EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

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CITY ENGINEER'S OFFICE

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

Index

Walker Notes
Hazard
Harbin Rd
9-9-45

PARADISE HILLS ~
CROSS SECTION ALLEGHANY St.
60' Wide 10' Cbs 10"/14s
from Rachel St. to Sea Breeze

USGS. Datum = 149.34 B.M. — 35' East and 35' South of ℄ 8th & Harbison - Nat'l City. USGS Brass Tablet in Conc. Mon Post
− 6.12.
143.22 = City Datum = Above BM

	5.21	148.43		143.22	
T.P. #1	0.60	136.21	12.82	135.61	
T.P. #2	1.39	125.01	12.59	123.62	
T.P. #3	1.16	115.16	11.01	114.00	
T.P. #4	4.96	112.74	7.38	107.78	
T.P. #5	11.49	123.19	1.04	111.70	
T.P. #6	12.37	135.21	0.35	122.84	
T.P. #7	12.30	146.87	0.64	134.57	
T.P. #8	11.57	157.75	0.69	146.18	
T.P. #9	6.57	161.64	2.68	155.07	
T.P. #10	13.06	174.18	0.52	161.12	
T.P. #11	9.95	183.57	0.56	173.62	
T.P. #12	SE. Top Fire Hydt.		0.94	182.63	Alleghany & Rachel

Check levels from starting B.M. To T.P. #12

	5.17	148.39		143.22	Starting B.M.
T.P. #1	0.69	136.30	12.78	135.61	
T.P. #2	0.99	124.62	12.67	123.63	.01
T.P. #3	1.02	115.02	10.62	114.00	
T.P. #4	5.00	112.80	7.22	107.80	

Check Levels Cont from Left Page

					diff.
		112.80			
T.P. #5	11.61	123.32	1.09	111.71	.01
T.P. #6	12.13	134.98	0.47	122.85	.01
T.P. #7	12.15	146.74	0.39	134.59	.02
T.P. #8	11.59	157.79	0.54	146.20	.02
T.P. #9	6.53	161.62	2.70	155.09	.02
T.P. #10	12.93	174.07	0.48	161.14	.02
T.P. #11	9.83	183.47	0.43	173.64	.02
T.P. #12 on Fire Plg.			0.82	182.65	.02
Mean Elev. " "			→	182.64	B.M.
	0.82	183.46		182.64	Above Fire Plg
Set Brass Plg. S.E. Rachel & Alleghany			3.27	180.19	
T.P.	9.25	192.41	0.30	183.16	
T.P.	8.32	200.37	0.36	192.05	
Set S.E. Brass Plg. Alleghany & Hurdinge			3.91	196.46	
T.P.	10.73	210.55	0.55	199.82	
Set Plg. S.W. Brass Plg. Alleghany & Reo St.			3.66	206.89	
T.P.	12.48	222.27	0.76	209.79	
T.P.	6.97	228.87	0.37	221.90	

Cont. P. 2

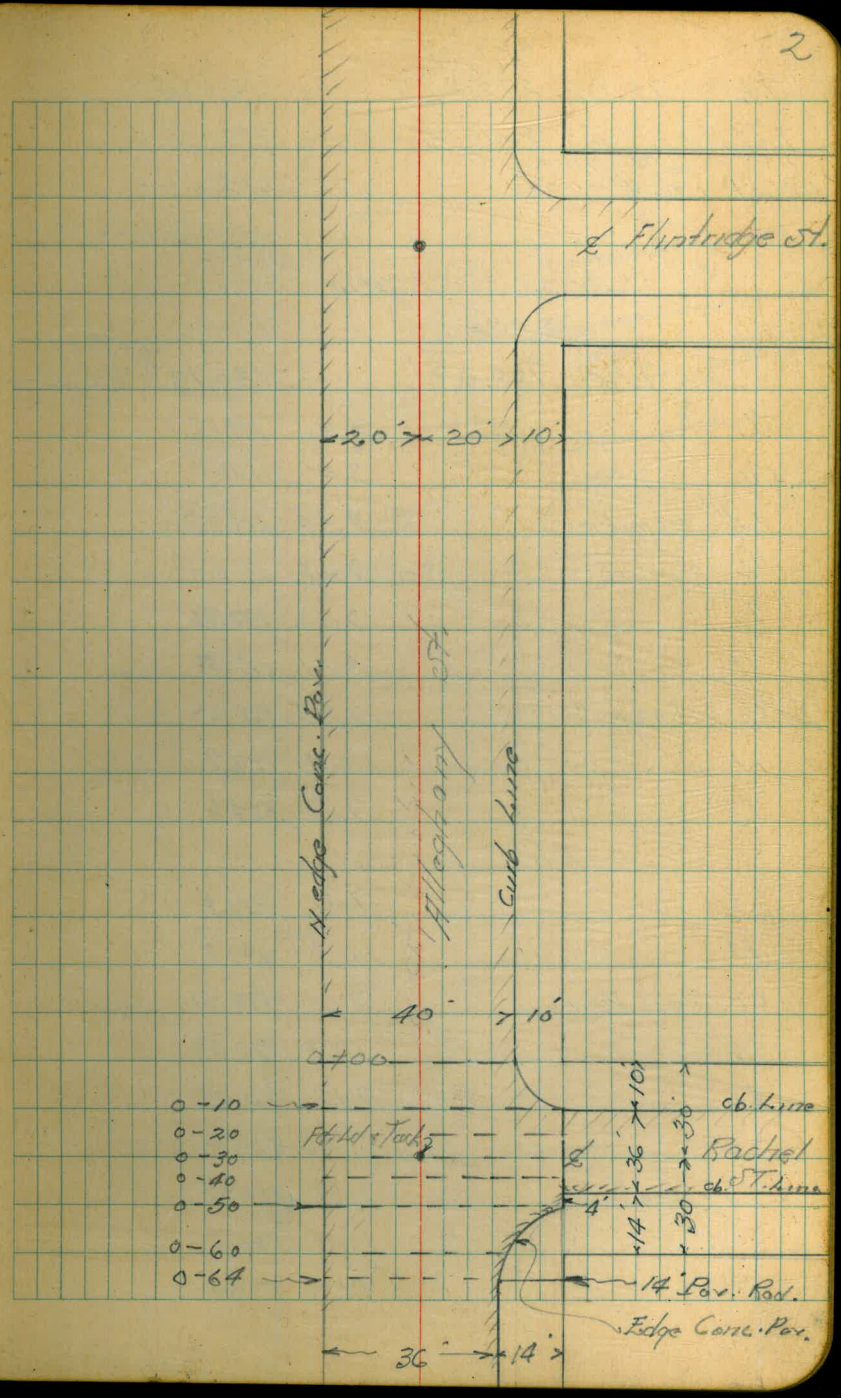
B.M.s on Allegheny St.
Cont. from p. 1

		228.87		
Set Brass Plg. SE. Allegheny & Rancho St			5.84	223.03 ~
T.P.	5.50	224.55 ~	2.82	219.05 ~
T.P.	12.61	236.53 ~	0.63	223.92 ~
Set Brass Plg. S.W. - Westport & Allegheny			9.54	226.99 ~
T.P.	11.49	247.66 ~	0.36	236.17 ~
T.P.	12.83	260.21 ~	0.28	247.38 ~
T.P.	12.34	271.80 ~	0.75	259.46 ~
T.P.	9.44	279.91 ~	1.33	270.47 ~
Set S.W. Brass Plg. Allegheny & Sea Breeze			5.50	274.41 ~

~ Check Levels on New BENCH Marks ~

Rachel & Allegheny — Allegheny from Rachel to Sea Breeze

S.E. B.P.	11.28	191.47		180.19 B.M.
T.P.	9.21	200.27	0.41	191.06
chk. S.E. B.P. Allegheny & Flintridge			3.80	196.47 .01
T.P.	10.54	210.52	0.29	199.98
chk S.W. B.P. Allegheny & Reo			3.63	206.89 ~
T.P.	11.79	221.58	0.73	209.79
T.P.	6.74	228.12	0.20	221.38
chk S.E. B.P. Allegheny & Rancho			5.08	223.04 .01
T.P.	6.35	225.41	9.06	219.06
T.P.	12.91	236.83	1.49	223.92
chk S.W. B.P. Allegheny & Westport			9.84	226.99
T.P.	13.05	249.22	0.66	236.17
T.P.	12.93	261.44	0.21	249.01



T.P.	12.02	261.44 272.86		0.60	260.84	
T.P.	7.53	280.09		0.30	272.56	
Chk SW B.P. Alleghany & Sea Breeze				5.68	274.41	

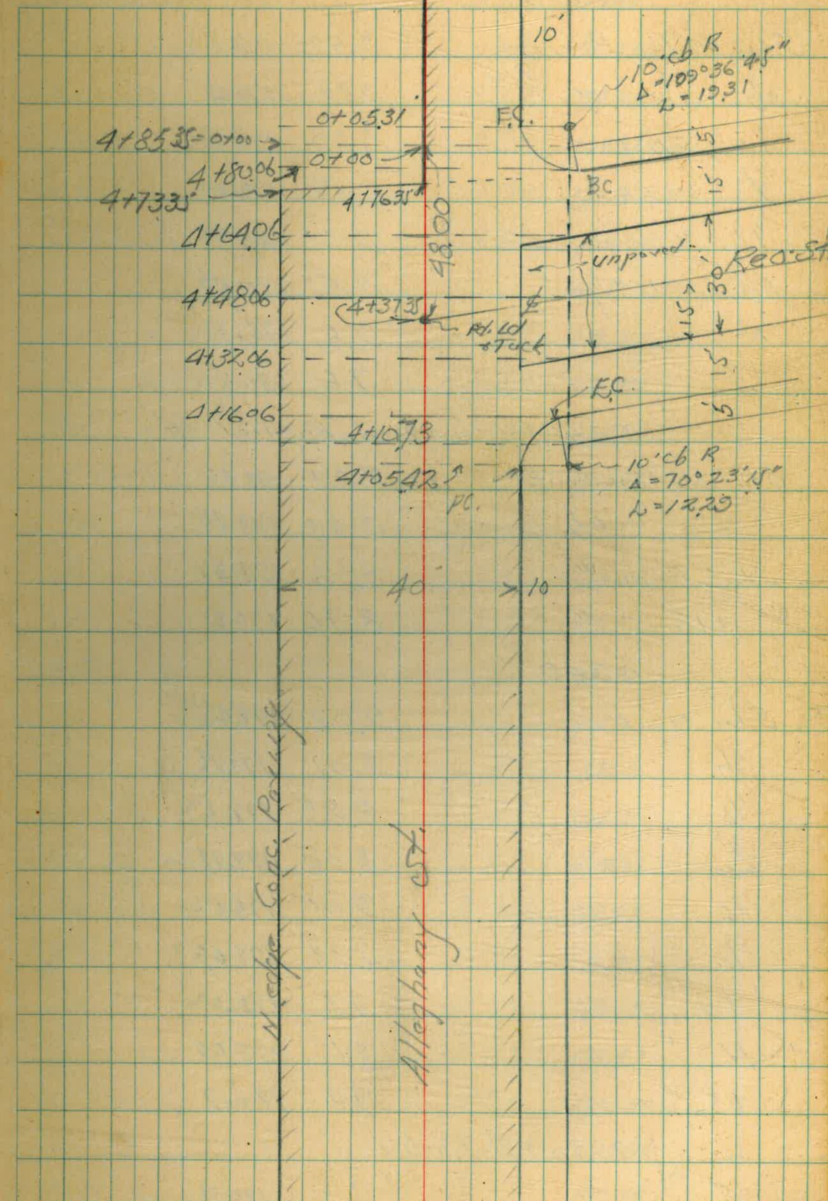
Cross Sections

10' cbs
10' 1/4s

0 - 64

	7.88	188.07			180.19	SE.B.P. Rachel & Alleghany
S.L.				9.2	178.9	
cb.				9.6	178.5	
+4' edge Pav.				9.58	178.49	
1/4				9.43	178.64	
℄				9.32	178.75	
1/4				9.51	178.56	
cb = N edge "				9.85	178.22	
N				10.4	177.7	
+3				7.5	180.6	
	0-60					
-3				7.2	181.9	
N				10.3	177.8	
cb. on Pav.				9.66	178.41	
1/4				9.38	178.69	
℄				9.18	178.89	
1/4				9.36	178.71	
+64 edge Pav.				9.53	178.54	
cb.				9.5	178.6	
S.L.				9.1	179.0	

Cont. p. 15



0-50

SL. on Top Paving	2.52	178.55
cb. on "	2.32	178.65
¼ on	2.10	178.87
℄ " "	2.03	179.04
¼ " "	2.21	178.86
cb. " N edge "	2.52	178.55
N	3.6	178.5
+3	7.6	181.5

0-46 = W cb. line Rachel ℄

SL. on Conc Gut.	2.21	178.86
" " " cb.	2.09	178.98
SL +3' on "	8.58	179.49
+13 " "	8.76	179.31

0-40

SL. on Pav.	2.02	179.05
cb.	8.91	179.16
¼	8.85	179.22
℄	8.88	179.19
¼	2.05	179.02
cb.	2.38	178.69
+9	2.5	178.02
N	9.1	178.06
+5	7.4	180.7

0-30 = ℄ Rachel

-5	7.7	180.4
N	9.1	179.0

cb. = N edge Pav	9.9	179.88
¼ " "	8.86	179.21
℄ on "	8.72	179.35
¼ " "	8.68	179.39
cb. " "	8.70	179.37
SL. " "	8.82	179.25

0-20

SL. " Pav.	8.82	179.25
cb. " "	8.58	179.49
¼ " "	8.50	179.57
℄ " "	8.55	179.52
¼ " "	8.73	179.34
cb " "	9.03	179.04
N	9.0	179.1
+5	6.9	181.2

0-10

-5	6.5	181.4
N	8.4	179.2
cb. on Pav.	8.81	179.26
¼ " "	8.51	179.56
℄ " "	8.32	179.71
¼ " "	8.39	179.65
cb. " "	8.60	179.42
SL. Gut.	8.81	179.20
" cb.	8.31	179.70
+10' on cb.	8.62	179.45

S.E. Rel. 3 Parts L = 15.71

S.L. Allegheny	8.37	179.70
① on cb.	8.24	179.83
① on Gut.	8.77	179.30
② on cb.	8.09	179.98
② " " Gut.	8.65	179.42
E.C. on E.L. Rachel cb	7.92	180.15
" " " " Gut.	8.60	179.47
0+00 = E Line Rachel St		
S.L.	7.6	181.5
cb.	7.92	180.15
Gut.	8.60	179.47
1/2	8.27	179.80
L	8.18	179.89
1/4	8.33	179.74
cb.	8.64	179.43
N	8.5	179.6
+5	6.4	181.7
0+50		
-5	5.2	182.9
N	6.6	181.5
+1	7.7	180.4
cb.	7.52	180.58
1/4	7.23	180.84
L	7.10	180.97
1/4	7.24	180.83

S. Gut.	7.55	180.52
S cb.	6.69	181.38
S.L.	6.1	182.0
1+00		
S.L.	4.9	183.2
cb.	5.47	182.60
Gut.	6.26	181.81
1/4	6.01	182.06
L	5.87	182.20
1/4	5.98	182.09
cb.	6.29	181.78
N	6.0	182.1
+5	3.8	184.3
1+50		
-5	2.1	186.0
N	4.0	184.0
+2	5.2	182.9
cb. on Pav.	5.10	182.97
1/4	4.77	183.30
L	4.63	183.44
1/4	4.77	183.30
Gut.	5.03	183.04
cb.	4.28	183.79
S.L.	3.6	184.5
2+00		
S.L.	2.3	185.8

	2+00	188.07		
S-Cb.			3.15	184.92
Gut.			3.23	184.14
¼			3.62	184.45
℄			3.46	184.61
¼			3.58	184.49
Cb.			3.89	184.18
+8			4.1	184.0
N			3.1	185.0
+5			1.3	186.8
	2+50			
-5			0.4	187.7
N			1.6	186.5
+2			2.8	185.3
Cb.			2.65	185.42
¼			2.41	185.66
℄			2.32	185.75
¼			2.45	185.62
Gut.			2.73	185.34
Cb.			2.07	186.00
SL.			1.6	186.5
	3+00			
SL.			0.8	187.09
Cb.			0.84	187.23
Gut.			1.47	186.60
¼			1.15	186.92
℄			0.98	187.09

188.07

¼			1.13	186.94
Cb.			1.45	186.62
N			1.5	186.6
+5			0.5	187.6
T.P.	11.37	199.38	0.06	188.01
	3+50			
-5			11.0	188.4
N			11.7	187.7
Cb.			11.50	187.88
¼			11.19	188.19
℄			11.04	188.34
¼			11.22	188.16
Gut.			11.53	187.85
Cb.			10.97	188.41
SL.			10.9	188.5
	4+00			
SL.			9.5	189.9
Cb.			9.71	189.69
Gut.			10.34	189.04
¼			10.05	189.33
℄			9.88	189.50
¼			9.96	189.42
Cb.			10.25	189.13
N			10.4	189.0
+5			9.5	189.9

	~~+O~~	199.38		
	4+50			
-5			8.2	191.2
N			9.1	190.3
cb.			9.11	190.27
1/4			8.81	190.57
℄			8.70	190.68
1/4			8.86	190.52
Gut.			9.15	190.23
cb.			8.48	190.90
S.L.			8.3	191.1
	5+00			
S.L.			7.1	192.3
cb			7.26	192.12
Gut.			7.91	191.47
1/4			7.64	191.74
℄			7.50	191.88
1/4			7.63	191.75
cb.			7.94	191.44
N			7.8	191.6
+5			5.8	193.6
	5+50			
-5			5.2	194.2
N			6.4	193.0
+2			6.9	192.5
cb.			6.70	192.68
1/4			6.37	193.01

	199.38		
℄		6.18	193.20
1/4		6.37	193.01
Gut.		6.73	192.65
cb.		6.10	193.28
S.L.		5.7	193.7
	6+00		
S.L.		4.5	194.9
cb		4.92	194.46
Gut.		5.50	193.88
1/4		5.24	194.14
℄		5.14	194.24
1/4		5.21	194.17
cb		5.46	193.92
cb+8'		5.9	193.5
N		5.2	194.2
+5		3.6	195.8
	6+45.07 = N/L. Flintridge	st. 50' wide 10' cbs 7.5' 1/4s.	
-5		2.4	197.0
N		4.3	195.1
cb.		4.45	194.93
1/4		4.18	195.20
℄		4.05	195.33
1/4		4.13	195.25
Gut.		4.37	195.01
cb		3.87	195.51
S.L.		3.8	195.6

SW. Ref. 15.71 = Length			3 Parts
P.C. on W.L. Flintridge cb.		3.87	195.57
"	Gut.	4.37	195.01
① on cb.		3.76	195.66
" " Gut.		4.13	195.25
② " cb.		3.63	195.75
" " Gut.		3.93	195.45
E.C. = S.L. Allegheny Gut.		3.97	195.41
" cb.		3.54	195.84
10' South on "		3.61	195.77
" " " Gut.		4.24	195.14
W cb. Flintridge			
S cb. on Paving.		3.97	195.41
+10' = 5¼ on "		3.85	195.53
℄		3.83	195.55
¼		3.96	195.42
cb.		4.23	195.15
N		4.2	195.2
+5		1.8	197.6
W ¼			
-5		1.2	198.2
N		3.9	195.5
cb.		4.12	195.26
¼		3.83	195.55
℄		3.68	195.70
S ¼		3.63	195.75

S cb.	3.75	195.63
S ℄	3.74	195.64
E Flintridge		
S ℄	3.51	195.87
cb.	3.57	195.81
¼	3.52	195.86
℄	3.51	195.87
¼	3.71	195.67
cb.	3.99	195.39
N	3.8	195.6
+5	0.9	198.5
E ½		
-5	1.5	197.9
N	3.1	196.3
+2	4.0	195.4
cb.	3.79	195.59
¼	3.55	195.83
℄	3.41	195.97
¼	3.43	195.95
cb.	3.54	195.84
S ℄	3.52	195.86
E cb		
-10' on cb.	3.03	196.35
-10' " Gut.	3.67	195.71
S ℄ cb.	3.89	195.49
" Gut.	3.51	195.87

Sch.	3.56	195.82
½	3.33	196.05
¼	3.25	196.13
½	3.42	195.96
ch.	3.70	195.68
+8	3.7	195.7
½	3.0	196.4
+5	1.8	197.6
0700 = E.L. Flintridge St.		
-5	1.1	198.2
½	2.8	196.6
+2	3.7	195.7
ch.	3.55	19583
¼	3.24	196.14
¼	3.05	196.33
¼	3.23	196.15
ch. on Gut.	3.53	195.85
" " ch	2.91	196.47
S.L.	2.6	196.8
S.E. Rot.		
① on ch.	2.95	196.43
" " Gut	3.54	195.84
2 " ch.	2.91	19647
" " Gut.	3.56	195.83
E.C. = S.L. Allegheny ch.	2.91	196.47
" " " Gut.	3.53	195.85

* Flintridge

T/L S.E. B.R. Allegheny	2.88	196.50
		196.46
		0.04 Error
12.70 209.16 corrected		196.46
0+50		
S.L.	11.1	198.1
ch.	11.53	197.63
Gut.	12.16	197.00
¼	11.85	197.31
½	11.70	197.46
¼	11.84	197.32
ch.	12.15	197.01
½	12.0	197.2
+5	10.2	199.0
1700		
-5	8.3	200.9
½	10.7	198.5
ch.	10.90	198.26
¼	10.59	198.47
½	10.44	198.22
¼	10.67	198.49
Gut.	11.03	198.13
ch.	10.34	198.82
S.L.	9.8	199.4
1750		
S.L.	8.7	200.5

2.09.16

1+50 Cont. from P-9

S Cb.	8.99	200.17
Gut.	9.65	199.51
1/4	9.33	199.83
C.	9.18	199.98
1/4	9.35	199.81
Cb	9.63	199.53
N	9.3	199.9
+5'	5.8	203.4
2+00		
-5	5.6	203.6
N	8.1	201.1
Cb.	8.43	200.73
1/4	8.08	201.08
C.	7.93	201.23
1/4	8.10	201.06
Gut.	8.43	200.73
Cb.	7.75	201.41
S.L.	7.6	201.6
2+50		
S.L.	6.21	202.95
Cb.	6.51	202.65
Gut.	7.13	202.03
1/4	6.81	202.35
C.	6.69	202.47
1/4	6.84	202.32

2.09.16

N Cb. - N edge Paving.	7.15	202.01
N	6.7	202.5
+5	4.4	204.8
3+00		
-5	3.7	205.5
N	5.2	204.2
Cb.	5.40	203.96
1/4	5.20	203.96
C.	5.15	204.01
1/4	5.40	203.76
Gut.	5.80	203.36
Cb.	5.25	203.91
S.L.	5.0	204.2
3+50		
S.L.	3.9	205.3
Cb.	3.95	205.21
Gut.	4.55	204.61
1/4	4.01	205.15
C.	3.67	205.49
1/4	3.52	205.64
N Cb.	3.54	205.62
N	3.5	205.66
+5	1.9	207.3
4+02.85		
-5	+0.2	209.4
N	1.5	207.7

4+02.25 20916

NCb. = N edge Pav.	1.62	207.54
¼	1.80	207.36
℄	1.99	207.17
¼	2.53	206.63
Gut.	3.03	206.13
Cb	2.31	206.85
SL.	2.8	206.4
Cbk. SW 1.8D Allegheny x Rco	2.29	206.87
on 8NL 9.67 216.56		206.89 .002 Error
SW Rot. Rco St.		
PC. on Cb.	2.71	206.85
" " Gut	10.34	206.22
E.C. on Cb.	2.85	206.71
" " Gut.	10.30	206.26
10' South on Cb.	10.17	206.39
" " " Gut	10.71	205.85
4+10.73 = Rt. Δ to SW Cor.		
SL.	10.0	206.6
+83 Cb.	9.75	206.81
= Gut.	10.21	206.35
Cb. on Pav.	10.19	206.37
½	9.63	206.93
℄	9.11	207.45
½	8.82	207.74
Cb.	8.76	207.84
N	85	208.1
+5	6.7	209.9

216.56

4+32.06

-5	6.1	210.5
N	7.9	208.7
Cb.	8.01	208.55
¼	8.24	208.32
℄	8.62	207.94
¼	8.74	207.82
Cb. = S. edge Pav.	9.00	207.56
S.L. = E " "	9.32	207.24
4+48.06		
S.L. Ground	8.6	208.0
Scb. = S edge Paving	8.49	208.07
¼	8.30	208.26
℄	8.25	208.31
¼	7.77	208.79
NCb.	7.41	209.15
N	7.0	209.6
+5	6.7	209.9
4+64.06		
-5'	6.0	210.6
N	6.5	210.1
NCb.	6.85	209.71
¼	7.30	209.26
℄	7.93	208.63
¼	7.94	208.62
Cb.	8.04	208.52
SL. = W. edge Paving	8.13	208.43

216.56

4+76.35 = diag. Section = Break in Paving

SL +7' = at cb Rot. on cb.	6.80	209.76
" " " Gut	7.60	208.96
cb. on Paving.	7.66	208.90
1/4	7.64	208.92
℄ = N edge Paving to East	7.67	208.89
N 1/4 on East edge Pav.	7.12	209.44
N cb. on N edge Pav. to West	6.68	209.88
N	6.3	210.3
+5	5.6	211.0

4+85.35 = 0+00 = Rt ∠ to S.E. Road.

-5	4.1	212.5
N	4.7	211.9
cb.	5.6	211.0
1/4	5.8	210.8
℄ = N edge Paving.	6.85	209.71
1/4	7.19	209.37
cb.	7.46	209.10
+2 Gut at Rot.	7.49	209.07
" on cb. "	6.65	209.91
SL	6.8	209.8

S.E. Rot 19.31 - Length 3 parts

E.C. on cb.	6.27	210.29
" " Gut	6.93	209.63
(1) " cb.	6.70	209.86
" " Gut.	7.55	209.01

216.56 -

(2) on cb.			6.93	209.63
" " Gut.			7.62	208.94
B.C. on cb.			7.00	209.56
" " Gut.			7.70	208.86
10' South on cb			7.39	209.17
" " " Gut			8.03	208.53
0+50			✓	
SL			1.4	215.2
+4			2.3	214.3
cb.			2.01	214.55
Gut.			2.64	213.92
1/4			2.23	214.33
℄ = N edge Pav			1.86	214.70
1/4			1.1	215.5
cb.			0.4	216.2
N			+0.8	217.4
+5			+1.3	217.9
T.P.	13.06	227.91	1.71	214.85
0+79.75 = Brk				
-5			7.6	220.3
N			8.1	219.8
cb.			9.2	218.7
1/4			10.1	217.8
℄ N edge Pav.			10.61	217.30
1/4			10.85	217.06
Gut.			11.10	216.81
cb.			10.47	217.44
+6			10.6	217.3
SL			9.8	218.1

1+04.75 = Brk.

SL.	8.2	219.7
+5	8.6	219.3
cb.	8.43	219.48
Gut.	9.05	218.86
¼	8.87	219.04
℄ = N edge Pav.	8.72	219.19
¼	8.0	219.9
cb.	7.3	220.6
N	6.3	221.6
+5	6.0	221.9

1+29.75 = Brk.

-5	4.7	223.2
N	4.8	223.1
cb	6.0	221.9
¼	6.2	221.7
℄ N edge Pav.	7.12	220.79
¼	7.37	220.54
Gut.	7.49	220.42
cb.	6.87	221.04
+5	7.0	220.9
SL.	6.6	221.3

1+54.75

SL	6.1	221.8
cb.	5.80	222.11
Gut.	6.43	221.48

Note: 1+26 = ℄ Proposed 12' Conc. Drive on North
Grades - Grade Book 215 - P 38

¼	6.18	221.73
℄ N edge Pav.	5.89	222.02
¼	5.1	222.8
cb.	4.5	223.4
N	3.4	224.5
+5	2.8	225.1

1+79.75

-5	1.9	226.0
N	2.4	225.5
cb.	3.3	224.6
¼	4.3	223.6
℄ N edge Pav.	5.02	222.89
¼	5.37	222.54
Gut.	5.65	222.26
cb.	5.07	222.84
SL.	5.0	222.91

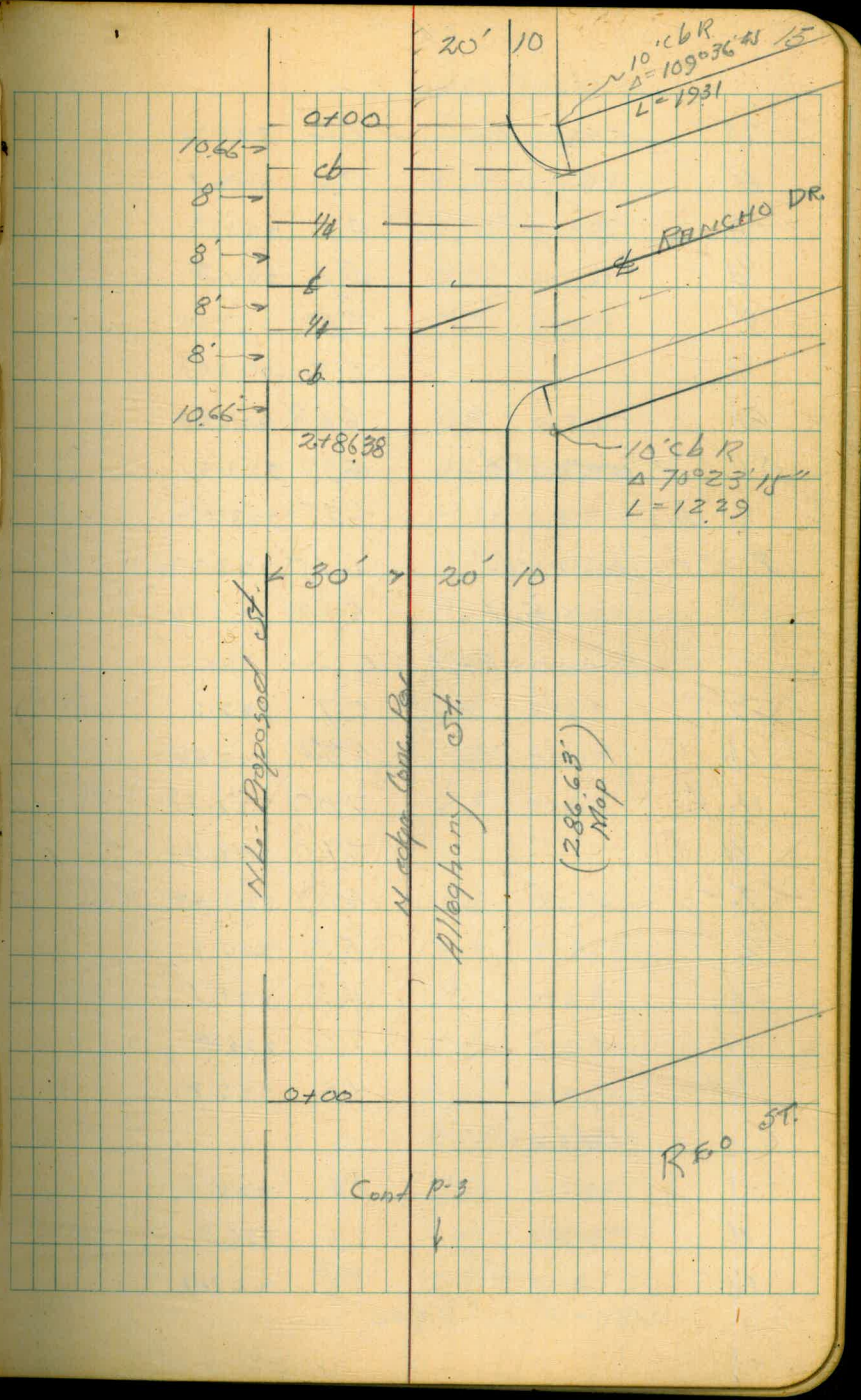
2+04.75

SL.	4.6	223.3
cb.	4.47	223.44
Gut.	5.10	222.81
¼	4.74	223.17
℄	4.35	223.56
¼	3.7	224.2
cb	2.9	225.0
N	1.5	226.4
+5	1.1	226.8

		227.91			S.E. Rancho Allegheny
ch. BM	6.34	229.37	4.88	223.03	
		2+29.75			
-5			2.0	222.4	
N			2.6	226.8	
cb.			4.0	225.4	
1/4			4.6	224.8	
℄ = N edge Pav.			5.34	224.03	
1/4			5.82	223.55	
Gut.			6.26	223.11	
cb.			5.65	223.72	
SL.			5.7	223.7	
		2+54.75			
SL.			5.1	224.3	
cb.			5.59	223.78	
Gut.			6.19	223.18	
1/4			5.69	223.68	
℄ = N edge Pav.			5.16	224.21	
1/4			4.3	225.1	
cb.			3.8	225.6	
N			2.3	227.1	
+5			1.7	227.7	
		2+79.75			
-5			1.5	227.9	
N			2.2	227.2	
cb.			3.9	225.5	
1/4			4.3	229.1	

		229.37		
℄		5.28	224.09	
1/4		5.77	223.60	
Gut.		6.17	223.20	
cb.		5.55	223.82	
SL.		5.5	223.9	
				Sketch P-15
	2+86.38 = Rt. ∠ to SW. Cor Rancho St.			
SL.		5.7	223.7	
cb.		5.56	223.81	
Gut.		6.18	223.19	
1/4		5.78	223.59	
℄		5.32	224.05	
1/4		4.3	225.1	
cb		3.9	225.4	
N		2.7	226.7	
+5		1.8	227.6	
	W cb Rancho St.			Sketch P-15
-5		1.8	227.6	
N		2.2	227.2	
cb.		3.9	225.5	
1/4		4.47	224.90	
℄		5.41	223.96	
1/4		5.80	223.57	
cb.		6.18	223.19	
SL. Gut.		6.89	222.48	
cb. = E.C. Rob.		6.20	223.17	
℄ (Rct. L=12.29)	cb. 5.65		223.72	
SW Cor Rancho	Gut 6.31			

	W 1/4	229.37		
SL.			6.64	222.73
cb.			6.14	223.23
1/4			5.83	223.54
℄			5.46	223.91
1/4			4.7	224.7
cb.			4.0	225.4
N			4.7	224.7
+5			1.4	228.0
	℄			
-5			1.3	228.1
N			2.3	227.1
cb.			4.1	225.3
1/4			4.7	224.7
℄			5.57	223.80
1/4			5.94	223.43
cb.			6.25	223.12
SL.			6.41	222.96
	E 1/4			
SL.			6.63	222.74
cb.			6.39	222.98
1/4			6.07	223.30
℄			5.67	223.70
1/4			4.9	224.5
cb.			4.2	225.1
N			2.6	226.8
+5			1.4	228.0



E. cb. Rancho Dr.

-5	1.2	228.2	
N	2.0	227.4	
cb.	4.1	225.3	
1/4	5.1	224.3	
℄	5.82	223.55	
1/4	6.30	223.07	
cb.	6.68	222.69	
SL. Gut. ~~of E.C. Rd~~	6.97	222.40	
" cb.	6.35	223.02	
℄ SE Rd. on cb	6.15	223.22	
" " Gut	6.83	222.54	

0+00 = Rt Δ SE. Cor Rancho

SL.	6.7	222.7	
cb.	6.33	223.04	
Gut.	7.00	222.37	
1/4	6.60	222.77	
℄	6.09	223.28	
1/4	5.3	224.1	
cb.	4.3	225.1	
N	2.6	226.8	
+5	1.6	227.8	

0+50

-5	1.8	227.6	
N	2.5	226.9	
cb.	5.5	223.9	

0+60 = ℄ 10' ~~Steps~~ on N

1/4	6.9	222.4	
℄	7.55	221.82	
1/4	8.14	221.23	
Gut	8.63	220.74	
cb	8.01	221.36	
SL.	7.7	221.7	

1+00

SL.	9.8	219.6	
cb.	9.63	219.71	
Gut.	10.28	219.09	
1/4	9.73	219.64	
℄	9.17	220.20	
1/4	8.1	221.3	
cb.	6.4	223.0	
N	5.4	224.0	
+5	2.8	226.6	

1+50

-5	3.8	225.6	
N	5.9	223.5	
cb.	7.5	221.9	
1/4	9.2	220.2	
℄	10.68	218.69	
1/4	11.21	218.16	
Gut.	11.69	217.68	
cb.	11.09	218.28	
SL.	11.3	218.1	

22937

1+69.81 = P.V.C

S.L.		11.5	217.9
cb.		11.4	218.0
Gut.		12.05	217.32
¼		11.58	217.79
℄		11.08	218.29
¼		9.5	219.9
cb.		7.6	221.8
N		6.1	223.3
+5		4.0	225.4
	1+89.81		
-5		4.6	224.8
N		6.5	222.9
cb.		8.0	221.4
¼		10.0	219.4
℄		11.56	21781
¼		12.09	217.28
Gut.		12.61	216.76
cb.		11.92	21745
+5		11.8	2176
S.L.		11.0	218.4
T.P.	10.49 2.27.89	11.97	2.17.40
	2+14.81 = West end	10' cb. Inlet on South	
S.L.		10.6	217.3
cb.		10.69	217.20
Gut. = Flow Grating		11.64	216.25

22789

5'E = ℄ Inlet Gut.		11.64	216.25 Grating = 3.5'x2'
10'E = E edge Inlet Gut =		11.59	216.30
" " " cb.		10.61	217.28
5 ¼		10.89	217.00
℄		10.27	217.62 ?
N ¼		8.5	219.4
cb.		6.8	221.1
N		5.4	222.5
+5		3.5	224.4
	2+39.81		
-5		3.9	224.0
N		5.7	222.2
cb.		7.1	220.8
¼		8.6	219.3
℄		10.26	217.63
¼		10.71	217.18
Gut.		11.28	216.71
cb.		10.55	217.34
S.L.		10.6	217.3
	2+64.81 E.V.C		
S.L.		10.7	217.2
cb.		10.23	217.66
Gut.		10.85	217.04
¼		10.39	217.50
℄		10.00	217.89
¼		8.6	219.3

22.7.89

N Cb	6.9	221.0
N	6.1	221.8
+5	4.0	223.9
3+00		
-5	4.6	223.3
N	6.4	221.5
Cb.	6.8	221.1
¼	8.2	219.7
℄	9.41	218.48
¼	9.78	218.4
Gut.	10.16	217.73
Cb.	9.54	218.35
SL.	9.7	218.2
3+50		
SL.	8.4	219.5
Cb	8.58	219.31
Gut.	9.19	218.70
¼	8.81	219.08
℄	8.38	219.51
¼	7.4	220.5
Cb.	6.2	221.7
N	5.5	222.4
+5	4.9	223.0
4+00		
-5	5.1	222.8
N	5.3	222.6

22.7.89

Cb.	5.8	222.1
¼	6.5	221.4
℄	7.29	220.60
¼	7.77	220.12
Gut.	8.18	219.71
Cb.	7.60	220.29
SL.	7.3	220.6
4+14.81 - P.V.C.		
SL	7.3	220.6
Cb.	7.22	220.69
Gut.	7.84	220.05
¼	7.38	220.51
℄	6.94	220.95
¼	6.1	221.8
Cb	5.5	222.4
N	5.0	222.9
+5	5.0	222.9
4+39.81		
-5	4.5	223.4
N	4.6	223.3
Cb.	4.8	223.1
¼	5.5	222.4
℄	6.23	221.66
¼	6.65	221.24
Gut.	7.16	220.73
Cb.	6.54	221.35
SL	6.9	221.0

227.89

	4+64.81		
SL.		6.0	221.9
cb.		5.57	222.32
Gut.		6.17	221.72
1/4		5.61	222.28
℄		5.21	222.68
1/4		4.6	223.29
cb.		4.1	223.8
N		3.8	224.1
+5		3.6	224.3
	4+89.81		
-5		2.5	225.3
N		2.7	225.2
cb.		3.1	224.8
1/4		3.6	224.3
℄		3.90	223.99
1/4		4.37	223.52
Gut.		4.90	222.99
cb.		4.29	223.70
SL.		4.5	223.4
	5+14.81 = EVC.		
SL.		3.0	224.9
cb.		2.79	225.10
Gut.		3.45	224.44
1/4		2.99	224.90
℄		2.53	225.36

227.89   19   330 Pl

N 1/4		2.4	225.5	
cb.		2.0	225.9	
N		1.8	226.1	
+5		1.6	226.3	10 cbs 7.5' 1/45
5+45.67 = Nap = W.L. Westport St.				
-5		+1.6	229.5	
N		+1.6	229.5	
cb.		+0.4	228.3 -	
1/4		0.4	227.5	
℄		0.78	227.11	
1/4		1.13	226.76	
Gut.		1.52	226.37	
cb.		0.91	226.98	
SL.		0.81	227.08	
T.P. chk B.M. 11.34	238.33	0.90	226.93	- SW. B.P. Westport + Alleghany
℄ SW. Rt. Westport St. on cb.		10.71	227.62	
" " " " ' Gut.		11.40	226.93	
W cb. Westport St.				
SL. on cb.		10.41	227.92	
" " Gut.		11.06	227.27	curb
cb. on Pav.		11.14	227.19	
1/4 " "		10.96	227.37	
℄ " "		10.71	227.62	
1/4		10.3	228.03	
cb.		9.0	229.33	
N		8.4	229.93	
+5'		8.5	229.83	

W 1/4 Westport St.

-5	7.8	230.53
N	8.0	230.33
cb.	8.7	229.63
1/4	10.0	228.33
℄ - Nodye Pouring	10.33	228.00
1/4 on "	10.51	227.82
cb.	10.61	227.72
SL.	10.55	227.78

℄ Westport

SL.	10.04	228.29
Gut.	10.21	228.12
1/4	10.06	228.27
℄	9.90	228.43
1/4	9.4	228.93
N cb.	8.0	230.33
N	7.8	230.53
+5	7.5	230.83

E 1/4 Westport

-5	6.5	231.83
N	6.9	231.43
cb.	7.4	230.93
1/4	9.0	229.33
℄	9.55	228.78
1/4	9.73	228.60
cb.	9.92	228.41

SL. 10.00

E. cb.

SL. on cb.	9.37	228.96
" " Gut.	9.95	228.38
cb. on Mor.	9.68	228.65
1/4	9.39	228.94
℄	9.11	229.22
N 1/4	8.3	230.03
cb.	6.7	231.63
N	5.7	232.63
+5	5.7	232.63

0+00 = E.L. Westport St.

-5	5.2	233.13
N	4.6	233.73
cb	5.8	232.53
+5	7.3	231.03
1/4	7.5	230.83
℄	8.33	230.00
1/4	8.79	229.54
Gut.	9.17	229.16
cb.	9.52	229.81
SL.	7.9	230.43

℄ S.E. Rot. Westport St.

on cb.	8.91	229.42
" Gut.	9.61	228.72

238.33

0+25

S.L.	6.0	232.33
cb.	5.80	232.53
Gut.	6.44	231.89
1/4	5.87	232.46
℄	5.36	232.97
1/4	4.6	233.73
cb.	3.3	233.03
N	3.4	234.93
+5	34	234.93

0+50

-5	0.0	238.33
N	0.2	238.13
cb.	0.8	237.53
1/4	1.5	236.83
℄	2.07	236.26
1/4	2.68	235.65
Gut.	3.32	235.01
cb.	2.71	235.62
S.L.	2.8	235.53
T.P. 12.82	251.02	0.13 238.20

0+75

S.L.	12.4	238.62
cb.	12.17	238.85
Gut.	12.77	238.25
1/4	12.08	238.94

251.02

21

℄	11.46	239.56
1/4	10.8	240.22
cb.	9.8	241.22
N	9.2	241.82
+5	9.4	241.62

1+00

-5	5.7	245.32
N	5.7	245.32
cb.	7.0	244.02
1/4	7.7	243.32
℄	8.18	242.84
1/4	8.85	242.17
cb Gut.	9.46	241.56
on cb.	8.86	242.16
S.L.	8.8	242.22

1+25

S.L.	5.1	245.92
cb.	5.52	245.50
Gut.	5.12	245.90
1/4	5.53	245.49
℄	4.92	246.10
1/4	4.5	246.52
cb.	3.8	247.22
N	3.6	247.42
+5	3.2	247.82

	1+50	25102		
-5			0.3	250.72
N			0.5	250.52
cb			0.7	250.32
1/4			1.4	249.62
d			1.68	249.34
1/4			2.24	248.78
Gut.			2.82	248.20
cb.			2.21	248.81
Sh			2.2	248.82
T.P.	12.57	262.96	0.63	250.39
	1+75			
SL.			10.9	252.06
cb			10.95	252.01
Gut.			11.51	251.45
1/4			10.98	251.98
d.			10.39	252.57
1/4			9.9	253.06
cb.			9.3	253.66
N			9.0	253.96
+5			8.0	254.96
	1+94.25 = P.I.C			
-5			6.3	256.66
N.			6.7	256.26
cb.			6.8	256.16
1/4			7.5	255.46
d.			7.99	254.97

262.96

SL		8.63	254.33
Gut.		9.15	253.81
cb.		8.54	254.42
SL		8.8	254.16
	2+19.25		
SL.		5.4	257.56
+3		6.0	256.96
cb.		5.60	257.36
Gut.		6.22	256.74
1/4		5.59	257.37
d.		4.91	258.05
1/4		4.4	258.56
cb.		3.1	259.26
N		2.8	260.76
+5		1.6	261.36
	2+44.25		
-5		+0.8	263.76
N		+0.5	263.46
cb.		0.5	262.46
1/4		1.5	261.46
d.		2.06	260.90
1/4		2.82	260.14
Gut.		3.52	259.44
cb.		2.92	260.04
SL.		3.0	259.96
T.P.	11.46	273.33	10.9	261.87

	2+69.25		
SL.		10.9	262.43
Cb.		10.83	262.50
Gut.		11.45	261.88
¼		10.75	262.58
L		10.02	262.31
¼		9.6	263.73
Cb.		8.3	265.03
N		7.5	265.83
+5		7.2	266.13
	2+94.25		
-5		5.4	267.93
N		5.5	267.83
Cb.		6.3	267.03
¼		7.5	265.83
L		7.90	265.43
¼		8.60	264.73
Gut.		9.26	264.07
Cb.		8.63	264.70
SL		8.7	264.63
	3+19.75		
SL.		6.8	266.53
Cb.		6.55	266.78
Gut.		7.18	266.15
¼		6.60	266.73
L		5.92	267.41

¼		5.7	267.63
Cb.		4.3	269.03
N		3.3	270.03
+5		2.9	270.43
	3+44.25		
-5		2.0	271.33
N		2.3	271.03
Cb.		2.9	270.43
¼		4.1	269.23
L		4.19	269.14
¼		4.76	268.57
Gut		5.28	268.05
Cb.		4.65	268.68
SL.		4.7	268.63
	3+69.25		
SL.		3.1	270.23
Cb.		3.12	270.21
Gut.		3.73	269.60
¼		3.23	270.10
~~¼~~ L		2.67	270.66
¼		2.4	270.93
Cb.		1.2	272.13
N		0.3	273.03
+5		0.0	273.33
TP	7.20	279.13	140 271.93

3+9425

-5	4.4	274.73
N	4.7	274.43
cb	5.7	273.43
1/4	6.9	272.23
℄	7.20	271.93
1/4	7.78	271.35
Gut.	8.25	270.88
cb.	7.62	271.51
SL	7.7	271.43

4+1925

SL	6.8	272.33
cb.	6.72	272.41
Gut.	7.34	271.79
1/4	6.83	272.30
℄	6.30	272.83
1/4	5.9	273.23
cb	4.7	274.43
N	3.8	275.33
+5	3.2	275.93

4+50

-5	2.3	276.83
N	3.4	275.73
cb.	4.0	275.13
1/4	5.0	274.13
℄ on Pvt.	5.32	273.81

1/4	5.83	273.30
Gut.	6.36	272.77
cb.	5.75	273.38
SL.	5.9	273.23

(4+80.72 chained) (479.75 MOP) = M.L. SEA BREEZE-SA.

SL	5.0	274.13
cb	4.86	274.27 ✓
Gut	5.46	273.67
1/4	4.90	274.23
℄	4.35	274.75
1/4	4.2	274.93
cb.	3.5	275.63
N	2.5	276.63
+5	1.6	277.53
SEA BREEZE CH. SW. BR Allegheny	4.10	274.43 —

2741
002

Walker & Hardin

PARADISE HILLS

9-1945 Recheck Bench Marks.

Harbison & 8th to Alleghany & Rachel

U.S.G.S. BM					B.M. city datum
8th & Harbison	5.26	148.48		143.22	P. 1
T.P. #1	0.853	136.443	12.89	135.59	
TP #2	0.566	123.998	13.011	123.432	
TP #3	2.570	113.912	12.656	111.342	
TP #4	11.210	118.030	7.092	106.820	
T.P. #5	12.008	129.796	0.242	117.788	
TP #6	12.348	142.166	0.478	129.818	
TP #7	12.310	153.746	0.730	141.436	
T.P. #8	12.306	165.740	0.312	153.434	
TP #9	10.176	175.086	0.830	164.910	
TP #10	9.264	182.870	1.480	173.606	
S.E.B.P.	10.095	190.345			
Chk. BM. Alleghany & Rachel			2.620	180.250	TP #12
TP #13	7.810	197.775	0.380	189.965	
TP #14	12.184	208.717	1.242	196.533	
TP #15	12.808	219.765	1.760	206.957	
TP #16	9.878	229.403	0.240	219.525	
TP #17	5.450	228.553	6.300	223.103	
TP #18	13.007	240.070	1.490	227.063	
TP #19	12.902	252.502	0.470	239.600	
TP #20	12.735	264.815	0.422	252.080	
TP #21	12.595	276.960	0.450	264.365	
TP #22	1.760	276.250	2.470	274.490	
TP #23	2.407	270.382	8.275	267.975	

Cont. P-26

VV

S.E.B.P. Alleghany & Rachel St.

S.E.B.P. " " Flintridge

S.W.B.P. " " Reo St.

S.E.B.P. " " Ranchostt

S.W.B.P. " " WESTPORT ST.

S.W.B.P. " " SEA BREEZE.

S.W.B.P. SEA BREEZE - POTOMAC

BENCH MARKS - PARADISE - HILLS

Cont. from P-25

270.382

T.P. #24	2.030	259.430	12.982	257.400
TP #25	3.761	255.444	7.747	251.683
TP #26	2.687	250.254	7.877	247.567
TP #27	1.748	239.094	12.908	237.346
T.P. #28	11.650	243.687	7.057	232.037
TP #29	13.023	254.975	1.735	241.952
T.P. #30	3.425	248.605	9.795	245.180
TP #31	10.848	254.970	4.483	244.122
TP #32	1.220	253.510	2.680	252.290
TP #33	0.432	244.555	9.387	244.123
TP #34	0.440	232.357	12.638	231.917
TP #35	1.662	226.537	7.482	224.875
TP #37	2.700	217.702	11.535	215.002
TP #38	0.985	211.395	7.292	210.410
TP #39	10.925	216.890	5.430	205.965
TP #40	2.680	225.140	1.430	215.460
T.P. #41	5.335	224.945	5.530	219.610
TP #42	0.140	218.345	6.740	218.205
T.P. #43	1.125	208.175	11.295	207.050
TP #44	9.520	212.967	4.728	203.447
TP #45	2.422	209.284	6.105	206.862
TP #46	9.482	211.131	7.635	201.649
~~T.P. #47~~	Chk TP #15-P-25		4.161	206.970

206.957

0.013 Errors.

VV

SW. BP SEA BREEZE And SCHUYLER ST.

SW. BP " " " ALBEMERLE ST

SW. BP " " " LAUDER ST.

SW. BP " " " CUMBERLAND ST.

SW. BP " " " EDGEWATER ST.

NW. Lead P/g in curb Water Service SEA BREEZE - Winchester St.

City Eng. on Aluminum Disk " " - Roanoke

Ld P/g T.P. #31

NW
~~SW~~. BP RANCHO And WINCHESTER

SW. BP " " CUMBERLAND ST.

SW. BP " " ALBEMARLE ST.

NW BP SCHUYLER " WESTPORT ST.

S.W. BP POTOMAC " " "

SW. BP RANCHO " POTOMAC ST.

SW. BP REO DRIVE " POTOMAC ST.

SW BP " " " BOLIVAR ST.

SW. BP REO " " ALLEGHANY

Bench Marks - Reo-Drive.

Cont. from P. 26

	12.688	219.550		206.862 B.M.
T.P.# 47	4.977	222.534	1.993	217.557
T.P.# 48	1.462	211.294	12.702	209.832
T.P.# 49	0.905	199.749	12.450	198.844
T.P.# 50	12.190	207.076	4.863	194.886
T.P.# 51	12.822	219.540	0.358	206.718
T.P.# 52	8.888	227.775	0.653	218.887
T.P.# 53	4.718	222.681	3.812	217.963
T.P.# 54	7.344	229.541	0.484	222.197
chk T.P.# 35			4.660	224.881
				224.875
				0.006 Error.

Bench Marks - Morningside St

	5.630	224.517		217.963
T.P.# 55	1.204	215.814	9.907	214.610
T.P.# 56	0.732	203.834	12.712	203.102
T.P.# 57	2.222	193.966	12.990	190.844
T.P.# 58	1.701	188.625	6.208	186.858
T.P.# 59	12.690	193.410	7.905	180.720
T.P.# 60	11.330	204.497	0.293	193.117
T.P.# 61	5.365	208.195	1.667	202.830
T.P.# 62	11.543	213.830	5.908	202.287
T.P.# 63	3.080	215.594	1.316	212.514
T.P.# 64	2.634	205.518	12.710	202.884
T.P.# 65	0.556	198.238	7.836	197.682

Void See P. 29 Now Lords

Cont. P. 28

(T.P.# 45 P. 26)

SW B.P. Reo Drive and Potomac st

SW B.P. " " " Albemarle st.

S.W. B.P. " " " Cumberland "

NW. BP " " " Winchester st

N.W. B.P. RANCHO " " "

Above TP # 53

N.W. B.P. Reo & Winchester

N.W. B.P. Winchester and Morningside st.

S.W. B.P. Cumberland " "

S.W. B.P. Midwick " " "

~~S.W. B.P. Albemarle~~ " " "

S.W. B.P. Albemerle " " "

S.W. B.P. Potomac and Morningside

Bench Marks.

Cont. from P. 27

198.238

TP #66	0.698	186.394	12.542	185.696
TP #67	10.568	185.632	11.330	175.064
T.P. #68	12.102	196.860	0.874	184.758
TP #69	8.128	200.486	4.502	192.358
cht.			2.966	197.520

Void

diff. in Stating = — 0.924

196.596

196.533

0.063 High.

This diff. Prorated among Turns from TP #55 to TP #69 See New Notes as adjusted P. 29

SW. BR Flintridge and Potomac St.

SW BR " " Bolivar St.

Walker Hardin 7-45

BENCH MARKS - Morningside & PARADISE HILLS

	5.630	223.593		217.963
T.P. #55	1.204	214.888	2.909	213.684
TP #56	0.732	202.905	12.715	202.173
TP #57	2.222	192.135	12.992	189.913
TP #58	1.767	187.691	6.211	185.924
TP #59	12.690	192.474	7.907	179.784
TP #60	11.380	203.558	0.296	192.178
TP #61	5.365	207.254	1.669	201.889
TP #62	11.543	212.886	5.911	201.343
TP #63	3.080	214.648	1.318	211.568
TP #64	2.634	204.569	12.713	201.935
TP #65	0.556	197.287	7.838	196.731
TP #66	0.698	185.434	12.551	184.736
TP #67	10.568	184.663	11.389	174.095
TP #68	12.102	195.882	0.883	183.780
TP #69	8.128	199.499	4.511	191.371
chk. SE BP Alleghany x Flintridge			2.966	196.533 √√

BM NW BP Rec Rd / Winchester

BM. NW BP Winchester Rd Morningside.

BM. SW BP Cumberland "

BM. SW BP Midwick "

BM SW BP Albemarle "

BM SW BP Potomac "

BM SW BP Potomac And Flintridge

BM SW BP Bolivar " Flintridge

= TP # 14 P. 25

Walker
Hurdin Jr
Hazard
9-45

~ BENCH MARKS ~
PARADISE HILLS ~
on RACHEL St. And WINCHESTER St.

	0.745	180.995		180.25
T.P.# 70	0.822	169.537	12.280	168.715
T.P.# 71	9.017	170.654	7.900	161.637
T.P.# 72	1.328	169.578	2.404	168.250
T.P.# 73	1.160	159.948	10.790	158.788
T.P.# 74	0.853	151.331	9.470	150.478
T.P.# 75	11.506	153.312	9.525	141.806
T.P.# 76	0.250	152.559	1.003	152.309
T.P.# 77	0.910	148.929	4.540	148.019
T.P.# 78	11.815	158.859	1.885	147.044
T.P.# 79	12.823	170.952	0.730	158.129
T.P.# 80	12.668	182.920	0.700	170.252
T.P.# 81	12.380	194.458	0.842	182.078
T.P.# 82	7.570	196.623	5.405	189.053
T.P.# 83	12.900	208.999	0.524	196.099
T.P.# 84	5.700	213.796	0.903	208.096
chk. N.W. B.P. Winchester And Morningside			0.110	213.686
				213.684 = T.P.# 55 P-29
				0.002

✓✓✓

B.M. S.E.B.P. Alleghany And Rachel St.

B.M. S.E.B.P. Potomac And Rachel St.
B.M. S.E.B.P. Gables " Rachel St.

B.M. S.E.B.P. Albemerle " Rachel St.

B.M. S.E.B.P. Cumberland " Rachel St.
B.M. S.E.B.P. Shaw " " "
B.M. N.E.B.P. Winchester " Rachel St.

B.M. N.E.B.P. Winchester " HOPKINS St.

Walker
Hurdin
Huntley.
11-14-45

~ BENCH MARKS ~
on FLINTRIDGE
And on HOPKINS St.

	11.340	185.935	174.095	B.M.
T.P. #85	6.464	191.369	0.530	184.905
T.P. #86	0.775	187.204	4.940	186.429
T.P. #87	2.943	187.209	2.943	184.261
T.P. #88	12.545	194.914	4.835	182.369
T.P. #89	2.00	194.962	1.952	192.962
T.P. #90	3.678	195.320	3.320	191.642
T.P. #91	8.532	192.132	11.720	183.600
Chk B.M.			3.070	189.062
				189.053
				.009

S.W.B.P. Flintridge And Potomac St. T.P. #67 P-29

N.E.B.P. " " Albemarle St.

S.W.B.P. Albemarle " Hopkins.

S.W.B.P. Cumberland " "

S.W. B.P. Stow " "

N.E. B.P. Winchester " "

Walker.
Hardin
Hunter
1-4-46
1-7-46

Cross Section Alley Blk. L Altadena Subd. between 32nd. and Bancroft Sts. from a point 300' N. N.L. Redwood to St. Thorn St.

BM Elev. W. Top cb. 5+98.3 FB 1539/49

	3.37	307.08		303.71
T.P.	5.91	308.41	4.58	302.50

N.L. Redwood = 0+00

3+00

W.L. on Par.		2.66	05.75
C. " "		2.75	05.66
E. " "		2.36	06.05
0+15 on Rim MH		3.15	05.26

3+25

E. on Par.		2.99	05.42
C. " "		3.43	04.98
W " "		3.36	05.05

3+48.5 = Dble 6.2' Lt of C

3+50

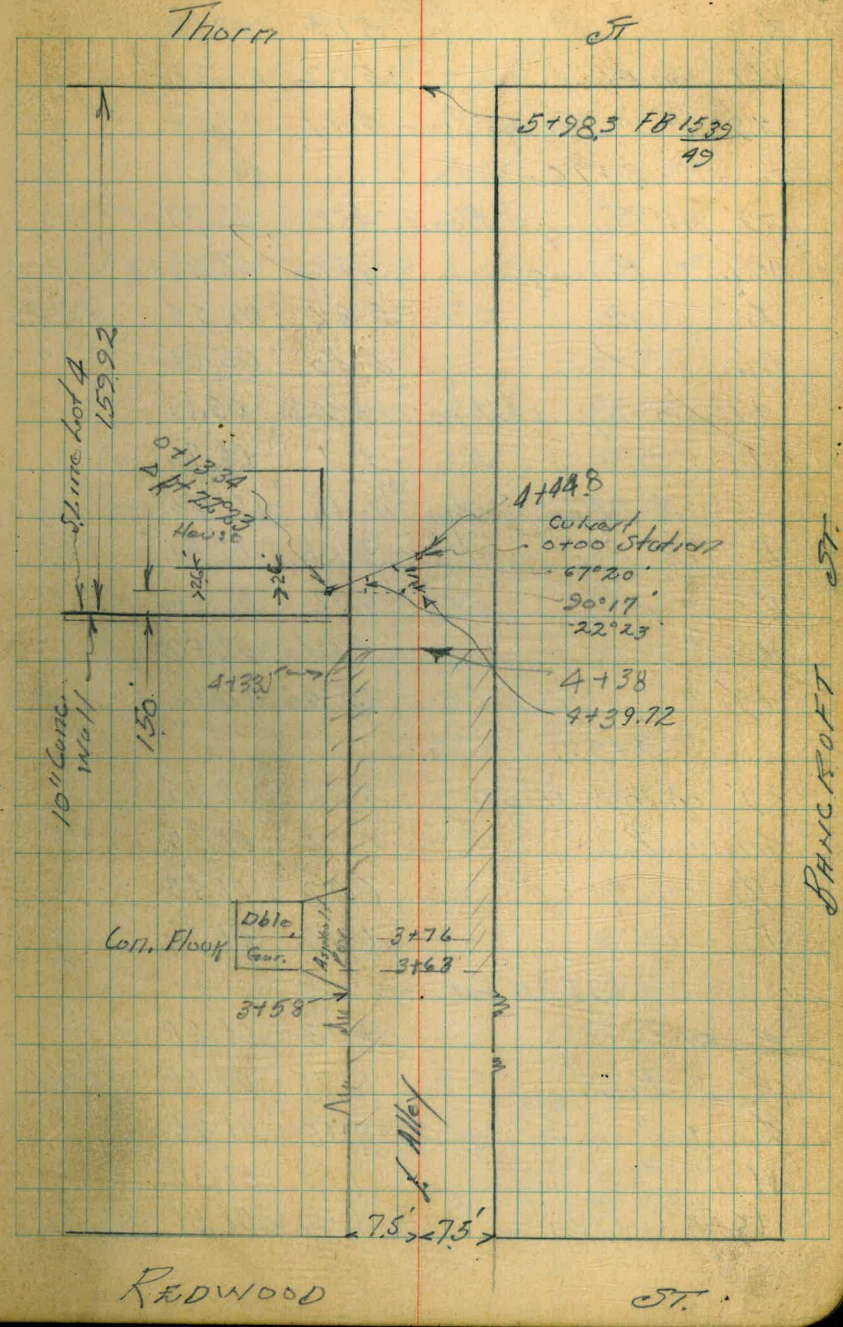
W		4.32	04.09
C		4.45	03.96
E		4.14	04.27
3+58 W.L. Par		4.74	03.67

3+69

E. -5'		2.8	06.6
E. - 1' on cobble wall		2.85	05.56
E. on Paving		4.67	03.74

Indexed cr. & K.

32



30841

℄	5.13	03.28
W.L. on Pav.	5.02	03.39
+9 " " = Garage Floor	4.47	03.94
3+76		
-9' on Garage Floor	4.52	03.89
W.L. " Paving.	5.78	02.63
℄ " "	5.86	02.55
E.L. " "	5.40	03.01
+1' on Top cobble wall	3.22	05.19
+5	3.7	04.7
3+79 = S edge of North Dbl. Garage		
E on Pav.	5.60	02.81
℄ " "	6.07	02.34
W " "	6.01	02.40
+9' " " = Gar. Floor	5.45	02.96
3+92		
-9' on Gar. Floor.	5.46	02.95
W " Pav	6.86	01.55
℄ " "	6.93	01.48
E " "	6.49	01.92
3+95 = N end cob. Wall on E		
E on Wall	4.13	04.28
" " Pav.	6.75	01.66
℄ " "	7.15	01.26
W " "	7.03	01.38
+5 " Conc. Pav	6.60	01.81

4+00		
-5' on Conc. Pav.	7.28	01.13
W " Pav.	7.39	01.02
℄ " "	7.44	00.97
E " "	7.06	01.35
+1.7 on Board Ret. Wall	6.04	02.37
+5	5.7	02.71
4+30		
-5	8.0	00.41
-1.7 on Board Ret. Wall	8.46	99.95
E " Pav.	9.36	99.05
℄ " "	9.73	98.68
W " "	9.68	98.73
+5 " Conc. Pav.	9.30	99.11
(4+33.5) 5' W.W.L.	9.31	99.10 on Conc. Pav.
4+38 = N end Asphalt Pav.		
-5	12.6	95.8
W on Conc. Pav. Ridge	9.87	98.54
+2' A.C. Pav	10.30	98.11
℄ " " "	10.46	97.95
E	9.92	98.49
+1.7	9.7	98.71
" on Board Wall	9.10	99.31
+5	8.7	99.71
4+39 = two 2½"x12" Boards Three 7"x7" posts. Barricades 1' N. N. end Pav.		
	10.95	97.46
4+44.8 on 0+00 of Proposed Drain.		

308.41

4+52 = ℄ 63' Conc. Porch on W 2' Back

-10'	10.6	97.8
E	10.6	97.8
℄	10.9	97.5
+6	10.9	97.5
W	12.7	95.7
+2	12.7	95.7
+2' on Porch	10.99	97.42
+6 " " at House	10.99	97.42

4+76

-10	13.6	94.8
W	13.6	94.8
+4	13.7	94.7
+6	11.0	97.4
℄	11.0	97.4
E	10.8	97.6
+10	10.7	97.7

4+78 = ℄ Dbl. Garage on W 32nd St. Entrance

-10	10.7	97.7
E	10.8	97.6
℄	11.0	97.4
+4	11.0	97.4
W.L.	13.6	94.8
+11 at Garage	13.6	94.8

308.41

4+78 = South end 4' Wood Porch on W

W - 3' on Porch	10.92	97.49	E edge
5+13 = N end Above Porch	10.96	97.45	

5+00

-7 under Porch	15.0	93.4
-3 " "	13.0	95.4
W	13.0	95.4
+2'	11.1	97.3
℄	10.5	97.9
E	10.7	97.7
+10'	10.4	98.0

5+18

-10	8.9	99.5
E	9.0	99.4
℄	9.3	99.1
+5	10.0	98.4
W	12.3	96.1
+10	13.2	95.2

5+23

-10	8.3	00.1
W	9.0	99.4
℄	8.7	99.7
E	8.2	00.2
+10	8.4	00.0

5+33

-10	7.0	

308.41

E.	6.9	01.5
℄	7.2	01.2
W	7.6	00.8
+10	8.6	00.8

5+39 S. end Stucco Store Bld on W 3.0 Back.

-10	11.2	97.2
W-3' at Bld	8.4	00.0
W	7.3	01.1
℄	6.6	01.8
E.	6.2	02.2
+10	6.3	02.1

5+44 to 5+51

℄ on Platform	4.50	03.9
W+3' "	4.50	03.9
" Floor Store Bld. Piggly Wiggly	4.35	04.06

5+50

-10	5.7	02.7
E	5.8	02.6
℄	6.2	02.2
W	6.0	02.4
+3 at Store Bld	6.0	02.4

5+75

-3	5.6	02.8
W	5.6	02.8
℄	5.5	02.9
E	5.4	03.0
+10	5.4	03.0

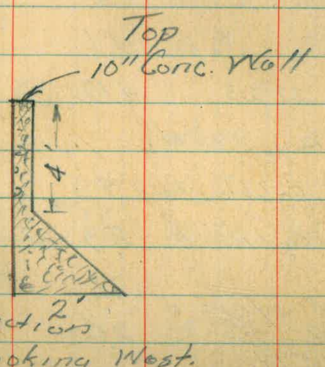
5+98.3 = St. Thorn St.

E. Top Cb	4.56	03.85
" Gutter on Pav.	4.78	03.63
℄ " "	5.02	03.39
W " " "	4.92	03.49
W Top Cb.	4.70	03.71
T.P. Z.56 300.02	10.25	297.46

Ground Profile	Proposed Drain	
0+00	2.56	97.46
+08	2.0	98.0
+10	4.1	95.9
0+13.3 W Δ Rt. 22°23'	4.19	95.83 on stake
0+14 = E end House 2.6 Rt.		
0+23 Loose Cobble Wall	4.9	95.1
+25 = Toe Wall	8.9	91.1
0+35	9.1	90.9
10' Rt. under House Basement	9.6	90.4
0+37 = E end Wall 1.5' Lt	9.19	90.83 10" Conc. Wall
2'	9.6	90.4
0+55 = W end House on N	9.3	90.7 2.6 Rt. of ℄
1.5' Lt on 12" Conc. Wall	9.10	90.92
2.5' Lt	14.4	85.6
1+01 = Approx ℄ Ernst. 36" Pipe	8.8	91.2
2' Lt. on Wall	8.90	91.12
2.5' Ht. Footing	13.74	86.28

		300.02		
0+86				
℄			8.9	91.1
2' Lt. on 10" Conc. Wall			8.87 (5.30)	91.15
2.5' Lt. on Top Footing			14.07	85.95
4.5 Lt.			15.4	84.6
T.P.	7.73	305.19	2.56	297.46
Chk. starting BM. W.G. Alley / S.L. Thom			1.48	303.71 ✓

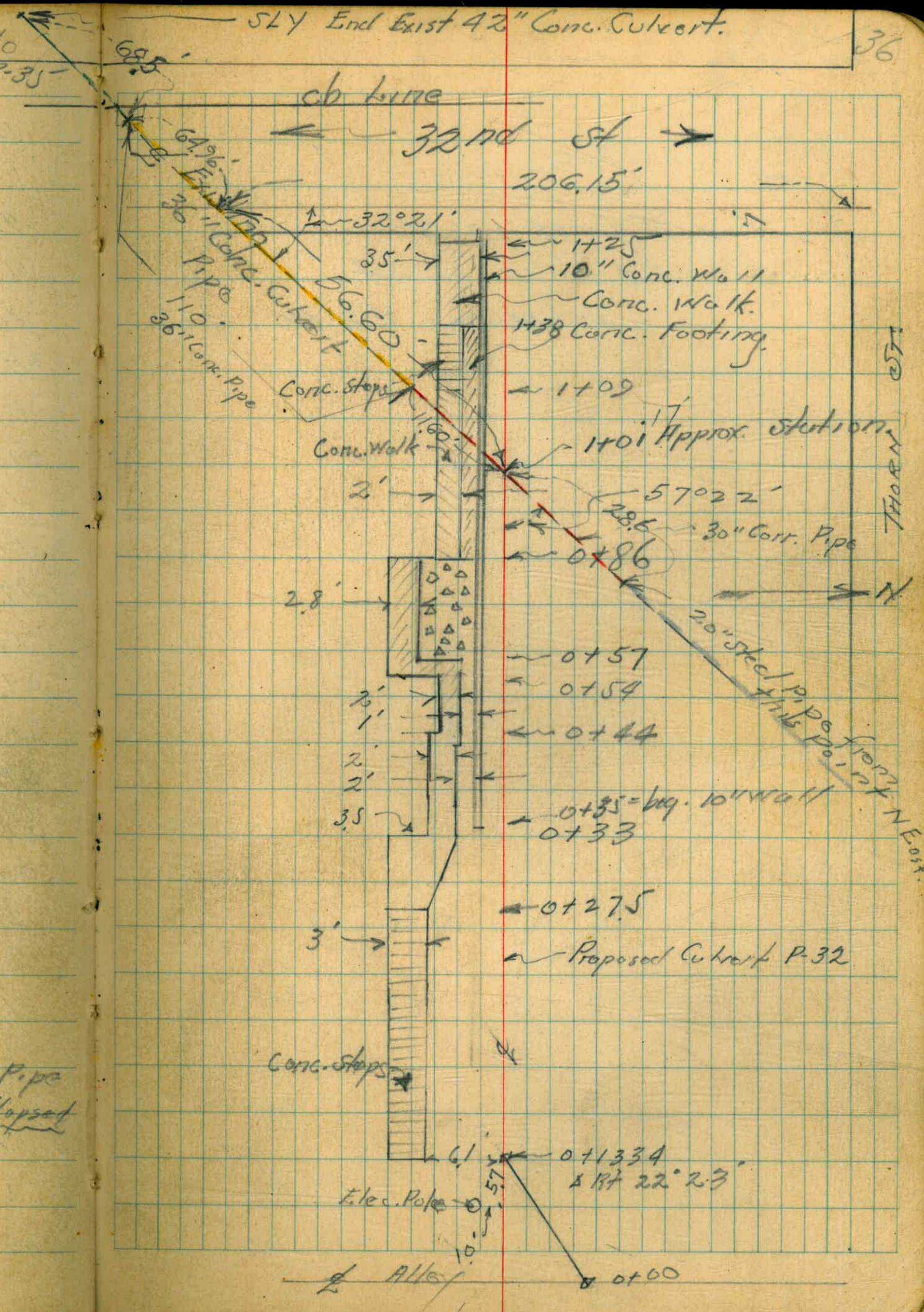
Proposed Culvert Profile Cont. from P-35



End Section
Elev. Looking West.

Legend:

Length 68.5' =	- - - - - (green)	= ℄ Existing 42" Conc. Pipe
" 110' =	- - - - - (yellow)	= ℄ " 36 " "
" 40' =	- - - - - (red)	= ℄ " 30" Corrg. Iron Pipe
" Indefinent =	- - - - - (grey)	= ℄ " 20" Iron Pipe - Collapsed

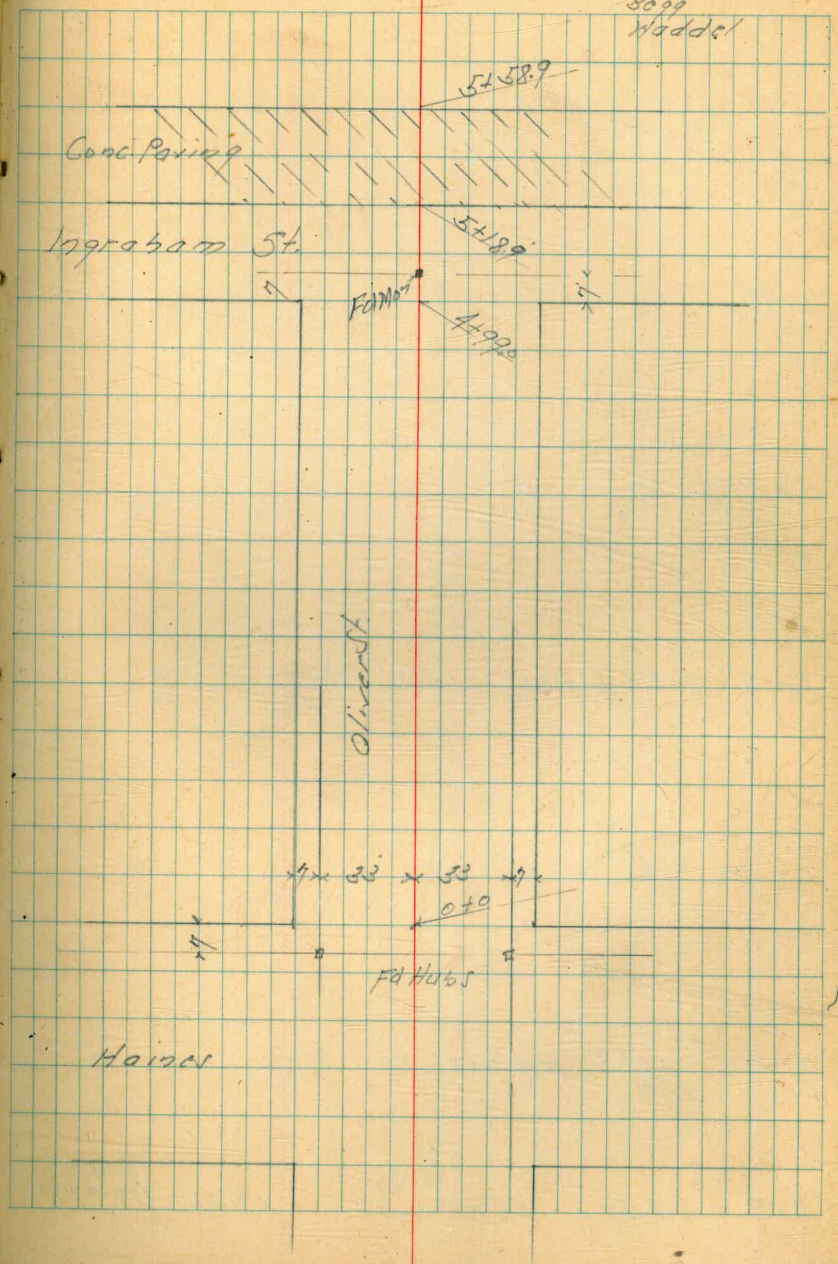


Cross Section Oliver St.
Haines to Ingraham St.

For RE Cross Sections
See FB 2074 - 50-54
C.B. Walker 9-18-50

Indexed
C.S.K.

Feb. 25-46 37
Sisson
Osborne
Boggs
Waddell



Oliver St.

Station						Lt: N		℄		Rt S	
1+50						9.0 / 40	9.2 / 20	8.6	8.5 / 20	7.8 / 40	7.35 / 40.3 = Bt Wall 3' Conc Wall
0+98						9.5 / 40	9.8 / 20	9.4	9.5 / 20	8.5 / 40	8.38 / 43.1 = Ely 8" Conc Wall
0+47						9.5 / 40	9.9 / 20	9.7	10.1 / 20	9.3 / 40	8.63 / 43.5 = H Conc Wall Top 8"
0+0	= E.L. Haines					9.9 / 40	10.3 / 20	9.7	10.2 / 20	9.2 / 40	
0−40	= ℄					10.5 / 40	10.9 / 20	10.9	10.9 / 20	10.8 / 40	
0−80	= H.L. Haines					10.3 / 40	10.5 / 26	11.1	11.0 / 26	11.1 / 40	
BM	6.59	52.95		47.36	Mon. 47' Line Ingraham ℄ Oliver			53.95			

Oliver St

4+0					
3+72					
TP	10.08	57.44	6.59	47.36	on Mon ℄ Oliver 7'W Ingraham
3+50					
3+0					
2+50					
1+98					
		5395			

Lt.=N			℄			Rt.=S
6.5 / 50	6.0 / 40	5.6 / 20	4.9	4.2 / 20	3.9 / 40	
				4.24 / 41 = HH 2.2' Brick Walk		
			57.44			
3.6 / 50	3.3 / 40	2.8 / 20	1.8	1.5 / 20	1.0 / 40	
5.1 / 50	4.7 / 40	4.1 / 20	3.2	2.7 / 20	2.1 / 40	
6.7 / 50	6.6 / 40	6.0 / 20	5.2	4.7 / 20	5.6 / 40	
8.5 / 50	8.3 / 40	7.9 / 20	7.1	6.8 / 20	5.92 / 38.6 = 4.2 + HH Conc Wal	5.86 / 400 on Walk
			5395			

Oliver St.

NE B.P. Grand Ave & Ingraham 55.35

BM			1.96	55.83
TP	7.98	57.77	0.85	49.79
TP	5.34	50.64	12.14	45.30

5+58.9 = East Edge Conc Paving

5+38.9 = ℄ Paving

5+18.9 = West Edge Conc Paving

4+99.0 = W.L. Ingraham

4+97 215 Lt of ℄ = Anchor Pole

4+95

4+50

57.44

Lt ℄ Rt 40.

10.23 90	9.60 40	9.59 20	9.59	9.63 20	9.63 40	9.87 90
10.17 90	9.54 40	9.58 20	9.55	9.56 20	9.62 40	9.89 90
10.22 90	10.15 40	10.14 20	10.13	10.15 20	10.22 40	10.42 90
10.0 50	9.9 40	9.7 20	9.4	9.8 20	9.4 40	
6.3 50	5.8 40	5.5 25	8.6 16	9.0	8.9 18	5.2 27	4.8 40
6.5 50	5.9 40	5.5 20	5.8	5.3 20	4.3 40	

57.44

Cross Section Alley Block 52 Ocean Beach
From Cable St to Sunset Cliffs Blvd
Between Newport & Niagara

Levels Next Page

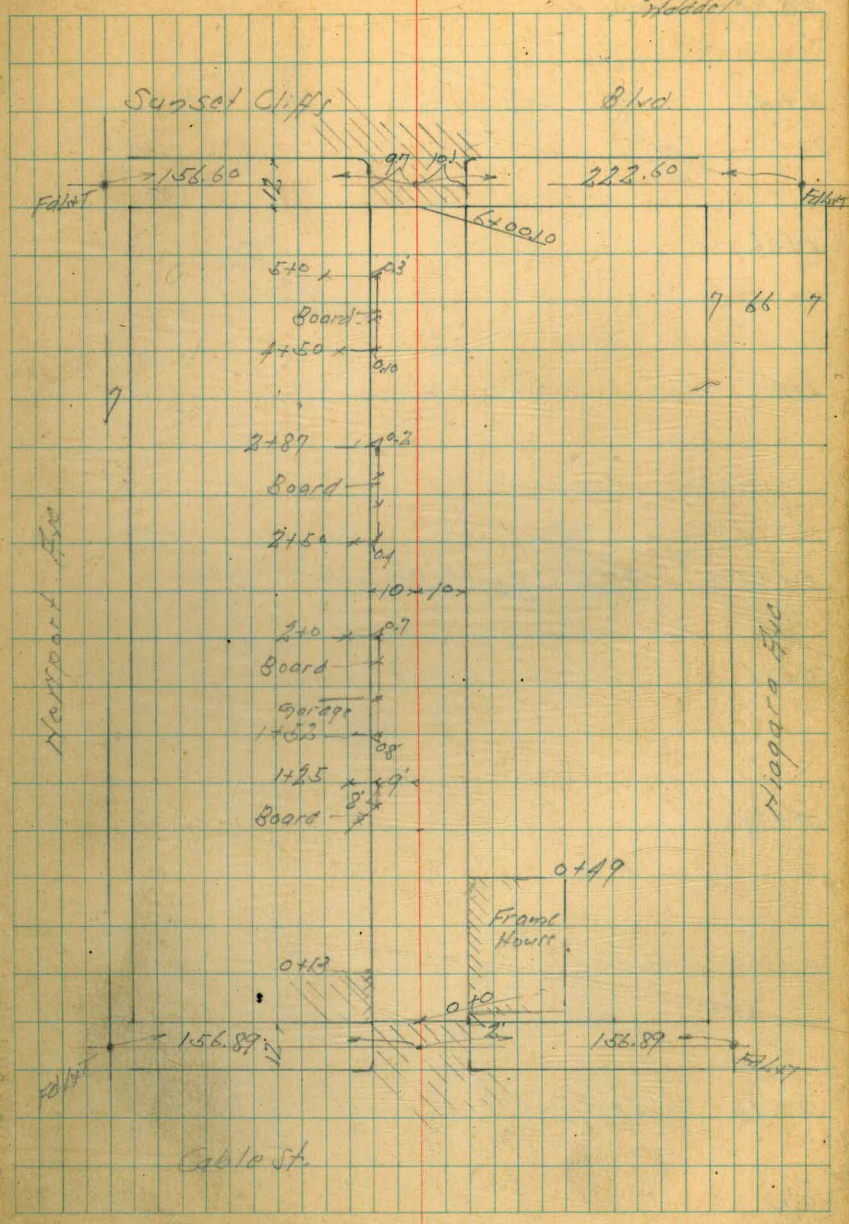
3-1-46 Notes reduced — Wherry. May 23-46 Sisson

Grades For L.C. Anderson Contractor

BM	4.85	30.39		26.04	N.W. C.P. Niagara & Sunset Cliffs
TP	4.58	28.55	6.42	23.97	
					N.L. Alley
1+0				22.73	5.82 on stks
1+20				23.04	5.51 on stks
1+40				23.42	5.13 out
1+50				23.62	4.93

Indexed
C.S.K.

Feb. 25-46 A1
Sisson
Osborne
BC99
Middel



Cross Section Alley Block 52 Ocean Beach

Sketch Page 41

Station	Note	Lt-N			℄		Rt	
1+41		21.1 2.0/25	21.1 2.0/10	20.4 2.7/5	20.5 2.6	21.1 2.0/10	21.3 1.8/16 = ℄ Garage Dirt Floor	
1+06			20.3 5.8/18.5 = ℄ Garage Dirt Floor					
1+0		20.1 2.0/25		20.3 2.8/10	19.8 3.3	20.4 2.7/10		
0+93						19.92 3.20/12.7 = Nly Conc Apron 11'		20.02 3.10/14.3 = ℄ Garage Conc Floor
0+51	8.7 Rt of ℄ - Sly Power Pole							
0+46			19.18 3.94/10 = Sly × ℄ 9.5 Conc Slab		19.1 4.0	19.7 3.4/10		
0+13			18.35 4.77/10 = Ely Conc Slab					
0+0	= East Line Cable St	18.34 4.78/9.8 = Cb	18.16 4.96/9.8 = Gutter on Pol		17.85 5.27	18.24 4.88/9.9 = Gutter on Pol		18.65 4.47/9.9 = Cb
0-12	= East Curb Line Cable St		17.49 5.63/10		17.54 5.58	17.68 5.44/10		
BM	7.11 23.12 16.01 N.E. SP Newport & Cable				23.12			

2+95

2+85

2+83

2+02

TP	7.13	28.08	2.17	20.95
2+01	8.6 Rt of ℄ = Sly Power Pole			

1+93

1+86

1+58

1+53

28.12

Lt ℄ Rt 43

22.1
6.0
11.9=2 Garage Diff Floor

22.0 21.8 22.1 22.7 22.8
6.1/10 6.3 6.0/6 5.4/10 5.3/13.1=2 Garage Diff Floor

21.8 21.7 21.3 21.6 21.85 22.14
6.3/20 6.4/10 6.8 6.5/10 6.33/13.8=Fly Conc Floor 5.94/16.3=Fly 3 Car Garage Floor Conc

21.85 22.15
6.33/13.6=Fly Conc Floor 5.93/16.6=Fly 3 Car Garage Floor Conc

28.08

21.42
1.70
13.6=Fly Conc Floor

21.3 21.0 21.4 21.54 21.69
1.8/10 2.1 1.7/10 1.58/13.5=Fly Conc Floor 1.63/15.5=Fly 4 Car Garage Floor Conc

21.0
2.4
4.9=2 Garage Diff Floor

21.52 21.65
1.60 1.47
13.9=Fly Conc Floor 15.9=Fly 4 Car Garage Floor Conc

Station		Lt.		℄	Rt.	
4+0		23.4 4.7 25	23.2 ✓ 4.9 10	23.2 ✓ 4.9	23.5 4.6 10	23.6 4.5 25
3+85					23.39 4.69 14 = N/S Conc Apron	23.71 ✓ 4.37 16 = ℄ Gar. Conc Floor
3+65					23.70 4.38 16.5 = ℄ Dr. Garage Conc Floor	
3+50			22.6 5.5 10	22.6 5.5	23.0 5.1 10	23.4 4.7 17
3+47					23.18 4.90 16.4 = E/S 2.6 Conc Block Walk	
3+37			22.3 5.8 50 = S/S Bldg 3' Entrance Conc Floor			
3+27						23.06 5.02 10.5 = W/S 2.6 Conc Block Walk
3+25	8.5 Rt of ℄ = S/S Power Pole					
3+0			22.2 5.9 16	22.2 5.9 = on M.H. Cover	22.7 5.4 16	

28.08

28.08

TP	5.08	30.63	2.53	25.55
5+50				
5+30				
+01	94 Rt of ℄ = Sly Power Pole			
5+0				
4+87				
4+64				
4+50				
4+43				
4+08				

28.08

Lt.		℄	Rt.			
25.6 2.5/25	25.7 2.4/10	25.5 2.6	25.7 2.4/10			
			26.1 2.0/10 = N'ly Cor. Garage West Entrance Board Floor			
25.2 2.9/25	25.3 2.8/10	24.9 3.2/6	24.5 3.6	24.8 3.3/8	25.6 2.5/10	25.7 2.4/25
			24.72 3.36/14.6 = E'ly Conc Apron		24.88 3.20/15.9 = E'ly Do. Gar Conc. Floor	
			24.37 3.71/14.6 = W'ly Conc Apron		24.84 3.24/15.9 = W'ly Do. Garage Conc. Floor	
24.1 4.0/25	24.2 3.9/10	24.0 4.1	24.3 3.8/10			
			24.2 3.9/14.7 = ℄ Garage Dirt Floor			
			23.8 4.3/14.2 = ℄ Gar Dirt Floor			

Cell Floor

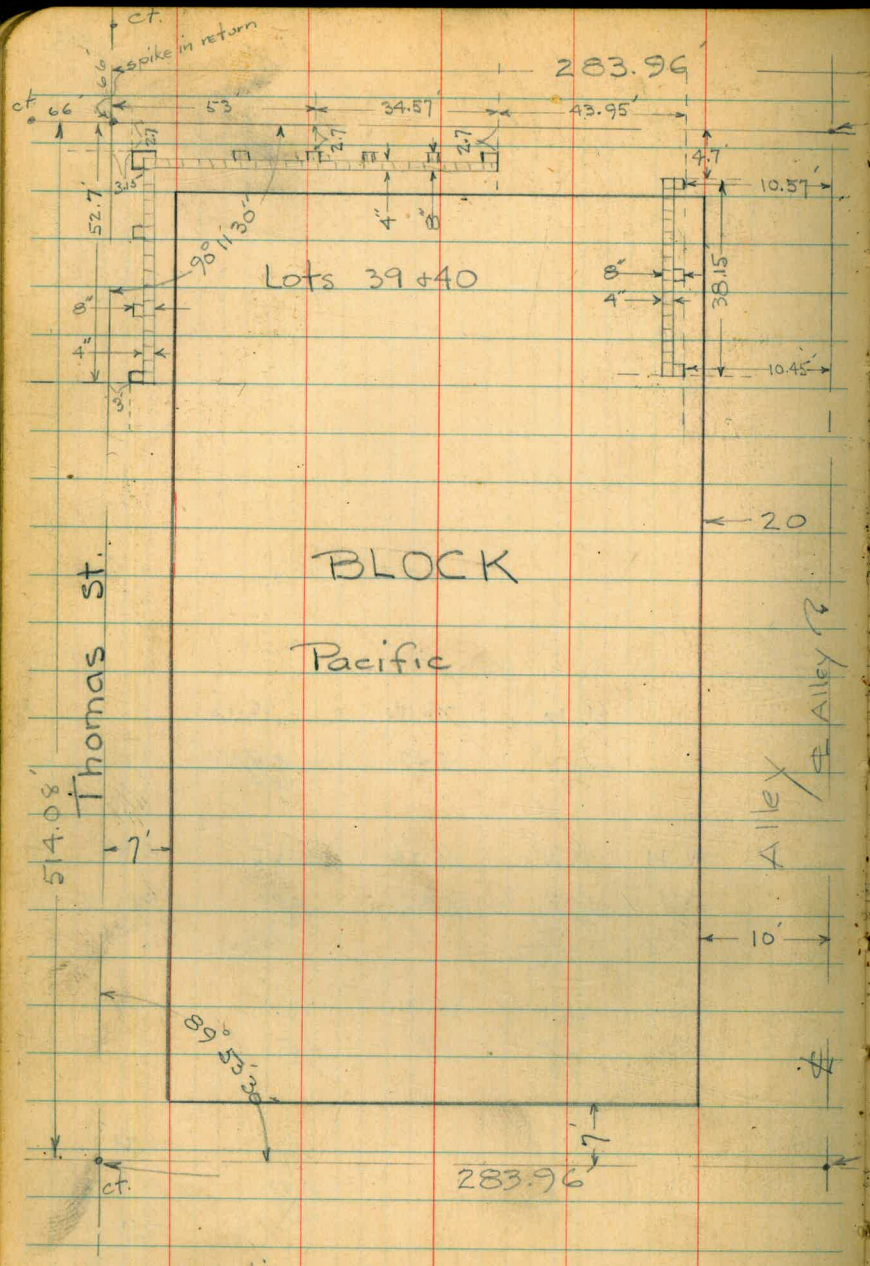
28.08

BM			4.60	26.03	H.W.B.P. Niagara + Sunset Cliffs 26.04
6+12.10 = West Curb Line					
6+00.10 = W.L. Sunset Cliffs Blvd					
5+80					
5+59					

30.63

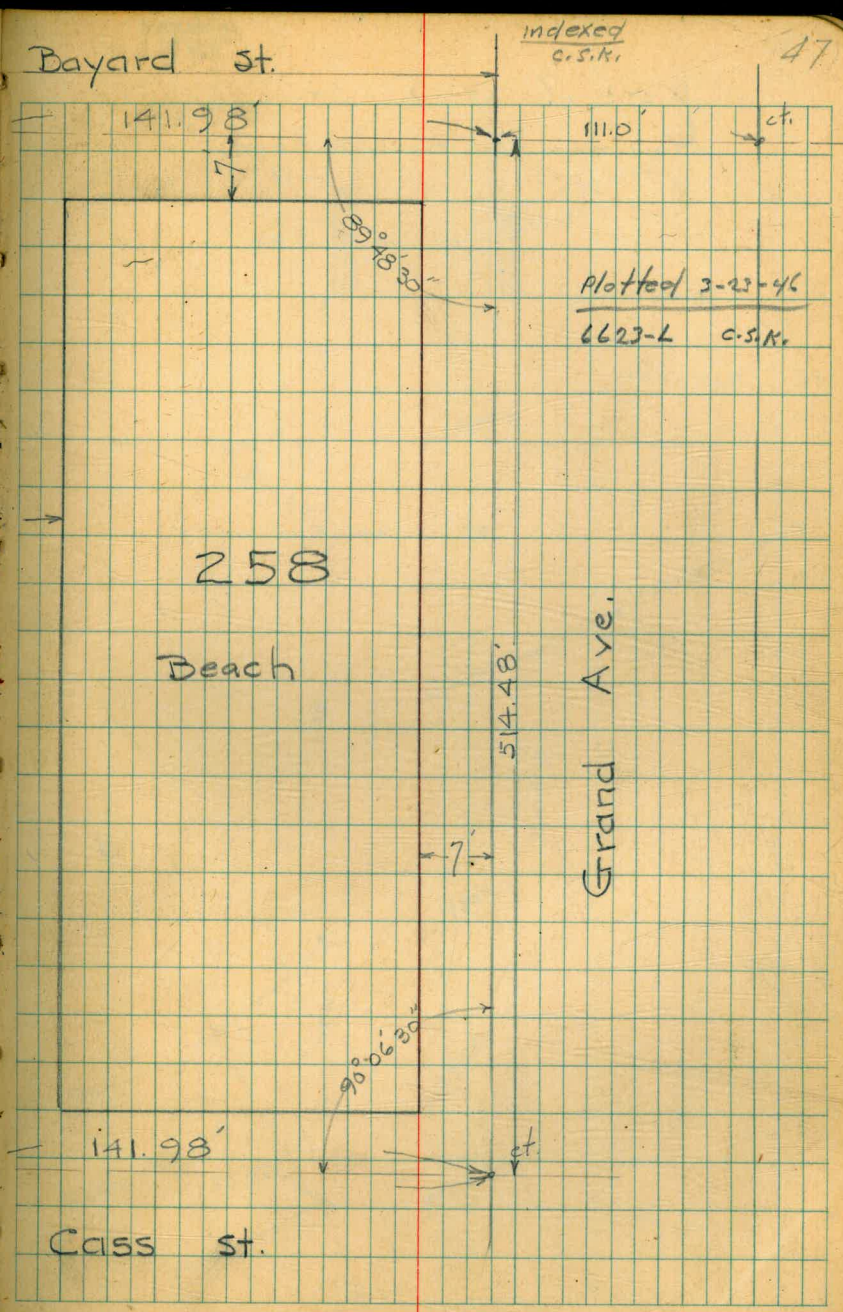
Lt.		℄	Rt.	
	25.10 5.53 / 10	26.16 5.47	25.23 5.40 / 10	
25.71 4.92 9.7 = Cb	25.56 5.07 9.7 = Gutter offset	25.38 5.25	25.65 4.98 10.1 = Gutter offset	25.88 4.75 10.1 = Cb
	26.1 4.5 / 10	25.7 4.9	26.1 4.5 / 10	
			26.10 4.53 12.1 = N/4 Conc	26.29 4.34 17.1 = N/4 Spr Conc floor

30.63



Location of 5' Brick wall - Lots 39 & 40.
Blk. 258 - Pac. Beach

Osborne
Grauencamp
Harden
3-18-46

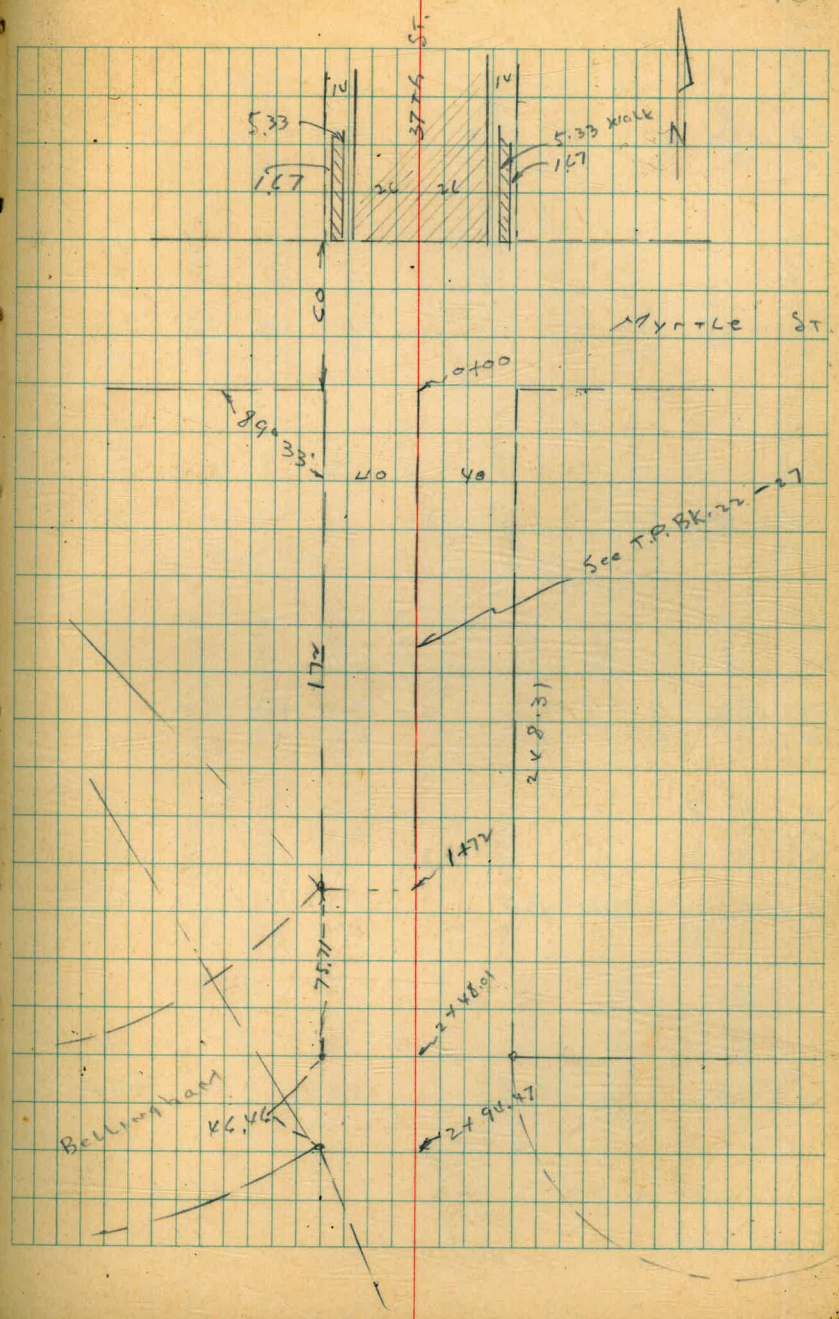


Indexed
C.S.K.

Plotted 3-23-46
6623-L C.S.K.

Indexed
C.S.K.

X sec. of 37th St
Myrtle to Bellingham



Left

Xsec 37th Myrtle Sly.

+	HI	−	E

0+59

0+37

0+18

0+05

0+00 S.L. Myrtle

N.L. Myrtle.

NW BM 2.39 313.13 310.74
37th & Myrtle

Right

LT = TO E. ℄ RT = to W

0+59: 302.5 (10.6/40); 301.7 (11.4/30); 292.4 (20.7/7); 291.0 (22.1); 288.6 (24.5/3); 289.5 (23.6/10); 287.3 (25.8/25); 295.1 (18.0/40); 302.6 (10.5/60)

0+37: 305.7 (7.4/40); 305.1 (8.0/20); 301.4 (11.7/15); 302.3 (10.8/12); 298.8 (14.3); 299.5 (13.6/11); 293.8 (19.3/16); 293.9 (19.2/27); 305.2 (7.9/36); 305.3 (7.8/40)

0+18: 308.5 (4.6/40); 307.6 (5.5/23); 306.4 (6.7/22); 307.7 (5.4/20); 307.8 (5.3); 304.8 (8.3/22); 301.4 (11.7/25); 301.2 (11.9/31); 306.2 (6.9/33); 307.2 (5.9/40)

0+05: 308.8 (3.3/40); 308.9 (4.2/29); 308.1 (5.0/24); 308.9 (4.2/18); 308.9 (4.2); 308.1 (5.0/23); 308.1 (5.0/27); 309.0 (4.1/31); 308.3 (4.8/33); 308.9 (4.2/40)

0+00: 308.9 (4.2/40); 309.0 (4.1/29); 308.3 (4.8/24); 308.9 (4.2/18); 309.0 (4.1); 308.6 (4.5/23); 307.1 (6.0/27); 306.4 (6.7/28); 308.5 (4.6/31); 309.2 (3.9/40)

N.L.: 310.18 (2.95/26/46); 309.56 (3.57/26/P); 310.25 (2.88/13/P); 310.53 (2.60/P); 310.46 (2.67/13/P); 309.88 (3.25/26/P); 310.54 (2.59/26/66)

Bottom

313.13

Sta.	+	H.I.	−	El.
1+47				
1+41				
T.P.	0.16	287.78	12.70	287.62
1+30				
1+13				
0+94				
0+76				
T.P.	0.18	300.32	12.99	300.14
		313.13		

LT = TOE ℄ 37th RT = TOW.

Row 1: 283.6, 280.3, 272.3, 263.9, 258.8, 259.2, 266.4, 273.3, 278.1, 286.8, 291.1
4.2/50, 7.5/40, 15.5/24, 23.9/13, 29.0/12, 28.6/5, 21.4, 14.5/13, 9.7/26, 1.0/40, +3.3/50

Row 2: 285.6, 281.6, 273.8, 264.6, 259.3, 259.4, 259.6, 269.3, 276.8, 286.3, 290.5
2.2/50, 6.2/40, 14.0/26, 23.2/6, 28.5/3, 28.4, 28.2/4, 18.5/13, 11.0/26, 1.5/40, +2.7/50

287.78

Row 3: 290.8, 286.8, 278.5, 278.8, 268.2, 260.7, 261.1, 272.4, 282.6, 288.6
9.5/50, 13.5/40, 21.8/20, 29.5, 32.1/10, 39.6/11, 39.2/21, 27.9/29, 17.7/40, 10.7/50

Row 4: 290.3, 285.9, 284.5, 278.8, 276.1, 296.4, 261.1, 269.6, 277.1, 284.9, 289.2
10.0/40, 14.4/30, 15.8/20, 21.5, 24.2/6, 39.3/12, 39.2/16, 30.7/17, 22.6/28, 15.4/40, 11.1/50

Row 5: 295.0, 291.5, 288.5, 282.0, 276.7, 268.1, 268.2, 273.6, 281.1, 286.1, 288.7
5.3/40, 8.8/27, 11.8/11, 18.3, 23.6/5, 31.6/8, 32.1/14, 26.7/18, 19.2/30, 14.2/40, 11.4/50

Row 6: 300.0, 293.7, 287.0, 281.2, 276.2, 277.8, 282.9, 288.0
0.3/40, 6.6/20, 13.3, 19.1/12, 24.1/15, 22.5/25, 17.4/40, 12.3/50

300.32

Lt = E ℄ 37th Rt = W

T.P. nail in P.P. at alley on Bellingham			12.05	287.18
T.P.	10.49	299.23	0.27	288.74
T.P.	12.27	289.01	0.00	276.74
2+94.47				
2+48				
2+30				
T.P.	1.55	276.74	12.59	275.19
1+97				
1+72				
		287.78		

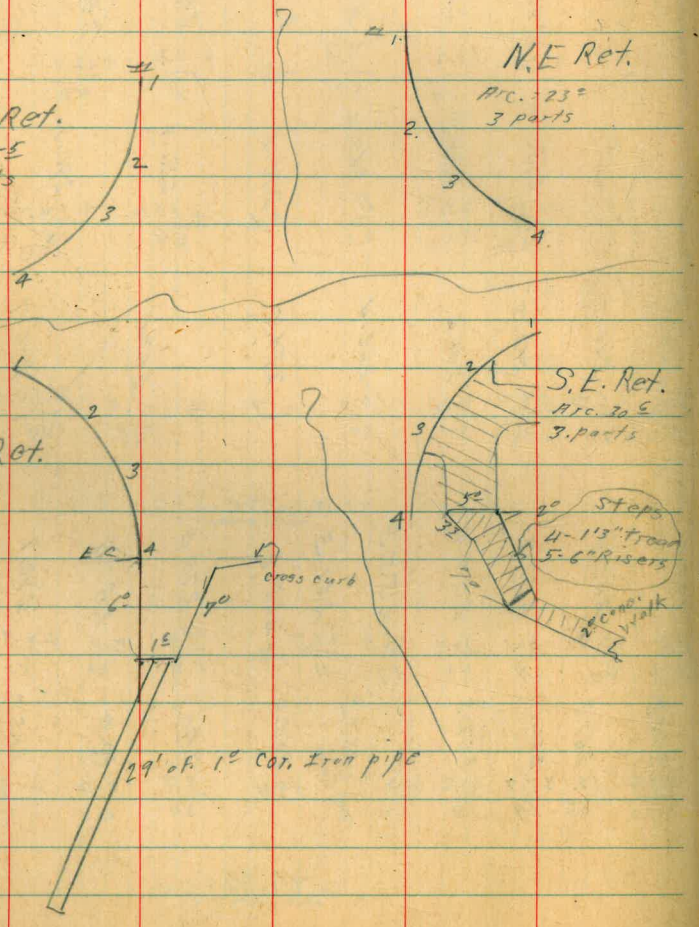
Cross-sections (cut/distance, elevation):

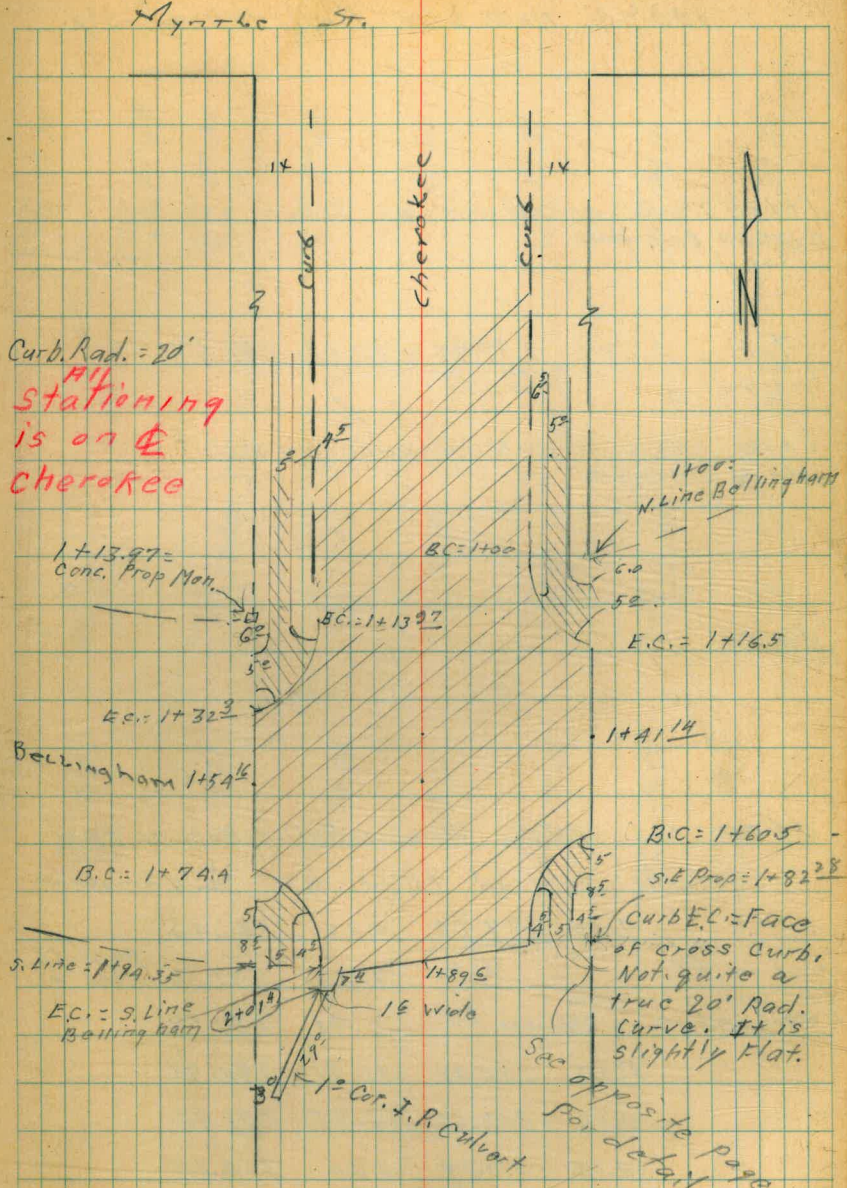
Station													
2+94.47			39.5/103, 237.2	32.5/75, 244.2	27.2/60, 249.5	18.2/40, 258.5	7.8/20, 268.9	+3.2, 279.9	+7.3/8, 284.0	+12.0/40, 288.7			
2+48	22.7/90, 254.5	26.0/77, 250.7	30.2/73, 246.5	28.7/47, 248.0	23.7/46, 253.0	21.5/40, 255.2	11.1/20, 265.6	0.6, 276.1	+10.2/24, 286.9	+14.2/40, 290.9			
	creek here												
2+30	15.0/70, 261.7	23.2/46, 253.5	27.2/44, 249.5	36.2/40, 240.5	36.2/34, 240.5	30.1/32, 246.6	14.3/20, 262.4	2.7, 274.0	+10.9/25, 287.6	+14.0/40, 290.7			
								276.74					
1+97	12.4/65, 275.4	21.9/40, 265.9	30.1/25, 257.7	32.4/22, 255.4	32.5/17, 255.3	26.5/11, 261.3	19.1, 268.7	9.0/15, 278.8	0.0/30, 287.8	+2.9/40, 290.7	+4.5/50, 292.3		
1+72	9.4/50, 278.4	13.6/40, 274.2	18.1/35, 269.7	27.7/19, 260.1	30.5/19, 257.3	30.3/12, 257.3	24.3/8, 263.5	19.4, 268.4	7.7/20, 280.1	+2.2/40, 290.0	+5.4/50, 293.2		
								287.78					

Sommermeyer
Begg Levels on Cherokee
at Bellingham

indexed
c.s.k.

Rod reading numbered 1-2-3-4





X-Sec. Cherokee

100' N. North Line Bellingham. Sly.

1+13.97 = B.C. cb. return on west
3+03.10 Bellingham

T.P. *Corr. Mon. See below.	2.35	289.93 299.90	12.32	287.58
1+00 = N. Line Bellingham - on East 3+84.46 Bellingham				
0+50				
0+00	100' No. - No. Line Bellingham on East			
Stations carried thru on ℄ Cherokee.				
	7.48	299.90	4.07	292.42
Nail in P.P. over tack in Corr. Mon. N.W. Cor. Bellingham & Cherokee		S.S.	9.31	287.18
		SS.	8.91	287.58
	5.54	296.49	11.71	290.95
	0.32	302.66	12.85	302.34
	0.35	315.19	3.64	314.84
N.W.B.P. 37th + Myrtle	7.74	318.48		310.74

Page 51 Line 4

℄

53

87.70	87.24	87.35	87.40	87.50	87.27	86.91	87.51
2.20	2.67	2.58	2.53	2.43	2.66	3.02	2.42
33.9 Top dk.	37.9 Out	26.	13		13	Out 26	Top dk. 26
89.26		88.68	88.72	289.93	89.53	88.13	88.78
10.64 dk.		11.22 Out.	11.18 13	11.13	11.37 13	11.77 26 Out.	11.12 26 dk.
94.10		93.38	93.48	98.59	93.20	92.83	92.97
5.80 26 Top dk.		6.52 26 Out	6.47 13	6.41	6.70 13	7.07 26 Out.	6.93 26 In drive
98.95		98.23	98.38	98.35	98.05	97.54	98.16
0.95 26 Top dk.		1.67 26 Out.	1.52 13	1.55	1.85 13	2.36 26 Out.	1.71 26 dk.

299.90

1+79.2 Start Cb. Return on West

1+60.5 Start Cb. Return on East

1+5A.16 ℄ Bellingham on West

1+A1.2 ℄ Bellingham on East

1+32.3 End Cb. Ret. on west

1+16.5 End curb Ret. on east

289.93

82.14	81.85	81.84	82.04	81.95	81.62	81.64	81.95	82.48
7.49	8.08	8.99	7.92	7.98	8.31	8.29	7.98	7.45
26.7 Top. Cb.	26.7 Cut	26	13		13	26	40 Cut.	40 Top. Cb.
84.21	83.61	83.27	83.34	83.08	83.43	82.90	83.36	83.4
5.72	6.32	6.66	6.59	6.85	7.00	7.03	6.57	6.5
40 Curb	40 Cut.	26	13		13	26	40	40 Ground
84.2	84.23	83.97	83.90	83.59	83.55	83.44	82.91	83.9
5.7	5.72	5.96	6.03	6.34	6.38	6.07	6.02	6.0
DV Ground	40	13	13		13	26	40	40 Ground
85.3	85.28	85.16	84.95	84.81	84.80	84.61	84.62	84.93
4.6	4.65	4.77	4.99	5.12	5.13	5.27	5.11	5.0
40 Ground	40	26	13		13	26	40	40 Ground
85.9	85.87	85.93	85.69	85.73	85.59	85.30	85.34	85.94
4.0	4.06	4.10	4.40	4.20	4.34	4.63	4.59	3.99
40 Ground	40 E. Pav.	26	13		13	26	40 Pav.	40 Top. Cb.
87.5	87.12	86.59	87.02	87.07	87.17	86.99	86.59	86.58	87.20
2.4	1.69 Top Cb. 39.7 End Ret.	3.24 Cut 39.7 Edge Pav.	2.91	2.86	2.76	2.94	3.34	3.35	2.73
40			26	13		13	26	26.3 Cut	26.3 Top Cb.

289.93

1+99 Continued

1+99 ℄

1+90 start at 9' cold lay drive

1+89 ℄ Cross curb. East curb end = Sta. 1+84 ℄
West curb = Sta. 1+94 ℄ see sketch Page 52
Taken on Diag.

1+76.53 on ℄ This Sec. taken on Diagonal.
S.E. Prop. Cor. = Sta. 1+82.78 + S.W. Prop.
cor = Sta 1+94.35

289.93

289.93 π

2+45

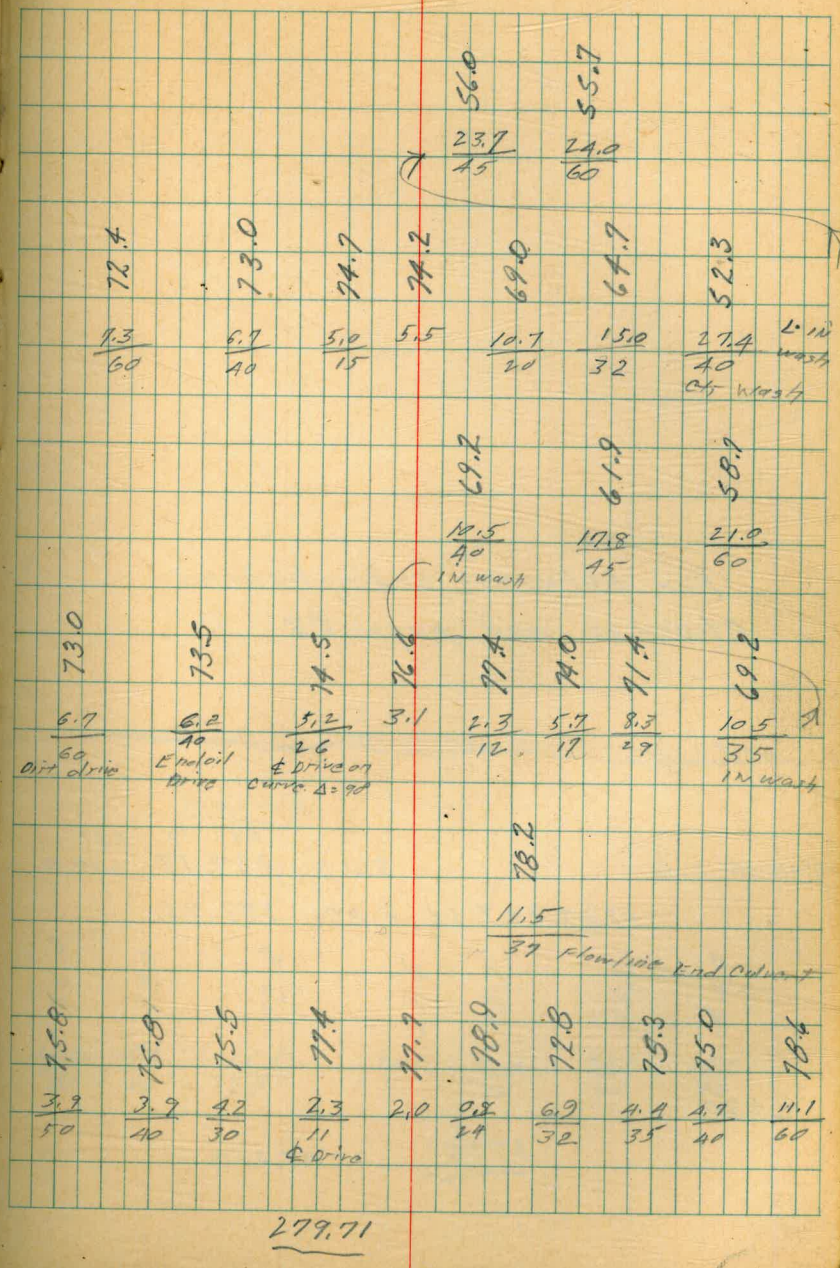
2+35

2+24 End culvert. Pipe Hangs in air from sta. 2+17 to 2+24

2+17 =

2.44 279.71 12.66 277.27

289.93



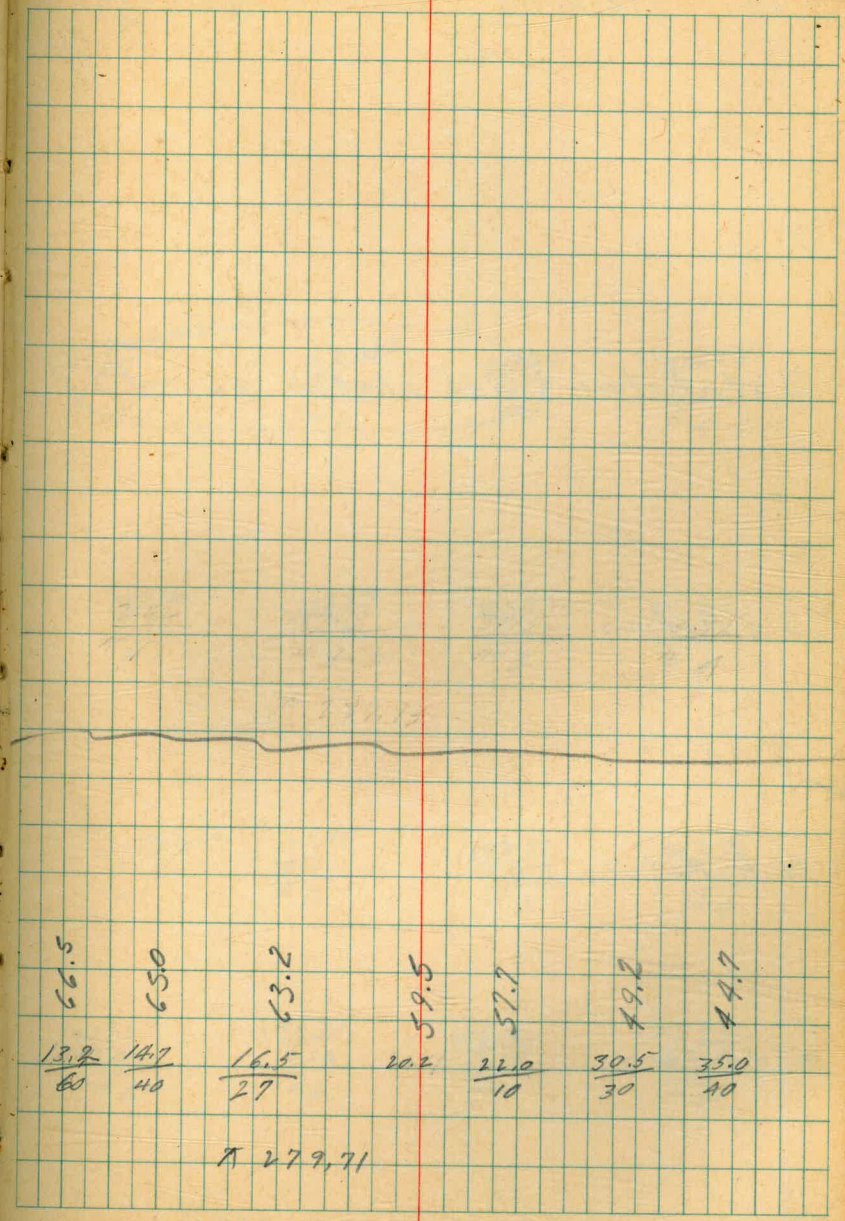
For Returns Bellingham & Cherokee see page 58

Error -0.01

			287.19		
Nail in pole		2.38	287.17	P.51	Line 4
12.27	289.55	2.45	277.26		

2+80

279.71



Sommermeyer

Begg Returns Bellingham &

S.W. Return (See sketch page 52.)

S.E. Return

N.E. Return

N.W. Return

spike. P.Pole. 2.75 289.93 — 289.18

P.51 Line 4

Cherokee

282.48 / 7.45 / #1

281.93 / 8.00 / #2

281.23 / 8.70 / #3

280.54 / 9.39 / #4

284.26 / 5.73 / #1

283.37 / 6.56 / #2

282.42 / 7.51 / #3

281.60 / 8.33 / #4

289.26 / 0.67 / #1

288.42 / 1.51 / #2

287.76 / 2.17 / #3

287.35 / 2.67 / #4

287.51 / 2.42 / #1

286.75 / 3.18 / #2

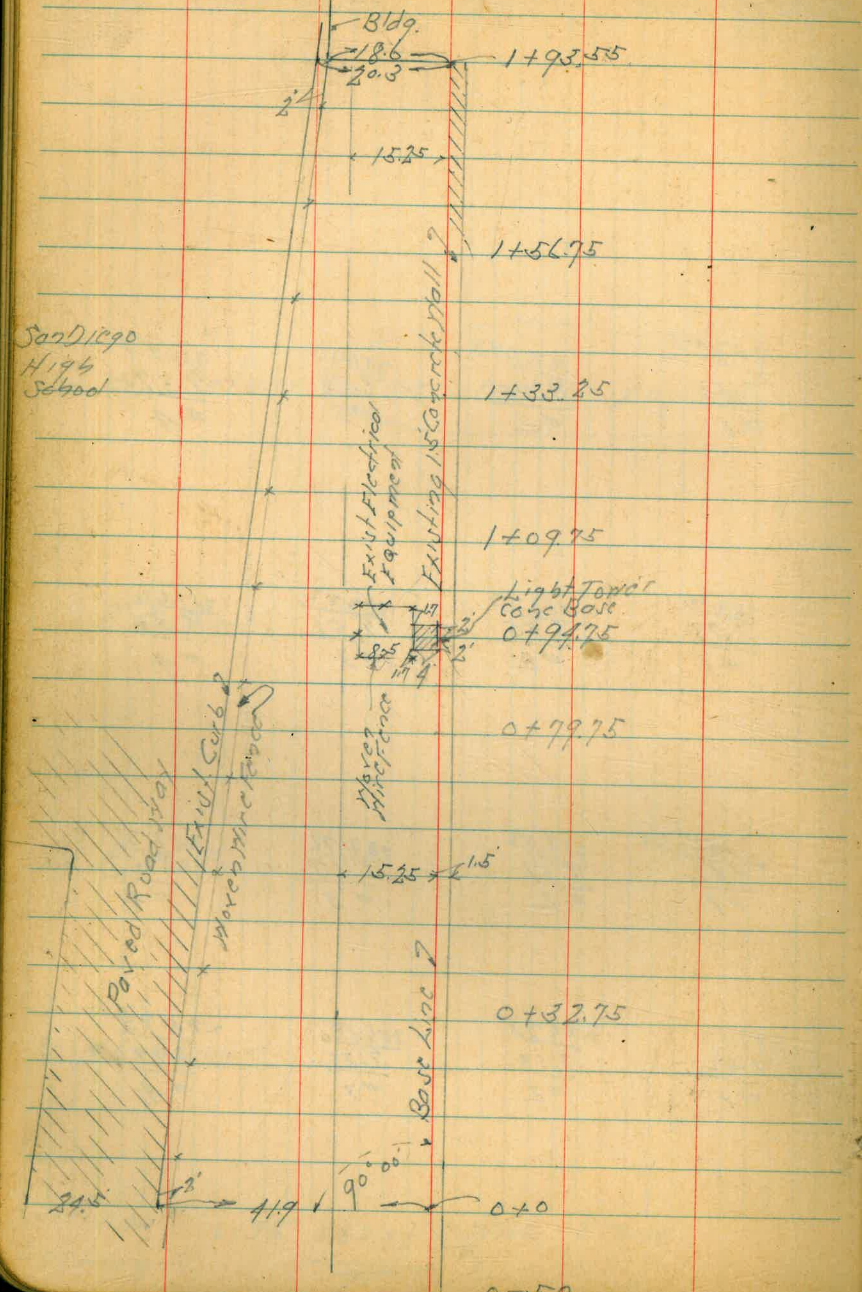
286.18 / 3.75 / #3

285.94 / 3.99 / #4

289.93

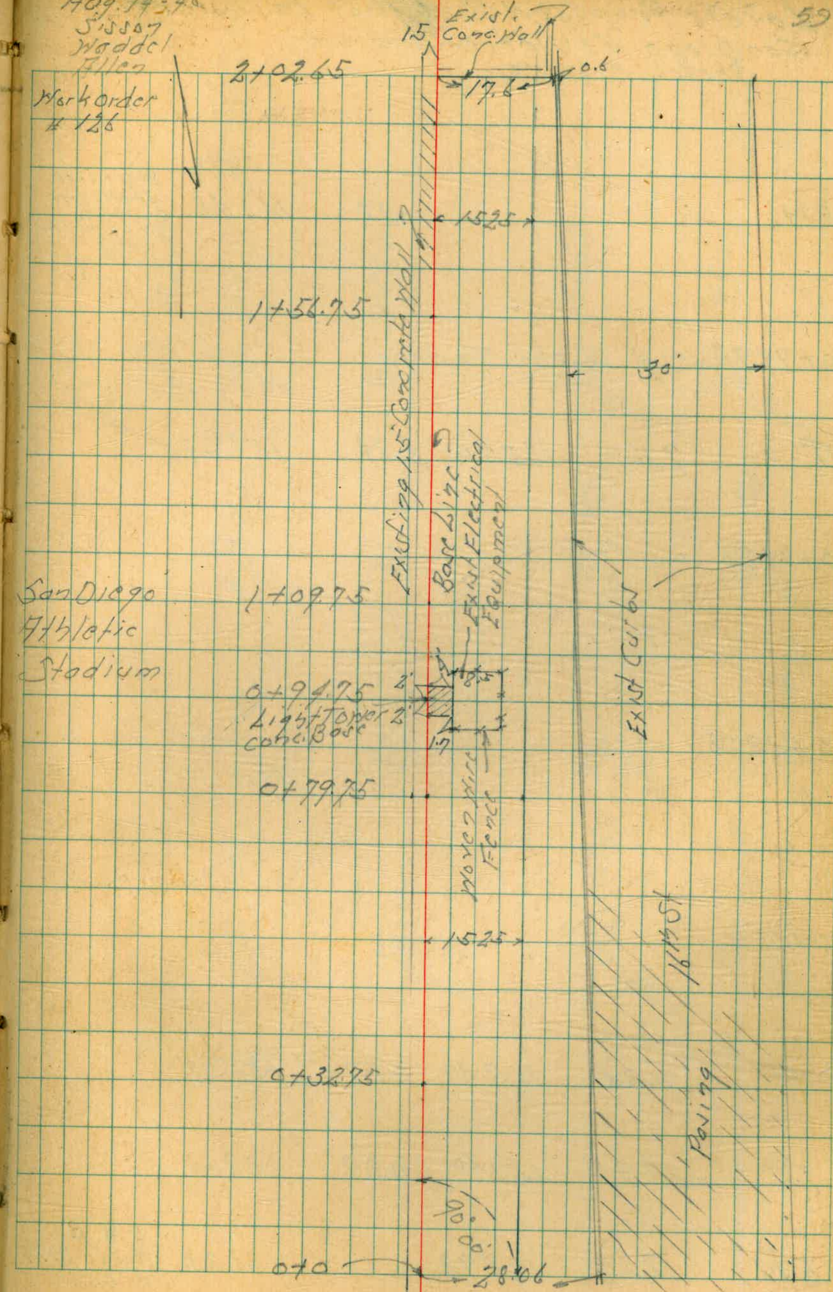
Proposed Buildings
San Diego Athletic Stadium

Indexed
C.E.K.



Aug. 14-46
Sisson
Waddel
Allen

Work order
126



Levels Proposed Buildings East Side.
San Diego Athletic Stadium
Sketch Page 59

BM			1.22	162.48	West Side Stadium Chisel □ Top of Steps 1402
0+94.75 = ℄ Light Tower					
TP	7.16	163.70	6.83	156.54	
0+79.75					
0+32.75					
0+0					
TP	11.84	163.37	0.07	151.53	
TP	12.97	151.60	0.29	138.63	
BM	12.69	138.92		126.23	S.W. B.P. Russ Blvd. 4/6/51

Aug 14-46
Sisson
Waddel
Allen

East

Base Line Fl. 7.5 Conc Wall

0+94.75	163.72 / 0.98 / 10 = W Conc Top Steps	163.85 / 0.85 / 7.5 = Conc Floor	163.19 / 0.51 Top Conc Wall	158.50 / 5.2 / 15.25	156.52 / 7.18 / 23.0 = Cb Top	155.56 / 8.14 / 23.0 = Gutter
TP			162.70			
0+79.75			162.77 / 0.20 = Top Conc Wall	158.8 / 5.1 / 15.25	155.90 / 7.47 / 24.0 = Cb	154.86 / 8.51 / 24.0 = Gutter
0+32.75			163.04 / 0.33 = Top Conc Wall	156.8 / 6.6 / 15.25	153.79 / 9.58 / 26.25 = Cb	152.74 / 10.63 / 26.25 = Gut
0+0			163.02 / 0.35 on Fl. Conc Wall	156.6 / 6.8 / 15.25 Ground	152.28 / 11.09 / 28.06 = Top Curb	151.26 / 12.11 / 28.06 = Gutter
TP			163.37			

2+02.65 = East + West Wall				
1+56.75				
TP	6.15	165.22	4.63	159.07
1+09.75				
		163.70		

East

Base Line

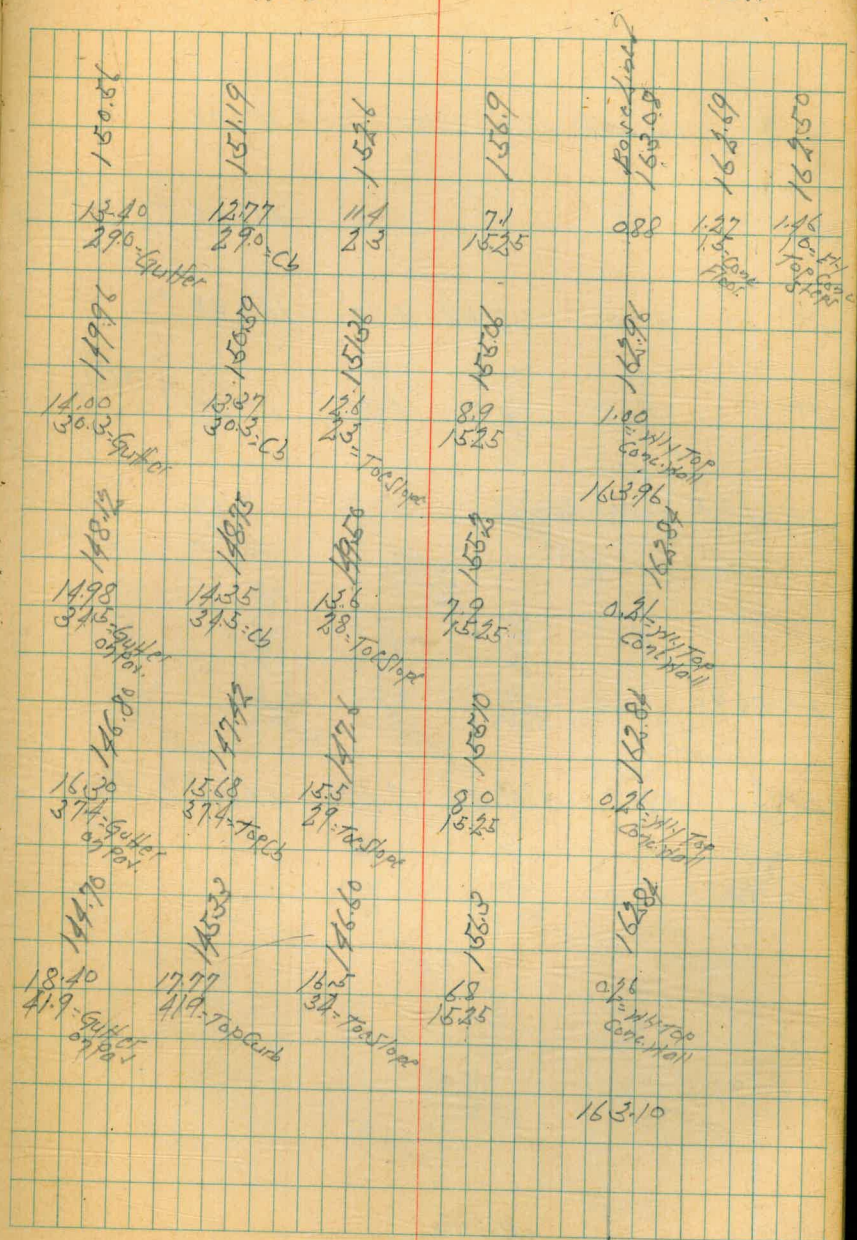
163.53	161.52	163.38	161.32	160.31
1.69 = Top Conc Wall	3.7 / 15.23	1.84 / 17.6 = Top Ext Wall	3.90 / 18.2 = Cb	4.91 / 18.2 = Gutter
163.37	159.82	159.37	158.29	
1.85 = Top Conc Wall	5.4 / 15.25	5.85 / 19.8 = Cb	6.93 / 19.8 = Gutter	
165.22				
163.26	158.4	157.18	156.14	
0.47 = Top Conc Wall	5.3 / 15.25 = Ground	6.52 / 22.2 = Top Cb	7.56 / 22.23 = Gutter	
163.70				

Levels Proposed Buildings West Side
San Diego Athletic Stadium
Sketch Page 59

0+94.75	℄ Light Tower				
0+79.75					
TP	8.32	168.96	7.46	155.64	
0+32.75					
0+0					
0-50					
TP	7.38	168.10	7.58	155.72	
BM	0.82	163.30		162.48	Page 60

West

East 62



Checked Back to Starting B M o.k

BM			1.52	176.06	B.P. N.E. Cor. Gym. S.D. High School 176.00
TP	9.00	177.58	0.70	168.58	} o.k.
TP	12.07	169.28	6.15	157.21	}
1+93.55 = S'ly Bldg.					
1+56.75					
TP	3.99	164.36	3.59	160.37	160.87
1+33.25					
1+09.75					
		163.96			

West. East 63

					Baseline
1+93.55	155.05 9.31 20.3 = Gutter	155.68 8.68 20.3 = Cb	156.03 8.33 18.6 = S.W. Cor. Bldg. [illegible] Floor	155.76 8.6 15.25 = Toe Slope	163.34 1.02 = N.W. Top Conc. Wall
1+56.75	153.02 11.34 23.5 = Gutter	153.66 10.70 23.5 = Cb	153.06 10.3 17 = Toe Slope	154.8 9.6 15.25	163.27 1.09 = N.W. Top Conc. Wall 164.36
1+33.25	152.07 11.89 25.6 = Gutter	152.72 11.24 25.6 = Cb	153.1 10.9 19 = Toe Slope	154.3 9.7 15.25	163.22 0.74 = N.W. Top Conc. Wall
1+09.75	151.16 12.80 27.6 = Gutter	151.76 12.20 27.6 = Cb	152.4 11.6 22 = Toe Slope	155.3 8.7 15.25	163.08 0.88 = N.W. Top Conc. Wall
					163.96

CITY OF SAN DIEGO
OFFICE OF CITY ENGINEER

INFORMATION REQUEST

3155

No 3015

W.O.NO. 21091

TO Gabrielson FROM Eckenrode DATE 12-22-48

Book-1692/64- Complete these notes. & continue to Noell St. Get Details of Covers & grades and additional openings- Wright & Estudillo Sts. Check opening #2.

REFERENCES: DRAWING NO. 2427-2429-2930L

FIELD BOOK NO. 1692
1805 (for notes)

REPORT BY Hampton TO Eckenrode DATE

Osborne Found openings covered by Paving - can get no information unless uncovered.

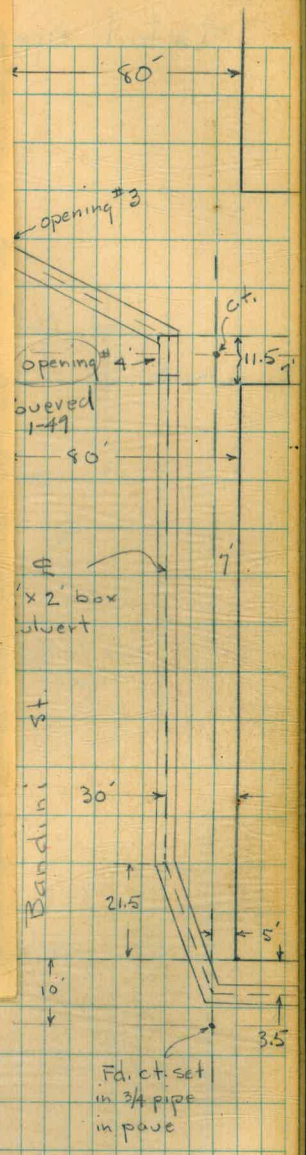
INFORMATION ON DRAWING NO.

DATA IN BOOK 1692-64

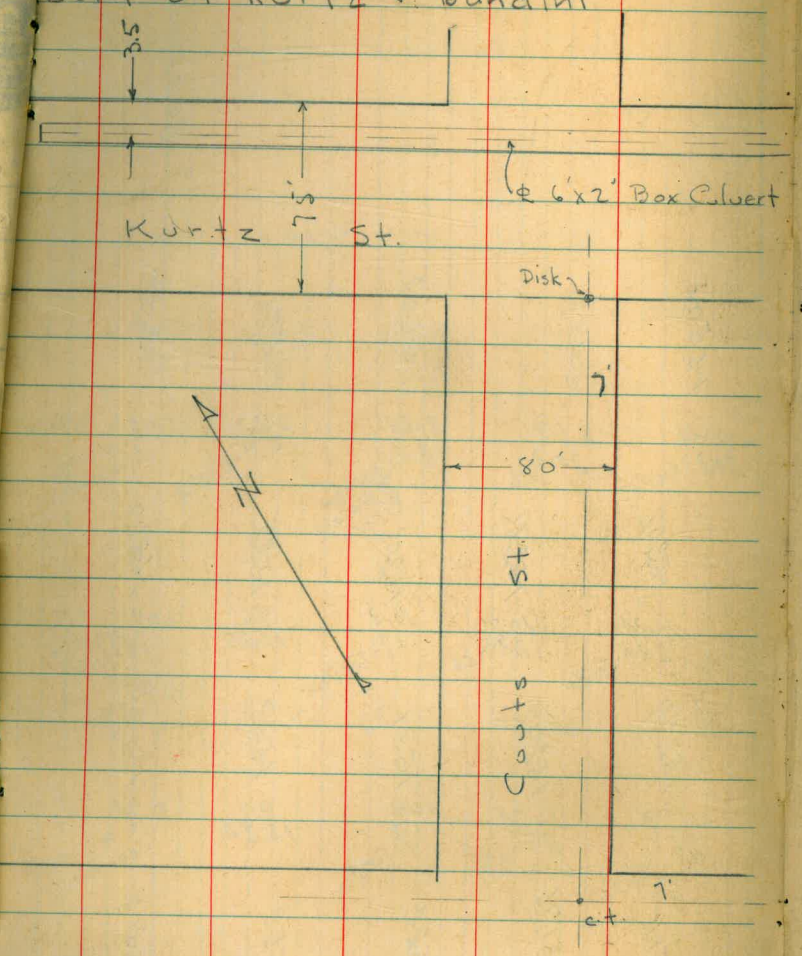
FORM 211

for Levels See Page 67

Pacific Hwy



cation of New Boxes on Old Box
wert on Kurtz + Bandini

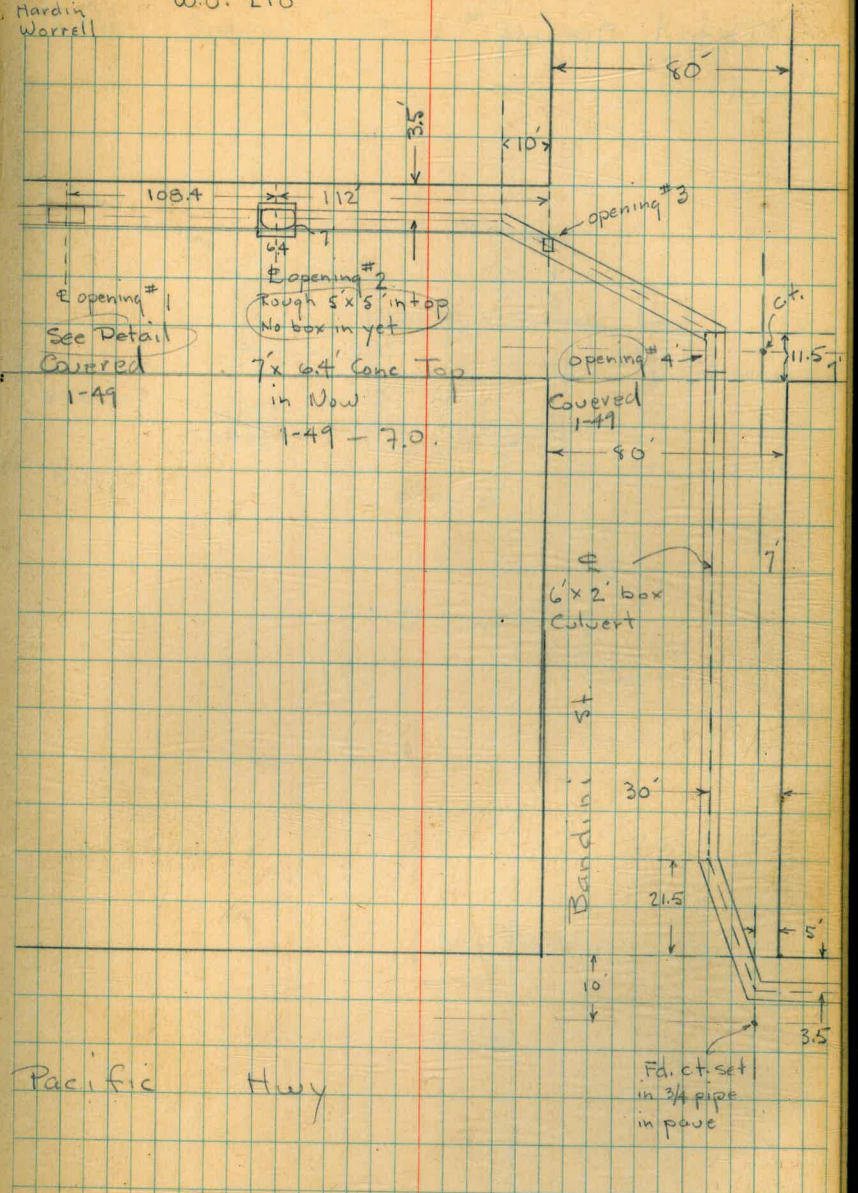


for Levels See Page 67

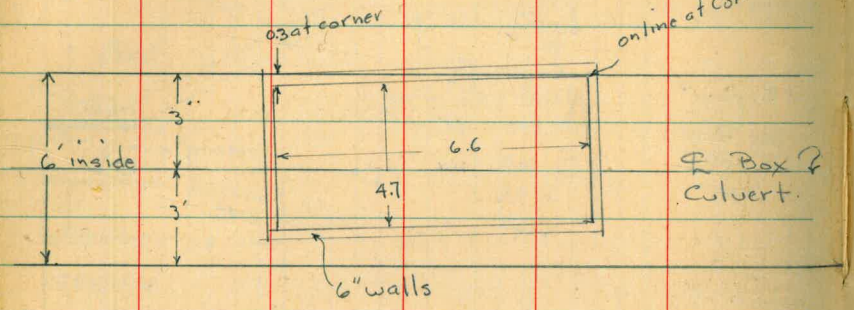
10-11-46 # 496
Osborne W.O. 210
Hardin
Worrell

indexed
C.S.K.

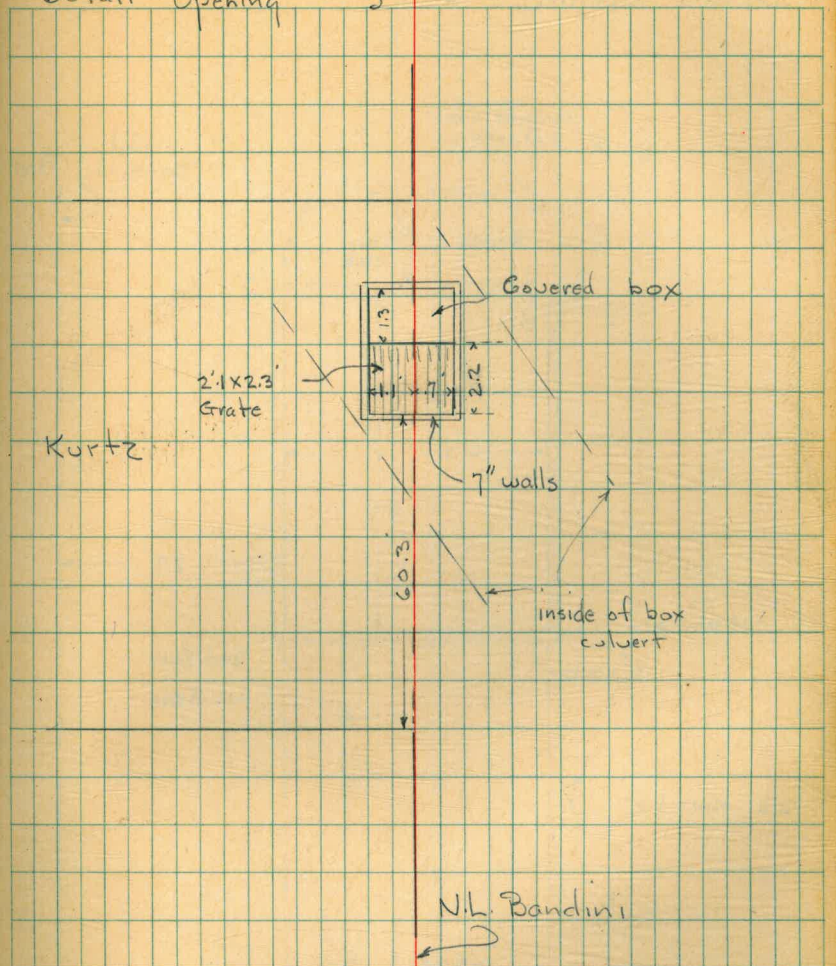
64



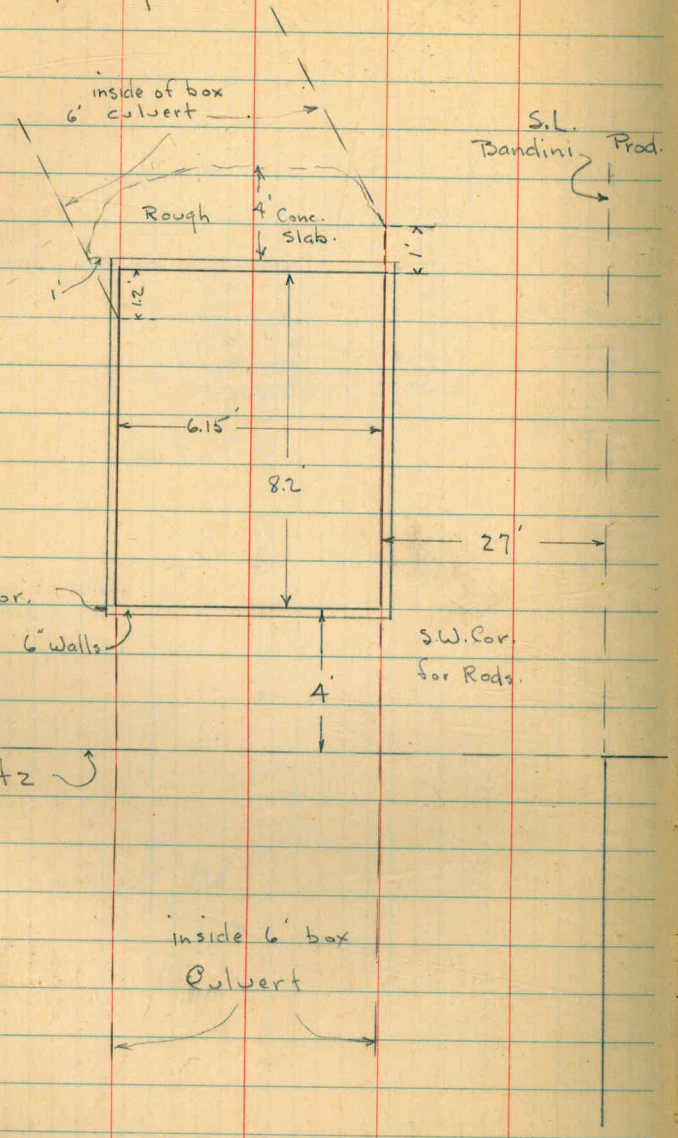
Detail Opening # 1



Detail Opening # 3



Detail opening # 4'



Levels on Openings in 6' Box Culvert on Kurtz & Bandini - See Sketch

B.M.	5.03	6.56 ✓	1.53	S.W. 9" tack Kurtz & Bandini

Opening # 1 - Elev. taken on ℄ opening unless otherwise noted.

Flow line of box Culv.	8.63	- 2.07
Top-inside of box Culv.	6.63	- 0.07
Top of walls of opening	8.16	- 1.60

Const. of opening not Completed

Opening # 2

F.L. Culvert	8.91	- 2.35
Top inside Culvert	6.91	- 0.35

No box built on opening

Opening # 3 6.56 ✓

F.L. Culvert	9.10	- 2.54
Top inside Culvert	7.10	- 0.54
Top of Grate	5.43	1.13
Top of Covered box	4.49	2.07

Opening # 4

F.L. Culvert - W. side opening	9.17	- 2.61
F.L. " - E. " "	9.17	- 2.61

Culvert 2' High inside here

Top of wall of box opening

S.W. Cor.	6.29	0.27
N.W. Cor	6.19	0.37
N.E. Cor	6.12	0.44
S.E. Cor	6.08	0.48
℄ Slab. at E. edge	6.17	0.39

C Moore
Smyn
W.?.
E.B.
10-23-42

Pav. Grades on Grape St.
Pacific to Harbor Dr.

Sta.		LT	℄	RT = N
1+60.62	E Co. drive W.O. # 58	6.21 / 3.42 ✓	6.44 / 3.19 ✓	6.32 / 3.31 / 3.33 / F 0.02
1+43.08		~~5.68~~ / out	6.47 / 3.16 ✓	5.93 / 3.70 / 4.96 / F 1.26
1+32.9	BMBP SE Belt + Grape = 5.96 / 3.67 / 9.63 = HI	5.44 / 4.19 ✓	6.45 / 3.18 ✓	5.88 / 3.75 / 4.01 / F 0.26
1+00		5.37 / 4.26 ✓	6.31 / 3.32 ✓	5.79 / 3.84 / 3.86 / F 0.02
0+55		5.28 / 4.35 ✓	6.16 / 3.47 ✓	5.65 / 3.98 / 3.86 / C 0.12
0+12	cb. E.C.			
0+00	W.L. Pacific	5.19 / 4.44 ✓	5.52	5.54 / 4.09 ✓

Indexed C.S.K.

68

3+64.13 Ely ROW Hanbon dr.

3+55.98 " " "

3

+50 H.I. 9.63

2+00

1169.39 = ~~w/ 4 Co. drive~~. Meet Ex Pav.

Lt & Rt

4.34
5.29
5.37
F 0.08

3.91
5.72
5.13
C 0.59

4.41
5.22
5.32
F 0.10

3.89
5.74
5.57
C 0.17

4.40
5.23
4.81
C 0.42

4.91
4.72
5.13
F 0.41

4.39
5.24
5.06
C 0.18

4.84
4.79
4.98
F 0.19

5.36
4.27
5.10
F 0.83

4.84
4.79
4.60
C 0.19

5.28
4.35
4.73
C 0.17

5.80
3.83
4.15
F 0.37

5.28
4.35
3.85
C 0.50

6.06
3.57 ✓

6.31
3.32 ✓

6.33
3.30
3.34
F 0.04

25' E of Ex. Pav. edge = valley gut.

3 + 84.13

3 + 74.13

3 + 73.32 Ely Row.

H.I.
9.63

Lt. | ℄ | Rt

3.37	3.30	3.23
6.26	6.33	6.40
6.51	6.51	6.74
F 0.25	F 0.18	F 0.34

3.92
5.71
5.57
C 0.14

4.19
5.44
5.45
F 0.01

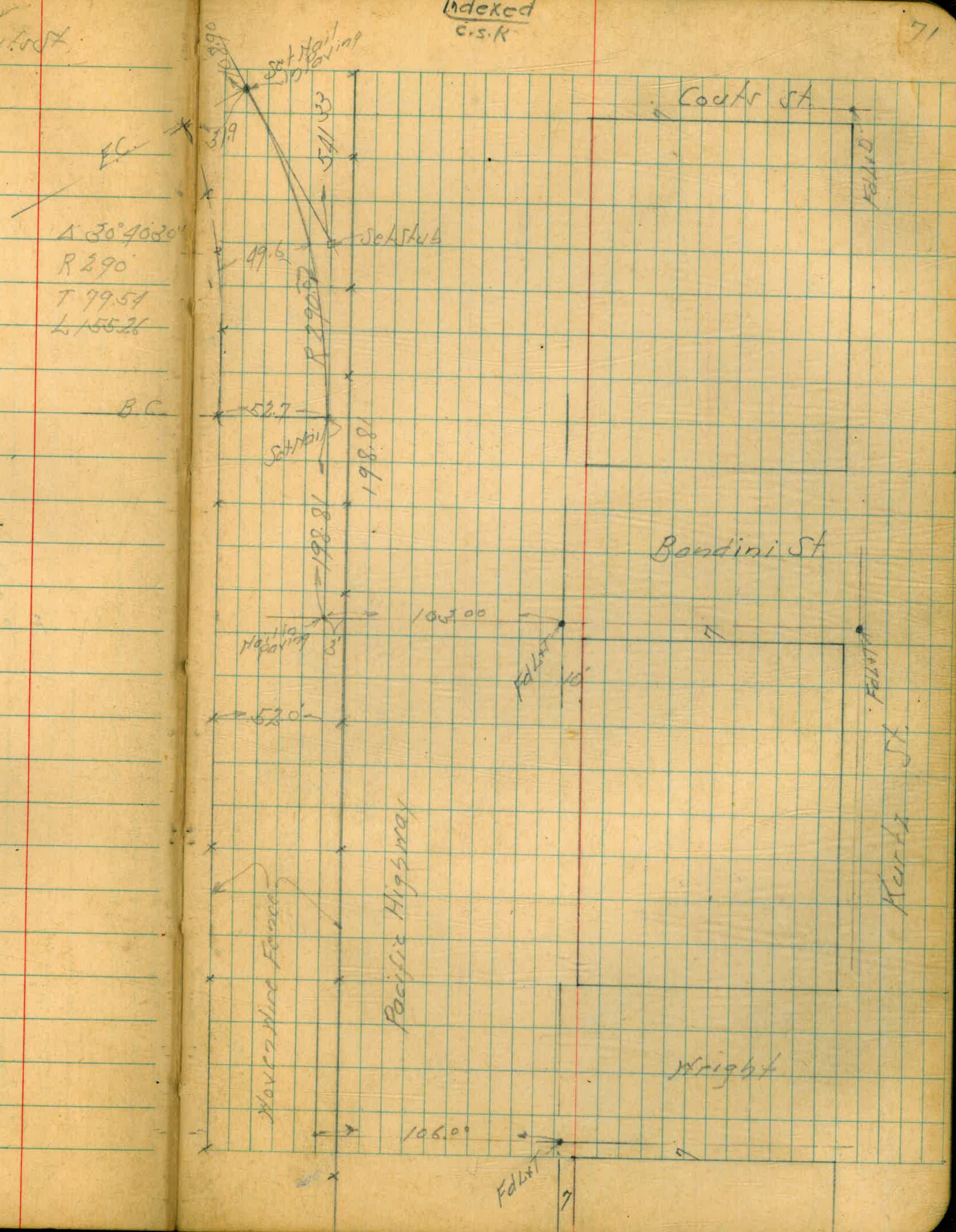
3.74
5.89
5.46
C 0.43

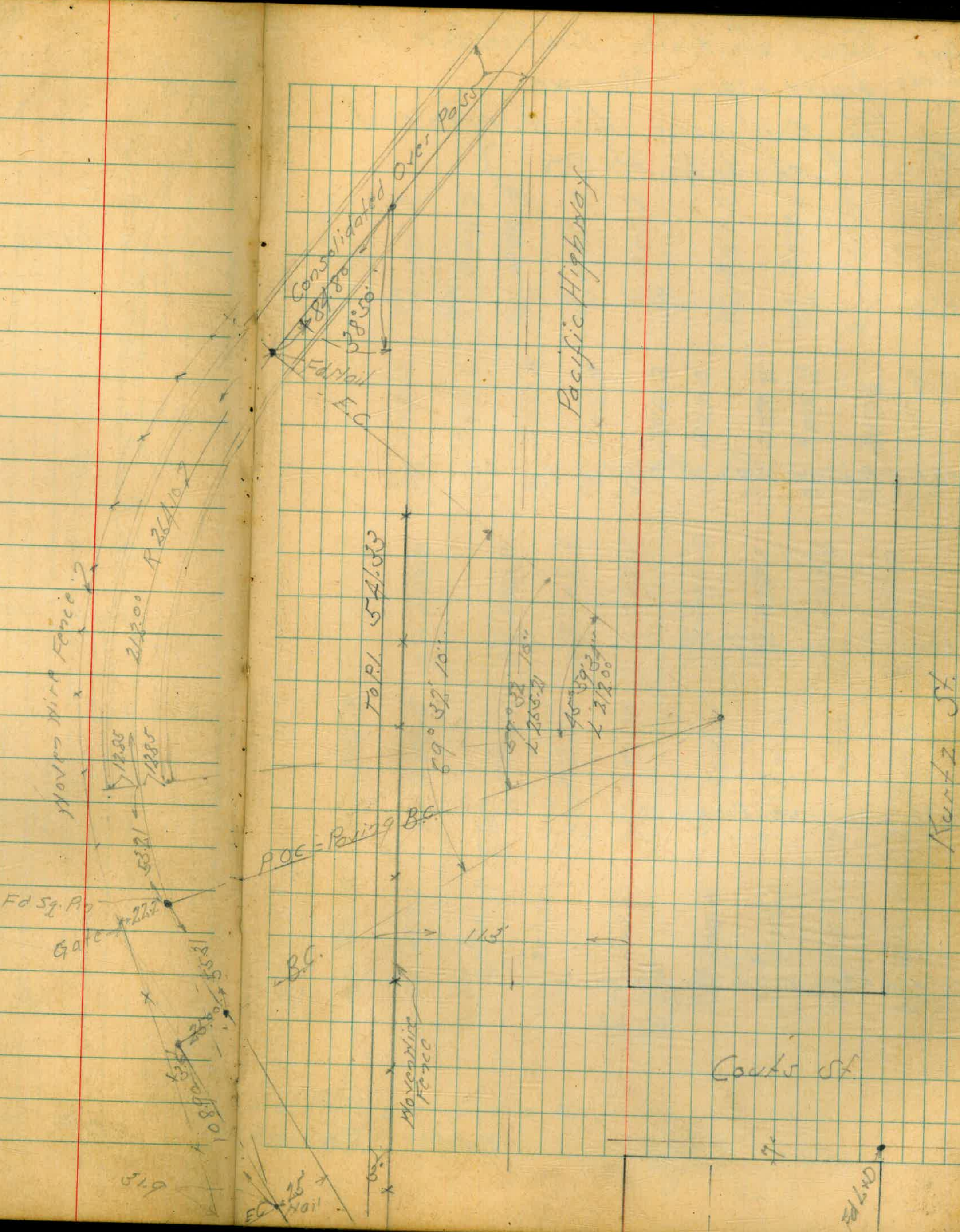
Proposed Opening Pacific Highway to Consolidated Over Pass Near Couts St.

Dec. 11-46
Sisson
McCoy
Haddel
Allen

Work Order #189

Indexed
C.S.K




Consolidated Over Pass
Fd Nail
E.C.
Pacific Highway
Woven Wire Fence
212.00
53.21
Fd Sq. Po
Gate
P.O.C. = Paving B.C.
TO P.I. 54.33
B.C.
Woven Wire Fence
EC
Nail
Kurtz St.
Couts St.

Walker
Hendricks
Becker
Johnson
6-16-47

Cross Sections - Winchester St. from Sea Breeze To East Line La Huerta Sub.
(sketch P-80)

0+50
243.1 rod 2.8 @ 45 · 243.9 rod 9.0 @ 30 · 244.7 rod 8.2 @ 20 · 245.4 rod 7.5 @ 12 · 246.0 rod 6.9 @ 9 · 246.1 rod 6.8 · 247.2 rod 5.7 @ 20 · 247.6 rod 5.3 @ 30 · 248.5 rod 4.4 @ 45

0+25 = E. Line Sea Breeze
243.5 rod 9.4 @ 45 · 244.6 rod 8.3 @ 30 · 245.3 rod 7.6 @ 20 · 245.9 rod 7.0 @ 15 · 246.2 rod 6.7 · 247.0 rod 5.9 @ 9 · 247.4 rod 5.5 @ 12 · 247.2 rod 5.7 @ 20 · 247.6 rod 5.3 @ 30 · 249.3 rod 3.6 @ 45

0+00 = ℄ Sea Breeze
243.0 rod 9.9 @ 45 · 243.9 rod 9.0 @ 30 · 244.4 rod 8.5 @ 20 · 245.8 rod 7.1 · 246.2 rod 6.7 @ 3 · 247.1 rod 5.8 @ 20 · 247.6 rod 5.3 @ 30 · 248.0 rod 4.9 @ 45

0-25 = W. Line Sea Breeze
242.9 rod 10.0 @ 45 · 243.9 rod 9.0 @ 30 · 244.11 rod 8.78 Cb. @ 20 · 243.51 rod 9.38 Gut Pav. @ 20 · 244.30 rod 8.59 Pav. · 246.0 rod 6.9 @ 7 · 246.6 rod 6.3 @ 20 · 247.0 rod 5.9 @ 30 · 247.3 rod 5.6 @ 45

0-50 = 25.0' West of W. Line Sea Breeze
240.0 rod 12.9 @ 45 · 241.4 rod 11.5 @ 30 · 243.1 rod 9.8 @ 28 · 243.32 rod 9.57 @ 20 Cb. · 242.75 rod 10.14 Gut @ 20 · 243.12 rod 9.77 SLY edge Pav · 244.4 rod 8.5 @ 4 · 245.2 rod 7.7 @ 20 · 245.7 rod 7.2 @ 30 · 246.1 rod 6.8 @ 45

252.89

8.77 252.89 244.12 B.M. N.Y.I. SEA- Ld Plg. (Water Service Plg) BREEZE And Winchester.

Winchester St.

X-Sections

2+50				
2+25				
2+00				
T.P.	12.99	260.20	5.68	247.21
1+50				
1+11				
1+00		252.89		

	Lt.			℄			Rt.	
		251.4			250.8			250.3
	8.8 45			9.4 30			9.9 45	
		250.0			249.3			249.4
	9.7 45	10.2 30		10.9 28			10.8 45	
250.5'		248.2			247.7			247.6
11.7 45		12.0 30		12.5 27			12.8 30	12.6 45
	245.8		245.6			245.4		
	7.1 45		7.3 30			7.5 20		
		244.3			244.4			244.2
	8.6 45		8.5 30		8.0 26		8.7 45	
		244.4			244.9			245.2
	8.5 30		8.0 26		7.7 20		7.4	
		245.5'			245.3			246.0
	7.4 7		7.6 8		6.4 10		5.8 20	
		247.4			247.3			246.6
	5.6 30		4.3 45					

260.30
245.9
7.0

252.89

Winchester Street
X-Sections

4+00				
T.P.	2.98	262.92	0.26	259.94
3+50				
3+30				
3+00				
2+88				
2+67		260.20		

Lt. ℄ Rt.

260.1	261.3	261.6	261.8	261.7	261.8	262.5	263.1	263.3	263.0	
9.8 45	8.6 30	8.3 20	8.1 9	8.0	8.1 6	7.4 9	6.8 20	6.6 30	6.1 45	
				259.92						
258.2	258.7	259.1	259.5	259.3	259.3	258.7	258.0	258.0	259.2	
2.0 45	1.5 30	1.1 24	0.7 20	0.9	0.9 8	0.5 10	0.4 20	0.1 30	1.0 45	
256.4	256.4	257.1	257.9	257.9	258.2	258.0	257.6	257.4		
3.8 45	3.8 30	3.1 20	2.3	2.3 7	2.0 9	2.2 20	2.6 30	2.9 45		
254.4	254.7	255.2	255.2	255.9	257.4	257.0	255.7	254.3		
5.8 45	5.5 25	5.0 20	4.3	4.3 6	2.8 10	3.2 20	4.5 30	5.9 45		
253.3	253.7	253.7	254.3	254.2	255.2	255.3	254.5	253.2		
6.9 45	6.5 30	6.5 20	5.9	6.0 6	5.0 10	4.9 20	5.7 30	7.0 45		
251.8	251.9	251.8	252.0	251.7	251.2	251.3				
8.4 45	8.3 30	8.4 20	8.2	8.5 20	7.0 30	8.2 45				

260.20

Winchester Street
X-Sections

5+30 = Beg. Wire Fence 21' Lt

6+64 = End Wire Fence 25' Lt

Station										
5+25.84	267.5 (2.4 / 30)	267.3 (2.6 / 20)	266.8 (3.1 / 13)	266.2 (3.7 / 8)	265.9 (4.0)	265.9 (4.0 / 4)	266.1 (3.8 / 8)	266.3 (3.6 / 11)	265.6 (4.3 / 20)	265.1 (4.8 / 30)
5+15.84	266.7 (3.2 / 30)	266.6 (3.3 / 20)	266.3 (3.6 / 13)	265.9 (4.0 / 8)	265.6 (4.3)	265.6 (4.3 / 3)	266.0 (3.9 / 9)	265.5 (4.4 / 20)	265.3 (4.6 / 30)	
4+95.84	265.6 (4.3 / 30)	265.7 (4.2 / 20)	265.9 (4.0 / 13)	265.5 (4.4 / 8)	265.2 (4.7)	265.5 (4.4 / 8)	265.3 (4.6 / 20)	265.0 (4.9 / 30)		
4+75.84	264.4 (5.6 / 30)	264.6 (5.3 / 20)	264.5 (5.4)	264.4 (5.5 / 15)	264.7 (5.2 / 20)	264.5 (5.4 / 30)				
4+65.84	263.6 (6.3 / 30)	263.9 (6.0 / 20)	264.1 (5.8)	264.1 (5.8 / 7)	264.7 (5.2 / 10)	264.7 (5.2 / 20)	265.0 (4.9 / 30)			
4+40.84	262.0 (7.9 / 45)	262.4 (7.5 / 30)	262.2 (7.7 / 20)	263.1 (6.8 / 9)	263.0 (6.9)	263.3 (6.6 / 7)	263.7 (6.2 / 12)	264.0 (5.9 / 20)	264.1 (5.8 / 30)	265.5 (4.4 / 45)

269.92

269.92

Winchester St.
X-Sections

↑ Cont. p-78

T.P.	3.74	262.43	11.23	258.69

Station												
6+60.86 = Sub. Line	269.6 0.3	268.0 1.9/30	267.2 2.7/20	266.6 3.3/13	265.5 4.4/9	265.2 4.7	265.4 4.5/7	264.2 5.7/13	263.5 6.4/20	262.6 7.3/30	261.6 8.3/45	
6+30.84	269.6 0.3/45	268.5 1.4/30	267.5 2.4/20	266.8 3.1/13	265.8 4.1/9	265.4 4.5	265.3 4.6/7	264.6 5.3/11	263.9 6.0/20	263.1 6.8/30	261.9 8.0/45	
6+00	270.0 +0.1/45	269.3 0.6/30	268.6 1.3/20	267.9 2.0/12	266.6 3.3/8	266.1 3.8	266.2 3.7/7	264.3 5.6/20	263.5 6.4/30	262.1 7.8/45		
5+75	269.8 0.1/45	269.3 0.6/30	269.2 0.7/20	268.6 1.3/13	267.5 2.4/8	266.7 3.2	266.7 3.2/3	266.9 3.0/5	266.5 3.4/10	265.3 4.6/20	264.0 5.9/30	263.0 6.9/45
5+50.84	268.9 1.0/45	268.6 1.3/30	268.5 1.4/20	267.8 2.1/11	267.1 2.8/8	266.7 3.2	266.6 3.3/4	266.8 3.1/61	266.3 3.6/13	265.4 4.5/20	264.6 5.3/30	263.7 6.2/45

269.92

269.92

Walker
Hendricks
Becker
Johnson
6-17-47

Cross Sections
Calle Gavioto St.
from Calle Adelfa to North end
(Sketch P. 80)

Sta.				
1+75				
T.P.	11.34	269.47	4.30	258.13
1+50				
1+00	all on Natural Ground			
0+50.17				
0+25.15 = N Line Calle Adelfa St				
0+00 = Subdivision Line	↑ from P-77 262.43			

Sta.	Lt						℄				Rt.	
1+75		262.7 (6.8/45)	261.2 (8.3/30)	260.4 (9.1/20)	259.9 (9.6/9)	259.1 (10.4/7)	258.6 (10.9)	257.9 (11.6/10)	255.9 (13.6/20)	255.3 (14.2/30)	254.2 (15.3/50)	
1+50	260.8 (1.6/45)	259.4 (3.0/30)	258.7 (3.7/20)	258.2 (4.2/15)	257.5 (4.9/13)	256.7 (5.7/8)	256.2 (6.2/6)	269.47 256.1 (6.3)	256.0 (6.4/5)	254.6 (7.8/20)	253.9 (8.5/30)	252.4 (10.0/50)
1+00	258.8 (3.6/45)	257.3 (5.1/30)	256.0 (6.4/20)	255.0 (7.4/13)	253.1 (9.3/6)	253.1 (9.3)	253.0 (9.4/5)	252.1 (10.8/11)	251.2 (11.2/30)	249.6 (12.8/50)		
0+50.17	255.8 (6.6/45)	254.2 (8.2/30)	253.6 (8.8/20)	252.6 (9.8/16)	251.9 (10.5/8)	251.2 (11.2/6)	251.2 (11.2) Nat. Ground	251.5 (10.9/16) 3' dump	252.1 (10.3/20) 2' Dump	251.0 (11.4/30) 2' dump	246.6 (15.8/45) Nat. Ground	246.1 (16.3/60) Nat. Ground
0+25.15	255.3 (7.1/45)	252.8 (9.6/30)	251.6 (10.8/19)	250.4 (12.0/14)	250.5 (11.9) Nat. Ground	251.0 (11.4/20) 4' Dump	251.3 (11.1/28) 3' Dump	250.8 (11.6/30) 4' Dump	250.2 (12.2/45) 8' Dump	245.5 (16.9/45) Nat. Ground		
0+00	255.1 (7.3/45)	252.6 (9.8/30)	251.0 (11.4/20)	250.4 (12.0/12)	250.5 (11.9) 262.43	249.8 (12.6/20) on 3' Rub	249.9 (12.5/30) on 3' of Rubbish	249.0 (12.6/45) on Rubbish Dump.	243.7 (18.7/45) Nat. Ground			

CALLE GAVIOTA

X Sections

Additional Sections FB 1762-55

Uniform Grade from 4+50 to 5+33.4

	SEA BREEZE					
Chk. S+1. B.P. Edgewater			12.39	245.18	Page 26	
T.P.	0.90	257.57	12.80	256.67		

Lt. — ℄ — Rt.

5+08
260.7 8.8 · 261.4 8.1/30 · 262.3 7.2/20 · 263.8 5.7 · 265.2 4.3/20 · 266.0 3.5/30 · 267.2 2.3/45

4+50
261.9 7.6/45 · 263.1 6.4/30 · 264.2 5.3/20 · 265.3 4.2 · 267.0 2.5/20 · 267.6 1.9/30 · 268.5 1.0/45

4+00
262.1 7.4/45 · 263.6 5.9/30 · 264.5 5.0/20 · 265.8 3.7 · 266.9 2.6/20 · 267.6 1.9/30 · 268.5 1.0/45

2+94
265.5 4.0/45 · 265.8 3.7/30 · 264.7 4.8/20 · 264.8 4.7 · 265.0 4.5/7 · 264.6 4.9/11 · 265.2 4.3/20 · 265.0 4.5/30 · 264.3 5.2

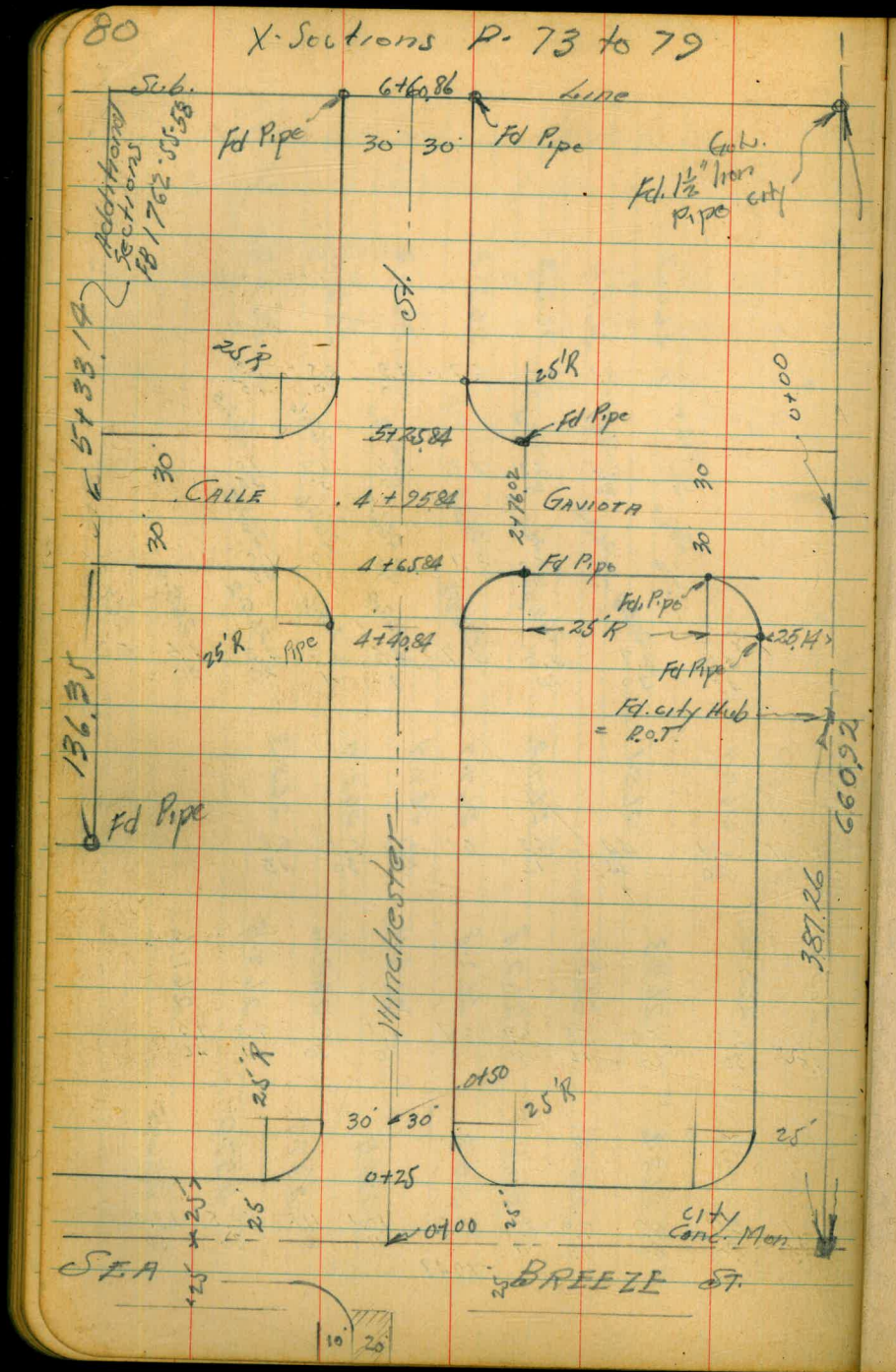
2+76.02
266.2 3.3/45 · 265.8 3.7/30 · 265.4 4.1/20 · 265.1 4.4/14 · 264.2 5.3/12 · 264.4 5.1 · 264.4 5.1/20 · 263.4 6.1/30 · 263.3 6.2/45

2+50
265.8 3.7/45 · 265.3 4.2/30 · 264.3 5.2/20 · 263.7 5.8/14 · 262.8 6.7/11 · 262.8 6.7 · 263.4 6.1/20 · 262.6 6.9/30 · 262.5 7.0/41 · 261.6 7.9/46

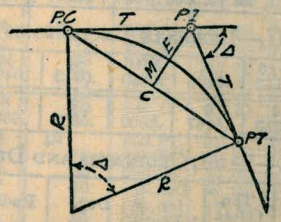
2+00
263.4 6.1/45 · 262.8 6.7/30 · 262.6 6.9/20 · 262.2 7.3/13 · 261.3 8.2/11 · 260.3 9.2 · 259.4 10.1/11 · 257.7 11.8/20 · 257.0 12.5/30 · 256.5 13.0/50

26947

26947



DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES



CURVE FORMULAS

Radius=R=$\frac{50}{\sin. D/2}$ (1) Degree of Curve=D and sin. $\frac{D}{2}=\frac{50}{R}$ (2)

Tangent=T=R tan $\frac{\Delta}{2}$ (3) Length of Curve=L=$100\frac{\Delta}{D}$ (4)

Middle ordinate=M=R(1—cos. $\frac{\Delta}{2}$) (5)=Rvers $\frac{\Delta}{2}$ (6)

External=E=T tan $\frac{\Delta}{4}$ (7)=R ÷ cos. $\frac{\Delta}{2}$—R (8)=Rexsec $\frac{\Delta}{2}$ (9)

Long Chord=C=2 R sin. $\frac{\Delta}{2}$ (10) Δ=Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. Δ=62° 10′ D=8° 20′. From Table IV for 1° curve T=3454.1 and ÷8⅓=414.49 ft. From Table V correction=.36 or T=414.85 ft. P. C.=Sta. P.I.—T=157 +45.50. Also from (4) L=746.00 and P. T.=Sta. P. C.+L=164+91.50.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset=7.27 $(54.50 \div 100)^2$=2.16 ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26)$=2.16 ft.

Deflections.—Deflection angle=½ D for 100 ft., ¼ D for 50 ft., etc. For c ft.=(in minutes) .3 x C x D° or=defl. for 1 ft. from Table III x C. For Sta. 158 of above curve=.3 x 54.5 x 8⅓=136.2′ or 2° 16.2′, or=2.50 x 54.5=136.2′ from Table III. For Sta. 159 deflection angle=2° 16.2′ +8° 20′ ÷2=6° 26.2′, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve E=960.6 for 8° 20′=960.6 ÷8⅓=115.27 and from Table V correction=.10 or E=115.37 ft. Or suppose Δ=32° and E is measured and found to be 42 ft. What is D? From Table IV E=230.9 and ÷42=5.5 or D=5° 30′.

437 35
48
485.35

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)÷2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.

MADE IN U.S.A.