EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

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CITY ENGINEER'S OFFICE

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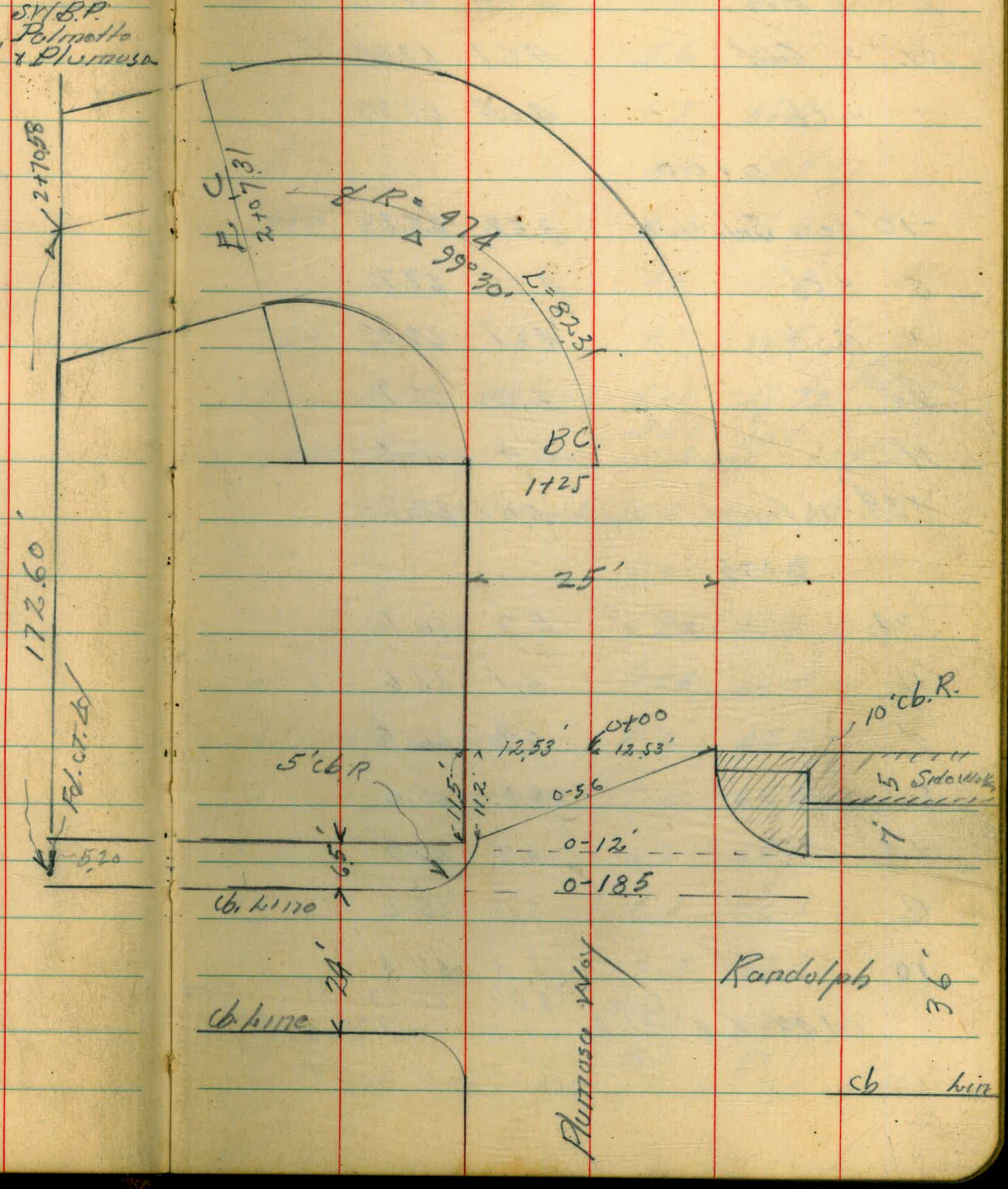
Made in U. S. A.

Walker
Hyden
Hunter
1-12-46

Cross Section — Plumosa Way — from Randolph St. East and North to Dead End

25' Wide

	2.44	271.75	269.31
	0 - 18.5		
-4.7' on cb P.C. 5'R		5.68	66.07
" " Gut. Pav.		6.27	65.48
N on "		5.98	65.77
L " "		5.22	66.53
S		4.65	67.10
+10 " "		4.24	67.51
0 - 12 = E. cb. Plumosa			
-10 on cb B.C. 10'R.		3.74	68.01
-10 " Gut " "		4.43	67.32
S		4.72	67.03
L " Pav.		5.20	66.55
+11.5' of cb on Gut		5.83	65.92
" on cb.		5.28	66.47
N		5.4	66.4
+3.4 at Lath Fence		5.4	66.4
0 - 5.6'			
N		5.4	66.4
+1+ on cb.		5.28	66.47
Gut.		5.83	65.92



Indexed
O.S.K.

2

Plumosa-Way
X-Sections

		HI			Rod	Elev.	
		271.75					
℄ on Pav					5.02	66.73	
S.L. " Gut					4.67	67.08	
" " cb.					4.05	67.70	
0+00							
-10' on Sidewalk					3.52	68.23	
S " cb					4.05	67.70	
" Gut					4.67	67.08	
℄					5.0	66.7	
N					5.4	66.4	
+3.4' at Fence					5.0	66.7	
0+25							
-3.4					5.0	66.7	
N					5.1	66.6	
℄					5.3	66.5	
S					5.2	66.6	
+3					4.9	66.8	
+6					3.5	68.2	
10					3.3	68.4	
					5.46	66.29	0.7' Back N end

0+43=℄ 8' Conc. Slab on N 0.7' Back

		HI		Rod	Elev.	
		271.75				
-10				3.8	67.9	
-6				4.0	67.7	
-3				5.6	66.1	
S				5.7	66.0	
℄				5.8	65.9	
+10				5.7	66.0	
N				4.9	66.8	
+3.4'				4.9	66.8	
T.P.	5.12	272.84		4.03	267.72	S.E. Top Cb. Plumosa & Randolph
				3.81	69.0	

0+26=℄ 4' Conc. Walk on South 13.8' Back

0+57=℄ Granite Block Steps on N

-5	6.0	66.8	
-1' on Top Step	5.94	66.9	
N " "	6.44	66.4	
+1 on Ground	7.0	65.8	
℄	7.0	65.8	
S	6.9	65.9	
+3	6.7	66.1	
+6	5.2	67.6	
+10	5.0	67.8	
	5.7	67.1	

0+60 Bog. Cobble Wall on N 0.4' in St.

1+00		
-14.7 on 3.8' Conc. Walk	3.93	68.91
-10	4.6	68.2
-4	4.9	67.9
-2	7.3	65.5
S	7.4	65.4
℄	7.7	65.1
+11.6 = Bottom Conc. step	7.8	65.0
N on Conc. step	7.34	65.5
1' West on Cobble Wall	6.0	66.8
+3	6.15	66.69
+10	6.2	66.6
	6.0	66.8
1+06 cobble wall on N 0.8' in st.		
1+25 = B.C. Lt. Curve in 3 Parts		
-10	6.5	66.3
N on cobble wall	6.5	66.3
+0.3 = Base Wall	8.3	64.5
℄	8.3	64.5
S	7.8	65.0
+5	5.4	67.4
10	5.0	67.8

1+32 = Beg. Conc. Walk on South		
℄ +11.5 = N. edge Walk	7.54	65.30
+14.5 = S. " "	7.30	65.54
1+45		
	6.33	66.51
℄ 11.9 on N edge Above Walk		
1+52.44 = Part 1		
-1' on Broken Conc. Walk	8.4	64.4
S	8.7	64.1
+3	9.1	63.7
℄	9.2	63.6
N = Base Cobble Wall	9.4	63.4
+ 0.5 Top " "	6.9	65.9
+10	6.9	65.9
	9.48	63.36
1+64 = ℄ 3.5 Conc. Walk on Rt. 1.9 in st.		
.04' Rt of Rt. Line on "	2.23	63.61	Bottom Rt. steps
1+68.6 = Beg. 2' Picket Fence on Rt. 1.9 inst		
1+78 = Δ in Above Fence 8.7 in st		
1+68.6 Conc. steps on Lt. 1.7' in st.		
Top steps.	7.54	65.30	
on Ground at steps	10.3	62.5	
1+79 = N end steps	10.2	62.6	on Step.

2.72 84

T.P.	2.69	264.64	10.89 261.95
1+79.88 = Point 2			
-10		+0.2	64.8
Lt. on Wall		+0.8	65.4
Lt. Base "		2.8	61.8
℄		2.7	61.9
S		2.1	62.5
+1' = S in Fence			
+5		2.0	62.6
1+99' 9.5 Rt. of ℄ = 14" Euc Tree			
2+07.31 = E.C. - End of 2' Fence 14 in Rt.			
-5		7.0	57.6
Rt.		4.9	59.7
+3 = ℄ 16" Euc Tree			
+2		4.1	60.5
℄		4.4	60.2
Lt. at Base Cobble Wall		4.6	60.0
+0.6 on " "		1.0	63.6
+5		0.8	63.8

264.64

2+30 = ℄ Garage on Rt. 3.4' inst. Wood Floor			
on Conc. Wall		5.63	59.01
" Wood Floor		5.63	59.01
2+20 = ℄ 12" Euc. Tree on Rt. 3.2' inst.			
2+35 = End Cobble Wall on Lt.			
-1.0 on Wall		2.2	62.4
-0.2 Toe "		6.7	57.9
℄		6.1	58.5
+8.4 = Conc. Wall Garage = Floor		5.64	59.00
Conc. Floor = 6.98			57.66 Now used as Apt.
2+42 = ℄ Garage on W 1.7' Back			
Lt.		7.1	57.5
℄		6.4	58.2
+9		6.3	58.3
Rt		8.2	56.4
+10		15.2	49.4 Slope cont. →
Conc. Floor		6.96	57.68 Now used as Apt.
2+57 = ℄ Garage on Lt			
2+62 = ℄ Garage on Lt. 1.7' Back.			
-10		19.0	45.6
Rt		11.8	52.8
+7.5		7.0	57.6
℄		7.0	57.6

26464

Lt.		7.3	57.3	
+0.6	Toe Conc. Apron	7.12	57.52	
+1.7	= Garage Conc. Floor	7.00	57.6	Not used At Apt.
	2+70.58 = End St.			
-5		4.7	59.9	
Lt.		7.5	57.1	
℄		7.0	57.6	
+5		7.9	56.7	
Rt.		12.8	51.8	
+10		19.8	44.8	Slope Cont. →
	2+75			
-10		20.6	44.0	Slope Cont. →
Rt.		16.7	47.9	
℄		12.0	52.6	
+2		7.1	57.5	
Lt.		7.3	57.3	
+5		6.3	58.3	
	2+93			
-5'		6.6	58.0	
Lt.		8.5	56.1	
+3		8.8	55.8	

26464

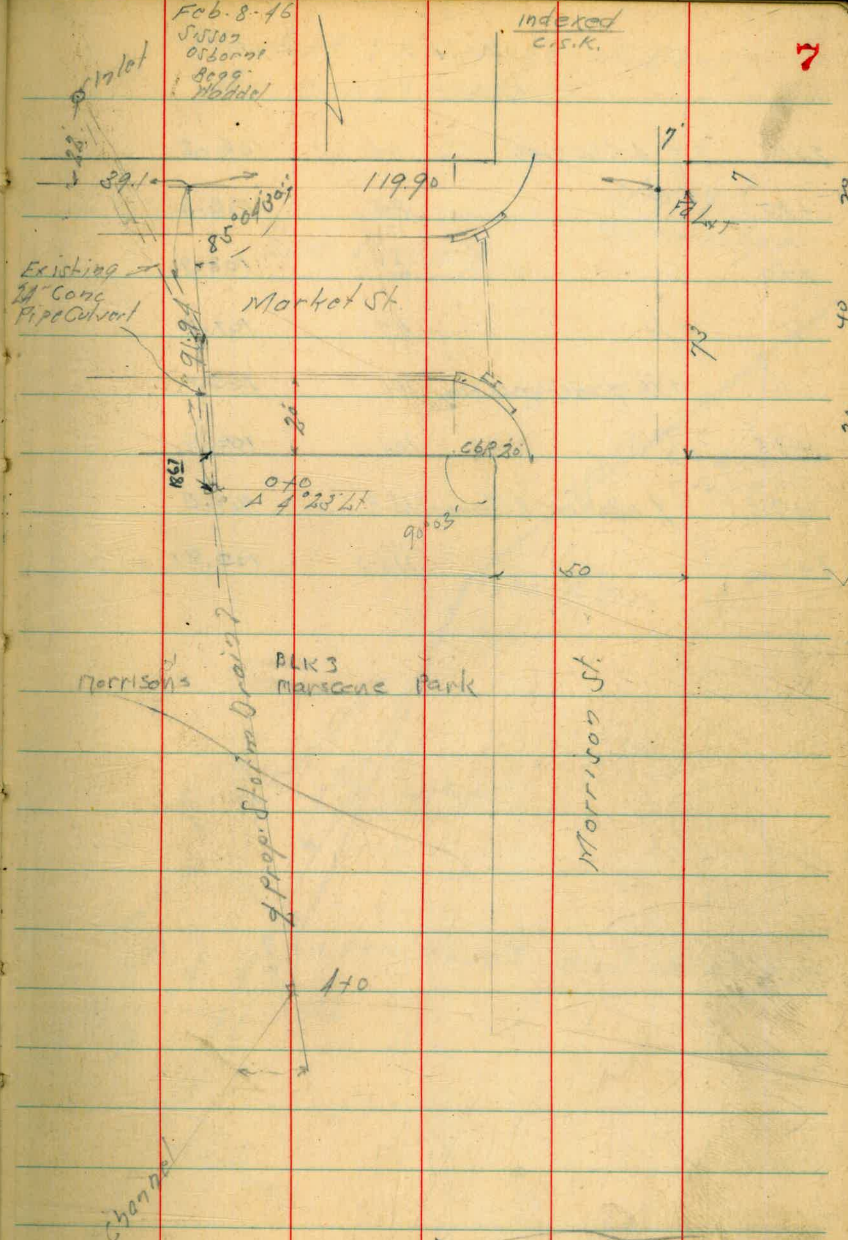
℄	13.4	51.2	
Rt.	20.7	43.9	
+10	24.4	40.2	
+25	31.0	33.6	Slope Cont.
3+10			
-25	30.0	34.6	Slope Cont.
-12	21.5	43.1	
Rt.	13.6	51.0	
+7.0	10.3	54.3	
℄	9.5	55.1	
+8	2.7	54.9	
Lt.	7.3	57.3	
+5	5.3	59.3	
2+41 = ℄ 18" Euc. Tree 9' Rt of ℄			
2+52 = ℄ 6 " " " 11.8' " "			
2+65 " 5" " " 7.7 " " "			
T.P. 8.27 271.35	1.56	263.08	
Chk Starting BM	2.03	269.32	
		269.31	
		0.01	

Proposed Storm Drain
South of Market West of Morrison St.

BM	0.22	125.61 ✓		125.39	N.W. B.P. Market + 41st St
Inlet Exist. 24" Conc. Pipe			11.55	114.06	Flow Line
0+0	= Sly 24" Conc Pipe Culv		12.83	112.78	Flow Line
TP	3.00	117.04 ✓	11.57	114.04	
+10	= Ely Bottom of Ditch		4.7	112.3	
+12			2.8	114.2	
+50			2.6	114.4	
"	9 Rt = Ely Top Ditch		3.0	114.0	
"	10 Rt = Ely Bottom of Ditch		5.0	112.0	
+88			3.6	113.4	
"	17 Rt = Ely Top Ditch		3.7	113.3	
"	18 Rt = Ely Bot of Ditch		5.3	111.7	
1+28			5.1	111.9	
"	8 Rt = Sly + Bottom Ditch		5.2	111.8	
+50	= Sly Water Way		5.6	111.4	
2+0			5.6	111.4	
"	23 Lt = ℄ Water Way		6.8	110.2	
+50			6.3	110.7	
"	8 Lt = ℄ Water Way		8.0	109.0	
3+0	= ℄ + Bottom of Channel		9.7	107.3	

Feb. 8-16
Sisson
Osborne
Begg
Waddel

indexed
C.S.K.



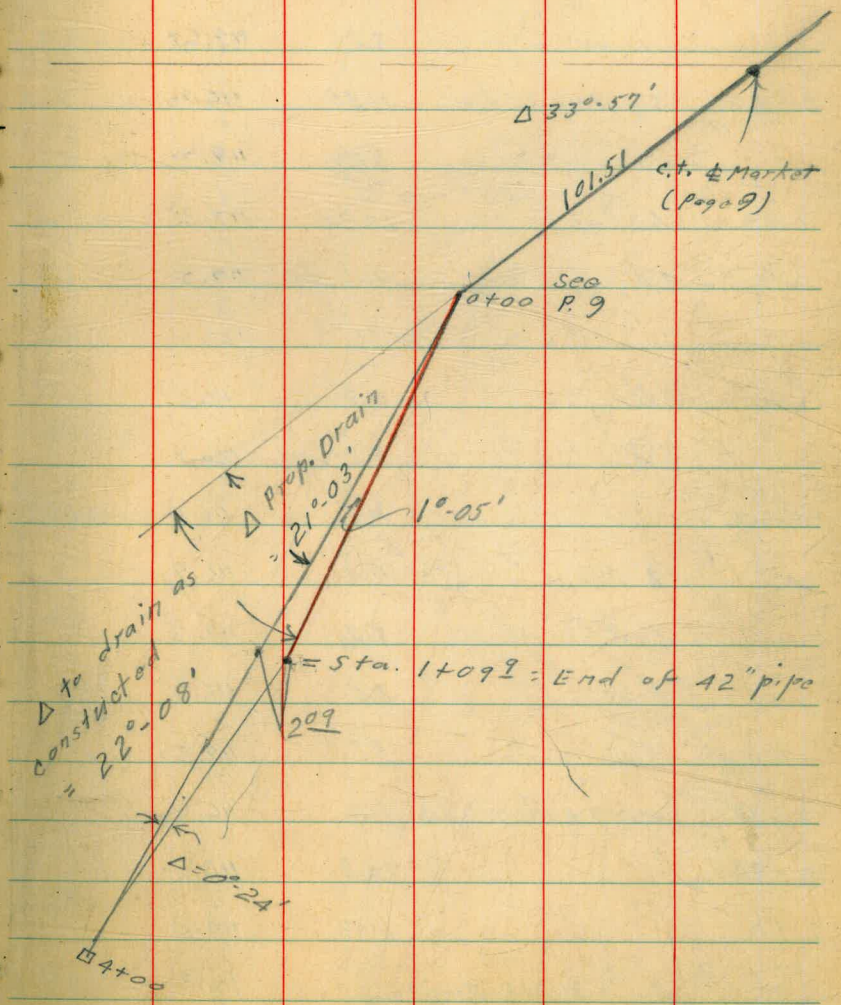
Roll. 4372 · MKT St Imp

	117.04 ✓		
3+16.	= 2' ↓ Channel	10.5	106.5
+33		8.5	108.5
+50		8.1	108.9
"	9' Lt	9.7	107.3
"	12' Lt = ↓ + Bottom 6' Channel	11.6	105.4
+85		10.1	106.9
+95	= ↓ + Bottom 8' Channel	12.2	104.8
4+0		11.63	105.91 on Stab

Market St. West of Denby
As constructed

3/10/47
Sommermeyer

See Page 9

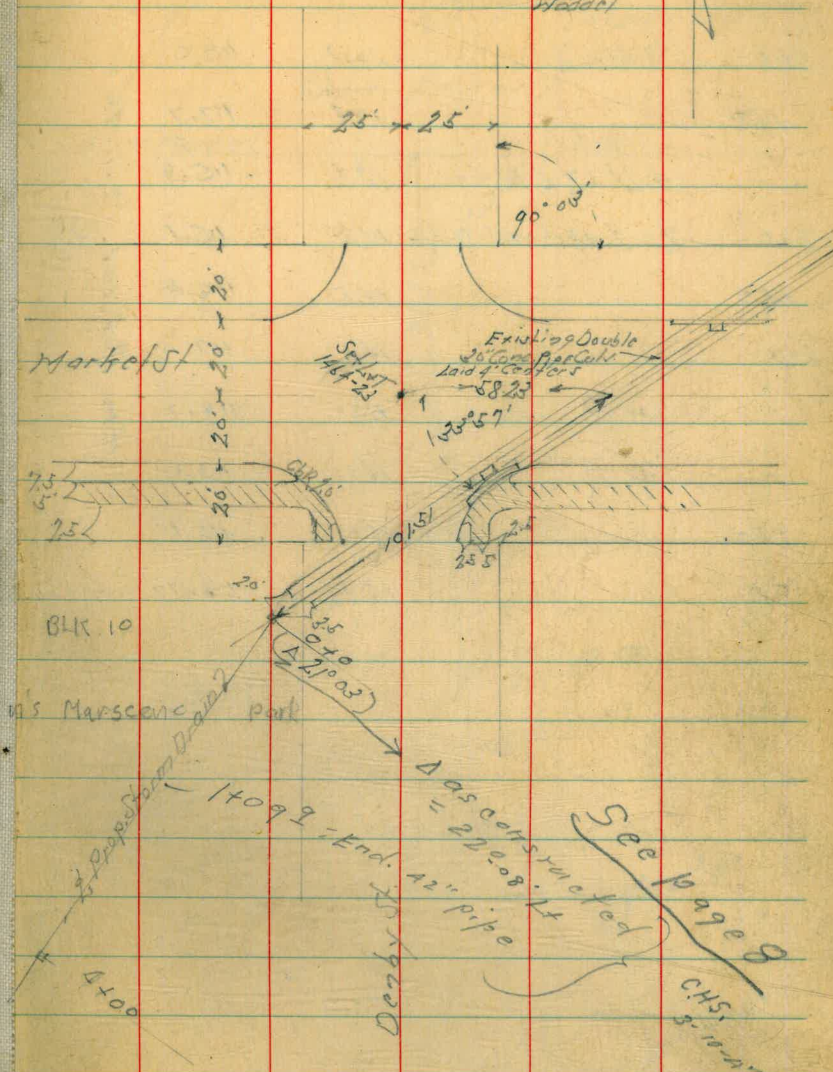


Proposed Storm Drain
South of Market St West of Derby St

BM	0.76	128.30		127.54	S.F.B.P. Market + 43rd
0-60	= S.E. Cb Inlet Market + Derby		10.53	117.77	Bottom of Pipe
0-35	= Sly East 30" Pipe		11.42	116.88	Flow Line
"	" " " "		8.63	119.67	Top Pipe
0-2.0	= Sly West 30" Pipe		11.40	116.90	Flow Line
"	" " " "		8.59	119.71	Top Pipe
0+0	= Δ 21°03' Lt		10.95	117.35	on Stub
"	3' Rt of ℄		11.1	117.2	
"	7' " " "		7.1	121.2	
"	5' Lt " "		11.0	117.3	
"	7' Lt		8.2	120.1	
0+50			11.4	116.9	
"	2' Rt		11.4	116.9	
"	3' Rt		8.8	119.5	
"	4' Lt		11.5	116.8	
"	5' Lt		8.8	119.5	
0+80	= Wly + Bottom Ditch		11.7	116.6	
0+83			10.3	118.0	
1+0			10.0	118.3	
"	3' Lt = Wly + Bottom Ditch		12.0	116.3	
"	6' Lt		12.1	116.2	

Indexed
C.S.K.

Feb. 8-46
Sisson
Osborne
Begg
Waddel

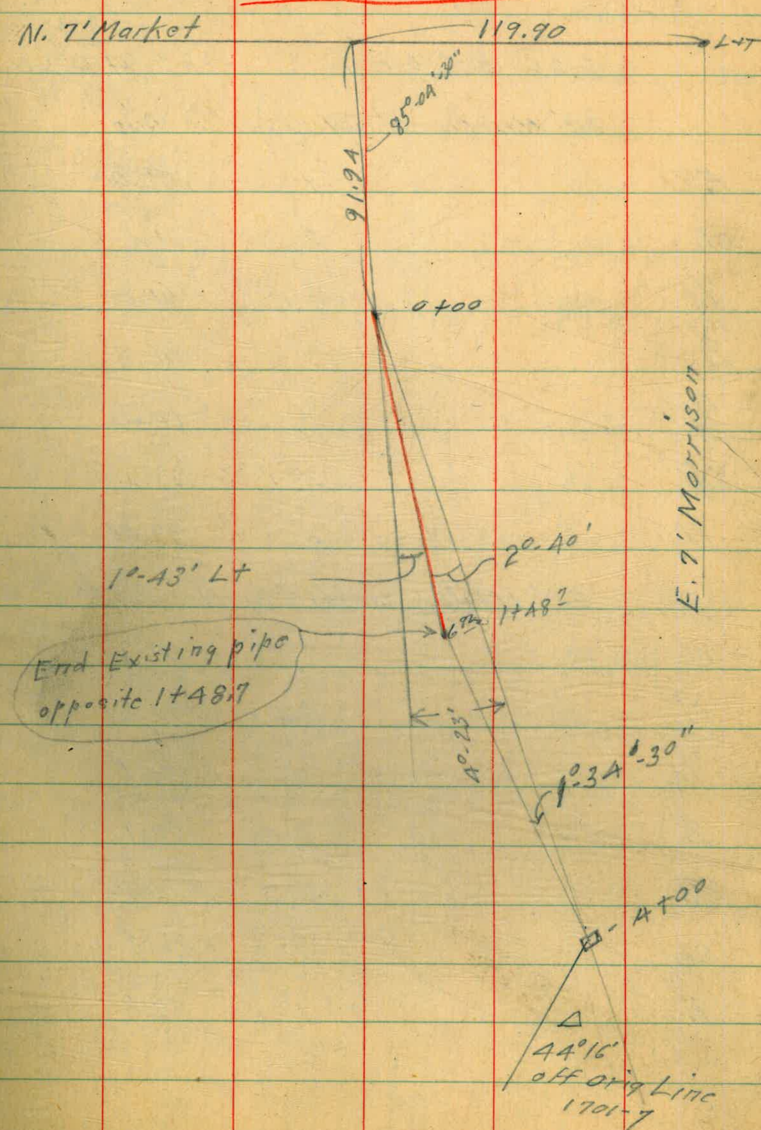


		128.30		
1+0	8' Lt of ℄	10.3	118.0	
+50		10.6	117.7	
"	4' Lt: ℄ 6' Ditch	12.4	115.9	
2+0	℄ = ℄ & Bottom 6' Ditch	13.2	115.1	
+50		13.5	114.8	
3+0		14.3	114.0	
"	10' Lt.	13.6	114.7	
"	10' Rt	14.7	113.6	
+50		15.2	113.1	
4+0		15.33	112.97	on stub

Notes Reduced. 2-11-26

Drain As constructed
So. of Market. W. of Morrison

See page 7



Walker
Hardin
Hunley
Begg
2-19-46

CROSS SECTION 36th St. 80' Wide 14' Cbs 13' Ws.
from Myrtle Ave
to Bellingham St.

See Sketch P-16

	0.66	303.60		302.94	NWBP Myrtle + 36th FB 1644-16
	30' North of S.L. Myrtle Ave				
E.			1.6	02.0	
cb			2.2	01.4	
1/4			2.6	01.0	
℄			2.8	00.8	
1/4			3.2	00.4	
cb.			3.7	99.9	
W			4.2	99.4	
	20' North of S.L. Myrtle				
W			4.5	99.1	
cb.			4.4	99.2	
1/4			3.6	300.0	
℄			3.5	00.1	
1/4			2.9	00.7	
cb.			2.3	01.3	
E.			1.8	01.8	

		30360			
	10' N of S.L. Myrtle				
E.			1.6	02.0	
cb.			2.0	01.6	
1/4			3.0	00.6	
℄			3.6	300.0	
1/4			4.2	99.4	
cb.			4.8	98.8	
W			5.1	98.5	= Rt ∆ to SW cor. 36th St
	0+00 = S.L. Myrtle				
-10			9.0	94.6	
W			9.2	94.4	
cb.			7.0	96.6	
1/4			9.0	94.6	
℄			6.7	96.9	
1/4			3.3	00.3	
cb.			2.3	01.3	
E.			2.3	01.3	
+10			1.9	01.7	
	0+15				
-10'			2.8	00.8	
E.			2.5	01.1	

	303.60	36th	St.
cb.		2.7	00.9
+10		2.9	00.7
1/4		4.7	98.9
+10		7.1	96.5
℄		11.0	92.6
+5		14.4	89.2
1/4		13.7	89.9
+8		11.1	92.5
cb.		10.2	93.4
W		11.8	91.8
+20		11.7	91.9
	0+30		
-20		12.4	91.2
W		13.3	90.3
+5		16.0	87.6
cb.		13.9	89.7
+2		16.9	86.7
+11		17.4	86.2
1/4		13.1	90.5
℄		9.6	94.0
+7		8.0	95.6

	303.60	36th	Street
1/4		4.8	98.8
+4		8.1	00.5
cb.		1.9	01.7
E		1.6	02.0
+10		2.7	00.9
	0+55		
-10		3.6	300.0
-3		3.0	00.6
E		2.1	01.5
cb.		5.5	98.1
+8		10.2	93.4
1/4		11.7	91.9
℄		16.4	87.2
1/4		19.5	84.1
+5 in ditch		21.4	82.2
cb.		19.4	84.2
+3		19.4	84.2
+6		16.6	87.0
W		13.9	89.7
+20		9.8	93.8

36th Street

	0+75	303.60		
20'			9.0	94.6
W			12.2	91.4
cb.			16.0	87.6
+9'			19.0	84.6
¼			20.7	82.9
+3			21.7	81.9
+5 in ditch			23.7	79.9
+9 " "			23.7	79.9
℄			19.7	83.9
¼			14.0	89.6
cb.			8.0	95.6
E			4.7	98.9
+10			4.5	99.1
	1+00			
-20			6.5	97.1
E.			9.7	93.9
TP	1.15	293.39	11.36	292.24
cb.			5.9	87.5
¼			8.7	84.7
+8			11.8	81.6
℄			14.4	79.0

36th St.

		293.39		
℄ +5 = ℄ Ditch			15.3	78.1
¼			9.6	83.8
cb.			5.0	88.4
+7			3.3	90.1
W			1.1	92.3
+20			+2.0	95.4
	1+25			
-20			+2.4	95.8
W			0.0	93.4
cb.			3.2	90.2
¼			6.4	87.0
+10			9.8	83.6
℄			12.3	81.1
+7 = W edge Ditch			16.5	76.9
¼ = ℄ Ditch			16.4	77.0
cb.			10.8	82.6
E.			9.2	83.5
+20			2.0	91.4
	1+50			
-30'			1.8	91.6
-5 in Ditch			18.7	75.1

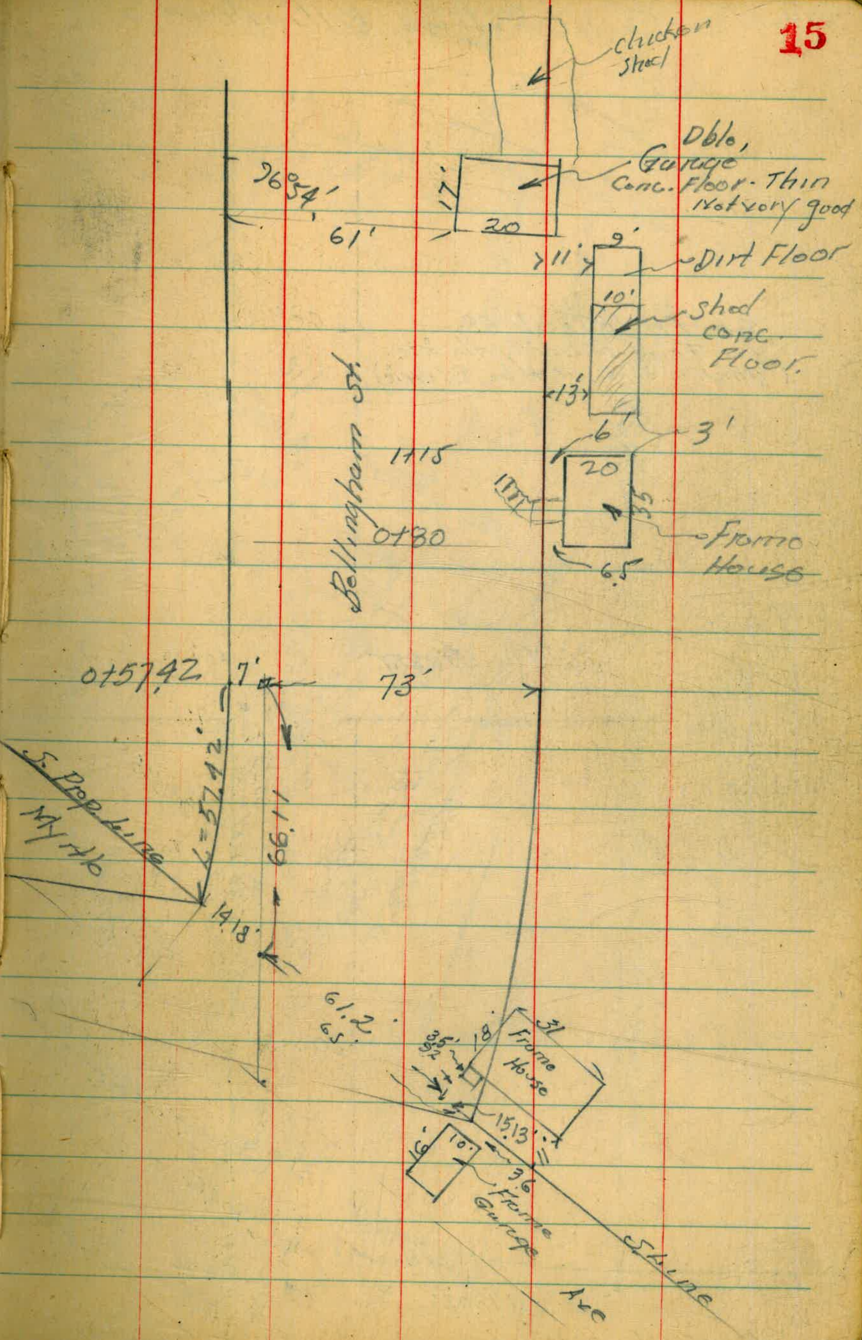
29339 36th St.

E	in Ditch	18.3	75.1
+5	" "	18.3	75.1
cb.		13.0	80.4
1/4		9.7	83.7
℄		7.0	86.4
1/4		4.0	89.4
cb.		0.9	92.5
W		+1.1	94.5
+15		+2.8	96.2
	2+00		
-15		+5.0	98.4
W		+2.7	96.1
cb.		+0.2	93.6
1/4		3.2	90.2
℄		7.3	86.1
1/4		12.2	81.2
cb		18.5	74.9
+2'	in Ditch	19.5	73.9
+11	" "	21.1	72.3
E	" "	21.1	72.3
+20		13.1	80.3
+30'		9.9	83.5

29339

	2+30			
-40			17.1	76.3
-25	in Ditch		22.0	71.4
E	" "	W. edge	21.6	71.8
cb			14.4	79.0
1/4			9.7	83.7
℄			6.3	87.1
1/4			1.9	91.5
cb.			+1.4	94.8
W			+4.1	97.5
+15			+5.8	99.2
	2+55			
-15			+6.4	99.8
W			+5.2	98.6
cb			+3.2	96.6
1/4			+1.1	94.5
℄			1.4	92.0
1/4			4.8	88.6
cb.			9.2	84.2
E			14.0	79.4
+19			23.0	70.4
+23			23.4	70.0

		29339		36TH ST.
+27	in Ditch.		26.0	67.4
+30			22.7	70.7
+37			23.0	70.4
+50			17.7	75.7
	2+81.79			
-45 in Ditch			27.0	66.4
26			17.1	76.3
℄			8.5	84.9
cb.			4.4	89.0
T.P.	12.15	302.53	3.01	290.38
1/4			10.4	92.1
℄			8.4	94.1
1/4			6.7	95.8
cb.			5.5	97.0
W. on Conc Mon			4.08	298.45
	Section on Curve		N.L. Bellingham	
W			4.08	98.45 ✓
cb.			5.1	97.4
1/4			6.7	95.8
℄			8.5	94.0
1/4			10.0	92.5
cb.			12.0	90.5
E.			14.0	88.5



Walker

Cross Sections Bellingham St.

Indexed
C.S.K.

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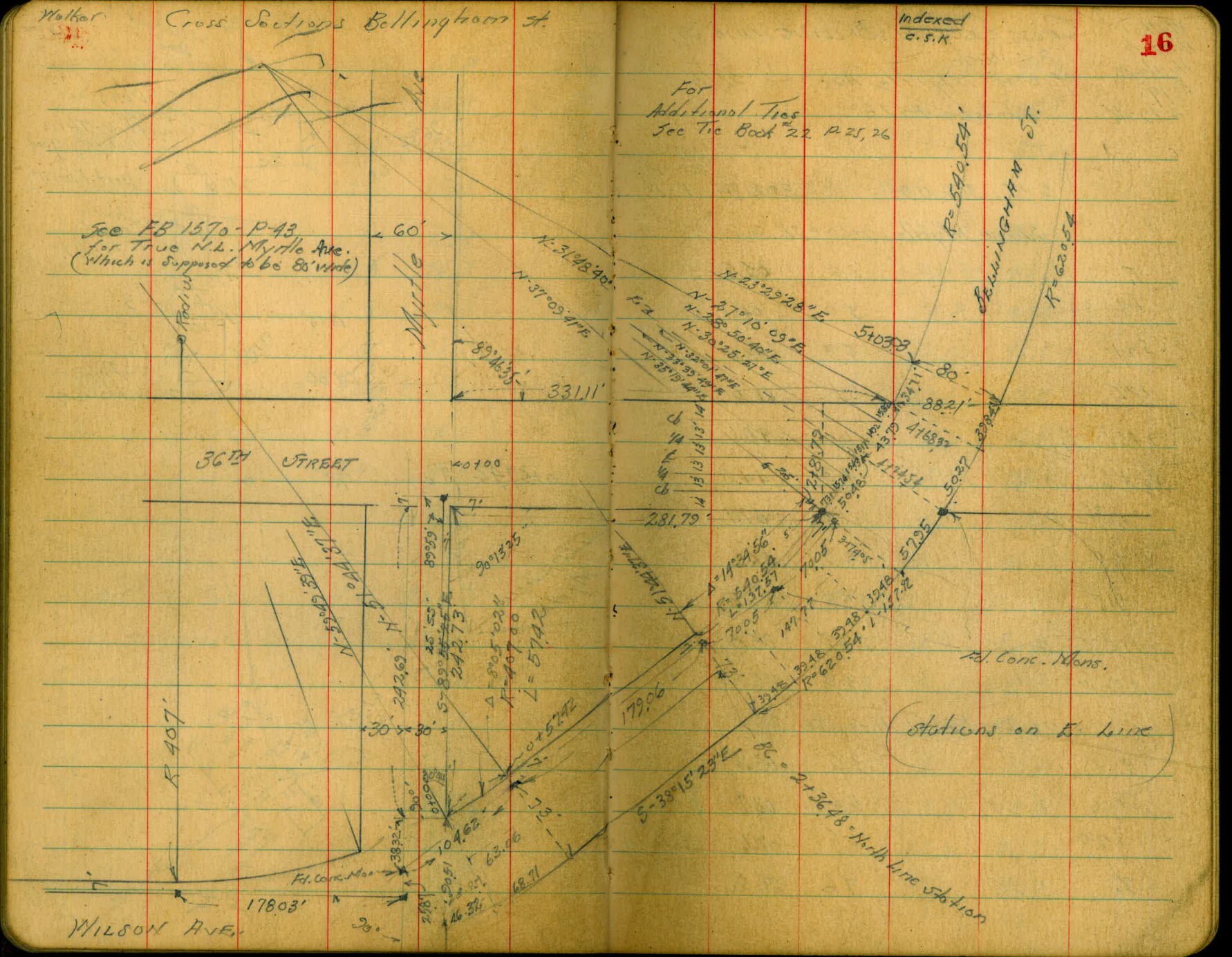

Walker
Hardin
Hunley
Bogg
2-19-46

CROSS SECTION - BELLINGHAM ST.
80' Wide
from Myrtle Ave to 36th St.
Sketch P-16

BM NW Bolt 36th & Myrtle P-11

	6.15 309.09	302.94	
	S. line Myrtle 0+00 = SE. Cor.		
E.		36	05.5
+8		5.0	04.1
+21		5.3	03.8
+35		8.1	01.0
+45.25 = ℄		11.0	98.1
℄ +60		14.3	94.8
" +45.25 = W		21.2	87.9
W +5		22.9	86.2
+15		25.3	83.8
NE Cor House		23.3	85.8
SE " "		23.3	85.8
	0+00 Radial thru SE Cor.		
E.		3.6	05.5
+16		5.4	03.7
+22		6.5	02.6
+40 = ℄		7.6	01.5

309.09

℄ +13	16.2	92.9
+40 = N	23.2	85.9
+20	27.0	82.1
0+28.71 Radial		
-20	27.0	82.1
N	23.2	85.9
+25	16.7	92.4
℄	12.5	96.6
+10	9.1	00.0
+20	8.9	00.2
+29	5.5	03.6
E.	4.7	04.4
+10	3.8	05.3
0+57.42 = E.C.		
-10	4.0	05.1
E.	5.1	04.0
+7' on Conc. Mon.	6.08	03.01
+10	6.0	03.1
+23	9.3	99.8
+30	12.9	96.2
℄	13.9	96.2
+3	13.0	96.1

309.09 Bellingham Street

℄ +6		15.7	93.4
+30	=10" Pepper Tree	20.8	88.3
W		23.7	85.4
+20		27.3	81.8
	0+80		
6.5 in W.L.	=NE Cor House	25.4	83.7
	1+00		
-6.5		26.4	82.7
W	on Brick Terrace	25.6	83.5
+8		24.0	85.1
+20	=W edge Dirt Drive	18.2	90.9
℄		17.6	91.5
+3	=E " " "	13.3	95.8
+15		8.9	00.2
+18		9.0	00.1
+32		5.8	03.3
E		5.1	04.0
+10		4.3	04.8
	1+25		
-10		4.8	04.3
E		5.7	03.8

309.09

℄ +11		6.2	02.9
+20		9.3	99.8
+30		10.3	98.8
+39		12.9	96.2
℄	=E edge Dirt Drive	20.0	89.1
+35	W " " "	20.8	88.3
+39		21.0	88.1
W		27.3	81.3
+13	Conc. Floor	28.3	80.8
	1+50		
-13	Sand Conc. Floor	28.3	80.8
-5		28.0	81.1
-4	=W edge Dirt Drive	22.1	87.0
W		21.9	87.2
+34	E " " "	21.7	87.4
℄		15.3	93.8
+5		11.2	97.9
+16		9.0	00.1
+20		8.8	00.3
+29		6.0	03.1
E		4.9	04.2
+10		4.5	04.6

309.09 Bellingham Street

1+75			
-10		4.7	04.4
E.		5.3	03.8
+11		6.3	02.8
+23		8.9	00.2
℄		14.9	94.2
+8		17.0	92.1
+11		19.0	90.1
+12 = E. edge Dirt Drive		23.4	85.7
+21		23.4	85.7
+31	Conc. Floor	24.4	84.7
W	" "	24.4	84.7
+11 at Shed		28.0	81.1
2+00			
-20	Slope Cont. for 75'	33.4	75.1
W = W edge Chicken Run		25.0	84.1
+13		24.5	84.6
+14		21.3	87.8
+20		21.3	87.8
+24		19.8	89.3
℄		14.8	94.3
+18		8.7	00.4

309.09

℄ +30		6.5	02.6
E.		5.6	03.5
+10		4.8	04.3
T.P.	2.67 304.95	6.81	302.28
E.L. Stations			
2+36.48 - B.C. Lt.			
-10		1.7	03.3
E.L.		1.8	03.2
+17		3.6	01.4
℄		10.5	94.5
+24		17.2	87.8
+26		19.4	85.6
W		22.6	82.4
+10		22.6	82.4
+11		27.0	78.0
+20	Slope Cont. for 75'	31.0	74.0
2+70.87	Curve in 4 Parts		
-20	in Chicken Run	23.0	82.0
W	" " Shed	23.0	82.0
+1		21.5	83.5
+10		21.0	84.0
+11		18.6	86.4

E.L. Stations

	304.95 Bellingham		
L		11.5	93.5
+25		4.1	00.8
E		2.8	02.2
+10		2.2	02.8
	3+05.27		
-10		3 6	01.4
E		36	01.4
+11.55	pt. 7.0' Ling on Conc Mon	4.58	00.37
+21		6 1	98.9
L		11.8	93.2
+35		21.8	83.2
+36		22.6	82.4
W+28'		28.8	76.2
	3+39.66		
-25		29.7	75.3
W		22.6	82.4
+20		17.8	87.2
L		11.1	93.9
+15		6.6	98.4
E		4.6	00.4
+10		5.1	99.9

	304.95		
	3+74.05 Radial thru NW 36th		
N.E. ckt on Mon		6.53	298.42 298.45 P-15
+22			0.03
+22		6.0	99.0
L		9.6	95.4
+20		16.1	88.9
W		22.4	82.6
+30		30.6	74.4
	3+99.29 EL station		
-35		30.2	74.8
SW		20.1	84.9
+20		14.4	90.6
L		9.4	95.6
+10		7.8	97.2
NE		8.2	96.8
	4+24.53		
NE		11.0	94.0
+20		9.7	95.3
L		10.4	94.6
+20		13.5	91.5
SW		17.7	87.3
+35		28.3	76.7

304.95 Bellingham

T.P.	1.38	224.35	11.98	292.97

N.E. Line Stations

4768.32 Radial thru N.E. Cor 36th

-20		12.7	81.6
SW		9.4	84.9
+20		5.7	88.6
℄		4.3	90.0
+20		4.5	89.8
NE Cor 36th		5.6	88.7

or E Line 36th = Diag Section

NE		5.6	88.7
+22		5.6	88.7
+44.1 = ℄		6.1	88.2
+22		7.1	87.2
SE Cor 36th		9.4	84.9
+15		11.3	83.0

5102.03 Radial thru SE Cor 36th

SE		9.4	84.9
+20		8.0	86.3
℄		8.2	86.1
+20		9.4	84.4
NE		10.9	83.4
+20		14.0	80.3

294.35

T.P.	8.56	301.99	0.92	293.43
Chk conc Mon P-15			3.57	298.42
				298.45
				0.03

Walker
Hardin
Hunley
2-20-46

Cross Section Intersection

Upas & Richmond St.

H. I.

	9.03	289.07	280.04
NW. B.P. Upas & Richmond	5.13	283.94	

Sec A

W cb Produced	5.8	283.27	
+3 on Pav.	6.31	282.76	
1/4 " "	6.01	283.06	
℄	5.90	283.17	
1/4 = E edge Pav.	5.98	283.09	
+7	5.9	283.17	
E cb Produced	5.0	284.07	
+5	4.3	284.77	

Sec B

-5	4.3	284.77	
E cb	5.4	283.67	
+5 = E edge Pav.	5.69	283.38	
1/4 on Pav.	5.76	283.31	
℄ " "	5.84	283.23	
1/4	5.94	283.13	
+4' W edge Pav.	6.09	282.98	
W cb.	5.4	283.67	

Indexed
C.S.K.

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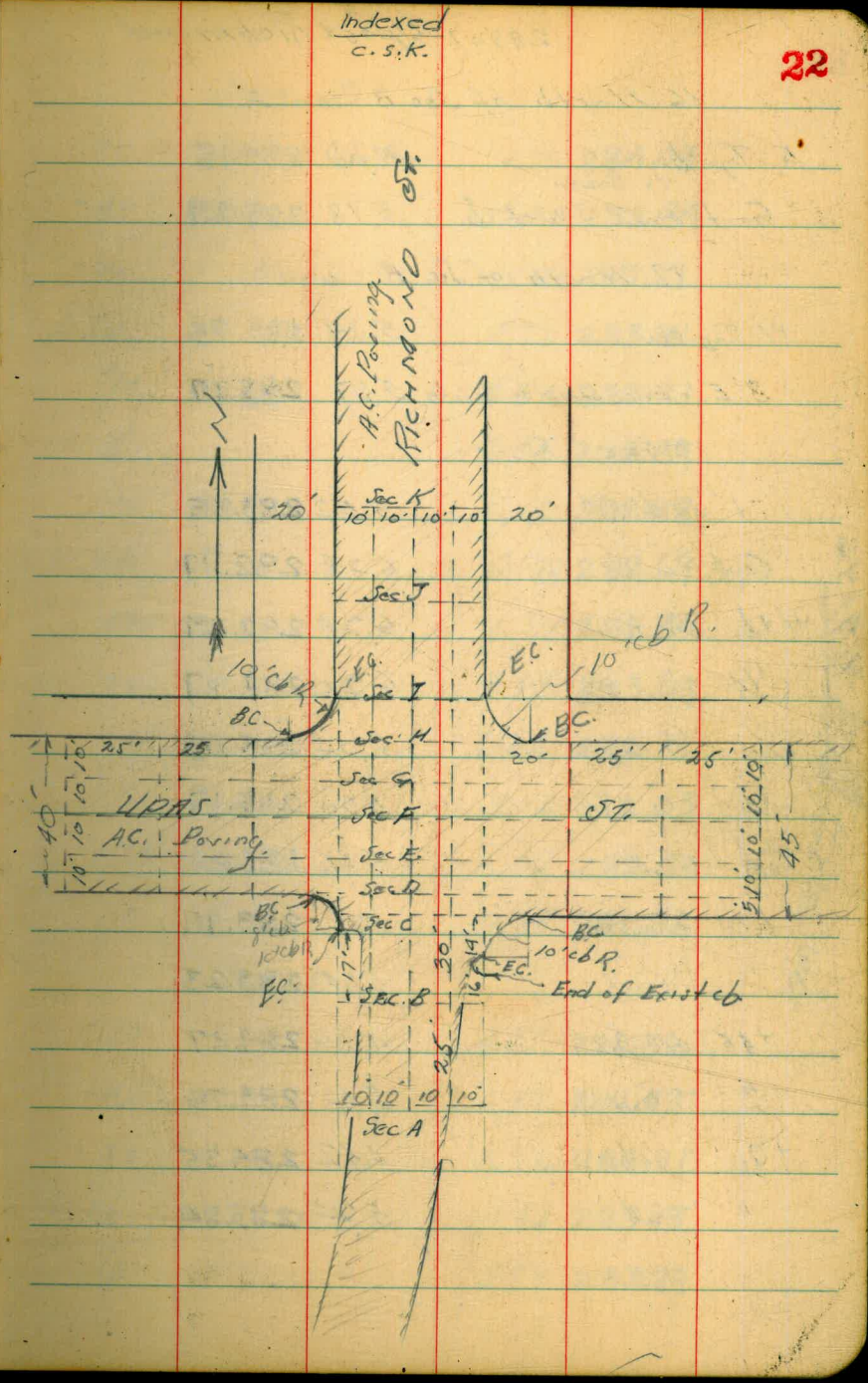


28907 Upost. Richmond

16' North of Sec. B on E		
E Top cb.	4.89	284.18
" Gut. Pav = 3' W of cb. to South	5.78	283.29
17' North of Sec B on W		
W Top cb.	5.29	283.83
3' E - Pav Strip to South	5.97	283.10
SEC. C =		
-1' on cb Rot.	5.52	283.55
Gut.	6.28	282.79
W cb. on Pav.	6.28	282.79
1/4 " "	6.20	282.87
1/2 " "	6.04	283.03
1/4	5.90	283.17
E Cb Gut.	5.86	283.21
+20 on cb.	5.16	283.91
" "Gut.	5.84	283.23
+45 on cb.	4.80	284.27
" " Gut.	5.18	283.59
+70 " cb.	4.52	284.55
" " Gut.	5.23	283.84

SEC. D		
-70' - 70' E Cb on Pav.	4.99	284.08
-45 on Pav.	5.23	283.84
-20 " "	5.56	283.51
E Cb.	5.76	283.31
1/8	5.86	283.21
1/2	6.08	282.99
1/4	6.19	282.88
W cb.	6.38	282.69
+20 Gut.	6.77	282.30
+20 on cb	6.03	283.04
+45 on cb.	6.26	282.81
" " Gut.	7.02	282.05
+70' on cb.	6.53	282.54
" " Gut	7.26	281.81
SEC E		
-70	6.75	282.32
-45	6.52	282.55
-20	6.26	282.81
W Cb.	5.94	283.13
1/4	5.78	283.29

28907 Upos & Richmond

Ø	5.58	283.49
¼	5.44	283.63
E cb.	5.28	283.79
+20'	5.03	284.04
+45'	4.69	284.38
+70'	4.44	284.63
SEC F		
-70	4.15	284.92
-45	4.39	284.68
-20	4.63	284.44
E cb.	4.92	284.15
¼	5.10	283.97
Ø	5.26	283.81
¼	5.44	283.63
W cb.	5.58	283.49
+20'	5.87	283.20
+45'	6.18	282.89
+70'	6.45	282.62
SEC G.		
-70	6.37	282.70
-45	6.09	282.98
-25	5.78	283.29
W cb.	5.56	283.51
¼	5.47	283.60
Ø	5.20	283.87
2' N=Ø MH. on Rim	5.17	283.90
¼	5.07	284.00
E cb.	4.94	284.13
+20'	4.64	284.43
+45	4.40	284.67
+70	4.17	284.90
SEC. H.		
-70' on cb	3.76	285.31
" Gut.	4.43	284.64
-45 "	4.68	284.39
" cb.	3.95	285.12
-20' "	4.14	284.93
" Gut	4.82	284.25
E. cb.	5.03	284.04
¼	5.18	283.89
Ø	5.35	283.72
¼	5.47	283.60

7/16/13 - w.w.

28907 Upos Richmond

W/cb. Gut.	5.69	283.38
+20 "	5.87	283.20
+20 on cb.	5.14	283.93
+45 " "	5.40	283.67
" "Gut.	6.10	282.97
+70' " "	6.37	282.70
" "cb.	5.64	283.43
SEC. I = N4 Upos-		
Wcb.	5.17	283.90
"Gut.	5.78	283.29
1/4	5.38	283.69
2.	5.13	283.94
1/4	5.02	284.05
Gut.	5.00	284.07
E Cb.	4.28	284.79
SEC. J		
E cb.	4.62	284.45
Gut.	5.37	283.70
1/4	5.33	283.74
2.	5.40	283.67
1/4	5.70	283.37
Gut.	6.15	282.92
W cb.	5.48	293.59

SEC K

Wcb	5.82	283.25
Gut.	6.53	282.54
1/4	6.06	283.01
2.	5.77	283.30
1/4	5.62	283.45
Gut.	5.70	283.37
E Cb.	4.96	284.11
chk Starting BM	9.03	280.04

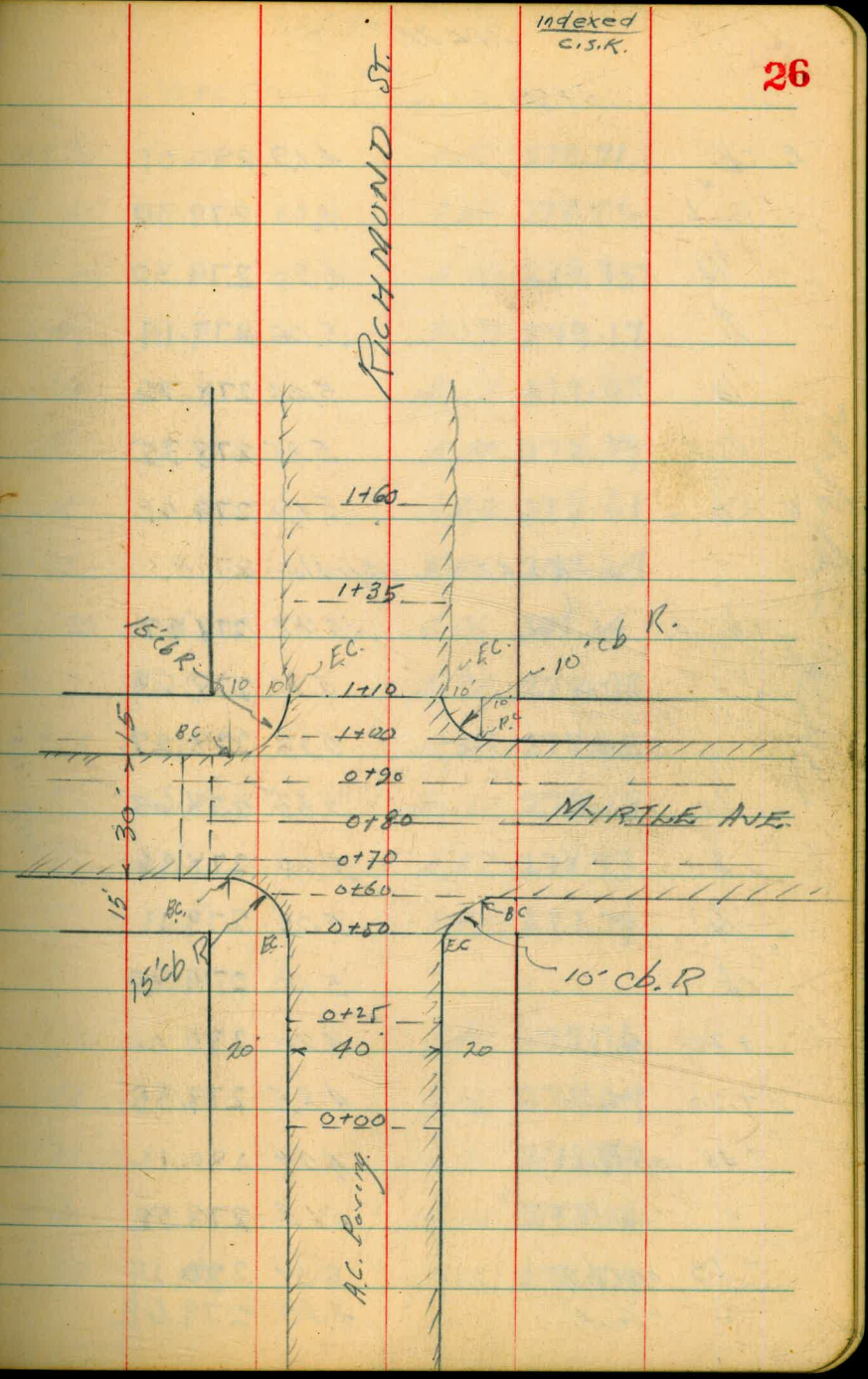
Elev. Returns P-31

Walter
Hardin
Hinley
Begg
2-20-46

CROSS SECTION - INTERSECTION MYRTLE AND RICHMOND ST

Indexed
C.S.K.

		B.M.	
	4.16	284.20	280.04
	0+00		
E cb.		3.60	280.60
Gut.		4.22	279.98
¼		4.17	280.03
℄ on Rim MH		4.27	279.93
¼		4.68	279.52
Gut.		5.12	279.08
cb.		4.44	279.76
	0+25		
cb.		4.80	279.40
Gut.		5.49	278.71
¼		5.06	279.14
℄		4.74	279.46
¼		4.60	279.60
Gut.		4.56	279.64
cb.		3.86	280.34



284.20

0+50

E cb.	4.19	280.01
Gut	4.90	279.30
1/4	4.90	279.30
℄	5.06	279.14
1/4	5.44	278.76
Gut.	5.85	278.35
W cb.	5.19	279.01
0+60 = 5 cb Myrtle on E		
cb - 4' on cb Rot.	5.23	278.97
" " Gut. Produced	5.91	278.29
W/cb Gut.	5.93	278.27
1/4	5.55	278.65
℄	5.24	278.96
1/4	5.09	279.11
cb.	5.00	279.20
+20 on cb.	4.20	280.00
+20 " Gut	4.85	279.35
+45 on cb	4.04	280.16
" " Gut.	4.68	279.52
+70 on cb	3.91	280.29
" " Gut.	4.58	279.62

4.5

284.20

0+65 = cb Line on South W/

cb-70	4.49	279.71
cb-45	4.64	279.56
" - 20	4.85	279.35
E cb.	5.03	279.17
1/4	5.17	279.03
℄	5.31	278.89
1/4	5.59	278.61
W cb	5.96	278.24
+20 on cb.	5.06	279.14
" " Gut.	5.77	278.43
+45' on cb	5.58	278.62
" " Gut	6.02	278.18
+70' W cb	5.87	278.33
" " Gut.	6.41	277.79
0+70		
-70'	6.44	277.76
-45	6.16	278.04
-20'	5.90	278.30
W cb.	6.04	278.16
1/4	5.66	278.54

	0+70	284.20		
℄			5.38	278.82
E ¼			5.22	278.98
E cb.			5.04	279.16
+20'			4.82	279.38
+45'			4.62	279.58
+70'			4.44	279.76
	0+80			
-70'			4.56	279.64
-45			4.71	279.49
-20'			4.91	279.29
E. Cb			5.19	279.01
¼			5.35	278.85
℄			5.53	278.67
¼			5.82	278.38
W Cb.			6.19	278.01
+20'			5.92	278.28
+45'			6.22	277.98
+70			6.62	277.58
	0+90			
-70'			7.32	276.88
-42'			6.88	277.32

9/10/42 - W.W.

		284.20		
-20			6.48	277.72
W Cb			6.55	277.65
W ¼			6.18	277.02
℄			5.83	278.37
E ¼			5.63	278.57
E cb.			5.48	278.82
+20			5.29	278.91
+45			5.13	279.07
+70			4.94	279.26
	0+95			
-70'			5.15	279.05
-45'			5.32	278.88
-20'			5.56	278.64
E cb.			5.68	278.52
E ¼			5.84	278.36
℄			6.06	278.14
W ¼			6.41	277.79
cb.			6.82	277.38
+20	on Cb		6.15	278.05
"	" Gut		6.68	277.52
+45'	on cb		6.74	277.46
"	" Gut.		7.26	276.94
+70'	on cb		7.10	277.10
"	" Gut		7.65	276.55

9/10/42 - W.W.

1+00		
Wcb-4' on cb Ret.	6.08	278.12
" " "Cut Inlet.	7.08	277.12
W cb : Pav.	7.01	277.19
W 1/4	6.59	277.61
℄	6.26	277.94
E 1/4	6.00	278.20
E cb.	5.86	278.34
+20 on cb.	5.17	279.03
" "Cut.	5.84	278.36
+45' on cb.	4.99	279.21
" "Cut.	5.58	278.62
+70' on cb.	4.72	279.98
" "Cut.	5.32	278.88
1+10 = N.L. = End Exist. cb.		
E cb.	5.14	279.06
Cut.	5.71	278.49
E 1/4	5.90	278.30
℄	6.07	278.13
1/4	6.52	277.68
Cut	6.91	277.29
cb.	6.02	278.18

1+20		
cb-4	6.1	278.10
"-2' on Rolled Asphalt cb	6.20	277.00
W cb. " " "	6.69	277.51
Cut	7.08	277.12
W 1/4	6.68	277.52
℄	6.19	278.01
E 1/4	6.06	278.14
+8	6.05	278.15
+9	5.98	278.22
cb. on Rolled Asphalt cb	5.60	278.60
+2'	5.35	278.85
+4 on "Walk	5.34	278.86
1+35		
-1'	5.96	278.29
-2'	6.10	278.10
E cb.	6.58	277.62
+1	6.84	277.36
E 1/4	6.69	277.51
℄	6.72	277.48
W 1/4	7.08	277.12
+9	7.57	276.63
W cb.	7.36	276.84
+2'	6.82	277.38

	1+35	28420	Myrtle & Richmond	
W Cb+4			6.7	277.50
	1+60			
W Cb-4			7.7	276.50
-2'			7.79	276.41
Cb.			8.12	276.08
+1			8.22	275.98
'14			7.96	276.24
L			7.58	276.62
E'14			7.70	276.50
+9			7.92	276.28
Cb.			7.47	276.73
+2			7.22	276.98
+4			7.1	277.10
	NE Return L=15.7' 3 Parts.			
on cb. = PC.			5.24	278.96
" Gut.			5.86	278.34
① on Gut.			5.86	278.39
② " Gut.			5.88	278.32
E.C. "			5.71	278.49
cb			5.14	279.06

NW Ret. L=23.7' 3 Parts		
E.C. on Cb.	6.02	278.18
" " Gut	6.91	277.29
① "	7.05	277.15
② "	7.10	277.10
3 PC. on Gut.	6.78	277.42
" " cb	6.06	278.14
SW Ret. L=23.7 3 Parts		
BC. on cb.	5.13	279.05
" " Gut.	5.80	278.40
① " "	5.89	278.31
② " "	5.88	278.32
③ EC "	5.85	278.35
" on Cb	5.19	279.01
SE Ret L=16.7' 3 Parts.		
E.C. on cb	4.19	280.01
" " Gut	4.90	279.30
① "	4.90	279.30
② "	4.88	279.32
③ BC cut.	4.86	279.34
" cb.	4.22	279.98

Walker
2-21-46

Levels on Returns
Upas & Richmond Cont. from P-25
Sketch P-22

	6.32	290.26		283.94	BM NW Cor. Upas & Richmond
	NE Ret	L=15.7		3 Parts	
B.C. on cb.			5.41	284.85	
" Gut.			6.06	284.20	
① "			6.09	284.17	
② "			6.13	284.13	
③ E.C. Gut.			6.16	284.10	
" on cb.			5.44	284.82	
	NW Ret.		L=15.7	3 Parts	
E.C. on cb.			6.35	283.91	
" " Gut.			6.95	283.31	
① "			6.98	283.28	
② "			6.91	283.35	
③ = BC "			6.97	283.29	
" cb.			6.30	283.96	
	SW Ret.				
B.C. on cb.			7.12	283.14	
" " Gut.			7.81	282.45	
①			7.60	282.66	
②			7.40	282.86	
③ = E.C. on cb.			6.40	283.86	
" " Gut			7.06	283.20	

ww 2/21/46

290.26

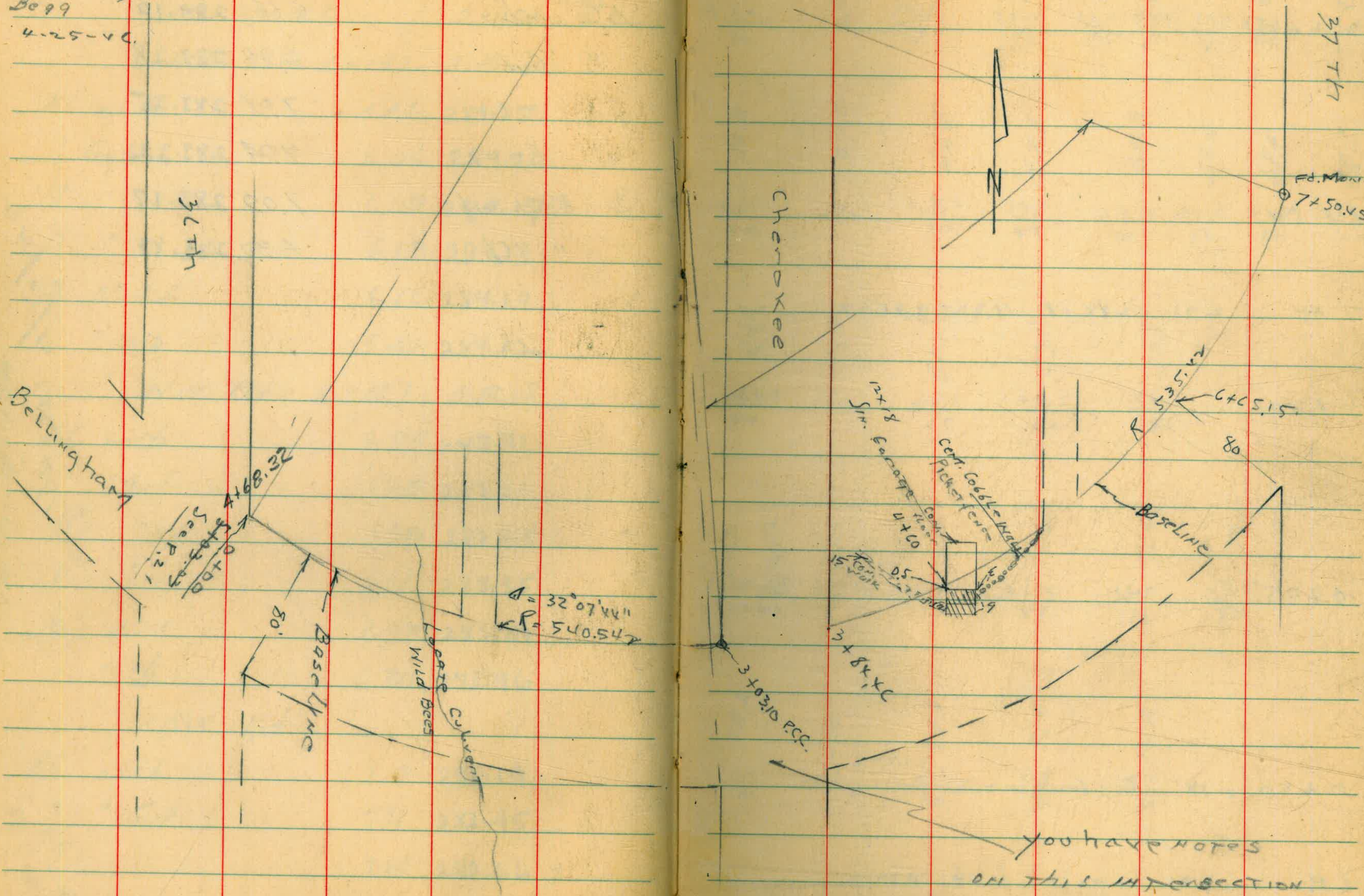
SE Return L=15.7 3 Parts

E.C. on cb.		6.16	284.10
" " Gut.		6.98	283.28
① "		7.01	283.25
② "		7.04	283.22
③ BC on Gut		7.09	283.17
" " Cb.		6.39	283.87

ww 2/21/46

Cross Section of Bellingham, 36th to 37th

C. Moore
Sonnenmeyer
Begg
4-25-4C



Bellingham

					LT
2+00					
L+50					
T.P.	2.91	284.18	11.37	281.27	63.4
L+10					29.2 / 40
					59.5
0+95					33.1 / 40
0+50 = 50' SEly from NE Cor 36th & Bellingham					
T.P.	3.51	292.64	10.49	289.13	
NW Cor. Condition 36th & Bellingham P.15	1.17	299.64		298.45	

N.6. Baseline

								Rt.
286.2	82.5	91.1	63.8	61.8	49.8	44.7	44.3	49.7
+2.0 / 10	1.7	13.1 / 18	20.4 / 40	22.4 / 52	34.4 / 80	39.5 / 90	39.9 / 110	34.5 / 125
77.8	67.0	56.0	52.1	50.3	54.6	61.4	67.6	
6.4 / 25	17.2	28.2 / 20	32.1 / 27	33.9 / 40	32.6 / 52	28.8 / 80	17.6 / 100	
		284.18						
57.4	56.8	54.1	63.1	68.9				
35.7 / 10	35.8	38.1 / 25	29.5 / 40	13.7 / 80				
57.2	57.5	61.1	66.3	76.6	79.1			
35.4 / 32	35.1	31.5 / 23	26.3 / 40	16.0 / 70	13.9 / 80			
78.2	78.8	84.9	86.8	86.8				
14.4 / 10	13.8	7.7 / 40	5.8 / 70	6.4 / 80				
		292.64						

Bellingham

Station					Lt.	H.L.				Rt.				
4						3.8 / 91.7	6.3/20 / 89.2	8.4/40 / 87.1	10.1/62 / 85.4	13.3/75 / 82.2	14.1/80 / 81.4	15.5/100 / 80.0		
3+84.46 = Radial with NE Cor Cherokee & Bellingham						6.2 / 89.3	7.8/20 / 87.7	9.1/40 / 86.4	9.8/55 / 85.7	15.0/80 / 80.5	15.3/90 / 80.2			
3+08.10														
2+75						7.6 / 87.9	8.0/12 / 87.5	9.2/19 / 86.3	10.9/40 / 84.6	13.4/68 / 82.1	19.6/80 / 75.9	25.7/100 / 69.8		
T.P.	12.20	295.55	0.83	283.35			295.55							
2+50					+4.2/10 / 88.4	+4.1 / 88.3	+2.0/31 / 86.2	1.9/40 / 82.3	23.1/80 / 61.1	31.8/101 / 52.4	44.1/133 / 40.1	44.6/160 / 39.6		
2+15					+2.7/10 / 86.9	+2.9 / 87.1	+2.9/2 / 87.1	4.9/12 / 79.3	12.2/40 / 72.0	21.6/60 / 62.6	33.1/80 / 51.1	40.5/93 / 43.7	41.5/115 / 42.7	39.5/132 / 44.7
		284.18				284.18								

Bellingham

Lt

6+00					
5+50					
5+00					
T.P. other Book	13.10	300.28	8.37	287.18	287.18 / 0.00
4+66					
4+50		295.55			

Rt.

98.3	94.1	89.8	81.8					
2.0	6.2 / 40	10.5 / 80	13.5 / 95					
96.8	92.3	88.0	85.7					
3.5	8.0 / 40	12.3 / 80	14.6 / 100					
95.7	95.6	94.5	93.0	91.0	90.6	88.8	86.3	84.8
4.6	4.7 / 6	5.8 / 7	7.3 / 30	9.3 / 36	9.7 / 40	11.5 / 55	14.0 / 80	15.5 / 100
95.32	95.32	93.92	89.1	86.2	83.9	83.3	80.7
0.73	2.3 / 33	1.63 / 113	5.4 / 40	9.3 / 67	11.6 / 75	12.2 / 80	14.8 / 100
gar. floor							
94.0	91.7	88.4	86.0	83.5	82.5	80.4	
1.5	3.8 / 20	7.1 / 40	9.5 / 66	12.0 / 73	13.0 / 80	15.1 / 100	

300.28

295.55

	Ni.			Pt	
7 + 50.45 E.C., you have					
7 + 00	3.9 96.1	9.1/40 91.2			
6 + 65.5	1.7 98.6	5.5/40 94.8	7.8/63 92.5	11.2/80 89.1	12.5/90 87.8
6 + 50	1.4 98.9	5.5/40 94.8	10.0/80 90.3	10.8/85 89.5	

300.28

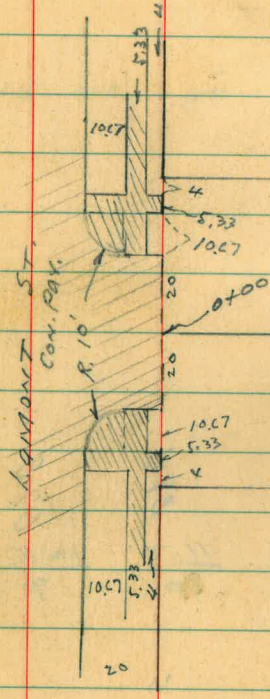
300.28

Xsec of Felspar ST. 80' wide 20' curbs

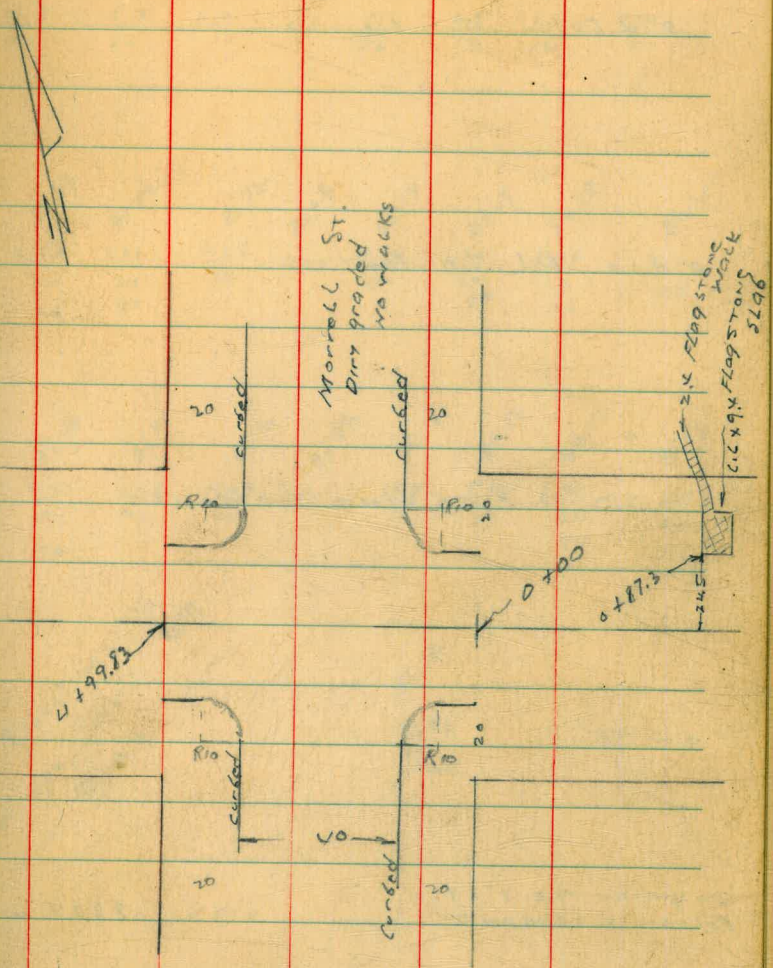
LAMONT to Noyes

For Water Line grades

C.Moore
Sommermeyer
W. Moore
Begg
5-28-46



Indexed
C.S.I.K.



Notes Reduced 6-3-46 mhenry-

xsec Felspar

0 + 50				
0 + 00 E.L. Lamont				
0 – 20 = E. C6. Line Lamont				
0 – 30				
Set BM. on N.E. 7' C.T. Felspar & Lamont			2.33	88.04 ✓
T.P.	12.26	90.37	0.86	78.11
B.M. SW B.P. Garnet & Lamont St.	13.14	78.97		65.83

85.7 LT	85.1	84.4	℄ 84.3	84.0	83.9 RT	84.2 ✓	83.2 ✓	
4.7/40	5.3/20	6.0/14	6.1	6.4/10	6.5/14	6.2/16	7.2/40	
87.9	87.83	87.06	86.72 ✓	86.08	86.17	84.27	84.89	85.2 ✓
2.5/40	2.54/20 C6	3.31/20 GT	3.65/10	4.29	4.20/10	6.10/20 GT	5.48/20 C6	5.2/40
88.01	87.40	86.79	86.30	85.84	86.18	84.53	84.02	84.76
2.36/40 C6	2.97/40 GT	3.58/20	4.07/10	4.53	5.19/10	5.84/20	6.35/40 GT	5.61/40 C6

Note: Elevations .15 Low per correct B.M. See p. 48.

85.54
4.83/10 Pav.

90.37

Felspar

T.P.	4.28	83.61	11.04	79.33
2 + 50				
2 + 00				
1 + 50				
1 + 00				
0 + 94.5	℄ do. Con. Ribbons	2' wide 6.5 overall		

90.37

LT		℄				FT
80.2	80.0	79.2	79.3	78.9	79.2	78.0
10.2 / 40	10.4 / 22	11.2 / 18	11.1	11.5 / 10	11.2 / 20	12.4 / 40
81.0	80.7	79.8	79.9	79.6	80.0	79.0
9.4 / 40	9.7 / 21	10.6 / 18	10.5	10.8 / 10	10.4 / 18	11.4 / 40
82.7	82.0	81.6	81.2	80.7	80.7	80.9	80.3
7.7 / 40	8.4 / 20	8.8 / 17	9.2	9.7 / 10	9.7 / 14	9.5 / 25	10.1 / 40
83.7	83.5	82.8	82.4	82.1	82.5	81.4
6.7 / 40	6.9 / 20	7.6 / 17	8.0	8.3 / 10	7.9 / 20	9.0 / 40
84.79	84.35	83.40				
5.58 / 49.3 gar. Con. fl.	6.02 / 40	6.97 / 19.6				

90.37

Felspar

4+00

3+75

3+50

3+02 & 3' Con. walk

3+00

83.61

Lt. C Rt.

Lt			C		Rt.		
79.5	78.8	79.6	77.3	77.0	76.6	77.8	77.5
4.1 / 40	4.8 / 28	6.0 / 18	6.3	6.6 / 10	7.0 / 17	5.8 / 26	6.1 / 40
80.7	79.7	78.3	77.7	77.3	77.2	78.5	77.9
2.9 / 40	3.9 / 25	5.3 / 20	5.9	6.3 / 10	6.4 / 15	5.1 / 25	5.7 / 40
80.7	79.7	78.6	78.0	77.9	77.7	78.4	78.1
2.9 / 40	3.9 / 27	5.0 / 17	5.6	5.7 / 10	5.9 / 17	5.2 / 23	5.5 / 40
80.52	80.19						
3.09 / 50	3.42 / 40.4						
80.0	78.9	78.9	78.4	78.3	77.4		
3.6 / 40	4.7 / 20	4.7	5.2 / 10	5.3 / 20	6.2 / 40		

83.61

Felspan

41

	Lt		℄		Rt		
4+75	76.4	75.6	74.0	74.2	73.9	73.8	75.4	75.0
	7.2 / 40	8.0 / 23	9.6 / 17	9.4	9.7 / 10	9.8 / 19	8.2 / 22	8.6 / 40
4+50	78.1	76.9	75.8	75.9	75.6	75.1	76.7	76.1
	5.5 / 40	6.7 / 20	7.8 / 17	7.7	8.0 / 10	8.5 / 17	6.9 / 22	7.5 / 40
4+30	78.5	77.9	76.8	76.7	76.3	76.0	77.3	76.7
	5.1 / 40	5.7 / 25	6.8 / 17	6.9	7.3 / 10	7.6 / 17	6.3 / 23	6.9 / 40
4+22 ℄ 7' Con. drive	78.94		78.70					
	4.67 / 50		4.91 / 40					
4+06 ℄ 7' Con. drive	79.62		79.38					
	3.99 / 50		4.23 / 39.8					

83.61

83.61

	Lt			℄			Rt	
0+00 = E.L. Morrell St.	72.8 10.8 40	72.19 11.42 20 cb end	71.2 12.4 20 gT	71.1 12.5	70.8 12.8 10	70.7 12.9 20 gT	70.88 12.73 20 cb end	70.7 12.9 40
E cb Line Morrell	72.39 11.22 40 cb	71.8 11.8 40 gT	71.2 12.4 20	71.1 12.5	70.8 12.8 10	70.6 13.0 20	70.3 13.3 40 gT	70.98 70.83 12.78 40 cb
℄ Morrell		73.2 10.4 40	72.6 11.0 20	72.1 11.5	71.8 11.8 10	71.6 12.0 20		71.1 12.5 40
W cb Line Morrell	72.4 11.2 40 gT.	73.39 10.22 40 cb	72.0 11.6 20	71.6 12.0	71.5 12.1 10	71.3 12.3 20	71.76 11.85 40 cb	70.9 12.7 40 gT
4+99.83 = W.L. Morrell St = 80' wide, 20' Curbs	73.9 9.7 40	73.40 10.21 20 cb end	72.5 11.1 20 gT	72.5 11.1	72.0 11.6 10	71.8 11.8 20 gT	71.98 11.63 20 cb end	71.9 11.7 40

Note: Elevations Low per Correct B.M. - .16 See p. 48

83.61

83.61

Felspar

Sta.				
1+00				
0+87.3 = W. edge Flagstone, Level, E & W (Slab)				
T.P.	7.20	78.35	5.07	71.15
0+50				
0+39 E do. Con. Rib. dr. 2' wide 7' overall				
0+25				
T.P.	4.98	76.22	12.37	71.24
		83.61		

	Lt			℄			Rt	
1+00	72.7	72.0	71.3	71.2	70.8	70.5	69.7	68.9
	5.6 / 40	6.3 / 25	7.0 / 20	7.1	7.5 / 10	7.8 / 20	8.6 / 25	9.4 / 40
0+87.3	72.89	72.67	72.49	72.12				
	5.46 / 40.7 E. edge Flag stone walk	5.68 / 33.9	5.86 / 26.5	6.23 / 24.5				
T.P.				78.35				
0+50	72.7	72.0	71.2	70.9	70.7	70.7	69.0	68.1
	3.5 / 40	4.2 / 28	5.0 / 20	5.3	5.5 / 10	5.5 / 20	7.2 / 26	8.1 / 40
0+39	74.31	72.84	72.42					
	1.91 / 66 Sin. gar. Con.	3.38 / 40	3.80 / 27					
0+25	72.8	72.3	71.3	71.0	70.7	70.7	69.8	69.7
	3.4 / 40	3.9 / 27	4.9 / 20	5.2	5.5 / 10	5.5 / 20	6.4 / 25	6.5 / 40
T.P.				76.22				

Fdspar

2+00

1+77.5 ℄ 2.C Con. walk with 1 step down

1+59 ℄ do. Con. Rib. dr. 2' Rib. 7' overall

1+45 ℄ C' Con. drive

1+22 ℄ 3' Con. walk

78.35

L	℄	R
72.7	72.3	71.8
5.C	C.0	C.5
X0	25	20
73.6	73.45	72.87
4.74	4.90	5.48
40	19.9	18.8
Walk	Top Walk	Top Step
	74.06	73.70
	4.79	4.C5
	50	40
	dr.	dr.
74.02	73.87	73.7
4.32	4.48	4.6
V4.2	42.7	40
Down drive		
74.03	73.90	73.62
4.32	4.45	4.73
50	42	41.3

L	℄	R
71.6	71.4	71.2
6.7	7.1	7.1
	10	15
71.6	71.1	71.0
6.7	7.2	7.3
	10	15
74.10		
4.25		
50		
drive		
71.8	71.5	70.9
6.8	7.4	7.4
	10	16

L	℄	R
72.6	73.1	72.5
5.7	5.2	5.8
17	25	40
72.9	73.6	73.1
5.2	4.7	5.2
17	25	40
72.7	72.1	
6.1	6.2	
17	40	

7835

Felspar | Lt | ℄ | Rt

2 + 90.5 ℄ do. con. Rib. Dr. 2' R.6. 6.6 overall

74.66 / 1.33 / 59.5 / 90 fl. — 74.29 / 1.70 / 56.4 / dr. — 73.57 / 2.42 / 40 / dr. — 73.54 / 2.45 / 38.2 / do.

2 + 50

73.2	72.6	72.0	71.7	71.3	71.9	71.7
2.8 / 40	3.4 / 24	4.0 / 19	4.3	4.7 / 10	4.1 / 13	4.3 / 40

2 + 47

73.0	72.6	72.2	71.7	71.3	71.5	71.5	69.7	68.4
3.0 / 40	3.4 / 24	3.8 / 19	4.3	4.7 / 10	4.5 / 16	4.5 / 21	6.3 / 26	7.6 / 40

2 + 40 ℄ do. con. Ribbon Dr. 2' wide 6.6 overall 1.93 / 59.5 / 90 fl.

73.56 / 2.43 / 56.3 / dr. — 73.10 / 2.89 / 40 / dr. — 72.71 / 3.28 / 24 / dr.

2 + 30

72.8	72.4	71.9	71.7	71.4	71.3	69.7	69.4
3.2 / 40	3.6 / 24	4.1 / 20	4.3	4.6 / 10	4.7 / 20	6.3 / 26	6.6 / 40

T.P. 3.25 75.99 5.61 72.74

78.35

75.99

Feldspar

	L	C	R	
4 + 00	70.3	69.5	68.8	68.5	68.1
	5.7 / 40	6.5 / 20	7.2 / 10	7.3 / 25	7.9 / 40
3 + 54	71.1	70.6	70.3	70.2	70.4	69.7
	4.9 / 40	5.4 / 20	5.7	5.8 / 10	5.6 / 15	6.3 / 40
3 + 50	71.2	70.6	70.4	70.4	70.4	70.9	71.5	71.2
	4.8 / 40	5.4 / 20	5.6	5.6 / 10	5.6 / 13	5.1 / 15	4.5 / 23	4.8 / 40
3 + 25	72.3	72.4	71.7	71.6	71.3	71.3	72.0	71.5
	3.7 / 40	3.6 / 27	4.3 / 15	4.4	4.7 / 10	4.7 / 12	4.0 / 13	4.5 / 40
3 + 00	73.7	73.2	72.2	71.8	71.5	72.2	71.7
	2.3 / 40	2.8 / 23	3.8 / 17	4.2	4.5 / 10	3.8 / 13	4.3 / 40

75.99

75.99

Feldspar

	Lt		℄		Rt	
W c6 + 5	66.8	66.4	65.7	65.5	64.9	
	9.2 / 40	9.6 / 20	10.3	10.5 / 10	11.1 / 40	
W c6 Noyes	68.0	67.5	65.9	65.6	65.4	66.9	65.7
	8.0 / 40	8.5 / 10	10.1 / 10	10.4	10.6 / 10	9.6 / 25	10.3 / 40
4 + 99.83 W.L. Noyes St. = 80' wide 20' Curbs	68.6	68.0	67.2	67.0	66.8	67.0	66.8
	7.5 / 40	8.0 / 10	8.8 / 6	9.0	9.2 / 10	9.0 / 23	9.2 / 40
4 + 75	68.8	68.4	67.9	67.7	67.5	67.2	67.0
	7.2 / 40	7.6 / 20	8.1 / 13	8.3	8.5 / 10	8.8 / 25	9.0 / 40
4 + 50	69.6	68.8	68.3	68.2	67.9	67.7	67.4
	6.4 / 40	7.2 / 17	7.7 / 13	7.8	8.1 / 10	8.3 / 25	8.6 / 40

75.99

75.99

Felspar

					Sisson
check to BM S.E. Top F.H. Diamond + Noyes			2.14	91.24	91.39 −0.15
T.P.	8.89	93.38	16.0	84.49	
T.P. on B.M.	8.66	86.09	0.47	77.43	
Set B.M. B.P.	N.W. curb Emerald Noyes		0.47	77.43	77.58
T.P.	7.95	77.90	6.04	69.95	

✓ = Corrected 6-15-46

Note: Elevations .15 low. For correct B.M. see above —

	Lt		℄		Rt	
E.L. Noyes St.	66.4 / 9.6 / 40	65.4 / 10.6 / 20	65.3 / 10.7	65.1 / 10.9 / 10	64.8 / 11.2 / 20	64.9 / 11.1 / 40
E cb Noyes	66.5 / 9.5 / 40	66.0 / 10.0 / 20	66.0 / 10.0	66.0 / 10.0 / 10	65.9 / 10.1 / 20	65.4 / 10.6 / 40
℄ Noyes +10	66.9 / 9.1 / 40	66.5 / 9.5 / 20	66.0 / 10.0	65.7 / 10.3 / 10	65.5 / 10.5 / 20	65.3 / 10.7 / 40
℄ Noyes St.	67.3 / 8.7 / 40	66.8 / 9.2 / 20	66.3 / 9.7	66.1 / 9.9 / 10	65.5 / 10.5 / 40	

75.99

75.99

48

C. Moore Curb Levels on
Sommermeyer
W. Moore
Begg

Emerald St. = 80' wide 20' curbs

5-29-46. Lamont to Noyes St.

For water line grades

Returns + Pav. same as at

Lamont + Felspar

Note! E.L. Lamont to E.L. Morrell = dirt Roadway

E.L. Morrell to W.L. Noyes oiled "

0 + 50

99.38	98.4	98.5	98.5	98.1	97.8	98.38
3.37 / 20 cb	4.3 / 20	4.2 / 10	4.2	4.6 / 10	4.9 / 20	4.37 / 20 cb

0 + 00 = E.L. Lamont St. Edge Con. Pav.

100.05 [99.90]	99.39 [99.24]	99.22	99.20 [99.05]	98.71	98.50 [98.35]	99.10 [98.95]
2.85 / 20 cb	3.51 / 20 gt	3.53 / 10	3.70	4.04 / 10	4.40 / 20 gt	3.80 / 20 cb

S.E. 7' C.T. Lamont & Emerald	3.76	102.75		98.99 ✓	
check to S. BP			2.4	105.76	105.95 −0.19
S.E. T.P. 7' C.T.	4.91	107.90	1.41	98.99 ✓	
N.E. 7' C.T. P. 38	12.36	100.40		88.04	

(106.03 in B.M. Book)

102.75

Lamont + Diamond

Lamont + Emerald.

Lamont + Felspar

	LT			℄		RT	
1+95	97.17 [97.14]	96.0	96.2	96.1	95.6	95.4	96.24 [96.09]
	5.63 / 20	6.7 / 20	6.5 / 10	6.6	7.1 / 10	7.3 / 20	6.66 / 20
	CB						CB
1+68	97.97	96.7	97.0	96.7	96.3	96.1	97.02
	4.78 / 20	6.0 / 20	5.7 / 10	6.50	6.4 / 10	6.6 / 20	5.73 / 20
	CB						CB
1+58	98.29 ~~98.33~~	97.0	97.2	97.0	96.6	96.1	97.33
	4.46 / 20	5.7 / 20	5.5 / 10	5.7	6.1 / 10	6.6 / 20	5.42 / 20
	CB						CB
1+48	98.40	97.2	97.5	97.2	96.8	96.3	97.42
	4.35 / 20	5.5 / 20	5.2 / 10	5.5	5.9 / 10	6.4 / 20	5.33 / 20
	CB						CB
1+00	99.04 [98.89]	98.1	97.8	97.8	97.4	96.8	98.07 [97.92] 28.95
	3.86 / 20	4.6 / 20	4.9 / 10	4.9	5.3 / 10	5.9 / 20	4.83 / 20
	CB						CB
	102.75			102.75			

4 + 50				
4 + 00				
3 + 50				
T.P.	2,75	94,66	10,84	91,91
3 + 00				
2 + 50				
		102,75		

88.48	87.3	87.5	87.4	86.7	86.5	87.21
6.18	7.4	7.2	7.3	8.0	8.2	7.45
20	20	10		10	20	20
C6						C6
90.18	89.4	89.4	89.3	88.7	88.1	88.90
4.48	5.5	5.3	5.4	6.0	6.6	5.76
20	20	10		10	20	20
C6						C6
91.85	91.0	90.9	90.9	90.7	89.9	90.68
2.81	3.7	3.8	3.8	4.5	4.8	3.98
20	20	10		10	20	20
C6						C6
			94.66			
93.60	92.6	92.5	92.5	91.9	91.7	92.40
9.15	10.1	10.2	10.2	10.8	11.0	10.35
20	20	10		10	20	20
C6						C6
95.28	94.1	94.3	94.2	93.8	93.4	94.17
7.47	8.6	8.4	8.5	8.9	9.3	8.58
20	20	10		10	20	20
C6						C6
			102.75			

0+00 = E.L. Morrell St.
Beg. oil Pav.

E cb Morrell

℄ Morrell

W cb Morrell

5+00 ± = W.L. Morrell = 80' wide
20' cbs.
8" Curb Returns
Same as on
Felspar + Morrell
No walks

Note Elevations per Correct B.M. .15 Low
See P. 48

94.CC

Lt ℄ Rt.

85.95 [85.80] 84.9 84.7 84.5 84.3 84.0 84.51 [84.36]
8.8C 20 cb | 9.8 20 | 10.0 10 | 10.2 | 10.4 10 | 10.7 20 | 10.30 20 cb

86.00 85.4 85.1 85.0 84.7 84.5 84.1 83.4 84.31
8.CC 40 cb | 9.3 40 | 9.6 20 | 9.7 10 | 10.0 | 10.2 10 | 10.C 20 | 11.3 40 | 10.35 40 cb

86.4 85.7 85.3 84.8 84.31
8.3 40 | 9.0 20 | 9.4 | 9.9 20 | 10.4 40

86.79 86.1 85.6 85.4 85.2 84.9 84.7 84.3 85.25
7.87 40 cb | 8.C 40 | 9.1 20 | 9.3 10 | 9.5 | 9.8 10 | 10.0 20 | 10.4 40 | 9.41 40 cb

86.98 [86.83] 85.8 85.7 85.7 85.3 85.0 85.58 [85.43]
7.83 20 cb | 8.9 20 | 9.0 10 | 9.0 | 9.2 10 | 9.7 20 | 9.23 20 cb

94.CC

2+50				
2+00				
1+50				
1+00				
T.P.	2.38	86.21	10.83	83.83
0+50				
		94.66		

Lt			℄		Rt	
81.50	80.5	80.5	80.5	80.0	79.6	80.15
4.71	5.7	5.7	5.7	6.2	6.6	6.06
20	20	10		10	20	20
C6						C6
82.34	81.2	81.4	81.2	80.8	80.4	81.09
3.87	5.0	4.8	5.0	5.4	5.8	5.12
20	20	10		10	20	20
C6						C6
83.29	82.4	82.3	82.1	81.6	81.2	81.85
2.92	3.8	3.9	4.1	4.6	5.0	4.36
20	20	10		10	20	20
C6						C6
84.06	83.1	83.2	83.0	82.4	82.0	82.58
2.15	3.1	3.0	3.2	3.8	4.2	3.63
20	20	10		10	20	20
C6						C6
			86.21			
84.88	84.1	84.0	83.4	83.5	83.1	83.57
9.78	10.6	10.7	10.8	11.2	11.6	11.14
20	20	10		10	20	20
C6						C6
			94.66			

P. 78

Check to NW BP — Emerald and Noyes — 8.79 — 77.42 — 77.43 (0.01)

5+00 ± W.L. Noyes = end 8" Curbs

4+50

11+00

3+50

3+00

86.21

	℄				RT	
	77.50 [77.35]	76.4	76.3	76.0	75.5	75.1	76.1 [75.96]
	8.86 / 20 / C6	9.8 / 20	9.9 / 10	10.2	10.7 / 10	11.1 / 20	10.25 / 20 / C6
	78.16	77.4	77.3	77.0	76.6	76.1	76.87
	8.05 / 20 / C6	8.8 / 20	8.9 / 10	9.2	9.6 / 10	10.1 / 20	9.39 / 20 / C6
	78.99	78.3	78.3	78.0	77.5	77.0	77.68
	7.22 / 20 / C6	7.9 / 20	7.9 / 10	8.2	8.7 / 10	9.2 / 20	8.53 / 20 / C6
	79.85	78.9	78.9	78.7	78.1	77.8	78.43
	6.36 / 20 / C6	7.3 / 20	7.3 / 10	7.5	8.1 / 10	8.2 / 20	7.78 / 20 / C6
	80.69	79.8	79.6	79.4	79.0	78.4	79.26
	5.52 / 20 / C6	6.2 / 20	6.6 / 10	6.8	7.2 / 10	7.8 / 20	6.95 / 20

80.21

Walker
Hendricks
Hanley
Carey
6-19-46

CURB AND GUTTER ELEVATIONS
EAST SIDE 8TH AVE. from K- to L-St.

	2.24	17.23 ✓	14.99	B.M. N.W. BR. K- + 8th

Note: Location of Existing RR Track from E cb.

0+00 = S. Line K St.			
E cb.	3.38	13.85	✓
Grating	3.41	13.82	✓
Flow	4.71	12.52	✓
5.6 Rt. on E Rail	3.61	13.62	✓
" " " Pav.	3.34	13.89	✓
W Rail	3.37	13.86	✓
0+03			
cb.	3.54	13.69	✓
Gut.	4.80	12.43	✓
2' Rt	4.85	12.38	✓
5.6 Rt. Rail	3.69	13.54	✓
0+10			
Cb	3.72	13.51	✓
Gut	4.87	12.36	✓
2.5' Rt	4.34	12.89	✓
5.6 Rt	3.84	13.39	✓

indexed c.s.k.

17.23

0+25			
cb.	3.91	13.32	✓
Gut	4.81	12.42	✓
2.5' Rt.	4.57	12.66	✓
5.6 Rt E Rail	4.17	13.06	✓
W "	4.16	13.07	✓
0+46			
cb.	4.09	13.14	✓
Gut	4.93	12.30	✓
Track covered			
0+75			
cb.	4.60	12.63	✓
Gut	5.27	11.96	✓
2' Rt	5.24	11.99	✓
5.6' Rt E Rail	4.93	12.30	✓
W "	4.89	12.34	✓
1+00			
No cb.			
Gut	5.44	11.79	✓
2' Rt.	5.39	11.84	✓
5.6 " E Rail	5.13	12.10	✓
W "	5.10	12.13	✓

1723

1+19 = ℄ Drive

Gut.	5.70	11.53	✓
2' Rt.	5.67	11.56	✓
5.6 Rt. E Rail	5.32	11.91	✓
W "	5.29	11.94	✓
1+27			
E ch.	5.32	11.91	✓
1+39 = ℄ 20' Drive			
Gut.	5.92	11.31	✓
4' Rt.	5.81	11.42	✓
5.6' Rt E Rail	5.56	11.67	✓
W "	5.49	11.74	✓
1+50			
E ch	5.62	11.61	✓
Gut.	6.06	11.17	✓
4' Rt	5.92	11.31	✓
6.1" E Rail	5.74	11.49	✓
" W "	5.68	11.55	✓
1+59.9 ℄ 7' Drive			
Gut	6.20	11.03	✓

1723

1+75 = ℄ 19' Drive

Gut.	6.46	10.77	✓
2' Rt.	6.44	10.79	✓
5' Rt.	6.22	11.01	✓
7.6' Rt. E Rail	6.16	11.07	✓
W "	6.13	11.10	✓
1+85			
E ch.	6.25	10.98	✓
Gut.	6.72	10.51	✓
2' Rt.	6.66	10.57	✓
5' Rt.	6.45	10.78	✓
8.5' Rt. E. Rail	6.37	10.86	✓
W "	6.35	10.88	✓
2+00			
E ch.	6.37	10.86	✓
Gut.	6.97	10.26	✓
2' Rt.	6.87	10.36	✓
7' Rt.	6.64	10.59	✓
10.5' Rt. on E Rail	6.68	10.55	✓
" W "	6.61	10.62	✓

1723

TP	471	14.96 ✓	6.98	10.25 ✓
	2+22 N end Drive			
Cb.			4.41	10.55 ✓
Gut.			4.99	9.97 ✓
2' Rt.			4.94	10.02 ✓
11.5'			4.61	10.35 ✓
13.9' Rt = E Rail			4.70	10.26 ✓
	W "		4.70	10.26 ✓
	2 Drive (Blocked)			
	2+41 = S end Drive			
Cb.			4.66	10.30 ✓
Gut.			5.43	9.53 ✓
2.3' Rt.			5.21	9.75 ✓
15' Rt.			4.90	10.06 ✓
17.2' Rt E Rail			4.95	10.01 ✓
	W "		4.96	10.00 ✓
	2+75			
Cb.			5.22	9.74 ✓
Gut			5.73	9.23 ✓
10' Rt.			5.51	9.45 ✓
19' Rt			5.38	9.58 ✓
21.6 Rt = E Rail			5.45	9.51 ✓
	W "		5.52	9.44 ✓

14.96

	2+95 = N end Inlet			
Cb.			5.46	9.50 ✓
Gut. Flow			6.10	8.86 ✓
7' Rt.			5.63	9.33 ✓
15' Rt.			5.63	9.33 ✓
21' Rt			5.71	9.25 ✓
23.2' Rt E Rail			5.79	9.17 ✓
	W "		5.85	9.11 ✓
	3+00.5 ± = N.L. L-St			
Cb.			5.46	9.50 ✓
Grating			5.50	9.46 ✓
Flow			6.65	8.31 ✓
3' Rt.			5.53	9.43 ✓
15' Rt.			5.64	9.32 ✓
21' Rt.			5.76	9.20 ✓
23.3' Rt E Rail			5.85	9.11 ✓
	W "		5.51	9.45 ✓
TP	6.07	18.23 ✓	2.10	12.86 ✓
Cbk. Starting BM.			3.94	14.99 ✓

Indexed
C.S.K.

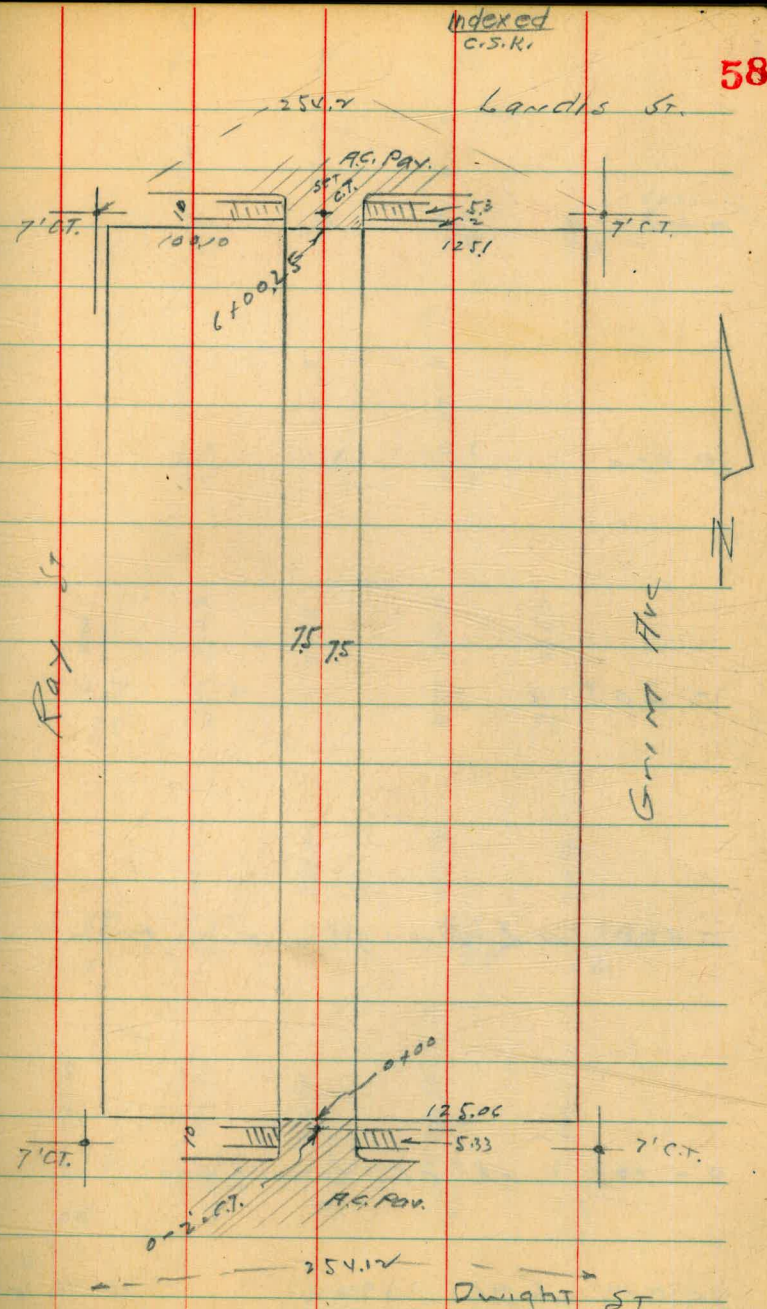
58

Xsec Blk H. McFadden & Buxton

" " " 3 Park Villas

Rush Survey

C. Moore
Begg
Allen
7-1-4C.
Also Semmermeyer



Station			W LT	℄	E RT	
0+47			336.2 3.2 7.5	336.2 3.2	336.3 3.1 7.5	Beg. Lattice fence 7.6
0+20			336.0 3.4 7.5	335.8 3.6	335.8 3.6 7.5	
0+05		334.7 4.7 7.5	334.2 5.2 3	334.2 5.2	334.3 5.1 4	335.3 4.1 7.5
0+00	N. G. Dwight edge pav.	333.54 5.88 CG	333.47 5.95 7.5	333.47 5.95	333.79 5.63 7.5	333.83 5.59 CG
0-10	N CG Dwight	333.29 6.13 CG	332.86 6.56 7.5 P	332.95 6.47 P	332.99 6.43 7.5 P	333.43 5.99 CG

NEBP 6.96 339.42 332.46 Ray + Dwight

339.42

1+25

T.P 5.49 342.48 2.43 336.99

1+11 gas. w. entrance

1+08 7.8. Lt Bd. fence

0+91 E 2' Con. walk

0+75

0+74 C.L LT to P.P.T NE Con Gas. Beg. fence 7.8 Lt.

0+58 S.E. Con gas. S. entrance

339.42

	Lt	℄	Rt
336.9	337.0	337.0	337.0
5.6 / 30	Fence 7.6	5.5 / 7.5	5.5 / 7.5	Fence 7.6	5.5 / 30
	SE Cor 9.5	337.2 2.2 / 7.5	337.0 2.4	336.9 2.5 / 7.5	Fence 7.8	336.7 2.7 / 30
		337.03 V. 0.9 / 8			
336.7	336.9	337.0	336.9	336.6
2.7 / 30	2.5 / 7.5	2.4	2.5 / 7.5	2.8 / 30
				Fence 7.6
336.42	336.2 3.2 / 8 dirt			

339.42

2+52 7.5 Lt: End picket fence

2+40

2+26 C[7] Lt: ⊕ 12' P. pole.

2+18 7.5 Lt. ⊕ ? Floor gar.

2+00

1+67 Ctr. 26' shed on left.

342.48

Lt	℄	Rt
337.7	337.8	337.8	337.8	337.6
4.3 / 30	4.5 / 7.5	4.7	4.7 / 7.5	4.9 / 30
			Fence 7.8	
	337.88			
	4.60			
	Bottom door 7.5			
337.2	337.6	337.3	337.3	337.2
5.3 / 30	Fence 7.8 / 4.9 / 7.5	5.2	5.2 / 7.5	Fence 7.8 / 5.3 / 30
337.2		337.1	337.3	337.3
5.3 / 7.5	shed 7.5	5.4	5.2 / 7.5	Fence 7.5 / 5.2 / 30
	342.48			

3+26 = 50 End 2E Conc Walk

3+24 6L Lt: Ctr. 12" P. pole

3+15 7E Lt. = NE. Cor. Frame Bldg.

3+00

2+96 8= Rt = ℄ 2E' Brick walk

2+74 8= Rt = S.E. Cor Frame Bldg

342.48

Lt		℄		Rt	
	338.3				
	4.17				
	7.8				
	338.4	338.32	338.2		338.0
Bldg.	4.1	4.16	4.3	Fence	4.5
7.7	7.5	M.H. Rim	7.5	7.9	30
			338.07		
			4.41		
			8=		
337.8	338.1	338.2	338.2		338.0
4.7	4.9	4.3	4.3	Fence	4.5
30	7.5		7.5	7.8	30
8= S.E. Cor Frame Bldg.					

342.48

		Lt	℄	Rt
4+00	7.9 Lt = N.E. Cor. Fr. Bldg 12' Wide	338.3 4.2 30	338.5 start slat Fence 7.9 338.3 4.0 7.5	338.1 4.2 338.2 4.4 7.5 Fence 7.6 4.3 30
3+95	7½ Rt = ℄ 2ᵉ conc. walk		338.2 4.22 7.7 walk	Fence 7.7
3+76	7½ Lt = End slat fence S.E. Cor. Stucco Gar. W. Ent. 12' Wide	338.2 4.3 30	338.0 4.5 7.5 338.0 4.5	338.1 4.4 7.5 Fence 7.7 338.2 4.3 25
3+45	8ᵉ Rt = ℄ 2ᵉ conc. walk			337.73 4.75 8ᵉ on walk
3+42	7½ Lt = start slat Fence			
3+38	7½ Lt = N. End Conc walk 2ᵉ Wide	338.38 4.15 7.8 on walk	338.3 4.2 7.5 338.1 4.4	338.0 4.5 7.5 Fence 8ᵉ 337.8 4.7 30
	342.48		342.48	

Sta.	Note / Readings				Lt. West	Fence		℄		Fence	Rt East
4+92	7.8 Lt = ℄ 3' Conc walk						4.23 / 7.8 on walk (339.47)				
4+76	6.5 Lt = Ctr. 12" P. pole										
4+65					5.1 / 30 (338.6)	Fence 7.5	5.0 / 7.5 (338.7)	4.8 (338.9)	5.0 / 7.5 (338.7)	Fence 7.5	5.1 / 30 (338.6)
4+41	7.7 Lt = ℄ 3' Conc. walk						5.10 on walk 7.7 (338.60)				
4+26					5.5 / 30 (338.2)	Fence 7.5	5.3 / 7.5 (338.4)	5.3 (338.4)	5.2 / 7.5 (338.5)	Fence 7.5	5.2 / 30 (338.5)
T.P1	5.28	343.70 / 342.48	4.06	338.42				343.70			

343.70

6+96.5 7.5 Rt. = End Fence

5+94.5 = 7.9 Lt = N.E. Cor. Stucco Gar. No. Ent.

5+77 7.8 Lt = End Fence also S.E Cor. Stucco Gar. N. Ent.

5+62

5+26

5+00

343.70

	Lt		℄		Rt	
	342.2	342.3	342.3		342.4	
	3.5 / 7.5		3.4	Fence / 7.5	3.3 / 7.5	
342.2	342.3	342.3	342.0		340.0	340.0
3.5 / 30	3.4 / 7.5		3.7	Fence / 7.3	3.7 / 7.5	3.7 / 30
339.7	339.7	339.7			339.7	339.7
4.0 / 30	Fence / 7.6	4.0 / 7.5	4.0	Fence / 7.3	4.0 / 7.5	4.1 / 30
339.7	339.7	339.5		339.1		339.0
4.0 / 30	4.0 / 7.5	Fence / 7.5	4.2	Fence / 7.5	4.6 / 7.5	4.7 / 30
339.4	339.7	339.4	339.0			338.9
4.2 / 30	4.0 / 7.5	Fence / 7.3	4.3	4.7 / 7.5	Fence / 7.7	4.8 / 30

343.70

				0.05
S.E.B.P. Landis St			shown as	340.71
Ray. Sts.			4.61	340.96
T.P.	5.09	345.57	3.22	340.48

6+10.25 = S. Cl. line Landis

346.12	339.77	339.82	339.77	340.04
3.58	3.93	3.88	3.93	3.66
Top Cl.	Cut		Cut	Top. Cl.
7.5	9.5		7.5	7.5

340.45	340.22	340.00	340.05	340.11
3.25	3.48	3.70	3.65	3.59
Top. Cl.	Cut.	Paving	Cut	Top Cl.
	7.5		7.5	

6+00.25 S. Line Landis St.

343.70

Walker
Hendricks
Allen
7-23-46

Cross Section - Opal St.

70' Wide
15' cbs 10' 1/4s

from Coss St. to Dowes St.

					BM. 5417 Jack Wilbur + Coss-Grd. 143/40
	12.27	92.92		80.65	
T.P.	8.94	101.48	0.38	92.54	
T.P.	7.38	108.30	0.56	100.92	St. 7' Jack Opal + Coss
	0-40' = ℄ Coss St.				
-5' NL +15			5.46	102.84	
= cb.			6.00	102.30	
1/4			6.33	101.97	
℄			6.61	101.69	
1/4			6.89	101.41	
cb.			7.15	101.15	
SL +5' = opp cb BC			7.82	100.48	
	0-24				
SL -5'			8.04	100.26	
SL +15 = cb			7.50	100.80	
1/4			7.20	101.10	
℄			6.86	101.44	
1/4			6.57	101.73	
cb.			6.31	101.99	
NL +5			5.71	102.59	

Indexed
C.S.K.
7-25-46 - Notes Reduced - mmerry - -

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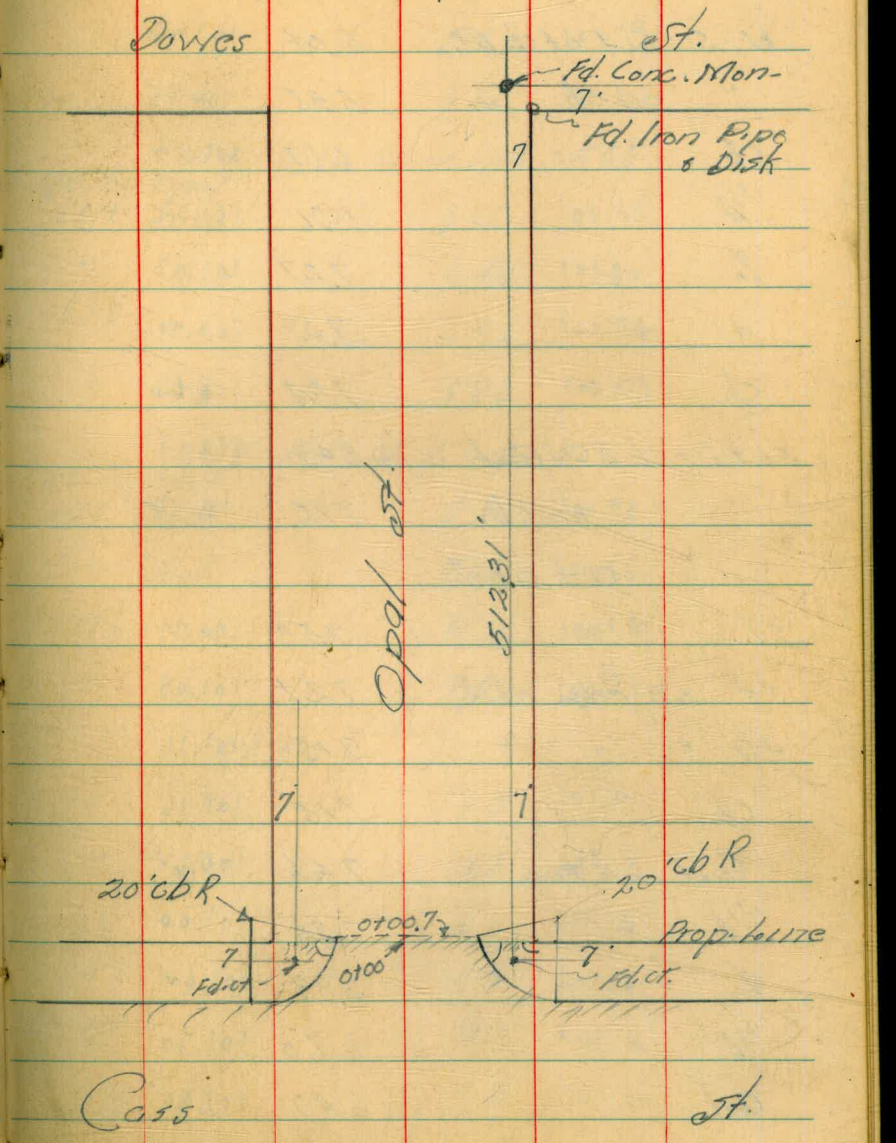


10830 - Opal St.

0-1+		
N-5 Cut at cb. BC	6.04	102.26
" on cb "	5.35	102.95
cb	6.66	101.64
1/4	6.96	101.34
℄	7.27	101.03
1/4	7.59	100.71
cb.	7.84	100.46
SL+5 - cb BC. Cut.	8.43	99.87
" " on cb.	7.76	100.54
0+00.7		
SL.	7.53	100.77
+4' on edge Walk	7.21	101.09
+9 " " "	7.19	101.11
cb.	7.15	101.15
Cut on Pav.	7.66	100.64
1/4 " "	7.30	101.00
℄ " "	6.88	101.42
1/4 " "	6.60	101.70
Cut	6.49	101.81
cb	5.86	102.44

10830

cb +6' on edge Walk	5.72	102.58
+9 " " "	5.51	102.79
NL.	5.2	103.1
N.E. Rot. cb Length - 26.8'		
BC. on Opal +8.9' on cb	5.95	102.35
" "Cut.	6.48	101.82
+17.8 " "	6.36	101.94
" "cb.	5.82	102.48
S.E. Rot cb. L = 26.4		
BC. on opal +8.8 on cb.	7.36	100.94
" "Cut	7.85	100.45
+17.6 " "	8.16	100.14
" "cb.	7.59	100.71
0+50		
-5	7.3	101.0
SL.	7.1	101.2
cb.	6.5	101.8
+2	6.5	101.8
+3	7.1	101.2
1/4	6.7	101.6
℄	6.3	102.0

	108.30		Opol St
N 1/4		6.2	102.1
+5		6.4	101.9
Cb.		5.4	102.9
N		5.2	103.1
+5'		5.0	103.3
	1+00		
-5'		4.6	103.7
N		4.9	103.4
Cb.		5.5	102.8
+2		5.3	103.0
+3		6.1	102.2
1/4		6.0	102.3
℄		5.7	102.6
1/4		6.1	102.2
+8		6.6	101.7
+9		5.9	102.4
Cb		5.9	102.4
S		6.5	101.8
+5		6.6	101.7
	1+27 = ℄ 2' Conc. Walk on N 13¢ in St.		
NL. on Walk		4.21	104.09
+13¢ on end Walk		4.80	103.50

108.30		
3' Ribbons.		07' Back 69
1+39.5 = Beg. Conc. Drive on South		
SL. +0.7' on Conc. Dr	5.89	102.41
+10 " " .	6.30	102.00
1+47.5 = E edge Dr		
SL-1.0' on Dr.	6.28	102.02
SL-0.7' " "	5.88	102.42
1+50		
-5	6.1	102.2
SL.	5.6	102.7
Cb	5.4	102.9
+4	5.4	102.9
+7	5.7	102.6
1/2	5.6	102.7
℄	5.0	103.3
1/4	5.2	103.1
+5	5.7	102.6
+7	4.7	103.6
Cb	4.7	103.6
N	3.9	104.4
+5	4.0	104.3

10830

2+00

-5		2.6	105.7
N		2.8	105.5
cb.		3.3	105.5
+5		3.5	105.3
+7		4.2	104.1
1/4		4.0	104.3
℄		4.0	104.3
1/4		4.7	103.6
+N		4.2	104.1
cb.		4.4	103.9
5		5.1	103.2
+5		5.2	103.1

2+50

-5'		3.8	104.5
5		3.7	104.6
cb		3.2	105.1
+7		3.1	105.2
1/4		3.7	104.6
℄		2.9	105.4
1/4		3.1	105.2

10830

1/4+5'			3.3	105.0
+8			1.7	106.6
cb.			1.8	106.5
N			2.0	106.3
+5			2.2	106.1
	2.784.6		℄ 2' Conc. Walk on South.	147' in St
54	on Walk		1.72	106.50
+147	" "		1.65	106.65
TP	11.43	117.25	1.78	106.52

3+00

5		10.3	107.6
N		10.3	107.6
cb		10.4	107.5
+3		10.3	107.6
+5		11.3	106.6
1/4		11.0	106.9
℄		10.7	107.2
1/4		11.1	106.2
+2		11.6	106.3
+9		10.8	107.1
cb.		10.8	107.1
5		10.7	107.2
+5		10.8	107.1

		11795	Opal St.	
	3+50			
-5			9.5	108.4
S			9.3	108.6
Cb.			8.9	109.0
+7			9.0	108.9
+9			9.7	108.2
¼			9.7	108.2
L			9.0	108.9
¼			9.0	108.9
+3			9.0	108.9
Cb			8.6	109.3
N			7.7	110.2
+5			7.5	110.4
	4+00			
-5			6.7	111.2
N			6.8	111.1
Cb.			7.8	110.1
+3			8.1	109.8
¼			7.7	110.2
L			7.8	110.1
+8			8.4	109.5
¼			7.6	110.3

		11795		
Scb.			7.6	110.3
S			8.2	109.7
+5			8.2	109.7
	4+50			
-5			6.7	111.2
SL			6.7	111.2
Cb.			6.4	111.5
¼			6.3	111.6
+1			6.7	111.2
L			6.4	111.5
¼			6.2	111.7
+5			6.3	111.6
+7			5.9	112.0
Cb			5.8	112.1
N			5.1	112.8
+5			5.1	112.8
	4+98.31-¼L. Dowes			
-5			3.9	114.0
N			4.0	113.9
Cb.			4.7	113.2
+4			4.5	113.4
+6			4.9	113.0

		117.95		Opal St.
N/A			4.6	113.3
℄			4.6	113.3
+9			5.0	112.9
½			4.7	113.2
℄			4.7	113.2
SL			5.0	112.9
S.L. on Pipe			5.01	112.94
+5			5.0	112.9
T.P.	0.61	106.15	12.41	105.54
T.P.	0.34	93.86	12.63	93.52
Chk. Starting B.M.			13.21	80.65 ✓

Cross Section Alley Block 4
Washington Heights
Levels next page

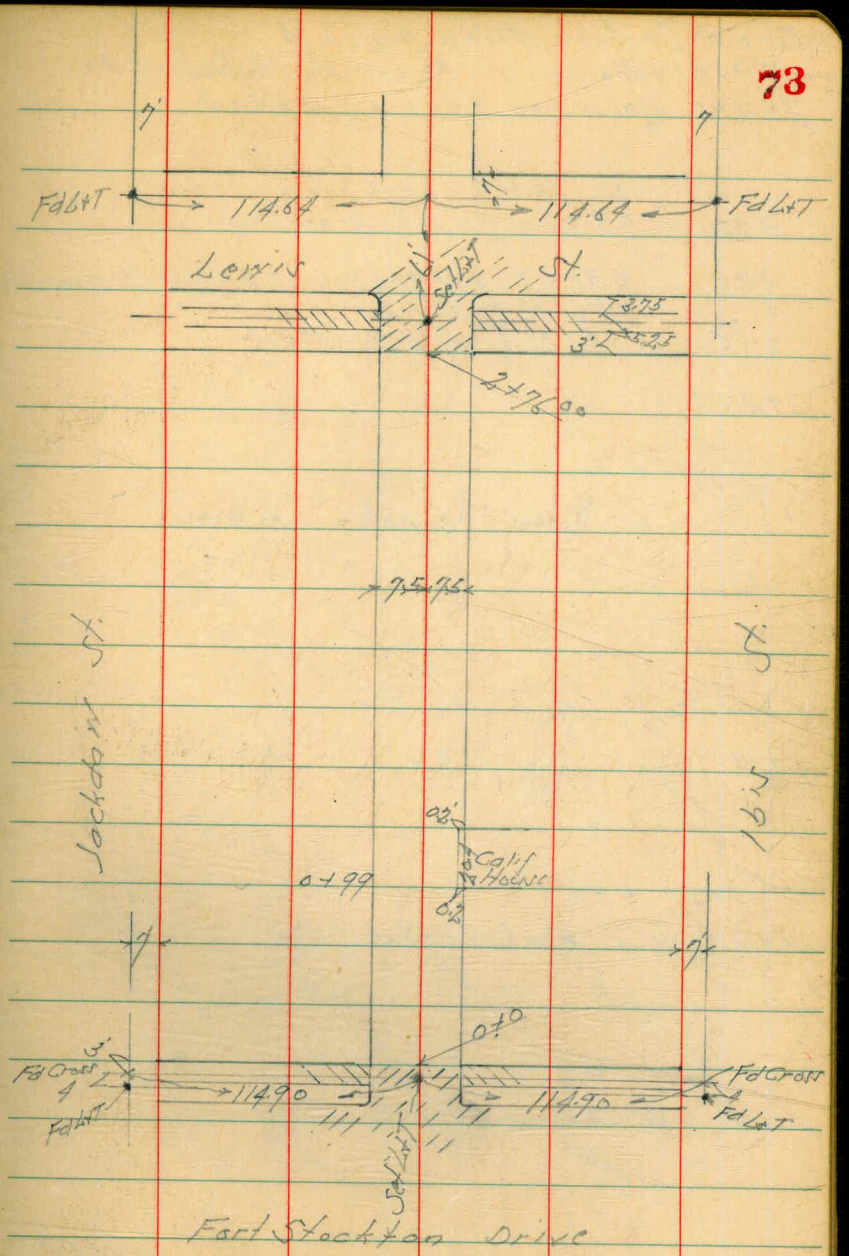
Indexed
C.S.K

Sept 18-46

Sisson
McCoy
Waddell
Alley

W.O. 24

FOR FRANK WHERRY
G.W.E.



Cross Section Alley Block 4
Washington Hts From Fort Stockton to
Lewis Between Ibis + Jackdaw

+72 8.1 Lt of ℄ = Lath Fence
7.2' Rt of ℄ = Nly Board Fence

+52 7' Rt of ℄ = Ely Tel Pole 7.2' Rt of ℄ = Sly Board Fence
7.5 Lt of ℄ = Sly La

+50 6.9 Lt of ℄ = Wly Power Pole

Notes Reduced - 9-13-46
Wherry -

Sta		Lt=W	℄		Rt=E
+47		272.3 / 4.3 / 7.5	272.3 / 4.3	272.3 / 4.3 / 7.5	272.26 / 4.36 / 7.9 = Lt Door on Conc
+32	272.35 / 4.27 / 10.3 = S Ely Conc Walk				
+19	272.57 / 4.05 / 10.2 = N Ely Conc Walk	272.1 / 4.5 / 7.5	271.9 / 4.7	271.8 / 4.8 / 7.5	271.45 / 5.17 / 7.9 on Conc Footing
0+0 = N.L. Fort Stockton Drive	271.87 / 4.75 / 7.4 = Cb	271.65 / 4.97 / 7.4 = Gutter	271.21 / 5.41 on Pav.	271.54 / 5.08 / 7.5 = Gutter	271.69 / 4.93 / 7.5 = Cb
0-10 = N Cb Line Fort Stockton	271.58 / 5.04 / 8.5 = Cb	271.11 / 5.51 / 8.5 = Gutter	271.02 / 5.60 on Pav	271.00 / 5.62 / 8 = Gutter	271.49 / 5.13 / 8 = Cb

BM 6.10 276.62 270.52 N.H. B.P. Fort Stockton + Jackdaw 276.62

+40	8.4 Lt of ℄ = Sly Lath Fence			
+38				
+29				
+15	8.2 Lt of ℄ = Hly Woven Wire Fence			
TP	5.15	277.90	3.87	272.75
1+0				
+96	8.1 Lt of ℄ = Sly Woven Wire Fence 6.5 Rt of = Sly 27" NHS Board Fence			
+95				
+89				
0+75				
		276.62		

Lt. ℄ Rt.

274.62
5.38
11.3 = ℄ Garage Conc. Floor

273.1
4.8
6.5 = ℄ Garage Dirt Floor

277.90

272.8
6.8
7.5

272.7
6.9

272.3
4.6
7.5

272.60
4.0
11.3 = NW Do. Gar. Conc. Floor

273.08
3.54
10.5 = ℄ Garage Conc. Floor

272.4
4.1
7.5

272.6
4.0

272.6
4.0
7.5

272.62
4.00
11.3 = Sly Do. Garage Conc. Floor

276.62

+06 8.4' Lt of Δ = Sly Wire Fence
270

+93 7.2 Rt of Δ = NWly Lath Fence & Sly Coli House

+85 7.3' Rt of Δ = Sly Lath Fence
85 Rt of Δ = NWly Board Fence
+81

+54 8.5 Rt of Δ = Sly Board Fence
+53

+50 8.5' Lt of Δ = NWly Lath Fence

+48
+43 7.2 Lt of Δ = Wly Power Pole
1741 6.6' Rt of Δ = Ely Tel Pole

277.90

Lt	Δ	Rt
273.1	273.1	273.1
4.8	4.8	4.8
7.5		7.5
273.28		
4.63		
11.2 = Δ Garage Conc Floor		
273.12		
4.78		
10.9 = NWly 3 Car Gar. Conc Floor		
273.06		
4.83		
10.9 = Sly 3 Car Gar. Conc Floor		
273.1	272.9	272.8
4.8	5.0	5.1
7.8		7.5
		272.8
		5.1
		7.7 = Δ Garage Dirt Floor

277.90

+84	= Break in Paving Grade			
+79	8.3 Rt of ℄ = ℄ x 12½ 2' Hedge			
2+76.00	= S.L. Lewis			
TP	4.07	275.22	6.75	271.15
+73	8.4' Lt of ℄ = 44½ Wire Fence + 44½ 4' Hedge			
	7.5 Lt of ℄ = 44½ Power Pole			
+55				
+53	8.1 Rt of ℄ = 51½ + ℄ 2' Hedge			
+52	5.9 Rt of ℄ = 51½ Tel Pole			
+51	7.1 Rt of ℄ = 44½ Frame Garage N Entrance			
+41	7.4 Lt of ℄ = 51½ Wire Fence x ℄ 4' Wide Hedge			
+35				
+31	7.2' Rt of ℄ = 51½ Frame Garage N Entrance			
+29	7.1 Rt of ℄ = 44½ Calif House			
+24	7.5 Lt of ℄ = 44½ Wire Fence			
2+14				
		277.90		

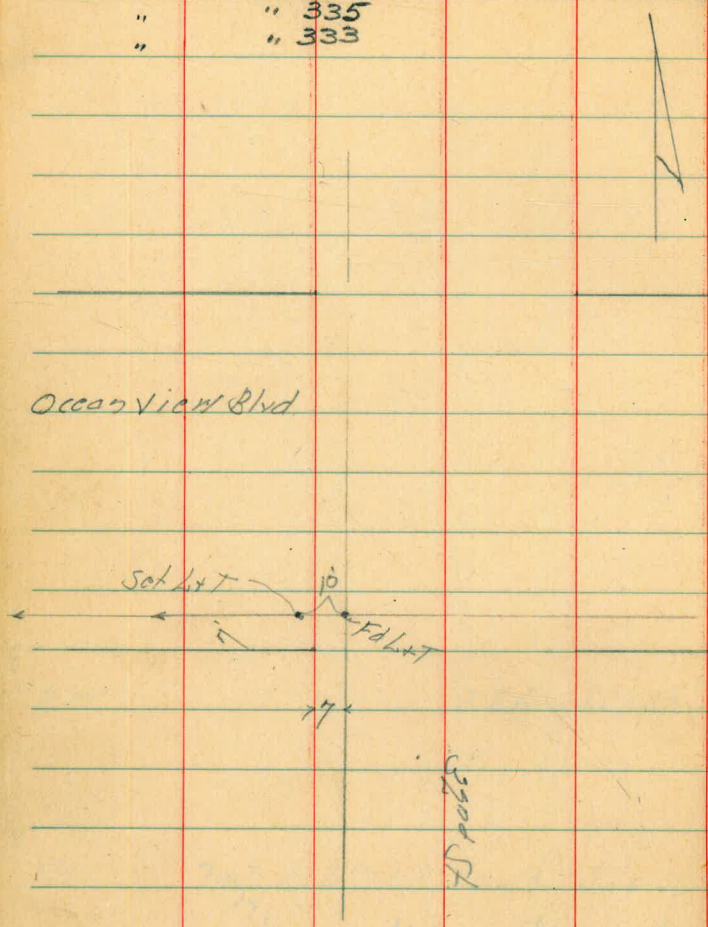
Lt.	℄	Rt	
270.71	269.90	270.46	
4.51	5.32	4.76	
7.6 = Cb x Pav.		7.3 = Pav	
270.96	270.90	270.38	270.54
4.26	4.32	4.84	4.68
7.6	7.6 = Gutter		7.3 = Gutter
	275.22		270.58
			4.64
			7.3 = Cb
271.9	271.7	271.6	271.57
6.0	6.2	6.3	6.32
7.5		7.5	9.2 = 44½ Conc Drive
272.5	272.2	272.2	
5.4	5.7	5.7	
7.5		7.2 = Bldg	
		273.75	
		4.15	
		7.3 = 4 Door Calif Mansion Floor	

BM			0.84	267.89	F.W. BP Lewis + Hawk 267.97
TP	7.13	271.73	10.62	264.60	
2+88	= SCB Line Lewis				
		275.22			

Lt.	℄	Rt
270.66	269.92	269.71
4.56	5.80	5.51
7.5 = CB	7.5 = Paving	269.55
		5.67
		7.7 = Paving + Drive
	275.22	

Tie Points Ocean View Blvd & 33rd St

PLOTTED - T.RS. 350 M.Q.
" " 335
" " 333



Indexed
C.S.K.

Plotted T.RS. 85. M.Q.

Dec. 11-46
S. Sloan
McCoy
Waddell
Allen
W.O. 210

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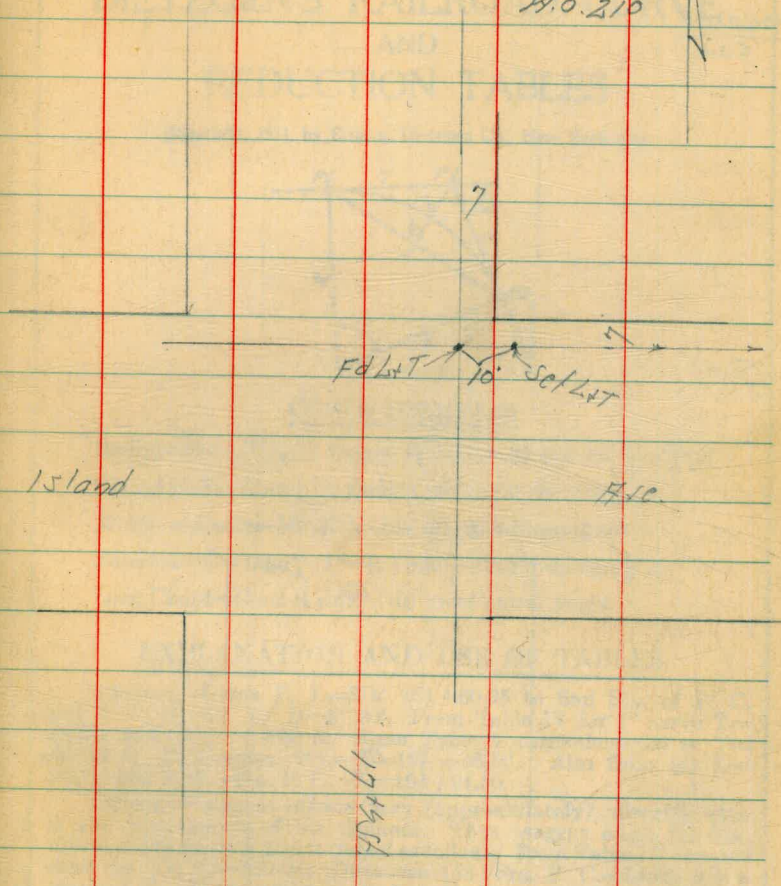
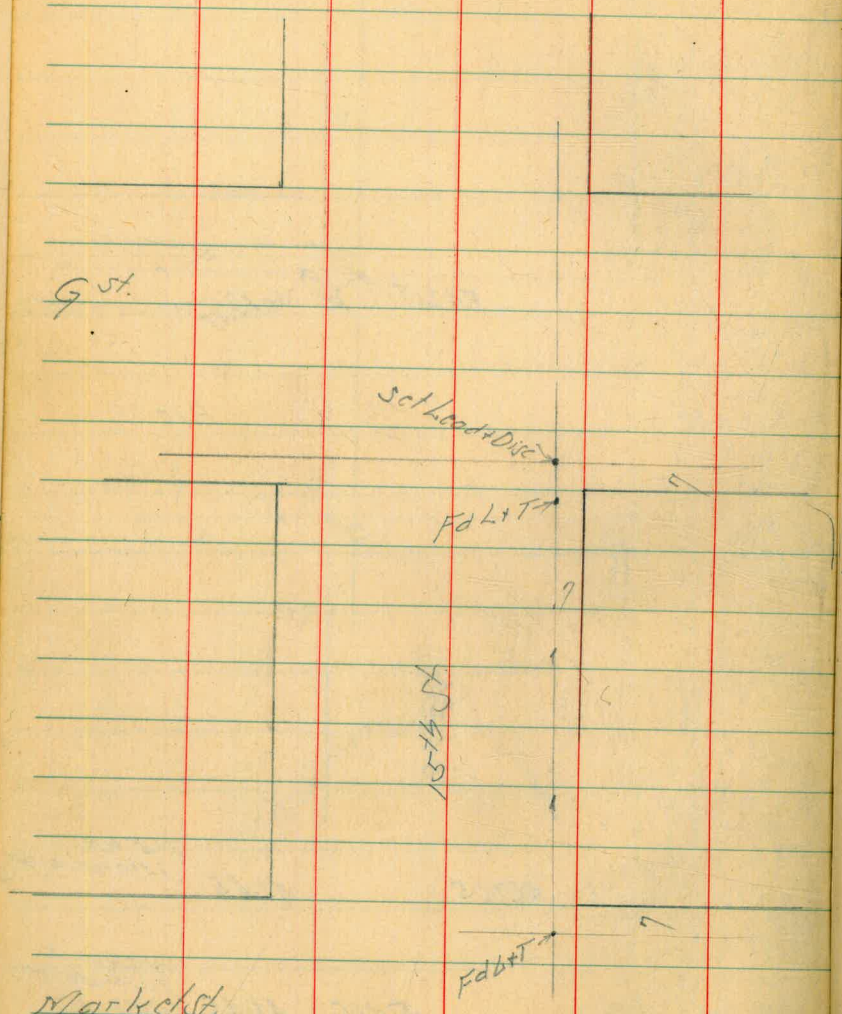


BM	5.315	46.765	41.45	N.F.B.P. Island Ave & 17th St
BM Set Nail		5.315	41.45	N.F.B.P. Island Ave & 17th St in Island

Tie Points G St + 15th St.
Re Set S.E. 7' L+D

Dec. 11-46
S... McCoy
... Allen

Indexed
C.S.K.



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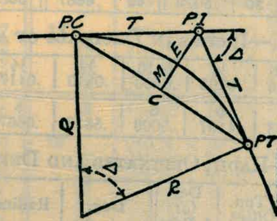
443

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES



CURVE FORMULAS

Radius=R=$\frac{50}{\sin. D/2}$(1) Degree of Curve=D and sin. $\frac{D}{2}=\frac{50}{R}$ (2)

Tangent=T=Rtan$\frac{\Delta}{2}$ (3) Length of Curve=L=100$\frac{\Delta}{D}$ (4)

Middle ordinate=M=R(1—cos. $\frac{\Delta}{2}$) (5)=Rvers $\frac{\Delta}{2}$ (6)

External=E=Ttan$\frac{\Delta}{4}$-(7)=R ÷ cos.$\frac{\Delta}{2}$—R(8)=Rexsec$\frac{\Delta}{2}$(9)

Long Chord=C=2 R sin.$\frac{\Delta}{2}$ (10) Δ=Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.=Sta. 161+60.35 to find Sta. of P. C. and P. T. Δ=62° 10′ D=8° 20′. From Table IV for 1° curve T=3454.1 and ÷ 8⅓=414.49 ft. From Table V correction=.36 or T=414.85 ft. P. C.=Sta. P.I.—T=157 +45.50. Also from (4) L=746.00 and P. T.=Sta. P. C.+L=164+91.50.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.=7.27 ft. Distance=158—Sta. P. C.=54.50, hence offset=7.27 (54.50 ÷ 100)²=2.16 ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus (54.50)² ÷ (2 x 688.26)=2.16 ft.

Deflections.—Deflection angle=½ D for 100 ft., ¼ D for 50 ft., etc. For c ft.=(in minutes) .3 x C x D° or=defl. for 1 ft. from Table III x C. For Sta. 158 of above curve=.3 x 54.5 x 8⅓=136.2′ or 2° 16.2′, or=2.50 x 54.5=136.2′ from Table III. For Sta. 159 deflection angle=2° 16.2′ +8° 20′ ÷ 2=6° 26.2′, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve E=960.6 for 8° 20′=960.6 ÷ 8⅓=115.27 and from Table V correction=.10 or E=115.37 ft. Or suppose Δ=32° and E is measured and found to be 42 ft. What is D? From Table IV E=230.9 and ÷ 42=5.5 or D=5° 30′.

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123
88
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263
125
138

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20—16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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