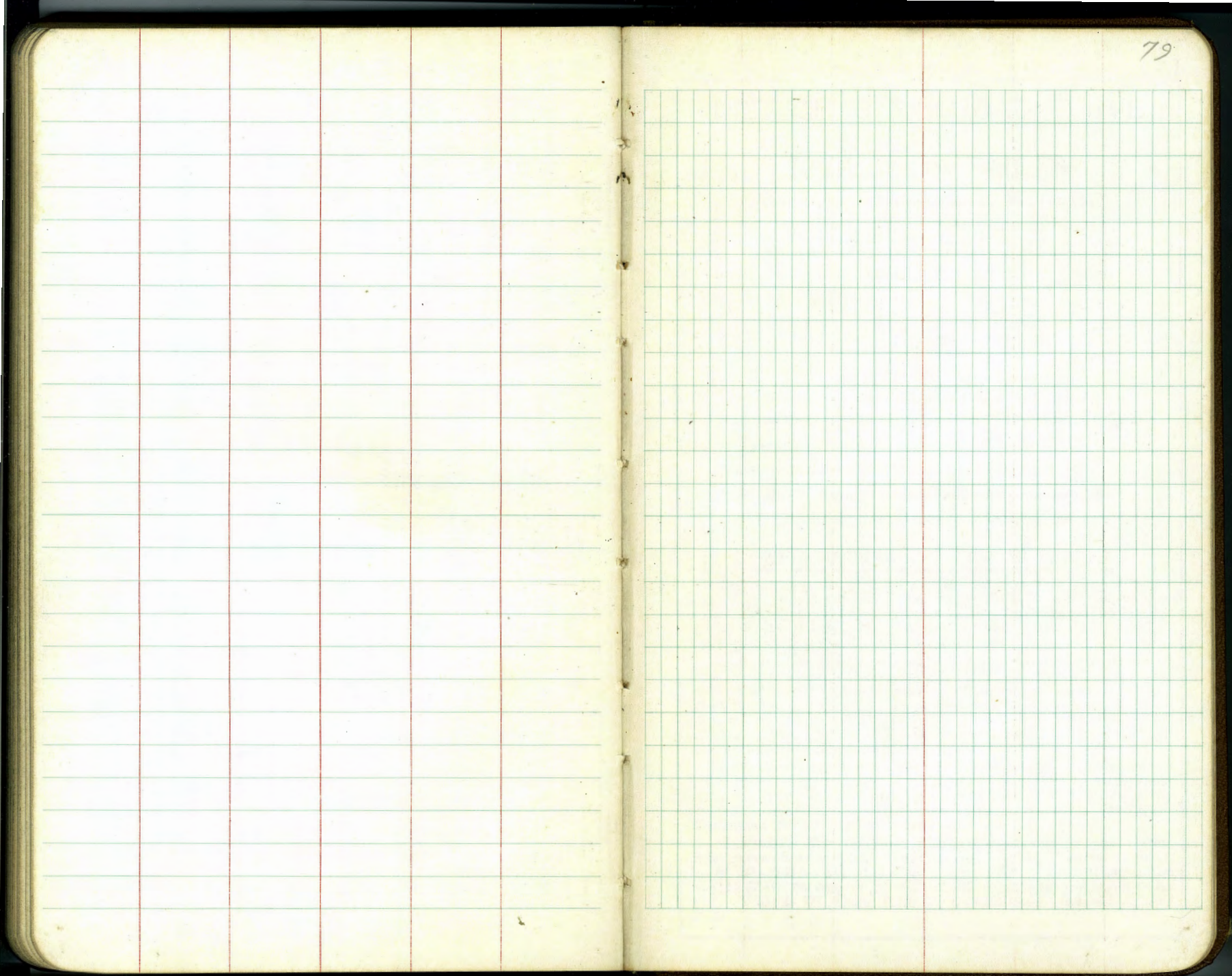


Euclid Ave

3105.33  
 3108.95  
 3114.06  
 3128.73  
 3183.85  
 3158.69  
 3153.64  
 5128.43  
 5128.43  
 6110.93  
 6132.91  
 6141.22  
 6141.22



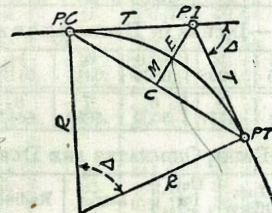
Walker  
 Johnson  
 Pope  
 Crawford  
 9-23-49





# DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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605  
528  
11.33

855  
137  
992  
598  
27  
1118

### CURVE FORMULAS

- Radius— $R = \frac{50}{\sin \frac{D}{2}}$  (1) Degree of Curve— $D$  and  $\sin \frac{D}{2} = \frac{50}{R}$  (2)
- Tangent— $T = R \tan \frac{\Delta}{2}$  (3) Length of Curve— $L = 100 \frac{\Delta}{D}$  (4)
- Middle ordinate— $M = R(1 - \cos \frac{\Delta}{2})$  (5)  $= R \text{vers} \frac{\Delta}{2}$  (6)
- External— $E = T \tan \frac{\Delta}{4}$  (7)  $= R \div \cos \frac{\Delta}{2} - R$  (8)  $= R \text{exsec} \frac{\Delta}{2}$  (9)
- Long Chord— $C = 2 R \sin \frac{\Delta}{2}$  (10)  $\Delta$ —Central Angle

### EXPLANATION AND USE OF TABLES

**Stations.**—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T.  $\Delta = 62^\circ 10'$   $D = 8^\circ 20'$ . From Table IV for  $1^\circ$  curve  $T = 3454.1$  and  $\div 8\frac{1}{3} = 414.49$  ft. From Table V correction—.36 or  $T = 414.85$  ft. P. C.—Sta. P.I.— $T = 157 + 45.50$ . Also from (4)  $L = 746.00$  and P. T.—Sta. P. C. +  $L = 164 + 91.50$ .

**Offsets.**—Tangent offsets vary (approximately) directly with  $D$  and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.—7.27 ft. Distance—158—Sta. P. C.—54.50, hence offset— $7.27 (54.50 \div 100)^2 = 2.16$  ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus  $(54.50)^2 \div (2 \times 688.26) = 2.16$  ft.

**Deflections.**—Deflection angle— $\frac{1}{2} D$  for 100 ft.,  $\frac{1}{4} D$  for 50 ft., etc. For  $c$  ft.—(in minutes)  $.3 \times C \times D^2$  or—defl. for 1 ft. from Table III  $\times C$ . For Sta. 158 of above curve—.3  $\times 54.5 \times 8\frac{1}{3} = 136.2'$  or  $2^\circ 16.2'$ , or— $2.50 \times 54.5 = 136.2'$  from Table III. For Sta. 159 deflection angle— $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$ , etc.

**Externals.**—May be found in similar manner to tangents. Thus  $E$  for curve above is 115.37. For from Table IV for  $1^\circ$  curve  $E = 960.6$  for  $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 115.27$  and from Table V correction—.10 or  $E = 115.37$  ft. Or suppose  $\Delta = 32^\circ$  and  $E$  is measured and found to be 42 ft. What is  $D$ ? From Table IV  $E = 230.9$  and  $\div 42 = 5.5$  or  $D = 5^\circ 30'$ .

TABLE I.—MINUTES IN DECIMALS OF A DEGREE.

Table with 12 columns representing minutes from 1' to 12' and 10 rows representing decimal values from .0167 to 1.0000.

TABLE II.—INCHES IN DECIMALS OF A FOOT.

Table with 11 columns representing inches from 1-16 to 7/8 and 11 rows representing decimal values from .0833 to .9167.

TABLE III.—RADI, ORDINATES AND DEFLECTIONS.

Large table with 5 columns for Radius, Mid. Ord., Tan. Offset, and Def. for 1 Foot, repeated for angles from 0 to 30 degrees.

Note, Chord Deflection=2 times tangent deflection.

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Table with 9 columns for Central Angle, Tangent, and External, repeated for angles from 10 to 30 degrees.

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
31°	1589.0	216.3	41°	2142.2	387.4	51°	2732.9	618.4
10'	1593.0	218.7	10'	2151.7	390.7	10'	2743.1	622.8
20	1806.9	221.1	20	2161.2	394.1	20	2753.4	627.2
30	1815.9	223.5	30	2170.8	397.4	30	2763.7	631.7
40	1824.9	226.0	40	2180.3	400.8	40	2773.9	636.2
50	1833.9	228.4	50	2189.9	404.2	50	2784.2	640.7
32	1643.0	230.9	42	2199.4	407.6	52	2794.5	645.2
10	1652.0	233.4	10	2209.0	411.1	10	2804.9	649.7
20	1661.0	235.9	20	2218.6	414.5	20	2815.2	654.3
30	1670.0	238.4	30	2228.1	418.0	30	2825.6	658.8
40	1679.1	241.0	40	2237.7	421.4	40	2835.9	663.4
50	1688.1	243.5	50	2247.3	425.0	50	2846.3	668.0
33	1697.2	246.1	43	2257.0	428.5	53	2856.7	672.7
10	1706.3	248.7	10	2266.6	432.0	10	2867.1	677.3
20	1715.3	251.3	20	2276.2	435.6	20	2877.5	682.0
30	1724.4	253.9	30	2285.9	439.2	30	2888.0	686.7
40	1733.5	256.5	40	2295.6	442.8	40	2898.4	691.4
50	1742.6	259.1	50	2305.2	446.4	50	2908.9	696.1
34	1751.7	261.8	44	2314.9	450.0	54	2919.4	700.9
10	1760.8	264.5	10	2324.6	453.6	10	2929.9	705.7
20	1770.0	267.2	20	2334.3	457.3	20	2940.4	710.5
30	1779.1	269.9	30	2344.1	461.0	30	2951.0	715.3
40	1788.2	272.6	40	2353.8	464.6	40	2961.5	720.1
50	1797.4	275.3	50	2363.5	468.4	50	2972.1	725.0
35	1806.6	278.1	45	2373.3	472.1	55	2982.7	729.9
10	1815.7	280.8	10	2383.1	475.8	10	2993.3	734.8
20	1824.9	283.6	20	2392.8	479.6	20	3003.9	739.7
30	1834.1	286.4	30	2402.6	483.3	30	3014.5	744.6
40	1843.3	289.2	40	2412.4	487.2	40	3025.2	749.6
50	1852.5	292.0	50	2422.3	491.0	50	3035.8	754.6
36	1861.7	294.9	46	2432.1	494.8	56	3046.5	759.6
10	1870.9	297.7	10	2441.9	498.7	10	3057.2	764.6
20	1880.1	300.6	20	2451.8	502.5	20	3067.9	769.7
30	1889.4	303.5	30	2461.7	506.4	30	3078.7	774.7
40	1898.6	306.4	40	2471.5	510.3	40	3089.4	779.8
50	1907.9	309.3	50	2481.4	514.3	50	3100.2	784.9
37	1917.1	312.2	47	2491.3	518.2	57	3110.9	790.1
10	1926.4	315.2	10	2501.2	522.2	10	3121.7	795.2
20	1935.7	318.1	20	2511.2	526.1	20	3132.6	800.4
30	1945.0	321.1	30	2521.1	530.1	30	3143.4	805.6
40	1954.3	324.1	40	2531.1	534.2	40	3154.2	810.9
50	1963.6	327.1	50	2541.0	538.2	50	3165.1	816.1
38	1972.9	330.2	48	2551.0	542.2	58	3176.0	821.4
10	1982.2	333.2	10	2561.0	546.3	10	3186.9	826.7
20	1991.5	336.3	20	2571.0	550.4	20	3197.8	832.0
30	2000.9	339.3	30	2581.0	554.5	30	3208.8	837.3
40	2010.2	342.4	40	2591.0	558.6	40	3219.7	842.7
50	2019.6	345.5	50	2601.1	562.8	50	3230.7	848.1
39	2029.0	348.6	49	2611.2	566.9	59	3241.7	853.5
10	2038.4	351.8	10	2621.2	571.1	10	3252.7	858.9
20	2047.8	354.9	20	2631.3	575.3	20	3263.7	864.3
30	2057.2	358.1	30	2641.4	579.5	30	3274.8	869.8
40	2066.6	361.3	40	2651.5	583.8	40	3285.8	875.3
50	2076.0	364.5	50	2661.6	588.0	50	3296.9	880.8
40	2085.4	367.7	50	2671.8	592.3	60	3308.0	886.4
10	2094.9	371.0	10	2681.9	596.6	10	3319.1	892.0
20	2104.3	374.2	20	2692.1	600.9	20	3330.3	897.5
30	2113.8	377.5	30	2702.3	605.3	30	3341.4	903.2
40	2123.3	380.8	40	2712.5	609.6	40	3352.6	908.8
50	2132.7	384.1	50	2722.7	614.0	50	3363.8	914.5

1291

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
61°	3375.0	920.2	71°	4086.9	1308.2	81°	4893.6	1805.3
10'	3388.3	925.9	10'	4099.5	1315.6	10'	4908.0	1814.7
20	3397.5	931.6	20	4112.1	1322.9	20	4922.5	1824.1
30	3408.8	937.3	30	4124.8	1330.3	30	4937.0	1833.6
40	3420.1	943.1	40	4137.4	1337.7	40	4951.5	1843.1
50	3431.4	948.9	50	4150.1	1345.1	50	4966.1	1852.6
62	3442.7	954.8	72	4162.8	1352.6	82	4980.7	1862.2
10	3454.1	960.6	10	4175.6	1360.1	10	4995.4	1871.8
20	3465.4	966.5	20	4188.5	1367.6	20	5010.0	1881.5
30	3476.8	972.4	30	4201.2	1375.2	30	5024.8	1891.2
40	3488.3	978.3	40	4214.0	1382.8	40	5039.5	1900.9
50	3499.7	984.3	50	4226.8	1390.4	50	5054.3	1910.7
63	3511.1	990.2	73	4239.7	1398.0	83	5069.2	1920.5
10	3522.6	996.2	10	4252.6	1405.7	10	5084.0	1930.4
20	3534.1	1002.3	20	4265.6	1413.5	20	5099.0	1940.3
30	3545.6	1008.3	30	4278.5	1421.2	30	5113.9	1950.3
40	3557.2	1014.4	40	4291.5	1429.0	40	5128.9	1960.2
50	3568.7	1020.5	50	4304.6	1436.8	50	5143.9	1970.3
64	3580.3	1026.6	74	4317.6	1444.6	84	5159.0	1980.4
10	3591.9	1032.8	10	4330.7	1452.5	10	5174.1	1990.5
20	3603.5	1039.0	20	4343.8	1460.4	20	5189.3	2000.6
30	3615.1	1045.2	30	4356.9	1468.4	30	5204.4	2010.8
40	3626.8	1051.4	40	4370.1	1476.4	40	5219.7	2021.1
50	3638.5	1057.7	50	4383.3	1484.4	50	5234.9	2031.4
65	3650.2	1063.9	75	4396.5	1492.4	85	5250.3	2041.7
10	3661.9	1070.2	10	4409.8	1500.5	10	5265.6	2052.1
20	3673.7	1076.6	20	4423.1	1508.6	20	5281.0	2062.5
30	3685.4	1082.9	30	4436.4	1516.7	30	5296.4	2073.0
40	3697.2	1089.3	40	4449.7	1524.9	40	5311.9	2083.5
50	3709.0	1095.7	50	4463.1	1533.1	50	5327.4	2094.1
66	3720.9	1102.2	76	4476.5	1541.4	86	5343.0	2104.7
10	3732.7	1108.6	10	4489.9	1549.7	10	5358.6	2115.3
20	3744.6	1115.1	20	4503.4	1558.0	20	5374.2	2126.0
30	3756.5	1121.7	30	4516.9	1566.3	30	5389.9	2136.7
40	3768.5	1128.2	40	4530.4	1574.7	40	5405.6	2147.5
50	3780.4	1134.8	50	4544.0	1583.1	50	5421.4	2158.4
67	3792.4	1141.4	77	4557.6	1591.6	87	5437.2	2169.2
10	3804.4	1148.0	10	4571.2	1600.1	10	5453.1	2180.2
20	3816.4	1154.7	20	4584.8	1608.6	20	5469.0	2191.1
30	3828.4	1161.3	30	4598.5	1617.1	30	5484.9	2202.2
40	3840.5	1168.1	40	4612.2	1625.7	40	5500.9	2213.2
50	3852.6	1174.8	50	4626.0	1634.4	50	5517.0	2224.3
68	3864.7	1181.6	78	4639.8	1643.0	88	5533.1	2235.5
10	3876.8	1188.4	10	4653.6	1651.7	10	5549.2	2246.7
20	3889.0	1195.2	20	4667.4	1660.5	20	5565.4	2258.0
30	3901.2	1202.0	30	4681.3	1669.2	30	5581.6	2269.3
40	3913.4	1208.9	40	4695.2	1678.1	40	5597.8	2280.6
50	3925.6	1215.8	50	4709.2	1686.9	50	5614.2	2292.0
69	3937.9	1222.7	79	4723.2	1695.8	89	5630.5	2303.5
10	3950.2	1229.7	10	4737.2	1704.7	10	5646.9	2315.0
20	3962.5	1236.7	20	4751.2	1713.7	20	5663.4	2326.6
30	3974.8	1243.7	30	4765.3	1722.7	30	5679.9	2338.2
40	3987.2	1250.8	40	4779.4	1731.7	40	5696.4	2349.8
50	3999.5	1257.9	50	4793.6	1740.8	50	5713.0	2361.5
70	4011.9	1265.0	80	4807.7	1749.9	90	5729.7	2373.3
10	4024.4	1272.1	10	4822.0	1759.0	10	5746.3	2385.1
20	4036.8	1279.3	20	4836.2	1768.2	20	5763.1	2397.0
30	4049.3	1286.5	30	4850.5	1777.4	30	5779.9	2408.9
40	4061.8	1293.6	40	4864.8	1786.7	40	5796.7	2420.9
50	4074.4	1300.9	50	4879.2	1796.0	50	5813.6	2432.9

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