1681

DIETZGEN

ENGINEERS
FIELD BOOK
No. 4[illegible]F

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg, Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

1681

CITY ENGINEER'S OFFICE

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

Levels on Reservoir above Switzer dam to Calc. yardage removed since 1943

See F.B. 1637-53

C. Moore

Boggs

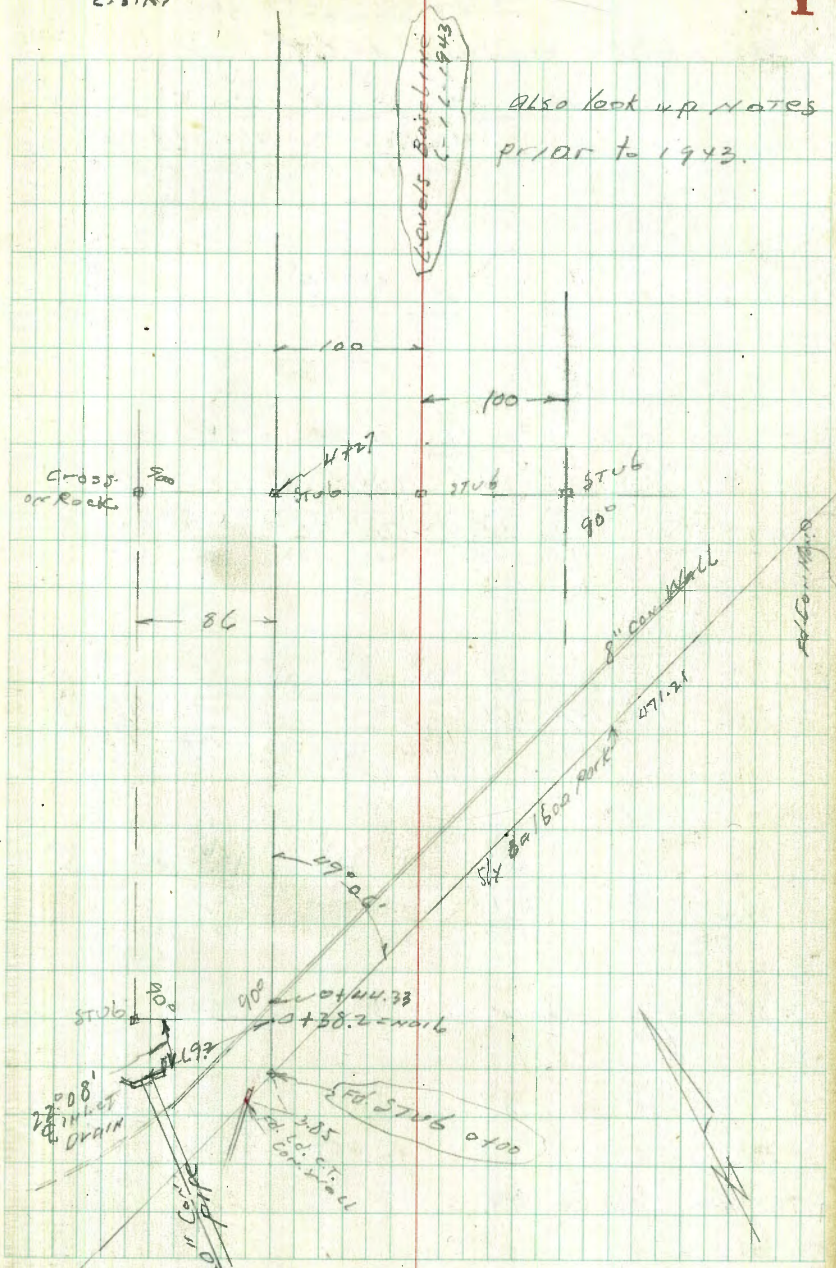
W. Moore

3-2-45.

Levels on same Sta. as 1637-53 & on same Baseline

indexed
C.S.K.

Also look up notes prior to 1943.



LT. = West 60.1

F.L. inlet 5' Pipe drain 10.6

Station									
1+25			66.7	64.5	61.5	59.6	60.9	61.6	64.1
			4.0 / 190	6.2 / 186	9.2 / 170	11.1 / 150	9.8 / 100	9.1 / 70	6.6 / 50
1+00			66.9	61.1	59.7	61.5	61.7	64.3	65.2
			3.8 / 186	9.6 / 175	11.0 / 150	9.2 / 100	9.0 / 84	6.4 / 75	5.5 / 60
T.P.	0.80	70.66	11.74	69.86					
0+75		69.8	64.6	61.4	59.9	61.4	62.1		
		11.8 / 208	17.0 / 200	20.2 / 183	21.7 / 160	20.2 / 125	19.5 / 100		
0+50	69.5	65.0	61.4	59.6	61.1	61.8	66.0	74.5	
	12.1 / 207	16.6 / 203	20.2 / 186	22.0 / 160	20.5 / 140	19.8 / 128	15.6 / 113	10.1 / 100	
0+38.2	69.9	61.5	61.3	62.6	73.8	75.65			
	11.7 / 197	20.1 / 183	20.3 / 160	19.0 / 140	7.8 / 107	5.95 / 107			
					Bot. wall	Top 8" wall			

Top 8" Con. wall above inlet of drain 6.20 ~~75.60~~ 75.40 ←

T.P.	4.53	81.60	1.04	77.07	
T.P.	5.93	78.11	1.95	72.18	
U.S.G.S. Hwy BM std disk	7.61	74.13		66.52	Bldg. NW Cor. 20th + B Cor. Foundation E. of Entrance 1637-54

B.G. Rt. = East

69.6	
1.3 / 40	
69.5	
1.2 / 52	
70.66	
← on dam face	
77.0	
4.6 / 100	rail on dam
Correction	
81.60	

Lt. — B.L. — Rt.

3+35

69.7	64.7	62.3	62.1	62.7	64.2	65.6	66.2	68.7	74.5
1.0 / 178	6.0 / 175	8.4 / 156	8.6 / 100	8.0 / 50	6.5	5.1 / 32	4.5 / 50	2.0 / 100	+3.8 / 150

3+25

64.2	64.6	70.7	71.7	72.5	74.7
6.5	6.1 / 32	0.0 / 39	+1.0 / 50	+1.8 / 100	+4.0 / 150

3+00

70.1	62.7	61.5	61.7	61.7	62.7	63.5	64.7	70.7
0.6 / 179	8.0 / 174	9.2 / 157	9.0 / 100	9.0 / 75	8.0 / 40	7.2	6.0 / 27	0.0 / 31

2+50

70.5	64.0	61.4	60.7	61.5	62.1	64.0	64.7	69.7
0.2 / 185	6.7 / 175	9.3 / 153	10.0 / 130	9.2 / 100	8.6 / 40	6.7	6.0 / 15	1.0 / 18

2+00

70.7	64.1	61.1	59.8	61.0	61.7	62.7	65.1	69.5
0.0 / 190	6.6 / 181	9.6 / 155	10.9 / 150	9.7 / 100	9.0 / 40	8.0 / 25	5.6 / 10	1.2

1+50

65.8	63.0	61.1	59.7	60.8	61.7	64.9	69.5
4.9 / 188	7.7 / 184	9.6 / 168	11.0 / 150	9.9 / 100	9.0 / 55	5.8 / 35	1.2 / 27

outside Rods to Rt + Lt = Top of present borrow

70.66 — 70.66

LT | B.L. | RT

4+87

LT	out		
B.L.	63.7 / 7.0	64.6 / 6.1 / 73	72.7 / +2.0 / 83

4+64

LT	out			
B.L.	64.1 / 6.6	64.5 / 6.2 / 65	71.8 / +0.9 / 74	75.7 / +5.0 / 92

4+50

70.0 / 0.7 / 144	63.7 / 7.0 / 139	62.0 / 8.7 / 129	62.1 / 8.6 / 100	63.2 / 7.5 / 50
64.5 / 6.2	64.7 / 6.0 / 67	70.7 / 0.0 / 71	72.0 / +1.3 / 100	77.2 / +6.5 / 110

4+27 — This was Baseline so Skip it

70.1 / 0.6 / 142	63.9 / 6.8 / 138	61.8 / 8.9 / 132	62.1 / 8.6 / 100	62.7 / 8.0 / 50	
64.7 / 6.0	64.3 / 6.4 / 47	66.7 / 4.0 / 53	70.7 / 0.0 / 64	70.0 / 0.7 / 105	75.2 / +4.5 / 112

4+00

72.5 / +1.8 / 176	67.3 / 3.4 / 173	65.9 / 4.8 / 155	61.8 / 8.9 / 134	62.3 / 8.4 / 100	62.7 / 8.0 / 50	63.5 / 7.2 / 15
64.4 / 6.3	65.7 / 5.0 / 50	70.4 / 0.3 / 85	71.2 / +0.5 / 121	76.2 / +5.5 / 127		

3+50

70.1 / 0.6 / 178	65.7 / 5.0 / 173	64.2 / 6.5 / 160	62.9 / 7.8 / 156	61.6 / 9.1 / 130	61.8 / 8.9 / 100	62.8 / 7.9 / 50
64.2 / 6.5	66.1 / 4.6 / 50	69.7 / 1.0 / 100	74.7 / +4.0 / 150			

70.66 | 70.66

LT. — B.L. — RT.

Station	LT.					
7+00	Missed before					
6+50		69.4 ✓ 1.3/116	62.0 ✓ 8.7/112	61.7 ✓ 9.0/102	62.7 ✓ 8.0/100	63.2 ✓ 7.5/50
6+00		70.2 ✓ 0.5/125	62.0 ✓ 8.7/116	62.2 ✓ 8.5/100	63.0 ✓ 7.7/94	63.0 ✓ 7.7/50
5+50		69.0 ✓ 1.7/126	62.1 ✓ 8.6/121	62.3 ✓ 8.4/96	62.9 ✓ 7.8/93	63.0 ✓ 7.7/50
5+25		69.1 ✓ 1.6/130	62.1 ✓ 8.6/120	63.1 ✓ 7.6/95	62.5 ✓ 8.2/55	
5+00	69.9 ✓ 0.8/144	64.1 ✓ 6.6/136	62.2 ✓ 8.5/123	62.2 ✓ 8.5/100	62.9 ✓ 7.8/95	63.1 ✓ 7.6/50

70.66

Station	B.L.	RT.					
7+00	63.1 ✓ 7.6	62.9 ✓ 7.8/35	59.2 ✓ 11.5/60	62.9 ✓ 7.8/82	68.4 ✓ 2.3/90	69.2 ✓ 1.5/102 Toe	82.9 ✓ +12.2/122 Shoulder
6+50	64.1 ✓ 6.6	63.5 ✓ 7.2/50	61.0 ✓ 9.7/65	63.6 ✓ 7.1/85	66.0 ✓ 4.7/110 Toe	82.2 ✓ +11.5/131 Shoulder	
6+00	63.5 ✓ 7.2	63.6 ✓ 7.1/50	65.6 ✓ 5.1/103 Toe Fill	81.7 ✓ +11.0/128 = Shoulder of Fill			
5+50	63.3 ✓ 7.4	64.0 ✓ 6.7/85	71.6 ✓ +0.9/95	75.3 ✓ +4.6/105			
5+25	63.1 ✓ 7.6	64.3 ✓ 6.4/78	70.6 ✓ 0.1/86	71.2 ✓ +0.5/107	76.2 ✓ +5.5/110		
5+00	63.6 ✓ 7.1	64.3 ✓ 6.4/67	67.4 ✓ 3.3/73	71.5 ✓ +0.8/100	75.9 ✓ +5.2/105		

70.66

6+00 to 7+00 = Recent Fill
over old borrow cut

Station											
9+00	Lt 76.1 / +1.0 / 107	65.0 / 10.1 / 99	65.9 / 9.2 / 78	66.0 / 9.0 / 50	B.L. 66.3 / 8.8	67.9 / 7.2 / 40	73.1 / 2.0 / 48	77.2 Rt / +2.1 / 78 Toe	87.2 / +12.1 / 95 Shoulder		
8+85	75.4 / +0.3 / 108	65.0 / 10.1 / 101	66.0 / 9.1 / 77	65.7 / 9.4 / 50	65.8 / 9.3	66.5 / 8.6 / 34	70.4 / 4.7 / 42	70.1 / 5.0 / 70	77.1 / +2.0 / 84 Toe	87.1 / +12.0 / 99 Shoulder	
8+50	75.1 / 0.0 / 110	64.3 / 10.8 / 101	65.6 / 9.5 / 79	64.9 / 10.2 / 50	65.0 / 10.1	64.4 / 10.7 / 40	69.3 / 5.8 / 48	68.9 / 6.2 / 81 Toe	85.6 / +10.5 / 104 Shoulder		
8+00	74.6 / 0.5 / 110	63.7 / 11.4 / 104	64.7 / 10.4 / 80	64.9 / 10.2 / 50	63.9 / 11.2	62.6 / 12.5 / 58	68.8 / 6.3 / 62	70.1 / 5.0 / 87 Toe	84.7 / +9.6 / 110 Shoulder		
7+75	74.7 / 0.4 / 109	63.1 / 12.0 / 105	63.1 / 12.0 / 83	64.5 / 10.6 / 78	63.8 / 11.3 / 50	63.5 / 11.6	62.9 / 12.2 / 12	60.1 / 15.0 / 20	62.6 / 12.5 / 64	68.1 / 7.0 / 67	70.1 / 5.0 / 95 Toe; 85.3 / +10.2 / 119 Shoulder
7+50	74.1 / 1.0 / 110	62.9 / 12.2 / 105	64.1 / 11.0 / 80	63.8 / 11.3 / 50	63.5 / 11.6	62.9 / 12.2 / 21	59.9 / 15.2 / 30	62.5 / 12.6 / 74	68.8 / 6.3 / 80	69.8 / 5.3 / 98 Toe	85.2 / +10.1 / 122 Shoulder

T.P. 9.23 75.12 4.77 65.89 — 75.12

Recent High water Mark 1.36 69.30

70.66

Lt

		78.3	68.9	68.6	67.2	73.1
11+50		3.3 / 96	12.7 / 90	13.0 / 53	14.4 / 28	8.5 / 25
I.P.	7.2%	81.57	0.79	74.33		
		78.1	68.2	67.8	72.5	
11+00		+3.0 / 92	6.9 / 89	7.3 / 33	2.6 / 30	
		78.4	66.9	67.0	71.5	
10+50		+3.3 / 95	8.2 / 88	8.1 / 38	3.6 / 35	
		77.2	65.9	66.6	70.5	
10+00		+2.1 / 100	9.2 / 94	8.5 / 44	4.6 / 39	
9+55						
		76.6	66.3	64.7	66.1	67.3
9+50		+1.5 / 104	8.8 / 99	10.4 / 87	9.0 / 74	7.8 / 50
		75.1				

B.L. Pt.

	74.4	74.6	77.5	80.2	81.3	92.6
	7.2	7.0 / 51	4.1 / 56	1.4 / 95	0.3 / 117	+11.0 / 127
	81.57					
	73.3	74.1	79.1	81.8	84.4	92.3
	1.8	1.0 / 51	+4.0 / 57	+6.7 / 100	+9.3 / 130	+17.2 / 138
	71.3	73.0	78.8	80.2	82.2	88.3
	3.8	2.1 / 53	+3.7 / 55	+5.1 / 100	+7.1 / 118	+13.2 / 132
	70.2	72.2	76.6	79.9	81.5	87.7
	4.9	2.9 / 45	+1.5 / 52	+4.8 / 69	+6.4 / 111	+12.6 / 138
	68.5	69.8	76.1	79.9	81.3	87.8
	6.6	5.6 / 30	+1.0 / 39	+4.8 / 81	+6.2 / 105	+12.4 / 131
	69.1	69.1	76.1	80.9	81.5	87.5
	7.0	6.0 / 31	+1.0 / 41	+5.3 / 81	+6.4 / 106	+12.4 / 121
	75.1					

			LT.			B.L.	RT.	
I.P.	12.40	91.53	2.44	79.13				
				82.7 ✓	76.1 ✓	76.4 ✓	77.1 ✓	78.7 ✓	82.1 ✓
13+50				+1.1	5.5	5.2	4.5	3.4	+0.5
				51	44	33		52	Co
				79.4 ✓	75.6 ✓	75.5 ✓	76.6 ✓	76.8 ✓	81.9 ✓
13+00				2.2	6.0	6.1	5.0	4.8	+0.3
				75	50	17		67	7x
				79.8 ✓	73.9 ✓	75.3 ✓	76.0 ✓	76.3 ✓	80.6 ✓
12+50				1.8	7.7	6.3	5.0	5.3	1.0
				71	62	37		62	67
				79.6 ✓	74.4 ✓	70.8 ✓	75.6 ✓	76.0 ✓	76.0 ✓	80.3 ✓	82.5 ✓	85.7 ✓	92.6 ✓
12+35				2.0	7.2	10.8	6.0	5.0	5.6	1.3	+0.9	+4.1	+11.0
				71	63	50	22	60	46	100	114	116
			75.6 ✓	68.5 ✓	79.1 ✓	72.0 ✓	69.2 ✓	70.1 ✓	76.0 ✓	76.1 ✓						
12+22			6.0	13.1	2.5	9.6	12.8	11.5	5.6	5.5						
			106	105	77	66	58	44	19							
			75.5 ✓	67.0 ✓	69.0 ✓	68.1 ✓	74.4 ✓	75.3 ✓	76.0 ✓	79.3 ✓	80.0 ✓	81.0 ✓	92.5 ✓
12+00			6.1	14.6	12.6	13.5	7.2	6.3	5.6	2.3	1.6	0.6	+10.9
			107	106	85	65	16		54	60	95	118	12 ✓
		81.57						81.57					

	LT			B.L.	RT					
check to B.M. B.P. Top Pillar on Cobble Bridge Pershing Dr. + Florida	1.67	89.86	89.88							
16+00				92.2 / +0.7	85.4 / 6.1 / 11	92.4 / +0.9 / 19	91.7 / +0.2 / 31	85.3 / 6.2 / 42	84.8 / 6.7 / 75	90.9 / 0.6 / 78
15+50			89.3 / 2.2 / 2	85.9 / 5.6	83.2 / 8.3 / 5	81.5 / 10.0 / 26	82.0 / 9.5 / 49	88.6 / 2.9 / 56	89.7 / 1.8 / 100	
15+00		84.2 / 7.3 / 21	80.3 / 11.2 / 17	78.7 / 12.8	81.1 / 10.4 / 37	85.1 / 6.4 / 41	89.4 / 2.1 / 100			
14+50	85.2 / 6.3 / 39	79.6 / 11.9 / 31	78.3 / 13.2 / 20	79.5 / 12.0	80.3 / 11.2 / 22	84.7 / 6.8 / 30	84.9 / 6.6 / 50	85.3 / 6.2 / 73	88.5 / 3.0 / 90	
14+00	84.0 / 7.5 / 41	76.5 / 15.0 / 34	76.9 / 14.6 / 17	79.0 / 12.5	79.2 / 12.3 / 13	81.0 / 10.5 / 16	81.1 / 10.4 / 40	82.8 / 8.7 / 54	87.7 / 3.8 / 65	
13+80	83.4 / 8.1 / 44	76.6 / 14.9 / 40	76.7 / 14.8 / 25	78.8 / 12.7	79.5 / 12.0 / 10	79.4 / 12.1 / 50	85.8 / 5.7 / 60	87.7 / 3.8 / 70		

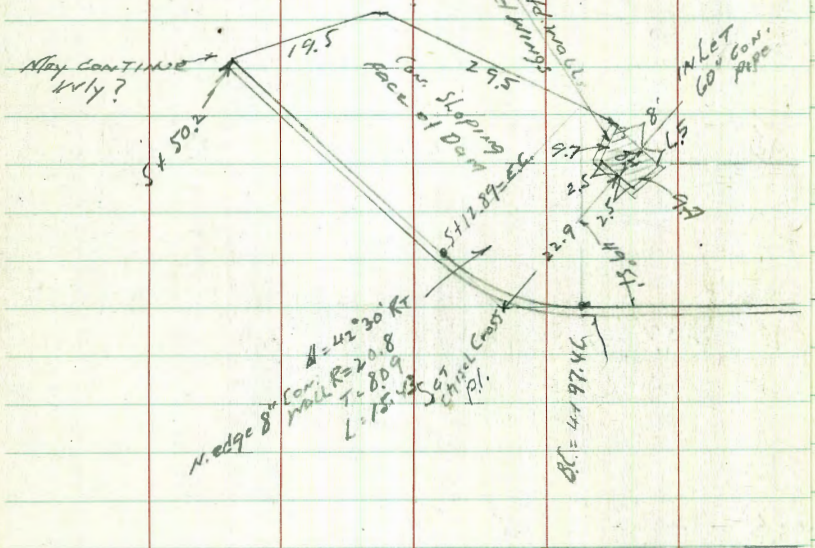
91.53

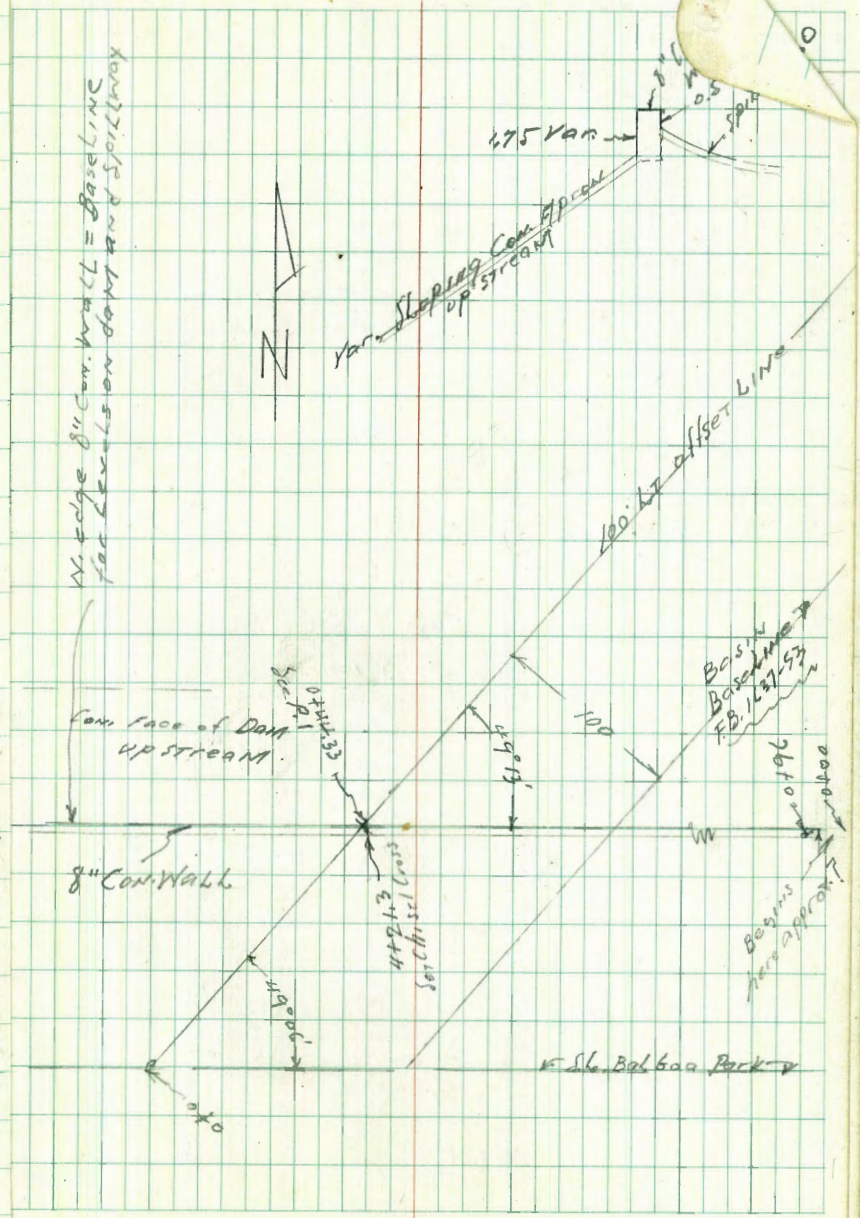
91.53

C. Moore
Sanitation Engrs
W. Moore
3-27-45.

Additional Levels on Switzer Dam Spillway and Basin.

34' = Average width of dam on top E of Spillway.





Levels on dam and Spillway, Sketch P.10

1+50

0+96 Pt. on wall where it was exposed
However wall begins East of this

0+88

0+50

0+07 Base of Hill slope

Sections at 90° from B.L.

0+0

Sec p.v 9.06 84.71 75.65 Top wall at 107 Lt of 0+38v

Lt = S B.L. Rt = N

80.4	80.1	75.7	74.3	71.5	71.1	71.0
4.3	4.6	9.0	10.4	13.2	13.6	13.7
20	6	Top Wall	0.05	4	15	30

80.9	80.4	75.7	72.5	71.7
3.8	4.3	9.0	12.2	13.0
20	8	Top Wall	4	30

81.1	80.6	79.7	79.5	73.6	72.6
3.6	4.1	5.0	5.2	11.1	12.1
20	10		14	20	30

80.6	80.7	79.8	76.7
4.1	4.0	4.9	8.0
20	10		30

84.0	84.6	79.6	79.5
0.7	4.1	5.1	5.2
20	10		30 ℄ Rd.

84.7	82.0	83.6	82.4	79.4	79.7
+1.0	2.7	1.1	2.3	5.3	5.0
20	15	10		9	40 ℄ Rd.

84.71

	Lt	BL. Top Wall	Rt
4+13	78.4 / 6.3 / 20	78.5 / 6.7 / 6	75.7 / 9.0
4+00	78.6 / 6.1 / 20	80.7 / 4.0 / 6	75.7 / 9.0
3+50	79.0 / 5.7 / 20	79.0 / 5.7 / 5	75.7 / 9.0
3+00	79.5 / 5.2 / 20	79.2 / 5.5 / 6	75.7 / 9.0
2+50	80.0 / 4.7 / 20	79.1 / 5.6 / 6	75.7 / 9.0
2+00	80.1 / 4.6 / 20	80.1 / 4.6 / 7	75.7 / 9.0

73.8 / 10.9 / 0.05	6.50 / 19.7 / 14 Cont. Approx	6.23 / 22.4 / 24	6.17 / 23.0 / 30			
73.7 / 11.0 / 0.05	6.68 / 17.9 / 11 Cont. Approx	6.42 / 2?.6 / 19	6.20 / 27.7 / 30			
73.7 / 11.0 / 0.05	7.00 / 14.7 / 7	6.90 / 15.7 / 19	6.51 / 19.6 / 23 Approx	6.45 / 20.2 / 30		
73.7 / 11.0 / 0.05	6.95 / 15.2 / 8	6.90 / 15.7 / 15	6.90 / 15.7 / 27 Cont. Approx	6.46 / 20.1 / 33		
73.7 / 11.0 / 0.05	6.97 / 15.0 / 7	6.94 / 15.3 / 15	6.94 / 15.3 / 30			
73.7 / 11.0 / 0.05	7.02 / 14.5 / 6	6.94 / 15.0 / 15	6.99 / 14.8 / 30			

8471

8471

Top 8" wall inside P.I. 9.31 75.40 chisel square
See Correction P.r

Station	Readings (Lt → B.L. Top Wall → Rt): elevation, rod / distance													
4+97.46 B.C. Rt.	72.34 12.37/20	73.29 11.42/10	73.85 10.86/4	74.16 10.55/25	74.81 9.90/0.7	75.33 9.38	73.57 11.14/0.05	69.9 14.8/9	68.3 16.4/14	63.9 20.8/29.8	60.7 24.0/30 Mud			
4+75	72.56 12.15/20	73.46 11.25/10	74.04 10.67/4	74.29 10.42/2.5	74.93 9.78/0.7	75.44 9.27	73.88 10.83/0.05	63.8 20.9/12	61.7 23.0/22	61.4 23.3/30				
4+50	75.0 9.7/35	76.99 7.72/31	74.19 10.52/24	73.96 10.75/22	73.96 10.75/12	74.29 10.42/10	74.47 10.24/2.5	75.04 9.67/0.7	75.58 9.13	73.81 10.90/0.05	65.0 19.7/14	64.1 22.6/23	60.7 24.0/30	
4+39	78.1 6.6/32	78.5 6.2/24	75.59 9.12/17	74.7 10.0/2.5	75.10 9.61/0.7	75.59 9.12	73.79 10.92/0.05	66.7 18.0/11	61.6 23.1/22	61.3 23.4/30				
4+32	78.5 6.2/30	78.4 6.3/20	76.86 7.85/15	75.64 9.07/0.7	75.66 9.05	73.8 10.9/0.05	66.2 18.5/12	62.7 22.0/19	61.7 23.0/25	61.7 23.0/30				
4+21.3 Beg. of Spillway and Int. with 100' Lt. Line of Basin Levels	78.3 6.4/20	78.1 6.6/7	75.7 9.0	73.9 10.8/0.05	65.5 19.2/13	62.5 22.2/22	61.9 22.8/30							

Notes: on apron; edge apron (4+97.46). apron (4+75, 4+50, 4+39, 4+32, 4+21.3).

84.71

84.71

I.P.	4.19	79.59	9.31	75.40	Top 8"
5+50.x	end of 8" wall may extend further West				
5+26					
5+18					
5+09					

84.71

Lt. B.L. Rt.

Top Wall

Con. wall inside of P.I. chiseled square

	80.5	80.4	75.9	75.7		74.5	73.4	68.5	72.5
	4.7 / 15	4.3 / 8	8.8	8.8 / 4.05 dirt		10.7 / 5 dirt	11.3 / 15	16.7 / 20	12.7 / 27

In wash from West

76.0	76.2	80.2	75.60	74.3	64.7	61.5	
8.7 / 20	8.5 / 16	4.5 / 7	9.11	10.4 / 4.05 dirt	20.0 / 24.6 Edge Apron	23.2 / 24.7	Mud

74.54	74.5	74.9	77.67	75.54	74.4	67.9	63.7	60.7
10.17 / 21	10.2 / 15	9.8 / 11	7.04 / 4	9.17	10.3 / 0.95 dirt on apron	16.8 / TC	21.0 / 27.9 Edge apron	24.0 / 28 Mud

73.44	73.6	74.1	75.04	75.44	73.84	67.4	62.1	60.0
11.27 / 20	11.1 / 10	10.6 / 4.5	9.67 / 4.7	9.27	10.87 / 0.95	17.4 / 17 apron	22.7 / 30.5 on Con. apron	24.7 / 30.6 Mud End W. Wing Wall of INLET

84.71

Additional Basin Levels
Left of Baseline

Reduced + plotted on Sections

	Lt.	B.L.
1+50	79.1	66.6
	0.5	13.0
	212	196
1+25	79.0	68.9
	0.9	10.7
	220	196
1+00	78.7	70.3
	0.9	9.3
	223	206
0+75	79.3	
	0.6	
	217	
0+50	79.1	
	0.5	
	223	
0+38.2	78.8	76.8	70.5
	0.8	2.8	9.1
	222	218	205

79.59 Final

79.59

additional levels to left

4+00				
T.P.	6.13	80.54	5.16	74.43
3+50				
3+25				
3+00				
2+50				
2+00				

79.59

Lt. Bk.

80.8 — 74.0
+0.7 — 6.6
199 — 186

80.54
79.6 — 71.0
0.0 — 8.6
203 — 189

79.6 — 70.4
0.0 — 9.2
206 — 190

79.8 — 71.1
+0.7 — 8.7
208 — 193

79.6 — 72.2
0.0 — 7.4
208 — 197

79.6
0.0
209

79.59

Levels to left.

L+50

L+00

5+50

5+25

5+00

4+50

8056

Lt B.L.

803
0.3
141

806
0.0
147

806 766
0.0 4.0
177 170

798 750
0.8 5.6
178 168

806 743
0.0 6.3
178 175

798 748
1.4 6.4
189 180

8056

Levels to Left.

T.P	7.27	81.46	6.37	74.19
8+00				
7+75				
7+50				
7+00				

See p. 5 This was Missed before

80.6	74.6	72.8
6.0	6.0	7.8
104	150	117

Borrow Cut

80.56

Lt. Bl.

80.6
0.0
100

80.6
0.0
104

80.6
0.0
103

62.6	63.0	64.3	63.6	63.2
100	17.6	16.3	17.0	17.4
108	78	46	50	

80.56

Additional Levels To Rt. of Baseline and Lt.

Reduced + Plotted on Sections

2+00

1+50

1+25

1+00

0+75

0+50

81.4L

Lt. Bl. Rt.

13.7	15.7	19.9
7.8	5.8	1.6
77	77	86
Base	Wall	dam

13.7	15.7	19.7
7.8	5.8	1.8
21.6	21.6	3.4
Base Wall	Top Wall	Top dam

11.8	13.7	15.7	19.4
11.7	7.8	5.8	2.4
21	7	7	3
	Base	Wall	dam

10.0	13.7	15.7	19.3
11.5	7.8	5.8	2.2
47	35	35	27
	Base	Wall	dam

6.4	13.7	15.7	18.8
17.3	7.8	5.8	2.7
90	64.2	64.2	55
	Base	Wall	dam

13.7	15.7	18.8
7.8	5.8	2.7
93.5	93.5	85
Base Wall	Top Wall	Top dam

81.4L

check B.M.	USGS	Hub	4.83	66.53	66.52 P.V.
T.P.	6.17	71.36	10.57	65.19	
T.P. chisel □	0.36	75.76	9.05	75.40	
check to chisel □	See P.IV		9.05	75.40	=
T.P.	3.42	84.45	0.43	81.03	

3 + 50

3 + 35

3 + 00

2 + 50

81.46

Top 8" walk inside Pl. on dam Spillway

78.7 — 7.8 / 175 — 79.5 — 7.0 / 200 Rd

78.0 — 3.5 / 175 — 79.3 — 2.7 / 200 Rd

77.5 — 4.0 / 158 edge Fill — 78.3 — 3.2 / 175 Filled Acre — 79.4 — 2.1 / 200 Rd.

73.1 — 8.4 / 142 — 79.7 — 1.8 / 155 Top dam dirt

81.46

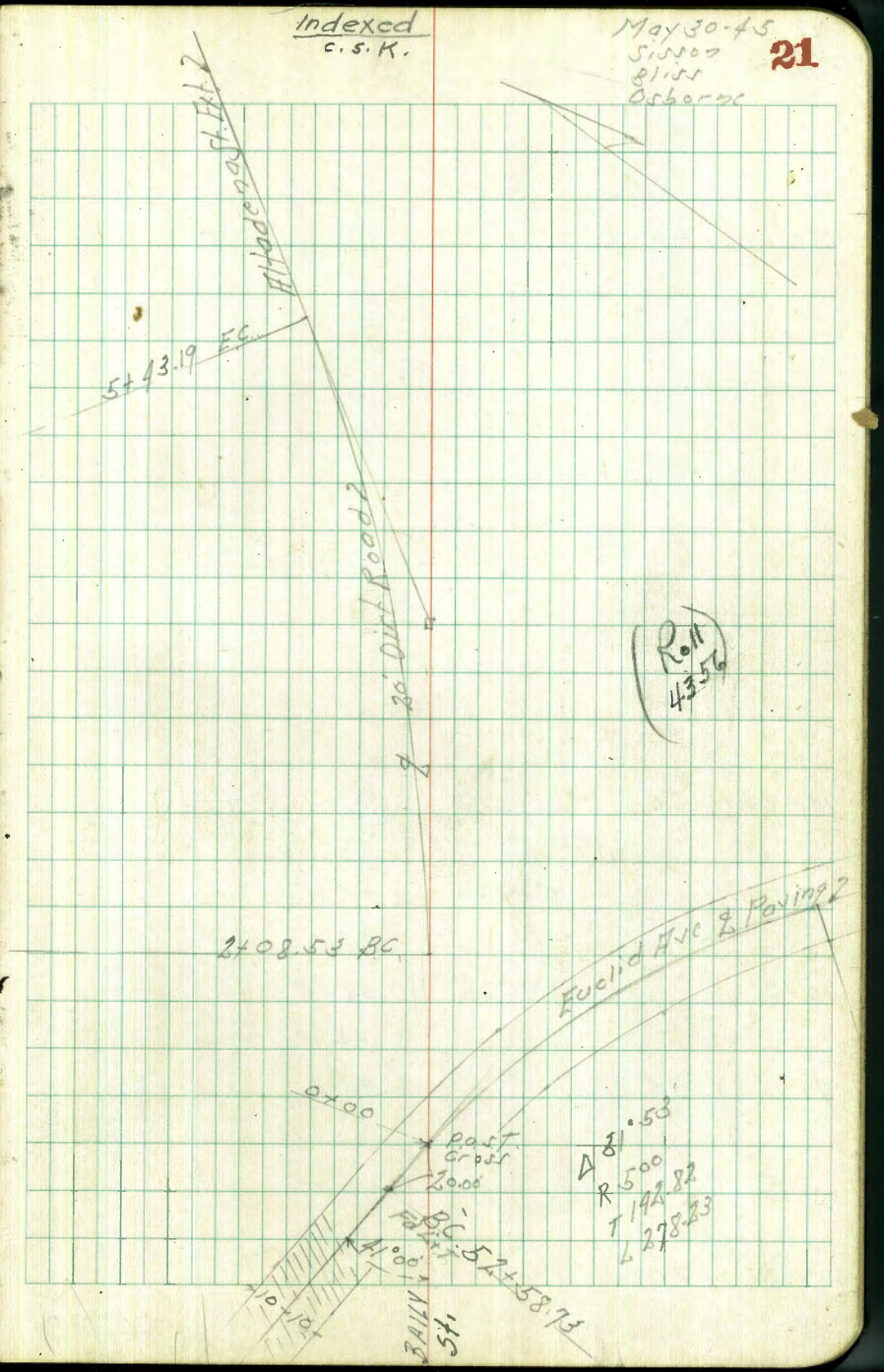
Alignment of Altadena St. Ext.
From Euclid Ave. to Altadena & Sterling Court

5+43.19	E.C.	11°16.75'	
5+0		9°49.40'	
+50		8°08.29'	Δ 22°33.30'
			R 850'
4+0		6°27.18'	T 169.52
			L 334.66
+50		4°46.07'	
3+0		3°04.96'	
+50		1°23.85'	
2+08.53	B.C. Lt.		
0+0			

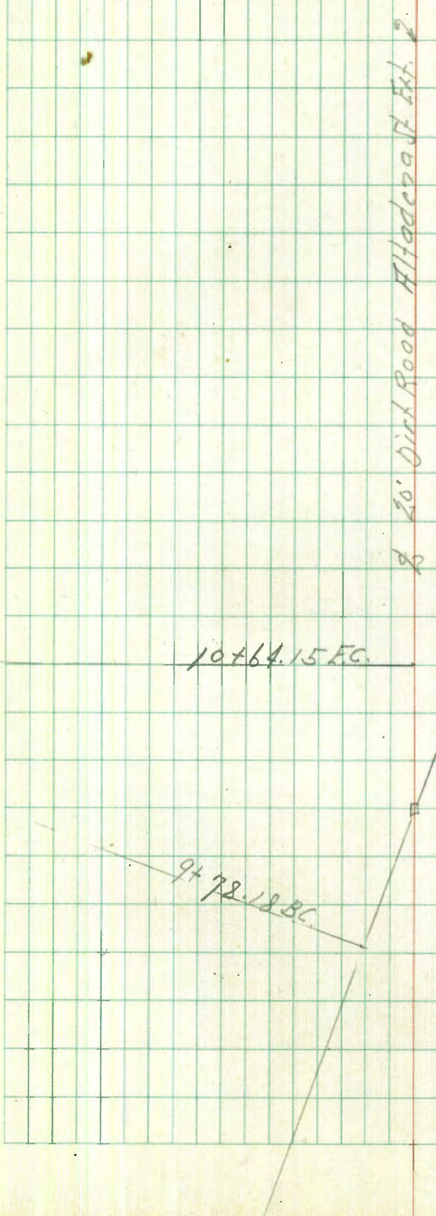
Indexed
C. S. K.

May 30-45
Sisson
Bliss
Osborne

21

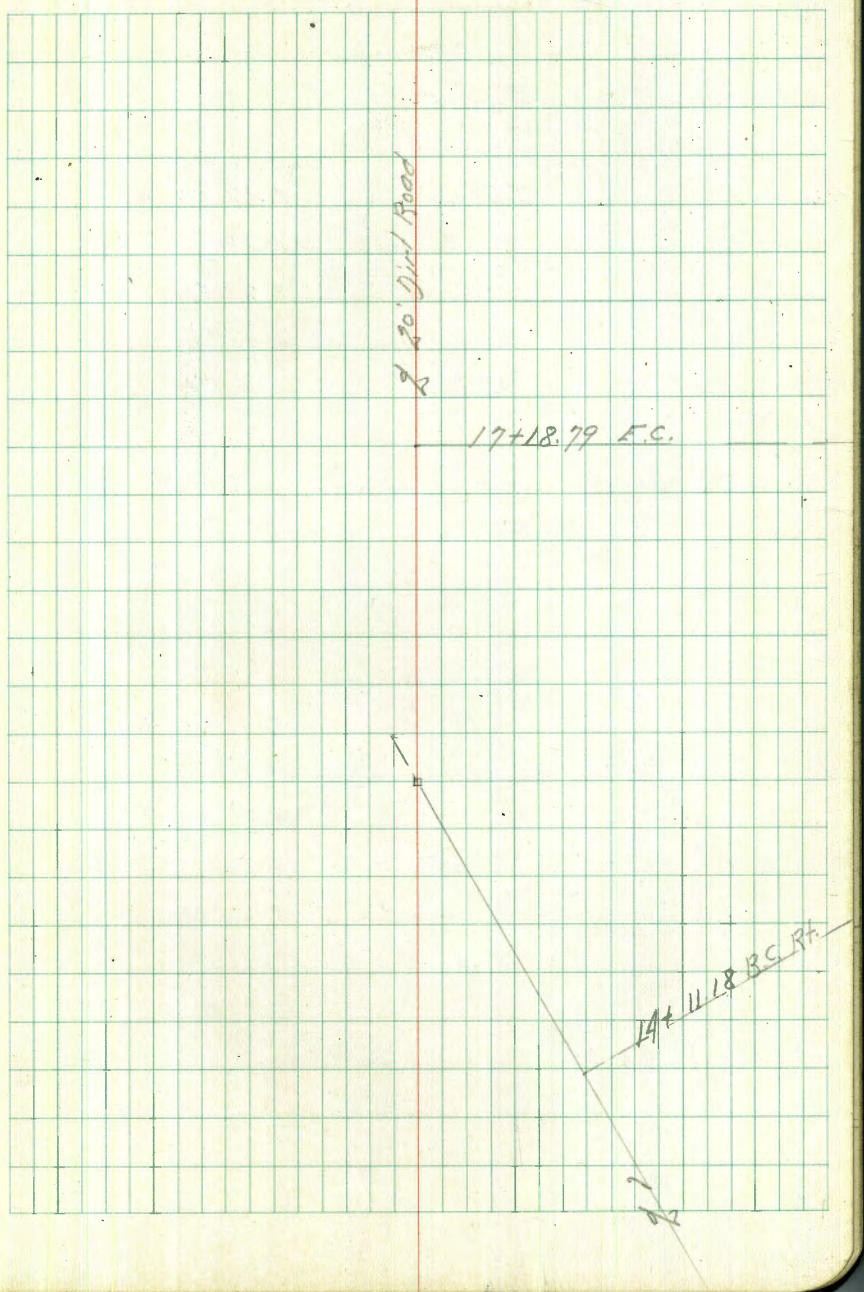


14+11.18	B.C. Rt.		
10+64.15	E.C.	10°15.75'	
+50		8°34.39'	Δ 20°31'30"
			R 240.0
10+0		2°36.28'	T 43.45
			L 85.97
9+78.18	B.C. Lt.		D 7.162
5+43.19	E.C.		

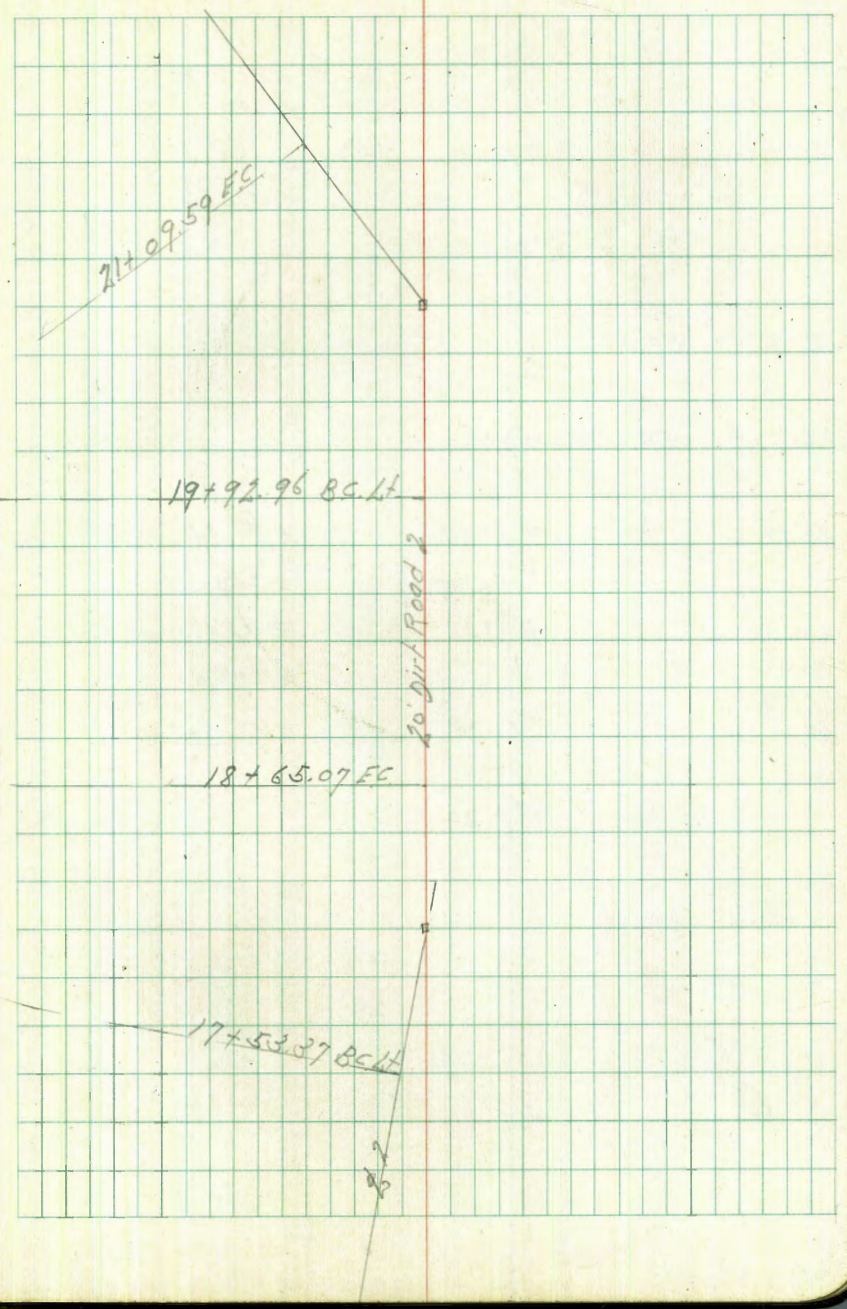


17+52.87 B.C. Lt.

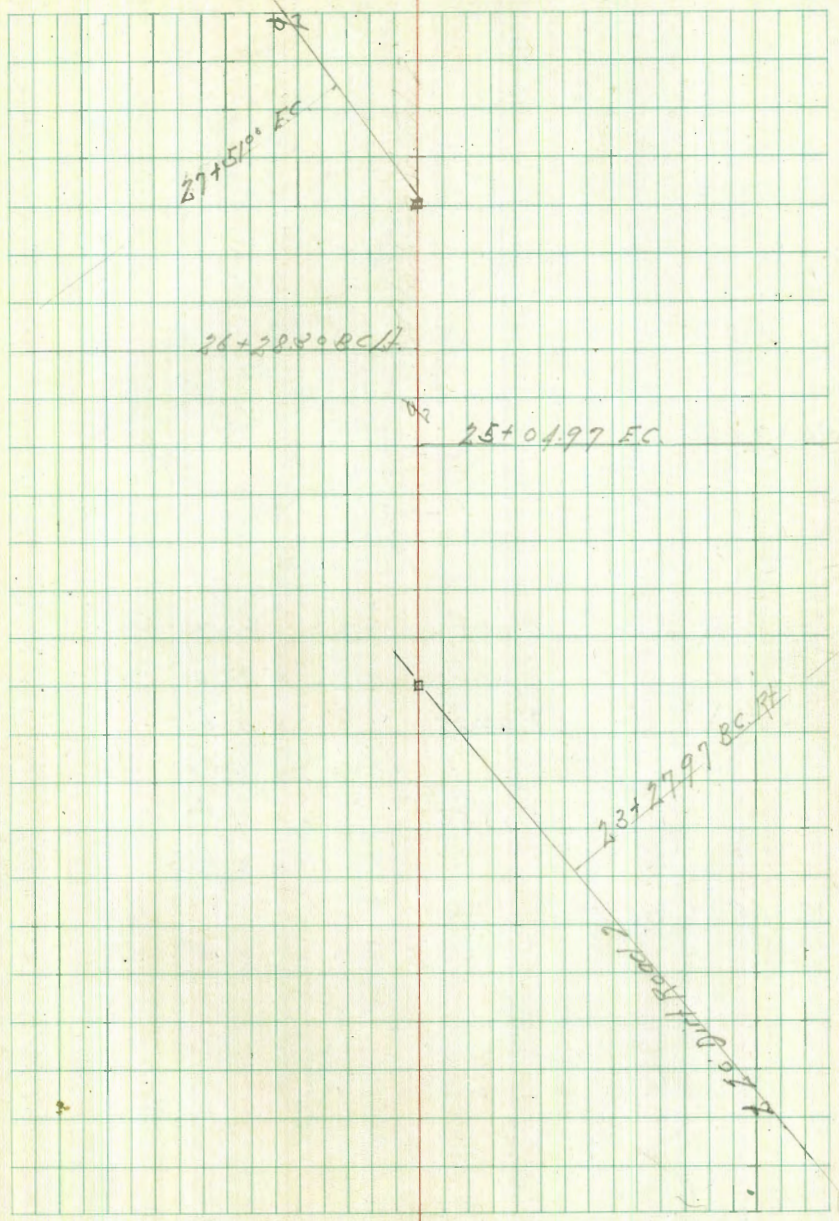
17+18.79	E.C.	14°41.25'	
17+0		13°47.12'	Δ 29°22'30"
+50		11°24.18'	R 600'.
			T 157.27
16+0		9°00.94'	L 307.61
			D 2.865
+50		6°37.70'	
15+0		4°14.46'	
+50		1°51.22'	
14+11.18	B.C. Rt.		



21+09.59	EC.	18° 33.75'	
21+0		17° 02.12'	Δ 37° 07' 30"
			R 180'
+50		9° 04.67'	T 60.49
			L 116.63
20+0		1° 07.22'	D 9.549
19+92.96	BC. Lt.		
18+65.07	EC.	4° 00'	
			Δ 8° 00
+50		2° 27.65'	R 800'
			T 55.94
18+0		1° 40.21'	L 111.70
			D 2.149
17+53.37	B.C. Lt.		



27+51.00	EC.	17°24.50'	
			Δ 55°09
			R 200'
27+0		10°16.20'	T 63.35
			L 122.90
			D 8.594
+50		5°06.50'	
26+28.50	BC. Lt		
25+04.97	EC.	20°17'	
25+0		19°42.88'	Δ 40°34'
			R 250'
+50		13°59.08'	T 92.40'
			L 177.00'
24+0		8°15.28'	D 6.876
+50		2°31.48'	
23+27.97	BC. Rt		



30+44.81

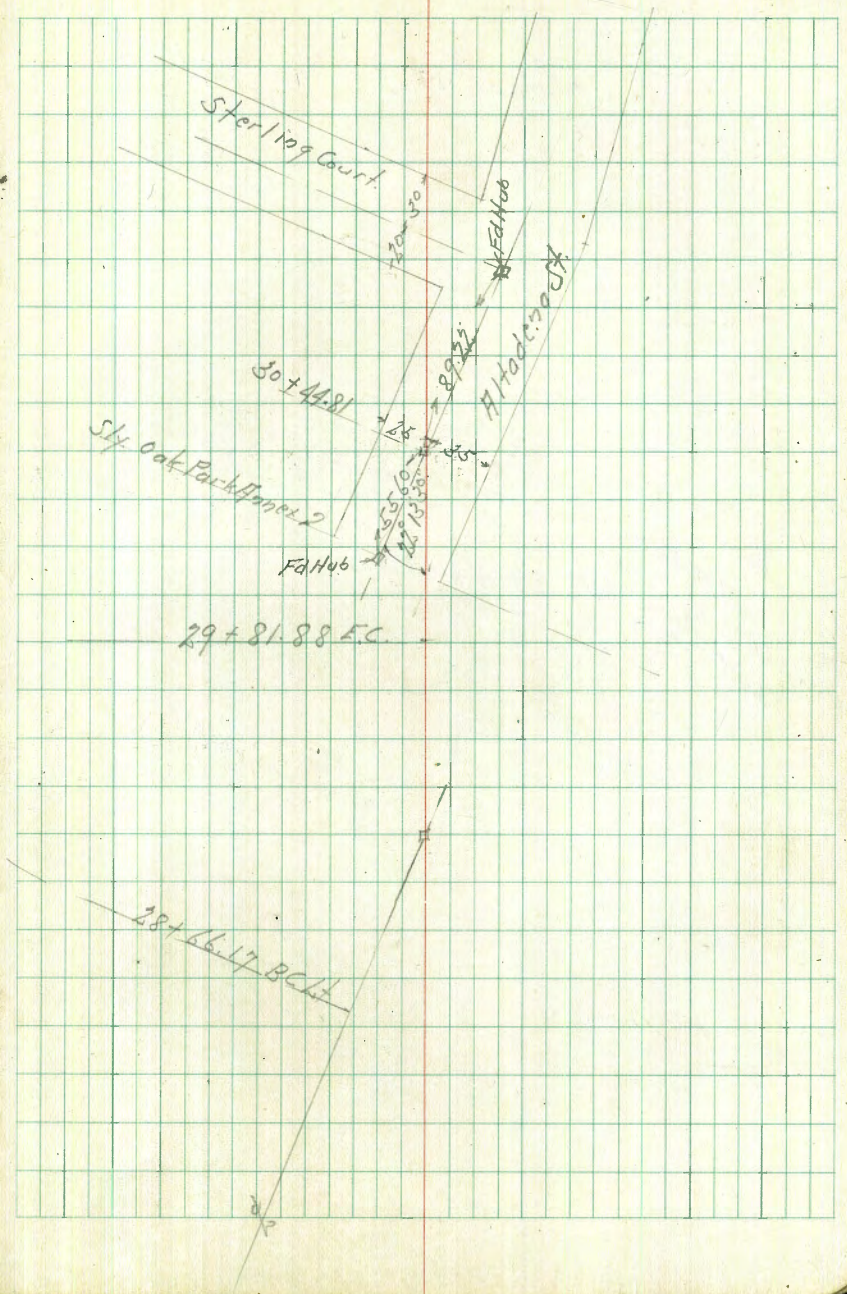
29+81.88 E.C. 11° 03'

+.50 8° 00.35

29+0 3° 13.85

28+66.17 B.C. Lt.

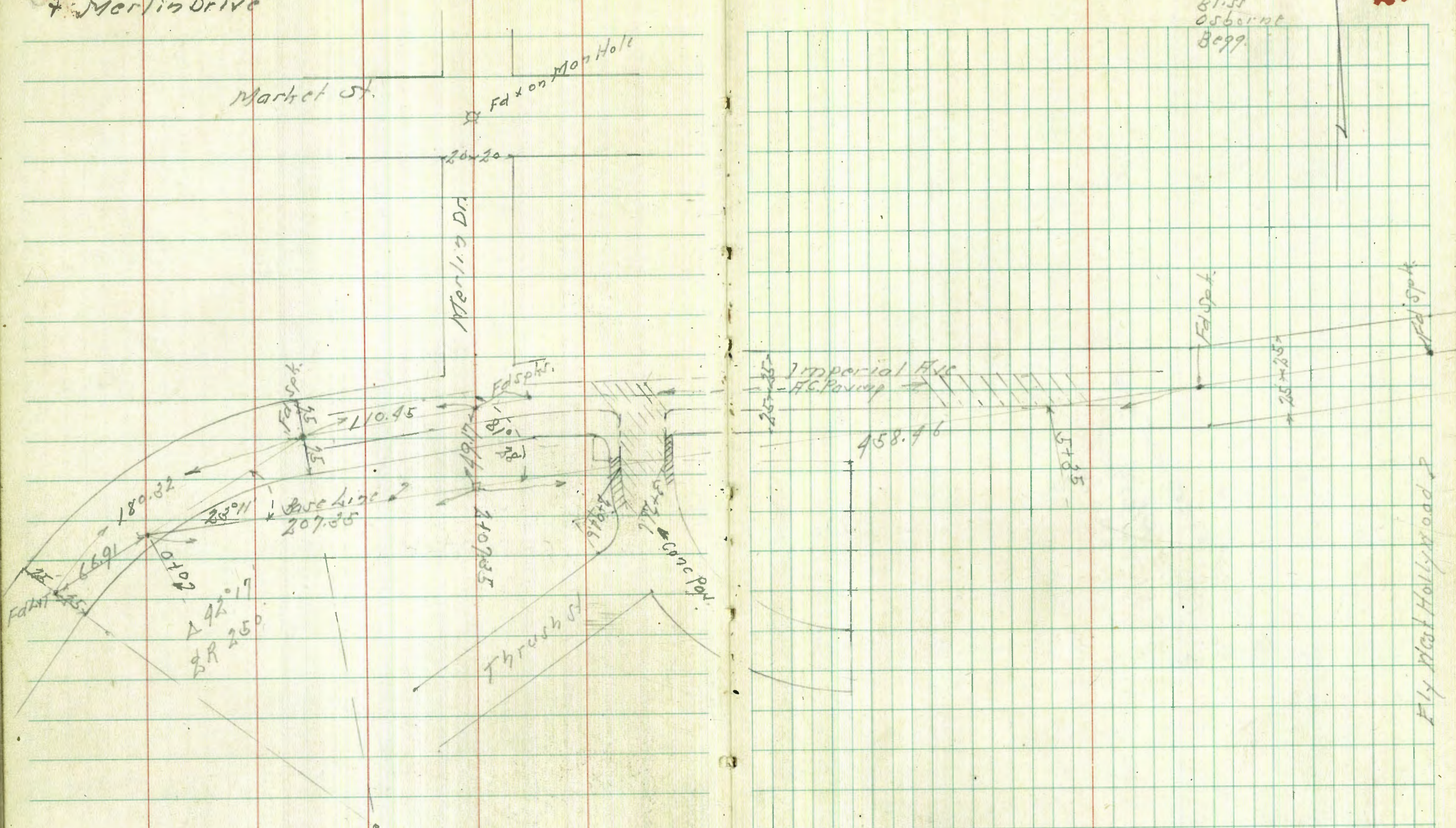
Δ 22° 06'
R 300
T 58.58
L 115.71
D 5.73



Proposed Opening Imperial Ave. & Merlin Drive

Indexed
C.S.K.

May 3-1945
Sisson
Bliss
Osborne
Begg



Cross Section Area South of Imperial Ave
At Merlin
Sketch Page 27

Station						Lt. N		B	Rt. S
1+0						157.1 / 15.2 / 28=S/Pal	161.4 / 10.9 / 22	163.4 / 8.9	164.4 / 7.9 / 15
0+75						156.1 / 16.2 / 22=S/Pal	159.2 / 13.1 / 18	161.3 / 11.0	163.3 / 9.0 / 15
0+45						154.8 / 17.5 / 10=S/Pal	154.8 / 17.5 / 7	159.1 / 13.2	160.7 / 11.6 / 15
0+25								153.9 / 18.4 =S/Pal	153.9 / 18.4 / 4	158.0 / 14.3 / 10
0+0								153.9 / 18.4	152.7 / 19.6 / 13=S/Paving
BM	11.04	172.31	9.09	161.27	BP in ECb Bridge Merlin Ret Market + Imperial	161.28 Holker		172.31	
BM	1.46	170.36		168.90	H.W. S LAT Market + 59th St				

Reduced 5-26-1945 EBH
Sections Platted
2' + 5' Scale

May 25-45
S 15507
81555
Osborne
8699

I.P.	10.96	172.23	11.04	161.27
+96.4 = Wcb 59th St.				
+95	4' Lt of ℄ - ℄ Power & Tel. Pole			
+91.4 = Wly Conc Walk 59th St.				
+80				
+40				
2+0				
1+50				
		172.31		

Lt.		℄	Rt.
161.5 / 10.8 / 30 = Sly A.C. Pav	163.5 / 8.8 / 23 = Nly Cb + Walk	163.74 / 8.57	164.24 / 8.97 / 15
161.4 / 10.9 / 22 = Sly	163.3 / 9.0 / 14	163.86 / 8.45	165.3 / 7.0 / 15
161.3 / 11.0 / 28 = Sly Pav	169.5 / 2.8 / 19	169.8 / 2.5	171.5 / 0.8 / 15
160.8 / 11.5 / 32 = Sly Pav	168.3 / 4.0 / 22	169.8 / 2.5	169.8 / 2.5 / 15
160.0 / 12.3 / 31 = Sly Pav	166.0 / 6.3 / 23	167.6 / 4.7	168.2 / 4.1 / 15
158.6 / 13.7 / 33 = Sly Pav	163.6 / 8.7 / 22	165.3 / 7.0	167.0 / 5.3 / 15

172.31

+35

+10

4+0

3+65

+40 15.5 Lt of ℄ = ℄ Anchor Pole

3+35

3+29 15' Lt of ℄ = ℄ Fire Hyd.

3+26.6 = E Cb of 59th St. 15' Lt of ℄ = Fire Hyd

172.23

161.6 160.9 158.7 161.7
10.6 11.3 13.5 10.5
14 = S/s Pav. 8 15

161.5 161.2 159.9 163.9 168.5
10.7 11.0 12.3 8.3 5.7
17 = S/s Pav. 8 ℄ 15

161.5 161.4 159.3 164.2 169.1
10.7 10.8 12.9 8.0 5.6
19 = S/s Pav. 13 4 15

161.4 161.5 159.9 164.9 165.3 166.9
10.8 10.7 12.3 8.2 6.9 5.3
24 = S/s Pav. 20 11 8 15

161.4 160.3 163.7 165.8 166.8
10.8 11.9 8.5 6.4 5.4
24 = S/s Pav. 16 15 15

161.5 161.97 163.49 164.99
10.7 10.26 8.74 7.24
29 15.8 = HHCb Walk 15 ork

172.23

4+35

5+0

4+65

172.23

B

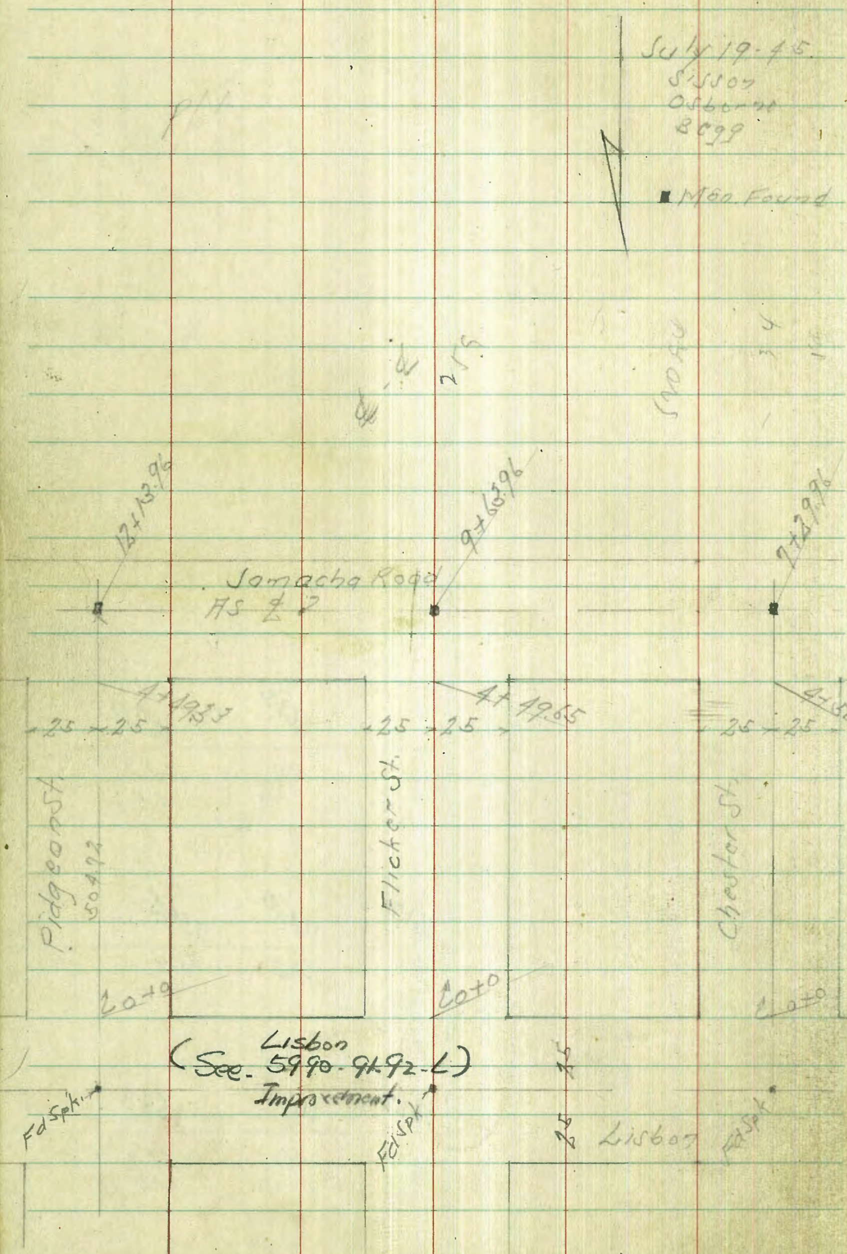
	161.2	159.0
	11.0	13.2
	5:1/4 Bv	15

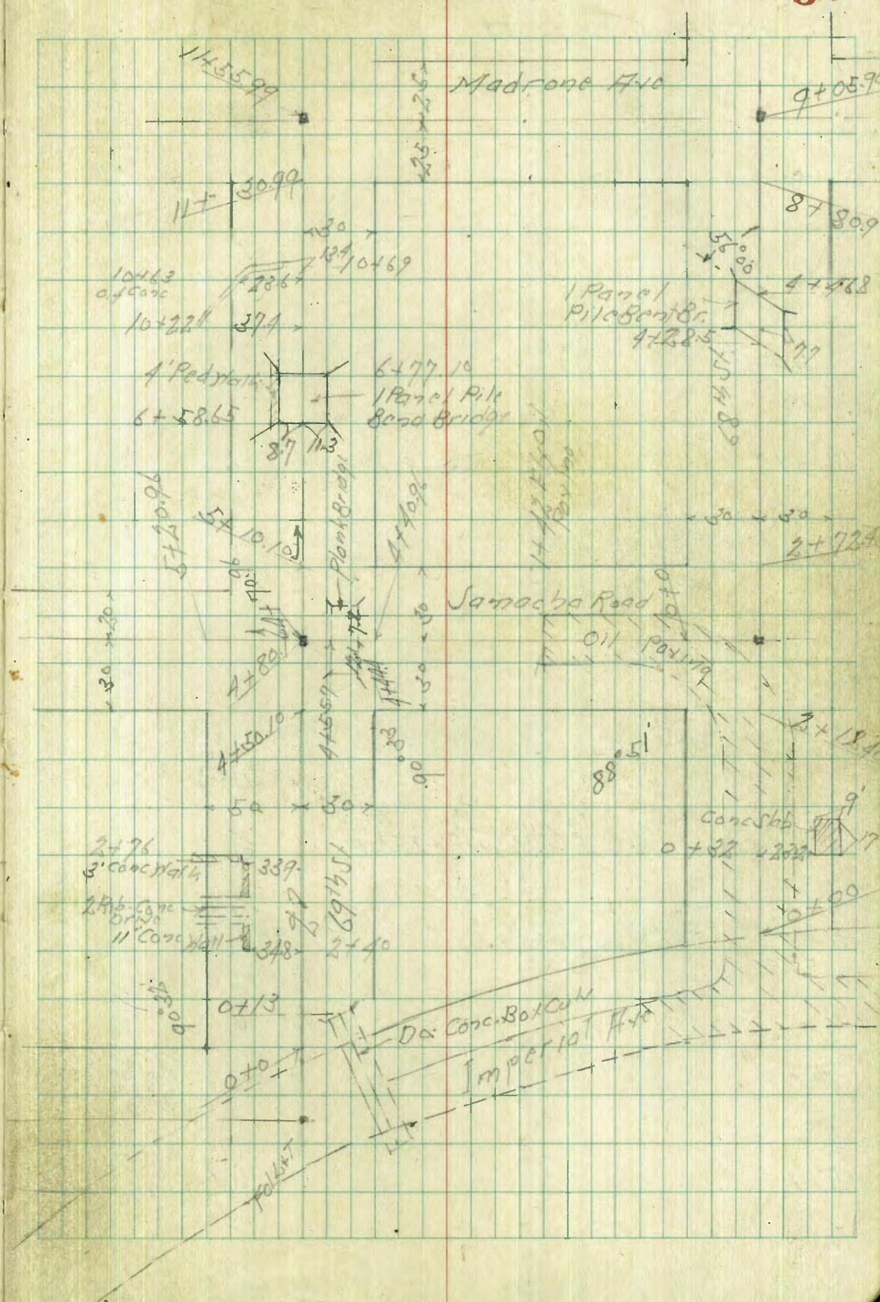
161.2	160.0	158.5
11.0	12.2	13.7
6:51/4 Bv		15

161.2	161.1	159.3
11.0	11.1	12.9
9:51/4 Bv		15

172.23

Cross Section 68th 69th Chester Flicker
Pidgeon Lisbon Samacho





Cross Section 68th St.
Imperial Ave to Madrone
Sketch Page 32

indexed
E.S.K.

+55					
+43					
+17	30' Lt of ℄ = Nly 18" Pepper Tree				
1+0					
0+49	= Sly Conc Slab on Rt				
0+45	21' Rt = Ely Power & Tel Pole				
0+0	= S.L. Imperial				
BM	0.54	249.80 ✓	4.78	249.26	S.W. Top F. Hyd Imperial & 68th St
BM	0.60	254.04 ✓		253.44	S.W. 2" Pipe Box Culv. Imperial 69

July 19-45
Sisson
Osborne
Begg

Lt = E ℄ Rt = W

+55:
241.8 / 8.3 — 41 = ℄ Door Gar. Dirt Floor

+43:
242.8 / 7.0 — 50 = ℄ Garage Dirt Floor
242.3 / 7.5 / 30
241.92 / 7.88 — 15 = Ely Oil Pav
242.02 / 7.78
241.57 / 8.23 — 16 = Wly Oil Pav
241.8 / 8.0 / 30

1+0:
244.18 / 5.62 / 30 — 8 = ℄ 3' Conc Walk
244.0 / 5.8 / 30
243.70 / 6.10 — 21 = Ely Oil Pav
244.17 / 5.63
243.45 / 6.35 — 16 = Wly Oil Pav
243.7 / 6.1 / 30

0+49:
246.3 / 3.5 / 30
245.85 / 3.95 — 16 = Ely Oil Pav
245.93 / 3.87
245.49 / 4.31 — 19 = Wly Oil
245.60 / 4.20 — 23.2 = SEly Conc Slab
245.6 / 4.2 / 30

0+0:
247.5 / 2.3 / 30
246.86 / 2.94 — 18 = Ely Pav
246.88 / 2.92
246.50 / 3.30 / 20
246.45 / 3.35 — 28 = Wly Oil Pav
246.7 / 3.1 / 30

249.80 ✓

✓

68+35+

+40 20.2 Rt = Ely Power Pole

3+0

TP	6.97	245.96 ✓	10.81	238.99	Rock 8' ℄ 68th + Samacha

+72.4 = S.L. Samacha Road

+50 21 Rt of ℄ = Ely 36" Palm Tree

+42.4 = ℄

+25 20.3 Rt of ℄ = Ely Pow + Tel Pole

+12.4 = N.L. Samacha Road

2+0

1+98

249.80 ✓

Lt. ℄ Rt.

238.4 / 7.6 / 15   238.4 / 7.6 / 30   238.5 / 7.5 / 15   238.6 / 7.4   238.5 / 7.5 / 15   238.6 / 7.4 / 30   238.5 / 7.5 / 15

245.96 ✓

239.4 / 10.4 / 30   238.8 / 11.0 / 15   238.8 / 11.0   238.4 / 11.4 / 15   238.6 / 11.2 / 30

239.6 / 10.2 / 30   239.4 / 10.4 / 15   239.3 / 10.5   238.8 / 11.0 / 10   239.6 / 10.2 / 30

240.1 / 9.7 / 30   240.05 / 9.75 / 25 = Ely Oil Pad   239.99 / 9.81 / 15   239.98 / 9.82   239.65 / 10.15 / 9 = Wly Oil Pad   239.7 / 10.1 / 17   240.6 / 9.2 / 30

240.7 / 9.1 / 30   240.20 / 9.60 / 17 = Ely Oil Pad   240.17 / 9.63   239.90 / 9.90 / 9 = Wly Oil Pad   239.8 / 10.0 / 14   240.8 / 9.0 / 30

241.05 / 8.75 / 30.7 = Lt Conc Walk

249.80 ✓

68th St.

+88 22 Rt of ℄ = Ely Power Pole

+84

+65

+46.8 = Sly Pile Bridge

+28.5 = Nly Pile Bridge

4+0

+55 26 Rt of ℄ = Ely 12" Olive Tree

3+50

245.96

Lt. ℄ Rt.

233.0 / 13.0 / 55 = Bottom Moss	240.1 / 5.9 / 30	241.0 / 5.0 / 15	~~242.0~~ 241.6 / 4.4	241.4 / 4.6 / 15	240.8 / 5.2 / 30	241.6 / 4.4 / 40		
235.1 / 10.9 / 47	232.7 / 13.3 / 30	238.8 / 7.2 / 17	240.8 / 5.2 / 8	240.8 / 5.2	240.4 / 5.6 / 15	240.2 / 5.8 / 30	239.5 / 6.5 / 45	
238.4 / 7.6 / 45	238.0 / 8.0 / 30	232.5 / 13.5 / 22	233.0 / 13.0 / 10	233.0 / 13.0 / 1	240.60 / 5.36 on Deck	239.8 / 6.2 / 15	239.3 / 6.7 / 30	238.8 / 7.2 / 45
238.3 / 7.7 / 45	238.3 / 7.7 / 30	238.0 / 8.0 / 20	240.3 / 5.7 / 9	240.58 / 5.38 on Deck	232.8 / 13.2 / 1	233.0 / 13.0 / 16	232.9 / 8.1 / 30	232.3 / 8.7 / 45
238.6 / 7.4 / 45	238.6 / 7.4 / 30	232.2 / 8.8 / 20	238.3 / 7.7 / 14	238.8 / 7.2	232.9 / 8.1 / 15	232.7 / 8.3 / 30 = Top of Bank Moss	232.2 / 13.8 / 55 = ℄ of Bottom Moss	
238.2 / 7.8 / 45	238.2 / 7.8 / 30	238.1 / 7.9 / 15	238.5 / 7.5	238.0 / 8.0 / 18	238.0 / 8.0 / 30	238.0 / 8.0 / 45		

245.96 ✓

68 1/2 St.

+50				
TP	12.60	281.60 ✓	0.28	269.00
+25				
6+0				
+60				
TP	12.91	269.28 ✓	1.47	256.37
+35				
TP	12.57	257.84 ✓	0.69	245.27
5+0				
		245.96		

Lt. 2 Rt.

268.5	269.2	270.1	270.0	270.6	270.9	273.4	275.3
13.10	12.4	11.5	11.6	11.0	10.7	7.7	6.3
30	30	22	15		14	17	30

281.60 ✓

267.1	267.7	268.1	266.6	266.2	266.5	271.0	272.3
3.7	1.6	1.2	2.7	2.6	2.8	11.7	1.3
30	15	7	6		14	16	30

262.6	263.2	264.5	260.9	264.4	261.5	268.7	270.3
6.7	6.1	4.8	8.4	7.9	7.8	4.1	1.0
30	18	7	5		12	17	30

253.2	254.5	256.1	253.9	252.9	252.7	262.1	263.7
17.1	14.8	13.2	16.3	16.4	16.6	7.2	6.1
30	15	6	5		11	17	30

269.28 ✓

245.3	246.4	248.1	246.6	242.1	246.4	251.8	252.7
12.5	11.2	8.7	11.2	10.7	11.2	6.0	5.6
45	30	6	6		12	14	30

257.84 ✓

239.0	240.5	241.7	242.5	242.3	241.8	242.8
9.4	5.5	4.3	3.5	3.7	4.2	3.2
45	30	12		15	30	45

245.96 ✓

68+55 Lt.

BM		4.26	302.06	℄ Mon Madrone #684
9+05.9	= ℄ Madrone			
+80.9	= N.L. Madrone 29.4 Lt of ℄ = Sly Maven Wire Fence			
+50				
TP	13.63	306.32	0.38	293.69
8+0	285.4 Lt of ℄ = Maven Wire Fence			
+80	23.5 Rt of ℄ = Fly Power Pole			
+50	288.4 Lt of ℄ = Maven Wire Fence			
TP	12.90	294.07	0.43	281.17
7+0				
		281.60		

Lt. ℄ Rt

289.5 / 16.8 / 90

288.8 / 7.5 / 30

301.4 / 4.9 / 10

303.7 / 2.1

304.9 / 1.4 / 15

305.2 / 1.1 / 20

303.6 / 3.3 / 60

298.3 / 8.0 / 90

285.3 / 21.0 / 90

295.5 / 10.8 / 30

298.3 / 8.0 / 15

299.1 / 7.2

299.6 / 6.7 / 10

301.7 / 5.1 / 20

302.5 / 3.8 / 60

303.0 / 3.3 / 25

298.3 / 8.0 / 90

290.9 / 13.4 / 40

291.5 / 14.8 / 30 - Wire Fence

294.1 / 12.2 / 15

294.5 / 10.8

306.32

298.4 / 10.9 / 14

297.9 / 8.4 / 18

299.4 / 6.9 / 30

282.0 / 18.3 / 40

284.1 / 10.0 / 30

287.3 / 6.9 / 15

289.2 / 4.9

289.4 / 4.7 / 14

294.8 / 5.3 / 17

293.7 / 6.4 / 30

278.5 / 18.3 / 40

276.9 / 17.2 / 30

280.5 / 13.4 / 20

283.4 / 10.7 / 10

283.0 / 11.1

283.1 / 11.0 / 15

286.0 / 8.1 / 30

286.8 / 7.3 / 35

294.07

279.6 / 9.0 / 40

282.8 / 8.8 / 30

279.55 / 5.8 / 15

279.9 / 4.7

279.9 / 4.7 / 14

280.0 / 4.6 / 18

281.2 / 3.4 / 30

281.60

68+55±

9+30.9 = S.L. Madrone

306.32

Lt. ℄ Rt.

291.0	302.2	306.3	302.9	308.1	302.5	302.8	298.3
15.3	5.1	0.0	+1.6	+1.8	+1.2	3.5	8.0
90	30	15		15	30	60	90

306.32 ✓

Cross Section Samacha Road
68th St to Pidgeon St.
Sketch Page 32

Indexed
C.S.K.

+32	= Conc Apron on Rt			
+20	21' Rt of ℄ = N'ly Power Pole			
+16	20 Rt of ℄ = N'ly 36" Palm			
2+0				
+91	20.5 Rt of ℄ = N'ly 36" Palm Tree			
+63	20.5 Rt of ℄ = N'ly 36" Palm Tree			
+50				
+47	20.5 Lt of ℄ = S'ly Tel Pole			
+31	20.5 Rt of ℄ = N'ly 36" Palm Tree			
+03	21.7 Rt of ℄ = N'ly Palm Tree			
1+0				
+87	21.3 Rt of ℄ = N'ly Power Pole			
+73	21 Rt of ℄ = N'ly 30" Palm			
+50				
+29	21.2 Lt of ℄ = S'ly Tel Pole			
0+0	= East Line 68th St.			
BM	8.10	247.09 ✓	238.99 ✓	Rock 8 Rt ℄ Samacha at 68th St. Page 34

Lt: N ℄ Rt: S

242.56 / 4.53 / 32 = N'ly Conc Apron

243.1 / 4.0 / 30 — 242.5 / 4.6 / 15 — 242.1 / 5.0 / 12 — 242.2 / 4.9 — 241.4 / 5.7 / 12 — 242.5 / 4.6 / 15 — 242.4 / 4.7 / 30

242.6 / 4.5 / 30 — 242.2 / 4.9 / 15 — 241.5 / 5.6 / 11 — 241.6 / 5.5 — 241.0 / 6.1 / 13 — 241.8 / 5.3 / 15 — 241.2 / 5.9 / 30

242.0 / 5.1 / 30 — 241.7 / 5.4 / 15 — 240.87 / 6.22 / 9 = N'ly Oil Pav — 241.04 / 6.05 — 240.44 / 6.65 / 12 = S'ly Oil Pav — 240.2 / 6.9 / 15 — 241.4 / 5.7 / 17 — 241.3 / 5.8 / 30

241.3 / 5.8 / 30 — 240.6 / 6.5 / 16 — 240.39 / 6.70 / 9 = N'ly Oil Pav — 240.34 / 6.75 — 239.66 / 7.43 / 10 = S'ly Oil Pav — 239.4 / 7.7 / 15 — 240.7 / 6.4 / 18 — 240.6 / 6.5 / 30

240.5 / 6.6 / 30 — 240.1 / 7.0 / 26 = N'ly Oil Pav — 239.94 / 7.15 / 15 — 239.66 / 7.43 = S'ly Oil Pav — 239.1 / 8.0 / 15 — 239.5 / 7.6 / 30

247.09 ✓

+44	20.2 Rt of ℄ = Nly Power Pole			
+40.96 = N.L. 69th St				
+23	22' Lt of ℄ = Sly Tel Pole			
+11	20' Rt of ℄ = Nly 16" Euc Tree			
4+0	19.4 Rt of ℄ = Nly 16" Euc Tree			
+91	20.2 Rt of ℄ = Nly 6" Euc Tree			
+85	19.7 Rt of ℄ = Nly 4" Euc Tree			
+77	20' Rt of ℄ = Nly 14" Euc Tree			
+67	20.6 Rt of ℄ = Nly Tree			
+50				
+44	20' Rt of ℄ = Nly 14" Euc. Tree			
+38	20' Rt of ℄ = Nly Tree			
+30	19.8 Rt of ℄ = Nly Tree			
+13	19.4 Rt of ℄ = Nly Euc Tree			
3+0				
TP	5.81	249.05 ✓	2.85	243.24
+91	= Conc Walk on Rt.			
+74	21' Lt of ℄ = Sly Tel Pole			
+54	20 Rt of ℄ = Nly 12" Euc Tree			
2+50				

247.09

Lt ℄ Rt

246.2 / 2.9 / 30 — 246.0 / 3.1 / 12 — 246.0 / 3.1 — 246.0 / 3.1 / 10 — 245.6 / 3.5 / 30

244.6 / 4.5 / 30 — 243.9 / 5.2 / 12 — 244.4 / 4.7 — 244.0 / 5.1 / 12 — 244.3 / 4.8 / 30

243.8 / 5.3 / 30 — 243.1 / 6.0 / 12 — 243.7 / 5.4 — 243.3 / 5.8 / 12 — 243.6 / 5.5 / 30

243.6 / 5.5 / 30 — 242.9 / 6.2 / 13 — 243.2 / 5.9 — 242.8 / 6.3 / 12 — 243.0 / 6.1 / 30

249.05 ✓

242.82 / 4.27 / 30 = Lt Nly 3.5 Conc Walk

242.3 / 4.8 / 30 — 242.8 / 4.3 / 15 — 242.4 / 4.7 / 12 — 242.9 / 4.2 — 242.4 / 4.7 / 12 — 242.8 / 4.3 / 15 — 242.6 / 4.5 / 30 — 242.49 / 4.60 / 32 = Lt Nly Conc Apron

247.09 ✓

Samocha Road Platted [illegible]

+83	24.7 Rt of ℄ : N'ly Power Pole				
+68	23.3 Lt of ℄ S'ly Tel. Pole				
+50					
5+20.96 -	E.L. 69th St. to North				
5+10	: ℄ Conc. Walk on Rt.				
BM -	8.80	254.66 ✓	3.19	245.86	℄ Mon Samocha + 69th St
+60					
+55.7					
4+47					

249.05 ✓

Lt.		℄		Rt.
248.3 / 6.4 / 30	246.8 / 7.9 / 18	246.9 / 7.8	248.1 / 6.6 / 20	248.0 / 6.7 / 30
242.8 / 7.2 / 30	246.6 / 8.1 / 20	246.7 / 8.0	242.7 / 7.0 / 20	242.6 / 7.1 / 30
				247.23 / 7.43 / 23.5 : 2x NH Conc Walk
		254.66 ✓		
246.1 / 3.0 / 30		246.2 / 2.9		246.6 / 2.5 / 30
243.2 / 5.4 / 30 : Bottom Wash	243.2 / 6.9 / 12 : Bottom Wash	246.05 / 3.64 on Deck Bridge	242.8 / 6.3 / 12 : Bottom Wash	242.7 / 6.4 / 30 : Bottom Wash
243.2 / 5.4 / 30 : Bottom Wash	243.2 / 5.9 / 12 : Bottom Wash	246.02 / 3.03 on Deck Bridge	242.7 / 6.4 / 12 : Bottom Wash	242.7 / 6.4 / 30 : Bottom Wash

249.05 ✓

+85	13.9 Rt of ℄ = Nly 5" Acacia Tree				
+73	21 Rt of ℄ = Nly Power Pole				
+69	13.8 Rt of ℄ = Nly 6" Acacia Tree				
TP	6.51	259.23 ✓	1.94	252.72	
7+54.96 = E.L. Chester					
BM			3.15	251.51 ✓	0.9 ℄ M07 Jonacha & Chester
+39	13.9 Rt of ℄ = Nly 6" Acacia Tree				
+29.96 = ℄ Chester					
+25	24.5 Lt of ℄ = Sly Tel. Pole				
+19	14.4 Rt of ℄ = Nly 10" Acacia Tree				
7+04.96 = W.L. Chester					
+99	14.5 Rt of ℄ = Nly 5" Acacia Tree				
+78	15 Rt of ℄ = Nly 8" Acacia Tree				
+50					
6+0					

254.66 ✓

Lt				℄				Rt
				259.23 ✓				

254.3	254.3	251.9	252.6	252.4	253.0	253.0	252.7
0.4	0.4	2.8	2.1	2.3	1.7	1.7	2.0
30	25	20	10		10	20	30

253.3	253.3	251.5	252.1	251.9	251.6	252.2	252.6	252.4
0.8	1.4	3.5	2.6	2.8	3.1	2.0	2.1	2.3
30	24	20	10		2	10	20	30

252.7	252.4	250.7	251.4	251.0	250.9	252.0	252.1	251.9
2.0	2.3	4.0	3.3	3.7	3.8	2.7	2.6	3.9
30	24	20	10		3	9	20	30

251.2	251.0	249.1	250.0	249.8	249.8	250.4	250.9
2.5	2.7	5.6	4.7	4.9	4.9	4.3	3.8
30	24	19	12		6	20	30

249.3	247.8	248.0	247.8	248.9	249.1	249.6
5.4	6.9	6.7	6.9	5.8	5.6	5.1
30	19		3	11	26	30

254.66 ✓

Samacha Road

+88.96 E.L. Flicker

B.M.		4.37	254.86 ✓	on ℄ Mos Samacha + Flicker

+72 19.4 Rt of ℄ = Nly Power Pole
+63.96 = ℄ Flicker

+38.96 = W.L. Flicker

9+0
+90 15.6 Rt of ℄ = Nly 5" Acacia Tree
+80 25.3 Lt of ℄ = Sly Tel Pole
+62 15 Rt of ℄ = Nly 12" Pepper Tree
+50

+34 14.8 Rt of ℄ = Nly 14" Pepper Tree
+07 14.8 Rt of ℄ = Nly 8" Pepper Tree
8+0

259.23

Lt.				℄			Rt.	
2577 / 1.5 / 30	257.5 / 1.7 / 25	2560 / 3.2 / 21	2563 / 2.9 / 10	2560 / 3.2	2569 (6) / 2.3 / 5	2520 / 2.2 / 20	257.05 / 2.18 / 209 = Z+11/3 Conc Walk	2570 / 2.2 / 30
2576 / 1.6 / 30	2573 / 1.9 / 27	255.5 / 3.7 / 20	256.0 / 3.2 / 10	2557 / 3.5	2563 / 2.9 / 5	2565 / 2.7 / 20	2564 / 2.8 / 30	
2568 / 2.4 / 30	255.4 / 3.8 / 20	255.5 / 3.7 / 10		2555 / 3.7	2561 / 3.1 / 10	255.9 / 3.3 / 20	2559 / 3.3 / 30	
2567 / 2.0 / 30		254.9 / 4.3 / 20		2548 / 4.4	254.5 (5) / 5.7 / 10	254.3 (5) / 3.9 / 20	255.6 / 3.6 / 30	
2552 / 4.0 / 30	2552 / 4.0 / 21	2537 / 5.5 / 20	254.0 / 5.2 / 10	2536 / 5.6	2547 / 4.5 / 8	2548 / 4.4 / 20	2546 / 4.6 / 30	
2542 / 5.0 / 30	254.4 / 4.8 / 24	2527 / 6.5 / 20	2531 / 6.1 / 10	2531 / 6.1	2539 / 5.3 / 7	254.2 / 5.0 / 20	2538 / 5.4 / 30	

259.23 ✓

Jamacho Road

Sta.					
+97	9.8 Rt of ℄ = Nly Power Pole				
+88.96	= ℄ Pidgeon		29.7 Lt of ℄ = Ely Wire Fence		
+87	26 Lt of ℄ = Sly Tel Pole				
+50					
11+0					
+89	29.5 Lt of ℄ = Nly Wire Fence				
+63					
+50					
TP	8.72	263.58 ✓	4.37	254.86	on ℄ Mon Jamacho x Flicker
+39	26 Lt of ℄ = Sly Tel Pole				
10+0					

259.23 ✓

Lt. ℄ Rt.

261.8 / 1.8 / 30	261.4 / 2.2 / 25	260.0 / 3.6 / 23	259.6 / 4.0 / 10	258.7 / 4.9	258.7 / 4.9 / 3	260.0 / 3.6 / 7	259.9 / 3.7 / 20	259.6 / 4.0 / 30
261.1 / 2.5 / 30	260.6 / 3.0 / 26	259.2 / 4.4 / 22	259.0 / 4.6 / 10	258.1 / 5.5	259.3 / 4.3 / 7	259.3 / 4.3 / 20	259.3 / 4.3 / 30	
260.1 / 3.5 / 30	259.7 / 3.9 / 25	258.1 / 5.5 / 21	258.1 / 5.5 / 10	257.3 / 6.3	258.2 / 5.4 / 3	258.7 / 4.9 / 20	258.3 / 5.3 / 30	

259.2
259.2 / 4.4 0 / 8.13
3' Rt Sty
3' Conc. Walk

259.1 / 4.5 / 30	258.9 / 4.7 / 25	257.3 / 6.3 / 21	257.3 / 6.3 / 10	256.6 / 7.0	257.5 / 6.1 / 3	258.4 / 5.2 / 20	257.7 / 5.9 / 30

263.58 ✓

257.9 / 1.3 / 30	257.9 / 1.3 / 27	256.2 / 3.0 / 20	256.5 / 2.7 / 10	256.0 / 3.2	256.9 / 2.3 / 4	257.2 / 2.0 / 20	257.1 / 2.1 / 30

259.23 ✓

Samocha Road

12+38.96 ℄ E.L.	Pidgeon				
B.M.			4.37	259.21 ✓	℄ Mon Samocha & Pidgeon
12+13.96 ℄	Pidgeon				
	263.58				

Lt. ℄ Rt.

262.6	262.4	260.4	260.5	259.7	259.6	260.7	260.6	260.7
1.0	1.2	3.0	3.1	3.9	4.0	2.9	3.0	3.1
30	25	23	10		3	9	20	30

261.1	260.4	260.0	259.2	259.1	260.2	260.6	260.0
2.5	3.2	3.6	4.4	4.5	3.4	3.0	3.6
30	20	10		3	9	20	30

263.58 ✓

Cross Section Chester St.
Lisbon to Jamacha Road
Sketch Page 32

indexed
C.S.K.

2+0					
+50					
1+0					
+50					
0+0 = S.L. Lisbon					
TP	9.47	275.33 ✓	0.66	265.86	
0-25 = ℄ Lisbon					
BM	13.08	266.52 ✓		253.44	S.W. 2" Pipe Box Culv. Imperial +69

Lt. E		℄		Rt. W
265.1 10.2 40	265.1 10.2 25	265.2 10.1	265.3 10.0 25	265.1 10.2 40
269.7 5.6 40	270.0 5.3 25	270.0 5.3	269.7 5.6 25	269.2 6.1 40
271.0 4.3 40	271.1 4.2 25	271.7 3.6	271.0 4.3 25	268.4 6.9 40
269.0 6.3 40	269.8 5.5 25	270.7 4.6	270.4 4.9 25	268.2 7.1 40
267.0 8.3 40	267.0 8.3 25	267.2 8.1	266.3 9.0 25	265.7 9.6 40
		275.33 ✓		
265.97 0.55 75	264.90 1.82 50	262.74 262.74 4.28 75 pk	259.68 6.84 50	257.51 9.01 100
		266.52 ✓		

BM			12.40	251.49 ✓	on ℄ Mon Samachot Chester 251.51 P42
+50.02 - N.L. Samacho					
4+0	19.3 Lt of ℄ - Wly Power Pole				
+50					
3+0					
TP	1.55	263.89 ✓	12.99	262.34	
2+50	19.5 Lt of ℄ - Wly Power Pole				
		275.33			

Lt		℄		Rt
	253.9 / 10.0 / 25	253.4 / 10.5	252.8 / 11.1 / 25	
254.9 / 9.0 / 40	254.5 / 9.1 / 25	254.0 / 9.9	253.4 / 10.5 / 25	253.1 / 10.8 / 40
256.7 / 7.2 / 40	256.2 / 7.7 / 25	255.2 / 8.7	254.7 / 9.2 / 25	254.1 / 9.8 / 40
258.8 / 5.0 / 40	258.4 / 5.5 / 25	258.0 / 5.9	257.2 / 6.7 / 25	257.2 / 6.7 / 40
		263.89 ✓		
262.13 / ~~250.7~~ / 13.2 / 40	261.83 / ~~250.4~~ / 13.5 / 25	261.3 / ~~249.2~~ / 14.0	260.8 / ~~249.4~~ / 14.5 / 25	260.7 / ~~249.3~~ / 14.6 / 40
		275.33 ✓		

Cross Section Flicker St
Lisbon to Samacho Road
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Indexed
C.S.K.

Lt = E | ℄ | Rt = W

+50							280.2 / 5.1 / 25	276.9 / 6.4	274.3 / 9.0 / 25	272.9 / 10.4 / 40	
1+0							280.4 / 2.9 / 25	277.6 / 5.7	274.9 / 8.4 / 25	273.9 / 9.4 / 40	
+50							277.7 / 5.6 / 25	276.2 / 7.1	274.8 / 8.5 / 25	273.8 / 9.5 / 40	
0+0	= SL Lisbon						277.2 / 6.1 / 25	276.4 / 6.9	275.2 / 8.1 / 25	274.5 / 8.8 / 40	
0-25	= ℄ Lisbon					279.98 / 3.34 / 100	277.46 / 5.86 / 50	275.15 / 8.17 / on Spk	272.47 / 10.85 / 50		270.93 / 12.39 / 75
TP	9.79	283.32 ✓	1.27	273.53				283.32 ✓			
BM	12.56	274.80		262.24	Nail ℄ Lisbon + Baxter P46						

275.15

BM			7.93	254.85 ✓	Z Mon Jamocha + Flicker 254.86 P43
+49.65 = N.L. Jamocha					
TP	4.22	262.78 ✓	12.65	258.56	
4+0					
+50					
3+0					
+50					
TP	0.94	271.21 ✓	13.05	270.27	
2+0					
		283.32			

Lt			℄	Rt
257.9 / 1.9 / 25	252.8 / 5.0 / 19	256.3 / 6.5 / 8	257.7 / 5.1	257.0 / 5.8 / 25
			263.78 ✓	
259.1 / 12.1 / 25			258.6 / 12.6	258.2 / 13.0 / 25 ; 257.9 / 13.3 / 40
261.1 / 10.1 / 25			260.7 / 10.5	259.9 / 11.3 / 25 ; 259.8 / 11.4 / 40
264.6 / 6.6 / 25			263.9 / 7.3	263.2 / 8.0 / 25 ; 262.8 / 8.4 / 40
269.4 / 1.8 / 25			268.7 / 2.5	267.1 / 4.1 / 25 ; 266.8 / 4.4 / 40
			271.21 ✓	
275.1 / 8.2 / 25			273.3 / 10.0	271.2 / 12.1 / 25 ; 270.3 / 13.0 / 40
			283.32 ✓	

Cross Section on Pidgeon St
Lisbon to Jamacha
Sketch Page 32

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2+09	21.5 Lt of ℄ : Wly 24" Euc. Tree				
+89					
+82	14.3 Lt : Wly 12" olive / 14.3 Rt of ℄ : Ely 12" Olive				
TP	5.06	297.26	1.60	292.20	
+64	15.4 Rt of ℄ : Ely 4" Oliver Tree				
+50					
+44	14.3 Lt of ℄ : Wly 18" Olive Tree				
+26	14.2 Rt of ℄ = 5" Olive Tree				
+24					
0+0	= S. L. Lisbon				
0-25	= ℄ Lisbon				
TP	8.44	293.80	0.91	285.36	
BM	11.12	286.27		275.15	℄ Nail Lisbon & Foster

Lt. ℄ Rt.

293.5 / 3.8 / 25 — 293.5 / 3.8 / 12 — 292.8 / 4.5 — 292.6 / 4.7 / 16 — 292.31 / 4.95 / 25 : Ely 22 Conc. Walk — 291.8 / 5.5 / 50

297.26

291.9 / 1.9 / 25 — 290.6 / 3.8 / 9 — 289.5 / 4.3 — 289.6 / 4.2 / 8 — 290.6 / 3.2 / 25 — 290.3 / 3.6 / 40

290.55 / 3.25 / 25 on Walk — 290.08 / 3.72 / 21.7 : ℄ + Wly 12.8 Conc. Walk Bottom Step

289.8 / 4.0 / 25 — 288.1 / 5.7 / 15 — 287.6 / 6.2 — 287.5 / 6.3 / 10 — 287.4 / 6.4 / 25 — 287.3 / 6.5 / 40

290.18 / 3.62 / 100 — 289.11 / 4.69 / 50 — 287.37 / 6.43 on Spk — 285.18 / 8.62 / 50 — 282.83 / 10.97 / 100

293.80

+89	15.3 Lt of ℄ = Wly 5" Olive Tree			
+50				
TP	0.20	284.48	12.98	284.28
+14	15.1 Lt of ℄ = Wly 12" Olive Tree			
2+0				
+96	14.7 Lt of ℄ = Wly 6" Olive Tree			
+88	24' Rt of ℄ = Ely 10" Pepper Tree			
+76	15.2 Rt of ℄ = Ely 4" Olive Tree			
+75				
+67	14' Rt of ℄ = Ely Power & Tel Pole			
+57	14.7 Rt of ℄ = Ely 4" Olive Tree			
+53				
+50				
	149 Lt of ℄ = Wly 12" Olive Tree			
+39	15.2 Rt of ℄ = Ely 5" Olive Tree			
1+25				

297.26

Lt ℄ Rt

279.5 / 5.0 / 25 — 278.8 / 5.7 / 8 — 277.4 / 7.1 / 5 — 272.1 / 7.4 — 272.1 / 7.4 / 9 — 278.4 / 6.1 / 12 — 277.6 / 6.9 / 25

284.48 ✓

285.7 / 11.6 / 25 — 285.3 / 12.0 / 9 — 284.0 / 13.3 / 3 — 284.1 / 13.2 — 284.0 / 13.3 / 10 — 285.6 / 11.7 / 13 — 285.5 / 11.8 / 25 — 285.3 / 12.0 / 40

289.8 / 7.5 / 25 — 288.1 / 9.2 / 5 — 288.1 / 9.2 — 287.8 / 9.5 / 11 — 289.5 / 7.8 / 13 — 289.5 / 7.8 / 25

292.78 / 4.48 / 26' = Wly 2.5 Conc Walk

292.6 / 4.7 / 25 — 292.5 / 4.8 / 14 — 291.8 / 5.5 / 7 — 291.9 / 5.4 — 291.3 / 6.0 / 11 — 291.8 / 5.5 / 25

293.5 / 3.8 / 25 — 293.5 / 3.8 / 15 — 293.2 / 4.1 — 293.0 / 4.3 / 11 — 292.8 / 4.5 / 25 — 292.2 / 5.1 / 40

297.26 ✓

Pidgeon St

Indexed
C.S.K.

BM		13.42	259.22	Z Mon Jamacha Pidgeon 259.21 P 45
+49.33	= H.I. Jamacha			
+42	10.4 Lt of Z = E 6" Risser to Gate			
+40	14.6 Lt of Z = W ly 12" Olive Tree			
+21	14.7 Lt of Z = W ly 7" Olive Tree			
+02	14.3 Lt of Z = W ly 8" Olive Tree			
4+0				
+83	14.6 Rt of Z = E ly 5" Olive Tree 14.8 Lt of Z = W ly 16" Olive Tree			
+64	15.1 Rt of Z = E ly 6" Olive Tree 14.7 Lt of Z = W ly 8" Olive Tree			
+50				
TP	0.99	272.64	12.83	271.65
	15 Rt of Z = E ly 5" Olive Tree			
+44	14.7 Lt of Z = W ly 14" Olive "			
+26	15 Lt of Z = W ly 5" Olive "			
+16	14.7 Rt of Z = E ly Pow + Tel Pole			
+08	15 Lt of Z = W ly 4" Olive T			
3+0				

284.48

Lt		Rt
262.2 / 10.4 / 5	261.1 / 11.5 / 3	261.8 / 11.5
260.7 / 11.9 / 15	261.7 / 10.9 / 18	261.8 / 10.7 / 25
265.8 / 6.8 / 25	265.2 / 9.4 / 7	264.7 / 8.4 / 5
264.4 / 8.2	263.5 / 8.7 / 10	264.2 / 7.9 / 12
263.9 / 8.7 / 25	263.2 / 9.4 / 40	
270.2 / 2.4 / 25	269.4 / 3.2 / 7	268.2 / 4.4 / 5
268.2 / 4.4	267.7 / 4.9 / 9	269.1 / 3.1 / 25
269.2 / 3.4 / 40		
272.64		
274.7 / 9.8 / 15	273.8 / 10.7 / 7	272.4 / 12.1 / 5
272.3 / 12.2	272.0 / 12.5 / 9	272.9 / 11.6 / 11
272.4 / 12.1 / 25	274.9 / 9.6 / 40	

284.48

Cross Section 69th St.
Imperial Ave to Madrone Ave
Sketch Page 32

Indexed
E.R.S.K.

Station	Notes				
+03	29.4 Lt of ℄ = Wly 18" Euc. Tree				
1+0					
+75					
+45	29.2 Rt of ℄ = Ely Anchor Pole				
+40					
+21	2.2 Rt of ℄ = Ely Anchor Pole				
+13					
0+0	= S.L. Lisbon				
0-25	= ℄ Lisbon to East				
BM	3.43	256.87 ✓		253.44	S.P. 2" Pipe Box Culv. Imperial & 69th St.

July 24 15
53
Lt. = E　　℄　　Rt. = W
S.I. Sloss
Osborne
Begg Rod

248.4 / 8.5 / 60	248.3 / 8.6 / 50	248.4 / 8.4 / 30	248.4 / 8.4 / 15	248.0 / 8.9	242.8 / 9.0 / 6	245.6 / 11.3 / 10: Ely Bottom Wash	245.0 / 11.9 / 23	248.4 / 8.5 / 27	248.4 / 8.5 / 30	247.4 / 9.5 / 50
249.1 / 7.8 / 60	248.7 / 8.2 / 50	248.9 / 8.0 / 30	249.0 / 7.9 / 15	248.5 / 8.4	247.8 / 9.0 / 6	245.7 / 11.2 / 10: Ely Bottom Wash	245.3 / 11.6 / 23	248.6 / 8.3 / 27	248.6 / 8.3 / 30	248.1 / 8.8 / 50
250.9 / 6.0 / 50	249.7 / 7.2 / 30	250.0 / 6.9 / 15	249.6 / 7.3	249.8 / 7.1 / 6	246.4 / 10.5 / 10: Ely Bottom Wash	246.3 / 10.6 / 24	249.1 / 7.8 / 60	248.9 / 8.0 / 40		
251.8 / 5.1 / 32.1	251.8 / 5.1 / 15	251.7 / 5.2	251.7 / 5.2 / 9	247.0 / 9.9 / 23: Outlet Dbl. Box Culv. 40. Conc. Bottom	251.67 / 5.20 / 24: Top Conc. Box Culv.	252.9 / 4.0 / 50	252.7 / 4.2 / 50			
252.9 / 4.0 / 31.8: Wly Bldg	253.1 / 3.8 / 22	253.1 / 3.8	253.20 / 3.67 / 15 on Paving	252.95 / 3.92 / 30 on Pav.	252.70 / 4.17 / 53: N. Wly Oil					
253.27 / 1.60 / 80	254.42 / 2.45 / 50	253.40 / 3.47	252.72 / 4.15 / 18: N.Wly Oil Pav.							

256.87 ✓

69th St.

Sta.					
+78	29' Lt of ℄ : Wly 14" Euc Tree Triple				
+54	30' Lt of ℄ : Wly 14" Euc Tree				
+50					
+28	29.6 Lt of ℄ : Wly 16" Euc Tree				
+02	29.8 Lt of ℄ : Wly 18" Euc Tree				
3+0					
+78	29.2 Lt of ℄ : Wly 24" Euc Tree				
+76	= S Edge 3' Conc Walk on Lt.				
TP	6.33	253.83	9.37		247.50
+50					
+15	28.9 Rt of ℄ : Ely Pow & Tel Pole				
2+0					
+78	28.9 Lt of ℄ = Wly 20" Euc Tree				
+53	29.7 Lt of ℄ = Wly 16" Euc Tree				
1+50					
+28	29.2 Lt of ℄ : Wly 12" Euc Tree				
1+16	28.3 Rt of ℄ : Ely Power Pole				
		256.87			

54

Lt. — ℄ — Rt.

248.7/5.1/50 — 248.6/5.2/30 — 247.5/6.3/25 — 247.3/6.5/15 — 246.1/7.7 — 245.5/8.3/6 — 242.6/10.8/10 = Ely & Bottom Wash — 242.9/10.9/22 — 245.8/8.0/25 — 246.2/7.6/30 — 244.9/8.9/50

248.9/4.9/50 — 247.4/6.4/30 — 247.2/6.6/15 — 246.2/7.6 — 245.5/8.3/6 — 243.1/10.7/10 = Ely & Bot. Wash — 243.0/10.8/20 — 247.6/6.2/30 — 245.2/8.6/50

250.59/3.24 on Walk — 249.85/3.98/34.7 = S Wly 3' Conc Walk

253.83 ✓

250.92/5.95/50 on Conc Drive — 249.62/7.20/33.3 = Ely 3' Conc Dr — 247.9/9.0/24 — 247.5/9.4/15 — 246.8/10.1 — 246.5/10.4/8 — 243.9/13.0/11 = Ely & Bot Wash — 243.4/13.5/23 — 247.2/9.7/30 — 245.4/11.5/50

254.7/6.2/50 — 248.1/8.8/30 — 247.8/9.1/15 — 246.9/10.0 — 246.9/10.0/7 — 244.4/12.5/10 = Ely & Bot. Wash — 244.1/12.8/22 — 246.9/10.0/26 — 248.9/8.0/30 — 246.1/10.8/50

248.6/8.3/60 — 247.7/9.2/50 — 247.5/9.4/30 — 248.0/8.9/15 — 247.1/9.8 — 246.1/10.8/7 — 244.7/12.2/10 = Ely & Bottom Wash — 244.5/12.4/22 — 247.2/9.7/25 — 248.6/8.5/30 — 246.6/10.3/50

256.87 ✓

69th St.

6+0

+79

+72 8' Lt. of ℄ = ℄ + Sly Tree Hedge

+50

5+10.10 = S.L. Samacho to West

5+08 9.5' Lt. of ℄ = Nly ℄ Acacia + Cypress Tree Hedge

BM	6.95	252.81 ✓	7.97	245.86	℄ Mon Samacho + 69th St. 245.86 P41

+50.10 = N.L. Samacho Road

4+0

253.83

Lt. ℄ Rt.

6+0: 246.0 / 6.8 / 30 — 245.7 / 7.1 — 245.5 / 7.3 / 12 — 241.5 / 11.3 / 16 = Edge + Bot. Wash — 241.5 / 11.3 / 23 — 244.1 / 8.7 / 26 — 243.8 / 9.0 / 30 — 243.4 / 9.4 / 50

+79: 246.72 / 6.10 / 28.2 = Nly Garage Conc Floor — 245.81 / 7.00 / 10.5 = Edge Nly Conc Apron

+50: 246.3 / 6.5 / 30 — 246.1 / 6.7 — 245.5 / 7.3 / 13 — 241.9 / 10.9 / 17 = Edge + Bottom Wash — 242.1 / 10.7 / 24 — 245.5 / 7.3 / 30 — 244.1 / 8.7 / 50

5+08: 246.9 / 5.9 / 30 — 246.4 / 6.4 — 246.6 / 6.2 / 13 — 242.6 / 10.2 / 17 = Edge + Bottom Wash — 242.7 / 10.1 / 24 — 245.4 / 7.4 / 30 — 244.9 / 7.9 / 50

252.81 ✓

+50.10: 247.4 / 6.4 / 50 — 247.5 / 6.3 / 30 — 246.6 / 7.2 / 15 — 246.2 / 7.6 — 246.2 / 7.6 / 9 — 243.6 / 10.2 / 14 = Edge + Bot. Wash — 243.6 / 10.2 / 24 — 246.2 / 7.6 / 30

4+0: 248.8 / 5.0 / 50 — 248.4 / 5.4 / 30 — 247.5 / 6.3 / 26 — 247.3 / 6.5 / 15 — 246.6 / 7.2 — 246.4 / 7.4 / 6 — 242.9 / 10.9 / 10 = Edge + Bottom Wash — 242.6 / 11.0 / 23 — 245.2 / 8.6 / 26 — 246.1 / 7.7 / 36 — 244.9 / 8.6 / 50

253.83 ✓

TP	11.70	264.24	0.27 ✓	252.54
8+0				
+76	17.6 Rt. of ℄: Ely 20" Peppertree			
+50				
+17	27' Rt of ℄: Ely Pow. & Tel Pole			
7+0				
+77.10	= Sly Pile Bridge			
+58.65	= Nly Pile Bridge			
6+50				

252.81

Lt. ℄ Rt.

242.8 / 5.0 / 50	247.8 / 5.0 / 30	245.4 / 4.4 / 14	252.2 / +0.4 / 6	253.4 / +0.6	252.5 / -0.3 / 13	245.6 / 7.2 / 27	245.1 / 7.7 / 30	244.7 / 8.1 / 50	
245.2 / 7.6 / 50	245.5 / 7.3 / 30	246.5 / 6.3 / 12	247.6 / 5.2 / 8	247.6 / 5.2	247.4 / 5.4 / 12	244.0 / 8.8 / 20	243.9 / 8.9 / 30	243.3 / 9.5 / 50	
244.8 / 8.0 / 50	244.8 / 8.0 / 30	242.2 / 5.8 / 13	246.9 / 5.9	246.7 / 6.1 / 11	244.0 / 8.8 / 19	244.0 / 8.8 / 30	243.4 / 9.4 / 50		
240.2 / 12.6 / 50	242.9 / 9.9 / 30	242.1 / 10.7 / 13	247.06 / 5.75 ⊙ Deck	240.9 / 11.9 / 12	241.1 / 11.7 / 27	243.4 / 9.4 / 30	243.0 / 9.8 / 50		
241.7 / 11.1 / 50	240.5 / 12.3 / 30	240.2 / 12.6 / 13	247.08 / 5.73 / 8.7 ⊙ Deck	247.04 / 5.77 ⊙ Deck	240.6 / 12.2 / 12	240.5 / 12.3 / 30	240.0 / 12.8 / 50		
244.3 / 8.5 / 50	244.6 / 8.2 / 30	244.6 / 8.2 / 20	246.9 / 5.9 / 10	246.8 / 6.0	246.4 / 6.4 / 15	241.7 / 11.1 / 16 = Ely Box Mailbox	241.0 / 11.8 / 25	244.3 / 8.5 / 30	243.5 / 9.3 / 50

252.81 ✓

69th St.

+35				
TP	11.73	287.45	0.37	275.72
+30	274R101 ℄: Ely Pow. & Tel. Pole			
+28				
9+0				
+75				
TP	11.88	276.09	0.03	264.21
+50				
8+30				
		264.24		

Lt. ℄ Rt.

286.2 / 1.3 / 30 — 285.3 / 2.2 / 28 — 278.2 / 12.3 / 18 — 273.3 / 14.1 / 4 — 273.3 / 14.2 — 273.6 / 13.9 / 10 — 273.9 / 13.6 / 22 — 281.0 / 6.5 / 26 — 280.9 / 6.6 / 30

287.45

285.3 / 7.9.2 / 30 — 284.5 / 7.8.4 / 28 — 274.1 / 3.0 / 17 — 272.5 / 3.6 / 6 — 272.3 / 3.8 — 272.8 / 3.3 / 15 — 273.3 / 2.8 / 30

9+75

(278.47 / 267 / 8.4 / 30: Top Rubble Wall) — 269.3 / 6.8 / 18 — 268.6 / 7.5 / 12 — 268.5 / 7.6 — 268.7 / 7.4 / 15 — 269.6 / 6.5 / 21 — 272.1 / 4.0 / 25 — 272.2 / 3.9 / 30 — 272.1 / 4.0 / 47: Ely House

269.05 / 7.04 / 50: Edge Garage Conc. Foot — 267.18 / 8.91 / 38: Conc. Drive — 266.89 / 9.20 / 22.5: Ely H.S. Conc. Drive — 265.4 / 10.7 / 10 — 265.0 / 11.1 — 265.0 / 11.0 / 15 — 265.5 / 10.6 / 36 — 266.7 / 9.4 / 50

276.09

253.6 / 30

261.8 / 2.4 / 36 — 257.8 / 1.4 / 20 — 261.2 / 3.6 / 7 — 260.7 / 3.5 — 260.8 / 3.4 / 16 — 250.5 / 13.7 / 36 — 251.2 / 13.0 / 50

249.7 / 30

252.6 / 11.6 / 50 — 251.0 / 13.2 / 30 — 251.2 / 13.0 / 18 — 252.8 / 6.4 — 257.5 / 6.7 — 252.7 / 6.5 / 16 — 248.0 / 16.2 / 33 — 246.5 / 17.7 / 50

264.24

69th St.

BM			9.32	278.13	0n ℄ Mon Madrone + 69th St.
+ 55.99 = ℄					
+ 46	13' Lt of ℄ = Wh Post + Tel Pole				
+ 30.99 = HL Madrone					
11+0					
+ 50					
10+0					
9+65					
	287.45				

Lt — ℄ — Rt

283.5 / 4.0 / 30 — 278.2 / 9.3 — 274.2 / 13.3 / 30 — 270.7 / 16.8 / 50

286.1 / 1.4 / 30 — 285.2 / 2.3 / 23 — 282.7 / 4.8 / 15 — 280.6 / 6.9 — 278.1 / 9.4 / 21 — 276.4 / 11.5 / 30 — 272.9 / 14.6 / 50

289.1 / +1.6 / 30 — 285.1 / 2.4 / 26 — 283.6 / 3.9 — 282.1 / 5.4 / 5 — 279.0 / 8.5 / 30 — 274.4 / 13.1 / 50

291.4 / +3.9 / 30 — 291.0 / +3.5 / 27 — 289.6 / +2.1 / 27 — 286.7 / 0.8 / 10 — 284.6 / 2.9 / 8 — 283.8 / 3.7 — 283.2 / 4.3 / 14 — 280.2 / 7.3 / 30 — 277.3 / 10.2 / 50

27 = Top of Conc Wall; 27 = Base of Conc Wall

292.9 / +5.4 / 30 — 292.7 / +4.6 / 26 — 282.9 / 4.6 / 21 — 281.6 / 5.9 / 10 — 281.0 / 6.5 — 281.1 / 6.4 / 10 — 280.6 / 6.9 / 20 — 281.7 / 5.8 / 25 — 281.7 / 5.8 / 30

290.5 / +3.0 / 30 — 279.2 / 8.3 / 18 — 277.4 / 10.1 — 277.5 / 10.0 / 10 — 276.9 / 10.6 / 22 — 283.7 / 3.8 / 27 — 283.4 / 4.1 / 30

287.45 ✓

69+5 St.

BM			3.62	302.12 ✓	on S Mon Madrone +68+5 St 302.06 P37
TP	9.45	305.74	0.44	296.29	
TP	11.25	296.73	1.97	285.48	

11+80.99 = S.L. Madrone

287.45

Lt. ℄ Rt.

281.3	277.4	272.2	270.3
6.2	10.1	15.3	17.2
30		50	50

287.45 ✓

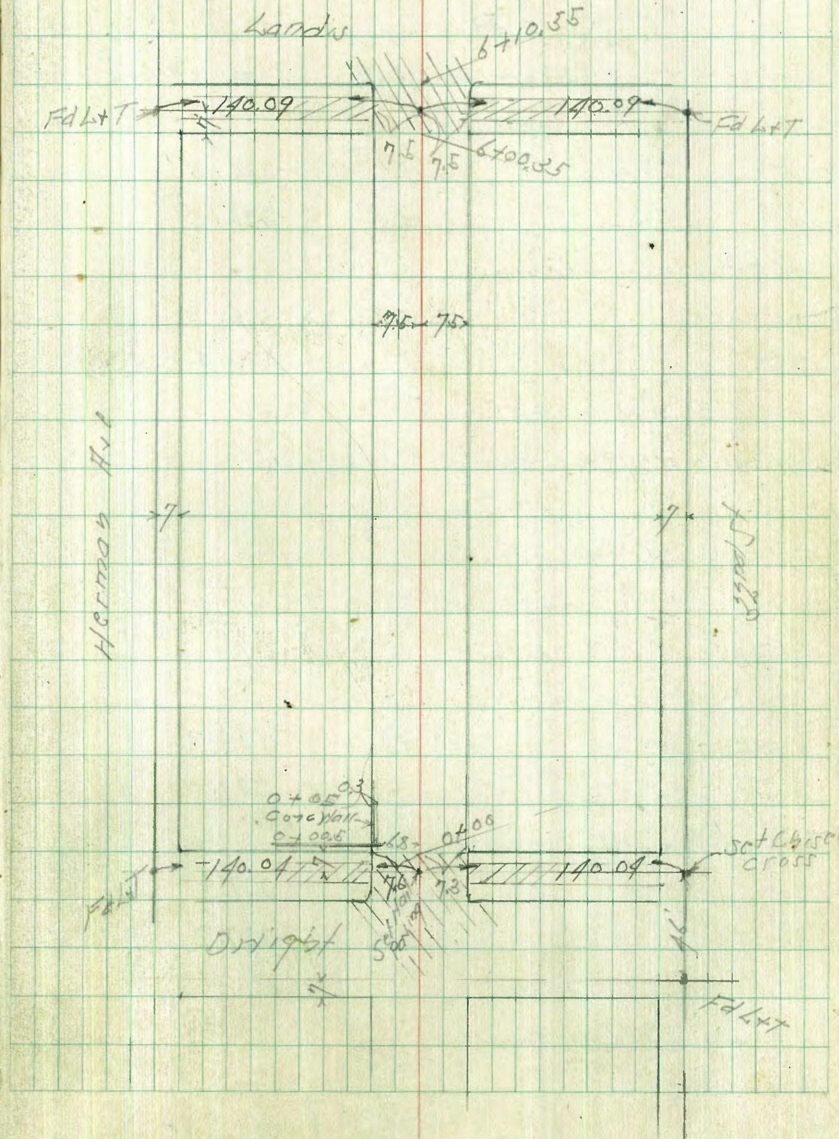
Cross Section Alley Block E McFadden + Buxtons North Park + Block 38 Park Villas Between Herman + 32nd St. From Dwight to Landis

Notes reduced C.S.K. Indexed C.S.K.

Plotted AEB 9-25-45

Sept. 24-45
Sisson
Bliss
Osborne

BM	5.53	338.05		332.52	NEBP Dwight + 31st St.
TP	5.81	340.09	5.77	334.28	
	0-10 = N Cb Line Dwight				
E			6.32	333.77	
℄			6.38	333.71	
W			6.40	333.69	
	0+0 = N L Dwight				
W	Top Cb		5.50	334.59	
"	Gutter		5.63	334.46	
℄			5.89	334.20	
E	Gutter		5.86	334.23	
E	Top Cb		5.74	334.35	
	0+10				
-2.3	= Wly House		4.1	336.0	
E			4.1	336.0	
℄			4.8	335.30	
+5.2	= Ely Power Pole				
W			3.7	336.4	
	0+23				
E +1.2	= Wly Power Pole				
	0+33				
W			3.4	336.7	
℄			3.5	336.6	
E			3.7	336.4	
+06	= ℄ + Wly 3.5' Conc Landing		3.23	336.86	



	340.09			
	0+36			
W+0.4 = Nly Board Fence				
	0+43			
E-0.3 = ℄ + Nly 4' Conc Landing		3.62		331.47
	0+50			
E		3.6		336.5
℄		3.3		336.8
+6.9 = Sly Lath Fence				
W		3.3		336.8
+20		3.7		336.4
	0+56			
W+0.6 = Nly Lath Fence				
	0+71			
W+0.8 = Sly Lath Fence				
	0+76			
W+2.1 = Ely Power Pole				
	1+0			
-15		3.8		336.3
W		3.1		337.0
+0.9 = Nly Lath Fence				
℄		3.0		337.1
E		2.9		337.2
	1+16			
W+0.9 = Sly Lath Fence				

	340.09			
	1+51			
E			2.5	337.6
℄			2.4	337.7
+6.4 = Nly Lath Fence				
W			2.7	337.4
+15			2.9	337.2
	1+64			
W + 1.2 = Sly Lath Fence				
	1+86			
E + 1.0 = Wly Tel Pole				
	1+89			
W + 1.3 = Nly Lath Fence				
	2+01			
-15			2.2	337.9
W			2.1	338.0
+1.2 = Sly Lath Fence				
+2.5 = Ely Power Pole				
℄			1.5	338.6
E			1.3	338.8
TP	7.41	346.30	1.20	338.89
	2+25			
W + 1.2 = Nly Lath Fence + Sly Wire Fence				
	2+50			
-15			7.4	338.9
E			7.1	339.2

346.30

℄	6.6	339.7
W	6.7	339.6
+15	7.0	339.3

2+76

W +1.0 = N'ly Wire Fence

2+90

W +1.1 = S'ly Wire Fence

3+0

-15	6.4	339.9
W	6.2	340.1
℄	6.3	340.0
E	6.1	340.2
+15	6.4	339.9

3+25

W +0.8 = N'ly Wire Fence

E +2.1 = W'ly Tel Pole

3+40

W +0.8 = S'ly Lath Fence

3+52

-15	5.8	340.5
E	5.4	340.9
℄	5.4	340.9
+5.5 = E'ly Power Pole		
W	5.2	341.1
+15	5.5	340.8

346.30

3+79

W +0.8 = N'ly Wire Fence

3+90

W +0.6 = S'ly Picket Fence

4+0

-15	5.2	341.1
W	4.7	341.6
℄	4.9	341.4
E	4.7	341.6
+15	5.4	341.2

4+25

W +0.2 = N'ly Picket Fence S'ly Board Garage W Entrance

4+38

W +0.2 = N'ly Garage +S'ly Lath Fence

4+50

-15	4.8	341.5
E	4.1	342.2
℄	4.4	341.9
W	4.2	342.1
+15	4.5	341.8

4+75

W = W'ly Lath Fence

W +1.4 = E'ly Power Pole

E +1.5 = W'ly Tel Pole

346.30

4+90		
W +0.1 = Sly Picket Fence		
5+0		
-1.5	3.8	342.5
W	3.2	343.1
℄	3.8	342.5
E	3.7	342.6
+1.5	4.4	341.9
5+25		
W +0.2 = Nly Picket Fence + Sly Wire Fence		
5+30		
-2.3 = Nly 2 Ribbon Conc Drive	4.15	342.15
E	3.6	342.7
℄	3.6	342.7
W	3.4	342.9
5+60		
W	3.4	342.9
℄	3.7	342.6
+7.3 = Nly 2 Ribbon Conc Drive	4.10	342.20
E	4.1	342.2
5+90		
-0.1 = Nly 2 Ribbon Drive	4.00	342.30
E	4.0	342.3
℄	4.0	342.3
W	3.9	342.4

346.30

5+99					
E +1.5 = Nly Tel Pole					
6+00.35 = S.L. Landis					
-0.5 = Nly Wire Fence					
W Top Cb			5.23	341.07	
W Gutter			5.35	340.95	
℄			5.73	340.57	
E Gutter			5.64	340.66	
E Top Cb			5.57	340.73	
+0.5' = Nly 2 Ribbon Conc Drive			5.35	340.95	
6+10.35 = South Curb Lin Landis					
E			6.31	339.99	
℄			6.11	340.19	
W			5.93	340.37	
TP	3.75	344.11	5.94	340.36	
BM			5.89	338.22	N.W. B.P. Landis + 32nd 338.47
TP	0.72	344.49	0.34	343.77	
TP	1.76	338.23	8.02	336.47	
BM			5.69	332.54	N.E. B.P. Dwight + 31st 332.52

Walker
Hozzard
Hardin
Begg 10-9-45

Cross Section - Dorcas St.
5' cbs
7.9' 1/45 Approx.
from Naples St. to Weeks St.

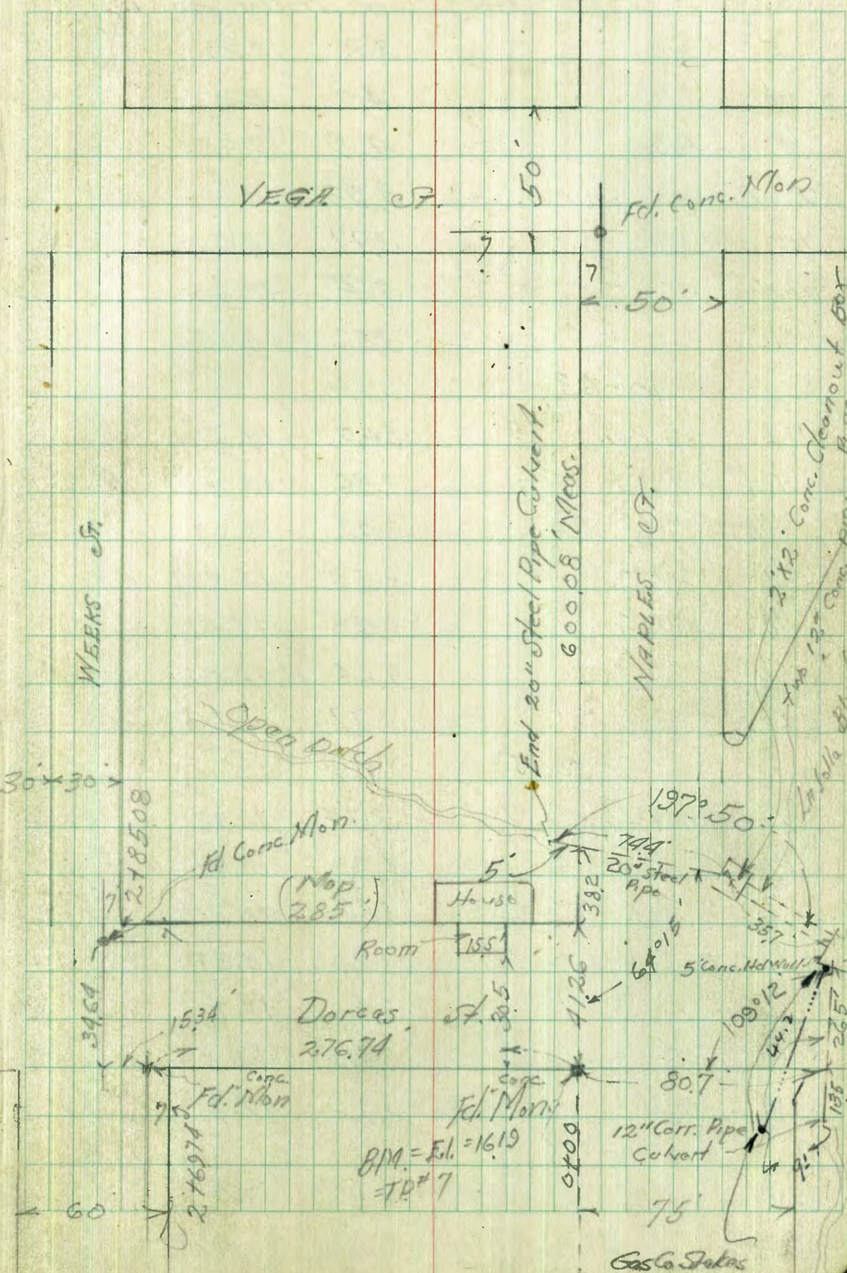
~~BM. BP.~~	4.55	24.62		
Taylor & Old Town Bridge Sly end				20.07
T.P. #1	5.36	17.75	12.23	12.39
T.P. #2	4.85	19.18	3.42	14.33
T.P. #3	4.38	19.23	4.33	14.85
T.P. #4	7.31	22.82	3.72	15.51
TP #5	5.44	25.49	2.77	20.05
T.P. #6	2.11	24.71	2.89	22.60
T.P. #7	5.88	22.07	8.52	16.19 on Mon. S'ELY Prop. Line Dorcas + Naples.

0 - 80.7 = Section Diag. over Exist. 12" Corr. Iron Pipe

W'LY end 12" Culvert	6.33	15.74
on Hd Wall over 12" Corr. Pipe	4.14	17.93
" " " over 12" Conc. Pipes	4.14	17.93
on Flow 12" " "	6.24	15.83
25' W'LY of E'LY Line	3.5	18.57
℄ Dorcas	3.7	18.37
E. Line	3.7	18.37
12' E	3.6	18.47
13.5 E on Flow 12" Corr. Pipe	5.50	16.57
40' E in Ditch	4.9	17.17
65' E " "	4.4	17.67

Limit of Cross Sections

Indexed C.S.K.



22.07

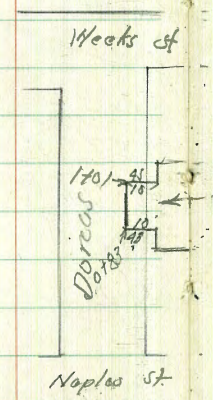
0-75 = NLy Line Naples on E.

E.	3.8	18.27
+5' = cb	4.0	18.07
¼ on Pov.	4.09	17.98
℄ Dorcas on Pov.	3.93	18.14
¼ " "	3.77	18.30
W cb " "	3.64	18.43
W.L. " "	3.52	18.55
0-63		
W.L. on Pov.	3.40	18.67
W cb " "	3.36	18.71
" ¼ " "	3.42	18.65
℄ " "	3.50	18.57
¼ " "	3.60	18.47
cb " "	3.66	18.41
E. " "	3.77	18.30
0-50.25		
E. on Pov	3.34	18.73
cb " "	3.29	18.78
¼ " "	3.26	18.81
℄ " " = Edge	3.20	18.87
¼	3.4	18.7
cb.	3.7	18.4
W	3.9	18.2
0-37.5		
W	4.5	17.6

22.07

cb	4.0	17.7
¼	4.2	17.9
℄	3.8	18.3
¼	3.4	18.7
E. cb.	3.1	19.0
E	3.0	19.1
0-24.75		
E	3.8	18.3
cb	4.1	18.0
¼	4.4	17.7
℄	4.6	17.5
¼	4.8	17.3
cb.	4.8	17.3
W	4.8	17.3
0-12		
W	5.0	17.1
cb	5.1	17.0
¼	5.0	17.1
℄	5.0	17.1
¼	5.0	17.1
cb	5.0	17.1
E	5.0	17.1
0+00 = SLy Line Naples St		
E.	5.3	16.8
cb.	5.1	17.0
¼	5.1	17.0

	22.07		Dorcas St.	
L			5.1	17.0
W			5.1	17.0
cb.			5.1	17.0
W			5.1	17.0
	0+50			
W-5			5.0	17.1
W			5.0	17.1
cb.			5.2	16.9
W			5.4	16.7
L			5.3	16.8
W			5.4	16.7
cb.			5.5	16.6
L			5.5	16.6
+5			5.5	16.6
	1+00			
-5			5.9	16.2
E			5.9	16.2
cb.			5.9	16.2
W			5.6	16.5
L			5.4	16.7
W			5.4	16.7
cb.			5.4	16.7
W			5.3	16.8
+5			5.3	16.8
TP #8	3.81	20.00	5.88	16.19



	20.00			
	1+50			
-5			3.7	16.3
W			3.7	16.3
cb.			3.3	16.7
W			3.6	16.4
L			3.6	16.4
W			3.7	16.3
cb.			3.6	16.4
E			3.7	16.3
+5			3.5	16.5
	2+00			
-5			2.2	17.8
E			2.4	17.6
cb.			2.5	17.5
W			2.6	17.4
L			2.8	16.8
W			3.3	16.7
cb.			3.7	16.3
W			4.0	16.0
House	+5		3.5	16.5
	2+50			
-5			3.5	16.5
W			3.2	16.8
cb			3.1	16.9
W			3.1	16.9
L			3.1	16.9

	2150	20.00		Dorcas St
E 1/4			2.8	17.2
cb.			2.9	17.1
E.			2.9	17.1
+5			2.7	17.3
	2+69.79 = NLY Line Weeks at an E			
-5			3.0	17.0
E			2.9	17.1
cb.			3.3	16.7
1/8			3.6	16.4
L			3.7	16.3
1/4			3.8	16.2
cb.			3.5	16.5
W			3.3	16.7
+5			3.3	16.7
	2+85.08 = NLY Line Weeks St.			10' cbs 10' 1/4S on W
W			4.2	15.8
cb.			4.3	15.7
1/4			4.2	15.8
L			3.8	16.2
1/2			3.6	16.4
cb.			3.7	16.3
E			3.2	16.8
	NLY cb. Weeks			
E			4.2	15.8
cb.			4.1	15.9
1/4			4.0	16.0
L			4.1	15.9

	20.00	
1/4	4.3	15.7
cb.	4.5	15.5
W	4.6	15.4
	NLY 1/4	
W	5.3	14.7
cb.	5.2	14.8
1/4	5.0	15.0
L	5.0	15.0
1/4	4.9	15.1
cb.	4.7	15.3
E	4.6	15.4
	Proposed - 2 Weeks St.	
E	5.6	14.4
cb	5.5	14.5
1/4	5.3	14.7
L	5.6	14.4
1/4	5.8	14.2
cb.	5.9	14.1
W	5.9	14.1
	NSLY 1/4	
W	7.4	12.6
cb.	7.2	12.8
1/4	7.1	12.9
L	6.8	13.2
1/4	6.5	13.5
cb.	6.4	13.6
E.	6.2	13.8

2000 Dorcas St

Proposed SLY cb Weeks st

E	6.8	13.2
cb	7.0	13.0
1/4	7.3	12.7
℄	7.5	12.5
1/4	7.6	12.4
cb	7.8	12.2
W	8.0	12.0
Proposed SLY Line Weeks		
W	8.6	11.4
cb	8.6	11.4
1/4	8.5	11.5
℄	8.3	11.7
1/4	8.0	12.0
cb	7.7	12.3
E	7.5	12.5
25' South of Above section		
E-15	7.8	12.2
E	8.5	11.5
cb	8.6	11.4
1/4	8.9	11.1
℄	9.3	10.7
1/4	9.6	10.4
cb	10.0	10.0
W	10.0	10.1
+25	9.9	10.1

indexed C.S.K.

Cross Section · Weeks St.

Proposed Width = 60
10' cbs
10' 1/4s

from Dorcas St - West
2000 opp Page

0+00 = WLY Line Dorcas St

S	8.8	11.2
cb	7.9	12.1
1/4	7.3	12.7
℄	5.9	14.1
1/4	5.4	14.6
cb	4.7	15.3
N	4.2	15.8
0+50		
N-10	5.0	15.0
N	5.5	14.5
cb	6.2	13.8
1/4	7.0	13.0
℄	7.6	12.4
1/4	8.8	11.2
cb	8.9	11.1
S	9.2	10.8
+15	9.6	10.4
1+00		
-15	11.9	8.1
S	11.3	8.7
cb	10.8	9.2
1/4	10.8	9.2
+5	10.3	9.7

WEEKS OF

20.00

L	8.6	11.4
1/4	7.9	12.1
cb.	6.6	13.4
N	5.9	14.1
+10	5.4	14.6
1+50		
-10	6.2	13.8
N	6.8	13.2
cb.	7.5	12.5
1/4	8.5	11.5
L	9.0	11.0
+5	10.2	9.1
1/4	11.0	9.0
cb	11.3	8.7
S	11.6	8.4
+15	12.3	7.7
1+90		
-15	13.5	6.5
S	13.0	7.0
cb	12.5	7.5
1/4	12.1	7.9
+5	12.0	8.0
L	9.9	10.1
1/4	9.5	10.5
+5	8.6	11.4
cb	8.1	11.9

20.00

N	8.1	11.9
+10	8.4	11.6
2+00		
-20	11.0	9.0
-10	11.1	8.9
N	10.2	9.8
cb.	9.4	10.6
+5	9.8	10.2
1/4	10.6	9.4
L	10.9	9.1
+5	12.3	7.7
1/4	12.7	7.3
cb	13.2	6.8
S	13.3	6.7
+20	14.1	5.9
2+06		
-20	14.8	5.2
S	13.6	6.4
cb	13.6	6.4
1/4	13.1	6.9
+5	12.7	7.3
L	11.5	8.5
1/4	11.3	8.7
cb.	11.2	8.8
N	11.3	8.7
+20	11.0	9.0

	2000	Weeks St.
	2+50	
-20	11.3	8.7
N	11.5	8.5
cb.	11.8	8.2
1/4	12.1	7.9
c	12.5	7.5
1/4	13.3	6.7
cb.	13.6	6.4
South	13.9	6.1
+20'	14.6	5.4
	2+60	
-20	14.5	5.5
S	13.8	6.2
cb.	13.2	6.8
1/4	13.2	6.8
+5	13.0	7.0
c.	11.7	8.3
1/4	11.5	8.5
cb.	12.1	7.9
N	10.9	9.1
+15	7.5	12.5
	2+70	
-15	6.9	13.1
N	8.3	11.7
cb.	9.7	10.3
1/4	10.6	9.4

	2000	Weeks St.
c	11.0	9.0
15	13.0	7.0
1/4	12.8	7.2
cb.	13.0	7.0
S	13.4	6.6
+20	13.7	6.3
TP Hg	6.00 16.65	2.35 10.65
	3+00	
-20	9.2	7.5
S	8.5	8.2
cb.	7.8	8.9
1/4	7.4	9.3
+7	6.9	9.8
c.	5.8	10.9
1/4	5.5	11.2
cb.	4.5	12.2
N	3.9	12.8
+10	3.3	13.4
	3+50	
-10	2.6	14.1
N	3.0	13.7
cb.	4.0	12.7
1/4	4.8	11.9
c.	5.5	11.2
1/4	6.5	10.2
1/4	7.2	9.5
S	8.0	8.7
+20'	8.8	7.9

4+00

-20	8.8	7.9
S	8.1	8.6
cb.	6.8	9.9
1/4	6.6	10.1
L	4.9	11.8
1/4	4.4	12.3
cb.	4.0	12.7
N	2.8	13.9
+10	2.0	14.7

4+20

-10	1.4	15.3
N	2.0	14.7
cb.	4.0	12.7
1/4	4.1	12.6
L	4.7	12.0
1/4	6.2	10.5
cb.	6.9	9.8
S	7.7	9.0
+20	8.8	7.9

4+50

-20	8.9	7.8
S	7.7	9.0
cb.	7.0	9.7
1/4	5.5	11.2
L	4.7	12.5
1/4	3.0	13.7

cb.	3.2	13.5
N	1.4	15.3
+10	0.8	15.9

5+00

-10 in Lawn	0.6	16.1
N	1.3	15.4
cb	3.0	13.7
1/4	3.0	13.7
L	4.3	12.4
1/4	6.1	10.6
cb.	8.2	8.5
S	8.5	8.2
+20	10.3	6.4

5+50

-20	13.0	3.7
S	10.6	6.1
cb.	9.6	7.1
+5	8.9	7.8
1/4	7.3	9.4
L	4.4	12.3
1/4	3.6	13.1
cb	3.0	13.7
N in Lawn	1.6	14.9
+10 in Lawn	1.5	15.2

6+00 = ELY Line VEGA ST. 19.4 7.5 1/2

N	2.6	14.1
+3	4.4	12.3

16.65 WEEKS St.

N cb.	4.7	12.0
1/4	4.8	11.9
+5	5.1	11.6
d.	7.8	9.4
1/4	11.7	5.0
cb.	13.1	3.6
S	14.1	2.6
+20	15.9	0.8
	Ely cb Vega St.	
-20	16.1	0.6
S	14.8	1.9
cb.	14.0	2.7
1/4	12.9	3.8
+7	10.9	5.8
d.	7.6	9.1
+5	5.2	11.5
1/4	4.6	12.1
cb.	4.1	12.6
N	4.1	12.6
	Ely 1/4 Vega St.	
N	3.5	13.2
cb.	3.6	13.1
1/4	5.3	11.4
+5	7.2	9.5
d.	9.9	6.8
+3	12.4	4.3

16.65

1/4	13.0	3.7
cb.	14.3	2.4
S	15.3	1.4
+20	16.3	0.4
	d. Vega	
-20	16.6	0.1
S	16.6	0.1
cb.	14.7	2.0
1/4	14.0	2.7
+7	13.3	3.4
d.	11.8	4.9
1/4	7.8	8.9
cb.	5.1	11.6
N	3.3	13.4
	Wly 1/4 Vega St.	
N	4.5	12.2
cb.	7.6	9.1
1/4	9.6	7.1
d.	12.7	4.0
+3	14.1	2.6
1/4	14.8	1.9
cb.	16.0	0.7
S	16.2	0.5
+20	16.9	-0.2
	Wly cb Vega	
-20	16.9	-0.2
S	16.2	0.5

cb.			16.0	0.7
1/4			15.5	1.2
+7			15.2	1.5
℄			12.8	3.9
1/4			11.6	5.1
cb.			9.8	6.9
N			6.0	10.7
	0+00 WLY Line Vega			
N			7.6	9.1
cb.			11.0	5.7
1/4			12.3	4.4
℄			15.3	1.4
1/4			16.4	0.3
cb.			17.1	-0.4
S			16.9	-0.2
+20			17.3	-0.6
	= 0+50	Mud Flats		
-20			16.7	0.0
S			16.7	0.0
cb.			16.7	0.0
1/4			16.7	0.0
℄			16.7	0.0
1/4			16.7	0.0
cb.			16.4	0.3
+7			15.4	1.3
N			14.5	2.2
+6			9.6	7.1
+15			9.0	7.7

1+00

-20			16.9	-0.2	
N			16.9	-0.2	
cb.			16.9	-0.2	
1/4			16.9	-0.2	
℄			16.9	-0.2	
1/4			16.9	-0.2	
cb.			17.0	-0.3	
S			16.9	-0.2	
+20			17.0	-0.3	
T.P. #10	2.74	11.53	7.86	8.79	Nail in Pole Naples St
T.P. #11 (350' W WL Vega St.)	3.41	7.71	7.23	4.30	
T.P. #12 (WLY Side Tecolote Bridge)	9.40	13.35	3.76	3.95	
Chk. B.M. B.P. o Morena Blvd.			3.29	10.06	
				10.04	
				0.02	

Walker,
Hazard
Hardin
Begg.
10-10-45

CROSS SECTION - NAPLES St.
50' Wide 10' cbs 75'/45
from WLY Line Dorcus St. WLY
Sketch P-64

	5.85	22.04		16.19
			3.66	18.38
on Cover	2"x2' Cleanout Box			
" Flow	{12" Conc. Pipe / 20" Steel Pipe		6.79	15.25
" Top	20" Steel Pipe SLY end		5.85	16.19
" Flow	" " " "		1.69 / 7.54	14.50

0+00 = WLY Line Dorcus St.

S-10	5.0	17.0
S	5.0	17.0
cb.	5.0	17.0
1/4	5.1	16.9
℄	4.8	17.2
1/4	4.6	17.4
cb.	4.4	17.6
N	3.9	18.1
+5	3.6	18.4

0+50

N-5	4.1	17.9
N	4.2	17.8
cb.	4.4	17.6
1/4	4.8	17.2
℄	4.9	17.1
1/4	5.0	17.0
Sb.	5.0	17.0
S	5.2	16.8
+5'	5.2	16.8

Indexed
C.S.K.

22.04
0+37 = 5" Cypress Tree 7' N of SL.
0+47 = Elec. Pole 8' N of SL.
1+02 = ℄ 16" Acacia Tree 7' N of SL.

1+00

-5	4.9	17.1
S	4.9	17.1
cb.	5.0	17.0
1/4	5.2	16.8
℄	5.0	17.0
1/4	5.0	17.0
cb	5.0	17.0
N	4.9	17.1

+1' at Conc. Foundation Bld on Ground
0+87 to 3+50 = Above Bld on N 1' Back

1+50

N	4.5	17.5
+8	4.3	17.7
cb.	4.7	17.3
1/4	4.6	17.4
℄	4.6	17.4
1/4	4.6	17.4
cb	4.7	17.3
S on ground	4.4	17.6

4.96 = Wall 5" conc.
~~+0.1 on Top~~

1+33 = ℄ 16" Accacia Tree on S 7' N of SL.
+48 " 4" " " " " " "
1+51 " Elec. Pole on S - 7' N of SL.
1+00 to 1+50 = 5" Conc. Ret. Wall on South
(on Line at 1+00) (0.4' in st of 1+50)

22.04 ✓ NAPLES ST.

1+93 - 6" Cypress on South 8' N of SL

1+50 to 2+00 = 5" Conc. Ret. Wall on South 1+50 = 0.4' in st. 2+00 = 0.8' in st.

2+00		
-5	3.7	18.3
S	3.9	18.1
cb.	4.1	17.9
1/4	4.1	17.9
℄	4.1	17.9
1/4	4.3	17.7
cb	4.5	17.5
+2	4.0	18.0
N	4.3	17.7
2+50		
N	4.0	18.0
+8	4.0	18.0
cb.	4.3	17.7
1/4	4.1	17.9
℄	4.1	17.9
1/4	4.1	17.9
cb.	4.0	18.0
S	3.5	18.5
+5	3.4	18.6

2+48 - Elec. Pole on S 7.5' N of SL

3+00		
-5	3.4	18.6
S	3.5	18.5
cb.	3.9	18.1 ✓

1/4			4.0	18.0
℄			4.1	17.9
1/4			4.1	17.9
cb.			4.2	17.8
N			4.0	18.0
3+50				
N			4.2	17.8
cb.			4.0	18.0
1/4			3.7	18.3
℄			3.8	18.2
1/4			3.7	18.3
cb.			3.6	18.4
S			3.2	18.8
+5			3.2	18.8
4+00				
-5			3.0	19.0
S			3.0	19.0
cb			3.8	18.2
1/4			3.7	18.3
℄			3.7	18.3
1/4			3.8	18.2
cb.			4.0	18.0
N			4.5	17.5
+5		✓	4.5	17.5
T.P.	1.12	19.44	3.72	18.32

✓

1944 ✓ NAPLES St

4+50

N-5	2.3	17.1	
N	2.2	17.2	
cb.	2.2	17.2	
1/4	1.8	17.6	
℄	1.6	17.8	
1/4	1.6	17.8	
cb.	1.8	17.6	
+4	0.8	18.6	
S	0.8	18.6	
+5	0.8	18.6	

4+50 = Elec Pole 6' N of S Line Rod = 2.18

4+85 = ℄ Conc. Drive on N 0.3' in st.

5+00

-5'	1.9	17.5	
S	1.9	17.5	
+6	1.8	17.6	
cb	2.2	17.2	
1/4	2.3	17.1	
℄	2.3	17.1	
1/4	2.6	16.8	
cb on Lawn	2.5	16.9	
N " "	2.6	16.8	
+5 " "	2.6	16.8	
5+34.5 = ℄ 7' Conc. Drive on North	2.83	16.61 ✓	0.6' in st.

5+50

-5	3.4	16.0
N	3.4	16.0

cb.	3.5	15.9
1/4	3.2	16.2
℄	3.0	16.4
1/4	2.9	16.5
cb.	2.8	16.6
+5	2.4	17.0
S	2.2	17.2
+5	2.2	17.2

6+00.08 = ELY Line VEGA St 50' wide 10' 2.45 7.5 1/4

-5	3.0	16.4
cb.	3.4	16.0
1/4	3.5	15.9
℄	3.3	16.1
1/4	3.5	15.9
cb.	4.0	15.4
N	4.2	15.2
+5	4.1	15.3
	3.24	16.20

5+46 = ℄ 11' Conc. Drive on N 1.2' in st.

6+10 = E cb Vega St

-5	4.5	14.9
N	4.3	15.1
cb	4.0	15.4
1/4	3.5	15.9
℄	3.4	16.0
1/4	3.5	15.9
cb	3.9	15.5
S	3.3	16.1

✓

E ¼ Vega St.

South.	3.5	15.9
Cb.	3.7	15.7
¼	3.6	15.8
Do.	3.6	15.8
¼	3.6	15.8
Cb.	3.8	15.6
N	4.2	15.2

E Vega St. = 6+25

N'	4.1	15.3
Cb.	3.9	15.5
¼	3.8	15.6
Do.	3.7	15.7
¼	3.7	15.7
Cb	3.6	15.8
South	3.3	16.1

W ¼ Vega St.

S	3.6	15.8
Cb.	3.8	15.6
¼	3.8	15.6
Do.	3.9	15.5
¼	4.0	15.4
Cb	4.3	15.1
N	4.5	14.9

W Cb. Vega St.

N	4.6	14.8

Cb.	4.6	14.8
¼	4.3	15.1
Do.	4.1	15.3
¼	4.1	15.3
Cb.	4.2	15.2
S	3.5	15.9

6+50 = W.L. Vega St.

S	3.8	15.6
¼	4.0	15.4
Cb.	4.3	15.1
¼	4.4	15.0
Do.	4.3	15.1
¼	4.6	14.8
Cb.	4.9	14.5
N	4.7	14.7

6+53 Elec. Pole 3.5' N of St.

7+00

S	6.4	13.0
N	6.3	13.1
Cb	6.3	13.1
¼	6.2	13.2
Do.	5.7	13.7
¼	5.9	13.5
Cb.	6.1	13.3
¼	5.2	14.2
S	4.8	14.6
15	48	14.6

7+50 1944

-5			5.9	13.5
S			6.1	13.3
+9'			6.6	12.8
Cb.			7.4	12.0
1/4			7.4	12.0
℄			7.3	12.1
1/4			7.6	11.8
Cb.			7.7	11.7
N			7.5	11.9
+5			7.7	11.7
	8+00			
-5			9.7	9.7
N			9.6	9.8
Cb			9.5	9.9
1/4			9.2	10.2
℄			9.0	10.4
1/4			9.0	10.4
Cb			9.1	10.3
+2			8.7	10.7
S			8.1	11.3
+5			7.6	11.8

8+00 = Elec Pole 37' N of ℄ Line
8+00 24" Accacia Tree 6.3' in st on N
+10 12" " " " "
+21 12" " 6.8 " " "
+32 10" " " 6.3 " " "

1944 Naples St

8+64 = 18" Accacia Tree on North 6' in st.
+89 " 10" " " " " 6.6 " "
9+58 30" Date on North 5 " "
+61 " " " " 6.5 " "

	8+50				
-5				10.5	8.9
S				10.5	8.9
Cb.				11.1	8.3
1/4				11.1	8.3
℄				11.0	8.4
1/4				11.1	8.3
Cb.				11.4	8.0
N				11.4	8.0
+5			1	11.4	8.0
T.P.	0.73		8.62	11.55	7.89
	9+00				
-5				2.2	6.4
N				2.2	6.4
Cb.				2.4	6.2
1/4				2.6	6.0
℄				2.6	6.0
1/4				2.8	5.8
+6				2.6	6.0
Cb.				2.6	6.0
S				2.8	5.8
+5				2.8	5.8

8.62 ✓ NAPLES ST.

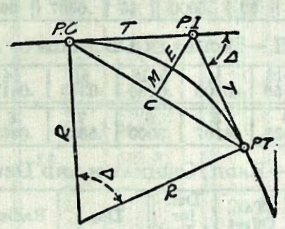
	9+50		
5-		6.5	2.1
South		6.4	2.2
cb.		6.0	2.6
¼		5.3	3.3
℄		5.2	3.4
¼		5.4	3.2
cb.		5.4	3.2
N		5.3	3.3
+5		5.3	3.3
	10+00		
-5		6.1	2.5
N		6.2	2.4
cb		6.5	2.1
¼		6.5	2.1
℄		6.4	2.2
¼		6.8	1.8
cb.		7.1	1.5
South		7.0	1.6
+5		7.0	1.6
	10+50		
-5		7.6	1.0
5		7.6	1.0
cb		7.5	1.1
¼		7.6	1.0
℄		7.3	1.3

8.62

¼	7.5	1.1
cb	7.5	1.1
N	7.4	1.2
+5	7.3	1.3
chk Nail in Pole 9+50	4.34	4.28
		4.30
		.02

✓-T.P. = 11
P-7.3

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES



729.96
470.96
259+

CURVE FORMULAS

Radius=R=$\frac{50}{\text{sin. } D/2}$ (1) Degree of Curve=D and sin. $\frac{D}{2}=\frac{50}{R}$ (2)

Tangent=T=R tan $\frac{\Delta}{2}$ (3) Length of Curve=L=100$\frac{\Delta}{D}$ (4)

Middle ordinate=M=R(1—cos. $\frac{\Delta}{2}$) (5)=R vers $\frac{\Delta}{2}$ (6)

External=E=T tan $\frac{\Delta}{4}$ (7)=R ÷ cos. $\frac{\Delta}{2}$—R (8)=R exsec $\frac{\Delta}{2}$ (9)

Long Chord=C=2 R sin. $\frac{\Delta}{2}$ (10) △=Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. △=62° 10′ D=8° 20′. From Table IV for 1° curve T=3454.1 and ÷8⅓=414.49 ft. From Table V correction=.36 or T=414.85 ft. P. C.=Sta. P.I.—T=157 +45.50. Also from (4) L=746.00 and P. T.=Sta. P. C.+L=164+91.50.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset=7.27 $(54.50 \div 100)^2$=2.16 ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26)$=2.16 ft.

Deflections.—Deflection angle=½ D for 100 ft., ¼ D for 50 ft., etc. For c ft.=(in minutes) .3 x C x D° or=defl. for 1 ft. from Table III x C. For Sta. 158 of above curve=.3 x 54.5 x 8⅓=136.2′ or 2° 16.2′, or=2.50 x 54.5=136.2′ from Table III. For Sta. 159 deflection angle=2° 16.2′ +8° 20′ ÷2=6° 26.2′, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve E=960.6 for 8° 20′=960.6 ÷8⅓=115.27 and from Table V correction=.10 or E=115.37 ft. Or suppose △=32° and E is measured and found to be 42 ft. What is D? From Table IV E=230.9 and ÷42=5.5 or D=5° 30′.

DIAGRA
HORIZON

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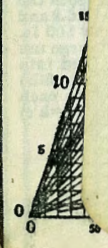
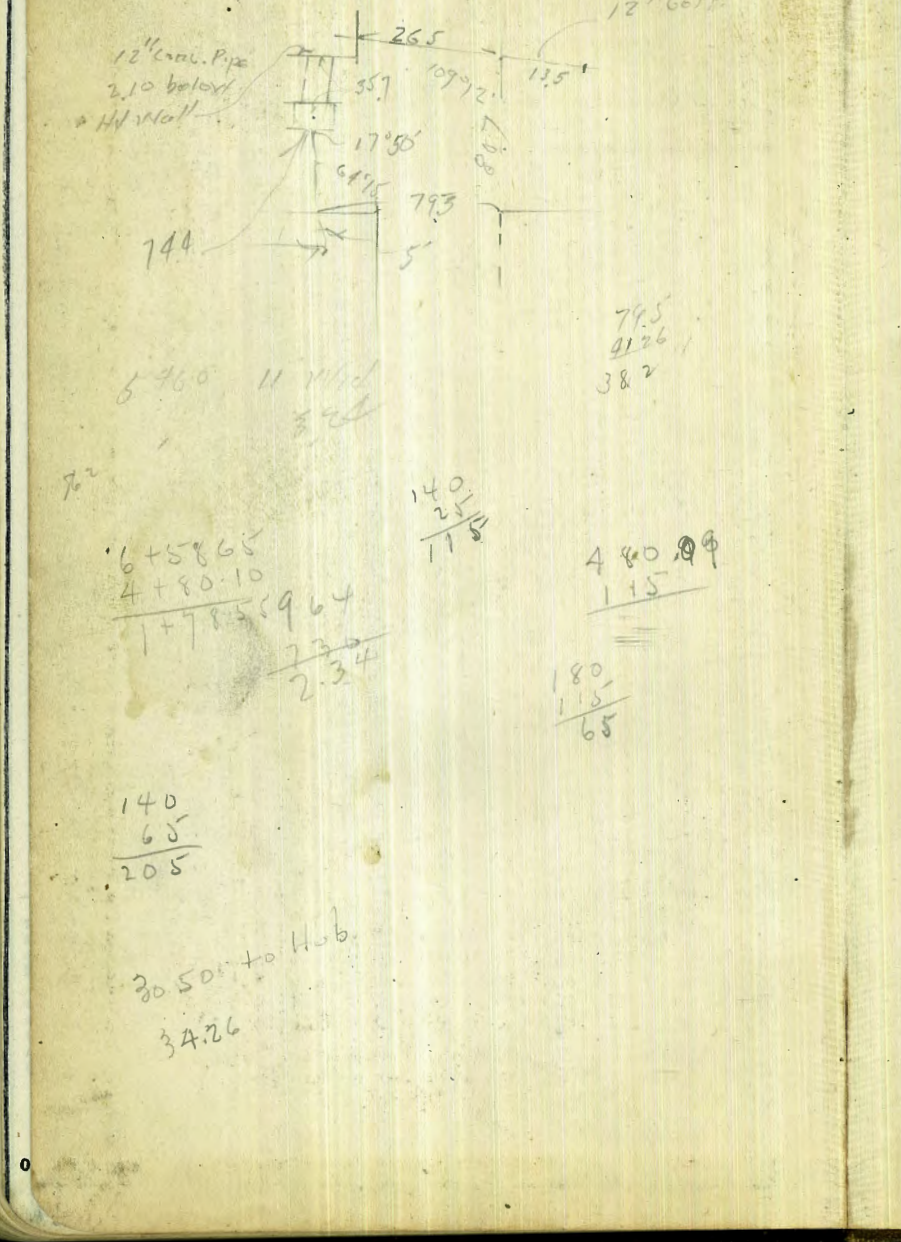
be added to
Distance T
scale plus a
5° of vertical
is the Vertic



STADIA READING X



DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway. 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)÷2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.