

1707

ENGINEERS
LEVEL BOOK
No. 410F

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.

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1707

50° 16'

77.26

CITY ENGINEER'S OFFICE

INDEXED

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This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

Survey Peri Lot #1 }
Rcsub villa
Lots 1 toll }
Normal Hqts. Map # 1155 }

77

Walker LOCATION - PROPOSED DRAINS
 Hardin Between Spruce And Redwood
 Hunley from STATE ST. to KETNER
 2-21-46
 Details on Page 4

5+20.82 = P.O.T. = Int 7' Line India St.

4+65.71 = East end Exst. 12" Conc. Drain Pipe

3+78.16 = E.C.

$\Delta = 17^{\circ}53'$
 $R = 20'$
 $L = 28.09'$

3+50.07 = B.C. RT

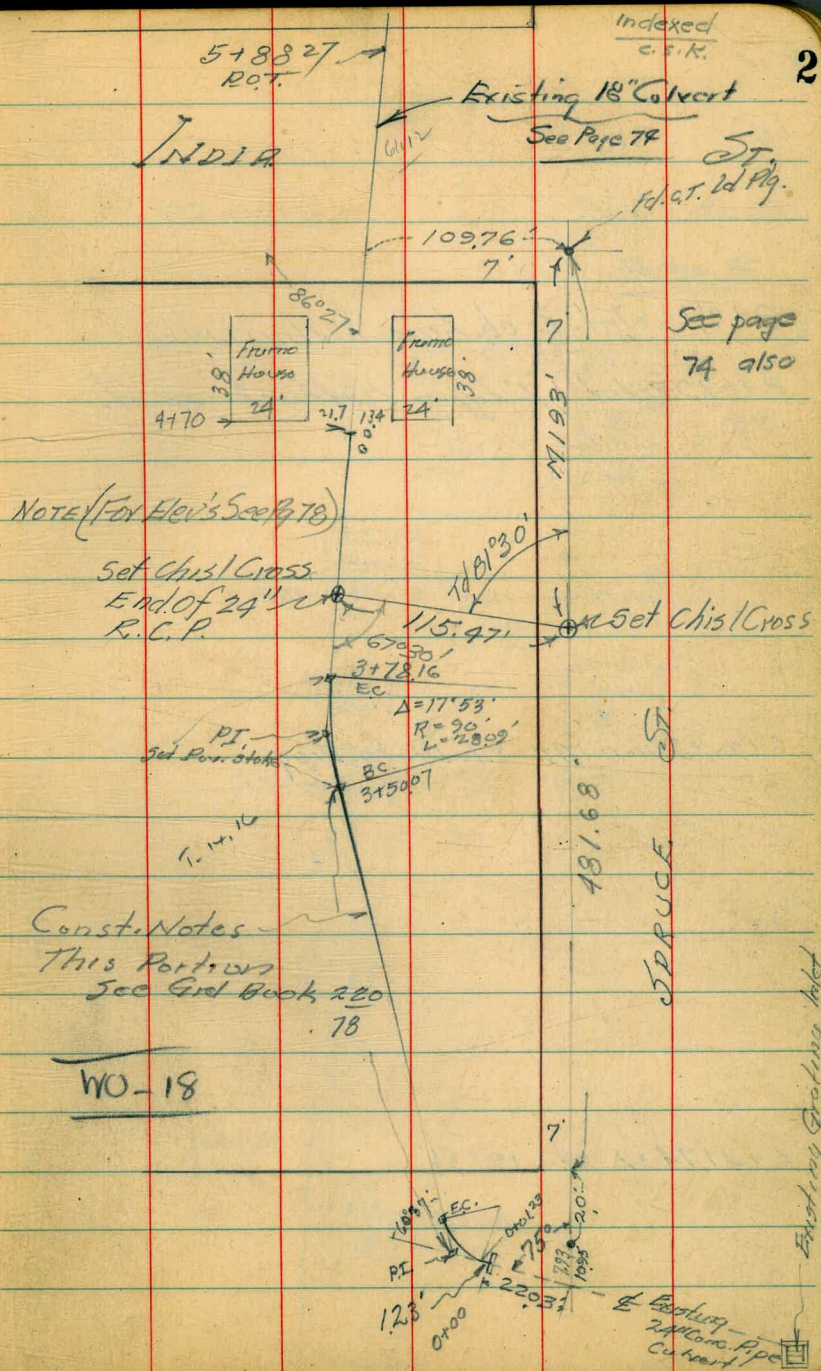
2+95 = 16" Tree 15' RT

0+17.09 = E.C.

$\Delta = 60^{\circ}37'$ RT
 $L = 15.86'$
 $T = 8.77'$

0+01.23 B.C. 15' Radius

0+00 = End Existing 24" Conc. Pipe = outside edge Conc. Hd. Wall



8+07.16 = Int. E. cb. Line Kettner Blvd.

8+01.95 = Int 7' Line Kettner Blvd.

6+90 = Sewer MH 8.7' Lt on Diag.

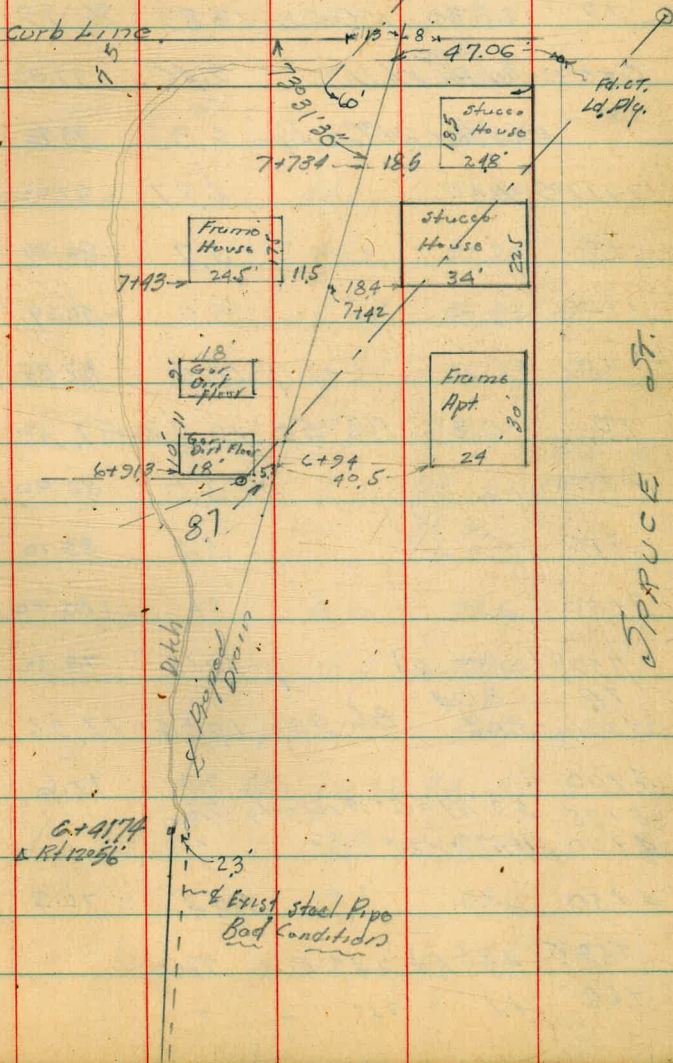
6+41.74 = Δ Bx 12° 56'

KETNER

BLVD.

See Page 75

curb line



Walker
Hordin
Hurler
2-23-46

LEVELS - PROPOSED DRAIN
as per location P. 2. 3

	130.3	99.05	86.00	BM SEBP - spruce INDIA
TP	10.96	109.82	0.19	98.86
TP	3.30	100.29	12.83	96.99
0+00	Corr.	on Hd. Wall	2.46	97.83
" "		on Flow 24" Conc. Pipe	6.33	93.96
0+17.09	F.C.		2.87	97.92
+50			5.7	94.59
1+00			9.0	91.29
+50			12.4	87.89
TP	0.93	88.50	12.72	87.57
2+00			3.1	85.40
+50			5.4	83.10
3+00			8.1	80.90
+50	07	BC. RT	10.18	78.32
TP	8.94			
3+78.16	E.C.	86.90	10.54	77.96
4+00			9.3	77.6
3+95	5.3' RT	= 6" Avocado Tree		
4+00	11.5' "	= 8" " "		
4+50			10.4	76.5
7585	4.5' RT	24" Euc. Tree		
766	4.1' "	24" " "		

86.90

4

4+65.71	on Flow 12" Drain	13.69	73.21	
+70		11.6	75.3	
+87		9.2	77.7	
TP	5.49	92.39	0.00	86.90
5+04		4.6	87.8	
+5		3.6	88.8	
5+26	on Top of E. cb Indica	3.71	88.68	
"	on Excit.	4.46	87.93	
5+51.5	E Indica	4.69	87.70	
+77	W. Excit	6.07	86.32	
"	on cb.	5.81	86.58	
+90	on Fill Ground x Corrected	5.7	86.7	
TP	1.56	87.56	6.36	86.03
5+28			86.00	0.03
5+98	Fill Ground	8.0	79.6	
6+02	" "	10.4	77.2	
+06	" "	11.1	76.5	
TP	110	75.67	12.99	74.57
6+11	Fill Ground	2.7	73.9	
+18	" "	7.1	68.6	
+29	" "	10.1	65.6	

65.71 ✓

	7567			
6+32		11.7	69.0	
TR	0.42	65.71	10.45	65.23
6+41.74-2 Rt	12° 56'	3.7	62.0	on Por. Stake Pipe No
2.3 Rt on Floor	1.3 steel Pipe	4.37	61.34	Good
6+60 in Ditch		6.3	59.4	
762		4.3	61.4	
6+90		7.4	58.3	
87' Lt. on Dig	on Rim = 2' MH	7.08	58.63	
" on Floor		11.56	54.15	
7+00		7.8	57.9	
(7+10) 35' Rt. on Floor	Porch Appt.	7.32	58.39	
7+50		8.8	56.9	
785		9.8	56.9	
8+07.16	1st Ecb line Kettner	11.42	54.29	in Drive No cb. there

Notes Reduced. 2.26.76

This line may be (if desired) extended to
 5' East of West cb Kettner thence north on Kettner
 Parallel to W cb to 5' N of S cb Sassafras st
 thence West on Sassafras Parallel to S cb
 to Existing Culvert at Sassafras st and
 SANTA FE TRACKS

TR 1103 76.37 ✓ 0.37 65.34

TR 12.84 87.83 ✓ 1.38 74.99

chk starting 1.84 85.99 ✓

86.00
0.01

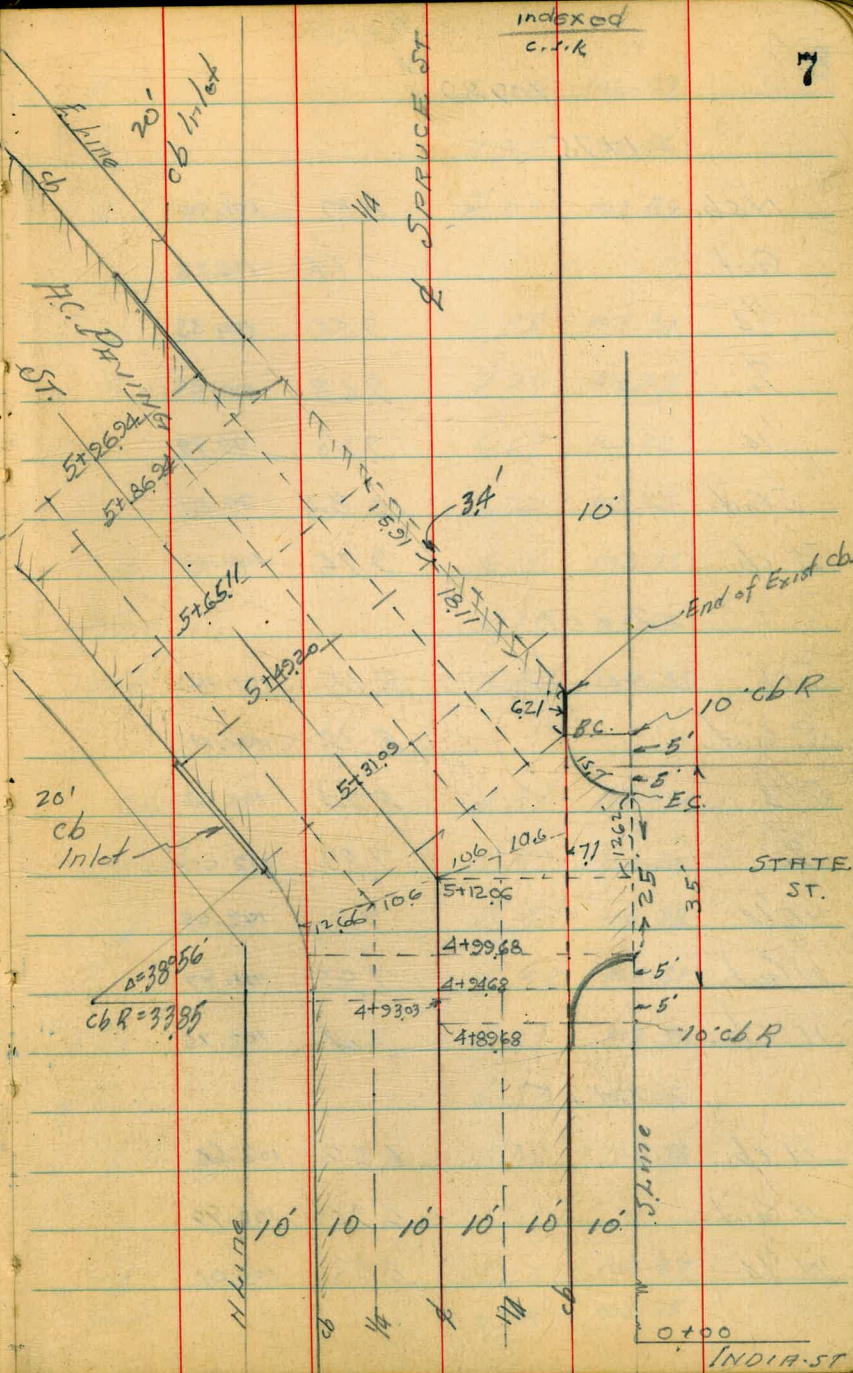
Walker
Harden
Hunloy
899
2-28-46

CROSS SECTION - INTERSECTION
SPRUCE AND IBIS ST.

INDEXED
C.P.K.

7

	12.48	98.48	86.00	India
TP	11.76	109.89	0.35	98.13
	1+50	= 150' E.E. Line India		
5' cb.		11.76	98.13	
cut.		12.26	97.53	
1/4		11.89	98.00	
1/2		11.58	98.31	
11/16		11.55	98.32	
cut.		11.72	98.17	
cb.		10.97	98.92	



	109.89		
	1+75		
N cb.	8.89	101.00	
Gut.	9.66	100.23	
1/4	9.56	100.33	
1/2	9.63	100.26	
1/4	9.90	99.99	
S Gut.	10.38	99.51	
S cb.	9.76	100.13	
	2+00		
S cb.	8.15	101.78	
S. Gut.	8.78	101.11	
S 1/4	8.24	101.65	
1/2	7.89	102.00	
N 1/4	7.80	102.09	
N Gut.	7.92	101.97	
N cb.	7.14	102.75	
	2+25		
N cb.	6.23	103.66	
N Gut.	6.90	102.99	
N 1/4	6.88	103.01	

1/2	7.00	102.89	
S 1/4	7.33	102.56	
S Gut. in Drive	8.00	101.89	
	2+50		
S cb.	6.58	103.31	
S. Gut.	7.20	102.69	
S 1/4	6.67	103.22	
1/2	6.24	103.65	
N 1/4	6.16	103.73	
N Gut.	6.25	103.68	
N cb.	5.54	104.35	
	2+75		
N cb.	4.87	105.02	
N Gut.	5.59	104.36	
N 1/4	5.51	104.38	
1/2	5.58	104.31	
S 1/4	5.99	103.90	
S Gut.	6.53	103.36	
S cb.	5.91	103.98	
	3+00		
S cb.	5.62	104.27	
" Gut.	6.24	103.65	

	3+00	109.89		
S 1/4			5.66	109.23
Lo			5.26	109.63
N 1/4			5.16	109.73
N Gut.			5.28	109.61
N cb.			4.56	105.33

	3+25			
N cb.			4.25	105.64
" Gut.			5.00	109.89
" 1/4			4.92	109.97
Lo			5.06	109.83
S 1/4			5.50	109.39
S Gut.			6.01	103.88
S cb.			5.38	109.51

	3+50			
S cb.			5.13	109.76
Gut.			5.84	109.05
1/4			5.18	109.71
Lo			4.72	105.17
N 1/4			4.60	105.29
N Gut.			4.73	105.16
N cb.			3.96	105.93

	3+75			
		109.89		
N cb.			3.63	106.26
Gut.			4.40	105.99
1/4			4.40	105.99
Lo			4.53	105.36
1/4			4.99	109.90
Stent.			5.62	109.27
S cb.			4.98	109.91
on Walk			5.02	109.87

	4+00			
S cb.			4.70	105.19
S Gut.			5.32	109.57
S 1/4			4.71	105.18
Lo			4.26	105.63
N 1/4			4.15	105.74
N Gut. in Drive			4.15	105.74

	4+25			
N cb.			3.17	106.72
Gut.			3.86	106.03
1/4			3.85	106.04
Lo			4.02	105.87

	4+25	10989		
S 1/4			4.17	105.92
S Gut.			5.09	104.80
S cb			4.43	105.96
	4+50			
S cb.			4.27	105.62
S Gut.			4.89	105.00
S 1/4			4.27	105.62
2			3.80	106.09
N 1/4			3.62	106.27
N Gut.			3.61	106.28
N cb.			2.91	106.98
	4+75			
N cb.			2.58	107.31
" Gut.			3.26	106.63
N 1/4			3.40	106.99
2			3.80	106.09
S 1/4			4.30	105.59
S Gut.			5.01	104.88
S cb.			4.24	105.65
T.R.	816	114.13	3.92	105.97

S.F. Tack
2d
Starter & Spruce

	114.13			
	4+84.25			end cb Inlet on South
Top cb			8.30	105.83
Gut			9.21	104.92
	4+89.68			-BC cb Ret on South
cb			8.22	105.91
Gut.			9.22	104.91
S 1/4			8.36	105.77
2			7.85	106.28
	4+93.03			
2			7.78	106.35
N 1/4			7.48	106.65
N Gut. in Drive			7.37	106.76
	4+99.68			
N on cb Ret			6.49	107.64
" " Gut. cd Ret			7.32	106.81
N 1/4			7.38	106.75
2			7.60	106.53
S 1/4			8.16	105.97
S cb.			8.96	105.17
ce T10 on Gut.			9.24	104.89
" " cb.			8.24	105.89

114.13

S.W. Rot

2 Rot on cb.	8.15	105.98
2 " on Grating.	9.18	107.95
2.3 N.E. " End "	9.06	105.07

5+12.06 section R/A to Back Tern

2	7.38	106.75
S'14	7.86	106.27
S Gut.	8.32	105.81
S Line on Poring	8.28	105.85

12.62 E. of Above section on South
= E cb line starts

S.L. Spruce on cb = End Rot = E.C.	7.38	106.75
" Gut.	8.00	106.13
10' N on Gut. line spruce	8.04	106.09
2 S.E. Rot on cb.	7.29	106.89
" " " " Gut	7.86	106.27
B.C. S.E. Rot. on cb.	7.32	106.81
" " " " Gut.	7.85	106.28
End of Exist cb. = 6.21' East of B.C.		107.92
on cb.	6.59	107.59
" Gut.	7.29	106.89

114.13

5+12.06 = (Bisector
Section) 11

N cb.	6.42	107.71
Gut.	7.30	106.83
'14	7.26	106.87
2	7.38	106.75
S'14	7.73	106.90
cb.	8.12	106.01

5+31.09

E-34' = E edge Por.	6.97	107.16
E on Por.	7.20	106.93
cb.	6.89	107.29
E'14	6.87	107.26
2	6.88	107.25
W'14	6.93	107.20
+8 on Grating E East edge	7.15	106.98
W Gut. on "	7.19	106.99
" on cb.	6.23	107.90
1.5' South = Sand Inlet.		
18.5' N on ^{North} end Inlet. Gut	6.88	107.25
" " " cb	5.91	108.22
5+49.20		
W Top cb.	5.94	108.19
Gut. inlet	6.97	107.16

W 1/4	6.63	107.50
Q	6.51	107.62
E 1/4	6.47	107.66
E cb.	6.45	107.68
E Line	6.27	107.86
+ 2' = Edge Par.	6.18	107.95
5+6511		
E - 1.0' on Edge Par	5.89	108.29
E cb.	6.15	107.98
1/4	6.16	107.97
Q	6.20	107.93
W 1/4	6.33	107.80
W Gut	6.50	107.63
W cb.	5.73	108.40
5+8624		
W cb. in Drive		
Gut	6.10	108.03
1/4	5.90	108.23
Q	5.78	108.35
E 1/4	5.86	108.27
E cb. Gut	5.96	108.17
E Line "	5.92	108.21
on cb Rot.	5.18	108.95

5+9624

E Top cb. Grating.	5.15	108.98
Gut. on Inlet	6.15	107.98
+ 2' " Grating.	6.06	108.07
E 1/4	5.73	108.40
Q	5.57	108.56
W 1/4	5.72	108.41
W Gut.	5.23	108.20
W cb.	5.29	108.89
6+1624 = N end Inlet on E.		
W cb.	4.89	109.22
Gut.	5.59	108.59
1/4	5.25	108.88
Q	5.14	108.99
E 1/4	5.38	108.75
E Gut.	5.78	108.35
E Top cb	4.83	109.30
6+50		
E Top cb	4.56	109.57
" Gut	5.18	108.95
1/4	4.74	109.39

	6+50	11413		
Lo			4.56	109.57
W 1/4			4.70	109.83
W Gut.			5.05	109.08
" cb.			4.42	109.71
	6+75			
W cb.			4.05	110.08
" Gut.			4.72	109.91
" 1/4			4.35	109.78
Lo			4.17	109.96
1/4			4.32	109.81
E Gut.			4.69	109.89
" cb.			4.18	109.95
	7+00			
E cb.			3.67	110.96
" Gut.			4.24	109.89
1/4			3.86	110.27
Lo			3.72	110.91
W 1/4			3.87	110.26
W Gut.			4.15	109.98
" cb.			3.49	110.69

		11413		13
	7+25			
W cb.			3.02	111.11
Gut.			3.71	110.92
W 1/4			3.44	110.69
Lo			3.36	110.77
1/4			3.49	110.64
Gut.			3.86	110.27
E cb.			3.27	110.86
	7+50			
E cb.			2.69	111.49
E Gut.			3.27	110.86
1/4			2.88	111.25
Lo			2.67	111.96
W 1/4			2.74	111.39
Gut.			3.10	111.03
cb.			2.37	111.76
	7+75			
Gut. in Drive			2.38	111.75
1/4			1.97	112.16
Lo			1.85	112.28
1/4			2.01	112.12

	114.13	Spruce & 16is	
F. Gut.	2.30	111.83	
E. cb.	1.64	112.49	
chk E. Hd Wall	16.31	97.82 ✓	
0+00 Page 4		97.83	
		0.01	

Additional Sections Spruce & 16is

16is			B.M. SETack
to Spruce	6.14	112.11 ✓	P-10
		105.97	
0+00 = W.L. State			

Sh. Spruce	6.1	106.0
+2	6.3	105.8
+18	12.8	99.3
+41	15.5	96.6
+64	5.8	106.3

0+20

-62	5.4	106.7
41	12.8	99.3
-34	13.9	98.21
-24	4.8	107.31
-7	4.2	107.9
Sh. Spruce	6.2	105.9

0+35 = E.L. State

Sh.	5.1	107.0
-----	-----	-------

	0+35	112.11		14
10' S SL.			5.1	107.0
31' S			12.8	99.3
35' S			12.8	99.3
50' S			5.7	100.9

0+60

40' S			5.7	106.9
35' S			7.0	105.1
25' S			8.3	103.8
12' S			10.7	101.9
SL.			2.9	109.2

0+80

-30			3.5	108.6
-10			2.2	102.9
SL.			2.5	102.6
+9			2.5	102.6
+40			2.3	109.8

TP 3.63 113.62 ✓ 2.12 109.99

1+07

51' H.			4.8	108.8
41' H.			10.7	102.9
Sh			10.5	103.1
Sh			9.4	109.2

1407 11362 ✓

5L +15	9.1	109.5
+25	8.5	105.6
+35	3.1	110.5
+40	2.0	111.6

1420

-25	2.0	111.6
+2'	7.5	106.1
5L	7.5	106.1
10' N	8.6	105.0
35' N	10.8	102.8
42' N	4.6	109.0
60' N = NL.	4.4	109.2

1437

J.L.	3.9	109.7
10' N	5.0	108.6
20' N	8.1	105.5
32' N	4.2	109.9

1447

20'	3.3	110.3
5	3.5	110.1
10' N	3.7	109.9
20' N	3.8	109.8

Notes reduced. 8-2-86

11362

15

clk standing BMI	7.64	105.98 ✓
		105.97
		0.01

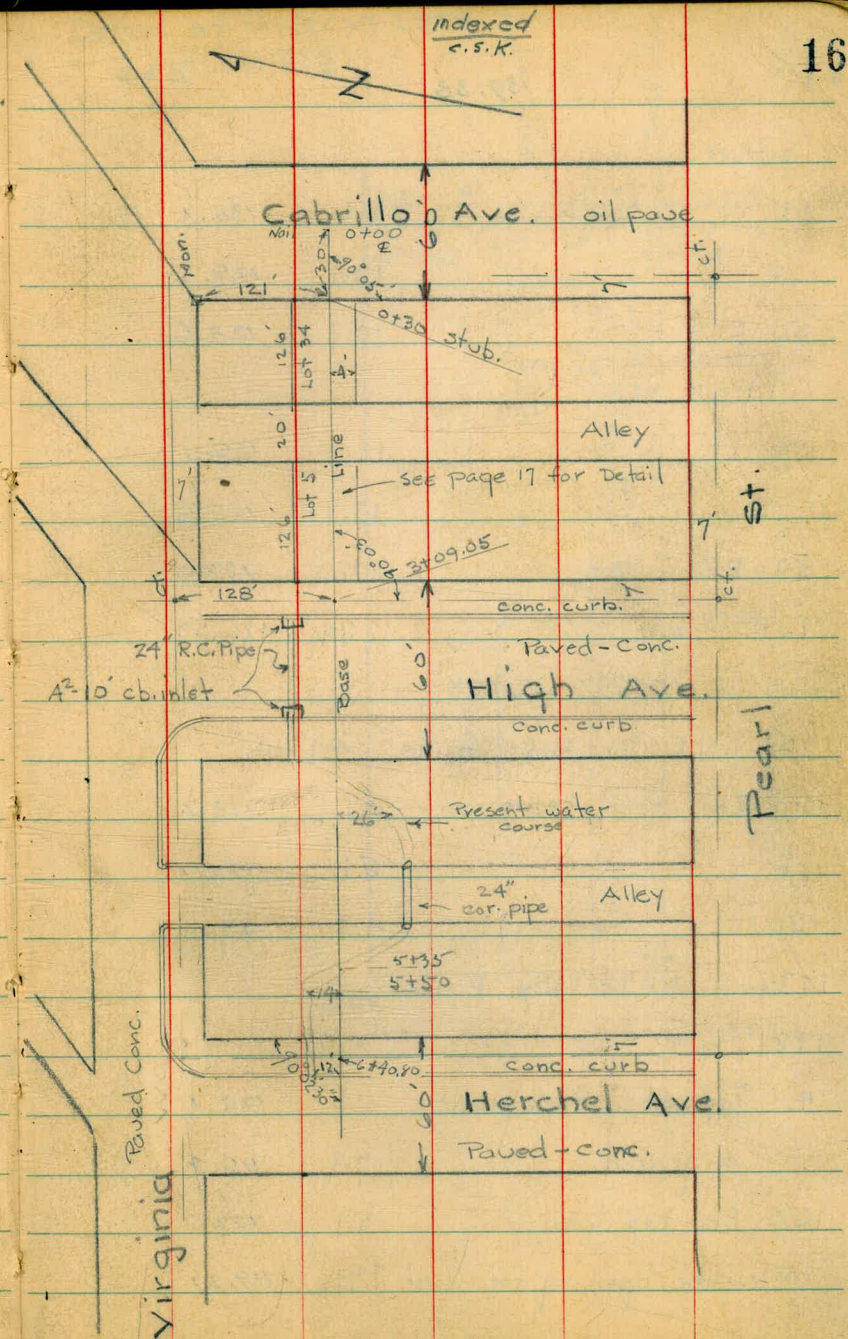
Survey for Ext. of Drain
100' S. of Virginia way - Cabrillo to Herschel.

Osborne
Crawencamp
Harden
3-15-46

Blks. 2 & 3, Center Addition

S.E. BR Pearl				
P.M. + Girard	3.18	118.35		115.17
T.P. on cb.	11.03	119.38	10.00	108.35
	12.12	130.91	0.59	118.79
	9.57	139.33	1.15	129.76
0+00 = Φ Cabrillo Ave.	4.0			135.3
50 Lt.		3.5		135.8
50 Rt.		3.9		135.2
0+20 = W. cb. Cabrillo (no curbs)				
Φ		4.5		139.8
27 Rt. = Natural water course	5.0			139.3
50 Rt.		4.7		138.6
50 Lt.		4.1		135.2
0+30 = W.L. Cabrillo Ave.				
50 Lt.		3.9		135.2
Φ on stub.		6.92		132.21
50 Rt.		4.8		132.5

Note: No definite water course thru lot 34

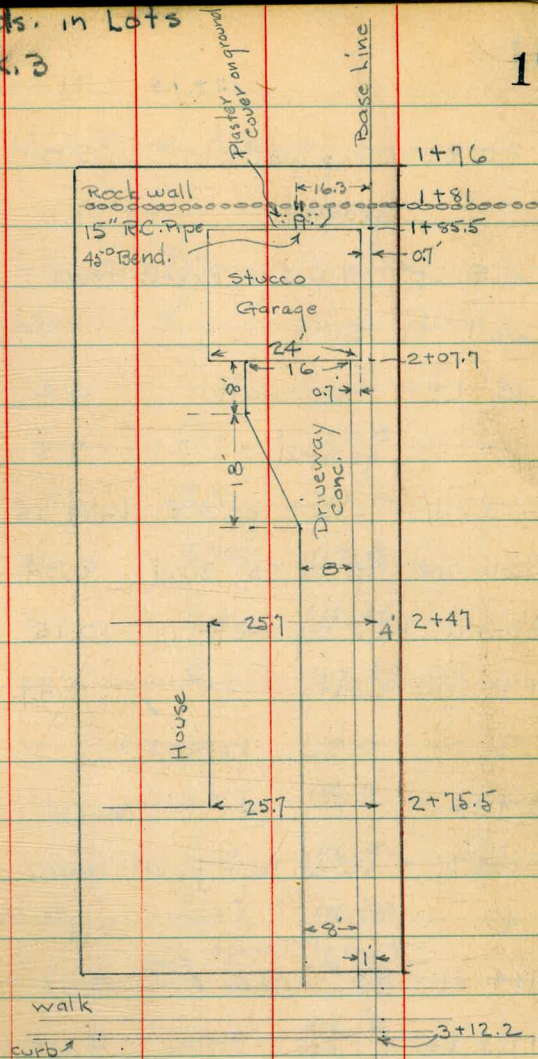


139.33

0+60			
48' Rt. = S. side House	8.6	130.7	
⊕	10.1	129.2	
50 Lt.	10.7	128.6	
1+00			
50 Lt.	13.3	126.0	
⊕	13.7	125.6	
50 Rt.	12.3	127.0	
T.P.	12.74	126.59	
0.59	127.18		
1+51 = N.E. Cor. Picket fence	4.9	Lt.	
50 Rt.	4.1	123.1	
⊕	5.1	122.1	
50	4.2	123.0	
1+75	3.1	Lt. = Nly P. pole	
1+81			
⊕ Top of 6" Rock wall	5.1	122.1	
on ground	7.3	119.9	
16.3 Rt. top wall	5.1	122.1	
Flowline opening for Culvert	7.91	119.27	

Detail of Blots. in Lots # 4+5 - BIK.3

17




127.18

30 Rt.	Top wall	5.0	122.2
	ground	7.0	120.2
4.8 Lt.	= NW. Cor. Pickett fence.		Begin 14" Rock wall to S.

15' Lt.	top wall	4.4	122.8
	ground	7.5	119.7

1+83.1	16.3 Rt. = E Inlet 15" R.C. Culvert		
--------	-------------------------------------	--	--

Flow line = lip of 45° bend	8.34	118.88	
-----------------------------	------	--------	---

Approx. f.l. Reg. sect.	10.15	117.03	
-------------------------	-------	--------	--

I.P. ^{Top} Bolt. in wall	4.49	122.69	
-----------------------------------	------	--------	--

0.32 123.01

2+04	1' Lt. = 4" 12" acacia		
------	------------------------	--	--

2+05.7	3.6' Lt. Begin picket fence		
--------	-----------------------------	--	--

4		3.9	119.1
---	--	-----	-------

1.4 Rt. = ^{Floor of Garage} edge of Drive + ^{conc.}	4.01	119.0	
---	------	-------	--

17.4 Rt. N. Edge of drive	4.09	118.92	
---------------------------	------	--------	--

20 Rt.		4.7	118.3
--------	--	-----	-------

35 R.		4.0	119.0
-------	--	-----	-------

10 Lt.		4.0	119.0
--------	--	-----	-------

123.01

2+15.5	1' Lt. = E 6" Acacia		
--------	----------------------	--	--

2+22	= .6 " " " "		
------	--------------	--	--

2+33	1.1 Lt. " 8" "		
------	----------------	--	--

2+37	1.6 Lt. " 4" "		
------	----------------	--	--

2+40			
------	--	--	--

10 Lt		5.2	117.8
-------	--	-----	-------

E		5.4	117.6
---	--	-----	-------

.7' Rt. S. edge dr.		5.20	117.81
---------------------	--	------	--------

8.7 Rt. N. " "		5.16	117.85
----------------	--	------	--------

30 Rt.		5.7	117.3
--------	--	-----	-------

2+80			
------	--	--	--

10 Lt		6.6	116.9
-------	--	-----	-------

E 1		6.6	116.9
-----	--	-----	-------

1' Rt. S. edge dr.		6.67	116.39
--------------------	--	------	--------

9' Rt. N. " "		6.71	116.30
---------------	--	------	--------

25 Rt		6.6	116.9
-------	--	-----	-------

2+83.5	3' Lt. = end picket fence		
--------	---------------------------	--	--

3+12.2 = E. eb. High.			
-----------------------	--	--	--

E Top. eb.		7.52	115.89
------------	--	------	--------

gut.		8.10	114.91
------	--	------	--------

18

3+12.2 (cont.)

20 Lt. topcb. 7.48 115.53

" gut. 8.04 118.97

21.5 Rt = Φ 3.5 x 2 box + Φ 24" RC pipe

Top cb. 7.44 115.57

on grating 8.44 118.57

Flowline 11.82 111.19

3+32.2 = Φ High 8.24 119.77

3+52.2 = W.cb. High

 Φ topcb. 8.63 119.38

gut. 9.18 113.83

20 Lt. top. 8.50 118.51

gut. 8.95 114.06

21.5 Rt. Φ box-Topcb. 8.45 118.56

grating 9.45 113.56

12.98 110.93

3+62.2 = W.line High

 Φ 8.6 119.9

16. Rt. 8.6 114.4

21.5 Rt. = F.L. end 24" ^{Pipe} 13.24 109.77

25 Rt. 7.7 115.3

25 Lt. 8.7 114.3

T.P. 11.58 111.43

2.58 114.01

3+88

 Φ = water 3.1 110.9

13. Rt. 1.3 112.7

19 Rt. + 1.4 115.9

20 Lt. 4.2 109.8

4+40

 Φ 4.1 109.9

15 Rt. 2.1 111.9

26 Lt. 5.5 108.5

50 Lt. 4.8 109.2

4+85

 Φ 5.7 108.327 Lt. = F.L. 24" Cor. ^{Pipe E.end.} 7.13 106.9

34 Lt. 4.0 110.0

15 Rt. 4.4 109.6

4+88 Φ 4.6 109.95+00 Φ 5.1 108.9

5+03

114.01

E	6.8	107.2
11.5 Lt = ♀ Tel. pole		
13' Lt. = " P. "	7.4	106.6
26 Lt. = F.L. w. end. ^{24" cor. pipe}	7.85	106.16
40 Lt.	6.3	107.7
20 Rt.	5.7	108.3

5+25

E in ditch	9.0	105.0
30 Lt	7.5	106.5
50 Lt	6.6	107.9
25 Rt.		

5+50

E	8.8	105.2
14 Rt. in ditch	9.4	109.6
30 Rt.	9.3	109.7
30 Lt.	7.5	106.5

5+54 - 21' Rt. begin board fence

5+76 End. fence beg. old frame garage

5+92 End. gar. 22' Rt.

Note: Ditch is 1' wide with small bank along fence + gar.

20

114.01

6+00

♀	8.7	105.3
12 Rt. in ditch	9.5	109.5
20 Rt.	9.0	105.0
30 Lt.	7.5	106.5
6+43.5 = E. cb. Herchel		

♀ top cb. 8.71 105.30

gut. 9.30 109.71

12' Rt. = End of ditch. which is tunneled under sidewalk and goes N. along back of curb for 12' and out thru a driveway

Top cb (in Rt.) 9.03 109.98

bottom of ditch 10.1 103.9

gut 9.61 109.90

24 Rt. gut. in driveway 9.94 109.07

41 Rt. top 9.87 109.19

gut. 10.41 103.60

30 Lt. top cb. 7.82 106.19

gut. 8.40 105.61

114.01

6+63.5 = E Herchel

E 9.29 108.73

40 Rt. 10.47 103.59

30 Lt. 8.48 105.53

Gutter at S. eb. line Virginia way and
w. line of alley opp. sta. 5+08 E. 108.67

Too high. - Nearest inlet is on w. side of
interc. of Virginia Way + Girard.

T.P. 5.67 108.34 ✓

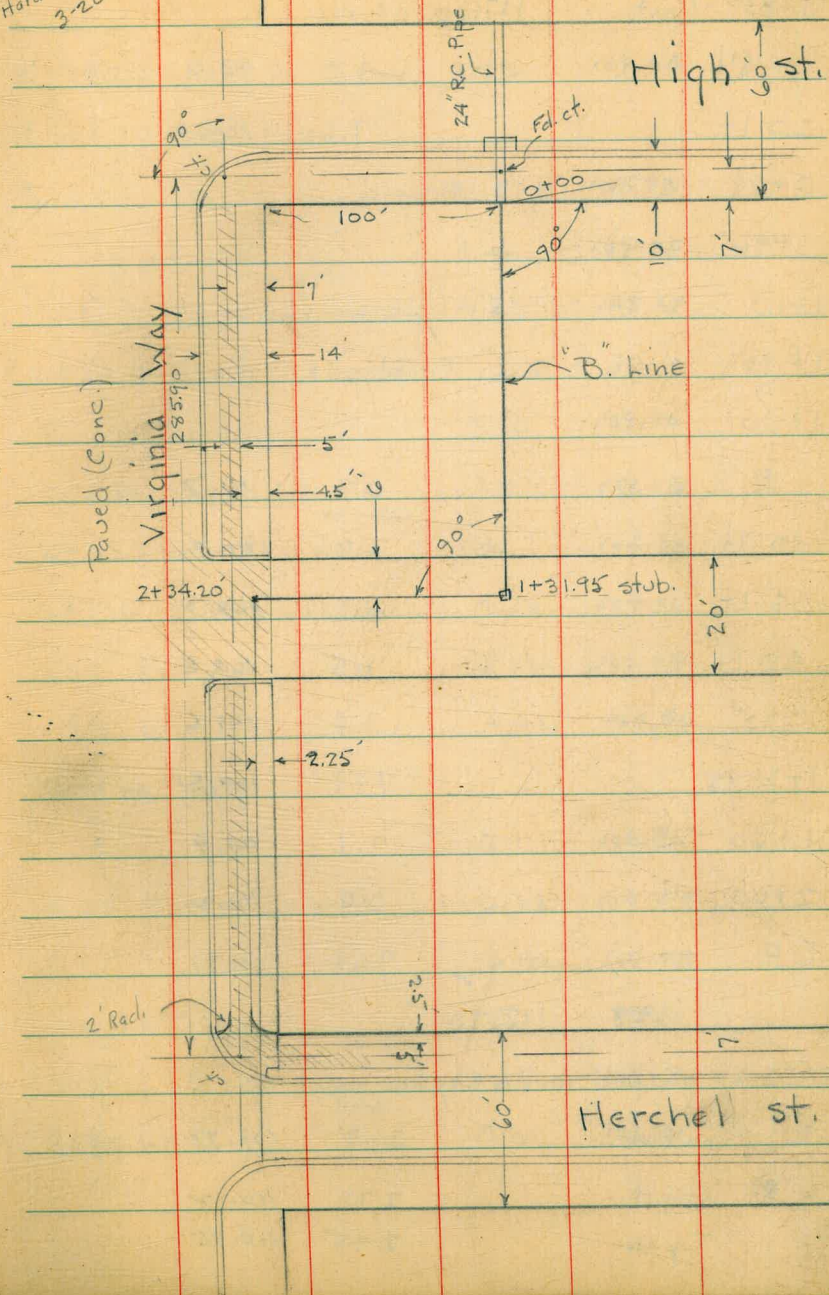
10.10 118.44 3.28 115.16 check B.M. ✓

Survey of "B" Line for Drain High to Herchel

B.M.	8.65	117.00	T.P. inch.
		RC. Pipe	P. 16
0+00 = W. Line High on outlet of 24"		109.77	EL. of F.L.
0+15			
☉		1.4	115.6
7' Lt.		5.9	111.1
10' Rt.		1.0	116.0
0+46 - 2.6' Rt. = 6" Pepper			
0+50			
☉		2.1	114.9
10 Rt.		2.0	115.0
4' Lt.		2.1	114.9
17' Lt.		6.3	110.7
0+58 - 2' Rt. = 6" Acacia			
0+64 - 2' Rt. = 4" "			
0+72 - 2' Rt. = 3" "			
0+80 - 2' Rt. = 4" "			
0+85			
☉		4.7	112.3

Osborne
Gravencamp,
Harden
3-20-46

22



0+85 - Cont.	117.00		
10 Rt.	4.0	113.0	
20 Lt.	7.1	109.9	
0+88 = 2' Rt. = E 3" Acacia			
+96 2' Rt. = " 6" "			
1+10 2' Rt. = " 5" "			
1+18 2' Rt. = E 2" Eucalyptus			
1+20			
E	5.3	111.7	
10 Rt.	5.3	111.7	
4 Lt.	7.3	109.7	
20 Lt.	8.5	108.5	
1+25	7.4	109.6	
1+31.95	7.49	109.51	on stub.
1+60	7.1	109.9	
2+00	6.8	110.2	
T.P.	7.68	109.32	
	3.58	112.90	
2+32.20 = Edge of Pavement in Alley			
E on conc.	3.19	109.71	
6' Rt. in gut.	2.78	110.12	
" Top cb.	2.45	110.95	

	112.90		
2+34.20 = Angle Pt. on conc.	3.22	109.68	
2+48.20 = W.L. Alley			
E gut.	3.17	109.73	
Top cb.	3.61	109.29	
11.75 Rt. = S. cb. Line Virg. Way	4.23	108.67	
2+54.3 = E. side of 7' drive			
E on conc.	3.80	109.10	
2.25 Rt. = S. edge Sidewalk on conc.	3.87	109.03	
2+61.3 = W. side of drive	4.17	108.73	
2+77.6 = E. of 3' walk conc.	4.95	107.85	
2.25 Rt on walk	5.12	107.78	
9.5 Lt. " "	4.41	108.89	
3+00			
E	6.1	106.80	
2.25 Rt S. on walk	6.38	106.52	
7.25 " N. " "	6.42	106.88	
10 Lt.	5.8	107.1	
3+32.9 = E. side 3' Conc. walk conc.	8.18	109.72	
3+50.6 = E. " 7' Drive	9.09	103.81	

		112.90	
3+57.6 = W. side 7 Drive			
Φ on conc.	9.29	103.61	
2.25 Rt. on walk s.	9.50	103.90	
7.25 Rt. " " N.	9.54	103.36	
10' Lt. on conc.	8.61	104.29	
3+74.6 = Edge of Ret.			
Φ	10.30	102.60	
2.25 Lt. = Cor. Ret.	10.32	102.58	
11.75 Rt. = Top cb. = P.C. Ret.	10.45	102.95	
gut.	10.95	101.95	
Φ of 10' Rad. Ret.			
Top cb.	10.72	102.18	
gut.	11.42	101.88	
3+81.7 = W. side of walk			
Φ on conc.	10.70	102.20	
10 Lt. " "	10.60	102.30	
2.25 = s. edge ret. conc.	10.71	102.19	
3+84.2 = E. cb. Herchel			
Φ Top cb.	10.90	102.00	
gut.	11.45	101.85	

		112.90	✓
2.25 Lt. Top	10.96	101.98	
gut.	11.44	101.96	
10' Lt. Top	10.83	102.07	
gut	11.40	101.50	
4' Rt. = E. end of gutter going across street.			
in gut	11.58	101.32	
10 Rt. on conc.	11.43	101.47	
4+04.2 = Φ Herchel			
Φ conc.	11.95	100.95	
2.25 Lt.	11.84	101.06	
10' Lt.	11.56	101.38	
8.4 Rt. = Φ cross gut.	12.12	100.78	
12' Rt.	12.01	100.89	
4+24.2 = W. cb. Herchel			
Φ Top	12.08	100.82	
gut	12.65	100.25	
2.25 Lt. gut.	12.65	100.25	
25' Lt. in gut	11.85	101.05	
10.3 Rt. = Φ cross gut.	12.74	100.16	
14' Rt.	12.70	100.20	

112.90 ✓

25

E of 10' Rad. Ret. S.W. Cor.

Top cb.			12.25	100.65
gut			12.76	100.14
4 + 34.2 = W.L. Herchel				
11.75 Rt. = S.cb.	"	end. of Ret.		
Top cb.			12.45	100.95
gut.			13.01	99.89
4 + 84.2 - 11.75 Rt. in gut.			14.19	98.71
T.P.	9.21	110.00	12.11	100.79
check on B.M.			1.65	108.35 ✓

Notes Reduced. 3.22.86

X- Sect. Alley BK. 120 - Univ. Hts.

N. & S. Alley of "T" Alley - Kansas & Utah

EL Cajon + Howard 20' Alley

for sketch See B. 599 - P. 32

0+41 = 9.4 Rt. = End of hedge - beg. slat. fence

0+49 = 8' Rt. = Wly of P. pole

0+21 = Top of conc. curb around basement
vent. window

0+13

0+01 = Begin 2' Hedge on Rt. on Line

0+00 = N.L. Howard

0-14 = S. cb. Line Howard - Paved - AC.

✓ B.M

2.50 376.45

5.74

370.71 =

373.95

sw. B.P.
Kansas &
Howard,
sw. B.P.
Utah &
Howard

Osborne
Hardin
Cary
Aug-46

Lt.

Rt.

Indexed
C.S.K.

Rt.

26

372.23
4.22 = on conc.
12.1 outside edge

72.0 71.9 371.3
4.4 4.5 10.1
10 10

372.06
4.39 Top 10
371.63
4.82 gut 10
371.57
4.88 on pave
371.39
5.06 gut 10
371.67
4.5 Top 10

71.51
4.94 30 gutter
71.45 10
71.44
5.01 10
371.32
5.26 30 gutter
71.19

376.45

1+50 = 8' Rt. = Wly. P. pole

1+38

1+32 = 10.1 Rt. = Reg. Board fence

1+05

0+85 = Single garage on Lt+Rt. - Conc. floor + Apron

0+78 = 9.7 Rt. = end slat. fence

0+70 = Φ = Single Garage - Conc. slab on Lt. with Conc. Apron joining gar. on S.

0+55 = Φ Single garage on Lt. Conc. floor

	Lt.	Rt.		
	371.4	371.1	371.1	371.5
	5.0	5.3	5.3	4.9
	15	10		10
	371.3	371.4	371.3	371.0
	5.1	5.0	5.1	5.4
	20	10		10
	72.17	72.01	371.8	371.9
	4.29	4.44	4.6	4.5
	18.7	13.4	10	10
	floor	edge of Apron		
	72.12	371.05		
	4.33	4.4		
	18.5	14.4		
	floor	= edge Conc. Apron		
	372.05	371.76	72.0	371.8
	4.42	4.69	4.4	4.6
	18.9	14.9	10	10
	floor	= edge of Conc. Apron		
				71.5
				71.5
				4.9
				20
			376.45	

4.00 373.94 check B.M.

T.P. 4.61 377.94 2.77 373.33

1+95 = N.L. of E.+W. Alley

1+85 = ± E+W. Alley

1+75 = S.L. of E.+W. Alley - Paved - very rough
 Pantrix oil pave

Also - 9.9 Rt. = end of board fence

T.P. 5.01 376.10 5.36 371.09

1+68

lt. ± Rt

371.35
 $\begin{array}{r} 4.75 \\ 40 \end{array}$
 370.89
 $\begin{array}{r} 5.21 \\ 10 \end{array}$
 370.90
 $\begin{array}{r} 5.20 \\ 10 \end{array}$
 370.81
 $\begin{array}{r} 5.29 \\ 10 \end{array}$
 370.71
 $\begin{array}{r} 5.39 \\ 40 \end{array}$

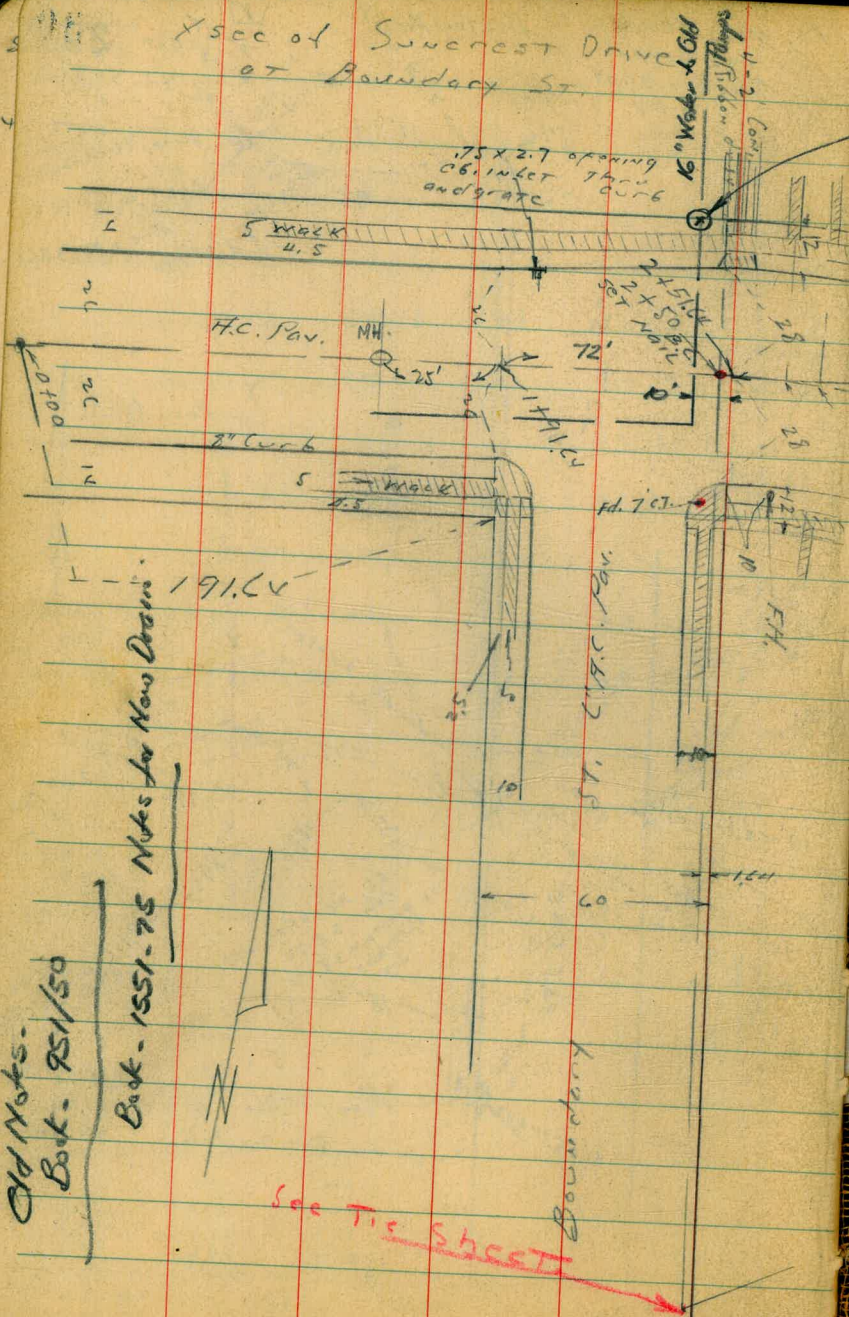
371.01
 $\begin{array}{r} 5.09 \\ 40 \end{array}$
 370.73
 $\begin{array}{r} 5.37 \\ 10 \end{array}$
 370.65
 $\begin{array}{r} 5.45 \\ 10 \end{array}$
 370.53
 $\begin{array}{r} 5.57 \\ 10 \end{array}$
 370.26
 $\begin{array}{r} 5.84 \\ 40 \end{array}$

371.10
 $\begin{array}{r} 5.00 \\ 40 \end{array}$
 370.90
 $\begin{array}{r} 5.20 \\ 10 \end{array}$
 370.86
 $\begin{array}{r} 5.24 \\ 10 \end{array}$
 370.82
 $\begin{array}{r} 5.28 \\ 10 \end{array}$
 370.71
 $\begin{array}{r} 5.39 \\ 40 \end{array}$

371.1
 $\begin{array}{r} 5.3 \\ 10 \end{array}$
 371.1
 $\begin{array}{r} 5.3 \\ 10 \end{array}$
 371.5
 $\begin{array}{r} 4.9 \\ 10 \end{array}$

376.45

X sec of Sincerest Drive
at Boundary St.



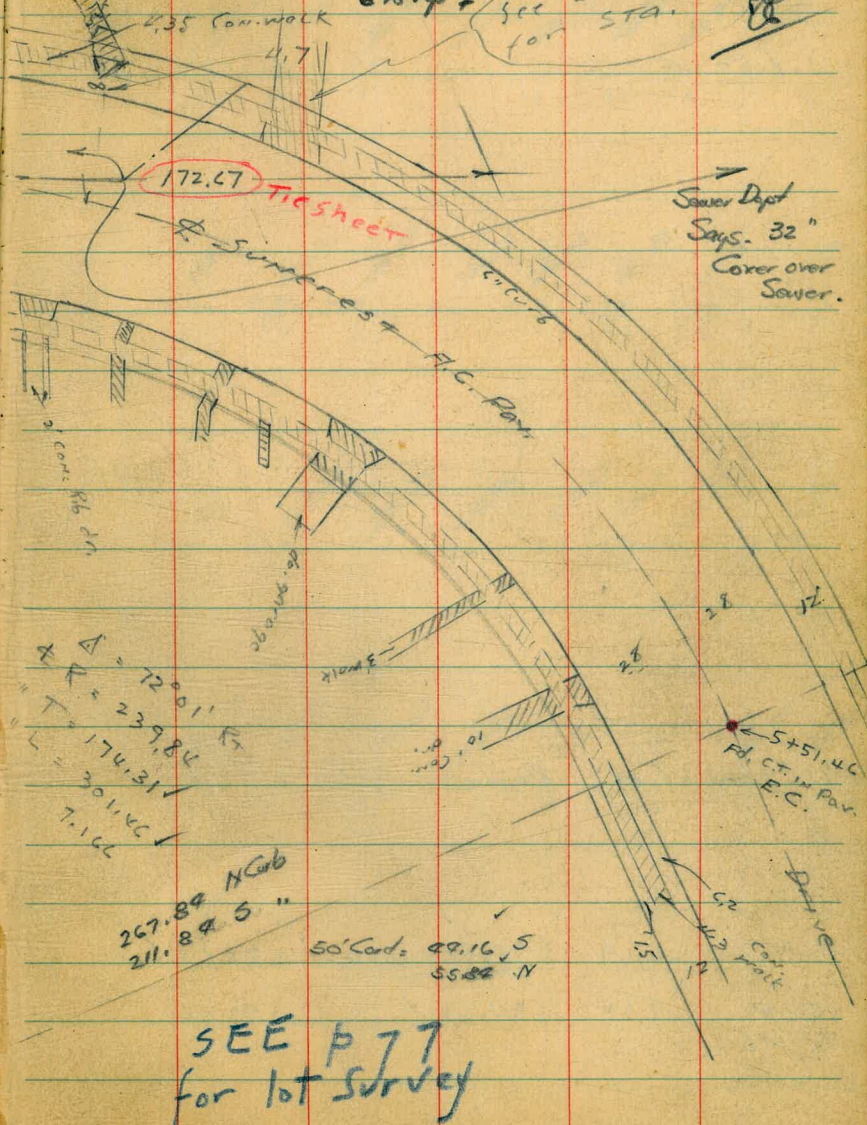
Old Notes.
Book - 95/50

Book - 1551-75 Notes for New Drain

C.M. work
Sincerest Drive
1999

Indexed
C.S.K.

5-8-46
Cooker Dist. Investigated. Says. 16" Valve & Valve Box on
Prop Line. Top of Valve Box. 4" Below ground level.
6" to top of Valve. Level
see STA.



1 sec on Suncrest Dr.
at Boundary St.

check up on Severns, Water + gas

1 x 50

/

0 + 50

191.4 w of walk Boundary St. = 0 + 00

T.P.	4.19	<u>390.81</u>	7.66	386.62 ✓
SEBP	3.72	394.28 ✓		390.96
Adams				
Boundary				

LT

R

R = 1/2 S.

31

386.11	385.84	385.33	385.89	386.19	386.11	385.79	386.70	386.78
4.70	4.97	5.48	4.82	4.62	4.70	5.02	4.41	4.03
	2c	2c	13		13	2c	2c	

386.29	385.91	385.31	386.04	386.25	386.22	385.83	386.88	386.76
4.52	4.90	5.50	4.77	4.50	4.59	4.98	4.33	4.05
	2c	2c	13		13	2c	2c	

386.89	386.11	385.61	386.29	386.95	386.37	386.01	386.59	386.86
4.32	4.70	5.20	4.57	4.36	4.44	4.80	4.22	3.95
	2c	2c	13		13	2c	2c	

386.51	386.20	385.68	386.33	386.55	386.97	386.15	386.77	386.88
4.30	4.61	5.13	4.68	4.26	4.34	4.66	4.09	3.93
M. edge	2c	2c	13		13	2c	2c	S edge
walk	66	97				97	66	walk

390.81 ✓

2 + 11.64 w 1/4 Bdry.

2 + 01.64

2 + 01.64 w c6 Bdry.

1 + 91.64 = wL Boundary

1 + 75

390.81

386.39	386.01	385.39	385.65	385.74	385.67	385.81	386.24	386.58
4.42	4.80	5.47	5.16	5.07	5.14	5.00	4.57	4.23
35.2	c6	9T	14		1/4	26 Par.	40	80

386.79	386.94
4.52	3.87
80	80
9T	c6

386.08	385.94	384.87	385.35	385.49	385.59	385.66	386.77	386.36
4.73	4.87	5.90	5.26	5.32	5.27	5.15	5.04	4.45
35.9	26	26 IRON GRADE	13		13	26	40	46
							9T	c6

386.14	385.76	385.19	385.54	385.77	385.65	386.71	386.21	386.61
4.67	5.05	5.67	5.27	5.04	5.16	5.10	4.50	4.20
35.9	26	26	13		13	26	26	26
							P.P. ↑ 28	

386.13	385.79	385.27	385.89	386.15	386.19	386.68	386.33	386.61
4.68	5.02	5.59	4.92	4.66	4.62	5.13	4.48	4.20
	26	26	13		13	26	26	
N edge work	c6	9T				9T	c6	S edge work

390.81 ✓

RE

5x0/

421.71

2 + 51.64 = E.L. Bdry.

2 + 41.64

2 + 41.64 E.C. Bdry.

2 + 31.64 E 1/4 Bdry.

2 + 21.64 E Bdry.

390.81

L T E R

33

37	7'	14'	14'	14'	14'	28'
	386.84	386.31	386.63	386.77	386.67	386.06
397	4.50	4.18	4.04	4.14	4.76	4.21
N edge walk	9T	1/4		1/4	9T	6
E drive	20' side					385
						26 walk

386.54

4.27
80
9T

387.14

3.67
80
6

386.75	386.66	386.01	386.92	386.98	386.37	386.11	386.15	386.67
4.06	4.15	4.80	4.29	4.33	4.44	4.70	4.66	4.14
37.1	6	9T	1/4		1/4	6 Pav	40 9T	40 6

386.60

386.99

385.81

386.16

385.19

386.08

386.09

386.92

386.77

4.21	4.32	5.00	4.65	4.62	4.73	4.72	4.39	4.04
36.8	6	9T	1/4		1/4	6 Pav	40	80

386.99

386.26

385.54

385.89

385.98

386.00

386.01

386.65

386.63

4.37	4.55	5.27	4.92	4.83	4.81	4.79	4.16	4.18
36.4	6	9T	1/4		1/4	6 Pav	40	80
N edge walk								

390.81

L +

←

P +

34

2 + 99

Tel. Pole
30

2 + 95

20" di. Palm
30

2 + 70

7
80
/2' Con. walk
4014" di. Palm
31

2 + 70

2.5' Con. walk
40

2 + 68

3' Con. walk
20 - 40

2 + 57

10" di. Palm
31

L+

±

R+

3+42

4' Con. Walk
40

3+33

Tree
32

3+29

5' Con
Walk
40

3+18

10' Con.
dr.
28

dr. Rib dr.
39

3+04

12" dr. Palm
31

3+00

386.04	385.79	385.13	385.63	385.91	385.81	385.97	386.03	386.26
4.77	5.02	5.68	5.8	4.90	5.00	5.34	4.78	4.35
37.2	26	97	14		14	97	06	S. edge
WALK								WALK

390.81

390.81 ✓

3+98

3+86

3+62

3+58

3+51

3+50

39081

L+

E

R+

4.5 Con Walk
403" dr. Palm
37R.P.
31E 16.5
Hedge
40E 19'
Con
drive
28Small
Tree
32

385.76		389.93	384.85	385.20	385.17	389.83	385.57	385.87
5.55	—	4.38	5.96	5.61	5.64	5.98	5.29	4.94
37	26	77	11/4	1/4	1/4	77	26	S. edge
N. edge		Hedge						WALK
WALK		drive						

39081 ✓

36

4+75

4+52

4+50

4+32

4+14

4+12

4+00

390.81

L7

Z

R7

37

16" Accasia Tree

31

± 19' Con. drive

28-40

389.19	389.90	389.30	389.67	389.97	389.05	389.76	389.66
6.62	6.91	7.57	7.14	6.84	6.70	7.05	6.15
	06	97	1/4		1/4	97	06
						1/4	drive

3" PALM

32

2' Con. walk

38.5

3" PALM

32

389.31	389.91	389.81	389.25	389.51	389.50	389.21	389.92	389.42
6.50	6.40	7.00	6.50	6.30	6.31	6.60	5.89	5.38
370								
N. edge	06	97	1/4		1/4	97	06	S. edge
Walk								Walk

390.81 ✓

check back to orig. B.M. 376 390.96 390.96 ✓

T.P. 6.82 394.22 3.41 387.40

5+51.46 E.C.

5+42

5+25

5+15

5+00

4+98

390.81

Notes Reduced - 5-16-06

LT

E

FF

38

383.11	382.77	382.70	382.61	382.98	382.99	382.86	383.37
7.70	9.04	8.11	8.20	7.83	7.82	7.95	7.44
Walk	CG	9T	1/4	1/4	9T	CG	
	drive						

~~57.47~~

10' CON. DRIVE
28 - 40

~~45.45~~

12" di. ACACIA
32

3' CON. WALK
28

383.71	383.51	382.77	383.19	383.67	383.51	383.30	383.85	384.11
7.10	7.30	8.04	7.62	7.19	7.30	7.51	6.96	6.70
N. edge	CG	9T	1/4	1/4	9T	CG		S. edge
WALK								WALK

12" ACACIA TREE
32

390.81 ✓

csm Addl. Levels on Suncrest Dr.
 C.S.
 E.B. at Boundary St.
 5-17-66.

Lt. \$ Rt. 39

3+25

	385.66		385.51		389.70		385.21		385.93		385.52		385.20		385.71		386.20
	$\frac{6.01}{37}$		$\frac{6.16}{06}$		$\frac{6.97}{97}$		$\frac{6.46}{14}$		$\frac{6.24}{14}$		$\frac{6.15}{14}$		$\frac{6.47}{97}$		$\frac{5.95}{06}$		$\frac{5.47}{S. edge walk}$
	N. edge		Wack														

2+75

	386.62		386.38		385.74		386.20		386.29		386.29		385.13		386.91		386.69
	$\frac{5.05}{26.9}$		$\frac{5.29}{06}$		$\frac{5.93}{97}$		$\frac{5.47}{14}$		$\frac{5.38}{14}$		$\frac{5.94}{97}$		$\frac{5.26}{06}$		$\frac{4.98}{S. edge walk}$		
	N edge		Wack														

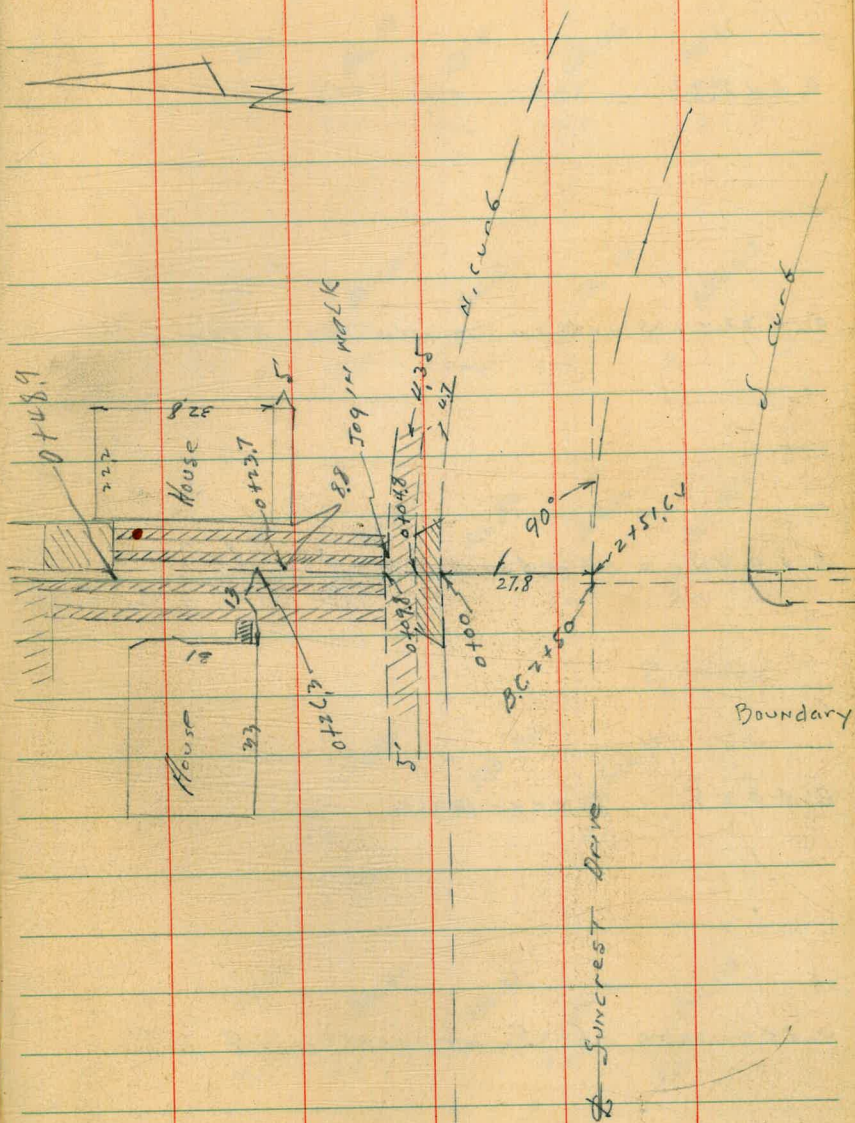
T.P. 3.70 391.67 0.70 387.97 ✓

391.67 ✓

SEBP BM 3.81 394.77 ✓ 390.96 ✓
 Adams
 + Bdry.

Location of 4" Ribbon Con. drive
at NE Cor of Suncrest Dr
& Boundary

See P 41 for Location
& Levels of 2" Ribbons



Levels on Ribbon Dr.

N.E. Cor. Sunset + Berry

0 + 48.9

0 + 33.4 Break in grade of Ribbons

0 + 09.8 = N. edge walk RT. & Lt. Ends are
on E of 2' Con. Ribbons

0 + 04.8 = S. edge walk

0 + 00 = N. cb Sunset Dr. = E Drive ^{ON}

391.67

LT

E
on Lawn

RT

386.54	386.58	386.9	386.26	386.23
5.13	5.09	5.3	5.41	5.34
7.15	2.25	LAWN	2.25	7

387.12	387.10	386.8	386.74	386.65
4.55	4.57	4.9	4.93	5.02
7.15	2.25	LAWN	2.25	7

386.77	386.8	386.84	386.90	386.86
4.90	4.85	4.83	4.77	4.81
7.15	2.25		2.25	7.0
E Ribbons			E Ribbons	

386.66	386.84	386.78
5.01	4.83	4.89
8.3		8.1

386.66	386.61	386.33	386.26	386.68
5.01	5.66	5.34	5.41	4.99
10.5	8.4		7.7	9.5

391.67 ✓

Levels for proposed opening
on S. Ely Cor. of Ingraham St.
and La Cima Drive.

C. Moore
Sundt & Meyer
W. Moore
B0093

5-27-46.

2108.6

Set Id. disk
1" W of E.L. Ingraham
on N.E. La Cima Dr.
180.88
N.L.

1" West of E.L.
of Ingraham St. = Base
6111C

La Cima Dr.

1458.6

Stone
Block

1" and 4" Cor.
Pipe roof drains

Baseline

0700
11'03" Rt.

True E.L. of
Ingraham St.
See Me

Indexed
C.S.K.

42

36.67
57
Comb.
C6. + Walk

2 + 08. Lo
Set Id. disk
1" W of E.L. of
Ingraham on
N.E. of La Cima

Baseline is 1" West
of E.L. Ingraham St.

La Cima Dr.

Chains
0.12 Short

1458.6

F.H. 0215
1130

Stone
Block

15
Ingraham

0781.9

122
64' W
200 0700
11'43" Rt.

567 Comb.
C6. + Walk

40'
Ber. disks

36.5

Gar.

E.L. Ingraham
St.

85.70

0 + 00 Δ 11° 43' RT.
Sec. 90° with Back T.

30.69	30.15	30.29
6.82	7.36	7.22
43.2	43.2	34
06	97	

0 - 40

30.23	29.70	29.89
7.28	7.81	7.62
43.2	43.2	34
06	97	

T.P. 4.90 37.51 6x3 32.61 ✓
disk 1' W of E.L.
Ingraham and N.L.
La Circa Drive

T.P. 7.27 39.04 1.82 31.77

Fd. B.M.B.P. Ingraham
N.W. Cor. La Mancha Dr 4.70 28.89 ✓ Sisson

T.P. 3.65 33.59 5.74 29.94

N.W. B.P. 1.82 35.68 ✓ 33.86 Ingraham
Northland

30.47	30.47	30.39	30.99	31.08	31.12	32.4
7.04	7.04	7.12	6.54	6.43	6.3	5.1
25	16	6.7	6.7	1		10
		97	06	edge		
				mark		

30.10	30.13	30.08	30.65	30.77	31.1	32.0
7.41	7.38	7.43	6.80	6.74	6.4	5.5
25	16	6.7	6.7	1		10
		97	06	edge		
				mark		

37.51 ✓

0 + 94.4

0 + 84.8

0 + 75

0 + 50

0 + 25

Sec. 5 at 90°

31.70	31.11	31.24
5.81	6.40	6.39
60.5	60.5	50
66	97	

31.94	30.87	30.99
6.09	6.64	6.52
54.1	54.1	40
66	97	

31.20	30.65	30.81
6.31	6.86	6.70
51.4	51.4	41
66	97	

67

B.L. 1st of
E.L. Ingraham

R.

44

31.88

5.63 Top 4" Con. Pipe dn

31.63

5.88 ← Top 4" Con. Pipe dn

31.35	31.18	31.10	31.67	31.67	32.6	32.5
6.6	6.33	6.41	5.84	5.84	4.9	5.0
41	32	22.5	22.5	15.8		10
		97	66	edge walk		

31.14	31.03	30.83	31.93	31.97	32.3	32.2
6.39	6.48	6.68	6.08	6.04	5.2	5.3
30	28	17.1	17.1	11.3		10
		97	66	edge walk		

30.88	30.80	30.63	31.19	31.24	31.8	32.3
6.63	6.71	6.88	6.32	6.27	5.7	5.2
32	22	12.3	12.3	6.4		10
		97	66	edge walk		

37.51 ✓

B.L. 1' W. of
E.L. IngrahamP_T

1 + 67.8

31.80

5.71

97

1 + 67.8

32.31

5.20

Top
of
C61 + 59.6 = S. edge walk =
1' N of S.U. of
La Cima Dr.

31.96

5.55

20

31.93

5.58

50

31.84

5.69

32

31.89

5.67

12.3

97

32.33

5.18

12.3

C6

32.45

5.20

Walk

32.36

5.15

11

Con. Cor
of Bldg.

32.27

5.24

25

Con

1 + 25

32.26

5.25

70.2

C6

31.61

5.90

70.2

97

31.80

5.71

59

31.77

5.74

46

31.49

6.02

35

31.49

6.02

23.7

97

32.04

5.47

23.7

C6

32.17

5.34

18.1

edge
walk

32.4

5.1

32.4

5.1

10

dir

1 + 00

32.08

5.43

67

C6

31.44

6.07

67

97

31.55

5.96

56

31.57

5.94

45

31.36

6.15

35

31.30

6.21

25.1

31.90

5.61

25.1

C6

32.00

5.57

19.5

edge
walk

32.1

5.4

32.61

4.90

11.8

on Con. walk
at doorway

37.51

1 + 98.6 N. of Line
on La CIMA

1 + 98.6 N. of Line on
La CIMA

1 + 83.6 = 9 La CIMA St.

1 + 68.6 = S. of Line

1 + 68.6 = S. of Line
La CIMA

LT

B.L. 1/4 of
E.L. Ingham

Rt. 46

32.63	32.44	32.24	32.34	32.28	32.13
4.88	5.09	5.29	5.17	5.23	5.38
500	32	15	109	21	52
907.	Pay	Pay	06	06	06

32.05	31.94	31.82	31.62
5.20	5.59	5.09	5.89
Pay	109	21	52
	97.	97	97

32.51	32.44	32.18	32.04	32.06	32.06	31.99	31.95
5.00	5.07	5.33	5.47	5.45	5.45	5.52	5.56
70	50	32	15		10	20	40

31.80	31.80	31.74	31.63
5.71	5.71	5.77	5.88
	10	20	40
	97	97	97

32.18	32.13	31.98	31.91	32.25	32.18	32.10
5.33	5.38	5.53	5.60	5.26	5.33	5.41
70	50	32	15	10	20	40
Pay	Pay	Pay	Pay	06	06	06

37.51 ✓

Bk.
1' W of E.L. of
Interpretation

Rt

2 + 40.6 S. edge driveway to store

33.34	32.77	32.76	32.80	32.57	32.26	32.81	32.85	33.59
4.19	4.74	4.73	4.71	4.94	5.25	4.70	4.66	3.92
124	124	34	24	15	5.8	5.8	edge	10
97	97				97	66	walk	Pav.

2 + 14.6

32.64	32.64	32.54	32.28	31.98	32.66	32.75	32.89	32.97
4.87	4.87	4.92	5.13	5.53	4.85	4.76	4.62	4.54
127	32	25	16	5.9	5.9	edge	10	20
97	97			97	66	walk		Pav. to STORE
IN DRIVE								BLDG

2 + 08.6 - N. E. LA GIMA

32.64	32.61	32.51	32.33	32.01	32.64	32.61	32.47	32.39	32.35
4.87	4.90	5.00	5.18	5.50	4.89	4.90	5.04	5.12	5.18
12	35	26	17	4.6	4.6	disk	10	20	30
97	97			97	66	edge wk.	on walk		
IN DRIVE									

2 + 02.6 Top c6. 5.02 32.49

2 + 02.6 9.05 5.47 32.04

37.51 ✓

check Back to orig. B.M.

48

check to BM orig 2.11 33.86 33.86

T.P. 5.88 35.97 3.75 30.09

T.P. 2.57 33.86 7.75 31.27

T.P. 4.65 39.02 3.14 34.37

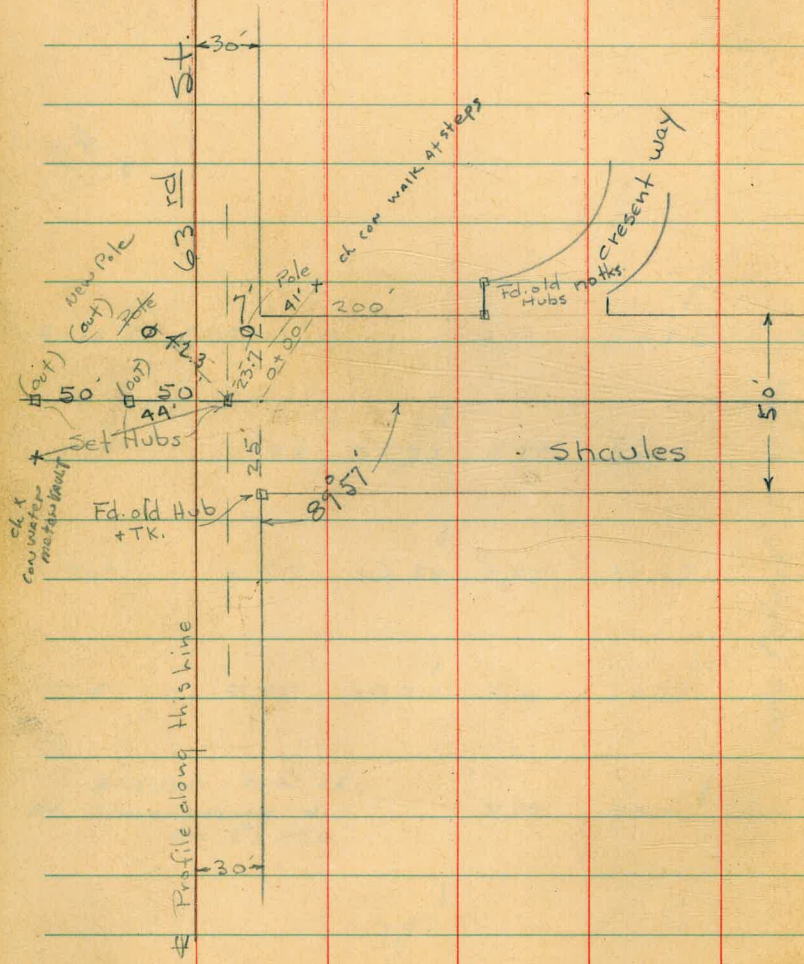
B.M. B.P. N.W. 66,
Rd. Longhorn +
La CIMO 4.30 33.71 Sisson

37.51

Notes Reduced - 5.29.86

X-Sect. Shaules - 63rd to 65th
 + Profile 65th - Sullivan to Madrone.

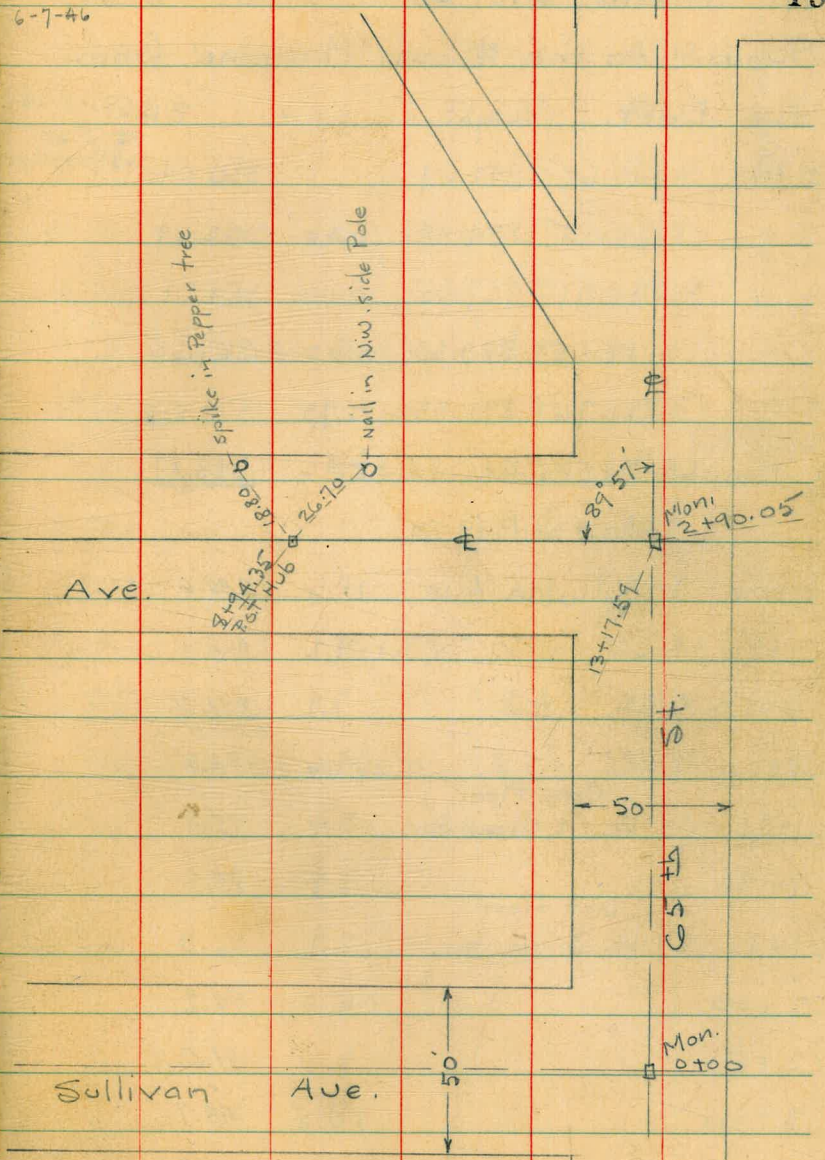
P-165



Osborne
 McCoy
 Hardin
 6-7-46

Indexed
 c.s.k.

Mon.
 6+85.42
 Madrone



Profile of 65th from Φ of Sullivan to the Φ of Madrone from the East. - Light oil pave

B.M.	12.65	342.69		330.04	
	12.25	354.94	0.00	342.69	
	12.71	367.65	0.00	354.94	
	12.65	380.30	0.00	367.65	
	11.76	391.33	0.73	379.57	
Φ Mon. 65 th + Shaules			2.46	<u>388.87</u>	
	10.33	399.20			
0+00 = Φ Sullivan Ave			11.6	387.6	
0+30 = N.L.			9.2	390.0	
0+50			7.9	391.3	
1+00			4.6	394.6	
1+25 - 70' Rt. = Φ Stone Gar.			3.4	95.8	on floor
1+50			3.4	95.8	
1+95 - 27' Lt. Single Gar.			2.9	96.3	on floor
2+00			5.0	94.2	
2+50			8.2	91.0	
3+00			10.5	88.7	
3+50			12.9	86.3	

F.O. 67-46

T.P.	0.31	386.56	12.95	386.25	50
4+00 = E. edge of Oil Road			3.6	83.0	
4+25			5.5	81.1	
4+50			11.0	75.6	
T.P.	0.03	373.89	12.70	373.86	
5+00			7.0	66.9	
T.P.	0.04	361.12	12.81	361.08	
5+50			8.3	52.8	
T.P.	0.04	348.37	12.79	348.32 ³	
6+00			9.5	38.9	
+13 =			12.3	36.1	
T.P.	3.01	338.42	12.96	335.41	
6+50			5.4	33.0	
6+85.42 = Φ Mon. 65 th + Madrone			8.39	330.03	330.04

Fairly steep slope - upon W. Down on E. from 4+00 on. to end

X-Sect. Shaules = 50' st. + Profile of 63rd
 N. & S. of E Shaules prod. From 63rd to 65th

B.M.	12.39	401.26		388.87	± Mon. 65 th + Shaules
	12.72	413.76	0.22	401.04	
	12.90	426.53	0.13	413.63	
B.M. = 3 nails in Pole by P.O.T.		8+94.35	0.62	425.91	
I.P.	0.14	413.97	12.80	413.73	
	0.05	401.25	12.67	401.20	
	0.02	388.43	12.84	388.41	
	0.55	376.33	12.65	375.78	
	0.06	363.89	12.50	363.83	
	0.19	350.99	13.09	350.80	
	0.48	338.93	12.54	338.45	
	0.15	326.34	12.74	326.19	
B.M. 3 nails in Pole - N.E.		63 rd + Shaules	6.03	320.31	
	1.05	321.36			

F.O.
6-9-46

51

Profile on 63rd - on probable E 63rd =
 30' W. of E.L. - See sketch. 0+00 = E Shaules
 prod. 321.36

Going N.				
0+00 = E Shaules	3.2		219.2	
0+25 = N.L. Shaules	5.4		16.0	
0+50	6.8		14.6	
1+00	10.6		10.8	
T.P.	0.15	309.18	12.33	309.03
1+45			3.0	306.2
T.P.	0.70	296.89	12.99	296.19
2+00			5.6	91.29
2+25 = end.			14.1	82.8

Going S.

B.M.	11.78	332.09		320.31
0+00 = E Shaules				
0+25 = S.L. Shaules	12.9		19.2	
0+50	11.5		20.6	
1+00	8.8		23.3	
1+50	6.4		25.7	

X-Section Shaules Ave 50' wide E = Baseline

1+50

1+25

T.P. 13.03 344.95 0.17 331.92

1+00 - Note Plus Rods on High side

0+50

0+00 = E.L. 63.14

From P. 51 332.09

H	H	H	H	H	H	Rt.	Rt.	Rt.
21.5	30.5	34.8	35.8	35.9	35.1	42.0	46.1	48.8
17.4	14	10.1	9.1	9.0	9.2	2.9	+0.2	+3.9
40	25	15	13		9	15	25	40

26.1	29.8	33.0	34.1	33.7	34.0	37.1	38.6	41.2
18.8	15.1	12.0	10.8	11.2	10.9	7.2	6.3	3.7 + 1.2
40	25	15	12		10	12	15	25 40

344.95

24.6	26.9	29.1	30.5	30.5	30.9	33.3	34.2	37.1
7.5	5.2	3.0	1.6	1.6	1.2	+1.2	+2.1	+5.6
40	25	15	10	16	10	12	15	25 35

21.9	22.6	23.8	25.2	25.9	27.1	27.6	28.9	30.8
10.2	9.5	8.3	6.9	6.2	5.0	4.5	3.2	1.3
35	25	15		10	12	15	25	35

19.4	19.9	19.7	20.8	22.1	22.6	23.4
12.7	12.2	12.4	11.3	10.0	9.5	8.7
35	25	15		15	25	35

332.09

6-11-46
70.

5+35 - 27.5 Rt. = ± 10" Acacia tree

T.P. 12.60 380.93 0.32 368.33

5+08 - 25 Rt. = ± 2p" Euc. tree

5+00 - 25' Rt. = end of wire fence

4+97 - 18' Lt. = ± P+Tel Pole

4+50

T.P. 12.34 368.65 0.39 356.31

4+00 - 26.7 = End Lath fence - beq. wire fence (poor Concl.)

3+50

54

58.6	65.8	69.6	74.9	74.4	74.3	76.3	77.7	80.9	85.5
22.3	15.1	11.3	6.0	6.5	6.6	4.6	3.2	0.0	+4.6
45	25	15	3		7	11	15	25	35

340.93

53.7	58.5	61.6	64.4	67.1	67.5	67.1	71.2	74.1	75.3	78.2
15.0	10.2	7.1	4.3	1.6	1.2	1.6	+2.5	+5.4	+6.6	+9.5
45	25	15	8	4		6	9	15	25	35

45.6	50.2	53.1	57.0	57.1	56.8	61.7	61.6	62.0	67.2	69.8
23.1	18.5	15.6	11.7	11.6	11.9	7.0	7.1	5.7	1.5	+1.1
45	25	15	2		7	12	15	18	25	35

368.65

36.7	41.3	44.3	49.5	47.6	55.4	56.7	59.9
20.0	15.4	12.4	7.2	7.1	5.3	0.0	+3.2
45	25	15	7	11	15	25	35

28.4	33.5	38.7	43.9	44.8	46.1	49.0	53.6	58.8
28.3	23.2	18.0	12.8	11.9	10.6	7.7	3.1	+1.6
45	25	15	4		10	15	25	35

356.70

7+25

21.4 45	15.4 25	12.5 15	6.7	5.9 9	3.5 15	1.1 25	+ 1.1 35
------------	------------	------------	-----	----------	-----------	-----------	-------------

6+90

25.8 45	19.7 25	14.9 15	8.5 3	7.9	6.9 8	2.3 10	1.0 15	+ 1.8 25	+ 4.7 35
------------	------------	------------	----------	-----	----------	-----------	-----------	-------------	-------------

6+50

26.0 45	20.0 25	17.8 15	11.9 3	11.6	11.9 11	9.2 12	7.5 15	3.4 25	0.4 35
------------	------------	------------	-----------	------	------------	-----------	-----------	-----------	-----------

6+44 - 16' Lt. = P. + Tel. pole

T.P. 13.09 406.08 0.63 392.99

6+00

23.0 45	18.2 25	15.6 15	10.9	10.1	8.2 10	6.0 12	1.7 15	+ 2.1 25	35
------------	------------	------------	------	------	-----------	-----------	-----------	-------------	----

T.P. 13.05 393.62 0.36 380.57

5+60

18.8 45	13.1 25	10.0 15	4.0	3.5 7	12 9	+ 1.0 15	+ 6.3 + 8.8 25	35
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380.93

9+50

9+18 = 12.5 = ϵ P. + Tel. pole

9+00

8+50

Check B.M.

11.09 428.51 0.79 417.42

8+00

T.P. 12.70 419.21 0.57 405.51

7+50

10
3520
2521
1525.2
1123.1
623.2
5.321.5
1520.0
2518.8
3523.8
4.1
3524.2
4.3
2524.5
4.0
1524.3
4.2
1523.5
5.0
1523.0
5.5
2522.4
6.1
3514.5
14.0
4017.9
10.6
2519.5
9.0
1521.6
6.9
1521.9
6.6
1223.0
5.5
1523.5
5.0
2523.9
4.6
3500.7
17.5
4505.0
13.2
2507.9
10.3
1512.1
6
1512.0
5.2
1214.4
3.8
1518.5
+0.3
2521.1
+2.9
3592.0
14.1
4595.0
11.1
2598.1
8.0
15104.0
2.1
10103.4
2.0
10105.7
0.4
11106.8
+0.7
15109.4
+3.3
25111.5
+5.4
35

406.08

12+00

11+77-9 Lt. = \neq Tel + P. pole

T.P. 0.04 404.23 12.32 404.19

11+50

11+00

10+50

T.P. 0.29 416.51 12.29 416.22

10+00

	Lt	\neq	Rt
	99.6	99.8	99.7
	4.6 35	4.4 25	4.5 15
	04.3	04.3	04.5
	12.2 35	12.2 25	12.0 15
			404.23
			04.0
			03.9
			03.6
			12.5 15
			12.6 25
			12.7 35
	11.9	11.0	10.6
	4.6 35	5.5 25	6.9 15
			8.3 5
			8.3
			8.7 15
			9.2 25
			9.8 35
	21.2	18.8	17.1
			16.5
			11.0
			14.3
			12.7
			11.6
			10.5
	+4.7 35	+2.3 25	+0.6 15
			0.0 10
			2.5 5
			2.2
			3.8 15
			4.9 25
			6.0 35
			416.51
	25.7	24.4	22.7
			19.5
			19.6
			17.6
			16.0
			4.5
	2.8 35	4.1 25	5.8 15
			9.0 7
			8.9
			10.9 15
			12.5 25
			14.0 35
			428.51

Lt.

±

Rt.

Shawles
 Check B.M. = ± Mon. 65th d 6.20 388.84[✓] 388.87[✓]

T.P. 1.90 395.04 11.09 393.14

12 + 92.59 = W.L. 65th

12 + 87 - 8' Lt. = ± P. pole

12 + 50

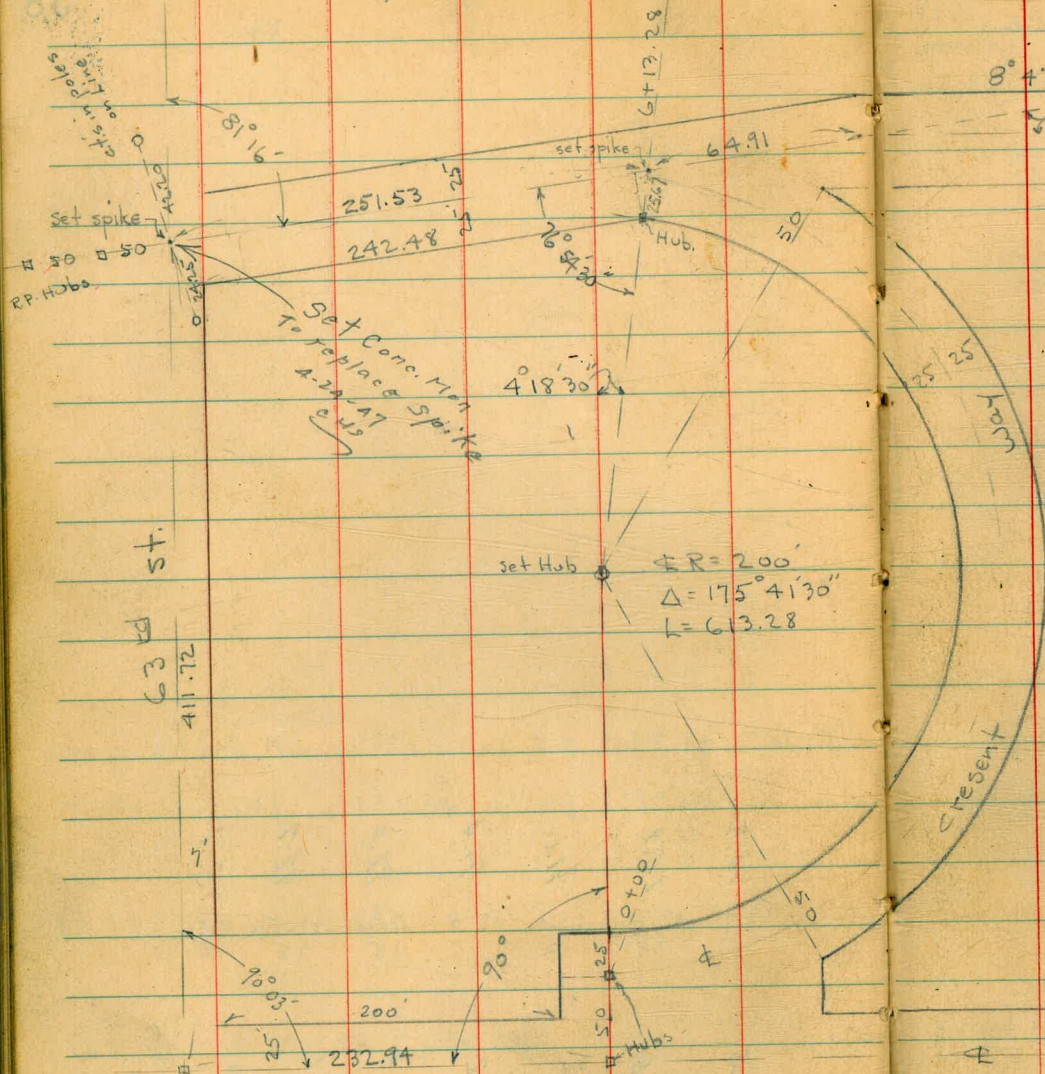
90.3	90.9	91.1	91.4	91.0	92.7	93.1
13.9 35	13.3 25	13.1 15	12.8	12.2 15	11.5 25	11.1 35
94.5	94.8	95.2	95.2	96.3	96.6	97.0
9.7 35	9.4 25	9.0 15	9.0	7.9 15	7.6 25	7.2 35

104.23

X-Sect. Crescent Way

6-24-46
70.

Platted-Tiepoint Sheet 3234 59
Oct 31. 46 - N.P.C.



Madrone Ave. Φ

For BIK to North
See F.B. 1677-53
4/2/47

Shaules Ave. Φ

changed to Dunlin place

X-Sect. of (Crescent Way) 50' wide
From Shaules to Madrone - Φ = Baseline

0+85 = Approx. opp. N.E. Cor. of Int. -

T.P. 1.09 325.23 12.18 324.14

0+50

0+25

0+00 = B.C. On curve - all sections taken Radially

0-26 = W. side of Intersection - Sect. Normal to Tang.

T.P. 10.88 336.32 4.23 325.44

B.M. 9.36 329.67 320.31

Nail in Pole
NE 63rd
+ Shaules

6-26-46

Osborne
McCoy
Hardin

Lt. = N

Indexed
C.S.K.

Φ

Rt. = S

60

10.8	14.4	19.2	17.1	20.8	15.5	22.3	22.2	22.8	15.5
50	25	25	40	25	25	25	17	25	25
13.2	12.0	21.0	15.3	23.0	13.3	23.1	26.9	22.7	10.3
9.9	9.9	22.7	13.6	25.2	11.1	27.7	30.9	29.8	25
5.8	5.8	325.23	13.2	27.7	8.6	28.1	31.2	33.4	25
3.1	3.1	Φ Road	9.4	30.9	5.4	28.1	31.2	33.4	25
6	6		15	30.9	5.4	28.1	31.2	33.4	25
22.1	22.1		17	30.9	5.4	28.1	31.2	33.4	25
22.7	22.7		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25
25.5	25.5		25	30.9	5.4	28.1	31.2	33.4	25
22.8	22.8		25	30.9	5.4	28.1	31.2	33.4	25

3+81 - 13.8 Rt. = S.W. Cor. Single gar. on Rt. Conc. floor

3+75 - Approx. beg. of Oil pave

3+50

T.P. 0.89 302.03 12.14 301.14

3+46 - 21' Rt. = N.W. Cor. shed.

3+40 - 18' Rt. = \pm 14" Pepper

3+39 = 16' Rt. = end wire fence

3+35 - 20.8 Rt. = S.W. Cor. of 12' x 11' shed.

3+28 - 19.1 Rt. = \pm 6" Pepper

3+25

3+08 - 19' Rt. = Reg. wire fence

3+00

2+75

T.P. 0.02 313.28 11.97 313.26

Crescent Way.

96.34 62

82.7	89.7	95.7	96.5	96.9	98.6	00.3
19.3 50	12.3 25	6.3 15	5.5 15	5.1 15	3.4 25	1.7 35
84.6	91.4	97.4	98.0	97.9	300.0	301.5
17.4 50	10.6 25	4.6 15	4.0 15	4.1 15	2.0 25	0.5 35
		Wedge Rd.				
			302.03			

89.9	96.7	00.2	00.1	01.4	04.5	06.0	06.2
23.4 50	16.6 25	13.1 15	13.2 15	10.9	8.8 15	7.8 25	7.1 35
		Wedge Rd.					
	95.2	03.1	03.3	07.1	09.3	10.8	12.5
	18.1 50	10.2 25	10.0 15	6.2	4.0 15	2.5 25	0.8 35
		Wedge Rd.					
98.7	05.5	05.6	05.8	08.3	12.2	15.8	18.3
14.6 50	7.8 28	7.7 25	7.5 15	5.0 12	1.1	+2.5 15	+5.0 25
	Wedge Rd.						+7.0 35
							313.28

5.69
13.9 on
floor

T.P. 1.61 276.88 11.36 275.27

5+75

5+50 = opp. of int. of Oil paved roads on Madrone + Present way

5+25

T.P. 1.75 286.63 12.74 284.88

5+06 - 16' Rt. = \pm 6" Pepper

5+05 - 14' Rt. = \pm 4" Pepper

5+04.6 = Approx. opp. Sharp Prop. Cor. on Rt.

5+01 - 25' Rt. = \pm 14" Pepper

4+81 - 11' Rt. = \pm 6" Pepper

4+75 - 17' Rt. = \pm 12" Pepper

4+68 - 15.5' Rt. = \pm 20" Cypress

78.1	77.3	75.9	73.2	72.4	69.5	69.7	70.1	69.9	69.6	62.6	57.4
4.5 35	9.3 25	10.7 15	13.4	14.2 4	17.1 7	16.9 9 edge pave	16.5 15	16.7 22 edge pave	17.0 25	24.0 40	29.2 60

60.3	80.1	79.5	78.5	75.2	74.4	74.1	74.0	73.9
6.3 35	6.5 25	7.1 15	8.1 3	11.4	12.2 7 edge pave	12.5 15	12.6 25	12.7 34 edge oil pave in int.

83.0	83.8	84.2	83.7	79.1	79.5	79.5	78.6	78.2	80.5	77.4
3.6 40	2.8 25	2.4 15	2.9 11	7.5 8 edge pave	7.1 5	7.1	8.0 10 edge pave	8.4 15	6.1 25	9.2 35

286.63

edge of Rd. on Madrone

85.9	87.3	87.6	82.7	83.1	83.1	83.0	82.7	86.9	86.7	86.0
11.7 40	10.3 25	10.0 18	14.9 13	14.5 9 edge pave	14.5	14.6 3 edge pave	14.9 15	10.7 15	10.9 25	11.6 35

= int. with SL Madrone

86.9	88.9	87.2	87.2	87.5	87.4	87.4	91.3	92.8	93.2	93.2
10.7 40	8.7 25	10.4 20	10.4 15	10.1 3	10.2	10.2 2	6.3 7	4.8 15	4.4 25	4.4 35

297.62

± Profile of Madrone from Angle pt. E. - Same H.I.

	276.89		
+13.03	289.30	-1.61	275.27
0+00 - Angle Pt. See sketch		15.0	
0+50		9.4	
1+00		4.3	

7+00 = ± Profile to show grade of Madrone = end.

6+50

Set B.M. - nail in Pole # 175672 10.43 266.45
opp. 6+58 on S. side

6+17 - 20' Rt. at 90° from ± Madrone = ± 12" Pepper

Note: From here W. Base line is ± of Madrone

Sect. taken on Rad. Line

Crescent way. note: ± of Madrone is .67 N. on Rad. Line

6+13.28 = P.C. - opp. the Int. of the S.L.'s of Madrone +

5+94 - 21' Rt. - ± 12" Holly tree

5+84 - 27' Rt. = ± 10" Pepper

Lt.	±	Rt.
		20.6
68.2	67.1	65.2
63.3	61.1	60.9
8.7 35	9.8 25	11.7 15
13.6 6	15.8 4	16.0
		14.0
		13.9
		19.4
		28.0 50
		25
		edge pave
		63.0
		57.5
		48.9

72.7	71.4	69.7	67.8	64.7	64.5	64.8	64.8	65.0	58.8	48.2
4.2 35	5.5 25	7.2 15	9.1 6	12.2 5	12.4	12.1	12.1	11.9	18.1 25	29.7 50
							edge at pave			

276.88 - See next page for check to starting B.M.

From P. 65

 π
276.88

12.33 289.02 - 0.19 276.69

12.82 301.62 0.22 288.80

12.55 314.11 0.06 301.56

12.73 326.66 6.18 313.93

6.32 332.95 0.03 326.63

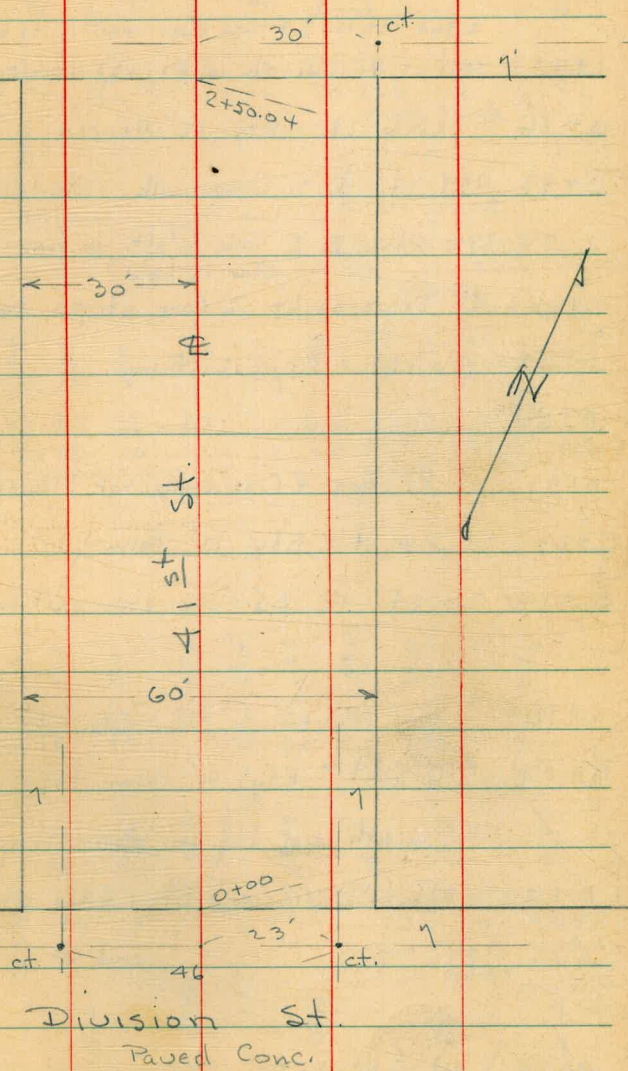
3.63 328.13 8.45 324.50

7.82 320.31 320.31 ✓

X-Sect. 41st St. 60 wide - From Div.
to Marine View - St. graded and side
walks in - no cbs. whole block shows the
remains of an old oil pave. - too broken up to
consider. Φ is base line
10' curbs.

7-24-46
Osborne
McCoy
Hardin
Waddel

Marine View Ave
Dirt-Graded.



2965 = Rt. 75 23 High Conc. wall - its back at 0+00
 1+00 = end of 4" Conc. cb. on Rt. 33 above walk

0+86 - 20.6' Lt. = Ely. 12" Acacia

0+83 - 19.9' Lt. = Φ 2' Conc. walk-slab out from walk

0+73 - 17.2' Rt. = Φ 5' Conc. Walk in front of Conc. steps.
 Gar. is low. Joins walk

0+61 = Φ Drive on Lt. 2' Conc. strips back of walk

0+52 - 20.7' Lt. = Ely. 12" Palm

0+50

0+47 - 28' Rt. = beg 4" Conc. curb for Flower bed .33 above
 edge of walk = Top.

0+23 - 20.4' Lt. = Ely. 12" Palm

0+14 - 20' Lt. = Φ 2.5' Conc. slab. out from walk

0+10

0+07 - 20.3' Lt. = Ely. 14" Palm tree

walk on Lt. in poor shape - needs repaving

0+00 = N.L. Division St. = edge of Conc. Pav +
 end of curbs.

0-14 = N.cb. line Div. St. on Conc. Pav
 NW-8P

B.M. 8.95 66.26 57.41 41st + Div.
 D1716-43

	59.2	59.4	59.30	59.3	59.0	59.5	60.0	59.9	60.6	60.74	60.76	61.0
			Lt. = W.							Rt.	F	
	7.1	6.90	6.96	7.0	7.3	6.8	6.3	6.4	5.7	5.52	5.50	5.3
	30	27.9	22.5	20	19	10		10	20	22.6	2.8	30
		w. walk	E. walk							w. walk	E. walk	
			59.06		7.20					59.60		
			19.9 = edge								60.19	
										6.66	6.07	
										17.2 = edge walk	22.6 = w. walk	
	58.7	58.75	58.64	58.6	58.3	58.6	59.1	59.2	59.8	60.66	60.98	61.1
	7.6	7.51	7.62	7.7	8.0	7.7	7.2	7.1	6.5	6.20	6.18	6.2
	30	27.8	22.4	20	19	10		10	20	22.7	2.80	30
		w. walk	E. walk							w. walk	E. walk	
	58.3											
	8.00 on edge slab.											
	58.2	58.10	58.14	58.2	57.8	58.1	58.4	58.5	59.3	59.47	59.56	59.6
	9.1	8.16	8.00	8.1	8.5	8.2	7.9	7.8	7.0	6.79	6.70	6.7
	30	27.9	22.6	20	19	10		10	20	22.8	2.81	30
		w. walk	E. walk		Top graded					w. walk	E. walk	
					cb.							
		57.97	58.03	58.13	57.90	58.31		58.47	58.51	59.19	59.34	
		8.29	8.23	8.13	8.36	7.95		7.79	7.75	7.07	6.92	
		22.6	20	20	10			10	20	20	22.8 =	
		E. edge of	Top cb.	put					put	Top cb.	w. edge	
		5.33 walk	end Ret.							end Ret.	5.33 Conc.	
		Poor Cond.									walk - fair	
			66.75		57.22	57.95		58.52	58.81	59.42	60.14	Concl
	55.24	57.20										
	11.02	8.86	9.51	9.04	8.31	7.74	7.45	6.84	6.12			
	50	30	30	20		20	30	30	50			
	gut.	Top cb.	gut.				gut	Top cb	gut.			
		PC 10 Rad										
		Ret.										
						66.26						

Check B.M.

8.85

57.41

Ret. on Rt. poor Cond.

1M on S. Corners.

2+50.04 = S.L. Marine View Ave. Not Paved - cb. + Ret.

2+49 = end Cobble wall on Rt.

2+48 = 21.1 Rt = Wly P. pole

2+30

2+00

1+61 = 18.8 Rt = ± 4' Conc. Walk out from Reg. walk

1+50 - on Rt Cobble (hoose) leaning wall at back of walk 2' High

1+50 - 29.8 Rt = end 2.3 High Conc wall

1+48 = 18.9 Rt = Wly. 6" Acacia

1+30 = 19.2 Rt = Wly. 8" Acacia

1+29 = 21.5 Lt = Ely. 8" Palm
May need leveling

from 1+05 to 1+25 Trees have cracked walk on Rt.

1+18 = 19.9 Rt = Wly. 10" Acacia

1+05 = 20.9 Lt = Ely. Guy Pole. + 20.8 Rt = Wly. P. pole

6626

E

Lt

Rt.

61.4	61.62	61.50	61.43	61.2	61.4	62.0	62.3	62.5	63.07	63.21	63.3
4.9	4.64	4.76	4.83	5.1	4.9	4.3	4.0	3.5	3.19	3.05	3.0
30	27.9	22.6	19.8	19.8	10	10	10	20	20	28.1	30
	w. walk	E. walk	Top cb	90+				90+	Top cb	E. walk	
			end Ret		broken down				end Ret.		
61.5	61.3	61.18	61.3	60.7	61.2	62.0	62.2	62.2	62.7	62.68	62.8
4.8	5.00	5.08	5.0	5.6	5.1	4.3	4.1	4.1	3.6	3.58	3.42
30	28.0	22.6	20	19	10	10	16	20	22.8	28.2	30
	w. walk	E. walk							w. walk	E. walk	
60.6	60.7	60.75	60.7	60.2	60.9	61.7	61.6	61.7	62.2	62.3	62.43
5.7	5.42	5.48	5.6	6.1	5.4	4.6	4.7	4.6	4.1	4.00	3.93
30	28.1	22.7	20	19	10	10	17	20	22.7	28.0	30
	w. walk	E. walk							w. walk	E. walk	
									61.60	18.8 = edge walk	
									4.66		
60.1	60.17	60.09	59.9	59.6	60.1	60.9	60.7	60.7	61.6	61.59	61.66
6.2	6.09	6.17	6.4	6.7	6.2	5.4	5.6	5.6	4.7	4.7	4.60
30	28	22.6	20	19	10	10	10	16	20	22.6	27.9
	w. walk	E. walk							w. walk	E. walk	

30 wire line comes out wall

6626

Check Elev. of Ext. Cold lay
 Pave on E. + W. 20' Alley in
 Blk. 120 Univ. Hts.
 for sketch see B 599 P. 32
 for N. + S. Alley See P 26 this book

0+58 - 11.6 Rt. pave jogs in from walk

0+40

0+24 - 11.5 Rt. = Pave goes out to Conc. walk

0+20

0+00 - E. L. Utah St. - N. cb. is broken down

Position and S. Ret. has been Moved over

0-14 - E. cb. line Utah - Note: N. Ret. is out of

B.M. 3.24 377.19 373.95

Indexed
 c.s.k.

70

8-1-46

Lt = N.

⊕

Rt. = S

Osborne

322.08
 5.10

11.6 = S. pave - Meets walk

322.21
 4.98

322.00
 5.19

322.17
 5.02

322.29
 4.90

10.8

10

11.5 - N. pave

N. pave

322.41
 4.78

11.5' on

Pave
 0.2' higher than
 walk

322.35
 4.81

322.18
 5.01

322.51
 4.68

10
 N. pave

10.8
 S. pave

322.57
 4.62

322.58
 4.61

322.56
 4.63

322.48
 4.71

322.53
 4.64

322.60
 4.59

322.23
 4.46

N. of Alley
 Pave

12.6
 Top cb
 end Ret.

12.6
 gut

7.1 N.
 edge of Conc.
 Strip

9.9
 S. edge of
 Conc. = gut.

9.9
 Top cb
 end Ret.

376.28
 5.40

322.36
 4.83

322.91
 5.28

322.02
 5.17

322.56
 5.23

322.56
 4.63

322.92
 5.22

322.11
 5.04

4.5

12.6

12.6

9.9

9.9

5.0

5.0

5.0

gut

Top cb.

gut.

gut

Top cb

gut.

gut.

2' Rad Ret

377.19

2+20 - 9.8 Rt. = edge of Conc. walk

2+06 - Conc. Dr. + Apron to laundry on Lt.

1+93 - Opening to laundry on Lt. Conc. floor

T.P. 4.22 374.60 6.81 370.39

1+60 - E.L. - 9.8 Rt. = Beg. board fence

1+50 - 17 Lt. = Sewer M.H.

1+40 = W.L. of N.+S. Alley

0+94 = Double Gar. on Rt. Conc. floor + apron

0+76 - Doub. Gar. on Lt. Conc. floor + Apron

Lt.

±

Rt.

371.02
3.58
9.8

<u>370.29</u>	<u>370.60</u>	<u>370.19</u>	<u>370.52</u>	<u>370.54</u>
3.81	4.00	4.41	4.08	4.06
11	9.8		8	9.8
Floor of Dr. in bld.	edge Conc. apron			

<u>371.61</u>	<u>370.70</u>	<u>370.27</u>	<u>370.56</u>	<u>370.82</u>
3.59	3.90	4.33	4.04	3.78
10.7	9.4 = edge		8	9.8
Floor of bld.	Conc. apron			

	<u>374.60</u>			
<u>370.80</u>	<u>370.54</u>	<u>370.22</u>	<u>371.06</u>	
6.39	6.68	6.42	6.13	
10		7.9	9.8 = rolled up to fence	

370.54
6.65
1.7
on Rim

<u>370.92</u>	<u>370.25</u>	<u>370.89</u>
6.27	6.44	6.30
10		10
N. pave		

<u>371.0</u>	<u>371.22</u>	<u>371.39</u>	<u>371.91</u>
5.79	5.97	5.90	5.24
10 =		9 = edge	11.7 = floor
N. pave		Conc apron	

<u>372.39</u>	<u>371.64</u>	<u>371.53</u>	<u>371.50</u>
4.80	5.55	5.66	5.69
12.3	9.5		10 = S. pave
Floor	edge Conc. Apron	<u>377.19</u>	

check BM

3.89

370.71

S.W. Kansas
+ Howard.
370.71

2+13.81 = W. cb Line Kansas

2+99.81 = W.L. Kansas St. - 9.8 Rt. = end board fence

2+80

2+60 - Beg portions of old Conc. slab pave.

2+35 = opp door to laundry

<u>368.20</u> 5.90 70 gut. Water standing Here	<u>369.68</u> 4.92 10 Top cb. 3 Rad.	<u>369.12</u> 5.48 10 gut.	<u>369.13</u> 5.47	<u>369.18</u> 5.42 9.7 gut.	<u>369.20</u> 4.90 9.7 Top cb. Square Cor.	<u>369.22</u> 5.28 70 gut.
--	--	-------------------------------------	-----------------------	--------------------------------------	--	-------------------------------------

<u>320.02</u> 4.58 10	<u>369.24</u> 4.86 10 gut. Conc pave	<u>369.62</u> 4.98	<u>369.26</u> 4.84 5 edge Conc.	<u>369.20</u> 4.90 9.7 gut.	<u>320.03</u> 4.58 9.7 Top cb.
-----------------------------	--	-----------------------	---	--------------------------------------	---

<u>369.88</u> 10.8 Conc. to bld.	<u>369.88</u> 4.72 10 on Conc.	<u>369.22</u> 4.87	<u>369.27</u> 4.73 5 edge of Conc.	<u>369.89</u> 4.61 8	<u>320.08</u> 4.52 9.8
--	---	-----------------------	--	----------------------------	------------------------------

<u>320.12</u> 4.43 11 Floor in doorway	<u>320.09</u> 4.51 10	<u>320.07</u> 4.53 6 edge Conc.	<u>369.83</u> 4.77	<u>320.03</u> 4.57 4 edge Conc. Pave	<u>320.11</u> 4.49 8	<u>320.42</u> 4.18 9.8 Rolled up to fence
--	-----------------------------	--	-----------------------	--	----------------------------	--

<u>320.24</u> 4.34 11 Floor of Bld.	<u>320.22</u> 3.83 11 Top step.	<u>320.21</u> 4.35 8.5 = edge Conc slab.	<u>320.02</u> 4.53 7 to door way	<u>320.25</u> 4.35	<u>320.42</u> 4.13 9.8 = along fence	<u>374.60</u>
---	--	---	--	-----------------------	--	---------------

Levels on Drive ways at E. Side
 Ingraham - S of La Cima St. See sketch
 P. 42

LISTED 8/16/46

8-14-46

Osborne
 McCoy
 Hardin
 W. Moore

0+33.3 = ± 12' Drive - Dirt only E. of walk ^{36.69} 59.6
 6.7
 gut.

0-47.4 = ± 8' Conc. Drive to Gar.

B.M. 4.04 36.65 32.61 Disk P 43

Lt. = W.

Base line used in
 Moore's sketch.

Rt. = E 73

	30.85	31.23	31.25	31.2	32.0	32.3
	5.80	5.42	5.40	5.4	4.6	4.3
	6.7	4.4 =	1' edge		9	5.0
	Bottom of Dr.	Brk. in Dr.	Walk			
	30.01	30.65	30.70	30.87	32.11	32.16
	6.64	6.00	5.95	5.78	4.54	4.49
	6.7 gut	4.3 = Brk. in Drive	1' edge Walk		7.5 = Brk. in Drive	13' = BC of curve in Dr.
						6.3 = floor Gar.
						See sketch
						36.65

Location + Levels Existing Storm Drain
Across India St Between Spruce + Redwood

BM	236	88.36	86.00	S.F.B.P Spruce + 17th St.
	101	77.06	12.31	76.05
	429	70.17	11.18	65.88
38.1	West of 7' L India	5.23	69.92	Top Vit. Pipe
40.1	" " "	4.29	65.88	Top Head Wall
42.6	" " "	7.33	62.89	Outlet Flux Line Steel Pipe

BM	6.17	92.17	86.00	S.F.B.P Spruce + India
	0.34	81.21	11.27	80.90
92.35	East of 7' L India	10.82	70.92	Inlet Flux Line
"	" " "	7.66	73.58	Top Head Wall

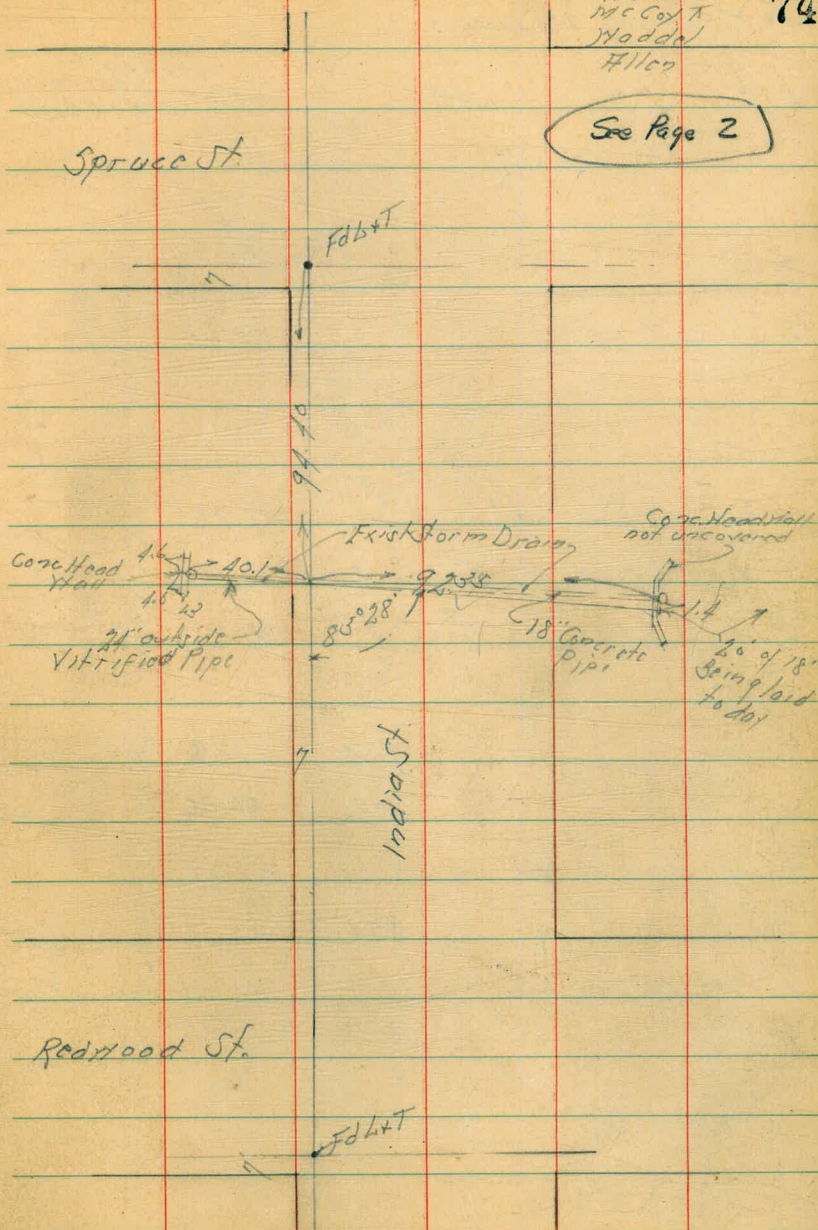
110.21

INDEX
E.S.N.

Sept. 10-46
H.S. 5565
McCoy T
Haddal
Allen

74

See Page 2



Location of Existing 24" Conc. Pipe Culvert
Kettner + Spruce

B.M. 2.96 61.49 58.53 S.F.B.P. Redwood Kettner

Inlet of Culvert 53.00 Plan. 8.49 8.74 8.75 1 c.s.k.

Outlet of Culvert 47.50 13.99 10.86 1 c.s.k.

Levels on Existing 24" Conc. Pipe Culvert

B.M. 2.19 61.22 58.53 S.F.B.P. Redwood Kettner

Inlet 9.54 51.68 Bottom Exit 24" Conc. Pipe

5.86 55.36 Top Conch. 24"

South End cb Ret 8.43 52.79

" " " 8.74 52.48

Outlet 24" Conc. Pipe 14.17 47.65 Bottom Pipe

Indexed
c.s.k.

Sept. 23-46
S. 10007
McCoy
Hadden

75

Slaps off set 5' SW
off Storm Drain

As Per Plan

Existing 30" Steel
Pipe Culvert
Fair Condition

7.5 52.48-cb

7.5 52.79-cb

11.0
Existing 24" Conc. Pipe Culvert

Ends Covered

Spruce St

Inlet
Elev Flowline
51.66

Kettner Blvd

Redwood

7.5 52.48

Located by water Dept.

16" C.I. pipe at sta shown as

curb face

offset from
baseline to curb face

Prop.

Plotted 6490-L-6-5-47M

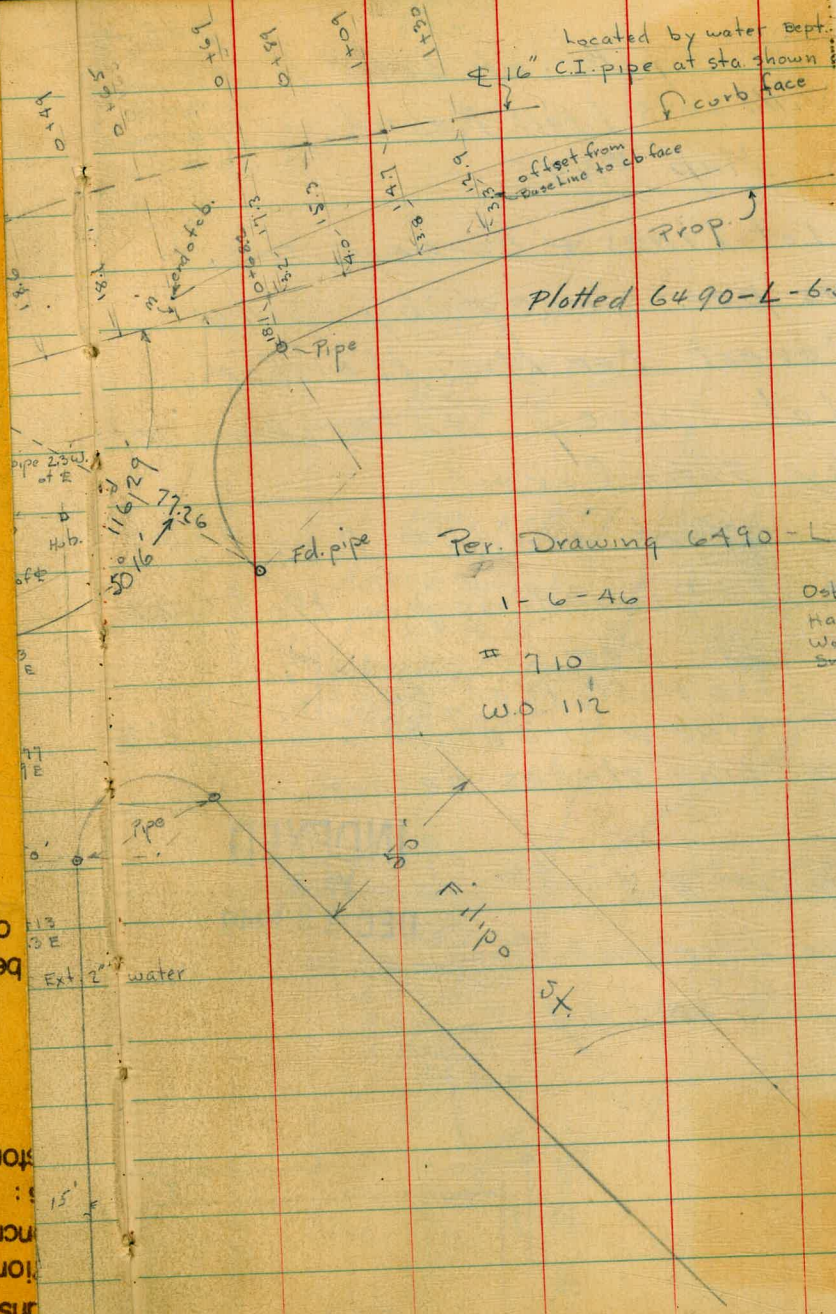
Per. Drawing 6490-L

1-6-46

710

W.O. 112

Osborne
Harrin
Warrell
Smith



Notes of the following work to be done in
 and specifications attached hereto.
 tion of the street shown hatched thus:
 concrete pipe culvert extensions as shown
 storm drain cleanout as detailed.

NOTES.

be Centrifugal Concrete Pipe having "D" L

or more.

d by water Dept.
 e at sta shown is,
 P curb face
 o face

76

Prop. ↗

6490-L-6-5-4717R

6490-L

Osborne
 Hardin
 Warvell
 Smith

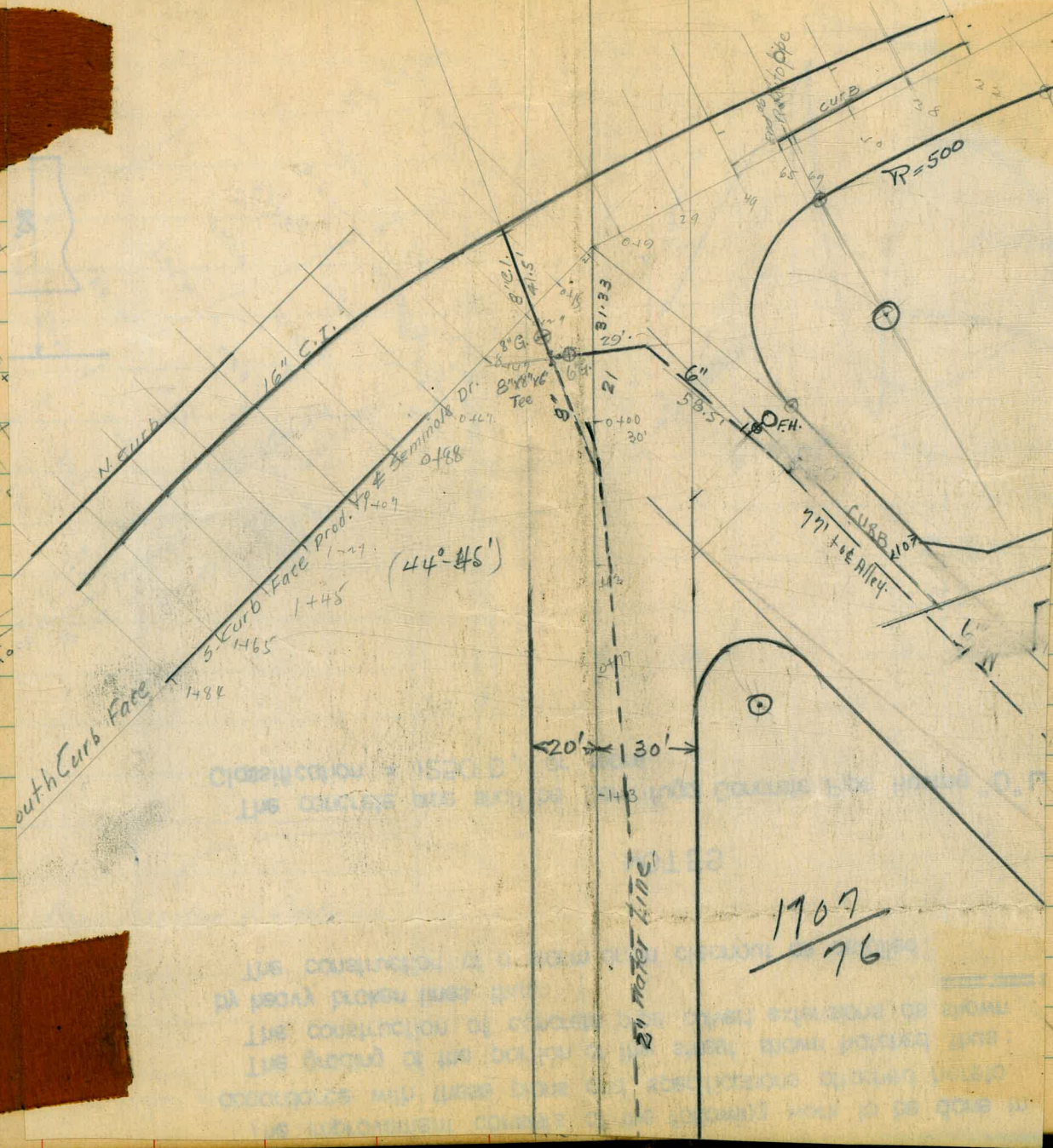
1707

 76

-- 30' MOTOR LANE --

20' | 30'

(44°-45')



Located by water Dept.

16" C.I. pipe at sta shown as

curb face

offset from
Baseline to curb face

Prop.

Plotted 6490-L-6-S-47119

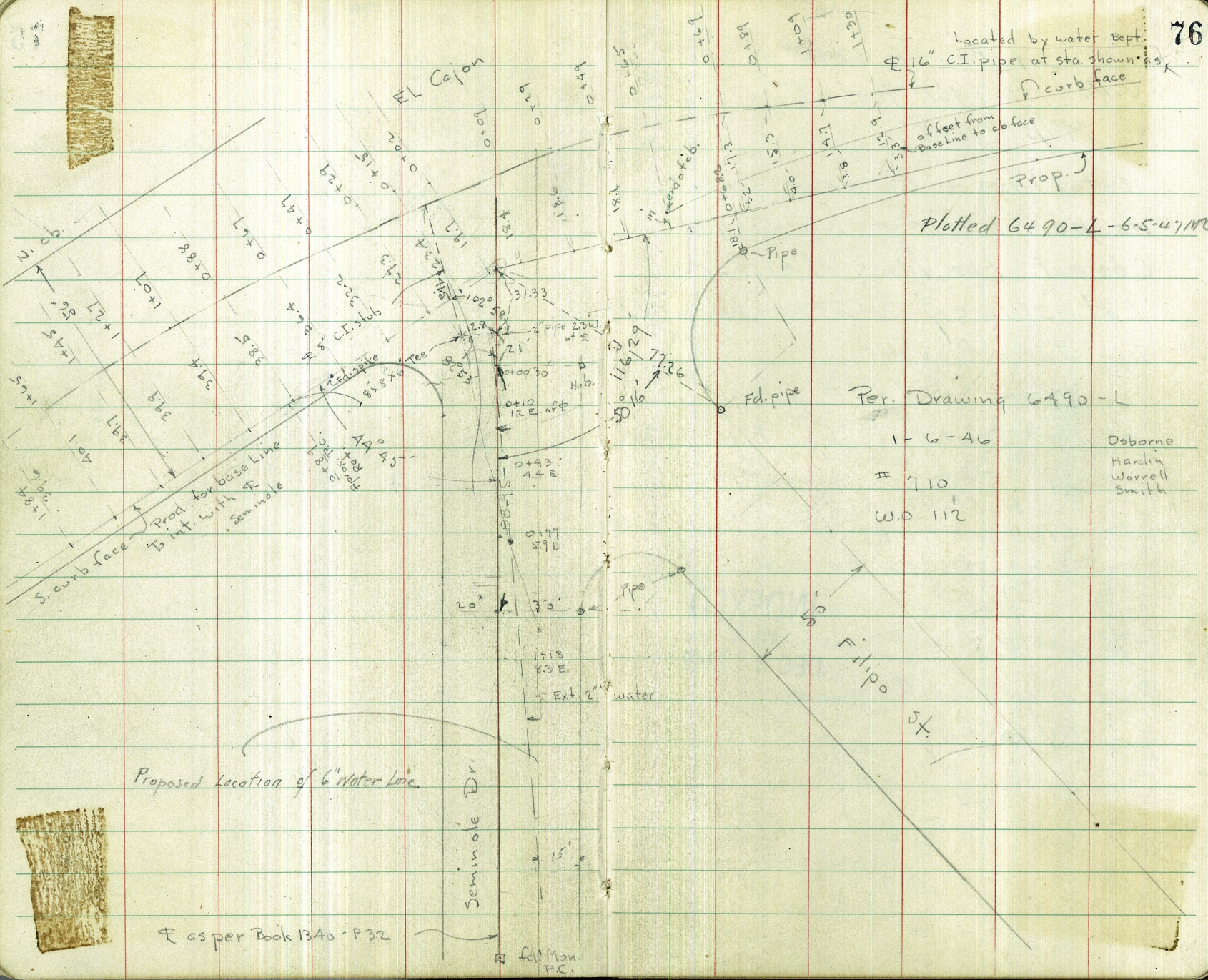
Per. Drawing 6490-L

1-6-46

Osborne
Hardin
Warrell
Smith

710

W.O. 112



Proposed location of 6" water line.

Seminole Dr.

Filipo St.

as per Book 1340-P32

fold Mon. P.C.

8-28-47

Survey Por. of Lot #1
Villa Lots 1 to 11 Resub.
Map #1155

Sommermayor
W Moore
Sherman
LaMore

Lot lines + corners reset
as per. survey by John
Covert for Mrs. Heisler.
Lot survey data furnished
by John Covert.

Work order # 21001

- = Lot found as per tie sheets
- = " set
- = 2x2 Hub + tack set.
- = Line nail set in window sill.
- X = Line stakes set.

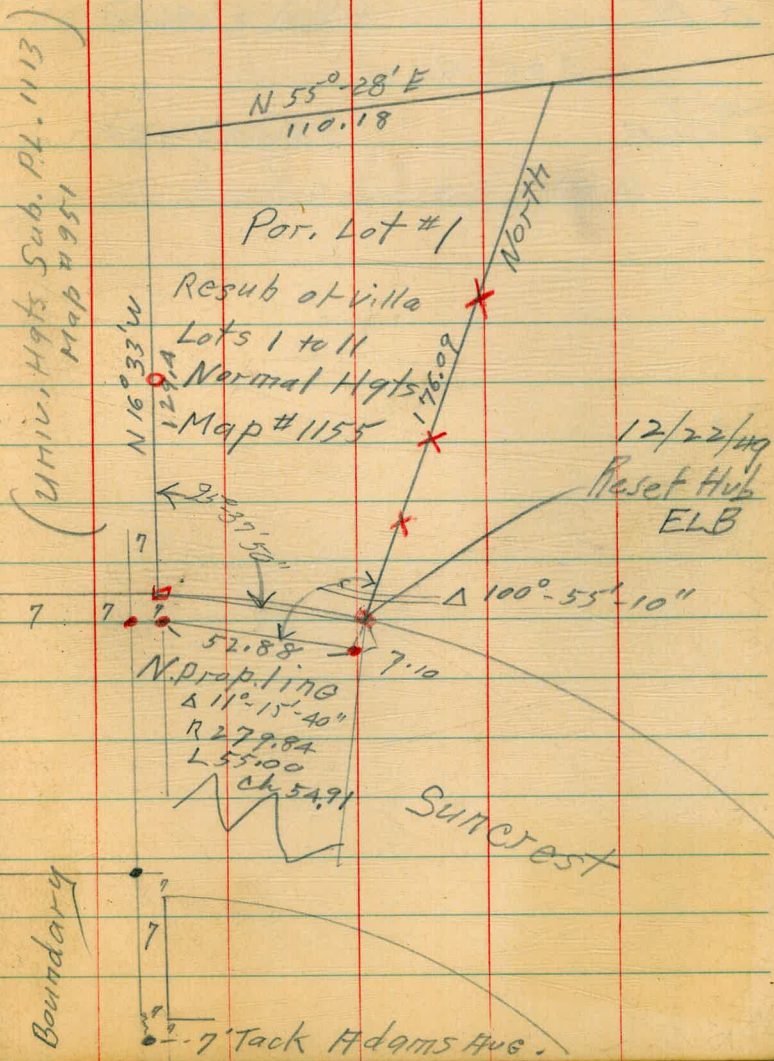
INDEXED
W.K.
DEC 23 1949

Reset Hub
Begg Sherman Crawford
12/22/49



Indexed
c.s.k.

77



LOCATION OF 24" R.C.P. SLY OF
SPRUCE ST. BETWEEN INDIA & STATE
STREETS W.O. 20006

Sta	+ H.I	- Elev.
B.M.		86.00
	8.35	94.35
End of 24" R.C.P.		15.50 78.85

11-23-54

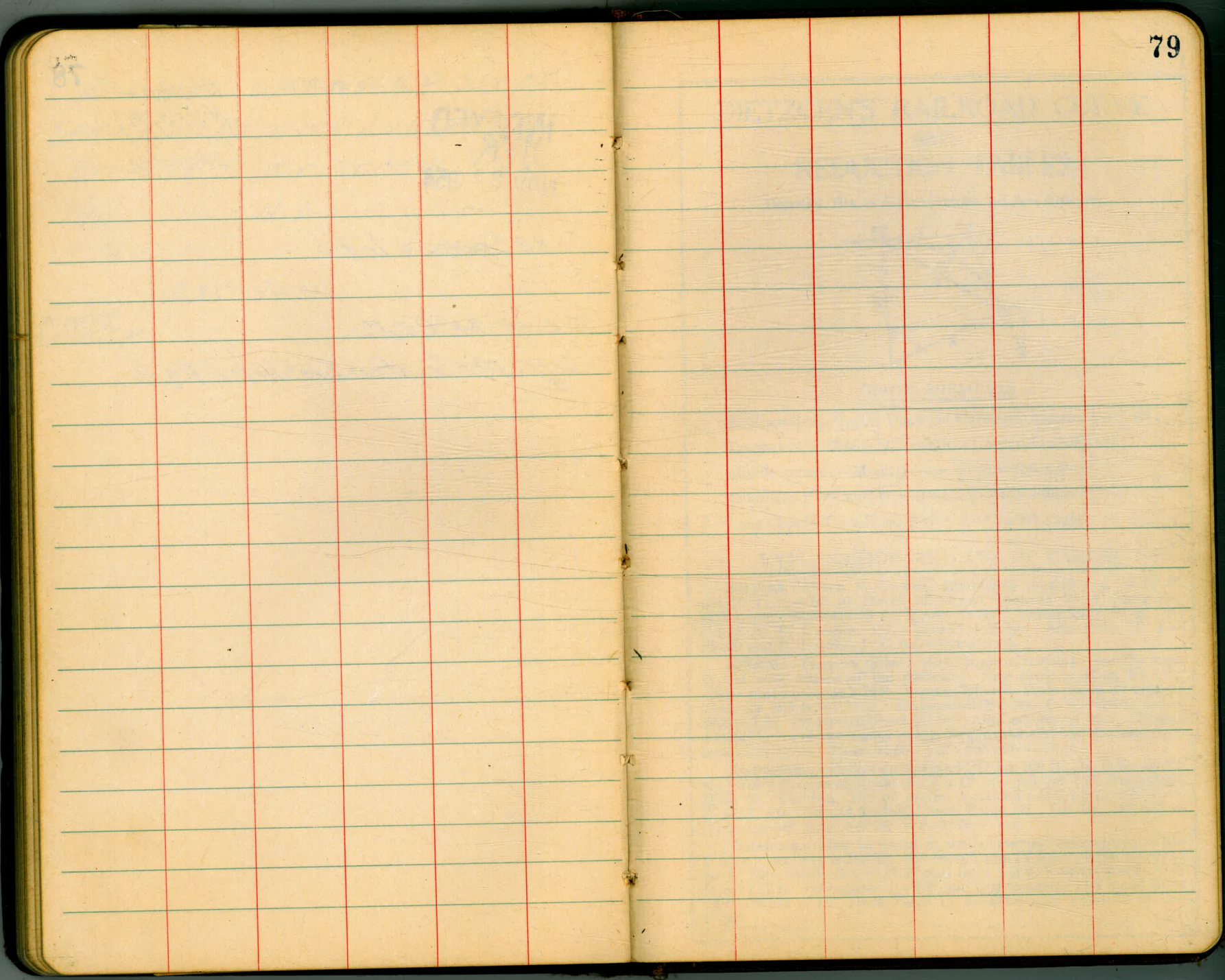
INDEXED
MER
NOV 24 1954

Stamped
Huffman
Nordahl
Elmore

SEBP Spruce & India

F.L. of 24" R.C.P.

NOTE: For location See Sketch Pg. 2



42' N 46
35' N 8.6
10' N 10.8
S.L. 75

173
40
474
632
1319

1292.5
7
25
1324.5

1.59
1320

632
474
1106

133
138

76
57
133

3 ch.
8 cuts - 562

49285
86
484.25

L-178051
89034
44.52
2010
4.92

11013
828
1059
192
62

275
325

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20-16) * 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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