

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6 + (20-16) ÷ 2 or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1 1/2 see inside of back cover.

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CITY ENGINEER'S OFFICE

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

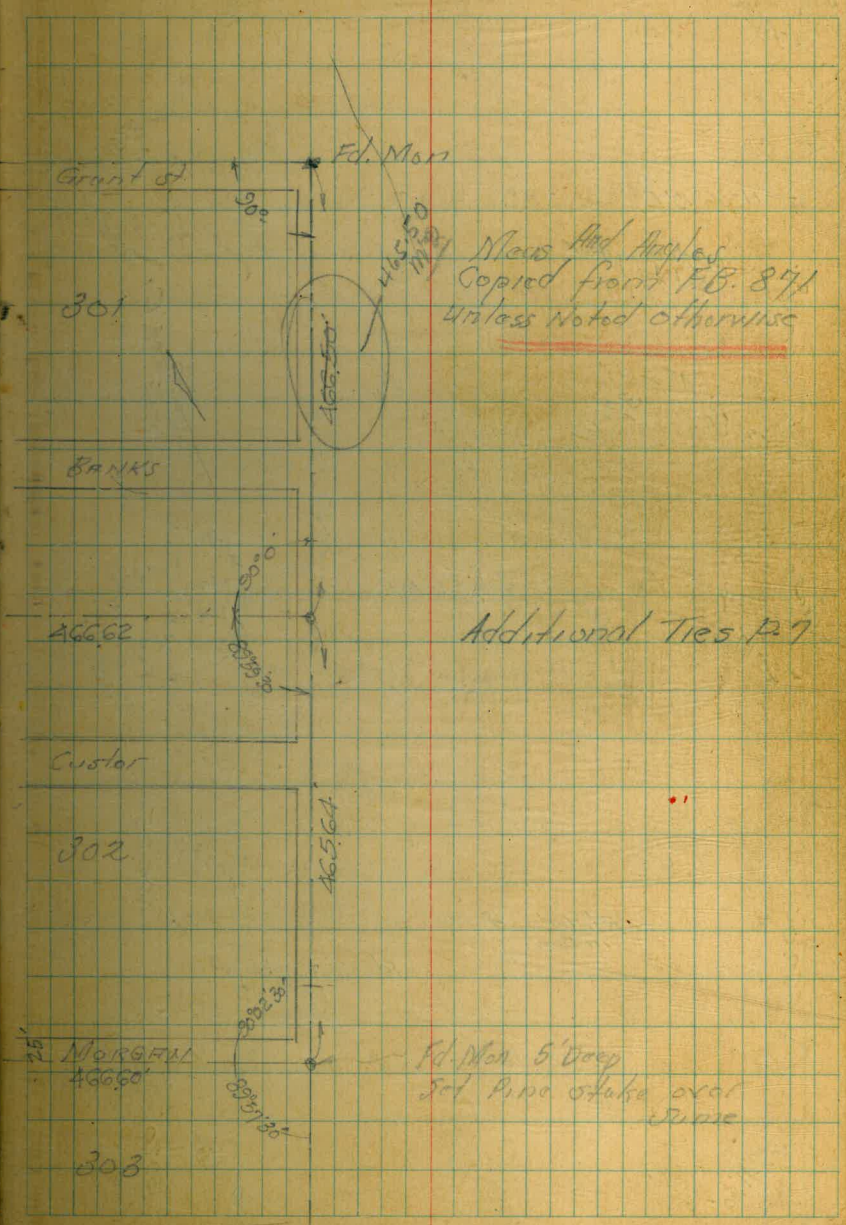
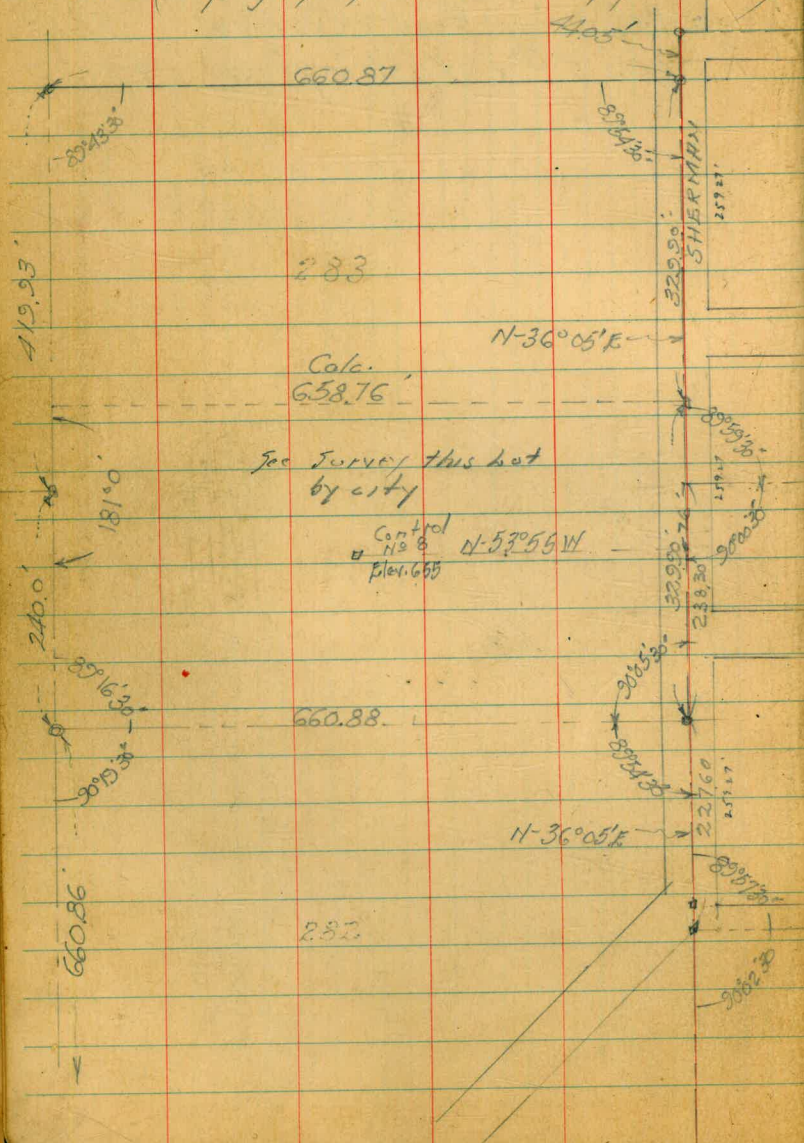
Made in U. S. A.

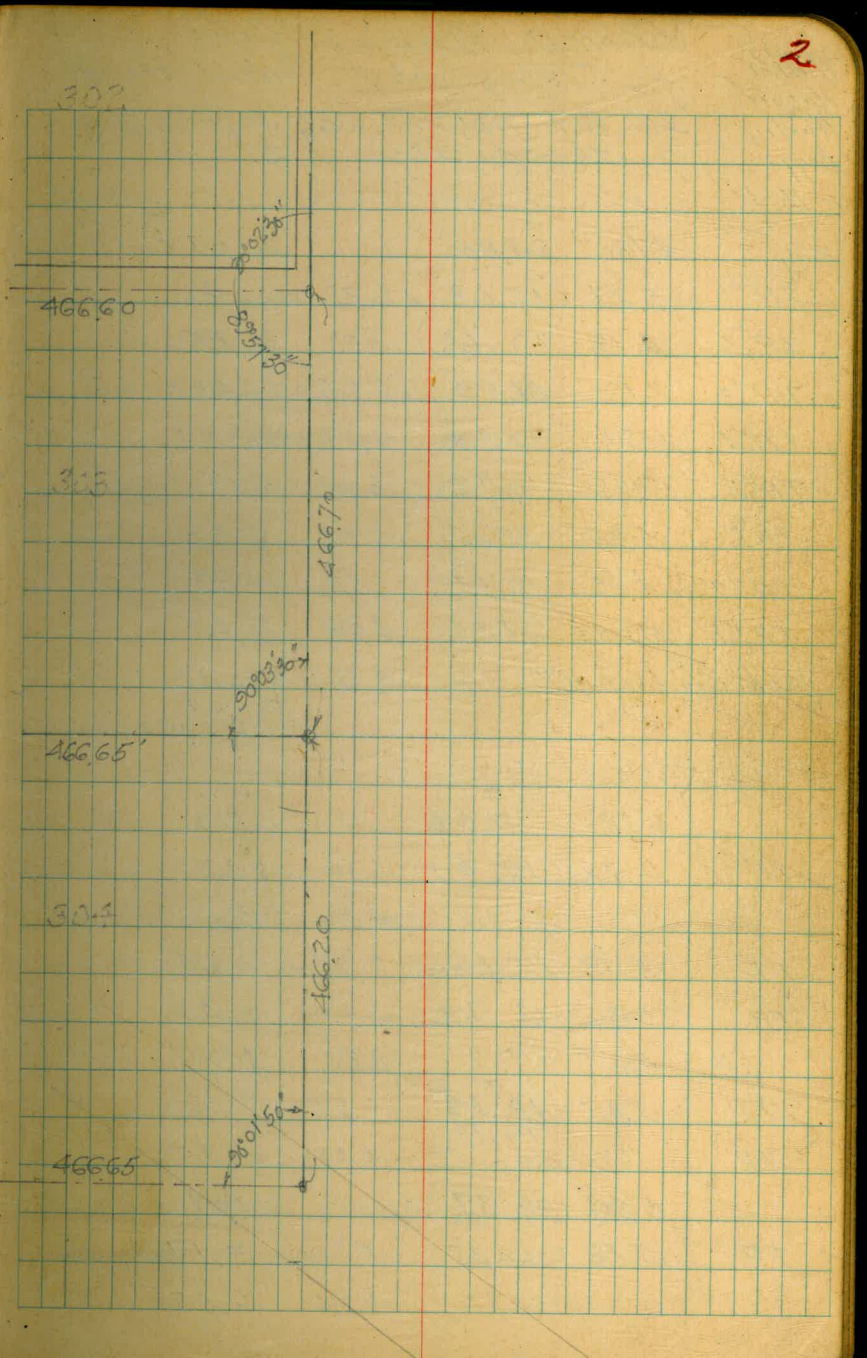
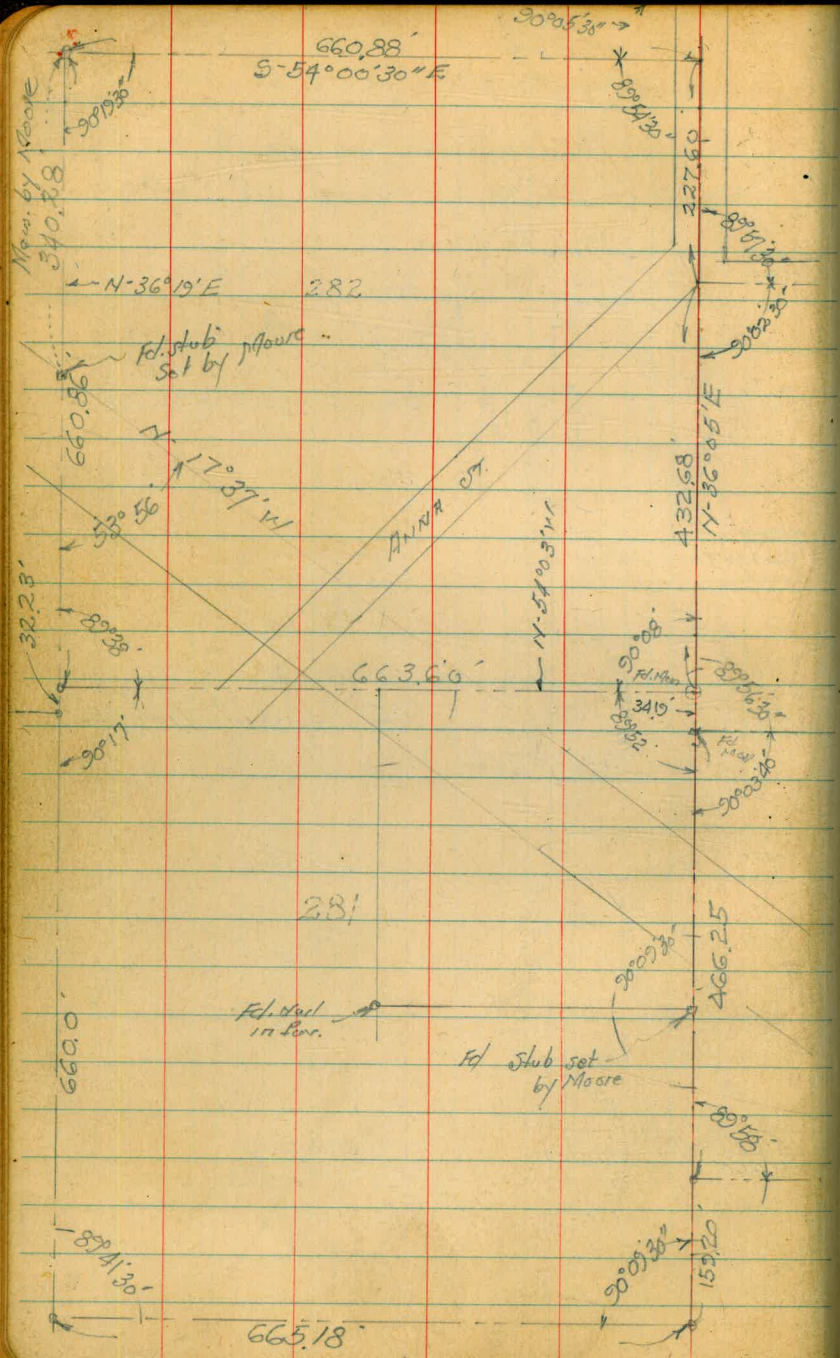
Index

Santa Barbara Place X-sec	64
Alley BIK. 108. Mission Beach	69
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X-sec. 5 th + Washington	77-79

Indexed
C.S.K.

Walker
Hazard
Hedin
8699
10-15-45
- Topography - Pueblo Lots -
Pl. 281, 282, 283, ~~301~~, 302, 303, 304.
Sketch of Control Points
(Topography on Hard Copy No. 7350)





Walker
Hazard
Hurdin
Begg

BENCH MARKS
for Topography Control Points
Dk. Lots 281, 282, 283, 301, 302, 303.
Sketch Page 1, 2.

10-15-45					B.M. B.P. Taylor's
Old Town Bridge	4.78	24.85		20.07	Steel Bridge
TP#1	5.21	17.68	12.38	12.47	
TP#2	4.78	15.13	3.33	14.35	
TP#3	2.18	14.66	6.65	12.48	
TP#4	6.51	9.80	11.37	3.29	
TP#5	7.65	19.72	6.73	3.07	
TP#6	5.85	15.65	0.92	9.80	
TP#7	4.40	18.73	1.32	14.33	
TP#8	12.51	24.86	6.38	12.35	
chk. Starting B.M.		4.76	20.10	20.07	
				0.03	Error

	6.56	9.85		3.29	
TP	6.72	10.01	6.56	3.29	
			4.20	5.1	
TP	5.68	12.16	2.97	7.04	
TP	5.26	13.73	3.59	8.47	
TP	5.2	10.1	8.82	4.91	
TP	5.2	12.36	6.57	7.16	
TP		10.10	4.25	5.85	
	5.30	8.37		3.07	
TP	5.18	12.35	1.20	7.17	
			5.80	6.55	

3

on Conc. Mason ~~SULLY~~ Cor PL 301
 " " " ~~SULLY~~ " PL 301
 on Stub NWLY " PL 301

on Mon Above SULLY PL 301

on Rock in Road 400' W of Control #1
 on Redwood Stub Control NO 2
 " " " " NO 3
 " " " " NO 4
 " " " " NO 5
 " " " " NO 6

on Above Stub NWLY Cor PL 301
 on Stub Control NO 7
 " " " " NO 8

Supplementary Topog. Notes. P.L. 281, 282, 283,
301, 302, 303.

Due to Drizzling Rain Field Mapping

Temporarily Abandoned

Az. from North Clockwise

Readings from station #7 Elevation = 7.17

Station	Az.	Stadia	Vert Δ	Horizy Dist.	Diff. Elev	True Elev.
	60°55'	88	0°			5.8
In E Road	33°40'	100'	0°			1.7
	56°05'	128	0°			1.6
	51°15'	152	0°			2.1
" " "	36°35'	164'	0°			1.6
" " "	51°15'	168'	0°			4.8
" " "	39°20'	287	0° x			7.3
	45°05'	293'	0° x			6.9
Tel. Pole	36°20'	280	0° x			7.8
	29°15'	156'	0°			3.0
Fence #1	30°15'	297	0° x			5.6
	15°20'	74	0°			1.5
" "	29°40'	2.21	0° x			2.2
" "	12°50'	64	0°			5.8
" "	27°20'	165'	0°			1.7
Tel. Pole	0°05'	30°	0°			8.0
Fence #1	27°	158	0°			1.0
Δ " #1	234°10'	86'	0°			8.1
" #1	24°35'	125	0°			3.0
Δ " #1	234°20'	137	0°			8.2

4

P.L. 301

* P.W. Cor.

P.L. 302

Elev. 6.55

Control N 28
N-53°55' W
312

Control #27
Elev. = 7.17

N-36°05' E

Station	Ry.	Stadia	VA	Hor. D.	Diff. E.
Fence #1	242°15'	146			
	345°15'	145			
Int. Fence #2					
Fence #1	348°10'	152			
	243°10'	182			
Fence #3	358°35'	181			
	1°20'	192			
Fence #2	275°30'	321			
	1°20'	198			
	302°	263			
	11°	244			
	11°	260			
	326°50'	252			
	11°30'	281			
	337°30'	252			
	340°45'	271			
	356°45'	324			
	354°40'	312			
	354°10'	298			
Fence #3	336°45'	313			
	345°15'	357			
	337°15'	313			
	346°40'	360			
	347°05'	368			
	347°05'	297			
	349°10'	242			

True Elev.

70
65
25
82
21
41
82
16
70
25 - out
61
55
67 - out
34
65
66 - out
61 - out
21 - out
41 ✓
28 - out
19 ✓
69 out
69
15 ✓
38

Station	Az.	Stadia	Horiz. D	Diff. Etc.
	342°15'	418		
	335°30'	360		
	340°40'	405		
	341°15'	393'		
10 Holo.	333°45'	357		
Cap. Fence #3	330°	392		
	331°	377'		
	324°36'	378		
	328°10'	365		
	325°	354		
	325°50'	333		
	317°10'	396		
	325°15'	317		
	317°	382'		
	316°36'	330'		
	316°45'	366'		
	317°	346'		
	313°45'	427'		
	306°	422		
	311°10'	375		
	304°45'	420		
	311°10'	351		
E 8	306°05'	312		

6

True Elev.	
64	out.
30	✓
55	- out.
38	out.
-37	
42	✓
-33	✓
50	✓
-40	✓
-17	✓
30	✓
54	✓
56	✓
09	✓
52	✓
0°	✓
31	✓
41	✓
19	✓
18	✓
65	✓
56	
65	

Tic Pts. in
Vernon Park

Indexed
C.S.R.
Plotted T.P.S. 593
8-29-47 M.M.

C. Moore 7-29-46, 5 hours
Spartan Maps
W.O. # 210
P. 899

• = set 2" Hubs & City disks

see p. 1

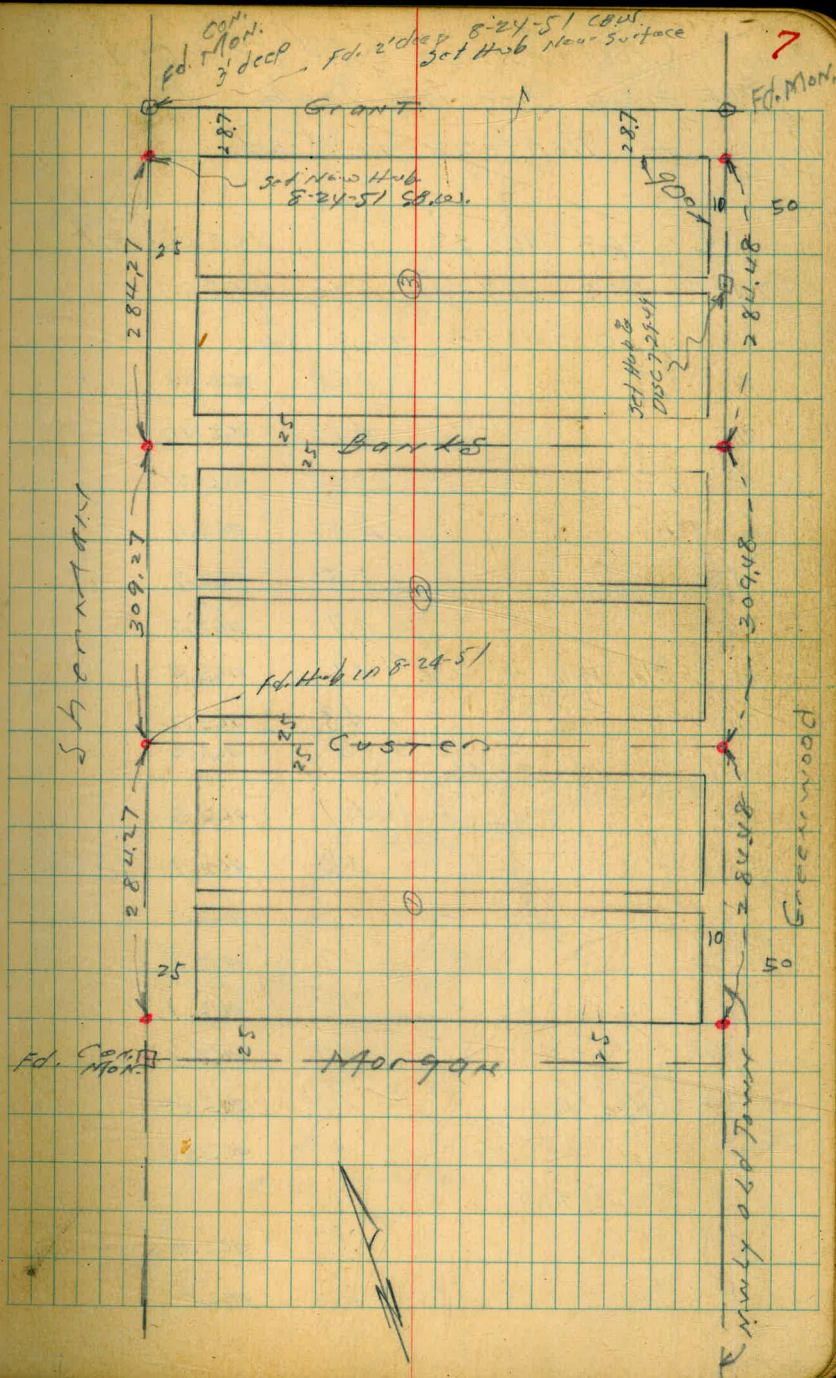
310

321

4317

5

1007

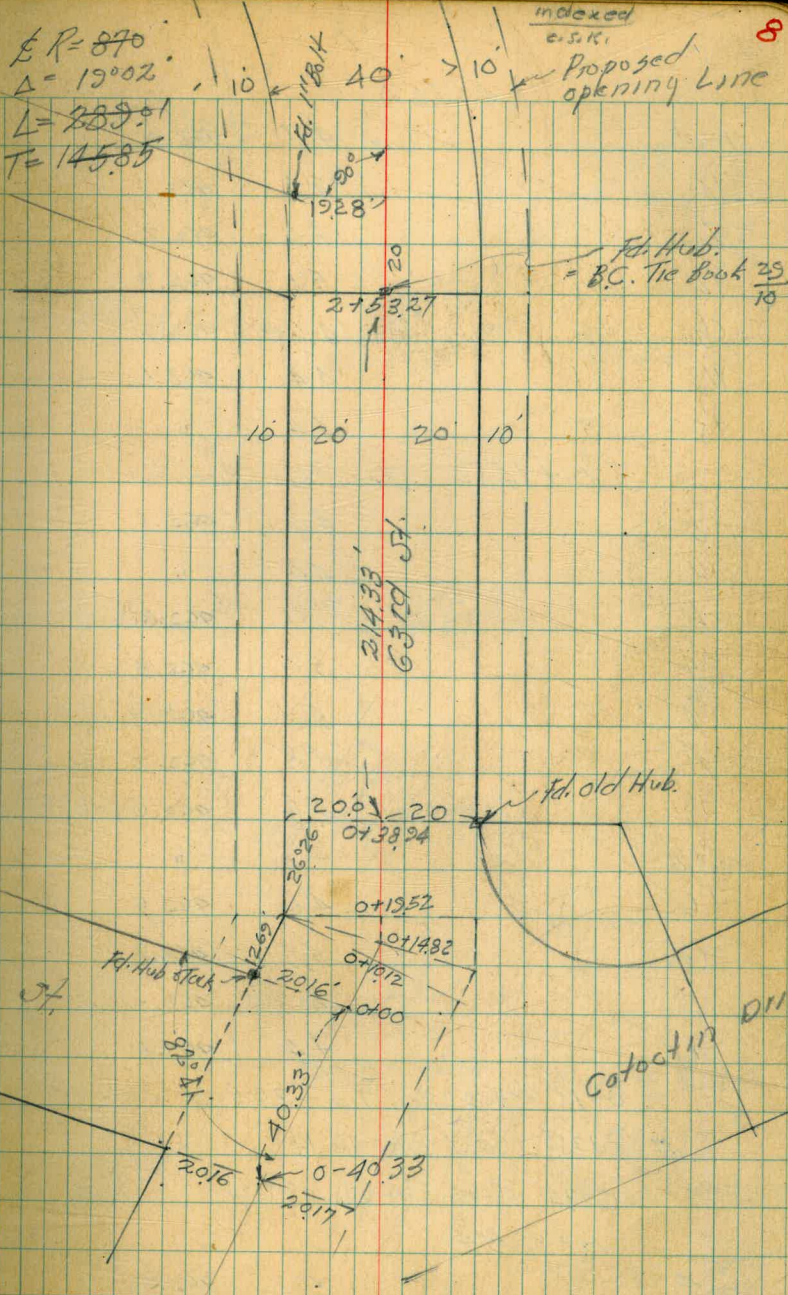


Walter Hendricks
Carey Allen
8-6-46

Cross section 6319 St. 60' wide
from Cotocotin Drive
to Montezuma Road.

BM
NW. B.P.
Cotocotin
+ El. Capon

	3.63	462.29	465.66
TR	3.23	467.52	5.00 464.29
	0 - 40.33 day Sec		
E		4.64	462.88
cb.		4.12	463.40
4		3.95	463.57
E		4.5	463.0
1/4		4.8	462.7
1/3		4.7	462.8
+6.3 = Elec. Pole		4.1	463.9
cb.		4.3	463.2
r		4.5	463.0
	0 - 20.16		
V1		4.7	462.8
cb.		4.6	462.9
1/4		4.8	462.7
E		4.7	462.8
1/4		4.4	463.1
cb.		4.2	463.3
+2 = Edge Pav		4.18	463.39
E		4.10	463.32
	0 7.00		
E-5		4.7	462.8
E		4.7	462.8



467.52

E. 6.	4.7	462.8
'14	4.6	462.9
E	4.8	462.7
'14	5.1	462.9
6.	4.6	462.9
W	4.4	463.1
±5	4.4	"

D+1482 Sec. on Bisceter

-5	4.4	463.1
'14	4.4	"
6.	4.7	462.8
+4	5.2	462.3
'14	5.1	462.9
E	4.8	462.7
	4.9	462.6
+4	4.9	"
+6	4.6	462.9
6.	4.5	463.0
E	4.3	463.2
±5	4.4	463.1

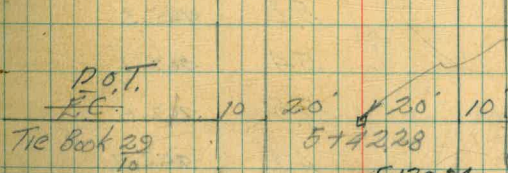
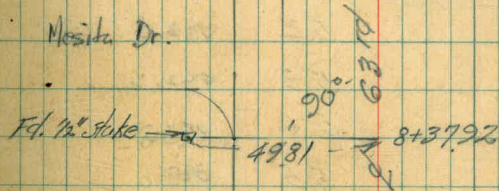
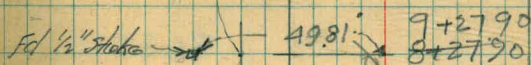
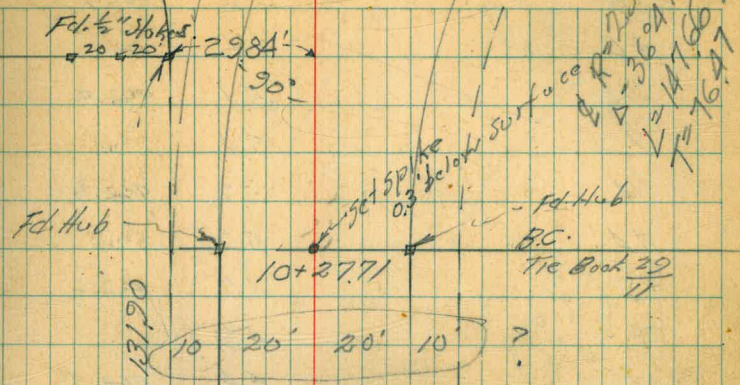
0+15 = E 8" Pop. Tree 20' R

0+255 = Guy Pole 16' R

0+34 Tel & Elec. Pole 18.1' L

0+3894

-5	5.2	462.3
E	5.0	462.5



$d.R = 890'$
 $\Delta = 19^{\circ}02'$
 $E = 2820'$
 $T = 14585'$

Make E Radius
 737.37'
 See Callwood Park

$\Delta = 19^{\circ}02'$
 $E.R = 737.37'$
 $T = 12361'$
 $L = 495.02'$

467.52

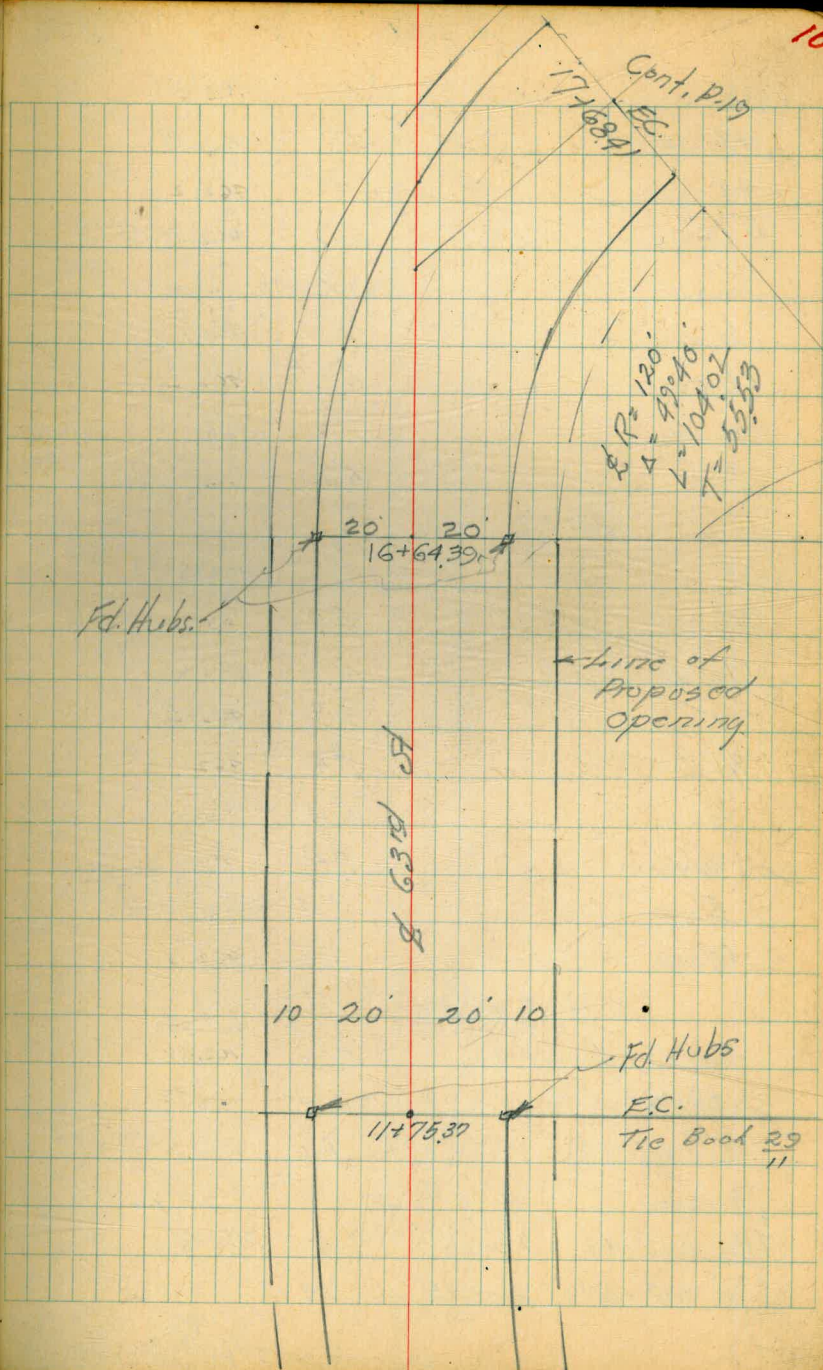
Ecb	4.6	462.9
+6	4.6	"
1/4	5.1	462.4
2	5.1	"
1/4	5.2	462.3
+4	5.2	"
+5	4.9	462.6
cb	4.9	"
W	4.4	463.1
+5	4.4	"

1+00

-5	5.0	462.5
W	5.0	"
cb	5.2	462.3
+7	5.3	462.2
+8	5.6	461.9
1/4	5.5	462.0
2	5.2	462.3
1/4	5.4	462.1
+6	5.5	462.0
+7	4.8	462.7
cb	5.0	462.5
E	5.6	461.9
+5	5.3	462.2

1+50

-5	5.8	461.7
E	5.8	"



46752 ✓

Cb	5.2	462.3
+3	5.0	462.5
+4	5.3	462.2
E 1/4	5.2	462.3
E	5.2	"
1/4	5.6	461.9
Cb	5.2	462.3
W	5.2	"
+5	5.2	"

2+00

-5	5.0	462.5
W	5.0	"
Cb	4.9	462.6
1/4	5.3	462.2
E	5.4	462.1
1/4	5.4	"
Cb	5.4	"
E	5.4	"
+5	5.5	462.0

2+14 = 8" Ac. Trac

79' Lt on Wick

2+20 = 4' Walk

2+26 = 16" Cocas Politt

2+49 16' Lt. = Elec Pole

" 16.6' R = Guy

T.P.

2.46 26689

3.09

464.43

Top Fire Hyd.

2+81 = 2 Fire Hyd 14' St.

17' Lt of E

462

462.90

468

462.89

19' Lt.

26689 ✓

2+5327 = BC Lt

-5	4.8	462.1
E	4.9	462.0
Cb	4.7	462.2
1/4	4.8	462.1
E	4.5	462.9
1/4	4.4	462.5
Cb	4.2	462.7
W	4.2	"
+5	4.2	"

3+00

-5	4.3	462.6
W	4.4	462.5
Cb	4.5	462.9
1/4	4.7	462.2
E	4.7	"
1/4	4.6	462.3
Cb	4.2	462.7
E	4.7	462.2
+5	4.7	"

3+50

-5	4.8	462.1
E	4.6	462.3
Cb	4.5	462.9
1/4	4.6	462.3
E	4.5	462.9

466.85 ✓

1/4	4.7	462.2
cb.	4.2	462.7
W	4.1	462.8
75	4.1	"
3+82.5 = Poles 17' RA = Gray 19' Lt. = Elk. Pole		
4700		

-5 4.2 462.7

W 4.4 462.5

cb. 4.8 462.1

1/4 4.8 "

E 4.5 462.4

1/4 4.6 462.3

cb. 4.6 "

E 5.0 461.9

75 5.1 461.8

4750

-5 5.4 461.5

E 5.4 "

cb. 5.0 461.9

1/4 4.9 462.0

E 4.7 462.2

1/4 4.9 462.0

cb. 5.3 461.6

W 4.9 462.0

75 4.9 "

5700

466.89 ✓

12

-5	4.9	462.0
W	4.8	462.1
cb.	5.1	461.8
1/4	5.1	"
E	4.9	462.0
1/4	5.0	461.9
cb.	4.9	462.0
E	5.4	461.5
75	5.5	461.8

5+20 = Poles 16.4 Lt 15.7 RA Gray

5742.28

-5 5.3 461.6

E 5.3 "

cb. 5.1 461.8

1/4 5.1 "

E 5.0 461.9

E on Hub. 5.15 461.79

1/4 5.1 461.8

cb. 5.2 461.7

W 5.3 461.6

75 5.3 "

6700

-5 4.7 462.2

W 4.5 462.4

cb. 4.5 "

1/4 5.2 461.7

E 5.1 461.8

466.89

+2	5.0	461.9
cb.	4.7	462.2
E	5.2	461.7
+5	5.1	461.8

6+50

-5	5.1	461.8
E	5.0	461.9
cb.	4.8	462.1
1/4	5.3	461.6
1/4	5.2	461.7
1/4	5.3	461.6
cb.	5.3	"
W	5.0	461.9
+5	5.1	461.8

5+25 = Pole 16.6' Lt.

7+00

-5	5.3	461.6
E	5.3	"
cb.	5.5	461.9
1/4	5.3	461.6
1/4	5.1	461.8
1/4	5.2	461.7
+2	4.9	462.0
cb.	5.0	461.9
E	5.5	461.9
+5	5.6	461.3

466.89

13

7+50

-5	5.4	461.5
E	5.5	461.9
+4	5.5	"
cb.	5.0	461.9
+2	4.3	462.6
+8	4.6	462.3
1/4	5.2	461.7
1/4	5.2	"
1/4	5.5	461.9
cb.	5.2	461.7
W	5.4	461.5
+5	5.6	461.3

7+67 = Pole 16' Lt.

8+00

-5	5.6	461.3
W	5.4	461.5
cb.	5.5	461.9
1/4	5.6	461.3
1/4	5.3	461.6
1/4	5.7	461.7
cb.	5.3	461.6
E	5.4	461.5
+5	5.4	461.5
-5	5.9	461.0
E	5.6	461.3

8+50

	8+50	46689		
cb			5.4	461.5
+6			5.5	461.2
1/4			5.9	461.0
E			5.6	461.3
1/4			6.0	460.9
cb.			6.1	460.8
W			5.9	461.0
+5			5.9	"
	9+00			
-5			6.5	460.9
W			6.2	460.7
cb.			6.2	"
1/4			6.0	460.9
E			5.8	461.1
1/4			5.9	461.0
+4			5.7	461.2
cb.			5.4	461.5
E			5.7	461.2
+5			5.7	"
T.P.	4.30	46547	5.72	461.17
	9+20	127'4	-pole	
	9+50			
-5			4.3	461.2
E			4.1	461.4
cb.			4.2	461.3
1/4			4.5	461.0
E			4.4	461.1

		46547		
1/4			4.8	460.7
cb			4.9	460.6
W			5.1	460.9
+5			5.2	460.3
	10+00			
-5			5.1	460.9
W			5.0	460.5
cb.			4.9	460.6
1/4			4.8	460.7
E			4.4	461.1
1/4			4.4	"
cb.			4.5	461.0
E			4.2	461.3
+5			4.3	461.2
	10+27.71	-8.6	R1	
-5			4.7	460.8
E			4.4	461.1
cb.			4.5	461.0
1/4			4.4	461.1
E			4.3	461.2
1/4			4.7	460.8
cb.			4.9	460.6
W			5.1	460.9
+5			5.1	"
	10+50			
-5			5.2	460.3
W			4.9	460.6

10+50 46547 ✓

cb.	5.0	460.5
1/4	4.7	460.8
E	4.2	461.3
1/4	4.4	461.1
cb.	4.4	"
E	4.4	"
+5	4.4	"

10+72 = Pole 14.4' RT

10+83 Fire Hyd 14' RT

on Fire Hyd. 2.61 462.86 ✓ 10+83
11+00

-5	4.5	461.0
E	4.6	460.9
cb.	4.2	461.3
1/4	4.4	461.1
E	4.2	461.3
1/4	4.5	461.0
cb.	4.4	461.1
W	4.8	460.7
+5	4.6	460.9

11+50

-5	4.5	461.0
W	4.7	460.8
cb.	4.7	"
1/4	4.6	460.9
E	4.3	461.4
1/4	4.1	461.4

46547 ✓

15

cb	4.0	461.5
E	3.5	462.0
+5	3.7	461.8
11+57.5 = A 3.5' Conc. W/LK 16.4' R		
16.4 RT. on W/LK	3.55	461.92
E " "	3.33	462.19

11+75.37 = EC.

-5	4.1	461.9
E	4.1	"
cb	4.3	461.7
1/4	4.1	461.9
E	4.3	461.7
1/4	4.7	460.8
cb.	4.9	460.6
W	4.9	"
+5	4.9	"

12+00

-5	4.8	460.7
W	4.9	460.6
cb.	4.8	460.7
1/4	4.7	460.8
E	4.4	461.1
1/4	4.3	461.2
cb.	4.1	461.9
E	4.1	"
+5	4.1	"

46547 ✓

11491 to 12466 = fence on 3.5' wire 20.3' Rt

12+10 = 24" Olive tree on 12.6' Rt

+15 = Pole 16.2' Lt.

12+34 = 24" Olive 12.8' Rt.

12+50

-5	4.0	461.5
E	4.0	"
cb.	4.0	"
1/4	4.4	461.1
1/2	4.4	"
1/4	4.7	460.8
cb.	4.8	460.7
W	4.6	460.9
+5	4.8	460.7

12+58 = 24" Olive 13.4' Rt

13+00

-5	4.8	460.7
W	4.8	"
cb.	4.9	460.6
1/4	4.8	460.7
1/2	4.6	460.9
1/4	4.4	461.1
cb.	4.4	"
E	4.5	461.0
+5	4.5	"

13+07 = 18" Olive 13' Rt.

13+32 " " "

46547 ✓

13+50

J	4.3	461.2
E	4.4	461.1
cb.	4.4	"
1/4	4.5	461.0
1/2	4.3	461.7
1/4	4.7	460.8
cb.	5.0	460.5
W	4.6	460.9
+5	4.5	461.0

13+56 = 18" Olive Tree 12.5' Rt.

13+67 16.2' Lt. = Pole

13+81 24" Olive 12.2' Rt.

+94 & 25' Conc. Walk on Rt. 19.5'

E line on Walk 3.70 461.77

14+00

J	4.4	461.1
W	4.4	"
cb.	4.7	460.8
1/4	4.6	460.9
1/2	4.4	461.1
1/4	4.3	461.2
cb.	4.2	461.3
E	4.0	461.5
+5	3.9	461.6

14+04 24" Olive T 13' Rt.

+28 " " "

465.47 ✓

14+50

-5	4.5	461.0
F	4.4	461.1
cb	4.4	"
1/4	4.5	461.0
2	4.3	461.2
1/4	4.6	460.9
cb	4.6	"
1/4	4.5	461.0
+5	4.5	"

14+52 = 10" Olive 13' RH

+76 12" " 13' "

15+00

-5	4.6	460.9
W	4.5	461.0
cb	4.5	"
1/4	4.7	460.8
2	4.4	461.1
1/4	4.6	460.9
cb	4.4	461.1
E	4.4	"
+5	4.4	"
T.P.	4.34	461.13

404 465.17

15+01 10" Olive Tree 13' RH

+18 Pole 16' Lt.

+24 12" Olive Tree 13A' RH

465.17 ✓

17

15+47 10" Olive 13.5' RH

15+50

-5	4.4	460.8
E	4.4	"
cb	4.2	461.0
1/4	4.6	460.6
2	4.2	461.0
1/4	4.4	460.8
cb	4.6	460.6
W	4.8	460.9
+5	5.0	460.2

15+71 12" Olive 14' RH

16+00

-5	4.5	460.7
W	4.7	460.5
cb	4.9	460.3
1/4	5.1	460.1
2	4.9	460.3
1/4	4.9	"
cb	4.8	460.2
E	5.1	460.1
+5	5.2	460.0

16+42 = 16" Olive 14.5' RH

16+64.39 = B.C. RH

-5	6.4	458.8
E	6.2	459.0

T 465.17 ✓

15+47: 10" Olive Tree 13.5' Rt.
16+64.39 Cont.

Ecb	6.0	459.2
1/4	6.3	458.9
E	6.1	459.1
1/4	6.2	459.0
cb	5.0	460.2
W	5.6	459.6
+5	5.8	459.9

16+66 = 16" Olive 14.5' Rt

16+86 = 18" " 13' Rt

16+90.39

-5	6.0	459.2
W	6.0	"
cb	6.2	459.0
1/4	6.3	458.9
E	6.6	458.6
1/4	6.8	458.9
cb	6.8	"
E	6.4	458.8
+5	6.7	458.5

17+16.4

-5	7.2	458.0
E	7.0	458.2
cb	6.9	458.5

465.17 ✓

18

1/4	6.9	458.3
E	7.0	458.2
1/4	6.7	458.5
cb	6.8	458.9
W	6.8	"
+5	6.8	"

17+42.4

-5	6.1	459.1
W	5.9	459.3
cb	6.7	458.5
1/4	7.1	458.1
E	7.5	457.7
1/4	7.3	457.9
cb	6.8	458.9
E	7.3	457.9
+5	7.6	457.6

17+68.41 = E.C.

-5	7.7	457.5
E	7.6	457.6
cb	7.3	457.9
1/4	7.8	457.9
E	7.3	457.9
1/4	6.9	458.8
cb	6.6	458.6
W	7.6	457.6
+5	7.4	457.8

465.17 ✓

Fire Hyd.
SE. 6 1/2 ft
Montezuma

T.P. 2.62 462.70 5.09 460.08

17+91.34 dog. Section

W	5.1	457.6
cb.	5.2	457.5
1/4	5.3	457.9
E	5.6	457.1
1/4	5.3	457.9
cb.	5.1	457.6
E	5.4	457.3

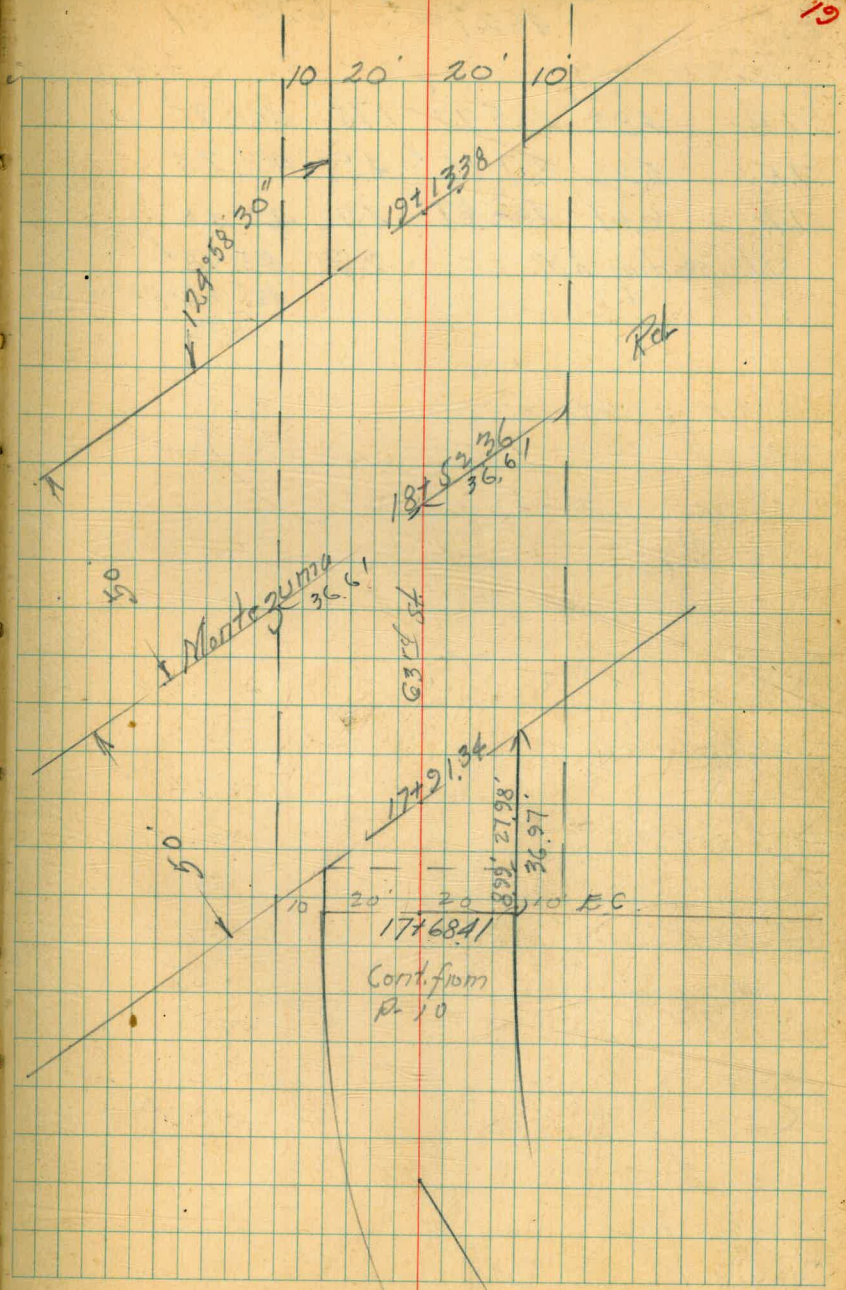
18+52.36

E	5.7	457.0
cb.	5.4	457.3
1/4	5.8	456.9
E	5.5	457.2
1/4	5.6	457.1
cb.	6.4	456.3
W	5.7	457.0

19+13.38

W	7.1	455.6
cb.	7.8	459.9
1/4	7.9	459.8
E	6.9	455.8
1/4	6.8	455.9
cb.	5.6	457.1
E	5.8	456.9

19



46270 ✓ 6319 54

20

T.P. 4.82 465.77 ✓ 175 460.95

T.P. 5.22 467.16 ✓ 453 461.24

T.P. 6.27 468.67 ✓ 476 462.48

chk. starting 8MI. 2.99 465.68 ✓
465.66-8MI-P.8
002

Milker
Hendricks
Carey
Allen
8-7-46

Curb & Paving Elevations.
Cocos Lane and College Ave

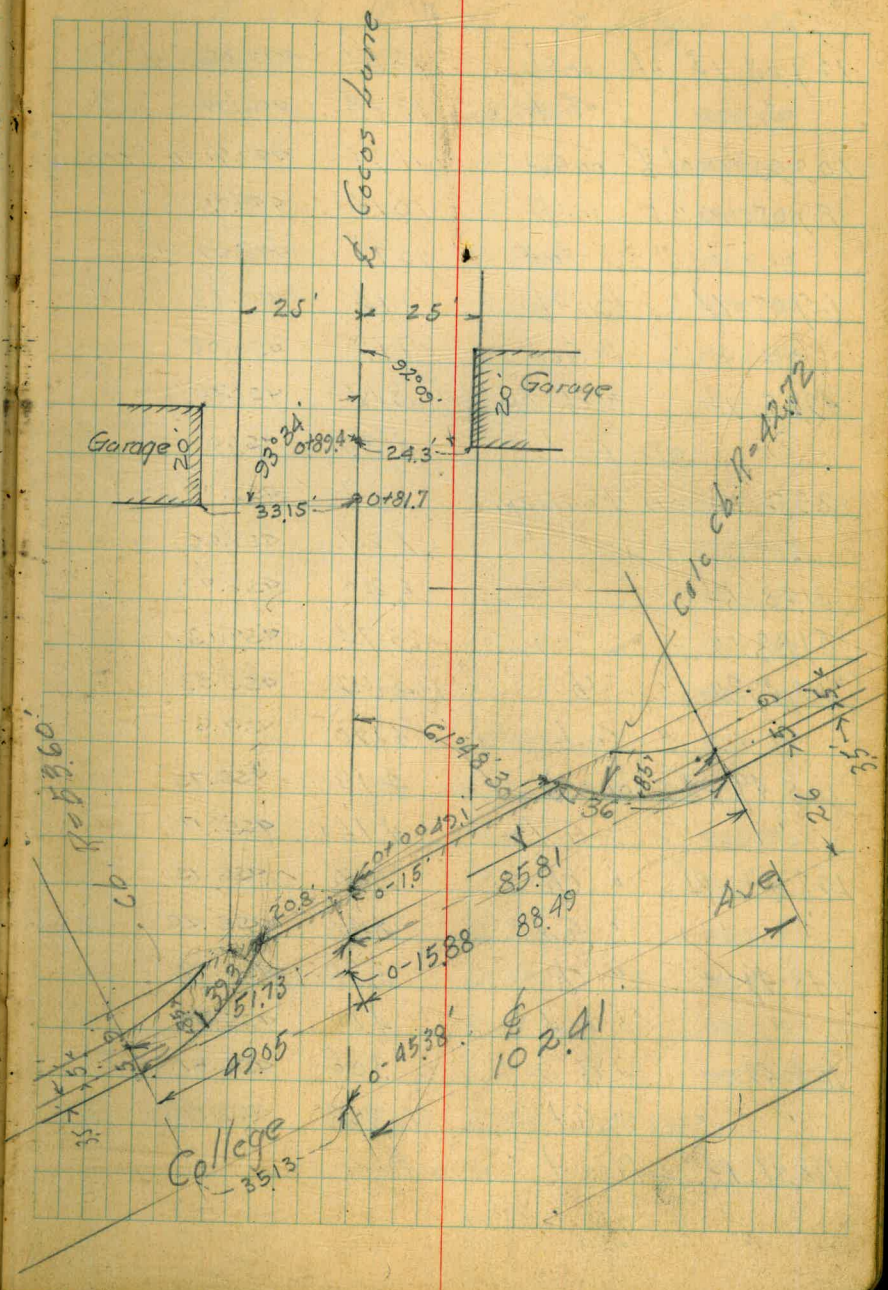
B.M.
on Fire Hpd.
P-15

	4.58	467.44	462.86	
T.P.	1.00	465.87	2.57	464.87
T.P.	6.56	459.87	12.56	453.31
0-45.38 = College				
20.241	ft of	Cocos Lane	3.28	456.59 on Pav.
18.241	"	"	3.45	456.92 "
16.241	"	"	3.76	456.11 "
14.241	"	"	4.00	455.87 "
12.241	"	"	4.43	455.94 "
10.241	"	"	4.94	454.93 "
7.38	"	"	5.44	452.93 "
4.52	"	"	6.12	453.75 "
2	"	"	7.41	452.96 "
9.26	ft	"	7.70	452.17 "
35.13	"	"	8.68	451.19 "
55.13	"	"	9.53	450.39 "
75.13	"	"	10.57	449.30 "
95.13	"	"	11.71	448.16 "
115.13	"	"	12.93	446.99 "
135.13	"	"	14.22	445.65 "

0-15.88 = E. cb line

149.05	ft of	on cb-	13.86	446.01
"	"	Gut.	14.56	445.31

indexed
E.S.K.



45987 ✓ Cocos Luma

129.05	1/4 of on cb	12.51	447.36
"	" Gut	13.13	446.74
109.05	1/4 of 1/2 on Gut	11.96	447.91 in Drive
89.05	" " " on cb	10.14	449.73
"	" Gut	10.78	449.09
69.05	1/4 on cb	9.14	450.73
"	" Gut	9.79	450.08
49.05	1/4 " cb BC	8.17	451.70
"	on Gut	8.85	451.07
23.2	1/4 on Paving	7.87	452.00
1/2	" "	7.21	452.66
31.28	1/4 " "	6.40	453.47
59.88	" " "	5.74	459.13
88.49	" " "	4.54	455.33
"	" Gut	5.20	459.67
108.49	1/4 on cb	4.12	455.75
"	" Gut	4.76	455.11
128.49	1/4 " cb	3.72	456.15
"	" Gut	4.41	455.46
148.49	" " cb	3.38	456.49
"	" Gut	4.00	455.87
168.49	" " cb	3.06	456.81
"	" Gut	3.68	456.19
188.49	1/4 left out car in Road		

45987 ✓

22

S.E. Ret 3 Parts Total cb Length = 36'

BC on Colloge		
Part 1 on cb	4.83	455.09
" " " Gut	3.46	459.91
" 2 " cb	5.12	459.75
" 2 " Gut	5.74	459.13
" 3 " cb	5.42	459.45
" 3 " Gut 15' from cb _{End}	6.07	453.80
N.E. Ret cb Length 39.3' 3 Parts		
BC on Colloge		
Part 1 on cb	7.67	457.20
" 1 " Gut	8.39	451.48
" 2 " cb	7.38	452.99
" 2 " Gut	7.94	451.93
" 3 " " 15' from End cb	7.71	452.16
" 3 on cb	7.04	452.83

0-1.5' = Edge existing Paving

10' 1/4 of 1/2 on Pav	7.45	452.42
1/2 on Pav	7.11	452.76
10' RT " "	6.90	452.97
20' " " "	6.70	453.17
30' " " "	6.46	453.41
40' " " "	6.22	453.65
TP 12.39	465.60	6.56
	453.31	

Corr. P-23

465.60 ↓

0781.7 - Garage on Lt. ⁵⁵⁵ 460.05

17017 " " Lt. ⁵⁵⁵ 460.05

0789.4 Garage on Rt. ⁴⁸⁵ 460.75

1409.4 " " ⁴⁸³ 460.77

TR 7.96 461.27 / 12.29 453.31

TR 0.31 449.53 / 12.05 449.22

TR 5.86 444.14 / 11.25 438.28

Cont. P-24

23

Walker
Hendricks
Carey
Allen
8-7-46

Levels Curb And Gutters
College And Mesita Drive

↓ from P-23
444.4

0-40 - College

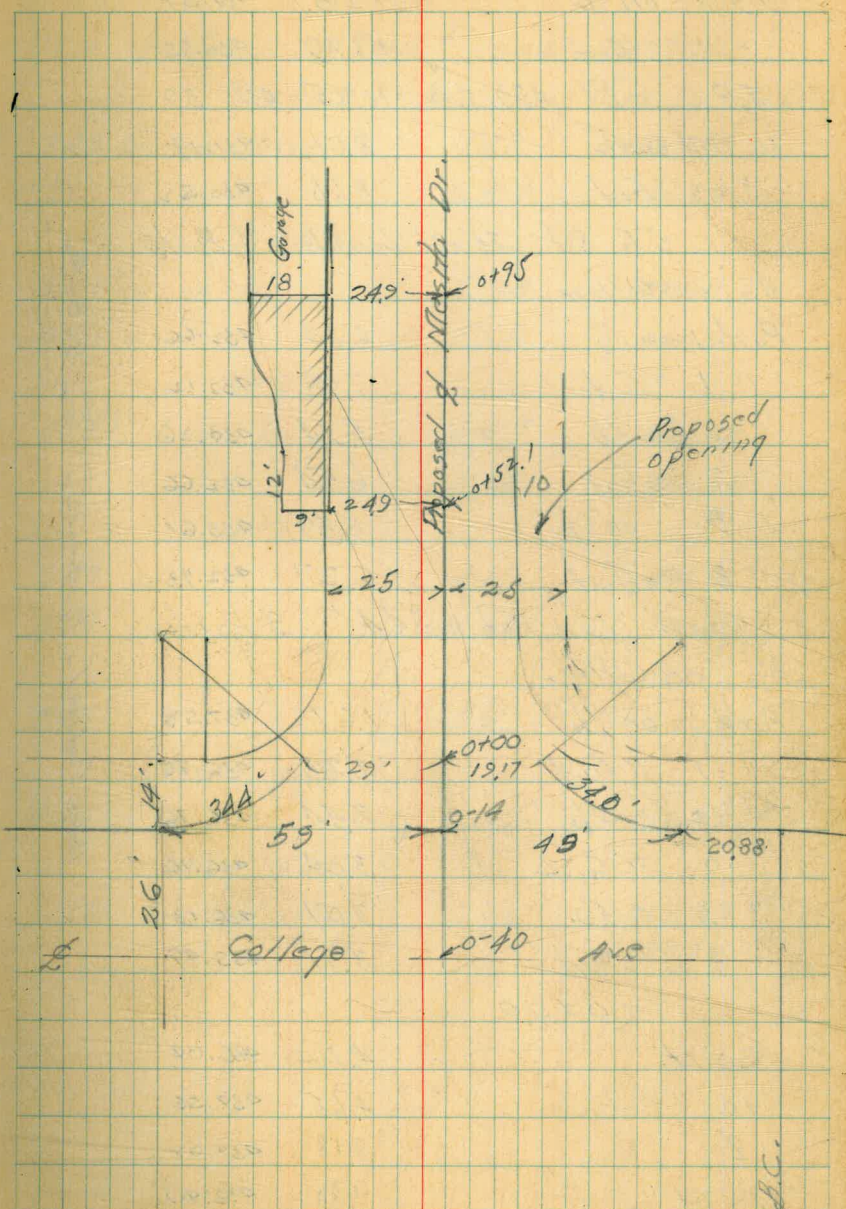
119' Lt.	2.06	442.08
99' "	3.44	440.70
79' "	4.84	439.30
59' Lt.	6.18	437.96
25' Lt.	8.48	435.66
∅	10.13	434.01
25' Rt.	11.48	432.66
49' Rt.	12.49	431.65
79' R.	13.57	430.57
109' Rt.	14.31	429.83

0-14

125' Lt on cb	1.30	442.89
" " Gut.	1.91	442.23
79' Lt " Gut in Drive	3.65	440.89
79' Lt on cb.	4.47	439.67
79' Lt " Gut	5.00	439.19
59' Lt on cb.	5.86	438.28
" " Gut.	6.48	437.66
25' Lt on Pav	8.86	435.28
∅ " "	10.27	433.87
25' Rt.	11.41	432.73
49' R. = cb BC. Ret on cb	11.89	432.25
" " Gut.	12.95	431.69

Indexed
C.S.K.

2A



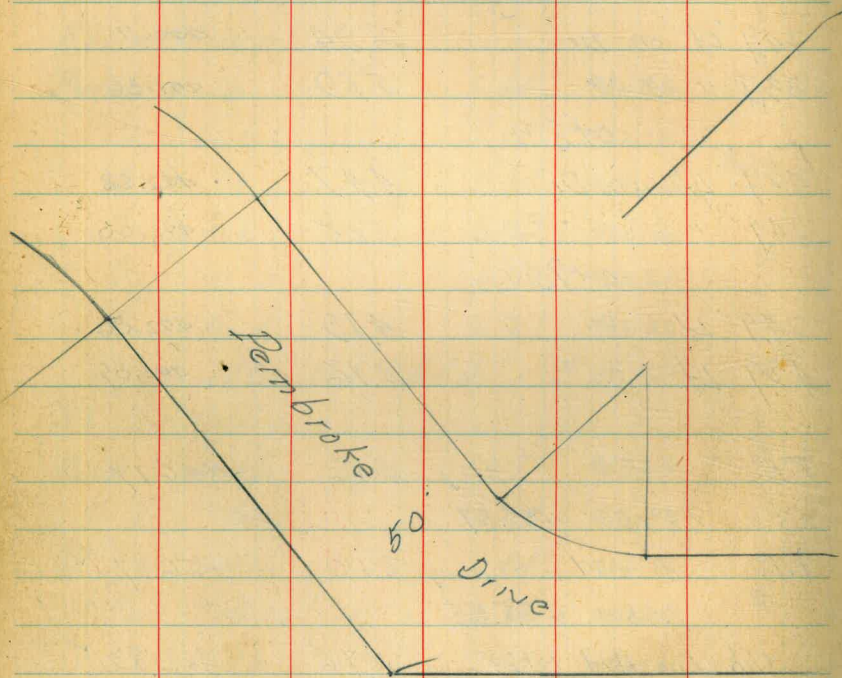
79' Rt on cb	12.57	431.57
" " " Gut	13.12	430.95
T.P. 6.81	439.20	11.75 432.39
109' Rt on cb	8.01	431.19
" " " Gut	8.68	430.52
JE Ret 34' = cb. Length, 3 Parts		
BS. on College		
Part 1 on cb	6.54	432.66
" 1 " Gut	7.08	432.12
" 2 " cb	5.94	433.26
" 2 " Gut	6.54	432.66
" 3 " on cb	5.59	433.61
" 3 " Gut	6.27	432.93
NE Ret = 344' 3 Parts		
BC on College		
Part 1 on cb	1.67	437.53
" 1 " Gut	2.25	436.95
" 2 " cb	2.44	436.76
" 2 " Gut	3.04	436.16
" 3 " cb	3.07	436.13
" 3 " Gut	3.71	435.49
0700		
20' Lt.	4.16	436.09
10 "	4.65	432.55
2	5.18	432.02
10 Rt	5.80	433.40
20 Rt		

Notes Reduced - Pg. 8425 - Pg. 8-8-96

T.P. 8.29	447.05	0.44 438.76
	0+52.1	- Beginning Conc. Dr on Lt.
249' Lt. on Drive	7.42	439.63
339 " " "	6.51	440.54
	0+62	
249' Lt. on Dr	6.94	440.11
339 " " "	5.69	441.36
	0+83	
429 Lt on Dr	4.47	442.58
249 " " "	5.05	442.00
	0+95	
249 Lt	4.19	442.86
429 Lt	4.16	442.89
T.P.	0.86	446.19
	12.18	458.37
T.P.	2.10	456.07
	9.38	465.65
chk Fire Hyd 10+83	2.76	462.89
P-15		462.86
		0.03

Walker
Hendricks
Becker
Osborne
8-30-46

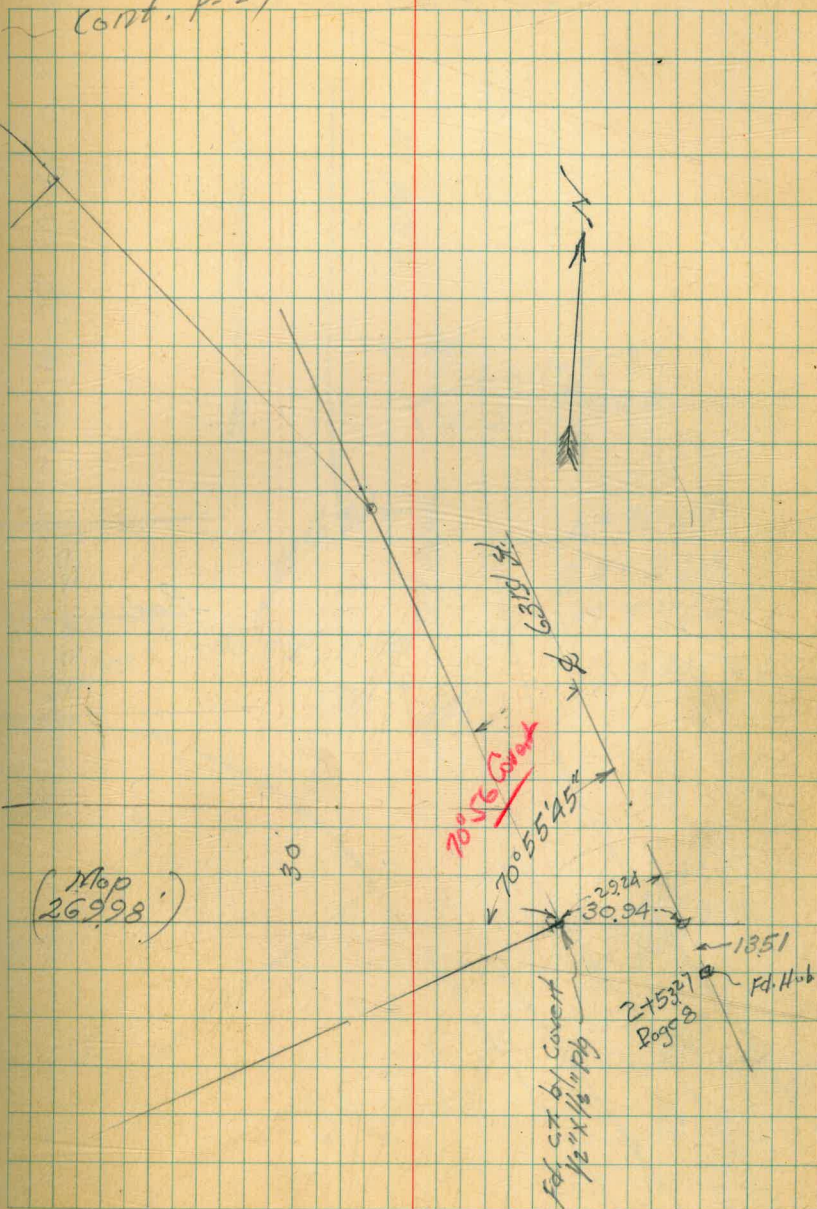
Tie to South Boundary
Collinwood Park + (3rd) St



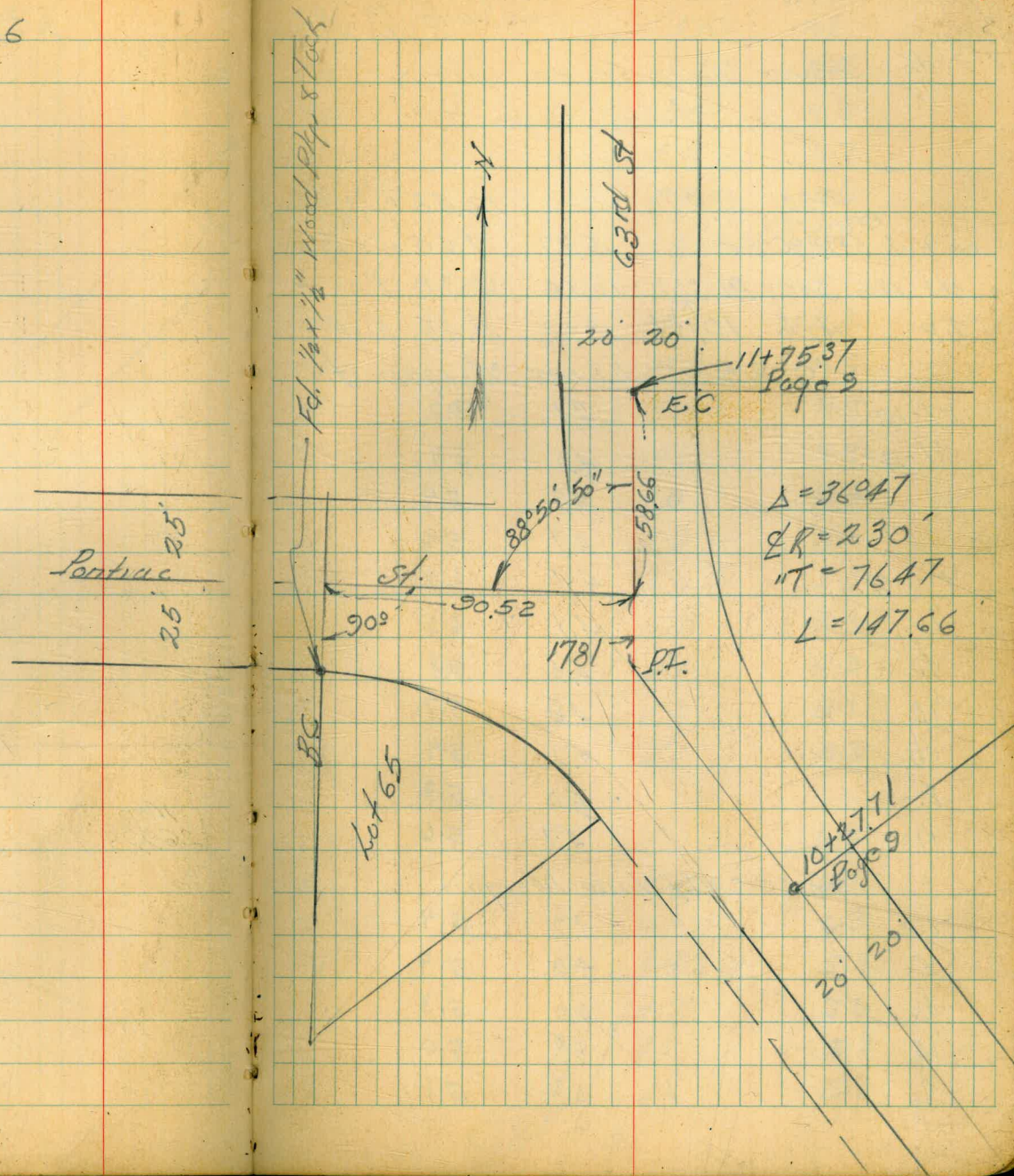
Cont. p. 27

Indexed
E.S.K.

26



Cont. from p-26



Walker
Hendricks
Secher
8-30-46

Cross Section - Greenwood St.
60' wide 10' cbs
10' 1/4s
from Morgan to Grant St.
See sketches Page 29

099 13.47 12.48
Greenwood on Hub 5+93.96 L Banks 5.87 7.60
P.M. Mon
SELY. Cor
PL. 301 - Page 3
10' FLY
of WLY Line

chk. Mon SWLY PL. 301 10.16 3.31 Page 3
T.P. 4.86 10.31 8.02 5.45 Rock

0-25 = SELY Line Morgan St.

W-10	7.1	3.2
W-4	4.9	5.4
W	4.9	5.4
+6	4.7	5.6
+10 = cb.	4.1	6.2
1/4	4.1	6.2
E	4.5	5.8
1/4	4.6	5.7
cb.	4.9	5.4
E	5.0	5.3
+10	4.7	5.6

0+00 = NLY Line Morgan

-10	4.2	5.4
E	4.9	5.4
cb.	5.0	5.3
1/4	5.3	5.0
E	5.4	5.1

10.31
0+00 Cont

Indexed
c.s. N.

28

W 1/4	5.5	4.8
cb	5.1	5.2
+5	5.8	4.5
W	5.6	4.7
+3	4.7	5.6
+12	6.5	3.8
0+50		
-10	5.1	5.2
-4	5.8	4.5
W	5.8	4.5
+3	5.9	4.4
cb.	5.0	5.3
1/4	4.9	5.4
E	5.0	5.3
E 1/4	5.0	5.3
cb.	5.1	5.2
E	5.2	5.1
+10	5.0	5.3
1+00		
-10	4.0	6.3
E	4.2	6.1
cb.	4.0	6.3
1/4	4.4	5.9
E	4.7	5.6
1/4	4.5	5.8
cb.	4.6	5.7

Cont. P-30

Walker
Headrule
Bocker

8-30-46

W.O. #230

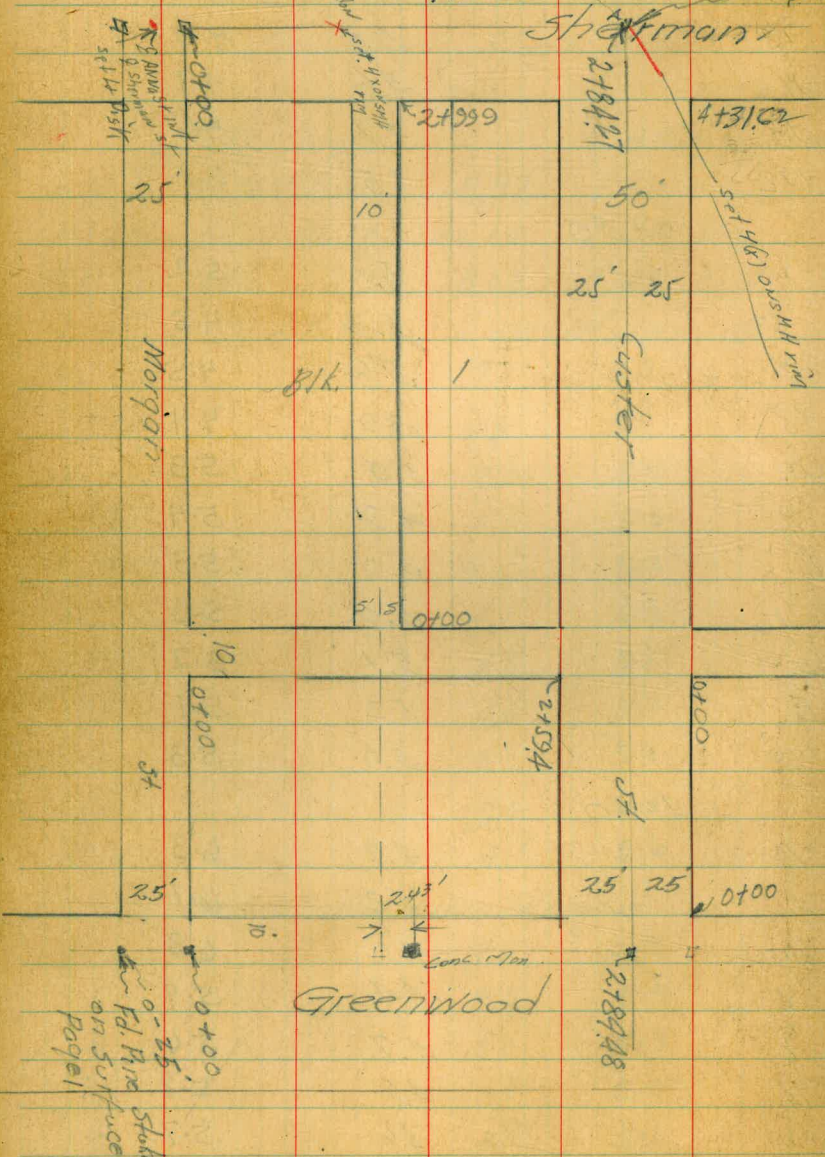
Sketch for X-Sections Sts.
Vernon Park Subdivision

Hub
Pd. 8-24-51

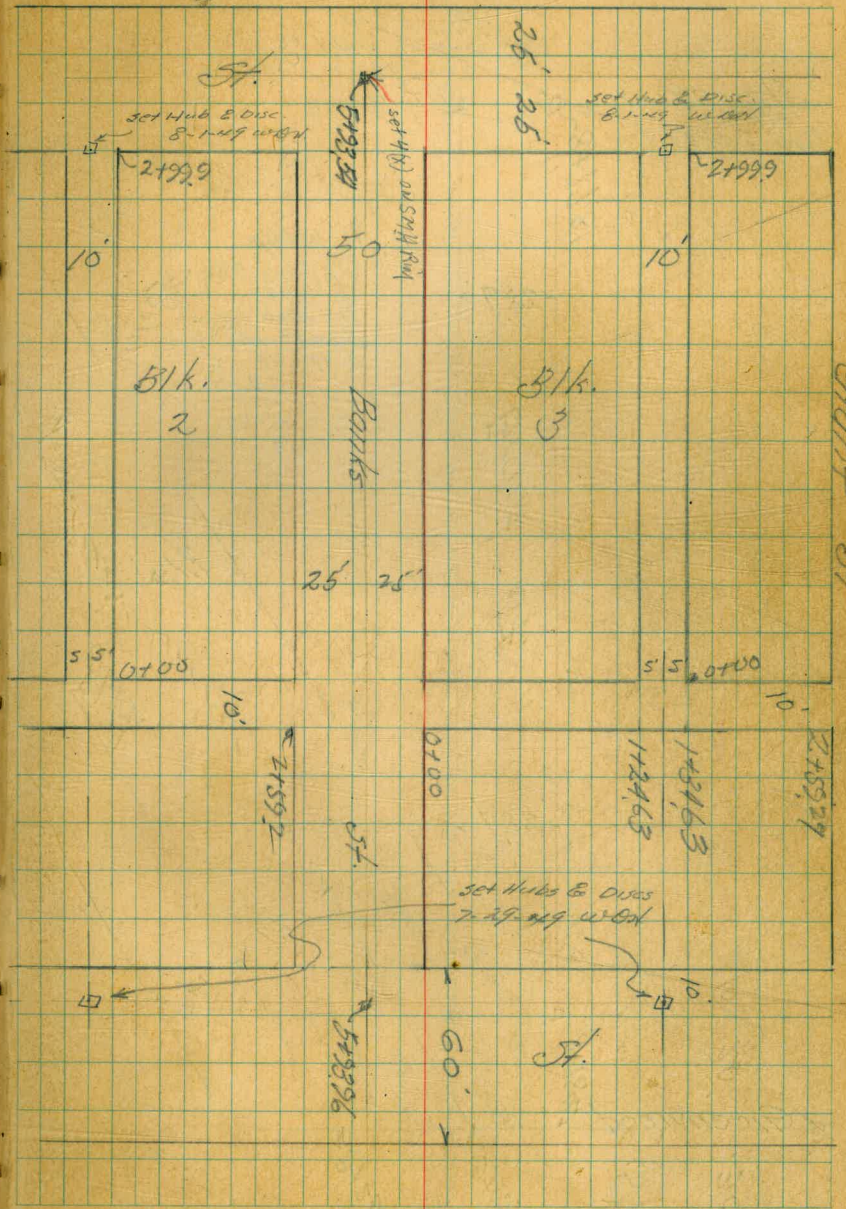
pd 7-27-49

Fd Hub
p-7

Shelton

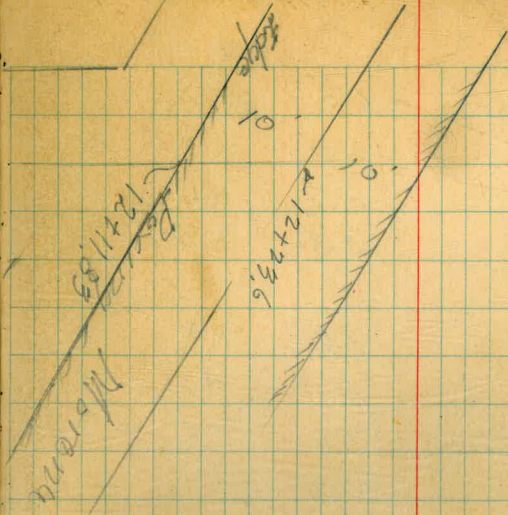
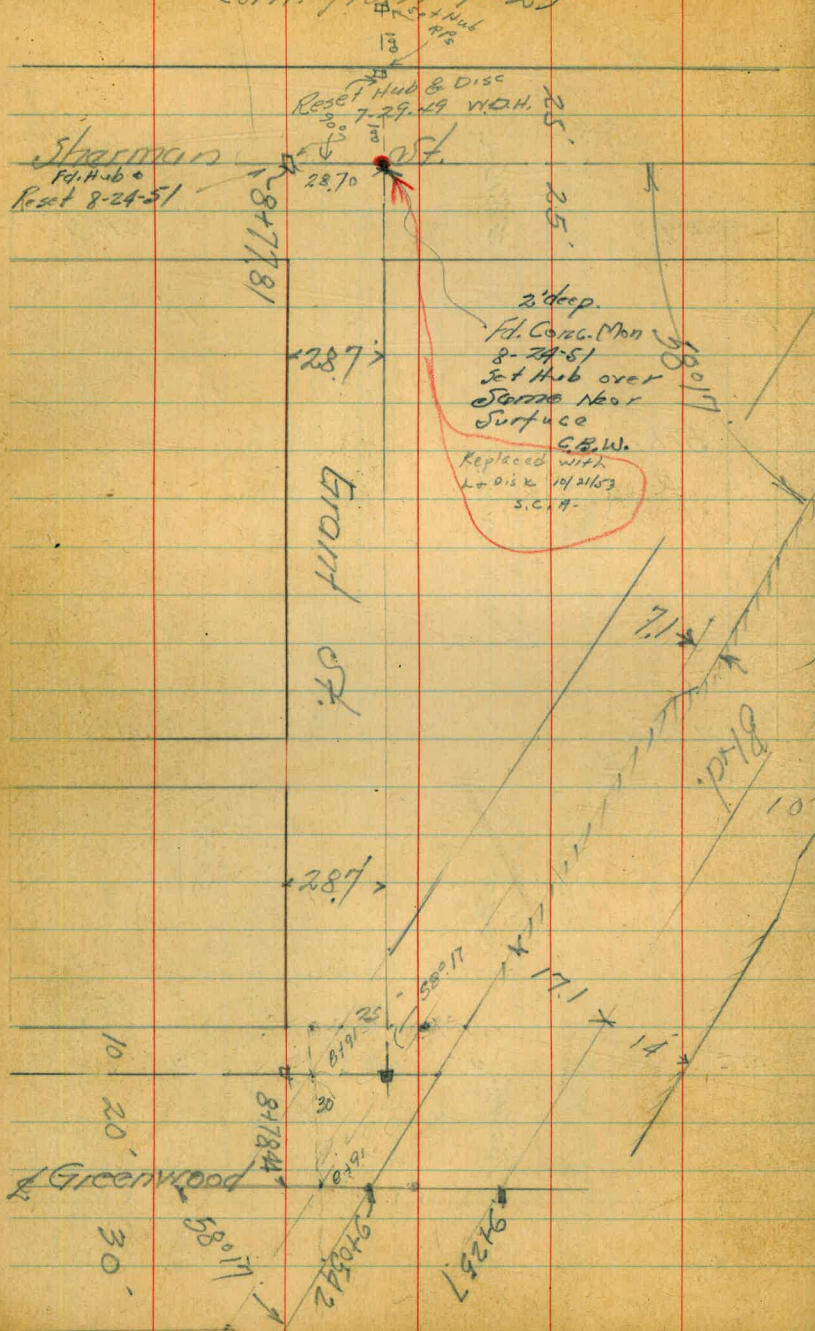


29



Cont. from p. 29

29-A



577	21
593	54
284	27
21	10
1	0
54	33

1400

10.31

Cont. from P. 28

Wcb+8	6.0	4.3
W	6.0	4.3
TS	5.7	4.6
+10	4.3	6.0

1750

-10	5.4	4.9
W-A	5.7	4.6
W	5.8	4.5
+A	5.9	4.4
cb.	5.3	5.0
1/4	4.7	5.6
E	4.4	5.9
1/4	4.1	6.2
cb.	4.0	6.3
E	4.0	6.3
+10	4.0	6.3

2+00

-10	4.2	6.1
E	4.2	6.1
cb.	4.4	5.9
1/4	4.6	5.7
E	4.7	5.6
1/4	5.0	5.3
cb.	5.4	4.9
W	4.8	5.5
+10	4.7	5.6

10.31

Greenwood st 30

2+50

-10	4.5	5.8
W	4.4	5.9
cb.	4.2	6.1
1/4	4.6	5.7
E	4.7	5.6
1/4	4.9	5.4
cb.	5.0	5.3
E	4.9	5.4
+10	4.7	5.6

2+59,48 = SLY line Custer st.

-10	4.7	5.6
E	4.9	5.4
cb.	5.0	5.3
1/4	4.7	5.6
E	4.6	5.7
1/4	4.6	5.7
cb.	4.1	6.2
W	4.0	6.3
+10	4.4	5.9

2+84,48 = SLY Custer st.

W	3.7	6.6
cb	4.0	6.3
1/4	4.4	5.9
E	5.0	5.3
1/4	4.6	5.7

10.31

Greenwood St

cb.	45	5.8
E	44	5.9
+10	44	5.9

3+0948 = NAY Line Custer St

-10	40	6.3
E	40	6.3
cb.	39	6.4
1/4	40	6.3
L	39	6.4
1/4	36	6.7
cb.	34	6.9
W	36	6.7

3+50

-10	3.8	6.5
W	3.4	6.9
cb.	3.5	6.8
1/4	3.8	6.5
L	4.1	6.2
1/4	4.1	6.2
cb.	4.4	5.9
E	4.6	5.7
+10	4.7	5.6

TR 543 10.88

3+62

E-10	5.0	5.9
E	5.2	5.7
cb	5.5	5.4

10.88

31

+3	51	5.8
1/4	51	5.8
+3	49	6.0
L	43	6.6
+8	49	6.0
1/4	51	5.8
cb	51	5.8
W	46	6.3
+10	48	6.1

3+75

-10	47	6.2
W	46	6.3
cb	47	6.2
+4	45	6.4
+6	37	7.2
1/4	38	7.1
L	37	7.2
+3	45	6.4
1/4	51	5.8
cb	45	6.4
E	48	6.1
+10	56	5.3

3+83

-10	5.7	5.2
E	5.5	5.4
cb	5.3	5.6

1088

R 1/4	5.2	5.7
+8	4.8	6.1
S	3.8	7.1
1/4	4.6	6.3
cb	4.7	6.2
W	4.7	6.2
+10	4.7	6.2

3791

-10	4.9	6.0
W	4.9	6.0
cb	5.0	5.9
1/4	5.0	5.9
S	5.0	5.9
1/4	5.3	5.6
cb	5.6	5.3
F	5.8	5.1
+10	5.6	5.3

4105

-10	6.7	4.2
F	6.1	4.8
cb	5.5	5.4
1/4	5.3	5.6
S	5.6	5.3
1/4	5.7	5.2
cb	5.6	5.3
W	5.7	5.2
+10	5.7	5.2

1088

Greenwood St. 32

4110

-10	5.4	5.5
W	5.2	5.7
cb	4.2	6.7
1/4	4.9	6.0
S	5.8	5.1
1/4	5.6	5.3
cb	5.6	5.3
F	6.1	4.8
+10	6.5	4.4

4121

-10	6.7	4.2
F	6.2	4.7
cb	5.7	5.2
1/4	6.1	4.8
S	6.0	4.9
1/4	5.2	5.7
cb	4.6	6.3
W	4.2	6.7
+8	4.6	6.3
+12	5.7	5.2

4146

-10	6.4	4.5
W	6.6	4.3
cb	7.8	3.1
1/4	7.4	3.5
S	7.5	3.4

4+46 10.88

E 1/4	6.5	4.4
cb.	6.0	4.9
E	6.5	4.4
+10	6.5	4.4

TP	9.71	13.03	7.57	3.31
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1102
SWLY
PL 301

4+53 SL edge Ch.

-10	8.3	4.7
E	9.4	3.6
1/4	8.4	4.6
cb.	8.3	4.7
1/4	8.2	4.8
E	8.3	4.7
+8	9.1	3.9
1/4	8.6	4.4
+5	9.3	3.7
cb	9.4	3.6
W	9.4	3.6
+10	9.2	3.8

4+81 = NLY edge Ch.

-10	9.5	3.5
W	9.4	3.6
cb.	9.0	4.0
1/4	9.3	3.7
E	9.1	3.9
1/4	9.0	4.0
cb.	9.0	4.0

18.02

Greenwood St. 33

cb+5	8.6	4.4
E	9.3	3.7
+10	9.3	3.7

4+92 Pocket in Ch

-10	8.3	4.7
E	8.6	4.4
+5	8.1	4.9
cb.	8.0	5.0
1/4	7.8	5.2
E	8.2	4.8
+7	9.4	3.6
1/4	10.6	2.4
cb	10.5	2.5
W	10.5	2.5
+10	10.4	2.6

5+04

-10	7.3	5.7
W	7.3	5.7
cb	7.5	5.5
1/4	7.7	5.3
E	7.3	5.7
1/4	7.5	5.5
cb	7.7	5.3
E	8.4	4.6
+10	7.3	5.7

1802

5+50

-10	6.9	6.1
F	6.7	6.3
cb	6.4	6.6
1/4	6.3	6.7
L	6.4	6.6
1/4	6.5	6.5
cb	6.8	6.2
W	6.5	6.5
+10	6.5	6.5

5+68.96 = 84 Line Banks of

-10	6.1	6.9
W	6.4	6.6
cb	6.2	6.8
1/4	6.1	6.9
L	6.3	6.7
1/4	5.6	7.4
cb	5.7	7.3
E	5.8	7.2
+10	6.3	6.7

5+93.96 = L Banks of

-10	4.8	8.2
E	4.7	8.3
cb	4.8	8.2
1/4	5.1	7.9
L	5.4	7.6

1802

Greenwood St 34

1/4	5.3	7.7
cb	5.3	7.7
W	5.2	7.8
+10	5.2	7.8

6+18.96 = 144 Line Banks of

-10	4.8	8.2
W	4.8	8.2
cb	4.6	8.4
1/4	4.8	8.2
L	4.7	8.3
1/4	4.7	8.3
cb	4.5	8.5
E	4.3	8.7
+10	4.4	8.6

6+50

-10	4.6	8.4
E	4.4	8.6
cb	4.4	8.6
1/4	4.3	8.7
L	4.5	8.5
1/4	4.5	8.5
cb	4.3	8.7
W	4.4	8.6
+10	4.4	8.6

7+00

-10	3.3	9.7
W	3.3	9.7

1302

w/cb.	3.3	9.7
1/4	3.4	9.6
E	3.8	9.2
1/4	4.1	8.9
cb	4.4	8.6
E	4.3	8.7
+10	4.0	9.0

7+50

-10	4.2	8.8
E	4.4	8.6
cb	4.4	8.6
1/4	4.4	8.6
E	4.3	8.7
1/4	4.6	8.4
cb	4.5	8.5
w	4.3	8.7
+10	4.2	8.8

8+00

-10	4.9	8.1
w	4.5	8.5
cb	4.4	8.6
1/4	4.3	8.7
E	4.3	8.7
1/4	4.3	8.7
cb	4.3	8.7
E	4.1	8.9
+10	4.4	8.8

1302

Greenwood st.

35

8+50

-10	4.3	8.7
E	4.7	8.3
cb	5.0	8.0
1/4	5.0	8.0
E	5.0	8.0
1/4	5.0	8.0
cb	5.1	7.9
w	5.5	7.5
+10	5.4	7.6
T.P.	6.55	12.47

6.59 19.07

8+78.45 = 5L/ line Grant st.

-10	11.5	7.6
w	10.5	8.6
cb	9.9	9.2
1/4	9.5	9.6
E	8.8	10.3
1/4	9.0	10.1
cb	8.8	10.3
+10	8.4	10.7
E	7.3	11.8
+6	4.8	14.3
+10	4.5	14.6
E	8.9	10.8
+10	8.3	10.8

E. Sta. = 8+91 = Section = Parallel to Paving.

1907

Fr.	8.8	10.3		
cb.	8.6	10.5		
1/4	8.6	10.5		
L	8.4	10.7		
cb.	8.5	10.6		
W	8.5	10.6		
+11.75	8.5	10.6		
T.P.	6.78	19.26	6.59	12.48

9100 on Dirt Berms Diag. Sec

-11.75	4.9	14.4
W	4.9	14.4
cb.	5.1	14.2
1/4	4.9	14.4
L	5.4	13.9
1/4	4.8	14.5
cb.	5.0	14.3
E	5.0	14.3
+11.75	5.0	14.3

9105 = Diag. Sec. on Asphalt cb. Berms

-11.75	4.74	14.52
E	4.81	14.45
cb.	4.85	14.41
1/4	4.79	14.47
L	4.79	14.47
1/4	4.81	14.45
cb.	4.82	14.44
W	4.63	14.63
+11.75	4.56	14.70

1926

910542 - sly edge Exist. Paving Diag. Sec.

-150'	5.07	14.22
-100	5.21	14.05
-50'	5.12	14.14
W	5.15	14.11
cb.	5.26	14.00
1/4	5.28	13.98
L	5.26	14.00
1/4	5.21	14.05
cb.	5.20	14.06
E	5.22	14.04
+11.75	5.16	14.10

9125.7 - Diag. Sec. on Painted White Line

-11.75	4.63	14.63
E	4.65	14.61
cb.	4.67	14.59
1/4	4.66	14.60
L	4.65	14.61
1/4	4.65	14.61
cb.	4.67	14.59
W	4.69	14.57
+50'	4.63	14.63
+100'	4.73	14.53

T.P.	0.53	13.01	6.78	12.48	B.M. on
T.P.	7.18	13.55	6.64	6.37	Rock

A Cont. P-37

Walker Cross Section Sherman St.

Hendricks
Becker
9-4-46

50' wide
10' cbs.
7.5' 1/4s.

from Morgan St. to Moreno Blvd.

13.55 from 36

0-2.5 = NLY Line Morgan St

-10	6.7	6.9
E	6.6	7.0
cb.	5.9	7.7
1/4	6.5	7.1
E	6.8	6.8
g on Mon.	7.11	6.44
1/4	6.9	6.7
cb.	6.9	6.7
1/4	7.2	6.4
+10	7.1	6.5

0+00 = NLY Line Morgan St

-10	7.0	6.6
1/4	6.9	6.7
cb.	6.9	6.7
1/4	6.9	6.7
g	6.9	6.7
1/4	6.9	6.7
cb.	6.9	6.7
E	7.0	6.6
+10	7.0	6.6

13.55

Indexed
C.S.K.

37

0+50

-1.5	6.1	7.5
E	6.8	6.8
cb.	6.8	6.8
1/4	6.7	6.9
g	6.5	7.1
1/4	6.4	7.2
cb.	6.8	6.8
1/4	7.0	6.6
+10	7.4	6.2

0+66

-10	8.9	4.7
1/4	8.2	5.4
cb.	7.6	6.0
1/4	7.4	6.2
g	7.0	6.6
1/4	7.0	6.6
cb.	7.2	6.4
E	6.8	6.8
+13	5.7	7.9

0+81

-10	7.3	6.3
E	7.5	6.1
cb.	7.5	6.1
1/4	7.9	5.7
g	7.0	4.6

0481 13.55

W 1/4	9.3	4.3
cb.	9.8	3.8
W	9.8	3.8
+10	2.7	3.9

1714

-10	9.5	4.1
W	10.4	3.2
+8	10.7	2.9
cb.	9.2	4.4
1/4	9.1	4.5
♀	9.1	4.5 ✓
1/4	9.0	4.6
cb.	8.9	4.7
E	8.8	4.8
+6	7.9	5.7

1750

-10	7.3	6.3
E	6.9	6.7
cb.	6.4	7.2
1/4	6.4	7.2
♀	6.5	7.1 ✓
1/4	6.4	7.2
cb.	6.9	6.7
W	6.9	7.3
+10	6.0	7.6

13.55

Sherman St. 138

1770

-10	5.9	7.7
W	6.1	7.5
cb.	6.4	7.2
1/4	6.3	7.3
♀	6.1	7.5 ✓
1/4	6.1	7.5
cb.	6.4	7.2
E	6.8	6.8
+10	6.9	6.7

1789

-10	6.7	6.9
E	7.2	6.4
cb.	6.7	6.9
1/4	6.6	7.0
♀	5.8	7.8 ✓
1/4	5.3	8.3
cb.	4.7	8.9
W	4.8	8.8
+10	5.1	8.5

2704

-10	6.0	7.6
W	5.5	8.1
cb.	6.1	7.5
1/4	6.4	7.2
♀	6.6	7.0 ✓

13.55

1/4	6.4	7.2
cb.	6.6	7.0
E	6.6	7.0
+10	7.2	6.4

2150

-10	7.3	6.3
E	7.1	6.5
cb.	7.0	6.6
1/4	6.9	6.7
2	6.7	6.9
1/4	6.1	7.5
+4	5.7	7.9
cb.	5.9	7.7
1/4	6.0	7.6
+10	6.3	7.3

2159.27 = SLV line Custer on 1/4

-10	6.3	7.3
W	6.1	7.5
cb.	6.0	7.6
+5	5.5	8.1
1/4	5.7	7.9
2	6.4	7.2
1/4	6.9	6.7
cb.	7.3	6.3
E	7.2	6.4
+10	7.2	6.4

13.55

Sherman St. 39

2169.27

-10	6.5	7.1
E	6.4	7.2
cb.	6.4	7.2
1/4	6.4	7.2
2	6.1	7.5
1/4	5.5	8.1
cb.	6.0	7.6
1/4	6.2	7.4
+10	6.4	7.2

2184.27 = 2 Custer

-10	6.9	6.7
1/4	6.3	7.3
cb.	6.2	7.4
1/4	5.9	7.7
+5	5.6	8.0
2	5.9	7.7
1/4	6.0	7.6
cb.	6.2	7.4
E	6.0	7.6

3109.27 = 1/4 line Custer

E	6.5	7.1
cb.	6.7	7.4
1/4	5.3	8.3
+3	5.4	8.2
2	5.9	7.7

1355

1/4	6.1	7.5
cb.	6.3	7.3
W	6.5	7.1
+10	6.5	7.1

3150

-10	6.0	7.6
W	6.3	7.3
cb.	6.4	7.2
1/4	6.4	7.2
E	6.3	7.3
1/4	6.0	7.6
+3	5.7	7.9
cb.	4.8	8.8
+7	4.5	9.1
E	5.3	8.3
+10	5.6	8.0

3180

-10	5.4	8.2
E	5.2	8.4
+7	5.1	8.5
cb.	6.1	7.5
1/4	6.3	7.3
E	6.5	7.1
1/4	6.8	6.8
cb.	6.4	7.2
+4	6.6	7.0
+7	5.7	7.9

1355

Sherman st. 40

W	5.6	8.0
+10	5.8	7.8

4100

-10	6.8	7.8
-5	5.4	8.2
W	5.7	7.9
+3	5.8	7.8
+5	7.5	6.1
cb.	7.2	6.4
1/4	7.4	6.2
1/4	7.1	6.5
1/4	6.6	7.0
cb.	6.4	7.2
E	6.5	7.1
+5	6.5	7.1
+15	6.0	7.6
TR	5.36	11.78
	7.18	6.37

R36

Rock

4121

-10	4.9	6.8
E	4.9	6.8
cb.	5.5	6.2
1/4	6.2	5.5
E	6.8	4.9
1/4	7.0	4.7
cb.	6.7	5.0
W	5.9	5.8
+10	5.5	6.2

1173

4+39

-10	7.5	4.2
W	8.2	3.5
cb.	8.5	3.2
1/4	8.4	3.3
2	8.6	3.1 ✓
1/4	8.0	3.7
cb.	6.9	4.8
E	6.1	5.6
+10	5.9	5.8

4+59

-18 in channel	8.8	2.9
E	8.3	3.4
cb.	8.9	2.8
1/4	9.6	2.1
2	9.9	1.8 ✓
1/4	9.8	1.9
cb.	9.7	2.0
W	10.1	1.6
+8	10.0	1.7
10	9.3	2.4

4+70

-10	9.8	1.9
W	9.6	2.1
cb.	9.9	1.8
1/4	10.2	1.5
2	10.4	1.5 ✓

1173

Sherman St.

41

1/4	10.1	1.6
cb.	10.3	1.4
E	10.1	1.6
+15	10.2	1.5
5+00		
-15	10.4	1.3
E	10.6	1.1
cb.	10.0	1.7
1/4	10.0	1.7
+2	10.5	1.2
E	10.4	1.3 ✓
1/4	10.0	1.7
+6	10.0	1.7
cb.	9.5	2.2
W	8.8	2.9
+10	8.2	3.7
5+23		
-10	9.2	2.5
W	9.1	2.6
cb.	9.0	2.7
+3	9.4	2.3
1/4	10.1	1.6
2	10.1	1.6 ✓
1/4	10.0	1.7
+4	9.8	1.9
cb.	9.9	1.8
E	9.4	1.3
+10	8.7	2.9

1173

5+31

-10	6.9	4.8
E	6.4	5.3
+4	7.0	4.7
+7	9.7	2.0
cb	9.8	1.9
1/4	10.0	1.7
L	10.3	1.4
1/4	10.2	1.5
+10	2.3	2.4
cb.	2.4	2.3
W	10.0	1.7
+10	10.0	1.7

5+68.54 = JLY Line Banks

-10	9.7	2.0
W	9.7	2.0
cb.	9.6	2.1
1/4	9.9	1.8
+4	8.8	2.9
L	9.1	2.6
1/4	8.7	3.0
cb.	8.6	3.1
+3	7.5	4.2
-17	7.3	4.4
E	6.4	5.3

1173

Sherman St.

42

5+93.54 = L Banks

E	5.0	6.7
+3	5.5	6.2
+5	7.0	4.7
cb.	7.4	4.3
1/4	7.6	4.1
+3	7.7	4.0
+5	7.2	4.5
L	7.5	4.2
L on Hub.	8.22	3.51
+3	9.2	2.5
1/4	9.2	2.5
cb.	8.3	3.4
W	8.1	3.6
+10	6.4	5.3

6+04

-10	5.7	6.0
W	6.0	5.7
cb.	6.2	5.5
1/4	6.4	5.3
L	6.0	5.7
+2	5.8	5.9
+4	7.1	4.6
1/4	7.2	4.4
cb.	6.8	4.9
+6	6.4	5.3
E	5.1	6.6

11.73

6+13

E	5.0	6.7
+2	4.7	7.0
+4	5.9	5.8
cb.	6.3	5.4
1/4	6.8	4.9
+3	6.8	4.9
+5	5.8	5.9
2	6.0	5.7 ✓
1/4	6.5	5.2
cb.	6.4	5.3
W	6.2	5.5
+10	6.6	5.1

6+18.5A - NY Lime Bank

-10	8.4	3.3
W	10.1	1.6
cb.	10.1	1.6
1/4	10.1	1.6
2	7.6	4.1 ✓
+4	5.2	6.5
1/4	6.4	5.3
cb.	6.0	5.7
+7	5.7	6.0
E	4.9	6.8

6+37

E-10	5.6	6.1
E-5	4.9	6.8

11.73

Sherman St. 43

E	4.7	7.0
cb.	5.0	6.7
1/4	5.0	6.7
+3	4.2	7.5
2	6.0	5.7 ✓
+5	10.0	1.7
1/4	10.4	1.3
cb.	9.8	1.9
W	8.5	3.2
+3	7.8	3.9
+11	5.1	6.6

6+45

-10	5.0	6.7
W	4.9	6.8
cb.	4.7	7.0
1/4	4.4	7.3
2	4.0	7.7 ✓
+5	4.1	7.6
1/4	4.6	7.1
cb.	4.7	7.0
E	4.6	7.1
+10	5.0	6.7

6+75

-1 Coric. Floor New BK. 2.14		9.59
E-1	3.3	8.4
E	3.3	8.4

1173

cb.	33	8.4
1/4	32	8.5
E	28	8.9 ✓
1/4	37	8.0
cb.	40	7.7
W	41	7.6
+10	46	7.1

7+07

-10	42	7.5
W	39	7.8
cb.	36	8.1
1/4	29	8.8
E	26	9.1 ✓
1/4	26	9.1
cb.	27	9.0
E	25	9.2

6+68 to 7+29 = New Bld on Rt 1' Back

7+50

-10	27	9.0
E	20	9.7
cb.	19	9.8
1/4	18	9.9
E	18	9.9 ✓
1/4	22	9.5
cb.	23	9.2
W	27	9.0
+10	28	8.9

1173

Sherman St. 44

TR 441 15.20 694 10.79

8+00

-10	60	9.2
W	58	9.4
cb.	59	9.3
1/4	58	9.4
+4	50	10.2
E	51	10.1
1/4	51	10.1
cb.	49	10.3
E	48	10.4

Red Floor = 558
 7+54 to 8+04 = New Bld on Rt. 1' Back
 8+50

-10	60	9.2
E-4	58	9.4
E-2	48	10.4
E	51	10.1
cb.	53	9.9
1/4	53	9.9
E	54	9.8 ✓
+6	61	9.1
1/4	61	9.1
cb.	63	8.9
W	63	8.9
+10	64	8.8

1520

8+77.81 = SLY Grant

-10	6.5	8.7
W	6.7	8.5
cb	6.5	8.7
1/4	6.1	9.1
+0	5.2	10.0
E	5.7	9.5
1/4	5.6	9.6
cb	5.7	9.5
F	5.3	9.9
+7	6.2	9.0
+10	6.5	8.7

9+06.51 = NLY line Grant st.

-10	6.8	8.4
-6	6.8	8.4
F	5.6	9.6
cb	6.0	9.2
1/4	5.8	9.4
E	5.9	9.3
+3	5.9	9.3
+6	6.8	8.4
1/4	6.9	8.3
cb	6.9	8.3
W	7.0	8.2
+10	7.0	8.2

9+50 1520

Sherman st. 45

-10	7.5	7.7
W	7.4	7.8
cb	7.8	7.9
1/4	7.1	8.1
E	6.3	8.9
1/4	6.1	9.1
cb	5.9	9.3
F	5.8	9.4
+7	6.8	8.4
+10	7.0	8.2

10+00

-10	6.6	8.6
-6	6.3	8.9
F	5.5	9.7
cb	6.2	9.0
1/4	5.4	8.8
E	6.1	9.1
1/4	6.8	8.4
cb	6.9	8.3
W	7.1	8.1
+10	7.0	8.2

10+50

-10	7.5	7.7
W	7.4	7.8
cb	7.2	8.0
1/4	7.0	8.2

15.20

75	59	9.3
♀	62	9.0 ✓
1/4	63	8.9
cb.	61	9.1
E	57	9.5
+6	67	8.5
+10	70	8.2

11+00

+10	79	7.3
-4	72	8.0
E	50	10.2
cb.	53	9.9
1/4	53	9.9
♀	54	9.8 ✓
+5	54	9.8
1/4	64	8.8
+3	75	7.7
cb.	77	7.5
W	79	7.3
+10	82	7.0

11+50

-15	87	6.5
W	86	6.6
cb.	45	10.7
1/4	40	11.2
♀	39	11.3 ✓

15.20

Sherman st. 46

E 1/4	40	11.2
cb.	41	11.1
+6	39	11.3
E	53	9.9
+8	93	5.9
+15	96	5.6

11+74.38 Day. Section on line ^{Morona} _{82nd}

-15	96	5.6
E-2	29	12.3
E	35	11.7
cb.	32	12.0
1/4	29	12.3
♀	30	12.2 ✓
+4	30	12.2
1/4	40	11.2
cb.	47	10.5
W	53	9.9
+10	60	9.2

11+95 Section Parallel to Pav.

-10	57	9.5
cb.	56	9.6
1/4	56	9.6
+4	24	12.8
♀	18	13.4
1/4	18	13.4
cb.	17	13.5

15.20

F	1.8	13.4
+10	2.2	13.0
T.P.	3.60	19.17
	1.63	13.57

12+09 Diag. Sec. Parallel to Pav

-10	5.4	13.8
E	5.1	14.1
cb.	5.1	14.1
1/4	5.1	14.1
1/2	5.0	14.2
1/4	4.9	14.3
cb.	4.8	14.4
W	4.8	14.4
+10	4.9	14.3

12+11.84 = Edge Exist. Pav. Diag. Sec.

-100'	4.05	15.12
-50'	4.33	14.84
W	4.48	14.69
cb.	4.46	14.71
1/4	4.47	14.70
1/2	4.51	14.66
1/4	4.55	14.62
cb.	4.55	14.62
E	4.53	14.64
+50	4.62	14.55
+100'	4.63	14.54

19.17

Sherman St. 47

12+23.6 = Edge Exist. Pav.

-100'	4.41	14.76
-50	4.32	14.85
E	4.35	14.82
cb.	4.36	14.81
1/4	4.35	14.82
1/2	4.34	14.83
1/4	4.30	14.87
cb.	4.28	14.89
W	4.23	14.94
+50	4.11	15.06
+100	3.83	15.34
T.P.	4.55	18.91
	4.81	14.36
chk. Main P-28	6.43	12.48

Walker
Hardnicks
Becker

Cross Section - Grant St. 28.7' wide
from Greenwood to Sherman St.

7-1-16

BM Mon

1,20 13,68

12,48 P-28

0+00 = W/L line Greenwood

N 5 2.3 11.4

N 3.4 10.3

E 4.3 9.4

South 5.6 8.1

0+50

5-5 5.4 8.3

5 5.4 8.3

E 5.8 7.9

N 5.9 7.8

+5 5.7 8.0

1+00

-5 5.6 8.1

N 5.2 8.5

E 5.7 8.0

5 5.5 8.2

+5 5.2 8.5

1+50

-5 4.7 9.0

5 4.7 9.0

E 4.9 8.8

N 5.3 8.4

+5 5.6 8.1

2+00 13,68

Indexed
c-s.k.

48

-5 4.7 9.0

N 4.6 9.1

E 4.5 9.2

5 4.6 9.1

+5 4.4 9.3

2+50

-5 4.9 8.8

5 5.0 8.7

E 5.1 8.6

N 5.1 8.6

+5 4.9 8.8

3+00

-5 4.9 8.8

N 5.0 8.7

E 4.9 8.8

5 4.9 8.8

+5 4.7 9.0

3+50

-5 5.2 8.5

5- 5.1 8.6

E 5.2 8.5

N 5.4 8.3

+5 5.3 8.4

4+00

-5 5.5 8.2

N 5.4 8.3

Grant St

1368

4100 cont. from P-48

E	5.3	8.4
S	5.3	8.4
+5	5.2	8.5

4131.62 = ELY line Sherman

4124

-5	4.5	9.2
South	4.9	8.8
E	5.3	8.4
N	5.3	8.4
+5	5.2	8.5

4131.62 = ELY line Sherman

-5	4.1	9.6
N	4.1	9.6
E	4.0	9.7
S	3.8	9.9
+5	3.4	10.3

1481 6' N NL = Guy Pole

" = Elec. Pole on Lt 4.7' in st.

Walker
Hendricks
Becker
9-1-46

Cross Section - Banks St. 50' wide
10' cbs.
7.5' 1/4s

from Greenwood to Sherman St.

4.32 11.92 7.60

BM on Herb
519396
P-28

0+00 = W. Greenwood St.

-10	3.4	8.5
N	3.7	8.2
cb.	3.9	8.0
1/4	4.0	7.9
2	4.1	7.8
1/4	4.2	7.7
cb.	4.6	7.3
S	5.3	6.6
+10	5.2	6.7

0+50 = Elec on Lt 17' in St.

-10	5.4	6.5
S	5.4	6.5
W	5.4	6.5
cb.	5.1	6.8
1/4	5.1	6.8
2	4.7	7.2
1/4	4.3	7.6
cb.	3.9	8.0
N	4.3	7.6
+10	3.7	8.2

1400

-10	3.9	8.0
-----	-----	-----

1400 11.92

Indexed
C.S.K.

50

N	4.0	7.9
cb.	4.8	7.6
1/4	4.7	7.2
2	4.8	7.1
1/4	5.2	6.7
cb.	5.7	6.2
S	5.9	6.0
+10	6.1	5.8

7150

-10	6.1	5.8
S	5.9	6.0
cb.	5.6	6.3
1/4	5.2	6.7
2	5.1	6.8
1/4	5.0	6.9
cb.	4.8	7.1
N	4.4	7.5
+10	4.1	7.8

2100

-10	4.8	7.1
N	4.5	7.4
cb.	4.9	7.0
1/4	5.0	6.9
2	5.1	6.8
1/4	5.2	6.7
cb.	5.3	6.6
S	5.7	6.2
+10	6.3	5.6

11.92

2+50

-5	5.1	5.8
S	5.8	6.1
cb.	5.5	6.4
1/4	5.5	6.4
2	5.3	6.6
1/4	5.3	6.6
cb.	5.0	6.9
N	4.9	7.0
+10	4.8	7.1

3+00

-10	5.3	6.6
N	5.6	6.3
cb.	5.6	6.3
1/4	5.5	6.4
2	5.6	6.3
1/4	5.5	6.4
cb.	5.7	6.2
S	5.9	6.0
+10	6.3	5.6

3+50

-10	6.9	5.0
S	6.5	5.4
cb.	6.2	5.7
1/4	6.0	5.9
2	5.9	6.2
1/4	5.6	6.3

11.92

Banks St. 51

cb.	5.8	6.1
N	5.6	6.3
+10	5.6	6.3
4+00		
-10	6.1	5.8
N	6.1	5.8
cb.	5.9	6.0
1/4	5.7	6.2
2	5.6	6.3
1/4	5.8	6.1
cb.	6.3	5.6
S	6.7	5.2
+10	6.9	5.0

4+20

-10	7.0	4.9
S	6.8	5.1
cb.	6.4	5.5
1/4	6.0	5.9
2	5.7	6.2
1/4	5.5	6.4
cb.	5.8	6.1
N	6.0	5.9
+10	5.8	6.1

4+31.62 = ELY. Line Sherman

-10	5.1	6.8
N	5.4	6.7

11.22

BANKS ST.

cb.	4.8	7.1
114	5.4	6.5
L	5.5	6.4
114	5.8	6.1
cb.	6.7	5.2
S	7.2	4.7
110	7.3	4.6

52

Walker
Hendricks
Becker
9-5-46

Cross Section - CUSTER ST. 50' wide
10' cbs
from Greenwood to Sherman 7.5' 145

6.34 11.79 5.45 B.M. Rock
P-28
0+00 = 144y Lute Greenwood St.

-10	5.0	6.8
N	5.1	6.7
cb.	5.2	6.6
1/4	4.8	7.0
2	5.2	6.6
1/4	5.1	6.7
cb.	5.3	6.5
S	5.4	6.4
+10	6.0	5.8

0+50

-10	4.8	7.0
S	4.7	7.1
cb	3.7	8.1
1/4	4.3	7.5
2	4.1	7.7
1/4	4.8	7.0
cb.	4.8	7.0
N	4.9	6.9
+10	5.1	6.7

1+00

-10	4.7	7.1
N	4.9	7.8
cb	5.6	6.2

SANTA BARBARA

11.79

indexed
c.s.k.

53

1+00

1/4	5.4	6.4
2	5.4	6.4
1/4	4.6	7.2
cb.	4.5	7.3
S	4.0	7.8
+10	4.3	7.5
1+26.7 on E. Stub	5.35	6.44
T.P. 5.34 12.62	4.51	7.28

1+50

-10	5.8	6.8
S	5.8	6.8
cb	5.8	6.8
1/4	5.8	6.8
2	5.8	6.8
1/4	5.9	6.7
cb.	5.7	6.9
N	5.4	7.2
+10	5.3	7.3

2+00

-10	5.2	7.4
N	5.4	7.2
cb	5.4	7.2
1/4	5.7	6.9
2	5.5	7.1
1/4	5.1	7.2
cb.	5.6	7.0
S	5.8	6.8
+10	5.9	6.9

12.62

Custer St

2+50

-10	6.0	6.6
S	6.2	6.4
cb	5.7	6.9
1/4	5.5	7.1
L	5.5	7.1
1/4	5.4	7.2
cb	5.5	7.1
N	5.3	7.3
+10	5.3	7.3

3+00

-10	5.3	7.3
N	5.2	7.4
cb	5.7	6.9
1/4	6.2	6.4
L	6.1	6.5
1/4	6.3	6.3
cb	6.2	6.4
S	6.3	6.3
+10	6.4	6.2

3+50

-10	7.0	5.6
S	6.8	5.8
cb	5.6	7.0
1/4	4.9	7.7
b	5.0	7.6

12.62

54

1/4	4.8	7.8
cb	4.8	7.8
N	4.5	8.1
+10	4.5	8.1

4+00

-10	4.5	8.1
N	4.9	7.7
cb	5.0	7.6
1/4	5.0	7.6
L	5.1	7.5
1/4	5.2	7.4
cb	5.6	7.0
S	6.1	6.5
+10	6.8	6.3

4+37.62 - ELY LINE SHERMAN

-10	6.4	6.2
S	6.3	6.3
cb	5.6	7.0
1/4	5.2	7.4
L	5.1	7.5
1/4	5.1	7.5
cb	5.4	7.2
N	5.1	7.5
+10	4.9	7.7

chk Rock P-40 6.25 6.37 ✓

Walker Cross Section - Morgan St. 25' wide
 Hendricks from Greenwood St. to Sherman
 Becker
 9-5-46

5.23 10.68

5.45. B.M. Rock
 P. 28

0+00 - WLY Line Greenwood

-10	5.2	5.5
S	5.2	5.5
E	5.7	5.0
N	6.0	4.7
+10	6.1	4.6

0+04

-10	5.2	5.5
N	5.1	5.6
E	5.4	5.3
S	5.2	5.5
+10	4.7	6.0

0+08

-10	7.9	2.8
S	8.3	2.4
E	7.3	3.4
N	7.1	3.6
+10	7.0	3.7

0+25

-10	5.5	5.2
N	5.5	5.2
E	7.0	3.7
S	7.0	3.7
+10	6.8	3.9

10.68

Indexed
 C.S.R.

218448 P. 29
 56

T.P.	5.13	11.36	4.45	6.23	Hub
T.P.	6.80	13.87	4.29	7.07	Rock
T.P.	4.85	11.73	6.99	6.88	

0+50

-10	6.8	4.9
S	6.8	4.9
E	7.8	3.9
N	8.0	3.7
+10	8.0	3.7

0+65

-10	8.0	3.7
N	8.0	3.7
E	7.8	3.9
S	8.0	3.7
+10	8.0	3.7

0+75

-10	6.2	5.5
S	6.7	5.0
E	6.8	4.9
N	5.2	6.5
+10	5.7	6.0

1+00

-10	5.0	6.7
N	6.5	5.2
E	4.9	6.8
S	4.8	6.9
+10	6.2	5.7

11.73

Morgan St.

1+26.7

-10	3.2	8.5
S	3.2	8.5
+8	2.6	9.1
L	4.6	7.1
N	3.2	8.5

1+50

-10	3.4	8.3
N	3.4	8.3
L	3.4	8.3
S	3.5	8.2
+10	3.4	8.3

2+0.0

-10	3.6	8.1
S	3.6	8.1
L	3.4	8.3
N	3.4	8.3
+10	3.4	8.3
T.P.	5.37 13.68	3.42 8.31

2+30

-10	5.6	8.1
N	5.5	8.2
L	5.5	8.2
S	5.5	8.2
+10	5.6	8.1

1368

56

2+50

-10	5.2	8.5
S	5.2	8.5
L	5.2	8.5
N	5.2	8.5
+10	5.3	8.4

3+00

A'ft of E rd ^{Conc. Floor}	3.43	10.25
4" " " Ground	4.6	9.1
L	4.6	9.1
S	6.1	7.6
+10	6.5	7.2

3+50

-10	5.8	7.9
S	5.6	8.1
L	5.4	8.3
N	5.4	8.3
+10	5.4	8.3
T.P.	4.48 11.41	6.75 6.93

4+00

-10	4.8	6.6
N	4.4	7.0
L	3.7	7.7
S	3.9	7.5
+10	3.9	7.5

11.41 Morgan
4+31.62 = ELY. Line Sherman

-10	4.4	7.0
5	4.7	6.7
E	4.5	6.9
N	5.0	6.4
+10	5.0	6.4
chk. Mon 0-25 P-37	4.97	6.44 ✓

Walker
Handricks
Becker
9-5-46

Cross Section 10 Alley BIK 1

Vernon Park N + S Alley ⁸¹⁴
5.85 12.92 7.07 Rock P-55

0+00 = NLY Line Morgan

-5	4.3	8.6
W	4.1	8.8
E	4.2	8.7
E	4.1	8.8
+5	3.9	9.0

0+50

-5	4.0	8.9
E	4.2	8.7
E	4.0	8.9
W	4.0	8.9
+5	4.0	8.9

1+00

-5	3.0	9.9
----	-----	-----

12.92 Alley BIK 1 57

W	3.2	9.7
E	3.1	9.8
E	3.4	9.5
+5	3.5	9.4

1+24.7 = SLY Line E+W Alley

-5	3.1	9.8
E	3.2	9.7
E	4.0	8.9
W	3.7	9.2
+5	3.7	9.2

1+29.7

-5	4.7	8.2
W	4.9	8.0
E	5.0	7.9
+5	4.7	8.2

1+59

-5	4.7	8.2
E	4.5	8.4
E	4.7	8.2
W	5.2	7.7
+5	5.6	7.3

1+71

-5	5.8	7.1
W	5.8	7.1
E	5.8	7.1
E	5.5	7.4
+5	4.7	8.2

12.92 Alley Blk 1
North & South

2+00

-S	58	7.1
E	59	7.0
S	56	7.3
W	56	7.3
+S	55	7.4

2+59.4 = 564 Line Custer

-S	57	7.2
W	56	7.3
S	52	7.7
E	51	7.8
	51	7.8

E & W Alley Blk 1

0+00 = WILY Line Alley

S	3.9	9.0
S	4.5	8.4
N	4.8	8.1

0+50

-S	6.0	6.9
N	5.8	7.1
S	5.6	7.3
S	3.9	9.0
+S	3.6	9.3

0+65

-S	5.1	7.8
S	5.9	7.2

indexed
C.S.R.

12.92

E & W Alley 58

S	5.9	7.0
N	5.9	7.0
+S	5.9	7.0

1+00

-S	5.6	7.3
N	5.5	7.4
S	5.4	7.5
S	5.3	7.6
+S	5.3	7.6

1+50

-S	5.3	7.6
S	5.3	7.6
S	5.1	7.8
N	5.0	7.9
+S	4.7	8.2

1+70

-S	5.1	7.8
N	5.2	7.7
S	5.3	7.6
S	5.1	7.8
+S	5.4	7.5

2+00

-S	6.0	6.9
S	6.4	6.5
S	6.8	6.1
N	6.6	6.3
+S	6.7	6.6

12.92

E + W Alley
Blk 1
Vernon Park

2+50

-5	6.7	6.2
N	6.9	6.0
L	6.9	6.0
S	6.8	6.1
+5	6.8	6.1

2+999 - ELY Line Sherman

-5	7.2	5.7
N	7.3	5.6
L	7.3	5.6
S	7.0	5.9
+5	7.7	5.2

chk 2 stub 17267
P-53

6.46	6.46
	6.44
	<u>0.02</u>

59

Walker Cross Section 10' Alley North
 Hendricks & South
 Becker Between Greenwood & Sherman
 2-5-46 from Custer to Banks

in Vernon Park (Blk. 2) ^{8m on}
 3.88 10.32 6.44 ^{Stub} P 59

0+00 = NLY Line Custer

-5	3.4	6.9
E	3.7	6.6
L	3.4	6.9
W	3.1	7.2
+5	3.1	7.2

0+50

-5	2.8	7.5
W	2.8	7.5
L	2.8	7.5
E	2.4	7.9
+5	2.4	7.9

1+00

-5	4.0	6.3
E	4.1	6.2
L	4.1	6.2
W	4.0	6.3
+5	3.9	6.4

1+24.63

-5	5.0	5.3
W	4.7	5.6
L	5.4	4.9
E	5.5	4.8
+5	6.5	3.8

1032

Indexed
 C.S.R.

60

1+3463

-5	6.5	3.8
E	6.5	3.8
L	6.5	3.8
W	6.0	4.3
+5	5.9	4.4

1+62 in Channel

-5	8.6	1.7
W	8.6	1.7
L	8.6	1.7
E	8.5	1.8
+5	8.3	2.0

2+97

-5	7.4	2.9
E	7.6	2.7
L	7.5	2.8
W	7.4	2.9
+5	7.5	2.8

2+04

-5	4.9	5.4
W	5.0	5.3
L	5.0	5.3
E	4.9	5.4
+5	4.7	5.6

2+59.7 = SLY Line Banks of

-5	4.5	5.8
----	-----	-----

2+59.2 10.32

Blk 2

Indexed
C.S.R.

E	4.6	5.7
E	4.4	5.9
W	4.2	6.1
+5	4.2	6.1

= End North & South Alley

10.32 π AboveCross Section East & West Alley
Blk 2 - Vernon Park

0+00 = W. Line N of South Alley

N	5.9	4.4
E	5.7	4.6
S	4.8	5.5

0+50

-5	4.7	5.6
S	4.7	5.6
E	4.2	6.1
N	4.6	5.7
+10	7.3	3.0

1+00

-5	5.1	5.2
N	5.2	5.1
E	5.2	5.1
S	4.0	6.3
+5	4.0	6.3

1+50 10.32

E+W Alley
Blk 2 - Vernon Park 61

-5	4.2	6.1
S	4.4	5.9
E	4.7	5.6
N	4.7	5.6
+5	4.6	5.7

2+00

-5	4.9	5.4
N	5.1	5.2
E	5.0	5.3
S	4.6	5.7
+5	4.5	5.8

2+50

-5	4.3	6.0
S	4.6	5.7
E	4.7	5.6
N	4.7	5.6
+5	5.3	5.0

2+99.9 = ELY Sherman

-5	5.6	4.7
N	5.0	5.3
E	4.6	5.7
S	4.4	5.9
+5	4.3	6.0

Greenwood & Bunks
Cik & Hub 5+22.1 P-42
Page 28

T.P. 7.00 13.79 3.53

 π cont P-625498.76
7.59
0.01
6.79
1+26.7
E Bunks
St.

Walker
Hendricks
Becker
2-10-46
Cross Section 10 Alley - Blk. 3
Vernon Park
Between Greenwood ^{and} Sherman
from Banks to Grant St ^{Stake}
7.00 13.79 6.79 1+267 P61

0+00 = W.L. Line Banks

-5	6.2	7.6
E	6.2	7.6
S	6.3	7.5
W	6.4	7.4

0+60

-5	5.2	8.6
W	5.1	8.7
S	5.1	8.7
E	5.0	8.8
+5	5.1	8.7

1+00

-5	4.6	9.2
E	4.6	9.2
S	4.6	9.2
W	4.5	9.3
+5	4.5	9.3

1+2463

-5	4.4	9.4
W	4.2	9.6
S	4.4	9.4
E	4.4	9.4
+5	4.4	9.4

13.79

Indexed
C.S.R.

62

1+3463

-5	4.3	9.5
E	4.2	9.6
S	4.2	9.6
W	4.1	9.7
+5	4.1	9.7

1+70

-5	4.4	9.4
W	4.3	9.5
S	4.3	9.5
E	4.2	9.6
+5	4.0	9.8

2+00

-5	4.1	9.7
E	3.9	9.9
S	3.9	9.9
W	3.9	9.9
+5	3.9	9.9

2+5927

W	5.0	8.8
S	5.2	8.6
E	5.4	8.4

E & W Alley Blk 3

0+00 = W.L. N & South Alley

N	4.0	9.8
S	4.2	9.5
W	4.4	9.6

13.79

E & W Alley Bk 3
Cont. from P-22

0+50

-5	4.5	9.3
5	4.6	9.2
2	4.7	9.1
N	4.7	9.1
+5	4.5	9.3

1+00

-5	5.1	8.7
N	5.1	8.7
2	4.9	8.9
5	5.2	8.6
+5	5.3	8.5

1+50

-5	5.4	8.4
5	5.3	8.5
2	5.5	8.3
N	5.4	8.4
+5	5.4	8.4

2+00

-5	4.8	9.0
N	4.8	9.0
2	4.9	8.9
5	4.8	9.0
+5	5.2	8.6

2+50

-5'	5.0	8.8
-----	-----	-----

13.79

63

South

50	8.8
2	8.9
N	4.6
+5	4.6

2+78.3 = 2' 14' Door on 4' & Pt. New Old.

N-0.2 on Conc Floor. 4.21 9.58

N	4.7	9.1
2	5.0	8.8
5	4.8	9.0

+15.3 5.3 8.5

+15.3 on 2' Doorway Conc. Floor 4.33 9.46

2+99.9 = ELY. Line Sherman St

2	4.2	9.6
2	4.1	9.7
N	4.1	9.7

chk Mon. P. 28 1.33 12.46

12.48
0.02

Santa Barbara Place

Cross section Santa Barbara Pl.

(24' wide) Strand Way to Mission Blvd.

4-29-47

W.O. # 25001

Sommermeier
W Moore X
Roberts
Malton

• Found L.T. or Disk
T.P. 25 P. 11

1.68 8.71 — 7.03 B.M. = B.P.

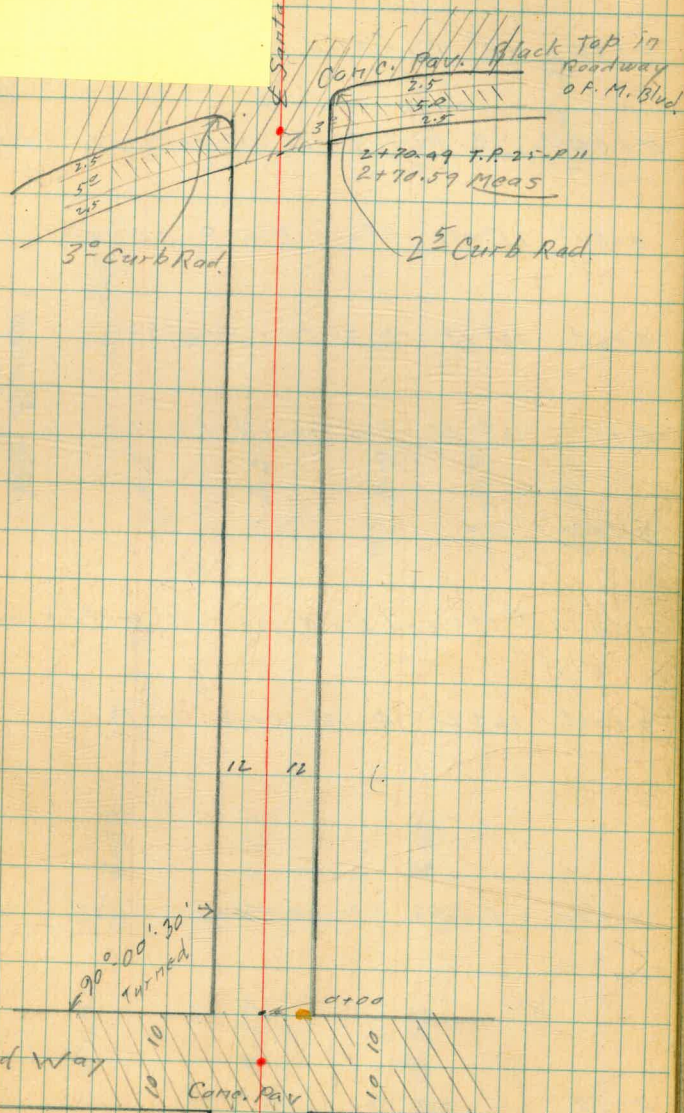
B.M. on Sea Wall at Santa Barbara Place

SANTA BARBARA

Indexed
C.S.K.

64

Rt. = South



Santa Barbara Place
Strand Way to Mission Blvd.

0+90 12° Rt. = End board fence.

0+76 13° Rt. = Φ 3° wide Conc. Walk

0+60[±] 12° Rt. = Start Board fence

0+60 12° Lt. = Φ 3° Conc Walk

0+57 12° Lt. = End board fence

0+50

0+34- 12° Lt. = End 3x6 Guard rail & start board fence

0+09[±] 11.7° Lt. = Φ 3° Conc. Walk

0+00 = E. Line Strand Way - Edge paving

0-10 ON Paving

8.71

NOTES REQUIRED

5-1-47

2002

Lt.

Φ

Rt.

65

2.9
 $\frac{5.8}{30}$

1.9
 $\frac{6.8}{12}$

1.8
6.9

2.1
 $\frac{6.6}{12}$

2.21
 $\frac{6.50}{13.2}$

3.09

$\frac{5.62}{12}$

3.7
 $\frac{5.0}{12}$

3.2
 $\frac{5.5}{7}$

3.2
5.5

3.4
 $\frac{5.3}{8}$

3.9
 $\frac{1.8}{12}$

4.3
 $\frac{2.4}{20}$

5.58

$\frac{3.13}{11.7}$

6.00

$\frac{1.71}{12}$

5.63
3.08

6.02

$\frac{2.67}{12}$

5.65

$\frac{3.06}{12}$

5.67
3.04

5.76

$\frac{2.95}{12}$

8.71

start 3x6
Guard rail
12.4

Santa Barbara Place

T.P. 4.75 4.44 9.02 -0.31

1+55 12² Rt. = Φ 2° wide Corro. Walk

1+50 12³ Rt. = End board fence

1+39 12² Rt. = Φ 3° Corro. Walk

1+25

1+20^E 12¹ Rt. = stard board fence

1+06 19⁸ Rt. = Φ 6° wide steps.

1+00

8.71

Lt.

Φ

Rt.

66

$\frac{8.9}{30}$
-0.2

$\frac{9.1}{12}$
-0.4

9.1
-0.4

$\frac{8.85}{12.3}$
-0.14

$\frac{7.0}{12}$
-0.3

$\frac{8.65}{12.2}$
0.06

$\frac{8.8}{12}$
-0.1

8.7
0.0

$\frac{8.6}{12}$
0.1

$\frac{7.9}{19}$
0.8
Grd.

$\frac{7.68}{19.8}$
1.03
Bottom stop

$\frac{7.8}{30}$
1.4

$\frac{7.9}{12}$
0.8

8.0
0.7

$\frac{7.8}{12}$
0.9

$\frac{7.9}{25}$
0.8

8.71

Santa Barbara Place

2+39 14² Lt. = Φ 3^o Conc. Walk

2+34 13² Rt. = Φ 2^o Conc. Walk

2+25

2+17 14^o Lt. = Φ 2^o Conc. Walk.

2+00

1+92 13² Rt. = Φ 3^o Walk - Conc.

4.44

Lt

Φ

Rt.

67

0.06
 $\frac{4.38}{14.2}$ $\frac{4.6}{14}$

-0.5
 $\frac{1.9}{12}$

-0.24
 $\frac{4.68}{14}$

-0.5
 $\frac{4.9}{12}$

-0.4
 $\frac{4.8}{30}$

-0.7
 $\frac{5.1}{12}$

-0.9
 5.3

-0.6
 5.0

-0.28
 $\frac{4.72}{13.8}$

-0.8
 $\frac{5.2}{12}$

-0.5
 $\frac{4.9}{12}$

-0.3
 $\frac{4.7}{30}$

-0.33
 $\frac{4.77}{13.9}$

4.44

Work order # 25001 5/14/47

Sommermeier
W. Moore &
L. Melton.

X-Section for grade Establishment.
Alley Bk. 108. Mission Beach
16' Wide. Going East.

0.67
4.75
5.42x

500 1789-16
For Bks 111 + 116.

Part shown in red is
new since 5/14/47

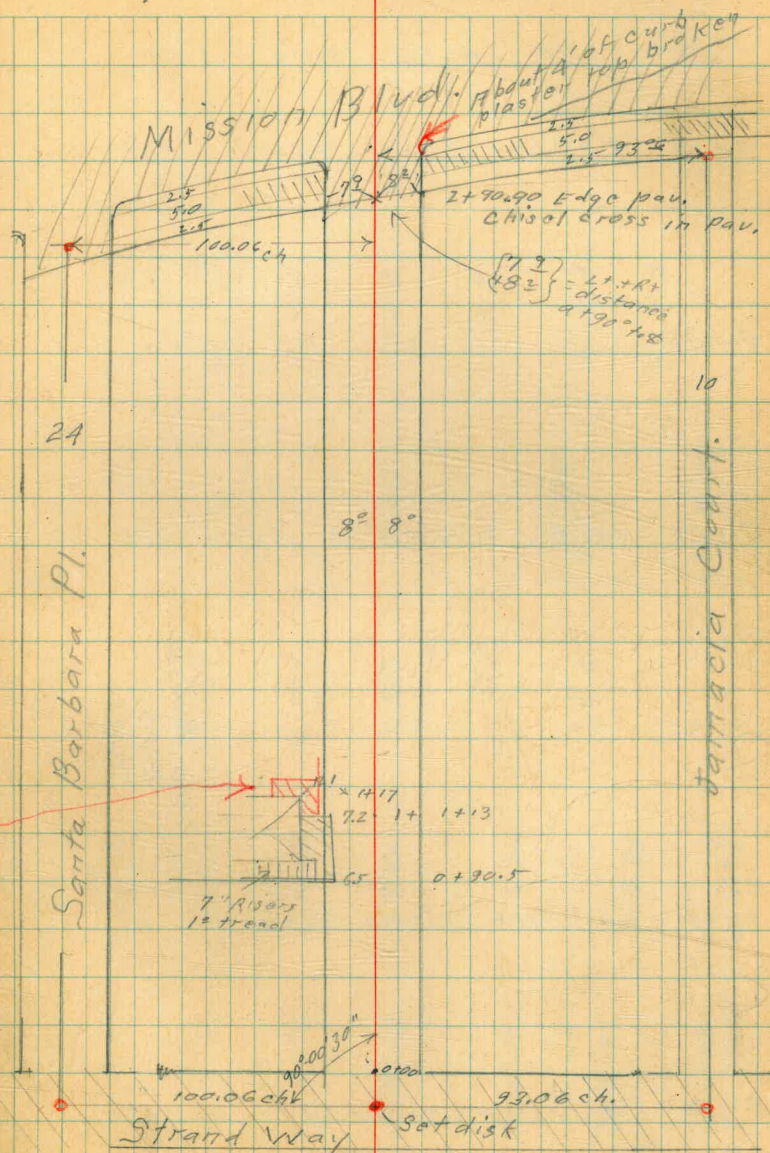
EL.

1+23 8' Lt = End new slab. 0.07

1+17 = 7' Lt. Brk. in Gr. 0.14

1+13 7' Lt = start Conc. Slab. 0.68

Alley Bk. 108 Mission Beach. Indexed
e.s.k. 69



Alley B/k. 108 Mission Beach

T.P. 1.70 4.16 8.46 2.46

0+58 8.9 Lt. = start board fence.

0+30

0+17 12° Rt. = door of Sing. Car. corr. floor

0+05

Notes Reduced
7-15-47
R.D.

0+00 = East line Strand Way.

0-10 = Strand Way

B.A. Top Sea Wall at Santa Barbara Pl. 3.89 10.92 — 7.03

Lt. N

⊥

Rt. S

70

6.0
50

4.9

6.0
20

4.9

6.9
8

4.0

7.1

3.8

7.0
8

3.9

6.6
10

4.3

6.0
40

4.9

4.8

6.1

5.4
12
Ground

5.55
12
Floor

5.0
15

5.9

5.1
8

5.8

5.3

5.6

5.1
8

5.8

4.9
15

6.0

5.29
100

5.63

4.90
88

6.02

4.80
50

6.12

4.75
8

6.17

5.11

5.81

4.70
8

6.22

4.57
50

6.35

4.45
100

6.47

5.25
100

5.67

5.11
50

5.81

5.01
8

5.85

5.10

5.82

5.09
8

5.88

4.90
50

6.02

4.79
100

6.13

10.92

Alley BIK. 108 M.B.

0+90

0+89 9° Lt = End double Gar.

0+84⁵ ± East 1/2 double Gar. Dirt floor

0+80 End Conc. Floor + Apron

garage West 1/2 Conc. Floor, East 1/2
dirt floor
8° Lt = End board fence. Start double

0+71 8° Lt = start Conc. Apron

0+70

4.16

Lt. = N

±

Rt. = S

71

1.1
3.1
2.5

1.0
3.2
8

1.0
3.2

1.1
3.1
8

2.1
2.1
2.5

1.3
2.9
5.0

1.6
2.6
8.9

1.25

2.31
8.7
Floor

1.51

2.65
8
Apron

1.95

2.21
8.9
Gar. Floor

1.82

2.34
8
Apron

1.9

2.3
8

1.8

2.4

1.9

2.3
8

2.7

1.5
2.5

4.16

1+23 10^s Rt. = Back Edge pole P.H. 7A8

1+23 Start Conc. Apron + double Gar.

1+17 End stucco Bldg 12' Lt. see sketch.

See page 69 for additions
10-2-47 on left.

1+13 End Conc. Apron + double Gar. opening

0+96 Entrance to double Gar. on Lt.

0+92^E = ^{9' Lt.} Conc. Stairs to 2nd Floor
see - sketch

0+90.5 6^E Lt. = Start Conc Apron

A.16

-0.11

4.27
12.2
Apron of
Bldg.

-0.13

4.29
7.2
Edge
Apron
7' Lt.

0.1

4.1
7.0

0.76

3.40
12.1
Gar. Floor

0.67

3.49
7.2
Edge Apron

0.4

3.8
6

0.3

3.9

0.5

3.7
8

0.4

3.8
30

1.2

3.0
50

0.79

3.37
12.1
Gar. Floor

0.73

3.43
6.8
Edge Apron

0.9

3.3
6

0.9

3.3

1.0

3.2
8

1.03

3.13
9.1
Bottom of Steps

1.12

3.04
9.1
Back
Edge Apron

0.98

3.18
6.5
Apron

A.16

Alley Bk. 108 M.B.

1+50

1+45 11° Rt. = \pm 10' Conc. Apron 11° = \pm 10' wide Gar. Core. floor.

1+41^E 7° Lt. = End Conc. Apron 12° Lt. = End Gar.

1+36^E 11° Rt. = \pm 2' Conc. Walk

1+35 12° Lt. = \pm East door Gar.

Garage doors have grout put
outside of doors to keep water
out. "they hope"

1+27 12° = \pm West door of Gar.

4.16

Lt.

\pm

Rt.

73

-0.4
 $\frac{4.6}{30}$

-0.4
 $\frac{4.6}{8}$

-0.5
A.7

-0.5
 $\frac{4.7}{8}$

-0.0
 $\frac{4.2}{30}$

-0.09

$\frac{4.25}{12.2}$
Apron at Bldg

-0.30

$\frac{4.46}{7.2}$
Edge
Apron

-0.2

$\frac{4.4}{6}$
Dirt

-0.3

4.5

-0.4

$\frac{4.6}{8}$

-0.44
 $\frac{4.60}{11}$
Apron

-0.34
 $\frac{4.50}{11.9}$
Gar. floor

-0.38

$\frac{4.54}{11}$
Walk

-0.11

$\frac{4.27}{12.2}$
on floor

0.07

$\frac{4.09}{12.5}$
on grout

-0.14

$\frac{4.30}{12.2}$
on floor

0.03

$\frac{4.13}{12.1}$
on grout

4.16

Alley Bk. 108 M. B

2+40

2+35 8° Rt. = End Apron. 10° Rt. = End Gar. opening

2+19 { 10° Rt. = start double garage, Conc. floor.
8° Rt. = End walk start conc. apron

2+17 Brk. in grade on E+W. walk

2+10 8° Rt. = Start (N.W. Cor.) 2' wide East + West walk

1+80

4.16

Lt.

Rt.

Rt.

74

4.6
-0.4
2.5

4.7
-0.5
8

4.9
-0.7
8

4.9
-0.7
8

4.9
-0.7
30

4.7
-0.5
8
dirt

4.63
-0.47
8
Apron
Edge

4.46
-0.30
10
Apron
Back
Edge

4.36
-0.20
10
Gar.
Floor

4.8
-0.6
8
dirt

4.63
-0.47
8
Endwalk
Edge Apron

4.49
-0.33
10
Apron
Back
Edge

4.35
-0.19
10
Gar.
Floor

4.65
-0.49
8

4.8
-0.6
8

5.0
-0.8
8

4.9
-0.7
8
dirt

4.67
-0.53
8
Edge
Walk

4.8
-0.6
2.5

4.9
-0.7
8

5.1
-0.9
8

4.8
-0.6
8

4.7
-0.5
2.5

4.16

Alley Bk. 108 Mission Beach

019.8M. (7.03)
 A 67 1.94 7.03
 -0.03 Error.

T.P. 9.68 8.94 5.70 -0.74

Reads 5.12 should be about 5.00
 Top of South cb. Ret. Broken. Top New

3+00[±] W. Cb. line Mission Blvd.

2+90[±] Meet edge paving (Taken on paving along line Mission Blvd)

2+90[±] End cb. returns. Taken concentric to Mission Blvd.

T.P. 4.91 4.96 4.11 0.05

2+50

2+49[±] 8° Rt. = Back edge pole # A 772

2+41[±] 8° Rt. = 2° wide Conc. Walk

4.16

Lt.

Rt.

Rt.

75

5.06 50 Top Cl.	5.55 50 pav	5.00 9 Top Cl. Ret.	5.48 8 pav	5.49	5.49 8.3 pav.	5.0? 7.5 Top Cl. Ret. Broken	5.56 150 pav	5.07 50 Top Cl.
-0.90	-1.39	-0.84	-1.32	-1.33	-1.33	-0.84(?)	-1.40	-1.16
.11	0.69	.09	1.07	1.01	1.00	0.80	1.00	0.80
4.85 8.05 Cl.	4.87 8.07 pav	4.95	4.96 8.38 pav	4.96 8.38 pav	4.96 8.38 pav	4.96 8.38 Top Cl.		
.10	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
4.86 8.08 End Cl. Top Cl.	4.9	5.0	4.96	4.9	4.96	4.96 8.38 End Cl. Top Cl.		
			4.96	4.9	4.9	4.96		
			1.0	1.0	1.0	1.0		
			4.9	4.9	4.9	4.9		
			4.16	4.16	4.16	4.16		

4.16

Location of sewers 6-3-47
Front + Quince

Also - Bench Marks
For Prop. Improvements

Schiller Meyer
W. Moore
L. Melton
E. Sherman

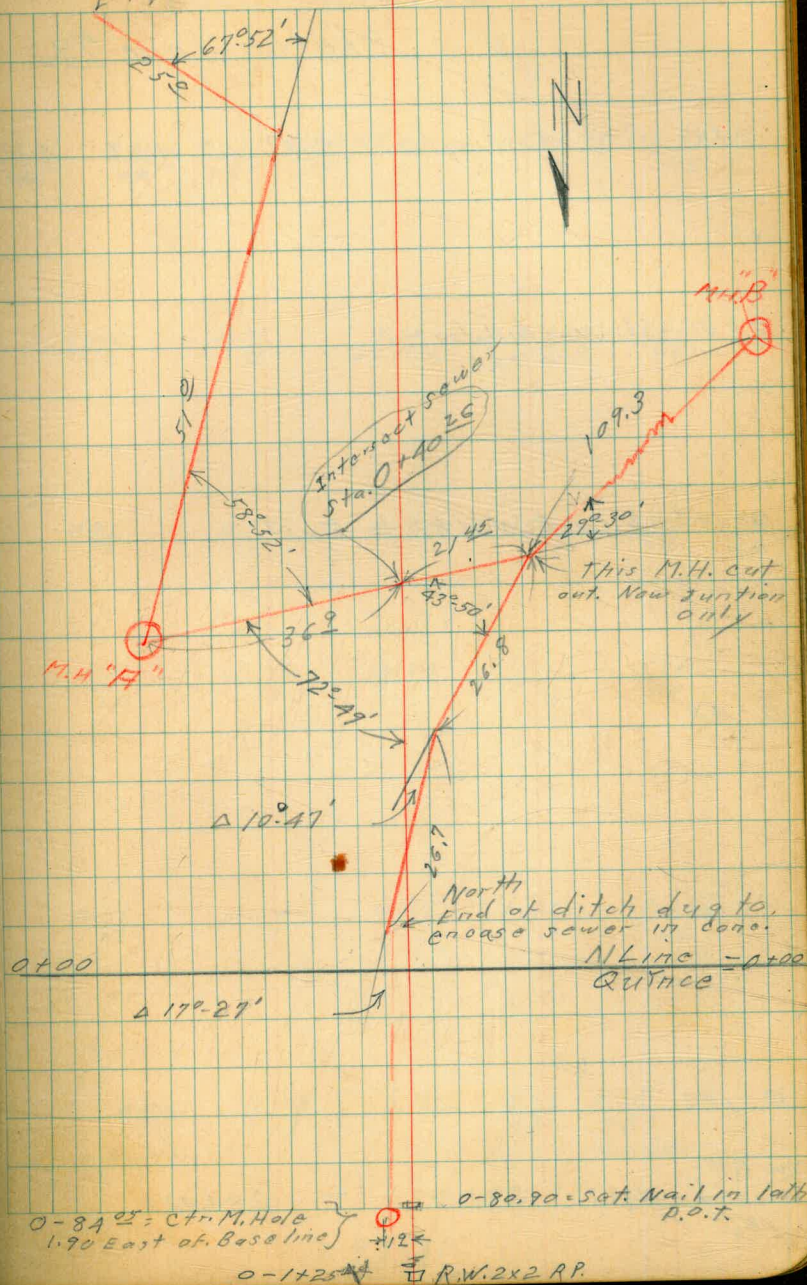
			-0.01	
N.E.B.P. Palma 1st			108.27	
Orig. B.M.	1.32		148.28	148.29
6.70	249.60	1.22	242.90	
10.54	244.12	0.76	233.58	
12.32	234.84	0.25	222.02	
11.54	222.27	0.19	210.63	
13.20	210.82	0.10	197.62	
11.97	197.72	0.24	185.75	
12.04	185.99	0.37	173.95	
13.07	174.32	0.57	161.25	
Chisel Cross N.W. side				
M.H. Rim. - Man Hole "B"	7.67		154.15	M.H. "B"
1.03	161.82	11.79	160.79	
0.22	172.58	13.27	172.36	
Chisel Cross N.W. side				
M.H. Rim. - Man Hole "A"	6.23		179.40	M.H. "A"
0.45	185.63	12.95	185.18	
0.29	198.13	12.74	197.84	
Chisel E. Back of East curb				
Front Street 230' North	2.56		208.02	M.H. "A"
N. Line Palm.				
0.66	210.58	13.05	209.92	
0.06	222.97	12.93	222.91	
0.31	235.84	13.02	235.53	
N.E.B.P.				
1st 4 Palm	0.26		248.29	
248.51	248.55		248.29	

Indexed
c.s.K.

Exposed 4"
Lateral

Φ
Front

Lined to 76.
L+T. & Palm + Front



5th + Washington
X-sec. Intersection

Indexed
C.S.K.

Sketch - Page 79

0+10 = S. Cutter line
Washington to West

$\frac{4.37}{90}$ $\frac{4.27}{65}$

0+00 = St. Washington
to West.

0-19² = S. Curb Wash. - to East.

0-40

0-70

0-100

SWBP
Wash +
5th

4.33

288.35

— 284.02

L. = West

5th

Rt = East 77

$\frac{4.71}{45}$ $\frac{4.44}{40}$ $\frac{4.63}{26}$ $\frac{4.80}{13}$ 5.01 $\frac{5.51}{13}$ $\frac{5.88}{26}$

$\frac{5.00}{26}$ $\frac{4.71}{13}$ 5.10
O.P.M.H. $\frac{5.48}{13}$ $\frac{5.96}{26}$

$\frac{4.97}{26}$ $\frac{4.77}{13}$ 4.94 $\frac{5.41}{13}$ $\frac{6.18}{26}$ $\frac{6.88}{40}$

$\frac{4.70}{26}$ $\frac{4.52}{13}$ $\frac{4.57}{13}$ $\frac{5.15}{13}$ $\frac{5.86}{26}$

$\frac{4.31}{26}$ $\frac{4.24}{13}$ 4.21 $\frac{4.65}{13}$ $\frac{5.38}{26}$

$\frac{4.14}{26}$ $\frac{3.79}{13}$ 3.82 $\frac{4.27}{13}$ $\frac{4.98}{26}$
Cutter Cutter

288.35

0+50 = N.utter Wash.
to west

$\frac{2.92}{90}$ $\frac{3.59}{65}$

$\frac{4.03}{45}$ $\frac{4.20}{40}$ $\frac{4.61}{26}$ $\frac{5.07}{13}$ 5.27 $\frac{5.97}{13}$ $\frac{6.40}{26}$ $\frac{7.05}{40}$

0+40 = N. 1/4 Washington
to west

$\frac{2.60}{90}$ $\frac{3.26}{65}$

$\frac{3.82}{45}$ $\frac{3.94}{40}$ $\frac{4.35}{26}$ $\frac{4.83}{13}$ 5.30 $\frac{5.73}{13}$ $\frac{6.04}{26}$

0+30 = E Wash. to west

$\frac{2.71}{90}$ $\frac{3.29}{65}$

$\frac{3.86}{45}$ $\frac{4.01}{40}$ $\frac{4.42}{26}$ $\frac{4.75}{13}$ 5.26 $\frac{5.70}{13}$ $\frac{5.96}{26}$

0+20 S. 1/4 Washington to West

$\frac{2.99}{90}$ $\frac{3.57}{65}$

$\frac{4.10}{45}$ $\frac{4.23}{40}$ $\frac{4.47}{26}$ $\frac{4.90}{13}$ 5.17 $\frac{5.60}{13}$ $\frac{5.91}{26}$

288.35

288.35

Aprox. Location of
Tracks - 5th + Washington

See 1768-26

Indexed
c.s.k.

50' W. West
Line 5th
250' W. West
Line 5th

W. 4. 5th

W. 4.

W 1/4

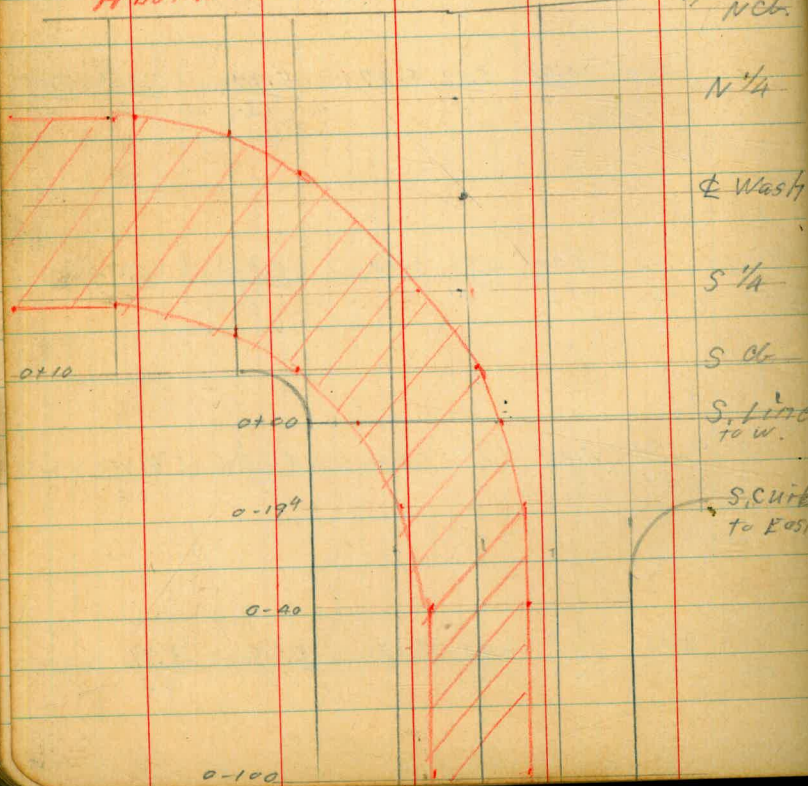
5th

E 1/4

E. Ok.

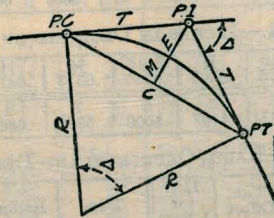
E. Line 5th

Abortive Scale



DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

- Radius— $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve— D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)
Tangent— $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve— $L = 100 \frac{\Delta}{D}$ (4)
Middle ordinate— $M = R(1 - \cos \frac{\Delta}{2})$ (5) $= R \text{vers } \frac{\Delta}{2}$ (6)
External— $E = T \tan \frac{\Delta}{4}$ (7) $= R \div \cos \frac{\Delta}{2} - R$ (8) $= R \text{exsec } \frac{\Delta}{2}$ (9)
Long Chord— $C = 2 R \sin \frac{\Delta}{2}$ (10) Δ —Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $+8\frac{1}{4} = 414.49$ ft. From Table V correction—.36 or $T = 414.85$ ft. P. C.—Sta. P. I.— $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T.—Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.—7.27 ft. Distance—158—Sta. P. C.—54.50, hence offset— $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle— $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft.—(in minutes) $.3 \times C \times D^\circ$ or—defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve—.3 $\times 54.5 \times 8\frac{1}{4} = 136.2'$ or $2^\circ 16.2'$, or— $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle— $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{4} = 115.27$ and from Table V correction—.10 or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

Page 79

76.47
58.66
17.81

177 41 4

58 50 52

58 66

N 89 48 15 E

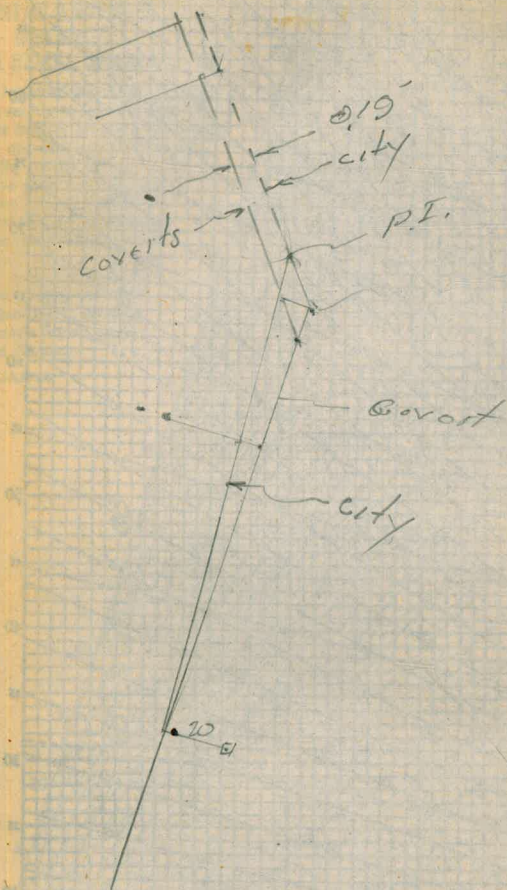
N 50 51 E

37 57 10

DIA
HORI

FR

Enter on
of the st
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run vertic
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the dotte
gives the
from the
"f+c"
be added
Distance
scale plu
g° of ver
ts the V
C



112.75
21.93

90.82



54 00 01 11.76
 36 05 50 12.1183
 90 05 51 12.7389
 179 59 60
 90 05 51
 89 54 09

382
 19.49
 401.49

53° 56' 30"

11.75

58.75
 11.75

46.00
 34.25

22.50
 11.75
 10.75

89° 13' 30"

90 06 45

11.75
 23.50
 35.25
 47.00
 58.75
 70.50

878.45
 287
 907.15
 55
 912.65

9107.15
 10.63
 9117.78

877.81
 287
 906.57
 25

431.6
 131.7
 299.9

36
 25
 61.11

314.60

166
 153
 319

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
 For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20-16)+2 or 2 ft. added to 41.9 =47.9. For slopes of 1 on 1 see inside of front cover.

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