



# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

# 1687

CITY ENGINEER'S OFFICE

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to  $30.6 = 32.6$ . For slopes of 1 on  $1\frac{1}{2}$  see inside of back cover.

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Walker PROPOSED CULVERT at -  
 Hardin  
 Hunley. E.L. CAJON Ave / FLORIDA ST.  
 1-8-46

B.N. SW. Pt.  
 Florida  
 E.L. Cajon  
 P-68

5.99 306.64

300.65

Locals Proposed Drain

0+00 on stake	5.10	301.59
+25	4.9	301.7
+50	4.7	301.9
+75	4.9	301.7
1+00	5.0	301.6
+25	5.2	301.9
1+49.36 $\Delta R$ , $60^{\circ}22'$	5.07	301.57
1+56.86 N edge Walk	5.26	301.38
+62.4 Bk. in Walk	5.12	301.52
1+68.2 S edge Walk	5.13	301.51
1+75.26 $\Delta R$ , $25^{\circ}54'$	5.57	301.07
1+99.2 E edge Side Walk	5.89	300.75
2+02.28 on Walk	5.92	300.72
4' South on Flow <sup>Box</sup> Culvert	13.08	292.66
" " on Grading	6.83	299.81
" " Top cb.	6.03	300.61
" Flow cb Inlet to East	10.12	296.52
East end cb. Inlet		
= $30^{\circ}$ E. E.L. Florida on cb	5.59	301.05
" " " " Flow	8.79	297.85
4" N.N. cb. E.L. Cajon		
35" E.L. Florida = 30" Euc. Tree		

For Rate of  
 Plans to mark  
 See Plan 377L  
 3785L  
 3786L

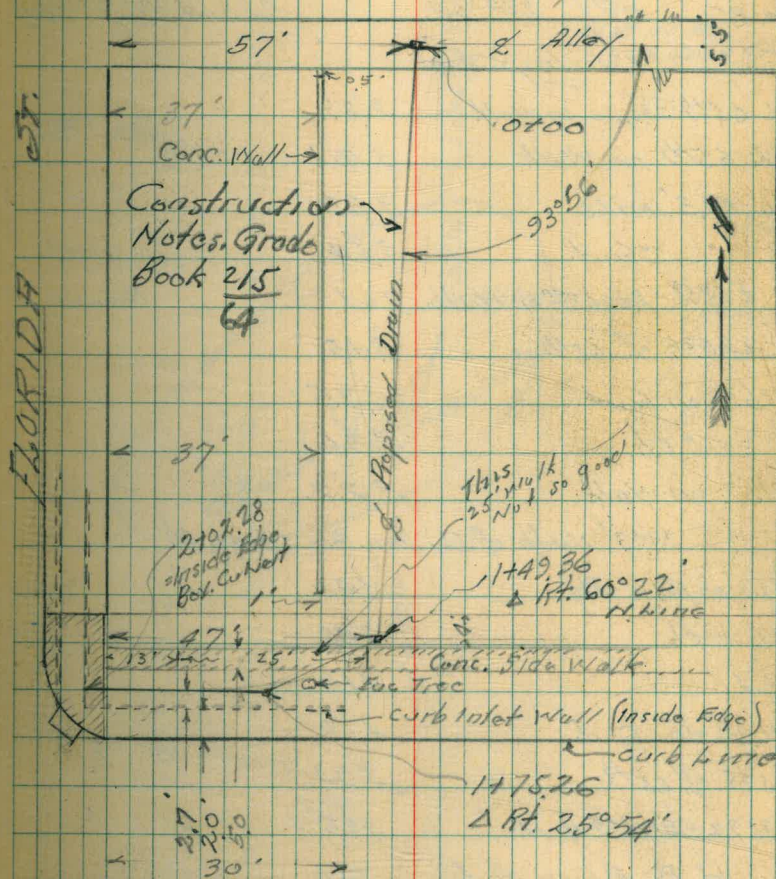
on N cb  
 E.L. Cajon

Cont. P. 80

B.R. 100, Univ. Hts. <sup>indexed</sup>  
 c.s.k.

1

Note: Cross Sections Alley P-68.



E.L. CAJON 8440.



Walker  
Hugard  
Hugard  
6-11-45

CROSS SECTION - 65th ST.  
from Sta. Imperial Ave 10' cbs } to St  
7.5' cbs } Brooklyn  
to Broadway Ave

FB. 1664  
Page 8

097 229.61

B.M. SE Top  
Imp. 65th  
223.64

Sta. Imp. Ave

W.L. 65th - 30.30 on Walk 2.83

W.L. 65th on Walk 3.21

W.L. + 9.3' on cb. 3.33

" " " Gut. 3.64

" + 13.58 = El. 65th on North. 3.61 Produced

W.L. + 25.26 = El. 65th 3.45

Fcb. on Gut. 3.75

" " cb. 3.36

El. on Walk 3.22

1363' North of Sta. Imp. Ave - East. Cb.

El. on Brass Ply 3.98

El. " cb. 3.49

Gut. 4.16

El. + 10.10 = G. Gut. 4.10

+ 25.25 = El. 65th 3.94

+ 36.92 = El. 65th on N. 3.85

W.L. at P.C. Return Gut 3.80

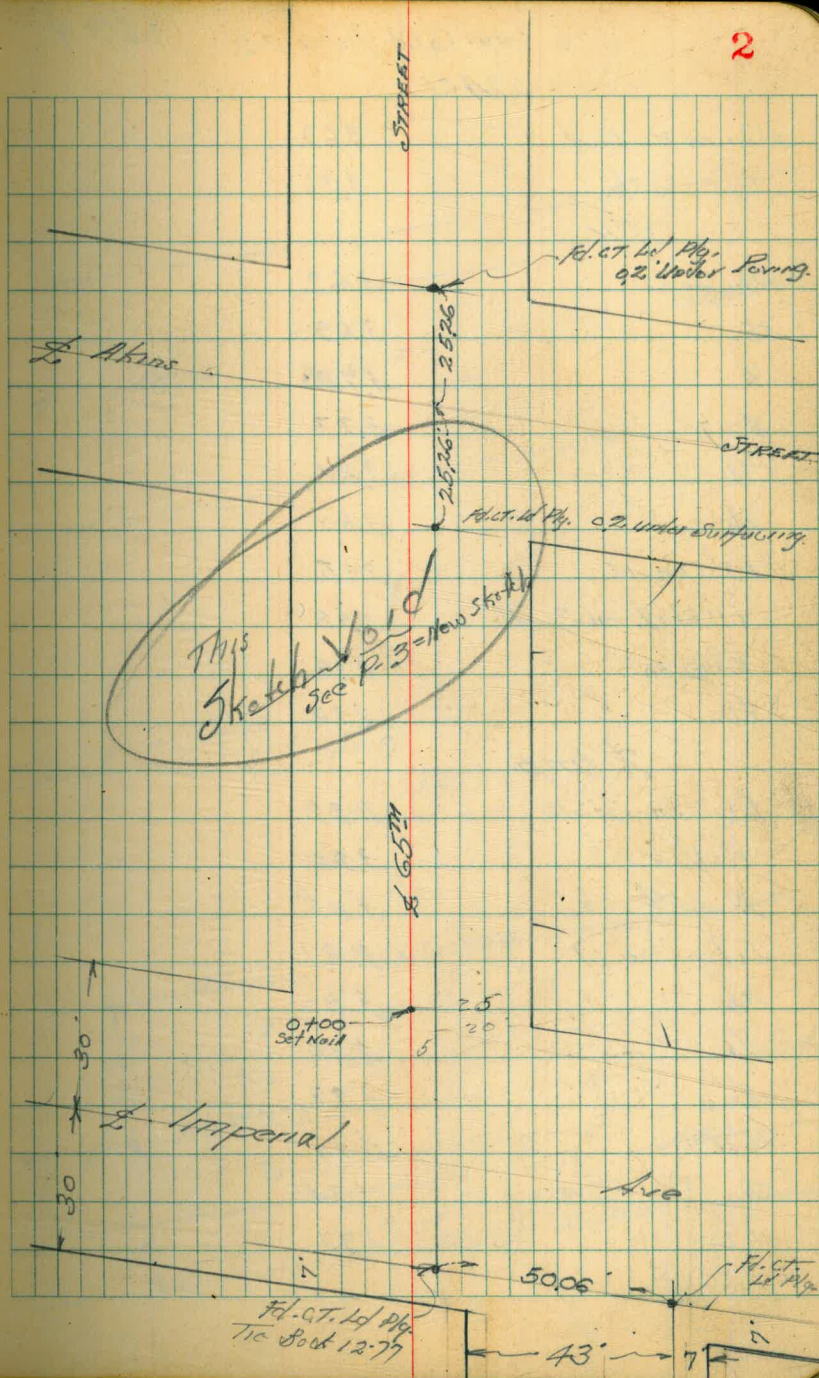
" on cb. 3.44

El. 65th - North Gut 3.81

W.L. 3.79

cb. 3.74

2





S cb. Imp. Cont. from p-2 65th St

22461

W.L. on N Gut 3.69

" " " cb. 3.32

S 1/4

W.L. on N 3.62

cb. 3.69

1/4 3.73

2. 3.77

1/4 3.81

cb. 3.80

E.L. on N 3.85

+11.67' on South 3.98

E. cb. on " 4.04

E.L. " " 4.10

S Imp.

E.L. on South 3.93

E. cb. " " 3.90

S 65th " 3.85

E.L. on N 3.81

cb. " 3.80

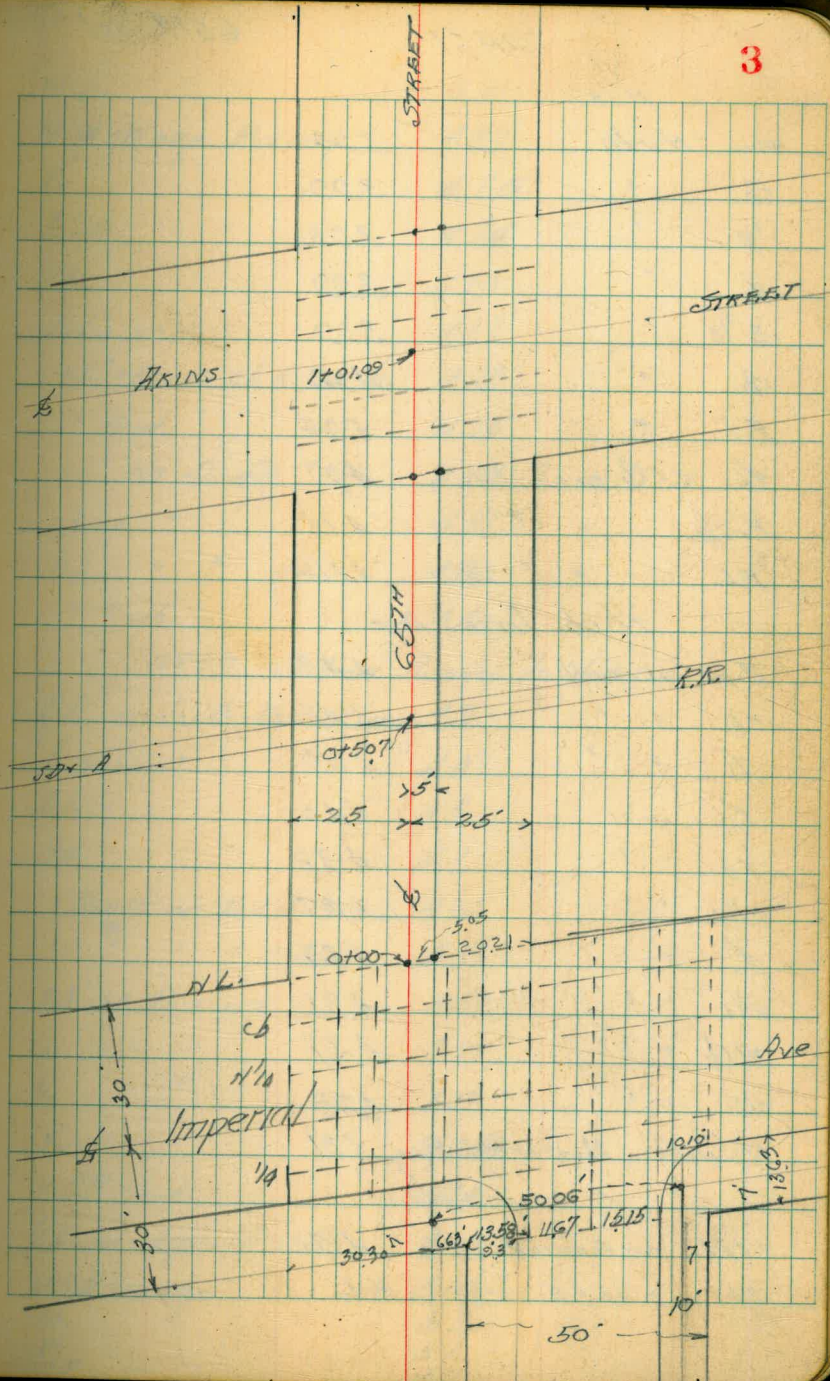
1/4 " 3.80

2. " 3.78

W 1/4 " 3.76

cb. " 3.74

W.L. " 3.71





22A.61

65TH ST

4

N 1/4		
W.L. - North		3.24
cb	"	3.29
1/4	"	3.28
2	"	3.29
E 1/4	"	3.29
cb.	"	4.02
EL.	"	4.04
To 65th on South.		4.07
E. cb.	" "	4.11
EL.	" "	4.11

N. cb. Imp. Arc

EL. on South		4.43
cb.	" "	4.46
2	" "	4.43
EL. on N		4.40
cb	" "	4.38
1/4	" "	4.37
2	" "	4.34
W 1/4	" "	4.31
W. cb	" "	4.27
W.L.	" "	4.23

1.5' North of Alaska - N. edge Paring. 4.31

0 + 00 = N.L.

-W.L. on Ground.		4.5
+4! 2' N - 2 20" E. cc. Pole		

W. cb.		4.6
W 1/4 - W. edge Paring.		4.87
2		4.75
E 1/4		4.74
cb.		4.79
EL. on N		4.87
+6' - B.C. 10' cb R on cb.		4.23
" East.		4.75
cb. on South		4.26
East " "		4.82
EL. " " cb		4.23
" East.		4.80

0 + 09 Section Parallel to Imp.

EL. on South Asphalt landing		4.3
2 65th "		4.5
EL.		4.6
+4		5.1
1' South on End cb Return		4.74
" " " " " East		5.33
+5' on Paring		5.59
cb	" "	5.39
1/4	" "	5.27
2		5.24
+5.3 = East.		5.35
1/4 on Asphalt West		4.94
+5.4 = W. edge "		5.10
cb.		5.3
W		5.1
+5		5.0



22A61

65TH ST

0+77.5 - 18.7 H of  $\phi$  = 12" Tol Pole.

0+80 Section Parallel to Atkins

-15	12.8
-8	11.4
W.L.	10.2
cb.	8.3
+3 = W edge Pav.	8.13
1/4 on "	7.81
2/4 " "	7.62
1/4 " "	7.57
cb.	7.78
+6 E edge "	8.09
E.L.	8.3
+2	8.1
+12	11.5
+15	11.8

1+01.09 = S.L. Atkins

-15	12.4
-7	11.7
E.L.	9.7
+4 = Edge Pav.	8.51
cb.	8.26
1/4	8.03
2/4	8.05
1/4	8.20
+3 = W edge Walk	8.24
cb.	8.6

22A61

6

W.L.	10.1
+15	12.0
5 cb. Atkins st.	
-15	12.2
W.L.	10.2
cb.	8.7
+5 = Edge Pav. 1774	8.43
1/4 on "	8.38
2/4 " "	8.22
1/4 " "	8.23
cb. " "	8.47
+6 E edge "	8.65
+8	8.8
E.L.	10.2
+6	11.7
+15	12.2
5 1/4 Atkins	
-15	11.9
-4	11.0
E.L.	9.7
+4 = E edge Pav.	8.78
E cb. on "	8.59
1/4 " "	8.36
2/4 " "	8.33
1/4 " "	8.44
+5 W edge "	8.58



22461

65TH ST

cb		8.8	
+2		9.1	
WL		11.3	
+15		13.2	
L. AKINS			
-15		13.7	210.9
WL		12.5	212.1
+7.3	2' N = 2 36° Euc. Tree		
+7		9.3	215.3
cb		9.2	215.9
+3	W edge Walk	8.29	216.32
+5.2	E. MH on Rim	8.29	"
1/4	on Walk	8.29	"
+1.5	on Gut,	8.45	216.16
E	on Parking	8.44	216.17
1/4	" "	8.47	216.18
cb	" "	8.69	215.92
+7		8.28	215.63
E.L.		10.3	219.3
+15		12.0	212.6
T.P.	4.57 220.70	8.48	216.13
N 1/4 AKINS			
-15		8.5	212.2
E		8.9	212.9
+2		5.1	215.5
+4	E edge Parking	5.04	215.66

22070

Ecb. on Parking	4.82	215.88
1/4 " "	4.61	216.09
E " "	4.57	216.13
+6 " "	4.58	216.12
1/4 " "	4.27	216.93
+5 Edge Walk	4.41	216.29
cb	5.4	215.3
+5	7.9	212.8
WL	9.7	211.0
+15	10.2	210.5
N CB - AKINS		
-15	10.2	210.5
W	9.6	211.1
+2	9.5	211.2
+2.5	8.6	212.1
cb	5.7	215.0
+3 W edge Walk	4.37	216.33
1/4 on Pav	4.31	216.39
+1 " "	4.69	216.01
E " "	4.62	216.08
1/4 " "	4.69	216.01
cb " "	4.89	215.81
+6.5 E edge Pav	5.13	215.57
E.L.	6.2	219.5
+2	7.13	213.9
+15	8.2	212.5



22070

65TH ST

145161 = N<sub>2</sub> Akins

-15		8.5	212.2
-4		7.2	213.5
±L.		5.4	215.3
+4	E edge Pav.	5.13	215.57
cb	on "	4.97	215.73
1/4	" "	4.79	215.91
±	" "	4.76	215.99
+6	" "	4.84	215.86
1/4	on Asphalt Walk	4.47	216.23
+6.5	W edge "	4.52	216.18
cb.		5.2	215.5
+7.5		8.5	212.2
+8		9.6	211.1
WL.		9.6	"
+15		10.2	210.5

1477.0 Section Pt A to 65<sup>1/2</sup>

-15		10.2	210.5
WL.		9.6	211.1
-2.5		9.7	211.0
+2.0		8.2	212.5
cb.		4.4	216.3
+3	W edge Walk	4.62	216.08
1/4		4.61	216.09
+1		4.61	"
+2		5.05	215.55
±		4.95	215.75
1/4		5.00	215.70

22070

8

cb.		5.10	215.60		
+3		5.14	215.56		
+6	on Wing Wall Bridge	4.93	215.77		
+7		6.7	214.0		
E		6.3	219.2		
+9		7.1	213.6		
+15		9.2	211.5		
T.P.	4.31	220.69	4.32	216.38	2150 & Mist
1487.9 = South end Wooden Bridge					
15		12.5	208.2		
E		7.8	212.9		
cb.		7.4	213.3		
+2	on Bridge	5.22	215.97		
1/4		5.01	215.68		
±		5.02	215.67		
+2.7	= W edge Bridge	5.06	215.63		
1/4	on Walk	5.08	215.61		
+3	W edge Walk	4.84	215.85		
cb.		5.3	215.2		
+2		5.9	219.8		
+7		8.9	211.8		
W		9.4	211.3		
+15		9.8	210.9		
1490					
-15		9.9	210.8		
W		9.6	211.1		



22069

65TH ST.

+3		20	211.7
cb.		67	217.0
+6.8	Ground at Bridge	7.1	213.6
1/4		15.3	205.4
L		15.3	205.4
1/4		15.3	205.4
+5.5		13.3	207.4
cb		11.4	209.3
E		9.8	210.9
+15		14.5	206.2
	2+00		
-15	in ch.	14.3	206.4
E.	" "	14.8	205.9
cb.		14.4	206.3
1/4		14.4	206.3
L		14.4	206.3
1/4		15.0	205.7
cb.		15.0	205.7
W		13.7	207.0
+15		12.1	208.6
	2+27		
-15	in ch.	16.0	204.7
W	" "	15.5	205.2
cb	" "	15.1	205.6
1/4	" "	14.8	205.9
L	" "	14.7	206.0
1/4	" "	14.5	206.2

22069

9

cb		14.8	205.9
E		14.5	205.8
+15		14.0	206.7
	2+35		
-15		9.3	211.4
-4		9.4	211.3
E		7.9	212.8
cb		8.7	212.0
+2		11.0	209.7
1/4		13.0	207.7
E.		14.3	206.4
1/4		13.0	207.7
cb		11.0	209.7
W		12.3	208.4
+15		15.5	205.2
	2+37.1 = N end Bridge		
-15		14.5	206.2
W		10.8	209.9
cb		8.6	212.1
+0.1	on wing wall	5.6	215.1
+6.5	on Bridge deck	5.10	215.59
1/4	" " "	5.10	215.59
+4.8	on " Pav.	4.74	215.95
L	" " "	4.76	215.93
1/4	" " "	4.73	215.96
+5	" " "	4.79	215.90



22069

65th St

cb. on wing wall	547	215.22
F	79	212.8
14	23	211.4
+15	24	211.3
	2+50	
-15	50	215.7
-6	86	212.1
F	55	215.2
+2	42	216.5
+8 = E edge Pav.	46	216.1
cb. on "	465	216.04
14 " "	433	216.36
2 on "	431	216.38
14 " "	441	<del>216.28</del>
+15' W edge "	458	216.11
cb	58	214.9
W	61	214.6
+15	88	211.9
	2+75	
-15	77	213.0
W	78	212.9
cb.	32	217.5
t3 = W edge	253	218.16
+7	240	218.29
1/4 Gutters	285	217.84
4	274	217.95

22069

10

14	273	217.96
cb	286	217.83
t3	285	217.84
+4	23	218.4
+7	26	218.1
F	35	217.2
+4	71	213.6
+15	75	213.2
TP	1095	230.63
	101	219.68
	2+21.85 ±	= S. L. Herrick on East
-15	161	214.5
E-4	152	215.4
E	140	216.6
+4	115	219.1
+6	112	219.4
+9 E edge Pav.	1171	218.92
cb on "	1169	218.94
14	1197	219.16
2	1151	219.12
+6	1166	218.97
14	1113	219.50
+5	1142	219.21
cb.	120	218.6
+7	137	214.9
W	166	214.0
+15	171	213.5



23063

65th St.

	3+26.852=opp	N.L. Herrick on East	
-15		16.3	224.33
W		15.2	215.4
+3		14.7	215.9
cb.		10.1	220.5
+3 on Walk		9.34	221.29
1/4 " "		9.03	221.60
+1 on Pav.		9.40	221.23
L " "		9.14	221.49
1/4 " "		9.07	221.56
cb " "		9.36	221.27
+1 E edge Pav		9.98	221.15
+3		8.8	221.8
+8		9.9	220.7
L		10.0	220.6
+15		10.1	220.5
	3 +50		
-15		7.9	222.7
E		7.7	222.9
+7		7.60	223.03
+8. E edge Pav		7.78	222.85
cb on "		7.60	223.03
1/4 " "		7.40	223.23
L " "		7.46	223.17
+6 " "		7.73	222.90
1/4 " walk		7.95	223.28

11

	746	223.17
+5		
cb	7.91	222.72
W	11.9	218.7
+15	12.4	218.2
	4100	
-15	10.3	220.3
W-4	9.7	226.0
-3	7.3	223.3
W	7.1	223.5
+8	3.7	226.9
cb.	3.5	227.1
+2 Asphalt Walk	3.41	227.22
1/4 " "	3.25	227.38
+1 Pav.	3.86	226.77
L on "	3.70	226.93
1/4 " "	3.71	226.92
cb " "	3.93	226.70
+2 " E edge Pav	3.95	226.68
+4	3.2	227.4
E	3.5	227.1
+15	3.0	227.6
	4120	
-5	1.6	229.0
E	1.9	228.7
+5	1.7	228.9
+8 E edge Pav	2.43	228.20

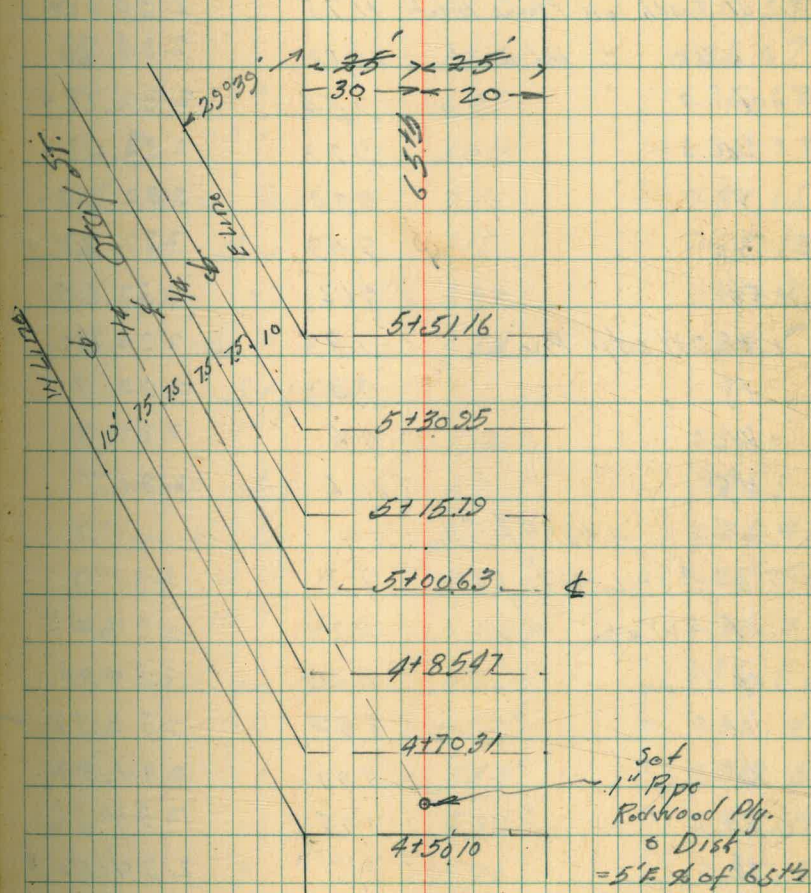


23063

65th

12

cb.	on Pav.	2.38	228.25 ✓
1/4	" "	2.06	228.57
1/2	" "	2.06	228.57
7/8	" "	2.15	228.48
1 1/8		1.51	229.12 ✓
7/4	W edge Walk	1.55	229.08
cb		1.5	229.1
+2		1.7	228.9
+4		2.5	228.1
W		3.1	227.5
+10		4.0	226.6
T.P.	11.99 242.31	0.31	230.32
Left B.M. on 1" Pipe	11.27	231.04	20' 10" SE of 65th
	4+50.10		
-5		13.0	229.3
W		12.7	229.6
+5		11.0	231.3
cb.	on Walk	10.80	231.51
+3	on 1"	10.88	231.45
+4	Guts	11.34	230.97
1/4	on Pav	11.25	231.06 ✓
1/2	" "	11.09	231.22
1/2	" "	11.08	231.23
cb.	" "	11.34	230.97 ✓
7/8	Edge "	11.38	230.93
+5		10.0	232.3
F		9.7	232.6
+5		9.9	233.0





24231

65th St

4+7031

-5		8.1	234.2
E		8.5	233.8
+A		8.9	233.4
+6 = E edge Pav.		9.73	232.58
11' South on Floor Inlet	11.75		230.56
" " Ad Wall	10.58		234.73
cb.	9.54		232.77 ✓
1/4	9.28		233.03
L	9.34		232.97
1/4	9.59		232.72 ✓
cb.	9.62		232.69
+6 = W edge Pav.	9.89		232.42
+8	9.4		232.9
W	9.6		232.7
+5	10.6		231.7

4+8597

-20.1 - W edge Otay	7.3		235.0
W = W edge Pav.	8.28		234.03
cb. on "	8.26		234.05
1/4 " "	8.32		233.99 ✓
L " "	7.99		234.32
1/4 " "	7.95		234.36
cb.	8.19		234.12 ✓
+5 = E edge "	8.43		233.88
+8	7.8		234.5
E	7.7		234.6
+5	7.5		234.8

24231

13

5+10063

-5		5.9	236.4
E		6.8	235.5
+A		6.9	235.4
+5 = E edge Pav.		7.22	235.09
cb on "		6.92	235.39 ✓
1/4 " "		6.64	235.67
L " "		6.69	235.62
1/4 " "		7.03	235.28 ✓
2.5 Valley East		7.16	235.15
cb. on Pav.		7.18	235.13
W " "		6.82	235.49
+6 = W edge "		6.74	235.57
		5+15.79	
W		6.2	236.1
+6 = East Otay		6.2	236.1
+7' on Walk		5.83	236.48
cb. " "		5.80	236.51
+A " "		5.58	236.73
+5 East on Pav.		5.96	236.35
1/4 " "		5.83	236.48 ✓
L " "		5.43	236.88
1/4 " "		5.39	236.92
cb. " "		5.70	236.61 ✓
+5 = E edge "		6.02	236.29
+6		5.9	236.4
E		5.5	236.8
+5		4.7	237.6



242.31

65TH

5+30.95

-5	3.5	238.8
F	4.2	238.1
+4	4.5	237.8
+5 = E. edge Pav.	4.58	237.74
cb on "	4.38	237.94
" " "	4.15	238.17
" " "	4.17	238.15
" " "	4.63	237.69
+2 Gut	4.73	237.59
+3	4.5	237.8
+7	4.1	238.2
cb. on Walk	4.36	237.96
+5 " "	4.19	238.13
W	4.3	238.0
5+51.16		
W	2.4	239.9
+3 on Walk	2.35	239.97
+8 " "	2.29	240.05
cb	2.22	240.10
+2	2.2	240.1
+4	2.8	239.5
+5 Gut on Pav.	3.02	239.29
" " "	2.90	239.41
" " "	2.51	239.80
" " "	2.49	239.82

242.31

14

cb	2.71	239.60
+5 E. edge Pav.	2.95	239.34
+6	2.67	239.64
F	2.3	240.0
+5	2.0	240.3
TR 12.90	254.64	0.57
		11.22
5+75 = E 3' Walk on East 12.4' Back		
6+00		
-5	11.0	243.6
F	11.1	243.5
+4	11.07	243.57
+5 = Gut on Pav.	11.28	243.36
cb. " "	11.03	243.61
" " "	10.80	243.84
" " "	10.79	243.85
" " "	11.06	243.58
+3 = Gut " "	11.16	243.48
+5	10.7	243.9
+6	9.4	245.2
cb	9.3	245.3
+4	9.33	245.31
+7	9.38	245.26
W	9.50	245.14
+5	10.0	244.6
Elec. Pole 13' Lt of E		
6+11.8 = Pole		



254.64

65th St

6+29 = L 2' Conc. Ribbon on E

18.5 RT of L	8.19	246.47
25 RT " "	7.51	247.13
6+33.8 = L N Ribbon		
25 RT	7.18	247.46
19 R	7.96	246.68

6+50

-5	5.0	249.6
W	5.3	249.3
+4 on walk	5.23	249.41
+7 " "	5.27	249.37
cb.	5.5	249.1
+3	6.7	249.9
+5 Gut. on Pav.	7.16	247.48
1/4 " "	7.04	247.60
L " "	6.83	247.81
1/4 " "	6.83	247.81
cb. " "	6.92	247.72
+5 Gut. " "	7.07	247.57
+6	6.7	247.9
E	5.8	248.8
+5	5.2	249.4

6+93

-5	2.2	252.4
E	2.8	251.8
+4	3.27	251.37
+5 = Gut on Pav.	3.48	251.16

254.64

cb. on Pav

3.56

251.08 ✓

1/4 " "	3.56	251.08
L " "	3.53	251.11
1/4 " "	3.92	250.72 ✓
+2 Gut " "	4.04	250.60
cb.	2.1	252.5
+2 on Walk	1.94	252.70
+6 " "	1.96	252.68
W	1.8	252.8
+5	2.3	252.3

6+96 = L Conc Ribbon

18 RT of L	3.18	251.42
28 " " "	2.01	252.63

7+01 = N Ribbon

28 RT on Con. G	1.88	252.76
18 RT " "	2.97	251.67
T.P. 13.13	267.47	0.30
		254.34

7+50

Web +5 = Gut.	12.38	255.09
1/4 on Pav	12.32	255.15 ✓
L " "	11.94	255.53
1/4 " "	11.94	255.53
cb. " "	12.23	255.24 ✓
+5 Gut	12.51	254.96
+6	12.0	255.5
E	11.5	256.0
+5	11.1	256.4



26747

0.2' Back.

7+53.6 = South end Conc Ret. Wall on E		
on Ground at Wall	10.9	256.6
" Top "	8.62	258.85
7+75		
E on Top Conc. Ret Wall	7.64	259.83
" " Ground at "	9.7	257.8
+3	10.0	257.5
+5 = Gut on Pav.	10.52	256.95
cb " "	10.23	257.24
1/4 " "	9.97	257.50
2 " "	10.03	257.44
1/4 " "	10.29	257.18
+2 = Gut " "	10.35	257.12
cb	8.4	259.1
+2 on Walk	8.29	259.18
+6 " "	8.25	259.22
W	8.2	259.3
+5	8.0	259.5
7+82.8 = Elec Pole on W 16' W of R		
8+00		
-5	5.9	261.6
W	5.9	261.6
+6.5 3' N - 24" Cypress		
W+2 on Walk	6.17	261.30
cb " "	6.4	261.1
+5 = Gut.	8.52	258.95

26747

65th St

16

1/4 on Pav.	8.46	259.01 ✓
2 " "	8.20	259.27
1/4 " "	8.18	259.29
cb " "	8.37	259.10 ✓
+5 = Gut.	8.60	258.87
E	7.9	259.6
on Wall	6.40	261.07
on Wall = 4.40		263.07
8+39 = 11' end Conc. Ret. Wall on E		
8+50		
-5	4.8	262.7
E	5.1	262.4
+7 Gut. Pav.	5.21	262.26
cb on "	5.11	262.36
1/4 " "	5.00	262.47
2 " "	5.01	262.46
1/4 " "	5.33	262.14
+2 Gut "	5.44	262.07
+5	3.6	263.9
cb = Walk	3.24	264.23
+4 "	3.13	264.34
W	2.4	265.1
+5	2.3	265.2
4.82		262.65
8+14 22.7' W of R = 2.6' Conc. Walk		
8+55 = 2' 7.3' Conc Drive on East 21.5' W of R		
21.5' Rt. on Drive	4.77	262.70
E " "	4.60	262.87



267.47

65TH ST.

8178 - 2 Conc Walk 3.5' wide on E

EL. on Walk	3.74	263.73
+4.5 " "	3.85	263.62
9+00		
-5	0.0	
W	0.5	267.0
+5 on Walk	0.58	266.79
+9 " "	0.70	266.77
cb.	0.7	266.8
+2	1.0	266.5
+5 = Gut on Pav.	2.43	265.04
1/4 " "	2.26	265.21
L " "	1.89	265.58
1/4 " "	1.87	265.60
cb. " "	2.17	265.30
+4 Gut	2.62	264.85
+6	2.2	265.3
+8	2.3	265.2
E	3.0	264.5
+5	2.2	264.3
chk 8178 ct. Id Hq. L. Brooklyn	0.43	267.04
		267.25 - session
chk. Nail Pav. 9+8135	0.33	267.14
FB 1683-3		267.17
Above Nail		0.03
T.P. 10.16	277.30	0.33
		267.14

277.30

9+13.74 - St. Brooklyn

17

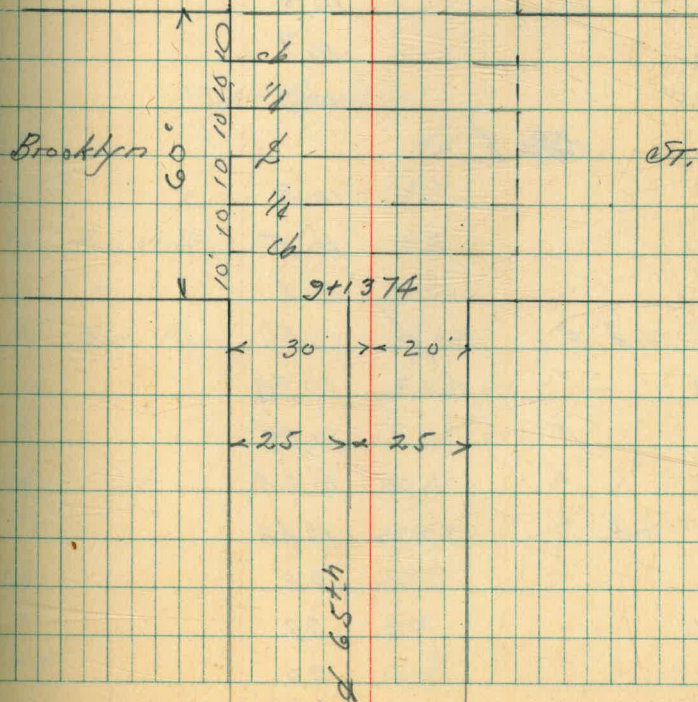
-10'	13.0	269.3
E	11.2	266.1
+3	11.2	266.1
+6 = Gut, on Pav.	11.80	265.50
cb " "	11.31	265.99
1/4 " "	10.99	266.31
L " "	10.97	266.33
1/4 " "	11.34	265.96
+2 Gut " "	11.56	265.74
+5	10.1	267.2
cb = Walk	9.88	267.1
+2 = Walk	9.80	267.50
+6 " "	9.70	267.60
W	9.7	267.6
+5	9.5	267.8
Cont. P. 24	9.5	267.8
S. C. Brooklyn	10' 14"	(from 11010 North)
-5	8.7	268.6
-2 = Walk	9.10	268.20
W on "	9.23	268.07
Cont. P. 18	P. 34	

Something Haywire with this Tack Elev. Must Not be the original



W+2	9.38	
+5	9.6	
cb = Gut Parking	<del>10.3</del> 4.03	266.27
+5 Gut	11.05	
1/4 = L. to South	<del>10.88</del> 10.88	266.65
L = L. " North	10.67	266.69
1/4 = Gut P.v	11.47	265.83
cb.	11.45	266.2
F.	11.8	
+5 Brooklyn	12.2	
NL = 0400 L of Par	3.14	268.16
0450 L " "	7.28	270.02
1400 L " "	5.18	272.12
+50 L " "	3.12	274.18

Sections cont P-34





65th St. Cont.  
from P- 18

5th Feb. Brooklyn  
277.30

-5	8.7
W.L.	9.5
cb.	10.0
+5 = Gut	10.79
1/4 on Porridge	10.54
1/2 " "	10.34
1/4 " "	10.70
+5 Gut "	11.07
cb.	10.8
F.	10.7
+5	10.9

~~1/4~~ £

-5	10.8
F.	10.5
cb.	10.5
+5 Gut. Por.	10.86
1/4 " "	10.36
1/2 " "	10.06
W 1/4 " "	10.25
+5 Gut "	10.48
cb.	9.8
76	9.2
W	9.0
+5	8.4

277.30

19

2. Brooklyn See P-34  
Partition this Int.

-5

W 1/4 - Brooklyn

-5	8.5
W	8.9
+5 Por. W.L.K	9.2
cb. " "	9.60
+5 Gut Por.	10.17
1/4 " "	9.94
1/2 " "	9.78
1/4 " "	10.11
+5	10.57
cb.	10.3
F.	10.4
+5	10.7



277.30 This Int. Cont from P. 34  
 H.C.B. Brooklyn

-5	10.7
E	10.4
cb.	9.7
+5 Gnt Per	10.21
1/4 "	9.80
1/2 "	9.48
1/4 "	9.64
+5 = Gnt "	9.86
cb.	9.5
+3 on walk	9.05
W	8.80
+5	8.2

0 + 100 = N.L. Brooklyn

-5	5.7
W = Walk	6.2
+4 "	6.3
cb.	7.7
+5 = Gnt Percy.	9.63
1/4 "	9.35
1/2 "	9.15
1/4 "	9.44
+5 " "	9.84
E	9.2
+5	9.7
N.E. Top Hght. Brooklyn	7.05 270.25

277.30 65th

20

0 + 15

-5	10.1
E	9.9
cb.	8.6
+2	8.7
+5 = Gnt Per.	9.24
1/4 "	8.84
1/2 "	8.66
1/4 "	8.81
+6 " "	9.13
cb.	7.0
+2	5.9
W	5.5
+5	5.4

~~0 + 50~~

<del>-5</del>	<del>3.7</del>
<del>W</del>	<del>4.2</del>
<del>+5</del>	<del>4.6</del>
<del>+8</del>	<del>4.7</del>
<del>cb.</del>	<del>5.4</del>
<del>+4 = Gnt, Perc</del>	<del>7.86</del>
<del>1/4 "</del>	<del>7.44</del>
<del>1/2 "</del>	<del>7.28</del>
<del>1/4 "</del>	<del>7.53</del>
<del>+6 " "</del>	<del>8.01</del>
<del>+8</del>	<del>7.5</del>
<del>cb.</del>	<del>7.5</del>
<del>+2</del>	<del>7.4</del>
<del>+4</del>	<del>8.9</del>



277.30

65th

0+50

-5		3.7
W		4.2
+5		4.6
+8		4.7
cb.		5.4
14'	East Perry	7.86
14	"	7.44
2	"	7.28
14	"	7.53
+6	" "	8.01
+8		7.5
cb.		7.5
+2		7.4
+4'		8.4

1+00

-5		7.4
F		7.0
+6		6.4
cb.		5.4
+5	East Perry	5.89
14	"	5.43
2	"	5.18
14	"	5.27
+6	" "	5.66
cb.		4.1

277.30

65th 21

cb+5		2.4
W		2.3
+5		2.2

1+50

-5		0.5
W		0.7
+5		1.1
+9		1.3
cb.		1.7
14	East Perry	3.61
14	"	3.21
2	"	3.13
14	"	3.43
+5	" "	3.87
+8		3.3
cb.		3.5
+3		3.4
+5		4.3
FL		4.5
+5		4.5

1+68.3 = S edge cb + Walk on West to School

16.3	W. of E. on East	2.75
"	" " " " cb.	3.05
W.L.	" Walk	1.1

1+78.6 = North edge Near Walk

16.3	W. of E. on East	2.33
"	cb	1.65
W.L.	on Walk	0.99

0  
1  
2  
3  
4  
5  
6  
7  
8  
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0  
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s of  
13.9.

S.A.



	277.30	65th St.
T.P.	2.05	285.26
	1.09	276.21
	2.00	
-5		2.4
E		2.4
+8		8.4
cb.		8.7
+4 Guit. Pos.		9.66
1/4 "		9.32
L "		9.05
1/4 "		9.12
+6 " "		9.48
cb		8.0
W		7.3
+5		7.0
	2.50	
-5		5.6
W		5.4
cb		5.9
+4 Guit. Pos.		7.43
1/4 "		7.05
L "		7.01
1/4 "		7.24
+6 Guit "		7.57
+9		5.8
cb.		5.7
E		6.2
+5		6.4

	285.26	22
	3.00	
-5		4.1
E		4.1
cb		3.8
+4 Guit. Pos.		5.73
1/4 "		5.22
L "		4.96
1/4 "		5.02
+6 Guit "		5.33
cb.		3.1
W		2.3
+5		2.1
	3.50	
-5		0.9
W		1.1
cb.		1.6
+4 Guit. Pos.		3.12
1/4 "		2.93
L "		2.90
1/4 "		3.14
+6 " "		3.57
cb		1.9
E		2.0
+5		2.0
	4.00	
-5		0.3
E		0.2



285.26

65th

cb		0.2
+ 4 Gut. Pave		1.51
1/4 "		1.08
L "		0.85
1/4 "		0.88
T.P.	2.44	293.85
0.85		284.41
1/4 + 6' Gut Pav		9.75
+ 8		8.7
cb.		8.6
W		8.1
+ 2.8 at steps on Asphalt		8.02
" on Conc. Steps		7.70
+ 5.9 = Top Step		6.21
4 + 36.06 = S.L. Wunderslitz	10' chs 10' 1/4's	
W on Conc. Wall		6.20
" on Ground		6.5
cb.		7.0
+ 2		7.2
+ 4 Gut Pav		8.19
1/4 "		8.00
L on "		7.96
1/4 " "		8.21
+ 6 Gut "		8.59
cb.		6.7
L		6.9
+ 5		6.9

293.85

St.

23

E	scb.	7.1
cb.		7.5
+ 4 Gut. Pav.		8.19
1/4 "		7.80
L "		7.53
1/4 "		7.57
+ 6 Gut "		7.75
cb.		6.7
W		5.9
	5 1/4 Wunderslitz	
W		5.50
cb.		6.7
+ 4 Gut. Pav.		7.31
1/4 "		7.15
L "		7.12
1/4 "		7.36
+ 6 Gut "		7.82
cb.		7.64
L		7.1
	L Wunderslitz	
E		7.1
cb.		7.3
+ 4 Gut. Pav.		7.46
1/4 "		6.98
L "		6.71
1/4 "		6.71



223.85

65th

## Wunderlin Cont.

W <sup>1/4</sup> + 5 East. Por	6.92
cb.	6.07
+ 6	4.96
W	4.85
N <sup>1/4</sup> Wunderlin	
W Por. Wells	3.76
cb	3.5
+ 5 East Por	6.45
W	6.28
♀	6.26
W	6.59
+ 5 " "	6.94
cb.	6.3
E	6.1
N cb.	
F	4.8
cb.	4.3
+ 3	5.9
+ 5 East. Por	6.29
W	6.08
♀	5.81
W	5.81
+ 5 East.	6.02
+ 8	3.2
cb	3.3
W	3.3

0+00=N.L. 223.85  
Wunderlin

ST

24

W	2.7
cb.	2.9
+ 2	3.1
+ 5 East Por	5.54
W	5.39
♀	5.33
W	5.59
+ 5 " "	5.83
+ 9	4.1
cb.	4.1
E	4.2
0+50	
- 5	2.7
E	2.5
cb.	2.3
+ 3	2.5
+ 5 East. Por	3.25
W	2.87
♀	2.68
W	2.81
+ 5 " "	3.17
+ 8	1.7
cb.	1.6
W	1.0
3' South = ♀ 3' Wells	0.99



~~1700~~

T.P. 12.31 305.76 0.40 29345  
 0+837 = 2 6.7 Conc. Ribbon Drive on W/  
 2' Back = Bit in Drive 11.32

1700

-5 10.7  
 W 10.8  
 cb 11.2  
 +5 Ent. Pav. 12.26  
 1/4 " 11.93  
 2 " 11.80  
 1/4 " 12.04  
 +5 Ent " 12.55  
 cb 12.1  
 E 12.4  
 +5 12.3

1750

-5 9.3  
 E 9.1  
 cb 9.1  
 +5 Ent. 9.43  
 1/4 9.18  
 2 9.00  
 1/4 9.20  
 +6 Ent 9.72  
 +9 8.9  
 cb 8.7  
 W 8.7

W+5

8.5

1+62 = 2 3' Conc. Walk on W on Line  
 1+77 = 2 7' Conc. Drive on W on Line  
 2+00

-5 6.3  
 W 6.0  
 cb 6.0  
 +1 6.1  
 +4 Ent Pav. 6.69  
 1/4 " 6.42  
 2 " 6.25  
 1/4 " 6.33  
 +5 Ent " 6.50  
 cb 5.8  
 E 5.9  
 +5 5.9

2+50

-5 2.2  
 E 2.3  
 cb 2.1  
 +3 3.7  
 +5 Ent Pav. 3.89  
 1/4 " 3.53  
 2 " 3.42  
 1/4 " 3.62  
 +6 Ent " 4.00



30576

65th

cb		3.2
W		3.0
+5		3.3
2+53.5% 3' Conc. walk	W. line	2.83
TR	11.94	317.04
	0.66	305.10
	3+00	
-5		11.2
W		11.5
+7		11.2
cb.		11.8
+3 Gult	Port	12.60
11	"	12.15
2	"	11.23
11	"	11.98
+5 Gult	"	12.31
+9		10.0
cb.		2.9
E		2.7
+5		2.8
	3+50	
-5		6.8
E		6.7
cb.		7.3
+4 Gult.		2.45
11		10.05
2		2.18

317.04

65th

25

11		2.41
+6 Gult.		2.79
cb.		2.0
W		8.6
+5		8.7
	3+57 - 2 3' Conc. walk on W. on line	7.34
	4+00	
-5		5.6
W		5.5
cb.		5.3
+4 Gult.		6.77
11		6.51
2		6.23
11		6.17
+7 Gult.		6.57
cb.		3.0
E		2.7
+5		2.9
	4+30	
-5		1.0
E		0.9
cb.		1.7
+3 Gult. to cutheart		3.9
+7		4.62
11		4.60
2		4.65



31704

65<sup>th</sup>

W 1/4	4.94
+6 Cont.	5.27
cb.	4.6
+4	4.1
W	4.2
+5	4.4

4+35.29 = SL. Broadway

W	4.5
+6	4.6
cb	4.7
+4 Cont.	4.92
1/4	4.68
2	4.46
1/4	4.36
+5 Edge Black Pav	4.42
+8	5.2
"	7.08
" 2.5' South on Flow 18" cut north	
cb.	4.7
E	3.9
+5	3.6

4+45.29 = South Edge Corner Pav

-10	3.28
E	3.47
cb.	3.64
1/4	3.84
2	4.01

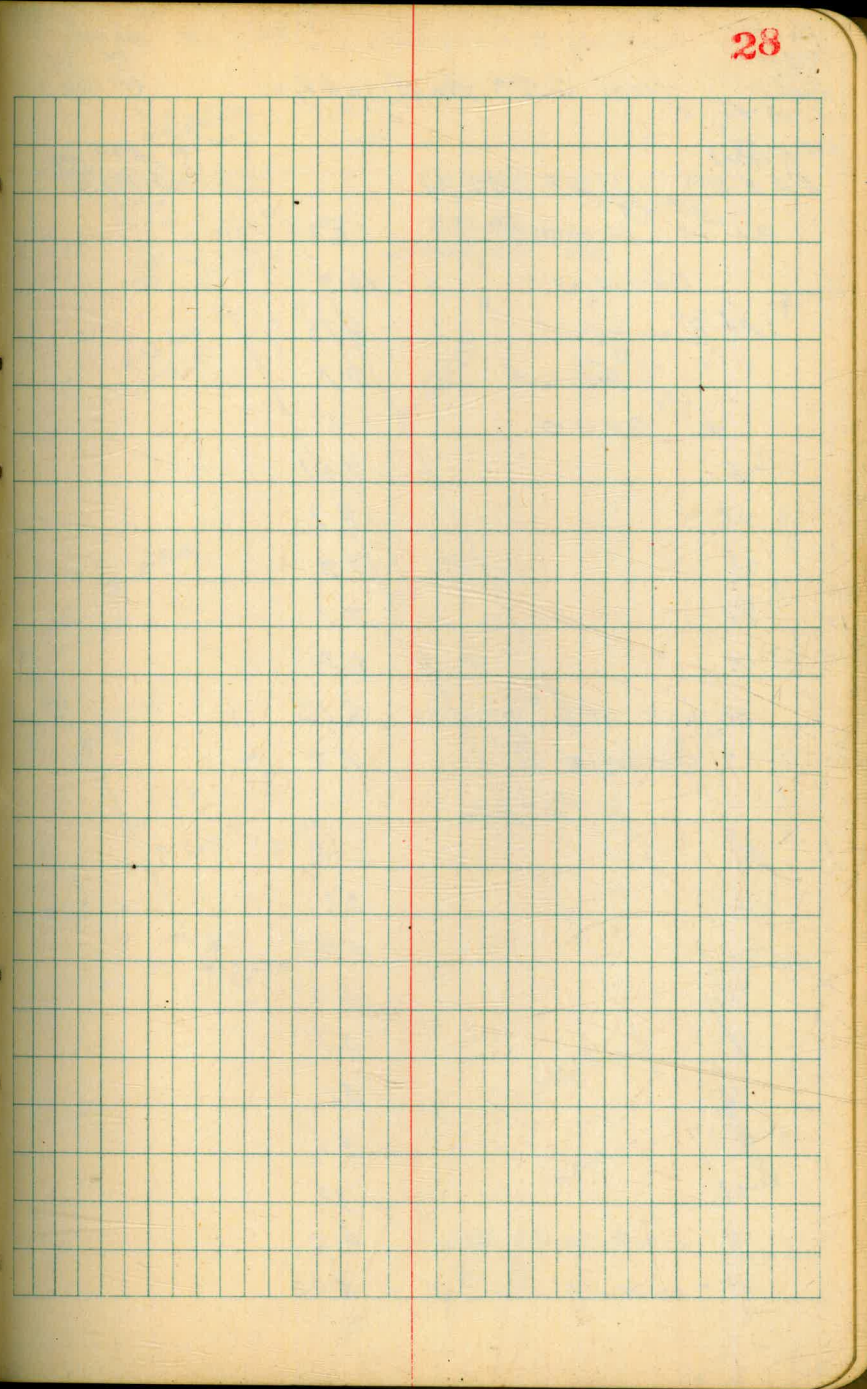
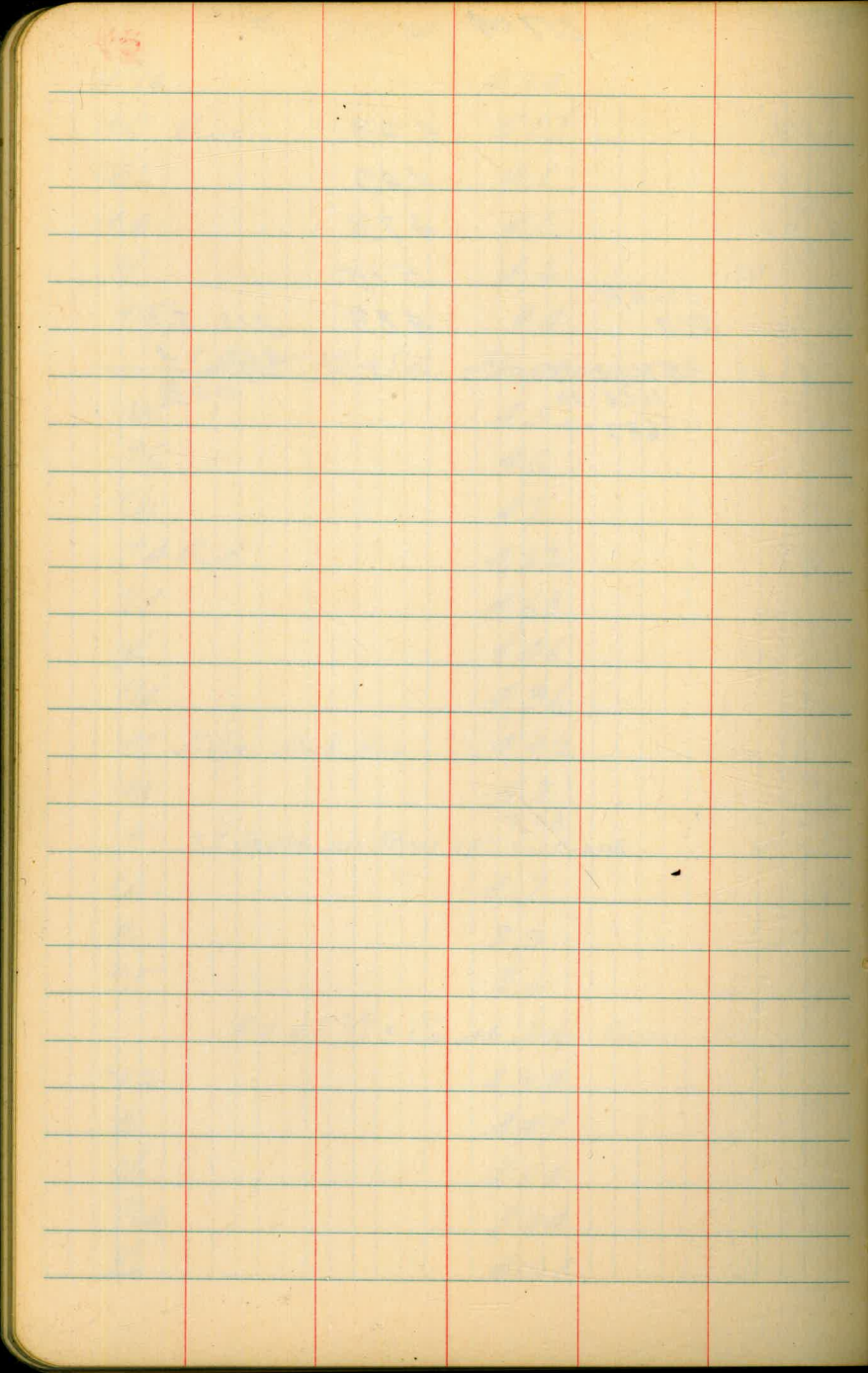
31704

ST

27

1/4	4.23	
cb.	4.49	
W	4.73	
+10	5.15	
chk SWBP BM	4.83	312.21
Bench FB 1660-45		312.24
1664-70		0.03
1682-2		











24227 Otay St.

0+82	W.L. on N end Con Wall	1.60
TP	13.09 255.10 0.26 242.01	
	1' West of	
0+82	W.L. on Wall E+W	11.89
	1' Back	
0+83	Seg. Stone Wall on W	11.3
0+78	- 1/2 Elec Pole 78' E of W.L.	
	1+00	
- 1'	on Stone Wall	10.7
W.L.		13.2
cb.		12.6
+2		12.5
+3		12.8
1/4		12.3
1/2		11.8
1/4		12.2
+4		12.5
cb.		11.4
E		10.8
+5		10.4
	1+20' N end Stone Wall	9.9
Ground	" " " "	10.6
	1+50	
-5		5.3
E		6.6
cb.		7.4
+3		7.5
+4		8.2

25510 Otay St. 30

1/4		8.0
1/2		7.6
1/4		8.0
+1		8.5
cb.		8.4
W		8.4
+5		8.5
		7.06
1+67	W.L. on 2' Conc Wall	
	1+91 = 1/2 Garage on E	4.50
	" on Floor	4.17
		4.35
1+98	3' Back on E - Conc Apron	
	7.5' Back on Garage Floor	4.16
	2+00	
W.L.-5'		4.8
W		4.6
cb.		4.1
1/4		4.2
1/2		3.6
1/4		4.0
cb.		4.0
E		3.8
+5		4.2
		4.20
2+08	= East 1/4 Conc Wall on Under Const on Line	
2+29.5	= 1/2 Elec. Pole 10.7' E of W.L.	
TP	11.92 266.80 0.22 264.83	

Circ. Apron  
on 4/17/26  
4' Back



2750

-5	11.2
E	11.2
cb.	11.4
1/4	11.6
2	11.6
1/4	11.8
cb.	11.8
W	12.2
+5	12.5

2770 - South end Conc. Wall on E. line  
on wall

7.65

Ground

10.7

2796 - N end Phase Wall

7.65

Ground

8.8

3400

-5	8.1
W	7.8
cb.	7.6
+4	8.0
+5	8.2
1/4	8.1
2	7.8
1/4	8.2
cb.	7.9
E	7.8
+5	7.7

3450

-5	4.4
E	4.1
1/4	4.1
2	3.9
1/4	4.1
+4	4.3
cb.	3.6
W	3.9
+5	3.6

T.P. 204 274.84 100 265.80

4200

-5	8.4
W	8.4
cb.	8.1
+5	9.0
1/4	8.9
2	8.5
1/4	8.7
cb.	8.7
E	8.5
+5	8.3

4440

-5	6.0
E	6.0
cb.	6.6



274.84

1/4	6.7
2	6.6
W 1/4	6.7
cb.	6.6
W	7.3
+5	7.8

4 + 50

-5	8.2
W	8.4
cb	7.1
1/4	6.2
2	6.1
1/4	6.3
cb.	6.6
E.	6.0
+5	5.9

4 + 61.91

E.	5.5
cb	5.8
1/4	5.7
2	5.8
1/4	6.3
cb.	6.0
W	6.9
<del>+5</del>	7.4

274.84

32

4 + 75.66 = section S.L. Brooklyn

W	6.7
cb.	5.3
1/4	5.1
2	5.2
1/4	5.5
cb.	5.5
E.	5.5

5 cb. Brooklyn

E.	5.1
cb.	4.9
1/4	5.2
2	5.4
1/4	5.3
cb.	5.1
W	7.5

5 1/4

-5	8.3
W	8.1
cb.	5.9
1/4	5.2
2	4.8
1/4	4.8
cb.	4.9
E.	4.5



274.84

Otoy St.  
E Brooklyn

E.	4.8
cb.	5.0
'14	5.2
E. Otoy	5.7
'14	5.8
cb.	6.6
W	7.8
+5	8.3

N '14

-5	8.8
W	8.1
cb.	5.3
'14	4.9
E.	5.9
'14	5.7
cb.	5.5
E	4.7

N cb.

E	4.8
cb.	6.0
'14	6.1
E	5.6
'14	4.4
cb.	4.8
W	8.0
+5	9.1

274.84

Otoy St. 33  
N.L. Brooklyn

-5	9.4
W	8.6
cb.	6.4
'14	4.9
E.	5.4
'14	6.4
cb.	6.3
E	4.8

Levels E Brooklyn

0+100 = E.L. Otoy	4.8
0+50	4.0
1+00	3.7
150	3.6
2+00	4.8
2+24.55 = N.L. 65th	6.3
cbk B.M. SE Top Hyd	4.58
Brooklyn +65th	p-20
	-270.26
	0.01



Walker  
Hogard  
Harden  
6-14-45

New boards for Portion  
Intersection 65th & Brooklyn  
from S cb Brooklyn

7.05 277.30 270.25 <sup>BM HW</sup> P-20

	S cb Brooklyn	
W-5		8.7
W		9.2
cb		9.5
+5 Gnt		11.05
'14		10.82
E A North		10.59
'14		10.92
+5 Gnt.		11.45
cb		11.2
E		11.3
710		11.9
	S '14	
-5		10.9
E		10.7
cb.		10.8
+5 Gnt. Par		11.05
'14	"	10.68
E	"	10.32
'14	"	10.55
+5 Gnt.	"	10.78
cb.		10.0
W		9.0
+5		8.7

277.30 65th St. 34  
E Brooklyn 0

-7		8.4
W		8.8
cb.		9.7
+5 Gnt		10.48
'14		10.24
E		10.06
'14		10.34
+5 Gnt.		10.86
cb.		10.5
E		10.5
+5		10.8
	N '14	
-5		10.7
E		10.4
cb.		10.3
+5 Gnt.		10.55
'14		10.10
E		9.78
'14		9.94
+5 Gnt		10.17
cb.		9.6
W		8.8
+5		8.5

Sections Cont P-20











356.48

50' N N.H. Benson

10' E of d = 9.25 347.23

L 8.67 342.81

6' W = W edge Pav. 8.74 347.74

100' N N.H.

2' W = W edge Pav. 11.80 344.68

L Woodman 20" 11.67 344.81

17' E = E edge Pav 11.96 344.52

0 - 61.72

5' S 10.8 357.3

J.L. 0.0 356.48

cb. 1.7 ~~354.6~~

'1/4 3.9 352.6

L 4.5 352.0

'1/4 4.9 351.6

cb. 4.8 351.2

N 6.0 350.5

+5 7.2 349.3

-5 5.46 351.02

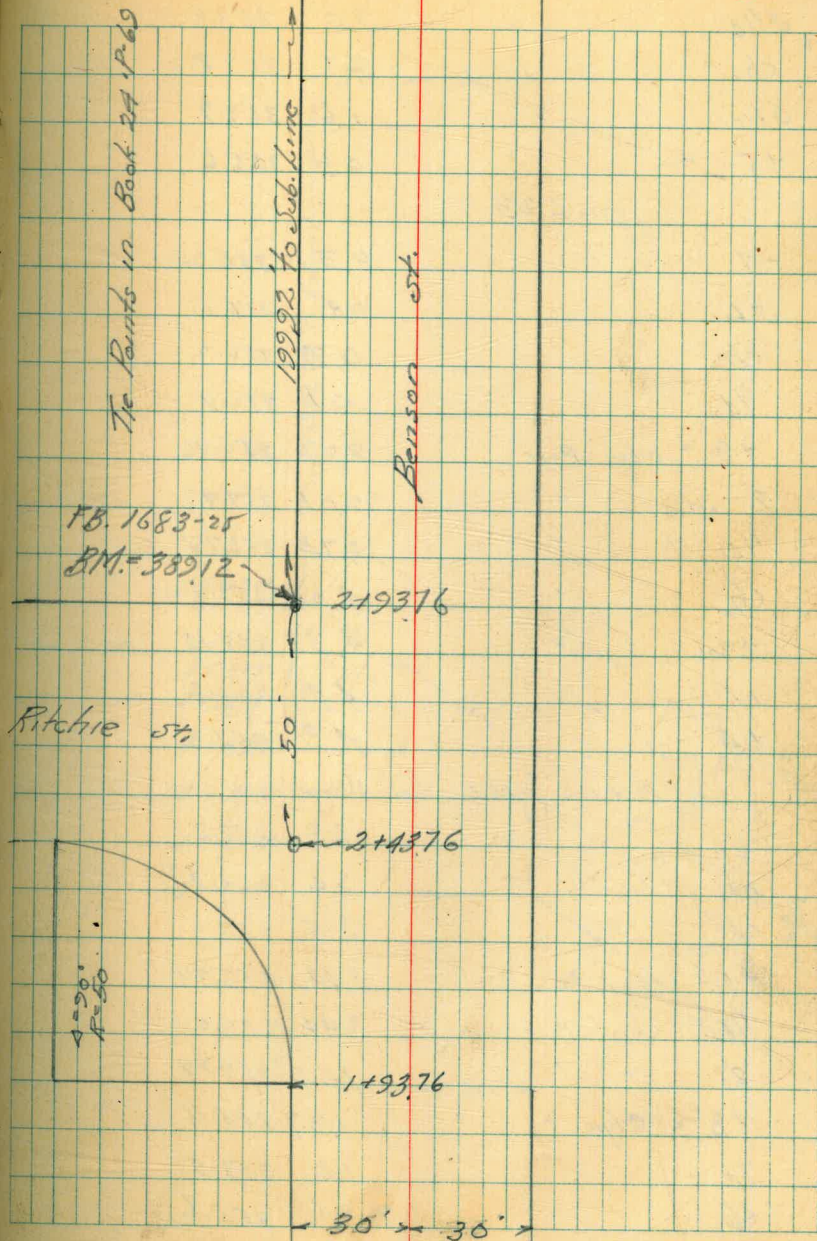
N 5.08 351.40

+9 = SW edge Pav 4.45 352.03

cb 4.5 352.0

'1/4 4.6 351.9

L 4.0 352.5













368.05 Benson St.

1+00

-10		8.5	364.6
5		4.5	363.6
cb.		4.4	363.7
1/4		4.3	363.8
L	= S edge oil Pav.	3.0	365.1
1/4	on " "	2.5	365.6
+6	N " " "	2.6	365.5
cb.		0.0	368.05
+2		+0.7	368.8
N		+2.7	370.5
+5		+3.4	371.5
T.P.	12.92 380.91	0.06	367.99

1+50

-5		4.0	376.9
N		4.6	376.3
+6		5.9	375.0
cb.		8.1	372.8
+2	N edge oil Pav.	9.0	371.9
1/4	" "	8.6	372.3
L	" " S edge	9.2	371.7
+3		9.1	371.8
1/4		10.9	370.0
cb.		11.1	369.8
S.L.		11.6	369.3
+10		11.3	369.6

380.91

1+80

-10		8.6	372.5
5		8.8	372.1
cb.		8.1	372.8
+9		7.2	373.7
1/4		6.9	374.0
+8		5.3	375.6
L	= S edge oil Pav.	5.7	375.2
1/4	on " "	4.7	376.2
+8	N " " "	5.3	375.6
cb.		4.9	376.0
+1		5.0	375.9
N		1.6	379.3
+5		1.3	379.6
	1+94 5' N of S.L. line = Elec. Pole		
T.P.	11.38 381.68	0.61	380.30
	2+10		
10' N of T.P.		8.4	373.3
N on "		10.3	381.4
+7		12.2	379.5
cb	= N edge oil Pav.	12.6	379.1
1/4	on " "	12.0	379.7
L	S " " "	12.9	378.8
+1		12.3	379.4
1/4		13.7	378.0
cb.		12.0	379.7

39



39168  
2+10 Const.

Benson St.

S.L.	15.9	375.8
+15	17.0	374.7
	2+43.76 = Sh. Ritchie	10' cbs 7.5' / 45
-15	13.5	378.2
S	12.5	379.2
cb.	11.4	380.3
'14	10.1	381.6
L	8.4	383.3
+6 S edge oil Port	9.0	382.7
'14 on " "	8.6	383.1
cb " " "	8.3	382.4
+5 N edge " "	8.4	382.3
N on Tan	7.7	384.0
+5	6.3	385.4
	cb.	
-5 on Port	6.1	385.6
N " "	6.4	385.3
cb " "	6.8	384.9
'14 = S edge Port	7.6	384.1
L	7.4	384.3
'14	8.9	382.8
cb.	10.3	381.4
S	11.7	380.0
+15	12.7	379.0
	W '14	
-15	14.7	379.5

W'14

40

S	11.0	380.7
cb.	9.3	382.4
'14	7.9	383.8
+3	7.1	384.6
L	6.6	385.1
'14 = edge oil Port	6.6	385.1
cb.	5.9	385.8
N	5.2	386.5
30' N on " "	3.5	388.2
70 N " " "	1.1	390.6
87 N	0.0	391.68
125 N " " "	+ 2.0	393.7
	Sh Ritchie = E edge oil Port on N	
125' N on Port	+ 2.0	393.7
87' N " "	0.1	391.6
50' N " " "	2.6	389.1
25 N " " "	3.5	388.2
N " " "	4.4	387.3
cb. " " Sapling edge	5.3	386.4
'14	6.0	385.7
L	5.7	386.0
'14	6.0	385.7
'14	7.0	384.7
cb.	8.8	382.9
S	10.4	381.3
+5	11.1	380.6
+15	11.4	380.3







405.01 Benson

3+41 = Olive Tree on South 9' 10 St	6"			
3+60 = " " " " 9 " "	5"			
3+69 = " " " " " " "	4"			
	4+00			
-27		6.4	398.6	
5/4		9.2	395.8	
+4		10.1	394.9	
cb		8.9	396.1	
+2		8.9	396.1	
1/4		6.2	398.8	
2		1.6	403.4	
1/4		1.6	403.4	
+6		1.6	403.4	
cb		3.2	401.8	
+3		4.2	400.8	
N		0.8	404.2	
+8		+5.0	410.0	
+20		+8.2	413.2	
TP	13.15	417.80	0.36	404.65
	A+37.25 = SE. Cor Aviation Drive			
-20		+1.5	419.3	
-7		2.7	415.1	
N		5.8	412.0	
cb		10.3	407.5	
1/4		9.9	407.9	
2		9.9	407.9	

417.80

Benson 42

5/4	10.1	407.7	
cb	14.5	402.3	
+3	3' W of Elec Pole		
5/4 line	15.2	402.6	
	4+49.25		
5	8.9	408.9	
cb	8.2	409.6	
1/4	8.5	409.3	
2	8.5	409.3	
1/4	8.9	408.9	
+6	8.5	409.3	
cb	7.2	410.6	
N	2.4	415.4	
+6	+0.5	418.3	
+20	+3.9	421.7	
	4+58.25		
-20	+5.5	423.5	
-7	+3.2	421.0	
N	+0.1	417.9	
cb	6.2	416.6	
1/4	7.5	410.3	
2	7.5	410.3	
1/4	7.7	410.1	
cb	7.4	410.4	
SL	7.1	410.7	



417.80 ✓ Benson St.

4+67.25

S.L.	6.4	411.4
cb	6.6	411.2
'14	7.2	410.6
L	6.6	411.2
'14	4.8	413.0
cb.	1.7	416.1
N	+2.3	420.1
+7	+5.5	423.3
+20	+8.0	425.8

4+76.25

-20	+11.0	428.8
-5	+6.7	424.5
N	+5.1	422.9
cb.	+3.0	426.8
'14	+2.0	419.8
L	+0.5	418.3
'14	3.8	414.0
cb.	5.1	412.7
S	5.6	412.2

4+85.25

S	2.5	415.3
T.P. on Rock	12.62	422.98
cb.	0.44	417.36
'14	12.2	417.8
'14	9.8	420.2
L	8.7	421.8

429.98

43

'14	6.2	423.1
cb.	6.0	424.0
N	2.5	426.5
+20	+0.5	430.5
4+97.27		
-20	+2.8	432.8
N	0.5	429.5
off Pipe - Dist		
Left BM on N	493.68	0.86
cb.	1.9	428.1
'14	3.7	426.3
L	5.1	424.9
'14	6.8	423.2
cb.	7.9	422.1
S	8.7	421.3
+20	13.0	419.0
5+0.3		
-40	12.1	417.9
S	8.3	421.7
cb.	7.3	422.7
'14	6.6	423.4
L	5.7	424.3
'14	2.5	426.5
cb.	1.8	428.2
N	0.6	429.4
+20	+2.0	432.0



42998 ✓ Benson St.

5+06

-20		+3.1	428.1
N		+1.6	421.6
cb.		+1.3	421.3
1/4		+0.3	420.3
1/2		+0.5	420.5
1/4		0.7	429.3
cb.		2.0	428.0
8 1/2		3.3	426.7
+5		3.7	426.3
+6		8.3	421.7
+40		12.0	418.0
T.P.	13.10	442.22	0.86 429.12

5+16

-30		14.7	429.5
S.L.		10.9	431.3
cb		10.6	431.6
1/4		8.6	433.6
1/2		7.8	434.4
1/4		8.3	433.9
cb.		8.0	434.2
N		7.2	435.0
+20		4.8	437.4

5+37

-20		+0.8	443.0
N		0.7	441.5

44222 ✓

44

cb.		2.9	439.3
1/4		2.9	439.3
1/2		2.9	439.3
1/4		3.3	438.9
cb.		2.8	439.4
5		3.6	438.6
+40		6.7	425.5
T.P.	12.44	454.45	0.21 442.01
		5+55	
-30		12.2	442.3
5		9.2	445.3
cb.		9.4	445.1
1/4		9.8	444.7
1/2		9.8	444.7
1/4		9.1	445.4
cb.		8.8	445.7
N		8.2	446.3
+20		5.4	449.1
T.P.	12.27	465.85	0.87 453.58
		5+80	
-20		11.5	454.4
N		11.0	454.7
cb.		10.5	455.4
1/4		11.0	454.9
1/2		12.3	453.6
1/4		12.2	453.7



465.85 ✓

Benson St.

cb.	11.8	454.1
S	12.5	453.4
+30	14.0	451.9
6+00		
-30	6.8	459.1
S.L.	7.9	458.0
cb.	7.9	458.0
1/4	7.5	458.4
2	7.7	458.2
1/4	7.5	458.4
cb.	7.9	458.5
N	7.4	458.5
+20	7.9	458.0
6+30		
-20	3.0	462.9
N	3.3	462.6
cb.	3.3	462.6
1/4	3.4	462.5
2	3.3	462.6
+2. 9.3 W = Guy Anchor		
1/2	3.2	462.9
cb.	3.0	462.9
+2. 2' W = Pole <sup>Elec.</sup>		
S	2.1	463.8
+30	2.3	463.6

465.85 ✓

45

6+40

T.P.	12.63	478.11	0.37	465.48	Large Nail in Pole 6+38
-20			12.7	465.4	
S			12.5	465.6	
cb.			12.2	465.9	
1/4			12.1	466.0	
2			13.1	465.0	
1/4			13.4	464.7	
cb.			13.5	464.6	
N			13.4	464.7	
+20			11.9	466.2	
6+50					
-20			10.8	467.3	
N			9.8	468.3	
cb.			10.3	467.8	
1/4			10.5	467.6	
2			10.7	467.4	
+4			10.8	467.3	
+7			9.3	468.8	
1/4			9.2	468.9	
cb.			9.5	468.6	
+3 1.5 E = Guy Anchor					
S			10.1	468.9	
+20			10.8	467.3	
<del>T.P.</del>			<del>0.37</del>	<del>487.99</del>	



478.11. ✓ Benson St

6+75

-20	6.2	471.9
S	6.2	471.9
cb.	5.3	472.8
1/4	4.8	473.3
1/2	4.6	473.5
1/4	4.4	473.7
cb.	4.0	474.1
t6	4.0	474.1
N	6.4	471.7
+20	8.2	469.9

7+00

-20	6.4	471.7
-10	4.9	473.2
8'	3.1	475.0
N	2.0	476.1
cb.	1.4	476.7
1/4	1.4	476.7
1/2	1.3	476.8
1/4	1.4	476.7
cb.	1.4	476.7
S	1.6	476.5
+20	1.9	476.2

TP 4.91 482.70 0.32 477.79

7+50

-20 4.0 478.7

7+50 Cont. 482.70

46

S	3.9	478.8
cb.	3.9	478.8
1/4	4.1	478.6
1/2	4.5	478.2
1/4	5.5	477.2
cb.	6.5	476.2
N	7.1	475.6
t11	8.6	474.1
t20	10.8	474.7

8+00

-20	13.5	469.2
N	2.3	473.4
cb.	7.7	475.0
1/4	6.7	476.0
1/2	6.3	476.4
1/4	5.5	477.2
cb.	5.0	477.7
1/4	4.7	478.0
+20	3.9	478.8

8+50

-20	3.8	479.4
cb.	4.4	478.3
1/2	4.5	478.2
1/4	5.1	477.6
1/2	5.7	477.0
1/4	6.3	476.4







48175

Benson St

cb.	6.0	475.8
S	4.8	477.0
2131.85		
S	6.5	478.3
cb.	9.3	472.4
'14	11.4	470.4
L	14.3	467.5
'14	16.7	465.1
cb.	20.6	466.2
N	24.6	457.2
+35	26.6	455.2
2145.20		
-35	28.0	453.8
N	26.0	455.8
cb.	25.4	456.4
'14	21.0	460.8
L	16.6	465.2
'14	13.7	468.1
cb.	12.0	469.8
S	10.9	470.9
TP	1.59	470.45
2160		
-20	+0.2	470.7
S	3.5	467.0
cb.	5.3	465.2
'14	9.5	461.0

470.45

48

L	12.7	457.8
'14	15.7	454.8
cb.	16.4	454.1
N	17.6	452.9
+35	20.6	449.9
TP	0.63	458.10
2180		
-40	16.1	442.6
-20	9.9	448.2
N	10.6	447.5
cb.	9.3	448.8
'14	8.5	449.6
L	7.0	451.1
'14	4.1	454.0
cb.	2.4	455.2
S	1.0	457.1
+12	+3.4	461.5
+30	+13.7	471.8
10400		
-40	+0.7	458.8
S	5.5	452.6
cb.	7.7	450.4
'14	11.7	446.4
L	11.0	447.1
'14	11.8	446.3
cb.	11.7	446.4
N	12.6	445.5



10+00 Cont Benson St.

45810

+10	13.0	445.1
+11	23.0	435.1
+20	18.0	440.1
+30	19.3	438.8
+40	23.6	434.5
T.R.	1.54	446.77
	12.87	445.23

10+20

-40	16.7	430.1
-15	10.1	436.7
-4	4.1	442.7
N	3.8	443.0
cb.	3.3	443.5
'14	2.6	444.2
2	2.2	444.6
'14	1.6	445.2
cb.	1.0	445.8
S	+0.2	447.0

+40

10+30

-40	+0.2	447.0
S N	1.6	445.2
cb.	2.2	444.6
'14	2.8	444.0
2	3.5	443.3
'14	3.9	442.9
cb.	4.1	442.6

44677

49

N	4.8	442.0
+20	14.0	432.8
+35	20.0	426.8
+50	23.5	423.3

10+50

-60	30.8	416.0
-40	27.0	419.8
-17	20.2	426.6
N	13.5	433.3
cb.	9.5	437.3
'14	7.0	439.8
2	5.7	441.1
'14	5.3	441.5
cb.	4.5	442.3
S	3.7	443.1
+25	2.4	444.4
+50	0.6	446.2

10+70

-55	2.8	444.0
-25	4.2	442.6
S	7.4	439.4
cb.	9.3	437.5
'14	11.6	435.2
2	14.6	432.2
'14	17.8	429.0
cb.	20.4	426.4



446.77

Benson

50

N	24.7	422.1
+25	29.6	417.2
+50	34.5	412.3
+60	37.5	409.3

11+00

-60	44.7	402.1
-30	39.7	407.1
N	35.0	411.8
cb.	33.0	413.8
1/4	31.2	415.6
L	30.0	416.8
1/4	29.0	417.8
cb.	24.0	422.8
S	21.7	425.1
+25	19.3	429.5
+50	15.8	431.0

11+35

South	33.0	413.8
L	39.7	407.1
N	43.7	403.1
T.P.	11.96	458.63
T.P.	11.70	470.03
T.P.	9.87	479.51
chk Pipe	8+58.89	P-47
		6.16
		473.35
		473.36
		0.01



Walker  
Hazard  
Hurdin  
6-20-45

CROSS SECTIONS AVIATION DRIVE  
from Stone Benson to S.L. Benson

50' wide  
10' cbs  
7.5' ups

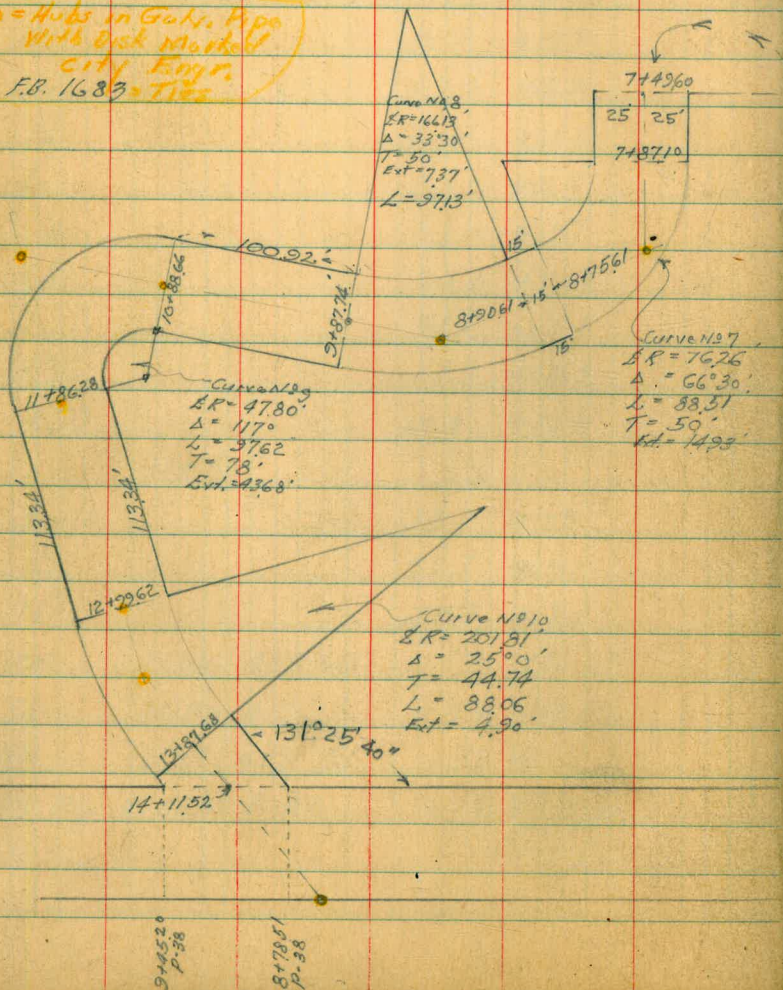
BM on Rock  
T.R. Page 43

3.17 420.53 417.36

0-0.98 Pt. A to E

E	3.1	411.9
F. 1/4	87	411.8

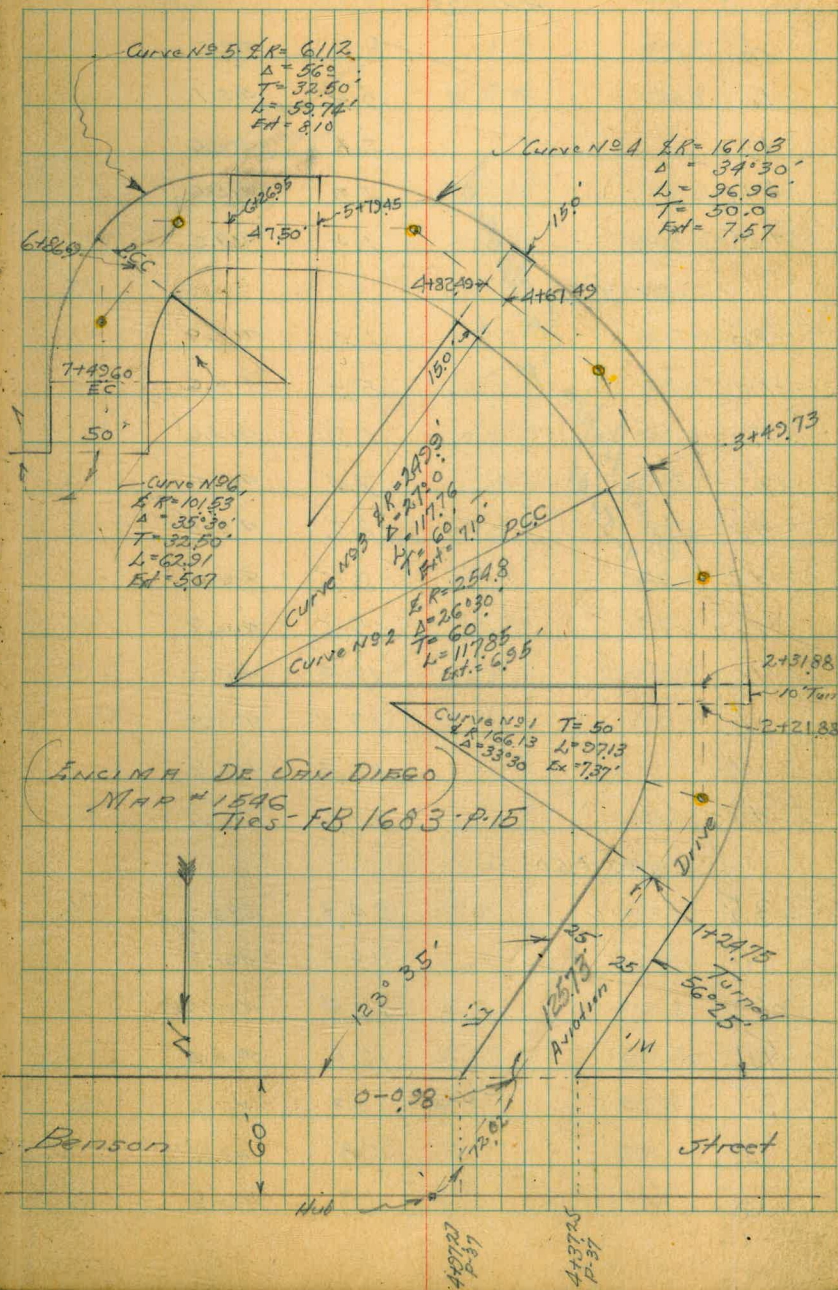
Fd. Cont. p-52  
o = Hubs in Gully, Pipe  
with Risk Marked  
city Engr.  
F.B. 1683 Ties



Indexed  
c.s.k.

Plotted - T.P.S. 2219-20  
17062

51



ENCINA DE SAN DIEGO  
MAP #1546  
Ties - F.B. 1683 - P.15

Benson

Street



0400 Cont from P-51

420.53

cb.	8.0	412.5
E	5.4	415.1
+9	2.1	418.4
+15	1.9	418.6
+25	1.0	419.5
-20	1.1	419.9
-10	5.9	419.6
E	6.9	413.6
cb.	7.4	413.1
1/4	8.2	412.3
+5	8.5	412.0
2.	9.6	410.9
1/4	13.3	407.2
cb.	17.1	403.4
W	19.3	401.2
+15	21.6	398.9
-35	24.8	395.7
W	18.8	401.7
cb.	16.3	402.2
1/4	12.0	408.5
2.	9.3	411.2
1/4	7.3	413.2
cb.	6.9	413.6

0430

Green Profile Sta. changed  
7-5-45 to

0450

420.53 Aviation Dr 52

E	5.4	415.1
+3	1.2	419.3
110	+2.0	422.5
	0+75	
-13	+8.0	423.5
-3	+3.0	423.5
E	0.3	420.2
+3	3.8	416.7
cb.	5.0	415.5
1/4	4.7	415.8
2.	5.4	415.1
1/4	6.6	413.9
cb.	8.1	412.4
W	13.9	406.6
+15	19.1	401.4
+35	23.6	396.9
	1400	
-35	21.9	398.6
-20	18.4	402.1
-5	13.2	407.3
W	8.1	412.4
cb. +3	6.2	414.3
cb.	5.7	414.8
1/4	4.2	416.3
2.	3.4	417.1
1/4	2.8	417.7



	1400	420.53	Aviation Dr.
E. cb.		2.3	418.2
+4		1.7	418.8
T.P.	10.07	430.25	0.35 420.18
E		6.4	423.8
+5		1.5	428.8
+15		+3.0	433.2
1+24.75 = BC. <del>14</del> Curve No. 1			
E. -15		+1.1	431.9
E. -6		0.2	430.0
E.		4.1	426.2
+8		10.9	419.8
cb.		10.6	419.6
1/4		10.7	419.6
2.		11.6	418.6
1/4		12.3	418.0
cb.		13.1	417.2
+8		14.6	415.6
W		21.1	409.2
+35		23.0	407.2
1+35			
-35		24.0	406.2
30		23.0	407.2
W		20.9	409.2
+5		13.4	416.8
cb.		12.5	417.8
1/4		11.5	418.8

	430.25	
2	10.8	419.4
1/4	10.3	420.0
cb.	10.0	420.2
+4	9.2	421.0
E	8.7	426.6
+5	1.1	429.2
+10	+1.4	431.6
1+40		
-10	+1.9	432.2
-5	0.6	429.6
E	3.2	427.0
+6	8.7	421.6
cb.	9.5	420.8
1/4	9.0	421.2
2.	10.3	420.0
1/4	11.0	419.0
cb.	12.5	417.8
W	13.0	417.2
+20	14.0	416.2
+35	24.0	406.2
T.P.	13.16	434.28
1+73.31 = Center Curve No. 1		
-25	24.1	401.2
5	30.5	413.8
W	18.2	416.1
cb.	14.3	420.0
+3	13.6	420.7



43428

## Aniotion Drive

W	13.1	421.2
cb.	2.3	425.0
1/4	7.1	427.2
L	5.4	428.9
1/4	4.5	429.8
cb.	4.3	430.0
L	3.2	431.1
+7	+2.2	436.5
+20	+5.8	440.1
4+08.61 = Ctr Curve No 3		
-20	+9.3	443.6
-7	+6.2	441.2
E	+0.4	439.7
+2	0.6	433.7
cb.	1.3	433.0
1/4	1.6	432.7
L	1.7	432.6
+7.1° on PI Hub in Pipe	3.89	430.4
1/4	4.0	430.3
cb.	6.0	428.3
W	9.4	428.9
+10	12.4	421.9
+30	17.8	416.5
4+67.49 = F.C. Curve No 3		
-30	11.7	422.6
-10	8.0	426.3

43428

55

W	5.7	428.6
cb.	3.2	431.1
1/4	0.6	433.7
L	7.1	436.4
1/4	+2.8	437.1
cb.	+2.6	436.9
+6	+2.6	436.9
E	+5.2	439.5
+6	+10.7	445.0
+20	+15.6	449.9
4+82.49 = B.C. No 4		
-20	+16.5	450.8
-6	+11.0	445.3
E	+5.6	439.9
+4	+3.3	437.6
cb.	+3.3	437.6
1/4	+3.5	437.8
L	+2.7	437.0
1/4	0.4	433.9
cb.	2.7	431.6
W	5.7	428.6
+10	8.1	426.2
+30	12.2	422.1
5+30.97 = F Curve No 4		
TP	11.25	445.95
	0.28	431.00

to  
ns of  
mple  
43.9.

S.A.



543097 445.95 ✓ Aviation Dr.

-35	25.3	420.6
-20	21.6	422.8
Rt. = Line	15.5	430.2
cb.	12.8	433.2
1/4 on PI <sup>on</sup> Disk <sup>Pipe</sup> -Hub	10.78	435.17
1/2	7.9	438.0
1/4	5.2	440.8
cb.	5.9	440.0
Lt. Line	6.4	439.6
+8	+1.8	447.8
+20	+6.5	452.8

547945 = E.C. Curve No 4

-20	+7.8	453.8
-7	+5.0	451.0
Lt.	1.0	445.0
+4	3.2	442.8
cb.	3.4	442.6
1/2	3.2	442.8
1/2 on Pipe	3.70	442.25
+4	3.9	442.0
1/4	5.2	440.0
cb.	9.4	436.6
Rt.	12.8	433.2
+15	17.8	428.2
+35	23.7	422.2

445.95 ✓  
6426.95 = E.C. No 5

56

-35	12.5	426.8
Rt.	9.6	436.8
cb.	6.1	439.9
1/4	3.0	443.0
1/2	1.5	444.8
1/4	0.9	445.0
cb.	0.3	445.6
+5	0.2	445.8
Lt.	+2.3	448.2
+8	+8.2	458.2
+20	+10.6	456.6

645682 Ch Curve No 5

-25	+11.7	457.6
-10	+10.3	456.2
Lt.	+3.4	449.8
+2	+2.3	448.2
cb.	+1.7	447.6
1/4	+0.6	446.6
1/2	0.2	445.8
1/4	2.9	443.0
cb.	4.5	441.8
Rt.	7.8	438.2
+35	15.0	431.0
TR 10.98	456.93	0.00 445.95







## 456.93 ✓ Aviation Drive

Rt.	21.3	435.6
+13	22.6	439.3
+16	25.0	431.9
+22	27.4	429.5
+25	31.6	425.3
+35	32.7	429.2
+40	40.0	416.9
+45	40.5	416.2
7+49.60 - E.C. Curve No 6		
-50	32.7	429.2
-17	31.2	425.7
-13	29.0	427.9
-11'	25.6	431.3
-6	27.9	432.0
Rt	21.5	435.9
cb.	15.2	441.7
'14	10.6	446.3
ℓ	7.3	449.6
'14	6.8	450.1
cb.	6.8	450.1
+6	7.3	449.6
Lt.	4.5	452.9
+7	+2.4	459.3
+20	+3.6	460.5
7+87.1° B.C. No 7		
-20	-10.6	467.2

## 456.93 ✓

58

-10	+5.2	462.1
Lt.	3.2	453.7
+3	4.5	452.9
cb.	4.7	452.2
'14	4.6	452.3
+3	4.7	452.2
ℓ	6.4	450.5
'14	10.1	446.8
cb.	15.1	441.8
Rt.	19.5	437.9
+20	21.0	435.9
+35	19.7	437.2
8+31.35 - ctr. Curve No 7		
-35	19.7	437.2
20	18.9	438.0
-10'	17.9	439.0
-7	11.2	445.7
Rt	10.0	446.9
cb.	6.9	450.0
'14	4.1	452.8
ℓ	2.7	459.2
'14	0.8	456.1
cb.	0.7	456.2
T.P.	12.91	469.52
0.32		456.61
Lt.	12.3	457.2
+3	8.0	461.5



469.52 ✓ Aviation Dr.

+20	+0.7	470.2
+30	+2.9	472.9
+40	+3.5	473.0

8+7861 = E.C. No 7 Curve

-20	+6.5	476.0
-8	+4.6	474.1
-6	3.2	466.3
Lt.	5.2	469.3
+5	8.3	461.2
cb.	8.7	460.8
1/4	9.2	460.3
2	9.0	460.5
1/4	11.8	457.7
cb.	14.4	455.1
+5	15.8	453.7
Rt.	22.5	447.0
+4	24.0	445.5
+8	28.8	440.7
+35	32.3	437.2

8+9061 = B.C. Rt No 8

-35	33.3	436.2
-4	28.1	441.9
Rt.	23.9	445.6
+7	17.0	452.5
cb.	15.9	453.6
1/4	12.8	456.7

469.52 ✓

59

2	9.3	460.2
1/4	7.5	462.0
1/4	7.8	461.7
cb.	7.5	462.0
+5	7.1	462.9
1/4	4.8	469.7
+4	2.2	467.3
+6	+4.2	473.7
+20	+7.0	476.5

9+3917 = ctr. Curve No 8

-20	+8.6	478.1
-12	+7.8	477.3
-5	+6.0	475.5
1/4	+3.7	478.2
+7	3.2	466.3
cb.	3.2	466.3
+5	3.0	466.5
1/4 on Pipe PI-12+737	3.69	465.83
2	7.8	461.7
1/4	12.5	457.0
cb.	17.0	452.5
Rt.	21.1	448.9
+8	25.4	444.1
+10	29.0	440.5
+35	31.8	437.7



9+87.74 - E.C. Curve No 8

-35	31.2	438.3
-7	28.0	441.5
-5	22.0	447.5
Rt.	18.4	451.1
cb.	11.2	458.3
1/4	6.2	463.3
L	1.7	467.8
+4'	+0.2	469.7
1/4	+0.4	469.9
cb.	+0.2	469.7
+4'	+0.3	469.8
Lt.	+3.8	473.3
+10	+5.5	475.0

10+20

-10	+6.5	476.0
-3	+5.2	477.7
Lt.	+2.7	472.2
cb.	+1.7	471.2
1/4	+1.3	470.8
+4'	+0.7	470.2
L	1.4	468.1
1/4	5.0	467.5
cb.	8.7	460.8
Rt	12.3	457.2
+25	22.3	447.2
+40	27.9	441.6

10+60

-30		14.9	459.6
Rt		5.6	463.9
+5		3.8	465.7
cb.		2.9	466.6
1/4		1.5	468.0
T.P.	13.14	482.34	0.32 469.20
L		12.7	469.6
1/4		11.7	470.6
cb.		9.8	472.5
+5		9.4	472.9
Lt.		6.8	475.5
+10		5.0	477.3
chk Hib & Tank site No 3		2.10	480.24 ✓
			480.26 P-47
			0.02

10+88.66 = B.C. Lt Curve No 9

-10		4.3	478.0
-3		5.3	477.0
Lt on Hub.		7.44	474.90
cb.		8.9	473.9
1/4		9.9	472.9
L on Disk in Pipe		12.64	469.70
1/4		13.5	468.8
cb.		14.6	467.7
5		16.7	465.6
+25		21.7	460.4



11+37.47 = ctr. Curve No 9

-30	19.4	462.9
Rt.	14.0	468.3
cb.	11.3	471.0
1/4	8.8	473.5
1/2	6.7	475.6
3/4	5.5	476.8
cb.	5.0	477.3
Lt.	4.3	478.0
+10	3.0	479.3
+20	2.9	479.9

11+86.28 = F.C. No 9 Curve

-10	1.9	480.9
Lt on Hub + Disk	1.63	480.71
cb.	2.0	480.3
1/2	3.2	479.1
1/2 on Disk in Pipe	4.82	477.5 ✓
1/4	6.8	475.5
cb.	8.5	473.8
Rt.	11.9	470.9
+13	17.8	469.5
+25	21.1	461.2
+35	24.0	458.3

12+00

-35	24.7	457.6
-20	20.1	462.2

Rt.	11.4	470.9
cb.	8.6	473.7
1/4	6.9	475.2
1/2	3.4	478.9
+3	2.4	479.9
1/2	1.8	480.5
cb.	1.2	481.1
Lt.	0.9	481.2
+10	1.3	481.0
T.P.	1.27	483.19
	1.12	481.22
	12+50	

-10	1.5	481.7
Lt.	1.4	481.8
cb.	2.4	480.8
1/4	3.4	479.8
1/2	4.2	479.0
+3	4.6	478.6
1/4	6.7	476.5
+11	9.1	474.1
cb.	10.0	473.2
Rt.	13.7	469.5
+35	26.7	456.5

12+99.62 = 80. No 10 Curve

-35	29.5	453.7
Rt.	14.5	468.7
cb.	10.7	472.5











Add. Levels on Newton  
 Betw. Old City Line and 43<sup>d</sup> St.  
 See Sketch 1615 P. 15

T.P. 12.80 44.56 0.27 31.76

0 + 65

0 + 35

0 + 13

0 + 00 City Line on diag.

T.P. 1.44 32.03 11.50 30.59

T.P. 0.55 42.09 12.68 41.54

T.P. 0.15 54.22 11.26 54.07

N.W. Cor. 1.03 65.33 14.30

Mon. disk  
 Newton  
 and 43<sup>d</sup>

1615 P. 21

C.S.M. Lt  
 C.S.  
 H.M.

E

Pt

64

9-13-45

Plotted *slip*

$\begin{array}{r} 27.6 \\ 4.6 \\ \hline 40 \end{array}$      $\begin{array}{r} 24.5 \\ 2.5 \\ \hline 20 \end{array}$      $\begin{array}{r} 20.4 \\ 2.1 \\ \hline 20 \end{array}$      $\begin{array}{r} 30.2 \\ 1.8 \\ \hline 20 \end{array}$      $\begin{array}{r} 24.3 \\ 2.7 \\ \hline 20 \end{array}$

$\begin{array}{r} 26.3 \\ 5.7 \\ \hline 40 \end{array}$      $\begin{array}{r} 27.1 \\ 4.9 \\ \hline 20 \end{array}$      $\begin{array}{r} 27.2 \\ 4.8 \\ \hline 20 \end{array}$      $\begin{array}{r} 27.3 \\ 4.7 \\ \hline 20 \end{array}$      $\begin{array}{r} 27.4 \\ 4.8 \\ \hline 20 \end{array}$

$\begin{array}{r} 25.4 \\ 6.6 \\ \hline 40 \end{array}$      $\begin{array}{r} 25.1 \\ 6.9 \\ \hline 20 \end{array}$      $\begin{array}{r} 25.3 \\ 6.7 \\ \hline 20 \end{array}$      $\begin{array}{r} 25.4 \\ 6.6 \\ \hline 20 \end{array}$      $\begin{array}{r} 22.9 \\ 9.1 \\ \hline 27 \end{array}$      $\begin{array}{r} 21.7 \\ 10.3 \\ \hline 40 \end{array}$

$\begin{array}{r} 23.2 \\ 8.8 \\ \hline 41.7 \end{array}$      $\begin{array}{r} 23.7 \\ 8.3 \\ \hline 20 \end{array}$      $\begin{array}{r} 24.5 \\ 7.5 \\ \hline 20 \end{array}$      $\begin{array}{r} 24.9 \\ 7.1 \\ \hline 18 \end{array}$      $\begin{array}{r} 21.8 \\ 10.2 \\ \hline 27 \end{array}$      $\begin{array}{r} 21.4 \\ 10.6 \\ \hline 41.7 \end{array}$

32.03 ✓

to of  
le 9.

A.



139

121

100

T.P. 12.83 57.28 0.11 44.45

165

140 approx. E G.I. dirt Rd. on South

100

44.56

67

8

PT 65

52.18

5.10  
40 Top of Pat.  
STEP IN WALL

52.96  
4.32  
Top wall

50.7 48.0 47.7 47.7 47.3 53.0 52.0  
C.C. 9.3 9.6 9.6 10.0 4.3 5.3  
40 35 20 14 21 40  
Begin. South  
Wall  
Ground

48.2 44.8 44.3 44.8 44.0 45.5 44.7  
9.1 12.5 13.0 12.5 13.3 11.8 12.6  
40 35 20 17 23 40

57.28 ✓

41.8 41.8 39.4 39.1 40.1 39.3 37.7 36.7  
2.8 2.8 5.2 5.5 4.5 5.3 4.9 7.9  
40 37 33 20 25 30 40

37.6 38.4 34.1 35.9 36.8 37.1 35.1 34.7  
7.0 6.4 8.5 8.7 7.8 7.5 9.5 9.9  
40 35 32 20 14 30 40

30.9 32.4 32.5 32.9 32.2  
13.7 12.4 12.1 11.7 12.4  
40 22 20 40

44.56 ✓



See Levels for balance  
of Newton in F.B. 1615-15

3 + 8 ~

3 + 65 = No change from  
here to xad.

3 + 39

€ 3' Cor.  
Walk

3 + 00

2 + 93

+ 75

T.P. 8.88 64.48 1.68 55.00

2 + 58

57.28

LT

€

RT

66

50.06  
58.54  
44.4  
50  
 $\frac{5.94}{40}$  € 8' Cor. drive

54.43 56.9 56.1 56.9 56.4 60.9 60.5  
5.05 5.5 4.4 7.6 8.1 2.6 4.0  
39.8 39 20 15 17 40

57.4 56.7 55.6 55.3 62.5 62.5  
7.1 7.8 8.9 9.2 2.1 2.0  
40 20 15 24 40

57.41  
70.7  
€ 3' Cor.  
Walk 39.8

56.4 54.9 54.6 54.1 52.8 59.5 61.4 61.1  
8.3 9.6 9.9 10.4 10.7 5.0 3.1 3.4  
40 36 20 15 20 25 40

62.48  
54.38 54.1 43.0 52.5 52.2 59.0 60.3 60.3  
2.90 3.2 4.3 4.8 5.1 + 1.7 + 3.0 + 3.0  
40 40 30 16 20 25 40  
Top ground  
Wall end of  
Cor. wall

57.28



check to Starting B.M. 3.28 64.31 64.30 ✓

T.P. 7.36 67.59 ✓ 425 6023 ✓

5 + 42

4 + 10

64.48

LT

£

RT

67

$$\begin{array}{r} 60.22 \\ 4.26 \\ \hline 40 \end{array} = \text{£ } 3' \text{ Con Walk}$$

$$\begin{array}{r} 60.60 \\ 3.88 \\ \hline 39.6 \end{array} = \text{£ } 3' \text{ Con Walk}$$

64.48 ✓



C. Moore  
 S. M. Meyer  
 M.F.M. X sec. of Alleys in Blk 100 Univ. Hts.  
 Oct. 8-45

X sec of 10' alley

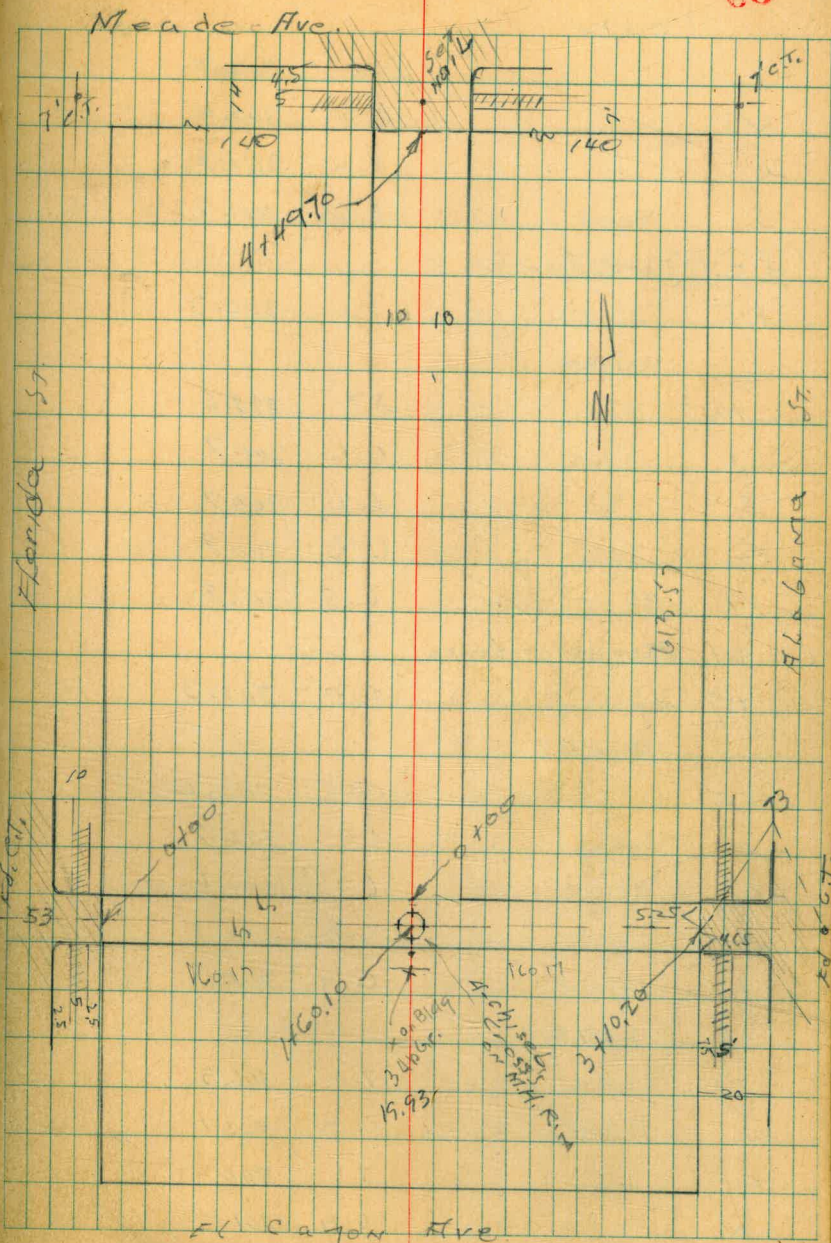
Plotted *ABB*

				300.65	
				612	
				306.59	
SW AP	5.83	306.48		300.65	EL Canyon Florida
T.P.	5.76	<u>308.28</u>	3.96	302.52	
	0-10				
S c6			5.57	302.71	
S 97			6.17	302.11	
C			6.11	302.17	
N 97			6.02	302.26	
N c6			5.37	302.91	
	0+100 EL Florida				
N c6			5.21	302.97	
N			5.55	302.73	
C			5.69	302.59	
S			5.61	302.67	
S c6			5.40	302.88	
	0+10				
-5			6.22	302.1	
-02	Beg. picket Fence				
S			5.9	302.4	
C			6.0	302.3	
N			5.9	302.4	
+3			5.22	303.1	

613.61

Indexed  
 C.S.K.

68





308.28

0+22

-J	6.0	302.3
N	6.3	302.0
C	6.4	301.9
S	6.6	301.2
+0.4 End fence		
+5	8.0	300.3

0+24

-10	8.7	299.6
-1	6.6	301.7
S	6.6	301.7
C	6.6	301.7
N	6.5	301.8
+1 Reg. wire fence		
+5	6.0	302.3

0+49

-5	6.3	302.0
N	6.6	301.7
C	6.7	301.6
S	6.8	301.5
+10	6.9	301.4

0+75

-10	7.0	301.3
S	7.2	301.1
C	7.1	301.2
N	6.9	301.4
+5	6.7	301.6

308.28

69

1+01

N-1.9 End wire fence

1+00.5

-7.6 E. Six Corn. Lem. H.	5.88	302.40
-1.5 E. cem. apron	6.49	301.79
N	6.7	301.6
C	6.9	301.4
S	6.9	301.4
+10	6.7	301.6

1+50.1 wire alley to N

-15.2 E gate yard	5.0	303.3
-9.8 edge oil pav.	5.40	302.88
S	5.5	302.8
C	5.7	302.6
N	5.4	302.9

1+60.1 E alley to N

N	5.2	303.1
C S. chisel x	M.H. Rim	5.30 302.98
S	5.2	303.1
+9.8	5.00	303.3

1+70.1 E. B. alley to N

-1.0 edge oil	4.70	303.58
S	4.8	303.5
C	5.0	303.3
N	4.9	303.4

+2 Cor. Picket fence



1+74

S-14.1	E 14	Con. apron	4.74	303.54	
S-16.6	E 14'	door	4.58	303.70	
		2+09.5			
-10			4.0	304.3	
N			4.3	304.0	
C			4.3	304.0	
S			4.3	304.0	
	N.W.				
+0.5	Con.	Brick Bldg.			
+1.9	N edge	doorway	4.16	304.12	CON FLOOR
+14.9	S "	"	4.11	304.17	WEST ENTRANCE
		2+17			
N-16	end	picket fence			
		2+35			
-0.5	against	Bldg	3.4	304.9	
S			3.4	304.9	
C			3.6	304.7	
N			3.7	304.6	
+10			3.4	304.9	
		2+50			
N-4.9	Top	Con. wall	0.55	307.73	ground Basement door
"		ground	2.8	305.5	
		2+60			
-4.9			2.2	306.1	
N			2.4	305.9	
C			2.6	305.7	

S			2.6	305.7	
+0.5	N.E. Con	Brick Bldg	2.5	305.7	ground
		2+66			
N-4.9	Top	CON. WALL	0.52	307.76	ground Basement entrance
		2+67			
S-4.6	E	Con. apron	2.35	305.93	9.5 wide Level
S-8.5	E	Sim. gar.	2.33	305.95	con. fl.
		2+68			
N+0.3	E	3.5 Con. walk	1.94	306.34	To Basement
N-5	"	"	1.87	306.41	
		2+69.7			
N-0.6	Bottom	9.6" Ret. WALL	0.53	307.73	TOP
		2+70			
S-4.5	N.W. Con	House	1.8	306.5	
S			1.8	306.5	
C			2.0	306.3	
+4			1.8	306.5	
N			0.9	307.4	
+0.6	Top	Con. wall	0.51	307.77	
		3+00			
N-0.3	Top	Con. wall	0.46	307.82	
N			0.8	307.5	
C			1.0	307.3	
S			0.9	307.4	
+4.5	N.E. Con	House	0.7	307.6	

H

01234567890123456789



30828

3+10.20 W.L. Alabama

S cb	0.57	302.61
S Pav	0.68	302.60
C "	0.71	302.57
N "	0.55	302.73
N cb	0.40	302.88
3+30.2 W. cb. Ala.		
N cb	0.66	302.62
9T Pav	1.16	302.12
C "	1.25	302.03
9T "	1.35	302.93
S cb "	0.96	302.32

71

N + S 20' alley Blk 100 V.H.

30828

0+100 P.C. 9 = H.L. of 10' alley

0+115 9' RT. E of 18" P.P.

0+120

-20	5.5	302.8
W	5.3	303.0
C	4.7	303.6
E	4.5	303.8
+10	4.3	304.0

0+143

W+13 Ctr 10" P.P.

0+50

-10	3.9	304.4
-0.6 Picket fence	4.4	303.9
E	4.8	303.5
C	4.64	303.64
+9 E 8' Con drive	4.64	303.64
W	4.64	303.64
+4.5 Big 2' Con. Ribbons	4.67	303.61
+9.2 Sm. gain, con.	4.85	303.43 and Ribbons
0+88		
W-4 E do. garage	4.5	303.8 dirt floor
0+99		
W-4	4.7	303.6



308.28

0499

W		4.7	303.6	
C		4.5	303.8	
E		4.3	304.0	
	+1 end fence			
	+10	3.9	304.4	
	1404			
E-3	SW Cor Dwelling	4.3	304.0	ground
	1409			
W-0.5	E 7' Wood shed			
	1421.5			
W+1.5	E 14" R.P.			
	1429			
W-3.3	E SW gar.	4.0	304.3	dirt fl
	1440			
E-3	NW Cor Dwelling			
E-0.7	Beq. picket fence			
	1450			
-10		3.1	305.2	
E		3.6	304.7	
C		4.1	304.2	
W		4.3	304.0	
+10		4.7	303.6	

1450 on E.

Beq. picket fence with 7 Corn Piers on  
post footings. Fence is 0.5 back and  
W. edge Piers are on E. L. alley

712

308.28

T.P.	890	313.26	3.92	304.36
	2 + 0.1			
-10			8.8	304.5
W			8.6	304.7
C			8.5	304.8
+5			8.5	304.8
E			7.8	305.5
	+0.5 and Picket fence			
	+10		7.2	306.1
	2 + 10			
E+0.8	E do. gar. dirt floor	8.0		305.3
				10' wide 0.8 in alley
	2 + 3.5			
W+1.5	E 10" R.P.			
	2 + 5.0			
-10			6.6	306.7
E			6.7	306.6
C			7.0	306.3
W			7.3	306.0
+10			7.5	305.8
	3 + 0.0			
-10			7.0	306.3
W			6.5	306.8
C			6.2	307.1
+5			6.1	307.2
E			5.4	307.9
+10			5.0	308.3



313.26

3+49

-5	4.5	308.8
E	4.8	308.5
+5	5.6	307.7
C	5.5	307.8
+5	5.4	307.9
+8	♀ 14" PP.	
W	5.8	307.5
+10	6.2	307.1

3+58

W - 13.5 ♀ sim. gap 5.7 307.6 dirt

3+80

-10	5.4	307.9
-0.2	Beq. picket fence	
W	5.3	308.0
C	5.4	307.9
+5	5.2	308.1
E	4.5	308.8
+5	4.2	309.1

3+93

E - 4.5 ♀ 8' wide 3.88 309.38 gap down cor. fl.

3+99

-4	4.2	309.1
-0.4	Beq. picket fence	
E	4.8	308.5

313.26

73

+5	5.2	308.1
C	5.2	308.1
+3	5.2	308.1
W	4.8	308.5
+10	4.8	308.5

4+11

E - 0.4 end fence

4+19

-0.5	Beq. con. walk	4.20	309.06	inside fence
W		4.2	309.1	
+7		4.7	308.6	
C		4.7	308.6	
+5		4.7	308.6	
E		4.3	308.0	
+2.5	against House foundation	4.3	309.0	ground

4+32.5

E - 0.9	♀ 4.7	Brick chimney	3.3	310.0	ground
E			3.3	310.0	
+6			3.8	309.5	
C			3.9	309.4	
+5			4.0	309.3	
W			3.3	310.0	

4+34.5

W - 0.6	end walk	3.22	310.04	inside fence
---------	----------	------	--------	--------------







30664

0+75

N-20	4.6	302.0
N-38	4.4	302.2
N-45	3.6	303.0
N-46 Scribber drive	3.48	303.16

1+00

N-20	4.7	301.9
N-36	4.4	302.2
N-45	3.5	303.1
N-46 Top S.Rib.	3.40	303.2

1+20

N Line alley	5.1	301.5
-4	5.0	301.6
-8	4.2	302.4
-25	4.2	302.4
-40	4.0	302.6
-46 S.Rib. drive	3.38	303.26

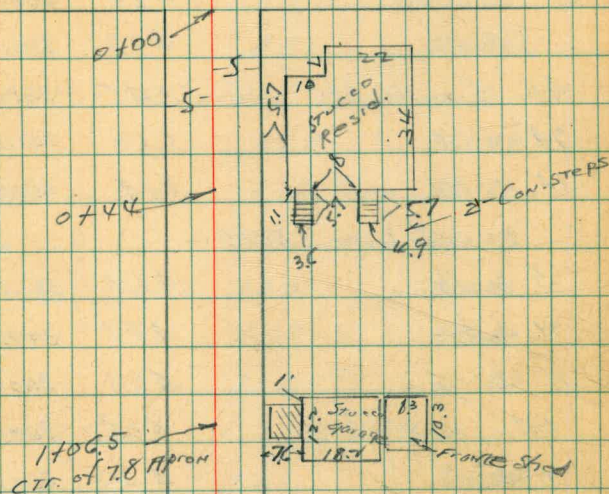
1+40

N-46 S.Rib.	3.14	303.50
N-40	3.5	303.1
N-25	3.5	303.1
N-10	3.9	302.7
N	4.5	302.1

garage floor 4.24 302.40 302.40 ✓

75

Florida





Walker  
Hazard  
Kudin  
Boyer  
10-20-45

Curb and Sidewalk - Levels  
on Curb Return N.E. Cor.  
30th and Wrightman

2nd  
10-26-51

301	354.65	351.64	RM SW. 82 Rt Wrightman
0-25 on cb Wrightman	3.81	350.84	
" Gut.	4.50	350.15	
5' South	4.29	350.36	
4.6 N on Walk	3.45	351.20	
2.4 " " "	3.50	351.15	
1.4 N = NL on "	3.14	351.51	
E Line 30th			
5' South	4.61	351.04	
N Gut.	4.71	349.94	
N cb	4.05	350.60	
+4.6 on Walk	4.06	350.59	
+2.4 " "	4.00	350.65	
+1.4 = NL on "	3.44	351.21	
Ret. = 24' 4 Parts			
① on cb	4.14	350.51	
" Gut.	4.68	349.97	
5' South	4.77	349.88	
② on cb	4.16	350.99	
" Gut.	4.65	350.00	
5' South	4.85	349.80	
③ on cb	4.15	350.50	
" Gut.	4.62	350.03	
5' SW.	4.52	350.13	

0+00 = N.L. Wrightman

El. 30th on Walk.	3.49	351.16
10' Rt. of cb on "	4.10	350.55
5' Rt " " "	4.06	350.59
E cb.	4.10	350.55
" Gut.	4.60	350.05
5' W	4.36	350.29
0+45 = 45' N.N.L. Wrightman		
El. on Walk	3.21	351.44
10' Rt. of cb on Walk.	3.38	351.27
5' " " " "	3.42	351.23
cb.	3.44	351.21
Gut.	4.08	350.57
6' W.	3.13	351.02
0+25		
El. on Walk	3.21	351.44
4' W. on "	3.76	350.89
2' W " "	3.80	350.85
13.3' on "	3.61	351.04
14' W on cb.	3.91	350.74
Gut.	4.53	350.12
7' W	4.00	350.65
E Wrightman E cb 30th		
	5.17	349.48
	5.57	349.08







Morena Blvd. Cont. from P. 77

2193 ✓

1+2166 = E.C.

S	3.23	18.70
E - 13'	3.46	18.97
N	4.07	17.86

2+25

N	4.11	17.82
E - 12'	3.50	18.93
S	3.27	18.66

2+50

S	3.24	18.69
E - 12'	3.47	18.96
N	3.91	18.04

3+00

N	3.75	18.18
E - 12'	3.30	18.63
S	3.39	18.52

3+50

S	3.22	18.71
E 11'	2.98	18.95
N	3.24	18.69

4+00

N	2.93	19.00
E 10'	2.68	19.25
S	2.96	18.97

2193 ✓

78

4+50

S	2.71	19.22
E 10'	2.44	19.99
N	2.63	19.30

5+00

N	2.44	19.99
E	2.23	19.70
South	2.45	19.98

T.P. 6.32 22.51 5.74 16.19

chk. Cleanout Box  
 177 Morena Blvd } 7.18 15.33 ✓  
 WLY of Darcus } FB 1681 = 15.35  
 74

5.72 21.91 ✓ 16.19 8M. Mon P. 77  
 on Top <sup>16"</sup> Water Main 7.12 14.79

on Top 6" Gas Main 6.69 15.22

on Conc. Slab  
 on Tel. Pile + 9MTD. 6.74 15.17 ✓

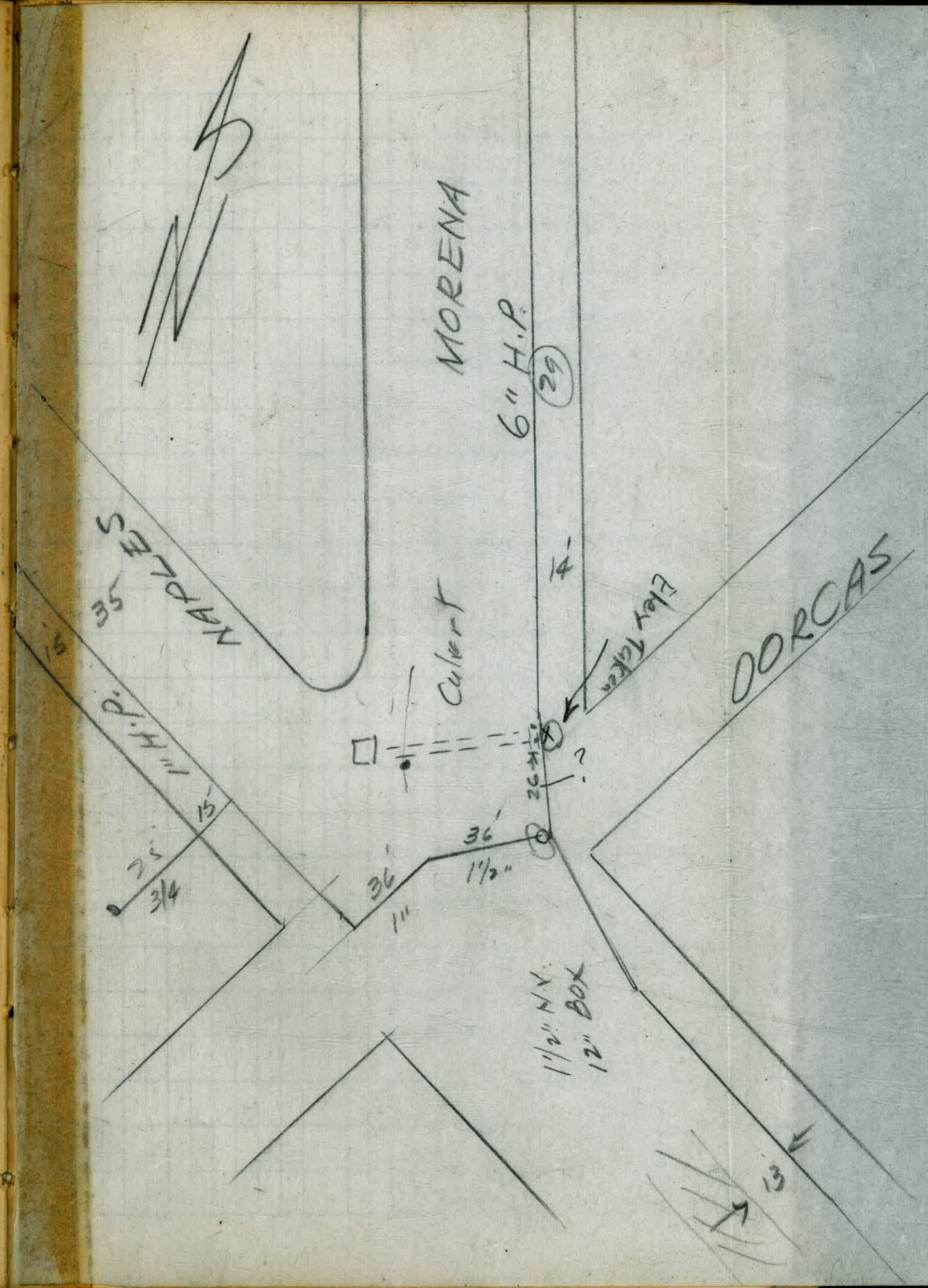
13.8

H  
0  
1  
2  
3  
4  
5  
6  
7  
8  
9  
0  
1  
2  
3  
4  
5  
6  
7  
8  
9  
0









From Gas Co.  
11-1-95.



80

306.64

Cont. from p. 1

Levels on Wall &amp; Ground

	Conc.		
0700 - End Wall on S.S.L. Alley	3.80	302.89	
0700 Ground	4.5	302.1	
1' Rt. on Ground	6.4	300.2	3.5 High
- Door to Basement			Door
0720 on Wall	4.01	302.63	
1' Rt. on Ground	7.4	299.2	
5' Rt. Grd. Floor	7.24	299.90	Basement on wood Sill
0764 on Wall	4.33	302.31	
1' Rt. "Ground"	8.0	298.6	
Basement Floor			Dirt
5' Rt. - at 3.5 High Door	8.02	298.62	
1717 on Wall	4.70	301.99	
1' Rt. "Ground"	9.1	297.5	
5' Rt. " " - Basement Dirt Floor	9.1	297.5	
5' Rt. on Wood Floor House	9.22	302.92	
1738.2 - End Wall	4.91	301.73	

III

TABLE IV.—TANGENTS AND EXTERNALS TO A 1° CURVE.

Central Angle	Tangent	External	Central Angle	Tangent	External	Central Angle	Tangent	External
1°	50.00	.22	11°	551.70	26.50	21°	1061.9	97.57
10'	58.34	.30	10'	560.11	27.31	10'	1070.6	99.16
20	66.67	.39	20	568.53	28.14	20	1079.2	100.75
30	75.01	.49	30	576.95	28.97	30	1087.8	102.35
40	83.34	.61	40	585.36	29.82	40	1096.4	103.97
50	91.68	.73	50	593.79	30.68	50	1105.1	105.60
2	100.01	.87	12	602.21	31.56	22	1113.7	107.24
10	108.35	1.02	10	610.64	32.45	10	1122.4	108.90
20	116.68	1.19	20	619.07	33.35	20	1131.0	110.57
30	125.02	1.36	30	627.50	34.26	30	1139.7	112.25
40	133.36	1.55	40	635.93	35.18	40	1148.4	113.95
50	141.70	1.75	50	644.37	36.12	50	1157.0	115.66
3	150.04	1.96	13	652.81	37.07	23	1165.7	117.38
10	158.38	2.19	10	661.25	38.03	10	1174.4	119.12
20	166.72	2.43	20	669.70	39.01	20	1183.1	120.87
30	175.06	2.67	30	678.15	39.99	30	1191.8	122.63
40	183.40	2.93	40	686.60	40.99	40	1200.5	124.41
50	191.74	3.21	50	695.06	42.00	50	1209.2	126.20
4	200.08	3.49	14	703.51	43.03	24	1217.9	128.00
10	208.43	3.79	10	711.97	44.07	10	1226.6	129.82
20	216.77	4.10	20	720.44	45.12	20	1235.3	131.65
30	225.12	4.42	30	728.90	46.18	30	1244.0	133.50
40	233.47	4.76	40	737.37	47.25	40	1252.8	135.35
50	241.81	5.10	50	745.85	48.34	50	1261.5	137.23
5	250.16	5.46	15	754.32	49.44	25	1270.2	139.11
10	258.51	5.83	10	762.80	50.55	10	1279.0	141.01
20	266.86	6.21	20	771.29	51.68	20	1287.7	142.93
30	275.21	6.61	30	779.77	52.89	30	1296.5	144.85
40	283.57	7.01	40	788.26	53.97	40	1305.3	146.79
50	291.92	7.43	50	796.75	55.13	50	1314.0	148.75
6	300.28	7.88	16	805.25	56.31	26	1322.8	150.71
10	308.64	8.31	10	813.75	57.50	10	1331.6	152.69
20	316.99	8.76	20	822.25	58.70	20	1340.4	154.69
30	325.35	9.23	30	830.76	59.91	30	1349.2	156.70
40	333.71	9.71	40	839.27	61.14	40	1358.0	158.72
50	342.08	10.20	50	847.78	62.38	50	1366.8	160.76
7	350.44	10.71	17	856.30	63.63	27	1375.6	162.81
10	358.81	11.22	10	864.82	64.90	10	1384.4	164.86
20	367.17	11.75	20	873.35	66.18	20	1393.2	166.95
30	375.54	12.29	30	881.88	67.47	30	1402.0	169.04
40	383.91	12.85	40	890.41	68.77	40	1410.9	171.15
50	392.28	13.41	50	898.95	70.09	50	1419.7	173.27
8	400.66	13.99	18	907.49	71.42	28	1428.6	175.41
10	409.03	14.58	10	916.03	72.76	10	1437.4	177.55
20	417.41	15.18	20	924.58	74.12	20	1446.3	179.72
30	425.79	15.80	30	933.13	75.49	30	1455.1	181.89
40	434.17	16.43	40	941.69	76.86	40	1464.0	184.08
50	442.55	17.07	50	950.25	78.26	50	1472.9	186.29
9	450.93	17.72	19	958.81	79.67	29	1481.8	188.51
10	459.32	18.38	10	967.38	81.09	10	1490.7	190.74
20	467.71	19.06	20	975.96	82.53	20	1499.6	192.99
30	476.10	19.75	30	984.53	83.97	30	1508.5	195.25
40	484.49	20.45	40	993.12	85.43	40	1517.4	197.53
50	492.88	21.16	50	1001.7	86.90	50	1526.3	199.82
10	501.28	21.89	20	1010.3	88.39	30	1535.3	202.12
10	509.68	22.62	10	1018.9	89.89	10	1544.2	204.44
20	518.08	23.38	20	1027.5	91.40	20	1553.1	206.77
30	526.48	24.14	30	1036.1	92.92	30	1562.1	209.12
40	534.89	24.91	40	1044.7	94.46	40	1571.0	211.43
50	543.29	25.70	50	1053.3	96.01	50	1580.0	213.86

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DISTANCES FROM CENTER OF ROADWAY FOR  
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2  
For Single Track Embankment.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) \* 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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