

1695

WEDGWOOD
PILLS

ENTIRE
LEVEL BOOK

No. 410F

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide, Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.

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1695

CITY ENGINEER'S OFFICE

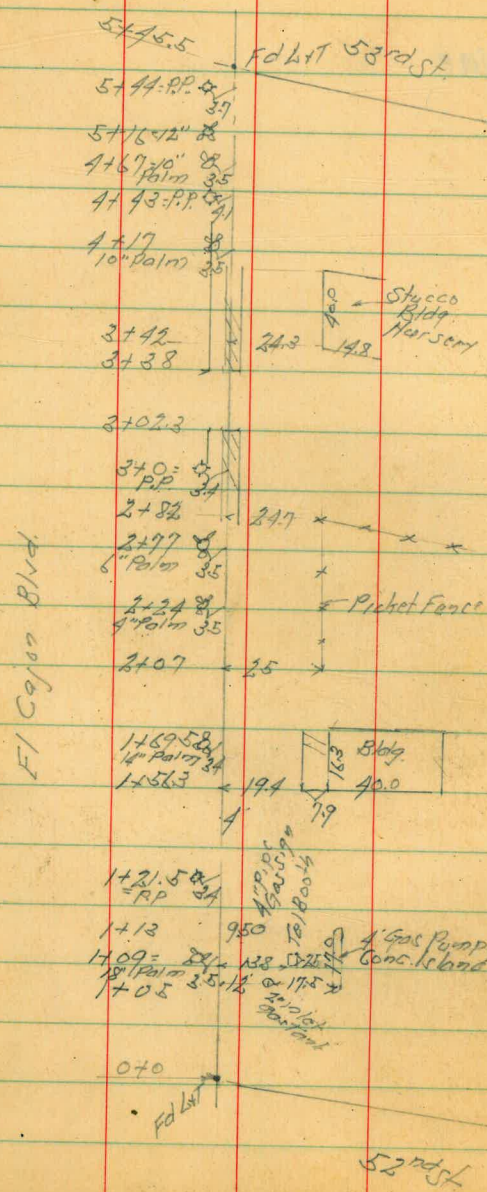
The paper stock of this book is made of a high grade 50% rag paper having a water resisting surface. This book is sewed with Bing Special Enamel Waterproof Thread.

Made in U. S. A.

Columbine

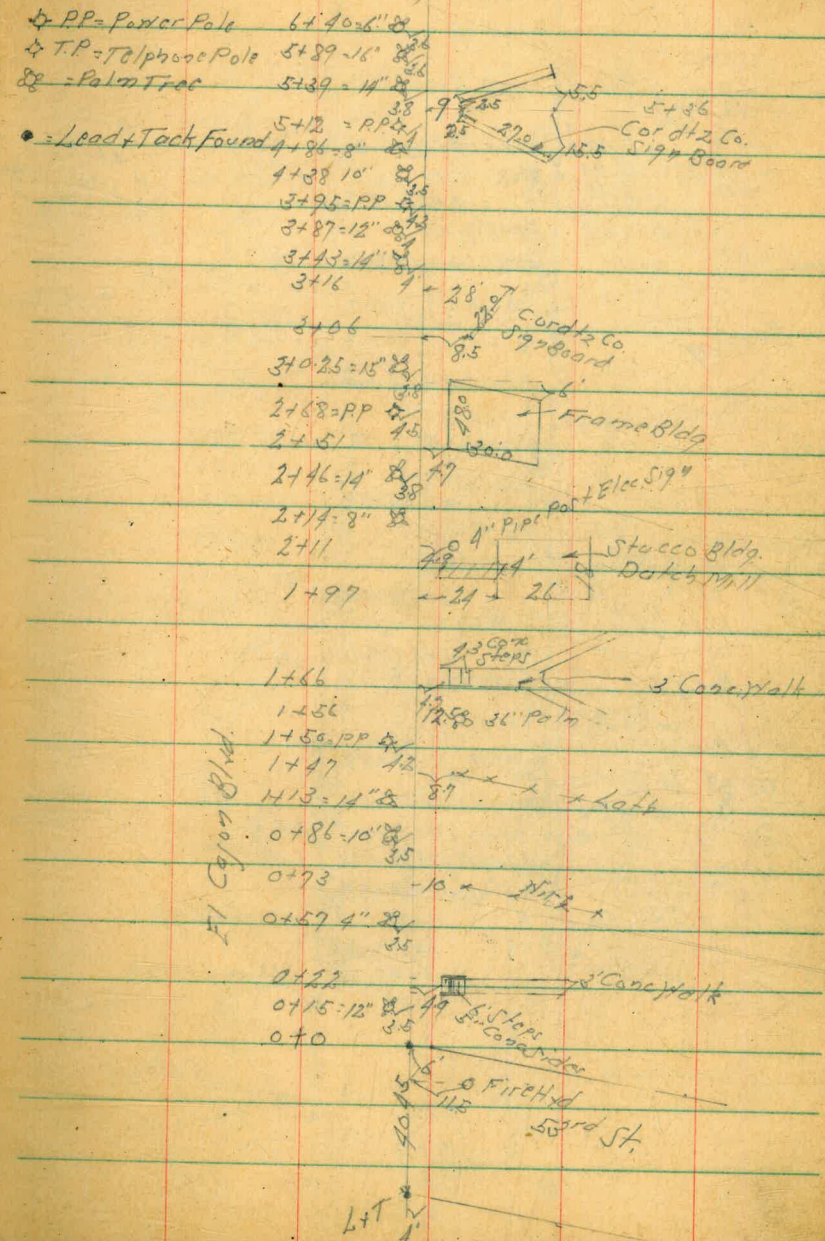
52

El Cajon Blvd Topography
52nd St. to 67th

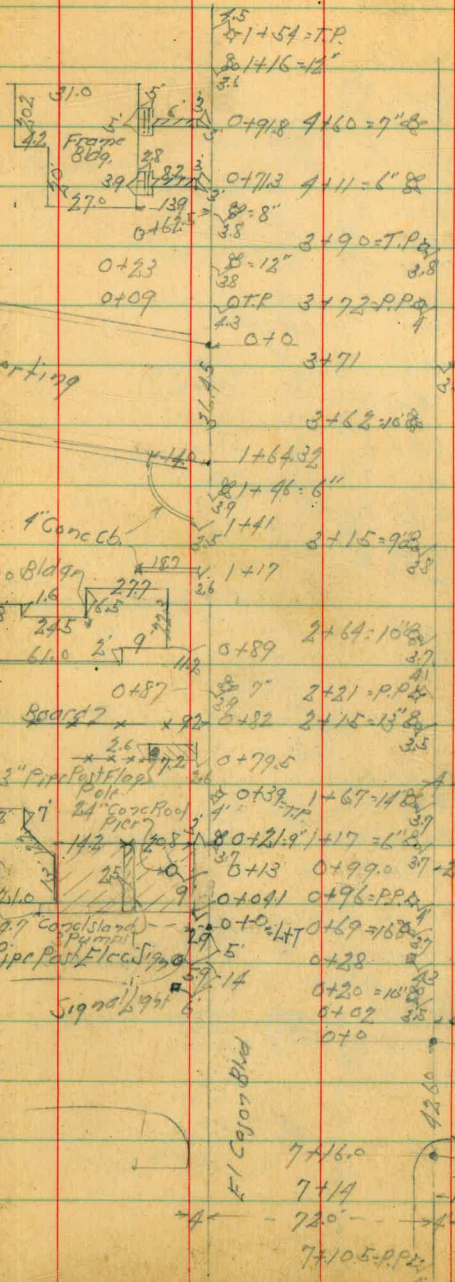


Oct. 23-45
S. J. J. O. Y.
81.55
Osborne

Indexed
c.s.k.

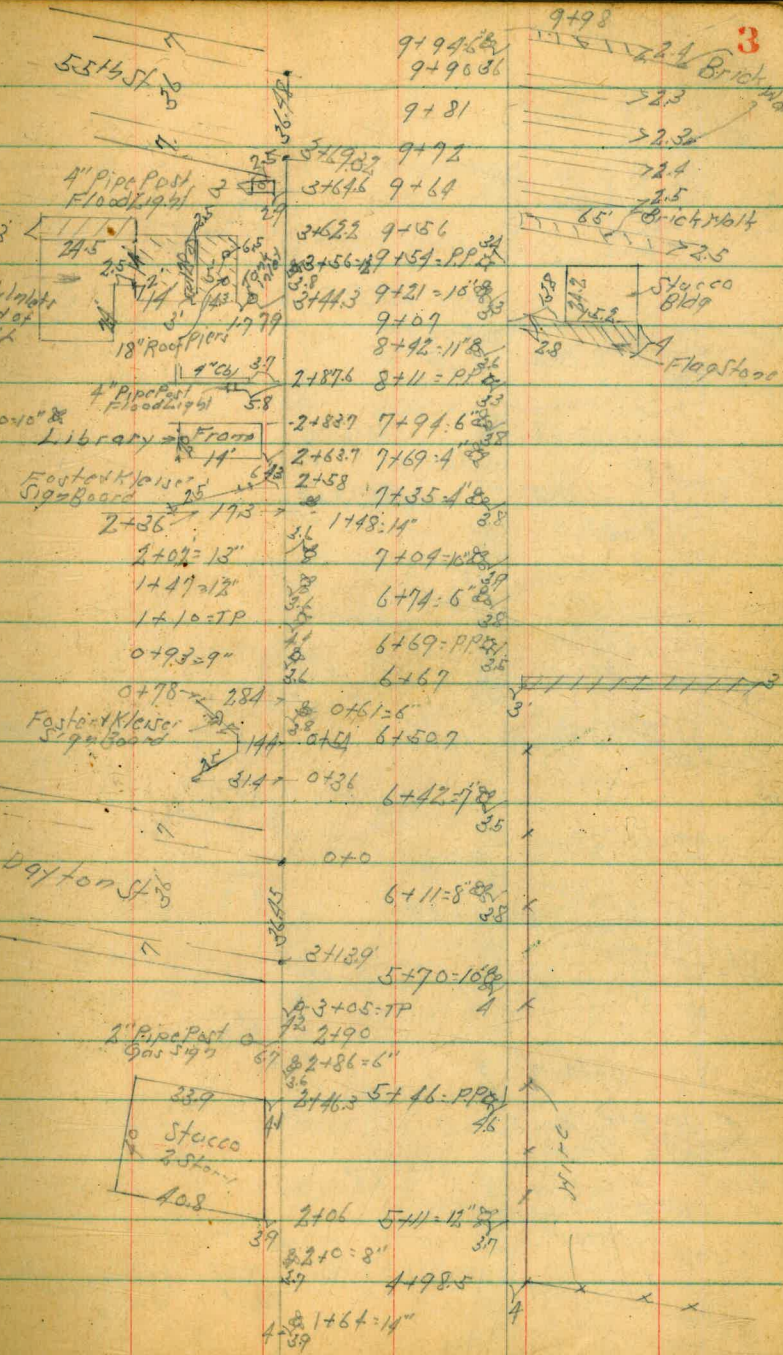


F1 Cajon Blvd



51+54=TP
 80+16=12"
 0+9.8 4160=7'8"
 0+71.3 4111=6'8"
 3+90=TP
 3+72=PP
 3+71
 3+68=10"
 1+64=32
 81+96=6"
 1+41 8+15=9'2"
 0+89 2+64=10'8"
 2+21=PP
 2+15=13'8"
 0+79.5
 1+67=14'2"
 0+21.9 1+17=6'8"
 0+99.0 37+215
 0+109.1 0+96=PP
 0+10=LT 0+69=16'8"
 0+28 5970=11961
 0+20=10'8"
 0+02 225=Tel Pole
 0+0
 7+16.0
 7+14
 720
 7+10.5=PP

3+64.2
 3+59.6 = 90
 Tank
 76' dia
 11'



9+98
 9+96.86
 9+81
 9+72
 9+64
 9+56
 9+42=18'8"
 9+16.7
 8+42=11'8"
 8+11=PP
 7+94.6
 7+69.4
 7+35.4
 1+48.14
 7+09=10'8"
 6+74=6'8"
 6+69=PP
 6+67
 0+61=6
 6+50.7
 6+42=7'8"
 0+0
 6+11=8'8"
 5+70=16'8"
 5+46=PP
 5+46=14"
 5+11=12'8"
 4+198.5
 4+89 1+64=14"

3

65' Brick wall

Stucco Bldg

Flagstone

280' Library

Fastener Sign Board

Fastener Sign Board

Dayton St

2" Pipe Post Gas

Stucco Bldg

Card Co 160 590 Board

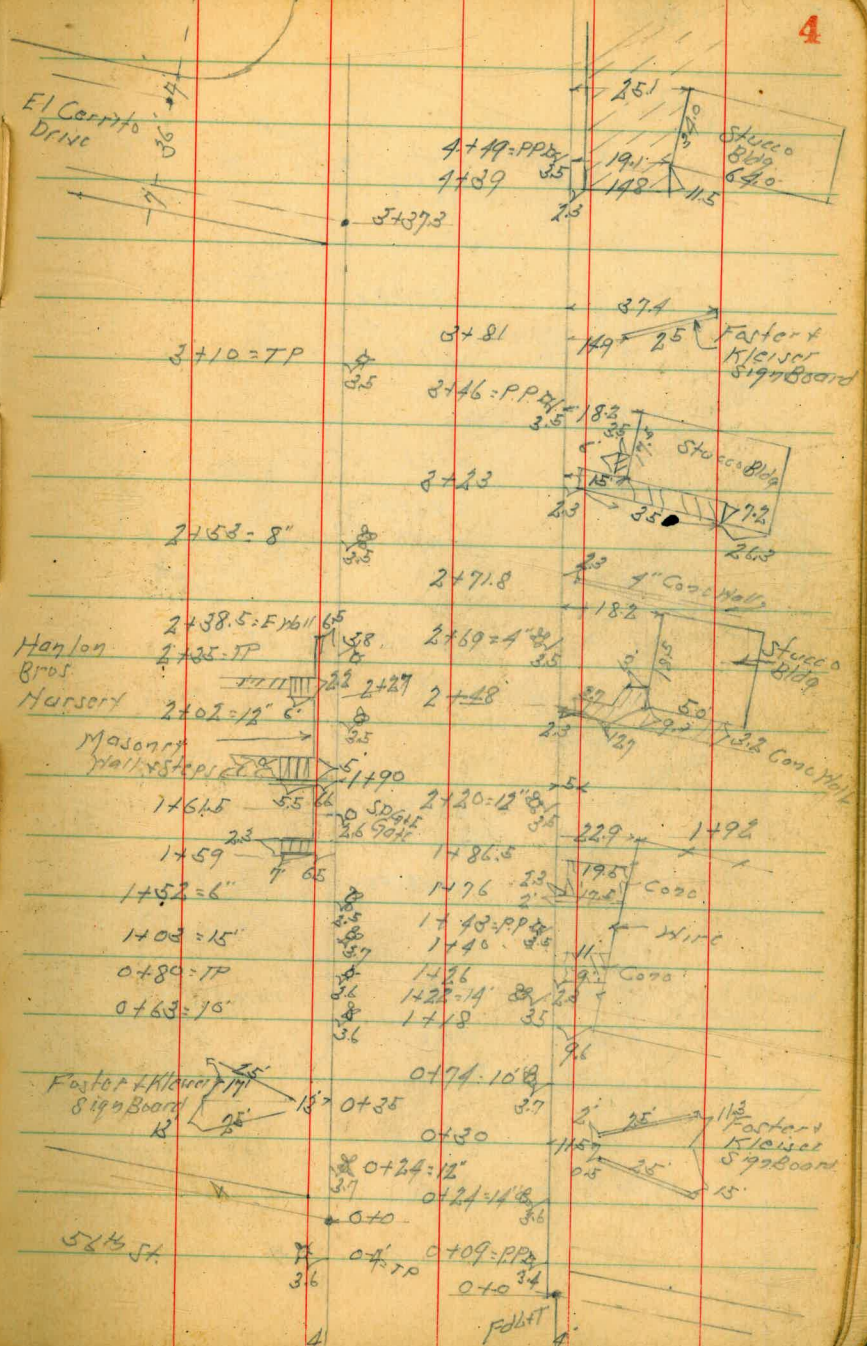
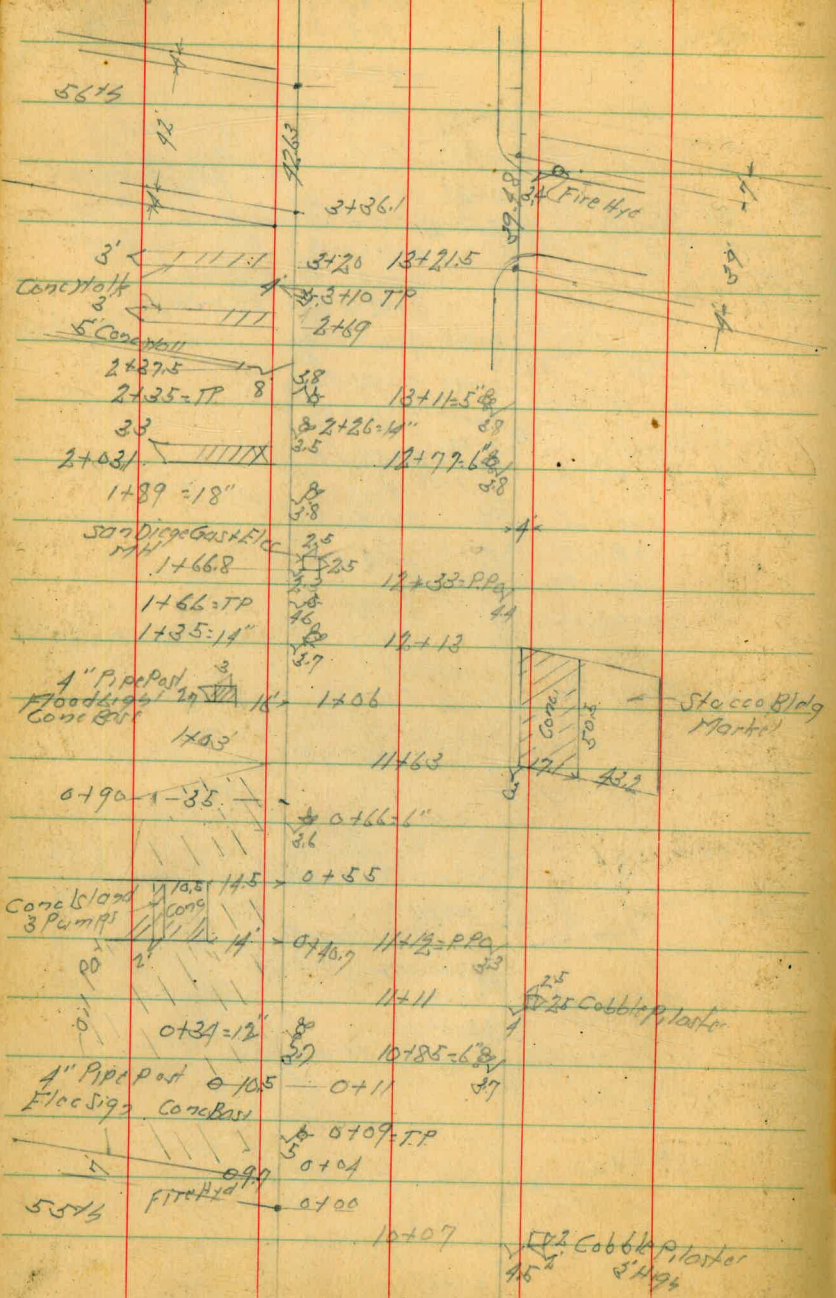
225 Tel Pole

51th St

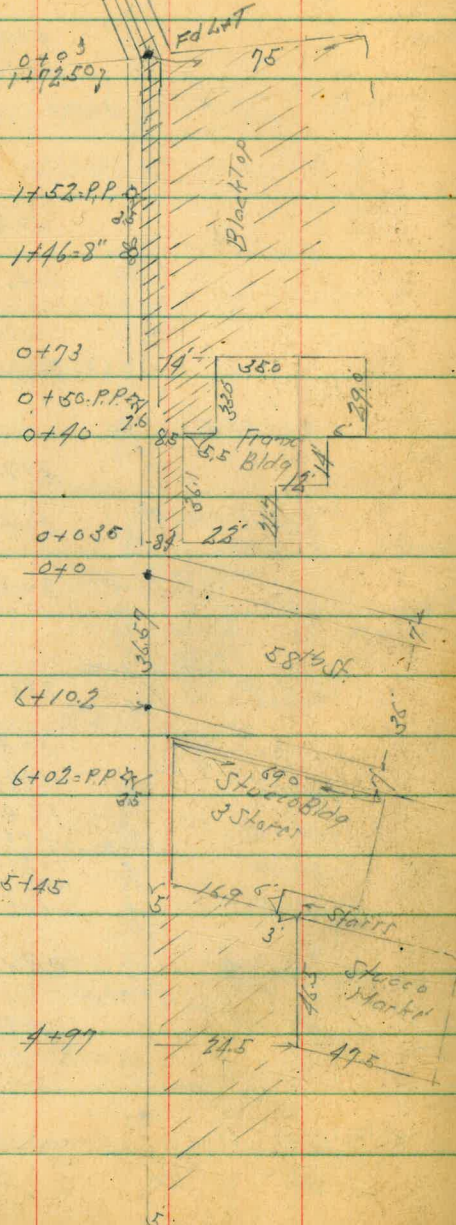
Sign Light

1950 Paper Pole

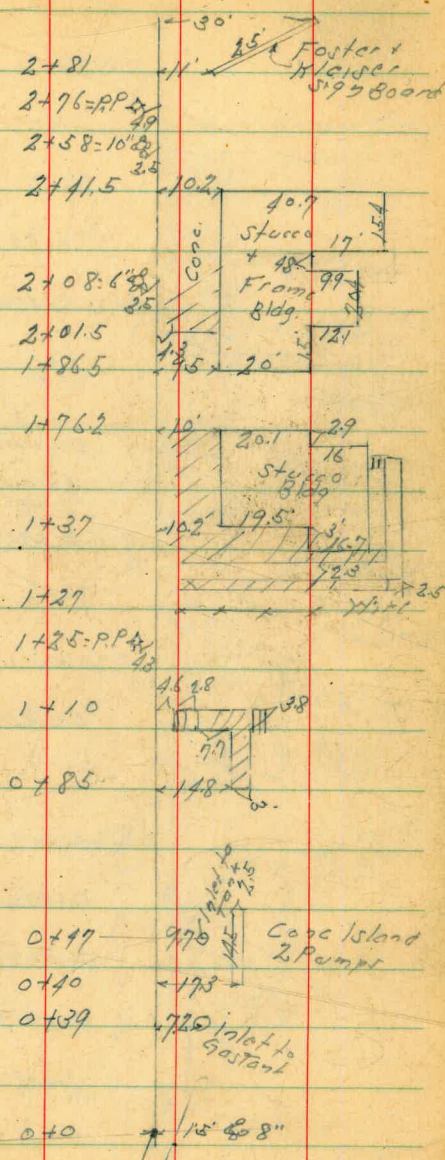
W.C.



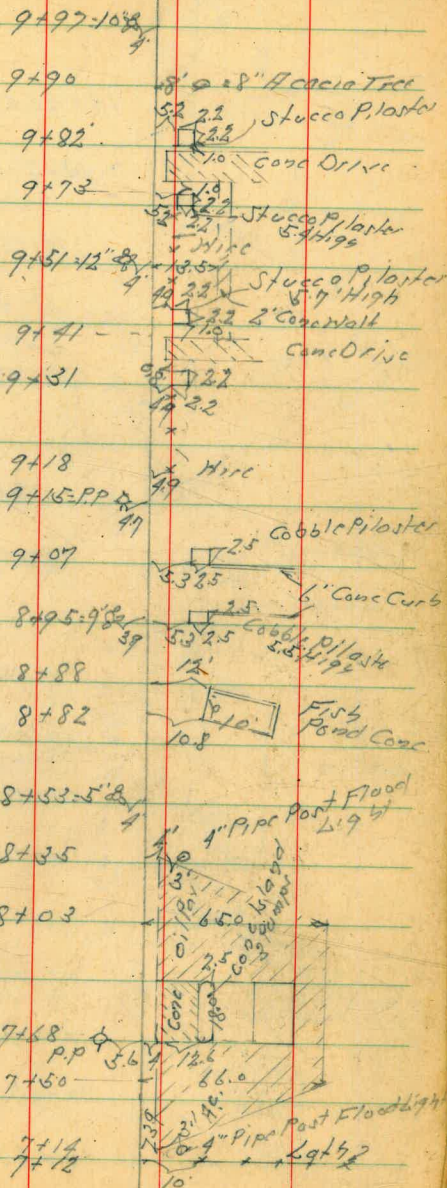
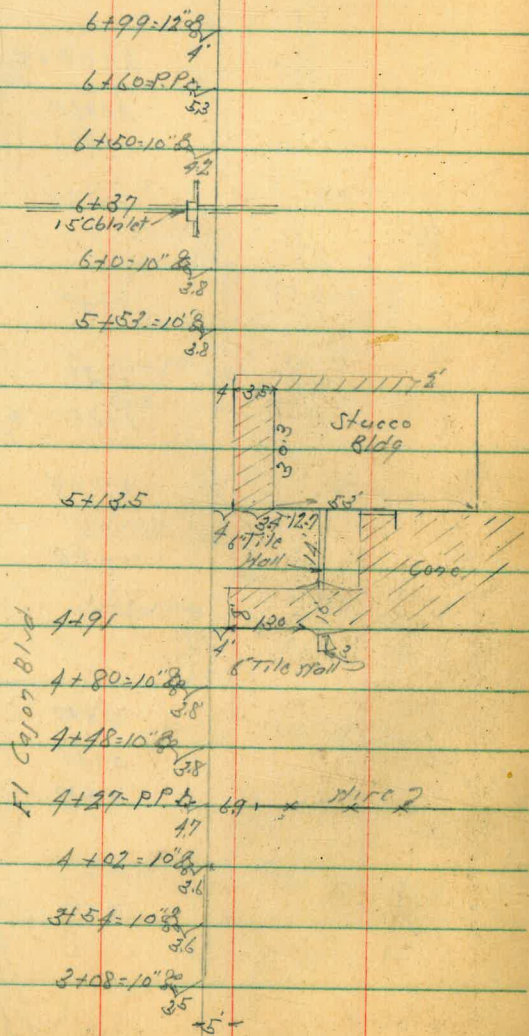
El Cajon Blvd.



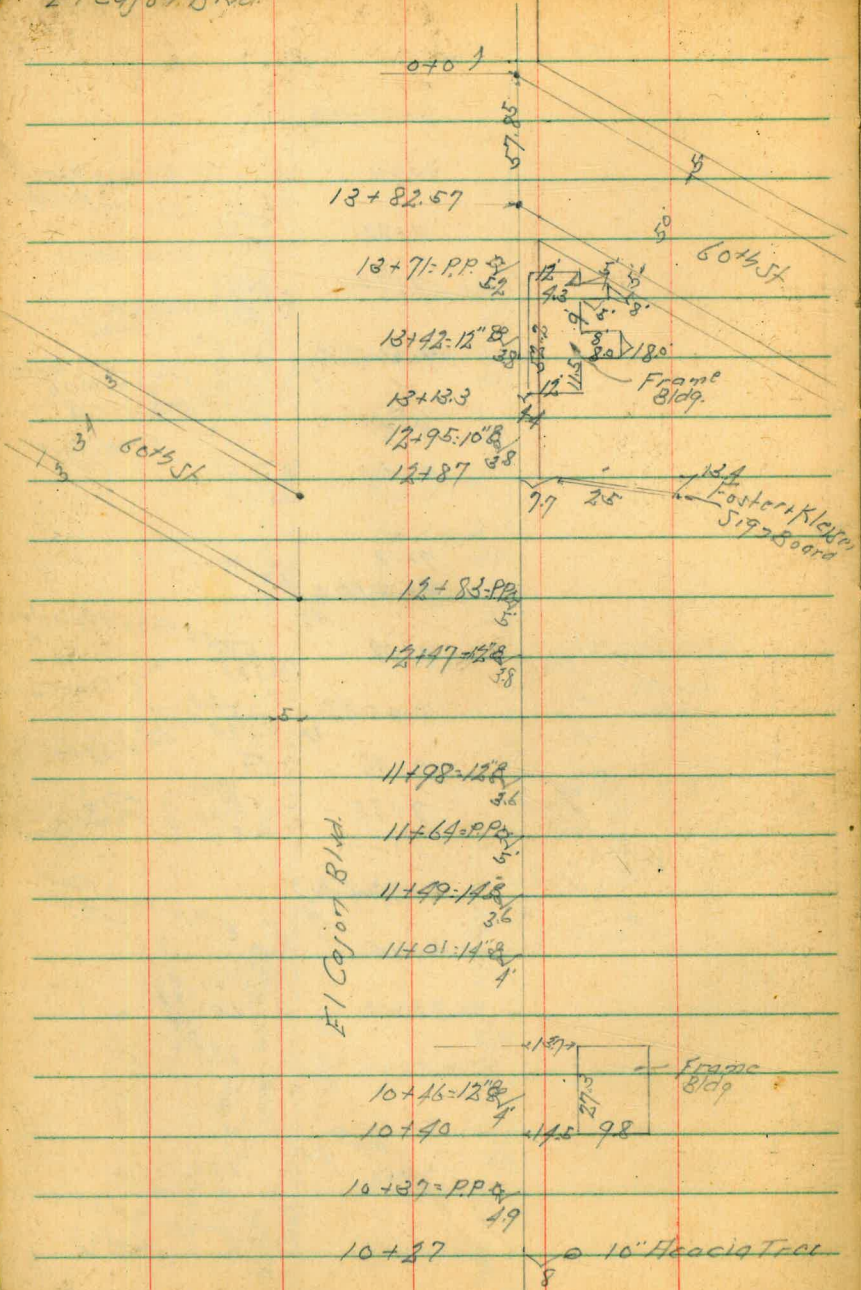
Alice St.



59th St.

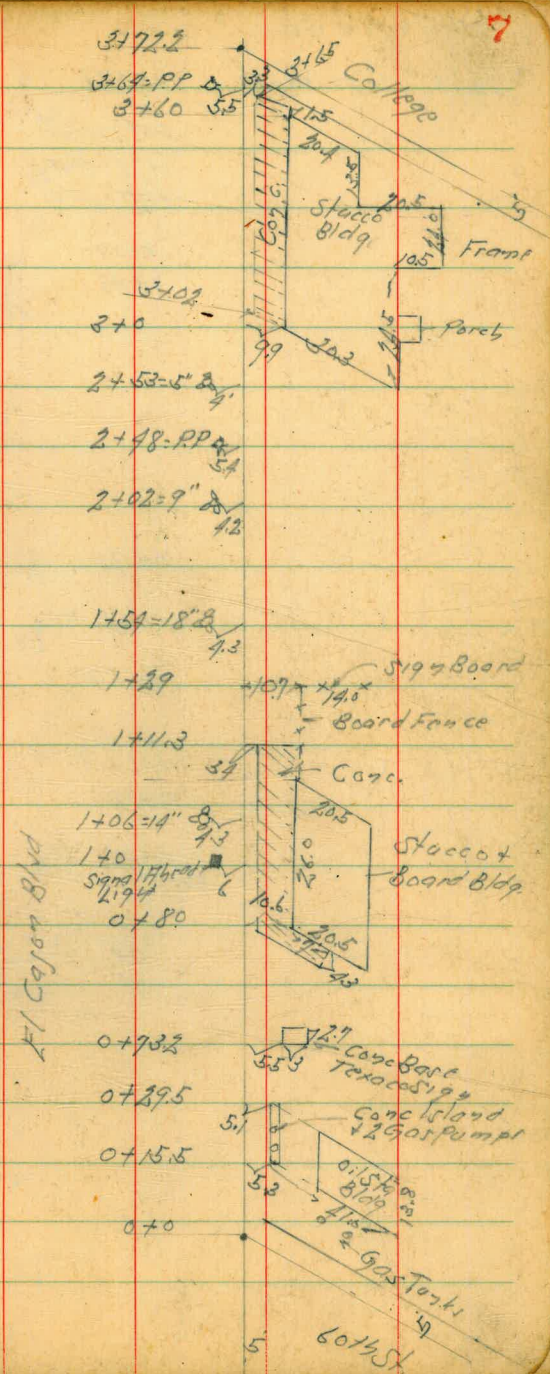


El Cajon Blvd.



El Cajon Blvd.

Nov. 1-45
S. 5007
BLIN
osborne



El Cajon Blvd.

El Cajon Blvd

East " 1580 Page 1 1+86.25

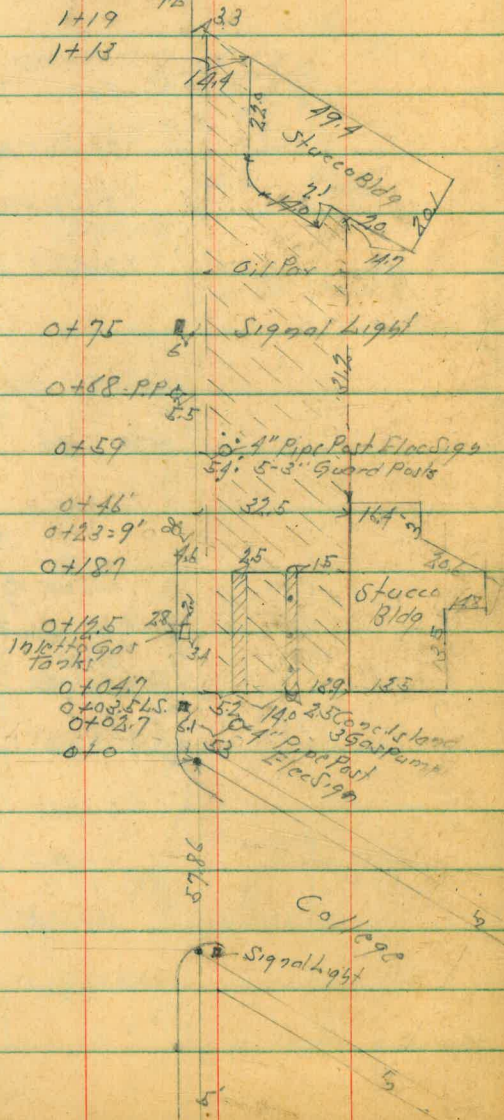
1+82 = PP 75

1+72 = 10' 55

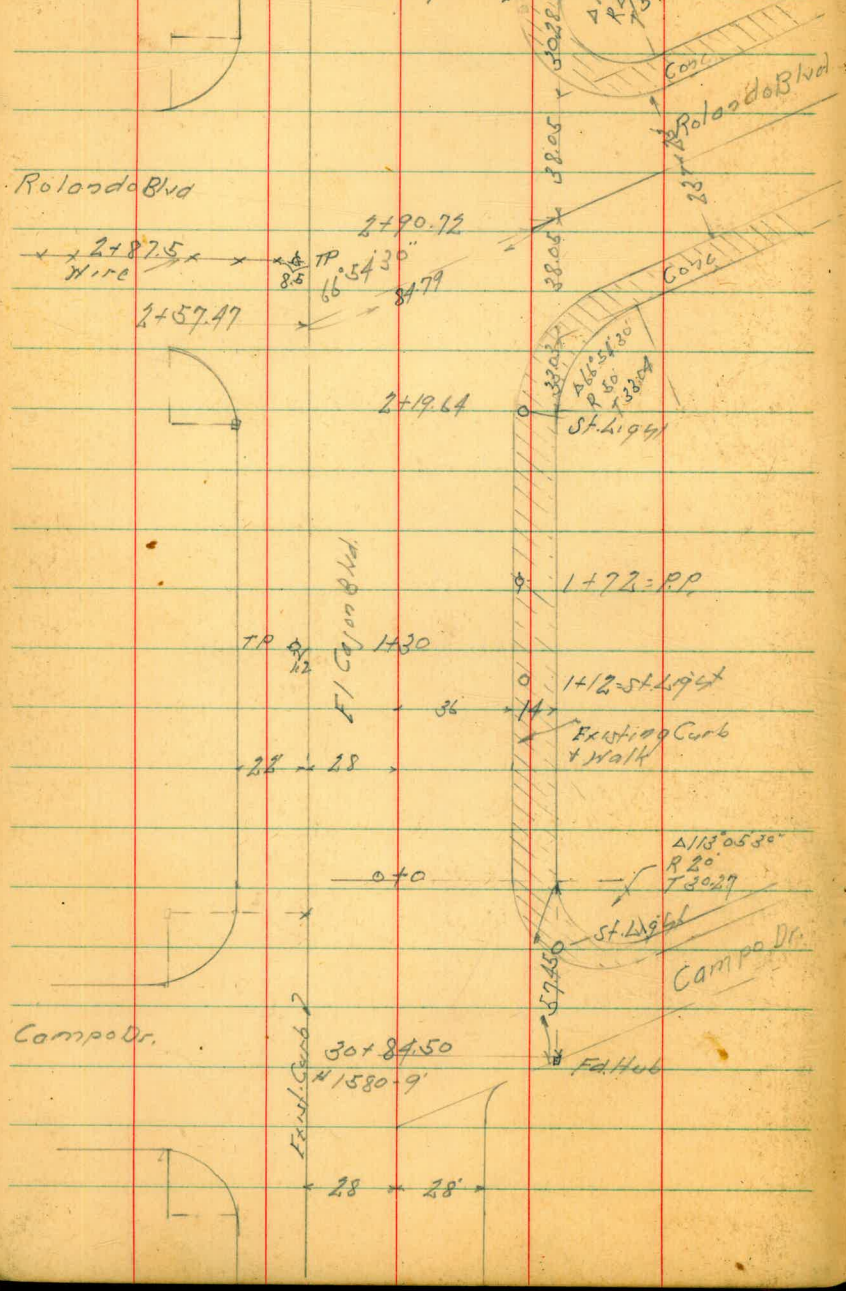
1+22 = 11' 82

1+19

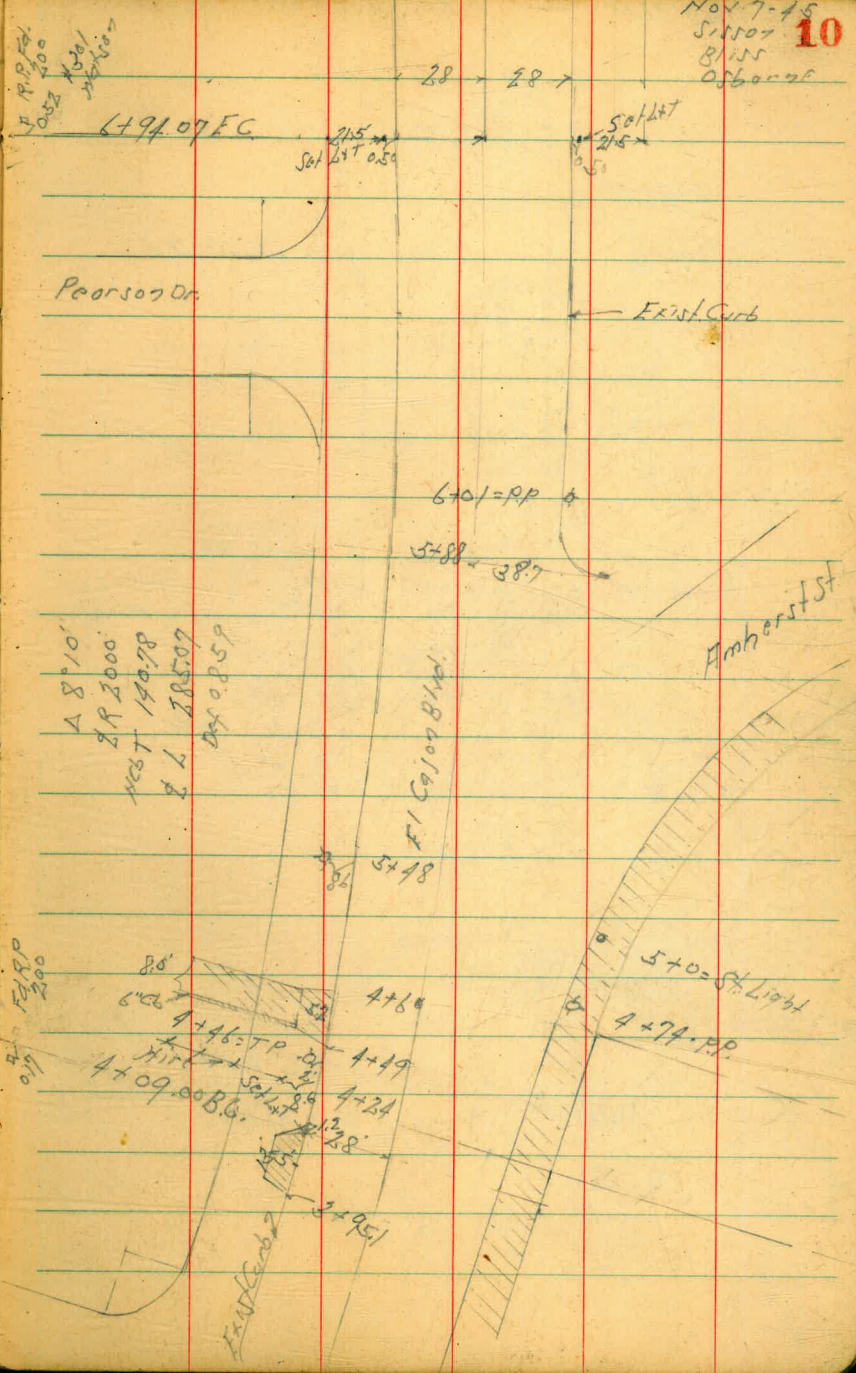
1+13



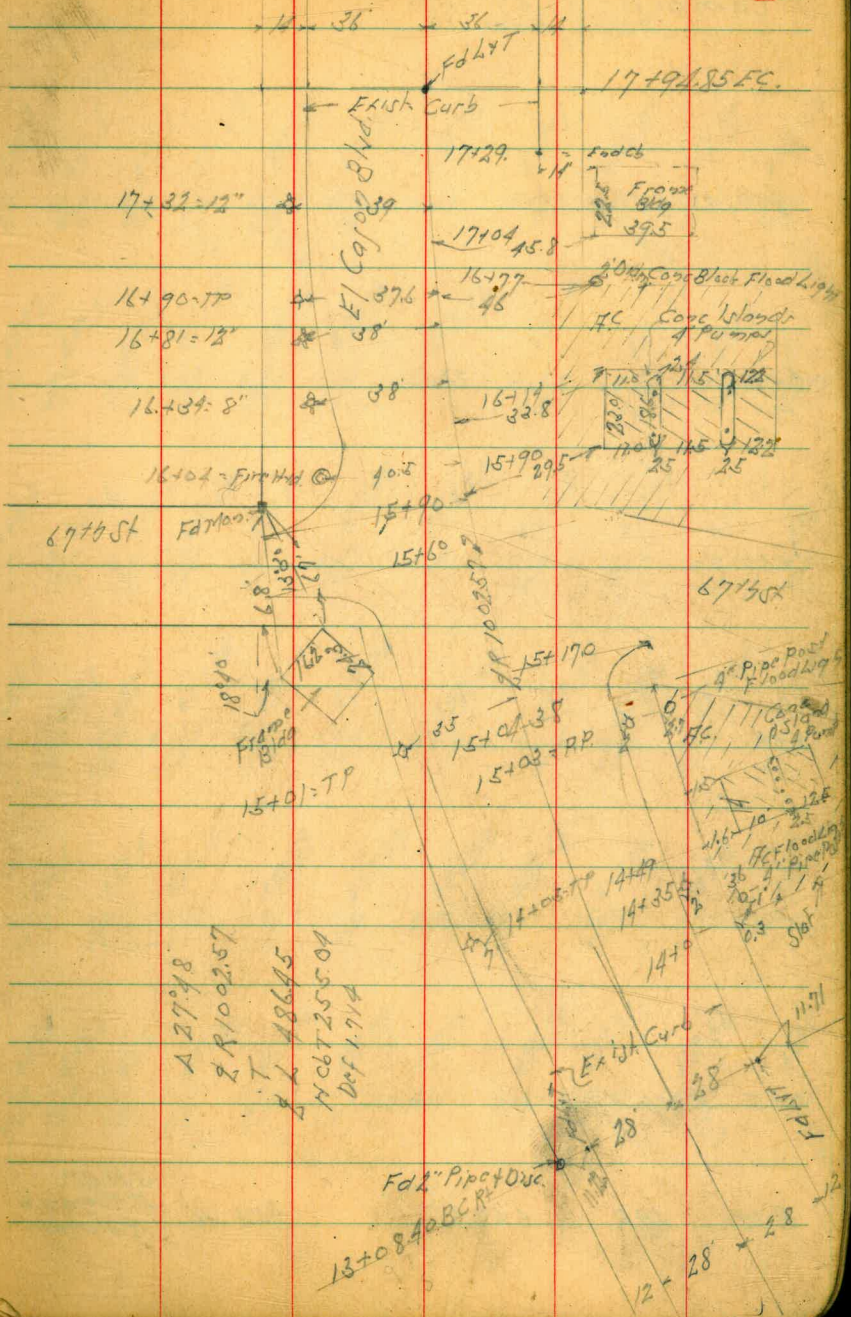
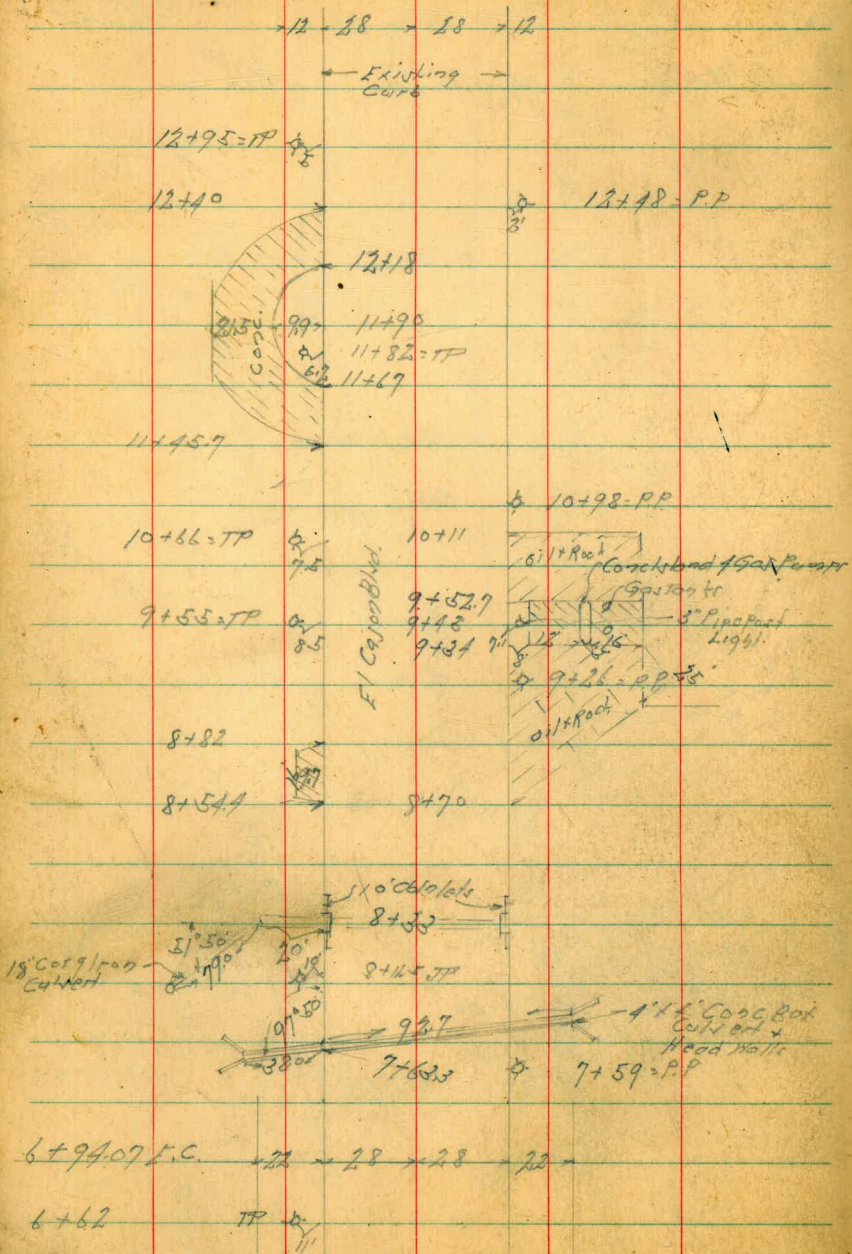
El Cajon Blvd. Topog. 2+63 = PP
 Campo Dr. to 67th St.
 3+60 St. Light
 3+59.05



Nov 7-15
 Sitton
 BAIN
 0.56000
10



F/Cajon Blvd.



Cross Section El Cajon Blvd.
 Campo Dr. to 67th St
 Sketch page 10

71964 - B.C. on Pt

7+0

+50

1+0

+50

0+0 Prop. EC Part of Campo

B.M

495

457.91

452.46

S.W.B.P.
 El Cajon
 Rolando

67-11

2

Nov. 13-45
 51500
 81111
 Osborn
 8099

Pt. 5 **12**

451.9 452.1 452.1 451.68 451.13 451.71 451.98 451.99 451.55 452.39 452.62
 55 53 53 57 68 57 54 54 58 50 49
 60 50 35 28 28 14 18 18 86-60 26 50-51/1014

450.7 452.2 452.3 451.72 451.18 451.73 452.06 452.06 451.59 452.41 452.64
 67 52 49 56 62 56 53 53 58 50 47
 60 50 35 28 28 14 18 18 36 36 50

448.9 449.6 450.5 451.88 451.25 451.84 452.20 452.22 451.74 452.47 452.71
 69 78 60 53 61 57 52 51 56 49 47
 60 50 38 28 28 14 18 18 36 36 50

450.5 450.7 452.0 452.08 451.49 452.08 452.34 452.37 451.91 452.60 452.79
 69 57 54 53 59 53 50 50 55 48 46
 60 50 34 28 28 14 18 18 36 36 50

452.1 452.5 452.15 451.57 452.22 452.52 452.48 452.06 452.71 452.95
 53 49 56 58 51 48 49 53 47 44
 60 50 28 28 14 18 18 36 36 50

449.5 452.1 452.7 452.32 451.66 452.39 452.70 452.73 452.21 452.86 453.05
 79 73 47 50 57 50 47 48 52 45 43
 60 50 38 28 28 14 14 18 36-60 36 50-51/1014

457.41

+5905 = Prop. EC. on Rt.

+328

3+27

TP 581 455.28 594 451.47

+9072 = 1/2 Rolando on South

+75

2+57

457.41

450.5 18 50	450.5 18 50	450.95 133 28-06	450.38 190 28-50	450.91 137 14	451.14 114	451.17 118 18	450.87 131 28-50	451.77 135 28-50	451.96 132 50-50
450.5 18 50	450.6 17 50	451.06 122 28	450.46 182 28	451.13 115 14	451.41 127	451.39 128 18	451.00 120 36	451.10 118 50-50	451.76 122 50-50
450.5 18 50	450.6 17 50	451.10 118 28	450.90 128 28	451.17 111 14	451.45 122	451.43 125 18	451.03 125 36	451.20 108 50	451.24 104 70-50
456.28									
450.8 66 50	450.8 66 50	450.64 677 28	451.26 695 14	451.64 577	451.65 576 18	451.25 616 36	451.83 552 50		
451.1 63 50	451.2 66 50	451.37 689 28	450.78 663 28	451.46 595 14	451.74 567	451.75 566 18	451.33 608 36	451.71 570 50	451.67 574 72-50
452.1 53 50	452.2 53 50	451.49 592 28-06	450.95 646 28-50	451.56 585 14	451.82 559	451.83 558 18	451.37 604 36	451.61 590 50-50	452.16 525 50-50
457.41									

+88

441.1	441.6	443.0	442.85	442.28	443.14	443.50	443.60	443.37	443.12	443.80	443.4
75	70	56	578	635	579	513	503	526	537	480	52
80	50	43	28.25	28.50	17	14	28	387	501	387	50

+50

445.0	445.0	444.72	444.16	444.94	445.23	445.30	445.10	444.85	444.67	445.28
36	26	391	447	369	340	333	352	328	326	335
80	50	28	28	14	14	28	50	86.5	501	28

5+0

447.6	447.8	447.11	446.48	447.18	447.45	447.54	447.07	446.90	447.56	447.65
10	80	103	215	145	118	107	154	167	107	098
80	58	28	28	14	18	36	41.501	41.50	50	50

TP 1.18 448.63 7.83 447.45

+50

448.8	449.0	449.25	448.82	449.14	449.26	449.25	448.95	449.04	448.86
65	63	603	664	614	603	603	603	634	543
80	50	28	28	14	18	36	4901	36.1	50

+09.0 = B.C.LL

449.8	450.0	450.06	449.68	450.18	450.26	450.28	449.91	450.73	451.00
55	52	522	564	510	502	500	537	455	438
80	30	28.001	28	14	18	36	36	36	36

410

450.0	450.0	449.97	449.90	450.36	450.43	450.47	450.07	450.97	451.22
53	53	531	528	499	485	481	521	431	406
80	50	28.501	28.501	14	18	36	36	36	36

455.28

455.28

7+50

4110
30.3
100
30.1
94

7+25

4109
30.4
100

19107 = EC

4114
26.9
100
27.3
68

6+50

TP 1.81 441.29 9.15 439.48

6+0

448.63

425.7 435.2 435.19 434.59 435.30 435.54 435.36 434.68 435.21 434.8 424.1
56 61 610 670 599 575 593 661 608 65 17.5
50 86 28.06 28.54 14 14 28 28 28.23 35 30
225 265 260
10 70 100

412.0 426.3 436.0 435.87 435.29 436.04 436.29 436.09 435.43 436.00 435.9 425.6
293 150 530 542 600 525 500 520 581 539 54 157
73 50 35 28 28 14 14 17 28 28 34 50
419.9 412 423
314 201 190
60 25 700

427.0 437.2 437.08 436.50 437.29 437.52 437.33 436.63 437.24 437.0 423.0
143 91 421 429 400 377 296 466 405 40 42.0
50 34 28 28 14 377 14 28 28 33 50
425.0 417.3
15.3 140
10 20

426.3 429.0 439.1 439.38 438.81 439.63 439.38 439.26 439.13 439.72 449.5 435.1
150 122 22 191 248 166 141 153 216 157 1.8 6.2
30 50 34 28 28 14 14 28 28 28 35 45

437.4 440.3 442.5 442.22 441.66 442.51 442.91 442.94 442.65 443.25 443.4
112 83 51 641 697 612 572 569 598 538 53
65 50 36 28x6 28.54 14 14 28.54 28.06 50
441.29 434.9 435.6
57 57
10 10

448.63

El Cajon Blvd.

8+50

8+33 = Carb Inlets Rt & Lt

8+0

7+75

7+63 = 4'x4' Conc Box Culvert N Carb Station 109

441.29

423.2
181
100

423.5
128
70

419.7
26
100

414.4
26.9
100

Lt

Rt

Fl

16

432.5 88 70	433.7 76 50	434.26 70.2 28.56	434.51 77.8 28.56	434.29 7.00 14	434.42 6.87 14	434.29 7.74 28	433.55 7.85 28	434.24 6.9 36	434.4 6.9 36	429.6 11.7 50	
432.9 84 56	434.3 72 45	434.27 70.2 28.56	434.21 67.8 28.56	434.26 8.88 28.56	434.22 7.07 14	434.39 6.90 14	434.24 7.05 14	433.24 8.05 28	429.44 11.85 28	434.27 7.02 36	434.4 6.9 36
417.9 234 63	423.9 174 50	434.2 71 35	434.24 6.95 28	433.73 7.56 28	434.47 6.82 14	434.62 6.57 14	434.46 6.85 14	433.82 7.47 28	434.23 6.96 28	434.0 7.3 36	434.1 1.66 50
414.0 27.9 77	426.3 1.50 50	434.5 6.8 37	434.64 6.65 28.56	434.06 7.22 28.56	434.80 6.49 14	434.99 6.20 14	434.79 6.50 14	434.16 7.12 28	434.73 6.56 28	434.1 3.6 36	433.5 1.98 50
412.53 28.76 Fl out of 18" Corp Culv	412.53							417.5 23.8 65	414.1 26.6 100		
				410.09 31.20 66 = Flank outlet				411.54 39.75 87.7 = Flank inlet			

441.29

Lt.

S

Rx

11+0

445.4	442.5	442.83	442.18	442.78	442.10	442.90	442.24	442.80	442.2	442.0
12	31	374	459	379	347	367	432	377	34	46
50	43	28-cb	28-50d	14		14	28-50d	28-cb	38	10

+50

443.1	441.0	440.30	439.68	440.31	440.52	440.33	439.80	440.6	445.7
35	56	627	689	626	605	624	677	60	09
50	42	28	28	14		14	28-50d Drive	40	50

10+0

440.6	438.8	437.92	437.29	437.95	438.18	438.02	437.45	437.9	438.1
60	78	865	928	862	829	855	912	87	85
50	42	28	28	14		14	28-50d Drive	43	50

+50

436.3	436.06	435.45	436.15	436.26	436.07	435.46	435.99	436.50
10.3	10.51	11.2	10.92	10.31	10.50	11.1	10.58	10.37
50	28	28	14		14	28-50d	28-cb	50 on-line

TP

11.24

446.57

596

435.33

446.57

9+0

434.4	435.2	434.79	434.88	434.88	434.99	434.82	434.31	434.9	434.8
69	51	650	741	641	680	627	628	54	65
70	50	28-cb	28-50d	14		14	28-50d Drive	50	75

441.29

441.29

12+50

12+32

11+90

11+58

TP 10.67 456.43 0.81 115.76

11+40

446.57

450.2 449.70 448.96 449.72 449.91 449.74 449.07 449.68 449.6
 6.2 6.87 7.47 6.71 6.52 6.69 7.36 6.75 6.8
 50 28 28.5ul 14 14 14 28.5ul 28.6 50

450.31 448.41 448.34 449.02 449.30 449.13 448.41 449.03 449.4
 6.12 8.02 8.09 7.41 7.12 7.30 8.02 7.40 7.0
 50 28 28 14 14 14 28 28 50
 50-51/2
 50

449.63 448.62 447.27 446.65 447.29 447.53 447.36 446.69 447.28 447.3
 6.80 7.81 9.16 9.78 9.14 8.90 9.07 9.74 9.15 9.1
 50 38-51/2 28 28 14 28 14 28 28.6 50
 50-50.5

448.05 445.19 445.09 445.79 446.01 445.86 445.19 445.82 445.8
 8.38 11.34 11.34 10.64 10.42 10.57 11.24 10.61 10.6
 50 28 28.6ul 14 14 14 28 28 38
 50-51/2 50-51/2 50-6ul 51.3 51.4
 51 50
 456.43 50

447.2 444.86 444.23 444.89 445.12 444.92 444.29 444.86 445.3 450.3
 1.96 1.71 2.21 1.68 1.45 1.55 2.28 1.71 1.3 1.37
 50 28.6 28.5ul 14 14 14 28.5ul 28.6 38.43
 446.57 51.2
 50

TP 6.32 460.03 2.72 453.71
 SWBP
 E/C0100 ✓
 67 1951
 453.70

1570

150

1410

150

1370840 = BC RT

45643

Lt. 2 Rt. 19

4528 453.63 453.00 453.77 453.91 453.68 453.06 453.69 453.42
 5.6 2.80 3.43 2.66 2.52 2.75 2.87 2.80 3.01
 50 33-23 33-24 14 14 14 28-54 28-52 50

4530 452.52 453.18 453.30 453.18 452.55 453.16 453.54
 5.4 3.91 3.35 3.13 3.35 3.81 3.37 2.91
 50 31.9 31.9 14 14 28 28 50

452.1 452.51 451.87 452.58 452.75 452.57 451.88 452.44 452.78
 5.2 5.93 4.56 3.85 3.68 2.86 4.55 5.99 3.65
 50 30.6-63 30.6-64 14 14 14 28 28 50

451.7 451.4 451.19 451.87 452.11 451.88 451.16 451.76 451.3
 4.7 5.0 5.24 4.56 4.32 4.55 5.27 4.67 5.1
 50 30 29-54 14 14 14 28 28 50

451.6 451.22 450.58 451.03 451.42 451.19 450.46 450.6 450.8
 4.8 5.21 5.95 5.4 5.51 5.24 5.97 5.37 5.6
 50 28-56 28-54 14 14 14 28 28-56 50

45643

E/Cajon 8/20

16+19 = C6 End on Lt

16+0

+90 = C6 End on Lt

+60 = C6 End on Lt

15+17 = C6 End on Rt

160.03

Lt

Rt

Rt

20

4551	455.09	454.53	454.88	454.90	454.72	454.22	454.50
49	4.94	5.50	5.15	5.13	5.01	5.81	5.53
50	34.6-C6	34.6-50	14		14	28	50 on Rt.

457.6	454.76	454.14	454.31	454.65	454.69	454.48	454.09	454.53
54	5.27	5.89	5.72	5.38	5.34	5.55	6.00	5.50
50	12-C6	12-50	34	14		14	28	50 on Lt

452.04	453.59	453.76	454.11	454.54	454.64	454.38	453.81	454.28
7.09	6.44	6.27	5.92	5.49	5.43	5.65	6.27	5.75
71-90	71-C6 End	50	33	14		14	28	50 on Lt

452.98	453.04	453.24	453.66	454.23	454.35	454.16	453.64	453.59
7.10	6.99	6.79	6.27	5.80	5.68	5.87	6.39	6.44
81-90	81-C6 End	56	34	14		14	28	50 on Lt

453.3	453.74	453.09	453.93	454.04	453.86	453.31	452.93	453.30
6.7	6.27	6.94	6.10	5.99	6.17	6.73	7.10	6.73
50	33-C6	33-50	14		14	28	710	403-C6 End
							452.81-54	
							7.6	50 on Lt

160.03

19485 EC

150

1710

16150

460.03

44

8

PT

21

456.2	456.03	455A3	456.25	456.26	456.31	455.60	456.12	455.53	454.6
2.8 50	1.00 36.1 -06	1.60 36.1 -94	3.28 14	3.17	3.72 14	1.13 35.64	3.91 36.1 -03	4.5 44	5.1 50

455.2	455.7	455.88	455.26	455.97	456.08	456.03	455.65	455.37	456.03	455.7
1.8 50	1.3 37	1.15 36.1 -06	4.77 36.1 -94	4.06 14	3.25	1.00 14	1.38 38	4.66 35.64	4.00 35.64	4.0 50

455.2	455.4	455.02	455.72	455.71	455.58	455.08	454.86	455.53	454.1
1.8 50	1.6 14	5.01 36.1 -94	4.01 14	4.32	1.45 14	4.95 28	5.17 36.1 -94	4.5 45	5.9 50

455.0	455.29	454.73	455.28	455.31	455.04	454.59	454.66
1.5 50	1.3 36.1 -06	5.58 36.1 -94	4.76 14	4.70	1.39 14	5.4 38	5.27 50

460.03

X sec 20 E and W ALLEY

Blk. 62 E.W. Moose Sub.

C. Moore
S. J. M. Moore
M. Moore
1-18-46

NWBP 1.58 208.56 o.k. 206.98 #428th

check to NWBP A. and G. Canada 3.00 205.56 205.50
0.06

T.P. Nail 1.53 206.44 2.65 204.91 #420 on E
NAIL IN Header

T.P. 1.72 195.45 12.71 193.73

0-10 in gutter

S 3.87

E 4.21

N 4.53

0-10 top curb

N 3.89

E 3.57

S 3.20

0-2.5 W.L. 5' Con. Walk

S 3.12

E 3.45

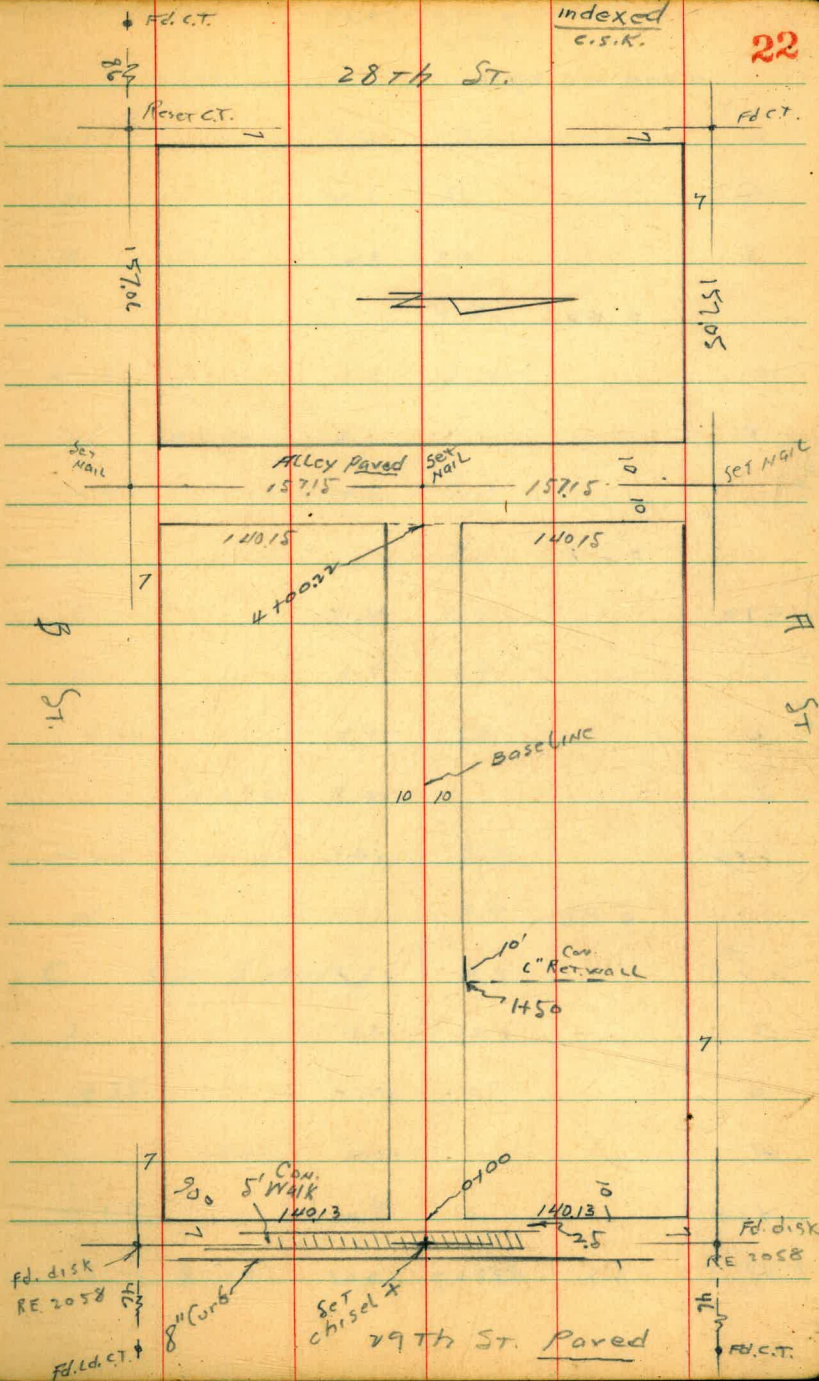
N 3.75

Fd. C.T.

indexed
C.S.K.

22

28th St.



195.45

0+00 WL 29th

N 3.5

E 3.2

S 3.0

0+06

S 3.1

E 3.2

N 3.2

0+18

-70 4.5

N 7.3

C 9.0

S 10.7

+10 10.0

0+31

-15 13.7

S 13.2

C 12.4

N 10.4

+10 9.0

T.P. 0.29 183.07 12.67 182.78

183.07

0+43

-15 1.3

N 3.1

C 2.4

S 2.8

+20 3.2

0+60

-25 7.3

S 7.1

C 6.6

N 5.9

+20 5.8

0+75

-25 8.2

N 9.9

C Run S.M.H. 9.5

S 10.8

+35 12.7

1+00

-35 12.4

S 10.9

23

ATTENTION!
C.R.H. and PHILL

183.07

C		10.6	
N		9.1	
+30		8.5	
	1+25		
-30		8.6	
N		9.9	
C	Run S.M.H.	10.2	
S		11.0	
+35		12.3	
	1+50		
-20		6.7	
-5		5.8	
S		2.4	
+3		1.5	
C		0.9	
N	6" Con. Ret. Wall	1.8	Base
N	Top "	+2.1	Top
+15		1.5	Base Wall
+15	Top wall	+2.0	

183.07

24

	1+51		
-15		+1.6	
N	Top wall	+2.1	
N	Base	0.8	
C		0.6	
+9.2	N end 8" Con. Ret. Wall and 8y. wire Fence	1.3	Top
S		1.3	
+15	Top wall	1.7	
+15	ground	6.4	
T.P.	1232	194.96	0.43 182.64
	1+63		
N	end Retain wall and 8y. wire fence	0.3	back
	1+66		
-12	Top another wall	10.2	
-12	ground of Base	12.7	
S	Top wall	9.9	
S	ground	11.8	
+2		7.7	
C		6.0	
+5		5.3	
N		8.6	
+10		8.0	

194.96

T.P. 11.48 205.22 1.22 193.74

1+90

-10

10.4

N

11.4

+5

9.0

C

9.8

S

13.8

+15

15.4

2+13

-10

11.2

S

10.8

C

7.2

+5 10" di. Pepper Tree

+8

6.8

N

8.4

+10

8.2

2+23

S+7.0 Cor. 14" PP.

2+29

S+0.8 end wire fence

NE Cor Bd garage

Bd. fence ends on N-ox

205.22

25

1+38

-4.3

9

Gar. dirt floor

5.6

N

6.0

C

6.4

+9.2

Sin gar.

Cow floor

6.85

2+44.5

S+0.9

NW Cor

Bd

garage and Beg wire fence

2+75.5

-5

4.6

S

3.9

C

3.9

N

3.3

+3

E Sin gar.

Cow floor

3.00

2+86

N-0.5

5' di. STUMP. and Beg. wire fence on LINE

S-1

end wire fence

2+92.6

S-1

E Sin gar dirt

3.8

3+00

N

2.0

C 29

S 3.3

+5 3.4

3+7.5

S+4.3 14" P.P.

3+28

N+0.2 end wire fence

3+48

-S 1.6

S 1.6

C 1.3

N+0.5 E Sing. gar. dirt 1.1

3+50

N Beg. Lark fence

3+61.6

End Lark fence +

N S.E. Cor House on line 0.9

C 1.1

+9.9 E do. gar. dirt fl. 1.1

4+00.22 = E.L. H + S alley

S Rough pay. 0.60

C pay. 0.36

N pay + pause ^{SW Cor.} 0.14

4+10.22 E H + S alley

N pay. 0.39

C " 0.66

S " 0.91

check to T.P. P. 0.30 204.92 204.91 ✓

X sec of Snowdrop St.

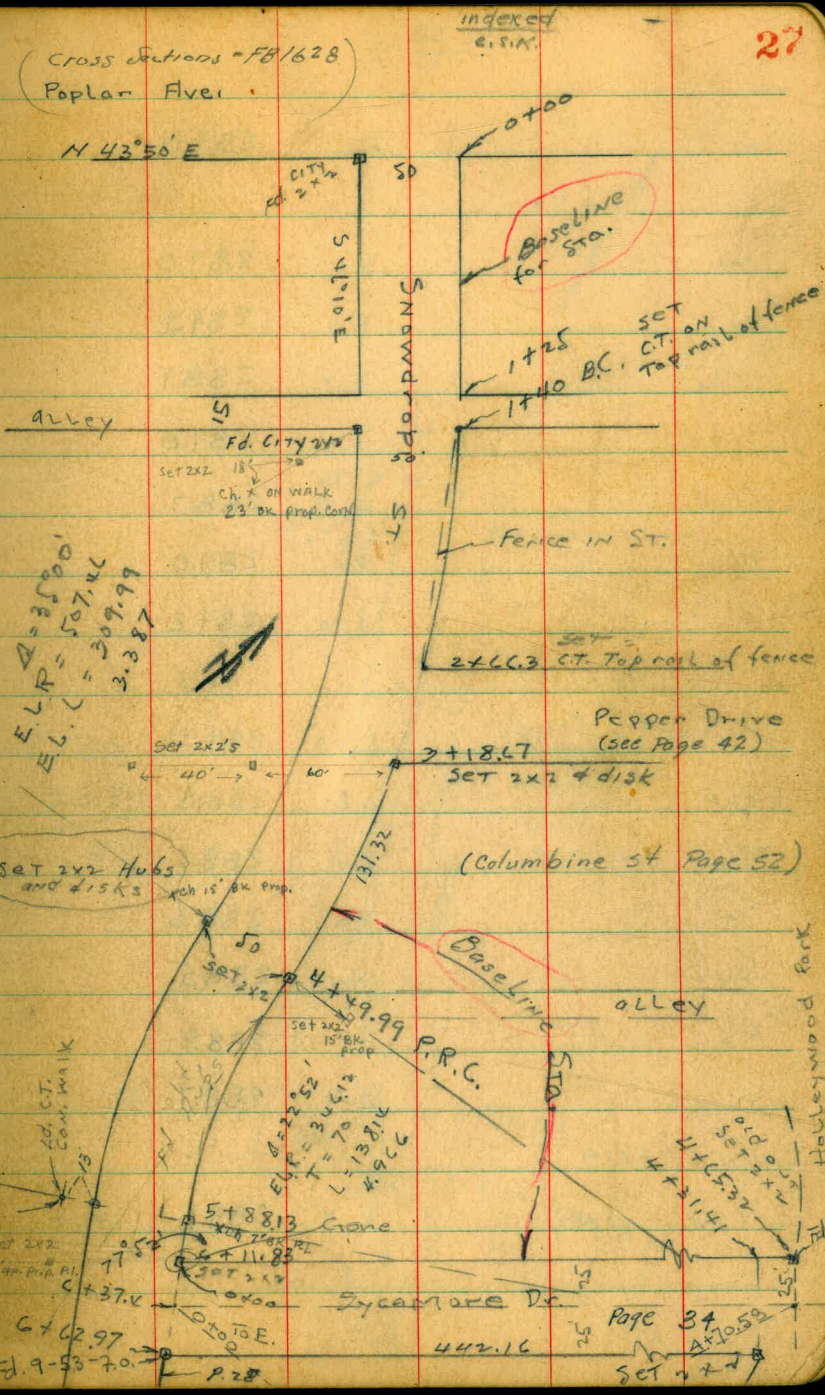
50' wide
10' cbs
7.8, 1/4 S

Poplar to Sycamore and
Sycamore, from Snowdrop Fly

Note! Sections
at 90° or Radial

C. Moore
Sommerville
N.E. 1/4
1-29-46

BM. SEBP	C. IX	303.33		297.19	Fairmont Quince
T.P.	0.45	299.25	4.53	298.80	
T.P.	0.33	290.91	8.67	290.58	
T.P.	4.93	294.29	3.55	287.36	
check to Snowdrop + Poplar		520		289.9	Record 289.14 0.05
SE Pipe Cor Snowdrop Poplar	3.44	292.58		289.14	Record
	0 + 00	S.L. Poplar			
E		3.5		289.1	
cb		3.9		288.7	
1 1/4		4.2		288.4	
C		4.2		288.4	
1 1/4		4.2		288.4	
cb		3.6		289.0	



indexed
e. s. n.

27

Cross Sections - FB/628
Poplar Ave.

Alley

Fd. City 2x2
SET 2x2 15'
CH. X ON WALK
23' BK Prop. Conf.

EL. R. = 350.00
EL. C. = 507.46
= 309.99
3.387

Pepper Drive
(see Page 42)

(Columbine St Page 52)

Baseline
Alley

Fd. C.T. Comp. Walk
SET 2x2
Comp. Prop. Pt.
C. 1-37.6

EL. R. = 222.52
L. = 34.512
L. = 70
L. = 13.814
966

5+88.13
11.83
SET 2x2
6+62.97
0+00

Sycamore Dr

Page 34
At 10.52

Fd. 9-58-70.
P. 28

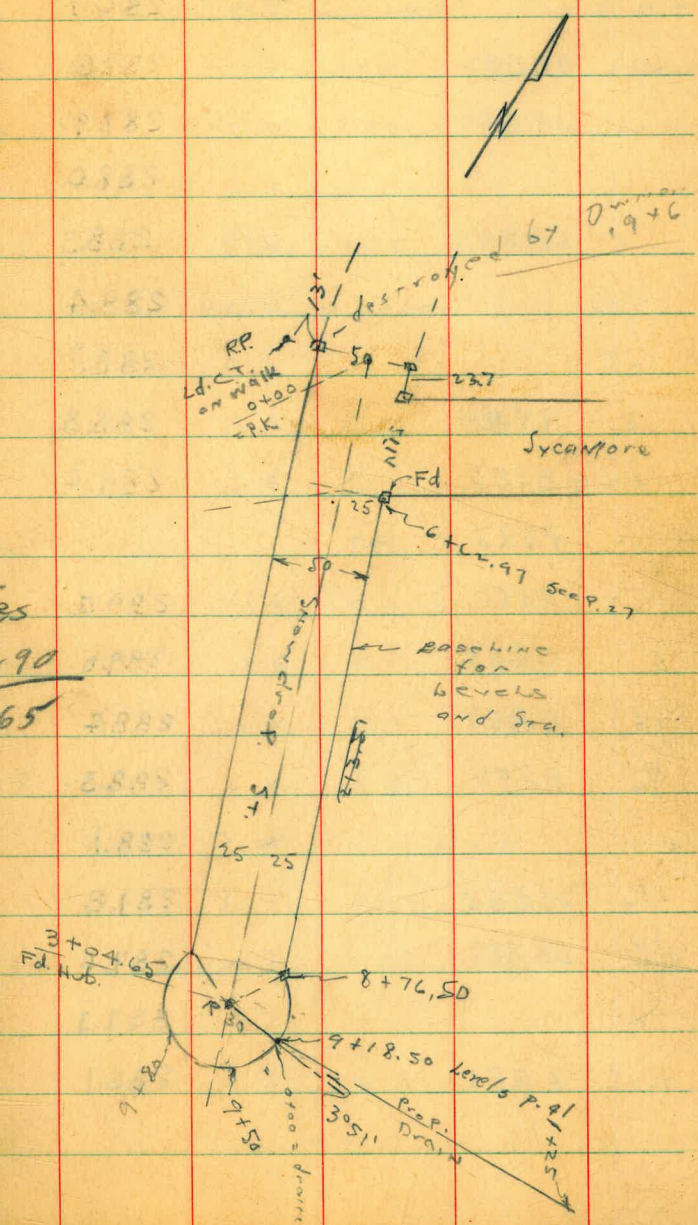
442.16

SET 2x2

w		3.6	289.0
	0+50		
w		3.6	289.0
cb		3.3	289.3
1/4		3.7	288.9
c		3.6	289.0
1/4		3.9	288.7
cb		3.6	289.0
E		3.4	289.2
	1700		
E	\$ 2.5 MARK	3.20	289.38
cb		3.8	288.8
1/4		4.0	288.6
c		4.0	288.6
1/4		4.1	288.5
cb		3.7	288.9
w		3.9	288.7
	1719		
E	+0.4 SINGAPORE	3.5	289.1

dirt

TICS
2290
65



1425

-25	5.9	286.7
W	5.1	287.5
cb	4.7	287.9
1/4	4.6	288.0
c	4.3	288.3
1/4	4.2	288.4
cb	3.9	288.7
E	3.8	288.8
+25	3.2	289.4

1440 BCBT

-25	3.1	289.5
E	3.6	289.0
cb	4.2	288.4
1/4	4.3	288.3
c	4.5	288.1
1/4	4.8	287.8
cb	5.0	287.6
W	5.3	287.3
+25	6.5	286.1

14474	⊕	Sim. 900.	Com. floor
E + 0.4		3.60	14 Street floor
E + 1.1		3.72	288.86 Com. Apron

1455

E	edge of 2' ^{Com} Walk	3.75	288.83
E + 2.2	Begin 3' High wire fence (in St.)		

1470

W	2885	5.5	287.1
cb	2885	5.1	287.5
1/4	2885	5.2	287.4
c	2885	4.9	287.7
1/4	2885	4.5	288.0
cb		4.3	288.3
+7	= fence	3.8	288.8

1487.5 ⊕ 3' Com. Walk

E	2885	3.73	288.85
+4.3	end walk	3.76	288.82 (in St.)
2700			
E	2885	4.0	288.6

+4.3 = fence in ST

	2+00			
E	cb		4.3	288.3
	1/4		4.6	288.0
	c		4.9	287.7
	1/4		5.2	287.2
	cb		5.3	287.3
	w		5.8	286.8
	2+12			
E	dirt		4.0	288.6
+1	fly edge	N + S CON WALK	4.00	288.58
+4'	fence	E of 3/4" high walk	3.95	288.63 \$ 997c
cb	in S CON WALK		4.05	288.53
+2	= end walk		4.10	288.48
	2+30			
w			5.7	286.9
cb			5.1	287.5
1/4			5.2	287.4
c			4.9	287.7
1/4			4.8	287.8
cb			4.5	288.1
+6.5	= fence			
E			3.9	288.7
	E of CON WALK	1.1	3.90	288.68

	2+46.3	= only Pepper	= Con. fence	
E			4.3	288.3
cb			4.5	288.1
1/4			5.0	287.6
c			5.1	287.5
1/4			5.3	287.3
cb			5.2	287.4
w			5.4	287.2
	E Pepper	Sec. = Radical		
w			5.5	287.1
cb			5.3	287.3
1/4			5.2	287.0
c			5.1	287.5
1/4			5.0	287.6
cb			4.9	287.7
E			4.9	287.7
	3+18.67	= Sly Pepper		
E	Req. distance		5.0	287.6
cb	5' High		5.5	287.1
1/4			5.9	286.7

	292.58		
c		5.8	286.8
1/4		6.3	286.3
cb		5.9	286.7
w		5.8	286.8
	3+50		
w		6.8	285.8
cb		6.8	285.8
1/4		7.0	285.6
c		6.7	285.9
1/4		6.7	285.9
cb		6.1	286.5
E		5.6	287.0
	4+00		
E		6.8	285.8
cb		7.1	285.5
1/4		7.8	284.8
c		8.0	284.6
1/4		8.3	284.3
cb		8.8	283.8
w		9.2	283.4

		292.58		31
T.P.	1.71	285.79	8.50	284.08
		4+29.99	PRC	
w - 10			7.0	278.8
w			4.9	280.9
cb			3.5	282.3
1/4			2.5	283.3
c			2.3	283.5
1/4			2.2	283.6
cb			1.3	284.5
E			0.9	284.9
		4+60.73	= only alley	
E - 25			0.1	285.7
				on N. Line
E			1.2	284.6
				Alley
				End. 6' High
				wire fence
				on N. Line.
		4+78.42	= S.L. alley	
E - 25			0.5	285.3
				on S. Line
E			1.8	284.0
				Alley
		4+89.5		
E			2.0	283.8
cb			2.4	283.4
1/4			3.4	282.4

285.79

285.79

32

1/4		3.4	282.4
c		3.1	282.7
1/4		3.5	282.3
cb		4.0	281.8
+9.5	± double 15' wide Ribbon drive, mean E.L.F.	3.96	281.83
A + 9.45			
W. = begin - picket fence (on line)			
5 + 1.3			
W	25' wide on walk. fence.	4.65	281.14
+0.5	End walk	4.64	281.15
cb		4.4	281.4
c		3.9	281.9
cb		3.7	282.1
1/4		3.9	281.9
+3		3.9	281.9
cb		2.8	283.0
E.		2.3	282.5
(East line stationing) 5 + 5.4			
W - 0.3	End picket fence.		

5 + 5.8			
E		3.1	282.7
cb		3.5	282.3
+5		4.6	281.2
1/4		4.6	281.2
c		4.5	281.3
1/4		4.9	280.9
cb		5.1	280.4
W		5.8	280.0
+2.0	± double 2' Ribbon drive. Tibbons Level	6.06	279.73 ₂₇
5 + 7.8			
W - 0.5	± 3' walk	6.15	279.64
E.C. = 5 + 88.13 (see P. 27)			
W		6.1	279.7
cb		5.8	280.0
1/4		5.3	280.5
c		4.9	280.9
1/4		5.1	280.7
cb		4.2	281.6
E		3.7	282.1

285.79

N. Line Sycamore Dr. 6+11.83 - Section at 90°

E.	4.3	281.5
ob.	4.5	281.3
+3	5.3	280.5
1/4	5.4	280.4
c	5.3	280.5
1/4	5.6	280.2
ob.	6.3	279.5
W	6.9	278.9

E, Sycamore (90° to snowdrop)

W-5°	8.0	277.8
W	7.5	278.3
ob.	7.0	278.8
1/4	6.4	279.4
c	5.8	280.00
1/4	5.5	280.3
ob.	5.4	280.4
E.	5.4	280.4

S. Line Sycamore 6+62.97 - 90° to snowdrop

E.	5.8	280.00
ob.	6.4	279.4

285.79

33

1/4	6.3	279.5
c	6.6	279.2
1/4	7.3	278.5
ob.	7.8	278.0
W	8.8	277.0
+10	10.1	275.7

7+00

W-	10.0	275.8
W	8.8	277.0
ob.	8.2	277.6
1/4	8.1	277.7
c	7.6	278.2
1/4	7.6	278.2
ob.	7.3	278.5
E	7.3	278.5

285.79

Set. Bal. Spike in S.E. cor. on
R. Polo. Sycamore & Snowdrop. 5.74 280.05

50' wide
10 CBS
7.5 W

Cross Sec. on Sycamore Dam

Snowdrap ELY

Spike B.M. 5.06 285.11 280.05 P 33

Sta. on N.L. Sec. at 90°

N	3.6	281.5
ob.	3.8	281.3
+2	4.6	280.5
1/A	4.9	280.2
C	4.8	280.3
1/A	5.0	280.1
ob.	4.8	280.3
S	5.0	280.1
+5	5.3	279.8
0+29		
S. Dirt	5.4	279.7
S. Top. N.+S. Rock Wall 2.8 wide	4.84	280.27
Top of N. End wall. +7 1/2 start picket fence	4.80	280.31
ob.	4.8	280.3
1/A	4.9	280.2
C	4.7	280.4

1/A	<u>285.11</u>	5.0	280.1
+3		4.9	280.2
ob.		3.2	281.9
N		2.9	282.2
0+45 & 42' Walk			
on & walk S-5		5.13	279.98
S		5.04	280.07
ob.		4.87	280.22
+3 1/2 End walk		4.84	280.27
0+62			
N		2.7	282.4
ob.		3.4	281.7
1/A		5.3	279.8
C		4.8	280.3
1/A		5.2	279.9
ob.		5.3	279.8
+2 1/2 End. E+W. Rock wall Top wall		5.25	279.86
S. Top. N.+S. Wall		5.30	279.81
S Ground		6.3	278.8

285.11

'0+74 : ϕ Single Garage

S-17 ²	^{c floor} Garage	7.60	277.5
S	conc. ribbons 5' center	6.30	278.8
+68		5.80	279.3

1+00

S-10		8.1	276.0
S		7.2	277.9
cb		6.4	278.7
1/4		5.8	279.3
C		5.4	279.7
1/4		5.6	279.5
+3		5.7	279.4
cb.		4.1	281.0
N.		3.3	281.8

1+35

N.		4.0	281.1
cb		5.0	280.1
+A		5.9	279.2
1/4		5.9	279.2
C		5.8	279.3

285.11

1/4		6.5	278.6
cb		7.1	278.0
S		7.9	277.2
+15		8.7	276.4

1+58

S-5	J.P.	7.5	277.6
-0.6	top. 5 wide E+M Wall. (Start wall).	7.04	278.07
S		7.3	277.8
cb		9.2	277.9
1/4		6.7	278.4
0		6.0	279.1
1/4		6.0	279.1
cb.		5.6	279.5
N		4.9	280.2

1+72 ϕ 3' Walk

S-0.3		6.81	278.3
-------	--	------	-------

1+87

N-5		5.5	279.6
N		5.6	279.5
cb.		5.9	279.2

35

285.11

1/4		5.9	279.2
C		5.9	279.2
1/4		6.2	278.9
cb		6.8	278.3
S		6.9	278.2
+0.2	Cor. 6" Conc. Ret. wall. Edge 10' wide dirt drive	6.70	278.4

1+97

S. Ground		6.8	278.3
S. Top Ret. wall,		5.7A	279.37

2+00

S. dirt		6.5	278.6
" top 6" Conc. wall		5.65	279.46
" begin wire fence (on line)			

cb. Ground		6.3	278.8
top. cobble wall		5.2	279.9

+2 beginning E.+W. cobble wall

1/4		5.9	279.2
C		5.6	279.5
1/4		5.7	279.4

36

285.11

cb.		5.6	279.5
N		5.5	279.6
+5		5.4	279.7
T.P.	7.31 287.48	4.9A	280.17

Beginning at 2+10 to 3+05

Line of 6 Acacia trees 2° S. of So. curb

2+30

N-5		7.3	280.2
N		7.4	280.1
cb		7.3	280.2
1/4		7.3	280.2
C		7.2	280.3
1/4		7.5	280.0
+5.5 Ground		7.3	280.2
top rock wall		6.3	281.2
cb.		6.8	280.7
S		6.9	280.6

2+57

S.	End. 35 Conc. Walk	6.04	281.44
----	--------------------	------	--------

287.48

~~285.11~~

2+74

E 10' conc. Drive

S-5	5.48	282.00
S	5.38	282.10
cb	5.5	282.0
1/4	5.9	281.6
C	5.9	281.6
1/4	6.1	281.4
ct	5.2	282.3
N	5.1	282.4
+5	5.1	282.4

3+00

N	4.1	283.4	
cb	4.3	283.2	
+5	5.4	282.1	
1/4	5.4	282.1	
C	5.1	282.4	
1/4	5.2	282.3	
+5.5	ground	5.1	282.4
	Top cobble wall	3.8	283.7
cb	4.6	282.9	
S	4.7	282.8	

287.48

~~285.11~~

3+20

End wire Fence on line

S	4.5	283.0	
cb.	4.4	283.1	
+2	1-p cobble wall	3.8	283.7
	Ground	4.9	282.6
1/4		4.9	282.6
C		4.7	282.8
1/4		5.0	282.5
+2		5.0	282.5
+5		4.3	283.2
cb		4.3	283.2
N		3.7	283.8
	3+60		
N		3.0	284.5
cb		3.3	284.2
+5		4.2	283.3
1/4		4.1	283.4
C		3.8	283.7
1/4		4.0	283.5
cb.		4.1	283.4
S		4.5	283.0

37

287.48

~~285.11~~

A+00

S-5	5.1	282.4	
S	5.0	282.5	
cl.	4.5	283.0	
1/4	4.1	283.4	
C	3.6	283.9	
1/4	3.2	284.3	
cl.	3.0	284.5	
N	2.9	284.6	
A+31.41 See Page 27			
N	3.2	284.3	
cl.	3.6	283.9	
1/4	4.2	283.3	
C	4.3	283.2	
1/4	5.0	282.5	
cl.	5.9	281.6	
S	7.35	280.13	on Hub
3+10	8.8	218.7	

A+65.32 = Sec. on Diag.

west line Hollywood park.

287.48

~~285.11~~

38

S	on Hub	7.35	280.13
s. cl.		6.4	281.1
♀	> calc. please	5.8	281.7
N. cl.		4.9	282.6
N.	on hub	4.42	283.06
287.48			
285.11			
T.P.	7.92	292.24	3.16 284.32
S.E. I.P. Poplar & snowdrop.		3.09	282.15 ✓
			282.14 0.01

$$\begin{array}{r} 287.98 \\ - 7.16 \\ \hline 280.82 \end{array}$$

C. Moore
 Springfield Add. Levels on Snowdrop =
 80995
 3-20-46 Sycamore to Sky and

Sketch P. 28

SP. 12 P. 10

SELY CON

1.80

281.85

280.05

Snowdrop
 Sycamore
 P. 33

for 7+00 sec p. 33

7+35 STA. ON E. LINE

- 10	6.7	275.2
E	6.5	275.4
cb	5.8	276.1
1/4	6.2	275.7
c	5.8	276.1
1/4	6.2	275.7
cb	6.1	275.8
w	6.9	275.0
7+10	8.0	273.9

7+65.25

- 10	11.3	270.6
w	10.1	271.8
cb	9.1	272.8
1/4	8.5	273.4

50' wide
 10' curbs
 7.5' 1/2"

281.85

indexed
 c. s. k.

39

C	8.0	273.9
1/4	8.2	273.7
cb	8.1	273.8
E	8.2	273.7
7+10	8.5	273.4
		7+85.70
- 10	10.5	271.4
E	10.2	271.7
cb	10.0	271.9
1/4	10.2	271.7
c	10.1	271.8
1/4	10.6	271.3
cb	11.2	270.7
w	11.9	270.0
7+10	12.9	269.0

T.P. 2.78 272.56 12.07 269.78

8+10

w-10

5.2 267.2

8+10 272.56

W	4.5	268.1
cb	3.7	268.9
1/4	3.4	269.2
C	2.9	269.7
1/4	3.3	269.3
cb	2.8	269.8
E	2.6	270.0
+10	2.9	269.7

8+45

-10	6.9	265.7
E	6.2	266.4
cb	5.1	266.5
1/4	6.4	266.2
c	6.2	266.4
1/4	6.7	265.9
ct	7.2	265.4
W	7.8	264.8
+10	8.3	264.3

8+76.5 Beg. of "Banjo"

-10	10.5	262.1
-----	------	-------

272.56 40

W	9.6	263.0
cb	9.6	263.0
1/4	9.4	263.2
C	8.6	264.0
1/4	9.1	263.5
cb	8.9	263.7
E	8.8	263.8
+10	9.0	263.6

9+18.5

Prop. Line	10.7	261.9
10' out	11.0	261.6

9+50

Prop. Line	11.8	260.8
10' out	12.1	260.5

9+80

Prop. Line	11.3	261.3
10' out	12.0	260.6

on 30' R. Hub

Hub	9.1	262.75
-----	-----	--------

P. 41 for draw levels

Levels for drain on
Sly end of Snowdrop St.

272.50

9+18.5 = 0.400 for drain 10.7 261.9 on Prop. Line

0+30 12.7 259.9

T.P. 0.34 260.19 ✓ 12.71 259.85 ✓

0+50 4.7 255.5

0+57 6.3 253.9

0+70 11.4 248.8

T.P. 0.20 247.39 ✓ 13.00 247.19 ✓

0+95 7.0 240.4

1+10 10.8 236.6

T.P. 0.10 236.69 ✓ 10.8 234.59

236.69

41

1+25 in Park 5.1 231.6 ^{could} _{exc'd} here

1+47 10.7 226.0

1+77 ^{Main} Bot. Wash 16.3 220.4

T.P. R. Hub 12.70 275.45 ✓ 26.25 P. 40

T.P. 9.19 282.89 ✓ 17.5 273.70 ✓

check to ^{Starting} BM 283 280.0 ✓ 280.0

Cross Sec. Pepper Dr. = 50' wide
 10' curbs
 75' HWS
 Snowdrop to Holleywood Park,
 and Holleywood Park
 to Columbine St.

Set 2"x2" hubs and disks
 N.L. = Sta. Baseline

S Ely Con				Poplar +
3/4" Pipe	3.48	292.62	289.14	Snowdrop P. 27

0+00 = S Ely Con, Pepper + Snowdrop
 Sec. at 90°

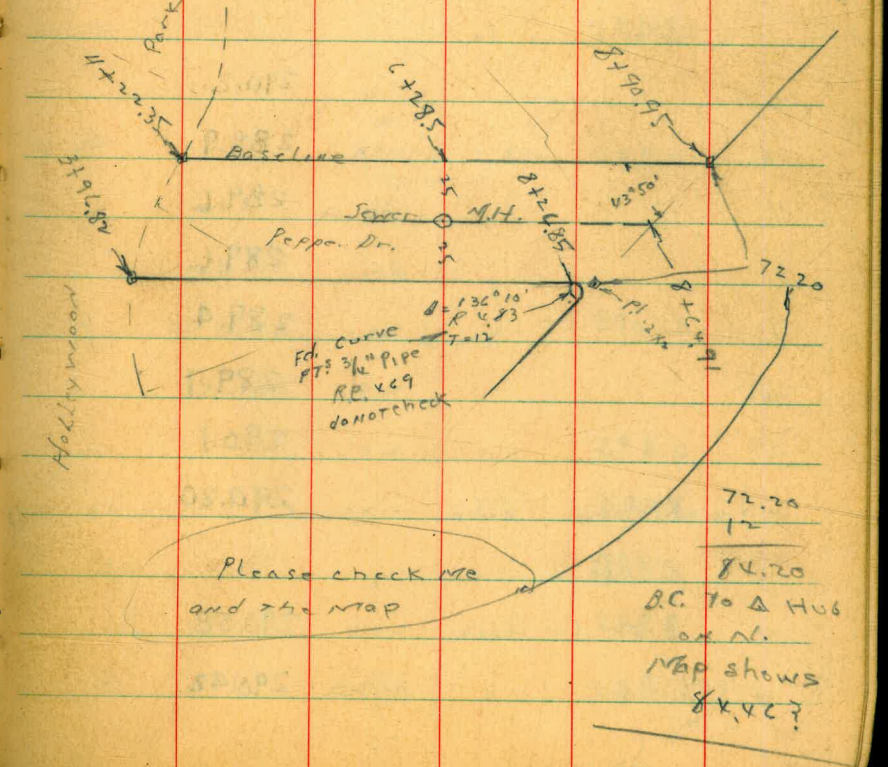
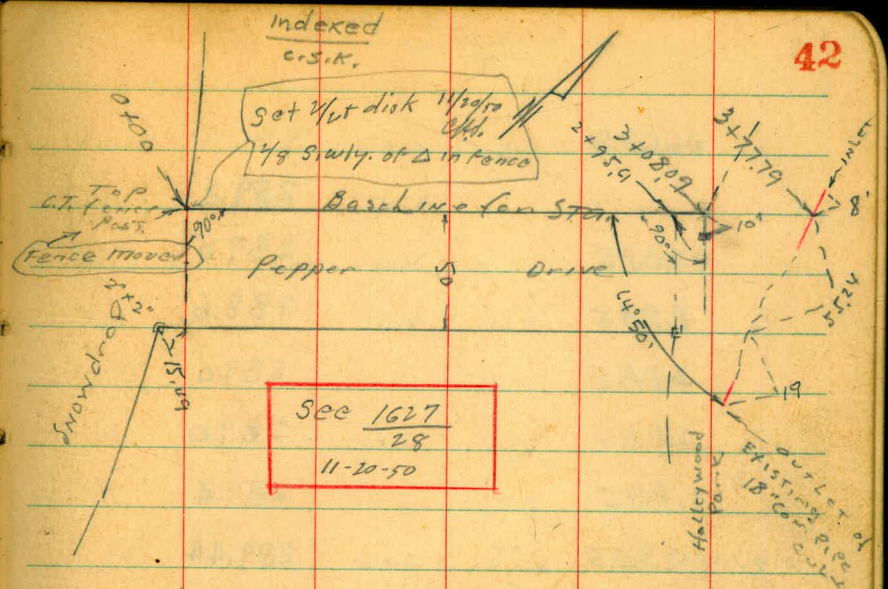
N		4.4	288.2
C6		4.5	288.1
1 1/4		4.8	287.8
C		4.9	287.7
1 1/4		5.2	287.4
C6		4.9	287.7
S		4.6	288.0

0+26.6

N	E 2.5 Con walk	3.55	289.07
+ 8	" " "	3.62	289.00 = 8' IN ST

0+39

S	E 2.8 Con walk	3.52	289.10 on Line
---	----------------	------	----------------



Please check me
 and the map

72.20
 12
 84.20
 B.C. to Δ HUB
 on N.L.
 Map shows
 8x400?

292.62

	2 + 42.8		
S		3.4	289.2
cb		3.6	289.0
1/4		4.0	288.6
c		3.6	289.0
1/4		3.6	289.0
cb		3.2	289.4
+ 9.1	8' wide	con. drive	3.18 289.44
	1 + 0.2		
N		2.4	290.2
cb		2.7	289.9
1/4		3.0	289.6
c		3.0	289.6
1/4		3.2	289.4
cb		2.9	289.7
S		2.5	290.1
+ 0.4	7' wide	con. drive	2.42 290.20
	1 + 10.3		
N	E 3.3	con. walk	2.04 290.58
+ 8.5	"	"	2.20 290.42

1/4 IN ST.

292.62

Peppin

43

	1 + 13.4		
S	0.2	E 2.9	con. walk 2.46 290.16
	1 + 40.7		
S		E 2'	con. walk 2.38 290.24
cb			2.7 289.9
1/4			3.2 289.4
c			3.0 289.6
1/4			2.9 289.7
cb			2.6 290.0
N			2.4 290.2
T.P.	1.74	291.64	2.72 289.90
	1 + 5.6		
S		E 3'	con. walk 1.51 290.13
	1 + 8.5		
N			1.6 290.0
cb			2.0 289.6
+ 2			2.8 288.8
1/4			2.8 288.8
c			2.7 288.9

29164
2

S	1/4	2.8	288.8
+3		3.2	288.4
cb		2.4	289.2
S		2.3	289.3
	2+28		
S		3.8	287.8
cb		3.9	287.7
+3		4.0	287.6
+4		5.5	286.1
1/4		5.3	286.3
c		4.8	286.8
1/4		5.3	286.3
+5		5.8	285.8
+6		4.1	287.2
cb		3.7	287.9
N		3.1	288.5
	2+50		
N		4.7	286.9
cb		5.1	286.5
+4		5.4	286.2

29164
1

44

cb	+4	7.3	284.3
1/4		7.0	284.6
c		6.7	284.9
1/4		7.0	284.6
cb		6.2	285.4
+5		5.6	286.0
S	¢ 93 gravel per	5.4	286.2
	2+75		
S		7.0	284.6
cb		7.2	284.4
+2		7.5	284.1
+4		9.2	282.4
1/4		9.1	282.5
c		8.9	282.7
1/4		9.0	282.6
+3		9.1	282.5
+5		7.0	284.6
cb		7.0	284.6
N		6.6	285.0
	2+95.1		
N		7.6	284.0

With 6" Con. Tile Ret. wall on each side approx. 1' High

	291.64		
cb		8.0	283.6
+2		8.5	283.1
+4		11.3	280.3
1/4		11.3	280.3
c		11.0	280.6
1/4		11.4	280.2
+3		11.4	280.2
+5		9.2	282.4
cb		9.1	282.5
S on Hub		9.77	281.87
	3+00		
S-5		10.7	280.9
S		10.5	281.1
cb		10.0	281.6
+3		10.1	281.5
+4		12.4	279.2
1/4		11.7	279.9
c		11.4	280.2
1/4		11.7	279.9
+4		11.7	279.9
cb		11.8	279.8

	291.64			45
1/4		10.2	281.4	
+5		9.8	281.8	
	3+08.09			
-5		10.0	281.6	
1/4		10.3	281.3	
cb on Hub		11.73	279.91	
+1		11.9	279.7	
+2		12.7	278.9	
1/4		12.5	279.1	
c		12.2	279.4	
1/4		12.5	279.1	
+4		13.1	278.5	
cb		12.2	279.4	
S		13.9	277.7	
+5		14.1	277.5	
T.P.	2/3	282.04	11.73	279.91
				T.P. on 0.60vc Hub on cb line 3+08.09
	3+38			
-18		15.3	266.7	
5		13.0	269.0	

28204

S c6	7.0	275.0
+ u	4.8	277.2
1/4	4.7	277.3
c	4.6	277.4
1/4	4.5	277.5
c6	4.5	277.5
N	4.2	277.8
+10	3.2	278.8
3+50		
-15	5.0	276.4
-4	8.4	273.6
N	8.2	273.8
+ c	7.4	274.6
c6	5.0	276.4
+2	4.7	277.3
1/4	4.7	277.3
c	4.7	277.3
1/4	4.8	277.2
+5	4.8	277.2
c6	6.8	275.2
S	12.5	269.5

28204

46

S + c	15.8	266.2
+19	20.2	261.8
+30	21.5	260.5
3+77.79 on N.L. ST, Levels on line of Ex. 18' Con. Pipe Culv.		
30' N of N.L. = 10500	12.6	269.4
0+22 F.L. INLET	14.05	267.99
0+23 S Ground	12.5	269.5
0+30 = N.L. "	12.0	270.0
0+44 S ST "	4.8	277.2
0+71 S ST "	5.0	277.0
0+85.24 = S.L. "	12.5	269.5
0+90 S ST "	15.2	266.8
1+04.24 F.L. 18" Pipe	20.9	261.1
1+08 S Ground	20.5	261.5
1+14 S ST "	19.1	262.9
This is only single strength pipe, No Reinforcing Steel also one on More angles under fill, can't see daylight, might have already failed. Do not recommend this.		

28204

	3+68		
S-20		10.6	271.4
S		12.2	269.8
+5		11.4	270.6
cb		7.1	274.9
+4		4.7	277.3
1/4		4.8	277.2
c		4.7	277.3
1/4		4.7	277.3
+5		4.7	277.3
cb		5.5	276.5
+9		11.2	270.8
N		11.2	270.8
+2		11.2	270.8
+8		10.7	271.3
+13		11.1	270.9
+20		9.3	272.7
	3+96.82		
N-25		12.5	269.5
N-5		11.6	270.4

28204

47

N		10.4	271.6
+8		9.3	272.7
cb		7.1	274.9
+6		3.0	278.4
1/4		3.0	278.4
c		3.5	278.5
1/4		3.2	278.6
cb		3.1	278.9
S		2.1	279.9
+10		1.4	280.6
T.P.	20.97	292.99	0.02
	4+22.35		
-10		14.0	279.0
N		13.0	280.0
cb		11.8	281.2
+3		12.0	281.0
+5		13.4	279.6
1/4		12.9	280.1

292.99

c	12.8	280.2
1/4	13.1	279.9
+3	13.3	279.7
+5	10.8	282.2
cb	10.5	282.5
S	10.3	282.7
u+50		
S	8.9	284.1
cb	9.3	283.7
+2	9.7	283.3
+5	11.5	281.5
1/4	11.4	281.6
c	11.1	281.9
1/4	11.5	281.5
+3	11.8	281.2
+5	9.8	283.2
cb	9.3	283.7
N	9.0	284.0

292.99

48

5+00

N	6.8	286.2
cb	7.0	286.0
+4	7.2	285.8
1/4	8.1	284.9
c	7.8	285.2
1/4	7.9	285.1
+3	8.0	285.0
cb	7.3	285.7
S	7.1	285.9

5+11.2

N + 0.3 E do. con. ribbon Dr. 5.79 287.20

Ribbons
= 1.7 wide
and c.7
overall
and level

5+35

S E 3' con. walk	5.45	287.54
cb	6.0	287.0
1/4	5.9	287.1
c	5.7	287.3
1/4	5.9	287.1
cb	5.1	287.9
N	4.9	288.1

	S+55				
	S+0.7	do. rib. con. drive	4.82	288.17	0.7 IN ST, ribbons 2' wide and 6.7 overall and level
	S+63				
	N+0.3	do 4' con. walk	3.98	289.01	0.3 IN ST.
	S+76				
	N		4.0	289.0	
	cb		4.2	288.8	
	1/4		4.4	288.6	
	C		4.3	288.7	
	1/4		4.7	288.3	
	S cb		4.4	288.6	
	+95	do. con. rib. dn	3.96	289.03	2' ribbons 7' overall
	S+82				
	N+0.5	do. rib. con. do	3.88	289.11	2' ribbons 6.7 overall 0.5 IN ST.
	S+95				
	S+0.3	do 3' con. walk	3.58	289.41	0.3 IN ST.
	L+00				
	S		3.6	289.4	
	cb		3.7	289.3	
	1/4		4.0	289.0	

	C		3.7	289.3	
	1/4		4.1	288.9	
	cb		3.9	289.1	
	N		3.8	289.2	
	L+12				
	N+15	do 3' con. walk	3.38	289.61	1.5 IN ST.
	L+19				
	S	do 2' con. rib. dn	3.33	289.66	7' overall
	L+22.5				
	E ST.	= M.H. RINT	2.64	290.35	
	"	= F.L. M.H.	10.19	282.80	
	L+38.1				
	N+0.2	do 2.5 con. walk	2.72	290.27	0.2 IN ST.
	L+41				
	S+0.3	do 4' con. walk	3.49	289.50	
	L+50				
	N		2.6	290.4	
	cb		2.4	290.6	
	+5		3.3	289.7	
	1/4		3.2	289.8	

292.99

c		2.7	290.3	
1/4		3.0	290.0	
cb		3.1	289.9	
S		3.4	289.6	
	6+59			
N.L.	E do. ^{2' wide} corr. rib.	2.40	290.59	7' small
	7+00			
S		2.0	291.0	
cb		1.8	291.2	
1/4		1.8	291.2	
c		1.7	291.3	
1/4		2.2	290.8	
+2		2.4	290.6	
cb		1.5	291.5	
N		1.5	291.5	

T.P. 8.00 297.81 3.18 289.81 ON CENTER
PIPE COR.
OR S.L.
C+L+I

7+22.5

N-0.1 $\frac{1}{2}$ 3' Cor. walk 6.17 291.64
o.1 back of ST. LINE

~~297.91~~
.81

			7+41.5	
N-0.1	$\frac{1}{2}$ 6.5 Cor. Dr.	6.10	291.71	
			7+50	
N		6.1	291.7	
cb		5.9	291.9	
1/4		6.1	291.7	
c		5.7	292.1	
1/4		5.8	292.0	
cb		5.7	292.1	
S		5.8	292.0	
			291+00	
S		4.5	293.3	
cb		4.3	293.5	
+1		4.3	293.5	
+2		5.0	292.8	
1/4		4.9	292.9	
c		4.8	293.0	
1/4		5.2	292.6	
+3		5.3	292.5	
+4		4.8	293.0	

~~297.91~~

.81

N cb	v. 6	293.2
N	v. 7	293.1
8 + 26.85 = B.C. on 5 th		
N	v. 0	293.8
cb	v. 0	293.8
+5	v. 8	293.0
1/4	v. 5	293.3
c	v. 11	293.7
1/4	v. 1	293.7
+6	v. 2	293.6
cb	3. 8	294.0
S	3. 9	293.9
8 + 38.85 = wly line of Columbine		
S = P. 1.	v. 0	293.8
cb	3. 9	293.9
1/4	3. 7	294.1
c	3. 8	294.0
1/4	v. x	293.4
+3	v. 6	293.2
cb	3. 5	294.3

~~297.91~~

297.81 ✓

51

N	3. 8	294.0
8 + 6.4, 91		
N	3. 3	294.5
cb	3. 4	294.4
+5	v. 0	293.8
1/4	3. 9	293.9
c	3. 5	294.3
8 + 71		
N to E do. 1.8 Com. ribbons 3.27 ^{Drive} 294.54 ^{C.5 overall}		
8 + 90.95 wly Columbine		
Sec on diag.		
N	3. 2	294.6
cb	3. 2	294.6
1/4	3. 5	294.3
c	3. 5	294.3
1/4	3. 2	294.6
cb	3. 4	294.4
S	v. 0	293.8
Set BM. RR spike in RR		
wly con of Peppon		
and Columbine		
2.41	295.40 ✓	

x sec of Columbine St = 10' Curbs
 7.5' 1/4" 50' wide
 Poplar St. Sly to Fairmount

B.M. R.P. spike

N.W. P.P. 5.22 300.87

Poppen

295.40 Columbine

0+00 Sly of Poplar St.

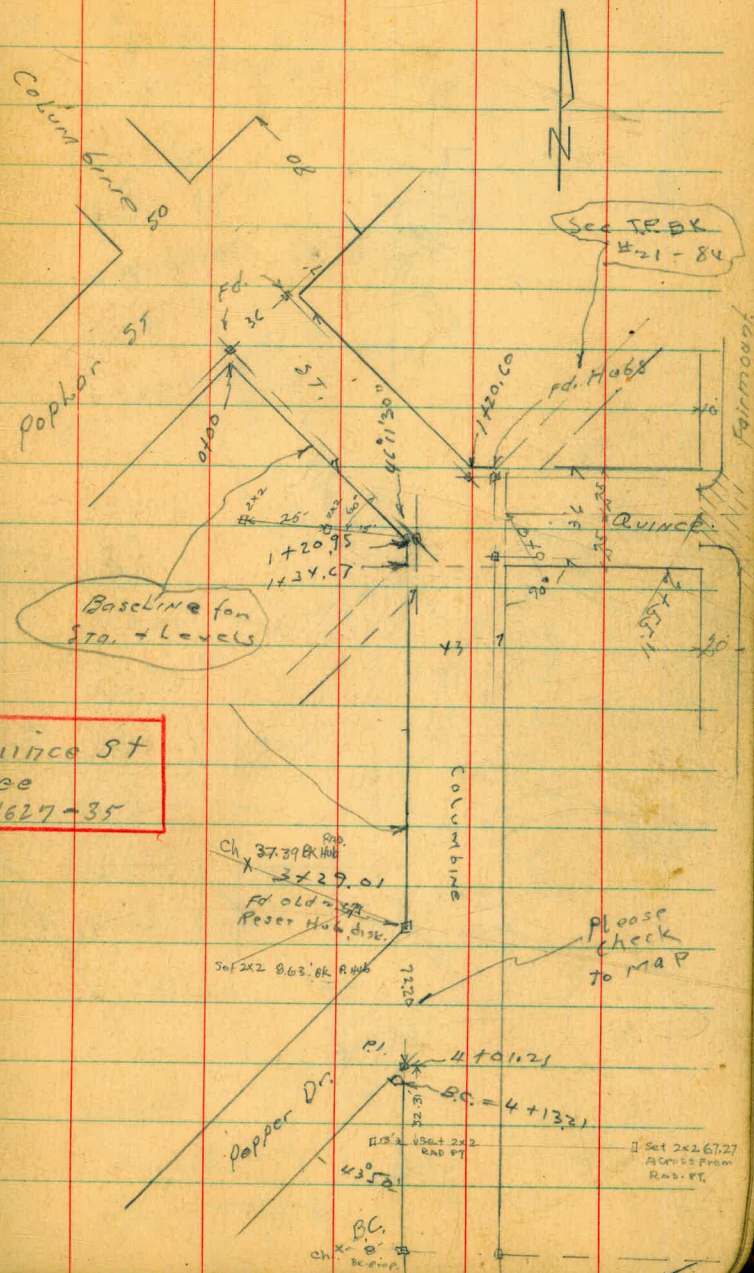
W	4.6	296.2
cb	4.6	296.2
+2	4.7	296.1
+4	4.9	294.4
1/4	4.9	294.4
c	4.0	294.8
1/4	5.9	294.9
+6	5.8	295.0
cb	4.6	296.2
E	4.2	296.6
0+50		
E	4.5	296.3
cb	4.5	296.3
+1	5.2	295.6
1/4	5.3	295.5

P. 54

indexed
 c.s.R.

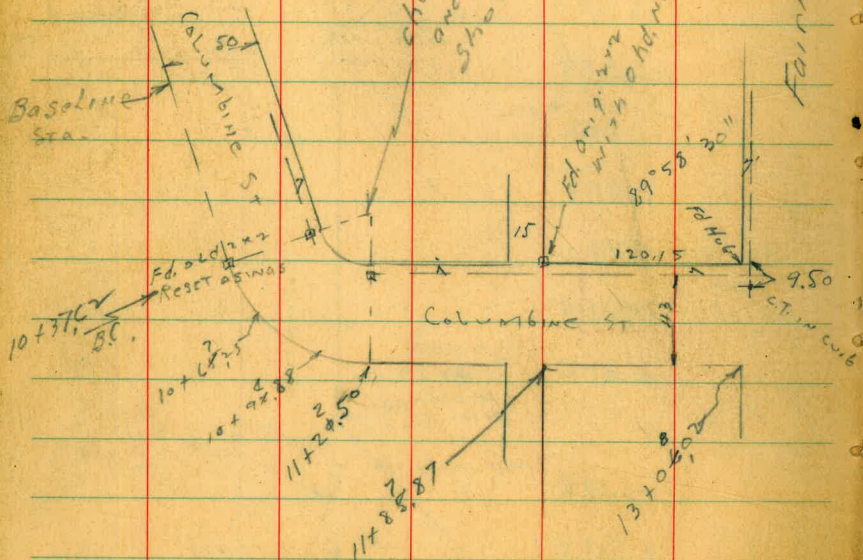
52

Ø = 2"x2" Hubs



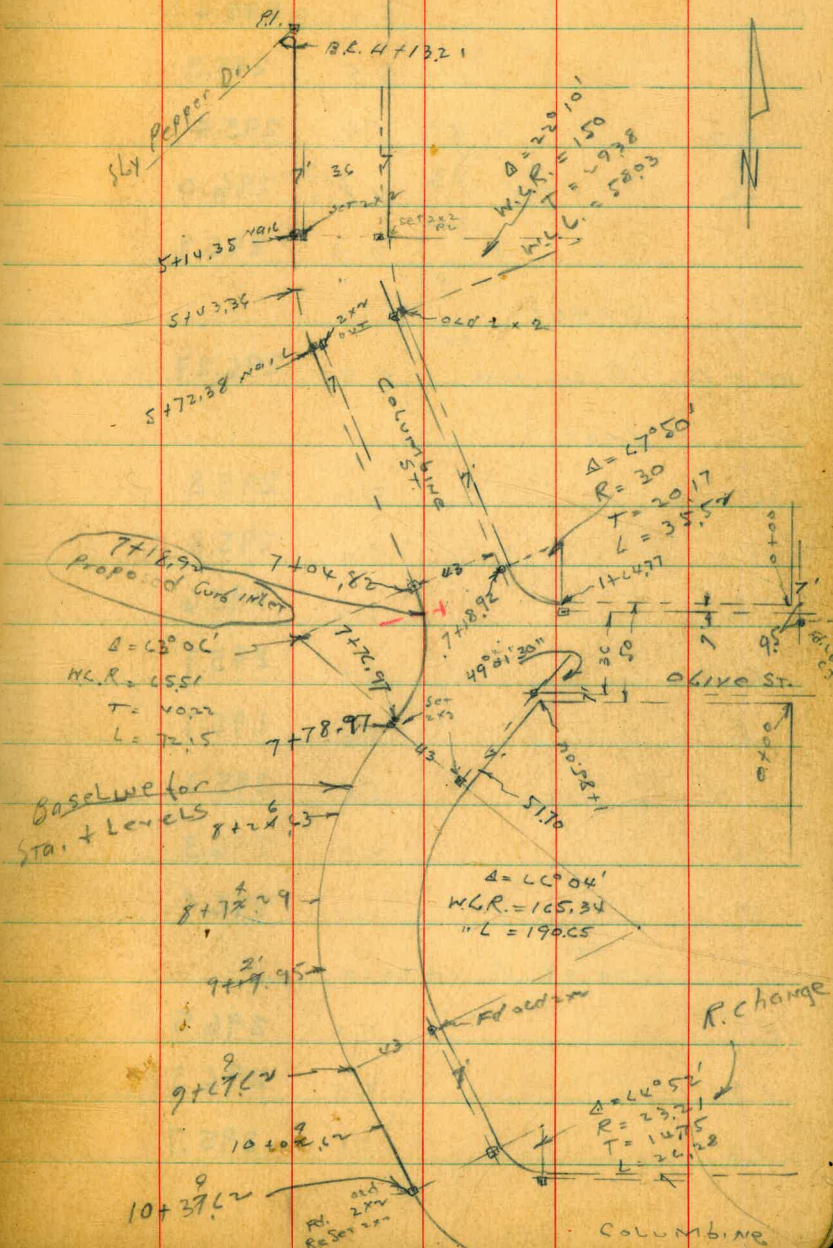
Columbine ST

Baseline
Sta.



changed R. to conform to old Hub at 11.57
and also to check T.P. BK #51 - 86

Ed. orig. 2m
with 0.1m nail O.K.



Baseline for
Sta. + Levels

R. change

COLUMBINE

300.82

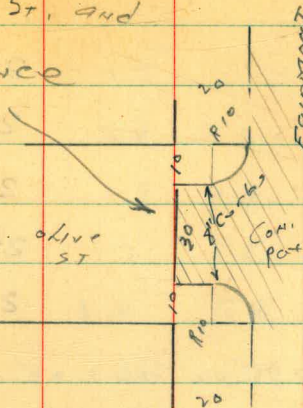
COLUMBINE

C		5.2	295.4
1/4		5.5	295.3
+2		5.2	295.4
c6		4.8	296.0
w		4.9	295.9
0+500			
W-12	E 214.900,	4.55	296.27
1+00			
x1		5.0	295.8
c6		5.0	295.8
1/4		5.2	295.6
C		5.1	295.7
1/4		5.1	295.7
+5		5.1	295.7
c6		4.5	296.3
E		4.4	296.4
Sec. 1+20.95 to 1+20.50			
E		4.3	296.5
+9		4.5	296.3
c6		5.1	295.7

Returns on FAIRMONT
at OLIVE ST. and

54

at QUINCE



1/4	5.1	295.7
c	4.8	296.0
1/4	5.1	295.7
cb	5.1	295.7
W = angle p7.	4.8	296.0
1 + 20.95 on SPLIT of Δ		
w	4.8	296.0
cb	5.1	295.7
1/4	5.1	295.7
c	4.7	296.1
1/4	4.7	296.1
cb	4.8	296.0
E+ = 50' front angle	4.9	295.9
1 + 34.67 = opp. SL. close to E		
E	4.9	295.9
cb	5.3	295.5
1/4	5.3	295.5
c	5.4	295.4
1/4	5.5	295.3
cb	5.0	295.8
W	5.2	295.6

1 + 50.5		
w	5.0	295.8
cb	4.9	295.9
tc	5.8	295.0
1/4	5.8	295.0
c	5.7	295.1
1/4	5.6	295.2
cb	5.5	295.3
E	5.2	295.6
+1 E 30' cor walk	4.96	295.86
2 + 00		
E E 30' cor walk	4.97	295.85
E	5.3	295.5
cb	5.6	295.2
1/4	5.8	295.0
c	5.9	294.9
1/4	6.1	294.7
cb	6.0	294.8
W	6.0	294.8
APS		

300.82

2 + 34.7

E - 02 E 3' Con. wall 5.55 295.27

2 + 50

W 6.5 294.3

cb 6.3 294.5

1/4 6.4 294.4

C 6.3 294.5

1/4 6.1 294.7

cb 5.9 294.9

E 5.7 295.1

3 + 00

E 5.7 295.1

cb 5.7 295.1

1/4 6.1 294.7

C 6.3 294.5

1/4 6.6 294.2

cb 6.2 294.6

W 6.4 294.4

3 + 29.01 = dry Pepper

3 c.!

W 6.1 294.7

300.82

56

W cb 6.1 294.7

+ 3 6.7 294.1

1/4 6.5 294.3

C 6.1 294.7

1/4 6.1 294.7

cb 5.9 294.9

E 5.5 295.3

T.P. ^{ON} ^{RR} spike 2.42 297.82 5.42 295.40 ✓ ✓
nw Pepper
Columbine

3 + 65.11

E 2.6 295.2

cb 2.8 295.0

+ 4 3.3 294.5

1/4 3.3 294.5

C 3.1 294.7

1/4 3.0 294.8

cb 3.1 294.7

W 3.5 294.3

297.82

4+01,21

W	4.0	293.8
cb	4.0	293.8
1/4	3.7	294.1
C	3.5	294.3
1/4	3.8	294.0
+4	3.8	294.0
cb	3.3	294.5
E	3.1	294.7

4+13,21

E	3.3	294.5
cb	3.5	294.3
+4	4.1	293.7
1/4	4.0	293.8
C	3.8	294.0
1/4	4.1	293.7
+5	4.4	293.4
+6	3.8	294.0
cb	3.8	294.0
W	3.8	294.0

297.82

4+27,7

W	4.0	293.8
cb	4.0	293.8
+2	4.0	293.8
+3	5.0	292.8
1/4	4.8	293.0
C	4.4	293.4
1/4	4.6	293.2
+3	4.6	293.2
cb	4.1	293.7
E	4.1	293.7
E	3.2	294.2
296.0		
E	4.7	293.1
cb	4.8	293.0
+5	5.4	292.4
1/4	5.3	292.5
C	5.0	292.8
1/4	5.3	292.5
+5		

57

297.82

c6	5.2	292.6
w	5.3	292.5
5+14.35 B.C.		
w	6.0	291.8
c6	5.8	292.0
+1	5.8	292.0
+2	7.1	290.7
1/4	6.9	290.9
c	6.6	291.2
1/4	7.1	290.7
+2	7.2	290.6
+5	5.1	292.7
c6	5.1	292.7
E	5.2	292.6
CTR. of Curve		
E	5.9	291.9
c6	5.8	292.0
+1	5.8	292.0
+6	8.1	289.7
1/4	8.1	289.7

297.82

58

c	8.0	289.8	
1/4	8.1	289.7	
+4	8.1	289.7	
c6	7.3	290.5	
w	6+48.35	6.5	291.3
5+72.38 F.C.			
w	7.7	290.1	
c6	8.7	289.1	
+5	9.2	288.6	
1/4	9.2	288.6	
c	9.1	288.7	
1/4	9.3	288.5	
+2	9.0	288.8	
+5	6.6	291.2	
c6	6.6	291.2	
E	7.1	290.7	
6+0.0			
-10	10.9	286.9	
E	10.9	286.9	
c6	10.6	287.2	

297.82

E 1/4	10.7	287.1
C	10.5	287.3
1/4	10.7	287.1
cb	9.8	288.0
W	9.3	288.5
C + 30		
W	11.0	286.8
cb	11.6	286.2
+ 5	12.3	285.5
1/4	12.3	285.5
C	12.2	285.6
1/4	12.3	285.5
cb	12.9	284.9
E	13.3	284.5
+ 15	13.1	284.7
+ 30	11.2	286.6
- 15	11.0	286.8
E	12.9	284.9
cb	12.8	285.0
1/4	12.9	284.9

This Prop. could
be filled at
slight cost,
if fall on E,
6 + 50

297.82

59

C	12.9	284.9
1/4	13.0	284.8
cb	13.0	284.8
W	12.6	285.2
T.P.	5.7x	290.6x
	12.92	282.90
C + 74		
W - 15	7.7	282.9
W	8.0	282.0
cb	8.9	283.7
+ 4	5.9	284.7
1/4	5.9	284.7
C	5.7	284.9
1/4	5.8	285.2
cb	4.4	286.2
E	2.9	287.7
C + 80		
E	2.5	288.1
cb	4.0	286.0

290.64

E 1/4	5.4	285.2
C	5.7	284.9
1/4	5.8	284.8
+2	5.7	284.9
c6	7.0	283.6
W	11.6	279.0
+10	13.6	277.0
+20	12.3	278.3
S+95		
-25	18.2	272.4
-13	17.8	272.8
W	11.7	278.9
c6	8.1	282.5
+5	5.7	284.9
1/4	5.7	284.9
c	5.4	285.2
1/4	5.2	285.4
+6	3.4	287.2
c6	3.3	287.3
E	2.4	288.2

290.64

60

7.7048V B.C. on W.L.

E	2.2	288.4
c6	3.1	287.5
+4	5.0	285.6
1/4	5.0	285.6
C	5.2	285.4
1/4	5.5	285.1
+2	5.5	285.1
c6	8.0	282.6
W	12.4	278.2
+16	20.2	270.4
+24	20.9	269.7
+35	17.8	272.8
7+18.92 = 8.5 on E.L. Columbus		
-38	21.0	269.6
-23	20.8	269.8
W	11.2	279.4
+7	9.4	281.2
c6	8.2	282.4
1/4	5.2	285.4

290.64

C		4.9	285.7
E 1/4		4.9	285.7
+3		4.8	285.8
cb		2.3	288.3
E		1.8	288.8
	7+28.87		
E	50' Sec.	3.3	287.3
cb		3.5	287.1
1/4		4.0	286.6
C		4.6	286.0
1/4		5.1	285.5
+4		5.2	285.4
cb		7.2	283.4
W		10.2	280.4
+25	Wash	20.8	269.8
+37	"	21.1	269.5
	Sec. = 7+52.92 to A PT. on S.E. 1/4 Cor ^{OLIVE and} Columbine		
-20		16.1	274.5
W		9.2	281.4
cb		5.8	284.8

290.64

1/4		5.6	285.0
C		5.0	285.6
1/4		4.8	285.8
cb		4.5	286.1
E	= 50' front W.L.	3.3	287.3
+7.5	to A on Prop. Line	2.8	287.8
	7+76.97 = E.C. on W.L.		
E		4.6	286.0
cb		5.6	285.0
1/4		6.0	284.6
C		6.0	284.6
1/4		6.4	284.2
+5		6.6	284.0
cb		7.5	283.1
W		9.5	281.1
+15		13.0	277.6
	7+78.97 = B.C.T. Sec. same as above		
	8+24.63		
W-15		13.2	277.4
W-7		10.6	280.0
W		9.1	281.5

290.62

w cb	7.5	283.1
+3	7.0	283.6
1/4	6.9	283.7
c	6.5	284.1
1/4	6.7	283.9
cb	6.2	284.4
E	5.4	285.2

 $8 + 74.29$

E	5.3	285.3
cb	5.6	285.0
+5	6.6	284.0
1/4	6.7	283.9
c	6.5	284.1
1/4	6.7	283.9
cb	7.1	283.5
w	8.5	282.1
+15	10.0	280.6

 $9 + 179.95$

-15	17.8	272.8
w	11.4	279.2

290.64

Columbine 62

w cb	11.7	278.9
1/4	6.8	283.8
c	6.4	284.2
1/4	6.5	284.1
+5	6.6	284.0
cb	5.5	285.1
E	5.0	285.6

T.P. 5.93 $\frac{290.13}{2}$ c.xx 284.20 $9 + 277.62$ EC

E	4.4	285.7
cb	4.9	285.2
+4	6.1	284.0
1/4	6.0	284.1
c	5.8	284.3
1/4	6.7	284.0
+2	6.1	284.0
cb	7.0	283.1
w	9.3	280.8
+7	15.0	275.1
+15	18.4	271.7

same slope to +25

290.13

	⁴ 10 + 07.12		
- 20		14.7	275.4
- 10		10.1	280.0
w		7.9	282.2
cb		6.5	283.6
+3		5.8	284.3
1/4		5.6	284.5
C		5.3	284.8
1/4		5.5	284.6
+2		5.0	285.1
cb		4.5	285.6
F		3.9	286.2
	⁶ 10 + 24.5		
F	E 22 Con. walk	3.52	286.61
+12.7		4.08	286.05
	³⁹ 10 + 37.02 80 LT		12.7 in ST
F		3.9	286.2
cb		4.1	286.1
+4		4.5	285.6
1/4		5.2	284.7

290.13

63

C		5.1	285.0
1/4	285	5.3	284.8
cb	285	5.8	284.3
w		6.9	283.2
+10	285	8.6	281.5
	⁷ 10 + 11.25		
w	285	5.6	284.5
cb	285	5.4	284.7
1/4	285	5.0	285.1
C	285	4.9	285.2
1/4	285	5.1	285.0
+2	285	5.1	285.0
cb	285	4.2	285.9
F		3.8	286.3
	⁸ 10 + 97.88		
F		3.7	286.4
cb	285	3.9	286.2
+5	285	4.9	285.2
1/4	285	4.9	285.2
C	285	4.7	285.4

290.13

1/4		4.6	285.5
c6		4.7	285.4
W on s.l.		4.9	285.2
	11 + 2 ² 50		
S.L. now		5.1	285.0
S c6		4.8	285.3
1/4		4.9	285.2
C		4.8	285.3
1/4		4.8	285.3
+ 2		4.2	285.9
c6		4.1	286.0
N.L. now ground		3.8	286.3
" = Edge of 23	Comp. walk	3.52	286.61
	11 + 5 ²		
N		3.6	286.5
c6		4.1	286.0
1/4		4.8	285.3
C		4.8	285.3
1/4		5.1	285.0
c6		5.1	285.0
S.L.		5.5	284.6

290.13

64

	11 + 8 ² 87		
S		5.2	284.9
c6		5.2	284.9
1/4		5.1	285.0
c		4.9	285.2
1/4		4.7	285.4
c6		4.5	285.6
N		4.1	286.0
	12 + 0 ²		
N		3.9	286.2
c6		4.5	285.6
1/4		4.7	285.4
c		4.8	285.3
1/4		5.0	285.1
+ 3		5.2	284.9
c6		4.8	285.3
S		4.4	285.7
	12 + 5 ²		
S		3.5	286.6
c6		4.0	286.1

S ↓		v.4	285.7
C		v.1	286.0
1/4		v.1	286.0
+3		v.2	285.9
cb		3.3	286.8
N		2.9	287.2
13 + 0.02 = W L FAIRMONT			
N		1.1	289.0
N cb end top		1.44	288.69
gut Pay		2.10	288.03
1/4		2.27	287.86
C		2.39	287.74
1/4		2.73	287.40
gut		2.98	287.15
S cb end top		2.43	287.70
SL		2.5	287.6
13 + 2.02 = W C B Line FAIRMONT			
SL Top cb		2.33	287.80
"		2.88	287.25
cb	on pay.	2.71	287.42

1/4	Pay		2.53	287.60
C	"		2.32	287.79
1/4	"		2.19	287.94
cb	"		2.07	288.06
N L	gut		1.90	288.23
"	Top cb		1.33	288.80
Set BM. on 7x9.5 L. CT. RP.				
	on cur cb NW Cor. of		1.36	288.77
Columbine & FAIRMONT				
		5.88	294.15	288.77
T.P.		5.95	298.04	256
			263	295.41
				295.40
				901
				P.51
Set Cor. 3/4" Pipe				
TR		3.93	293.07	289.14
		8.16	296.05	5.18
TR		4.43	299.71	0.77
Check to spike				
			4.34	295.37
NW Cor. Poplar & Columbine				
				295.40
				0.03
				error

1 sec of Cherokee Lane

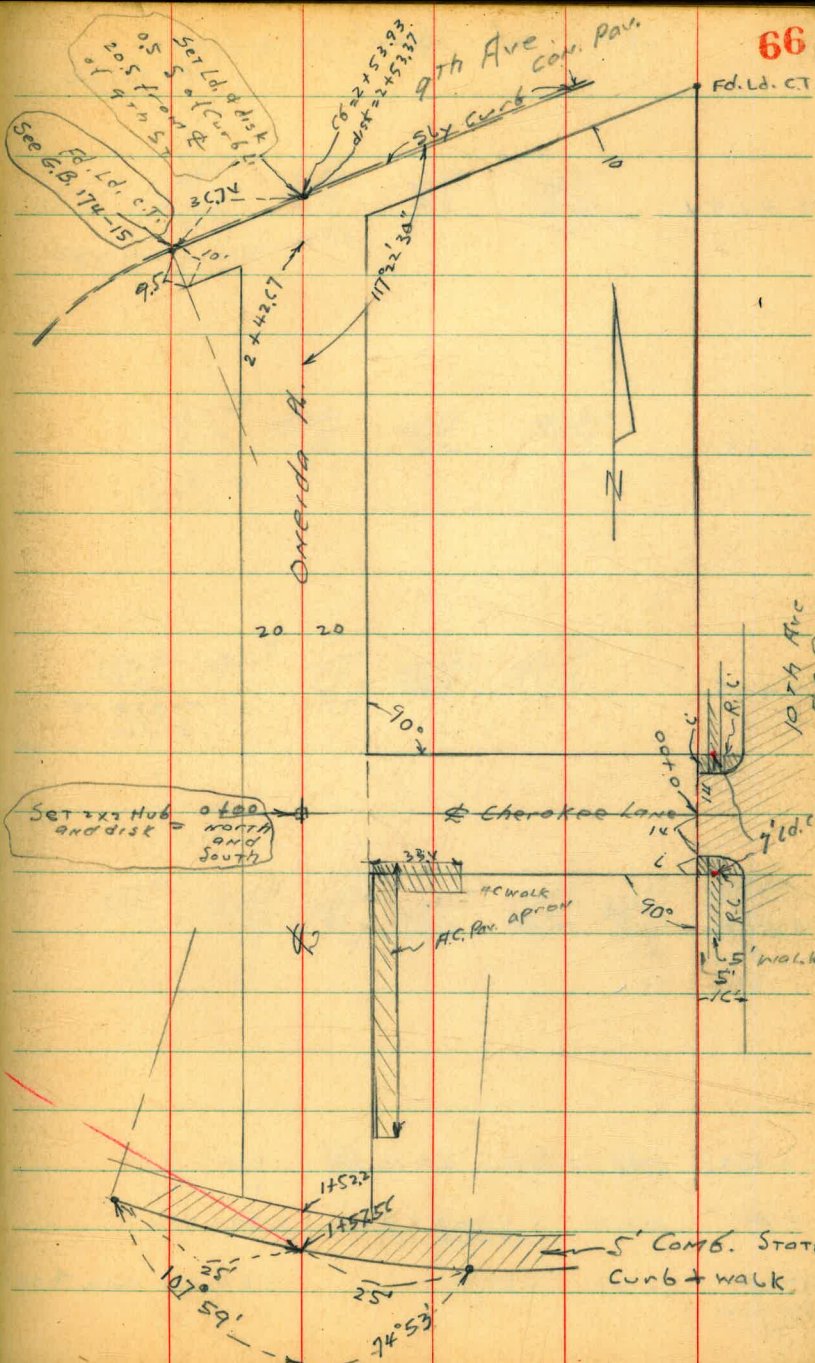
" " Overda Place

C. Moore
Surveyor
8099 4-22-46

See 1174-31

$\text{Curb} \rightarrow \Delta = 22^{\circ} 52'$
 $R = 500$
 $T =$
 $L =$
 $\text{Chords} = 25'$

set chisel
cross
of Overda Pl.
and Nly curb on
Robinson



X sec of Cherokee Lake
40' wide

0 + 6.54

0 + 35.5

0 + 15

N. edge of
E/W com.
walk

0 + 00 = W. b. 1074

0 - 10 = W. c. b. line of 1074

I.P. 3.49 285.57 3.27 282.08

BMBP 3.33 285.35 282.02 Univ. & 1074
SW con.

Lt = to So.

¢

Rt

67

	<u>281.85</u>	<u>281.05</u>	<u>281.8</u>	<u>282.0</u>	
End	3.74	3.71	3.8	3.6	
com. walk	21.2			20	
Beg. A.C. walk		+17.3			

	<u>282.28</u>	<u>282.1</u>	<u>282.4</u>	<u>282.7</u>	
	3.29	3.5	3.2	2.7	
com. walk	21.2	20		20	

	<u>282.51</u>	<u>282.4</u>	<u>P.P.</u>	<u>282.5</u>	<u>282.2</u>
	3.06	3.2		3.1	2.4
	21.2	20	15.5		20

<u>281.89</u>	<u>281.61</u>	<u>281.91</u>	<u>281.97</u>	<u>281.84</u>	<u>281.64</u>	<u>281.83</u>
3.08	3.96	3.06	3.60	2.73	3.93	3.74
14	14	7		7	14	14
06	97				97	06

309	414	<u>3.57</u>	3.43	<u>3.58</u>	4.10	<u>3.70</u>
14	14	7		7	14	14
06	97		<u>285.57</u>		97	06

Cherokee Lane

Lt = S.

⊕

R-

68

1+00 = F.L. Oneida Place

0+99

0+71 ⊕ Sing. 900 Con. floor

285.57

81.8
4.4
20

81.3
4.3

81.5
4.1
20

81.32

4.25

17.3

Con. A.C. Pav

P.P

10.4

282.01

3.56

Floor 23.5

Floor 23.5

81.81

3.76

17.3

A.C. Pav

285.57

1 sec Oneida Pl. 40' wide
Cherokee Lane nly to 9th St.

0+13

0+47 E 3.5 Con. Walk

0+70

0+75 E 3.7 Con Walk

0+00 = E Cherokee Lane ground

285.57

LT = to W.

~~1~~

Pt

69

80.4	80.6	81.5	81.52	81.97
5.2	5.6	4.1	4.05	3.60
20		20	20.2	26.3
			HP 20.2	E Sin.
				gan.
				CON.

80.43
M
19.2

80.5
5.6

81.0

81.5

80.71
4.86
18.4

80.4

80.9

81.3

5.2

4.7

4.3

20

ON

2 x 2 RW Hub

4.99

280.58 ✓

set B.M. E
Cherokee
+ Oneida

285.57

Oneida Pl.

1+76

1+72

1+54

1+35

1+22 = P.P. 19.5 RT

1+05

285.7

LT

E

RT

70

78.97

E 5 $\frac{6.60}{\text{Con. 19.4}}$
walk

78.9

$\frac{6.7}{20}$

79.1

6.5

80.32

5.25

17.8

Con. of can
edge

80.53

17.9

Con. of can

80.64

4.93

19.8

5. end of
3 can. gar
Con.

81.05

4.5

20

E Sin
gar.
Con.

79.41

79.3

80.2

E 4.5 $\frac{6.6}{\text{Con. 20.5}}$
walk

$\frac{6.3}{20}$

5.4

80.9

4.7

20

79.6

80.4

81.2

81.3

$\frac{6.0}{20}$

5.2

81.2

4.3

21.4

E Sin. gar.
dent.

285.57

Oncida PL.

2+13

T.P. 076 279.81 6.52 279.05

2+03

£

2+01

1+98

1+947

£ Sin. gar. con. fl.

285.57

LT. = to W.

£

R_T

71

72.9

$\frac{6.9}{30}$

73.2

$\frac{6.6}{20}$

77.9

1.9

$\frac{1.1}{20}$ 78.7

279.81

$\frac{7.7}{20}$ 77.9

£ 78.7

79.47

$\frac{6.10}{19.4} = \text{ground and } \frac{1.7}{1.7} \text{ Con Walk}$

78.5

$\frac{7.1}{20}$

78.7

£ 79

80.17

$\frac{5.40}{18.3}$

$\frac{5.27}{19.9} = \text{N. end Con. apron}$

$\frac{5.27}{19.9} = \text{N. end 3 car. gar. Con.}$

80.30

$\frac{5.27}{19.9} \text{ gar. floor}$

78.73

$\frac{6.84}{19.4}$

285.57

Oneida PL.

check to Orig. BM, 0.90 282.01 282.92
0.01

T.P. 12.01 282.91 0.08 270.30

2 + 53.93 = gutter

2 + 53.93 = 5ly Top
Cut on 974

2 + 42.67 on diag. = 5ly gutter

2 + 42.67 Sec. 97 90° 1/2 RT

T.P. 2.59 270.38 12.02 267.79

2 + 22

279.81

LT = W

69.15
10.16
22.52

69.69
10.14
22.52

70.5
9.3
22.52

69.5
10.3
30

12.1
35
Top edge
Cut on 974

R

71.99
8.32

71.96
7.85
Top
edge

73.4
6.4

73.4
6.4

270.38
72.5
73

279.81

R

73.69
6.12
22.52

74.20
5.61
22.52

73.9

5.9
22.52

75.4
4.4
20

73.7
6.1
20

79.4

0.4
21

77.2
5.6
30

72

X sec Oneida Pl. 40' wide
 Cherokee Sky to Robinson

0+51

0+40

0+29

0+23.5 13.5 Rt to Guy Pole

0+20

0+14 E do. Con. Fib. drive 2' wide

0+00 = E of Cherokee Lane

BM. HVL 372 284.30 280.58
 E Cherokee
 + Oneida
 P.C. 9

LT = to E

E

Rt = % W. 73

281.35
 295
 272
 E 90' Con. f

280.86
 292
 21
 apron

281.68
 292
 272
 E 90' Con. f

281.07
 293
 21
 apron

281.68
 292
 272
 E 90' Con. f

281.18
 292
 21
 R.C. apron

281.36
 304
 21
 R.C.P.
 apron

281.1
 312
 20
 31
 20

280.6
 3.7
 20

280.8
 3.51
 17.7

284.30

Owida PL

1+21

1+16

1+07

0+91.5

0+80 = E 7 wide Corri drive

0+62.5

284.30

LT = E

€

R = W 74

5.1
2.7

= Top of Bot.
Con. step to
Porch

	79.84	
	<u>4.40</u>	4.94
	26.4	21
E	gar	apron
	Con.	

	80.50	79.74	
	<u>3.80</u>	4.56	
	26.4	21	5.1
E	gar	apron	79.2
	Con		

	80.50	79.92	
	<u>3.80</u>	4.38	
	26.4	21	
E	gar	apron	
	Con		

	80.50	80.25	
	<u>3.80</u>	4.05	
	26.4	21	4.52
E	gar	apron	20.3
	Con		

	81.35	80.64		
	<u>2.95</u>	3.66	4.2	
	27.2	21		4.5
E	gar	apron		20
	Con.		284.30	

Oncida PL

check to 222 HUB 496 280.60 280.58
Q Charobee
Oncida

T.P. 9.44 284.66 5.95 275.22

1+57.56 = 14 gutter Con. Pav. (state

1+57.56 = on top curb

1+52.2 diag. on N. edge Con. walk

T.P. 6.82 281.17 9.95 274.35

1+46 194 LT. to Tel. Pole

1+37

1+26.5

284.30

Lt = to E

E

R

75

78.10

6.20
25

78.74

5.50
25

78.83

5.47
25

79.76

4.54
20

E 90 S.
CON

79.84

5.46
20

E 90 S.
CON.

79.2

5.1
20

79.19

5.13
21

E 90 W.
CON

79.36

4.94
21

E 90 W.
CON

281.17

77.3

78.6
20

77.3

5.7
20

284.30

76.82

7.48
25

77.45

6.85
25

77.48

6.82
25

75.94

8.30
25

76.55

7.25
25

76.61

7.09
25

74.8

9.5
20

74.9

7.4
20

Cross Section Olive St. Fairmount
to Columbine
Sketch Page 53

0+60

0+32

0+03

0+0 = W.L. Fairmount = W.L. Paying + Cbs
17' L of L = 8 1/2' Post or Pole

0-10

0-20 = W.C.B. Line Fairmount

BM 760 298.15

290.55

072 Stub
Olive Hill
W of Fairmount
1711-10

April 29-96

ht = 5

2

Rt. N

76

294.6	294.3	293.6	293.8	293.5	294.1	294.6	295.3
35 25	35 25	10 25	10 25	10 25	10 25	10 25	10 25
295.6	295.2	294.8	294.9	295.1	295.6		
35 25	35 25	11 25	11 25	10 25	10 25		
296.3	295.9	294.4	294.6	295.0	295.3	296.0	
18 25	18 25	17 25	15 25	12 25	13 25	12 25	
294.9	294.71	294.10	294.69	294.72	295.31	295.9	
22 25	31 15-Cb	10 15-Gut	24 25	24 15-Gut	28 15-Cb	22 25	
294.8	294.61	294.17	294.54	294.57	295.20	295.3	
23 25	25 15-Cb	39 15-Gut	11 25	25 15-Gut	19 15-Cb	23 25	
294.62	294.09	294.15	294.34	294.39	294.57	295.13	
25 25	10 15-Gut	10 25	38 25	27 15	32 25-Gut	10 25-Cb Top	

298.15

31-2-10
294.6
295.3

01 No St.

47-5

2

R1=11

77

1485.04 = Δ 07/11

1464.77 = BC. 05/11

+35 17 1/2 to 1/2 Sly Power Pole

1427.45 = 1/2 N.Y.S. Alley

1408

0472

29815

10.2	10.4	10.8	10.2	11.3	9.0	9.0
25	5	10	15	15	20	25
287.8	287.7	287.3	287.9	286.8	289.1	289.1
287.5	289.4	288.7	288.8	288.3	290.1	290.1
8.6	8.7	9.1	9.6	9.8	8.0	8.0
25	5	10	10	10	14	15
290.8	290.8	290.3	290.5	290.4	291.1	291.3
7.3	7.6	7.8	7.6	7.7	7.0	8.0
25	15	10	10	8	15	25
292.06	291.8	291.2	291.4	291.4	292.2	292.2
6.9	6.3	6.9	6.7	6.7	5.9	5.9
38	15	9	10	10	15	25

292.06
6.9
38
40-1/2 to 1/2 N.Y.S. Alley
Sly Power Pole
Con. Floor

292.2
6.9
38
40-1/2 to 1/2 N.Y.S. Alley
Sly Power Pole
Con. Floor

29815

Cross Section Quince St.
Columbine to Fairmount
Sketch Page 52

0+92

0+85

sec F.B 1627
35

0+73

0+62

0+24 17 ft of 2 = Sly Parrot Pole

0+0 = EL Columbine to South

BM 6.26 303.45

297.19
SF BP
Quince +
Fairmount

April 29-46
Sisson
Haddel
H/167

Lt. N

2

Rt. S

78

288.30

288.03

297.5

297.1

297.2

297.3

4.95

5.15

5.9

6.3

6.8

6.1

5.46
Sly
Graft
Foot

5.15 = 2.5 ft
Comp. H

6.10
2.97 = 2.4 ft
Comp. H

297.39

6.06
3.5 = 2.5 ft
Comp. H

297.0

297.0

296.5

296.4

296.62

296.53

296.5

296.7

296.0

296.3

296.2

6.9

6.7

7.4

7.1

7.2

296.7

296.3

295.9

295.7

295.8

6.7

7.7

7.5

7.7

7.6

303.45

1+52 18 ft of $\frac{1}{2}$ = 64 Power Polc

1+50

1+14

1+81

1+40

1+20

1+19 144 ft of $\frac{1}{2}$ = 114 Anchor Polc 17.8 ft of $\frac{1}{2}$ = 64 Power Polc

1+13

300.45

40 297.4
15

53 299.6
35

307 00.38
32.7 = 1st + 2nd
Cone Floor

41 299.3
32

40 299.4
15

340 300.05
25.5 = 1st + 2nd
Cone Floor

48 298.6
58

40 299.4
12

41 299.3
15

61 299.3
51

44 299.0
10

47 298.7
9

64 297.0
14

46 298.8
4

48 298.6
48

61 297.3
51

44 299.0
5

48 298.6
19

56 297.8
15

44 299.0
5

43 299.1
5

48 299.1
30

44 299.0
5

46 298.8
15

44 299.0
15

46 298.8
15

46 298.8
15

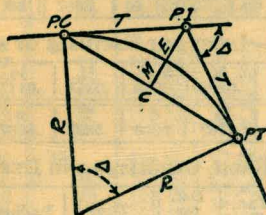
557 297.88
15 = 1st + 2nd
Cone Floor

577 297.73
15 = 1st + 2nd
Cone Floor

300.45

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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CURVE FORMULAS

Radius= $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve= D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)

Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)

Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2})$ (5) $= R \text{vers} \frac{\Delta}{2}$ (6)

External= $E = T \tan \frac{\Delta}{4}$ (7) $= R \div \cos \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)

Long Chord= $C = 2 R \sin \frac{\Delta}{2}$ (10) $\Delta = \text{Central Angle}$

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.—Sta. 161 +60.35 to find Sta. of P. C. and P. T. $\Delta=62^\circ 10'$ $D=8^\circ 20'$. From Table IV for 1° curve $T=3454.1$ and $\div 8\frac{1}{2}=414.49$ ft. From Table V correction=.36 or $T=414.85$ ft. P. C.=Sta. P.I.— $T=157 +45.50$. Also from (4) $L=746.00$ and P. T.=Sta. P. C. + $L=164 +91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset= $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle= $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft.= (in minutes) $.3 \times C \times D^\circ$ or =defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve= $.3 \times 54.5 \times 8\frac{1}{2} = 136.2'$ or $2^\circ 16.2'$, or= $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle= $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve $E=960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{2} = 91.27$ and from Table V correction=.10 or $E=91.37$ ft. Or suppose $\Delta=32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E=230.9$ and $\div 42 = 5.5$ or $D=5^\circ 30'$.

	297.11	297.04	296.91	296.78	296.66	297.15
2+7511.2 N.Cb. to South	6.34 25	6.41 15	6.54	6.67 15	6.79 25	6.30 25.06

	297.34	296.72	296.76	296.85	296.70	297.18	297.2
2+6511.2 N.Cb. to North	6.11 25.06	6.73 25	6.69 15	6.60	6.75 147.90	6.26 147.06	6.2 25

	297.8	297.41	296.90	296.87	296.65	297.22	297.4
2+5511.2 N.L. Fairmount + N.Y. Pav. + Cbs	5.6 15	6.04 15.06	6.55 15	6.58	6.80 147.90	6.23 147.06	6.0 15

308.75

4+70.58 = opp. N. Cor.
Hollywood Park

99.7
654
34.3

319

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING. 25

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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