EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

1700

CITY ENGINEER'S OFFICE

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

Univ. Heights Blk 54 X-Sect. Pg 67

" 70 " Pg 62

" 105 " { 57
{ 71

Walker
Hardin
Hunley
12-7-45

CROSS SECTION - BAKER ST.

from Morena Blvd. 5'cbs. 7.5 1/4's.
To East end

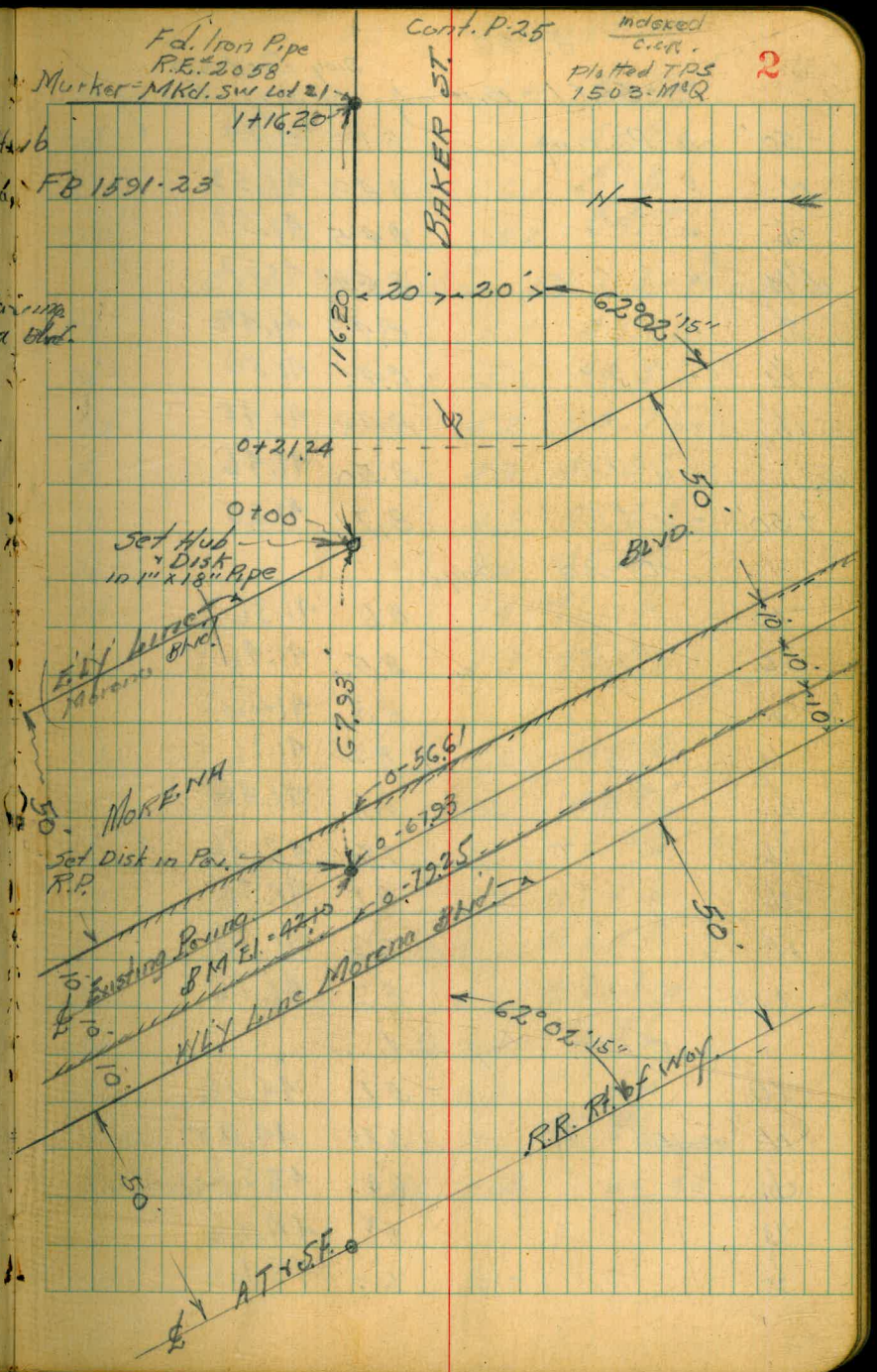
		68.75		67.30	BM NW 7" Hub & Princeton & Ticonderoga
	1.45	~~69.96~~ 57.58		~~67.64~~ 56.00	
T.P. #1	1.58	~~57.89~~	12.75	~~56.31~~	
T.P. #2	4.40	49.96	12.02	45.56	on Disk in Paving N.L. Baker & Paving Morena Blvd.
Set BM.			-8.17	41.79	

0 - 79.25 - diag. Sections

50' N	on Paving		8.23	41.73
N	"	"	8.38	41.58
C.	"	"	8.38	41.58
1/4	"	"	8.38	41.58
L.	"	"	8.36	41.60
1/4	"	"	8.41	41.55
C.	"	"	8.46	41.50
SL.	"	"	8.46	41.50
+50'	"	"	8.67	41.29

0 - 67.93 - L. Existing for diag. Sec.

-50	on Paving.		8.51	41.45
S	"	"	8.33	41.63
C.	"	"	8.31	41.65
1/4	"	"	8.26	41.70
L.	"	"	8.24	41.72
1/4	"	"	8.20	41.76
C.	"	"	8.19	41.77
N	"	"	8.17	41.79
+50'	"	"	8.04	41.92



4996

Diag. Section

0-56.61 = East edge Existing Paving

-50'	on Paving	8.22 41.74
N	" "	8.43 41.53
cb.	" "	8.45 41.51
N 1/4	" "	8.44 41.52
℄	" "	8.47 41.49
S 1/4	" "	8.46 41.50
S cb.	" "	8.48 41.48
SL.	" "	8.50 41.46
+50'	" "	8.71 41.25

0-20 diag.

-10		8.6 41.36
SL.		8.5 41.46
cb.		8.3 41.66
1/4		8.2 41.76
℄		8.1 41.86
1/4		7.6 42.36
cb		8.2 41.76
N		8.2 41.76
+10		8.2 41.76

0+00 diag. Section

-10		5.7 44.26
N ~~on Hub~~		5.88 44.08
cb.		6.4 43.56
1/4		5.8 44.16
℄		6.3 43.66

4996 BAKER St. 3

S 1/4		6.4 43.56
S cb.		6.1 43.86
SL.		6.1 43.86
+10'		5.2 44.76

0+21.24 Section Rt ∠ to S.E. Cor. Prop. Line

SL.		6.1 43.86
cb.		5.6 44.36
1/4		5.2 44.76
℄		4.9 45.06
1/4		4.3 45.66
cb.		4.4 45.56
N		3.8 46.16
+10'		4.3 45.66

0+50

-10'		1.5 48.46
N		1.2 48.76
cb		1.6 48.36
1/4		1.7 48.26
℄		2.1 47.86
1/4		2.6 47.36
cb.		2.4 47.56
SL.		2.7 47.26
+10'		3.0 46.96
T.P.#3	12.29	61.56 0.64 49.32

1+00

-10'		10.0

SL.	9.4	52.16
cb.	9.4	52.16
1/4	8.6	52.96
℄	8.0	53.56
1/4	8.2	53.36
cb.	8.3	53.26
N	8.1	53.46
+10'	8.1	53.46
1+16 = Elec. Pole 4.2 South of N Line		
1+30		
-10'	4.4	57.16
N	5.7	55.86
cb.	6.0	55.56
1/4	5.1	56.16
℄	4.9	56.66
1/4	5.4	56.16
cb.	5.6	55.96
SL.	6.1	55.46
+10	6.3	55.26
1+50		
-10	3.0	58.56
SL	4.0	57.56
cb.	3.4	58.16
1/4	2.9	58.66
℄	2.5	59.06
1/4	2.6	58.96

cb.	2.9	58.66
N	3.8	57.76
+10'	3.2	58.36
TP #1 1279	67.27 7.08	59.98 on P.P.O SW Cor Lot 21 West end = 5' in at
1+60 = West edge Asphalt Drive on N.		
-10	6.1	61.17
N on Drive	6.24	61.03
+5 = cb on Drive	6.54	66.73
1/4	7.0	60.27
℄	7.2	60.07
1/4	7.5	59.77
cb.	8.1	59.17
S	8.7	58.57
+2	9.1	58.17
+6 — "	7.2	60.07
+10	7.0	60.27
1+75 = E edge Above Drive		
-10	3.9	63.37
-8	4.0	63.27
-5	6.6	60.67
S	7.2	60.07
cb.	6.8	60.47
1/4	5.9	61.37
℄	5.6	61.67
1/4	5.3	61.97
cb	4.9	62.37
N on Drive	4.55	62.72
+10 " "	4.05	63.22

67.27 Baker St.

2+00

-20'			1.5	65.77
-10'			1.8	65.47
N			2.4	64.87
cb.			2.5	64.77
1/4			2.8	64.47
℄			4.0	63.27
1/4			1.3	65.97
cb.			1.6	65.67
S			2.4	64.87
+6			+1.0	68.27
+10			+1.2	68.47
+20			+0.4	67.67
T.P.#5	1218	78.54	0.91	66.36

2+33

-20'			7.6	70.94
-10'			6.8	71.74
-5			6.5	72.04
S			8.4	70.14
cb.			8.3	70.24
1/4			7.8	70.74
℄			8.6	69.94
1/4			9.6	68.94
cb.			10.7	67.84
N			12.0	66.54
+10			11.7	66.84
+20			11.0	67.54

78.54

2+50

-20'			8.8	68.74
-10'			7.5	71.04
N			6.6	71.94
cb.			6.3	72.24
1/4			5.2	73.34
℄			5.0	73.54
1/4			4.9	73.64
cb.			5.9	72.64
S			4.0	74.54
+10			4.7	73.84
+20			5.5	73.04

2+75

-20			2.2	76.34
-10'			1.4	77.14
S			0.8	77.74
cb			2.0	76.54
1/4			2.3	76.24
℄			1.1	77.44
1/4			1.3	77.24
cb.			0.8	77.74
N			1.1	77.44
+10			2.0	76.54
+20			4.2	74.34
+25			2.4	76.14
T.P.#6	12.01	90.35	0.20	78.34

90.85 Baker ct

	3+00		
-20'		11.9	78.45
-10'		9.7	80.65
N		9.7	80.65
cb.		9.7	80.65
1/4		10.2	80.15
℄		11.0	79.35
1/4		10.4	79.95
cb.		10.3	80.05
S		10.5	79.85
+10'		11.2	79.15
+20'		11.8	78.85
	3+50		
-20'		5.0	85.35
-10'		4.9	85.45
S		4.8	85.55
cb.		4.8	85.55
1/4		5.1	85.25
℄		4.7	85.65
1/4		4.4	85.95
cb.		4.5	85.85
N		4.5	85.85
+10		4.3	86.05
+20		4.1	86.25
T.P. #7	12.87 101.82	1.40	88.95
	4+00		
-20'		8.8	93.02
-10'		8.7	93.12

101.82

N		8.8	93.02
cb.		8.7	93.12
1/4		9.1	92.72
℄		9.4	92.42
+12		9.6	92.22
+13	ditch	12.0	89.82
+17	"	12.0	89.82
1/4		9.0	92.82
cb.		8.8	93.02
S		8.8	93.02
+10		9.0	92.82
+20'		8.8	93.02
	4+50		
-20'		2.2	99.62
-10		1.9	99.92
S		1.5	100.32
cb.		1.5	100.32
1/4		1.5	100.32
+4		2.1	99.72
℄ in Ditch		4.5	97.32
+4		1.8	100.02
1/4		1.3	100.52
cb.		1.2	100.62
N		1.4	100.42
+10'		1.5	100.32
+20'		1.3	100.52

101.82 BAKER St.

T.P.8	12.60	113.94	0.98	101.34
		5+00		
-20'			6.1	107.84
-10'			6.1	107.84
N			6.1	107.84
cb.			6.1	107.84
1/4			6.3	107.64
+5	in ditch		10.6	103.34
℄			7.3	106.64
+3			6.7	107.24
1/4			7.0	106.94
cb.			7.2	106.74
S			7.3	106.64
+10			7.9	106.04
+20'			8.3	105.64
		5+50		
-20			2.3	111.64
-10'			1.9	112.04
S			1.6	112.34
cb.			1.2	112.74
1/4			0.8	113.14
℄			0.6	113.34
1/4			1.0	113.94
+2	in Ditch		1.3	112.64
cb.			0.8	113.14
N			1.4	112.54
+10			0.1	113.84
+20			+ 0.1	114.04

113.94

7

T.P.9	12.56	125.72	0.78	113.16
		6+00		
-20'			5.2	120.52
-10'			5.4	120.32
N			5.4	120.32
cb			5.5	120.22
+4			6.3	119.42
1/4			8.2	117.52
+2			8.2	117.52
+4			6.1	119.62
℄			6.0	119.72
1/4			6.3	119.42
cb.			6.6	119.12
S			6.8	118.92
+10'			7.1	118.62
+20'			7.3	118.42
		6+34		
-20'			3.1	122.62
-10'			2.6	123.12
S			2.0	123.72
cb			2.0	123.72
1/4			1.7	124.02
℄			1.6	124.12
+3			1.5	124.22
+5			4.0	121.72
1/4			4.4	121.32

		125.72	BAKER ST.	
cb.			4.4	121.32
N			3.6	122.12
+2			3.3	122.42
+4			1.1	124.62
+10'			1.1	124.62
+20'			0.4	125.32
T.P.#10	12.33	137.54	0.51	125.21
	6+50			
-20'			10.1	127.44
-10'			10.4	127.19
N			10.5	127.09
cb.			10.5	127.09
1/4			11.0	126.54
℄			10.7	126.84
1/4			10.8	126.74
cb.			11.1	126.44
S			11.3	126.24
+10'			11.9	125.74
+20'			12.6	124.94
	7+00			
-20'			4.9	132.64
-10'			4.5	133.04
S			4.2	133.34
cb.			4.2	133.34
1/4			4.1	133.44
℄			4.1	133.44
1/4			4.0	133.54

		137.54		
cb.			4.1	133.44
N			3.8	133.74
+10'			3.7	133.84
+20'			3.1	134.34
	7+25			
T.P.#11	11.85	148.15	12.4	136.30
-20'			10.8	137.35
-10'			10.7	137.45
N			10.6	137.55
cb.			10.5	137.65
1/4			10.7	137.45
℄			10.7	137.45
1/4			11.0	137.15
cb.			11.3	136.85
S			11.4	136.75
+10			11.5	136.65
+20			11.6	136.55
	7+50			
-20'			8.3	139.85
-10'			7.7	140.45
S			7.9	140.25
cb.			8.0	140.15
1/4			8.0	140.15
℄			8.0	140.15
1/4			8.2	139.95
cb.			7.9	140.25
N			7.9	140.25
+10			7.8	140.35
+20			7.7	140.45

SE. Cor Lot #1	148.15	BAKER JT		7+73.00
Set BM on Pipe		5.53	142.62	
	8+00			
-20'		2.6	145.55	
-10'		2.7	145.45	
N		2.7	145.45	
cb.		2.7	145.45	
¼		2.7	145.45	
℄		2.6	145.55	
¼		2.8	145.35	
cb.		3.0	145.15	
S		3.0	145.15	
+10'		3.1	145.05	
+20'		3.2	144.95	
T.P. #12	10.45	157.90	0.70	147.45
	8+50			
-20'		8.0	149.90	
-10'		7.6	150.30	
S		7.0	150.90	
cb.		6.7	151.20	
¼		6.1	151.80	
℄		6.3	151.60	
¼		6.8	151.10	
cb.		6.7	151.20	
N		6.7	151.20	
+10'		6.9	151.00	
+20'		6.5	151.40	

157.90

9

	9+00			
-20'			+0.2	158.1
-10'			0.1	157.8
N			+0.1	158.00
cb.			0.0	157.9
¼			0.4	157.5
℄			0.8	157.1
¼			1.0	156.9
cb.			1.3	156.6
S			1.6	156.3
+10'			2.6	155.3
+20'			3.5	154.4
T.P. #13	0.56	157.86	0.60	157.30
T.P. #14	6.95	151.97	12.84	145.02
T.P. #15	0.95	143.46	9.46	142.51
T.P. #16		N.W.L. on Hwy Trenton	Ticonderoga	6.93 137.03
T.P. #16	0.67	131.29	12.84	130.62
T.P. #17	0.73	119.05	12.97	118.32
T.P. #18	0.45	107.66	11.84	107.21
T.P. #19	0.49	95.23	12.92	94.74
T.P. #20	1.25	84.04	12.44	82.79
T.P. #21	1.98	76.90	9.12	74.92
Chk Sterling B.M.			9.56	67.34
				67.30 - Sterling B.M.
				0.04

On large sharp Rock 1'N of St. 9+09

Check Levels Cont. P-10

BAKER ST.

				B.M. B.P.
	11.32	46.27		34.95 & Culvert (on W side) Culvert #E-261 FB 563 P 63 P-74
Page 2				
T.P. Chk T.P. #2	5.17	50.73	0.71	45.56
T.P. #22	10.14	60.64	0.23	50.50
Chk B.M. Nail in Pole			0.89	59.75
				59.72
				0.03

Note. Fd. Sturdivy B.M. 67.61 P-2 off 0.31
Should be as now shown P-2 = 67.30

SE Bunker Hill & Morena Blvd. FB 563-74 FB 1591-31

181.79 π Cont. from Lt. Page

B.M. on T.P. #13 P-9	12.01	169.31		157.30
T.P. #23	13.27	181.79	0.79	168.52
	9+50			
-20			23.4	158.39
SL.			20.0	161.79
℄			18.3	163.49
N			17.4	164.39
+20			16.6	165.19
	10+00			
-20			10.8	170.99
N			12.1	169.69
+10			13.2	168.59
℄			14.8	166.99
SL.			18.7	163.09
+25			25.4	156.39

10+35		
-40	32.6	149.19
-20	27.9	153.89
SL.	22.3	159.49
℄	16.8	164.99
NL.	12.3	169.49
+20	8.3	173.49
+30	7.0	174.79
10+65		
-30	4.5	177.29
-20	6.1	175.69
N	8.7	173.09
+8	10.5	171.29
℄	14.1	167.69
S	21.1	160.69
+20	28.7	153.49
+40	34.1	147.69
11+00		
-50	36.1	145.69
+40	33.6	148.19
-20	27.7	154.09

BAKER ST.

	181.79		
SL.		22.7	159.09
E		15.6	166.19
NL.		8.2	173.59
+6		5.5	176.29
+20		2.6	179.19
+30		1.1	180.69
	11+30		
-30		+2.5	184.29
-20		+0.5	182.29
N		3.8	177.99
E		11.9	169.89
SL.		20.5	161.29
+20'		26.6	155.19
+50'		31.1	150.69
	11+50		
-50		28.9	
-25		25.5	152.89
SL.-7'		21.1	160.69
SL.		18.6	163.19
E		9.6	172.19
+10		4.1	177.69
NL.		1.8	179.99
+20'		+2.4	184.19
+30'		+4.3	186.09
T.P.#24	12.85	19367	0.97 180.82

19367

11

	11+86		
-30		4.7	188.97
-15		8.1	185.57
NL.		12.1	181.57
+10		14.5	179.17
E		18.7	174.97
SL.		25.1	168.57
+36		36.8	156.87
+44		37.8	156.67
T.P.#25	11.26	195.70	9.23 184.44
+60		32.6	163.10
	12+12		
-46'		35.0	160.70
-39'		36.4	159.30
-35'		36.8	158.90
28'		35.2	160.50
SL.		27.7	168.00
E		20.2	175.50
+7		16.6	179.10
NL.		13.1	182.60
+20		7.6	188.10
+35		4.1	191.60
	12+50		
-35'		3.5	192.20
-20'		6.5	189.20
NL.		12.4	183.30
+12		15.1	180.60

Baker St.

	12+50	19.70	
℄		19.2	176.50
S.L.		25.9	169.80
+20		30.8	164.90
+27		31.6	164.10
+33		30.8	164.90
+45		25.6	170.10
	12+75		
-47		19.0	176.70
-30		24.4	171.30
-22'		28.1	167.60
-17'		29.5	166.20
-9'		27.3	163.40
S.L.		23.2	172.50
℄		19.2	176.50
+15		14.3	181.40
N		13.0	182.70
+15		8.8	186.90
+35		3.4	192.30
	13+00		
-40'		6.7	189.00
-20		10.9	184.80
N.L.		16.8	178.90
℄		22.6	173.10
S.L.		26.6	169.10
+13'		29.0	166.70
+31'		23.6	172.10
+45		18.1	177.6

195.70

	13+12		
-56'		9.9	185.80
31'		19.9	175.80
18'		23.1	172.60
S.L.		28.6	167.10
℄		27.2	168.50
+3		27.0	168.70
N.L.		22.8	172.90
+20		14.0	181.70
+40		8.2	187.50
	13+36		
-81'		6.4	189.3
-61'		13.0	182.7
-45		14.5	181.20
-28'		18.4	177.3
N.L.		20.9	174.8
℄		19.8	175.9
S.L.		18.5	177.20
+30		11.1	184.60
+50		8.2	187.50
+60		3.7	192.00
T.P. 26	13.07	208.09	0.68 195.02
	13+75		
-40		5.2	202.89
-20'		9.0	199.09
S.L.			

	13+75	208.09	Baker St.	
℄			14.5	193.59
N			16.6	191.49
+13			18.0	190.09
+33			24.1	183.99
+62			26.0	182.09
+77			26.0	182.09
	14+00			
-65			16.8	191.29
-32			13.8	194.29
-13			10.1	198.00
NL.			8.0	200.09
℄			2.3	205.79
SL.			1.0	207.09
+25			+1.2	209.29
+40			+2.3	210.39
TP#27	12.40	220.01	0.48	207.61
	14+33.5			
-40			0.3	219.71
-20			1.0	219.01
SL-0.4	on 1" Iron Pipe		1.69	218.32
℄			2.8	217.21
NL.			7.2	212.81
+30			11.5	208.51
+60			12.1	207.91
TP#28	12.77	232.67	0.11	219.90

	14+50	232.67	
-40		18.2	214.47
-20		16.5	216.17
N		14.9	217.77
℄		12.6	220.07
SL.		10.1	222.57
+30		9.4	223.27
40		7.7	224.97
	14+80		
-40		4.8	227.87
-10		4.3	228.37
SL.		5.4	227.27
℄		6.7	225.97
NL.		7.9	224.77
+20		8.4	224.27
+40		9.2	223.47
	15+00		
-40		4.6	228.07
-20		4.0	228.67
NL.		4.2	228.47
℄		3.7	228.97
SL.		2.4	230.27
+20		2.3	230.37
+40		2.3	230.37
TP#29	1.70	234.26	0.11 232.56
	15+50		
-40		10.3	233.96

	15+50	244.26	Baker	ST.
S-20			10.0	234.26
SL.			10.4	233.86
L			10.1	234.16
HL			10.9	233.36
+20			10.2	234.06
+40			10.1	234.16
	15+75			
-40			9.0	235.26
-20			9.2	235.06
NL.			9.6	234.66
L			9.0	235.26
S			8.7	235.36
+20			8.9	235.36
+40			8.8	235.46
	16+00			
-40			7.9	236.36
-20			7.7	236.56
SL.			7.4	236.86
L			7.0	237.26
H			7.2	237.06
TP+29	11.69	244.25	11.70	232.56
+20			6.3	237.95
+40			6.2	238.05
	16+25			
-40			4.8	239.45
-20			5.2	239.05

244.25

N		5.7	238.55
L		5.8	238.45
SL.		6.7	237.55
+20		5.8	238.45
+40		6.9	237.35
	16+50		
-40		6.6	237.65
-20		5.8	238.45
SL.		5.4	238.85
L.		4.7	239.55
N		3.8	240.15
+20		3.1	241.15
+40		2.7	241.55
	17+00		
-40		1.6	242.65
-20		1.8	242.45
N		1.8	242.45
L		2.8	241.45
SL.		4.0	240.25
+20		4.3	239.95
+40		4.7	239.55
TP+30	5.92	248.37	1.80 242.45
	17+50		
-40		6.9	241.47
SL-20		6.5	241.87
SL.		5.7	242.67

			Baker St.
	17+50	248.37	
℄		5.6	242.77
N		5.3	243.07
+20'		4.7	243.67
+40'		3.7	244.67
	18+00		
-40'		2.7	245.67
-20'		3.7	244.67
N		4.0	244.37
℄		4.2	244.17
S		4.9	243.47
+20		5.2	243.17
+40		5.5	242.87
	18+20		
-40		6.9	241.47
-20		5.5	242.87
SL.		4.5	243.87
℄		3.9	244.47
N		3.5	244.87
+20		3.4	244.97
+40		3.1	245.27
	18+50		
-40		6.3	242.07
-20'		6.7	241.67
N		7.0	241.37
℄		7.1	241.27
SL.		7.7	240.67
+20		8.4	239.97
+40		10.0	238.37

248.37

18+65		
-40	12.2	236.17
-20	11.0	237.37
S	10.6	237.77
℄	9.5	238.87
N	9.5	238.87
+20	8.6	239.77
+40	7.4	240.97
TP#31 10.39 246.25	12.51	235.86
Top 2nd fence Post North of Baker on Sumter St	0.00	246.25 6"x6" Post
Temp BM.		
TP#32 0.64 236.50	10.39	235.86
19+00		
-50'	9.2	227.3
-26	8.2	228.3
N	11.9	225.1
℄	12.2	224.3
S	12.7	223.8
+25'	12.8	223.7
+45'	10.8	225.7
TP#32 1.21 224.86	12.85	223.65
19+27		
-62	11.0	213.86
-45	12.6	212.26
-30	16.6	208.26
-15	14.6	210.26
SL.	14.5	210.36

224.86 Baker St.

℄		15.6	209.36
N		13.4	211.46
+22'		11.0	213.86
+45'		10.1	214.76
+60'		10.0	214.86
I.P.#37	0.55 212.93	12.48	212.38
	19+50		
-79		0.5	212.43
-48		6.6	206.33
-24		9.0	203.93
N		11.1	201.83
℄		12.7	200.23
S		14.3	198.63
+25		15.2	197.73
+46		10.7	202.23
+63		9.7	203.23
	19+87		
-102'		29.0	183.93
-53		26.5	186.43
-37		25.8	187.13
-16		23.7	189.23
S.L.		23.0	189.93
℄		22.9	190.03
N.L.		20.9	192.03
+15'		18.3	192.63
+43'		9.8	201.13
+77		3.1	207.83

212.93

on Rock T.N.N.L. 23+47

I.P.#39	0.76	202.04	11.65 201.28
	20+00		
-82'		+1.9	213.94
-37'		+1.5	203.54
N		5.8	196.24
+16		8.9	193.14
℄		10.4	191.64
+10		15.3	186.74
S.L.		17.8	184.24
+28		20.3	181.74
+64'		20.8	181.24
+134'		24.4	177.64
	20+30		
-137		37.4	164.64
-106		30.2	171.84
-73		30.0	172.04
-54		32.0	170.04
-33		24.2	177.84
S.L.		17.0	185.04
℄		10.4	191.64
N.L.		3.8	198.24
+8'		0.3	201.74
+45		+6.5	208.54
+87		+13.4	215.44
	20+50		
-88		+17.1	219.14

20+50	202.04	Baker St.	
-69		+ 11.9	213.94
-30		+ 7.0	209.04
-21		+ 2.6	209.64
N		3.2	198.84
℄		13.2	188.84
S		18.2	183.84
+74		30.9	171.14
+86		36.9	165.14
+123	℄ trash	46.6	155.44
+139	Top slope starts up from here	42.7	159.34
+171		35.5	166.54
IP #35	0.21 189.83	12.92	189.62
20+72			
-175		14.7	175.13
134		15.5	174.33
-95		28.8	161.03
-80		30.0	159.83
-68		24.6	165.23
-47		17.3	172.53
-26		12.3	177.53
S.L.		9.8	180.03
+10		8.8	181.03
℄		6.8	183.03
N		1.6	188.23
+22		+9.0	198.83
+46		+16.0	205.83
+89		+26.8	216.63
+108		+31.6	221.43

189.83

20+92		
-87	+20.0	209.83
-52	+7.0	196.83
-31	+1.1	190.93
N.L.	7.1	182.73
℄	9.0	180.83
S.L.	10.5	179.33
+14	12.5	177.33
+64	23.7	166.13
+73	15.7	174.13
+122	10.6	179.23
+148	7.5	182.33
21+12		
-145	+1.3	191.13
-110	7.8	182.03
-78	11.3	178.53
-34	29.5	160.33
-18	19.5	170.33
S.L.	15.3	174.53
℄	11.1	178.73
N	9.9	179.93
+15	5.6	184.33
+64	+4.9	194.73
+85	+12.7	202.53
21+25		
-95	+11.7	201.53

21+25	189.83	Baker St.	
-74		+3.9	193.73
-42		0.2	189.63
-10		12.0	177.83
N		15.0	174.83
+12		17.7	172.13
+15 in Wash		27.7	162.13
E in "		27.7	162.13
SL " "		28.3	161.53
+14		29.0	160.83
+16		25.3	164.53
+32		23.5	166.33
+71		4.4	185.43
+91		2.1	187.73
21+50			
-85		+12.4	202.23
-44		0.0	189.83
-19		8.5	181.33
SL.		16.2	173.63
E		19.2	170.63
+12		21.5	168.33
N.L. in Wash		26.2	163.63
+17		20.6	169.23
+49		12.0	179.83
+71		2.8	187.03
+90		+0.8	190.63

189.83

21+60	
-113	+6.0 195.83
-81	2.7 187.13
-61	8.7 181.13
-23	-22.1 167.73
-21 in Wash	25.2 164.63
-7	18.9 170.93
NL.	16.6 173.33
E	12.1 177.73
SL.	8.7 181.13
+32	+1.8 191.63
+84	+16.7 206.53
T.P. 36	130.5 202.73 0.15 189.68
T.P. 37	12.08 214.41 0.40 202.33
22+00	
-88	+9.1 223.51
+78	+7.8 222.21
-36	2.5 211.91
SL.	4.7 209.71
E	15.8 198.61
NL.	22.7 191.71
+21	28.2 186.21
+40	32.9 181.51
+60 in Wash	48.0 166.41
+65 " "	48.0 166.41
+68	45.4 169.01
+96	31.9 182.51
+125	25.9 188.51

214.41

TP #37	12.13	225.11	1.93	212.98
TP #38	12.56	236.80	0.87	224.24
	22+50			
-153'			55.5	181.3
-128'			67.5	169.30
-98'			61.0	175.80
-62			54.0	182.80
-43			44.4	192.4
-18			33.0	203.80
N.L.			27.6	209.20
℄			16.9	219.90
SL.			5.7	231.10
+40			+2.3	239.10
+72			+2.5	239.30
TP #39	10.23	246.29	0.74	236.06
Chk 6"x6" Post P-15			0.03	246.26
		π Corrected		
	0.03	246.28		246.25 P-15
	22+75			
-50'			0.8	245.48
-30'			0.5	245.75
-11			2.7	243.58
SL.			8.5	237.78
℄			17.3	228.98
+8			25.5	220.78
N.L.			31.5	214.78
+40			50.0	196.28
+57			57.1	189.19

246.28

19

+72		57.5	188.78
+90		61.7	184.58
+127		62.3	183.93
TP #40	12.52	255.40	3.40	242.88
	23+00			
-129			43.4	212.0
-105			56.9	198.5
-75			56.4	199.0
-46			47.9	207.50
-31			46.4	209.0
N.L.			31.8	223.60
℄			21.0	234.40
+14			10.8	244.6
SL.			8.5	246.9
+18			4.2	251.20
+43			3.7	251.70
+50			4.2	251.20
TP #41	12.35	265.62	2.13	253.27
	23+25			
-50			10.4	255.22
-13			10.6	255.02
SL			14.5	251.12
℄			21.6	244.02
N			34.3	231.32
+17			45.5	220.12
+43			44.7	222.92
+73			55.3	210.32
+108			52.8	212.82
+134			53.5	212.12

	23+50		
-135		43.6	222.02
-119		40.2	225.42
-93		41.2	224.42
-75		39.5	226.12
-57		39.5	226.12
-21		31.0	234.62
-3		29.6	236.02
N		28.6	237.02
℄		19.9	250.72
S.L.		10.1	255.52
+15		8.0	257.62
+40		10.2	255.42
	23+75		
-40		10.5	255.12
-20		8.9	256.72
S.L.		5.3	260.32
+16		9.4	256.22
℄		11.4	254.22
N		18.1	247.52
+27		14.3	251.32
+46		26.0	239.62
+69		25.2	240.42
	23+95		
-45		10.9	254.72
-20		8.2	257.42

N		8.1	257.52
℄		7.5	258.12
S.L.		6.5	259.19
+20		9.0	256.62
+40		10.3	255.32
	24+25		
-40		9.2	256.42
-20		8.0	257.62
S.L.		7.1	258.52
℄		6.7	258.92
N.L.		6.6	259.02
+20		6.1	259.52
+40		6.0	259.62
	24+50		
-40		4.3	261.32
-20		5.4	260.22
N.L.		5.8	259.82
℄		5.0	260.62
S.L.		6.0	259.62
+20		7.0	258.62
+40		7.3	258.32
	25+00		
-40		5.6	260.02
-20		4.4	261.22
S.L.		4.8	260.82
℄		4.0	261.62

25+00 26562

NL.	4.5	261.12	
+20	4.2	261.42	
+40	4.2	261.42	
2.5+50			
-40'	3.0	262.62	
-20'	2.7	263.52	
N	2.8	262.82	
℄	3.2	262.42	
SL.	3.4	262.22	
+20	4.0	261.62	
+40	4.6	261.02	
26+00			
-40'	4.1	261.52	
-20'	2.5	263.12	
SL.	1.2	263.72	
℄	2.7	262.92	
N	1.8	263.82	
+20'	2.0	263.62	
+40	2.0	263.62	
T.P.#42	9.11	274.15	0.58 265.04
26+50			
-40'	9.2	264.95	
-20'	9.5	264.65	
N	9.3	264.85	
℄	10.2	263.95	
SL.	10.6	263.55	
+20	11.1	263.05	
+40	11.5	262.65	

274.15

21

27+00

-40'	11.4	262.75
-20'	10.6	263.55
SL.	10.3	263.85
℄	9.4	264.75
N.	8.6	265.55
+20	7.9	266.25
+40	7.5	266.65

27+53.76 = End 40' St. from West = Beginning 60' St. to East.

-40'	7.1	267.05
-10 = ~~NL to East~~	8.1	266.05
NL to West	8.4	265.75
℄	9.5	264.65
SL. " "	9.6	264.55
SL on 1½ Pipe	9.22	264.93 BM.
+10 ~~St. to East~~	10.0	264.15
+40	10.8	263.35

→ This pipe moved (Driven down) 5 months after Elevation taken. To cross Section Ahead will Turn up from BM 6"x6" Post P-19

	808	254.33		246.25 " "
T.P. 12.17 = chk #41 TP		265.44	1.06	253.27 ← on 1½" Pipe
T.P.#43	3.20	267.78	0.86	264.58

X-Sections Baker St. in Pl. 1207

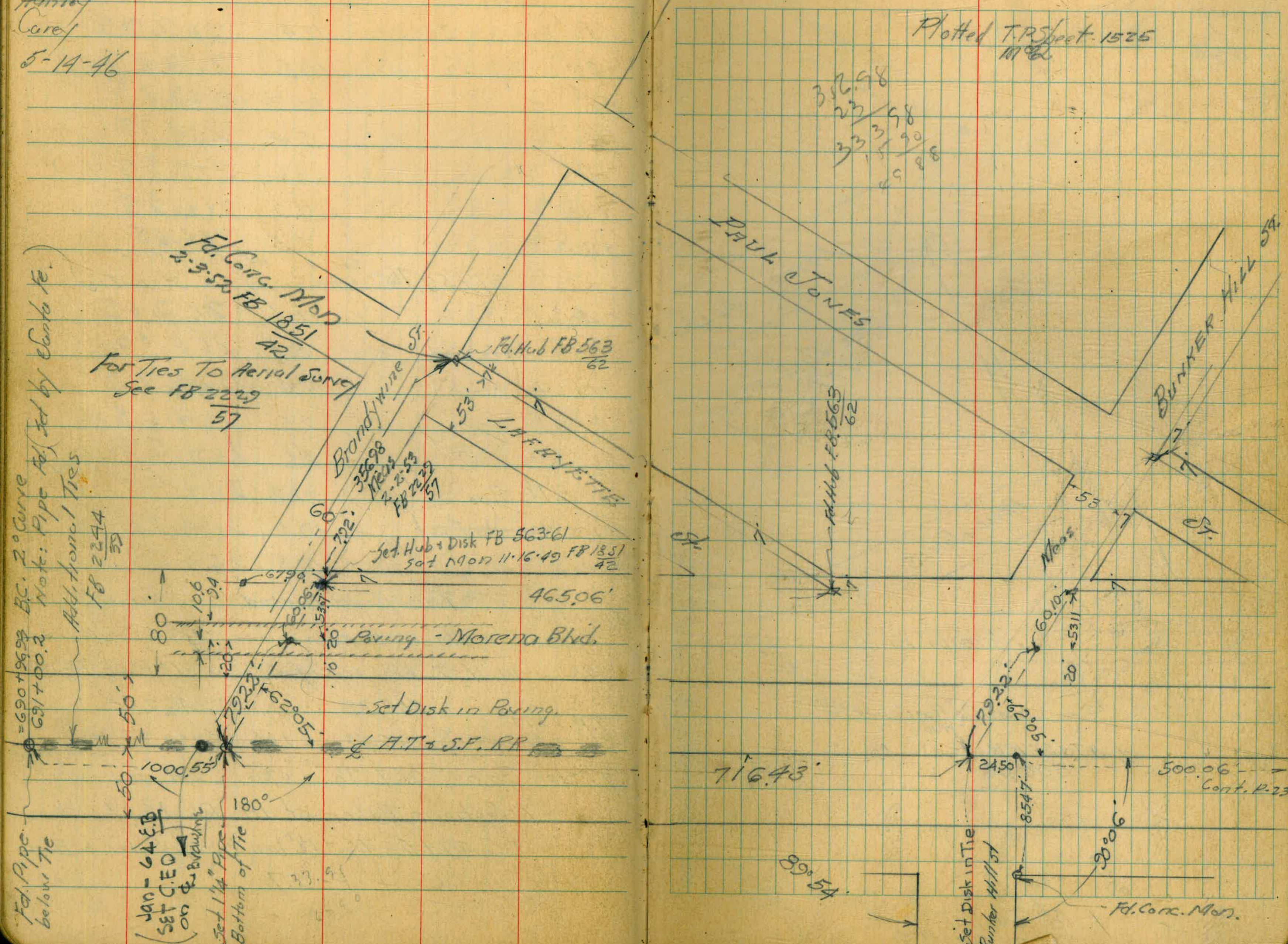
27+53.76 = 1½" Iron Pipe = ℄ Baker to East.

Cont. P-27

Walker
Hendricks
Hanley
Carey
5-14-46

Ties - in Pueblo Lot 1208

Indexed
C.S.K.



Walker
Hendricks
Hunter
Corey
5-14-46

Ties - in Pueblo Lot 1308

Plotted — Nov. 6 '46
T.P. Sheet 1514
MB.

PRINCETON

Fd. Hub. FB 563 / 61

TICONDEROGA

ETHAN ALLEN

Ties This Subdivision
in FB 563 (61)

Bunker Hill St.

PAUL JONES

Set Disk in Paving

Set Hub

Morena Blvd.

80'

50'

50'

20'

60.10'

53.11'

Fd. Hub

79.23'

C 20°06'05"

Set 1/4" Pipe & Tag

180°

℄ AT&SF RR

500.06'

170.33'

24.56'

85.37'

89°53'15"

90°06'

Fd. Conc. Mon.
Ties FB 1427 - 64
1735 - 35

Glendora St.

90°06'45"

Set Hub

Bunker Hill St.

60.10'

53.15'

20'

C 20°06'

Set Disk in Paving

399.73'

85.40'

89°53'15"

Fd. Mon.

35'

Rosewood St.

90°06'45"

79.23'

C 20°02'15"

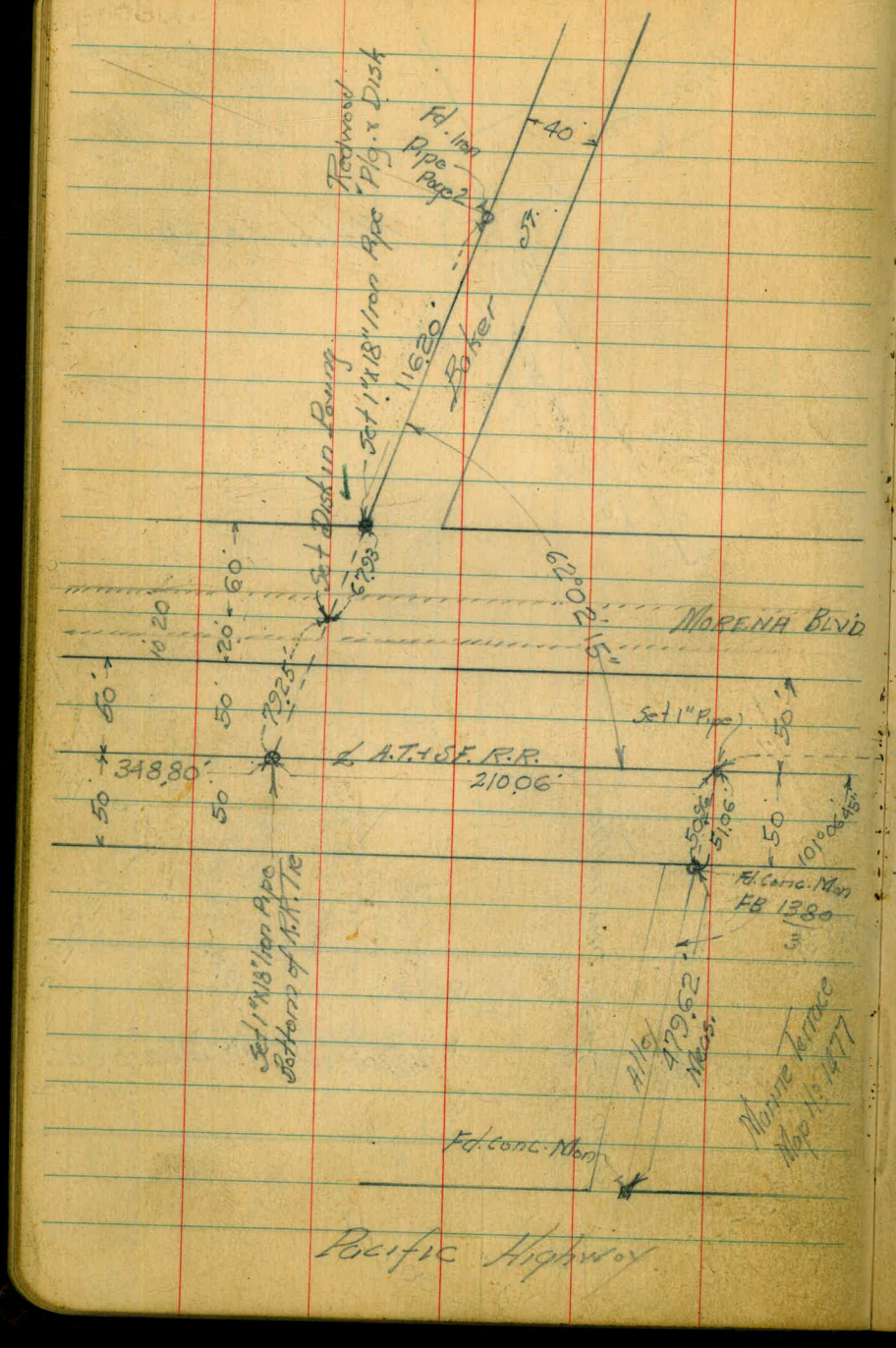
348.80'

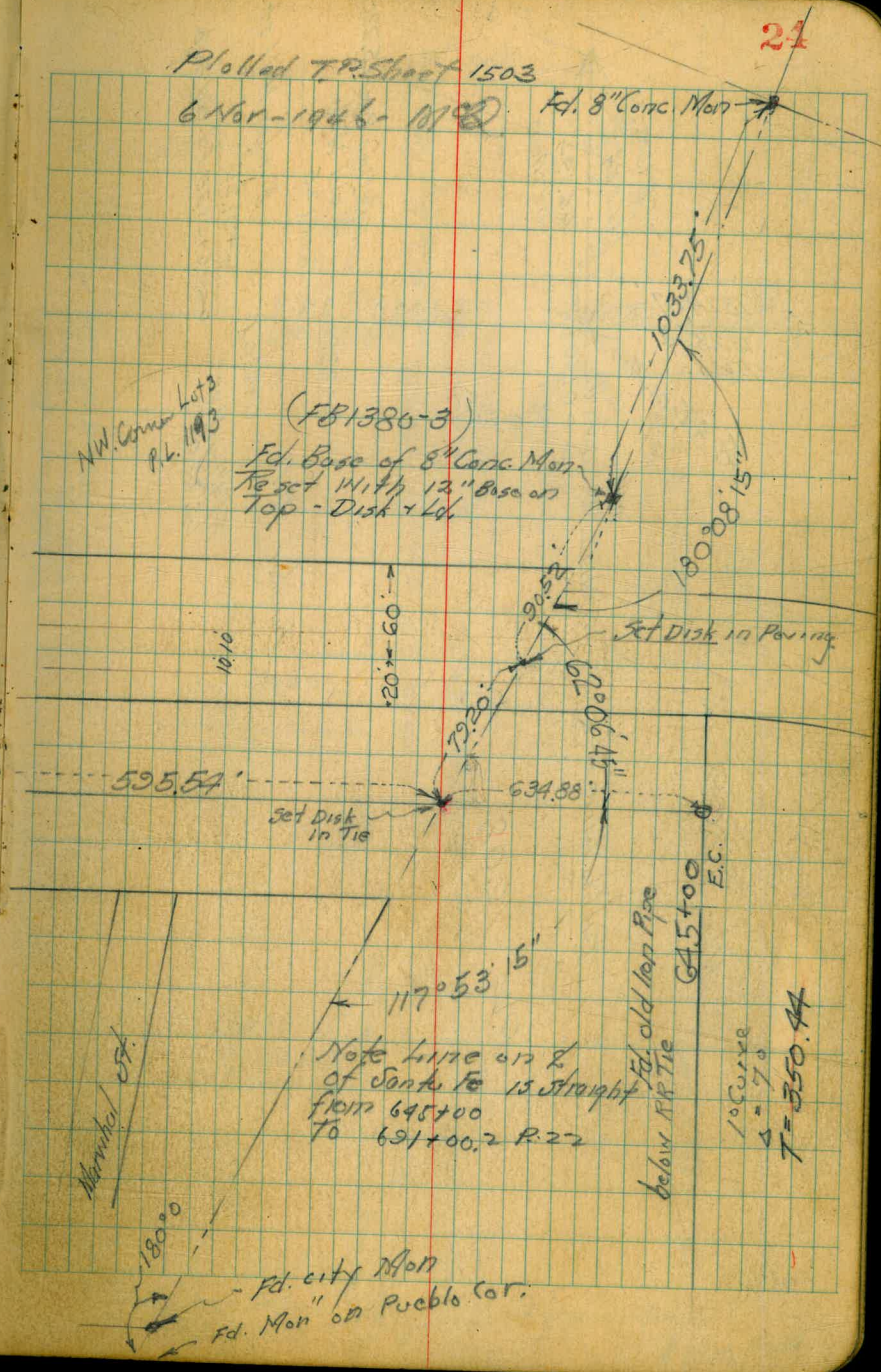
210.06'

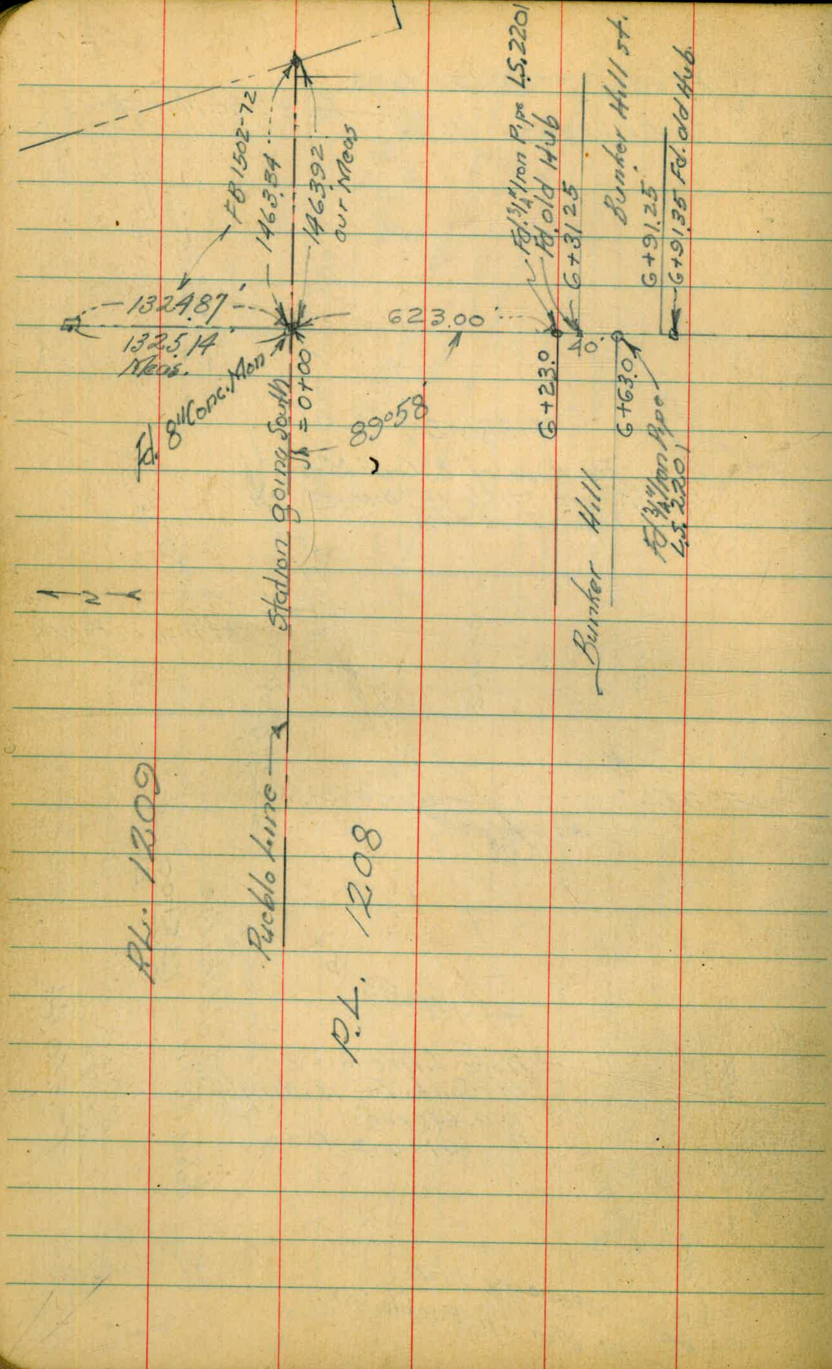
Cont. P. 24

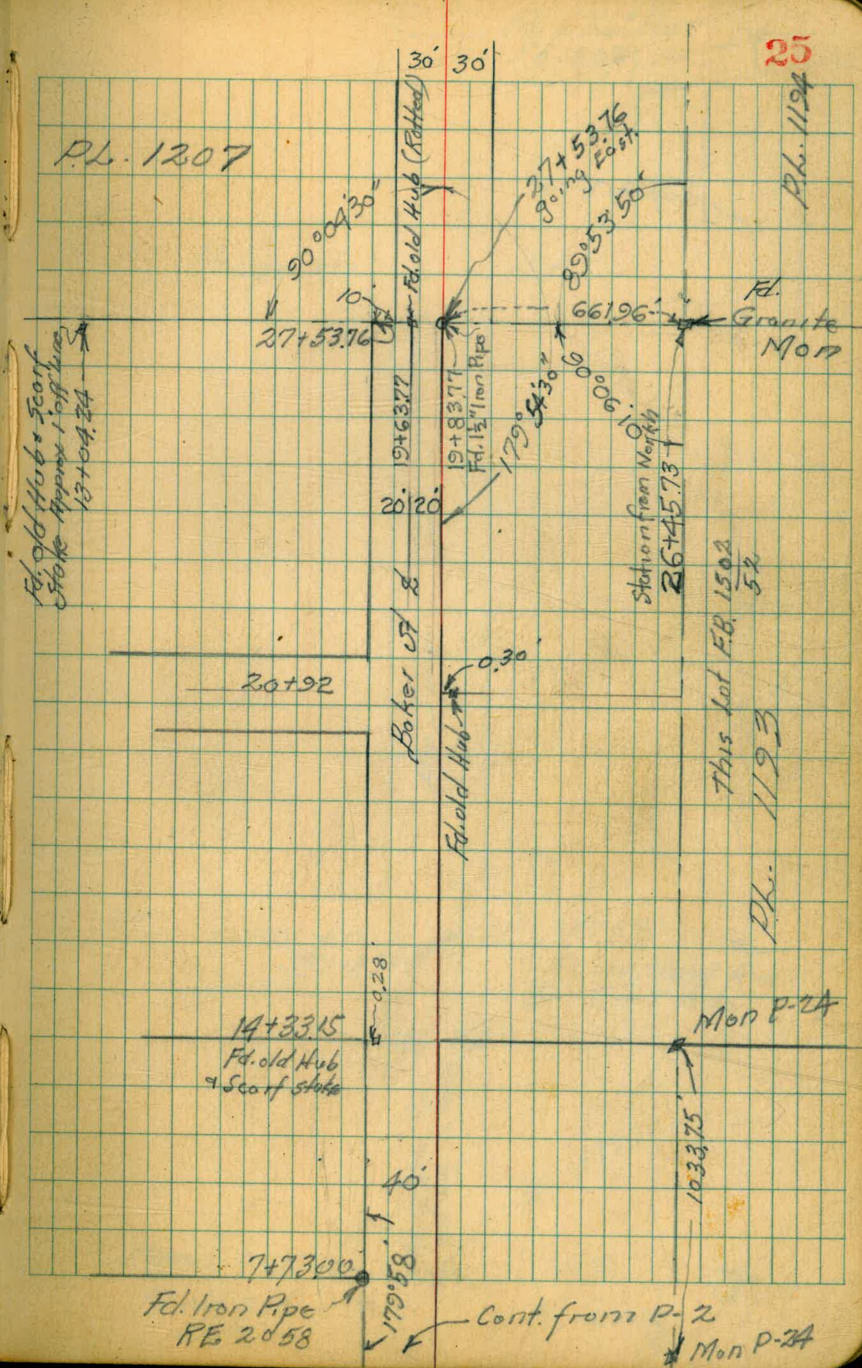
Baker St.

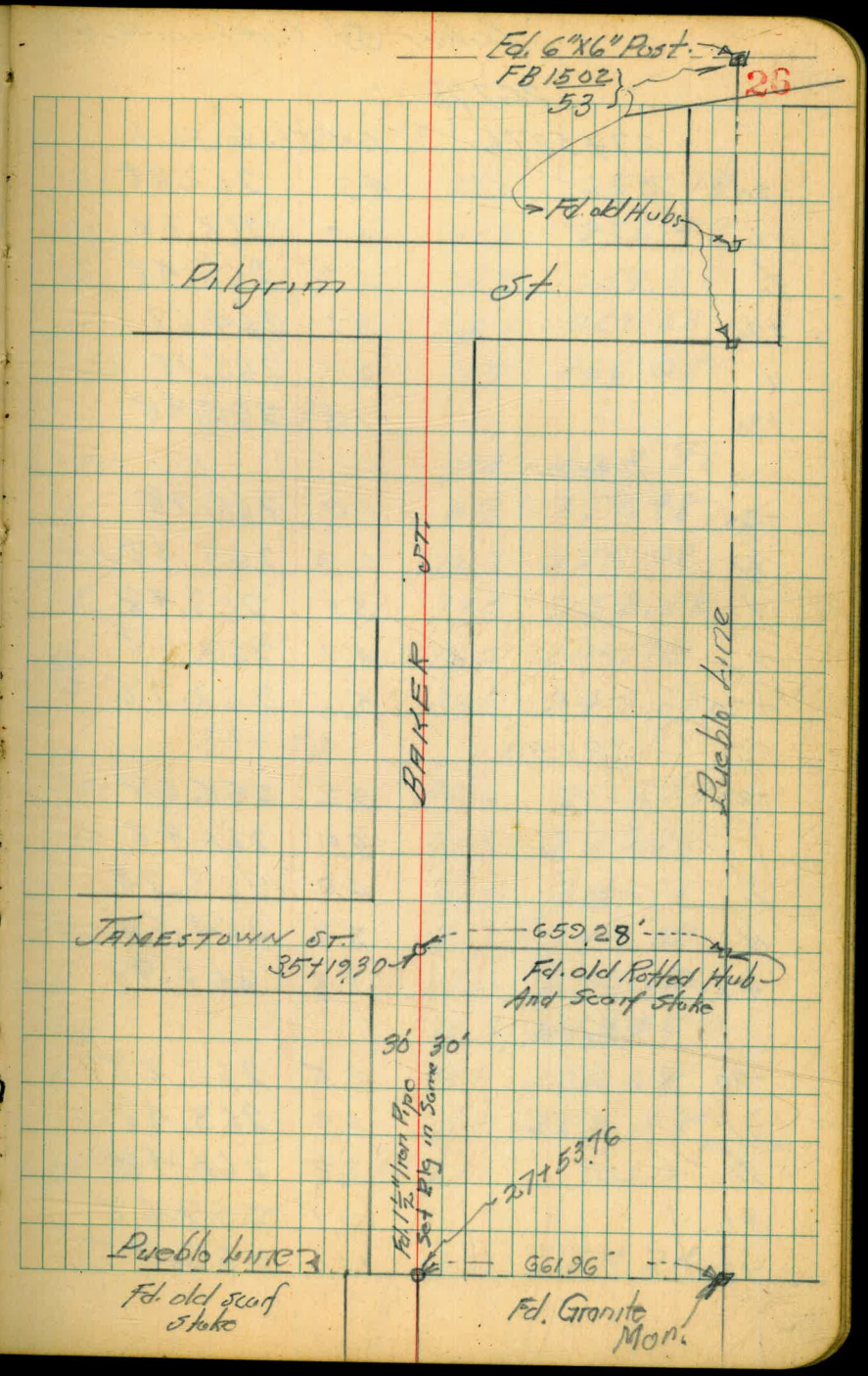
Plotted T.R. Sheet 1503
6 Mar - 1946 - DJR






F.B. 1502-72
1463.54
1463.92 our Meas
1324.87
1325.14 Meas.
Fd. 8" Conc. Mon
Station going South
= 0+00
89°58'
623.00
Fd. 3/4" Iron Pipe L.S. 2201
Fd. old Hub
6+31.25
Bunker Hill St.
6+91.25
6+91.35 Fd. old Hub
6+23.0
40'
6+63.0
Fd. 3/4" Iron Pipe L.S. 2201
Bunker Hill
N
Pueblo Line
P.L. 1209
P.L. 1208


30' 30'
P.L. 1207
90°00'30"
Fd. old Hub (Rotted)
37+53.76 going East
89°53'50"
P.L. 1194
10'
27+53.76
19+63.77
19+83.77 Fd. 1½" Iron Pipe
661.96'
Fd. Granite Mon
179°54'30"
90°00'10"
Station from North
26+45.73
20' 20'
Fd. old Hub & Scarf Stake Approx. 1' off line 13+04.24
Baker St.
0.30'
20+92
Fd. old Hub
This Lot F.B. 1502/52
P.L. 1193
14+33.15
Fd. old Hub & Scarf Stake
0.28
Mon P-24
1033.75
40'
7+73.00
179°58'
Fd. Iron Pipe RE 2058
Cont. from P-2
Mon P-24


Fd. 6"x6" Post
FB 1502
53
26
Fd. old Hubs
Pilgrim
St.
BAKER
ST.
Pueblo Ave
JAMESTOWN ST.
659.28'
Fd. old Rotted Hub
And Scarf Stake
35 19 30
30'
30'
Fd. 1/2" Iron Pipe
Set Flg in Same
21
53.16
Pueblo Line
661.96'
Fd. old scarf
Stake
Fd. Granite
Mon.

Baker St. Cont. from P-21

267.78

27+53.76 60' St. to East

-20	4.9	262.88
SL.	4.0	263.78
℄	2.3	265.48
+20	3.1	264.68
N	2.6	265.18
+20	1.8	265.98

28+00

-20	1.0	266.78
N	2.3	265.48
℄	3.8	263.98
S	4.7	263.08
+20	5.6	262.18

28+50

-20	9.2	258.58
S	5.8	261.98
℄	4.0	263.78
N	3.2	264.58
+20	1.8	265.98

29+00

-20	2.5	265.28
N	4.3	263.48
℄	7.3	260.48
SL.	10.1	257.68
+20	12.0	255.78

29+15

267.78

-25	12.6	255.18
SL.	10.8	256.98
℄	8.2	259.58
N	4.1	263.68
+20	1.7	266.08

29+40

-20	4.4	263.38
N	8.3	259.48
+20	12.7	255.08
℄	13.9	253.88
SL.	18.0	249.78
+30	22.5	245.28

29+50

-40 in ditch	32.6	235.18
-30	30.6	237.18
SL.	26.0	241.18
+20	20.7	247.08
℄	17.6	250.18
+6	14.7	253.08
N	10.9	256.68
+20	5.7	262.08
TP #4	8.86	273.44 3.20 264.58 on P. pc P-21

29+70

-20	9.2	264.24

273.44 BAKER ST. X-SECTIONS

29+70		
N	12.4	261.44
℄	17.6	255.84
S.L.	22.8	250.64
+40	28.2	245.24
30+00		
-20	13.8	259.64
S.L.	11.9	261.54
+20	8.5	264.94
℄	8.3	265.14
+20	7.5	265.94
N.L.	5.9	267.54
+20	4.9	268.54
30+25		
-20	3.3	270.14
N	4.7	268.74
+15	5.3	268.14
℄	5.7	267.74
S.L.	7.1	266.34
+20	8.4	265.04
30+50		
-20	7.3	266.14
S.L.	6.1	267.34
℄	4.9	268.54
+13	4.1	269.34
N.L.	2.7	270.74

273.44

+20	2.7	270.74
31+00		
-20	1.8	271.64
N	2.3	271.14
℄	3.7	269.74
S.L.	4.5	268.94
+20	5.5	267.94
31+50		
-20	3.8	269.64
S.L.	3.3	270.14
℄	2.4	271.04
N	1.6	271.84
+20	0.5	272.94
T.P. 445	10.93	282.53 1.84 271.60 on Lo 31+50
32+00		
-20	8.6	273.93
N	9.2	273.33
℄	9.8	272.73
S.L.	10.2	272.33
+20	10.5	272.03
32+50		
-20	9.2	273.33
S.L.	9.0	273.53
℄	8.4	274.13
N	9.2	274.33
+20	7.9	271.63

282.53 BAKER ST.
X-Sections

	33+00		
-20		7.0	275.53
N		7.1	275.43
℄		7.7	274.83
SL.		8.2	274.33
+20		8.8	273.73
	33+50		
-20'		7.6	274.93
SL.		7.0	275.53
℄		6.7	275.83
N		6.5	276.03
+20		6.3	276.23
	34+00		
-20		4.8	277.73
N.L.		5.5	277.03
℄		6.0	276.53
SL.		6.5	276.03
+20		7.0	275.53
	34+50		
-20		6.1	276.43
SL.		5.5	277.03
℄		4.8	277.73
N		4.4	278.13
+20		3.8	278.73
	35+00		
-20		1.8	280.73
N		2.9	279.63

282.53

20

℄				3.0	279.53
SL.				4.5	278.03
+20				4.8	277.73
	35+19.30 = ℄ Jamestown St.				
-20				4.6	277.93
SL.				4.0	278.53
℄				2.8	279.73
℄ on 1½" Pipe				2.58	279.95
N				2.1	280.43
+20				1.5	281.03
T.P. #46	5.08	285.03	2.58	279.95	on Pipe
T.P. #47	6.19	282.20	9.02	276.01	on Iron Pipe
T.P. #48	7.96	287.94	2.22	279.98	6+23 Sta. Ln. P.S. on 8"x8" Conc. Mon. N.E. Cor. Pk. 1208
T.P. #49	3.58	289.42	2.10	285.84	
T.P. #50	4.67	281.18	12.91	276.51	
T.P. #51	4.49	272.97	12.70	268.48	
T.P. #52	0.58	261.65	11.90	261.07	
T.P. #53	3.59	264.22	10.2	260.63	
T.P. #54	-0.02	251.20	13.00	251.22	
T.P. #55	0.10	238.48	12.82	238.38	
Chk 7" Hub SL. Brandywine + Trenton FB. 1591 47				12.14	226.34
					226.26
					0.08

Addl. Levels on Hayes, Balboa and Grand Ave.

E. Moore
S. on M. on Hayes
W. on Moore
Beg.
5-31-4C.

40 — 40 — N.L. Hornblend

0+00 — 40

3+12.16

E Hornblend

2+30

12°33'

3+48.03

4.77

40.98'

Mon. on ℄

77°37'

4+76.09

Stub
El. 44.07

Section ℄

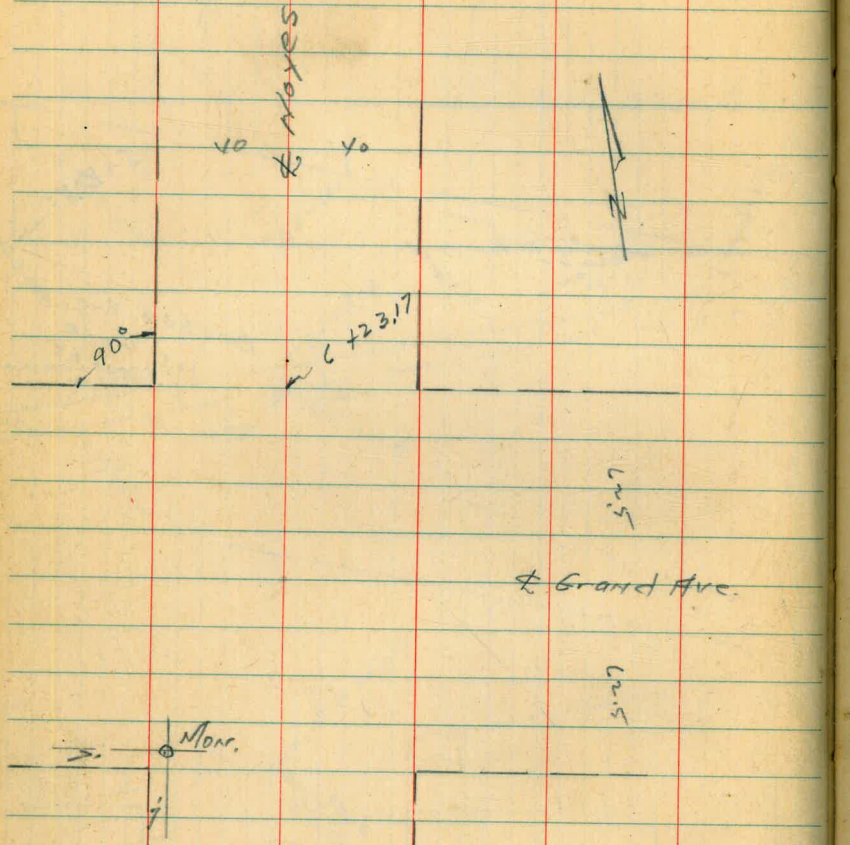
4+01.16

Mon. 7'

Baseline

5+80.85 — 40

Balboa Ave.
125' Wide
20' curbs


Notes
40
40
N
90°
6+23.17
Grand Ave.
Mon.

XSec on Hornblend St. 80' wide
Sketch = P. 30

1+25

1+00

0+70

0+40

200' W of W.L Noyes = 0+00 XSec @ 90°

T.P.	2,93	55.97	10.00	53.04	
NWBP	1,06	53.04		41.98	Garnet Noyes St

Lt. = to North ℄ Baseline Indexed Cusick Rt. 32

5.1 / 40	1.8 / 20	7.5	8.5 / 20	9.8 / 40	9.9 / 50
6.4 / 40	8.0 / 20	9.2	9.9 / 20	10.0 / 40	— / 50
7.8 / 40	9.1 / 20	9.8	9.7 / 20	10.1 / 40	— / 50
8.3 / 40	9.5 / 20	9.9	9.5 / 20	10.1 / 40	10.2 / 50
8.1 / 40	9.3 / 20	9.8	10.1 / 20	10.3 / 40	10.3 / 50

55.97

Hornblend

3 + 80

3 + 60

3 + 20

2 + 80 = E.L. Noyes St

See other Book for INTERSECTION

2 + 00 = W.L. Noyes St

1 + 60

55.97

LT = N

℄ Baseline

RT

4.8 / 40 | 5.2 / 20 | 7.0 | 10.8 / 4.8

4.6 / 40 | 4.7 / 20 | 5.9 | 6.7 / 5 | 10.7 / 9.2

2.3 / 40 | 2.5 / 20 | 3.7 | 5.0 / 14 | 10.6 / 18.1

1.9 / 40 | 2.3 / 20 | 2.9 | 3.7 / 17 | 4.7 / 22 | 9.0 / 27

2.2 / 40 | 3.2 / 20 | 3.9 | 4.9 / 20 | 5.8 / 40

2.8 / 40 | 3.8 / 20 | 4.7 | 5.6 / 20 | 6.9 / 40 | 7.4 / 49 Top Bank

55.97

Hornblend

5+80.85

5+55.8 ℄ 3' Walk and Con. Steps

3.50 50 Con Walk | 3.80 40.2 Top Steps

5+11.4 ℄ 3' Con Walk

4+69.4

4+38.8 ℄ 8' Con. drive

4+01.16 = Intersection ℄ of Hornblend and N.L. of Balboa Ave.

T.P. Stub ℄ & Noyes SL Balboa 6.34 | 50.41 | 11.90 | 44.07 ✓

55.97

Lt = N | ℄ = Baseline | Rt. 34

6.8 40 ⚠ on N.L. | 7.9 34 | 8.6 23 | 9.4 20 | 9.2

4.29 40 on Steps | 7.32 33.7 Walk & Bot. Steps | 7.46 25.1 Walk | 7.91 21.7 end Walk | 9.3 12 | 8.8

3.05 40 Walk | 3.28 37.1 end Walk | 6.7 24.5 | 8.1 20 | 8.7

2.3 40 | 3.7 23 | 4.0 20 | 5.9 15.1 | 7.2 12 | 8.0

1.21 68.2 gar. | 1.90 42.6 end Dr. | 1.9 40 ground | 3.0 20 | 4.9 8.3 | 6.5

0.0 40 | 0.4 20 | 1.5 4 | 5.2

50.41

LT = NI

℄ Baseline

X sec of Balboa Ave. 125' wide at Noyes St.

2+00 W.L. Noyes — Sec. parallel with Noyes

1+50 Sec 90°

1+00 Sec 90°

0+50 Sec 90°

200' W of W.L. of Noyes on ℄ Balboa Ave. = 0+00 sec. at 90°

T.P. Stub p. 34 — 5.09 — 49.16 — 44.07

2.5 / 64	3.8 / 60	4.4 / 44	4.1 / 17	4.7 / 13	4.7	5.3 / 20	5.0 / 40	5.1 / 48	5.0 / 64
3.8 / 62.5	3.8 / 50	4.9 / 38	4.2 / 14	4.8 / 11	4.8	5.3 / 19	5.8 / 40	5.1 / 47	5.1 / 62.5
3.7 / 62.5	4.1 / 46	4.8 / 40	4.3 / 13	4.9 / 10	4.8	5.2 / 18	5.8 / 39	5.0 / 47	5.0 / 62.5
	3.9 / 62.5	4.8 / 36	4.1 / 13	4.8 / 10	4.9	5.1 / 19	5.7 / 36	5.0 / 48	4.9 / 62.5
4.0 / 62.5	4.0 / 50	4.9 / 38	4.0 / 13	4.9 / 10	4.7		5.1 / 18	5.7 / 41	4.9 / 47	5.3 / 62.5

49.16

Balboa

3 + 50 Sec 90°

3 + 20 Sec. at 90°

2 + 81.9C = EL Noyes Sec. parallel with Noyes

2 + 61.47 Sec. parallel with Noyes

2 + 40.98 ℄ Noyes Parallel with Noyes

2 + 20.49 Sec parallel with Noyes

49.1C

LT = x1 ℄ Rt 36

3.8 / 62.5	4.4 / 55	5.3 / 36	5.4 / 16	5.2	6.7 / 22	6.6 / 40	5.8 / 44	5.6 / 62.5
	3.7 / 62.5	4.9 / 40	5.0 / 15	5.0	5.8 / 22	6.0 / 42	5.4 / 46	5.3 / 62.5
	2.0 / 64	3.1 / 57	4.2 / 30	4.9	5.7 / 21	5.8 / 37	5.4 / 44	5.1 / 64
	1.4 / 64	2.6 / 52	4.2 / 25	4.8	5.4 / 22	5.9 / 40	5.0 / 64	
1.7 / 64	2.8 / 60	3.5 / 44	4.3 / 29	4.5 / 13	4.7	5.5 / 20	5.8 / 40	5.1 / 44	5.1 / 64
1.8 / 64	3.8 / 57	4.4 / 40	4.7 / 18	4.6 / 13	4.7	5.3 / 20	5.7 / 40	5.0 / 50	5.1 / 64

x 9.1C

Balboa ave

6+50

6+00

5+50

5+00

4+50

4+00 Scl. at 90°

49.6

LT = N ℄ Rt

6.0	7.0	8.1	8.9	8.7	8.8	9.6	9.6	9.0	9.1	8.3
62.5	58	45	38	20		19	40	48	60	62.5
5.2	6.9	8.2	8.2	8.0	8.8	9.0	8.4	8.5	7.7	
62.5	57	40	17		20	40	45	60	62.5	
6.2	7.7	7.5	7.1	8.1	8.3	7.6	7.7	6.3		
62.5	40	17		20	40	45	60	62.5		
4.9	6.1	7.2	7.0	6.4	7.6	7.5	7.2	7.0	5.7	
62.5	58	40	17		22	40	44	60	62.5	
4.4	5.3	6.3	6.2	5.9	6.9	7.4	6.6	6.3	4.6	
62.5	55	37	17		22	40	45	60	62.5	
4.2	5.0	6.0	5.8	5.5	6.5	6.4	6.7	6.1	5.9	4.3
62.5	55	40	17		22	27	41	45	60	62.5

49.16

X sec of Noyes St. 80' wide
Balboa Ave to Grand Ave.

T.P. Grand + Noyes (on Pipe, N.W. Cor.) 9.47 39.69

4+23.17 = N.L. Grand Ave.
P. 31

0+00 at 90°

5+50 at 90°

5+00 at 90°

4+76.09 = S.L. Balboa Ave. (E Noyes and Sec at 90°
P. 30

Y 9.16

Lt. = East ℄ Indexed o-s-N Rt = W

9.0 / 40	9.6 / 20	9.0	9.1 / 20	9.5 / 40
8.0 / 40	8.4 / 20	7.7	7.6 / 20	7.6 / 40
5.7 / 40	6.0 / 20	5.8	5.6 / 20	5.8 / 40
4.4 / 40	5.1 / 37	5.0 / 20	5.0	5.1 / 20	5.1 / 40
3.5 / 40	5.0 / 36	5.0 / 20	5.1		

Y 9.16

X sec of Grand Ave 125' wide 20 obs.
200' E & W of Noyes ST.

2 + 00 = W.L. Noyes

1 + 50

1 + 00

0 + 50

0 + 00 = 200' W of W.L. Noyes ST.

T.P. NW Pipe
Grand & Noyes 5.17 44.86 39.69

LT = N & Indexed e.s.k. RT = S 39

						5.2 / 12.5	6.0 / 35	7.2 / 6	9.3	9.0 / 17	7.5 / 22	9.0 / 42	11.8 / 62.5	13.8 / 70	14.7 / 90
6.8 / 80	2.4 / 62.5	5.8 / 52	6.7 / 12	8.7 / 8	8.9	9.0 / 19	7.6 / 23	10.5 / 58	11.7 / 62.5	13.4 / 70	14.9 / 90				
	8.3 / 80	8.0 / 62.5	6.1 / 53	7.0 / 12	8.4 / 9	8.4	9.2 / 21	8.0 / 24	9.3 / 55	11.7 / 62.5	12.7 / 68	14.1 / 90			
7.8 / 90	8.2 / 71	7.5 / 62.5	6.7 / 57	6.7 / 13	7.7 / 9	7.8	8.1 / 18	6.8 / 21	8.0 / 57	9.6 / 62.5	12.2 / 72	13.2 / 90			
8.1 / 75	7.8 / 62.5	5.5 / 55	6.0 / 11	7.2 / 7	7.4	7.8 / 20	6.3 / 27	7.8 / 55	9.7 / 62.5	11.8 / 75					

44.86

Grand Ave.

3 + 50

3 + 00

2 + 80 E. L. Noyes

2 + 60 E C6 Line Noyes

2 + 40 ℄ Noyes

2 + 20 W C6 Line Noyes

44.86

LT = N ℄ RT.

1.4 / 65 Top Cut | 2.7 / 62.5 | 6.7 / 57 | 9.3 / 45 | 10.9 / 30 | 10.6 | 10.3 / 13 | 11.4 / 22 | 11.0 / 42 | 9.1 / 56 | 7.9 / 62.5 Top Cut

4.0 / 62.5 | 8.1 / 50 | 8.7 / 30 | 9.0 / 5 | 10.1 | 9.4 / 13 | 10.4 / 20 | 11.1 / 48 | 8.1 / 58 | 8.6 / 62.5

4.7 / 62.5 | 7.6 / 35 | 8.3 / 5 | 9.8 | 8.8 / 12 | 9.5 / 35 | 10.6 / 62.5

5.3 / 62.5 | 7.4 / 25 | 8.0 / 5 | 9.5 | 8.7 / 10 | 9.6 / 35 | 11.3 / 62.5 | 11.5 / 70

4.7 / 62.5 | 5.8 / 30 | 7.5 / 5 | 9.5 | 9.2 / 15 | 8.2 / 25 | 9.8 / 40 | 11.9 / 62.5 | 12.1 / 70

4.8 / 62.5 | 5.6 / 30 | 7.6 / 4 | 9.3 | 9.1 / 14 | 7.8 / 30 | 10.4 / 55 | 12.6 / 62.5 | 13.1 / 70

44.86

Grandave.

Check to N in BP Garnet + Noyes		1.77	62.00	61.98 / 0.02
T.P.	10.23	63.77	0.63	53.54
T.P.	10.29	54.17	0.98	43.88
5+00				
11+50				
11+00				
		44.86		

LT. = N

PT 41

0.0 / 70	6.7 / 62.5	10.7 / 40	11.9 / 27	12.0	12.1 / 13	13.0 / 19	11.5 / 24	11.9 / 47	10.0 / 52	3.2 / 62.5
Top Cut										Top Cut

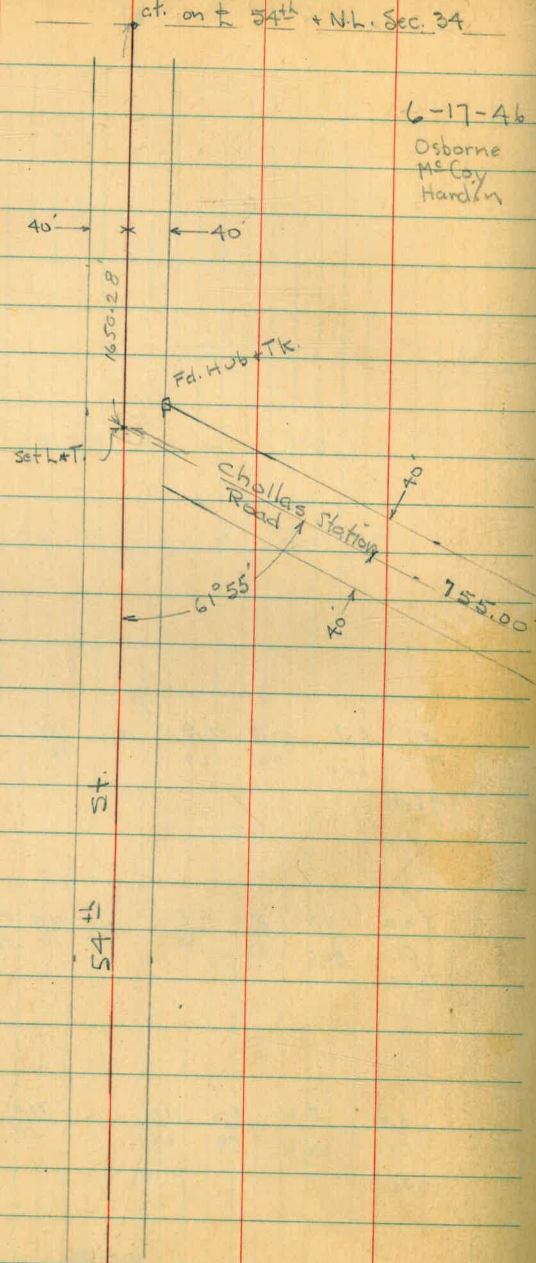
0.2 / CC	5.7 / 62.5	8.1 / 60	11.8 / 35	11.4	11.4 / 14	12.6 / 18	11.3 / 23	11.6 / 52	4.7 / 62.5	2.8 / 1.4
Top Cut										Top Cut

0.5 / 67	5.3 / 62.5	7.2 / 59	11.2 / 33	11.0	11.0 / 14	12.1 / 19	11.2 / 25	11.5 / 48	9.7 / 55	4.2 / 62.5	2.7 / 6.5
Top Cut											Top Cut

44.86

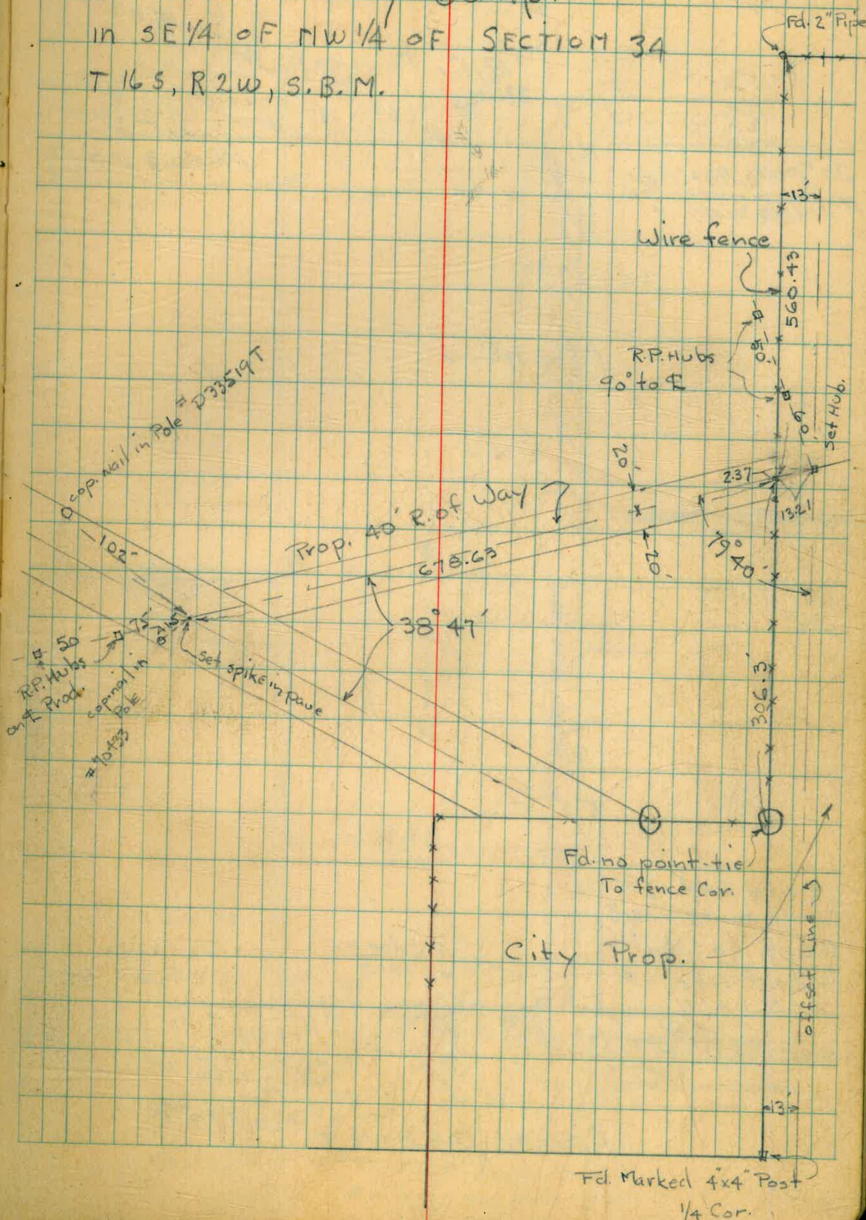
6-17-46

Osborne
McCoy
Hardin



Location of Proposed 40' Right of Way for Road to City Dump.

in SE 1/4 of NW 1/4 of SECTION 34
T 16 S, R 2 W, S.B.M.

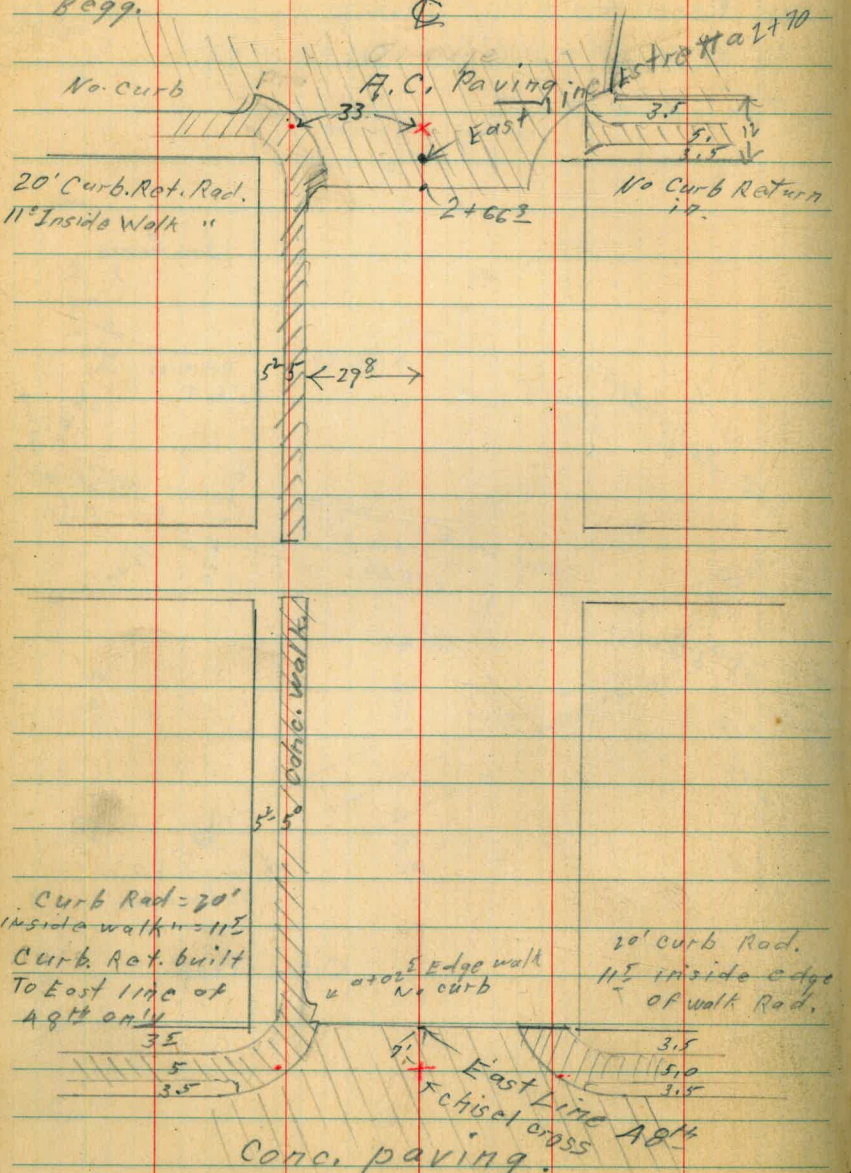


Oct. 1- 1946

Sommermeyer
W. Moore
Begg.

X-Section Orange Euclid to Estrella.

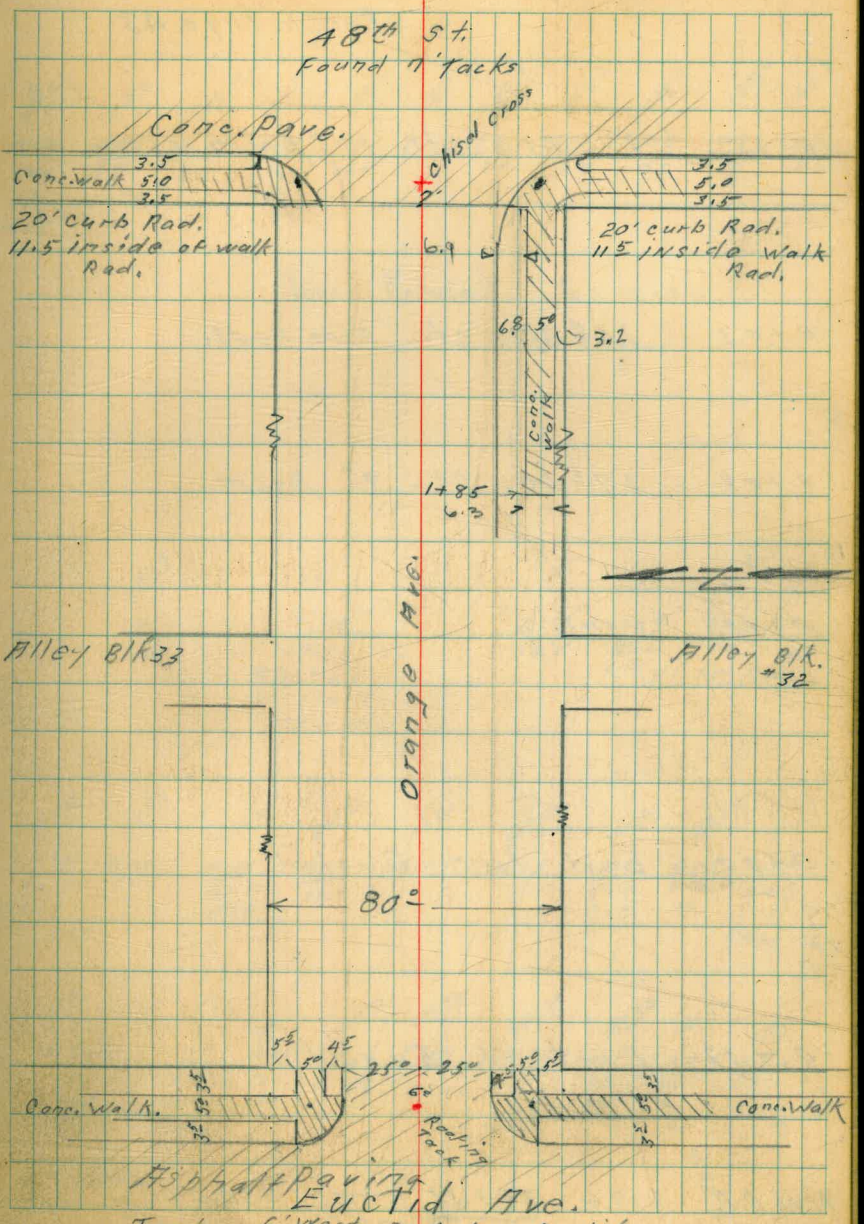
Orange ℄



Ave. - An 80' street. ℄

Indexed
C.S.K.

43



Tacks 6' West. East Line Euclid.
+ 7' off Lines on orange

Orange Ave — Euclid

Sketch. Page 43

0+25 — 27.2 Rt = ctr. 10" palm tree — 349.3 / 4.2 / 40

0+05 — 26½ Rt. = ctr. Fire Hydt.

0+02 = 27½ Lt = ctr. 9" palm

0+00 — cont.

0+00 = East line Euclid

0 — 12 — East cb. Euclid

N.W.B.P.	2.86	353.55	—	350.69	Euclid & orange

Going East — ctr 1+05

East — Lt = North — ℄ orange — Rt = South — 44

349.41	348.8	348.6	347.5	348.2	348.4	347.9	347.3	348.7	348.6	347.3
4.1A	4.7	4.9	6.0	5.3	5.1	5.6	6.2	4.8	4.9	6.2
39.3	39	26	24	12.5		12.5	24	26	40	42
0.7 wall										

Notes Reduced 10-10-46 mhenry

	349.8		350.01			349.7	/	348.4	348.9	
	3.7		3.54			3.8	39.7	5.1	5.1	
	40		39.3 = Start 0.5 Conc wall Top wall			37.5	wast and picket Fence	40	45	
349.78	349.50	348.89	349.33	349.56		349.40	348.53	349.51	349.97	
3.77	3.97	4.66	4.22	4.05		4.15	4.62	4.03	3.58	
34.6 INSIDE Edge walk	25.1 Top Cb.	25.1 Out	12.5			12.5	24.8 Out.	24.8 Cb.	31.7 Inside Edge walk	
349.16	349.59	349.50	349.91	349.98		349.88	349.44	349.71	349.21	
1.39	3.96	4.05	3.64	3.57		3.66	4.11	3.83	4.34	
37 Out.	35 Top Cb. Rot. BC.	25 Cb. Brick	1/4			1/4 12.5	25 Cb. Brick	35	37 Out	

353.55

Top Cb. Rot. BC

0+97	27½ Rt = ctr. 9" palm tree
0+96	Lt. = ℄ 2 car. Gar. with conc. Apron & Floor
0+73	26.9 Rt = ctr. 9" palm
0+63	37.0 Lt. = End 6". conc. Wall
0+50	
0+48	38½ Lt. = ℄ 3' walk with 2. steps
0+40	27° Lt = ctr. 12" tel. Pole.
0+31	27½ Rt = ctr. 16" power pole

353.55

Lt ℄ Rt

346.94 — 6.61 — A1.5 Floor

346.11 — 6.84 — 40.5 Apron

348.94 — 4.61 — 37

349.1	348.9	347.7	346.7	347.4	347.6	349.0	346.1	347.6	347.6	346.1
4.4	5.6	5.8	6.8	6.1	5.9	6.5	7.4	5.9	5.9	7.4
40	39	46	24	11.5		12.5	24	46	42	42

349.14 — 4.41 — 37.1 Top 2nd step

348.64 — 4.91 — 38.1 Top 1st step

353.55

1+51 27² Rt = ℄ 2³ Conc. walk

1+45 36.9 Lt = 50. End. N+S. slat fence.

1+35 = ℄ Alley.

1+25 39° Lt. = End board + wire fence

1+24 { 27.5 Rt = ctr. 12" p. pole
25.9 Lt = ctr. 12" Tel. pole

1+22 26⁸ Rt. = ctr. 10" palm

1+05 39° Lt = start board + wire fence

1+00 40° Rt. = End picket fence

353.55

Lt. = No. ℄ orange Rt. = South

344.66 8.89 27.3 End walk

344.68 8.87 ℄ on walk

345.2 8.3 40

344.7 9.3 23

344.8 8.7 12.5

345.1 8.9

344.9 9.1 12.5

344.1 9.4 25

344.5 9.0 40

346.9 6.6 40

346.6 6.9 39

345.9 7.6 37

345.7 8.3 23

345.8 7.7 12.5

345.9 7.6

345.4 8.1 14.5

344.6 8.9 24

345.9 7.6 25

345.8 7.7 40

353.55

2+34 41.6 Lt = ℄ 6" wide Double Ribbon Dr. 2' Ribbons

2+21 41.3 Lt ℄ 7" Conc. Ribbon Dr. 2' Ribbons

2+02 39.9 Lt = ℄ 3' conc walk

1+85 Start of curb & walk on south

1+80 ℄ 6" conc. Ribbon Dr. on Left. 2' Ribbons

1+60 ℄ 3' wide walk on left.

3.49 348.06 8.98 344.57

353.55

Lt.	℄	Rt
344.18		
3.88		
41.6		
344.40		
3.66		
41.3		
344.83		
3.23		
39.9		
344.9	344.4	343.8
3.2	3.7	4.3
40	28	22
343.9	344.2	343.8
4.2	3.9	4.3
12.5		12.5
343.5	344.16	344.44
4.6	3.94	3.62
45	25	36.2
Curb.	Top Dr.	In side walk
344.6		
3.5		
40		
344.88	344.80	
3.18	3.18	
40	37.7	
	5.4 end of drive	
345.41	345.34	
2.665	2.72	
40	39.2	

348.06

2+66 26.8 Lt = Ctr. 12" Tel pole

2+62 Appr. curb B.C. on Rt.

2+60 28.5 Lt. = Ctr. 8" palm

2+53 39.1 Lt = ℄ 3' Conc walk

2+46 28.5 Lt = Ctr. 8" palm

2+40 37.2 Lt = start picket fence

2+35

348.06

Lt. North ℄ Rt. South

343.9	343.5	343.1	343.3	343.3	343.1	342.7	343.31
4.2 / 40	4.6 / 27	5.0 / 25	4.8 / 12.5	4.8	5.0 / 12.5	5.4 / 25 Out	4.35 / 25 tapol.

343.90	343.86
4.16 / 40	4.20 / 39.1

344.7	343.8	343.2	343.4	343.4	343.2	342.9	343.54
3.9 / 40	4.3 / 26	4.9 / 24	4.7 / 12.5	4.7	4.7 / 12.5	5.7 / 25 Out.	4.57 / 25 Ctr. top

348.06

X-Sec. Orange Ave 48th to Estrella.

0-12	East Cb. line 48th				
S.E.B.P. Orange+48	6.42	349.23	—	342.81	See Below this page
orig. B.M. Page 44			1.62	250.70	Start at 250.69
	7.23	252.32	2.97	245.09	
S.E.B.P. Orange + 48.	5.25	348.06	5.25	342.81	← shown in bench book as 342.96
3+82 E	West curb line 48th				
3+70 E	West Line 48th				
		348.06			

Lt. North ℄ Rt South

343.58	343.14	343.01	342.97	342.94	342.82	342.65	342.48	342.89
5.65	6.09	6.22	6.26	6.29	6.41	6.58	6.80	6.34
45 Top Bk. B.C.	45 Cut	25	12.5		12.5	25	45 Gutter	45 Top Bk. B.C.

349.23

343.64	343.15	343.05	343.01	342.98	342.81	342.64	342.46	342.94
4.42	4.91	5.01	5.05	5.10	5.25	5.42	5.60	5.12
45 Top Bk.	45 Cut	25	12.5		12.5	25	45 Cut	45 Top Bk.

343.45	343.01	343.06	343.31	343.29	343.06	342.69	342.56	343.01
4.61	5.44	5.00	4.75	4.77	5.00	5.42	5.50	5.05
Top Bk.	Cut	25	12.5		12.5	25	26.8 Cut	26.8 Top Bk.

348.06

1+05 40.3 Rt = ℄ 3° Conc. Walk.

1+00

0+91 39° Rt. ℄ 6° Wide 2'wide Conc. Ribbon Drive

0+50

0+18 26° Lt. = ctr. 12" Tel. pole

0+05 27° Rt = ctr. Fire Hydt.

0+02.5 End of Flare in walk See Sketch P. 43

0+00 East Line 48th

349.23

Lt ℄ Orange Rt South

344.38
4.85
40.3

344.68 344.2 343.7 344.0 344.1 343.7 343.4 344.0 344.2
4.55 5.0 5.5 5.2 5.1 5.5 5.8 5.2 5.0
29.8 25 23 17.5 12.5 23 27 10
walk

344.12
5.11
39.7

344.10 343.9 343.0 343.5 343.5 343.1 342.9 343.3 343.6
5.13 5.3 6.2 5.7 5.7 6.1 6.3 5.9 5.6
29.8 25 23 12.5 12.5 23 25 40
walk

343.50
5.73
26.5

343.57 343.08 343.08 343.38 343.24 343.04 342.62 342.56 343.02
5.92 5.15 6.15 5.95 5.99 6.19 6.61 6.67 6.21
26.6 26.6 25 12.5 12.5 25 26.7 26.7
top ℄ Out Out Ctr. Top

349.23

1+98 37.7 Rt = ℄ 2° Conc walk

1+85 = ℄ double ribbon drive on Right (63 wide 2° ribbons)

1+51 39.6 Rt = ℄ 4° Conc. walk.

1+45.5 Start of 5° Conc. Walk on No. also Ctr. 12" Tel. pole 27° Lt.

1+24.5 End of 5' walk on North

1+24 27° Rt = ctr. 16" P. pole

349.23

Lt North	℄ Orange	Rt South
		345.32 / 3.91 / 37.7
		345.31 / 3.92 / 40
345.72 / 3.51 / 29.8 walk	344.6 / 4.6 / 24	344.8 / 4.4 / 12.5
	345.0 / 4.2	344.7 / 4.5 / 12.5
	344.9 / 4.8 / 25	344.8 / 4.4 / 27
	345.35 / 3.88 / 37.8 drive	345.30 / 3.93 / 40
345.12 / 4.11 / 39.6		
345.29 / 3.91 / 34.8 N. Edge walk	345.28 / 3.95 / 29.8 S. Edge walk	344.9 / 4.3 / 25
	344.2 / 5.0 / 23	344.4 / 4.8 / 12.5
	344.6 / 4.6	344.3 / 4.9 / 12.5
	343.9 / 5.3 / 25	344.4 / 4.8 / 27
	344.9 / 4.3 / 40	
344.97 / 4.26 / 34.8 N. Edge walk	344.91 / 4.32 / 29.8 S. Edge walk	344.0 / 5.2 / 23
	344.2 / 5.0 / 12.5	344.4 / 4.8
	344.1 / 5.1 / 12.5	343.6 / 5.6 / 24
	344.0 / 5.2 / 25	344.3 / 4.9 / 40

345.3 / 3.4 / 40

345.4 / 3.8 / 40

349.23

S.E. 48th & orange. 6.42 642.81 ok.

Back up to 2+76

349.23

℄ 5' walk to south see sketch P. 43

2+82

4.09 / 55 on pav. No curb

2+70

2+68 26.7 Rt. = Ctr. P. pole.

2+66.3 Start A.C. Paving (Edge Rough)

2+65 26.9 Lt = Ctr 14" P. pole

2+25

349.23

℄ ORANGE

345.95

3.28 / 39.8

346.43 — 280 / 43 / Comb

345.89 — 3.65 / 43 / End Ret. Cut

346.12 — 3.11 / 25

346.23 — 3.00 / 12.5

346.12 — 3.11

345.92 — 3.31 / 12.5

345.53 — 3.70 / 25

344.93 — 4.30 / 45 / End. N+80. Curb. on Estrella

345.75 — 3.48 / 45

346.53 — 2.70 / 26.5 / Top. Ok.

345.73 — 3.50 / 26.5 / Cut.

346.09 — 3.14 / 12.5

346.08 — 3.15

345.81 — 3.42 / 12.5 / Pav

345.30 — 3.93 / 26 / Pav

346.3 — 2.9 / 29

346.5 — 2.7 / 40

346.47 — 2.75 / 25.3 / End Ok. Ret.

345.7 — 3.5 / 25.3 / Cut.

345.9 — 3.3 / 12.5

346.0 — 3.2

345.7 — 3.5 / 12.5

345.2 — 4.0 / 25 / Edge Pav. A.C.

346.2 — 3.0 / 27

346.5 — 2.7 / 40

346.10 — 3.13 / 29.8 / Walk

345.6 — 3.6 / 25

345.0 — 4.2 / 22

345.3 — 3.9 / 12.5

345.6 — 3.6

345.3 — 3.9 / 12.5

344.7 — 4.5 / 25

345.6 — 3.6 / 27

345.7 — 3.5 / 40

349.23

Walker
Hendricks
~~Becker~~
Greer
11-12-46

Cross Section Alleys Blk 105 Univ. Hts.

Between El Cajon & Meade Ave
And " Arizona & Hamilton St.

East & West Alley Sections

BM NE BP El Cajon & Hamilton

429 372.64 368.35

0-2.0

S on cb.	517	367.47
" " Fac.	577	366.87
L " "	571	366.93
N " "	567	366.97
N " cb.	529	367.40

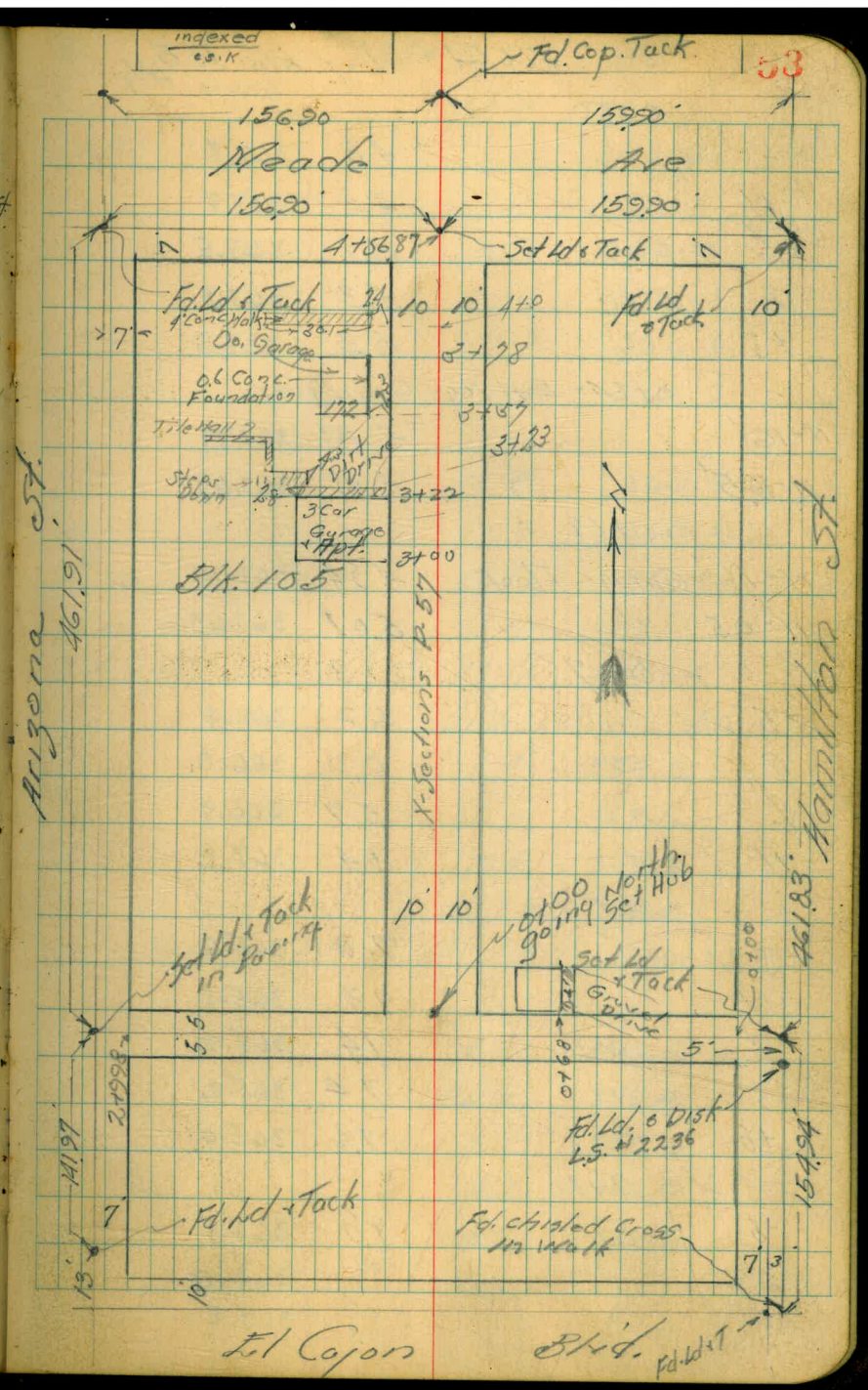
0-01 - End Paving

N cb	476	367.88
N Gut.	494	367.70
L	508	367.56
S Gut.	512	367.52
S. Top cb.	495	367.69

0+10

-S	42	368.4
S	43	368.3
L	43	368.3
N	42	368.4
+S	41	368.5

Reduced and checked by R.E. Coburn 11/19/46



37264 ✓ Alley Blk 10 Univ. 5 Hts.

	0+50		
-5		4.8	367.8
N		4.8	367.8
℄		5.1	367.5
S		5.3	367.3
+5		5.3	367.3
	0+64 - East edge Conc. Apron		
N-16'		4.85	367.79
N-0.5'		4.95	367.69
	0+68		
N-16'	=Garage Floor	4.94	367.70
N-0.5	" "	5.01	367.63
	0+75.		
-5		6.2	366.4
S		6.0	366.6
℄		5.7	366.9
N		5.4	367.2
	1+00		
-5		7.0	365.6
N		7.3	365.3
℄		7.4	365.2
S		7.4	365.2
+5		7.6	365.0
	1+20		
-5		8.5	364.1
S		8.6	364.0
℄		8.8	363.8

37264 ✓

N		9.3	363.3
+5		9.0	363.6
	1+39.9 = Edge of N & South Alley		
N		10.6	362.0
℄		10.5	362.1
S		10.2	362.4
+5		10.3	362.3
	1+49.9		
-5		11.8	360.8
S		12.2	360.4
℄ on Rim MH.		13.76	358.88
N on Hub		13.11	359.53
T.P. 1.05	360.58	13.11	359.53
	159.9' = M.L. North - South Alley		
N		1.4	359.2
℄		2.0	358.6
S		2.4	358.2
+5		1.8	358.8
	1+61.5 = P.P. on Lt 1.3 in Alley = ℄ Pole		
	1+72		
-5		4.1	356.5
S		4.0	356.6
℄		4.2	356.4
N		4.1	356.5
+5		4.1	356.5

360.58 Alley Blk. 105

	Ultim. Hts.	
1+25		
-5	7.1	353.5
N	7.1	353.5
℄	6.5	354.1
S	6.0	354.6
+5	6.5	354.1
2+00 = Beg. Paved yard on South		
-1' on Paving Asphalt	10.26	350.32
S " " Asphalt cb	9.53	351.05
S +0.1	8.1	352.5
℄	7.0	353.6
N	7.7	352.9
+5	7.7	352.9
2+25		
-5	10.6	350.0
N	10.1	350.5
℄	10.0	350.6
S℄ Asphalt cb.	10.17	350.41
+1 on " Pav	10.68	349.90
2+35		
S on Asphalt cb	10.62	349.96
℄	10.8	349.8
N	11.1	349.5
+5	11.1	349.5
2+37.5 = Back of Gar on N Entrance Arizona St. West		
-5	13.4	347.2
N	11.7	348.9
℄	11.7	349.4
S on Asphalt cb	10.79	349.79

2+50 = West end Paved yard on South		
-1' on Pav.	11.15	349.43
S on Asphalt cb	11.21	349.37
+2	12.7	347.9
℄	13.1	347.5
+3	13.1	347.5
N	13.8	346.8
+2.6 at Garage	14.1	346.5
T.P 0.42 348.16 12.84 347.74 Nail in Pole 2+62		
2+54		
-8.6 = ℄ Garage Arizona St Entrance	2.32	345.84
-2.6	2.3	345.9
N	1.7	346.5
℄	1.3	346.9
S	1.0	347.2
+5	1.1	347.1
2+57.7 = ℄ 2' Conc. Walk on South 1.4' South of Shine on Walk 1.4' Back	1.52	346.64
T.P 0.17 347.91 0.42 347.74 Nail in Pole.		
2+67		
-5.5 on Ribbon Drive	3.40	344.51
N	3.4	344.5
℄	3.1	344.8
S	3.1	344.8
+2	3.0	344.9

34791 ✓ Alley Blk 105 Univ. Hts.

2+86		
-2	5.1	342.8
S	5.0	342.9
℄	4.9	343.0
N	4.8	343.1
5.5 on Ribbon Drive	4.76	343.15
2+99		
-5.5 on Ribbon Drive	6.83	341.08
N	7.3	340.6
℄	7.3	340.6
S	7.3	340.6
+N	7.2	340.7
2+99.8		
S cb.	7.69	340.22
Gut	7.87	340.04
℄	7.95	339.96
Gut.	7.82	340.09
N cb	7.65	340.26
3+13.8		
N cb	8.12	339.79
Gut	8.57	339.34
℄	8.65	339.26
S Gut	8.64	339.27
S cb	8.17	339.74
T.P. 2.05 350.21 ✓	6.75	341.16 ✓
Chk BM. NW 7 Tuck Meade & Arizona	8.20	342.01 ~ 342.09 (340.05 = Record, 0.04 = diff.)

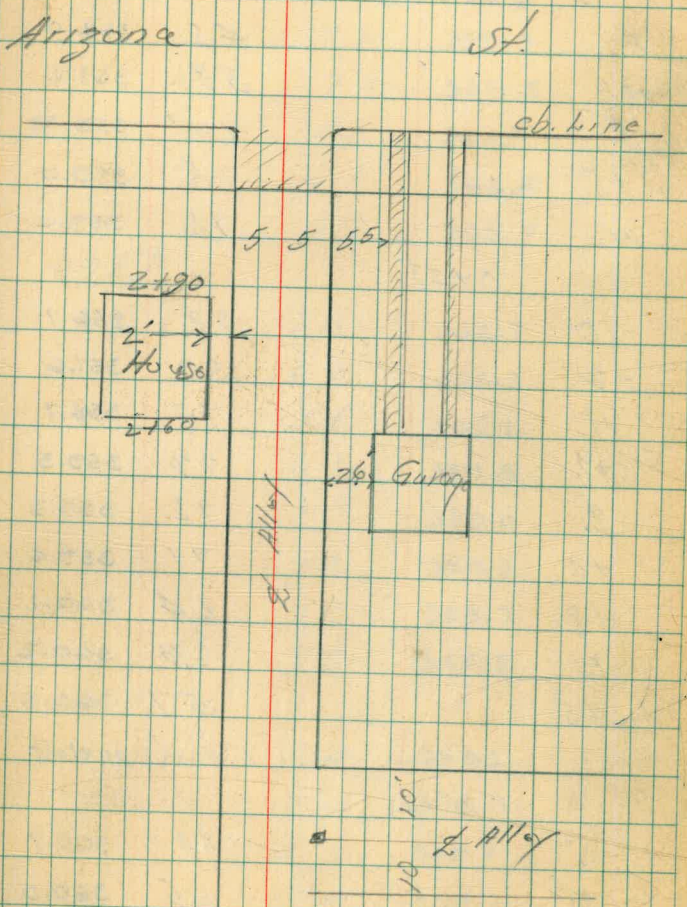
350.21 ✓

56

T.P. 12.35 361.71 ✓ 0.85 349.36 ✓ (See Page 61 for check)

On Lot 6 Tuck 4+56.87 225 359.46 → 57

Sketch P. 53



Walker
Hendricks
Becker
Greer
11-14-46

X-Section North & South
Alley Blk 105 Univ. Hts.
Sketch Page 53

7.01 366.54 ✓ 359.53 BM on Hub 1+49.9 P.54

0+00 = N. Line East & West Alley

E.		4.5	362.0
+3		5.3	361.2
℄		7.01	359.53
+5		7.5	359.0
W		7.5	359.0
	0+25		
-10		9.8	356.7
-2		8.9	357.6
W		7.8	358.7
+3		7.2	359.3
℄		7.2	359.3
+4		7.1	359.4
+8		6.4	360.1
E		6.3	360.2
+5		5.7	360.8
	0+26 = Pole	1' Back	on West
	0+35		
-5		5.8	360.7
E		6.5	360.0
℄		7.6	358.9
+7		7.6	358.9
W		8.3	358.2
+10		9.7	357.3

0+50? 366.54 ✓

57

-10		9.2	357.3
-2		8.3	358.2
W		7.4	359.1
+3		7.0	359.5
℄		7.2	359.3
+3		7.0	359.5
+6		4.8	361.7
E		4.1	362.4
+5		3.8	362.7
	0+77		
-5		3.8	362.7
E		4.2	362.3
+2		4.4	362.1
+6		6.7	359.8
℄		7.5	359.0
+7		7.3	359.2
W		7.8	358.7
+10		9.3	357.2
	1+00		
-10		9.2	357.3
W		8.2	358.3
+2		7.8	358.7
℄		7.8	358.7
+5		7.4	359.1
E		6.7	359.8
+2		5.7	360.8
+5		5.5	361.0

366.54 ✓ Alley Blk 105 Uptn. Alts.

1+05 = Beg. 4 Car Garage on W 6.5' Back

W -6.5' on Conc. Walk	8.92	357.62
W-4.5 " " " = Edge	8.89	357.65
1+14.5 = Pole 1' Back		
1+15 = Beg. Conc. Apron to 4 Car Garage on W		
W-6.5 = Gar. Floor	8.94	357.60
-4.5 = ℄ Valley Gut	9.08	357.46
-1.3'	8.57	357.97
W	8.4	358.1
℄	8.2	358.3
+5	8.1	358.4
+6	7.1	359.4
E.	3.3	363.2
+1 at Shed	3.3	363.2
1+29 = ℄ 16" Pepper Tree 1.3' in Alley		
1+47 = N and 4 Car Garage on W		
E	6.2	360.3
+5	7.0	359.5
+8	8.0	358.5
℄	8.1	358.4
+7	8.0	358.5
W	8.4	358.1
+1.3' = Toe Apron	8.60	357.94
+4.5 = Valley Gut	9.21	357.33
+6.5' = Garage Floor	9.00	357.54

366.54 ✓ Conc. Floors

1+52 = Beg. 4 Car Garage on W 6.5 Back

-6.5' on Gar. Floor	8.93	357.61
-5 = Valley Gut	9.05	357.49
-1.6 = Toe Conc. Apron	8.38	358.16
W	8.2	358.3
+3	7.9	358.6
℄	7.8	358.7
+3	7.6	358.9
+5	6.7	359.8
E.	5.8	360.7
1+86 = N and Conc. Apron on West		
E+1	5.3	361.2
+4	6.6	359.9
+7	7.4	359.1
℄	7.6	358.9
+7	7.8	358.7
W	8.1	358.4
+1.6' on Conc. Apron	8.41	358.13
+5' " Valley Gut	9.05	357.49
+6.5 " Conc. Floor	8.91	357.63
1+94 = N. end 4 Car Garage on W		
W-4.5' on Conc. Walk	9.11	357.43
2+00		
-10	9.8	356.7
W	8.6	357.9
+3	7.3	359.2

366.54 ✓ Alley Blk 105 Univ Hts

℄	7.4	359.1
+2	7.3	359.2
+6	6.9	359.6
E	5.3	361.2

Ends of shed on line ℄ = 1+75 to 2+00 = Shed on E. 1' in Alley

2+15

-5	1.5	365.0
E.	2.4	364.1
+3	3.3	363.2
℄	6.0	360.5
W	6.7	359.8
+10	8.5	358.0
+15	10.5	356.0

2+35 = Pole on W. 1' Back

2+44.5 = ℄ M.H. Rim = 370		362.84

2+50

-20	11.1	355.4
-12	10.5	356.0
-8	7.3	359.2
W	4.6	361.9
+2	4.0	362.5
℄	4.0	362.5
+4	3.3	363.2
+6	2.0	364.5
E.	1.6	364.9
+5	1.4	365.1

366.54 ✓

59

2+60

-5	0.2	366.3
E.	0.5	366.0
+5	3.7	362.8
℄	4.2	362.3
W	4.2	362.3
+9	7.9	358.6
+12	10.2	356.3
+19 at House	10.2	356.3

2+66

+19	10.2	356.3
+12	10.2	356.3
+9	8.3	358.2
W	4.5	362.0
+2	4.0	362.5
℄	4.3	362.2
E	3.7	362.8
+1 at Garage	3.7	362.8
2+72 = ℄ Garage on E.	3.71	362.83 1' Back Conc. Floor

2+78

E. -1'	3.7	362.8
℄	4.1	362.4
+8	4.1	362.4
W	5.0	361.5
+4	6.8	359.7
+10	8.4	358.1
+12	9.6	356.9
+17 on Walk	10.41	356.13

366.54 ✓

3+00 = South edge Apt. over 3 Car Garage House on W on Line

-10	2.5	357.0
W.L. at Bld	4.8	361.7
+2	3.9	362.6
℄	3.7	362.8
+3	3.4	363.1
+6	2.4	364.1
E.	1.2	365.3

See Sketch P53

3+22 = N End Apt. on W over 3 Car Gar.

E.	2.0	364.5
+3	2.6	363.9
+7	4.2	362.3
℄	4.5	362.0
W	4.3	362.2
W on Top 8" Conc. Tile Wall	3.74	362.80
+ 0.7' Toe Conc. Apron	8.34	358.20
+10 = Floor Dble Gar.	10.1	356.4

Floor First Garage

3+36 = N end 8" Conc. Tile Wall on West.

W - 0.7'	7.1	359.4
W on Wall	3.74	362.80
+1	5.6	360.9
℄	5.3	361.2
+3	5.1	361.4
E.	3.7	363.3
+1.5 at Bld	3.0	363.5

366.54 ✓ Alley Blk 105 Univ. Hts.

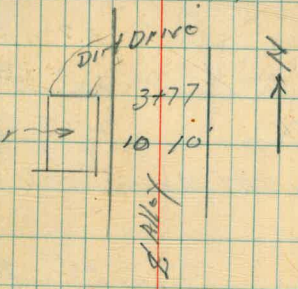
3+50

-1.5 at Bld	4.1	362.4
E	4.1	362.4
+3	4.6	361.9
+6	5.8	360.7
℄	5.8	360.7
W	6.5	360.0
+10	7.5	359.0

3+54 = Pole on W 0.3' in Alley

T.P. 552 2654 ✓	6.62	359.92 ✓
3+77	7.47	357.97

Floor Garage



-4	7.4	358.0
W	5.9	359.5
+3	5.1	360.3
℄	5.1	360.3
+4	5.0	360.4
+6	3.9	361.5
E. at Fence	3.2	362.2

4+00

E.	3.1	362.3
+4	3.6	361.8

36544 ~

+8	4.6	360.8
℄	5.0	360.4
+7	5.1	360.3
W	5.6	359.8
+5	6.0	359.4

4+02 = ℄ 4' Conc. Walk on W Back 2.2'

W-2.2 = ℄ Walk	5.57	359.87

4+75

-2	5.6	359.8
W	5.3	360.1
℄	4.6	360.8
+5	3.2	362.2
E	2.5	362.9
+2.1' on Walk	2.25	363.19
	2.17	363.27

4+42 N end Above Walk

4+45

-2	2.3	363.1
E	2.5	362.9
+5	3.8	361.6
℄	5.4	360.0
W	5.9	359.5
+2	6.2	359.2

4+49.87 = 5L Meade

W-0.9' = W cb	6.30	359.14
" on Gut	6.38	359.06
℄	5.85	359.59

36544 ~ Alley Blk 105 Univ. Hts. 61

E. +0.25 = E. Gut	4.80	360.64
" on Top cb.	4.34	361.10

4+63.87

E. cb.	4.37	361.07
E Gut	5.00	360.44
℄	6.10	359.34
Gut	7.12	358.32
Top cb	6.56	358.88

4+23 = ℄ 8" Apricot Tree on East 0.5' Back = = West edge.
This property owner circulated Petition for Boring, and is very anxious to save this Tree

4+56.87 chk Tack P-56 5.99 359.45 ~
359.46
0.01

Walker
Hendricks
Baker
Greer
11-14-46

Cross Section 20' Alley Blk 70
Univ. Hts.
Between Arizona & Hamilton
from Meade to Monroe Ave.

BM on Tack
4+56.87
P-61

6.41 365.87 359.46

0-14 = N cb Meade

E. Top cb.	3.68	362.19
E. Gut.	4.45	361.42
℄	5.70	360.17
W "	6.78	359.09
" Top cb	6.27	359.60

0+00 = N.E. Meade

W cb.	6.06	359.81
" Gut.	6.09	359.79
℄	5.31	360.56
E. Gut.	4.06	361.81
E. cb.	3.64	362.23

0+25

E-2	2.6	363.3
E	3.9	362.0
+2	5.0	360.9
℄	5.5	360.4
W	5.8	360.1
+0.8 on Walk	5.68	360.19

0+52

-0.8 on N. end Walk	5.45	360.42

Reduced and checked by R.E. Coburn 11/19/42

Indexed C.S.K.

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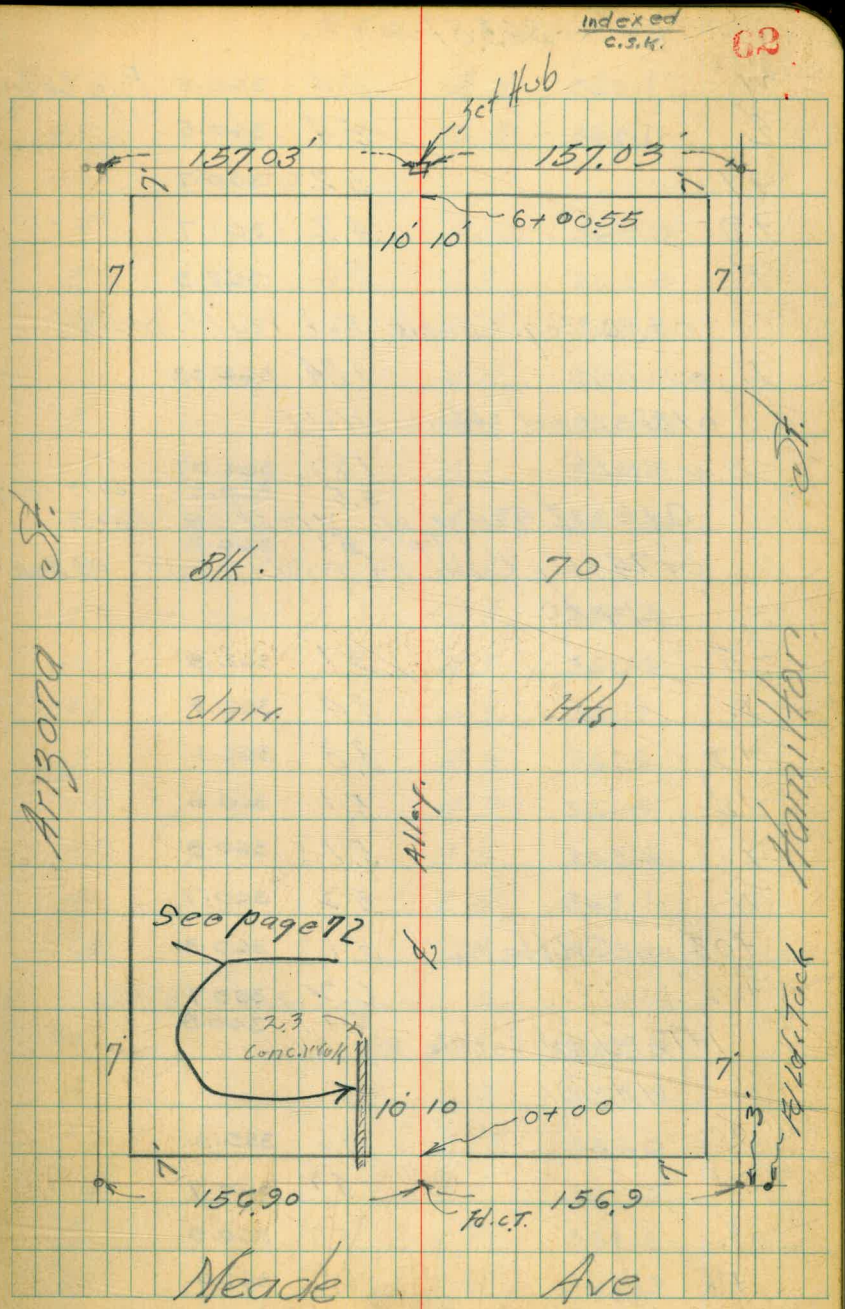

36587

W	5.4	360.5	Pole on W side
℄	5.4	360.5	
+7	5.2	360.7	
+9	4.2	361.7	
E	3.6	362.3	
0+50 = Beg. Cobble Rot Wall on E			
E on Top	1.84	364.03	
0+88 = Head Above Wall			
E on Wall	1.80	364.07	
	5.5	360.4	Dirt Floor
0+60 = ℄ Garage on West 4' Back			
	Top = 5.1	360.8	
0+74 = Beg Cobble Rot Wall on W. 0.9' Back			
1+00			
-5	3.1	362.8	
E	3.4	362.5	
+2	3.8	362.1	
+4	5.1	360.8	
℄	5.1	360.8	
W	5.2	360.7	
+0.3 on Cobble Wall	5.1	360.8	
+2	6.2	359.7	
1+12 = Head Cobble Wall	5.1	360.8	
1+50			
-10	6.6	359.3	
W	5.2	360.7	
℄	5.0	360.9	
+6	4.9	361.0	
+8	3.1	362.8	

36587 Alley Blk. 70

E	2.8	363.1
+8	2.8	363.1
2+00		
-5	3.0	362.9
E	3.1	362.8
+1	3.5	362.4
+6	4.8	361.1
℄	5.0	360.9
W	5.1	360.8
+1 of Bld	5.3	360.6
2+50		
-2.3 of Shed	6.7	359.2
W	4.5	361.4
+1	4.2	361.7
℄	4.3	361.6
+5	4.3	361.6
+7	3.5	362.4
E	2.8	363.1
+4	2.8	363.1
2+76 = Pole on W 2.1' in Alley		
-5	2.0	363.9
E	2.0	363.9
+2	1.9	364.0
+4	3.4	362.5
E	3.7	362.2
W	3.6	362.3
+5	4.6	361.3

365.87

T.P. 3+00 ℄ MH Rim 3.32			362.55
9.88	372.43		
3+00			
-10		12.2	360.2
-2		11.8	360.6
W		10.4	362.0
+2		10.0	362.4
℄		9.9	362.5
+6		9.5	362.9
+8		8.3	364.1
E		7.7	364.7
3+50 End Board Fence			
E		7.2	365.2
+3		8.0	364.4
+5		9.1	363.3
℄		9.5	362.9
W		9.6	362.8
+5		10.3	362.1
3+80=5 end Dble Garage on E			
-5		9.6	362.8
W		8.9	363.5
+2		8.5	363.9
℄		8.4	364.0
+5		7.9	364.5
E		7.4	365.0
+6.5=Toe Apron		7.25	365.18

372.43 Alley Blk 70 Univ. Hts.

E +10.5=Garage Floor	6.18	366.25
3+94=N end Above Garage		
Flour	6.21	366.22
Apron	6.83	365.60
4+00		
-5	7.0	365.4
E	7.1	365.3
+2	7.3	365.1
+3	7.8	364.6
℄	8.0	364.4
+8.3=Pole		
W	8.0	364.4
+2	8.0	364.4
4+02=Beg. Cottage on W 2' Back		
W +2 on Ground	8.5	363.9
+2' on Wall	7.47	364.96
4+19=N end Above Cottage		
-2' on Wall	7.61	364.82
-2 " Ground	8.2	364.2
	8.33	364.10 2.4' Back
4+21=℄ 3' Conc Walk on West		
4+30=℄ Garage on W		
-1.8' on Conc Wall	8.27	364.16
W +1.2' Toe Apron	8.37	364.06
℄	7.9	364.5
+6	7.5	364.9
+8	6.6	365.8
E	6.3	366.1
+24	6.1	366.3

37243 ✓

4+37 = ℄ Garage on W Conc Floor		
℄ +8.8 = Toe Apron	8.35	364.08
W +1.8 = Garage Floor	8.2X	364.19
4+40		
W -1.8 Floor	8.31	364.12
W +1.2 Toe Apron	8.37	364.06
+5	7.8	364.6
℄	7.4	365.0
+6	6.9	365.5
E.	6.1	366.3
+2 of Fence	6.0	366.4
4+50		
-2	5.5	366.9
E.	5.5	366.9
+1	6.2	366.2
℄	6.6	365.8
+4	6.7	365.7
W	6.3	366.1
+3	7.1	365.3
4+80		
-5	6.2	366.2
W	5.6	366.8
+2	5.1	367.3
℄	4.7	367.7
E.	4.4	368.0
+2	4.4	368.0

37243 ✓ Alley Blk 70-4min. N 85

4+94 = ℄ Garage on W, dirt Floor 3.2' Back		
" Floor = 5.3	367.1	= Beg. Conc. Apron
5+00 = Pole on W 2.5' in Alley		
-1.7 on Apron	3.28	369.15
E.	3.8	368.6
+2	4.3	368.1
℄	4.8	367.6
W	4.9	367.5
+3	5.1	367.3
5+07 = ℄ Garage on East 5.4' Back		
E-5.4 on Conc. Floor	2.48	369.95
-1.7 " Toe Apron	3.26	369.17
5+13 = W end Apron	3.25	369.18
5+25		
-5	4.5	367.9
-3	4.4	368.0
-2	3.9	368.5
W	2.9	369.5
+4	4.3	368.1
℄	4.2	368.2
+5	4.0	368.4
E.	3.3	369.1
+1.4 at Fence	2.8	369.6
5+45		
-1.4	2.3	370.1
E.	2.5	369.9

37243

E+3	3.1	369.3
+5	3.5	368.9
℄	3.8	368.6
+6	3.7	368.7
+8	3.4	369.0
W	3.1	369.3
+2	3.4	369.0
+3	4.0	368.4
+5	4.1	368.3
5+50		
-5	4.3	368.1
W	4.1	368.3
+4	3.6	368.8
℄	3.6	368.8
+6	3.4	369.0
E	2.6	369.8
+14	2.3	370.1
5+56.4 = ℄ 2' Conc Walk on W	2.8 Back	
W-2.8' on Walk	4.39	368.04
5+70		
-2.8 at House	3.6	368.8
W	3.6	368.8
+3	3.4	369.0
+4	2.8	369.6
℄	2.6	369.8
+6	2.4	370.0
E	2.0	370.4

37243 Alley Blk 70-Univ. Hts. 65

E+2.3 at House	2.0	370.43
5+90		
E	1.9	370.5
+4	2.4	370.0
℄	2.9	369.5
+8	3.1	369.3
W	3.5	368.9
+2.4	3.5	368.9
6+00.55 = SL. Monroe		
W+0.3 = W cb	3.50	368.93
Gut. Ground	3.8	368.6
℄ on "	3.4	369.0
+6	3.1	369.3
E Gut	2.4	370.0
E cb.	2.38	370.05
6+14.55 = S cb. Mo. Mon		
E cb.	2.65	369.78
Gut	3.6	368.8
℄	4.0	368.4
W	4.3	368.1
W cb	3.89	368.54
6+07.55 on ℄ Mk. b	3.89	368.54
T.P 895 377.49 Monroe & Hamilton	3.89	368.54 ✓
cbk. 55.80	2.21	375.28 ✓
		375.30 - Record
		-.02

Walker
Hendricks
Backer
Greer
11-14-46

Cross Section 20' Alley - Univ. Hts
Blk 54.
Between Hamilton And Oregon
from Monroe to Madison

6.45 381.75 ✓ 375.30 BM. S.F. BP Monroe & Hamilton

0 - 14 - N. cb. Monroe Ave

E. cb.	4.63	377.12
" G.t Ground	5.2	376.6
L "	5.2	376.6
W " "	5.4	376.4
W Top cb	4.68	377.07

0+00 = N.L. Monroe Ave

W +0.3 on W cb	4.51	377.24
G.t. Ground	4.7	377.1
L "	4.9	376.9
E. G.t "	4.7	377.1
E Top cb	4.45	377.30

0+00 to 0+50.5 = Picket fence on W/L 0.75' in Alley 0.25' in Alley

0+25

E-1	4.2	377.6
E	4.2	377.6
L	4.4	377.4
W	4.2	377.6

0+44 = L Gurge on E

L +2.8 = Toe Apron	3.91	377.84
E +1.4' = Brk on "	3.74	378.01
E +3.5' on Conc. Floor	3.46	378.29

Reduced and checked by R.E. Coburn 11/19/46

Indexed c.s.k.

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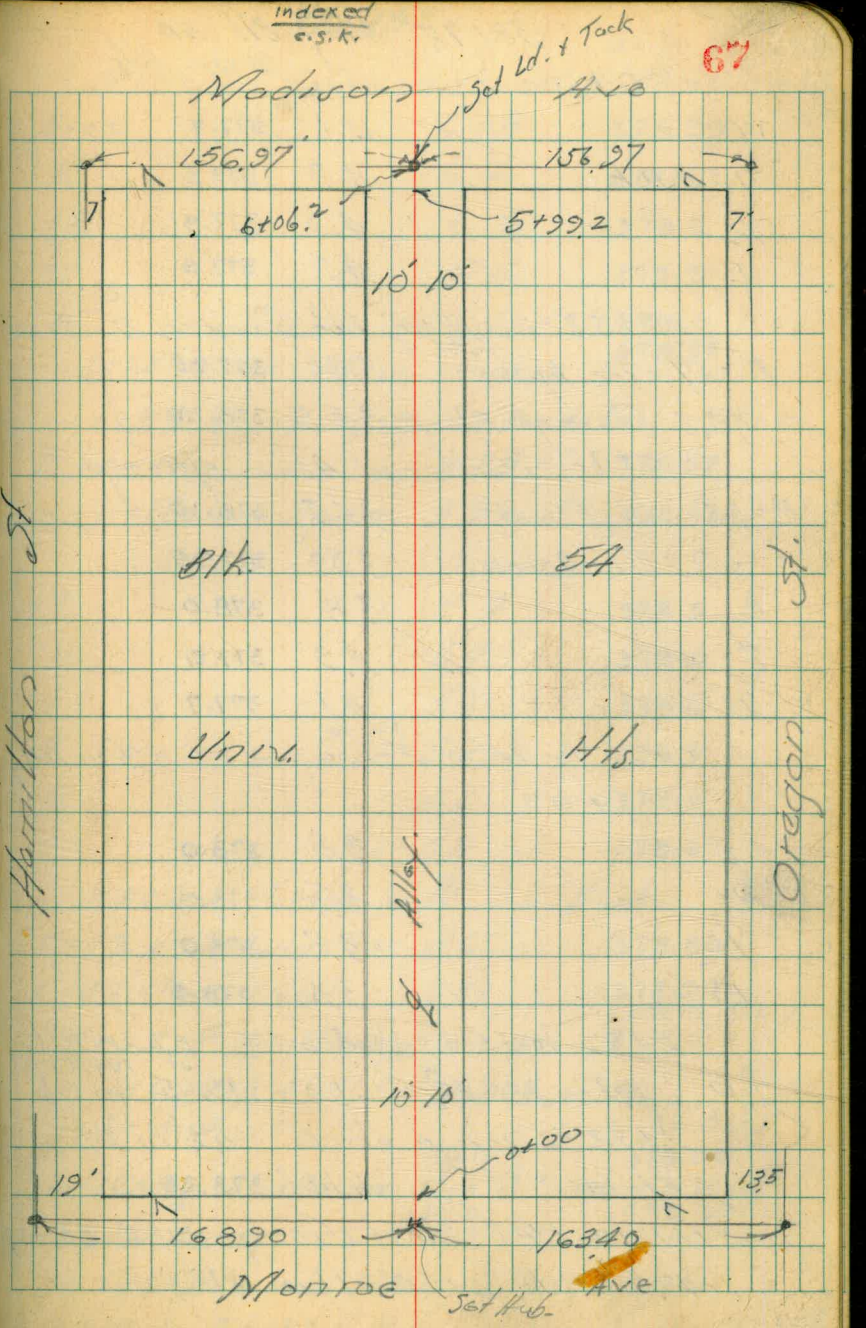


38175 Alley Blk 54 Univ. Hts.

0+50			
W		4.1	377.7
+13 = Pole		4.3	377.5
C		4.0	377.8
E		4.0	377.8
0+52 = South edge Dble Garage on E. Conc. Floors			
E-0.7 = Toe Apron		3.80	377.95
-3.5 Garage Floor		3.55	378.20
0+72 = North end Above garage			
E-3.5' on Floor		3.65	378.10
"-0.7 = Toe Apron		3.80	377.95
E		3.8	378.0
C		3.9	377.9
W		4.1	377.7
0+50 to 1+00 Wire Fence on W 0.3' in Alley			
1+00			
-5		3.8	378.0
W		3.8	378.0
C		3.8	378.0
E		3.8	378.0
0+82 to 1+00 = Shed on E 0.2' in Alley			
T.P.	4.77 384.42	2.10	379.65 Nail in Pole
1+32 = C Garage on E 0.2' in Alley			
Floor		6.14	378.28
1+17 to 1+48 = Shed & Garage on E. 0.2 in Alley			
1+49.5 = Pole on W 1.1 in Alley			

38442 0.2 in Alley

1+50 = Beg. 3' Conc. Walk on E Parallel to Alley			
E+02		6.03	378.39
E		6.2	378.2
+6		6.2	378.2
W		5.5	378.9
+5		6.1	378.3
1+74 = N end Above	58N Walk		378.57
1+93 = C Garage on E 3' Back Conc Floor			
E-3' = Floor		5.85	378.57
E-1' = Toe Conc. Apron		5.99	378.43
2+00			
-5		5.9	378.5
W		5.4	379.0
+4		5.8	378.6
C		5.9	378.5
E		5.6	378.8
+3		5.8	378.6
2+05 = C Garage on E. 32' Back			
E-3.2' = Toe Conc. Floor		5.62	378.80
E-4.2' = Conc. Floor		5.48	378.94
2+05 = C 12' Garage on W. St. Ent. - 0.3 in Alley			
1+50 = Beg. 4' Picket fence on W 0.2' in Alley			
2+00 = E " " " " 0.2 Back			
2+12 = Beg 5.8' Wide Conc Slab Porch on West 0.3' Back		5.33	379.09
2+48 = End " " Conc Slab Porch West 0.3' Back.		5.22	379.20
2+45 = Pole on West 1' in Alley			
2+12 to 2+48 = 4' Picket fence on W. 0.3' in Alley			

2+48 = ℄ 2' Conc. Walk on E 0.2' Back			
on Walk		5.25	379.17
2+50			
-5		5.7	378.7
E.		5.4	379.0
℄		5.7	378.7
W		5.5	378.9
		5.3	379.1
2+55 = ℄ Gurage on W 1.3' Back			Dirt Floor
2+79 ℄ Gurage on W 2.5' Back			
Dirt Floor		5.3	379.1
2+50 to 3+00 = 6' Picket Fence on E. on Line			
3+00			
-5		5.7	378.7
W		5.3	379.1
℄		5.3	379.1
E.		5.2	379.2
+5		5.4	379.0
3+08 = ℄ Gurage on W		Conc. Floor.	
W-0.3' = Toc Conc Apron		5.39	379.03
W-9.4 = Gurage Floor		5.31	379.11
3+28 = ℄ Gurage on E Conc. Floor			
E-0.3' Toe Conc Apron		5.25	379.17
E-3.3		5.07	379.35
3+49 = Pole on W 1' in Alley.			
3+50			
-5		5.3	379.1
E.		5.1	379.3

℄		5.3	379.1
W		5.1	379.3
+3		5.1	379.3
3+57 = ℄ Gurage on West 3' Back			
W-3' = dirt Floor		5.0	379.4
3+74 = ℄ Gurage on E. Conc. Floor			
E-3.7 = Toc Conc. Floor		5.02	379.40
E-4.7 = Main " "		4.94	379.48
4+00			
-5		5.0	379.4
E.		4.8	379.6
℄		5.1	379.3
W		5.1	379.3
+5		4.9	379.5
4+07 = ℄ Garage on E 3.5' Back.			
Rubble Floor		4.59	379.83
4+14 to 4+49 = 5' Board Fence on E. on Line			
4+49 = Pole on W 1' in Alley			
4+50 = Beg. Conc Ret Wall West on Line			
-5		4.9	379.5
W		4.8	379.6
℄		4.8	379.6
E.		4.6	379.8
(West on Wall)		4.31	380.11
4+98.5 = N. end Above Wall			
West on Wall		4.31	380.11
" " Ground		4.5	379.9
Above Wall has 3' Wire Fence			

38442 Alley Blk 54- 2/17/14 Hts

5+00

S	4.7	379.7
W	4.5	379.9
℄	4.5	379.9
+4	4.5	379.9
+6	4.1	380.3
E	4.2	380.2
+5	4.5	379.9

5+05 = ℄ Garage on E on Line

Dirt Floor	4.3	380.1

5+18 = Beg. Dble Garage on W 4.5 Back

W-0.2 Toe Apron	4.11	380.31
W-4.2	4.11	380.31
5+22.5 = ℄ Garage Floor	3.98	380.44

5+38 = N end Above Garage

W-0.2 = Toe Apron	4.04	380.38
W-4.2 = Floor	3.99	380.43

5+49 = Pole on W 0.5' in Alley

5+50

W	3.7	380.7
℄	4.1	380.3
+8	4.2	380.2
E	4.0	380.4

5+85

E	3.9	380.5
+4	4.3	380.1

℄	4.4	380.0
+8	4.1	380.3
W	3.8	380.6

5+99.2 = SL. Madison

W+0.1' on Sh.	4.25	380.17
" " Gut. Bur.	4.57	379.85
℄ on Bur.	4.74	379.68
+9.9" Gut.	4.43	379.99
	4.11	380.31

6+13.2 = S Cb. Madison Ave.

Cb.	4.29	380.13
E Gut.	4.77	379.65
℄	4.86	379.56
W Gut.	4.90	379.52
Cb.	4.66	379.76
T.P. 482 384.43	4.81	379.61 on Ldl Plg. 6+06.2
Chk SS.BP Madison & Hermitage	5.39	379.04

378.99 - Record
0.05 = Error

Additional Levels North & South Alley
Block 105 University Hts.
Sketch Page 53 W.O. #1823

1+40 = Sly Conc Walk on West					
BM		457	359.45 ✓	2+47 1+56.87	
2+78 = Hly Do. Garage on West					
TP	3.77	361.02 ✓	5.32	360.25 ✓	
3+57 = Sly Do Garage on West					
3+50					
3+86					
3+23 = Hly Conc Apron on West					
BM	6.11	365.57 ✓		359.46	2+47 1+56.87

Dec. 15-46
Sisson
McCol
Waddel
Allen

Lt : W

Indexed
C.S.K.

71

354.6 9.4 5.0

357.07 6.85 4.25 = Sly Conc Walk Ground

358.4 5.6 4.5 = Ground

358.69 5.33 4.5 = Sly Conc Walk

359.7 4.3 1.3 Ground

359.87 4.15 1.4 = Sly Conc Walk

356.18 7.84 4.5 = Sly Conc Steps Down

357.76 6.26 2.61 = Hly Conc Apron

358.07 5.95 1.4 = Sly Conc Apron

359.99 4.03 1.35 = Nly Top Foundation Conc Garage

360.4 3.6 1.0

360.2 3.8

364.02 ✓

354.1 11.5 5.0

356.7 8.9 4.3

358.7 6.9 2.5

361.61 3.96 1.23 = Sly Conc Ground of Garage

359.9 5.7 1.0

360.4 5.2

358.01 7.56 4.6.6 = Hly Top Foundation

358.7 6.9 2.5

360.1 5.5 1.0

357.76 7.81 4.66 = Top Conc Tile

357.6 8.0 4.6

358.1 7.5 2.5

359.5 6.1 1.0.7 = Base Wall

362.81 2.76 1.16 = Hly Top Foundation

356.16 9.41 4.66 = Top Step Down

356.37 9.20 2.06

357.87 7.70 1.8.7

358.12 7.45 1.0.5 = Nly Top Foundation

362.81 2.76 1.0 = Top Wall

365.57 ✓

5-29-47

Sommermeyer

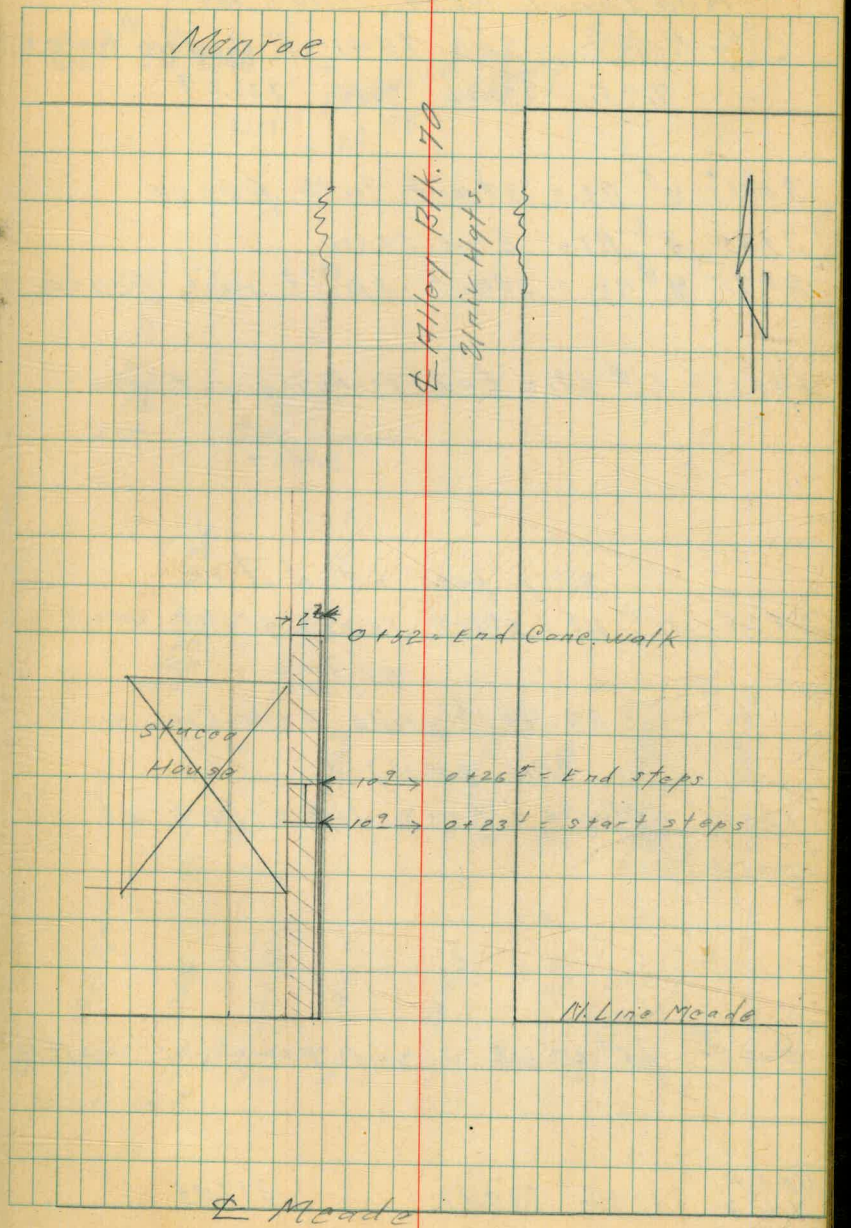
See page 62

Top (2nd) step - 7" Riser - 14" tread

Bottom step. 7" riser 12" tread

0+23.1 = start 3' wide conc. steps

0+00 = N. Line Meade



Additional Notes Alley Blk #1.
City Hgts. - See 1641 - P. 9. for Notes.

	7.95	330.22	7.10	322.27
3+25	8 Rt.	: start lath fence		
3+25	8 Rt.	: End same		
2+75	9 Rt.	: start split rail fence		
2+61	11 Lt.	: End rock + grout wall.		
		very poor condition		
2+25	11 Lt.	: start rock + grout wall		
	12 Rt.	: ± 1' wide E.+W. Conc. walk this point)		
1+14		(looks like a little fill at		
0-02	15 Lt.	: ± 3' wide E+W Conc walk		
N.E.B.P. Hole + Dwight.	12.32	329.37		317.05

INDEXED
W. K.
SEP 20 1948

Notes Reduced 9-29-48 photographic

324.2
5.2 / 12 Top

322.6
6.8 / 11 Base of wall + Grd.

323.6
5.8 / 10 Top wall

321.7
7.7 / 11 Grd + Base of wall

323.3 — 6.1 / 10
322.2 — 7.2 / 9
321.5 — 7.9
321.4 — 9.3 / 10
320.0 — 9.4 / 10.2
319.72 — 9.65 / 12.8 walk
319.51 — 9.86 / 25 on walk

326.77 — 2.12 / 25
326.6 — 2.60 / 15 walk
325.37 — 2.8 / 15 Grd
324.7 — 4.0 / 10
324.3 — 4.7 / 8
323.8 — 5.1
5.6 / 10

4+40 9^{E} Lt. = End Conc. Apron to double Gar.

Conc. Apron to double Gar.

4+02 9^{E} Lt. = end picket fence + start.

yard. 48' Lt. = start drain

3+75 9^{E} Lt. = ℄ 3½" E.+W. Conc. drain from

9^{E} Rt. = End lath fence

9^{E} Lt. = start picket fence

3+75 9^{E} Lt. = ℄ 6" wide E.+W. Conc. wall.

3+74 8^{E} Lt. = End Conc. Apron to double Gar.

to double garage.

3+49 8^{E} Lt. = start rough Conc. Apron

330.22

1A

326.74 — 3.48 — 25 E — Gar. Floor

326.32 — 3.90 — 9 E

326.72 — 3.50 — 25 E — Floor

326.03 — 4.19 — To

326.01 — 4.21 — 9 E — Apron

325.8 — 4.4 — 9 E — End

326.13 — 4.09 — 48 — invert

324.91 — 5.31 — 9 E — invert

325.61 — 4.61 — 15 — top wall

325.31 — 4.91 — 9 E — Top wall

324.5 — 5.7 — 9 E — Base wall

324.9 — 5.3 — 9 E — End

326.08 — 4.14 — 28 — at Gar.

325.49 — 4.73 — 17

325.04 — 5.18 — 10

324.83 — 5.39 — 8 E

326.05 — 4.17 — 28 — at Gar.

325.50 — 4.72 — 17

324.46 — 5.76 — 10

324.29 — 5.93 — 8 E

Alley Blk. 1 City Hgts.

Note. 2 B.M. on 1 corner.

on N.E. Cor. Dwight + Boundary are 2 Brass plugs. 3½' apart. one should be destroyed

From. A. on page 73 = 329.37

Record =			324.98
North. B.P. (NE Boundary		4.41	324.96 - 0.02
South. B.P. + Dwight)		4.45	324.92 - Use

From. P. 73 329.37

3.47 329.02 (328.99 FB 1641 P.12)

T.P. 6.15 332.49 3.88 326.34

E.+W. open drain (0.2' deep)

4+23² 9' ℄ = ℄ 18" wide dished Conc.

330.22

North plug in Poor shape so pulled it out.

Change in office book to Read

N.E. B.P. Boundary + Dwight = EL. 324.92

326.50

3.92

25

Bottom of drain

326.09

4.13

91

Bottom on ℄

Additional Notes Alley Blk 136.
2/nin. Hgts. (E. + W. Alley)
Orig. Notes Ia. 1671 / 35 + 39

3+49 20' Lt. = End same

Conc. floor. No apron.

3+34 20' Lt. = start double Gar.

2+01 10 4 Rt. = End Conc. slab

1+97 1/2 10 4 Rt. = start Conc. slab

1+97 10 9 Rt. = End Conc. Apron to double Gar.

Conc. Apron + Floor.

1+84 10 9 = start apron to double Gar.

Hub. T.P. 6.56 294.41 — 287.85
F81C71
P. 42

INDEXED
W.K.
SEP 20 1948

Notes Reduced
9-29-48 J.E. Thompson

290.99
3.42
20
Floor

291.01
3.40
20
Floor

292.38
2.03
10 4
Slab

292.54
1.87
15'
Back of slab

292.40
2.01
10 4
Slab

292.54
1.87
15'
Back of slab

292.19
2.22
10 9
Apron

292.54
1.87
15'
Gar. Floor

292.07
2.34
10 9
Apron

292.58
1.83
15'
Gar. Floor

294.41

N. + S. Alley Blk. 136 Univ. Hgts

5+42 $\frac{2}{=}$ 11° Lt. = ℄ 6" wide N. + S. Conc. wall

5+41 $\frac{5}{=}$ 11° Lt. = End conc. wall + fence

for driveway thru fence

5+30 $\frac{5}{=}$ 11° Lt. = step down in wall

5+06 11° Lt. = line - (face) of wall.

6" wide top

shown in F.B. 1671

This wall is new. not the one

4+79 10 $\frac{9}{}$ Lt. = start Conc. Wall.

also = start wire fence on top of wall

294.41

Notes Reduced 9-28-43 gelbampton

288.31	287.3	287.6
6.10	7.1	6.8
11	11	11
Top wall	Base wall	Grd.
288.03	287.3	287.6
6.38	7.1	6.8
11	11	11
Top of Wall	Base of wall	Grd
288.01	288.53	287.3	287.8
6.40	5.88	7.1	6.6
11 $\frac{4}{}$	11 $\frac{4}{}$	11 $\frac{4}{}$	11 $\frac{4}{}$
top of Step down	Top wall	Base wall	Grd.
288.73	287.4	288.1
5.68	7.0	6.3
11 $\frac{2}{}$	11 $\frac{2}{}$	11 $\frac{2}{}$
top of wall	Base of wall	Grd
288.79	287.6	288.4
5.42	6.8	6.0
10 $\frac{9}{}$	10 $\frac{9}{}$	10 $\frac{9}{}$
top of wall	Base wall	Grd

294.41

orig B.M. for check 6.56 287.85 ✓

Rt. = N.E. Cor. Gar.
floor = S.E. Cor.
5+66 2^{2} Rt. = Front of Gar. Conc.

18^{7} Rt. = N.E. Cor. Apron.
to double Gar. (East front.
5+52 2^{2} 2^{3} Rt. = S.E. Cor. Conc. Apron

294.41

278.32
6.09

288.32
6.09
2^{3}
S.E. Cor Gar.

288.36
6.05
18^{7}
N.E. Cor. Gar.

287.98
6.43
2^{2}
S.E. Cor
Apron

288.10
6.21
18^{7}
N.E. Cor.

294.41

11-30-48 Additional Notes Alley Blk 1 City Hts

Hendricks

Bramby Dwight to Landis Bet. Hyle & Boundary

Greer

Rever 6.96 322.08 322.05

WO 31453

2+50					
2+00					
1+50					
1+08	℄ garage on Lt. 16.2'				
1+00					
T.P.	5.88	329.04	5.38	323.16	
0+52					
0+43	℄ Single Garage on Lt. 9' Apron				
0+00					
0-14	No. Cb Line Dwight				
BM	1149	328.54			317.05

(2+75)
324.0 322.0 321.8 ℄ 321.4 321.5 321.7 322.5 322.7
5.0 7.0 7.2 7.6 7.5 7.8 6.5 6.3
50 10 6 10 27 50 70

Ck conc walk 10' Rt
2+81 FB 1641 P 10
326.3 324.6 323.9 322.2 321.3 320.8 320.4 320.9 320.0 321.1 321.9
2.7 4.4 5.1 6.2 7.1 8.2 8.5 8.1 9.0 7.9 7.1
28 25 11 10 7 5 11 24 50 70

325.8 323.8 321.7 320.5 320.2 319.9 320.2 320.2 320.5
3.3 5.1 7.3 8.5 8.8 9.1 8.8 8.8 8.5
50 21 13 7 9 18 50 70

324.2 325.4 324.0 320.8 320.4 320.3 321.0 320.3 320.5
4.8 3.6 5.0 8.2 8.6 8.1 8.0 8.7 8.5
16.2 40 17 8 8 12 50 70
FL

325.2 323.9 322.4 322.0 321.4 320.4 319.7 319.5 319.2
3.8 5.1 6.6 7.0 7.5 8.6 9.3 9.5 9.8
40 10 6 11 12 34 50 90

329.04
326.3 325.4 325.5 324.2 324.1 322.9 321.8 321.8 320.7 319.3 318.8 318.7
2.8 3.1 3.4 4.3 4.4 5.6 6.7 6.7 7.8 9.2 9.7 9.8
50 21 10 5 11 12 23 34 35 50 90

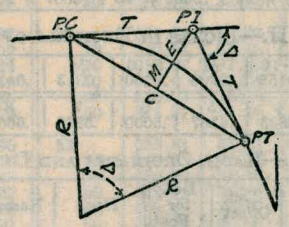
326.27 325.85 324.5 324.2 322.4 321.1 319.5 318.9 318.4
2.27 2.69 4.0 4.3 5.1 7.4 9.0 9.6 10.1
14.8 11 4 10 27 36 49 90
FL Apron

327.2 326.7 326.1 324.6 324.3 323.1 322.4 318.6 317.5
1.3 1.8 2.4 3.9 4.2 5.4 6.1 9.9 11.0
50 16 12 8 18 29 60 95

325.9 325.7 324.6 324.5 324.0 322.1 319.0 318.4 317.7
2.6 2.8 3.9 4.0 4.5 6.4 9.5 10.1 10.8
50 18 10 10 36 60 71 95

329.54
NEBP Dwight & Hyle

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES



CURVE FORMULAS

Radius=R=$\frac{50}{\text{sin. } D/2}$ (1) Degree of Curve=D and sin. $\frac{D}{2}=\frac{50}{R}$ (2)

Tangent=T=R tan $\frac{\Delta}{2}$ (3) Length of Curve=L=$100\frac{\Delta}{D}$ (4)

Middle ordinate=M=R(1—cos. $\frac{\Delta}{2}$) (5)=R vers $\frac{\Delta}{2}$ (6)

External=E=T tan $\frac{\Delta}{4}$ (7)=R ÷ cos. $\frac{\Delta}{2}$—R (8)=R exsec $\frac{\Delta}{2}$ (9)

Long Chord=C=2 R sin. $\frac{\Delta}{2}$ (10) Δ=Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. Δ=62° 10′ D=8° 20′. From Table IV for 1° curve T=3454.1 and ÷8⅓=414.49 ft. From Table V correction=.36 or T=414.85 ft. P. C.=Sta. P.I.—T=157 +45.50. Also from (4) L=746.00 and P. T.=Sta. P. C.+L=164+91.50.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset=7.27 $(54.50 \div 100)^2$=2.16 ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26)$=2.16 ft.

Deflections.—Deflection angle=½ D for 100 ft., ¼ D for 50 ft., etc. For c ft.=(in minutes) .3 x C x D° or=defl. for 1 ft. from Table III x C. For Sta. 158 of above curve=.3 x 54.5 x 8⅓=136.2′ or 2° 16.2′, or=2.50 x 54.5=136.2′ from Table III. For Sta. 159 deflection angle=2° 16.2′ +8° 20′ ÷2=6° 26.2′, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve E=960.6 for 8° 20′=960.6 ÷8⅓=115.27 and from Table V correction=.10 or E=115.37 ft. Or suppose Δ=32° and E is measured and found to be 42 ft. What is D? From Table IV E=230.9 and ÷42=5.5 or D=5° 30′.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)+2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.