

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.
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1699

CITY ENGINEER'S OFFICE

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

Alley Blk 3 Hartleys North Park 28-33

Water Linc Loma Alta #2 1-11

Cross Sec. Valcost. Comalcost. W Plumo 12-29

" " Alley Blk 3 Hartleys North Park 28-33

Prop. Sewer 43rd St. San Geronimo of Beta 34-36

X sec. alley Blk 50 Ocean Beach 37

" Albion Jennings } Sewer Prelim. Also 75+176.7

Silvergate - Dupont } " " 46 to 77

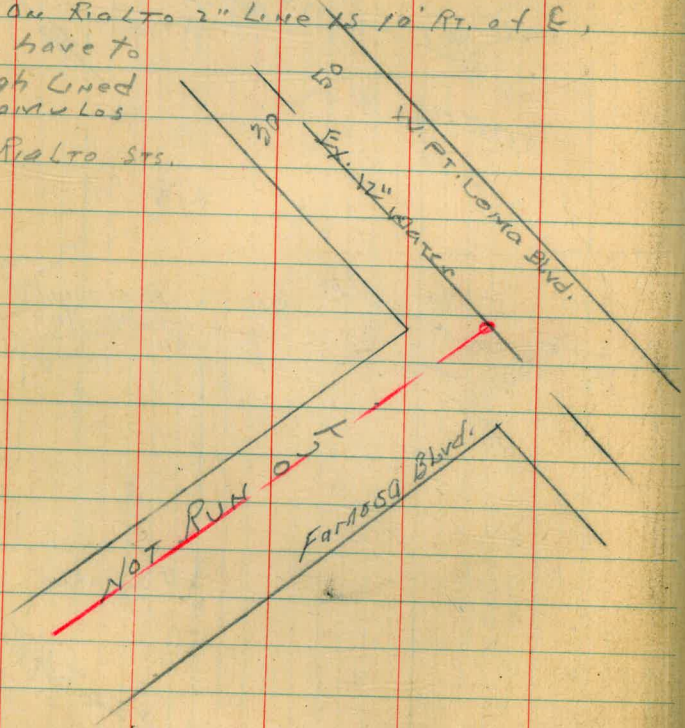
Catalina - } " " 68 to 74

Sta. 21+75.71 to Sta. 32+26

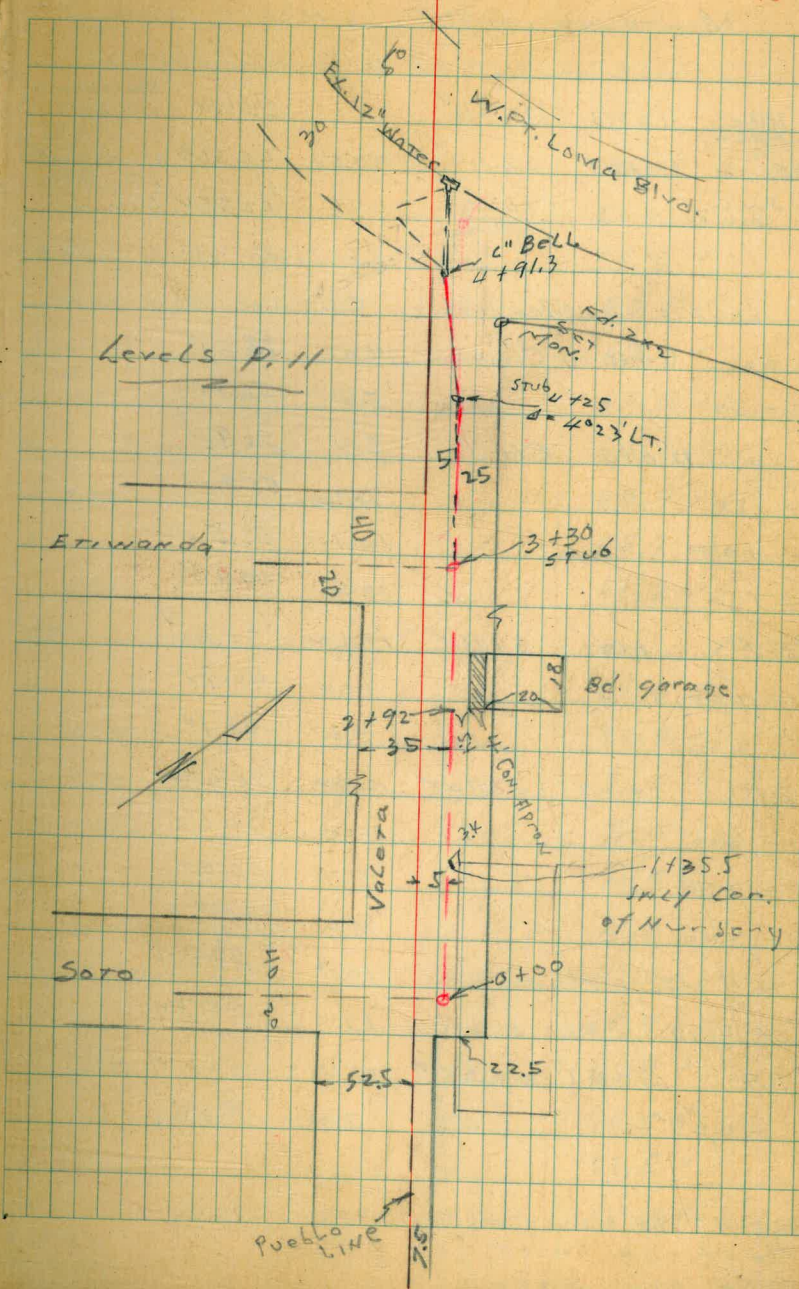
Catalina Blvd. So. of Warner }
tract. Also Arthur Subdivision } 78

Note,

Existing 2" water lines are on
the Sly sides of Mantulco,
Mentone & Temacula, & ~~Rialto~~ STS
on Camulos. Existing 2" water
line is on the Ely side of E St
on Rialto 2" line is 10' ft. of E,
will have to
be High lined
on Camulos
and Rialto sts.



2



Montalvo water levels

SE SPIKE P.P.	12.97	76.96 ✓		13.99	Montalvo Clovis
T.P.	2.68	68.99 ✓	10.65	66.31 ✓	
T.P. SW. Con SPIKE P.P.	0.08	62.63 ✓	6.44	62.55 ✓	Montalvo Clovis ✓

Levels on Montalvo, Camulos Ely

0 + 00	Cross on Camulos	4.0	58.6 ✓	
0 - 30		5.9	56.7 ✓	
"	12" Nly F.H.	5.7	56.9 ✓	
- 50		7.02	55.4 ✓	
- 100		10.1	52.5 ✓	
- 150		12.8	49.8 ✓	
T.P.	1.10	51.1 ✓	12.62	50.01 ✓
- 200			4.4	46.7 ✓
- 250			9.0	42.1 ✓
T.P.	0.47	38.70 ✓	12.88	38.23 ✓
- 300			2.0	36.7 ✓
- 350			5.7	33.0 ✓
- 400			9.4	29.3 ✓
- 420	= Plate		10.9	27.8 ✓
- 450	= Top Bluff		13.4	25.3 ✓
T.P.	0.57	24.65 ✓	12.62	26.08 ✓
- 465			7.0	19.6 ✓

SET T.P. to North
to check to on
Montalvo Levels

9.01 17.64 ✓

Water Levels on Montalvo

Camulos to W.P. Loma Blvd.

B.M. SW Spike P.P.	0.76	69.31 ✓		62.55	Montalvo + Camulos
0 + 00	X on Camulos	10.7	58.6 ✓		
+ 50		8.8	60.5 ✓		
1	IN THIS Block	7.2	62.1 ✓		
+ 50	LINE IS ON Nly edge of old PAVING	6.3	63.0 ✓		
2		5.6	63.7 ✓		
+ 50		4.4	64.9 ✓		
3		3.6	65.7 ✓		
+ 50		2.1	67.2 ✓		
T.P.	4.49	73.49 ✓	0.31	69.00 ✓	
4		3.9	69.6 ✓		
+ 25		3.0	70.5 ✓		
+ 50		2.5	71.0 ✓		
+ 75		2.5	71.0 ✓		
5		2.6	70.9 ✓		
+ 25		3.5	70.0 ✓		
+ 50		4.5	69.0 ✓		
6		7.0	65.9 ✓		
+ 30		9.0	63.9 ✓		
"	12" Nly F.H.	8.0	65.5 ✓		
C + 60.1	X on Clovis	11.0	62.5 ✓		
T.P.	0.41	64.40	9.50	63.99 ✓	63.99

SE SPIKE
Montalvo
CLOVIS

		CU. YD		
7			4.9	59.5 ✓
+50			9.7	54.7 ✓
T.P.	0.14	51.48 ✓	130.6	51.34 ✓
8			1.3	50.2 ✓
+50			4.5	47.0 ✓
9			6.0	45.5 ✓
+50			6.6	44.9 ✓
10			6.9	44.6 ✓
+50	Thru oil		7.2	44.3 ✓
11	pay. 7 hrs block		7.4	44.1 ✓
T.P.	3.42	47.51 ✓	7.39	44.09 ✓
+50			3.8	43.7 ✓
12			4.1	43.4 ✓
+50			4.5	43.0 ✓
13			5.0	42.5 ✓
+50			6.3	41.2 ✓
+75			7.4	40.1 ✓
14			9.0	38.5 ✓
+25			11.4	36.1 ✓
T.P.	0.17	34.87 ✓	12.81	34.70 ✓
14 + 50			1.3	33.6 ✓
15 + 00	<u>Δ 2° 50' LT.</u>		6.4	28.5 ✓
15 + 28	on Pav		8.9	26.0 ✓
"	F.L. 6" stub		11.70	23.2 ✓

34.87 ✓

T.P. 4.92 29.90 ✓ 9.89 24.98 ✓

Check to Spike BM 582 2408 ✓ 2406

Sully P.P. MONTONE 2.02

W. Pt Laine Blvd

X.M.

Montalvo St. is Oiled Surface W. Pt. L. Blvd to
 Paris St on Water & Sewer locations

Montalvo Clovis to Carnules Oil Surfacing
 Water Main location comes near
 N. side of Surfacing but should be considered
 in Surfacing

Carnules Intersection + St. not Surfaced.

Montalvo St. is ^{0.1} Surfaced W. Pt. L. Blvd. to Clovis

Clovis St. not Surfaced, Montalvo is Oil
 Surfaced to about 15' N of E of Clovis.
 at this intersection.

Tenecula Water Levels
Camulos to W. PT. Loma Blvd.

BM SPIKE	4.57	7.65 ✓	3.08		
T.P.	9.84	16.86 ✓	0.63	7.07 ✓	
T.P. Stub	10.13	19.29 ✓	7.70	9.16 ✓	
0+00	Tree on Camulos	12.2	7.1 ✓		
+04		11.3	8.0 ✓		
+40		11.3	8.0 ✓		
+60		10.2	9.1 ✓		
1+00	Top bank	6.2	13.1 ✓		
"	3' S. in road	7.5	11.8 ✓		
T.P.	1280	30.99 ✓	1.10	18.19 ✓	
1+50	Top bank	9.2	21.8 ✓		
"	3' S in road	12.7	18.3 ✓		
2		7.0	24.0 ✓		
+50		3.0	27.4 ✓		
3		0.5	30.5 ✓		
T.P.	1275	42.9 ✓	0.82	30.17 ✓	
3+50			9.9	33.0 ✓	
4			6.9	36.0 ✓	
+50			5.1	37.8 ✓	
5			4.0	38.9 ✓	
+50			3.8	39.1 ✓	
6			2.5	40.4 ✓	

SE Cor. of
Fountain
W. PT. Loma

25' NELY of
NLY Cor. of
Tenecula and
Camulos

42.92

5

6+50					40.7 ✓
C+60-1	Tree at Clovis	17.5	41.19 ✓		Stub
T.P.	4.75	45.92 ✓	1.75	41.17 ✓	"
Check to SE SPIKE			2.7	43.80 ✓	43.79
IN RR Clovis & Tenecula					0.01
7+00			4.9	41.0 ✓	
+50			6.3	39.6 ✓	
8			7.6	38.3 ✓	
+25			8.9	37.0 ✓	
+50			10.5	35.4 ✓	
+75			12.5	33.4 ✓	
T.P.	0.04	32.72 ✓	13.24	32.68 ✓	
9+00			1.0	31.1 ✓	
+50			7.1	25.6 ✓	
9+73	EH Tee		9.9	22.8 ✓	
"	12' NLY EH		11.2	21.5 ✓	
T.P.	3.84	24.63 ✓	11.93	20.79 ✓	
10+00			4.0	20.0 ✓	
10+22.6	par. over stub		6.2	18.4 ✓	
"	at W. PT. Loma Blvd.				
"	EL. STUB		8.9	15.7 ✓	

SELY Cor RR
Check to BM SPIKE MENTIONS
GWT W. PT. LOMA Blvd. 0.85 24.08 ✓ 24.06
0.02

10 22.6
6 60.1
3 62.5

Mentone water levels

Bet. Farrosa & W. Pt. Loma Blvd.

T.P.	5.8	<u>23.32</u> ✓		17.64	See P. 3 ✓
Campulos - 267			15.1	8.2 ✓	TOP of Sewer Cut
- 250			12.2	11.1 ✓	
- 235 PLAN			10.2	13.1 ✓	
- 195			7.1	16.2 ✓	
- 193 in wash			10.8	12.5 ✓	
- 187 " "			10.8	12.5 ✓	
- 180			6.8	16.5 ✓	
- 177			3.5	19.8 ✓	
- 164			1.3	22.0 ✓	
- 150			0.3	23.0 ✓	
T.P.	12.27	<u>35.51</u> ✓	0.08	23.24 ✓	
- 100			7.2	28.3 ✓	
- 50			2.9	32.6 ✓	
- 15			0.6	34.9 ✓	
			0.7	34.8 ✓	
			0.7	34.8 ✓	
T.P.	12.50	<u>47.62</u> ✓	0.29	35.12 ✓	
0 + 20			12.7	34.9 ✓	
0 + 30			11.0	36.6 ✓	
0 + 50			9.3	38.3 ✓	
1 + 00			6.5	41.1 ✓	
+ 50			3.9	43.7 ✓	

47.62

6

7			2.0 ✓	45.6 ✓	
T.P.	13.03	<u>60.12</u> ✓	0.53	47.09 ✓	
2 + 50			11.7	48.4	
3			8.3	51.8 ✓	
+ 50			4.8	55.3 ✓	
4			1.9	58.2 ✓	
+ 50			0.2 ✓	59.9 ✓	
T.P.	5.09	<u>65.11</u> ✓	0.10	60.02 ✓	
5			4.0	61.1 ✓	
+ 50			3.0	62.1 ✓	
6			3.5	61.6 ✓	
6 + 30	F.H. Tee		4.0	61.1 ✓	
"	12' Nly F.H.		3.8	61.3 ✓	
6 + 60	Cross at Clovis		4.0	61.1 ✓	
check to	B.M. spike on RR, SE cor. Mentone and Clovis		2.8 ✓	62.9 ✓	62.34
6 + 75	Reg. oil Pav.		4.3	60.8 ✓	0.03
7			5.3	59.8 ✓	
+ 50			7.3	57.8 ✓	
8			9.1	56.0 ✓	
+ 50			10.4	54.7 ✓	
9			11.7	53.4 ✓	
T.P.	0.07	<u>53.46</u> ✓	11.72	53.39 ✓	
+ 50			1.5	52.0 ✓	
10			2.9	50.6 ✓	
+ 50			4.9	48.6 ✓	

MENTONE WATER LEVELS

53.46 ✓

11 + 00	NAIL PQT	7.7	45.8 ✓	
+ 50		11.1	42.4 ✓	
T.P.	0.71	41.31 ✓	12.86	40.60 ✓
12		2.0	38.3 ✓	
+ 50		7.5	33.8 ✓	
13		11.7	29.6 ✓	
T.P.	0.12	28.81 ✓	13.12	28.19 ✓
+ 50		4.2	24.6 ✓	
0.60 to 67. or Wly = 13 + 71.2		6.3	22.5 ✓	Pos. over stub end
13 + 71.2	EL. STUB END.	8.5	20.3 ✓	
	at W. PT. LOMA BLVD.			
check to BM Spike Sely		4.76	24.05 ✓	24.06
Cor. Mentone + W. Pt. Loma				

CLOVIS water Levels
Montalvo to Temecula

BM Spike	47.5	<u>68.24</u> ✓		63.99	SELY R.R. Montalvo Clovis
0 + 00 = Tee at		Clovis + Montalvo	5.8	62.4	oil pav
+ 23		edge oil Pav.	5.2	63.0 ✓	
+ 50			5.1	63.1 ✓	
1			5.2	63.0 ✓	
+ 50			5.0	63.2 ✓	
2			5.6	62.6 ✓	
+ 50			6.1	62.1 ✓	
3			6.6	61.6 ✓	
+ 25.1 = Cross at		Mentone + Clovis	7.1	61.1 ✓	
+ 50			7.6	60.6 ✓	
4			9.5	58.7 ✓	
+ 50			12.1	56.1 ✓	
T.P.	0.43	<u>56.57</u> ✓	12.10	56.1 ✓	
+ 75			2.4	54.2 ✓	
5			6.4	52.2 ✓	
+ 50			8.8	47.8 ✓	
6			12.8	43.8 ✓	
+ 50.1 = Tee at		Temecula + Clovis	15.5	41.1 ✓	
check to SE Spike			12.77	43.80 ✓	43.79
Clovis + Temecula					<u>0.01</u>

CANULAS Water Levels
 MONTALVO to FAMOSA thence
 VIA FAMOSA to RIALTO

BM P₃
 Swly
 Spike P.P. 0.50 63.05 ✓ 62.55 CANULAS &
 MONTALVO

Station	Offset	Reading	Height	Height
0+00 = Tee at ^{CANULAS} MONTALVO		4.4	58.6	✓
+50		7.4	55.8	✓
1		10.2	52.8	✓
+50		13.2	49.8	✓
T.P.	0.33	<u>50.56</u> ✓	12.8	50.23 ✓
2		3.8	46.8	✓
+50		8.1	42.5	✓
3		13.3	37.3	✓
T.P.	0.26	<u>37.69</u> ✓	13.13	37.43 ✓
2+24.9	Cross at ^{MONTALVO} ^{AND} ^{CANULAS}	2.8	34.9	✓
+50		5.2	32.5	✓
4		9.7	28.0	✓
+50		13.6	24.1	✓
"	LT. in Road	14.7	23.0	✓
T.P.	0.66	<u>25.56</u> ✓	12.79	24.90 ✓
5+00	Top Bank	4.2	21.4	✓
"	2' LT. in road	7.7	17.9	✓
+10	in road	9.2	16.4	✓
+50		13.6	12.0	✓
T.P.	0.29	<u>13.51</u> ✓	12.34	13.22 ✓

13.51

9

Station	Offset	Reading	Height	Height
6+00			11.0	9.5 ✓
6+50.2 = Tee			6.3	7.2 ✓
T.P.	0.75	<u>15.90</u> ✓	4.26	9.15 ✓
7			8.0	7.9 ✓
+25			7.7	8.2 ✓
+50			6.0	9.9 ✓
+75			4.6	11.3 ✓
7+95.08	4 35° 20' LT		3.7	12.2 ✓
8			3.7	12.2 ✓
+50			4.1	11.8 ✓
9			5.2	10.7 ✓
+50			6.4	9.5 ✓
10			8.4	7.5 ✓
+15.83	Δ 54° 39' LT		9.1	6.8 ✓
T.P.	11.79	<u>18.25</u>	9.44	6.4 ✓
+40			11.0	7.2 ✓
+50			10.5	7.7 ✓
11			6.3	11.9 ✓
+50			3.3	14.9 ✓
12			1.6	16.6 ✓
+50			0.9	17.3 ✓
13			1.4	16.8 ✓
+50			2.5	15.7 ✓
14			3.7	14.5 ✓
+25			5.3	12.9 ✓

p. 5

9.16

0.01

ground
 on Δ
 STUB

		18.25 ✓		
T.P.	.1.00	<u>13.60</u> ✓	5.65	12.50 ✓
14750			2.8	10.8 ✓
14794	F.H. Tee		6.1	7.5 ✓ IN Rd
"	12' nly		5.4	8.2 ✓ on bank
15			6.6	7.0 ✓
+20			7.6	6.0 ✓
+30			8.1	5.5 ✓
15+40	0.5 LT to	Stub	9.0	4.6 ✓ ground
"	0.5 LT F.L.	Stub	11.70	1.90 ✓ F.L.
	check to BM Spike		10.54	3.06 ✓
	FANTOSA +			<u>3.08</u>
	W. Pt LOMTO Block			002

Valera water levels

Sketch P.V

BM SPI
SELY RP. 2.06 66.05 ✓ 63.99
T.P. 0.15 53.48 ✓ 12.72 53.33 ✓

Set BM. NELY Cor. of
SPIKE RP. Soto + Valera 11.09 42.39 ✓

0 + 00 at Soto St. 11.2 42.3 ✓
+ 50 9.6 43.9 ✓
1 7.6 45.9 ✓
+ 50 6.4 47.1 ✓
2 6.3 47.2 ✓
+ 50 7.1 46.4 ✓
3 9.8 43.7 ✓
+ 30 + Tee at Etiwanda 12.3 41.2 ✓

STUB
T.P. 3+30 0.00 41.80 ✓ 12.24 41.14 ✓

~~3 + 50 2.0 39.2 ✓
4 9.3 32.5 ✓~~

T.P. 0.22 28.94 ✓ 13.08 28.72 ✓

~~4 + 50 3.0 25.9 ✓
+ 62 4.5 24.4 ✓
+ 90 7.5 21.4 ✓~~

~~5+03 8.6 20.3 ✓ Beq. Pav
5+07 Δ 22 30' RT 8.6 20.3 ✓ Pav
5+19 = over 12" Main 8.4 20.5 ✓ Pav.
approx. 3' deep to FL.
T.P. 6.06 49.85 ✓ 5.15 23.79 ✓~~

check to BM Spike SE RP. 5.76 24.09 ✓ 21.05
Montano & W. Mt. Lavinia Blvd 0.03

1+35.5 34 RT to Sully Cor. of Plant Nursery
1+37 22 RT to Sly edge of Tel. Pole
" 3' RT. Beq. picket fence
2+91 1.6 RT to Sly edge Tel. Pole
" 3.3 RT end picket fence
2+92 Sly edge of 18x20 Bd. garage
4+09 19" RT to Tel. pole

Levels on line change 6-22-46
T.P. 3+30 0.38 41.52 ✓ 41.14 STUB

4+25 Δ = .4° 23' LT 12.3 29.4 ✓ STUB
T.P. 0.01 28.73 ✓ 12.80 28.72 ✓
4+50 2.9 25.8 ✓
4+75 5.7 20.0 ✓
4+91.3 ground 7.7 21.0 ✓
" Top 6" Bell 9.4 19.0 ✓

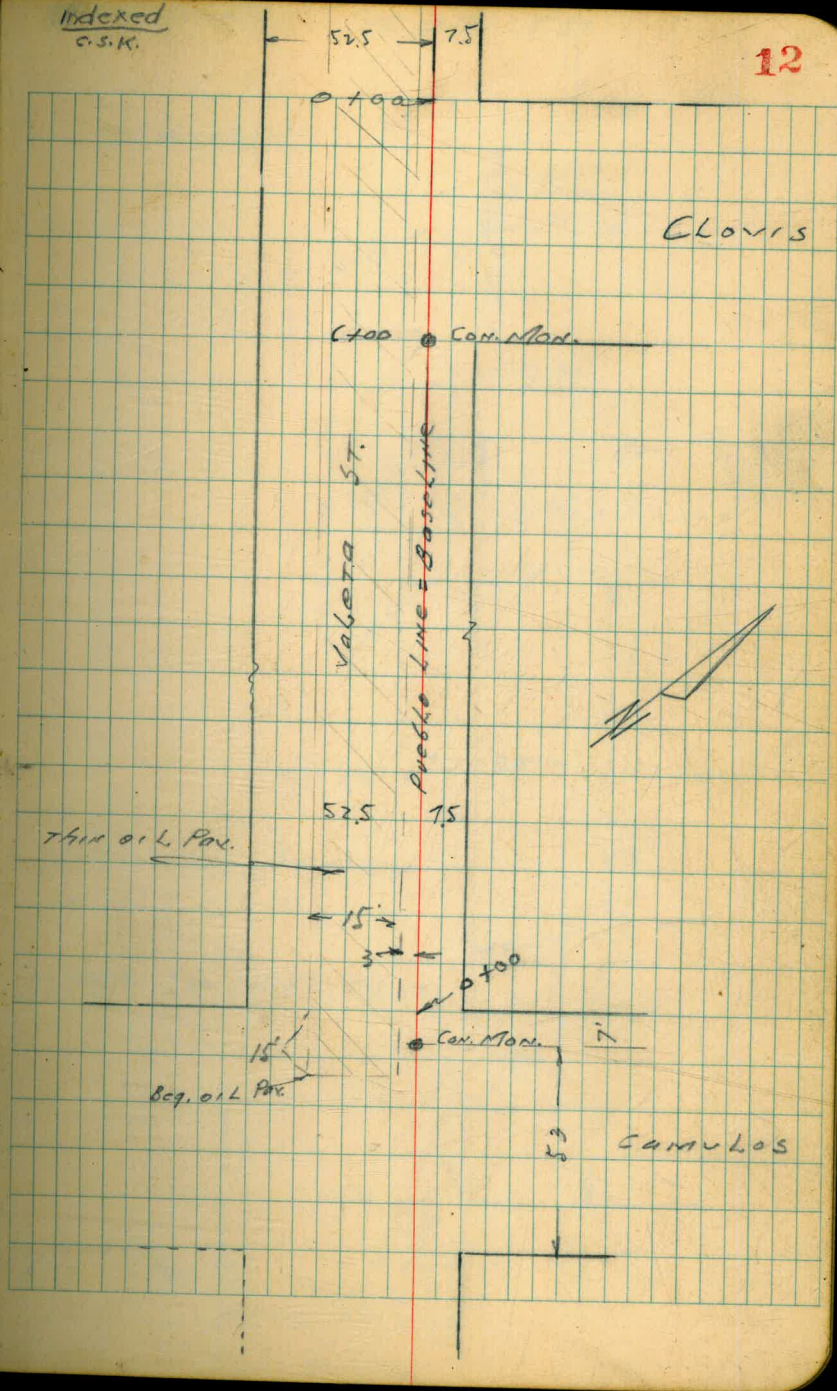
Cross Sec. Valeta St.
Camulos to W Paloma Blvd

C. Moore
Sommer Meyer
W. Moore
Bogg
6-24-46.

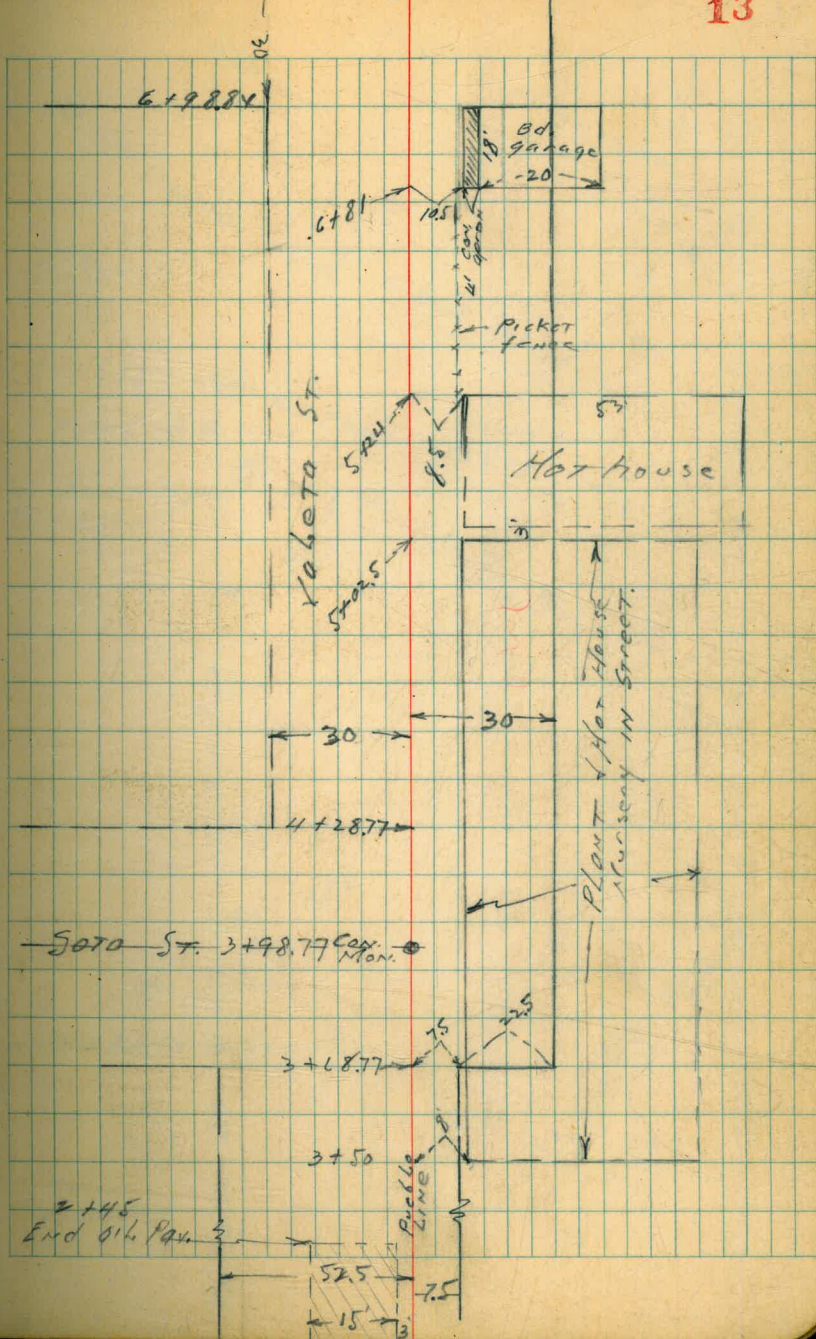
G.B. 178-27
F.B. 1375-6 1067-27
" 1337-4
Map # 1084

Indexed
C.S.K.

12



Etivwanga St. Cor. Mon. 7+28.84



2+45 End Oil Pav. 3

X sec Valera St.
to Establish Grade.

0 + 50

0 + 100 Wly Camulos St.

0 - 15 Beg. - 14' oil Pat. & strip approx.
10' S of Pueblo Line.

0 - 30 ϕ Camulos St.

00 - 60' = Ely Camulos St.

SWLY SPIKE
IN PP.
Montalvo
and
Camulos
P 3
THIS BOOK

12.43

74.98

62.55

LT = 56y.

Pueblo
Line
B.L.

Rt. 15

2.7
52.5

71.6
52.5

69.8
52.5

69.0
52.5

69.2
52.5

68.0
52.5

67.0
29

70.7
4.3
22.5

69.6
5.4
22.5

69.2
5.8
22.5

68.5
5.5
22.5

67.1
4.9
22.5

70.4

4.0
7.4

Beg.
St.
Fence

69.5

12" PP.
6.3

5.5
7.5

66.7
7.5

67.2
7.5

67.5
8.4
7.5

74.98

1+47 E 8' wide con apron + Sim. 900. Con. Fl.

1+24 E 2' Con. Walk

1+09 E Sim. 900. diat fl.

1+00

0+93 E Sim. 900. Con. Floor

0+88 end Lamb house

0+68 end Bd. + Bop. Lamb house

0+53 E 2.5 Con. Walk.

LT.

B.L.

16

5.17	11
9.4	4.98
	11.7
	99.2
	22.

4.97	70.0
7.5	

4.7	70.3
8.1	

72.2
2.8
52.5

70.7
4.3
22.5

21.7
0.2

70.4
4.6
7.5

10.33
4.65
11.7

40-4
House
7.8

Fence	Lamb
7.4	House
	7.8
4.205	
4.50	
7.8	

74.98

3 + 50

3 + 40 & Sem. gas. diet FL.

3 + 00

2 + 50

T.P. 10.05 79.78 5.25 69.73

2 + 00

1 + 50

74.98

6L.

8L.

R.T. 17

73.0
6.8
52.5

73.1
6.7
30

72.7
7.1
22.5

70.8
7.0
7.5

73.1
7.7
11.5

72.1
7.7
52.5

72.0
7.8
35

70.9
8.9
22.5

70.6
9.4
7.5

71.4
8.4
52.5

69.6
10.7
22.5

69.1
10.7
7.5

79.78
7.0
4.0
52.5

69.6
5.4
22.5

8.12 P.P.
62

68.4
5.6
7.5

71.4
4.0
5

70.2
4.8
22.5

70.0
5.0
7.5

74.98

5+00

4+75

4+50

4+25

4+00

3+89 E de. 9ac. dirt FL.

79.78

L.T.

24
52.5

24
52.5

24
52.5

24
52.5

24
52.5

24
52.5

24
52.5

24
52.5

24
52.5

24
52.5

24
52.5

24
52.5

B.L.

18

72.2

73.6

73.1

74.1

75.0

74.4

74.1

74.4

75.3

73.5

74.3

74.9

75.6

74.8

74.8

74.8

75.4

74.1

76.2

79.78

6405

6400 = Fly Clovis ST.

5493

T.P. 1.17 68.60 12.85 66.93

5475

5450

5425

79.78

L.T.

B.L.

R.

19

62.5

6.1

52.5

68.0

4.6

22.5

64.4

4.7

64.4

4.7

7.5

63.3

3.3

52.5

66.5

2.1

30

68.6

4.0

22.5

65.2

2.1

66.8

1.8

7.5

66.0

2.6

52.5

67.3

1.3

29

65.1

3.5

52.5

66.0

2.6

70.2

+ 1.6

7.5

67.6

12.2

52.5

68.60

68.8

11.0

30

67.2

12.6

52.5

68.4

11.4

3

70.5

9.3

7.5

69.0

10.3

52.5

70.5

9.3

34

69.4

10.4

52.5

71.9

7.9

7.5

71.4

8.4

52.5

72.4

7.4

30

71.7

8.1

22.5

72.9

6.9

164
PP
6.1

74.2

5.0

7.5

79.78

0 + 50

T.P. 0.40 56.50 12.50 56.10 ✓

0 + 20

6 + 60 = 0 + 00 = WLY Clovis St.

6 + 45

6 + 40

6 + 30 ~~to~~ Clovis St.

68.60

LT.

53.3
75

53.5
72.5

54.0
22.5

53.1
76

56.1
75

56.0
56.50
56.8
72.5

56.3
22.5

56.0
78

59.2
72.5

60.3
22.5

59.3
78

60.5
52.5

62.1
32

61.0
22.5

62.0
52.5

61.6
22.5

62.1
52.5

62.7
22.5

68.60

EX.

PT.

20

53.1
3.1

53.9
7.5

56.1
72

57.0
12.50
6.8

59.7
8.9

60.3
7.5

61.5
7.1

62.8
7.5

62.4
7.5

63.0
7.5

1 + 90 ± 10' Cen. apron + 900. can FL
Levels

1 + 75

T.P. spike
in RP
1 + 75
C.S. RT.

42.1

47.92

12.79

43.71

1 + 50

1 + 28

1 + 00

0 + 75

56.50

LT.

B.L.

R.

21

42.7	42.7	43.1	42.5	42.4	42.8
$\frac{5.2}{75}$	$\frac{5.2}{52.5}$	$\frac{4.8}{22.5}$	$\frac{5.4}{75}$	$\frac{5.5}{75}$	$\frac{5.1}{75}$
44.0	44.5	44.7	44.1	44.0	44.4
$\frac{12.5}{75}$	$\frac{12.0}{52.5}$	$\frac{11.8}{22.5}$	$\frac{12.4}{13}$	$\frac{12.5}{75}$	$\frac{12.1}{75}$
46.3	46.4	46.4	45.8	45.9	45.9
$\frac{10.4}{75}$	$\frac{10.1}{52.5}$	$\frac{10.1}{22.5}$	$\frac{10.7}{13}$	$\frac{10.6}{75}$	$\frac{10.6}{75}$ & 1.5 Brock Wock
48.9	48.9	49.0	48.1	48.2	48.8
$\frac{7.6}{75}$	$\frac{7.6}{52.5}$	$\frac{7.5}{22.5}$	$\frac{8.4}{13}$	$\frac{8.3}{75}$	$\frac{7.7}{75}$
50.8	51.5	51.5	50.9	50.8	51.3
$\frac{5.7}{75}$	$\frac{5.0}{52.5}$	$\frac{5.0}{22.5}$	$\frac{5.8}{70}$	$\frac{5.7}{75}$	$\frac{5.2}{75}$

56.50

42.1
5.80
7.8
±
apron

RP
5.46
11.6
900.

3 + 00

2 + 75

2 + 50

2 + 25

2 + 15 E do. gas. Cor. Fl. 20' wide

2 + 00

4792

LT.

B.L.

22

RT.

38.6
9.3
75

38.8
9.1
52.5

39.6
8.3
22.5

39.2
8.7
22.0

39.6
8.3

40.1
7.8
7.5

38.7
9.2
75

38.9
9.0
52.5

39.5
8.5
22.5

39.6
8.3

40.0
7.9
7.5

39.3
8.0
75

39.4
8.5
52.5

39.8
8.1
22.5

39.8
8.1

40.1
7.8
7.5

40.5
7.4
75

40.2
7.7
52.5

40.2
7.7
22.5

40.3
7.6

41.0
6.9
7.5

41.5
6.40
11

41.5
6.5
75

41.4
6.5
52.5

41.3
6.6
22.5

41.1
6.8

41.7
6.2
7.5

4792

5+75

5+48

5+25

5+22 E Singora Floor?

5+10 E Condoire 6.5 wide

T.P. 5.53 51.46 199 4593

5+00

47.92

Lr

8.6.
Rebbo
Line

Rr

24

47.0
4.5
30

46.8
4.7
20

46.8
4.7

47.6
3.9
10

47.8
3.7
30

46.38

5.08

31

2.5 Condoire

46.5
5.1
30

46.1
4.8

47.3
4.7
10

47.6
5.9
30

46.0
5.5
30

46.0
5.2

47.2
5.3
10

47.2
5.9
30

47.5
5.9
30

45.79

5.67
38.3

45.36
5.10
37

45.7
5.12
30

51.46
5.12
37

46.4
1.5

46.4
1.5
8

46.9
1.0
30

47.92

6+79

6+75

6+50

6+25

6+13

2 3' Con. walk 21.6 in street

6+00

51.46

LT

ST.
Pueblo
Time

RT

25

Tot. P.
7

6.4
30 45.1

5.5
18 46.5

7.1
10 44.4

7.5
10 44.0

7.4
4 44.1

9.1
1 45.4

1.1
30 45.4

5.7
30 46.0

5.3
20 46.2

7.0
18 45.5

6.2
10 45.3

5.1
10 46.4

4.9
30 46.6

5.0
30 46.0

P.P.
21

5.2
20 46.3

5.4
10 46.1

4.0
10 46.9

5.3
30 47.2

4.7
8.4
10 47.19
walk

3.9
30 47.56
walk

4.5
30 46.9

5.0
15 46.5

5.0
10 46.5

4.1
10 47.4

3.9
30 47.6

51.46

Alley Bk. 3 Hartleys North Park
31st to Herman. Sec. of Univ.

Conc. Pav. 15' Wide

8.2 Lt. = B.C. Conc. Ret. wall. End of wall
7.9 Lt. = Start Beard Fence

0+18

0+10

0+00 = E. line 31st - 75 RT. = start E+W. Conc. Wall

0+08 75 Lt. = start cold lay service yard

0-00² Sunken paving

0-10 Continued

0-10 = E. ab. line 31st

N.W.B.P.
Univ. + Iowa

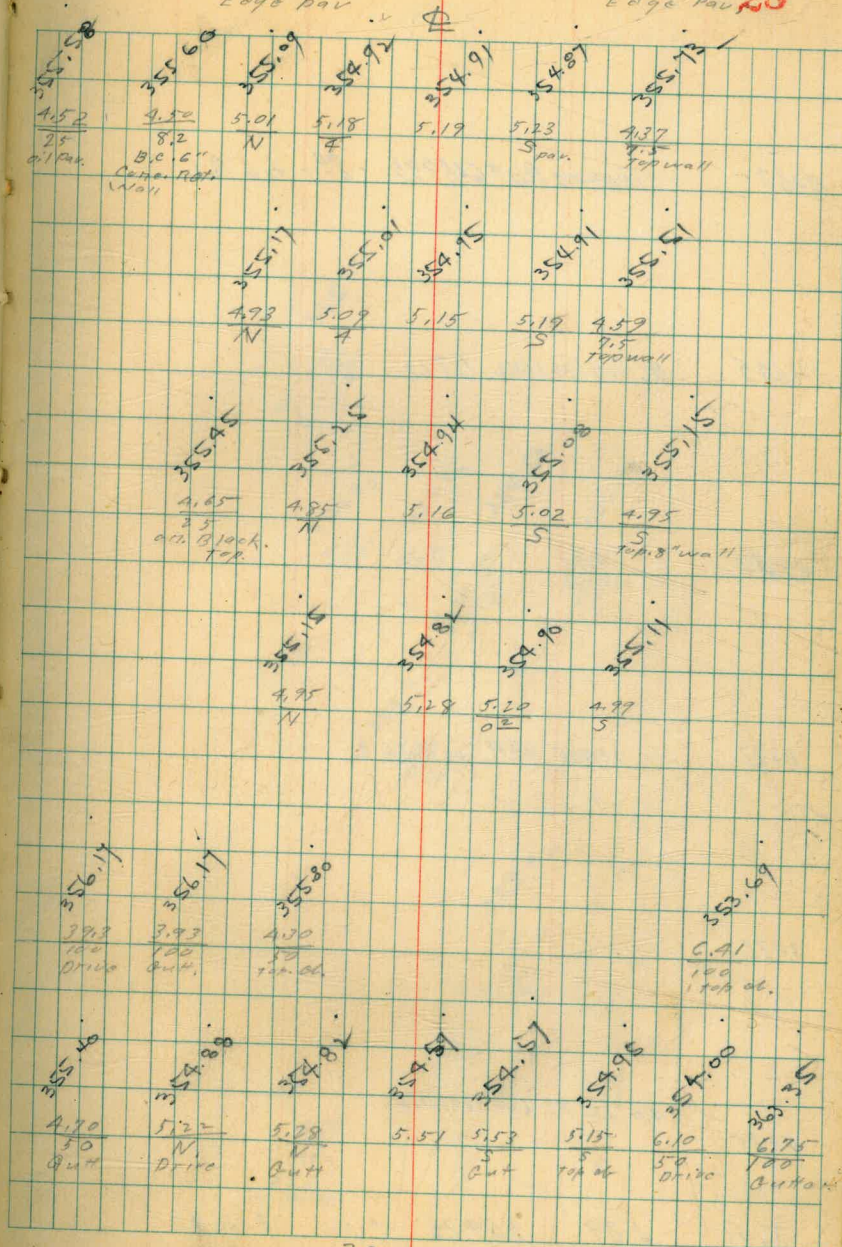
5.99 360.10 6.17 354.11

3.78 360.28 — 356.50

Indexed
c.s.k.

N = 75 Lt. of d =
Edge pav

S = 75 RT of d =
Edge Pav 23



360.10

0+63

Telephone Pole # 648995 - 8'-Lx to 6" Post.

0+60.5

B.C. Conc. Ret. Wall 11.7 Lx

0+50

0+27

SEWER M.H. on Axis of

0+22

0+21

11.6 Lx. E.C. Conc. Ret. Wall

T.P.

4.39

359.25

5.24

354.86

360.10

N = 75 Lt = Edge

conc Pav.

Φ
11/04

S = 75 Rt = Edge
paving 23

359.59

3.66

11.7

B.C. Conc.
Ret. Wall

354.90

4.35

N

354.46

4.80

4.72

7.5
S Pav

354.13

354.73

3.52

7.5
Top Wall

354.11

4.48

R.M

359.80

3.15

7.5
Top Wall

354.50

3.69

11.6

E.C. Conc.

Ret. Wall

359.25

1+06 2^o Wide Conc. Walk 7⁵ Left on North

355.51	354.56	354.51	354.40	354.31	355.66
3.94	4.69	4.73	5.05	4.93	3.59
1.35	7 ⁵	N. Pav		S. Pav	Top Wall
2 ^o Walk	2 ^o Con. Walk				

1+03 S.E. Cor. Stone Bldg. on North 9⁵ Left

0+88

354.53	354.26	354.35	355.70
4.72	4.99	4.90	3.55
N. Pav.	S. Pav.	S. Pav.	Top Wall

0+83 3 Conc. Steps 4' Wide - Entry To Med. Clinic Bldg on North 8⁵ Left

356.67	354.63
3.58	4.02
1.15	8 ⁵
Top of Landing	Bottom - Ground Level

0+72² Con. Steps 3^o Wide on South - 7⁵ St.

354.33	355.11
4.92	3.54
7 ⁵	9.7
S. Pav	Top Step

0+67² S.W. Cor. Stone Bldg. on North 9⁵ Left

0+6A 8.3 Lt. E.C. 6 Ret Wall + End of Walk
7.9 Lt. End Board Fence.

359.25

355.63	354.80	354.34	354.41	355.71
3.62	4.45	4.91	4.84	3.52
8 ⁵	N. Pav	S. Pav	S. Pav	7.5
E.C. + End Ret. Wall				Top Wall

359.25

1+58 8" Conc. Brick Wall - N. & S. on LEFT - 7.5 LEFT
Wall is 5.80 High above Pav.

1+50.5 E of Conc. APRON + 2 GAR. GARAGE on Rt.
APRON is LEVEL + 2 1/6 WIDE, GARAGE is 20"

T.P. 5.19 359.05 5.34 353.86

1+40 E. LINE of T ALLEY N. & S.

14 E of T ALLEY N. & S. + SEWER M.H. on E.S.

1+25 W. LINE of T ALLEY N. & S.

1+19 End of E.T.M. Wall on South 7' E RT.

359.25

N = 7.5 Lt. = Edge Pav.

±

S = 7.5 Rt. = Edge Pav.

31

353.97
5.08
N. Pav.

353.79
5.26

354.01
5.04
S. Pav.

354.02
5.03
N. Pav.

353.78
5.27

354.01
5.04
S. Pav.

354.19
4.86
11.5
FLOOR GAR.

359.05

354.14
5.11
N. Pav.

353.91
5.31
42

353.85
5.40

354.00
5.25
S. Pav.

354.31
4.94
50

353.93
5.32
100

354.18
5.07
N. Pav.

353.94
5.31
42

353.80
5.45
R.M. M.H.

353.97
5.28
S. Pav.

354.17
5.08
50

353.84
5.41
100

354.23
4.92
N. Pav.

354.11
5.14
42

354.00
5.25
S. Pav.

354.05
5.20

354.35
4.90
50

354.11
5.14
100

354.16
5.09
S. Pav.

354.60
3.65
TOP 8"
CONC. WALL

359.25

2+63 8^E Rt. = Ctr. 14" x 14" Conc. post.

2+55

2+52 8^E Rt. = Ctr. 14" x 14" Conc. Post.

2+42 8^E Rt. = Ctr. 14" x 14" Conc. Post

2+35

2+32 8^E Rt. = Ctr. 14" x 14" Conc. Post.

2+21 8^E Rt. = Ctr. 14" x 14" Conc post

2+15

2+00

1+82 8" Conc. Brick Wall N.E.S. on Left - 7.5' Long

Wall is 3.90 above Pavement

359.05

N = 7^E Lt. = Edge pav

S = 7^E Rt = Edge pav 32

353.00	353.26	353.15	353.16
<u>537</u>	<u>579</u>	<u>590</u>	<u>589</u>
252	N. Pav.		S. Pav.
IN PARKING AREA			

353.03	353.40	353.26	353.24
<u>522</u>	<u>565</u>	<u>579</u>	<u>581</u>
252	N. Pav.		S. Pav.
IN PARKING AREA			

353.97	353.41	353.19	353.25
<u>508</u>	<u>564</u>	<u>586</u>	<u>580</u>
252	N. Pav.		S. Pav.
IN PARKING AREA			

354.06	353.57	353.40	353.42
<u>500</u>	<u>548</u>	<u>565</u>	<u>563</u>
252	N. Pav.		S. Pav.
IN PARKING AREA			

354.23	353.80	353.65	353.12
<u>480</u>	<u>525</u>	<u>540</u>	<u>532</u>
252	N. Pav.		S. Pav.
IN PARKING AREA			

354.04	353.75	353.85	
<u>501</u>	<u>530</u>	<u>520</u>	
N. Pav.		S. Pav.	

359.05

STARTING B.N.H.

			3.70	396.50
T.P.	6.18	360.20	5.03	354.02

2+78 Cont.

2+78+00 - W. CURB LINE HERMAN

2+67 End of CURB RETURN ON LEFT

2+65± = W. L. Herman

359.05

N = 75 Lt. = Edge Pav.

±

S = 75 Rt. = Edge Pav.

33

353.99
 5.06
 5.00
 CURB TOP

352.12
 6.93
 5.00
 CURB

353.11

5.94
 50
 GUTTER

352.84
 6.21
 75
 CUR. DRIVEWAY CURB

351.65
 6.40
 N. Pav

352.97
 6.58

352.43
 6.62
 S. Pav.

352.80
 6.25
 75
 TOWARD GUTTER

351.61

7.44
 50

353.22
 5.83
 75

353.61

5.44
 250
 PARKING AREA

353.22
 5.83
 N. Pav

353.11
 5.94

353.11
 5.94
 S. Pav.

352.09
 5.96
 ALLEY RETURN

359.05

74.22

2+0		88	65.4	
+50		5.7	68.5	
3+0		26	71.6	
"	6.1 Lt of $\frac{1}{2}$ Fly Pav.	2.49	71.73	
"	50 Rt of $\frac{1}{2}$	78	66.4	
TP	12.96	86.38	0.80	73.42
+31.94		12.96		73.42
+50		11.8		74.6
4+0		88		77.6
"	50 Rt of $\frac{1}{2}$	15.6		70.8
"	6.2 Lt of $\frac{1}{2}$ Fly Pav	8.55		77.83
+50		5.7		80.7
+89	6.7 Rt - Fly Emmet Hour	6.8		79.6
5+0		3.2		83.2
"	6.1 Lt of $\frac{1}{2}$ Fly Pav	2.75		83.53
+50		1.1		85.3
TP	6.58	92.28	0.68	85.70
6+0		5.7		86.6
"	5.6 Lt of $\frac{1}{2}$ Fly Pav.	5.36		86.92
"	50 Rt of $\frac{1}{2}$	6.4		85.9
+21	= Fly oil + Peck Paving	5.4		86.9
+49.42	= 30 Cts St	5.10		87.18
+89	= Fly oil + Peck Pav	4.2		88.0
7+0		4.2		88.1
"	4.1 Lt of $\frac{1}{2}$ Fly Pav	4.07		88.21

0.75 Hub
3+31.940.72" out by
3/16 Tube in
GovernmentNail Pav
opp. 5+50

35

92.28

7+50		4.8		88.5
8+0		3.2		89.1
"	5.2 Lt of $\frac{1}{2}$ Fly Paving	5.12		89.16
"	50 Rt of $\frac{1}{2}$	2.7		89.6
+50		2.8		89.5

Proposed Sawyer Bata St.

43rd St. to 600' East.

Sketch page 34

0+0	= 6+49.42	92.28	86.62	Stucco House on Floor
0+41	12 Lt of $\frac{1}{2}$ = Sly 24' Palm Tree = Nly Palm			
"	12 Rt " " Nly " "			24' Centers to East
+50	on oil + Rock Pav.	5.66	86.62	
+73	29 Lt of $\frac{1}{2}$ = S.Fly	2.43	87.85	Stucco House on Floor
+70	on oil + Rock Pav.	6.02	86.26	
+40	48 Rt of $\frac{1}{2}$ = $\frac{1}{2}$ + Nly	4.90	87.38	Stucco Ho. on Floor
"	44 Lt " " = $\frac{1}{2}$ + Sly	3.45	88.73	Frame House on Floor
TP	7.30	93.72	5.86	86.42
+50	on oil + Rock	7.38	86.34	
+97	56 Lt of $\frac{1}{2}$ = $\frac{1}{2}$ + Sly	3.80	89.92	Stucco House on Floor
3+0	on oil + Rock	7.00	86.72	
+41	49 Rt of $\frac{1}{2}$ = $\frac{1}{2}$ + Nly	4.86	88.86	Stucco House on Floor
+50	on oil + Rock	6.37	87.35	
+92	51 Lt of $\frac{1}{2}$ = $\frac{1}{2}$ + Sly	2.32	91.90	Frame Ho. on Floor
3+0	on oil + Rock	5.74	87.98	
+20	58 Rt of $\frac{1}{2}$ = $\frac{1}{2}$ + Nly	3.83	89.89	Stucco Ho. on Floor
+50	on oil + Rock	5.08	88.64	
"	45 Lt of $\frac{1}{2}$ = S.Fly	1.57	92.15	Stucco Ho. on Floor
4+0	on oil + Rock	4.31	89.41	
"	48 Rt of $\frac{1}{2}$ = $\frac{1}{2}$ + Nly	2.59	91.13	Frame Ho. on Floor
TP	6.25	96.66	3.31	90.41
+50	on oil + Rock	6.40	90.26	
"	101 Rt of $\frac{1}{2}$ = N.Fly	7.13	89.53	Frame Ho. on Floor
5+0	on oil + Rock Pav	5.50	91.16	

36

96.66

5+0	41 of $\frac{1}{2}$ = $\frac{1}{2}$ + Sly	2.76	93.90	Stucco House on Floor
+50	on oil + Rock Pav	4.25	92.41	
"	49 Rt of $\frac{1}{2}$ = $\frac{1}{2}$ + Nly	2.92	93.74	Stucco Ho. on Floor
"	47 Lt " " = $\frac{1}{2}$ + Sly	2.60	94.06	Stucco Ho. on Floor
+93	= Fly Palm tree 24' Centers to West			
6+0	on Rock + Oil Pav	3.63	93.03	
+21.88		3.67	92.99	on R.P. + Disc
+42.5	= Fly oil + Rock Pav.	3.91	92.75	
7+0		3.1	93.6	
+12	= $\frac{1}{2}$ + Nly	0.98	95.88	Frame Ho. on Floor
TP	2.82	91.46	8.02	88.64
	6.09	95.82	1.72	89.73
BM		5.69	90.13	S. X. Ch. 1/2 Alpha + 1/2 90/6

2 + 42 Sing. gar. Con. FL.

2 + 41.5 10.7 LT SW Cor shed

2 + 36 Sing. gar. dirt FL.

2 + 26.5 Sing. gar. Con. FL. 11.8 RT.
" " dirt " 15.9 LT

2 + 20 11' LT end Sch. fence

T.P. No. 1 3.37 33.55 2.90 30.18
P.P. 2101

2 + 01 8.6 RT P.P. J.P.A. 260 4429/5 H

2 + 00 10.3 RT H end fence

1 + 85 Sing. gar. on RT Con. FL.

33.08

LT

Rt

Rt

40

30.17
3.38
11

15.1
1.9
dirt

15.9
1.0
dirt

10.4
28.8

5.0
28.6

10.4
29.6

33.55

10.1
28.5

11.6
28.5

10.1
29.3

13.8
29.28
12.6
20.1

fence
11.3

10.1
11.6

11.6
11.6

33.08

3+24 9.9 Rt Beg. Bd fence

3+15.5 10.5 Rt NE Cor Bd Dwelling

3+00 9.8 Lt SE Cor shed + Beg Bd fence

2+91 10.9 Rt NW Cor Bd Dwelling

2+87 9.7 Lt SW Cor shed
9.7 Lt end Bd Fence

2+74 8.3 Rt P.P. PH #454 4 8x8 ft end Bd fence

2+69 10.2 Lt SE Cor shed + Beg. Bd. fence

2+61 E 4' Cor. step thru gate

2+51.5 8.4 Rt. Beg Bd Fence

2+50 10.1 Lt SW Cor shed
10.4 Lt SE Cor. shed

33.55

Bd Fence
9.7

4.2
9.7

4.2

4.0
9.9

4.3
9.8

4.53
194.
RIM

4.1
10

4.3
10

4.6

4.7
10

5.1
5.8

11.2
8.3

4.6
10

11.8

4.0
10

33.55

Lt

Rt

Rt

41

3491 E Sin. 900 Con approx 4 Floor

3483 Sin. 900 dirt FL.

3480 9.5 ft end Bd Fence

175

174 8.8 ft P.P. P.H. 4840

3466 15 ft Sin 900 Con floor

T.P. 4.51 35.11 29.5 30.60

160 14.9 end Bd fence

153 9.8 ft Δ in fence

3450

3430.5 E 6' Con walk

33.55

430.337
18.7
900

51030.10
17.01
aprox
8 wide

29.7
5
7.6

29.7
5

30.1
10
5

30.0
11.3
15
5

35.11

Fence
9.8

29.7
3.9
9.8

29.5
4
1

29.8
1.8
9.7

Fence
9.7

29.77
3.78
10.05

33.55

Px 42

4+77 8.8 RT PP # 4820

4+66 Singar. Con apron 83 wide

+150 9.9 Lt Beg Bd Fence

+149 15.8 RT end Con BLK wall

4+35 E Con walk on RT

4+25 8.9 Lt end Bd Fence

+33.5 15.8 RT Beg Con BLK wall

4+23 E do gar. 18 wide Floor level

4+12 12 RT end Lath fence

4+05 9.2 LT Beg Bd Fence

4+00

+97.5 11.4 RT⁸⁻⁹ Lath fence

3+93 Singar dirt FL.

35.11

LT

R

RT

43

4.6
10
30.8

4.6
10
30.8

4.6
10
30.5

4.1
31.0

4.1
30.7

5.1
30.0

3.7
31.4
10
31.84

4.0
31.1

4.8
10
30.31

2.97
1.58
900
32.14

3.00
15.8
2 wide
con walk
31.45

3.53
15.9
31.58

4.8
11.5
30.31

35.11

alley Blk 50 O.B.

5+50 end 2.5 Con walk // with alley

+45 7 Rt end Salt hedge.

5+40

5+30

+20 7' Rt Beg. salt Bush hedge

5+06 Sing. gar. dent floor

5+00.2 Beg. 2.5 wide Con walk Parallel with alley

T.P. 5.62 37.50 37.3 31.88

5+00 9.9 Lt end Bd Fence

4+95 Sing. gar. 8 wide Con approx ↓ FL

3511.

Lt

4.57
32.93
12.3

S. edge
walk

4.61
32.89
12.3

S. edge con walk

5.09
32.41
12.3

S. edge
con walk

5.1
32.4

5.10
32.5

4.7
32.8

5.1
32.3
12.9

5.32.15

5.35
32.15
12.3

S. edge
walk

37.50

3.4
31.7
9.9

Fence →

3.4
31.7

3.3
31.9
10

3.07
32.04
13
approx

13.23

2.80
32.31
16.2
con.

3511

44

Check to SEBP
Del Monte + Sunset 2.87 37.01 37.05
cliff Blvd.

6+11.94 W. of Blvd.

T.P. 7.05 39.88 4.67 32.83

5+99.94 WIL Sunset cliff Blvd.

5+95

5+70

37.50

curb Sunset
Bad Condition

32.36	31.90	32.84	32.50	32.76	32.83	33.18	33.28	33.28
7.52	7.98	7.04	7.38	7.12	7.05	6.70	6.60	6.20
07 06	50 97	12 06	12 97		12 97	11 06	10 97	09 06

33.03	35.93	39.88	
4.47	4.57	32.82	
9.95	9.9	4.68	
06	Pay	Pay	

33.2	33.0	32.98
4.13	4.5	4.57
10		9.95
		Pay

33.8	33.0	33.4
4.17	4.3	4.1
10		10
		Pay

37.50

Sewer Prelim

Albion - Dupont - Silvergate - Jennings

11-26-49

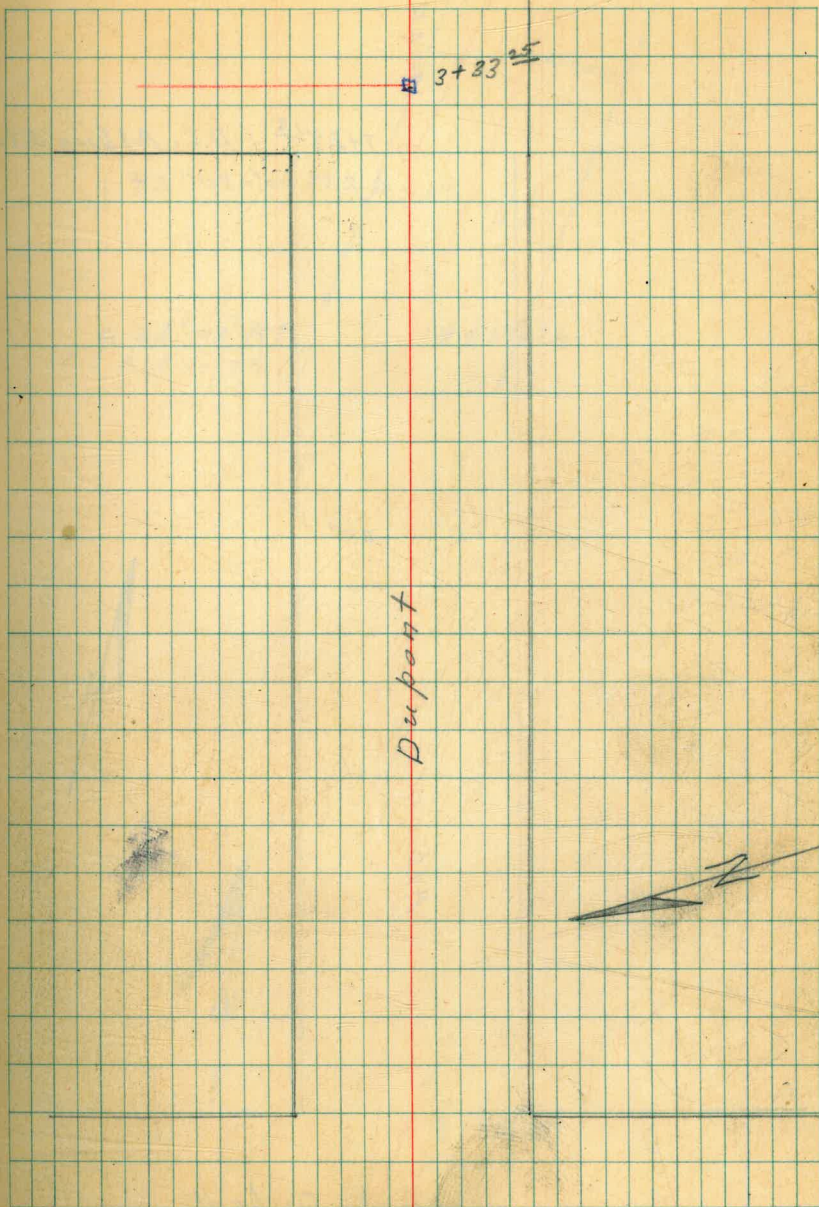
Sommermayor
McCoy
Allen
Jones

INDEXED

WK
DEC 1 1948

- = Fd. Man.
- = Fd. V. Hub
- = Set Hub + Nail
- = Fd. prop. pipe

46



Dupont

Locals - P. 51
OTOD

Silvergate Ave.

□ - P.I. @ Albion St.

40.22

7+28.18 = B.C. Albion St.
 $\Delta 23^{\circ}00' - 30''$ Lt.

25' 25'

Albion

□ Dupont

47

10+00

25'

25'

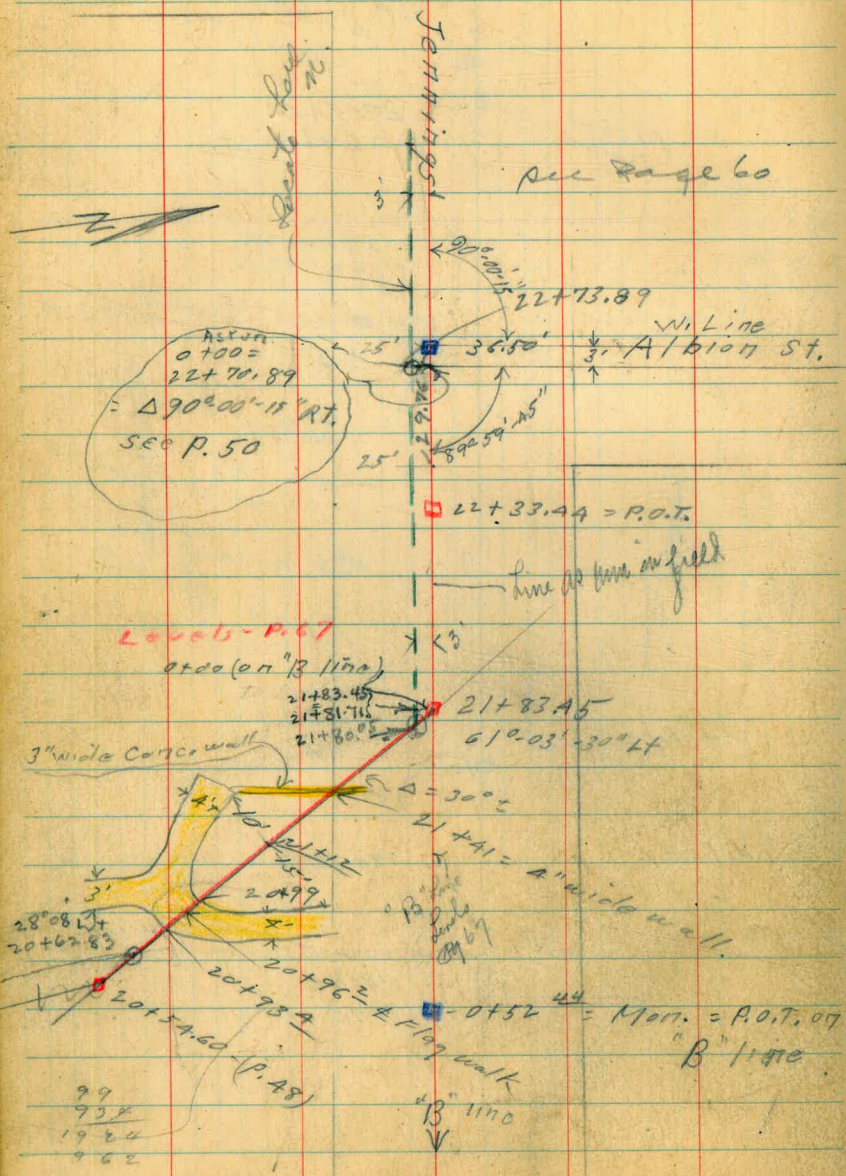
$\Delta 23^{\circ}02'$ Rt.
E.C. Albion St.

9+27.74

7+28.18

Silvergate

24+98.31 $\Delta 0^{\circ}06'LT$
- Fd 1/1 (& Silvergate)



Fd. 2" pipe
& Jennings
& Catalina
A.C. Pave
28+51.5 (on line)
Fd. Exist Dead end cop.

A.C.
Pave.

Fd. 2" pipe 27+81.66
 $\Delta 0^{\circ}04'RT$

see p. 75

24+98.31
 $\Delta 0^{\circ}06'LT$

Albion St.
Jennings - North

Levels on P. 63.



W. Line Albion. (Pueblo line)

Fd Mon. 90°-00'-15"
(P. 47.44)

2736.00

0700

26.75

2173.88

2170.89

3'

3'

3'

50

Fd. Mon.

at Talbot

Exist sewer.

151.90 to Note.

Δ 10°-07'-30" Lt.

Fd. Exist M.H.
7+82.00

3'

3'

Duport - Albion
Sketch Page 46

2+00

T.P. 0.72 <284.29> 12.98 <283.57>

1+50

1+00

+60

+30 = E.L. Silvergate

0+00 \pm Silvergate \pm Duport to East (on oil pipe)
 $= 15 + 452 \pm$ Duport to 711 - 11.77 \pm Duport \pm 2849 = \pm 15 + 35 \pm 34

Set B.M. on 1407 (on tack)
 \pm Silvergate and
 \pm Duport to East.

6.56 <289.99> B.M.#1

T.P. 1.87 <296.55> 12.38 <294.68>
Spike in N.W. R.P. 1.52 <307.06> - 305.54
Silvergate + Pico

F.R. 1751
34

±

51

12/1/48
Kells & Co
Duport

281.5 ✓
2.8

<284.29>

283.1 ✓
12.8

286.0 ✓
10.6

287.8 ✓
8.7

289.1 ✓
7.4

290.4 ✓
6.1

<296.55>

5+00

4+50

4+00

3+60 End oil pave.

3+45

3+23²⁵

Hub 1/2.

7.55 276.74

B.M.# 2

3+23²⁵

oil. oil pave.

3+00

2+50

284.29

276.4 ✓
7.9271.6 ✓
 $\frac{12.7}{100}$ 276.8 ✓
7.5277.0 ✓
7.3272.3 ✓
 $\frac{12.0}{100}$ 276.6 ✓
7.7277.1 ✓
7.2276.9 ✓
7.4278.2 ✓
6.1279.9 ✓
4.4

284.2 ✓

8+50

8+00

7+50

T.P. 2 6.85 $\langle 282.13 \rangle$ 9.01 $\langle 275.29 \rangle$ → B.M. #2
 7+28¹⁸ Δ 23° 00' - 30" Lt.

7+00

6+50

6+00

5+50

 $\langle 284.29 \rangle$
 $\langle 275.7 \rangle$
 6.4

 $\langle 275.6 \rangle$
 6.5

 $\langle 271.4 \rangle$
 $\frac{10.9}{100}$
 $\langle 275.3 \rangle$
 6.8
 $\langle 282.13 \rangle$
 $\langle 275.28 \rangle$
 $\frac{9.01}{11.8}$
 $\langle 275.1 \rangle$
 8.6

 $\langle 271.1 \rangle$
 $\frac{13.2}{100}$
 $\langle 275.9 \rangle$
 8.4

 $\langle 276.1 \rangle$
 8.2

 $\langle 270.9 \rangle$
 $\frac{13.4}{100}$
 $\langle 276.0 \rangle$
 8.3

 $\langle 284.29 \rangle$

11+30

L+T. West End - S.W. of Rot.
Dudley + Albion2.27 $\langle 280.25 \rangle$ B.M. #4

T.P.

5.02 $\langle 282.52 \rangle$ A.63 $\langle 277.50 \rangle$

11+00

10+50

10+00

9+50

 $\approx \frac{1}{2} \Delta$ B.M. (9+27²⁴)5.48 $\langle 276.65 \rangle$ B.M. #39+27²⁴ Δ 23°-02' RT.

9+00

 $\langle 282.13 \rangle$ 277.9 ✓
A.6271.5 ✓
 $\frac{11.0}{100}$ 282.52 ✓277.5 ✓
A.6277.0 ✓
5.1276.8 ✓
5.3271.7 ✓
 $\frac{10.4}{100}$ 276.6 ✓
5.5276.65 ✓
5.48
H.W.B.277.0 ✓
 $\frac{10.1}{100}$

90° to Ewd. Tang

276.1 ✓
6.0 $\langle 282.13 \rangle$

S.W. 7' Mon. Albion + Charles 5.77 276.75 B.M. #5

 $14+09 \overset{77}{=} \Delta 89^{\circ} 49' \text{RT. (on Hub)}$

13+88.77 So. Line Charles

+50

13+00

+50

12+00

11+58.6+ Aprox. \pm Dudley $\langle \underline{282.52} \rangle$ 275.16 ✓
7.36275.9 ✓
6.6276.9 ✓
5.6277.6 ✓ 277.4 ✓
4.7 $\frac{10.3}{100}$ 278.1 ✓
4.4278.3 ✓ 271.2 ✓
4.2 $\frac{11.3}{100}$ 278.1 ✓ 271.0 ✓
4.4 $\frac{11.5}{100}$ $\langle \underline{282.52} \rangle$

16+00

15+93 11² Lt. = 30" diam Cypress15+53 11⁸ Lt. = 24" diam Cypress

15+50

15+38 10' Rt. = start row of Eucalyptus
Trees Average 14" diam. and 10' apart.

T.P.

1.51

271.45

12.58

269.94

Mon 21' Rt + 15+18⁷²

11.75

270.77

BM# 6

15+28⁷³ = Δ 90°-06' Lt. (on hub)

15+00

14+50

14+30

22' Lt. = S.W. Cor. House

282.57

267.5

3.9

258.4

13.0
100

269.0

2.4

267.8

3.6
50

263.2

8.2
80

259.0

12.4
100

271.45

269.94
12.58271.3
11.2273.1
9.4

272.9

2.6

22

1st floor

10001

272.8

2.7

22

2nd.

274.0

8.5

282.52

T.P.
18+36 88
E Wilcox

1.08 $\langle 265.03 \rangle$ 7.50 $\langle 263.95 \rangle$ B.M. # 7

18+11 $\frac{1}{2}$ Cross 8" wide 4' high E.W. Adobe wall

18+00 72' Rt. = Rim of canyon

17+96 9' Lt. = start ^{N. + S.} 5' High Adobe wall,
Conc. Footing

17+78 9' Lt. = 30" Cypress

17+50 61' Rt. = Rim of canyon

17+17 11' Lt. = 30" Diam Cypress

17+14 15' Lt. = S.E. Cor. House

17+00

16+86 10' Lt. = 30' Cypress

16+50

+00 10' Lt. = 24" stump 12' High

$\langle 271.45 \rangle$

~~1.08~~
~~265.03~~

~~7.7~~
~~8.0~~
~~Rim of Canyon~~

263.9 ✓
7.7
Brd.
Base
Conc. Footing

262.1 ✓
7.7
269.2 ✓
12.2
72

265.5 ✓
5.9
261.2 ✓
10.2
61
267.6 ✓
23.8
100

267.0 ✓
4.4
15
Floor
267.0 ✓
4.5
15
Brd.
265.8 ✓
5.6

266.0 ✓
5.5

266.5 ✓
4.9
260.0 ✓
11.4
50
250.0 ✓
21.5
100

$\langle 271.45 \rangle$

of Retained line
19+80 7th Lt. = 24" diam. Cypress ϕ .

19+50 16' Rt. = Rim of canyon.

5' Rt. of Retained line
19+35 2nd Lt. = ϕ 3' Diam Vertical Cross Rock.
concrete top + pipe connection from house.
19+20 7th Lt. = End Rock wall

19+00

18+63

18+62 = 7' Lt. = Start N. + S. Rock wall
in ϕ = Cross Rock wall (1' wide)

18+61

18+36⁸⁸ ϕ Wilcox

18+21 3' Lt. = Pole # 3535

18+20 10' Rt. = End row of Eucalyptus

$\langle 265.03 \rangle$

260.8[✓] 258.8[✓]
4.2 $\frac{6.2}{10}$

260.3[✓] 262.0[✓] 264.1[✓]
4.7 3.0 3.9
7 7 7
Base top Ord
wall

260.7[✓]
4.3

261.6[✓] 260.8[✓]
3.4 4.2
Ord. $\frac{4.2}{\phi}$
Base of wall

1 263.6[✓]
1.4
top of wall

263.2[✓]
1.8

263.9[✓] 255.3[✓]
1.1 9.7
80
Rim of Canyon

$\langle 265.03 \rangle$

18+36 88 = S
3508 = S
18+32.50 = Alley
7.50 = Alley
2007-88 = Alley

21+12 15' Rt. = Wly. edge of East walk } p 49
10' Lt. = Ely. edge west walk

20+96² \pm Flagstone + Conc. walk

T.P. 8.03 $\langle 266.09 \rangle$ 6.97 $\langle 258.06 \rangle$

20+96 6' Lt. = \pm 18" Cypress

2+85 14' Rt. = \pm clump of palms. 8' Diam.

Also = rim of canyon.

20+74 = cross picket fence

20+61.88 = 20+62.83

20+54⁶⁰ Δ 29°-00' Lt. 11.00 254.03 B.M. #8
8.23

20+45² \pm . Cross rim of Canyon.

20+35 10² Lt. = 30" diam. Cypress

20+31.88 Δ ^{near dip.} also = start picket fence.

20+26² 9² Lt. = N.E. Cor. house

20+11³ 9² Lt. = S.E. Cor. frame house

20+01.88 Δ Alley to N. (Cal.) ^{idea here from corner of line 3/4}

20+00 10' Rt. = Rim of Canyon

$\langle 265.03 \rangle$

257.2²
8.9

$\langle 266.09 \rangle$

257.3²
7.7

255.1

254.0¹ 250.4¹
11.00 14.6
Hub. 10

900 to back tang

255.5¹
7.5

261.3¹ 260.3¹ 257.8¹
3.7 4.7 7.2
9² 9²
Floor Ord

258.2¹ 255.0¹
6.8 10.0
10

$\langle 265.03 \rangle$

21+83⁴⁵ ori. Hub 6.57 259.52 B.M. #9

21+83⁴⁵ = Δ 61° 03' - 30" Lt. = pueb. line

concr. wall (runs to west)

2+58^E 5" Lt. = East end of east + west

2+56 6" Lt. = 24" Cypress

(runs to east) Concr. wall

2+53^E 4" Rt. (at 90°) = west end / east + west

21+52 5" Rt. = 20" diam. Cypress

21+42 Ornd.

21+41 Top of 3" wide concr. wall

21+40⁸ Base of wall

21+40

21+13

(266.09)

#

60

259.6 ✓
6.5

21+83.45

262.4 ✓
3.7
5" top wall

259.3 ✓
6.8
5" Base wall

259.0 ✓
6.2
5" Ornd

259.4 ✓
6.7

258.6 ✓
7.5
12 Rims of Canyon

259.3 ✓
6.8
4" Ornd

258.3 ✓
7.8
4" Base Wall

261.8 ✓
4.3
4" top of wall

259.4 ✓
6.9

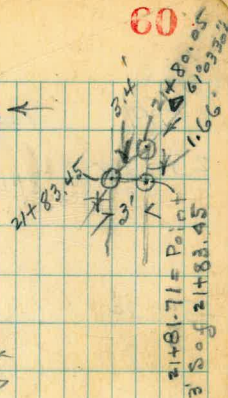
259.4 ✓
6.7

258.5 ✓
7.6

258.8 ✓
7.3

258.5 ✓
7.6

(266.09)



Jennings St.

T.P. 12.50 $\langle 278.48 \rangle$ 0.11 $\langle 265.98 \rangle$
23+50

23+30

23+00

22+82² 2' R.T. = Ctr. $2' \times 2'$ gas valve chamber

~~F.P.~~
22+73⁸⁹
conc. Men.
Albion +
Jennings

2.12 263.97 B.M. #10

22+70⁸⁹ = 0+00 for line on Albion to
North. (sketches - P. 49+50 - Levels
page)

22+33⁴⁴ = P.O.T. (P. 49)

22+00

$\langle 266.09 \rangle$

6

61

266.1 ✓
0.0
10

266.1 ✓
0.0
10

266.69 ✓
+ 0.6
10

264.9 ✓
1.2

264.7 ✓
1.4

264.7 ✓
1.4

264.7 ✓
1.4
2

264. ✓
1.9

261.84 ✓
4.25
Hub + 3rd.

260.2 ✓

5.9
 $\langle 266.09 \rangle$

Jennings

T.P.
Pole # 3625

0.42 $\langle 266.9 \rangle$ 11.99 $\langle 266.49 \rangle$

+50

26+00

25+50

3 Nails in 20' Lt.
Pole # 3601 25+L3

4.27 $\langle 274.21 \rangle$ BM# 11

24+98² & Silvergate A 0°-06' Lt.

24+80

24+50

24+25 61' Rt. = S.E. Cor House 1/4/28

24+00

$\langle 278.48 \rangle$

±

62

265.9[✓] 266.3[✓] 265.0[✓]
 $\frac{12.6}{10}$ 12.2 $\frac{13.5}{10}$

268.1[✓] 268.4[✓] 267.0[✓]
 $\frac{10.4}{10}$ 10.3 $\frac{11.5}{10}$

270.9[✓] 270.5[✓] 269.8[✓]
 $\frac{7.6}{10}$ 8.0 $\frac{8.7}{10}$

274.9[✓] 275.8[✓] 275.1[✓]
 $\frac{3.6}{10}$ 2.7 $\frac{3.4}{10}$

275.0[✓] 276.6[✓] 276.3[✓]
 $\frac{3.5}{10}$ 1.9 $\frac{2.2}{10}$

275.7[✓] 274.5[✓] 275.3[✓]
 $\frac{4.8}{10}$ 4.0 $\frac{3.2}{10}$

269.6[✓] 270.4[✓] 271.1[✓]
 $\frac{8.9}{10}$ 8.1 $\frac{7.4}{10}$

$\langle 278.48 \rangle$

Jennings

Dec 16 99 ^{Remm} 76. 7' N of k

2" pipe & Catalina +
& Jennings

9.99 (249.41) B.M. #12

29+67 = Exist M.H. (About 20' deep (see - field check of sewer))

T.P. 3.71 (259.40) 11.22 (255.69) ✓

28+51^E Top of cap at dead end

28+58^E = start pull width pave. (Rods on Pave)

28+10

27+81^{CS} = Δ 0204' RT.
= N.E. cor pave.

27+77 7⁵' Lt. = 36" Cypress

27+50

27+39 1⁵' Lt. = 36" Cypress

27+00

26+99 2' Lt. = 36" Cypress

266.91

63

257.11 ✓
9.80

257.09 ✓
9.82
10

257.06 ✓
9.85

256.81 ✓
10.10
10

257.56 ✓
9.35
10
Pave

257.61 ✓
9.30
10
Pave.

257.5 ✓
9.4
10
Dirt

258.11 ✓
8.80
10
Pave

258.16 ✓
8.75
10
Pave

257.9 ✓
9.0
10
Dirt

260.3 ✓
6.6
10

259.9 ✓
7.0

259.1 ✓
7.8
10

263.4 ✓
3.5
10

263.1 ✓
3.8

261.7 ✓
5.2
10

266.91

Albion St. North of Jennings

2+00

1+50

1+ 41' Mt. = N.W. Cor. House

1+00

0+91 44' Mt. = N.W. Cor. House

0+60

0+36.5

0+00 = Sta. 22+70.89 - Page 49

B.M. #10
P. 61

1.60

265.57

263.97

4

64

256.8 ✓
8.8

258.7 ✓
6.7

258.3 ✓	258.9 ✓
7.3	6.7
41	41
End	Floor level

260.3 ✓
5.3

260.1 ✓	260.5 ✓
5.5	5.1
44	44
End	Floor level

261.6 ✓
4.0

262.8 ✓
2.8

264.3 ✓
1.3

265.57

Albion St

T.P. 0.21 <240.98> 12.81 <240.77>

5+50

5+00

4+50

4+00

3+50

T.P. 0.95 <253.58> 12.94 <252.63>

3+00

2+50

2+20 51' Rht. = N.W. Cor. House

<265.57>

240.4
13.2

242.6 110 100	246.8 6.8 32	244.3 7.3 17	244.6 9.0	244.2 9.4 12	248.6 5.0 18	246.4 7.2 110
---------------------	--------------------	--------------------	--------------	--------------------	--------------------	---------------------

Rim of Canyon

247.3
6.3

249.4
7.2

251.4
2.4

<253.58>

254.5 11.1 100.	255.6 10.0 30	253.1 12.5	251.0 14.6 100
-----------------------	---------------------	---------------	----------------------

255.1
10.5

256.2 9.4 51 Ord.	257.2 8.4 51 Floor Level
----------------------------	--------------------------------------

<265.57>

Albion

± Mon. Albion +
Talbot.

F.R. 1751-PA

11.92	217.26	217.35
		<u>10</u>
		0.09

7+82 = Ctr. exist M.H.

216.88 ✓	221.28 ✓
<u>12.30</u>	<u>7.90</u>
invert	Ritt

7+90 ± ^{Exist} So. side man hole

217.17 ✓
<u>12.01</u>
invert

7+50

221.9 ✓
<u>4.3</u>

T.P. 1.23 <229.18> 13.03 <229.95>

<229.18> ✓

7+00

228.0 ✓
<u>13.0</u>

6+50

231.4 ✓
<u>9.6</u>

6+00

231.8 ✓	236.9 ✓	235.1 ✓	235.7 ✓
<u>9.2</u>	<u>4.1</u>	<u>5.9</u>	<u>5.3</u>
100	30	19	

<240.98>

<240.98>

12/3/49 "B" line (see page 49)

0+52

0+42

0+30

65 Lt. = Rim of Canyon

0+15

0+00 = (page 49 61'-03" W Lt Sta. 21+83.45 on orig. line)

B.M. #9 4.16 <263.68> <259.52> Pg 60
Page 60

Go down to get
to this corner
of here

67

245.6 ✓
18.1
65

243.5 ✓
20.2
30

244.3 ✓
19.4

249.7 ✓
14.0
100

249.7 ✓
14.0
65

246.9 ✓
15.8
30

247.7 ✓
16.0

251.0 ✓
12.7
100

255.6 ✓
8.1
65

253.0 ✓
10.7
30

252.9 ✓
10.8

255.6 ✓
7.9
100

257.0 ✓
6.7
65

257.9 ✓
5.8
30

254.0 ✓
4.7

<263.68>
259.52 ✓
4.16

<263.68>

12-7-48

Catalina Blvd

Sommermeijer
McCoy
Tenes
Gregory

- +57 Intersect Power Cable $\frac{FB 1751}{11}$
- 23+40 Approx Φ Charles
- +12 19' Lt. = Ctr. 3' Diam pepper tree
- +09 13' Lt. = Ctr. 4' Diam. palm.
- 23+00
- 22+89 9' Lt. = Φ 3' wide brick walk
- +80 12' Lt. = Ctr. 4' Diam. palm.
- +60 10' L. = Ctr. \odot box.
- 22+50 13' Lt. = Ctr. 4' Diam. palm.
- 22+19 13' Lt. = Ctr. 4' Diam. palm
- 21+99 10' Lt. = Φ 9' wide brick drive.
- 21+88 14' Lt. = Ctr. 4' diam. palm.
- 21+75 2L $\frac{1751}{10}$ sketch (E.P. = Edge of Pav.)
= Φ Alley between Wilcox + Charles
- B.M. =
21+75 2L
1751 P. 7 6.96 $\left\langle \begin{array}{l} 269.58 \\ 262.62 \end{array} \right\rangle$

 Φ = 2d west of E.
line Catalina 63

$$\begin{array}{r} \checkmark \\ 266.4 \\ \underline{3.2} \\ 20 \end{array} \quad \begin{array}{r} \checkmark \\ 266.0 \\ \underline{3.6} \\ 20 \end{array} \quad \begin{array}{r} \checkmark \\ 265.9 \\ \underline{3.69} \\ 10 \\ E.P. \end{array}$$

$$\begin{array}{r} \checkmark \\ 265.9 \\ \underline{3.7} \\ 20 \end{array} \quad \begin{array}{r} \checkmark \\ 265.3 \\ \underline{4.3} \\ 10 \end{array} \quad \begin{array}{r} \checkmark \\ 264.7 \\ \underline{4.7} \\ 10 \end{array} \quad \begin{array}{r} \checkmark \\ 265.7 \\ \underline{4.36} \\ 10 \\ E.P. \end{array}$$

$$\begin{array}{r} \checkmark \\ 265.9 \\ \underline{3.7} \\ 20 \end{array} \quad \begin{array}{r} \checkmark \\ 265.6 \\ \underline{3.95} \\ 9 \end{array} \quad \begin{array}{r} \checkmark \\ 265.2 \\ \underline{4.35} \\ 9 \end{array}$$

$$\begin{array}{r} \checkmark \\ 265.5 \\ \underline{4.1} \\ 20 \end{array} \quad \begin{array}{r} \checkmark \\ 265.5 \\ \underline{4.1} \\ 15 \end{array} \quad \begin{array}{r} \checkmark \\ 264.3 \\ \underline{5.3} \\ 9 \end{array} \quad \begin{array}{r} \checkmark \\ 263.9 \\ \underline{5.7} \\ 10 \\ E.P. \end{array} \quad \begin{array}{r} \checkmark \\ 264.25 \\ \underline{5.33} \\ 10 \\ E.P. \end{array}$$

$$\begin{array}{r} \checkmark \\ 264.7 \\ \underline{4.9} \\ 20 \end{array} \quad \begin{array}{r} \checkmark \\ 264.5 \\ \underline{5.1} \\ 15 \end{array} \quad \begin{array}{r} \checkmark \\ 263.4 \\ \underline{6.2} \\ 10 \end{array}$$

$$\begin{array}{r} \checkmark \\ 264.1 \\ \underline{5.8} \\ 20 \end{array} \quad \begin{array}{r} \checkmark \\ 263.6 \\ \underline{6.0} \\ 12 \end{array} \quad \begin{array}{r} \checkmark \\ 262.7 \\ \underline{6.7} \\ 9 \end{array} \quad \begin{array}{r} \checkmark \\ 262.7 \\ \underline{5746} \end{array} \quad \begin{array}{r} \checkmark \\ 262.66 \\ \underline{6.92} \\ 10 \\ E.P. \end{array}$$

$$\left\langle \begin{array}{l} 269.58 \\ 262.62 \end{array} \right\rangle$$

Catalina

+50

+46 12' Lt. = Ctr. (W) box

+29 20' Lt. = 3rd wide Hedge.25+15⁸ = 4 Alley so. of Charles

25+05 21' Lt. = End Facad stone wall

25+00

24+74 19' Lt. = Ctr. 1' Diam. Acacia

T.P. 7.61 $\langle 275.67 \rangle$ 1.52 $\langle 268.06 \rangle$

+52 19' Lt. = Ctr. 1' Acacia

24+50

+32 19' Lt. = Ctr. 1' Diam Acacia

+11 20' Lt. = 6" Diam. Acacia.

24+00

+96 15' Lt. = Ctr. 18" acacia.

23+87 = 18" C.I. Culvert. ^{on Lt. only.} 5' Head wall. Conc.

19' Lt. = 8" Acacia tree.

+71 10' Lt. = Fire Hydr.

+67 12' Lt. = Steel street sign. Conc. base

23+66 21' Lt. = start cut stone. stone wall

 $\langle 269.58 \rangle$

69

268.9 [✓]	269.3 [✓]	269.4 [✓]
$\frac{6.8}{20}$	6.4	$\frac{6.25}{10}$
		E.P.

268.6 [✓]	268.5 [✓]	268.87 [✓]
$\frac{7.1}{20}$	7.2	$\frac{6.80}{10}$
		E.P.

268.4 [✓]	268.2 [✓]	268.62 [✓]
$\frac{7.5}{20}$	7.5	$\frac{7.05}{10}$
		E.P.

 $\langle 275.67 \rangle$

267.8 [✓]	266.7 [✓]	267.5 [✓]	267.7 [✓]	267.80 [✓]
$\frac{1.8}{20}$	$\frac{2.9}{11}$	$\frac{2.1}{3}$	1.9	$\frac{1.78}{10}$
				E.P.

267.6 [✓]	267.5 [✓]	265.9 [✓]	267.0 [✓]	267.0 [✓]	266.98 [✓]
$\frac{2.0}{30}$	$\frac{2.1}{17}$	$\frac{3.7}{10}$	$\frac{2.5}{4}$	2.6	$\frac{2.50}{10}$
					E.P.

264.2 [✓]	266.4 [✓]	263.26 [✓]
$\frac{5.35}{42}$	$\frac{9.14}{49}$	$\frac{6.32}{49.5}$
Invert	Top Hd wall	Invert - No head wall.

 $\langle 269.58 \rangle$

27+50 Cont

Catalina

+50

16' Lt. = start faced rock N+S wall.

+17 12^E Lt. = start faced rock wall

+15

+14 } 11^E Lt. = ctr. \odot box.

+13

27+00

+91 = Approx \oplus Dudley = 26' wide E. + W. oil pass.

20' Lt. = end. hedge.

+68 } 12' Lt. = ctr. \odot box.

+57 4' Lt. = steel street sign. Conc. base.

+53 4^E Lt. = ctr. 10" Diam. Eucalyptus

26+50

H. = C.

+45 4^E Lt. = ctr. 8" Diam Eucalyptus+37 4^E Lt. = ctr. 9" Diam Eucalyptus+23 5^E Lt. = ctr. 1" Diam Eucalyptus+08 11^E Lt. = ctr. \odot box

26+02 4' Lt. = ctr. 18" Diam Eucalyptus.

26+00 5^E Lt. = ctr. 16" Eucalyptus+93 12^E Lt. = 1" Diam - 4' high pine.

25+88 6' Lt. = ctr. 30" Diam Eucalyptus.

275.67

276.8[✓]

+1.1

20

276.6[✓]

+0.9

16

top of
wall + end.275.4[✓]

0.3

15

end of
wall \oplus 275.3[✓]

0.4

12

top
wall
+ end.274.4[✓]

1.3

12

end
of
wall274.1[✓]

1.6

6

274.0[✓]

1.7

273.95[✓]

1.72

10

E.R.

273.4[✓]

2.3

20

on oil pass.

272.1[✓]

3.6

8

272.2[✓]

3.5

272.4[✓]

3.21

10

E.R. on Catalina

273.4[✓]

2.5

20

272.0[✓]

3.7

8

272.1[✓]

3.6

272.24[✓]

3.43

10

E.R.

272.7[✓]

3.0

20

271.6[✓]

4.1

15

271.4[✓]

4.5

271.29[✓]

4.38

10

E.R.

270.5[✓]

5.2

20

270.5[✓]

5.2

270.34[✓]

5.35

10

E.R.

275.67[✓]

70

28+65 2' Lt. = 6" Diam Acacia

28+55 Cont

14' Lt. = End loose rock wall.

28+55 12' Lt. = End loose rock wall.

14' Lt. = top of steps

28+25 12' Lt. = 3' wide rock + conc. steps

14' Lt. = start N.Y.S. loose rock wall

+05 } 12' Lt. = also = start N.Y.S. loose rock wall
12' Lt. = End N.Y.S. Rock + conc. wall

+03 15' Lt. = Ctr. 3' Diam palm.

Face E.W. rock + conc. wall

28+01 12' Lt. = start N.Y.S. rock + conc. wall

15' Lt. = End faced rock N.Y.S. wall

27+90 } 11' Lt. = End faced rock N.Y.S. wall

T.P. 10.36 $\left\langle \begin{array}{l} 285.74 \\ 275.67 \end{array} \right\rangle$ 0.29 $\left\langle \begin{array}{l} 275.38 \\ 275.67 \end{array} \right\rangle$

✓	✓
280.2	279.7
5.5	6.0
20	14.4
	Top of wall
	+ End

✓	✓	✓	✓	✓
279.2	279.4	278.1	277.7	277.8
6.5	6.5	7.6	8.0	7.94
14.4	12	12		10
End	Top of wall	End		E.P.
	+ End			

✓	✓
279.1	277.8
6.6	7.9
11.5	12
Top of top step	Top of bottom step

✓	✓	✓	✓	✓	✓
278.1	277.5	277.5	276.4	275.7	275.8
7.0	8.2	8.2	9.3	10.0	9.92
14.5	14.5	12	12	10	10
Top wall + End	End	Top wall + End	End		E.P.

✓	✓	✓	✓	✓	✓
279.0	277.7	278.6	276.6	275.6	275.67
6.7	8.0	7.1	9.1	10.1	10.02
20	20	12.5	12		10
Top wall + End	End	Top wall + End	End		E.P.
of wall	of wall	of wall			

✓	✓	✓	✓	✓	✓
278.2	278.0	276.9	276.8	275.8	275.27
7.3	7.7	8.8	8.9	9.9	10.17
20	15.5	15.5	11.2	11.4	10
Top wall + End			Top wall + End		E.P.

 $\left\langle 285.74 \right\rangle$

29+39 7' Lt. = End Conc. Dr.

29+23 Cont.

29+23 10' Lt. = End Conc. wall.
7' Lt. = Start conc. drive

27+11 9' Lt. = Ctr. (W) box.

28+94 11' Lt. = Δ in wall.

28+90 17' Lt. = start. 8" wide Conc. wall.

28+78 11' Lt. = 12" Diam. Acacia

T.P. 11.51 $\left\langle 293.71 \right\rangle$ 3.54 $\left\langle 282.20 \right\rangle$ 28+65⁸ = Alley $\frac{FB 1751}{11}$ $\left\langle 285.74 \right\rangle$

282.90	281.84
<u>10.81</u>	<u>11.87</u>
20	7'

282.90	281.9
<u>10.81</u>	<u>11.8</u>
20	11
Cont	Cont
+0.100	

282.7	281.8	281.62	280.6	280.78
<u>11.5</u>	<u>11.9</u>	<u>12.09</u>	13.1	<u>12.93</u>
10	10	7.3		10
top of wall	Cont	Drive + Cont.		E.P.

283.0	282.5	282.06	281.6	280.1
<u>10.7</u>	<u>11.2</u>	<u>11.65</u>	<u>12.1</u>	13.6
20	12.5	11.5	11.5	
	Cont	top of wall	Cont	

282.6	282.26	282.1	279.3	279.31
<u>11.1</u>	<u>11.45</u>	<u>11.6</u>	14.4	<u>14.40</u>
20	17	17		10
	top of wall	Cont		E.P.

 $\left\langle 293.71 \right\rangle$

280.6	280	278.4	278.0	278.26
<u>5.1</u>	<u>5.3</u>	<u>2.5</u>	7.7	<u>2.48</u>
20	15	8		10
				E.P.

 $\left\langle 285.74 \right\rangle$

Catalina

(For culvert see $\frac{1757}{8}$)

- +91 18' Lt. = 1' diam. Eucalyptus
 +90 19' Lt. = 1' diam. Eucalyptus.
 +89 17' Lt. = 1' Diam. Eucalyptus
 30487 7² Lt. = steel street sign, Conc. base

strip of oil & Rock pave. Not much ^{good.}
 30442 = Approx. Warner = ϕ of 40'

30400 12' Lt. = Ctr. 16" diam. Acacia

29+92 21' Lt. = Ctr. 6"

+74 20' Lt. = Ctr. 8"

+72 18' Lt. = Ctr. 6"

+68 18' Lt. = Ctr. 18"

+65 15' Lt. = Ctr. 6"

+64 18' Lt. = Ctr. 3"

+62 17⁵ Lt. = Ctr. 6"

+58 21' Lt. = Ctr. 4"

+56 4⁸ Lt. = Ctr. 14"+53 18' Lt. = ^{ctr.} "A"

Eucalyptus

29+50

 $\sqrt{293.71}$ ϕ

73

$$\begin{array}{r} 288.7 \\ 5.0 \\ \hline 20 \end{array} \quad \begin{array}{r} 288.1 \\ 5.6 \\ \hline 10 \end{array} \quad \begin{array}{r} 287.8 \\ 5.9 \\ \hline 10 \end{array} \quad \begin{array}{r} 288.3 \\ 5.38 \\ \hline 10 \\ \text{E.P.} \end{array}$$

$$\begin{array}{r} 285.7 \\ 8.0 \\ \hline 20 \end{array} \quad \begin{array}{r} 286.0 \\ 7.7 \\ \hline 10 \\ \text{E.P. on Catline} \end{array} \quad \begin{array}{r} 286.16 \\ 7.55 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 283.7 \\ 10.0 \\ \hline 20 \end{array} \quad \begin{array}{r} 283.4 \\ 10.3 \\ \hline 11 \end{array} \quad \begin{array}{r} 282.7 \\ 11.0 \\ \hline 9 \end{array} \quad \begin{array}{r} 283.6 \\ 10.1 \\ \hline 10 \end{array} \quad \begin{array}{r} 284.25 \\ 9.46 \\ \hline 10 \\ \text{E.P.} \end{array}$$

$$\begin{array}{r} 282.9 \\ 10.8 \\ \hline 20 \end{array} \quad \begin{array}{r} 282.5 \\ 11.2 \\ \hline 12 \end{array} \quad \begin{array}{r} 281.6 \\ 12.1 \\ \hline 10 \end{array} \quad \begin{array}{r} 281.3 \\ 12.4 \\ \hline 4 \end{array} \quad \begin{array}{r} 281.7 \\ 12.0 \\ \hline 10 \end{array} \quad \begin{array}{r} 282.0 \\ 11.70 \\ \hline 10 \\ \text{E.P.} \end{array}$$

 $\sqrt{293.71}$

Catalina
32+26 12" Lt. = 6" wide E. + W. Conc. block walls

32+158 Alloy $\left(\frac{1751}{8}\right)$

+05^E 17' Lt. = End 2' wide N. + S. Conc. walk
(Level with ground.)

32+00

+91 17" Lt. = W. edge N. + S. walk 2' wide

+81 20' Lt. = w. edge N. + S. Conc. walk 2' wide

31+79 19' Lt. = Ctr. 42" Diam. Eucalyptus

31+50

+36 16" Lt. = 6" wide conc. block E. + W. wall

+33 4' Lt. = Ctr. 3" Diam. Eucalyptus

+23 13' Lt. = Ctr. bot.

+19 16' Lt. = Ctr. 30" Diam. Eucalyptus

31+10-13" Lt. = 3' wide Conc. walk

31+00

$\left\langle \frac{293.71}{8} \right\rangle$

£

74

$$\begin{array}{r} 293.7 \checkmark \\ 0.0 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 293.0 \checkmark \\ 0.7 \\ \hline 10 \end{array}$$

$$\begin{array}{r} 292.5 \checkmark \\ 1.2 \\ \hline \end{array}$$

$$\begin{array}{r} 292.86 \checkmark \\ 0.85 \\ \hline 10 \\ \text{E.P.} \end{array}$$

$$\begin{array}{r} 292.97 \checkmark \\ 0.74 \\ \hline 20 = \text{E.P.} \\ \left(\frac{1751}{8} = 293.875\right) \end{array}$$

$$\begin{array}{r} 293.6 \checkmark \\ 0.1 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 294.1 \checkmark \\ 0.4 \\ \hline 14 \end{array}$$

$$\begin{array}{r} 291.4 \checkmark \\ 2.3 \\ \hline 7 \end{array}$$

$$\begin{array}{r} 292.2 \checkmark \\ 1.5 \\ \hline \end{array}$$

$$\begin{array}{r} 293.56 \checkmark \\ 0.35 \\ \hline 10 \\ \text{E.P.} \end{array}$$

$$\begin{array}{r} 291.5 \checkmark \\ 2.2 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 291.4 \checkmark \\ 2.3 \\ \hline 16 \end{array}$$

$$\begin{array}{r} 289.2 \checkmark \\ 4.5 \\ \hline 8 \end{array}$$

$$\begin{array}{r} 290.2 \checkmark \\ 3.5 \\ \hline \end{array}$$

$$\begin{array}{r} 290.66 \checkmark \\ 3.05 \\ \hline 10 \\ \text{E.P.} \end{array}$$

$$\begin{array}{r} 292.8 \checkmark \\ 0.7 \\ \hline 16 \text{ Top of wall} \end{array}$$

$$\begin{array}{r} 290.9 \checkmark \\ 2.8 \\ \hline 16 \text{ Base of wall} \end{array}$$

$$\begin{array}{r} 289.37 \checkmark \\ 4.34 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 289.20 \checkmark \\ 4.51 \\ \hline 13 \end{array}$$

~~4.51~~

$$\begin{array}{r} 289.1 \checkmark \\ 4.6 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 288.6 \checkmark \\ 5.1 \\ \hline 13 \end{array}$$

$$\begin{array}{r} 287.1 \checkmark \\ 6.6 \\ \hline 9 \end{array}$$

$$\begin{array}{r} 287.2 \checkmark \\ 6.5 \\ \hline 5 \end{array}$$

$$\begin{array}{r} 288.3 \checkmark \\ 5.4 \\ \hline 3 \end{array}$$

$$\begin{array}{r} 288.5 \checkmark \\ 5.2 \\ \hline \end{array}$$

$$\begin{array}{r} 288.73 \checkmark \\ 4.98 \\ \hline 10 \\ \text{E.P.} \end{array}$$

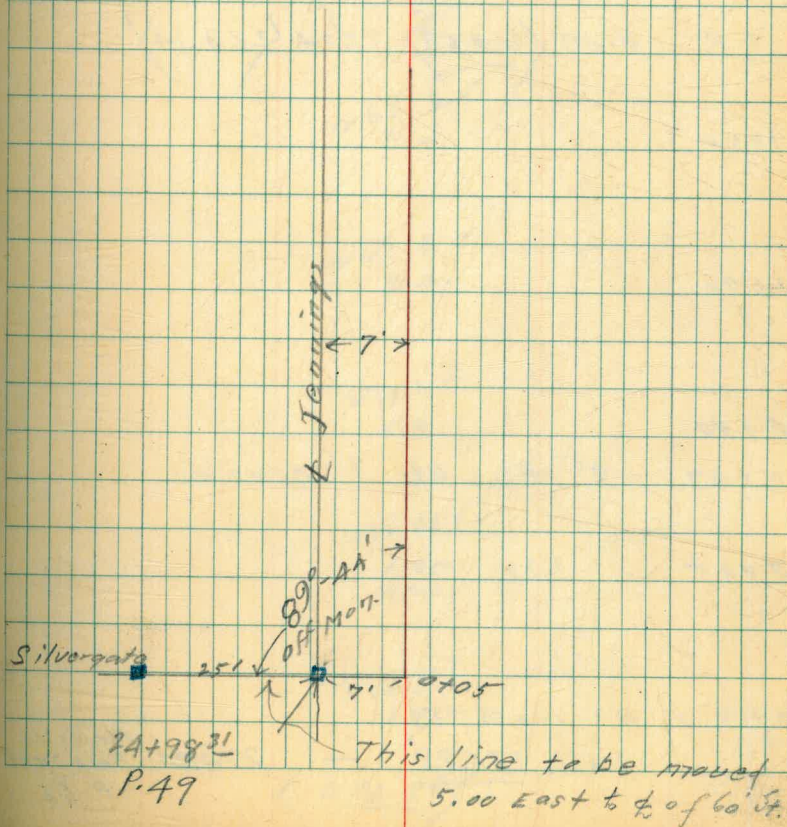
$\left\langle \frac{293.71}{8} \right\rangle$

Line 7 No. of Jennings
Silvergate west to Exist Sewer

Sammermeyer
McCoy
Jenos

⊕

75



24+98.31
P.49

Jennings

2+82 1A' Lt. = Ctr. 3' Cypress

2+50

2+46 9' Lt. = Ctr. 3' Cypress

2+06 9^E Lt. = Ctr. 3' Cypress

2+00

T.P. 0.49 $\left\langle \frac{264.63}{} \right\rangle$ 12.74 $\left\langle \frac{264.14}{} \right\rangle$

1+50

1+00

0+50

0+49 9' Rt. = Ctr. 1' Acacia

0+05 P.75

0+00 = Δ (See P. 75)

2.67 276.88

— 274.21

Nails in
Pole 3601
P 62

4

76

259.6 ✓

5.0

262.4 ✓

2.2

$\left\langle \frac{264.63}{} \right\rangle$ ✓

265.5 ✓
11.4

267.5 ✓
9.4

270.1 ✓
6.8

275.43 ✓
1.45
546

275.6 ✓
1.3

$\left\langle \frac{276.88}{} \right\rangle$ ✓

3+59 6⁹ Lt. = ctr. dead end cap

256.97
7.66

3+58 start full width pave.

256.90
7.75

3+00

see p. 19
for paving

257.8
6.8

2+89 7' Lt. = edge para

258.18
6.45

276.88
264.63

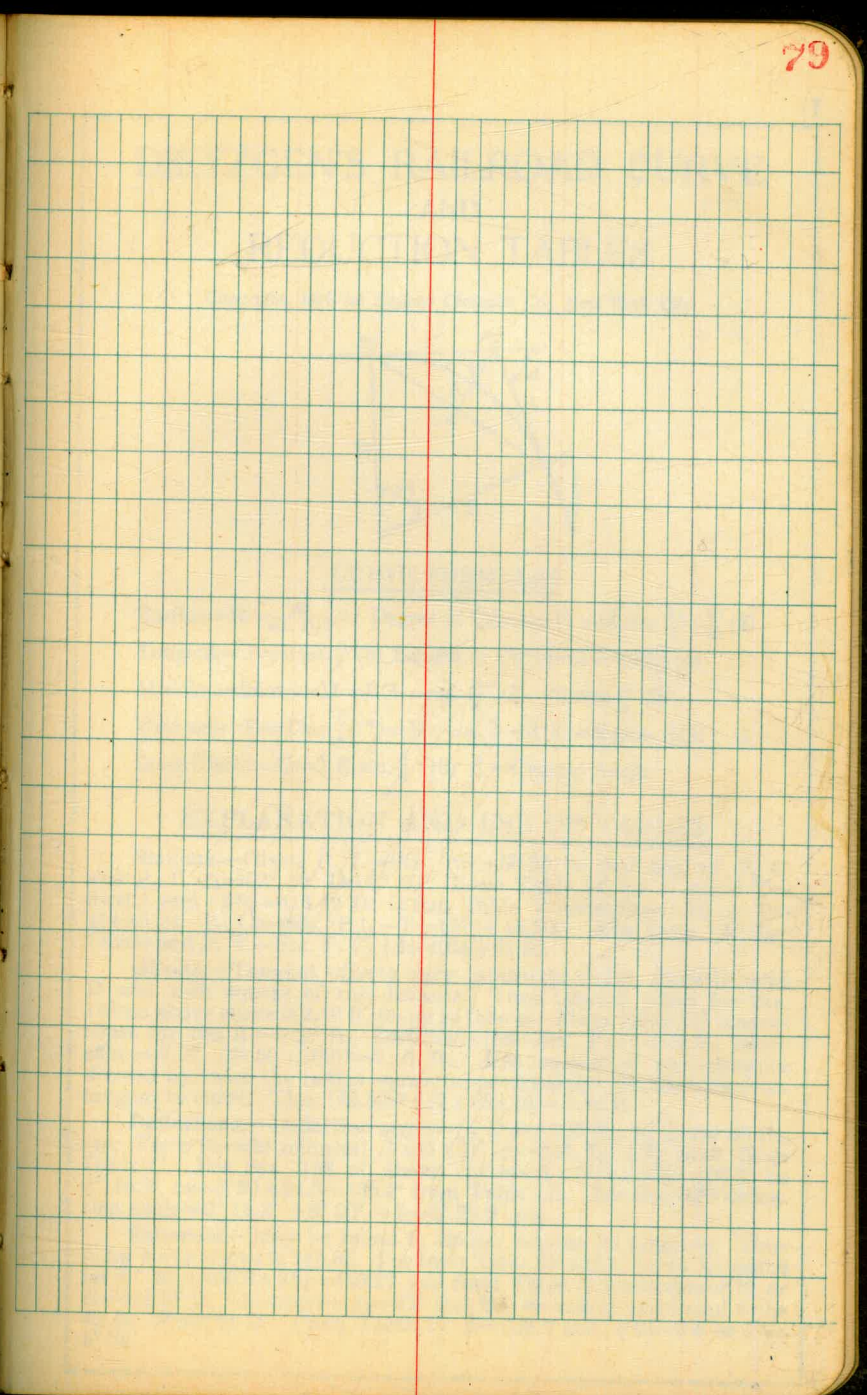
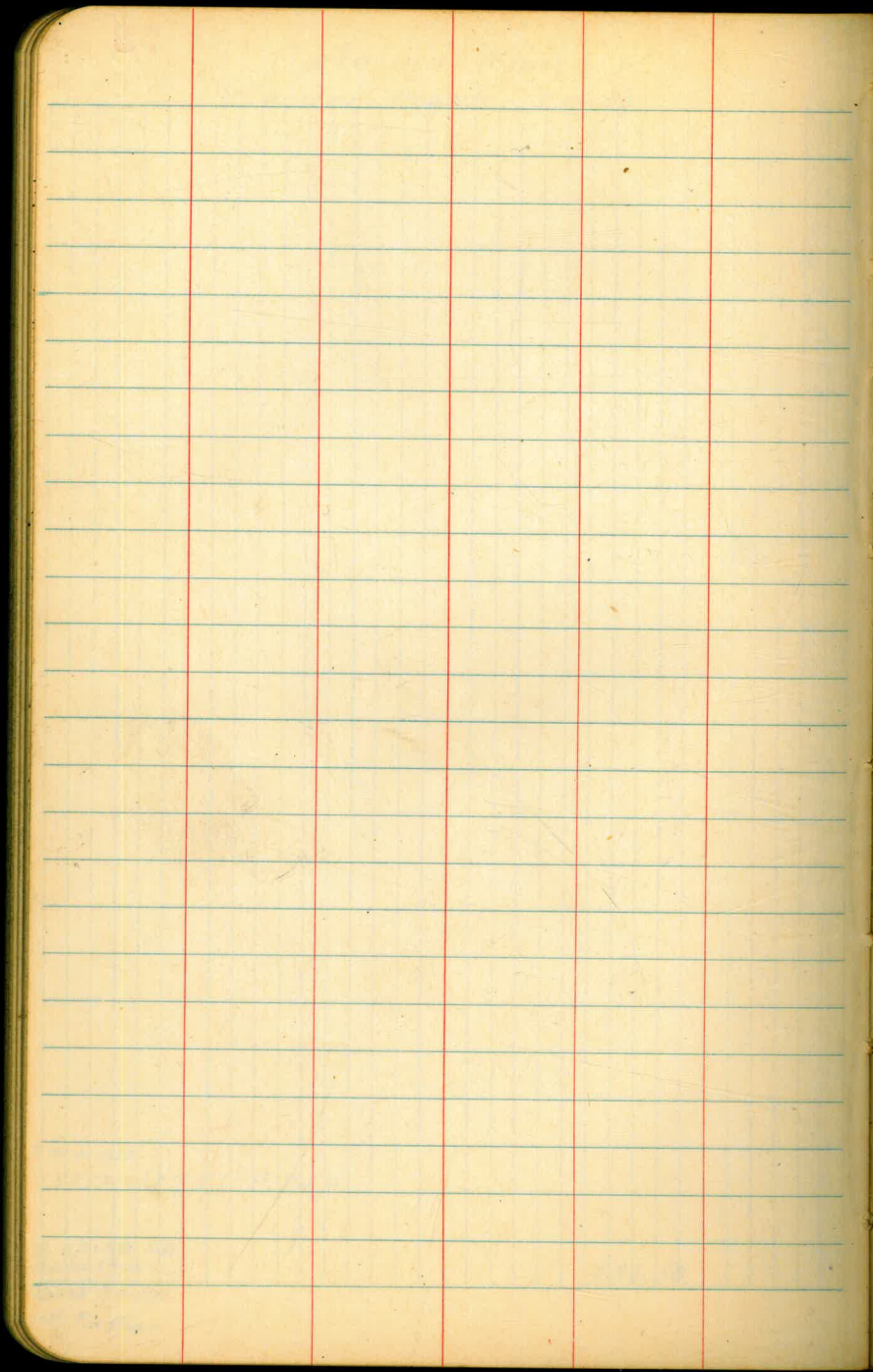
Catalina Blvd
Warner tract - South.

78

20+00
18+52 (1751-P.74)=

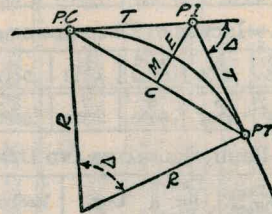
Spike on
Catalina
600' South
of Hooper

306.50



DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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CURVE FORMULAS

- Radius= $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve= D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)
 Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)
 Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2}) = R \text{vers} \frac{\Delta}{2}$ (5) (6)
 External= $E = T \tan \frac{\Delta}{4} = R \div \cos \frac{\Delta}{2} - R$ (7) (8) = $R \text{exsec} \frac{\Delta}{2}$ (9)
 Long Chord= $C = 2 R \sin \frac{\Delta}{2}$ (10) Δ = Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I. = Sta. 161 + 60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{3} = 414.49$ ft. From Table V correction = .36 or $T = 414.85$ ft. P. C. = Sta. P. I. - $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T. = Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = $158 - \text{Sta. P. C.} = 54.50$, hence offset = $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^\circ$ or = defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8\frac{1}{3} = 136.2'$ or $2^\circ 16.2'$, or = $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 115.27$ and from Table V correction = .10 or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

lateral West of Valeta

Ground - 1.0 below ground

$\frac{1}{2}$ to alley 5 higher than floor

398.77

5+02.5

5+05.5

5+20

728.84
398.77
330.07

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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