

1694

DEEGEN
ILLUSTRATED

ENGINEERS'
LEVEL BOOK

No. 410F

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

1694

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

CITY ENGINEER'S OFFICE

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$ For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.

Copyright, 1914, by Eugene Dietzgen Co.

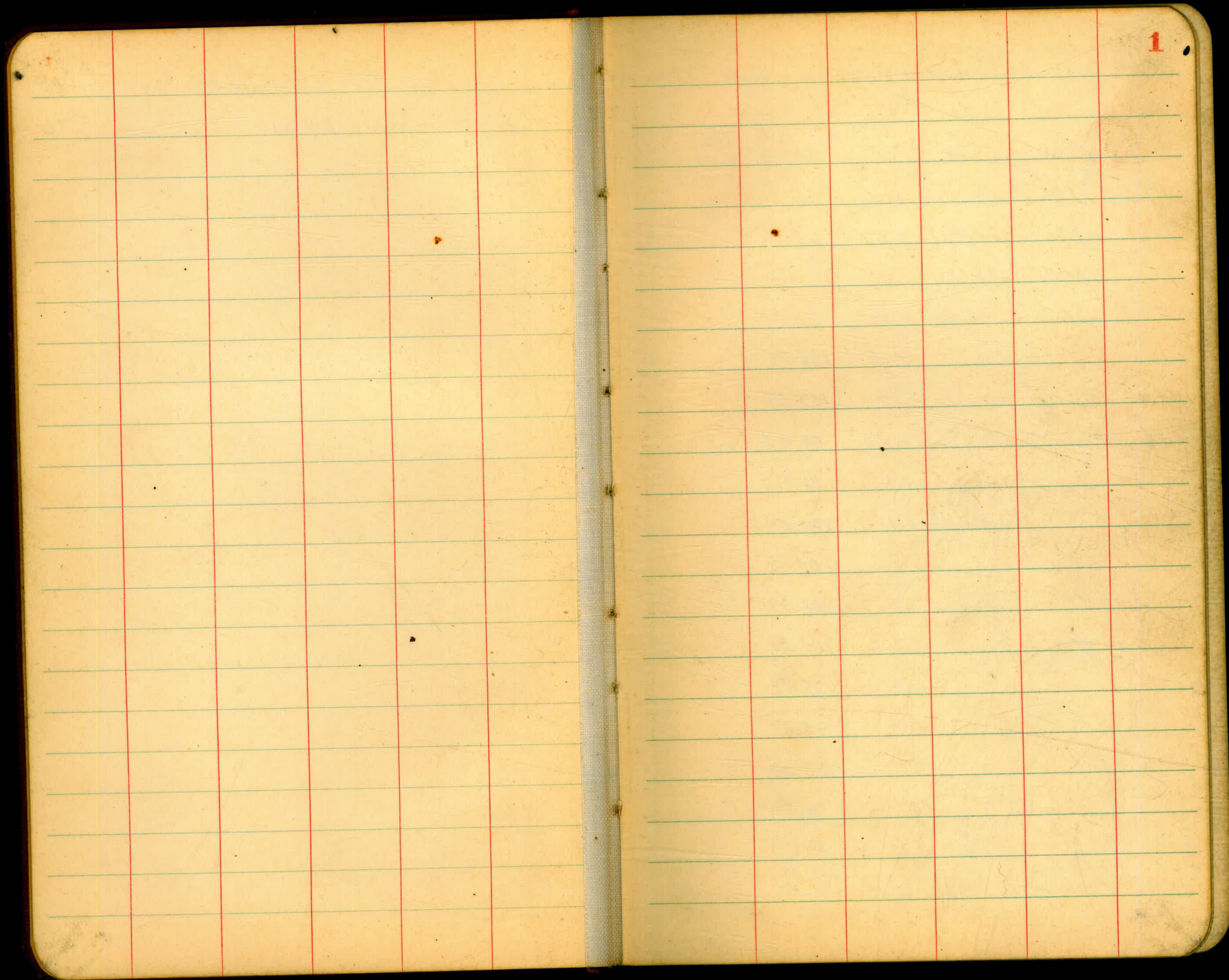
The paper stock of this book is made of a high grade 50% rag paper having a water resisting surface. This book is sewed with Bing Special Enamel Waterproof Thread.

Made in U. S. A.

X-Sect. Blk 211 Univ. Heights 68

Storm Drain Blk 211 " " 76

The paper of this book is made of a
high grade pulp paper having a water
resisting surface. This book is bound with
Eng Special Fanned Waterproof Thread.



Proposed Storm Drain

Congress + Conde St. From East Line of Old Town to Existing 6" Storm Drain South of Moor St.

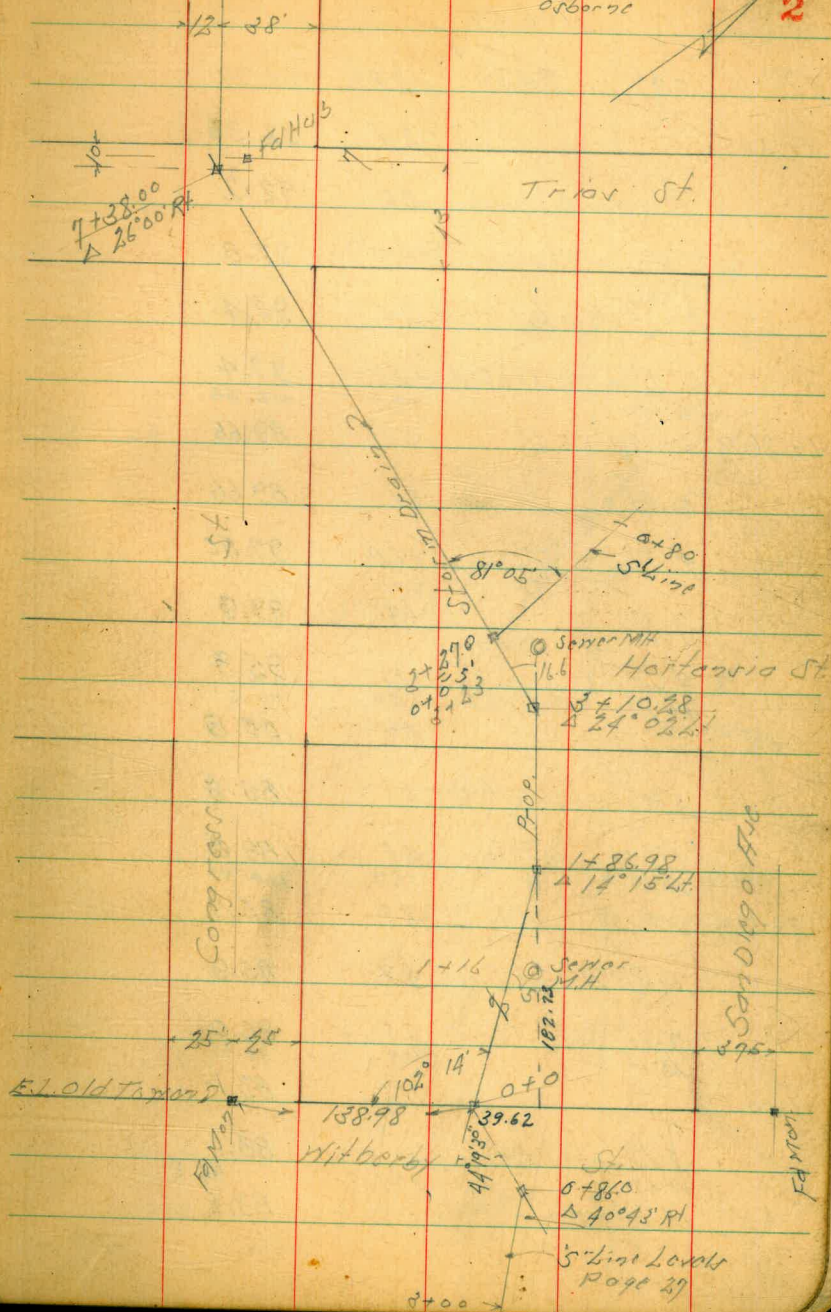
BM	4290	56.65		43.75	SE 8P 17mpudis + LaSalle
TP	12.95	69.15	0.46	56.19	
TP	12.86	81.46	0.55	68.60	
TP	12.97	94.12	0.31	81.15	
TP	12.93	106.59	0.46	93.66	
6-66	- Top New Fill		+1.98	126.39	✓
0-40	- Top New Fill		+3.0	109.59	✓
0+0	= East Line Old Town	0.24		06.35	by Hub
+50			6.6	99.99	
"	5' RT - N of Bottom Ditch	6.4		100.19	
"	7' RT - " Top "	2.4		104.19	
"	7' Lt - S of Bottom Ditch	5.2		101.39	
"	11' Lt - " Top "	0.7		105.89	
1+0			10.9	95.69	
"	2' RT		10.9	95.69	
"	4' RT		7.2	99.39	
"	9' Lt		9.8	96.19	
"	11' Lt - Top Ditch	6.2		100.29	
"	18' Lt	0.6		106.00	
1+16	5' RT of 1/2 Front MH	15.40		91.19	Floating Sewer

6526-27-28L

INDEXED
C.S.K.

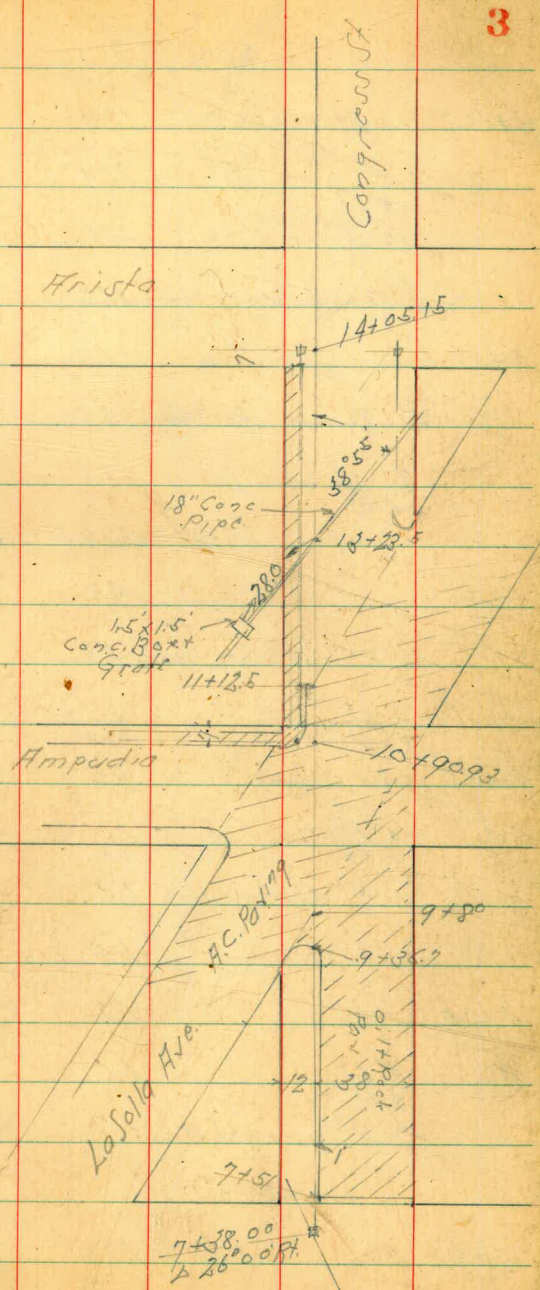
Oct 17-45
S. S. from
Bliss
0.66070

2

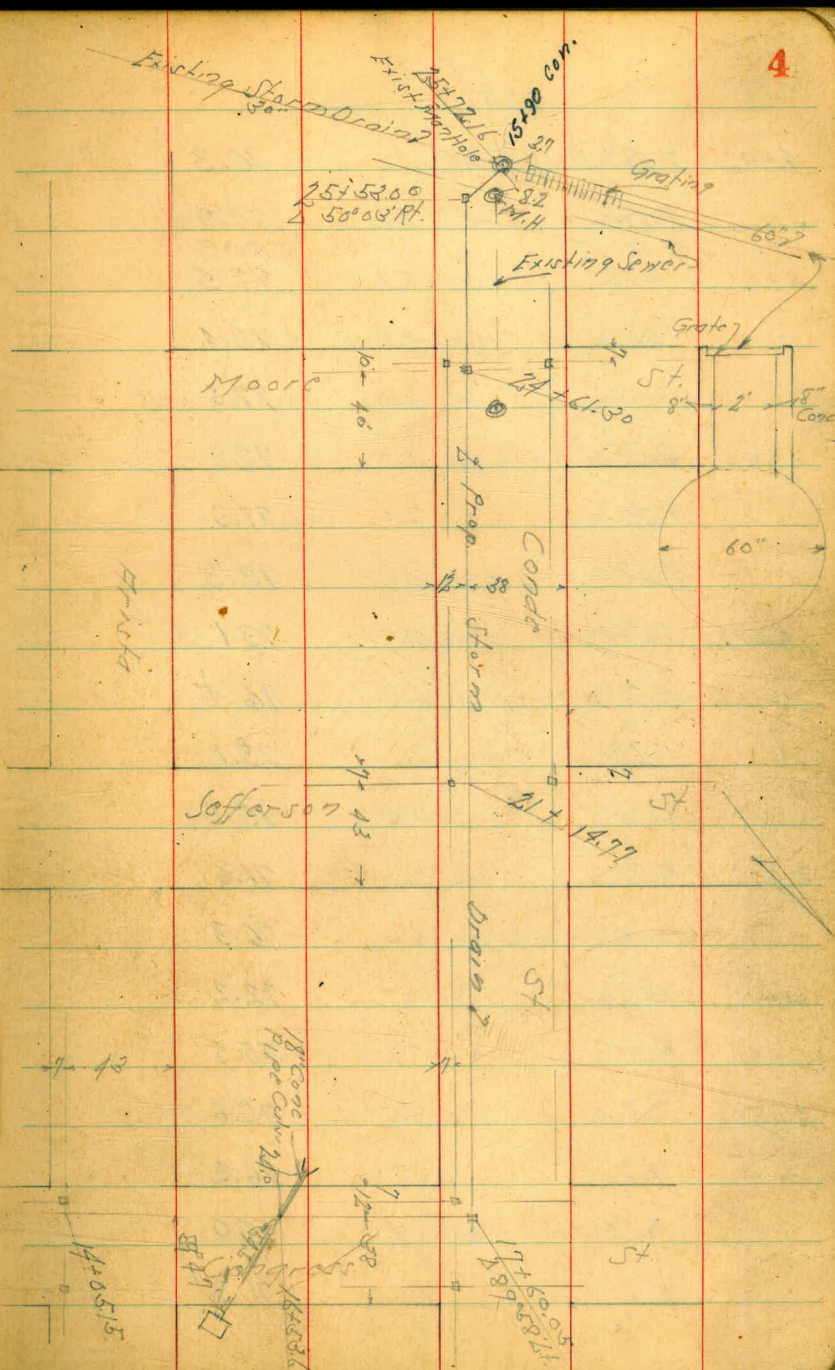


		106.59		
TP	0.97	94.76	12.80	93.79
1+50			2.4	92.36
"	6' Rt = N/4 Bot Ditch		2.5	92.3
"	8' Rt = " Top Cut		+3.0	97.8
"	6' Lt = S/4 Bot Ditch		2.4	92.4
"	8' Lt = S/4 Top Cut		+2.6	97.4
"	14' Lt		+7.9	102.66
1+86.98 = 2	14' 15' Lt		5.10	89.66
"	5' Rt		5.1	89.66
"	9' Rt		+3.0	97.80
"	7' Lt		4.9	89.9
"	9' Lt		+1.1	95.9
"	15' Lt		+5.9	100.5
2+0			6.0	88.8
"	5' Rt = N/4 Bot Ditch		6.0	88.8
"	6' Lt = S/4		5.8	89.0
"	16' Lt		+5.7	100.46
2+50			8.9	85.9
"	6' Rt = N/4 Bot Ditch		8.9	85.9
"	7' Lt = S/4		8.8	86.0
"	13' Lt		+7.9	96.46
3+0			11.2	83.1
"	3' Lt = S/4 Bot		11.7	83.1
"	11' Lt		+0.7	95.5
"	11' Rt = N		11.7	83.1

07 Hub



Station	Description	Dist	Elev	Notes
2+10.28	Δ 21° 02' Lt	12.38	82.38	on Hub
"	5' Lt - 1/4 Bot Ditch	12.9	82.4	
"	12' Lt	1.1	93.66	
"	10' Rt - 1/4 " "	12.1	82.7	
3+23	1/2 Rt of 1/2 Sewer MH	15.80	78.96	flooring
3+50		14.8	80.0	
"	5' Rt - 1/4 Bot Ditch	14.9	79.9	
"	9' Lt - 1/4 Bot " "	14.8	80.0	
"	14' Lt	4.7	90.00	
TP	1.09	82.91	12.94	81.82
4+10		4.8	78.1	
"	6' Rt - 1/4 Bot Ditch	4.8	78.1	
"	9' Lt - 1/4 " "	4.8	78.1	
"	9' Lt	4.27	85.61	
4+50	= 1/4 Ditch	5.5	77.4	
"	4' Lt - Top Cut	1.6	81.3	
"	9' Lt	0.0	82.91	
"	1' Rt - 1/4 Bot Ditch	6.3	76.6	
"	12' Rt - 1/4 " "	6.4	76.5	
4+75		6.2	76.7	
"	4' Lt	2.5	80.4	
"	8' Lt	0.8	82.1	
"	2' Rt - 1/4 Bot Ditch	6.7	76.2	
"	13' Rt - 1/4 Bot Ditch			
4+92		6.1	76.8	



82.91 ✓

4+92	8' Rt = 11/4 Bol Ditch	6.6	76.3
"	8' Lt	5.0	77.9
"	14' Lt	1.6	81.3
5+0		5.1	77.5
"	7' Rt	4.5	78.4
"	7' Lt	5.3	77.6
5+06	11/4 Cut Ditch	5.0	77.9
"	9' Rt	5.0	77.9
"	8' Lt	4.6	78.3
5+12		9.8	73.1
"	4' Rt	6.5	76.4
"	4' Lt	9.8	73.1
"	8' Lt	7.4	75.5
5+22		11.3	71.6
"	3' Rt	6.1	76.3
"	10' Lt	10.7	72.2
5+23		7.4	75.5
5+50		7.1	75.8
"	10' Rt	6.7	76.2
"	7' Lt	7.9	75.0
"	15' Lt	11.6	71.3

82.91 ✓

5

5+75		9.8	73.1
"	10' Rt	8.5	74.4
"	7' Lt	11.3	71.6
6+0		13.4	69.5
"	10' Rt	11.6	71.3
"	10' Lt	15.7	67.2
7+08		15.7	67.2
"	5' Lt	15.7	67.2
"	9' Lt	14.9	68.0
"	2' Rt	15.7	67.2
"	6' Rt	12.3	70.6
TP	0.49	70.78	12.62
6+38		5.4	65.4
"	5' Rt	5.4	65.4
"	5' Lt	2.9	67.9
6+50		2.9	67.1
"	5' Rt	3.0	67.8
"	10' Rt	3.0	67.8
"	10' Lt	3.6	67.2

70.78 ✓

6+74	29 Rt of 2 Sly Anchor Pole		
6+75		3.8	67.0
" "	10' Rt	2.4	68.4
" "	8' Lt - bot wash	6.7	64.1
7+0		3.4	67.4
" "	10' Rt	2.5	68.3
" "	5' Lt	3.9	66.9
" "	10' Lt	5.3	65.5
7+38	= 1 25' 00' Rt	5.50	65.28 <small>02 Hub</small>
7+51	= Fly O. 1/2 Back Paving	6.0	64.8
8+0		9.7	61.1
8+50		13.7	57.1
TP	0.13	58.06	12.85 57.93
9+0		4.4	53.7
+25		5.5	52.6
+36.7	= Fly O + P. Pav	7.6	50.5
+50	02 " " "	9.0	49.1
+80	= Fly H.C. Paving	12.18	45.88
10+0	02 " " "	12.84	45.22
TP	0.21	45.34	12.93 45.13 ✓

45.34 ✓

BM		1.60	43.74 ✓	SE8P Impudia + La Jolla 43.75
10+40	02 H.C. Paving	1.35	43.99	
+90.93	= 1/2 7' Disc Impudia	3.55	41.79	
11+12.5	1/4 H.C. Paving	4.34	41.00	
+50		6.8	38.5	
12+0		8.4	36.9	
+12	4' Lt = 1/4 15' Pepper Tree			
+50	35' Lt = 1/4 Pole	11.5	33.8	
+61	42' Lt = 1/4 18' Pepper Tree			
TP	0.24	32.98 ✓	12.60 32.74 ✓	
+97	35' Lt = 1/4 18' Pepper Tree			
13+0		2.2	30.8	
+23.5	= 2 Storm Drain	3.4	29.6	Top 18' Core PIPE
+44	4' Lt = 1/4 15' Pepper Tree			
+50		4.7	28.3	
+70	43' Lt = 1/4 15' Pepper Tree			
+95	35' Lt = 1/4 18' " "			
14+0		6.6	26.4	
+50	35' Lt = 1/4 Pole	8.8	24.2	
15+0		9.9	23.1	

6

3298 ✓

15479	35 Lt - 1 1/4 Power Pole			
+50		111	21.9	
1640		121	20.9	
TP	2.53	23.35	1216	20.82
+50		3.3	20.1	
+53.6	545 Ft - Inlet 18" Con. 7.83 Pipe Culvert		15.52	Flow Line
"	440 Lt - Outlet 18" Con. 9.67 Pipe Culvert		13.68	"
+73	35 Lt - 1 1/4 Power Pole			
1740		42	19.15	
+50		50	18.4	
+60.05	A 89° 58 Lt	5.33	18.02	on Hub
TP	0.15	21.75	1.75	21.60 ✓ NET on Hub Congr. + Culvert
+85		37	18.1	
1840		6.3	15.4	
+50		7.6	14.2	
+50		78	14.0	
1940		90	12.75	
+50		100	11.8	
2040		10.5	11.2	
+25		6.6	15.1	

2175 ✓

7

20450		6.2	15.6	
+75		5.8	16.0	
2140		6.7	15.1	
+16		6.8	15.0	
+50		9.2	12.5	
2240		130	08.8	
TP	0.37	9.31	12.81	8.94
+50		44	4.9	✓
+65	35 Lt 1/2 - 1 1/4 Power Pole			
2340		6.3	3.0	
+50		7.0	2.3	
2440		7.2	2.1	
+50		7.3	2.0	
2540		7.7	1.6	
+53.0	A 50° 03 Rt	8.16	1.15	on Hub
+72.16	First Storm Drain Man Hole	7.8	1.5	Ground
"		6.55	2.76	on Rim
"		17.17	-7.86	Flow Line
Sp. on C.M.H. 82.5 Storm Drain		6.85	2.46	on Rim
"	"	11.43	-2.12	Flow Line

9.31
TP 12.86 22.00 ↓ 0.17 9.14

TP 10.83 32.43 ↓ 0.40 31.60

B.M. 0.39 32.04
H.W. P.P.
Co. d.
Carpenter's
31.95

X sec of Dwight St
 Fairmont to Chamaine

80' wide

14' curbs

13' 1/4

Indexed
 C.S.K.

entrance
 Suter Meyer
 W.F.M.
 10-29-45

Chamaine to 46th

80' wide curbs 9 1/4

11/2 B.P. 5.58 3x6x7

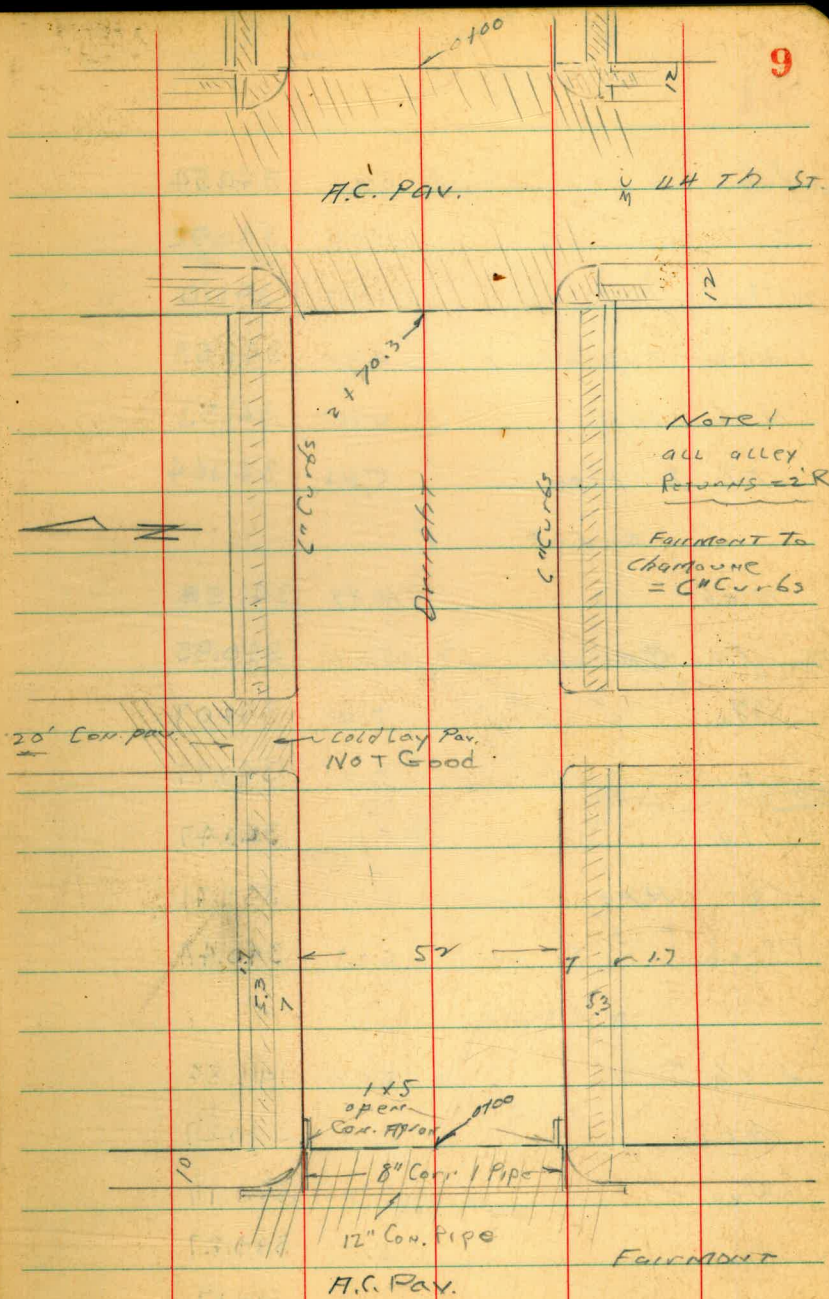
0-10 Pav

1/2 c b line	5.06	341.41
1/4	5.21	341.16
c	5.55	340.92
1/4	5.75	340.72
5 c b line	5.95	340.52

0+00 E.L. Fairmont Pav. edge

S c b top	6.06	340.41
E.L. 8" pipe	6.8x	339.63
+ 1 Hdwr. Top	5.98	340.49

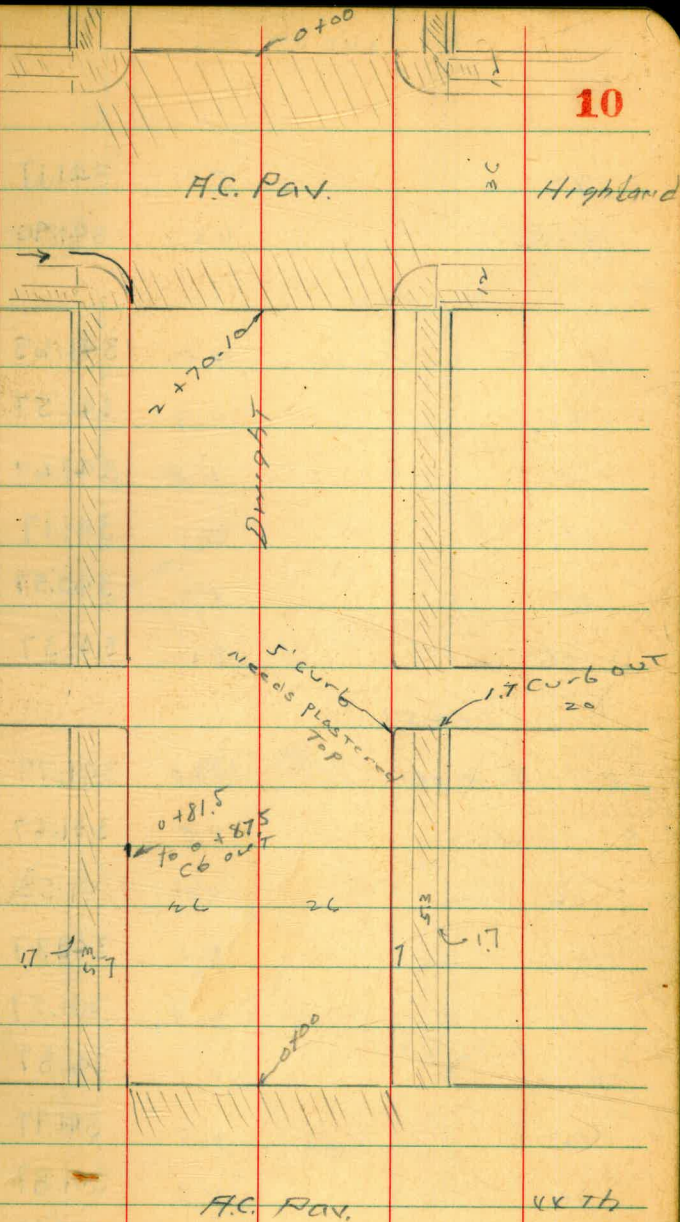
Dwight
 Fairmont



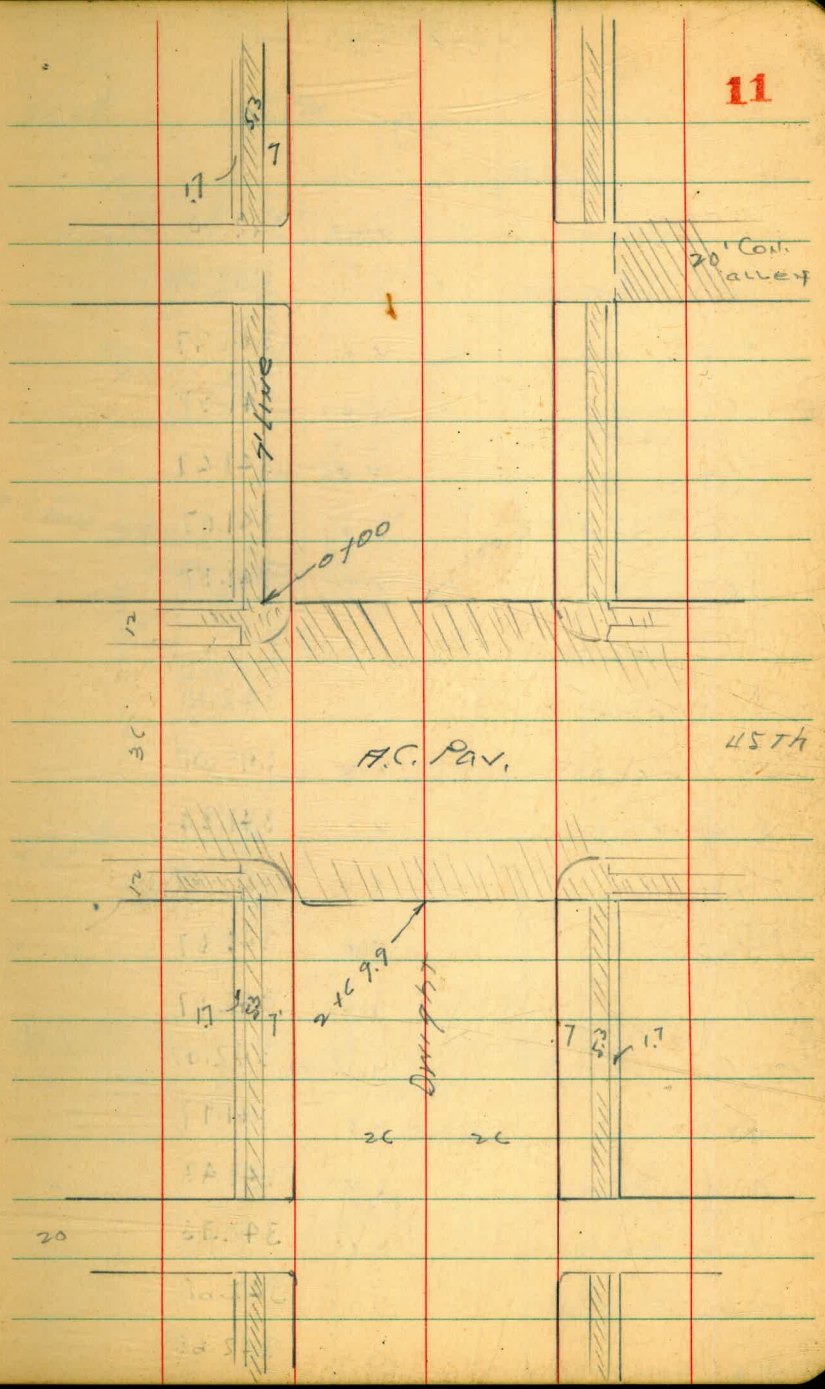
340.47

S 1/4	593	340.54
C	555	340.92
N 1/4	537	341.10
4 1/2 Top Hdwr	494	341.53
N c6, Top	494	341.53
FL 8" PIPE	523	340.64
0 + 0.5		
N c6	489	341.58
FL Apron	552	340.95
1/4	5.4	341.07
C	5.5	340.97
1/4	6.0	340.47
9.5 Apron	6.76	339.71
5 c6	6.03	340.44
0 + 5.0		
5 c6	5.23	340.84
9.7	6.2	340.27
1/4	5.7	340.77
C	5.2	341.27
1/4	5.3	341.17

10



97		5.3	341.17
N cb		4.57	341.90
/400			
N 97 in drive		4.82	341.65
1/4		4.9	341.57
c		4.8	341.67
1/4		5.3	341.17
97		5.9	340.57
S cb		5.10	341.37
/425.1			
S.L. Top. cb		4.08	341.79
S.L. drive		4.8	341.67
S cb		4.89	341.58
97		5.6	340.87
1/4		4.9	341.57
c		4.6	341.87
1/4		4.5	341.97
97		4.6	341.87
N cb		4.02	342.43
NL cb		3.80	342.61
NL Pav. Con		3.80	342.61



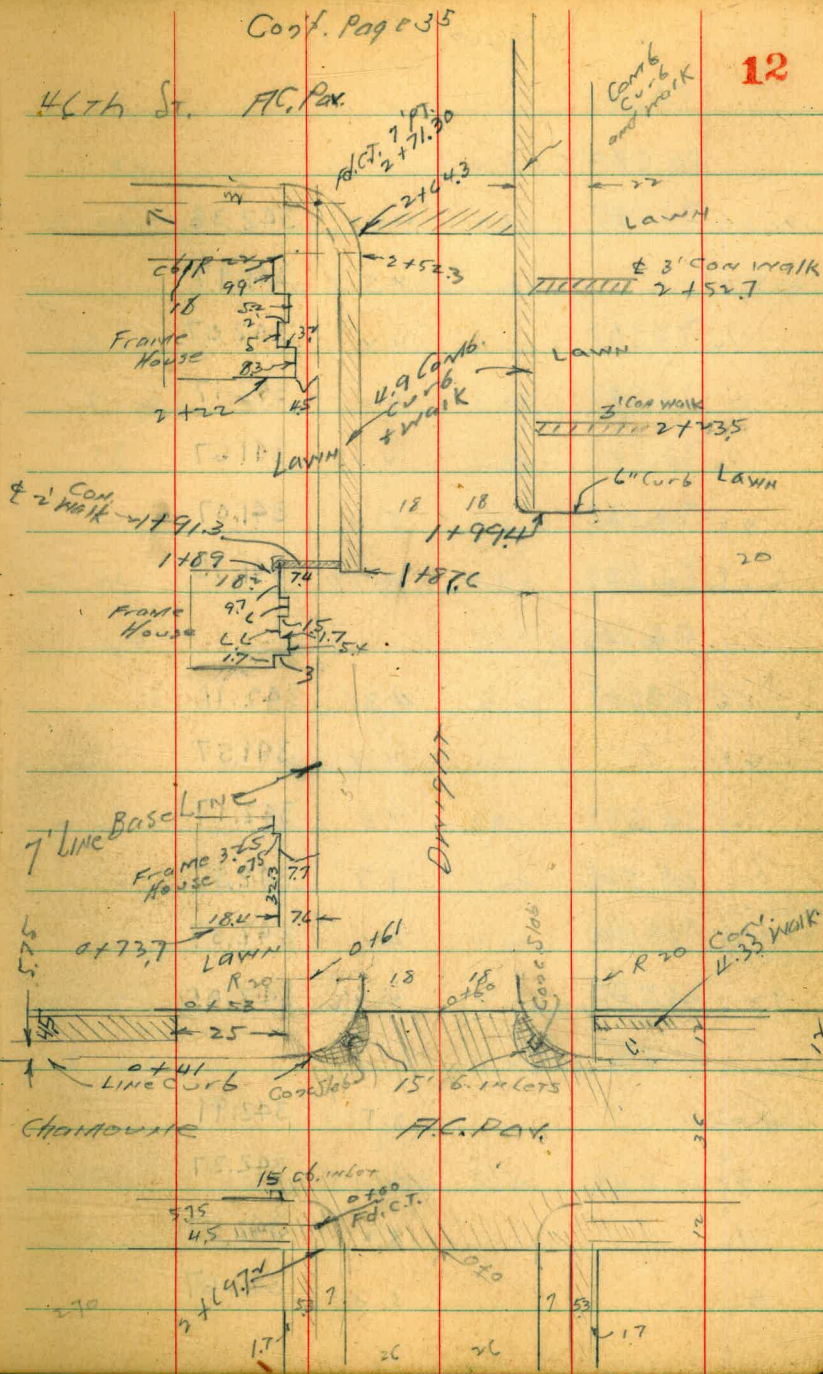
346.47

1+3.5		
NL	Con Pav.	4.7 342.40
CB	9T	4.4 342.07
1/4		4.5 341.97
C		4.5 341.97
1/4		4.8 341.67
CB	9T	5.4 341.07
SL		4.7 341.77
1+4.51		
SL	Top CB	4.37 342.10
SL	DIRT	4.4 342.07
S	CB Top	4.65 341.82
9T		5.4 341.07
1/4		4.8 341.67
C		4.4 342.07
1/4		4.4 342.07
9T		4.5 341.97
N	CB Top	3.99 342.48
+ 2	oil pav	4.11 342.36
NL	Top of oil	3.79 342.68
NL	Con Pav	3.79 342.68

See Level Notes for other IMPTS.

Cont. Page 35

12



34647

7+50

N c b 4.09 342.38

9T 4.5 341.97

1/4 4.4 342.07

C 4.3 342.17

1/4 4.8 341.67

9T 5.4 341.07

S c b 4.77 341.70

2+00

S c b 4.31 342.16

9T 4.9 341.57

1/4 4.3 342.17

C 3.9 342.57

1/4 4.1 342.37

9T in drive 4.42 342.05

2+50

N c b 3.56 342.91

9T 4.1 342.37

1/4 3.9 342.57

C 3.8 342.67

34647

13

1/4 4.0 342.47

9T 4.4 342.07

S c b 3.82 342.65

2+70.3 Pav. edge = WL 44th St

S c b 3.62 342.85

S 9T pav. 3.86 342.61

1/4 " 3.82 342.65

C " 3.82 342.65

1/4 " 3.84 342.63

9T " 3.67 342.80

N c b 3.41 343.06

2+82.3 on pav valley 9T

N c b Line pav 3.85 342.62

1/4 " 4.07 342.40

C " 4.02 342.45

1/4 " 4.12 342.35

S c b " 4.07 342.40

T.P. 6.61 349.98 3.10 343.37

Lower
St. Dept.
Should
Top this

349.98

0-12 on par. valley gnt

S cb Line 7.30 342.68

1/4 7.26 342.72

c 7.29 342.69

1/4 7.26 342.72

N cb Line 7.19 342.79

0+00 = EL 4x7H par edge

N cb 6.62 343.36

9T 7.10 342.88

1/4 6.8x 343.14

c 6.9x 343.04

1/4 6.92 343.06

9T 7.29 342.69

S cb 6.9x 343.04

0+25

S cb 6.58 343.40

9T 7.0 342.98

1/4 6.7 343.28

c 6.4 343.58

349.98

14

1/4 6.5 343.48

9T 6.8 343.18

N cb 6.31 343.67

0+43

N cb 6.13 343.85

9T 6.6 343.38

1/4 6.2 343.78

c 6.1 343.88

1/4 6.6 343.38

9T 6.8 343.18

S cb 6.27 343.71

0+60

S cb 6.06 343.92

9T 6.6 343.38

1/4 6.3 343.68

c 5.9 344.08

1/4 6.0 343.98

9T 6.5 343.48

N cb 5.71 344.27

349.98

1100

N c6	5.27	344.71
9T	5.9	344.08
1/4	5.4	344.58
c	5.2	344.78
1/4	5.5	344.48
9T	5.1	343.88
S c6	5.56	344.42

1125

S L dirt	5.2	344.78
+ 1.7 curb top	4.82	345.16
S c6	5.17	344.81
9T	5.6	344.38
1/4	5.2	344.78
c	4.8	345.18
1/4	5.0	344.98
9T	5.3	344.68
N c6	4.79	345.19
N L c6	4.65	345.33
N L dirt	4.8	345.18

349.98

1145

15

N L dirt	4.3	345.68
N L c6 top	4.06	345.92
N c6	4.31	345.67
9T	4.9	345.08
1/4	4.7	345.28
c	4.6	345.38
1/4	5.1	344.88
9T	5.3	344.68
S c6	4.72	345.26
S L dirt	5.1	344.88
S L c6 top	4.74	345.24
		344.70
S c6	4.48	345.50
9T	5.2	344.78
1/4	4.6	345.38
c	4.2	345.78
1/4	4.5	345.48
9T	4.7	345.28
N c6	4.08	345.94

349.98

2700

N cb	3.52	346.46
9T	4.3	345.68
1/4	3.9	346.08
C	3.7	346.28
1/4	4.4	345.58
9T	4.8	345.18
S cb	4.01	345.92
2+50		
S cb	3.36	346.62
9T	4.1	345.88
1/4	3.4	346.58
C	3.1	346.88
1/4	3.3	346.68
9T	3.6	346.38
N cb	2.83	347.15
2+70.1 v L Highland pav. edge		
N cb	2.52	347.46
9T	3.10	346.88
1/4	2.93	347.05
C	2.97	347.01

349.98

16

1/4	3.13	346.85
9T	3.52	346.46
S cb	3.07	346.91
532482 on pav No valley		
S cb	3.35	346.63
1/4	3.04	346.92
C	2.83	347.15
1/4	2.84	347.14
N cb	2.85	347.13
TP on BM NW 18.000 2.38 347.60 347.53		
Dwight	2.51	347.53
Highland	1.12	0.07
NWBP 352.78 347.50		
Dwight + Highland	4.68	347.53
from here EXY 4570 ?		

~~35221~~

35228 ✓

0-12 Valley gutter			
N cb line	pav	5.40	346.88
1/4	"	5.49	346.79
c	"	5.69	346.59
1/4	"	5.72	346.56
S cb line	"	5.80	346.48
0+00 EL Highland pav edge			
S cb		5.38	346.90
gt.	pav	5.76	346.52
1/4	"	5.33	346.95
c	"	5.07	347.21
1/4	"	5.08	347.20
gt	"	5.11	347.17
N cb		4.75	347.53
0+50			
N cb		4.66	347.62
gt		5.1	347.18
1/4		5.0	347.28
c		4.8	347.48
1/4		5.1	347.18

~~35228~~

35228

17

gt		5.3	346.98
S cb		5.3	347.15
	7.00		
S cb	5.1.20	5.01	347.27
gt	5.1.10	5.2	347.08
1/4	8.1.10	4.8	347.48
c	8.1.10	4.7	347.58
1/4		4.8	347.48
gt	10.1.10	5.0	347.28
N cb	11.1.10	4.5	347.83
	2.1.25		
NL cb	10.1.10	4.02	348.26
NL dirt		4.3	347.98
N cb	10.1.10	4.30	347.98
gt	8.1.10	4.7	347.58
1/4	8.1.10	4.5	347.78
c	8.1.10	4.5	347.78
1/4	8.1.10	4.7	347.58
gt	8.1.10	5.1	347.18
S cb	1.1.10	4.90	347.38
SL cb		4.67	347.61
SL dirt		4.7	347.58

352.28
~~352.21~~

	1 + 45		
SL cb	4.50	347.78	
SL dirt	4.5	347.78	
Scb Top	4.76	347.52	
gt	4.9	347.38	
1/4	4.7	347.58	
c	4.3	347.98	
1/4	4.4	347.88	
gt	4.6	347.68	
Scb	4.29	347.99	
NL dirt	4.0	348.28	
NL cb	4.06	348.22	
	1 + 70		
N cb	4.19	348.09	
gt	4.5	347.78	
1/4	4.4	347.88	
c	4.2	348.08	
1/4	4.7	347.58	
gt	5.0	347.28	
Scb	4.67	347.61	

2100

352.21
~~352.28~~

18

Scb		4.63	347.65
gt		5.1	347.18
1/4		4.5	347.78
c		4.1	348.18
1/4		4.3	347.98
gt		4.5	347.78
NL cb		4.18	348.10
	1 + 2 + 50		
N cb		3.97	348.31
gt		4.5	347.78
1/4		4.2	348.08
c		4.1	348.18
1/4		4.4	347.88
gt		4.9	347.38
Scb		4.53	347.75
	2 + 69.9 = pay edge		W.L. 457h
Scb		4.40	347.88
gt	pay	4.88	347.40
1/4	"	4.34	347.94
c	"	4.09	348.19
1/4	"	4.17	348.11

35221
35228

gt Pav.	4.40	347.88
N c6	3.96	348.32
2 + 81.9	No valley gut.	
N c6 Line Pav	4.30	347.98
1/4	4.11	348.17
c	4.11	348.17
1/4	4.26	348.02
S c6 Line	4.65	347.63

NWBP Dwight + 45TH 3.93 ^{348.35} ~~348.28~~ 348.37
0.02

19

NWBP	1.74	[✓] 350.11	348.37 + 45TH
0-12	No valley		
N c6 Line Pav.	2.49	347.62	
1/4	2.18	347.93	
c	2.20	347.91	
1/4	2.43	347.68	
S c6 Line	2.81	347.30	
0 to 00	Paved edge E.L. 45TH		
S c6	2.68	347.43	
gt Pav.	3.15	346.96	
1/4	2.67	347.44	
c	2.34	347.77	
1/4	2.50	347.61	
gt	2.83	347.28	
N c6	2.28	347.83	
0 + 12			
N c6	3.30	346.81	
gt	4.3	345.81	
1/4	3.9	346.21	

Note: N c6 line
Base line for STA.

350.11

c	3.8	346.31
1/4	4.0	346.11
gr	4.4	345.71
5 ob	3.72	346.39
0 + 50		
5 ob	7.11	343.00
gr	7.8	342.31
1/4	7.5	342.61
c	7.2	342.91
1/4	7.3	342.81
gr	7.7	342.41
N ob	6.68	343.43
1 + 00		
N ob	11.13	338.98
gr	12.0	338.11
1/4	11.6	338.51
c	11.5	338.61
1/4	11.8	338.31
gr	12.3	337.81
5 ob	11.39	338.72

20

350.11

T.P.	0.58	338.14	12.55	337.56
1 + 24.9 w/ alley				
S.L. ob		1.30		336.84
SL Pay.		1.63		336.51
5 ob Top		1.39		336.75
gr		2.1		336.04
1/4		1.7		336.44
c		1.7		336.44
1/4		1.7		336.44
gr		2.0		336.14
N ob		1.14		337.00
N L ob		1.09		337.05
366				
N L dirt		1.4		336.74
d alley				
N L		1.5		336.64
gr		2.8		335.34
1/4		2.5		335.64
c		2.4		335.74
1/4		2.5		335.64
gr		2.9		335.24
S.L. Pay		2.61		335.53

338.14

1744.9

SL cb	2.90	335.24
SL Pav.	2.98	335.16
Scb	3.32	334.82
9T	3.8	334.34
1/4	3.5	334.64
C	3.3	334.84
1/4	3.5	334.64
9T	3.7	334.44
Ncb	3.05	335.09
NL cb	2.83	335.31
NL dirt	2.5	335.64

1770

Ncb	5.27	332.87
9T	5.9	332.24
1/4	5.8	332.34
C	5.5	332.64
1/4	5.7	332.44
9T	6.0	332.14
Scb	5.48	332.66

338.14

21

2100

Scb	19.258	8.09	330.05
9T	21.658	8.6	329.54
1/4	54.855	8.4	329.74
C	31.257	8.3	329.84
1/4	11.858	8.7	329.44
9T	52.252	8.6	329.54
Ncb	02.212	7.9x	330.20

T.P. 32.85 329.03 11.97 326.17

217.50

Ncb		3.30	325.73
9T		3.9	325.13
1/4		3.9	325.13
C		2.8	325.23
1/4		3.9	325.13
9T		4.0	325.03
Scb		3.37	325.66

329.03

	2 + L 9.7	=	WL Chamoune	
S c6		5.04	323.99	
97 pav		5.45	323.38	
1/4 "		5.40	323.63	
c "		5.25	323.78	
1/4 "		5.32	323.71	
97 "		5.51	323.52	
N c6		5.03	324.00	
	W c6 Line Chamoune			2+81.7
	W c6 Line Pav.	5.88	323.15	
1/4 "		5.70	323.33	
c "		5.62	323.41	
1/4 "		5.69	323.34	
S c6 line		5.88	323.15	
NWB P	Dwight & Chamoune	5.03	324.00	324.00

NWB P
BM 7.45 331.45 324.00

30' Rdwy
22 Walks
9' 1/4"

22
Dwight
Chamoune

0+00 = Fd. NWL 7' Ct. Dwight & Chamoune

0+41 Ec6 Line Chamoune

NL c6		7.95	323.50	3+17.7
NL 97 Pav		8.63	322.82	
N c6 Line Pav.		8.64	322.81	
1/4 Pav		8.52	322.93	
c "		8.54	322.91	
1/4 "		8.68	322.77	
S c6 Line Pav		9.05	322.40	
SL c6		8.48	322.97	
SL Pav.		9.16	322.29	
	0+53 = Pav edge			3+29.7
SL dict		8.1	323.35	
+20.7 c6		8.40	323.05	
+20.7 97		9.23	322.22	
1/4 Pav		8.49	322.96	
c "		8.52	322.93	

331.45

1/4 par	8.57	322.88
cb. "	8.81	322.64
+ 1.3 qt	8.83	322.62
+ 1.3 cb	7.98	323.47
+ 7	7.3	324.15
N.L.	7.2	324.25
+ 25 ^{end of E.} _{edge walk}	7.27	324.18 ✓
o + c1 end Returns		
N.L.	7.2	324.25
+ 20	7.4	324.05
N.C.B.	7.87	323.58
qt	8.7	322.75
1/4	8.0	322.85
C	8.4	323.05
1/4	8.0	322.85
qt	9.0	322.45
S. cb	8.33	323.12
+ 2	7.9	323.55
S.L.	7.2	324.25

3+37.7

331.45

1/400		
S.L.	6.9	324.55
S cb	7.0	324.45
+ 1	7.9	323.55
1/4	8.0	323.45
C	7.0	323.85
1/4	7.4	324.05
cb	7.7	323.75
+ 1	7.0	324.45
N.L.	6.8	324.65
21 + 41		
- 0.4	5.2	326.25 ^{dirt} _{floor}
N.L.	5.2	326.25
7 + 46.5		
N + 4	4.80	326.65
N	4.85	326.60
31 + 50		
N.L.	5.1	326.35
+ 20	5.2	326.25
cb	5.8	325.65
1/4	5.7	325.75

23

3+76.7

331.45

C	MHRM	5.6	325.85
1/4		6.5	324.95
cb	around	7.1	324.35
+2		5.9	325.55
SL		5.5	325.95
1+58.8			
N+165 = S. end Lark fence			
1+60			
SL		5.3	326.15
+15		5.4	326.05
+20		5.7	325.75
cb	ground	6.9	324.55
1/4		6.9	324.55
c		5.5	325.95
1/4		5.3	326.15
cb		5.5	325.95
+2		4.9	326.55
+5		4.9	326.55
+6		4.2	327.25
NL		3.9	327.55

331.45

24

1+70			
N+7 (Tr. 10" di. acacia tree			
1+87.6			
NL		2.9	328.55
N cb	end	3.57	327.88
+1		4.3	327.15
1/4		4.0	327.45
c		4.4	327.05
1/4		5.0	326.45
cb		5.6	325.85
+1		5.0	326.45
SL		4.7	326.75
1+99.4			
SL	Top curb	4.50	326.95
SL	Dirt	4.7	326.75
S cb	Top of R. Return	4.71	326.74
97	2P. 1-2	5.3	326.15 ~
1/4	2P. 1-2	4.7	326.75
c		4.0	327.45
1/4	2P. 1-2	3.5	327.95

331.45

9T	3.7	327.75	
N cb in drive	3.66	327.79	
+ 2/1 on walk	3.0x	328.41	
N L Lawn	2.6	328.85	
2+03.3			do. 1.5 Con Ribbons gar. to drive
N-6.5 Sin gar dirt	2.3	329.15	
2+08.6			
N+10.6 S end lath fence			
2+15			
N+15 Sin gar dirt	1.8		do. 1.5 Con. Ribbons gar. to drive
2+23.5			
2+35.5 2+61.5 was error			
N L Lawn	1.8	329.65	
cb Top	2.05	329.40	
9T	2.9	328.55	
1/4	2.9	328.55	
C	3.3	328.15	
1/4	4.0	327.45	
9T	4.7	326.75	
S cb Top	4.08	327.37	
SL walk	3.24	328.21	

331.45

25

2+52.3	cb B.C. on N		1+99.3
SL on walk	2.46	328.99	
cb Top	3.21	328.24	
9T	3.7	327.75	
1/4	2.9	328.55	
C	2.5	328.95	
1/4	2.11	329.35	
9T	1.8	329.65	
N cb Top B.C.	0.82	330.63	
N L Lawn	0.3	331.15	
2+64.3 = walk 4 C + 7 =			Paving edge
N L Lawn	0.0	331.45	
+18.6 Top cb	0.37	331.08	
+18.6 pay 9T	1.18	330.27	
cb Line pay	1.19	330.26	
1/4 pay	1.33	330.12	
C "	1.77	329.68	
1/4 "	2.49	328.96	
9T "	3.40	328.05	
S cb Top	2.83	328.62	
SL Lawn	2.3	329.15	

(over)

Suggest, that 10' be excepted
in the grading on N & S side
of the block between
Charlton & 46th, that is
between property lines and
the inside edge of sidewalks.

S Line Prop Storm Drain
 Congress + Condo Sts
 Sketch Page 2

BM	1266	11901	106.35	50 Hubs 0° 40' Page 2
0+0			12.7	106.3
+13			8.8	10.2
+30			4.0	15.0
"	15 Lt		3.7	15.3
"	15 Rt		4.8	14.2
TP	12.90	131.27	0.64	118.57
+60			10.1	21.2
"	6 Rt		10.1	21.2
"	15 Rt		6.0	25.3 Top Non Fill
"	15 Lt		9.7	21.6
+75			4.8	26.5
0+860	A 40° 43' Rt		4.39	26.88 07 Stub
"	15 Rt		4.3	27.0 07 Non Fill
"	15 Lt		2.6	28.7
+10			3.6	27.7
"	15 Rt		3.8	27.5
"	15 Lt		1.5	29.8
+50			1.0	30.3
"	15 Rt		2.0	29.3
"	15 Lt		4.06	31.9

Nov. 16
 51507
 8155
 056000
 8099

27

		131.27		
TP	12.97	142.53	1.71	129.56
2+0			11.0	31.5
"	15 Rt		11.6	30.9
"	15 Lt		8.7	33.8
2+50			9.4	33.1
"	15 Rt		9.7	32.8
"	15 Lt		5.4	37.1
3+0			7.5	35.0
"	15 Rt		7.7	34.8
"	15 Lt		6.7	35.8

S' Line Prop Storm Drain

Congress + Condo Sts

Stake Page 2

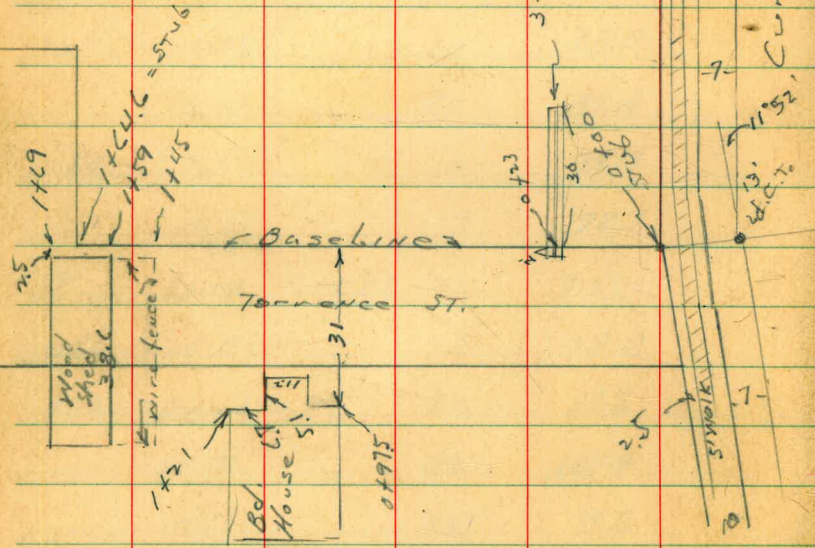
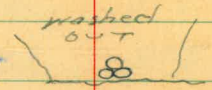
28

B.M.	12.97	95.35		82.48	on Hub 3+10.28 Page 1
040	= 2+29.0		14.03	81.32	on Stake
+09'	= Bottom Ditch		14.7	80.65	
+13	= Top Cut		7.8	87.5	
"	15' Lt		7.8	87.5	
"	15' Rt		6.6	88.7	
+30			4.0	91.3	
"	15' Rt		2.3	93.0	
"	15' Lt		5.9	89.4	
+50			1.0	94.3	
"	15' Lt		3.2	92.1	
TP	10.00	105.35	0.0	95.35	
+50	15' Rt		7.3	98.0	
+80	= Drain A to Rt.		8.1	97.2	
"	15' Rt		4.9	100.4	
"	15' Lt		5.8	99.5	

Xsec Terrace ST 24.4 wide

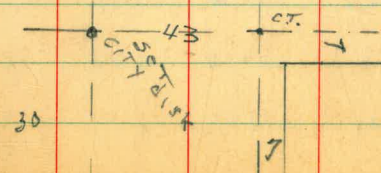
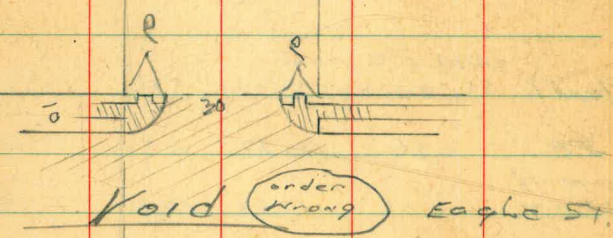
curlew vly.

CSM
CS
W-M
11-23-45



Indexed
C.S.K.

Terrace



Levels on Torrence
N.L. = Baseline

0+00 at 90°

0+00 W of Curlew

0-10 W of Curlew

0-10 W of Curlew

13' d. C.T. 0.13 147.60 141.47

Chisel & Gutter
Check to S.L. Brooks - SE Cor 5.86 147.01 147.03
0.02

T.P. 2.84 152.87 11.60 150.03

T.P. 13' d. C.T. 0.16 141.63 10.83 141.47 / at Torrence
and Curlew

T.P. 0.06 172.30 12.45 172.24

T.P. 0.23 184.69 12.77 184.46

SE Ret. 0.10 197.23 197.13 Curlew
S.L. Pennic + Pennic

LT

B.L.

Rt

30

160.13
7.3
24.4

160.3
7.3
24.7

160.05
7.55
24.9

159.44
8.16
24.9

161.16
14

161.20
14

161.80
5.80

161.16
14

147.60

= GB. 128-28

0 + 31

0 + 28

0 + 23

0 + 20

0 + 17

0 + 13

0 + 03

16760

LT.

8.590
8.0
24.4

8.590
8.6
24.4

8.590
8.6
12

11.9
5
55.7

10.4
10.4
57.2

7.0
7.0
60.6

10.4
8
57.4

10.4
20
58.0

31

38.8
8.8
8.0

38.6
9.0
24.4

38.9
11.7
12

38.9
10.7
5

32.4
15.2
5

36.7
10.9
10.4

38.3
9.3
7.0

34.3
13.3
10.4

37.5
10.1
20

11.4
8.0

11.5
24.4

12.7
12

15.9
8

16.3
2
FL. Pipe

10.4
10.4

12.4
12

15.3
30
FL. INLET

14.1
8.0

13.2
24.4

16.0
16.0
12

14.9
14.9

12.3
12

17.6
8.0

12.7
24.4

14.5
12

11.7
11.7

13.7
13.7

17.6
8.0

16.7
24.4

12.1
12

10.7
10.7

13.7
13.7

160.3
7.3
24.4

161.20
161.20

16760

1132

1121

T.P. 11.69 181.24 0.14 169.55

0+97.5

0+82

T.P. 6.19 169.69 4.10 163.50

0+57

0+38

167.60

LT.

B.L.

R.

32

	11.697	72.3	72.7	72.8	72.0
	<u>11.5</u>	<u>8.9</u>	<u>8.5</u>	8.4	<u>8.4</u>
	36	24.4	12		20

	67.0	166.84	68.88	69.5	72.0	72.0
ground	<u>14.7</u>	<u>14.4</u>	<u>12.80</u>	11.7	<u>9.4</u>	<u>9.2</u>
next con	31	24.4	12		6	20
house						

181.24

27	ground	10.8	10.0	10.0	26.8	11.0	10.9
Floor	con.	<u>31</u>	<u>24.4</u>	<u>12</u>	2.9	7	20
el.	house						

	58.3	58.8	58.0	58.1	63.2	68.1	68.4
	<u>11.4</u>	<u>11.9</u>	<u>11.7</u>	<u>11.0</u>	6.5	8.0	1.1
	35	24.4	12	10		20	20

	58.6	58.2	57.6	57.1	58.0	64.6	64.6
	<u>7.0</u>	<u>9.4</u>	<u>10.0</u>	<u>10.5</u>	8.0	10.0	10.0
	35	24.4	12	8		20	20

	59.2	59.2	60.2	56.0	57.1	64.3	64.2
	<u>8.4</u>	<u>8.4</u>	<u>7.4</u>	<u>11.0</u>	10.5	3.0	3.4
	35	24.4	12	3		13	24

167.60

S. edge dyke

S. edge N. edge

Dyke

check to 13' ld C.T. 7.57 161.46 161.47

T.P. 13.2 169.13 131.2 167.81

Z.P. 0.38 180.93 12.84 180.55

2+25

✓

1+666

7.P. 12.84 193.39 0.69 180.55

1+53

181.24

LT

B.L.

R

33

201.59

+8.7
36

92.2
1.1
35

201.4

+8.0
24.4

92.4
1.0
24.4

98.8

+5.4
12

92.2
1.2
12

98.2

+4.8
20

91.5
1.9
20

97.3

+3.5
20

91.2
2.1
20

97.4

+5.0
55

91.4
5.1
55

81.5
11.9
24.4

81.5

11.9
12

81.5

11.9
20

81.4

12.0
20

82.4

11.0
55

193.39

78.1
3.1
35

78.2
3.0
24.4

77.8
3.4
12

78.3
2.9
1

78.3
2.3
1

78.9
1.4
4.4

78.7
7.5
18

78.9
1.3
25

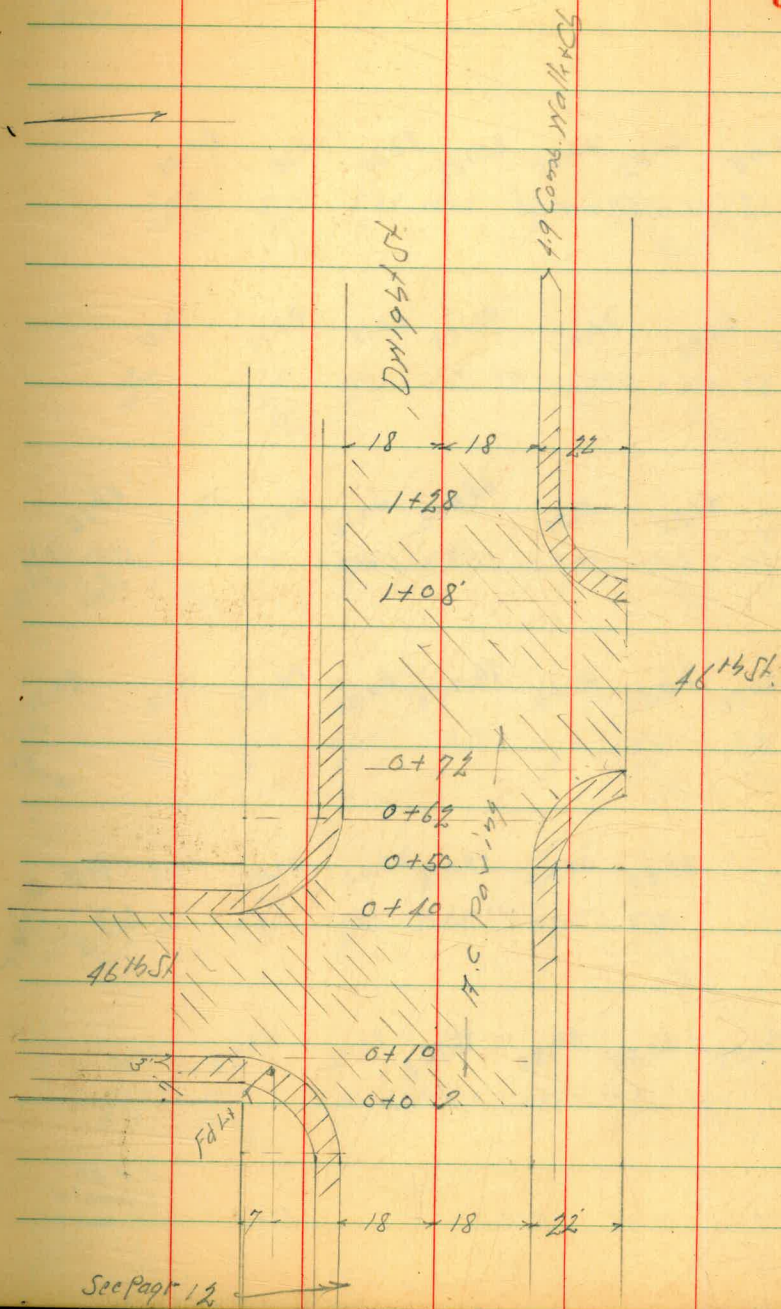
181.24

Cross Section Dwight St. At 46th St.

Levels next Page

indexed
c.s.k.

34



See Page 12

Cross Section Dwight St. At 48th St

Sketch Page 34

0+62 = Cb EC on Wt

0+50 = Cb BC on Rt

0+40 = EC Line of 48th to North

0+25

0+10 = WCb Line 48th to North

0+0 = Wt 48th St to North - Wt

BM 10+56 334.36 334.00

11th St
Dwight +
Chalmers

307.25-46
S. 3300
Osborn
3099

Lt. W

2

Rt. 5

35

32.27 31.65 31.53 331.33 30.66 29.66 30.39
2.09 2.71 2.83 3.03 2.70 4.70 3.97
18-Cb 18-Gut. 9 9 9 20.7-Gut 20.7-Cb

31.95 31.64 31.33 331.10 30.45 29.63 30.17
2.41 2.72 3.03 3.26 3.91 4.23 4.19
21.4-Cb 21.4-Gut. 9 9 9 18-Gut. 18-Cb

31.93 31.52 31.20 31.06 330.83 30.18 29.36 29.83
2.43 2.84 3.16 3.30 3.53 4.18 5.00 4.53
40-Cb 40-Gut. 18 9 9 18-Gut. 18-Cb

32.08 31.45 30.89 30.69 330.41 29.76 28.85 329.40
2.38 2.91 3.47 3.67 3.95 4.60 5.51 4.96
65-Gravel 40 18 9 9 18-Gut. 18-Cb

31.19 30.71 30.52 30.35 329.92 29.30 28.54
3.17 3.65 3.84 4.01 4.44 5.06 5.82
40-Cb EC 40-Gut. 18 9 9 18-Gut. 18-Cb

31.13 30.32 30.17 329.71 28.98 28.06 28.64
3.13 4.04 4.19 4.65 5.38 6.20 5.72
21.5-Cb 21.5-Gut. 16 9 9 18-Gut. 18-Cb

334.36

1+28 = C6 FC 02 Rt

1+08 = F C6 Line 46th to South

0+90

0+72 = H, C6 Line 46th to South

23436

Lt.

R

Rt

36

33.93	33.11	32.85	332.44	31.79	30.94	31.29
0.12 18-cb	1.25 18-sub	1.51	1.92	2.57 9	3.42 18-sub	3.07 18-cb

33.39	32.66	32.45	332.07	31.38	30.47	30.44	30.55	30.96
0.99 18-cb	1.70 18-sub	1.91 9	2.29	2.98 9	3.89 18	3.92 20	3.81 40-sub	3.40 40-cb

32.96	32.25	32.08	331.75	31.06	30.18	30.15	30.66
1.40 18	2.11 18	2.58 9	2.61	3.50 9	4.18 18	4.21 20	3.70 40-sub

32.54	31.84	31.73	331.46	30.83	30.00	29.83	29.87	30.42
1.82 18-cb	2.52 18-sub	2.63 9	2.90	3.52 9	4.26 18	4.50 20	4.49 40-sub	3.91 40-cb

33

Cross Section Drivest St At Chamounc St

Sketch Page 12

+60 = E.L. Chamounc = Fly Paul Mix Pav 129

+51.7

+48 = F.C. 6 Line

+30 = Chamounc

+12 = H.C. 6 Line

0+0 = H.L. Chamounc St = 1/4 plant Mix

BM

371

327.71

324.00

N.H. & P.
Drivest +
Chamounc

Feb 13-46
S. 1007
S. 1008
S. 1009
W. 1001

Lt. 11

2

Rt. 5

37

323.49	322.57	322.87	322.95	322.97	322.22	323.05
4.22 19.8-Cb.	5.14 19.8-Cb.	4.84 10.	4.76	4.74 10	5.49 20-Gutter	4.66 20-Cb
323.49	322.53	322.59	322.73	322.85	322.93	322.72
4.42 20	5.18 20-Gutter	5.14 20-Gutter	4.98 20-Gutter	4.86 13	4.78	4.99 10
323.49	323.54	322.88	322.64	322.91	322.92	322.65
4.42 20	4.17 10-Cb	4.83 10-Gutter	5.07 20-Gutter	4.80 13	4.79	5.86 13
32402	323.90	323.04	323.11	323.15	322.96	322.81
3.69 20-Gutter	4.81 10	4.67 26	4.60 13	4.56	4.75 13	4.90 26
32209	323.97	323.42	323.17	323.35	323.43	323.29
4.62 20-Gutter	3.74 20-Cb	4.89 10-Gutter	4.54 26	4.31 13	4.28	4.42 10
32402	323.53	323.69	323.78	323.58	323.37	323.99
3.69 20-Cb	4.18 20-Gutter	4.82 10	3.93	4.13 10	4.34 20-Gutter	3.77 20-Cb

327.71

Check Cross Sections

C. Moore
S. Moore
W. Moore
Dwight St. Chamaine Ely

B599 4-1-46

NW1/4 7.45 331.45 324.00 Dwight Chamaine

W 7' Line Chamaine = 0 + 100

1 + 87.6 from p 24

Top N cb. end 3.56

1 + 99.4

S.L. Top cb. 4.51

S cb " " 4.70

N cb in drive 3.65

steeply
ramped
drive

+ 2.1 on walk 3.03

+ 4.9 N edge walk 2.97

~~2 + 3.5~~ (error) on p. 25
No section taken here
2 + 23.5 = 0.K.

N cb TOP 2.05

S " " 4.09

SL walk 3.23

2 + 52.3

S cb TOP 3.24

N cb " B.C. 0.81

Re-cross Section of 15' N x S alley

BLK. 37 Normal Hts.

B.M. SEB9 Adams & 32nd destroyed

See Sketch FB. 1590-72

W.L.
Top
B.M. Cur 6
0+00

4.72 387.76 383.04 1590-72
515304

0-12 N of Madison Ave

E Pav. } 5.67 382.09

C " } Cold Lay Patch 5.51 382.15

W " } 5.56 382.20

0+00 N. of Madison

W Top 6. 4.72 382.04

W Pav. 4.88 382.88

C " 5.28 382.48

E " 5.30 382.46

E Top 6. 5.22 382.54

0+8.5

E 4.3 383.5

+2 4.9 382.9

G 5.0 382.8

+5 4.9 382.9

387.76

W 3.8 384.0

+0.4 E.L. Tap 2' Con. Walk 3.32 384.44

0+15

E-0.5 Dep. picket fence & wire

0+38.5

W-0.2 E.L. M. end 2' Con. Walk 3.35 384.41

0+46

W-4.9 9' Six 900, 3.41 384.35 Con. fl.

W+0.1 " Con. apron 3.59 384.17 7' wide

C 4.0 383.8

+4 4.0 383.8

E 3.4 384.4

0+50

E-0.7 end wire fence
800. 800.

0+53

W+1.4 E 12" P.P.

0+61

W-1.3 1.5 Con. walk 3.45 384.31

387.76

TR 5.17 389.14 379 383.97

0+64

W-04 SE Con C corr gar 4 Cor. gar's face West

0+71

E 5.0 384.1

C 5.1 384.0

W 4.6 384.54

+0.4 E S. gar 4.55 384.59 Con fl.

0+76

E-0.1 End Bd. fence + Beg Bd. Shed

0+97

E-0.7 end Bd. Shed, Beg Bd. fence

1+17

W-0.2 E Nly gar. 4.51 384.63 con fl.

W 5.0 384.1

C 5.1 384.0

E 5.2 383.9

+2.5 5.2 383.9

1+20

E-0.6 end Bd. fence
Beg " Shed

389.14

40

1+24

W-0.2 NE Con. C corr gar

1+26

W-0.1 E 1.5^{CON. WALK} 4.14 384.50

1+27

E-0.8 end Bd. Shed + Beg wire fence

1+50

-2.5 5.4 383.7

-1.4 end wire fence

E 5.2 383.9

C 5.0 384.1

W 5.0 384.1

+2.5 4.8 384.3

1+57

E-0.6 E S. gar, 5.0 384.1 dirt

1+62

E-0.6 Beg. Bd. fence

1+68

E-0.3 A in Bd. "

389.14
2

1+09

W-17 Beg wire fence

1+99

W-20

5.3 383.8

-15 end wire fence

W

5.1 384.0

C

5.3 383.8

E

5.7 383.9

+20

5.3 383.8

2+01

E 0.4 end Bd. fence + Beg. Bd. shed
ON LINE

2+15

E +0.1 end Bd. Shed + Beg. picket fence

W-5.5 E Sim. gap, 5.1 384.0 dirt fl.

2+28

W+2.1 E 16" R.P.

T.P. 4.53 388.84 4.83 384.31

388.84

41

2+30

-25

4.7 384.1

-1

5.1 383.7

E

5.0 383.8

C

4.9 383.9

W

4.6 384.2

+15.4 E Sim. gap 4.5 384.3 dirt fl.

2+50

W +1.5 edge Beg. Cypress hedge

W-12 Hedge roots, prop. owner says she
is going to take out.

E +0.4 picket fence

2+52

W-2.5 E 18" di. Eucalyptus

2+85

-10

4.4 384.4

-1.3 end hedge, same out.

W-1.4 Beg. Bd. fence

W

4.6 384.2

C

4.7 384.1

+7 Picket fence

E

4.5 384.3

+10

4.4 384.4

	3+00			
E	+0.5	end picket + Beg. wire fence		
	3+33			
E	-10	v.c	384.2	
E	+0.3	end wire fence + Beg. Bd. Shed		
E	+0.3	v.c	384.2	
C		v.8	384.0	
W		v.7	384.1	
	+0.8	Picket fence		
	+10	v.5	384.3	
	3+50			
E	+0.7	end Bd. Shed + Beg. Bd. fence		
T.P.	6.00	<u>389.59</u>	5.25	383.59
	3+52			
W	-10		5.6	384.0
W			5.5	384.1
C			5.8	383.8
E			5.0	384.6
	+10		5.5	384.1

	3+62.5			
E	Line ^{on} 4' Com walk	5.55	384.04	
	3+65			
E	+0.7	end Bd. fence + Beg. Bd. Shed		
	3+79			
E	-1.3	end of Bd. Shed		
E	+0.3	Beg. Bd. fence		
	3+84			
W	+1	2 1/2" P.P.		
	4+00			
E	-10		5.3	384.3
E			4.8	384.8
	+0.5	End Bd. fence + Beg. Shed		
C			5.2	384.4
W			4.9	384.7
	+0.7	end picket fence + Beg. Bd. fence		
	+10		4.8	384.8
	4+19			
E	Line ^{on}	end Bd. Shed + Beg. Bd. fence		

389.59

4+50

W-15 5.3 384.3

W 4.7 384.9

+0.1 end Bd fence

C 4.9 384.7

E 4.8 384.8

+1' end Bd fence + Beg. wire fence

E+15 5.1 384.5

4+65

-8 4.9 384.7

E 4.6 385.0

C 4.6 385.0

W 4.4 385.2

+15 4.6 385.0

4+87

E-0.7 end wire fence

4+92

W-0.7 E 12' Con. slab 4.24 385.35

Future
gar.
W. entrance

4+93.5

W-0.7 Con. slab 4.24 385.35

389.59

43

W 4.6 385.0

C 5.3 384.3

E 5.3 384.3

+0.8 E sim. gar. 4.52 385.07 Con. sl.

5+00

W-0.7 S.E. Cor. Succogar. W. entrance

5+19

E-10 5.3 384.3

E 5.6 384.0

C 5.3 384.3

W 4.9 384.7

+0.7 ^{Stucco} N.E. Cor. gar. W. entrance

+1' Beg. Lath fence 4.6 385.0

+10 4.6 385.0

5+25

W +0.6 E 12" P.P.

5+51

-10 4.5 385.1

-0.4 end Lath fence + Beg. wire fence

W 5.0 384.6

C 4.8 384.8

389.59

E		5.1	384.5
W	+0.1	Boq. Bd fence	
	+10		4.7 384.9
		5+86	
E-0.7	±	4' Con. Walk	4.63 384.96
"	-0.1	= Bd fence	
		5+99	
E		4.7	384.9
C		4.5	385.1
W		4.4	385.2
W to 2	end wire fence + Boq. L ^o h fence	4.3	385.3
			W-1.8
T.P.	5.70	390.65	4.64 384.95

6+21

W to 2 E 14" P.P.

6+22

W-4.1	±	2' Con. Walk	5.36 385.29
W			5.6 385.1
C			5.4 385.3
E			5.3 385.4

390.65

44

6+27

W-2.5	end Lath fence		
"	"	5 E. Con. 900. N. entrance	
		6+46	
W-2.6	N E Cor	"	"
		6+49	

E		5.0	385.7
C		4.9	385.8
W.		4.9	385.8

6+50.67 = S.W. of E + W alley paved

W	on Pav.	5.56	385.09
C	"	5.55	385.10
E	"	5.54	385.11

EL. 3 rd		5.03	385.62	385.58
N L alley top curb,				↑

1590-77

BM	2.57	391.66	389.09	N.E. BP Hdout W.M. Stone
S&B M	4.77	390.56	385.79	S.E. BP Hdout
FL 32 nd N L Alley	4.99		385.57	

Walker
Handricks
Hartley
Curey
6-23-46

CROSS SECTION - SEA BREEZE

From Cumberland to Edgewater

10' cbs.
50' wide 75' 1/4"

See Roll # 4464 - Plan sheet # 2

" " " - Profile " # 20

B.M. S.W. B.P. SEA BREEZE (CUMBERLAND

F.B.

1692.26 10.27 257.92 241.95

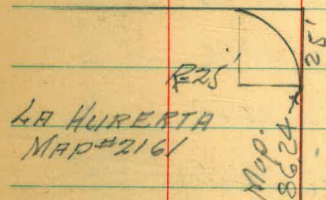
N.L. Cumberland

-10	12.7	40.2
W	12.55	40.4
cb.	12.55	40.37
Gut.	13.2	39.7
1/4	13.1	39.8
2	12.6	40.3
1/4	12.9	40.0
cb.	12.5	40.4
E	11.7	41.2
+10	10.8	42.1
N cb.		
-10	10.6	42.3
E	11.2	41.7
cb.	12.0	40.9

Indexed
c.s.k.

45

Edgewater



Subdivision Line 25' 15' 10'

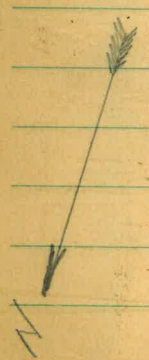
Existing curb

Prop. Line

0+00

Cumberland St.

Conc. Paving



20.4'

15' 10'

27.50
10'
40'
10'

N cb.

252.92

E 1/4	127	40.2
£	122	40.7
W 1/4	127	40.2
Gut	126	40.3
W Gut	1266	40.26
W cb.	1208	40.84
+10 on cb	1232	40.60
" Gut	1294	39.98

N 1/4

-10 on Pass	1238	40.54
W " "	1215	40.77
+46 " "	1128	40.94
cb.	120	40.92
1/4	121	40.8
£	116	41.3
1/4	112	41.7
cb.	108	42.1
E	103	42.6
+10	100	42.9

252.92

S Cumberland

46

-10	9.6	43.3
E	10.2	42.7
cb	10.3	42.6
1/4	10.6	42.3
£	11.2	41.7
1/4	11.7	41.2
cb	11.6	41.3
+56 on Pass	11.59	41.33
W " "	11.67	41.25
-10 " "	11.87	41.05
S 1/4		
-10 on Pass	11.86	41.06
W " "	11.63	41.29
+46 " "	11.54	41.38
cb.	11.2	41.7
1/4	11.3	41.6
£	11.0	41.9
1/4	10.5	42.4
cb.	10.0	42.9
E	9.5	43.4
+10	8.4	44.5

25292

S curb Cumberland

-10		7.5	45.4
E		7.7	45.2
+8.5	0.5' South = N edge Guy Pole		
cb		7.7	45.2
1/4		8.5	44.4
+8		9.7	43.2
E		10.0	42.9
1/4		10.8	42.1
cb		11.2	41.7
+4.6	on Pav.	11.40	41.52
W	" "	11.59	41.33
"	on cb	10.95	41.97
+10	" "	11.25	41.67
"	" Gut.	11.90	41.02
	0+00 = V. line Cumberland		
-10		8.2	44.7
W		8.8	44.1
+5		10.4	42.5
cb		10.36	42.56
Gut.		10.9	42.0
1/4		10.7	42.2

25292

SEA BREEZE

47

1/4+5'		10.1	42.8
E		8.1	44.8
+2		7.7	45.2
1/4		7.4	45.5
cb		7.3	45.6
E.L.		7.2	45.7
+10		6.6	46.3
	0+25		
-10		4.9	48.0
E		5.2	47.7
cb		5.6	47.3
1/4		5.3	47.6
+6		5.6	47.3
E		6.9	46.0
+2		8.6	44.3
1/4		9.1	43.8
Gut.		9.2	43.7
cb		8.47	44.45
+6		8.3	44.6
W		6.5	46.4
+10		6.4	46.5

25292

0+50

-10	42	48.7
W	4.0	48.9
+1	6.4	46.5
cb	6.37	46.55
Gut.	7.3	45.6
1/4	7.2	45.7
+5	6.7	46.2
∅	4.7	48.2
+2	3.7	49.2
1/4	3.4	49.5
cb.	3.7	49.2
E	3.3	49.6
+10	3.2	49.7
0+76 = PVC 100' V. curve		
-10	1.3	51.6
E	1.6	51.3
cb.	1.9	51.0
1/4	1.9	51.0
+5	2.0	50.9
∅	4.1	48.8
+2	4.9	48.0

25292

48

1/4	5.4	47.5
Gut.	5.4	47.5
cb.	4.31	48.61
+7	4.5	48.4
W	3.2	49.7
+10	3.6	49.3
1+01		
-10	2.6	50.3
-1	2.2	50.7
W	2.8	50.1
+1	3.1	49.8
cb.	3.01	49.91
Gut.	3.8	49.1
1/4	3.8	49.1
∅	3.1	49.8
+5	1.2	51.7
1/4	0.7	52.2
cb.	0.9	52.0
E	0.6	52.3
+10	0.4	52.5
T.P.	3.57 254.58	1.91 251.01

25458

Sea Breeze

1+26

70	1.5	53.1
E	1.9	52.7
cb.	1.9	52.7
1/4	1.8	52.8
+2	2.0	52.6
+6	3.4	51.2
E	3.6	51.0
1/4	4.4	50.2
Grvt.	4.5	50.1
cb.	3.79	50.79
+8	4.0	50.6
W	3.5	51.1
+10	4.1	50.5

1+51

-10	4.2	50.4
W	3.8	50.8
cb.	3.58	51.00
Grvt.	4.4	50.2
1/4	4.1	50.5
E	3.4	51.2
+2	3.2	51.4

25458

2+6

1.5	53.1	49
1/4	1.5	53.1
cb.	1.9	52.7
E	1.4	53.2
+10	1.2	53.4

1+76 = E.V.C

Dirt Floor

-10 in Garage	1.1	53.5
E " " SW end	1.5	53.1
cb.	1.8	52.8
+8	2.0	52.6
1/4	2.4	52.2
E	3.8	50.8
1/4	4.4	50.2
Grvt.	4.8	49.8
cb.	3.95	50.63
W	4.2	50.4
+10	4.1	50.5

2+100

-10	4.8	49.8
W	4.7	49.9
cb.	4.95	49.63

	2+00	254.58		
WGut			56	49.0
'4			54	49.2
+4			50	49.6
♀			42	50.4
+5			29	51.7
'4			30	51.6
cb			24	52.2
E			18	52.8
+10			14	52.2
	2+25			
-10			20	52.6
E			27	51.9
cb			33	51.3
'4			32	51.4
+3			32	51.4
♀			52	49.4
+3			61	48.5
'4			66	48.0
Gut.			68	47.8
cb			603	48.55
+6			62	48.4
W			46	50.0
+10			57	48.9

	2+50	254.58		50
-10			66	48.0
W			63	48.3
+4			71	47.5
cb			715	47.43
Gut			79	46.7
'4			74	47.2
+5			70	47.6
♀			59	48.7
+4			43	50.3
'4			43	50.3
cb			42	50.4
E			38	50.8
+10			37	50.9
	2+75 = N.W.	Edgewater St		
-10			49	49.6
-1.5	7'H = 12"	Pepper Tree		
E			53	49.3
cb			55	49.1
'4			57	48.9
+3			58	48.8
♀			77	46.9

25458

1/4	84	46.2
Gut	88	45.8
cb.	818	46.40
+6	82	46.4
W	70	47.6
+10	8.1	46.5
N cb.		
-10 on cb.	921	45.37
" "Gut	987	44.71
W on cb.	865	45.93
" Gut.	929	45.29
cb.	91	45.5
1/4	86	46.0
2	81	46.5
1/4	68	47.8
cb.	62	48.4
E	59	48.7
+10	60	48.6
N 1/4		
-10	63	48.3
E	66	48.0

25458

51

cb.	7.1	47.5
1/4	7.6	47.0
2	84	46.2
1/4	8.7	45.9
cb.	89	45.7
WL. Por.	927	45.31
+10 "	989	44.69

L. Edgewater

-10 on Por.	986	44.72
W " "	929	45.29
cb.	91	45.5
1/4	89	45.7
2	86	46.0
1/4	81	46.5
cb.	75	47.1
E	70	47.6
+10	69	47.7

S 1/4

-10	72	47.4
E	75	47.1
cb.	81	46.5

25458

E 1/4	8.5	46.1
d	9.0	45.6
1/4	9.3	45.3
cb.	9.5	45.1
W on Pav	9.59	44.99
110 " "	10.20	44.38

South Curb.

-10 cb.	9.95	44.63
" Gut	10.54	44.04
W cb.	9.43	45.15
" Gut.	10.04	44.54
cb.	9.9	44.7
1/4	9.8	44.8
d	9.2	45.4
1/4	8.8	45.8
cb.	8.3	46.3
E	7.9	46.7
+10	7.4	47.2

South Line Edgewater

-10	7.8	46.8
E	8.5	46.1
cb.	8.6	46.0

25458

52

1/4	9.0	45.6
d	9.8	44.8
1/4	10.3	44.3
Gut.	10.5	44.1
cb.	10.06	44.52
+5	9.9	44.7
W	9.6	45.0
+10	9.9	44.7

chk SIMBML BP	9.41	245.17
Sea Breeze & Edgewater	245.18	-FB 1692
	0.01	26

Cross Section - Cumberland St.

Wulker
Handachs
Corey

60' Wide
10' cbs
10' 1/4"

8-8-46

from Rancho Drive

to 254' E ELY line Sea Breeze

BM
518P
Rancho
& Cumberland

12.56 222.97

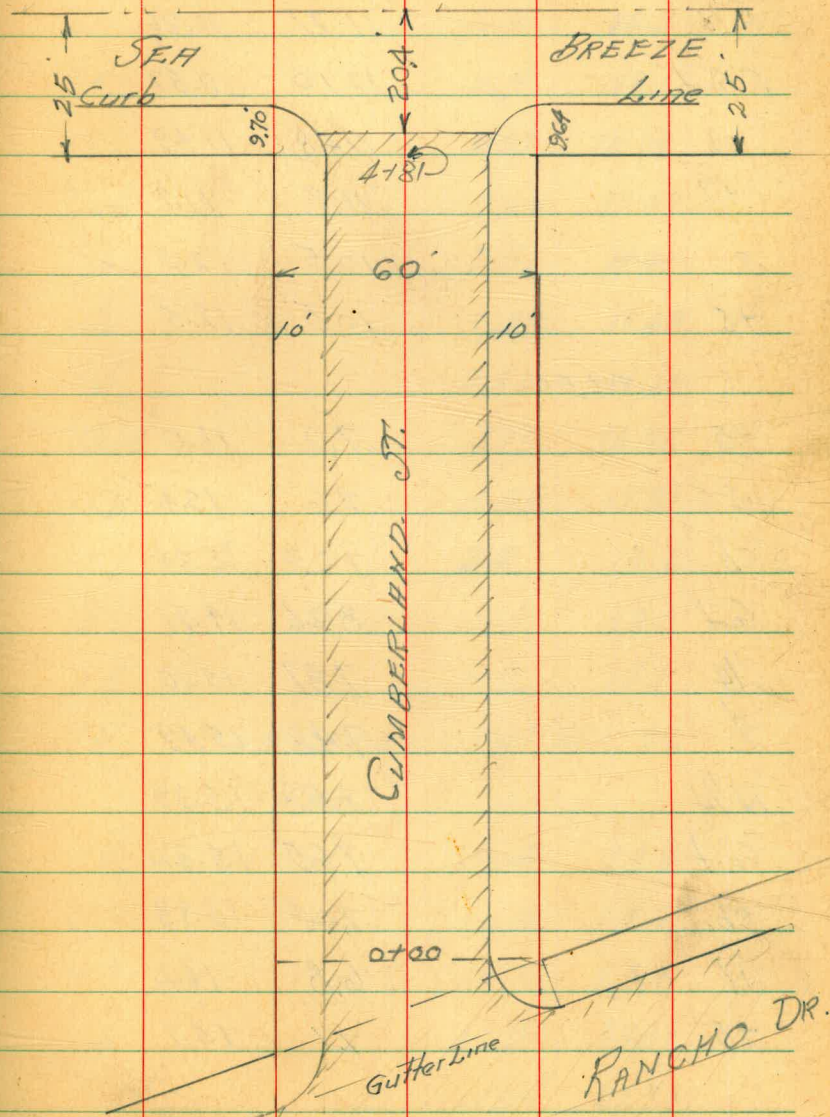
2.1041

ELY Gutter Line

S		
BC. cb	11.68	11.29
Gut	12.81	10.66
S cb "	12.55	10.42
S 1/4	12.67	10.30
L	12.85	10.12
N 1/4	13.09	09.88
N cb Gutter	13.26	09.71
BC on cb.	13.06	09.91
" " Gut	13.70	09.27
	0 + 00	
-S	11.0	12.0
N	11.3	11.7
cb	10.98	11.99
Gut	11.60	11.37

LISTED SWE

53



222.97

H ¹ / ₂	11.52	11.45
£	11.42	11.55
S ¹ / ₄	11.71	11.26
S Gut.	12.10	10.87
cb	11.48	11.49
+7	11.3	11.7
S	10.5	12.5
+5	10.5	12.5
0+50		
-5	7.0	16.0
S	7.6	15.4
cb.	7.63	15.34
Gut	8.26	14.71
¹ / ₄	7.87	15.10
£	7.48	15.49
N ¹ / ₂	7.58	15.39
Gut	7.65	15.32
cb.	7.04	15.93
N	6.8	16.2
+5.	7.1	15.9

222.97

Cumberland St.

54

1+00

-5	2.2	20.8
N	2.3	20.7
+5	2.9	20.1
cb.	2.27	20.00
Gut.	3.60	19.37
¹ / ₄	3.56	19.41
£	3.49	19.48
¹ / ₂	3.86	19.11
Gut	4.19	18.78
cb	3.58	19.39
+7	3.4	19.6
S	2.5	20.5
+5	2.9	20.1
T.P.	12.65	234.21
	1.41	221.56
1+50		
-5	10.4	23.8
S	10.3	23.9
+3	10.8	23.4
cb.	10.82	23.39
Gut	11.44	22.77

1750

234.21

Cumberland St.

1/4	11.15	23.06
L	10.82	23.39
N 1/4	10.25	23.26
Gut	11.00	33.21
cb	10.91	23.80
N	10.5	23.7
+5	10.7	23.5

2+00

-5	7.1	27.1
N	7.0	27.2
cb	6.71	27.50
Gut	7.37	26.84
1/4	7.12	27.09
L	6.83	27.38
1/4	7.16	27.05
Gut	7.47	26.74
cb	6.86	27.35
+7	7.2	27.0
South	5.7	28.5
+5	5.8	28.4

2+50

234.21

55

-5	1.0	33.2
S	14	32.8
+3	3.3	30.9
cb	2.90	31.31
Gut	3.48	30.73
1/4	3.25	30.96
L	2.95	31.26
1/4	3.31	30.90
Gut	3.60	30.61
cb	2.95	31.26
N	3.3	30.9
+5	3.6	30.6
T.P.	12.52	245.91
	0.82	233.39
	2+91.75 = P.V.C	
-5	12.3	33.6
N	12.0	33.9
cb	11.56	34.35
Gut	12.19	33.72
1/4	11.81	34.10
L	11.52	34.39

24591

Cumberland

S ¹⁴	11.84	34.07
Gut.	12.05	33.86
cb.	11.43	34.48
+7	11.5	34.4
S	10.2	35.7
+5	10.4	35.5
3+16.75		
-5	8.1	37.8
S	8.7	37.2
+5	9.8	36.1
cb.	9.68	36.23
Gut	10.30	35.61
¹⁴ / ₄	10.13	35.78
L	9.90	36.01
¹⁴ / ₄	10.15	35.76
Gut	10.39	35.52
cb.	9.78	36.13
N	10.4	35.5
t5	10.6	35.3
3+41.75		
-5	9.2	36.7

24591

N	9.0	36.9	56
cb	8.43	37.48	
Gut	9.02	36.89	
¹⁴ / ₄	8.76	37.15	
L	8.51	37.40	
¹⁴ / ₄	8.73	37.18	
Gut	8.90	37.01	
cb.	8.31	37.60	
+7	8.3	37.6	
S	6.5	39.4	
+5	6.1	39.8	
3+66.75			
-5	3.2	42.7	
S	4.0	41.9	
+3	4.3	41.6	
+5	6.6	39.3	
cb	7.14	38.77	
Gut	7.75	38.16	
¹⁴ / ₄	7.65	38.26	
L	7.48	38.43	
¹⁴ / ₄	7.89	38.02	
Gut	8.20	37.71	

24591

Cumberland St.

N cb	7.60	38.91
N	7.7	38.2
+5	8.2	37.7
3+91.75 = E.V.C		
-5	9.0	36.9
N	8.5	37.4
+3	7.1	38.8
cb.	6.94	38.97
Gut.	7.56	38.35
1/4	7.19	38.72
2	6.80	39.11
1/4	6.91	39.00
Gut.	6.98	38.93
cb.	6.36	39.55
+7	6.3	39.6
S	3.4	42.5
+5	3.8	43.1
41.50		
-3	1.4	44.5
S	2.5	43.4
+6	4.8	41.1

57

scb	4.81	41.10
Gut.	5.42	40.49
1/4	5.43	40.48
2	5.35	40.56
1/4	5.92	39.99
N Gut.	6.40	39.51
N cb.	5.80	40.11
N	6.0	39.9
+5	6.5	39.4
4+81 = W.L. 5.F.H. BREEZE		
-5	5.4	40.5
2	5.4	40.5
cb	5.08	40.83
Gut	5.65	40.26
1/4	5.14	40.77
2	4.68	41.23
1/4 Gut	4.6	41.3
Gut	4.55	41.36
cb	3.91	42.00
+5	3.7	42.2
S	1.4	44.5
+5	1.2	44.7

24591

T.P. chh 8th BP 3.99 241.92 SW. Sea

x Corrected
10.16 252.11 241.95-8M.x-Section
Intersection Sea Breeze P-45

5+20

-5 63 45.8

5 66 45.5

cb 69 45.2

+3 75 44.6

+6 91 43.0

1/4 93 42.8

2 96 42.5

1/4 103 41.8

+2 110 41.1

cb 112 40.9

N 117 40.4

+5 117 40.4

5+50

-5 93 42.8

N 94 42.7

cb 93 42.8

1/4 89 43.4

Breeze + Currierlund

252.11

2 85 43.6

+5 84 43.7

+7 73 44.8

1/4 70 45.1

cb 64 45.7

5 58 46.3

+5 53 46.8

6+00

-5 39 48.2

5 42 47.9

cb 49 47.2

1/4 55 46.6

2 59 46.2

1/4 62 45.9

cb 58 46.3

N 56 46.5

+5 56 46.5

6+15

-5 59 46.7

N 52 46.9

58

252,11

Cumberland st.

Ncb	49	47.2
1/4	49	47.2
2	47	47.4
1/4	45	47.6
cb	39	48.2
S	35	48.6
+5	32	48.9
6+50		
-5	15	50.6
S	1.6	50.5
cb	2.4	49.7
1/10	3.0	49.1
2	3.6	48.5
1/4	4.2	47.9
cb	4.4	47.7
N	4.2	47.9
+5	3.5	48.2
6+80		
-5	5.1	47.0
N	4.7	47.4
cb	4.1	48.1

252,11

59

N 1/4	3.1	49.0
2	2.3	49.8
1/4	1.9	50.2
Scb	1.9	50.2
S	1.6	50.5
+5	0.7	51.4
6+96		
-5	0.3	51.8
S	1.3	50.8
cb	1.5	50.6
1/4	0.5	51.6
2	1.8	50.3
+7	1.9	50.2
1/4	0.8	51.3
+1	0.3	51.8
cb	1.2	50.9
+4	2.1	50.0
+5	3.4	48.7
N	3.6	48.5
+5	4.7	47.4

25211

Cumberland St.

7+20

-5 3.9 48.2

N 3.5 48.6

cb. 3.3 48.8

'14 2.2 49.9

2 1.2 50.9

'14 0.8 51.3

cb. 0.9 51.2

5 0.4 51.7

+5 0.0 52.1

7+60

-5 +2.2 54.3

5 +2.1 54.2

cb. +1.3 53.4

'14 +0.6 52.7

2 +0.3 52.4

'14 0.3 51.8

cb. 0.8 51.3

N 1.4 50.7

+5 1.7 50.4

60

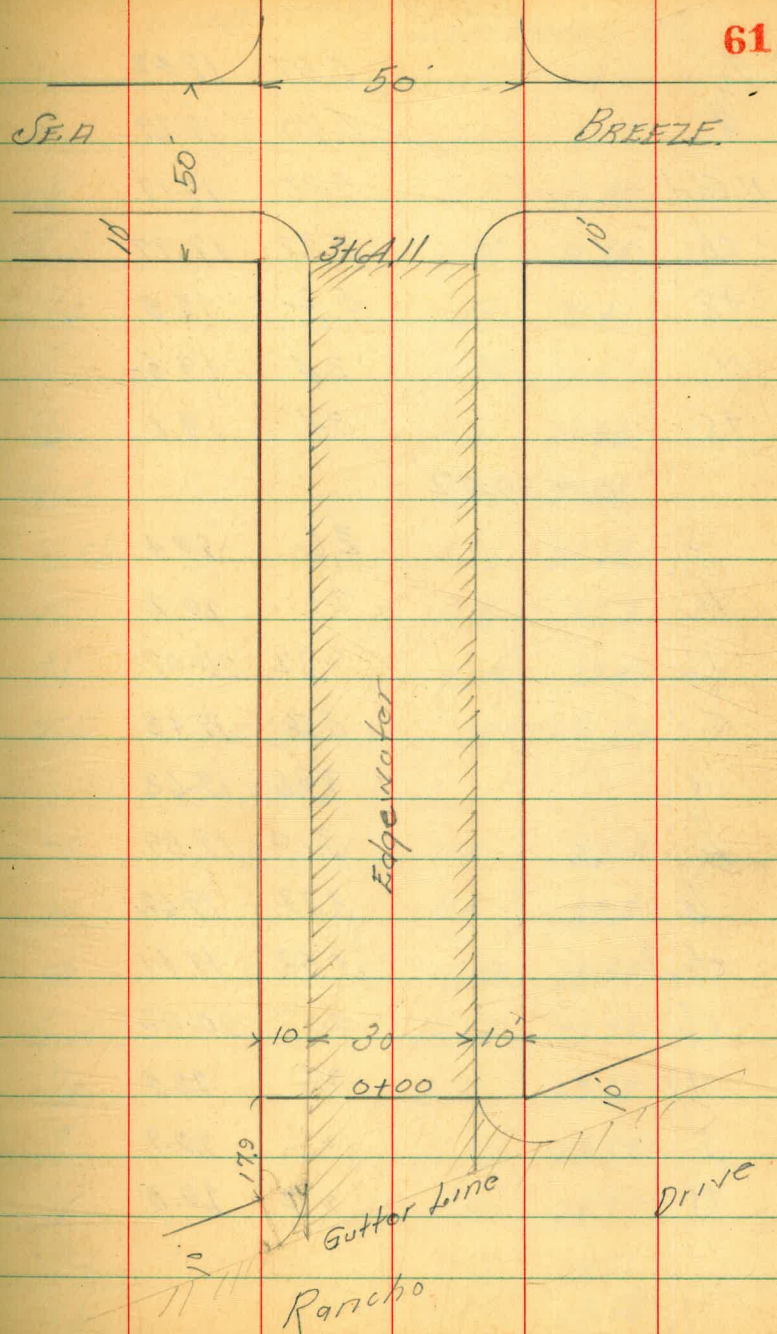
Walker Cross Section Edgewater St. 50' Wide
 Hendrick from Rancho Drive 10' Cbs
 Carey 7.5' 1/4
 8-8-46 to East end
 F.B. 1272-5 B.M. ~~30~~
 B.M. 24518 Rancho Edgewater

12.58 222.99 210.41 B.M. P53

Gutter Line

N cb BC	6.51	16.48
Gut.	7.11	15.88
cb 1/4	6.94	16.05
1/4	6.79	16.20
1/4	6.68	16.31
1/4	6.53	16.46
cb	6.49	16.50
86 Gut	6.40	16.59
1 on 6	5.71	17.28
0+00		
-5	4.1	18.9
5	3.9	19.1
+3	5.3	17.7
cb	5.24	17.75
Gut	5.21	17.08
1/4	5.76	17.23

61



222.99

2	5.57	17.42
1/4	5.70	17.29
N Gut	5.82	17.17
cb.	5.22	17.77
+8'	5.2	19.8
N	3.4	19.6
+5	3.4	19.6

0+39.42

-5	2.6	20.4
N	2.8	20.2
cb	2.92	20.07
Gut	3.56	19.43
1/4	3.36	19.63
2	3.10	19.89
1/4	3.37	19.62
stent	3.58	19.41
cb.	2.97	20.02
+9	2.6	20.4
5	2.1	20.9
+5	2.2	20.8

0+64.42 222.99

Edgewater St. 62

-5	0.6	22.4
0	1.2	21.8
cb	1.11	21.88
Gut	1.75	21.24
1/4	1.58	21.41
2	1.36	21.63
1/4	1.67	21.32
Gut	1.96	21.03
N cb.	1.36	21.63
N	0.7	22.3
+5	0.6	22.4

T.P. 12.45 235.09 0.35 222.64

0+89.42

-5	11.4	23.7
N	11.4	23.7
cb.	11.55	23.54
Gut	12.17	22.92
1/4	11.86	23.23
2	11.57	23.52
1/4	11.72	23.37
Gut	11.87	23.22
cb.	11.24	23.85

52

018942
23509

5		11.1	24.0
+5		11.5	23.6
	1750		
-5		6.4	28.7
5		6.5	28.6
cb		6.27	28.82
Gut.		6.89	28.20
1/4		6.72	28.37
2		6.46	28.63
1/2		6.70	28.39
1/4 Gut.		6.91	28.18
Ncb.		6.29	28.80
+7		6.5	28.6
N		5.6	29.5
+5		5.6	29.5
	2+00		
-5		0.6	34.5
N		0.6	34.5
+3		2.1	33.0
Ncb.		2.02	33.07
N Gut.		2.64	32.45

23509

Edgewater St. 63

N 1/4		2.39	32.70
2		2.08	33.01
5 1/4		2.32	32.77
S. Gut.		2.50	32.59
S. cb.		1.92	33.17
5L		2.2	32.9
+5		2.5	32.6
TP	11.86	246.40	0.55 234.54
	2+50		
-5		9.7	36.7
5		9.3	37.1
cb.		8.94	37.46
Gut.		9.54	36.86
1/4		9.36	37.04
2		9.15	37.25
1/2		9.42	36.98
Gut.		9.67	36.73
cb.		9.06	37.34
+7		9.2	37.2
N		7.9	38.5
+5		6.8	39.6

246.40
2+8942

-5	3.2	43.2
N	3.2	43.2
+3	5.6	40.8
Ncb	5.60	40.80
N Gut	6.20	40.2
N 1/4	6.08	40.32
♀	5.86	40.54
S 1/4	6.09	40.31
S Gut	6.23	40.17
S. cb.	5.65	40.75
S Line	5.7	40.7
+5	6.8	39.6

3+1442

-5	5.4	41.0
S	4.2	42.2
cb.	3.85	42.55
Gut	4.45	41.95
1/4	4.27	42.13
♀	4.03	42.37
N 1/4	4.20	42.20

Edgewater St.

246.40

64

N Gut	4.26	42.14
N cb	3.66	42.74
+7	3.5	42.9
N L	1.9	44.5
+5	1.0	45.4

3+3942

-5	0.1	46.3
N	0.3	46.1
+4	1.9	44.5
cb	1.99	44.41
Gut	2.63	43.77
N 1/4	2.56	43.84
♀	2.50	43.96
S 1/4	3.78	42.62
S Gut	3.09	43.31
S. cb.	2.48	43.92
S Line	2.2	44.2
+5	2.3	44.1
TR	1.23	245.17

10.53 255.71

376411 = W.L. Sea Breeze

5078P.
Edgewater
Sea Breeze

381 P.52

25571 Edgewater St
346411

SL-5	101	45.6
SL	107	45.0
cb	1053	45.18
gut.	1115	44.56
1/4	1074	44.97
L	1040	45.31
1/4	1038	45.33
gut.	1039	45.32
cb	976	45.95
+7	92	46.5
N	84	47.3

X Sections - See Breezo Int. = 52

4100

5	67	49.0
N	62	48.8
cb	77	48.0
1/4	84	47.3
L	90	46.7
1/4	95	46.2
cb	99	45.8
5	98	45.9
+5	100	45.7

4150 25571

-5	89	46.8
5	86	47.1
cb	80	47.7
1/4	80	47.7
L	74	48.3
1/4	70	48.7
cb	64	49.3
N	55	50.2
+5	48	50.9

Cocos
4159 = 3" Palm on N 6.5' in st
770 6" " " " 7' " "
+87 " " " " 7' " "

65

5100

-5	40	51.7
N	40	51.7
cb	52	50.5
1/4	58	49.9
L	63	49.4
1/4	66	49.1
6	68	48.9
5	70	48.7
+10	82	47.5

5+50

-5	6.7	49.0
5	6.3	49.4
cb	6.2	49.5
1/4	5.8	49.9
2	5.0	50.7
1/4	4.8	50.9
cb	4.4	51.3
N	3.7	52.0
+5	3.0	52.7
5+70 = 24" Cypress 14' 11" st. on Rt Owlmer says save this tree		
6+00		
-5	1.1	54.6
N	1.3	54.4
cb	2.5	53.2
1/4	3.2	52.5
2	3.5	52.2
1/4	4.0	51.7
cb	4.2	51.5
S	4.6	51.1
+5	4.4	51.3

T.P	7.59	260.95	2.35	253.36
6+50				
-5			7.6	53.4
S			7.7	53.3
cb			7.8	53.2
1/4			7.5	53.5
2			7.2	53.8
+6			7.1	53.9
1/4			6.4	54.6
cb			6.5	54.5
N			6.1	54.9
+5			5.7	55.3
7+03.77				
-5			4.3	56.7
N			4.2	56.8
cb			4.3	56.7
1/4			4.4	56.6
2			4.8	56.2
1/4			5.0	56.0
cb			5.0	56.0
S			4.7	56.3
			4.9	56.1

260.95

Edgewater St

7+2.5

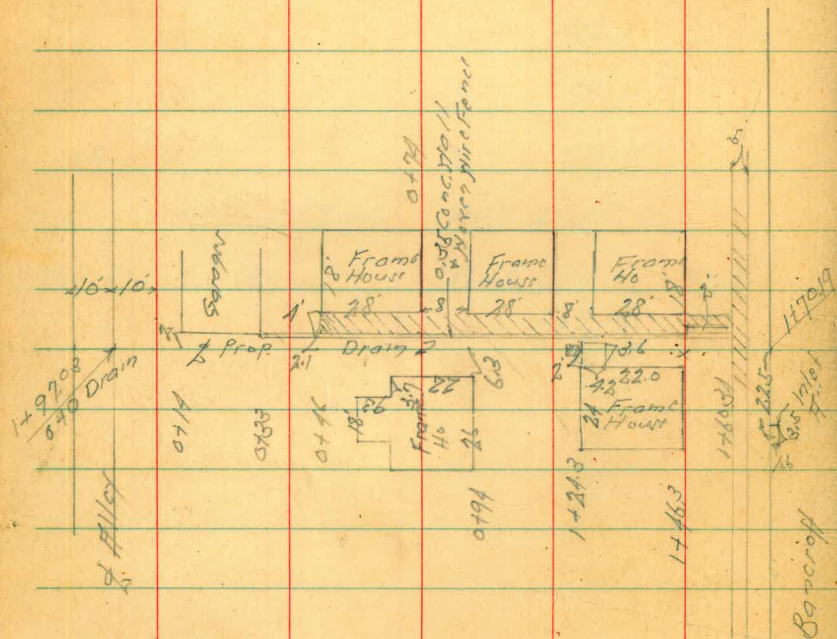
67

-5	39	57.1
5	37	57.3
cb.	36	57.4
5 1/4	33	57.7
2	31	57.9
1/4	29	58.1
cb.	29	58.1
N	29	58.1
+5	29	58.1

TP	157	253.85	8.67	252.28
chk BM	Edgewater	Sec 8	8.66	245.19 P-64
			245.18	
			0.01	

Cross Section Alley Block 211 University Ave
From University Ave to Lincoln Ave

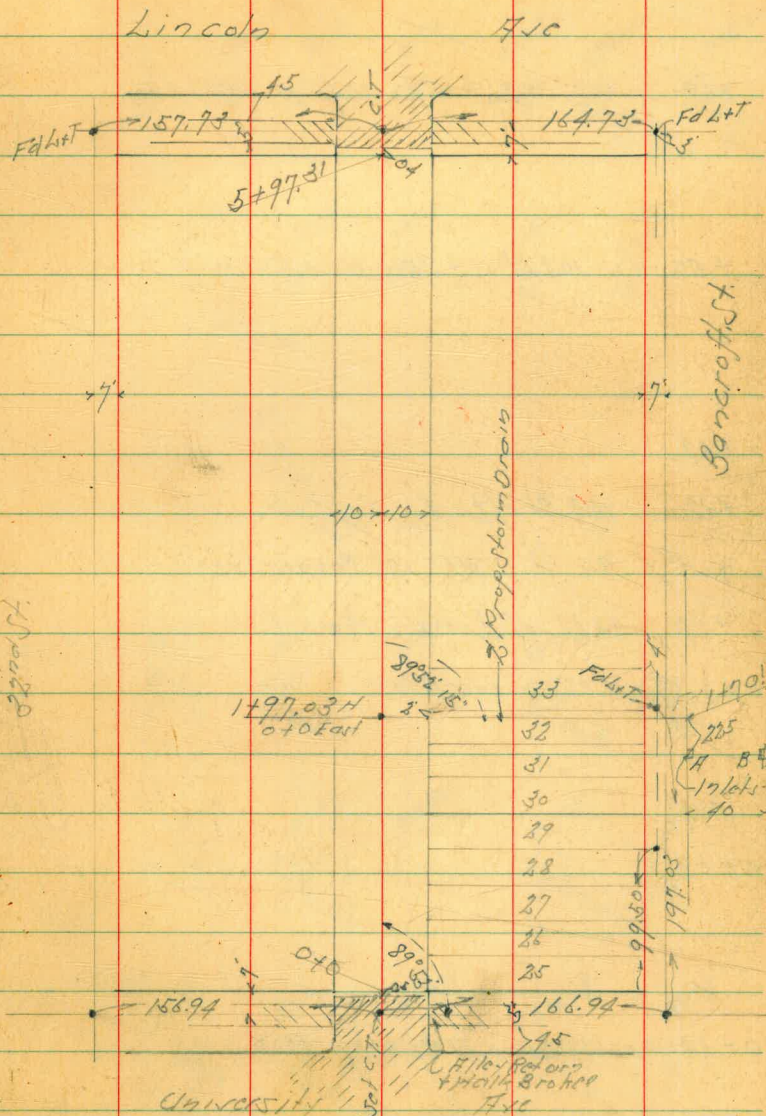
Notes Reduced 9-17-46 Merry-



Indexed
e.s.k.

Sept 5-46
Sisson
McCoy
Haddel
Allen

68



+69 10.2 Lt of $\frac{1}{2}$ - $\frac{1}{4}$ Wire Fence

+50 10.4 Lt of $\frac{1}{2}$ - Sly Wire Fence

+39

+32 10.2 Rt of $\frac{1}{2}$ - Fly Tol Pole

+05 9.1 Rt - $\frac{1}{4}$ 18" Pepper Tree

+01 8.3 Lt of $\frac{1}{2}$ - $\frac{1}{4}$ Paper Pole

0+0 - H. L. University

0-07'

0-14 - H. C. Line University Etc

B.M. 1.94 353.85

351.91

S.M. B.P.
University
+350.55

Lt. H

R

Rt. E

69

348.7	348.49	347.9	347.0	346.7	346.62	346.72
5/10	5.36	5.9	6.8	7/10	7.23	7.13
	9.54	6.50			5.54	1.52
	Slab	Conc			Slab	Conc Floor

349.45	348.9	348.0	347.7	347.1
1.10	4.9	5.8	6.1	6.7
10.4	10	10	10	15
	10.4			
	Slab			
	Conc			

349.4	348.9	348.0	347.7	347.1
1.6	4.9	5.8	6.1	6.7
10.3	10	10	10	15
	10.3			
	Slab			
	Conc			

349.72	349.45	349.00	349.13	349.07
4.13	4.40	4.85	4.72	4.78
10-Cb	10-Gutter		10-Gutter	10-Cb

349.65	349.43	348.85	349.03	349.01
4.25	4.14	5.00	4.82	4.84
9.9-Cb	10-Gutter		10-Gutter	10-Cb

349.59	348.95	348.63	348.18	348.78
4.76	4.90	5.22	5.67	5.07
10-Cb	10-Gutter		10-Gutter	10-Cb

353.85

210
 +99 10' Lt of $\frac{1}{2}$ = Sly Picket Fence
 8.9' Lt of $\frac{1}{2}$ = Nly Board Fence
 TP @ 1.42 345.94 9.33 344.52

+78 9.5' Lt of $\frac{1}{2}$ = N. Car Garage + Shed + Sly Board Fence
 +59

+50 9.3' Rt of $\frac{1}{2}$ = Fly Tel + Power Pole
 +49 9.4' Lt of $\frac{1}{2}$ = S. Car Garage + Shed
 +39

+34 11.7' Rt of $\frac{1}{2}$ = Nly Picket Fence
 10.5' Lt of $\frac{1}{2}$ = Δ Board Fence
 +31 8.2' Lt of $\frac{1}{2}$ = Nly 7' Acacia Tree

+22 8.9' Lt of $\frac{1}{2}$ = Nly Power Pole
 +20 15.6' Lt of $\frac{1}{2}$ = Sly Board Fence

170 109' Rt of $\frac{1}{2}$ = Sly Picket Fence

0+94

353.85

LT S RT 70

345.1 344.8 343.9 343.5 343.1 342.82 342.83

2.8 1.6 2.0 2.4 2.8 3.12 3.11

20 10 5 2.4 10 14.3 Sly Car Apron 14.8 Sly Car Apron Floor

345.94'

345.3 344.7 344.0 343.6

8.5 9.1 9.8 10.7

9.7' + 10' Garage + 10' Shed + 10' Floor 21' Nly Bedg.

347.8 345.8 345.2 345.1 345.3

6.0 8.0 8.5 8.7 8.5

10 5 10 10 11.8' + 4' Garage + 10' Floor

347.74

6.11 15.6' = Nly Dog Apron + 10' Floor

347.77 347.64 346.3 346.4 346.47 346.72

6.08 8.21 7.5 7.4 7.38 7.13

15.5' Sly Dog Apron + 10' Sly Balcony Apron 10.5' = Nly Car Apron 14.9' = Nly Dog Apron Floor

347.7

6.11' + 14.7' = 4' Garage + 10' Floor 353.85

+64

+49 9.6 lb of 1/2 - Wly Pass Pale 10.7 lb of 1/2 - Wly Picked Front

+35

+33

+30.5

2+30

34594

344.12	342.52	342.3	341.1	340.6	341.3	341.19	341.55	341.78
1.80	3.42	3.6	4.8	5.0	4.6	4.75	4.39	4.16
36 = 1/2 Wly Cont Floor	11 = 1/2 Wly Pass	10		2	10	10.3 = 1/2 Wly Pass	13.7 = 1/2 Wly Pass	16.0 = 1/2 Wly Pass

343.84	342.92
2.05	3.02
10.9 = 1/2 Wly Pass	16.7 = 1/2 Wly Pass

345.0	343.8	342.8	342.4	342.2	341.65	341.74
0.9	2.0	3.1	3.5	3.7	4.29	4.20
2.5	10	5		10	14.1 = 1/2 Wly Pass	14.9 = 1/2 Wly Pass

341.87
4.07
14.5 = 1/2 Wly
Pass

342.36
3.59
10.2 = 1/2 Wly
Pass

342.59
3.35
13.1 = 1/2 Wly
Pass

34594

+53 8.2 Lt of $\frac{1}{2}$ = NY Power + Tel Pole

+45

+29

+19

370

+98 PART of $\frac{1}{2}$ = ELX TEL Pole

270

345.94

Lt.

L

Rt

72

339.1

6.8

12.1 = NY Power
Dist Floor

340.55

5.39

12.1 = NY Power
Dist Floor

340.20

5.74

10.1 = NY Power
Dist Floor

339.7

6.3

10

339.0

6.9

339.1

6.8

10

340.1

5.8

14.1 = NY Power
Dist Floor

338.5

7.4

10

339.9

6.0

12.3 = NY Power
Dist Floor

340.59

5.55

12.1 = NY Power
Dist Floor

340.25

5.90

10.1 = NY Power
Dist Floor

339.6

6.2

10

339.38

6.56

10.1 = NY Power
Dist Floor

339.3

6.6

10

339.0

6.1

14.1 = NY Power
Dist Floor

341.84

4.10

11.1 = NY Power
Dist Floor

341.58

4.36

11.6 = NY Power
Dist Floor

342.22

3.74

11.1 = NY Power
Dist Floor

342.0

3.9

10

340.6

5.3

10

340.3

5.6

10

340.4

5.5

10

338.7

7.2

10

337.4

2.5

10

345.94

429

10.2' R1 of 2 = 1/4 Board & Picket Fence

+24

10.9' H of 2 = 5/4 Lath & Fence

+18

+05

IP 8.11 347.80 6.25 339.69

4+0

+82 10.8' H of 2 = 5/4 24" Fuc Tree

+81 10.6' R1 of 2 = 5/4 Board & Picket

+72

+70 10.1' H of 2 = 5/4 30" Fuc Tree

3465

34594

L.H.W

2

R1-E

73

340.56

77.34

12.3 = 1/4 Gopool
5 1/2" Floor
Couch Milk

341.3

6.5

13.6 = 1/4 Gopool
5 1/2" Floor

342.1

5.7

10

341.1

6.7

10

339.4

8.1

10

339.3

8.5

10

339.1

8.7

10

347801

339.1

6.8

10

339.9

6.5

10

339.3

6.6

10

339.1

6.7

10

338.9

7.0

10

339.2

6.7

10

338.5

7.1

10

12.3 = 1/4 Gopool
5 1/2" Floor

338.8

7.1

10

338.5

7.1

10

338.9

7.0

10

338.9

7.0

10

338.8

7.1

10

12.3 = 1/4 Gopool
5 1/2" Floor

34594

+97

+95

+80

+79

+74 107 Lt of $\frac{1}{2}$ - Nly Lot 4 Fence

+73 87 Lt of $\frac{1}{2}$ = Wly Parcel Pole

+50

+48 93 Rt of $\frac{1}{2}$ = Fly Td Pole

4732

347.80

Lt

Rt

Rt

74

342.40

5.10

17.7 = Nly Do. Gar
Conc Floor

342.58

5.22

13.3 = Nly Do. Gar
Conc Floor

342.37

5.43

17.5 = Nly Do. Gar
Conc Floor

342.53

5.27

13.3 = Nly Do. Gar
Conc Floor

342.6

5.7

10

342.1

5.7

10

340.8

7.0

4

340.6

7.2

341.4

6.6

6.44

11.3 = Nly Do. Gar
Walk

341.86

340.83

6.97

13.9 = Nly Do. Gar
Fly Td

340.92

6.88

15.6 = Nly Do. Gar
Conc Floor

340.78

7.08

13.3 = Nly Do. Gar
Fly Td

340.95

6.85

15.5 = Nly Do. Gar
Low Floor

347.80

IP x 8.30 336.96

IP 2.32 345.29 5.34 342.97

67 11.31 = S.C. 6 Line Lincoln

+97.31 = S.L. Lincoln

TP 5.00 348.31 4.49 343.31

x80

10.9' R of 2 = Sly Picket Fence

+48 93 R of 2 = Fly Tel Pole

+40

5x0

347.80

Lt.

T

Rt.

75

5 205-42

→ P. 200 ft. →
H. 1.347. 200 ft. →
Contact 348.81
5.000 004.20.18

342.13
342.12

342.87
342.86

342.78
342.29

342.83
342.82

342.06
342.05

4.88
10-Cb

5.41
10-Gutter

5.53

5.18
10-Gutter

4.95
10-Cb

342.62
342.61

343.16
343.15

342.25
342.74

343.39
343.38

343.10
343.09

4.69
10-Cb

4.85
10-Gutter

5.06

4.72
10-Gutter

4.71
10-Cb

348.31

342.2

342.2

343.9

342.5

3.5
10-Cb

3.6
10

3.9

3.0
10

10.9' R of 2 = Sly Picket Fence
93 R of 2 = Fly Tel Pole

343.5
4.0
10

343.6
4.2
10

343.5
4.3
10

343.5
4.3
10

343.4
4.4
10

10.9' R of 2 = Sly Picket Fence
93 R of 2 = Fly Tel Pole

342.7
5.1
10

342.4
5.1
10

342.2
5.5

342.3
5.5
10

342.5
5.0
10

347.80

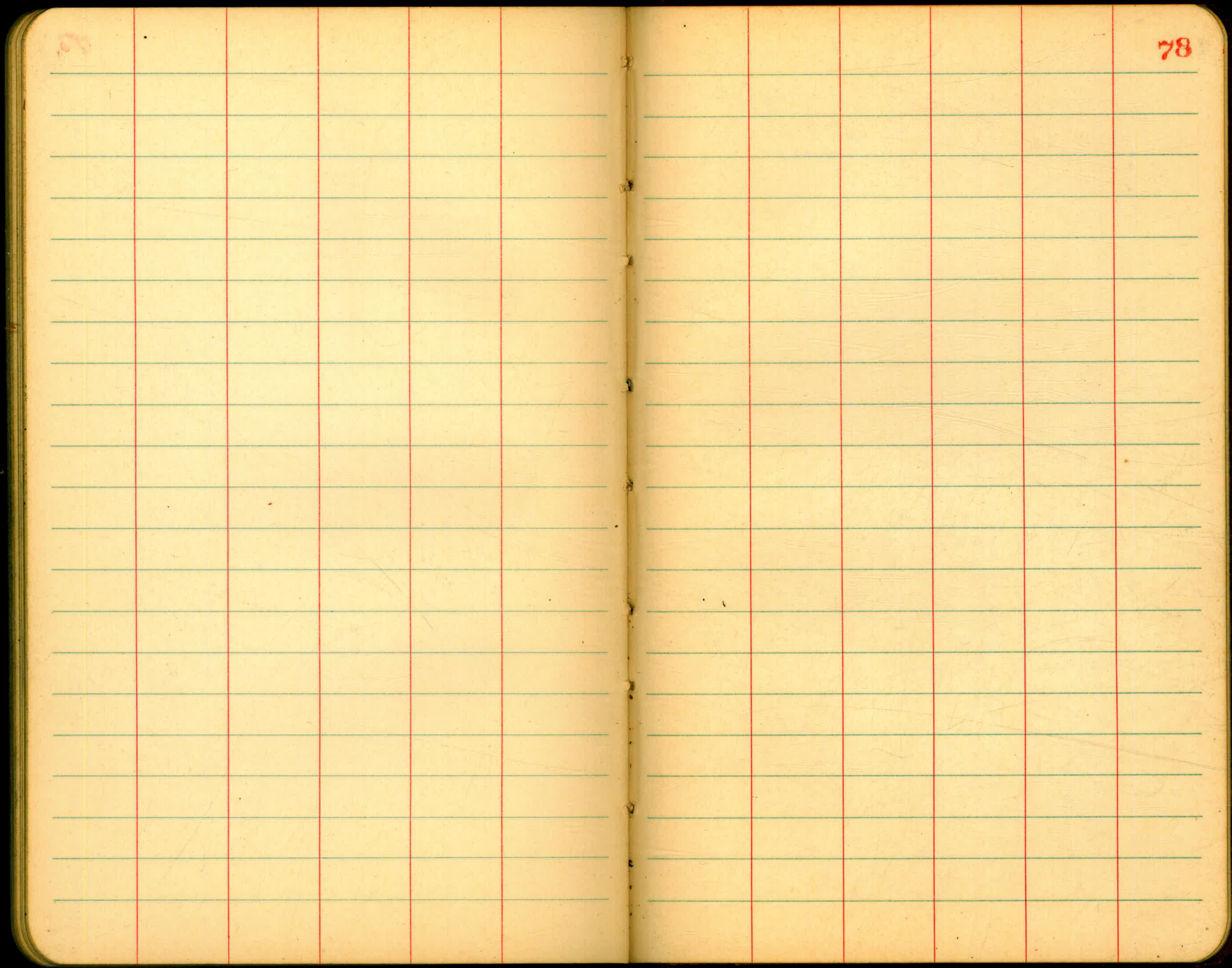
Levels Proposed Storm Drain
Block 211 University Hts
Sketch Page 68

TP #	Description	Height	Level	Page 70
TP #	1.55	3.46.07	344.52	
0+0	1+97.03 Alley	2.3	343.8	
+31		3.5	342.6	
+32.4	2' Lt of Top Conc Wall	5.23	340.88	
+35	Wly Larrn	5.2	340.9	
+38	18 R/O of Small Orange Tree			
+50		6.4	339.7	
+74	Grade Break of Wall			
"	2' Lt of Top Conc Wall	8.14	337.93	
"	2.35' Lt of Conc Wall	8.49	337.58	
TP	3.17	341.00	8.24	339.83
1+0		4.7	336.3	
"	2' Lt of Top Conc Wall	3.14	337.86	
"	2.35 " " = Conc Wall	3.54	337.46	
+21	Wly 2.5' Conc Landing	5.20	335.80	
+25.5	Wly Plant Porch	3.03	337.97	Top
+46.3	2' Lt of Top Wall Top	3.38	337.67	
"	" " " " " Top	4.22	336.78	
"	2.35' Lt = Wall	3.75	337.05	
+60.33	Wly Conc Wall	4.65	336.35	
+70.19	Wly Conc Basement	4.76	336.04	
"	Gutter on Pav	5.58	335.15	

TP	Description	Height	Level	Notes
			341.00	
TP	4.96	341.35	4.61	336.39
Inlet A	Wly Basement	6.52	334.83	on Grating
		5.54	335.81	Top Cb
		8.15	333.70	Bottom Box
12" Pipe Chimney		14.42	316.93	Floor Line
Inlet B	Fly Basement			
		6.46	334.89	Top Cb
		7.50	333.85	on Grating
		9.35	332.00	Bottom Box
		4.38	336.97	TP x 75 336.76
TP	12.86	351.70	2.51	338.84
TP	6.15	356.85	1.00	350.70
BM		4.95	351.90	S.W.B.P. C/O N.V. 3200 351.91

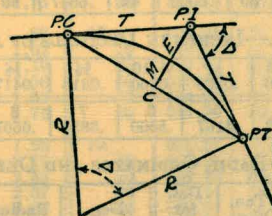
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DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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CURVE FORMULAS

Radius= $R = \frac{50}{\sin. \frac{D}{2}}$ (1) Degree of Curve= D and $\sin. \frac{D}{2} = \frac{50}{R}$ (2)

Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)

Middle ordinate= $M = R(1 - \cos. \frac{\Delta}{2})$ (5) $= R \text{vers} \frac{\Delta}{2}$ (6)

External= $E = T \tan \frac{\Delta}{4}$ (7) $= R \div \cos. \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)

Long Chord= $C = 2 R \sin. \frac{\Delta}{2}$ (10) $\Delta =$ Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161 +60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{3} = 414.49$ ft. From Table V correction=.36 or $T = 414.85$ ft. P. C.=Sta. P.I.— $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T.=Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance= $158 - \text{Sta. P. C.} = 54.50$, hence offset= $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle= $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft.=(in minutes) $.3 \times C \times D^\circ$ or=defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve= $.3 \times 54.5 \times 8\frac{1}{3} = 136.2'$ or $2^\circ 16.2'$, or= $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle= $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 91.27$ and from Table V correction=.10 or $E = 91.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

1 + 34.4 " 140 S

2 71.4 W to W

2 71.3

30466

59911

70377

17 86
42

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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