

1705

THE

ENGINEERS

LEAD BOOK

1887

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 - (20 - 16) \div 2 = 27.6$ ft. For slopes of 1 on 1½ see inside of back cover.

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1705

CITY ENGINEER'S OFFICE

INDEXED
Completely

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

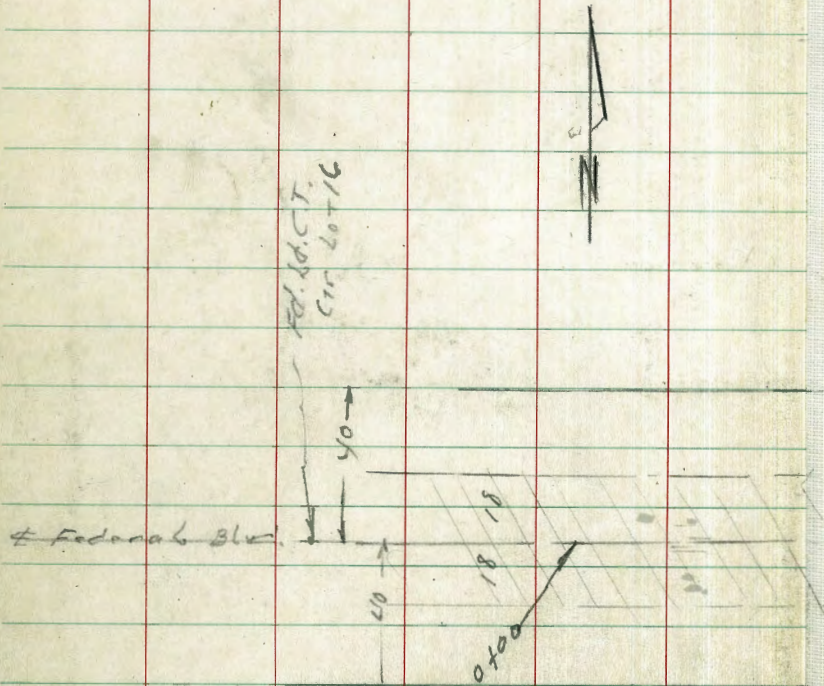
Made in U. S. A.

Levels on PAVING AT

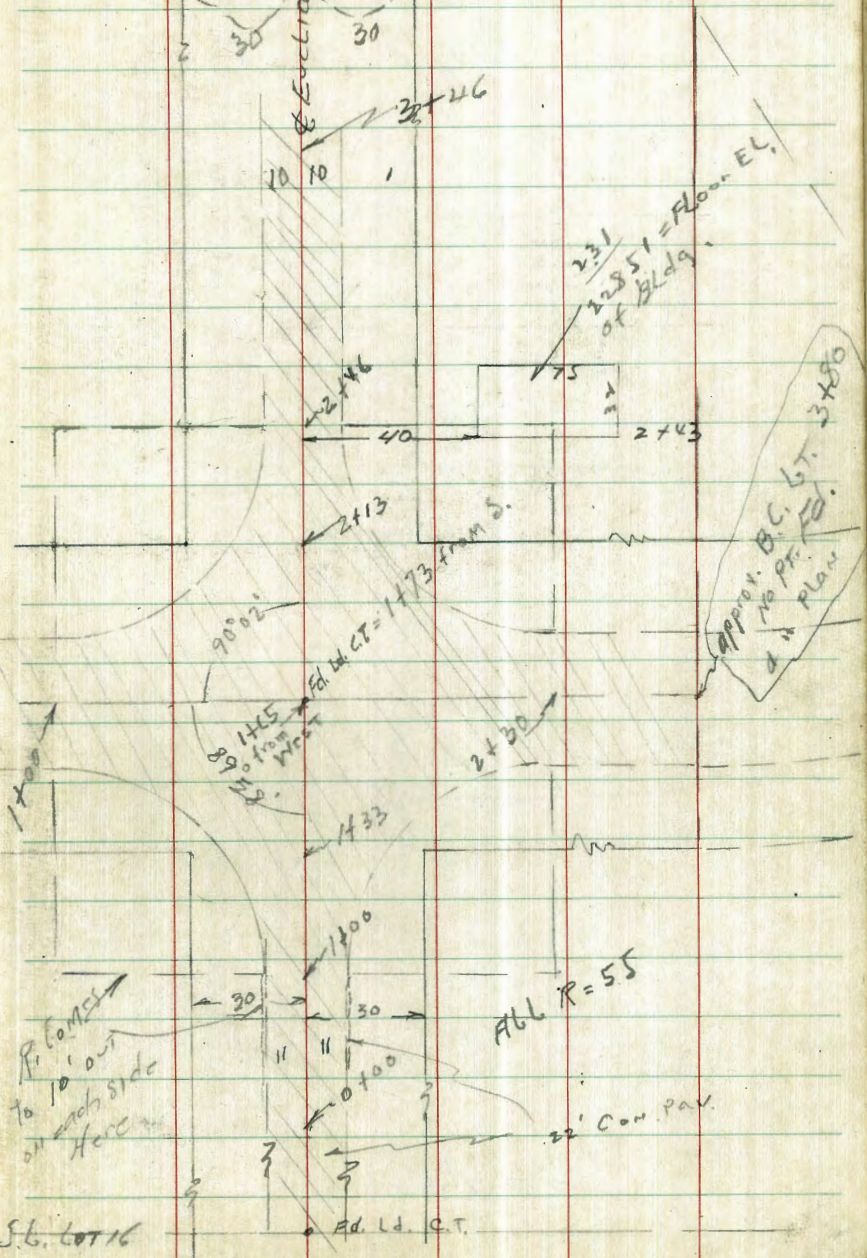
S. Moore
Surveyor at
W. Moore
7-7-46

Federal Blvd. and Euclid Ave.

Roll 4420



N.L. Lot 16

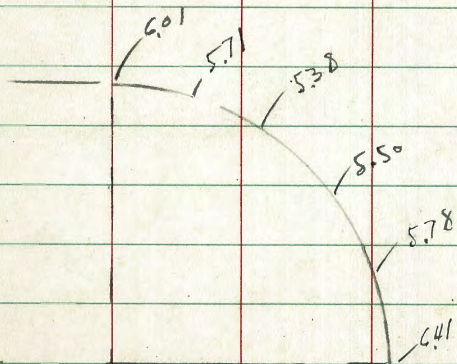
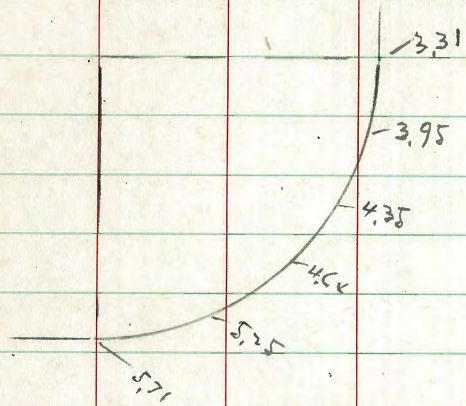


Approx. B.C. Lt. 3+850
No Pr. P.D.
Plan

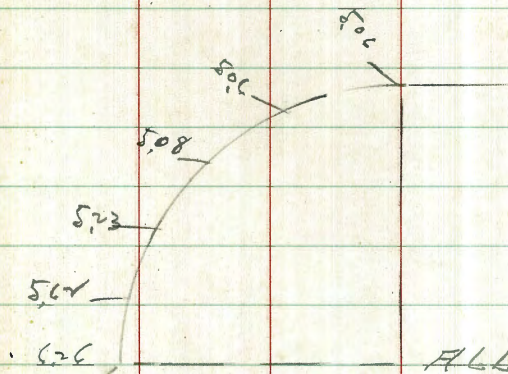
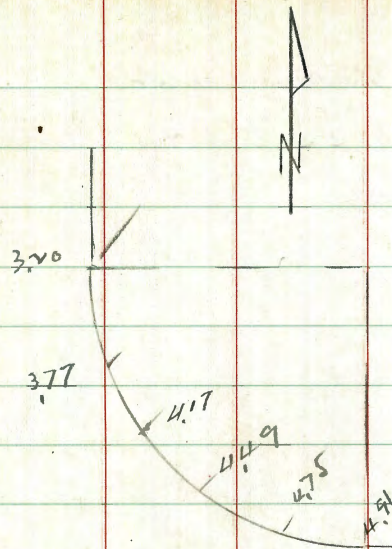
ALL R=55

P. Compt.
To 10' out
on each side
Here

Levels on Ret. Pav. edge
Curves IN 5 Eq. Parts.



$\frac{230.82}{41.2}$
H.I. R



ALL R = 55'
= Pav. edge

Levels on Federal Blvd.

0+00 = W of Euclid Ave
See sketch

1+55 E Euclid

1+35 = W of Euclid

1+00 B.C. RT. & L.T.

0+50

0+00

T.P. 10.53 230.82 0.94 220.29

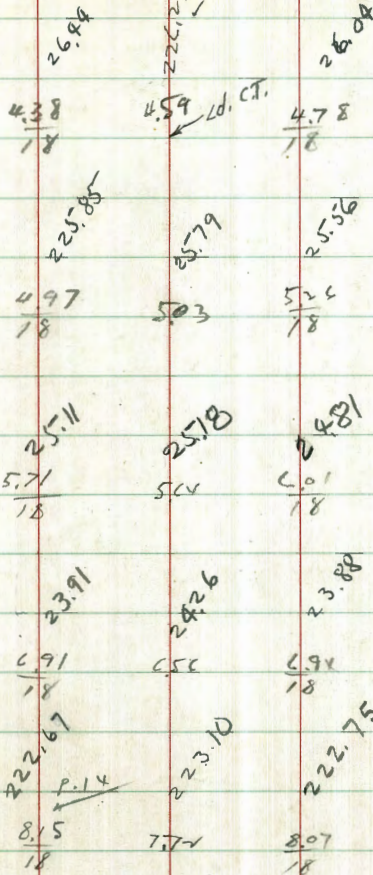
T.P. 6.31 221.23 7.18 214.94

T.P. 1.92 222.10 7.98 220.18

B.M. Top FH 2.83 228.16 225.33

LT

RT = South
3



S.E. Cor. Federal + 497th P.B. 1082-77

Federal Blvd.

3+80 APPROX BCLT.

5+45

3+40
1+65
5+05

2+00
1+65
4+65

2+65
1+65
4+30

1+30 = E.C.S of Pav.

1 65
3+95

1+95 = E.L. Euclid

1 65
3+60

230.82

L-

←

R

4

26.62
4.20
18

26.94
3.88

26.54
4.24
18

26.90
4.47
18

26.68
4.14

26.37
4.45
18

24.12
4.70
18

26.49
4.33

26.11
4.71
18

25.91
4.91
18

26.28
4.54

25.87
4.95
18

25.91
4.91
18

26.08
4.74

25.76
5.06
18

26.12
4.70
18

26.01
4.80

25.81
5.01
18

230.82

PLAN GRADE
22 G.I.

+50
7+15

+25
6+90

5
6+65

+75
6+40

+50
6+15

+25
5+90

V+00
5+65

230.82

25.47
 $\frac{5.35}{18}$

26.06
 $\frac{4.76}{18}$

26.96
 $\frac{4.36}{18}$

26.71
 $\frac{4.11}{18}$

26.96
 $\frac{3.86}{18}$

26.91
 $\frac{3.91}{18}$

26.11
 $\frac{4.05}{18}$

25.88
4.94

26.36
4.46

26.76
4.06

27.01
3.81

27.20
3.52

27.19
3.53

27.10
3.72

25.89
 $\frac{5.33}{18}$

26.09
 $\frac{4.78}{18}$

26.38
 $\frac{4.44}{18}$

26.67
 $\frac{4.15}{18}$

26.86
 $\frac{3.96}{18}$

26.88
 $\frac{3.92}{18}$

26.75
 $\frac{4.07}{18}$

230.82

Federal Blvd.

Lr.

¢

Rr.

6

6+00
7+65

5+75
7+40

~30.80

24.05
6.77
18

24.35
6.47

23.99
6.83
18

24.88
5.94
18

25.23
5.59

24.82
6.00
18

230.82

Levels on Euclid Ave

1+55
3+22

1+33 = sl Federal
3+00

1+25 Rolled up edges and base
2+92

1+10
2+77

1+00 Beg Curve Pt + LT.
2+67

0+50
(2+17)

0+00 S of Federal See Sketch

23082

LT

4.95
10

5.31
10

5.22
10

5.92
9

5.41
11

8.78
11

11.26
11

25.51

25.40

24.98

24.41

22.04

19.56

4.78
10

5.08
10

5.23
10

5.87
9

5.30
9

8.66
9

11.26
9

4.84
10

5.00
10

5.19
10

5.90
9

5.27
9

8.86
9

11.29
9

Rt to East

25.98

25.63

24.92

24.45

22.14

19.33

Rollled up edge

23082

Euclid

2 + CC

4 + 33

2 + VL EC^s R + LT

4 + 13

V + 26

3 + 93

2 + 13 = VL Federal

3 + 80

1 + 91

3 + 58

1 + 73 = F Federal

3 + 40

23092

Lr

Q

Rt

8

28.82	29.55	28.52
$\frac{240}{10}$	27	$\frac{230}{10}$

27.51	27.67	27.62
$\frac{231}{10}$	315	$\frac{270}{10}$

26.76	26.98	26.83
$\frac{206}{10}$	388	$\frac{379}{10}$

26.56	26.66	26.52
$\frac{426}{10}$	416	$\frac{428}{10}$

26.31	26.29	26.31
$\frac{457}{10}$	438	$\frac{451}{10}$

26.13	26.23	26.11
$\frac{469}{10}$	449 CT.	$\frac{471}{10}$

23080

Euclid Ave

Lr

E

Rr

3

34x6
5+13

TR 7.18 237.03 0.97 229.85

3400
4+67

230.92

4.80
10
32.23

4.72
32.31

4.89
10
232.14

29.98
0.2x
10

237.03
30.11
0.71

230.00
0.82
10

230.82

2-11-44.

Grid Levels at Federal +

Euclid Ave

Levels on $S \frac{1}{2}$ Federal

2+15 = 0+50 P.3

2+00 = 100' W of W. Euclid

1+55 = 0+00 on sketch P1

1+00

+50

0+00 = 300' W of W. Euclid

BM Id CT
& Federal
Euclid

0.12

$\sqrt{2635}$

226.23

Fed.

P. = 76.5

10

23.65	21.65	17.35	14.05
$\frac{27}{36}$	$\frac{47}{32}$	$\frac{90}{90}$	$\frac{123}{140}$

23.97	23.61	23.55	20.85	17.45	13.85
$\frac{238}{18}$	$\frac{274}{18}$	$\frac{218}{28}$	$\frac{55}{35}$	$\frac{89}{90}$	$\frac{125}{140}$

23.25	18.75	16.05	14.15
$\frac{31}{29}$	$\frac{26}{35}$	$\frac{103}{90}$	$\frac{122}{140}$

21.97	21.27	21.35	19.85	18.25	14.62
$\frac{458}{18}$	$\frac{508}{18}$	$\frac{510}{28}$	$\frac{115}{38}$	$\frac{126}{85}$	$\frac{117}{140}$

20.62	20.25	20.75	11.85	09.95	11.35	14.35
$\frac{523}{18}$	$\frac{610}{18}$	$\frac{56}{27}$	$\frac{145}{40}$	$\frac{164}{64}$	$\frac{150}{100}$	$\frac{120}{140}$

219.72	19.35	19.65	08.75	06.25	02.25	209.25
$\frac{663}{18}$	$\frac{700}{18}$	$\frac{67}{28}$	$\frac{126}{43}$	$\frac{201}{15}$	$\frac{191}{100}$	$\frac{171}{140}$

$\sqrt{27635}$

S 1/2 on Federal

ld.
T.P.C.T. 4.56 232.79 0.12 226.23

3 + 60 = F.L. Euclid

3 + 50

3 + 50

3 + 06

3 + 00 = w.l. Euclid

2 + 45 = 1700 P.3 BER + LT on Pav.

226.35

Fed.

P.T.

11

25.95
0.8
40

29.05
2.3
90

22.85
3.5
110

16.65
9.7
140

25.95
0.9
40

22.35
4.1
90

21.15
5.2
110

17.05
9.3
140

25.68
0.7
40
on Pav.

23.35
3.0
90

23.35
3.0
110

21.85
4.5
140

25.25
1.1
40

23.95
2.4
90

21.35
5.0
140

25.25
1.1
40

29.05
2.3
90

20.65
5.7
90

18.25
8.1
140

29.35
2.0
33

21.95
4.8
55

18.95
7.8
90

16.65
9.7
140

226.35

$S \frac{1}{2}$ on Federal

$5+65 = 4+00 \text{ P.1}$

$5+45 = 3+80 \text{ P.1}$ ^{See} approx B.C. Lt

$5+05 = 3+40 \text{ P.1}$ ^{See}

$4+65 = 3+00 \text{ P.1}$

$4+30 = 2+65 \text{ P.1}$

$3+95 = 2+30 \text{ P.1}$ ^{See}

$3+80$

23279

~~FT.~~
Fed.

$\frac{25.99}{26}$	$\frac{28.29}{30}$	$\frac{29.29}{40}$	$\frac{27.99}{90}$	$\frac{28.29}{102}$	$\frac{12}{28.99}$
$\frac{4.8}{26}$	$\frac{4.4}{30}$	$\frac{3.5}{40}$	$\frac{4.8}{90}$	$\frac{4.5}{102}$	$\frac{3.8}{140}$

$\frac{25.79}{26}$	$\frac{29.19}{30}$	$\frac{30.09}{40}$	$\frac{27.99}{90}$	$\frac{28.1}{101}$	$\frac{29.39}{140}$
$\frac{7.0}{26}$	$\frac{3.6}{30}$	$\frac{2.7}{40}$	$\frac{4.9}{90}$	$\frac{4.8}{101}$	$\frac{3.4}{140}$

$\frac{25.59}{26}$	$\frac{27.89}{27}$	$\frac{27.79}{40}$	$\frac{26.99}{90}$	$\frac{26.89}{140}$
$\frac{7.1}{26}$	$\frac{4.9}{27}$	$\frac{5.0}{40}$	$\frac{5.8}{90}$	$\frac{5.9}{140}$

$\frac{25.59}{25}$	$\frac{26.29}{30}$	$\frac{26.39}{40}$	$\frac{25.79}{90}$	$\frac{24.69}{140}$
$\frac{7.2}{25}$	$\frac{5.5}{30}$	$\frac{5.4}{40}$	$\frac{7.0}{90}$	$\frac{8.1}{140}$

$\frac{25.49}{25}$	$\frac{26.09}{30}$	$\frac{26.19}{40}$	$\frac{25.19}{90}$	$\frac{22.69}{140}$
$\frac{7.3}{25}$	$\frac{6.7}{30}$	$\frac{6.6}{40}$	$\frac{7.6}{90}$	$\frac{10.1}{140}$

$\frac{25.99}{24}$	$\frac{26.29}{28}$	$\frac{29.89}{80}$	$\frac{22.19}{125}$	$\frac{18.69}{140}$
$\frac{7.3}{24}$	$\frac{6.5}{28}$	$\frac{7.9}{80}$	$\frac{10.0}{125}$	$\frac{14.1}{140}$

$\frac{25.59}{26}$	$\frac{25.89}{40}$	$\frac{23.99}{110}$	$\frac{17.29}{140}$
$\frac{7.2}{26}$	$\frac{6.9}{40}$	$\frac{9.3}{110}$	$\frac{15.5}{140}$
<u>32.79</u>			

S $\frac{1}{2}$ Federal

$$L + L0 = 300' \text{ E of FL E. L. id}$$

$$L + 40 = 4 + 75$$

$$L + 15 = 4 + 50$$

$$S + 90 = 4 + 25 \text{ P. 1}$$

$$\sqrt{3 \times 79}$$

5
Fed.

R_T

13

27.36	26.96	26.29	32.99	52.29	30.59	28.59
593	633	70	+0.2	0.5	2.2	1.2
Par.	8	25	29	40	90	100
	Par.					

26.29	31.99	31.69	30.19	28.49
2.5	0.8	1.1	2.6	4.3
24	27	40	90	140

26.19	30.59	30.09	29.19	28.19
2.6	2.7	2.7	3.6	4.6
25	29	40	90	140

26.09	29.19	28.99	28.19	27.69
2.7	3.6	3.8	4.6	5.1
25	29	40	90	140
	$\sqrt{3 \times 79}$			

N $\frac{1}{2}$ of Federal

TR 9.90 ≈ 33.63 2.60 223.73

1+15 = 2+00 See sketch p1

1+13

1+00

0+90

0+50

0+00 = 300 W of W.L. of Euclid

B.M. of L.C.T.
Federal 0.10 226.73 226.23
+ Euclid

L.T. = to North

Fed. 14

$\frac{70.1}{140}$ $\frac{1.6}{90}$ $\frac{3.0}{40}$

for Pav.
See p.3

$\frac{1.5}{140}$ $\frac{3.2}{90}$ $\frac{4.8}{40}$ $\frac{4.85}{18}$
Pav

$\frac{8.8}{140}$ $\frac{8.6}{110}$ $\frac{8.1}{80}$ $\frac{4.7}{50}$ $\frac{5.0}{40}$ $\frac{5.3}{32}$ $\frac{5.14}{18}$
Pav.

$\frac{9.6}{140}$ $\frac{8.5}{90}$ $\frac{10.2}{40}$ $\frac{5.6}{28}$ $\frac{5.37}{18}$
Pav

$\frac{12.5}{140}$ $\frac{13.6}{90}$ $\frac{14.7}{40}$ $\frac{5.6}{28}$ $\frac{6.14}{18}$
Pav.

$\frac{17.0}{140}$ $\frac{17.1}{128}$ $\frac{18.2}{77}$ $\frac{17.5}{43}$ $\frac{6.6}{27}$ $\frac{7.08}{18}$
Pav.

226.73

N 1/2 Fed

3 + 56

3 + 50

3 + 06

3 + 00 = v.l. Euclid

2 + 65

2 + 15

2 + 00

233.63

LT = 1/10 74 Fed 15

$\frac{2.8}{90}$	$\frac{5.2}{90}$	$\frac{7.2}{40}$
30.63	27.73	26.62
$\frac{3.0}{40}$	$\frac{5.9}{90}$	$\frac{7.01}{40}$
		0.4 pav.

$\frac{2.8}{100}$	$\frac{5.9}{90}$	$\frac{7.5}{40}$
29.83	27.73	26.13

$\frac{4.1}{100}$	$\frac{5.9}{90}$	$\frac{7.7}{40}$
29.53	27.73	25.93

$\frac{4.8}{100}$	$\frac{6.7}{90}$	$\frac{8.1}{40}$
28.83	26.93	25.53

$\frac{6.4}{100}$	$\frac{7.8}{90}$	$\frac{9.5}{40}$
27.23	25.83	24.13

$\frac{7.0}{100}$	$\frac{8.4}{90}$	$\frac{9.8}{40}$
26.63	25.23	23.83

233.63

N 1/2 Fed

5+05

4+65

4+30

TP 11.94 238.58 1.99 226.64

3+95

TP

3+80

3+60 = E L F - clid

233.63

LT

Fed. 16

38.18
0.1K
140

37.78
0.8
134

27.08
11.5
129

27.08
11.5
90

26.48
12.1
40

38.78
+0.2
140

38.18
0.4
134

27.88
10.7
129

27.48
11.1
90

26.78
11.8
45

38.88
+0.3
140

38.58
0.0
134

28.18
10.4
129

27.68
10.9
60

26.48
12.1
40

37.6
+4.0
140

37.4
+3.8
134

28.23
5.4
129

27.33
4.3
60

26.93
7.2
40

36.4
+2.8
140

36.1
+2.5
134

28.33
5.3
129

27.33
4.3
60

26.63
7.0
40

29.93
3.7
140

28.13
5.5
90

26.93
7.2
40

233.63

check to 2d. CT
 12.36 22.122 22.623
 1001

6+6 = 200' E of EL, Euclid

6+40

6+15

5+90

5+65

5+55

5+45 = approx. B.C. LT.

239.58

LT. = 1/2
 453-
 + 6.9
 140
 39.9
 + 1.3
 30
 TOP
 12.3
 27
 TOC

43.6
 + 5.0
 140
 490
 + 1.4
 90
 37.3
 13
 35
 TOP
 CUT
 12.0
 20
 TOC

41.5
 + 2.9
 140
 39.3
 + 0.7
 90
 36.2
 2.4
 40
 35.2
 2.4
 11.9
 20

400
 + 1.4
 140
 36.6
 2.0
 90
 33.7
 4.9
 47
 TOP
 CUT
 12.9
 37
 TOC

40.2
 + 1.4
 140
 39.9
 + 1.3
 134
 TOP
 CUT
 236.4
 90
 34.1
 4.5
 48
 TOP
 CUT
 12.8
 58
 TOC

40.18
 + 1.5
 140
 39.78
 + 1.2
 134
 27.08
 11.5
 129
 26.48
 90
 26.8
 12.2
 28
 44%
 14 CUT
 12.5
 40
 TOC

39.48
 + 0.9
 140
 38.58
 + 0.3
 134
 26.8
 11.0
 129
 26.8
 90
 26.8
 12.1
 28
 44%
 14 CUT
 12.5
 40
 TOC
 238.58

18
 Fed. 17

Levels on Euclid
S of Federal

LT.

Euclid
Pav.

Rt = % East,

18

1 ± 67 = 0 ± 100 sketch P.1
Pav. elev. P.7

1 ± 50

1 ± 00

T.P.
0 ± 50

0 ± 100 = 300' S of S.L. Federal

T.P.
B.M. Euclid
and Fed.

14.7	14.7	19.6	20.2	14.6	15.4	21.1	23.5
100	100	51	4.5	10.1	9.3	3.4	1.7
57	31	23	20	28	57	100	130

18.7	18.70	18.57	18.46	18.43	18.57	19.2	13.5	14.0	17.5	22.2
6.0	6.4	6.23	6.08	6.31	6.7	5.5	11.7	10.7	7.4	2.5
23	11	9	108	9	11	20	27	59	80	130

16.3	16.42	15.92	16.04	15.80	15.98	16.4	11.3	11.2	14.8	17.4	20.0
8.4	8.6	8.8	8.7	8.9	8.7	8.3	13.4	13.5	9.9	7.3	4.7
22	11	9	10	9	11	20	27	35	60	90	130

13.6	13.58	13.39	13.59	22.74	13.44	13.5	08.6	11.6	13.4	15.1
4.3	4.31	4.50	4.60	4.60	4.45	4.4	9.3	6.3	4.5	2.8
23	11	9	40	9	11	21	29	55	90	130

0.59	11.2	11.11	10.93	11.03	10.79	10.98	11.29	06.4	09.9	22.2
120	4.7	4.78	4.7	4.8	4.7	4.7	6.6	11.5	8.0	5.7
30	23	11	9	9	9	11	20	27	17	130

217.89

Levels on Euclid
N. of Federal

Contd. P. 21

T.P. 8.04 24796 215 23992

1+70 Shoulder of fill 130 299 11.7 9.9 31.4 33.2

5+50

1+52 13.8 12.8 11.2 29.3 30.3 31.9

5+32

1+33 = 3+46 Skerch P. 1 15.2 27.9 13.8 8.0

5+13

1+14 4+94 16.1 14.2 27.0 28.9 13.0 8.0

0+00 = N. of Federal Blvd

T.P. 8.70 24307 220 234.37

BM. Ld. check to C.F. 1038 226.3

T.P. 12.07 23657 024 224.50

224.74

From P. 18

Lt.

Euclid

RT = 70 East

19

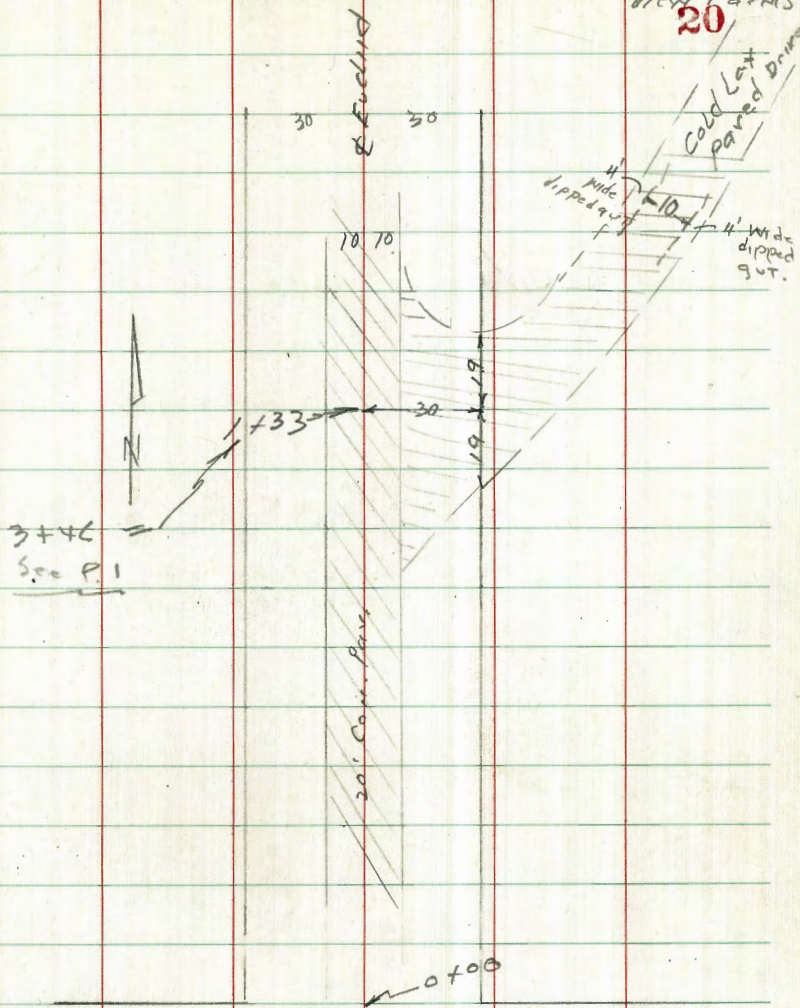
33.4 32.9 34.17 34.24 34.03 34.0 37.9 38.2 39.21 40.67 41.3 43.1 43.3
 4.7 10.2 8.90 8.83 9.04 9.1 5.2 4.8 3.8 2.4 1.8 0 2.0
 20 17 10 Pav 10 Pav 18 20 30 43 Pav 11 90 130

32.5 32.0 33.23 33.27 33.10 33.16 35.14 37.40 39.3 41.8 42.9
 9.6 11.1 9.82 9.80 9.97 9.91 7.93 5.7 3.8 1.3 0.2
 21 17 10 Pav 10 Pav 18 30 50 57 90 130

29.3 31.1 32.29 33.85 34.66 37.5 40.6 41.7
 13.8 12.0 Pav 10.78 9.22 8.4 5.6 2.5 1.4
 8.0 30 Pav 18 30 43 48 70 130

30.9 30.8 31.28 31.39 31.25 32.25 32.05 35.3 37.9 39.8 39.9
 12.7 12.3 11.79 11.68 11.82 10.82 11.04 7.8 5.2 3.3 2.2
 30 15 10 Pav 29 Pav 30 30 65 100 130

Broad
View Farms
20



Federal Blvd

Euclid N. of Fed.

LT.

check to P. Id. CT. BM
Euclid + Fed. 10.62 22622 22673

T.P. 1.90 23487 13.02 23494

3+00 = 300' N of
W.K. Federal
6+80

	27.3	28.8	35.3	39.7	40.3
	20.7	19.7	11.7	8.3	7.7
	130	110	77	30	20

2+75
6+55

2+50
6+30

	26.6	28.7	34.7	37.4	37.9
	21.4	19.3	13.3	10.6	10.1
	130	108	98	30	20

2+00
5+80

	24.9	25.7	31.5	32.26	34.3	35.3	34.3
	22.1	22.3	16.5	15.7	13.7	12.7	13.7
	130	125	114	80	30	20	17

247.96

Euclid

R.

21

39.5	40.63	40.72	40.60	39.2	41.2	55.4	60.7	61.9	62.0
8.5	7.33	7.4	7.36	8.8	6.8	+7.4	+12.7	+13.9	+14.0
17	10	10	10	22	30	47	100	117	130

drive

39.56	39.67	39.58
8.40	8.29	8.42
10		10

36.9	38.36	38.42	38.31	37.5	42.8	48.5	57.9	57.8	58.1
11.0	9.60	9.52	9.65	10.5	5.2	+0.5	+3.7	+4.8	+6.1
17	10	9	10	22	30	40	83	96	130

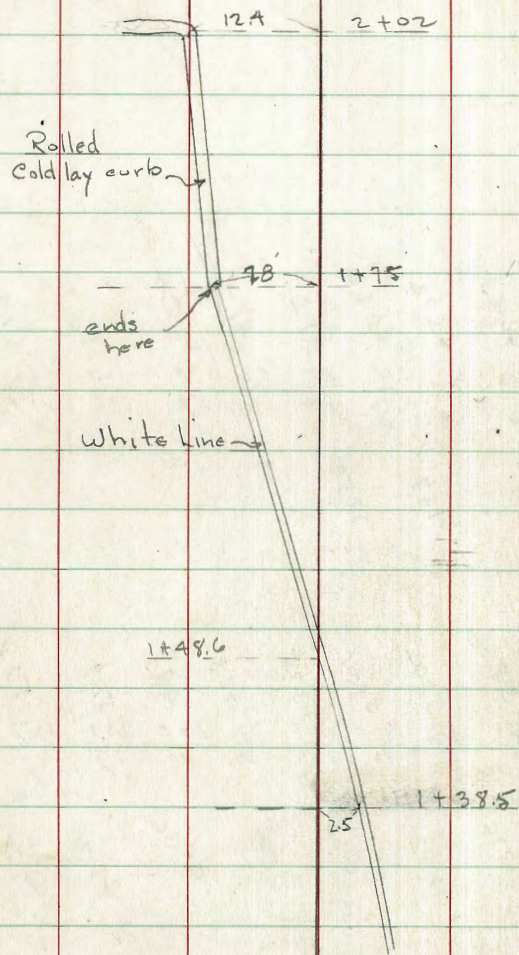
drive

34.74	35.82	35.60	35.7	41.36	43.81	44.78	47.1	47.9	47.9
12.32	12.4	12.36	12.3	6.6	4.15	3.18	0.9	0.9	0.1
10	12	10	13	30	61	77	100	100	130

drive

247.96

Gutter levels for prop. curb & walk
around the "Machado House" - old town



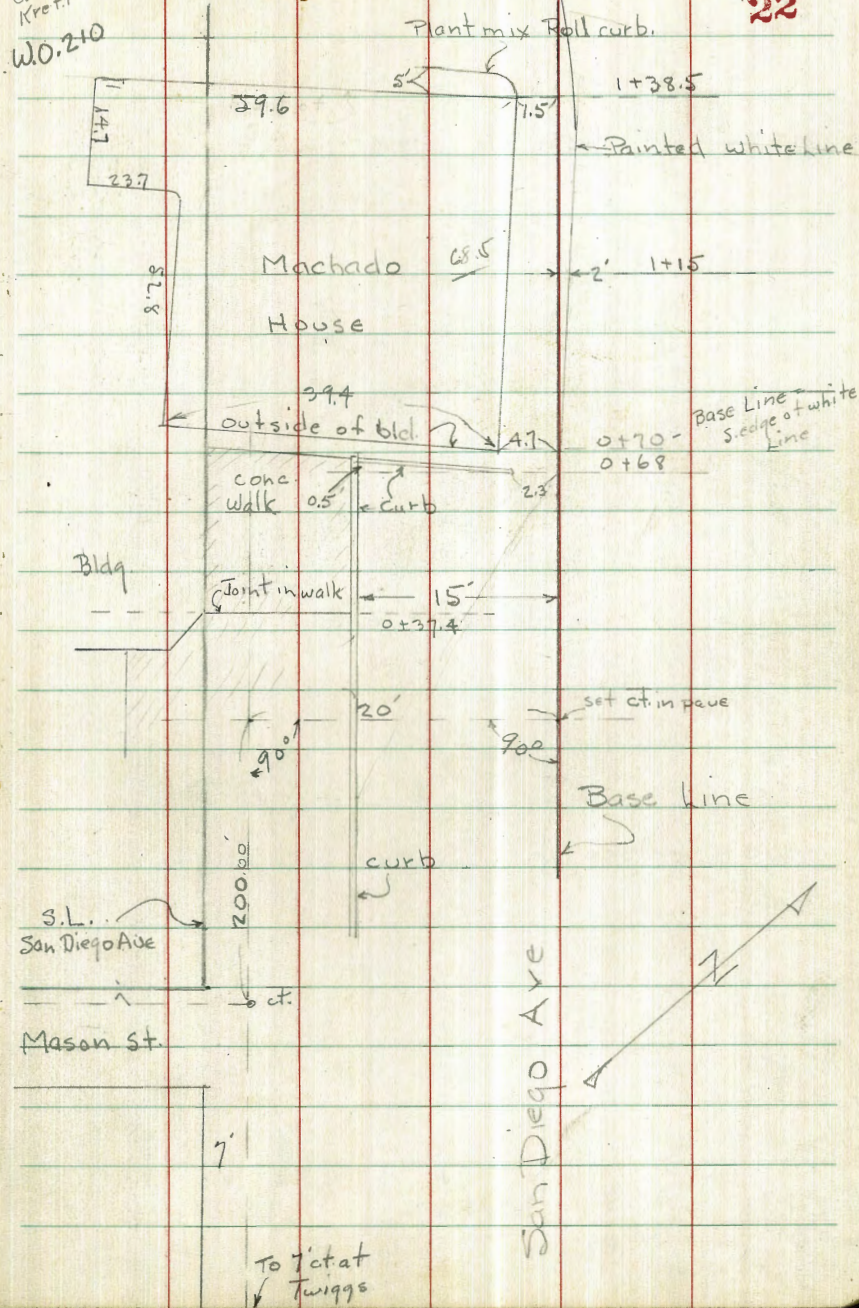
Osborne
Hardin
Cavey
Kreit

4-24-46

W.O. 210

indexed
C.S.K.

22



0+27.5 = 4" drain tile outlet in cb.

0+19 = \pm of 11.3 driveway

0+12.6 = 4" drain tile outlet in cb.

0+00 - See sketch

0-30

B.M. 1.28
SW.B.P. - San Diego
+ Mason

23.50

22.22

Lt.

\pm = Base line see sketch

Rt. 23

16.99

6.51 = FL. Drain

17.99

5.56 Top of
21" walk

17.00

6.46 = gut

17.21

6.29 = FL. Drain

18.06

5.44 = Top of
15" cb.

17.38

6.16 = gut

17.08

5.62

18.66

4.84 Top of
15" cb.

17.89

5.61 = gut

15" = cb. line
San Diego

23.50

T.P. 4.59 21.21 6.88 16.62

0+78 = 4' Doorway in Bld.

0+68 = Approx. face of cross curb.

0+60

0+50

0+35

17.82
6.06
27
walk at Bld.

16.75 16.72 16.68 16.72 16.70 16.69 16.55 16.75
6.71 6.78 6.62 6.78 6.30 6.91 6.85 6.75
15 = Top of Intersection
12 = Top of curb
5 = Top of curb
2.3 = end of cross curb

16.90 16.76 16.81 16.82
6.60 6.74 6.81 6.66
15 Top 15 = Top

17.52 17.11 16.83 16.78 17.03
5.88 6.39 6.67 6.72 6.47
27
walk at Bld.
15 = Top 15 = Top

17.83 16.90 17.30
6.07 Top 6.60 = Top 6.20
14.9 14.9

23.50 ↓

Lt.

ℓ = base Line

Rt

24

1+38.5

1+27 = 3.8 Doorway to bld.

1+15

1+03 = 5.8 Doorway in Bld

0+85

Lt.

E

Rt.

26.51
5.25
1.10
Cor. of
Bld.15.29
5.92
0.8
= gut.2 = sledge of
Line15.29
5.77
516.09
5.12
2 = edge of
5.1726.51
15.29
5.75
1 = gut15.29
5.12
516.03
4.78
2.8
Bld.15.68
5.57
1.8
= gut15.65
5.5615.68
5.33
516.02
4.79
3.1 = on
edge of sill15.98
5.23
2 = gut15.93
5.2816.05
5.12
516.96
4.25
4.0
Top of roll
of Bld.16.16
5.05
2.6
= Base of
roll16.25
4.9616.03
4.78
5

21.21 ✓

Check Levels to Levels in Book 1675-33

Lt.

R

Rt.

26

B.M	1.10	23.32	22.22	B.T. Mason + San Diego see below
			10.87	12.45
				ct. WL. S.D. N.L. Wallace to E. 1675-33 12.55 12.45 +10 diff.

Note Reduced. 10-22-16

			2.39	22.22	check B.M.
T.P.	5.47	24.61	2.07	19.14	
check B.M.			8.68	12.53	Nail in pole S.W. Wallace + S.D. 12.62

1+50

14.18	19.01	15.07	15.20
7.03	6.40	6.14	6.01
NO			5
on oil/pave Driveway		on line white	

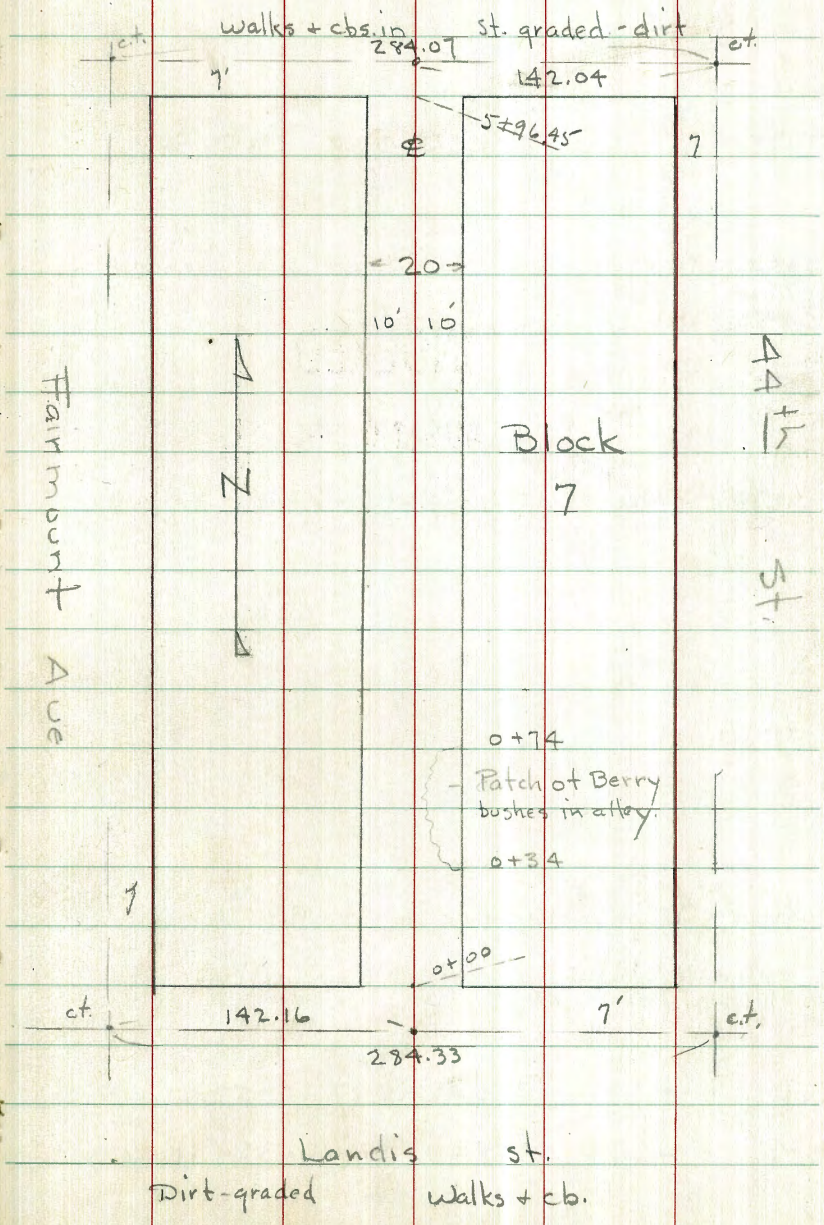
1+44 = Line of Cold lay roll curb in front of Bld.

15.57	15.36	19.98	15.13	15.12
6.54	5.95	6.27	6.08	5.89
12	5	5		5
on pave in front of Doorway	Top of Roll oil cb.	5 = gut		S edge Line
			21.21	

Osborne
Hardin
Covey
Kreft. 4-26-46

Wrightman St. 27

X-Sect. 20' Alley in Blk 7 - City Hts.
Annex # 1



5-10-46 Notes Reduced Cherry-

INDEXED
W.K.
AUG 10 1949

Lt

E

Rt

28

T.P. 5.62 358.66 3.38 353.04

0+50 - 10.8 Rt. = end 4" Conc. wall with fence.

0+50 - 10.1 Lt. = end wire fence

0+47 - 9' Lt = R P. pole

0+34 = step down in top of Conc. wall

0+10

0+01 = Begin wire fence on Lt. 99

0+00 = N.L. land is - beg. 6" Conc. wall on Rt.

T.P. + 3.81 356.42 - 5.87 352.61 N.W. B.P.

B.M. + 3.77 358.48 354.71 44th Wightman

351.6

4.8
20

351.3

5.1
20

350.96

5.47

9.9 face of cb
Top end Alley
dirt Return

351.9

4.5
10

351.6

4.8
10

352.5

3.9

351.7

4.7

351.1

5.3

E

352.5

3.9
10

351.8

4.6
8

351.95

5.07
face 9.6 =

Rt

353.07

3.35 = Top face of
10.8 wall

352.74

2.68
10.8
wall to S.

352.4

4.0
10

351.5

4.9
ground

28

352.99

3.43
10.8
wall to N.

353.31

3.11
10.8 - face of
wall - Top.

356.42

+ Beg. wire fence - poor Cond.
1+56 = 9.5 Lt = end of wire fence + Rose hedge

1+54 = 2.5' Conc. walk on Lt.

1+50

with Rose Hedge

1+23 - 9.7 Lt = end of picket fence + begin wire fence

1+09 = 2 Single garage on Rt. Dirt floor

1+00 = 2 3.5 Conc. walk on Lt

0+80 = N. end Garage + Begin Picket fence 10.1 Lt.

0+51 = S. end of 3 car garage on Lt. Conc. floor + Apron.

Lt.

2

Rt.

29

353.27

5.39

10 = edge of walk

353.27

353.4

353.5

353.8

5.5
2.0

5.3
1.0

5.2

4.9
1.0

353.6

5.2

12.4 = floor gar.

352.66

352.83

353.0

353.5

353.7

353.5

6.00

5.83

5.7

5.2

5.0

5.2

2.0

10.6

10

7

10

on walk

edge of

conc. walk

352.71

352.65

353.5

353.5

353.2

353.0

5.95

6.01

5.2

5.2

5.5

5.7

13.3

Floor

9.8

Apron

6

10

20

352.65

352.66

6.01

6.10

13.5

Floor gar.

9.9

edge of

Apron

358.66

T.P.
 3+50 5.91 360.58 3.99 354.67

3+00

2+97 - 8.7 Lt. = P. pole

2+95 = 9.3 Lt. = N.E. Cor. back of garage ^{wire fence} + begin

2+85 - 9.3 Lt. = S.E. Cor. garage - dirt floor - drive to 44th

2+85 - 9.6 Lt. = End of wire fence

2+93 - 9.6 Lt. = P. 18 Conc. walk

2+63 - 11' Rt. = ^{Dirt floor} P. of Back of 20' Gar. on ^{EL} Rt. Floor 353.5

2+50

2+46 - 9.2 Lt. = end slat fence + Beg. wire fence

2+00

1+99 - 8.2 Lt. = P. pole

1+97 - 9.0' Lt. = end wire fence + beg. slat fence

Lt. Rt. 30
 354.9 354.9 354.8 354.9 355.3 354.8

3.8 3.8 3.9 3.8 3.4 3.9
 36 10 5 10 40

354.7 354.2 354.3

4.0 4.5 4.4
 10 10

O.K. - F.O.

5-29-46

354.68

3.98
 9.6 = edge

2+52 - Double Garage
 - conc. floor
 to High Land

354.1 354.1 354.0 354.0 353.7 353.7

4.6 4.6 4.7 4.7 5.0 5.0
 30 10 10 12 40

353.6 353.5 353.9 354.0

5.1 5.2 4.8 4.7
 15 10 10

358.66

5+26 - 10.1 Rt. = end picket fence

5+13 - 9.8 Lt. = N.E. Cor. shed.

5+00

4+98 - 10' Rt. begin picket fence

4+98 8.6 Lt. = P. pole

9.5 Lt. = S.E. Cor. Board shed.

4+97 - 9.6 Lt. = end of wire fence

4+58 = Single garage (unused) on Rt. - dirt floor

4+55 - 9.9 Lt. = begin wire fence

4+49 = N. end garage + apron

4+32 = S. end double garage on Lt. Conc. floor + apron

4+27 - 9.5 Rt. = N.W. Cor. House

4+00

3+99 - 9.8 Rt. = S.W. Cor. House (frame) - no Conc. foundation

3+93 - 9.3 Lt. = P. pole

3+78 - Single garage on Lt. Conc. floor.

3+71 = 9.8 Lt. = end of wire fence

Lt. C Rt.

355.5

355.3

355.6

355.2

5.1

5.3

5.0

5.4

10

10

20

355.3

5.3

18.6 on floor

355.50

355.29

355.4

355.3

355.2

355.3

5.00

5.29

5.2

5.3

5.4

5.3

14.9
Floor gar.
Conc.

11.3

10

10

20

edge of apron

355.64

355.26

4.94

5.32

14.9 = Floor gar.

11.3 = apron

354.8

355.3

354.9

354.7

355.0

5.8

5.3

5.7

5.9

5.6

20

10

10

10

30

354.76

5.82 on floor
10 Conc.

360.58

5+90 - 9.8 Lt. N.E. Cor. Church bld.

5+85

5+52 - Φ Single garage on Rt. Conc. floor + apron not used as garage

5+47 - 10' Lt. = S.E. Cor. Conc. foundation wall of old church Bld.

5+46 = N. end Double garage on Lt.

5+38 = Φ Single garage on Rt. - Conc. floor + Apron + Apron

5+28 = S. end of double garage on Lt. Conc. floor

	LT.	Φ	RT.
	4.20		
Top. Conc. foundation wall	9.8		
	355.2	354.8	355.3
	5.4	5.8	5.3
	10		10
			355.65
			356.05
			4.93
			4.53
			11.8 apron
			15.2 floor
	356.37		
	4.21		
	10 = Top of conc. foundation		
	355.65	355.56	355.6
	4.93	5.02	5.0
	12.5	10.5 apron on conc.	10
		5.0	5.3
		5.0	5.0
			10
			355.63
			355.71
	355.64	355.60	
	4.94	4.98	4.95
	12.2 floor conc.	10.2 = edge of Apron Conc.	15 Apron
			4.87
			18.9 floor

check B.M.			4.86	354.73	354.71
------------	--	--	------	--------	--------

T.P.	5.26	359.59	6.25	354.33	
------	------	--------	------	--------	--

5+96.45 = s.b. Wightman

354.89

354.6

354.79

5.09

6.0

5.79

9.8 end of cb.
+ dirt10-end of cb.
+ dirt

X-Sect. 20' Alley in Block 8
City Hts Annex # 1

5-10-46 Notes Reduced Cherry.

INDEXED

W.K.
AUG 10 1949

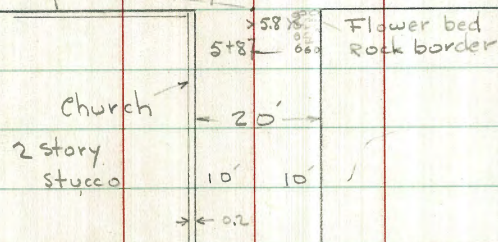
4-26-46
Osborne
Hardin
Carey
Kreft.

Wightman St.

34

Set RL 3/23/62
D.A.S.

~~Nothing set?~~



7'

↑
Z
↓

Block

8

Highland

5)
4
4



Landis St.

1+00

	Lt.	R	RT.
	354.3	355.8	355.1
	4.5	4.0	3.7
	50	20	10

0+75

	Lt.	R	RT.
	354.1	354.7	354.8
	4.7	4.0	3.8
	20	10	10

0+49 - 89 Lt. = P. pole

0+41 = Single garage on Lt. Conc floor + apron

	Lt.	R	RT.
	354.40	354.22	354.5
	4.42	4.6	4.3
	12.5 floor gar.	10.6 apron	10

0+15

	Lt.	R	RT.
	354.10	353.6	354.1
	4.72	5.2	4.7
	12.3	10	10

Not in B.M. Area to be low

0+00 = N.L. landis

	Lt.	R	RT.
	353.48	353.5	353.41
	5.39	5.3	5.41
	10.2 end of cb.		9.8 = face of end of cb.

B.M. 5.23 358.82

353.59 N.W. 1/4 Tack landis + High land.

358.82

T.P. 4.39 360.14 3.07 355.75

3+00

2+97 - 9' Lt. = \pm P. pole

2+50

2+00 - 9.1 Lt. = \pm P. pole

1+50

1+42 = \pm Single Garage on Lt. Conc. floor + apron

Lt.

\$

Rt.

36

355.8

355.7

355.6

355.5

355.4

3.0

30

3.1

10

3.2

3.3

10

3.6

30

355.5

355.4

355.3

3.3

10

3.4

3.5

10

355.1

355.2

355.4

355.4

355.4

3.7

30

3.6

10

3.4

3.4

10

3.4

30

355.0

355.1

355.2

3.8

10

3.7

3.6

10

355.07

354.66

3.75

16.8

floor

4.16

11.2

apron

358.82

4+54 = \$ Single gar. on Lt. Conc. floor

4+48 - 9' Rt. = \$ Tel. pole

4+41 - 10.8 Rt = end picket fence

floor of former garage - used as horse

4+39 - 9' Lt. = end of picket fence + 16.4 Lt. = Conc.

4+00

3+96 = 8.5 Lt. = \$ P pole + 10.2 Rt. = beg. picket fence

3+86 - \$ Single garage on Rt. Conc. floor + apron

3+77 - 9.6 Lt. = beg. old picket fence.

3+77 = 9.8 Rt. = end board fence

3+50

3+46 - 10.2 Rt. - beg. board fence

\$ Lt. Rt.
355.01 355.1 355.0 355.1

5.13 5.0 5.1 5.0
16.3 floor of 10
gar. Conc. 10

355.44

4.70
16.4 - floor

354.8 355.0 355.1 354.7 354.4

5.3 5.1 5.0 5.4 5.7
30 10 10 10 30

355.04 355.14

O.K. - F.O.
5-29-46

5.10 5.00
11.6 apron 14 - floor

355.4 355.3 355.1

4.7 4.8 5.0
10 10

360.14

check B.M. 345 354.71
354.72 NW.B.P.
44th Wight.

T.P. 5.41 358.17 7.38 352.76

5+96.47 = S.L. Wightman

5+87 - 9.5 Rt. = Φ Tel. pole

5+80

5+53 - 10.1 Rt. = Φ 1.5' Conc. walk

5+40

5+14 - 10.2 Lt. = vent. in Church foundation

5+06 = Φ Double qgr. on Rt. Gravel floor

5+00 - 10' Lt. = Φ 4' Conc. landing to steps for Church

4+97 - 8.6 Lt. = Φ P. pole

Lt. Φ Rt. 38

352.76 352.9 352.59

7.38 7.2 7.55
10 - Φ end cb. 9.8 = end cb.

355.0 354.2 354.5

5.1 5.9 5.6
10 10

354.68

5.46
10.1 = edge of walk

354.8 354.0 354.9 354.6

5.3 5.3 5.2 5.5
10 10 20

355.72

4.42
10.2 = Top of sill
of vent.

354.1

6.0
33 = floor
qgr.

355.00 354.9 354.9

5.14 5.2 5.2
10 10

10 on edge
conc.

360.14

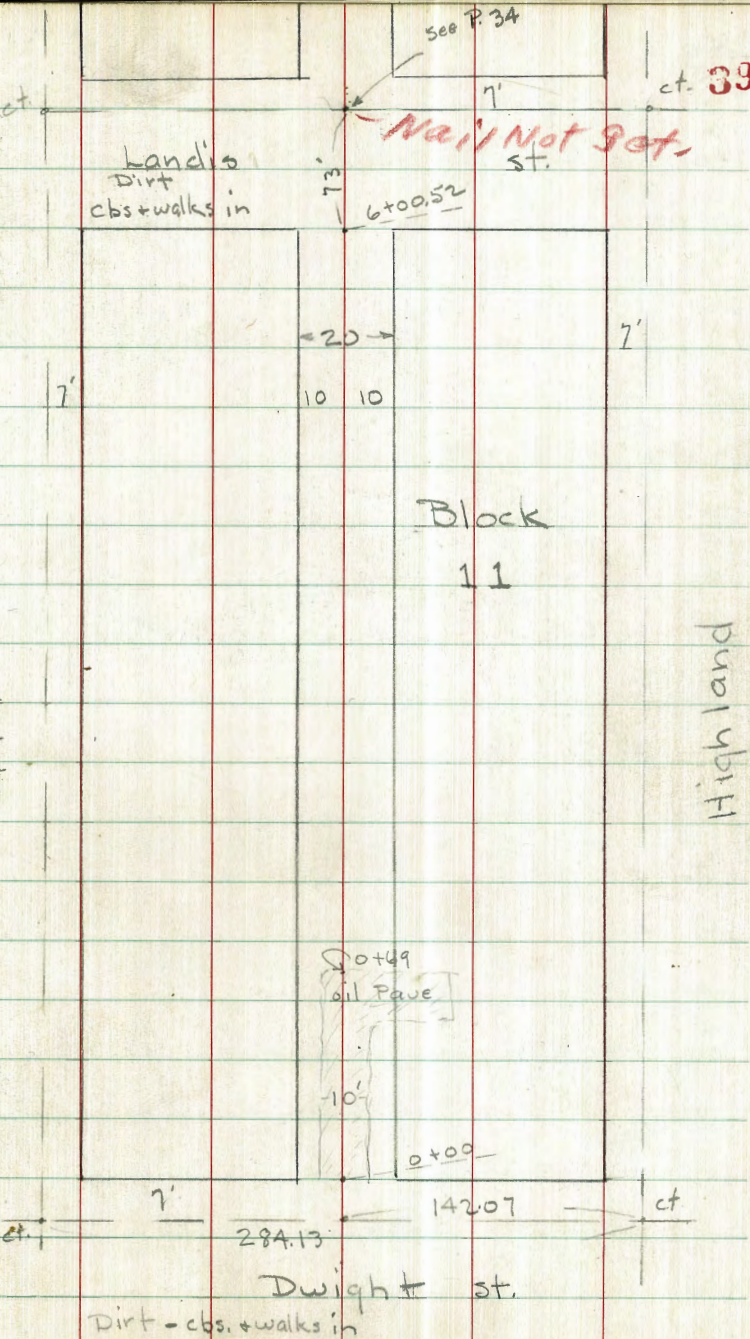
4-27-46
Osborne
Hardin
Carey
Kreft.

X-Sect. 20¹ Alley in Block 11
City Hts. Annex

5-10-46 - Notes Reduced - Wherry -

INDEXED

W.K.
AUG 10 1949



1+00

0+89 = # Single Gar. - Conc. floor

0+78 - 8.1 Lt. = # P. pole

0+60 - # Single gar. on Rt. Conc. floor /

0+56 = # Single Gar. on Lt. - dirt floor

0+10

0+00 = N.b. Dwight edge paving new check plans

1.65 353.86 6.04 352.21

B.M. 4.66 358.25

353.59 kondisettigland

new track

346.7

7.2
30

347.2 Lt.

6.7
20

347.4

6.5
10

R

347.2

6.5
10

347.9 Rt

6.0
10

50

348.18

5.08
19.7 = Floor

348.31

5.55
19.7 = floor
gar.

346.2

7.7
10.5
gar. floor

346.2

7.7
10

346.6

7.3
10

347.2

6.7
10

345.7

8.2
10

345.7

8.2
10

346.2

7.7
10

345.05
New

345.4

345.8

345.99

345.60

345.12

9.4

345.40

8.46
10 = end cb.

345.4

8.5

345.8

8.1
9.7
dirt

345.99

7.87
9.7 = end cb.

345.60

9.4

353.86

2+70 - ^{Rt} Single Gar. Conc. floor + apron

2+51 - 9.4 Lt. = beq. board fence

2+38 - ^{Rt} Single Gar. on Rt. Conc. floor + apron + floor
of House on Lt. is comparatively low

2+13 - ^{Rt} Single gar. on Rt. Conc. floor + Apron

2+00

1+96 ^{15'} ^{Rt} NW cor 4 garages con floor + apron apt above

1+86 - 9' Lt. = ^{Rt} P. pole

1+55

1+50 ^{15'} ^{Rt} SW cor 4 garages con floor + apron apt above

1+17 - ^{Rt} Single gar. on Rt. Conc. floor

350.1 Lt. 350.3 350.5 350.7 Rt. 350.6 41 351.0
3.8 3.6 3.4 3.2 3.25 2.85
20 10 10 10 10.3 apron 1.5 floor

350.26 349.3 349.7 349.9 350.5 350.5 350.88
3.60 4.6 4.2 4.0 3.4 3.35 2.98
14.5 14.5 10 floor level House = ground 13.3 apron 17.1 Floor

350.3 350.90
3.55 2.96
13.4 = apron 17.1 = floor

349.2 349.7 349.2 349.9
4.7 4.2 4.7 4.0
20 10 10

349.59 350.13
10 = apron 1.5 = floor

348.1 348.2 348.7 349.2 349.54 350.18
5.8 5.5 5.2 4.7 4.93 3.52
20 10 10 floor gar.

348.93

4.93
14.4 = floor gar.

353.86

7.0. OK, give up

4+08 = S. Side Double Gar on Lt Conc floor

4+00 = 83 Lt = P. pole

x 3+84 = £ 2' Conc. walk on Rt. 11.2

x 3+74 = £ Single gar on Rt. - Conc. floor + Apron

3+63^{18"} Lt £ double garage con floor + apron

3+50

3+26 = £ Double Gar on Lt Conc. floor - Used as store room

3+15 = 96 Lt. = End slat fence

3+13 = N. end double gar. on Rt.

J.P. 5.89 357.25 2.50 351.36

3+01 = 9.5 Lt = end board fence - beg old slat fence

3+00 = 84 Lt = P. pole on Rt.

2+95 = S. end Double gar / Conc. floor + Apron

	Lt.	E	Rt.	
	352.30			
4.95 Floor 18 gar.	351.9	351.8	352.1	352.2
	5.3 20	5.4 10	5.1	5.0 10
				352.46
352 ⁰⁸ 18 Floor	351.0	351.4	351.7	351.8
	6.2 20	5.8 10	5.5	5.4 10
				352.8
				22.5 = apron
				25.3 floor
	350.59			
6.66 18 = floor				
	50.7	380.9	351.3	351.6
	6.5 20	6.3 10	5.9	5.6 10
				5.63 15.4 apron
				5.30 17.9 floor
				351.62
				351.93
				357.25
				351.59
				351.96
				2.27 15.4 = apron
				1.90 17.9 floor
				353.86

5+36 - 9.7^{w. side} Rt. = Beg. 3' Hedge 5' High

5+32 = Single Gar. on Rt. Conc. floor + apron

5+00 - 8.4 Lt. = P. pole

4+91 = Single Gar. on Lt. Dirt floor

4+50

4+40 = Single Gar. on Lt. Conc. floor

Note: fence with gate in front of gar.

4+26 = Single Gar. on Rt. Conc. floor + apron

4+24 = N. end Double gar. Conc. floor Lt

4+09 = Single Gar. Conc. floor + apron (on Rt.)

43

Lt.

Rt

352.5

4.7
20

352.5

4.7
17.8 floor
gar.

351.9

5.3
30

352.24

5.01
17.8
Floor

352.29

4.96

18 on Conc.
floor gar.

352.8

4.4

352.1

5.1
10

352.2

5.0

357.25

353.0

4.2
10

352.2

5.0
10

353.66

3.59
23.2
apron

352.90

4.35
22.7
apron

353.06

4.19

9.6 apron
16.6 floor

353.88

3.37
26 Floor

353.18

4.07
25.6
Floor

Lt. E Rt.

check B.M. 4.47 353.60 353.59

6+00.52 = S.L. Landis - 9' Rt. = W. side of end 3' Hedge
edge paving now check plans

T.P. 4.97 358.07 4.15 353.10

5+97 - 7.8 Lt. = E. side of end 2' Hedge

5+80

5+66 - 8.2 Lt. = E. side - begin 2' Hedge 2.5 high

5+55 = Single Gar. on Lt. Conc. floor + apron

5+40

5+27 15' Lt & double garage + apt's above con floor + apron
under const.

353.20
353.2
353.17
353.07

9.4
4.87
9.9 = end cb. + dirt
4.9
4.90
9.9 = end cb. + dirt
9.4

358.07

353.4
3.8
10
353.4
3.8
10
353.4

353.35
3.90
10 = floor gar.
353.18
4.07
8 = edge of apron

353.58
15' floor
353.37
10' apron
353.1
4.1
10
353.2
4.0
353.0
4.2
10
357.25

46th St.

Paved (A.C.)

48.75 ₀₊₁₀₀

24'

48.9

0+71.4

0+94.6

50'

25' 25'

Orange Ave

20' Alley
Dirt.

1+45

49.9

Orange

A

50' ₂₊₂₅

49.8

Menlo Ave

Note: Showing
True dist. bet. Top
face of cbs. for est.

Menlo Ave

45

Paved (A.C.)

49.9

50' ₀₊₅₀

50' ₁₊₂₅

Orange

20' Alley
Dirt.

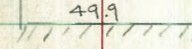
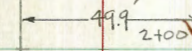
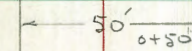
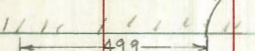
20' Alley
Dirt.

5.5' cb broken
out.

49.9' ₂₊₀₀

49.9'

47th St.



47th St.
Paved A.C.

49.8' 0+00

49.8' 0+25

0+50 50'

Ave

1+25 49.9'

1+48 49.8'

Orange

49.8' 2+25

49.8'

20' Alley
Dirt.

Euclid

Paved A.C.

Ave

Dirt.

Orange Ave

46

ct. 141.07

Mail

282.15

ct.

5+77.12

\$

10' 10'

BLK. I

Chester Park
Add.

MENLO AVE

Notes in 1691-49-

46

6'

6'

ct.

4

141.02

0+00

282.03'

ct.

Set Cap. Nail

Polk Ave

Paved A.C.

8.85'

10.8'

2.2 2+25

Sidewalk MARKS

X-Sect. Orange Ave. from W.L. 46th
to E.L. Euclid Ave. 80' st. +
15' cbs. - except first 100' E. of 46th.

R = Base line - Sketch - P. 45
5' walks - 8' Back of cb.

INDEXED

W.K.
AUG 10 1949

0-12 = E cb of 46th

353.28

2.75
40
9ut

354.00

2.03
40
Top
cb

353.34

2.69
40
9ut

353.64

2.49
24

353.73

2.80
12.5

353.81

2.22

353.79

2.24
12.5

353.66

2.37
25

353.58

2.45
40
9ut

354.18

1.85
40
Top
9ut

353.46

2.57
65
9ut

0-30 = ~~R~~ 46th

353.73

2.30
40

353.72

2.31
24

353.75

2.28
12.5

353.75

2.28
on MH.

353.71

2.32
12.5

353.63

2.40
25

353.61

2.42
40

0-48 = W. cb. of 46th

353.30

2.73
80
9ut

353.29

2.74
61
9ut

low spot
pool water

353.92

2.11
40
Top cb.

352.38

2.65
40
9ut

353.51

2.52
24
N. cb. line
Orange

353.69

2.34
12.5

353.70

2.33

353.55

2.48
12.5

353.23

2.80
25
S. cb. line
orange

353.06

2.97
40
9ut

353.69

2.84
40
Top
9ut

352.87

3.16
65
9ut

0-60 = W.L. 46th = W. edge A.C. Paving

353.98

2.05
Top cb
end Ret.

353.34

2.69
24
9ut

353.58

2.45
12.5

353.67

2.36

353.45

2.58
12.5

352.96

3.07
25
9ut

353.65

2.38
25
Top cb
end of Ret.

B.M. 2.09 356.03 353.94 + Orange NW. B.P. 46th

356.03

6-12-46
Osborne
McCoy
Hardin

Lt.

R

Rt.

47

Notes. Reduced - 6-20-46
rsherry-

0+946 = Angle in N. cb.

	LT.	#	RT.
	352.13		
	3.90	47	4.1
	25	25	3.6
	Top.	gut.	12.5
			3.8
			4.4
			3.87
			25
			25
			Top

0+774 = Angle in N. cb.

	LT.	#	RT.
	352.46		
	3.57	44	3.7
	24	24	3.4
	Top	gut.	12.5
			3.6
			4.1
			3.51
			25
			25
			Top

0+50

	LT.	#	RT.
	353.16		
	2.87	37	3.2
	33	24 = on	2.9
	S. edge of walk	edge of Dr.	12.5
			3.1
			3.5
			gut.
			3.36
			25
			32 =
			on edge of Drive
			N. edge of walk
			2.70

0+25

	LT.	#	RT.
	353.39		
	2.64	34	2.8
	24	gut.	2.7
	Top		12.5
			2.7
			3.2
			25
			gut.
			2.50
			25
			Top

0+00 = E. L. 46^H = E. edge of A.C. pave.

	LT.	#	RT.
	353.95		
	2.10	27	2.2
	24	24	2.2
	Top.	gut.	12.5
			2.35
			2.55
			19.5
			25
			25
			Top

356.03

2+32 = \$ 20' Conc. Dr. on Lt.

2+11 = \$ 8' Dirt Dr. on Rt. - no conc. broken out by owner

2+00

1+86 = \$ 10' Conc. Drive

1+75

1+45 = E.L. Alley

1+34 = \$ 8' Drive - Conc. \$51.73

1+35.8 = Sewer M.H. on \$ 4.30 on rim

1+29 = 12' Lt. = \$ 15" Dia. Gate Cover 351.30 = E.L.

1+25 = W.L. 20' Alley on S.

Lt. Rt. 350.01 349.19 349.6 349.6 349.5 348.9 349.64

6.02 6.84 6.4 6.4 6.5 7.1 6.39
33 25 12.5 12.5 12.5 25 25
+gut. = edge of Dr. gut. Top

350.23 349.2 349.9 350.1 349.9 349.2 350.15

5.70 6.6 6.1 5.9 6.1 6.6 5.88
25 25 12.5 12.5 12.5 25 25
Top gut. Top

350.67 349.92 350.67 349.8 350.3 350.6 350.3 349.8 350.53

5.36 6.2 5.7 5.5 5.7 6.2 5.50
25 25 12.5 12.5 12.5 25 25
Top gut. Top

351.17 350.9 350.9 351.2 350.9 350.4 350.96 351.12

4.86 5.6 5.1 4.8 5.1 5.6 5.07 4.91
25 25 12.5 12.5 12.5 25 25 on Ret. +gut
Top cb. end-Top

351.64 350.88 4.39 5.15
33 25
walk Dr.

351.59 350.8 351.2 351.7 351.3 351.0 351.71 351.3 351.75

4.44 5.2 4.6 4.3 4.7 5.0 4.32 4.7 4.28
25 25 12.5 12.5 25 25 25 25
Top gut on 2' Rad. Ret.

356.03

Top ab

T.P. 5.77 355.14 6.66 349.37

3+30.2 = 0+00 = E.L. Menlo + E. edge pave.

3+18.2 = E. cb. Menlo

3+00.2 = ± Menlo

Orange
Check B.M. - N.W. B.P. Menlo + 6.66 349.37 B.M. Book 349.33

2+82.2 = W. cb. Menlo

2+70.2 = W.L. Menlo Ave. = W. edge A.C. paving

6-13-46
70.

Lt.

±

Rt.

50

349.37 348.71 348.91 348.04 348.88 348.54 349.08
6.71 7.32 7.12 6.99 7.15 7.49 6.95
25 25 12.5 12.5 25 25 25
Top. 9ut. 9ut. 9ut. 9ut. Top. Top.

348.87 348.30 348.80 348.69 348.66 348.63 348.61 348.55 348.53 349.20 348.85
6.73 7.23 7.34 7.37 7.40 7.42 7.48 7.50 6.83 7.60
40 40 25 12.5 12.5 12.5 25 40 40 6.5
Top 9ut. 9ut. 9ut. 9ut. 9ut. 9ut. 9ut. 9ut. Top. 9ut.

349.08 349.03 348.88 348.82 348.82 348.83 348.83
6.95 7.00 7.15 7.21 7.21 7.20 7.20
40 25 12.5 on M.H. 12.5 25 40

349.37 348.73 348.70 348.67 348.65 348.58 348.55 348.44 349.06 348.48
6.66 7.30 7.33 7.36 7.38 7.45 7.50 7.59 6.97 7.60
40 40 25 12.5 12.5 12.5 25 40 40 6.5
Top 9ut. 9ut. 9ut. 9ut. 9ut. 9ut. 9ut. 9ut. Top. 9ut.

349.38 348.73 348.82 348.87 348.74 348.48 349.07
6.65 7.30 7.19 7.16 7.29 7.55 6.96
25 25 12.5 12.5 12.5 25 25
Top 9ut. 9ut. 9ut. 9ut. 9ut. 9ut. Top

356.03

1+00

0+95 = # 10' Conc. Dr. on Rt.

Note: 5' walk on Rt. 4.5 in from cb. in this Block

0+82 = # 8' Conc. Dr. on Lt.

0+75

0+50

0+25

51

	Lt.	#	Rt.	
	351.15	350.6	350.6	350.1
	399 25	4.5 25	4.5 12.5	4.4 12.5
				350.4 350.1
				4.7 25
				5.0 25 9.4
				4.25 25 Top
				350.28 350.94
				4.86 Dr. 25
				4.20 walk 29.5
	350.95	350.34		
	4.19 walk 33.1	4.82 Dr. 25		
	350.00	350.3	350.4	350.1
	4.34 25 Top.	5.1 25 9.4	4.8 12.5	4.7 12.5
				5.0 25 9.4
				5.6 25 9.4
				4.67 25 Top
	350.31	349.7	349.9	350.0
	4.83 25 top	5.4 25 9.4	5.2 12.5	5.1 12.5
				349.5 349.2
				5.6 12.5
				5.9 25 9.4
				5.23 25 Top
	349.75	348.9	349.5	349.6
	5.39 25 Top	6.2 25 9.4	5.6 12.5	5.5 12.5
				349.3 348.9
				5.8 12.5
				6.2 25 9.4
				5.66 25 Top
				349.48
				355.14

1+75 - 12.5 Lt. = # 2.5 x 2.5 S.D.G. + E. Conc. M.H.

1+45 = E.L. 20' Alley

Note: in alley to N. Grade falls S. towards Orange

in Alley to S. - Grade falls S. Away from "

1+34.7

1+33 = E. Side 7' x 4.3 M.H.

1+29.4 = W. side of 5.3 x 3.4 S.D.G. + E. Conc. M.H.

1+26 = W. side 7' x 4.3 S.D.G. + E. Conc. M.H.

T.P. 5.79 358.17 2.76 352.38

1+25 = W.L. 20' Alley

52

352.69	352.18	352.28	352.29	352.2	352.0	351.5	352.37
5.48	6.4	5.93	5.88	6.0	6.2	6.7	5.80
25	25	13.6	11.1	12.5	12.5	25	25
Top.	gut	N. side M.H.	S. M.H.			gut	Top

352.4	352.99	352.20	351.3	351.6	351.6	351.4	351.1	351.82	351.8	352.00
5.8	5.68	5.97	6.9	6.6	6.6	6.8	7.1	6.35	6.4	6.17
40	34.5	25	25	12.5	12.5	12.5	25	25	40	40
ground.	end of	Top.	gut.				gut.	Top	gut	Topcb
	Ret. broken						2 Rad.			end Ret.
	out.						Ret.			

351.25	351.31								
6.92	6.86								
NE. Cor. 20.5	16.2 = SE. Cor.								

351.35	351.39								
6.82	6.78								
N.W. Cor. 13	9.6 = on S.W. Cor								

351.15	351.19								
7.02	6.98								
N.W. Cor. 20.5	16.2 S.W. Cor								

351.92	351.8	351.60	351.1	351.1	350.9	350.7	351.26	351.2	351.46
3.22	3.3	3.54	4.0	4.0	4.0	4.2	4.4	3.78	3.9
40	40	25	25	12.5	12.5	12.5	25	25	40
endcb.	gut	Top	gut.				gut.	Topcb	gut.
Alley ret.							2 Rad.		
							Ret.		

3+00 = # 47th

2+82 = w. cb. 47th

2+70 = w.l. 47th + w. edge A.C. paving

2+45

2+08 = # 20' Conc. Dr. on Lt.

Note: E. of Alley 5' walk on N. is 4.5 back of cb.

2+00

	Lt.			Rt.		
354.59	354.98	354.43	354.35	354.37	354.24	354.10
3.58 40	3.69 25	3.74 12.5	3.82	3.80 2.5	3.93 25	4.07 40

357.60	354.04	354.00	354.05	353.98	353.88	353.65	353.45	354.13	353.24
3.57 40 Top.	4.13 40 gut.	4.17 25	4.12 12.5	4.19	4.29 12.5	4.52 25	4.72 40 gut.	4.04 40 Top	4.93 65 gut.

354.45	353.91	353.98	354.07	353.91	353.43	354.04
3.72 25 Top.	4.26 25 gut.	4.19 12.5	4.10	4.26 12.5	4.74 25 gut.	4.13 25 Top

353.99	353.1	353.9	353.4	353.1	352.8	353.61
4.18-Top 25	5.1-gut 25	4.9 12.5	4.8	5.1 12.5	5.4 25 gut.	4.56 25 Top
353.57	352.7					
4.60 29.5	5.40 25					

352.12	352.4	352.7	352.7	352.5	352.0	352.78
5.05 25 Top	5.8 25 gut.	5.5 12.5	5.5	5.7 12.5	6.2 25 gut.	5.39 25 Top

358.17

0+15

0+50 = # 20' Conc. Dr. on Rt.

0+25

3+30 = 6+00 = E.L. 47th + E. edge AC. paving

3+18 = E. cb. 47th

354.54
3.63
65
40
Top

Lt. # Rt.

354.87	354.2	354.5	354.7	354.4	354.9	354.97
3.30	40	3.7	3.5	3.8	3.8	3.20
25	25	12.5		12.5	25	25
Top	gut.				gut	Top

354.92	354.3	354.5	354.7	354.6	354.51	355.09
3.25	3.9	3.7	3.5	3.6	3.66	3.08
25	25	12.5		12.5	25	29.5
Top	gut.				Dr.	walk

354.96	354.5	354.5	354.6	354.7	354.4	354.93
3.21	3.7	3.7	3.6	3.5	3.8	3.24
25	25	12.5		12.5	25	25
Top	gut.				gut.	Top

354.94	354.32	354.68	354.19	354.71	354.44	355.01
3.23	3.85	3.49	3.38	3.46	3.73	3.16
25	25	12.5		12.5	25	25
Top	gut.				gut.	Top

355.04	354.51	354.51	354.69	354.70	354.71	354.54	354.34	354.17	353.94
3.13	3.66	3.66	3.48	3.47	3.46	3.63	3.83	3.20	3.23
40	40	25	12.5		12.5	25	40	40	65
Top	gut.						gut.	Top	gut

358.17

1+70

Lt.				Rt.			
353.45	353.6	353.1	353.2	353.2	353.0	353.75	
40.6	5.0	4.4	4.3	4.3	4.5	37.6	
2.5	2.5	12.5		12.5	2.5	2.5	
					gut.	Top	

1+45 = E.L. 20' Alley

354.29	354.15	353.4	353.7	353.8	353.8	353.6	354.51
3.22	3.36	4.1	3.8	3.7	3.7	3.9	3.00
4.0	2.5	2.5	12.5		12.5	2.5	2.5
Top ob. + gut.	Top					gut.	
end. Ret.							

1+25 = W.L. 20' Alley - Note: Grade of Alley to N.
falls to N.

354.9	354.71	354.68	353.7	354.0	354.3	354.1	353.9	354.65
3.1	2.80	2.83	3.8	3.5	3.2	3.4	3.6	2.66
4.0	4.0	2.5	2.5	12.5		12.5	2.5	2.5
gut.	Top	Top ob. gut.					gut.	Top
		2' Rad. Ret.						

1+00

354.79	354.0	354.3	354.6	354.4	354.1	354.88
2.72	3.5	3.2	2.9	3.1	3.4	2.63
2.5	2.5	12.5		12.5	2.5	2.5
Top	gut.				gut.	Top.

T.P. 3.43 357.51 4.09 354.08

357.51

0+86 = # 12' Conc. Dr on Lt.

354.91	354.20
3.26	3.97
29.5	2.5
edge walk	on Dr.

358.17

1
 T.P. on B.M. 673 357.49 625 350.76
 2+70.2 = W.L. Euclid Ave = W. edge A.C. Paving

350.69 = B.M.
 Book
 N.W. 13P.
 Euclid + Orange

6-15-45
 7.0.

1+50

2+32 = Φ 10' Conc. Drive on Lt.

2+25

2+00

1+90 = Φ 10' Conc. Drive on Lt.

1+85 = Φ 18' Conc. Drive on Rt

	Lt.	+	Rt.
	350.11 6.80 25 Top	350.31 7.20 25 gut.	350.58 6.93 12.5
	350.71 6.80	350.8 6.7	350.8 6.7
	350.55 6.96 12.5	350.71 6.80	350.55 6.96 12.5
	350.15 7.26 25 gut.	350.63 6.88 25 Top	350.15 7.26 25 gut.
	351.21 6.30 25 Top	350.7 6.8 25 gut.	350.8 6.7 12.5
	351.83 5.68 27.5 walk	351.24 6.27 25 Dr.	350.8 6.7 12.5
	351.91 5.60 25 Top	351.2 6.3 25 gut.	351.6 6.0 12.5
		351.5 6.0 12.5	351.6 5.9
		351.4 6.1 12.5	351.4 6.1 12.5
		351.1 6.4 25 gut.	351.1 6.4 25 gut.
		352.01 5.50 25 Top	352.01 5.50 25 Top
		351.7 4.94 25 Top	351.7 5.8 25 gut.
		352.3 5.2 11.5	352.4 5.1
		352.2 5.3 12.5	352.2 5.3 12.5
		352.0 5.5 25 gut.	352.0 5.5 25 gut.
		352.79 4.72 25 Top	352.79 4.72 25 Top
	352.98 4.53 29.5 walk	352.49 5.12 25 Dr.	
			352.79 4.72 25 Dr.
			353.40 4.11 29.5 Walk

357.51

Check B.M. N.W. 46th + Orange 0.30 353.92 353.94
 T.P. 0.31 354.22 3.58 353.91
 3+30.2 = E.L. Euclid + E. edge of A.C. Paving

349.65
 348.96
 349.43
 349.57
 349.48
 348.99
 349.57
 7.86
 25
 Top
 8.53
 25
 gut.
 8.06
 12.5
 7.92
 8.01
 12.5
 8.50
 25
 gut.
 7.92
 25
 Top

3+18.2 = E. cb Euclid

348.89
 349.58
 349.22
 349.49
 349.94
 349.97
 349.91
 349.49
 349.23
 349.75
 349.44
 348.90
 8.60
 65
 gut.
 7.91
 40
 Top
 8.27
 40
 gut.
 8.00
 25
 7.55
 12.5
 7.52
 7.58
 12.5
 8.00
 25
 8.26
 40
 gut.
 7.74
 40
 Top
 8.55
 75
 Top
 8.59
 75
 gut.

3+00.2 = E Euclid

350.65
 350.72
 350.71
 350.71
 350.68
 350.64
 350.62
 6.84
 40
 6.77
 25
 6.78
 12.5
 6.78
 6.81
 12.5
 6.85
 25
 6.87
 40

2+82.2 = W. cb. Euclid Ave

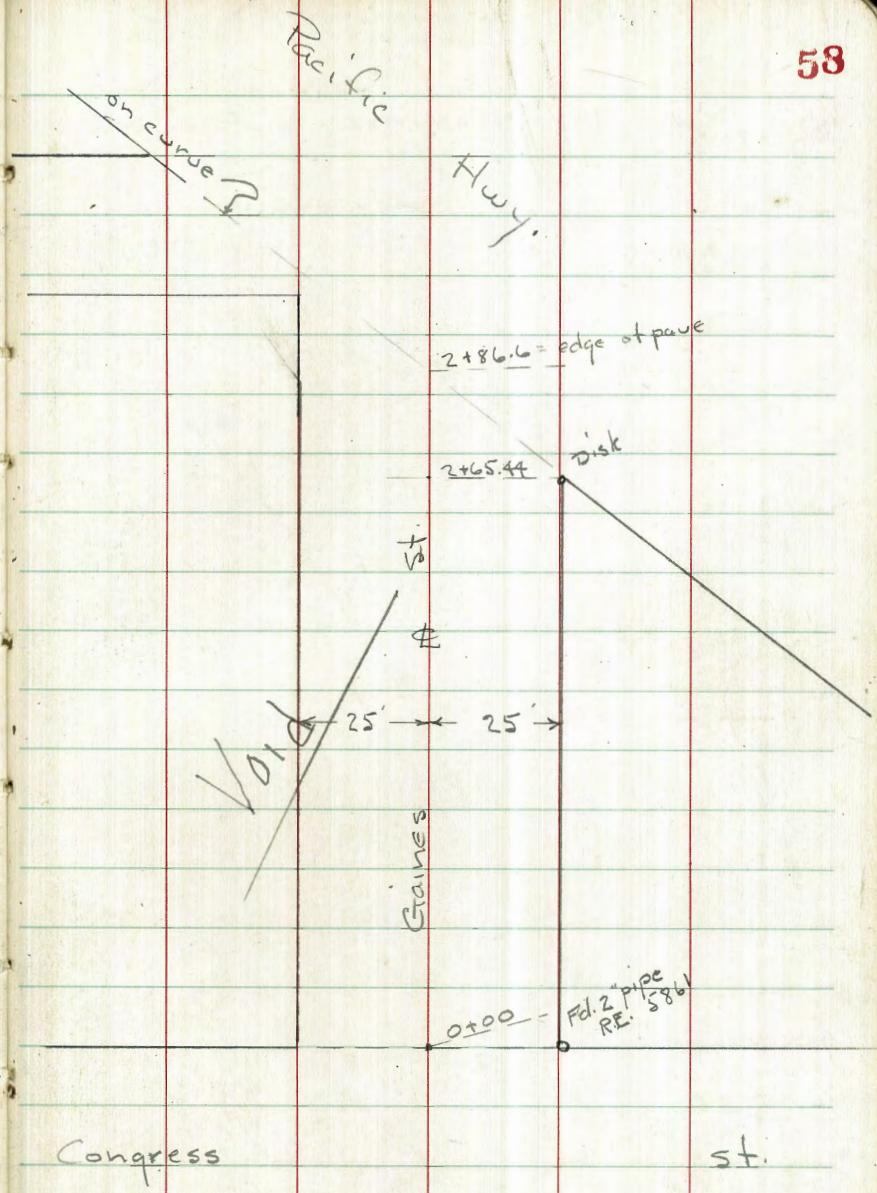
349.82
 350.63
 350.12
 350.73
 350.54
 350.61
 350.53
 350.27
 349.95
 350.54
 349.68
 7.67
 65
 gut.
 6.86
 40
 Top
 7.37
 40
 gut.
 7.16
 25
 6.95
 12.5
 6.98
 6.96
 12.5
 7.22
 25
 7.54
 40
 gut.
 6.95
 40
 Top
 7.81
 75
 gut.

357.49

X-Sect. Gaines 50' from Congress
to Pac. Hwy.

INDEVENT

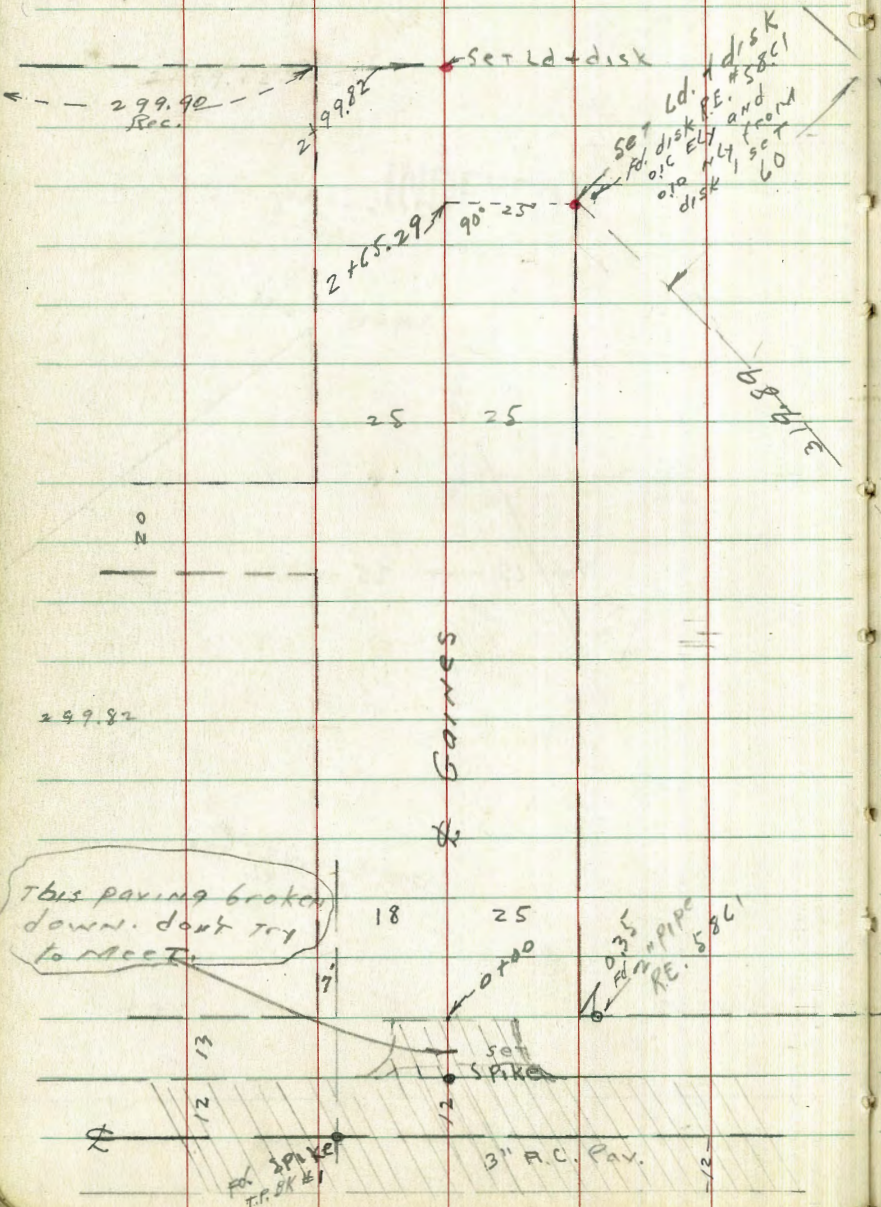
See page 59



Fd. Nail to EC

Xsec Gaines
Congress to Pacific

San Diego Ave



This paving broken down. don't try to erect.

Indexed
C.S.K.

C. Moore
S.M. McInroy
W. Moore
B299

& Pac.

10-3-46

K.O. #137

7° 56' 30"

5000
= 6930
0.2 x 38

Fd. Iron Pin
Paving
"STATE"

B.C.

Pacific Hwy.

Fd. Spike &
F.C.
"STATE"

Congress

- 1 0° 34.38
- 2 1° 08.75
- 3 1° 43.14
- 4 2° 17.52
- 5 2° 51.90
- 6 3° 26.28

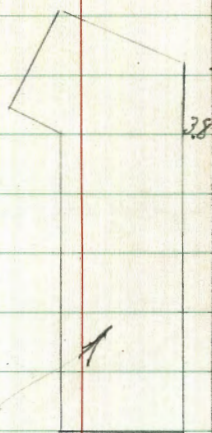
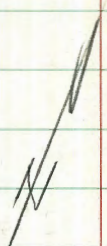
EC, 47904 3° 58.25

San Diego Ave.

Set Ld. disk

2+99.84
3.5

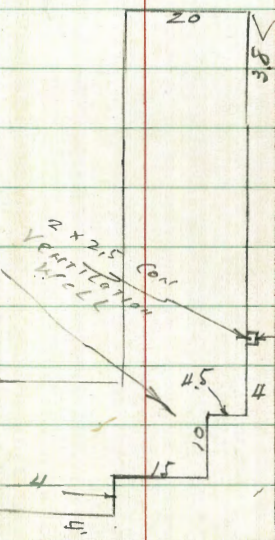
2' diam. Beacon no High



2+56.3
3.8

25 25

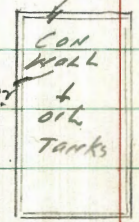
El Padre March



2 x 2.5 CON VENTILATION WALL

1 x 60
1 x 40

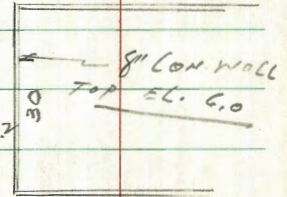
80 Games



TOP EL. 8.7

11.55

0 + 95



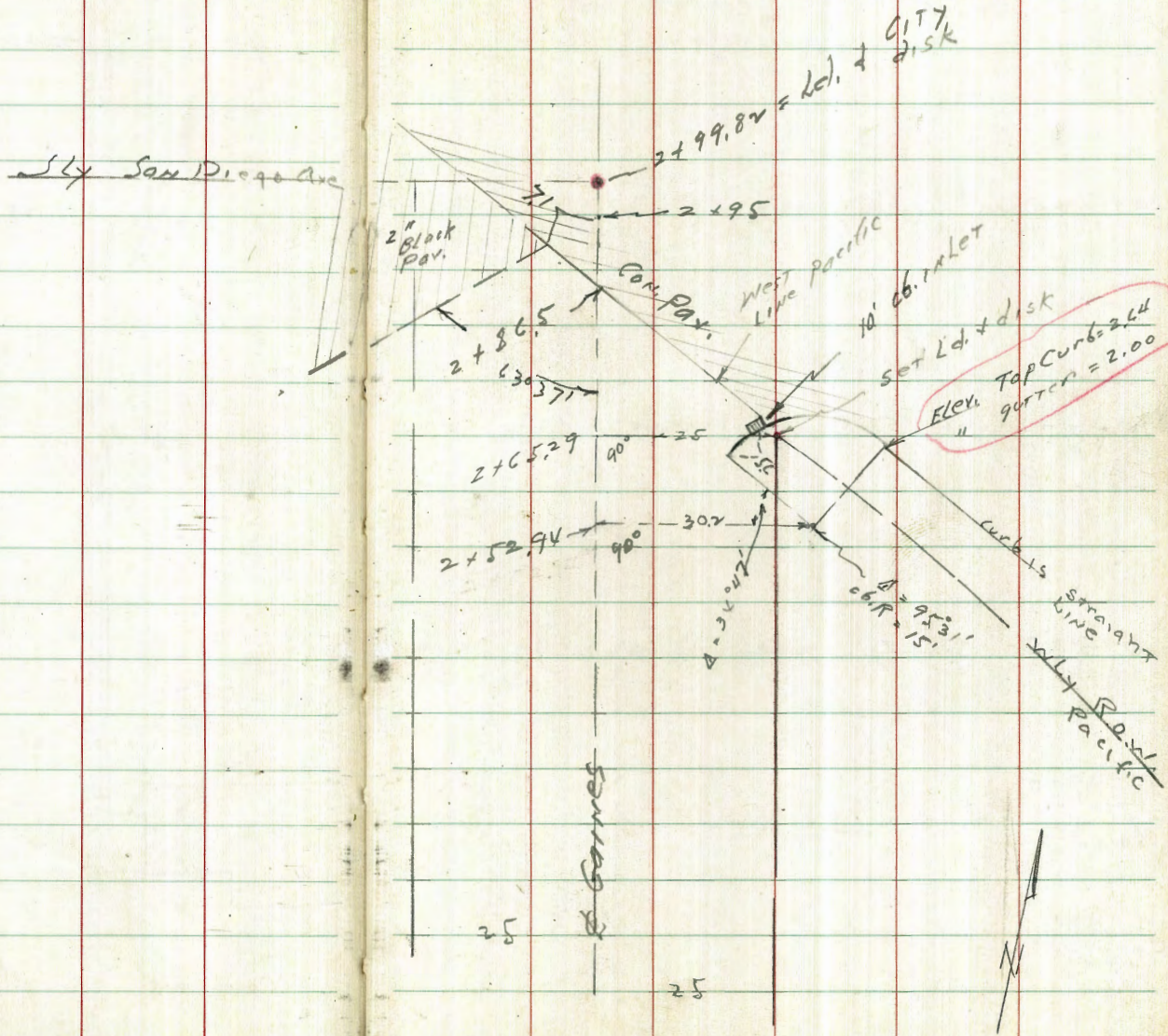
8\"/>

Congress

0+00
25.35
1\"/>

1\"/>

Detail of State Return



Xsec on Gaines St
Congress to Pacific

0-100 Nly Congress

0-13 N edge pav.

0-25 E Congress M.H. Rim

0-37 S edge pav. (2' wide)

T.P. Spike
E Congress
N.7' of
Gaines

4.38 7.65 5.40 3.27

NW BP
Congress
to
Pacific

4.42 8.67 4.25

LT = to West &

Pt 62

$\frac{4.9}{25}$ $\frac{5.51}{12}$ $\frac{5.42}{1}$ $\frac{5.02}{12}$ $\frac{5.13}{25}$

Pay Broken down

$\frac{4.47}{75}$ $\frac{4.52}{50}$ $\frac{4.68}{25}$ $\frac{4.66}{15}$ $\frac{4.84}{12}$ $\frac{4.83}{12}$ $\frac{4.93}{20}$ $\frac{4.83}{25}$ $\frac{4.77}{50}$ $\frac{4.62}{75}$

$\frac{4.22}{75}$ $\frac{4.29}{50}$ $\frac{4.36}{25}$ $\frac{4.42}{15}$ $\frac{4.42}{12}$ $\frac{4.48}{12}$ $\frac{4.80}{20}$ $\frac{4.66}{25}$ $\frac{4.50}{30}$ $\frac{4.33}{75}$

$\frac{4.40}{75}$ $\frac{4.48}{50}$ $\frac{4.58}{25}$ $\frac{4.65}{15}$ $\frac{4.70}{15}$ $\frac{4.63}{15}$ $\frac{4.70}{20}$ $\frac{4.70}{25}$ $\frac{4.65}{50}$ $\frac{4.63}{75}$

7.65

1409

Top 2x2.5 Con. Vent Well

0495

0476

Top 2x2.5 Con. Vent Well

0450

0432

Top Con. Vent Well

7.65

4.87
26.5

5.4
25

5.6
15

6.1

5.8
15

5.6
25

4.91
26.5

5.4
25

5.7
15

5.8

5.7
15

5.5
25

5.0
25

5.5
15

5.3

5.3
15

5.2
25

4.46
26.6

4.9
25

5.1
15

4.8

5.2
15

5.1
25

7.65

2 + 25

1 + 95

1 + 68

T.P. 3.91 6.34 5.22 2.43

1 + 62 20' LT. to P.P. =

1 + 55

1 + 35

7.65

Top 2x2.5 Com. Vent. well

Top 2x2.5 Com. Vent. well

Top 2x2.5 Com. Vent. well

Lt

$\frac{4.72}{25}$

$\frac{5.7}{15}$

5.1

$\frac{4.9}{15}$

Rt

$\frac{4.6}{25}$

64

$\frac{3.91}{20.5}$

$\frac{4.3}{25}$

$\frac{5.7}{15}$

5.2

$\frac{4.6}{15}$

$\frac{4.7}{25}$

$\frac{3.77}{20.5}$

6.34

$\frac{5.0}{25}$

$\frac{4.3}{15}$

4.3

$\frac{5.6}{15}$

$\frac{5.4}{25}$

$\frac{4.95}{20.5}$

$\frac{5.4}{25}$

$\frac{6.1}{15}$

6.1

$\frac{5.6}{15}$

$\frac{5.6}{25}$

7.65

2 + 86.5

2 + 87 in 2 Games

4.21

sewer
M.H. Pipe

2 + 45.29

at 90°

2 + 61.2

2 + 52.94

2 + 53

£ 375 ^{wide} Con. STEP

2 + 45

Top 2x2.5 Con. Vauzibaten Well

6.34

Lr

R

R

65

4.12
edge
C.M.
Pav

4.38

4.24

15

25

Pav.
Valley
P.L.T.

Pav

4.2

4.3

4.8

4.8

4.83

2.83

3.8

25

15

15

27.9

22

25

approx

Top
cb.

ground

7.52

INJECT
of Catch Basin

3.98

17.9

Top end Curb
Return

4.2

4.5

4.9

4.5

4.3

25

15

15

25

3.57

276

TOP BOT. STEP

3.84

26.4

6.34

check to orig. B.M. 209 4,25 4,75

2+99.8v S.L. San Diego ave 90°

2+95 on edge of F.C. Pav.
ON ANGLE see sketch

4.34

Lr

t

Pr

4.11

25

2" Pav

4.17

15

edge
Cov.
Pav

4.32

Cov.
Pav.
cut.

4.11

15

Pav.

4.01

25

Pav

3.94

4.17

4.25

50

25

15

← ↑
2" F.C. Pav.

4.17

7.1
edge
Cov.
Pav

4.31

Cov. Pav.

4.34

X-Sect Int Macaulay + Plum

626

11-15-46

Osborne
Hardin
Worrell
Smith

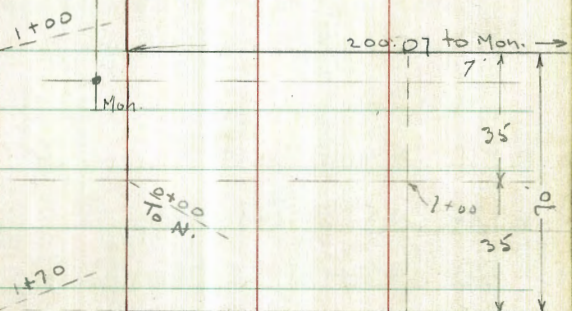
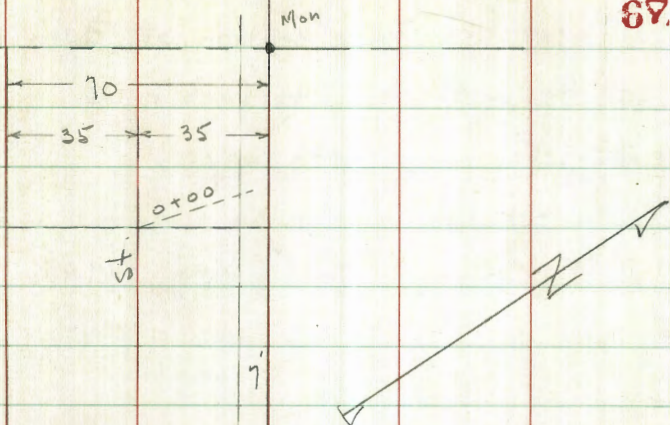
W.O. 230

INDEXED

Plum St &

Indexed
c.s.k.

87



0+00
To S.

Macaulay
2+70

X - Sect. of Intersection of Plum + Macaully
 70' Sts. + 18' cbs. 43' Curb radius.

$\pm 100'$ from int. both ways.

Plum - from S.L. Macaully - S. for 100'

T.P. 8.67 102.83 4.46 94.16 $\frac{3}{4}$ " Pipe S.W. Cor.

± 100

0+88 = S. side Gar. on Lt.

0+75

0+71 - N. side Double Gar. on Lt. Conc. floor + Apron

0+71 - 35.5 Lt. = end Hedge

0+56 - 43.4 Lt. = S.W. Cor House

0+50

0+46 - 26.2 Rt. = P. pole

0+25

0+16 35.4 Lt. = Begin + of 4' Hedge 5' High

0+00 = S.L. of Macaully

B.M. 11.40 98.62

87.22 = lowel

S.W. P. Plum

Lt. - E

Rt. = W 58

87.55	87.95	87.8	87.0	87.5	87.97	88.13	88.20	88.3	88.2	88.4
130	12.5	12.3	12.02	11.65	11.42	11.3	10.4	10.7	10.2	
50	35	17	edge pave	14	edge pave	17	35	50		
11.07	11.1									
382	352	87.8	87.0	87.5	87.97	88.13	88.20	88.3	88.8	89.5
Floor apron										
11.2	11.6	11.1	10.65	10.49	10.42	10.3	9.8	9.1		
35	22	17	10-edge pave	14-edge pave	17	35	50			
		87.57		87.7						
		11.03		11.13						
		382		352-apron						
		Floor								
91.13										
7.49	88.6	87.9	88.9	87.69	87.58		87.37	89.3	90.4	91.0
43.4										
Floor House										
10.0	10.1	9.7	89.3	9.4	9.30	9.3		8.2	7.6	
35	23	17	11-edge pave	16-edge pave	17			35	50	
87.8	87.7	90.4	91.37	91.30	90.81	90.48	90.8	92.7	92.5	
35	23	17	7	7	20.5	24		31	35	
			edge pave	edge pave	edge pave					
		92.8	92.5	93.1	93.13	93.16	92.87	92.29	92.6	
		5.8	6.1	5.5	5.47	5.46	5.80	6.33	4.0	
		35	17			2-edge at Paved strip	17	26	32 edge pave	

98.62

Plum St. Cont'd Macaulay to No. (94.16)

1517
T.P. 10.17 100.92 1.01 90.75

2170.07 N. line Newell

INDEXED
W.K.
AUG 10 1949

Notes Reduced & Plotted
M. Claren 8/11/49

2135.02 R. Newell (R. Sewer MH)

2125

2100.07 S. line Newell St. (End wire fence 347 ft)

1264 Reg wire fence 347.44

T.P. 1.01 91.76 10.18 90.75

1450

1317 6.77 100.93 94.16

✓ 1401 - N side Gar on Lt

✓ 1400 - 354 ft = P. pole # 1776

3/4" I.P. Macaulay & Plum R

70

95.8
6 0 8 2 10 14 17 20 23 25
50 35 20 20 35 50
87.6
11 10 10 8 8 8 8 8 8 8
50 35 20 12 26 35 50
88.8
30 35 55 8 11.6 14.2 18.1
50 35 20 Rim 78 35 50
90.5
11 11 2 10 4 10 10 11 12 15
50 35 20 25 35 50

92.5
10 0 17 17 75 8 9 10 12
50 35 20 20 27 31 35 50

95.8
5 6 8 10 11 14 16 17
50 35 27 5 100.93 21 35 50

3/4" Pipe (REG) SW Cor. Macaulay & Plum (RCS)

96.51
6.22
36
Floor

96.28
6.55
34.3
apron

94.2
6.6
35

94.1
8.7
28

93.9
8.9
7

94.0
8.8
8

92.5
10.3

94.8
12.0
17

89.9
12.9
35

87.9
14.9
60

102.83

1+52 = E. cb. Plum.

1+35 = Φ Plum.

1+18 = W. cb. line Plum.

1+01 - 35.2 Lt. = end edge 2' Hedge

1+01 - 32.7 Lt. = end brick border

1+01 - 21.2 Lt. = end. s. side 6.5' Parkway

1+00 = W.L Plum

0+95 - 24.5 Lt. = Φ 6" Palm

0+77 - 24.5 Lt. = Φ 6" Palm

0+76 - 26' Lt. = Φ P. pole

0+75

Lt.

Rt.

100.3	99.5	99.3	98.0	97.7	98.1	95.7	92.4
2.5	3.3	3.5	4.8	5.1	4.7	7.6	10.4
35	7	5	3	5	2	7	35

102.8	98.9	97.9	96.7	96.8	94.8	93.1
2.0	3.9	4.9	6.6	6.0	8.0	9.7
35	7	5	6	2	7	35

99.1	97.5	96.1	95.03	94.71	92.95
3.5	5.3	6.7	7.80	8.12	9.88
35	17	6	14	7	35
			edge		
			Pave		

94.5	92.8	94.71	96.51	94.72	93.85	92.65	92.7	94.6
3.3	5.5	6.12	6.32	8.11	9.98	10.18	10.6	8.2
35	7	2 = edge	6	17	24	30	33	35
		Pave				edge		
						Pave		

94.8	94.3	94.13	96.88	95.28	94.8	96.8	94.8	95.3	94.3
3.4	4.5	4.7	5.95	7.59	8.0	6.0	6.0	7.5	8.5
35	7	14	5	12	13	14	17	35	50
		edge		edge					
		Pave		Pave					

102.83

check B.M.

T.P. 5.11 96.25 11.69 91.14 90.4 87.21 87.22

2+70 = end.

2+30

2+14 - 24' Lt. = P. Pole

2+00

1+70 = E.L. Plum.

Nodes Reduced. 11-29-86

Lt.

P

Rt.

73

95.8	95.7	98.1	93.7	92.5	92.8	92.8	91.0	90.1	87.9	85.8
7.0	7.1	8.7	9.1	10.3	10.4	10.0	11.8	12.7	14.9	17.0
50	55	17	14	7	3	8	17	35	50	50

97.8	97.8	97.1	96.8	95.7	95.8	95.9	93.0	91.5	88.0
5.4	5.0	5.7	6.0	7.6	7.4	6.9	9.8	12.3	14.8
50	35	17	30	12	14	29	17	35	50

98.8	99.1	98.8	98.3	96.9	97.2	97.6	97.3	92.3	88.8
4.4	3.7	4.4	4.5	5.9	5.6	5.2	7.5	10.5	14.0
50	35	17	5	14	6	12	17	35	50

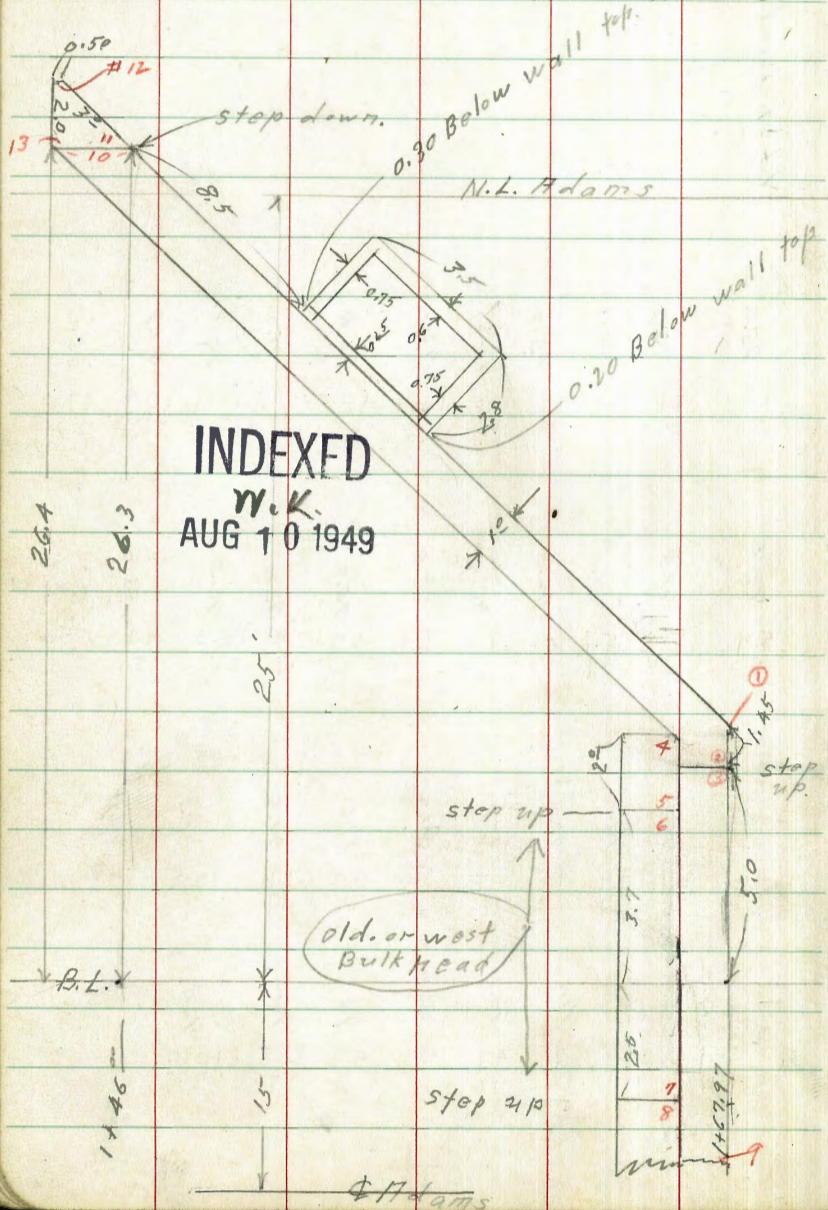
99.7	99.3	99.1	98.1	98.0	98.1	96.0	92.8
3.1	3.5	3.7	4.5	4.8	4.5	6.8	10.0
35	17	15	13	48	3	7	35

102.83 ↓

(13 edge road

Texas St. Bridge E.L. on Bulkhead.
N. W. wing wall.

Base line is 25' south of N. Line Adams



INDEXED

W.K.
AUG 10 1949

Work order #

3/11/45
Summer
W. Moore
J. Green. 74

Level	Distance	Station	FB
Louisiana Adams S.E. 7' 2 1/2	3.46	35A.20	350.74
#1	5.41	348.79	
#2	5.97	348.83	
#3	8.30	345.90	
#4	5.51	348.69	
#5	5.00		
#6	6.03		
#7	6.03		
#8	6.40		
#9	8.3		
#10	3.95	350.25	
#11	10.43	343.77	
#12	10.44	343.76	
#13	10.43	343.77	

Level shots taken as indicated by numbers on sketch.

Station to 2" down riser on water

Line = 1+67.3

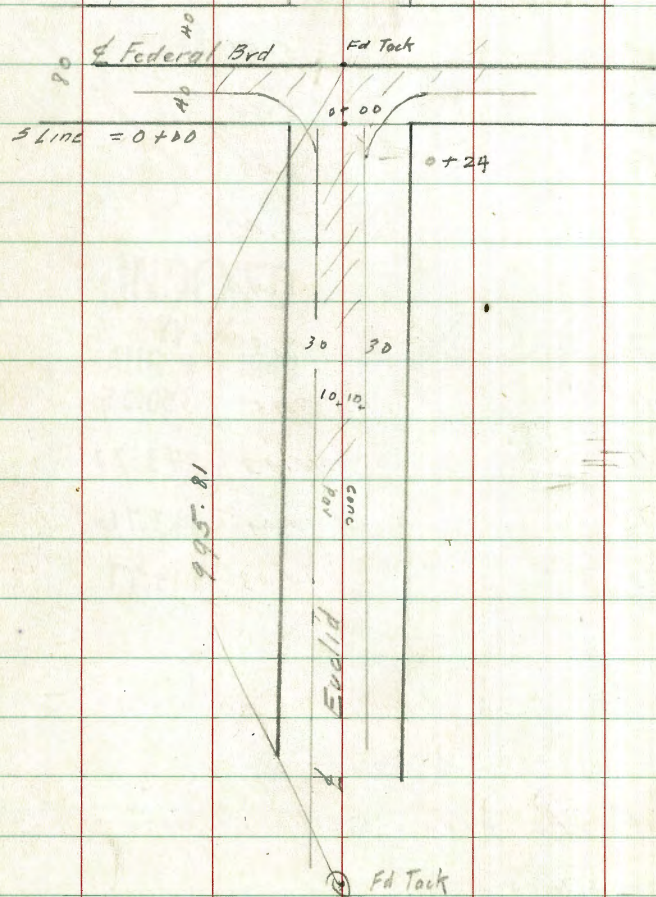
Stationing area = E. Line Louisiana

See 1671-44.01

X sec. Euclid ave from S. property line
Federal Bvd to South 600'

order # 25001 Blue # 1181

reference drawing # 4420



13/6/47

indexed
C.S.K.

Begg
Greer
Roberts

75

X Section Euclid Ave from
S Line of Federal Southerly

1 + 00

0 + 50

0 + 24

0 + 16

0 + 00

2.84 229.01

226.23

note East Side of Road is being filled

229.01
B.M. set out of Euclid & Federal

see p 21

12.3 50	6.9 22	7.81 10.9	7.76	7.92 9.5	7.76 11.1	7.8 20	7.8 26	10.5 30	11.7 50
216.8	224.4	223.77	223.70	223.53	223.62	223.7	224.0	221.1	219.2
222.2	225.2	224.97	224.90	224.72	224.85	224.6	224.2	222.3	
221.26	224.9	224.72	224.90	224.72	224.85	224.6	224.2	222.3	
221.31	223.62	223.7	224.0	224.72	224.85	224.6	224.2	222.3	
221.15	223.53	223.7	224.0	224.72	224.85	224.6	224.2	222.3	
221.31	223.62	223.7	224.0	224.72	224.85	224.6	224.2	222.3	
221.3	223.7	224.0	224.9	224.72	224.85	224.6	224.2	222.3	
221.3	223.7	224.0	224.9	224.72	224.85	224.6	224.2	222.3	
218.6	221.1	222.3	224.0	224.72	224.85	224.6	224.2	222.3	
217.4	219.2	222.3	224.0	224.72	224.85	224.6	224.2	222.3	
226.1	225.4	225.53	225.75	225.35	225.3	224.5			
3.0 50	3.7 31	3.44 21.9	3.32	3.72 22.5	3.9 24	4.6 50			

3+50

3+00

2+50

2+0

1+50

+ #1 -

TP 1.86 217.92 13.01 216.06

229.07

13.7	14.0	17.7	9.17	9.31	9.16	9.29	9.12	8.7	8.6	12.8	11.3
50	30	21	10.9	9.8	9.8	9.5	11.4	20	24	31	50
204.2	203.9	208.6	208.2	208.61	208.76	208.63	208.80	209.2	209.3	205.7	208.6

9.7	10.9	6.6	6.92	7.10	6.88	6.97	6.82	6.7	7.0	11.8	9.8
50	30	21	10.9	9.8	9.8	9.8	11	20	24	32	50
208.2	207.0	211.3	211.00	210.82	211.04	210.95	211.10	211.2	210.9	206.1	208.1

6.0	7.8	4.2	4.42	4.56	4.40	4.49	4.32	4.2	4.2	10.2	
50	27	22	11	9.7		9.8	11.0	20	23	33	
211.9	210.1	213.7	213.50	213.36	213.52	213.43	213.60	213.7	213.7	207.7	

4.5	1.7	1.92	2.09	1.85	1.97	1.77	1.7	2.0	2.0	2.0	2.0
50	21	10.5	9.5		9.7	11.1	20	23	33	50	
213.4	216.2	216.00	215.83	216.07	215.98	216.15	216.2	215.9	210.5	209.1	211.3

14.4	10.3	10.50	10.64	10.42	10.5	10.37	10.5	10.7	10.9		
50	21	11.0	9.8		10.0	11.1	20	24	30		
214.1	218.8	218.57	218.63	217.92	218.52	218.70	218.6	218.4	214.2		

229.07

205.7

+52 storm flume 14.5R to 24 R6

5+50 15.0 50

5+00 group of Willows 2.5 R6

4+50 11.7 50

TP 3.67 209.04 12.55 205.37

A+01 17.4 50

217.92

193.0	160	5.6	5.62	5.77	5.64	5.84	5.67	72	12.8	14.0
203.44	38	19	11.3	10.5		9.5	10	20	40	50
203.42										
203.27										
203.40										
203.20										
203.37										
201.8										
196.2										
195.0										

194.2	14.8	5.1	5.25	5.49	5.25	5.38	5.21	5.0	4.9	11.7
203.9	35	20	11	9.0		9.5	10.5	20	23	30
203.79										
203.55										
203.79										
203.66										
203.83										
204.0										
204.1										
197.3										
197.3										

197.3	11.7	4.0	4.27	4.44	4.25	4.35	4.16	3.7	3.6	8.2
205.0	32	21	11.2	9.9		9.4	10.6	20	23	30
204.77										
204.80										
204.79										
204.69										
204.88										
205.13										
205.4										
200.8										
202.1										

200.4	17.5	11.3	11.42	11.62	11.45	11.54	11.38	11.2	11.2	15.7
206.6	31	21	11.0	9.5		9.5	10.9	20	23	30
206.50										
206.30										
206.47										
206.38										
206.54										
206.7										
206.7										
202.2										
202.9										

217.92

7

H1

-

L

E

R

79

BM			2.54	226.25	226.23
	9.48	228.79	1.12	219.81	.02
TP	12.42	220.43	1.03	208.07	

cT Federal & Euclid

6 + 06.8 End of Flaired Edge on the right
+ left of Paring

6 + 00

190

19.0
50209.04

192.3	204.4	203.89	203.68	203.81	203.62	203.83	203.9	200.7	201.7
16.7	4.6	5.15	5.76	5.83	5.42	5.21	5.1	8.3	7.4
70	21	11	9.6		7.5	10.4	20	24	50

209.04

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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