

1709

ENGINEERS
LEVEL BOOK
No. 410F

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.
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1709

CITY ENGINEER'S OFFICE

This Field Book is manufactured of a High
Grade 50% Rag Paper having a WATER
RESISTING SURFACE, and is sewed with
Bing Special Enamel Waterproof thread.

Made in U. S. A.

Profile 69th St from City Limits N

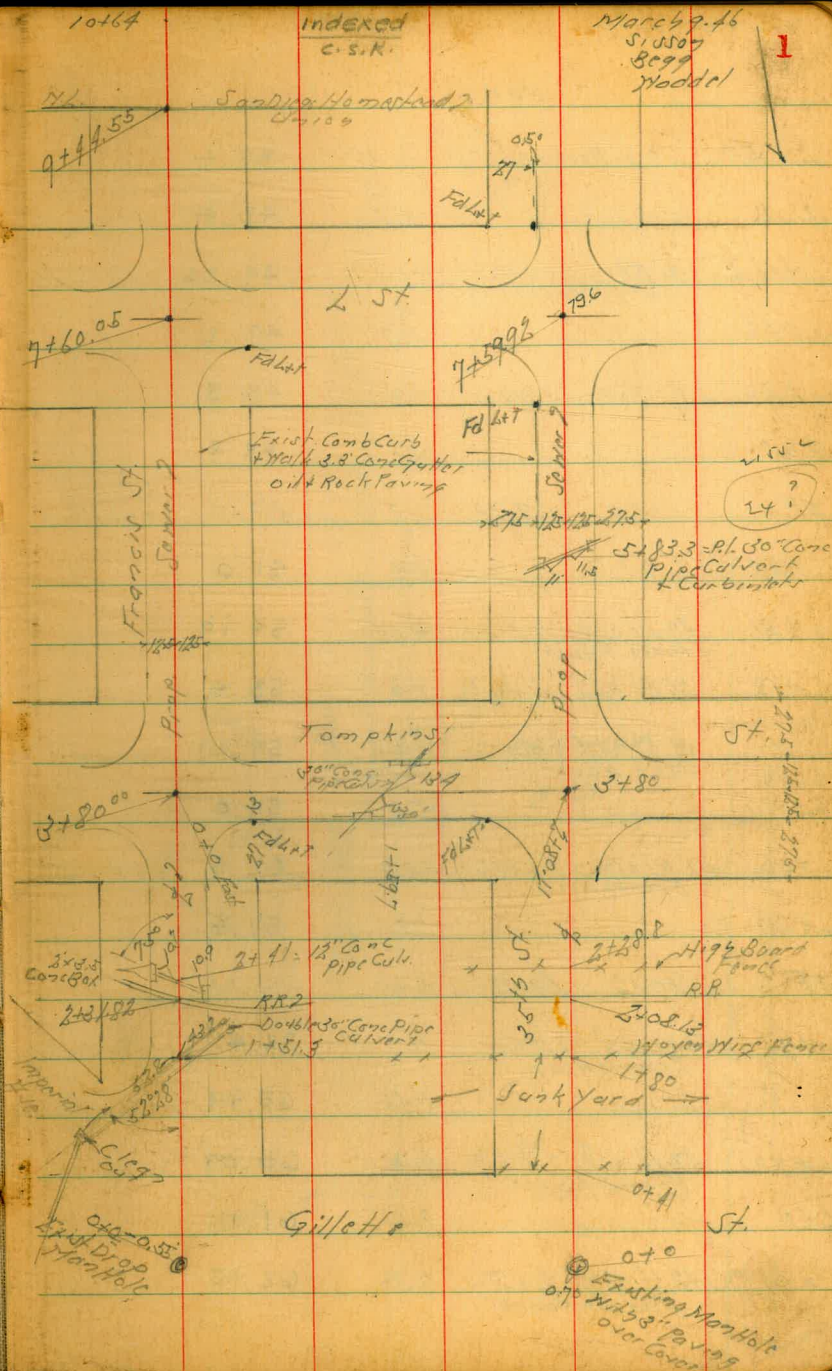
Sta. 9+50-12+17

73-74

File
Alley BIK { 100 } Ocean Bay
X-sec. { 101 } Beach Sub 61-72
 { 102 }

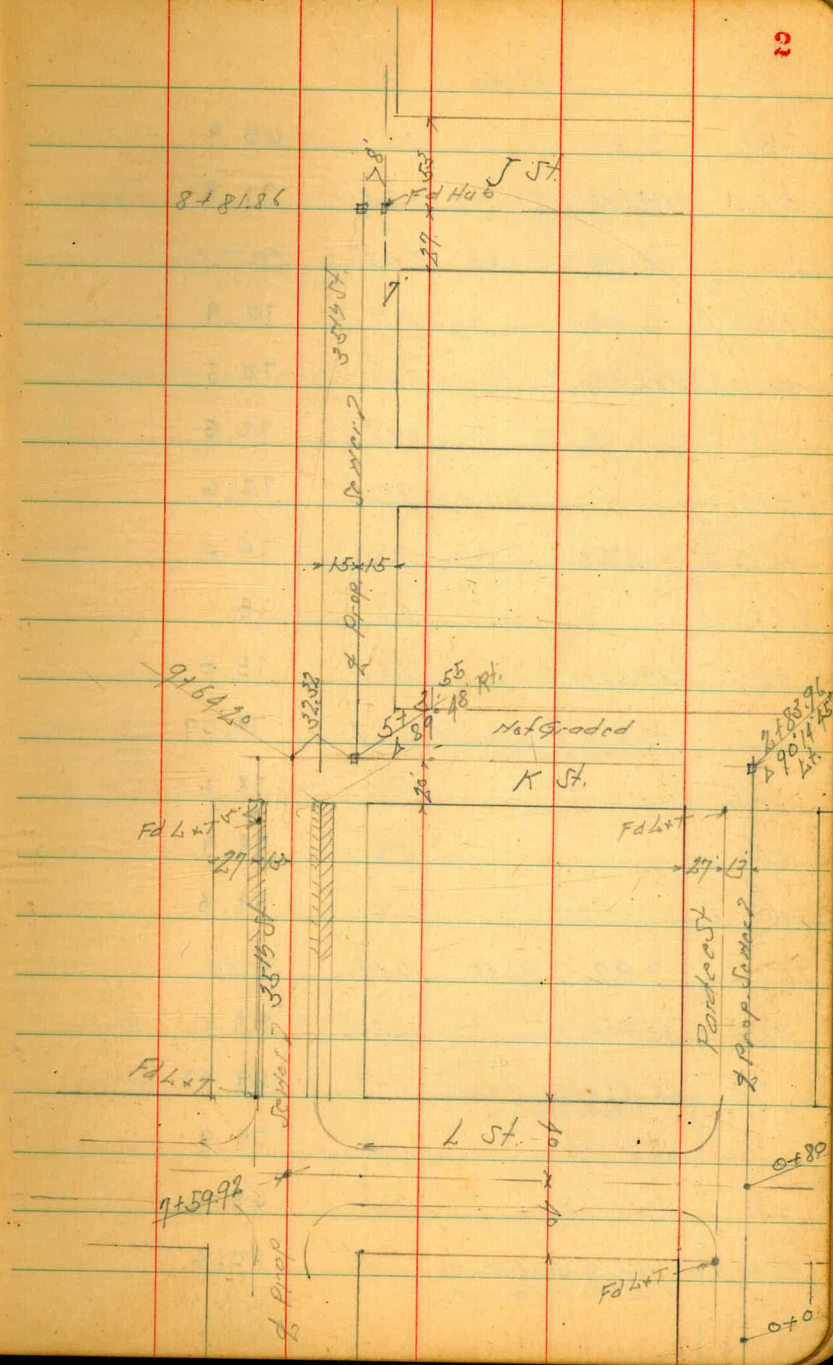
Proposed Sewer Francis St
 Gillette St. to N.L. San Diego Homestead Union

BM	319	32.76	29.57	RD & N Rail of Under F.O. 33' oil & imp.	
TP	7.57	35.77	4.56	28.20	on H. Mol Culvert 5-2' 10" pipe
0-0.55	= Exist Drop MH		7.89	27.88	02 Pipe
"			13.84	21.93	Flow Line
"			17.78	17.99	Flow Line
0+09			7.8	28.0	
+17			5.0	30.8	
+21	= Sly. H.C. Paving		5.9	29.9	
+50	07	"	6.67	29.10	
1+0	07	oil & Rock Pav.	6.26	29.51	
TP	4.40	38.63	1.54	34.23	
+51.3	= P.L. Do. 30" Culv		7.0	31.6	on Pav
"	62.8	S.M. Clean out	19.14	19.49	Flow Line
"	43.2	H.F. - E End 30" Culv	16.33	22.30	Flow Line of North Side
2+0	07	oil & Rock Pav.	3.3	35.3	
+31.82	= S.D. & H. RR		0.56	38.07	Top of Sand Soil
+41	= P.L. Culvert		0.6	38.0	
"	10.9	F	2.75	35.68	Flow Line Cone Bot.
"	10.7	H	5.42	33.21	Flow Line Cone Bot.
TP	12.07	49.92	0.77	37.81	



19.93

2+50	07 Rect + Oil Pav	11.5	38.4		
3+0	" " " "	6.5	43.4		
+16.5	46 Rt of 1/2 = S.W. Cor Calif House	+0.67	49.26	07 Floor	
+40		2.7	47.2		
+80	7 Torapkins	1.4	48.5		
4+0		1.1	48.8		
TP	10.71	59.32	1.31	48.62	07 SF 4x7 Francis Torapkins
+50		8.3	51.0		
+51	47 Lt of 1/2 = N.E. Cor Stucco House	5.14	54.19	07 Floor	
+68	26 Rt of 1/2	5.9	53.4	Ground	
	46 Rt of 1/2 = N.W. Cor Calif. House	0.06	59.27	07 Floor	
5+0		5.3	54.0		
+06	53 Rt of 1/2 = 7 x 11 1/4 Frame House	+3.2	62.5	07 Floor	
+50		1.9	57.4		
TP	10.12	69.95	0.00	59.33	
+73	53 Rt of 1/2 = S.W. Cor Frame House	11.1	58.4	07 Garage Floor	
"		8.46	65.99	07 Floor House	
+90	47 Lt of 1/2 = 7 x 11 1/4 Frame House	9.36	60.09	07 Floor	
6+0		8.4	61.1		
+44	47 Lt of 1/2 = 7 x 11 1/4 Frame House	7.30	62.15	07 Floor	



69.45

6+80			3.6	65.9	
+55	48 Rt of 1/2 - 7 x 11 1/4 Frame House	+2.3		71.8	02 Floor
TP	13.06	81.83	0.62	68.83	
7+0			10.9	70.9	
"	24 Lt of 1/2		11.3	70.5	Ground
"	45 " " "		19.3	72.5	"
7+20			9.2	72.6	
+60.05	1/2 L St.		7.8	74.0	
8+0			6.7	75.1	
+25	29 Lt of 1/2		6.8	75.0	Ground
"	48 Lt of 1/2 - 7 x 11 1/4 Frame House	7.74		74.09	02 Floor
+50			3.5	78.3	
+60			2.9	78.9	
9+0			2.0	79.8	
TP	9.97	91.61	0.19	81.64	
+24	33 Rt of 1/2		8.6	83.0	Ground
"	55 Rt of 1/2 - 7 x 11 1/4 Stucco House	2.18		89.43	02 Floor
"	30 Lt of 1/2		11.7	79.9	Ground
"	80 Lt of 1/2		23.4	68.2	"
9+44.55	- NLY side Wall x 6 + 1/4 Rock Paving	11.0		80.6	

91.61

10+0			12.1	79.5	
+46				9.6	82.0
"	24 Lt of 1/2 - S.W. Cor Frame House	10.70		80.91	02 Floor
+64			8.0	83.6	
"	59 Rt of 1/2 - S.W. Cor Frame House	7.43		95.9	02 Floor
TP	12.13	102.07	1.67	89.94	
B.M.			3.21	98.86	02 5/16 2 1/2 x 3/4 to Norfolk

Proposed Sewer 35/6 St Gillette St to 2 K St.				Indexed C.S.K.	
Sketch Page 1 + 2					
BM	6.95	35.15	28.20	07 NW Cor S.L. Imperial + Frame	
0 + 0	Existing Man Hole		5.32	29.83	02 R/W
"		5.06	30.09	07 Paving	
+ 32	= 1/2 x Bottom Wash 8' W/W		7.2	28.0	
+ 41	= E.W. Wire Fence		5.5	29.7	
+ 50		5.4	29.8		
+ 54	1.2 Lt of 1/2 = Fly H' Fac. Tree				
+ 70	59' Rt of 1/2 = NW Cor Frame 8' 1/2		2.67	32.48	07 Floor
1 + 0		4.9	30.3		
+ 50		4.5	30.7		
TP	11.83	42.48	4.50	30.65	07 P.C. 21452
+ 80		9.1	33.4		
+ 95		5.1	37.4		
2708.13	= 1/2 S.D. + F.R.R.		2.93	38.55	Top Rail
+ 17		3.8	38.7		
+ 23		0.5	42.0		
TP	12.86	54.08	1.26	41.22	
+ 50		9.8	44.3		
TP	11.97	65.78	0.27	52.81	
3 + 0		10.4	55.4		

				March 13-76 S. 5582 Waddel Hardin
				65.78
3 + 0	= 1/2 Fly Oil Rock Pav		3.8	62.0
+ 80	= 1/2 Tomptier		2.81	62.97
4 + 0			2.3	63.5
TP	6.83	70.27	2.34	63.44
+ 18	37.5 Rt of 1/2 = SW Cor Frame House		1.78	68.49
+ 50			6.2	64.1
+ 93	24 Lt of 1/2		4.8	65.5
"	14 Lt of 1/2 = NE Cor Frame House		11.4	58.9
"	21 Rt of 1/2		0.6	69.7
"	53 Rt of 1/2 = 1/2 W/W Frame House		12.0	72.3
5 + 0			4.9	65.4
+ 50			3.8	66.5
+ 83.3	110.4 Lt = Fly Conc Box		13.00	57.27
"	115 Rt = 1/2 W/W		11.78	58.49
6 + 0			2.4	67.9
+ 20			1.4	68.9
TP	11.61	81.65	0.23	70.04
+ 50			10.5	71.2
+ 82	57.4 Lt of 1/2 = SE Cor Stucco House		3.35	78.30

35 1/2 St

		81.65			
6+82	52.5 Rt of 1/2 = 1/2 L Entr. 56 1/2 High House	3.6	78.1	Basement Floor	
7+0		4.9	76.8		
+20		3.1	78.6		
+59.92 = 1/2 L St		2.1	79.6		
8+0		0.8	80.9		
TP	12.70	93.86	0.19	81.16	
+30	34 Rt of 1/2	4.0	89.9		
"	51 Rt of 1/2 = 1/2 + 1/2 L Frame House	0.55	93.31	on Floor	
+50		8.0	85.9		
+72	40 Lt of 1/2 = 1/2 + 1/2 L Frame House	3.2	90.7	on Floor	
+78	35 Rt of 1/2	0.7	93.2	Ground	
"	94 Rt of 1/2 = 1/2 L Frame House	1.12	95.1	on Floor	
9+0		2.4	91.5		
TP	8.02	101.41	0.17	93.39	
+17	41 Lt of 1/2 = 1/2 + 1/2 L Frame House	7.70	93.71	on Floor	
+29	32 Rt of 1/2	4.4	97.0	Ground	
"	94 Rt of 1/2 = 1/2 + 1/2 L Frame House	1.9	99.5	on Floor	
+4	1/2 Cb + 1/2 Walk + 1/2 L oil + Rock Pav	5.2	96.2		
+64.8	20 1/2 of 1/2 L St	3.7	97.7		
		2.55	98.86	on Floor of 1/2 L of 1/2 L + 1/2 L + 1/2 L 98.86	

Proposed Center Tompkins St
Francis St to 35 1/2 St

March 14 46
5
52 1/2 St
Tompkins
+ Francis
18912

		Indexed e.s.k.			
8+11	12.04	60.66	48.62		
0+0	1/2 Francis	12.2	48.5		
+50		11.8	48.9		
1+0		9.8	50.9		
+58	32 Lt of 1/2 = 1/2 L Cor Calc. House	1.3	59.4	on Floor	
+40		7.6	53.1		
+59.7	P. 1 30" Conc Pipe Calc	6.1	54.6	on Pav	
"	12.4 Lt = 1/2 L Conc Box	13.5	47.2	Frame House	
"	12 Rt of 1/2 L " "	14.8	45.9	" "	
2+0		2.3	58.4		
+13	50 Rt of 1/2 = 1/2 L Cor Frame House	+0.10	60.76	on Floor	
TP	7.54	67.77	0.43	60.23	
+10		5.9	61.9		
+80.11 = 1/2 35 1/2 St		4.83	62.94	on Roof Hall	

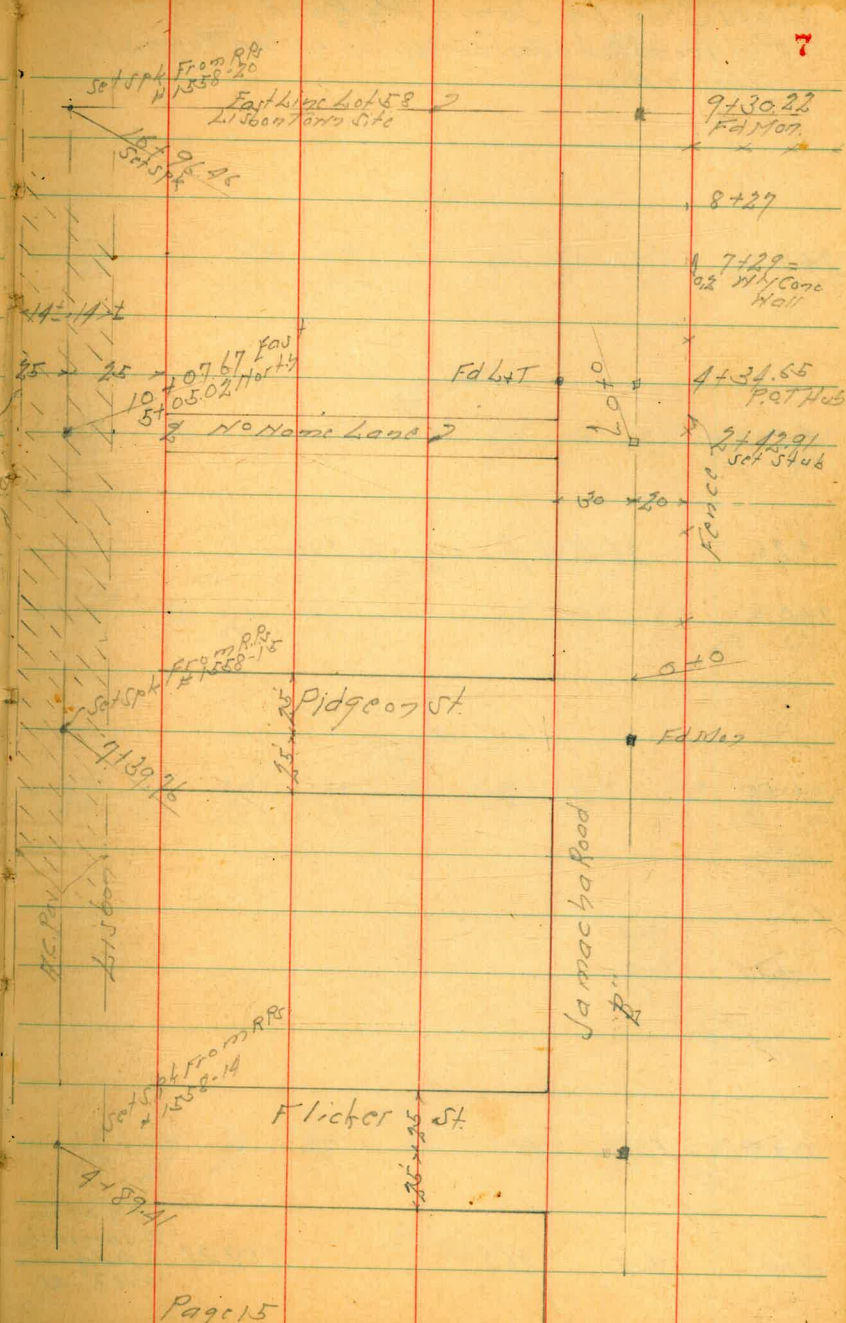
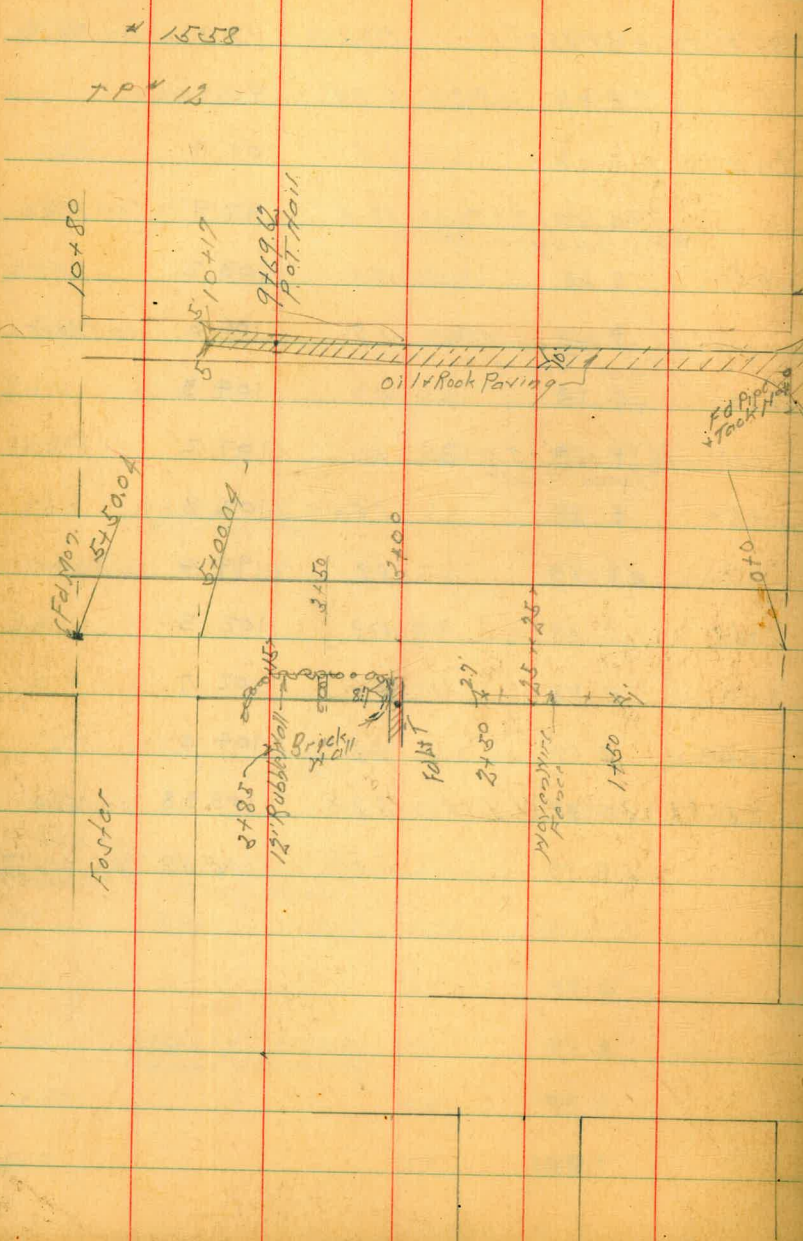
Sketch Page 2

B.M.	11.55	96.47	84.92	S.W. BP LST + Parcel
0+0	= 40' S of S.E. LST	12.2	84.3	
+40		11.4	85.1	
+80	= 1/2 LST	10.5	86.0	
+140		10.2	86.3	
+150		9.8	86.7	
+240		9.3	87.2	
+150		8.6	87.9	
+64	= 1/4 Cbr + Walk + Oil + Rock Pav.	8.2	88.3	
+8396	Δ 90° 14' 45"	7.81	88.66	on Stub
+340		7.8	88.7	
+19		7.0	89.5	
+45	40.5' Pt of 1/2 = S.E. Cor Frame House	+1.3	97.8	on Floor
+50		3.5	93.0	
"	27' Pt of 1/2 = N.E. Cor Frame House	3.35	92.92	on Floor
TP	8.90	105.13	0.84	96.23
+40		7.5	97.6	
+11	33' Pt of 1/2 = N.E. Cor Garage and Hallway	7.3	97.8	on Floor
+50		5.4	99.7	
+510		5.0	100.1	

105.13

5431.55	Δ 89° 48' Pt	6.23	98.90	on Stub
TP	9.37	108.27	6.23	98.90
+40		6.4	101.9	
"	79.5' Pt of 1/2 = S.W. Cor + Ely Garage and Driveway	10.4	97.9	on Floor
+50		5.1	103.2	
"	31' Pt of 1/2 = S.W. Cor Frame House	1.7	106.6	on Floor
+40		4.0	104.3	
+10	26' Pt of 1/2 = S.W. Cor Stucco House	1.1	107.2	on Floor
+50		5.5	102.8	
"	14' Pt of 1/2	8.9	99.4	Ground
+68		5.8	102.5	
+80		5.6	102.7	
+50		4.3	104.0	
+81.86	= 27' Pt of S.E. LST	2.89	105.38	on Stub
"		2.88	105.39	on Stub 18' Line LST E 7 1/2' med 10' 1/2' W

Proposed Sewer + Cross Sections
 Samacha Road - Lisbon St. Flicker + Pidgeon



Cross Section Samacho Road
 Pidgeon St. to Far Line Lot 58 Lisbon Town Site
 Sketch Page 7

Indexed
 c.s.k. $\frac{8}{2}$
 Lt: 11
 May 27-16
 Station
 of center
 of road
 made
 Ellen

+20

					262.9					
2.3	26	1.9	4.7	5.5	5.8	4.0	4.0	4.0	4.1	
30	27	22	10		2	4	10	20	30	

+50

					262.1					
4.0	4.3	5.7	5.7	6.3	6.3	4.6	4.7	5.2	5.4	
30	27	22	10		2	6	10	20	30	

+20

28 ft of $\frac{8}{2}$ = 114 Tol Pile

+10

					261.0					
3.8	4.1	6.5	6.6	7.4	7.3	5.8	6.0	6.2	6.7	
30	27	23	10		2	3	10	20	30	

+50

					260.3					
4.5	5.1	7.4	7.4	8.1	8.1	6.7	6.8	7.0	7.2	
30	26	23	10		2	5	10	20	30	

+34

263.4
 5.2
 66 = 114 ft from floor

+0 = F.L. Pidgeon

					259.8					
5.9	5.9	7.9	8.0	8.6	8.2	8.2	8.2	8.2		
30	26	23	10		10	20	30			

BM

9.19 268.90

259.21

09 27 00
 2 Samacho
 4 Pidgeon
 4/15/81-45

268.40

Samocbo Road

+50

+70

+92

+78

+73

+60

196 Rt of $\frac{1}{2}$ S/W Power Pole

+53

276 Lt of $\frac{1}{2}$ N/W Tel Pole

2+50

268.40

Lt=N

$\frac{1}{2}$

Rt=S

9

266.2

$\frac{0.8}{30}$ $\frac{1.2}{20}$ $\frac{2.2}{18}$ $\frac{2.2}{10}$ $\frac{2.2}{22}$ $\frac{2.2}{7}$ $\frac{1.4}{5}$ $\frac{1.7}{10}$ $\frac{2.6}{20}$ $\frac{2.7}{30}$

265.7

$\frac{0.8}{30}$ $\frac{1.2}{23}$ $\frac{3.0}{18}$ $\frac{2.9}{10}$ $\frac{2.7}{27}$ $\frac{2.6}{13}$ $\frac{2.2}{5}$ $\frac{2.5}{10}$ $\frac{2.9}{20}$ $\frac{3.3}{30}$

263.72

4.68

93 = 4 + 1/2 from
House on Floor

266.1

+2.3

466 = 5 1/2 from
House on
Floor

1.03

31 = 2 + 5 1/2 + 18
Corner 1/4

264.4

$\frac{1.7}{30}$ $\frac{2.1}{21}$ $\frac{3.1}{19}$ $\frac{3.7}{10}$ $\frac{4.0}{40}$ $\frac{4.0}{2}$ $\frac{2.2}{7}$ $\frac{2.2}{10}$ $\frac{3.1}{20}$ $\frac{3.6}{30}$

268.40

Somacha Road

670

+61

184 Rt of $\frac{3}{8}$ = Sly Power Pole

+50

+02

272 Lt of $\frac{3}{8}$ = 1 1/4 TC Pole

570

+50

+35

TP

6.76

274.12

1.04

267.36

07/10/58
4+34.65

+15

197 Rt of $\frac{3}{8}$ = Sly Power Pole

470

268.40

H.N

8

91-5

Nov 27-46
5800
of 1000 ft
Woods
Eller 10

268.12

1033

44

46

58

56

268.5

56

57

52

65

73

35

30

21

19

10

5

7

20

30

Sly

Stucco

House on Floor

268.4

38

43

56

55

268.4

57

59

52

60

70

30

22

19

10

5

8

10

20

30

268.2

38

41

55

56

268.2

59

61

55

58

67

30

20

17

10

5

7

10

20

30

267.6

133

51

69

68

267.6

65

67

60

69

78

31

20

16

10

Sly

1 1/2" Cap

Dist. 2.8 Ribben

267.65

10.75

5.28

183

Sly

3 1/2" 90°

183

Mark

274.12

59

1 1/2" Ply Form

House on Floor

266.9

36

04

14

14

266.9

15

16

0.8

10

30

30

18

16

10

1

5

20

30

268.40

Jamaica Road

+75

+50

+25

265 Lt of P = NY TEL Pa/c

+06

195 Lt of P = Sly Parker Pa/c

+70

+80

+56

+750

279.12

Lt-N

308

87-5

11

267.80

6.32
42.5 = 44 1/2 Front
House on Floor

4.5 5.0 6.7 6.3 6.3 6.3 5.9 6.3 7.0
30 13 20 10 5 7 20 30

267.8

6.90

40 = 42 1/2 Cap
Found for
For 90-01

267.8

4.8 5.9 6.4 6.2 6.6 6.0 6.4 6.2 7.6
30 19 18 10 6 7 16 20 30

273.94

6.18
55.6 = 57 1/2 Sly Stocco
House

308 390
Found 347 = 35 1/2 Ribbon
CONCRETE

268.0

4.8 5.8 6.0 6.1 6.4 5.8 5.9 6.1 7.3
13 17 10 5 7 10 20 30

279.12

BM

7.55 266.57

82 No 7
9+30.22

+71 - 1/4 top of Ditch on Rt

9+0

+73

+50

+28

8+0

274-12

Lt-N

8

Rt-S

12

267.5
4.3 4.7 4.4 6.1 6.6 7.0 4.7 5.3 5.8
30 22 17 10 3 8 20 30

267.6
4.0 4.4 5.6 6.5 6.3 6.5 6.8 6.2 5.5 5.3 7.2 6.6 6.8
30 23 22 18 10 4 8 10 19.5 19.5 30 24 24
123 = Lt-N
123 = Rt-S
123 = Lt-N
123 = Rt-S
123 = Lt-N
123 = Rt-S
123 = Lt-N
123 = Rt-S

6.18 6.88
123 = Lt-N
123 = Rt-S
123 = Lt-N
123 = Rt-S

267.6
4.5 4.6 6.2 6.5 6.5 6.5 6.3 5.9 6.6 8.2
30 25 23 20 10 8 8 20 30

6.67
123 = Lt-N
123 = Rt-S

267.6
4.4 4.5 6.3 6.6 6.4 6.5 6.9 5.2 6.6 6.8 7.8 8.1
30 24 23 20 10 7 7 13 19.5 19.5 21 30
123 = Lt-N
123 = Rt-S

274-12

+50

+35

26.5 Lt of B = NY Tc / Pole

+04

19.3 Rt of B = Sly Power Pole

10+0

9+68

9+50

9+32 = Fly top of Ditch on Rt.

9+26 = Bottom Ditch on Rt.

274.12

24 30	37 20	56 15	53 10	269.0 51	51 5	44 7	36 20	34 30	272.04 208
----------	----------	----------	----------	-------------	---------	---------	----------	----------	---------------

44 = 4 1/4
From 100 ft
to 107 ft

17 30	46 21	62 16	61 10	268.4 57	57 4	51 10	45 20	56 30
----------	----------	----------	----------	-------------	---------	----------	----------	----------

272.88
1.24
55.0
17.00
Fly top of Floor

50 30	57 20	61 17	62 10	267.7 54	65 4	57 6	56 10	46 20	65 30
----------	----------	----------	----------	-------------	---------	---------	----------	----------	----------

17 30	50 22	64 17	61 10	267.5 66	77 3	58 10	48 20	60 30
----------	----------	----------	----------	-------------	---------	----------	----------	----------

15 30	45 22	64 17	62 10	267.5 66	77 3	79 8	8.5 20	8.6 30	8.8 50
----------	----------	----------	----------	-------------	---------	---------	-----------	-----------	-----------

274.12

B.M. 6.14 300.97
 3" Pipe 6-2
 Lisbon Fort
 Lion Lt 58
 Lisbon Torroite

TP 10.48 307.11 0.71 296.63

TP 12.34 297.34 0.61 285.00

TP 12.39 285.61 0.90 273.22

11+0

27 270.4
 30 38 44 40 37 31 30 36
 20 16 10 20 30

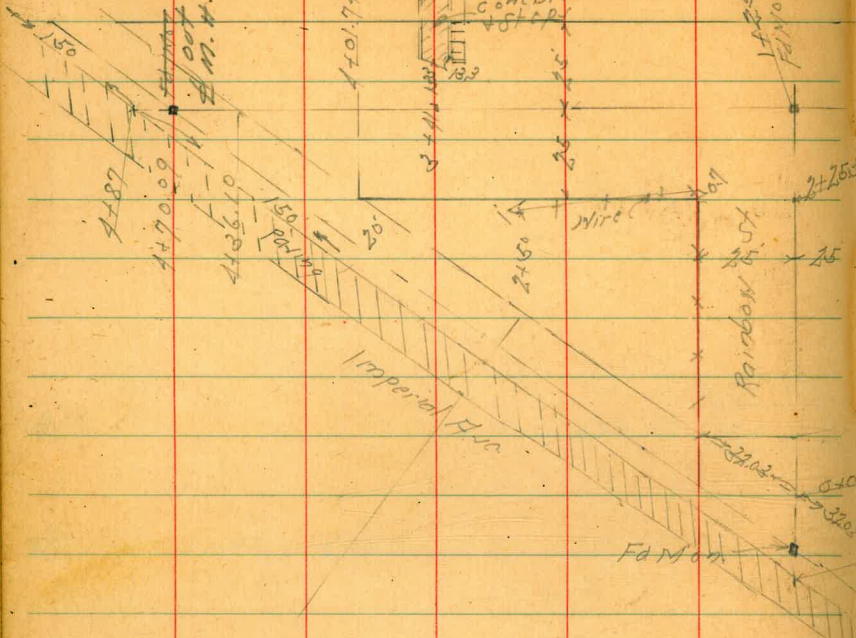
10+67

287
 21-1-11-1-5
 Conc. Walk

274.12

274.12

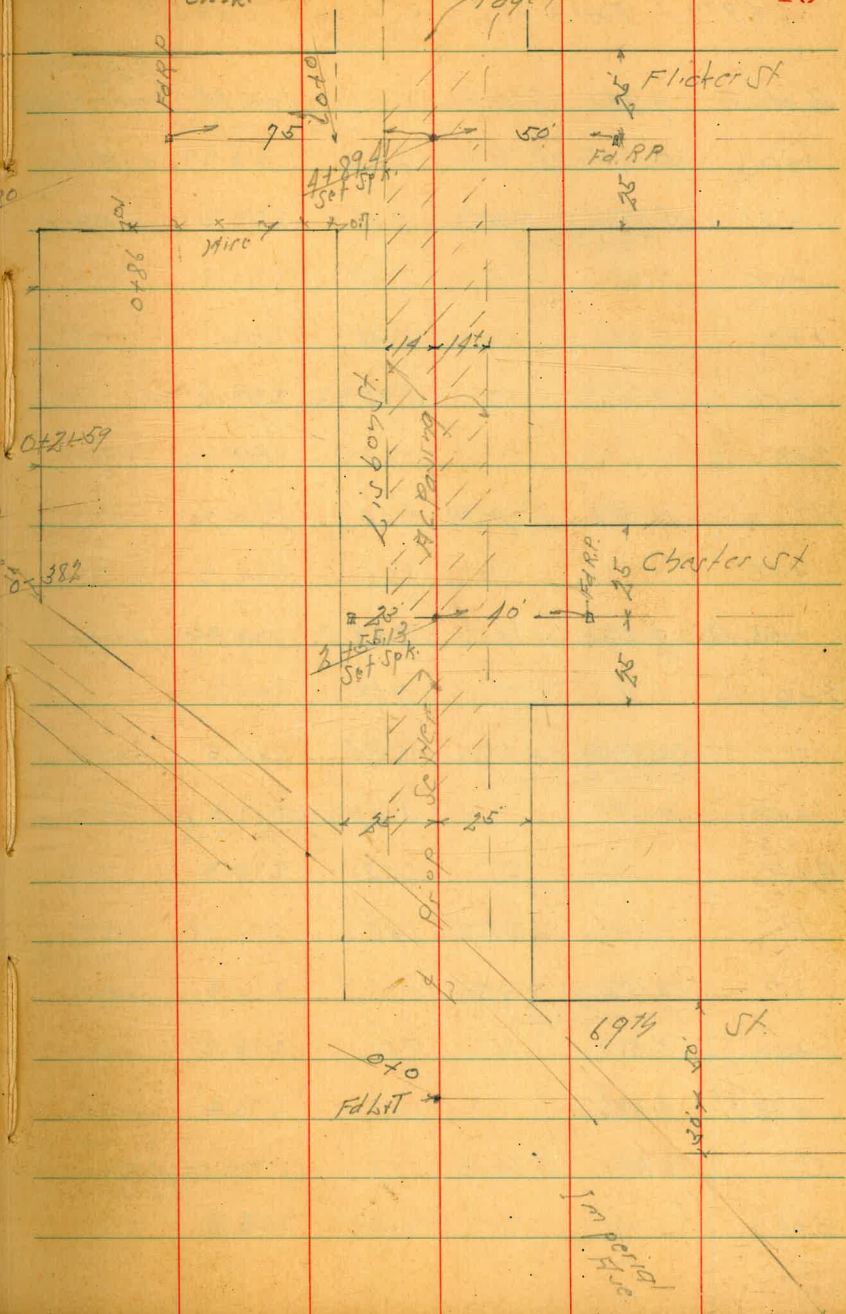
Proposed Sewer Lisbon St
 69th St to East Line of Lot 58



Indexed
 C.F.K.

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Levels Proposed Sewer Lisbon St
69th to East Line Lot 58 Lisbon Town Site

286.44

BM	7.95	261.39	252.44	Sp. Box Cdn. Imperial 4896
0+0	= 50' W of EL 69th St	8.00	253.39	on HC Pav.
+31	32' Rt of 1/2 - NW 1/4 Frame Bldg	8.12	253.3	on Floor
+50		6.54	254.9	
1+0		5.24	256.1	
+50		3.78	257.6	
2+0		1.75	259.6	
TP	11.53	272.29	0.63	260.76
+50		10.11	262.2	
+55.13	= 1/2 Chester St	9.88	262.4	on Spt
3+0		7.68	264.6	
"	365' W of 1/2 x S 1/4 Calif House	5.84	266.5	on Floor
+50		5.02	267.3	
4+0		2.02	270.3	
TP	9.90	280.73	1.46	270.83
+41	58' Lt of 1/2 - 1/2 x S 1/4 Frame House	4.26	276.4	on Floor
+50		7.50	273.2	
+89.91	= 1/2 Flicker	5.32	275.4	on Spt
TP	11.03	286.44	5.32	275.41 on Spt 1/2 Flicker + Lisbon
5+0		10.51	275.9	

5+41	393' Lt of 1/2 - 1/2 x S 1/4 of Calif House	5.21	281.2	on Floor
+50		8.14	278.3	
6+0		5.55	280.8	
+50		2.94	283.5	
7+0		0.53	285.9	
TP	11.57	297.48	0.53	285.91
7+39.76	= 1/2 Pidgeon St	9.85	287.63	on Spt
+50		9.46	288.0	
8+0		7.84	289.7	
"	20.58' Lt of 1/2 - 1/2 x NW 1/4 Stucco House	5.18	292.3	on Floor
"	47' Lt of 1/2 - 1/2 x S 1/4 Shingle House	1.88	295.6	on Floor
+50		6.90	290.6	
+83	52' Rt of 1/2 - 1/2 x NW 1/4 Calif House	5.5	292.0	on Floor
9+0		6.32	291.1	
+50		5.84	291.7	
10+0		5.13	292.4	
+50		4.18	293.3	
11+0		2.81	294.7	
+50		0.99	296.5	
TP	11.77	308.85	0.40	297.05

Lisbon St.

308.85

17

11+58	50' Lt of $\frac{1}{2}$ - $\frac{1}{2}$ x Sly Frame House	7.00	301.9	07 Floor
12+0		10.27	298.5	
+50		7.98	300.9	
13+0		5.50	303.3	
+41	65' Rt of $\frac{1}{2}$ - $\frac{1}{2}$ x Stucco House	7.62	301.3	07 Floor
+50		3.54	305.4	
14+0		2.51	306.4	
+50		2.33	306.6	
+75	87' Lt of $\frac{1}{2}$ - $\frac{1}{2}$ x Sly Frame House	7.85	317.4	07 Floor
+85	65' Rt of $\frac{1}{2}$ - $\frac{1}{2}$ x Stucco House	4.3	304.6	07 Floor
15+0		3.74	306.1	
+50		3.50	305.3	
16+0		4.56	304.2	
+50		5.88	303.0	
+96.46	F Line Lot 58	7.38	301.4	07 Spt
BM		7.88	300.97	3/4 Pipe Sk Lisbon Fl. Lot 58 300.97 Page 14

Cross Section Flicker St.
 Lisbon St to Imperial Ave
 Sketch page 15

indexed
 C.S.M.

May 29-46
 Rt. F 18

+52 18.7 W of $\frac{1}{2}$ My Power Pole

+50

LT = W

$$\begin{array}{r} 277.1 \\ 71 \\ 25 \\ \hline 60 \\ 13 \\ \hline 6.5 \\ 10 \\ \hline 59 \\ 57 \\ \hline 28 \\ 16 \\ \hline 21 \\ 2.5 \end{array}$$

+25.04 = $\frac{1}{2}$ Rainbow 6.36 276.59 02 May

$$\begin{array}{r} 277.3 \\ 69 \\ 25 \\ \hline 56 \\ 14 \\ \hline 60 \\ 12 \\ \hline 60 \\ 10 \\ \hline 57 \\ 55 \\ \hline 42 \\ 7 \\ \hline 33 \\ 10 \\ \hline 23 \\ 2.5 \end{array}$$

140

$$\begin{array}{r} 277.2 \\ 65 \\ 25 \\ \hline 58 \\ 15 \\ \hline 61 \\ 14 \\ \hline 60 \\ 10 \\ \hline 57 \\ 56 \\ \hline 35 \\ 10 \\ \hline 26 \\ 2.5 \end{array}$$

+94

$$\begin{array}{r} 276.0 \\ 70 \\ \hline 287.2 \\ 287.2 \\ \hline 287.2 \\ 287.2 \\ \hline 287.2 \\ 287.2 \\ \hline 287.2 \\ 287.2 \end{array}$$

+50

$$\begin{array}{r} 276.6 \\ 72 \\ 25 \\ \hline 65 \\ 18 \\ \hline 69 \\ 16 \\ \hline 68 \\ 10 \\ \hline 64 \\ 55 \\ \hline 47 \\ 10 \\ \hline 37 \\ 2.5 \end{array}$$

0+0 = N.L. Lisbon St.

$$\begin{array}{r} 275.7 \\ 78 \\ 25 \\ \hline 84 \\ 17 \\ \hline 80 \\ 10 \\ \hline 7.5 \\ 6.1 \\ \hline 57 \\ 10 \\ \hline 50 \\ 2.5 \end{array}$$

B.M 7.54 282.95

275.41

Spike 2
 Lisbon +
 Flicker
 Page 16

282.95

Flickerst.

+32

- 792 21' ht of 2nd Fly Poster Pole

370

+92

+63

+50

2+0

282.95

Lt.

2

Rt

19

23098

10.00

12.33

12.33

12.33

12.33

12.33

12.33

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121
33

111
25

95
14

99
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96
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90
10

52
25

273.4

269.1

139

139

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27
25

74
13

276.2

68

66

33
16

28
25

282.95

139

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Flicker St.

Lt.

S

Rt.

20

4+87 = Fly Edge Pavmg Taken on Line Pavmg

12.24 11.82 11.45 11.20 10.91 10.46 10.00
 $\frac{150}{150}$ $\frac{100}{100}$ $\frac{50}{50}$ $\frac{260.5}{260.5}$ $\frac{50}{50}$ $\frac{100}{100}$ $\frac{150}{150}$

4+7009 = East 20' Line Imperial 11.55 260.19 on Map

11.23 11.0 11.3 10.8 10.8
 $\frac{260.7}{260.7}$ $\frac{10}{10}$ $\frac{10}{10}$ $\frac{25}{25}$ $\frac{25}{25}$
 Fly Pav

4+36.10

16.6 9.8 8.8 8.8 8.5 8.3 7.6 8.0
 $\frac{263.2}{263.2}$ $\frac{25}{25}$ $\frac{10}{10}$ $\frac{10}{10}$ $\frac{7}{7}$ $\frac{7}{7}$ $\frac{25}{25}$

TP 0.17 271.74 11.38 271.57

271.74

4+01.74 = Fly Line of Imperial on Lt.

19.2 17.1 14.6 14.3 14.3 8.3 7.7
 $\frac{268.7}{268.7}$ $\frac{35}{35}$ $\frac{25}{25}$ $\frac{8}{8}$ $\frac{10}{10}$ $\frac{10}{10}$ $\frac{16}{16}$ $\frac{25}{25}$

+50

13.2 12.1 11.1 11.0 11.0 11.0 6.3 6.0
 $\frac{272.0}{272.0}$ $\frac{35}{35}$ $\frac{25}{25}$ $\frac{15}{15}$ $\frac{10}{10}$ $\frac{10}{10}$ $\frac{10}{10}$ $\frac{22}{22}$ $\frac{25}{25}$

3+41

12.6 12.1 10.9 10.7 10.5 10.8 11.30 10.98 10.77
 $\frac{272.5}{272.5}$ $\frac{35}{35}$ $\frac{25}{25}$ $\frac{15}{15}$ $\frac{10}{10}$ $\frac{10}{10}$ $\frac{10}{10}$ $\frac{10}{10}$ $\frac{10}{10}$ $\frac{272.16}{272.16}$
 18.5-21.5
 25.0-27.0
 28.0-30.0
 31.0-33.0
 34.0-36.0
 37.0-39.0
 40.0-42.0
 43.0-45.0
 46.0-48.0
 49.0-51.0
 52.0-54.0
 55.0-57.0
 58.0-60.0
 61.0-63.0
 64.0-66.0
 67.0-69.0
 70.0-72.0
 73.0-75.0
 76.0-78.0
 79.0-81.0
 82.0-84.0
 85.0-87.0
 88.0-90.0
 91.0-93.0
 94.0-96.0
 97.0-99.0
 100.0-102.0
 103.0-105.0
 106.0-108.0
 109.0-111.0
 112.0-114.0
 115.0-117.0
 118.0-120.0
 121.0-123.0
 124.0-126.0
 127.0-129.0
 130.0-132.0
 133.0-135.0
 136.0-138.0
 139.0-141.0
 142.0-144.0
 145.0-147.0
 148.0-150.0
 151.0-153.0
 154.0-156.0
 157.0-159.0
 160.0-162.0
 163.0-165.0
 166.0-168.0
 169.0-171.0
 172.0-174.0
 175.0-177.0
 178.0-180.0
 181.0-183.0
 184.0-186.0
 187.0-189.0
 190.0-192.0
 193.0-195.0
 196.0-198.0
 199.0-201.0
 202.0-204.0
 205.0-207.0
 208.0-210.0
 211.0-213.0
 214.0-216.0
 217.0-219.0
 220.0-222.0
 223.0-225.0
 226.0-228.0
 229.0-231.0
 232.0-234.0
 235.0-237.0
 238.0-240.0
 241.0-243.0
 244.0-246.0
 247.0-249.0
 250.0-252.0
 253.0-255.0
 256.0-258.0
 259.0-261.0
 262.0-264.0
 265.0-267.0
 268.0-270.0
 271.0-273.0
 274.0-276.0
 277.0-279.0
 280.0-282.0
 283.0-285.0
 286.0-288.0
 289.0-291.0
 292.0-294.0
 295.0-297.0
 298.0-300.0

282.95

282.95

Cross Section Pidgeon St
Lisbon to Foster St
Sketch page 7

indexed
C.S.K.

See F.B. 1766 9/14/49
21
C.H.S.

+70
TP 8.35 307.69 0.47 299.34

+50 18 ft of 2" x 1/4" Paver Paving

+30

+10

+50

81
35

+25

0+0 = N.L. Lisbon

B.M 12.18 299.81 287.63

Spike 2
Lisbon v
Pidgeon
Page 16

Lt. W S Rt. E
Mord. 16
5.500721
of Foster
Haddell
7/11/27

300.6
94 8.7 8.6 7.2 7.4
25 25 19 15 12 71 73 5.3 3.8
5 10 25

307.69

298.4
1.40
39.5
H.W. of Floor
2.1 1.5
2.1 1.5
2.1 1.5
2.1 1.5
17 17 7.9 7.8
3 25

296.3
4.8 3.9 3.5 4.1 3.3 3.5 3.7 1.8 1.3
35 25 19 16 5 5 3 7 25

291.7
7.7 7.5 8.4 8.1 7.8 8.1 8.3 6.9 6.2
25 16 14 10 5 3 10 25

289.9
10.4 9.9 9.6 10.6 10.2 9.9 9.8 9.1 7.7
35 25 18 13 10 8 10 25

288.1
11.4 11.5 12.8 12.2 11.7 11.6 10.2 9.5
25 20 17 10 5 10 25

299.81

+02 167 Lt of $\frac{1}{2}$ 2 1/2 Ply Parquet Panel
 +83 21' Rt of $\frac{1}{2}$ = Fly 12" Olive Tree
 +64 21' Rt of $\frac{1}{2}$ = Fly 12" Olive Tree Double

+50

+44 22' Rt of $\frac{1}{2}$ = Fly 12" Olive Tree

+24 203 Rt of $\frac{1}{2}$ = Fly 14" Olive Tree

+21

+03

2+0

307.69

302.5

$$\begin{array}{r} 96 \\ 35 \\ \hline 131 \end{array}$$

$$\begin{array}{r} 794 \\ 250 \\ \hline 1044 \end{array}$$

$$\begin{array}{r} 6.79 \\ 15.5 \\ \hline 22.29 \end{array}$$

$$\begin{array}{r} 58 \\ 10 \\ \hline 68 \end{array}$$

$$\begin{array}{r} 52 \\ 10 \\ \hline 62 \end{array}$$

$$\begin{array}{r} 4.3 \\ 19 \\ \hline 23.3 \end{array}$$

$$\begin{array}{r} 1.5 \\ 19 \\ \hline 20.5 \end{array}$$

$$\begin{array}{r} 0.6 \\ 25 \\ \hline 25.6 \end{array}$$

Notes: 2507 Wall, 14' x 7', Fly Comp 30' wide

302.6

$$\begin{array}{r} 93 \\ 95 \\ \hline 188 \end{array}$$

$$\begin{array}{r} 79 \\ 25 \\ \hline 104 \end{array}$$

$$\begin{array}{r} 58 \\ 10 \\ \hline 68 \end{array}$$

$$\begin{array}{r} 51 \\ 48 \\ \hline 99 \end{array}$$

$$\begin{array}{r} 1.8 \\ 18 \\ \hline 19.8 \end{array}$$

$$\begin{array}{r} 0.5 \\ 25 \\ \hline 25.5 \end{array}$$

936
 13807 Code Drive
 766
 21' = 24' Fly 12" Ribbon
 21' Code Drive

300.0

$$\begin{array}{r} 77 \\ 13 \\ \hline 90 \end{array}$$
 77 = 24' Fly from House on floor

836
 24' = 24' Fly 12" Code Wall

301.8

$$\begin{array}{r} 85 \\ 35 \\ \hline 120 \end{array}$$

$$\begin{array}{r} 83 \\ 25 \\ \hline 108 \end{array}$$

$$\begin{array}{r} 87 \\ 20 \\ \hline 107 \end{array}$$

$$\begin{array}{r} 69 \\ 14 \\ \hline 83 \end{array}$$

$$\begin{array}{r} 59 \\ 59 \\ \hline 118 \end{array}$$

$$\begin{array}{r} 4.0 \\ 10 \\ \hline 14 \end{array}$$

$$\begin{array}{r} 2.3 \\ 25 \\ \hline 27.3 \end{array}$$

307.69

410

+94

TP 334 302.80 8.23 299.46

+68

+52

+50

+43 20' RT of 1/2 = ELY 5" Olive Tree

3+22

307.69

Lt.

2

RT.

23

298.6

9.2 8.1 5.5 4.2 3.3 3.3 2.8 2.3
35 25 10 10 10 16 21 25

8.81
8500 Cone
Dr. Mt
5.97
16.5 = 2 x ELY 2.5"
Cand. Dr. V. = 309.80

295.49

12.20

3.38

3.38

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12.5 12.4 12.2 7.4 7.3 6.1 5.6 3.0 1.1
35 25 17 16 Top Rubbl 10 15 25

9.7 9.6 8.98 7.4 7.3 6.1 5.5 2.9 1.2
35 25 17 16.5 Top Rubbl 10 15 25

298.67
9.7 8.9 8.7 6.9 6.1 5.4 4.9 2.5 0.6
35 25 16 15 Top Rubbl 10 15 25

307.69

Pidgeon St.

BM 17.87 260.20

TP 0.18 278.07 12.21 277.89

TP 0.12 290.10 12.82 289.98

5 + 50.04 = W.L. Foster 10.37 292.43

+ 31

+ 19

5 + 100.04 = S.L. Foster

+ 56 16' H of 1/2 = W.L. Parker Polc.

+ 50

At 41

302.80

27 Mon
Flicker
Imperial
280.19 P20

27 Mon
2 Pidgeon
W.L. Foster

300.94
292.97
8.51

Lt.

2

84

24

170 149 116 292.6
35 25 10 10.2 8.3 4.9 2.5 + 2.5
10

161 143 115 293.4
35 25 17 101 94 79 4.8 3.2
10 25 25

219 173 146 289.4
50 25 10 84 115 9.6 5.8
15 25 35

162 150 145 293.6
35 25 19 111 92 76 4.8
10 25

125 112 87 295.4
35 25 10 7.4 5.9 3.7 2.7
10 21 25

186
27.5 + W.L. Foster
207.2 + W.L. Foster
370.7 + W.L. Foster

302.80
1.90
300.27

Proposed Survey No Home Lane

From Samocha Road

Sketch Page 7

BM	9.48	276.84	267.36	on Hub 1434.65 Samocha Road Page 7
0+0	= 2+42.91	Samocha Rd	12.78	264.06
+18			11.9	264.9
+31			10.7	266.1
+50			10.0	266.8
+70			8.6	268.2
+50			6.7	270.1
"	75 West of $\frac{1}{2}$		5.0	271.8
2+0			3.9	272.9
+50			1.1	275.7
TP	11.67	288.43	0.08	276.76
3+0			9.4	279.0
+15	135 ft of $\frac{1}{2}$ = $\frac{1}{2}$ + Ely Frame House	4.92		283.51
+50		6.7		281.7
+57	78 ft of $\frac{1}{2}$	5.3		283.1
"	" " " " + Wly Calif House	2.45		285.98
4+0		3.7		284.7
+50		0.8		287.6
TP	12.76	300.45	0.74	287.69
+70		11.4		289.1

Indexed
c.s.R.

300.45

May 31-46
Station
of
17000
H 1107

25

4+93.5	254	7.5	8.7	291.8
5+0	0.0	"	8.15	292.30
+18	114	7.5	8.2	292.3
+50			6.1	294.4
+96	41	Rt of $\frac{1}{2}$ = $\frac{1}{2}$ + Wly Frame House	0.23	300.22
6+0	2	Ely Oil & Rock Pav.	2.6	297.9
TP	12.42	312.43	0.44	300.01
+50			9.6	302.8
+80	118	Lt of $\frac{1}{2}$	4.1	308.3
"	118	Lt of $\frac{1}{2}$ = S.E. Cor Frame House	1.92	310.51
7+0	2	Ely Oil & Rock Pav.	4.1	308.3
TP	12.81	325.23	0.01	312.42
+26	41	Rt of $\frac{1}{2}$ = $\frac{1}{2}$ + Wly of Frame House	10.4	314.8
+50			9.6	315.6
"	71	Rt of $\frac{1}{2}$ = $\frac{1}{2}$ + Wly of Frame House	10.5	314.7
+83	35	Rt of $\frac{1}{2}$	4.1	321.1
"	35	Rt of $\frac{1}{2}$ = NW Cor Frame House	2.70	323.53
+95	111	Lt of $\frac{1}{2}$	1.6	323.6
"	111	Lt of $\frac{1}{2}$ = S.E. Cor Frame House	1.9	327.1
8+0	2	Ely Rock & Oil Pav.	2.3	327.5

		325.23			
TP	12.00	336.42	0.81	324.42	
8+50			6.5	329.9	
9+0	Z = 2.5' W of E Edge Pav		0.9	335.5	
TP	8.10	343.62	0.90	335.52	
+30			6.0	337.6	
+50			5.5	338.1	
+80	28.4' W of $\frac{1}{2}$ = N.E. Cor From House		7.55	336.07	on Floor
10+0	$\frac{1}{2}$ = $\frac{1}{2}$ 0.1' W of Rock Pav		5.5	338.1	
+27	9' W of $\frac{1}{2}$ = E.H. Stucco House		8.0	335.6	on Floor
+50			5.7	337.9	
+55	12.2' W of $\frac{1}{2}$ = E.H. Calyf House		10.5	333.1	on Floor
+80			6.2	337.4	
TP	4.30	339.82	8.10	325.52	
TP	1.02	329.01	11.83	327.99	
TP	1.40	317.54	12.87	316.14	
TP	3.63	309.19	11.98	305.56	
BM			8.23	300.96	3" Pipe S.L. 156.02 Feet W of Lot 52 300.97 Page 14

Cross Section Rainbow St.
 Imperial Ave to Fichter St.
 Sketch Page 15

Indexed
 C.S.N.

Just 1-4
 System
 of eastern
 Model
 #1102

Lt. N

8

Rt. S

27

1+0

112
50

100
25

95
12

266.2
8.9

76
10

68
25

0+50

136
25

133
14

262.8
12.3

143
5

110
17

143
25

IP

12.11

275.12

0.01

263.01

275.12

+21.59

32
25

40
10

258.7
7.1

37
10

21
20

22
25

+06

74 Lt of 2" Fly 16 Fuc. Trce

+01

2 Lt of 2" Fly 17 Fuc. Trce

0+0

East Line of Imperial Taken on Diagonal

33
32.11

49
15

257.0
6.0

44
15

66
32.52

0-26.42

7.11

02 Mon

0-38.2 - Fly Paving on Imperial taken on line of passage

574
100

626
50

257.21
6.81

726
50

772
100

B.M

9.58

263.02

253.44

SW Box Cul
 2" Pipe
 Imperial 76913

267.02

Rainbow St.

Lt=N

2

pt-S

28

BM

4.71

276.59

07 May
W. Flicker +
Rainbow
276.59
Page 18

27253 = W.L. Flicker

54
28

54
12

275.9
54

42
15

53
25

JP

7.30

281.30

1/2

274.00

281.00

2+0

06
35

06
25

14
18

07
16

273.9
12

11
13

09
25

1+50

60
35

55
25

53
12

269.7
54

44
20

45
25

1+29

268.79
6.82

15 - SF Cor Fram
1 hour on floor

275.12

275.12

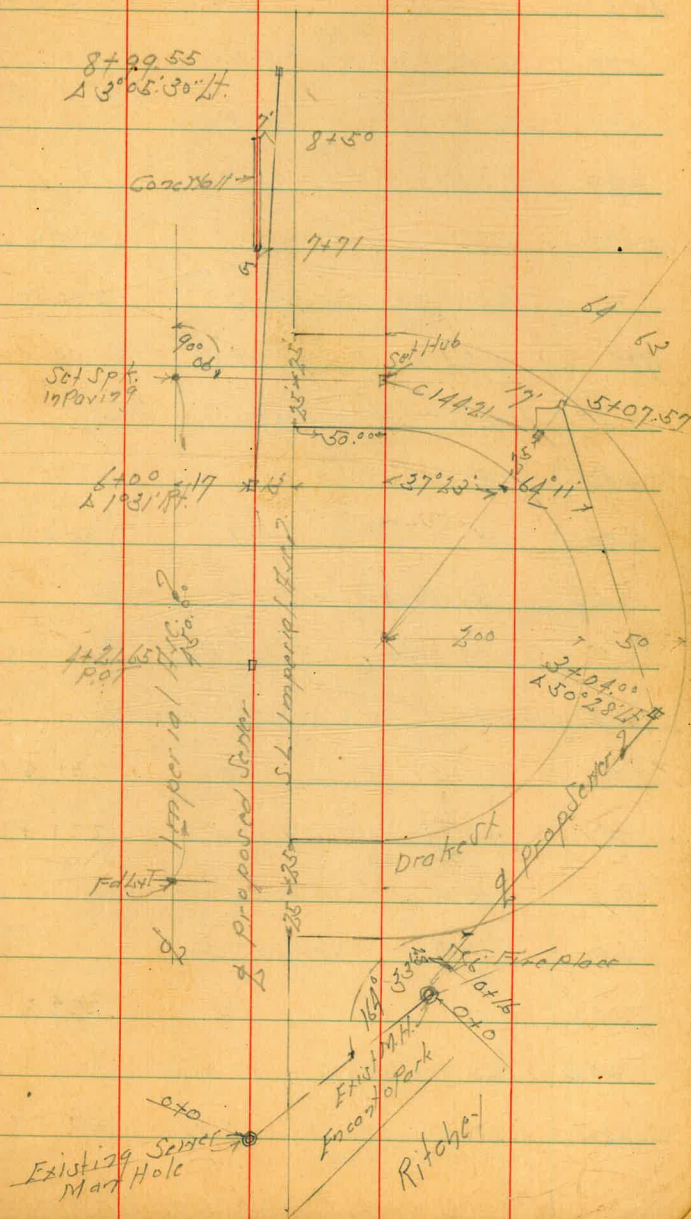
Proposed Sewer Imperial Ave
Ritchey St to Foster St.

BM	392	234.22	230.20	5' L. Woodma- 5' L. Imperial on Sealed Cover
040	Exist. Man Hole	12.60	221.62	
+10		12.7	221.5	
+30		6.7	227.5	
+37	3' R of 1/2 - 1 1/4 Local Tree 18" Diam			
+50		6.1	228.1	
+55	4' R of 1/2 - 1 1/4 Acacia Tree			
+82	4' R " " " " " "			
+10		5.3	228.9	
+98	5' R of 1/2 - 1 1/4 Acacia Tree			
+14	5' R " " - 1 1/4 Tel. Pole			
+21	2' R " " - 1 1/4 Anchor Pole			
+31	4' R " " " " " 7" Acacia Tree			
+50		5.0	229.2	
"	9' L of 1/2 - 1 1/4 Strip 4.6 Paving		229.6	
+55	5' R of 1/2 - 1 1/4 4" Acacia Tree			
+82	3.5' R " " " " 9" " "			
+10		4.4	229.8	
+07	4.5' R of 1/2 - 1 1/4 5" Acacia Tree			
+33	4' " " " " 9" " "			

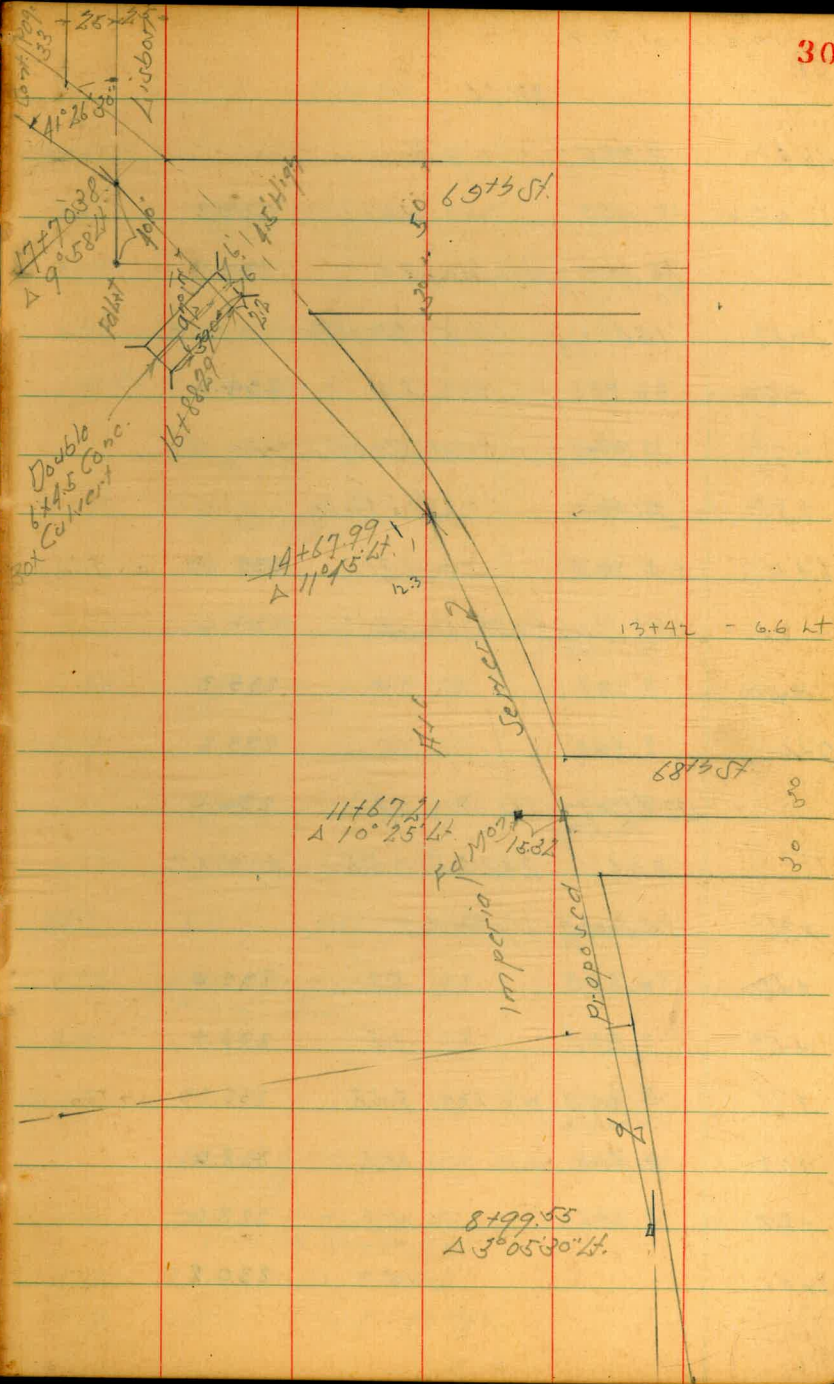
June 17-46
S. 8802
Hadden
Allen

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29



		234.22		
2+50		4.0	230.2	
+79	5' Rt of $\frac{1}{2}$ - N 1/4 Acacia Tree			
+87	5.5' Rt " " Tel Pole			
+99	4' Rt " " 7' Acacia Tree			
3+0		2.6	230.6	
"	9.5' Lt of $\frac{1}{2}$ - S 1/4 Strip 27		230.5	
JP	5.84	236.24	3.82	230.40
+22	4.2' Rt of $\frac{1}{2}$ - N 1/4 12' Acacia Tree			
+45	4' " " " 12' " "			
+50		5.3	230.9	
+68	4.1' Rt of $\frac{1}{2}$ - N 1/4 Acacia Tree			
+84	4.4' " " " " Post & Tel Pole			
+91	4.1' " " " " 12' Acacia Tree			
4+0		4.6	231.6	
"	9.1' Lt of $\frac{1}{2}$ - S 1/4 Strip 48		231.4	
+11	4' Rt of $\frac{1}{2}$ - N 1/4 8' Acacia Tree			
+30	4' Rt " " - N 1/4 Tel Pole			
+50		4.1	232.2	
+55	3' Rt of $\frac{1}{2}$ - N 1/4 9' Acacia Tree			
+63	2.5' Rt of $\frac{1}{2}$ - N 1/4	2.32	233.92	02 Floor
	5' 1/2" 1916 House			



236.24

4+98	2' Rt of 1/2" 11/4 7" Acacia Tree			
5+0		3.0	233.2	
"	9/16 Lt of 1/2" Sly Strip Paving	3.3	232.9	
+22	1.5 Rt of 1/2" 11/4 5" Dead Acacia Tree			
+50		2.0	234.2	
+72	2' Rt of 1/2" 11/4 12" Acacia Tree			
+88	2.5 Rt " " Tel Pole			
6+0	4 1° 31' Rt	1.21	235.03	on Stab
"	9/16 Lt of 1/2" Sly Strip Paving	1.6	234.6	
+50		0.9	235.3	
7+0		1.0	235.2	
"	122 Lt of 1/2" Sly Strip Paving	0.2	236.0	
TP	8.06	243.75	0.55	235.69
+26	1.6 Lt of 1/2" Sly Tel Pole			
+50		8.8	235.0	
+57		8.4	235.4	
+71	5 1/2 Lt of 1/2" 11/4 Top Couch	8.52	235.23	on Top
+72	8.0 Lt of 1/2" Sly	15.2	228.6	
+85	" " "	15.2	228.6	
8+0		13.0	230.8	

243.75

8+41		13.0	230.8	
+56	7' Half-Hy Conc Walls	7.04	236.71	on Top
+62		6.5	238.3	
+71	1' Lt of 1/2" Sly Tel Pole			
+99 ⁵⁵	4 3° 05' 30" Lt	4.17	239.58	on Stab
"	176 Lt of 1/2" Sly Strip Paving	3.6	240.2	
9+40	56.5 Rt of 1/2" 11/4 Shingle House	3.6	240.2	on Floor
+50		2.6	241.2	
+74	5.5 Lt of 1/2" Sly Acacia Pole			
+84	2.5 Rt of 1/2" 11/4 Calf House	1.9	241.9	on Floor
10+0		1.1	242.7	
"	146 Lt of 1/2" Sly Strip Paving	0.9	242.9	
+17	5 Lt of 1/2" Sly Tel Pole			
TP	8.01	231.07	0.69	243.06
+25	74 Rt of 1/2" 11/4 Frame House	8.4	242.67	on Floor
+50		7.2	243.9	
11+0		5.2	245.9	
"	146 Lt of 1/2" Sly Strip Paving	5.7	245.4	
+10	21 Rt of 1/2" 11/4 Stucco Shop Store House	5.3	245.8	on Floor
+12	5 Lt of 1/2" Sly Tel Pole			
+19	1 Lt " " Sly 4" Sign Pipe			

251.07

11+19	16' R/O of $\frac{1}{2}$ = NY + 2 16.3 4.72 Cable 15' 16.3 d 3 Gas Pumps	246.35	on Conc
+36	3.4 ft of $\frac{1}{2}$ = $\frac{1}{2}$ Fire Hyd.		
+40	NY Oil & Rock Pav. 4.7	246.4	
+67.21	$\frac{1}{2}$ 6.8' of $\frac{1}{2}$ $\frac{1}{2}$ 10' 25' of $\frac{1}{2}$	246.91	on Stab
+78	NY Oil & Rock Pav. 4.2	246.9	
12+0		247.6	
"	14.8 ft of $\frac{1}{2}$ SLY Strip Paving	247.7	
+09	9.2 ft of $\frac{1}{2}$ = NY Frame Bldg	248.54	on Floor
+50		248.4	
+70	NY Oil Pav. For Gas Station	248.5	
13+0		248.8	
"	8.2 ft of $\frac{1}{2}$ SLY Strip Paving	248.8	
+25	2.2 ft of $\frac{1}{2}$ = NY Bldg	249.2	on Floor
+42	11 ft of $\frac{1}{2}$ = NY + $\frac{1}{2}$ 218 Cable Island 4 Gas Pumps	249.45	on Conc
+50	on Oil Pav	249.3	
+57	2.87 ft = $\frac{1}{2}$ NY Bldg on Floor	249.54	
14+0		249.4	
"	11' 1/2 of $\frac{1}{2}$ = SLY Strip Paving	249.7	
+12	NY Oil Paving For Gas Station	249.5	
+50		249.5	
+51	5.0 ft of $\frac{1}{2}$ = $\frac{1}{2}$ NY Frame Floor	248.6	on Floor

251.07

14+67.99	11' 45" of $\frac{1}{2}$	1.54	249.53	on Stab
TP	7.49	257.02	1.54	249.53
+94	1.5 R/O of $\frac{1}{2}$ = NY Anchor Pole			
15+0		6.3	250.7	
"	12.1 ft of $\frac{1}{2}$ SLY Strip Paving	6.9	250.6	
"	2.0 ft of $\frac{1}{2}$	9.1	247.9	Ground
+50		6.2	250.8	
16+0		5.5	251.5	
"	6' 1/2 of $\frac{1}{2}$ SLY Strip Paving	5.3	251.7	
"	15' R/O of $\frac{1}{2}$	9.6	247.4	Ground
+50		4.6	252.4	
+88.29		5.43	251.57	Top Con Box
"	2.2 ft of $\frac{1}{2}$ NY Box Culv.	10.26	246.64	on Flanking
17+0		4.4	252.6	
"	4.5 ft of $\frac{1}{2}$ SLY Strip Pav.	3.9	253.1	
+13	= SLY Oil & Rock Paving	4.1	252.9	
+50	on Oil & Rock Pav.	2.05	253.95	
+70.38	9' 58" of $\frac{1}{2}$ = $\frac{1}{2}$ 4.56 on St.	2.39	254.41	on Roof Deck 2" Pipe 5/16 Box Culv Imperial 480% 253.44
BM	7.01	260.42	3.61	253.41
18+0		5.7	254.7	

		26795			
23150			70	261.0	
2410			75	260.5	
	7' Lt of d = Ely Strip		78	260.2	
+50	Paving		72	260.8	
2540			71	260.9	
"	11' Lt of d = Ely Strip		72	260.8	
+11.16	1.55' 02' 30" RT		685	261.10	at Stub
+50			59	262.1	
+90			28	265.2	
2640			0.2	267.8	
TP	12.13	278.89	1.19	266.76	
+18			8.5	270.4	
+30			41	274.8	
TP	12.55	290.56	0.88	278.01	
+50			10.9	279.7	
+78			54	285.2	
2740			25	288.1	
TP	8.69	297.38	1.87	288.69	
+21.60	1/2 Pidgeon		6.99	290.39	at Stub
B.M.			1.95	292.43	Nov. 8. Pidgeon Mt. Foster 292.43 Page 34

Levels Proposed Center Atkins Ave
 And 69th St. North East.
 Sketch Page 33

BM	7.25	260.69	253.44	2" pipe 5-22 Box Culv. Imperial & 69th St.
+40	= First Man Hole Atkins + 69th St.	7.11	252.98	02 RR
+50		7.6	253.1	
+69	42 Plot of NW 20' Paper Tree			
+76	55 RI " " 13 " " 53 1/2' of Wire Fence			
+10		6.4	254.3	
+11	31 Plot of NW 4' Tol Pole			
+50		6.9	253.8	
+96.33	= 69° 23' 30" RT	6.81	253.88	02 RR
+16		6.8	253.9	
+28	= Bottom Post	11.1	249.6	
+46		2.5	258.2	
+50		5.5	255.5	
+59		5.1	254.6	
+65		5.8	256.9	
+74	= 2' RR	3.21	257.48	02 NW Rail
+82		3.4	257.3	
+89		4.4	254.3	
+70		6.8	253.9	
+08		8.6	252.1	

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 e.s.R.

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260.69

+18		8.8	251.9	
+27		8.9	256.8	
+41.4	= NW 1/2 Strip Pav 179	3.66	257.03	
+59.8	= SE 1/4 " "	3.00	257.39	
+65		2.3	257.4	
+76.42	= 21406.40	1.04	259.65	02 5/4 257.63-953

Levels Encanto Park + Drake St.
Proposed Sewer
Sketch Page 29

BM	4.17	234.47	230.30	217 S. 74 Imperial Ave W.L. Woodman
TP	12.29	240.44	228.15	
+40	Existing Man Hole	9.53	230.91	07 Rise
"	"	15.40	225.04	Flush Hole
+50		9.6	230.8	
+74	76' Lt off 1/2 SW Cor Frame House	9.12	231.32	07 Floor
+40		8.0	232.2	
+42	1/4 DIRT Road	6.9	234.0	
+60		6.2	234.2	
+40		5.6	234.8	
+11	60' Lt off 1/2 SW Cor Calif. House	7.05	233.39	07 Floor
+50	1/2 DIRT Road	4.0	236.4	
+80		3.4	237.0	
3 x 01°	150° 28' 41"	1.83	238.61	07 Stub
+21	1/4 DIRT Road	3.4	237.0	
+50		3.4	237.0	
+82	2' Rt off 1/2 6" Local Tree			
TP	3.14	240.65	229.3	237.51
+40		4.1	236.6	
+12	25' Lt off 1/2 Fly Tel Pole			

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240.65

June 21-46
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Waddell
Allen

36

+450	4.1	236.6	
+81	65' Rt off 1/2 SW Cor Frame House	+0.60	241.25 07 Floor
+50		5.6	235.1
+07.57		5.23	235.32 07 Stub
+09	2' Lt off 1/2 Fly 12" Pepper Tree		
+07.57	19.5' Lt off 1/2 SW Cor Stucco House	3.77	336.88 07 Floor
For Check	7.35	233.20	07 Hub 9458.81 2332 #166-52

F. Osborne
M. Coy
Hardin
Waddel

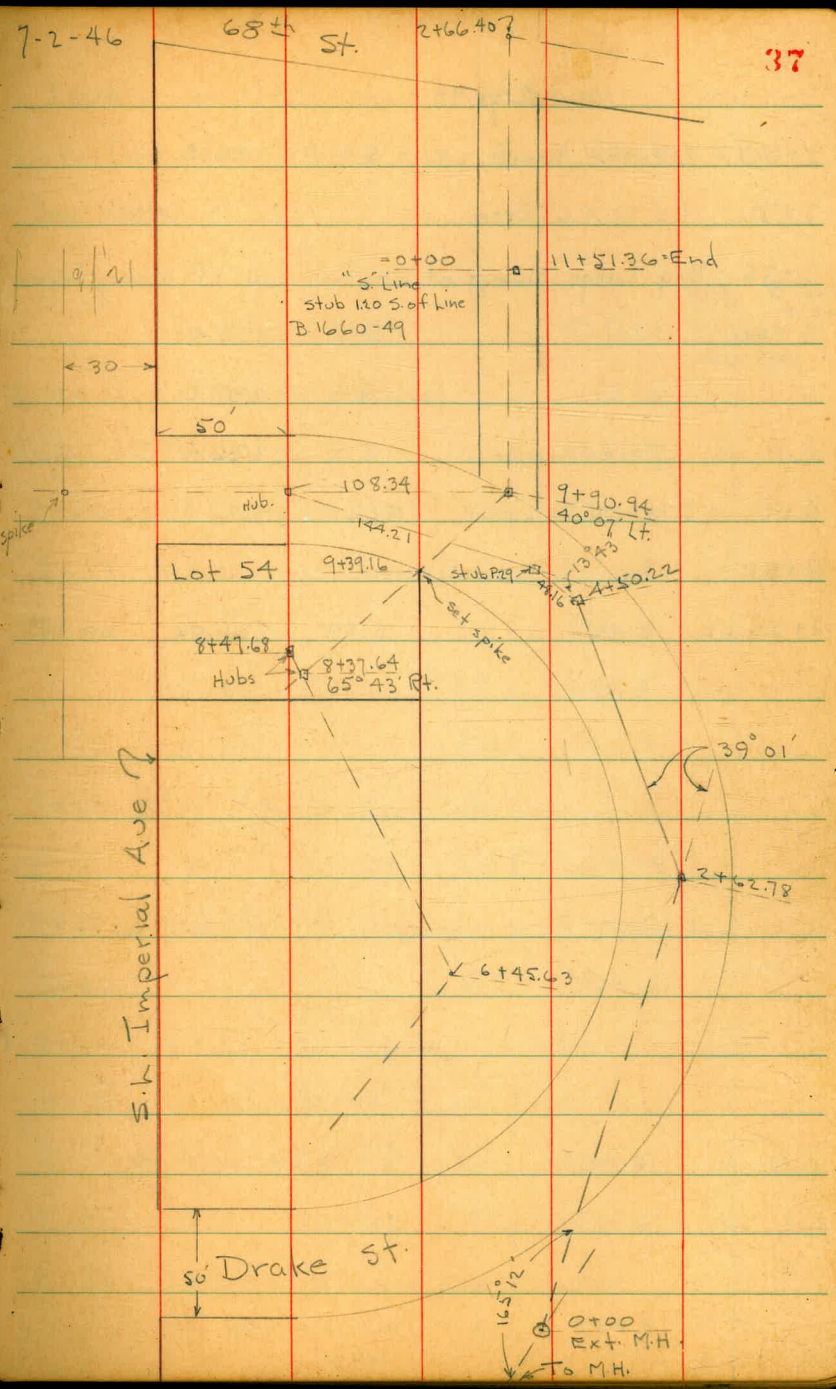
7-2-46

68th St. 2+66.40?

37

Levels on Prop. Sewer - new location
Encanto Park + Drake St.

B.M.	3.29	241.90	238.61	stub 3+04 T.36
0+00 =	∅ Exist M.H.	10.98	230.92	
	Incinerator 3' High			Inc.
0+15 =	∅ 6x3 Conc + Tile	11.7	230.2	ground at
0+28 =	4.8' Rt = ∅ 3" Euc. Tree			
0+50		11.0	230.9	
0+76 =	9' Rt = ∅ 12" Euc. Tree			
1+00		9.3	232.6	
	10' Rt	7.6	234.3	
	20 Lt.	11.3	230.6	
1+50		7.8	234.1	
2+00		7.0	234.9	
	10' Rt.	6.7	235.2	
	20 Lt.	8.6	233.3	
2+30		5.9	236.0	
2+62.78 =	Ang. 39° 01' Lt.	5.16	236.74	on stub.
3+00		5.3	236.6	
	10' Rt.	4.8	237.1	
	9' Lt. = wire fence	6.4	235.5	



241.90

3+50 - 2.8 Lt. = fence 5.4 236.5

3+72 - 9.5 Rt. = 6" Tree

3+85 - Beg. large clump of cactus on Lt. along fence

4+00 5.5 236.4

10 Rt. 4.7 237.2

7' Lt. = fence 5.5 236.4

4+12 - 5' Lt. = Tel. pole # 412442

4+48 - 8' Rt. = # 24" Euc.

4+50.22 = End 5.84 236.06 on stub.

38

Levels on New Line Prop. Sewer Thru
S.E. Cor. lot 54 + Alley E. of Drake st.

See sketch P. 37

10.17 236.49

226.32

Hub B1660
P. 52
8+47.68
New Elev.

Begin at 8+37.64 on old line

Angle 65°43' Rt. 10.20 226.29 on Hub

8+60 = # 8' Clump of Cactus 5.4 231.1

8+88 - 2.9 Lt. = # 2" Acacia

9+00 3.5 233.0

15' Rt. 3.7 232.8

15' Lt. 3.8 232.7

9+24 - 5' Rt. = # 6" Euc. Tree

T.P. 5.19 239.33 2.35 234.14

9+39.16 = lot Cor. # large clump of cactus

9+50 5.5 233.8

9+54 - 9.8 Rt. = # P. pole # 70934

9+84 14' Rt. = # 30" Euc. Tree

9+90.94 Angle 40°07' Lt 4.72 234.61 on stub.

T.P. 4.77 239.38 4.72 234.61 on stub.

9+98 - 28.7 Rt. = N.W. Cor. Stucco house

10+30 - 47' Rt. = N.E. Cor House 4.6 234.8 on #

	239.38		
10+30	- 47 Rt. = House ground at	3.5	235.9
" "	floor house	1.98	237.40
10+50		4.5	234.9
11+00 =	20" willow bush	4.2	235.2
"	15 Lt	4.6	234.8
"	15 Rt	3.8	235.6
11+22	w. bank wash	4.4	235.0
11+38 =	wash	10.5	228.9
"	15 Lt. - in wash	9.7	229.7
"	15 Rt. in wash	10.7	228.7
11+51.36 =	end = 0+00 of S line	6.83	232.55 on stub

Prelim. Location Prop. Sewer stub from
 E 68th E. on S. side Imperial Ave.

Req. at 11+67.21 - See P. 30 - Note: Topo. taken seems

Complete on other line - will just show E Profile
 on stub
 11+67.21 P. 32

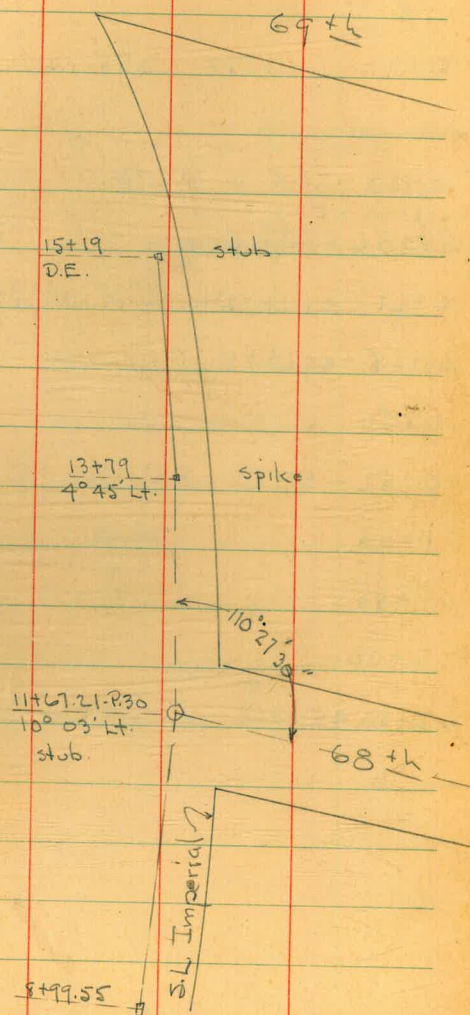
B.M.	7.24	254.15	246.91	
11+67.21 = Beg.	7.24	246.91	on stub.	
11+78.7 = edge of pave	7.30	246.9		
12+00 - 14' Lt. = Gas line	6.6	247.6		
+50	5.8	248.4		
13+00 - 8' Lt. = Gas line	5.4	248.8		
+50	4.9	249.3		
13+79 = Δ 4° 45' Lt.	4.70	249.45	on spike	
14+00 - 8' Lt. = Gas line	4.6	249.6		
+50	4.3	249.9		
15+00	3.4	250.8		
15+19 = D.E.	4.10	250.05	on stub.	
10 Rt.	6.4	247.8		
9.7 Lt. = Gas line				
11.3 Lt. = edge pave	3.31	250.84		

7-3-46

Osborne
 McCay
 Hardin
 Waddel

indexed
 C.R.K.

40



New location - Prop. Sewer - 69th + Lisbon
to miss Gas + Water Lines

D.M.	1.98	255.42	253.44	2" Pipe in Box Culvert
------	------	--------	--------	------------------------

0+00 on Lisbon Line P 15

0+00 = 34.5 E. of Ct.	1.10	254.32	on Pav.
-----------------------	------	--------	---------

0+08.4 = 2.3 Rt = F 8" Gate cap.

0+20.6 = edge pave	1.78	253.64	old Bld.
--------------------	------	--------	----------

0+21 = 4.1 Lt = Nly. Cor of Dubbed doorway on N.W. Cor.			
---	--	--	--

0+26.5 = 0.9 Lt = Sly. Cor. doorway	2.18	253.24	on floor
-------------------------------------	------	--------	----------

0+50	4.6	250.8	
------	-----	-------	--

0+52 = 5.3 Lt = S.W. Cor. Bld.

1+00	6.4	249.0	
------	-----	-------	--

+50	7.1	248.3	
-----	-----	-------	--

2+00	7.7	247.7	
------	-----	-------	--

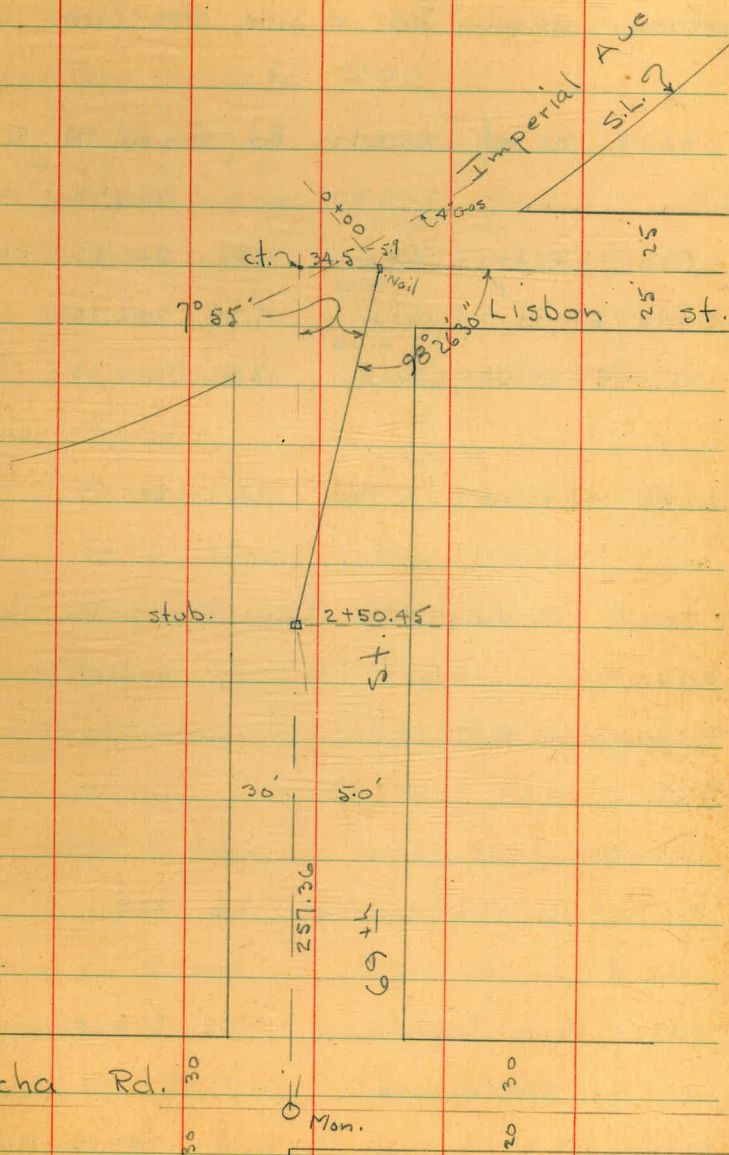
2+50.45 = end. join old line	8.04	247.38	on stub
------------------------------	------	--------	---------

7-3-46

Osborne
Mc Coy
Hardin
Waddel

Indexed
c.s.K.

59
41



Jamacha Rd.

Location of Houses and floor Eleu.
along Jamacha Rd. + side sts. - sketch 1681-32
68th St.

0+00 = E of Jamacha Rd. - Going N	Line			
BM.	6.27	247.20	240.93	Line = Base Noil 2+66.40 1660-49
0+33 - 52' Lt. = E Small frame House	4.87	242.33		Floor.
0+45 - 52' Rt. = E Med. fr. House	4.24	242.96		"
1+23 - 49' Lt. of E = E Med. fr. fr. House	2.82	244.38		
1+44 - 45' Rt. of E = E Med. fr. House	1.27	245.93		

Jamacha Rd. Going E.

0+00 = E.L. of 68 th (to match X-Sept.)				
E Jamacha = Base line				
B.M.	1.87	247.73	245.86	Mon. E Jam + 69 th
0+70 - 100' Rt. (S) = Vacant lot.	8.6	239.1		
0+92 - 49' Lt. = Foundation of Prop. House	3.05	244.68		Approx. floor
1+75 - 57' Rt. = E Small fr. House	3.98	243.75		Floor

		247.73		
1+91 - 48' Lt. = E of Found. of Prop. House	2.95	244.78		Approx. floor
2+42 - 43' Rt. = E of upstairs Apt over doub. gar.	4.93	242.80		Floor
2+83 - 73' Rt. = E Large stucco House	2.90	244.83		Floor
3+29 - 69' Lt. = E Med. frame House	2.02	245.71		Floor
4+00 - 85' Rt. = Vacant lot.	4.1	243.6		ground.
T.P.	10.89	256.75	1.87	245.86
5+04 - 50' Rt. = E Med. Frame House	8.37	246.38		Floor
6+00 - 75' Lt. Vacant	6.3	250.5		ground.
6+03 - 50' Rt. = E Med. frame House	5.38	251.37		Floor
7+00 - 116' Rt. = E Small frame House	7.63	249.12		Floor
7+30 - 50' Rt. = E Med. frame House	3.51	253.24		Floor
T.P. on Mon. E Chester	11.32	262.82	5.25	251.50

Note! E. of E.L. of 69th Base line or prop.
Sewer is 30' from N.L. and 20' from S.L. of Jamacha

8+00-60 Lt. = Vac. Lot	8.0	254.8	
8+45-60 Rt. = Vac. Lot.	8.8	254.0	
9+10-48' Rt. = Φ Med.	5.99	256.83	Floor
frame House			
B.M. For Flicker	0.45	262.37	on rock
9+89-48' Rt. = Φ small	4.64	258.18	Floor
Frame House			
10+68-61 Lt. = Φ Med.	0.88	261.94	
Stucco House			
11+00-80' Rt. = Vac. Lot.	4.7	258.1	
12+77-65' Rt. = Φ Small	+ 0.24	263.06	Floor.
frame House			
check B.M. Mon. & Pidgeon	3.59	259.23	1681 P. 45' 259.21

Pidgeon St. N. from Jamacha Rd.			
0+00 = 30' S. of N.L. Jamacha	Φ = base Line		
B.M.	12.71	271.92	259.21 Mon & Pidgeon
1+00-100 Rt. = Vacant Lot.	2.8	269.1	
100' Lt. = Vacant Lot	9.0	262.9	
T.P.	12.66	284.40	0.18 271.74
T.P.	12.73	296.87	0.26 284.14
2+62-67 Rt. = Φ Med.	10.98	285.89	Floor
frame House			
3+16-59' Rt. = Φ Med.	3.07	293.80	Floor
frame House			
3+55-47' Lt. = Φ Large	3.13	293.74	Floor
frame House = Highest point on Hill			
75' Rt. Highpt. on E.	2.7	294.2	ground
check walk 1+53-1681 P. 51	4.10	292.77	292.78

Flicker St. N. from Sewer in Jamacha Rd

0+00 = 30' S. of N.L. Jamacha $\text{E} = \text{Base}$

B.M. 11.57 273.94 262.37 P. 43

1+00 = 32.5' Lt = E Med. 14.15 259.79 Floor

frame House

2+05 = 26' Rt = E 5' 7.00 266.94 on edge walk

Conc walk

2+07 = 41' Rt = E Small 3.62 270.32 Floor

frame House

2+10 = 75' Lt = Vacant Lot 9.5 5

T.P. 12.46 285.18 1.22 272.72

3+30 = opp. Highest ground

60' Rt. 1.0 272.9

85' Lt. 15.7 258.2

Chester St. N. from Sewer in Jamacha Rd.

0+00 = 30' S. of N.L. Jamacha $\text{E} = \text{Base}$

B.M. 12.67 264.18 251.51 $\text{Mon. E Chester + Jamacha}$

1+00 = 100' Lt = Vac Lot. 11.7 252.5 ground

-75' Rt. = " " 8.5 255.7 "

2+20 = 89' Lt = E Small 3.08 261.10 Floor

frame House

-75' Rt. = Vac. Lot. 1.0 263.2

T.P. 10.87 274.12 0.93 263.25

3+65 = High point

-75' Rt. = Vac. Lot. 3.9 270.2

-75' Lt. = " " 11.8 262.3

69th St. N. from Sewer in Jamacha Rd.

0+00 = Mon. on \pm Jamacha to W. and 50' W. of F.L.

69th - Line 50' W. of F.L. = Base line

B.M.	9.91	257.29	247.38	2+50.45 P41 Stub.
------	------	--------	--------	----------------------

1+00 - 75' Rt. = Vac. Lot.	7.7	249.6	
----------------------------	-----	-------	--

2+14 - 68' Rt. = \pm Small Frame House	2.61	254.68	Floor
---	------	--------	-------

- 75' Lt. = Vac. Lot	12.0	245.3	
----------------------	------	-------	--

2+66 - 67' Rt. = \pm Small Frame House	0.30	256.99	Floor
---	------	--------	-------

3+60 - 75' Rt. = Vac. Lot	8.9	248.4	
---------------------------	-----	-------	--

70' Lt. = " "	10.3	247.0	
---------------	------	-------	--

	232.93		
1+00			
10-Lt	10.3	222.6	
10-Rt	5.9	227.0	
1+06 - 9.5 Rt. = Φ 12" Pepper			
1+10 - Beg. Park Lawn.	5.8	227.1	
1+22 - 4.6 Lt. = Φ 13" Pepper			
1+50	5.7	227.2	
2+00	5.2	227.7	
1+50	4.9	228.0	
2+51 - 3.1 Lt. = Φ 2" Euc. tree			
2+77 - 3' Lt. = sly. 36" Euc. tree			
3+05.08 = Ang 27° 58' Lt. 3.89	229.04	on stub	
3+23 - end Park lawn			
3+31 - 4.7 Rt. = Nly. 26" Euc. tree			
3+38 = Poor lath fence			
3+50	3.0	229.9	
3+51 - 4.5 Lt. = Cor. Med. House			
Floor elev.	1.56	231.37	
3+63 - 4.1 Lt. = Cor. Same House - This is small add. on back			
3+84 - 8.1 Lt. = Φ 5" Apricot tree			

	232.93		
4+00	2.7	230.2	
T.P.	4.33	235.43	1.83 231.10
4+15 - 8' Lt. = Φ 8" Pepper			
4+19.5 = Cross board fence			
4+22 = Top bank of Creek	5.2	230.2	
4+30 = Bot. bank - in creek	12.4	223.0	Level both sides
4+31 - 6' Rt. = Φ 10" Holley bush			
4+60	8.6	226.8	
10 Rt	9.8	225.6	
10 Lt.	4.9	230.5	
	Floor elev. = 4.5		
4+55 - 6.2' Lt. = Φ Small House	230.9		
4+61 = 2' Rt. = Φ 24" Willow stump			
4+70 - 4' Lt. = sly. 36" Euc. tree			
4+74 - 5.5 Lt. = edge of Small old shed.			
creek swings about 25' S. here.			
4+83 - 6.4 Lt. = sly. of 40" Euc.			
+87 - 9.4 Lt. = sly. of 36" Euc.			
+91 - 7.2 Lt. = edge Poor fence - (board.)			

235.43

4+9.8 - 32' Rt. = Φ Small House	2.70	232.7	Floor
5+00 - Φ Creek	10.2	225.2	
- 10 Rt.	10.4	225.0	
- 5 Lt. for Sept. Tank. from N.	10.4	225.0	
10 Lt. = Fl. of outlet	7.40	228.0	
5+04 - 21' Rt. = Φ of 5x5' Conc. top to Septic tank 75' Deep	7.23	228.2	Top tank
5+07 - edge of creek	10.3	225.1	
10 Lt.	10.5	224.9	
10 Rt.	8.0	227.4	
5+08 - 61' Lt. = Φ of Large House			
Floor elev	1.1	234.3	
5+14 - 12.4 Rt. = Cor. Conc. slab for wash house			
Top. slab.	4.35	231.08	
5+26 = Top bank - level to Rt.	5.2	230.2	
10 Lt.	9.1	226.3	
5+28 - 4.6 Rt. = Cor. slab	3.92	231.51	on slab

48

235.43

Ground nearly level from here on.			
5+35 - 10' Rt. = Φ 15" Large Holly			
5+50 - 2.8 Rt. = Cor. old wire fence			
5+50 - 6.6 Lt. = Φ + end of 4' Wooden foot bridge			
Top Bridge	4.6	230.8	
on Φ Sewer	4.6	230.8	
T.P.	4.76	237.56	2.63 232.80
5+55 - 5.7 Lt. = sly. 12" Tree			
5+67 - 8' Lt. = sly. 12" Tree			
5+87 - 2.5 Lt. = sly. 3" Fig tree			
6+00	5.6	232.0	
6+05 - 1.5' Lt. = sly. 6" Lemon tree			
6+17 - 3' Lt. = sly. 12" fig stump.			
6+19 - 7.7 Rt. = Nly 12" Tree			

237.56

6+25 - Beg. group of Cactus beds both sides

6+33 - 27 Lt. = Sly. 2" Tropical Tree

6+38 - 88 Rt. = Nly 3" " "

6+39 - 11 Lt. = Sly. 4" Orange "

6+49 - end Cactus beds

6+50 5.2 232.4

6+51 - 2.3 Rt. = E 2" Tropical tree

+53 - Cross - lath fence - poor Cond

+54 - 3.8 Lt. = Sly. 9" Pepper

+68 - 1.5 Lt. = E 2" Euc. tree

+90 - 4' Rt. = E 2" Pepper

+92 - 1.5 Lt. = E 2" Euc.

7+00 3.3 234.3

7+04 = edge of Large Cactus Hedge along
line of Drake St.

237.56

49

7+12 = Cross wire fence + 6.3 Rt. = E 8" Pepper

7+17 = E. edge of Cactus Hedge + 13 Rt. = E. P. pole

T.P. 8.12 241.70 3.98 233.58

7+37.19 = Ang. 53° 28' Rt. 7.95 233.75 on stub.

7+72.51 = Ang. 53° 27' Lt. 7.14 234.42 on stub

= 10+00 on old line

Check on stub 9+90.94 7.07 234.63 ^{P 38} 234.61

Levels on Lateral in Drake st.

0+00 on Stub. 7+37.19 - See sketch P 46

From P. 49

241.70

0+00

7.95 233.75

0+30

7.5 234.2

10' Rt. = edge of Large Cactus Hedge along fence
on R.L. of Drake

0+50 - 6' Rt. = edge Hedge 7.1 234.6

1+00 6' Rt. = Hedge 6.0 235.7

+26 10' Rt. = "

1+42.15 = Ang. 40° 26' Rt. 4.66 237.04 on stub.

1+60 - 10' Rt. = Hedge

1+70 = edge graded road 4.9 237.3

+75 - 9.2' Rt. = end Cactus Hedge

+80 5.1 236.6

241.70

50

1+89 - 4.6 Lt. = Φ 5" willow tree - (no good.)

2+00 - 8' Rt. = ^{fence} beq wire 5.3 236.4

+30 - 5.9 Rt. = fence 5.5 236.2

10 Rt. 5.7 236.0

10 Lt. 4.8 236.9

2+50 5.5 237.2

edge graded road
+60 - 10.8 Rt. = fence 5.0 236.7

2+99.93 = end = check. 4.97 236.73 ^{236.74} on stub

= 2+62.78 on old Line

Location - Poles - Drives - walks etc. on 30th

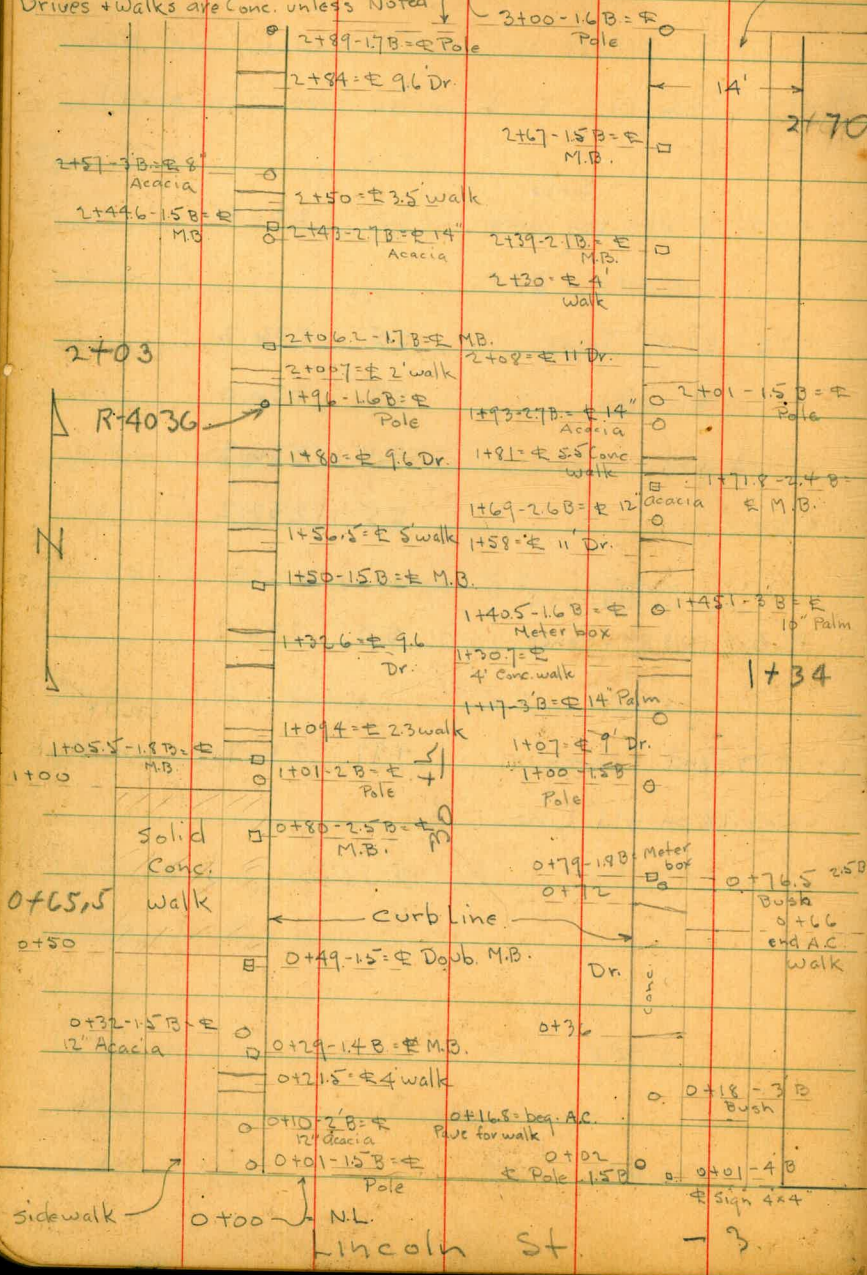
B = Back of cb. face - or base line

M.B. = Meter Box - water

Drives + Walks are Conc. unless Noted

otherwise

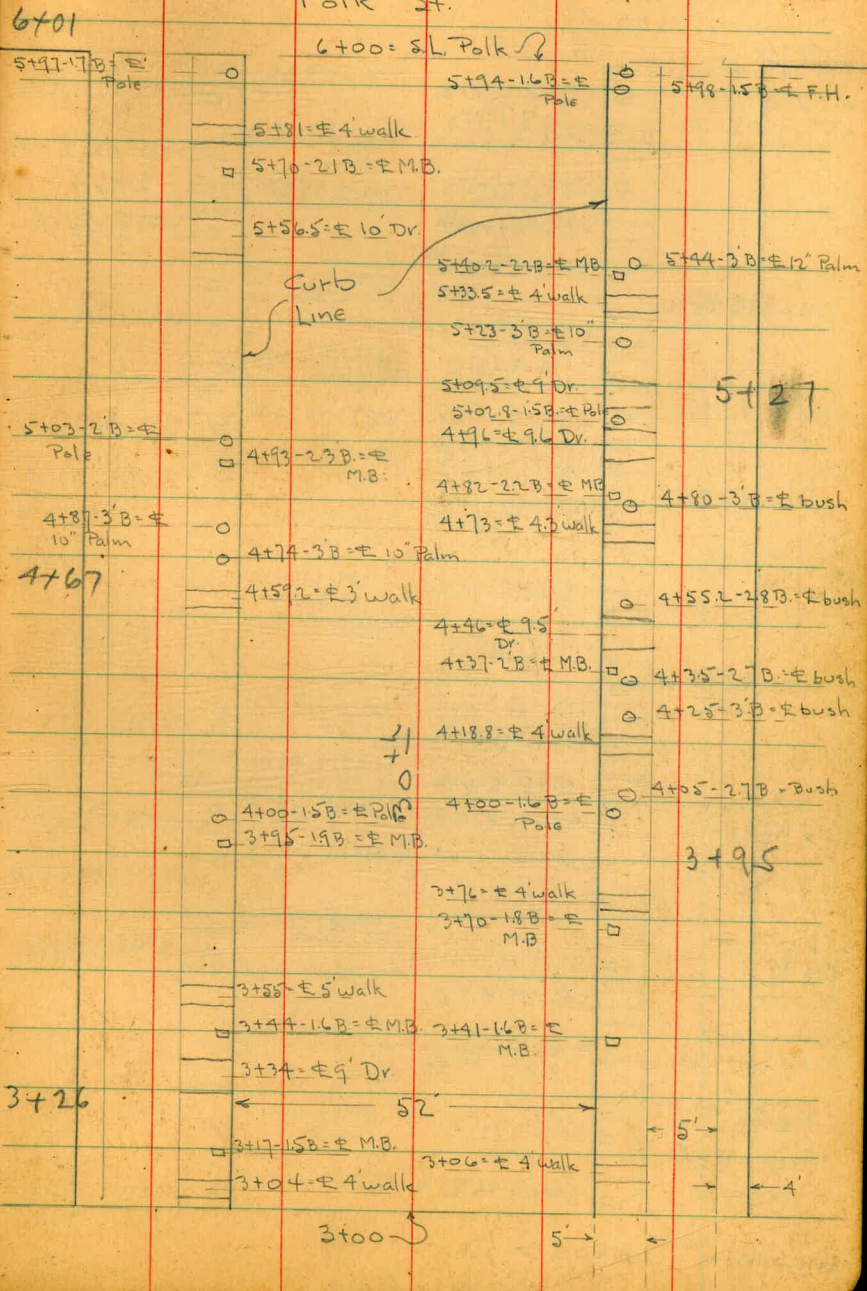
sidewalk



Lincoln to EL Cajon.

8-14-46

Polk St. LISTED 8/16/46 GWE 51



Howard St.

6+03

6+00 S.L.

5+99-17B Pole

5+98 Pole

Drive to Sen Sta

5+67

curb line

5+20-17B M.B.

5+00-5' walk

4+67

4+94-18B Pole

4+30-2B M.B.

4+09-3' walk

3+98-16B Pole

3+62-16B M.B.

3+35-18B M.B.

3+32

3+68-3B Conc slab

3+59-15' walk

3+46-27B Bush

3+27-3' walk

3+23-3B Bush

3+06-5' 9' Dr.

5+97-16B Pole

5+81-8-5' walk

5+67-3B 12" Palm

5+56-10' Dr

5+25-4' walk

4+99-16B Pole

4+97-5-3' walk

4+83-19B M.B.

4+61-22B M.B.

4+50-28B 10" Palm

4+27-4' walk

4+11-9' Dr.

4+01-14B Pole

3+90-15B M.B.

3+74-5' walk

3+65-9' Dr.

3+40-19B M.B.

3+24-3' walk

3+05-8.5' Dr.

5+98-17B E.F.H.

5+92-29B E.P. Blm

5+78-18B M.P.

5+33

5+09-16B M.B.

4+67-28B 10" Palm

4+54-5-4' walk

4+38-33B 3' Ac.

4+19-18B M.B.

3+97

3+85-29B 10" Ac.

3+66-28B 12" Ac.

Note: owner wants Both trees taken out

J.T. Wood - 4159-30th OWNER

3+00

2+98-18B Pole

2+80-16B M.P.

2+90-16-27B 14" Palm

2+77-4' walk

2+68-26B 12" Palm

2+58-3' walk

2+45-3B 14" Palm

2+22-18B M.B.

2+20-3' walk

2+14-25B 16" Palm

2+04-10' Dr.

1+96-17B Pole

1+79-17B M.B.

1+60-4.5' walk

1+45-27B Bush

1+36-25B bush

1+31-3' walk

1+26-15B M.B.

1+08-10' Dr.

1+01-25B 8' Pine

1+00-2' Pole

0+92-2.5' slab walk

0+79-15B M.B.

0+63-11' Dr.

0+71

0+25-22B M.B.

0+20-25B M.B.

0+01-18B Pole

0+00

2+99-16B Pole

2+80-19B M.B.

2+61-9.5' Dr.

2+38-28B 6" Palm

2+19-3' walk M.B. in walk

2+02-2-3' walk

1+90-7-3B 10" Pepper

1+74-26B 24" Pepper

1+59-32B 14" Pepper

1+10-5-9.6' Dr.

1+00-4-16B Pole

0+87-15B M.B.

0+64-5-3' walk

0+59-9' Dr.

0+15-27B 14" Acacia

0+10-13B Pole

2+92-3B 12' Ac

2+75-27B 10' Ac

2+52-28B 5" AC

2+26-7-29B 5" Palm

2+09-5-29B 5" Palm

1+98-16B Pole

1+85-19B M.B.

1+98-18B M.B.

1+94-27B 10' Ac

0+94-3B 8" Ac

0+65-27B 14" Acacia

0+30-3B 8" Ac

0+10-13B Pole

0+01-13B Pole

0+01-13B Pole

0+01-13B Pole

0+01-13B Pole

0+01-13B Pole

0+01-13B Pole

0+01-13B Pole

0+01-13B Pole

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0+01-13B Pole

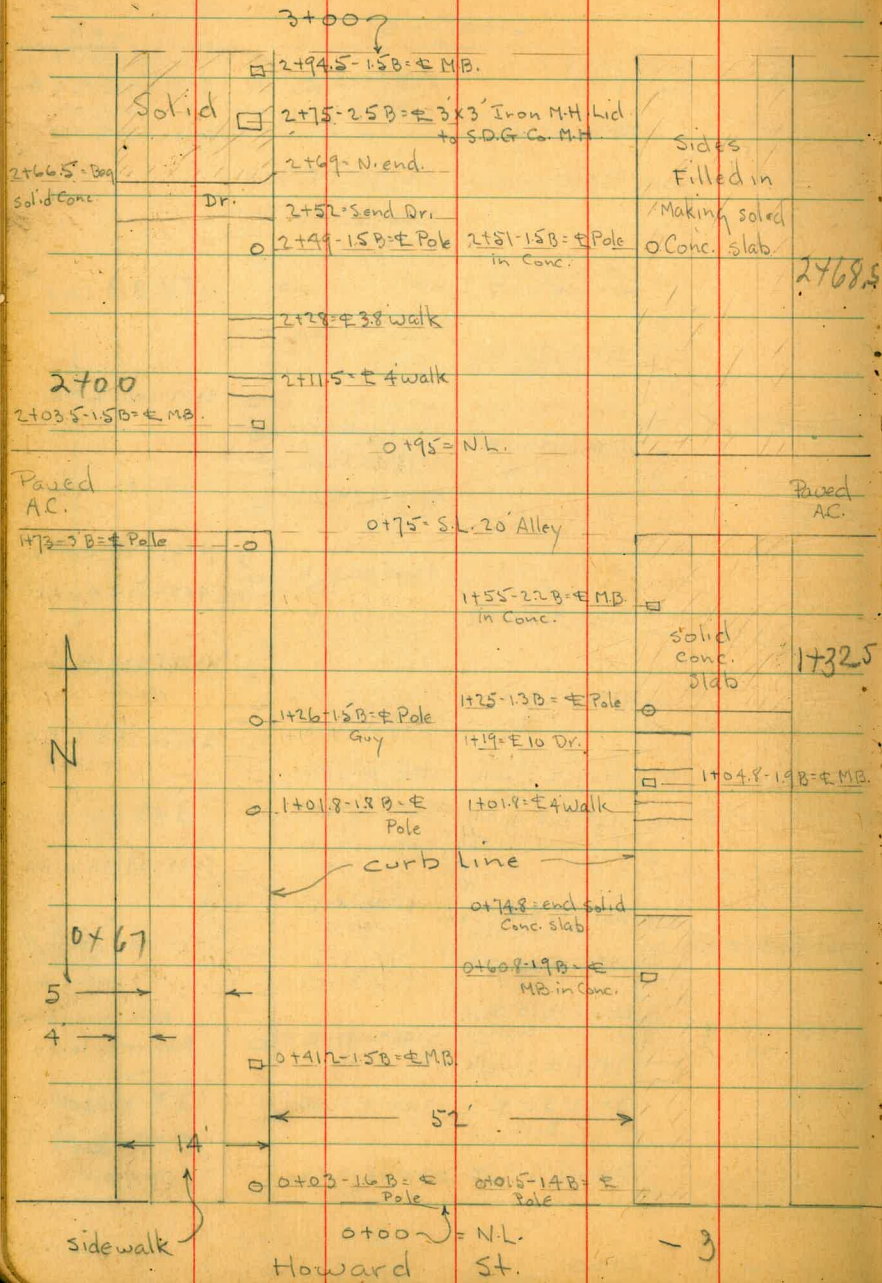
0+01-13B Pole

-0.315

Sidewalk

0+00 N.L. Polk Ave

3+00



8-15-46
Osborne
McCoy
Hardin
W. Moore

145
70
215

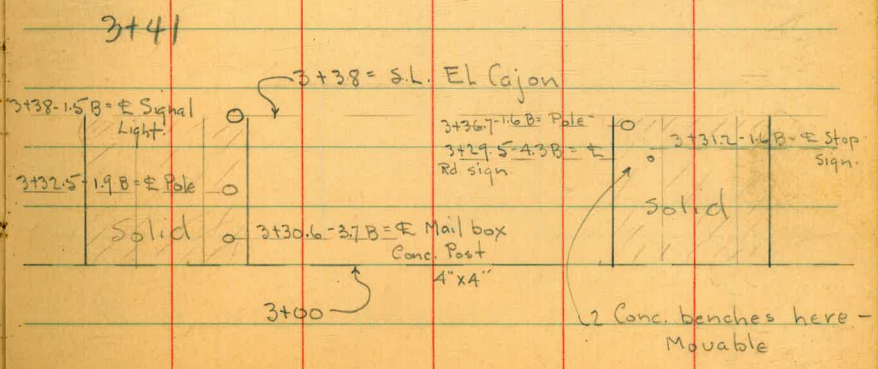
Most of the curbs throughout the entire job have been pushed out, but are fairly regular. In the Block bet. Lincoln & Palk on the W. side - from 1+00 to 3+70 the curb is bad - leans out at about 45° angle

132.5
68
200.5

190
70
260

1 36

338
70
268



#1

X-Section Lotus - Abbott to Bacon

11-18-46

635

W.O. 1213

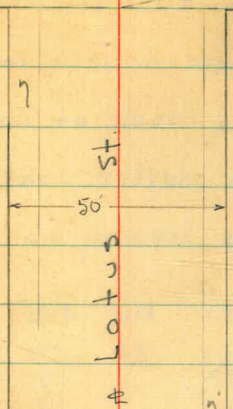
Osborne
Hardin
Warrell
Smith

Indexed
c.s.k.

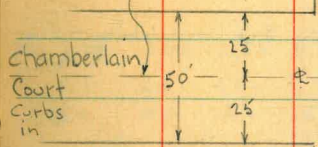
Bacon St. Paved-A.C.

ct.

6+00.41



From split of cbs.



3+50.12



20' Alley Dirt

3
walks
+
Curbs

{ Start old cl.
 1+99.8 = End New cl.
 { Start new cl.
 1+93.4 = End old cl.
 { Start old cl.
 1+62.8 = End New cl.
 { Start old curb
 1+41.6 = End old curb
 { Start New "

C.H.S. 7-3-47

2+00

Paved (A.C.) Abbott St.

ct.

X-Section Lotus St. 50' wide 10' cbs. in
from Abbott to Bacon

Note: All curbs are in very bad condition -
should be replaced, inside of cbs. are like
sandstone - with a plaster coat which has broken
off in many spots, leaving no good support for
paving

0+50

0+38 = end Coldlay walk on Lt. - beg 5.5' Conc Walk 4.5' back
of cb.

0+15

0+00 = Beg Rough Coldlay walks on both sides

0+00 = E. L. Abbott = edge of H.C. Paving

2.5' x 2' Box inlet with Grate at \oplus of Ret. on S.E. Cor.

Flow Line box 7.54 -0.10

Top grate on gut. Line 5.88 1.60

0-10 = E. cb. of Abbott

B.M. 5.01 7.48

2.47

sw. B.M. Abbott
+Voltaire

Lt. = N



Rt. = S

EL. 3.24	3.13	2.92	2.18	2.18	1.98	2.89	2.98	3.18
4.24	4.35	4.56	5.3	5.3	5.5	4.64	4.5	4.3
2.5	19.5	15.1	15.1		14.9	14.9	19.5	2.5
	walk	Top	gut.				walk	

EL. 2.78	2.68	2.55	1.78	2.18	2.08	1.58	2.93	2.58	2.68
4.7	4.8	4.93	5.7	5.3	5.4	5.9	5.05	4.9	4.8
25.4	19.8	15.2	15.2	10		15	15	19.8	25.2
	walk	Top	gut.			gut	Top	walk	

EL. 2.58	2.98	2.92	2.02	2.28	2.33	2.07	1.80	2.33	2.38	2.48
4.9	5.0	5.06	5.46	5.20	5.15	5.41	5.68	5.15	5.1	5.0
25.4	19.8	15.2	15.2	7.5		7.5	15	15	19.8	25.2
	walk	Topcb.	gut			gut	Top	Top	edge	walk
		P.C.					gut	P.C. Ret.		

EL. 1.75	2.32	1.87	2.20	2.35	2.38	2.22	1.91	1.74	2.29	1.81
5.73	5.16	5.61	5.28	5.13	5.10	5.26	5.57	5.74	5.19	5.67
7.5	2.5	2.5	1.5	7.5		7.5	1.5	2.5	2.5	7.5
gut.	Topcb.	gut					gut	gut	Topcb	mgut
	P.C.								P.C. Ret.	

7.48

T.P. 7.79 11.42 3.85 3.63

1+00

1+83 - ± 10 Conc. Dr. on Lt.

1+83 - ± 16 Dr. on Rt. (dirt - cb. broken out)

1+75 end broken cb. on Lt.

1+71 - Beg cb. broken out on Lt.

1+52 - ± 12 Dr. on Rt. (dirt - cb. broken out)

1+50

1+20 = E.L. Alley

1+10 - for profile of ± Alley

1+00 = W.L. 20 Alley on Lt.

0+75

		Lt.					Rt.				
EL.	4.75	4.63	4.56	3.68	3.88	3.88	3.58	4.53	4.48	4.58	
	2.73	2.85	2.92	3.8	3.6	3.6	3.9	2.95	3.0	2.9	
	25	19.5	14.9	14.9	10		14.9	14.9	19.6	26	
	walk		Top	gut.			gut.	Top			

EL.	4.34	3.98	3.68	3.28	4.18
	3.14	4.0	3.8	4.2	3.30
	14.9	14.9		15	15
	Top	gut.		gut.	Top

EL.	4.25	4.16	4.03	3.08	3.48	2.88	3.98	4.08
	3.23	3.32	3.45	4.4	4.0	4.6	3.5	3.4
	25	19.5	14.9	14.9		15	19.8	25.2
	walk		Top	gut.		gut. in Drive		walk

EL.	4.02	3.98	3.75	2.78	3.18	2.58	3.62
	3.46	4.0	3.73	4.7	4.3	4.9	3.86
	25.1	25.1	14.9	14.9		15	15
	Top cb. end Ret.	gut	Top cb. Ret.	gut		gut	Top

EL.	3.38	2.88	2.68	2.98	3.08
	4.1	4.6	4.8	4.5	4.4
	75	25	15	10	

EL.	3.74	3.08	3.56	2.48	2.78	2.88	2.38	3.94	3.58	3.58
	3.74	4.4	3.92	5.0	4.7	4.6	5.1	4.04	3.9	3.9
	25	25	15	15	10		15	15	19.5	25
	Top cb. end Ret.	gut	Top on Alley Ret. (broken)	gut.			gut			walk

EL.	3.26	2.38	2.58	2.28	3.12
	4.22	5.1	4.9	5.2	4.36
	15	15		14.9	14.9
				gut	Top

7.48

Lt

=

Rt.

= wherry

3+35.12 = w. cb. line

3+25.12 = w. L. Chamberlain Court

3+22 = end patch on Lt.

3+12 = beg. Cold Lay Patch in walk on Lt.

3+00

2+75

2+54 = end cb. broken out on Lt.

2+52 = end patch on Lt.

2+50

2+46 = beg. Cold Lay patch in walk on Lt.

2+42 = beg. cb. broken out for dr.

2+25

EL.	6.03	5.62	6.06	5.32	5.22	5.62	5.52	5.22	4.89
	5.39	5.8	5.36	6.1	6.2	5.8	5.9	6.2	6.53
	75	75	25	25	15	75		15	15
	Top	gut	Top	gut					
			PC Ret						

EL.	6.20	6.06	5.95	5.32	5.32	5.12	5.82
	5.22	5.36	5.47	6.1	6.1	6.3	5.60
	25	15	15	15		15	15
	walk		Top	gut		gut	Top
			PC Ret				

EL.	5.87	5.76	5.66	5.02	5.02	4.72	5.58	5.72	5.92
	5.55	5.66	5.76	6.4	6.4	6.7	5.84	5.7	5.5
	25	19.5	15	15		15	15	19.5	25
	walk		Top	gut		gut	Top		walk

EL.	5.46	4.72	4.72	4.42	5.35
-----	------	------	------	------	------

EL.	5.14	5.96	6.7	6.7	7.0	6.07
	6.28	14.9	14.9		15	15
	15	Top	gut		gut	Top
	Top cb.					

end. EL.	5.32	5.19	4.52	4.42	4.02	5.06	5.12	5.22
	6.10	6.23	6.9	7.0	7.4	6.36	6.3	6.2
	25.1	19.4	15		15	15	19.3	25
	walk		gut in Dr.		gut	Top		walk

EL. 5.19

6.23

15

Top cb.

end

EL.	4.85	4.02	4.12	3.92	4.77
	6.57	7.4	7.3	7.5	6.65
	15	15		15	15
	Top	gut		gut	Top

11.42

4+61 - \$ 15' Conc. Dr. on Rt.

4+52 - beg. cb. broken on Lt. - (no plaster Top)

4+50

4+46 - end 1/2 patch on Lt. walk

4+25

4+24 - Beg. patch on S. 1/2 of walk on Lt.

4+23 - end Cold lay walk on Rt. + Beg. Conc. walk

4+13 - beg. Cold lay patch on walk on Lt.

4+00

3+75.12 = E.L. Chamberlain

3+65.12 = E. cb - (Return in poor Cond. - curb broken out from 20.5 Lt. to 36.4 Lt.)

3+50.12 = \$ Chamberlain = \$ Sewer M.H. on \$

Lt.

Rt.

EL.	7.02	6.92	6.81	6.12	6.32	6.32	6.97	7.05	7.25
	4.40	4.50	4.61	5.3	5.1	5.1	4.45	4.37	4.17
	25	19.6	15	15		15	15	19.5	25
	walk		Top	gut		gut.	Top		walk

EL.	6.89	6.82	6.62	6.02	6.12	6.02	6.72	6.84	7.00
	4.53	4.6	4.80	5.4	5.3	5.4	4.70	4.58	4.42
	25.1	AC 19.7	15	15		14.9	14.9	19.5	25
	conc. walk		Top	gut		gut.	Top		walk

EL.	6.69	6.53	6.45	5.82	5.92	5.72	6.46	6.62	6.72
	4.73	4.89	4.97	5.6	5.5	5.7	4.96	4.8	4.7
	25	19.5	15.1	15.1		14.9	14.9	19.5	25
	walk (Conc.)		Top	gut.		gut.	Top		walk

EL.	6.49	6.39	6.27	5.72	5.82	5.72	6.24		
	4.93	5.03	5.15	5.7	5.6	5.7	5.18		
	25	19.5	15	15		15	15		
	walk		Top	gut		gut	Top		

EL.	6.37	5.62	6.26	5.92	5.82	5.52	5.82	5.72	5.62	6.15
	5.05	5.8	5.16	6.0	5.6	5.9	5.6	5.7	5.8	5.27
	75	75	36.4	36.4	25	15	7.5		15	15
	Top gut.		Top gut		cb. broken out to here				gut.	Top

EL.	6.02	5.72	5.62	5.72	5.74	5.72	6.01	6.12	6.22
	5.4	5.7	5.8	5.7	5.68		6.0	5.41	5.3
	75	25	15	7.5	on Rim M.H.		15	15	19.7
							gut Top		walk.

11.42

5+80 = Beg. Conc. Dr. on Lt. #4" Pipe Drain

5+75

5+50 = Beg. Solid Conc. walk back of cb. on Lt.

5+25

5+20 = end broken out cb. on Rt.

5+18 = end Cold lay walk on Lt. (beg. conc.)

5+15 = end Conc. walk on Rt. (beg. Cold lay)

5+00

4+98 = Beg. badly broken cb. on Rt. (No plaster top)

4+94 = end broken out cb. on Lt.

4+90 = end Cold lay walk on Rt. (beg. Conc.)

4+75

4+70 = cb. on Lt. completely broken out for Dr.

4+65 = Beg. Cold lay walk - both sides

EL. 7.86 7.27

2.56 4.15

15 15

Topcb. F.L.

#4" drain

EL. 7.94 7.80 7.12 7.22 7.32 8.27

3.48 3.62 4.3 4.2 4.1 3.15

25 15 15 15 15

walk Top gut gut. Top

EL. 7.78 7.60 6.82 7.02 7.02 7.98 8.12 8.22

3.64 3.82 4.6 4.4 4.4 3.44 3.3 3.2

25 15 15 15 15 19.6 25

walk Top gut gut. Top walk

EL. 7.62 7.52 7.42 6.62 6.92 6.62 7.72

3.80 3.90 4.00 4.8 4.5 4.8 3.70

19.8 19.5 15 15 15 15

walk Top gut gut. Top

EL. 7.52 7.32 7.20 6.52 6.62 6.32 7.41 7.53 7.67

3.9 4.1 4.22 4.9 4.8 5.1 4.01 3.89 3.75

25 19.5 15 15 15 15 19.5 25

walk Top gut gut. Top walk

EL. 7.22 7.02 6.32 6.52 6.32 7.24

4.2 4.4 5.1 4.9 5.1 4.18

25 19.5 15 15 15 15

walk gut in Dr. gut Top

Note - BM at N.E. Bacon + Voltaire is out.

check starting B.M. 6.02 2.48 2.47 ✓

T.P. 0.80 8.50 6.02 7.70

G+11 = 24.3 Lt. = \pm of W. side of 2.5' x 2.5' Grate on box inlet

G+10.41 = W. cb Line Bacon (in Cross Gutter)

+ end Coldlay walk on Rt.

Edge of A.C. pave 0.5 W. of W.L.

G+00.41 = W.L. Bacon = end Conc. Dr. on Lt.

G+93 = end broken cb on Rt.

T.P. 5.80 13.72 3.50 7.92

G+85 = Reg. cb broken out by Palm tree roots on Rt.

Lt

\pm

Rt.

Note This section appears to be reversed - wheeew -

EL. -1.25 7.33
14.97 6.39
24.3 24.3
F.L. box edge grate

EL. 7.06	7.92	7.34	7.40	7.66	7.82	7.97	8.50	7.99
6.66	5.80	6.39	6.32	6.06	5.90	5.75	5.72	5.73
7.5	2.5	2.5	15		15	2.5	2.5	7.5
gut.	Topcb	gut.				gut.	Topcb	gut.
	PC Ret.						PC Ret.	



8.72	8.62	8.48	7.86	7.98	7.95	7.76	7.45	7.98	8.14
5.0	5.1	5.14	5.86	5.74	5.77	5.96	6.27	5.74	5.58
2.5	1.5	1.8	1.8	7.5		7.5	14.8	14.8	2.5
walk		Topcb	gut				gut	Topcb	walk
		PC Ret.						PC Ret.	

13.72

11.42

EL. 8.57
2.85
15
Top
end
cb

Cross Section CHAMBERLAIN COURT + Adjacent Alley

1213 61

BIKs $\begin{cases} 100 \\ 101 \\ 102 \end{cases}$ Ocean Bay Beach

• = Set hub - 1/2 Red wood

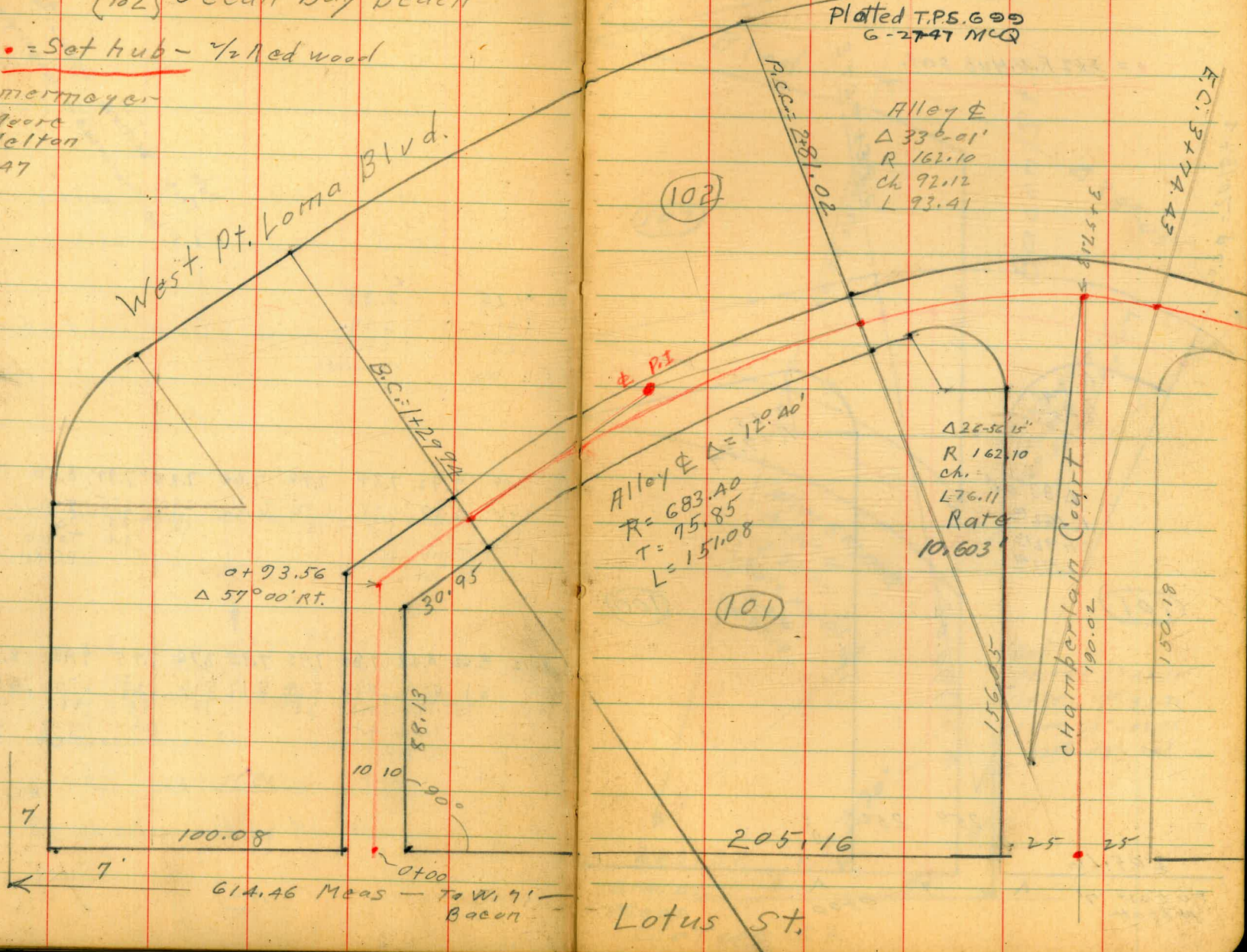
Sommermeier

W Moore
L. Melton

4-1-47

West Pt. Loma Blvd.

Abbott St.



Indexed
C.S.K.

Plotted T.P.S. 699
6-27-47 M.C.

Alley Δ
Δ 33°-01'
R 162.10
Ch 92.12
L 93.41

(102)

Alley Δ Δ = 12°-00'
R = 683.40
T = 75.85
L = 151.08

(101)

Δ 26-50-15'
R 162.10
Ch. 176.11
Rate 10,603'

E.C. 3474.43

Chamberlain Court

205.16

Lotus St.

614.46 Meas - To W. 7' Bacon

Tie Pts.
Ocean Bay Beach Sub.
Blks. 100 - 101 + 102

West Pt.

Loma Blvd

Bacon St.

102

$\Delta 38^{\circ}05'$

Int. Line Bacon
G + 25.61
W. L. M.

Filey ER = 138.22
 $\Delta = 36^{\circ}40'$
L 88.68
Rate per ft.
12.404
64.87.18

Def
5+50.00 $2^{\circ}42.12'$
+75 $7^{\circ}52.22'$
6+00 $13^{\circ}02.32'$
+25 $18^{\circ}20'$

225.22

614.46
Meas
Lotus St.

• = 2x2 R.W. Hub set.

3474.43 E.C.

2+81.02 = P.C.

R. 24
T 25

$\Delta 93^{\circ}01'$
R 162.10
Ch 92.12
L 93.41

T 25
R 19.94

101

100

156.05

190.02

810.18

250

250

90

205.16

To East of
Abbott

0+00

Chamberlain Court

X-sec.

Lt

☐

Rt

0+75

4+61 0.5 piece broken out of Rt. Ob.

4+51 - 1' topping of Rt. Ob.

0+33 Beg. good curb on left

0+11E start curb on Rt. start good walk on Rt.

0+10 Curb on left broken + out of line start of break

0+00 = Nly. Line Lotus going Nly.

6.07 10.50 2.84 4.43

0+00 for Alley (on Hub) S.S.

4.54 2.73 B.M.#1

B.M. 4.80 7.27 - 2.47 SW. R.P. Hbb. # + Voltaire

6.12
4.38
1.5
top ob.

5.2
1.5

5.8
4.7
1.0

6.1
4.4

5.8
4.7
1.5

6.18
4.02
1.5
top ob.

6.02
4.48
1.5
top ob.

5.6
4.9
1.5

6.9
4.6

5.3
5.12
1.5

6.37
4.13
1.5
top ob.

5.96
4.54
1.5
top ob.

5.5
5.0
1.5

5.7
4.8

5.4
5.1
1.5

6.27
4.23
1.5
ob.

6.04
4.46
1.5
top ob.

5.4
5.1
1.5

5.7
4.8

5.5
5.0
1.0

6.2
4.3
1.5

W. Edge Walk
19.5

10.50
Walk Broken

Chamberlain - Court.

1+90 ⁰² 2x2 Hub. Int. Alley + Chamberlain courts. 4.30 6.20 B.M.# 2

1+75 End Curb on left.

1+65

1+56.05 Curb B.C. on left.

1+50.18

Curb Rot. + walk Curb B.C. on Rt. broken - Rebuild.

1+25

6.35
4.15
33.8
top end
Curb Rot.

6.49	5.8	5.9	6.4
4.01	4.7	4.6	4.1
19	19	15	
top cl.			

4.06
15
top cl.

6.35	5.7	5.8	6.1	6.0	5.9	6.9
4.15	4.8	4.7	4.4	4.5	4.6	3.81
15	15	10		10	15	15
top cl.						top cl.

6.26	5.3	5.6	6.0	5.9	5.1	6.60
4.24	5.2	4.9	4.5	4.6	4.8	3.90
15	15	10		10	15	15
top cl.						top cl.

10.50

Alley BIKs ¹⁰⁰ } Ocean Bay Beach.
¹⁰¹ }
¹⁰² }

⊕

65

start picket fence on Lt. 0² Back.

0+93⁵⁶ L on ⊕ taken on split

△
3
5.2
Line

△
3
5.4

△
3
5.5
Line

0+88¹³ L on Rt.

△
3
5.5
10

△
3
5.4

△
3
5.5
10

0+65² End same on line

0+53 start frame dwelling on line on Lt.

0+45

△
3
5.3
10

△
3
5.5

△
3
5.0
7

△
3
4.7
10

0+34.7 9² Lt = End same

0+13² 9⁶ Lt = Beg. Frame Apt. House

0+00

△
3
5.20
10
End Ret.

△
3
5.8
10

△
3
6.0

△
3
5.4
9.9

△
3
4.90
9.9
top Ret

BM² / P63. 6.21 8.94 — 2.73
 0+00 = Nly. line Lotus. ⊕ 20' Alley
 Going North + East.

8.94

2+06 8² Rt. = V. edge Papula # 5064

1+96 13² Lt. = ctr. Sing. Bar dirt floor.

1+86 9² Lt. = End picket fence

1+75

1+63 8² Lt. = ctr. 30" Eucalyptus

1+61 9² Rt. start wire fence

1+29.9A = B.C. Rt. 9² Lt. = fence

1+27^E 8² Lt. = N. side tel. pole # 92673 H
5074

1+15^E 9² Rt. = S. side P. Pole # PL 2-52

0+98.99 opposite L on Rt. taken at 90°

8.9A

2

4.1	4.1	4.3		5.0
4.8	4.8	4.6	Fence	3.9
10		6	9.5	10

3.8
5.1
13.6

4.7	4.1	3.8	4.1	4.1
10	4.8	5.1	4.8	4.2
	3		7	10

3.8	3.0	3.6	4.1
5.1	5.3	5.3	4.8
10		5	10

3.6	3.4	3.4
5.3	5.5	5.5
10		10

8.9A

2+71 9²Lt = End Fence start frame Bldg.
 2+61 10²Lt = start board fence.

2+54 10²Lt = Φ Sing. gar. Conc. Floor

2+45 10³Rt = ^{start} old wire fence

2+44 9²Lt = N. side Tel. pole # 300537 H

2+40 12⁵Rt. = Φ Sing Gar. dirt floor

2+26 18²Rt = Φ Sing Gar. dirt floor

2+22 9²Rt = End wire fence.

2+13 14⁶Lt = Φ Sing. Gar. dirt floor

8.94

Lt.

Φ

Rt.

5.0	5.1	5.1	5.1	5.6
3.9	3.8	3.7	3.7	3.4
9.7		4	6	10

4.79
 4.15
 10¹²
 Floor

4.6	4.6	4.7	4.7
4.3	4.3	4.2	4.2
10		10	12.5

4.9
 4.0
 18

4.7
 14.6

8.94

B.C. Hub
 5+36.73 4.90 13.08 3.53 8.18

3+84 6⁸ Lt. = ctr. 14" Eucalyptus
 3+74.43 E.C

3+773 8⁸ Lt. = End frame Bldg. start board fence

3+57.13 = Chamberlain SS Hub, 5.51 6.20 BM #2 P.64

2+56 9² Lt. = End Fence + start frame Bldg.

2+50 8² Lt. = ctr. 12" Eucalyptus.

2+43 9⁶ Lt. = N. Edge. tel pole # A4128H

2+27 17⁰ Lt. = ctr. 24" pepper. Large limbs over hardy alloy

2+27 10' Lt. = 4 17 Fence.

3+23 Curb. B.C. on Rt.

+07 10⁴ Lt. to Fence.

3+07 10² Rt. = W. Edge. P. Pole # 175054A

2+84 10² Lt. = End Frame Bldg. Start board fence

T.P. 6.85 11.71 4.08 4.86

2+81⁰² P.C.C. 10' Lt to frame Bldg.

8.94

⊕

6.1 6.0 6.1 6.4
 5.0 4.9 5.0 5.3
 10 10 20

Bldg. 6.3 6.0 6.6 6.0
 5.4 5.1 5.2 5.1
 9.5 9.5 10 20

6.1 6.0 6.0 5.8 6.25
 5.6 5.7 5.7 5.9 5.36
 10 7 16.3 16.3
 7 16.3 16.3
 7 16.3 16.3

11.71

5.3 5.4 5.7 5.6 5.0
 3.6 3.7 3.7 3.3 3.9
 10 3 5 10
 8.94

484129H
 A+72 98 Lt. = N. Edge Tel. Pole # J.P.R. 5027
 start board fence
 A+67 10⁶ Lt. = End frame shed
 A+57 19⁵ Rt. = Φ Sing. gar. dirt floor

4.8
 $\frac{5.3}{19.5}$

start frame shed
 A+49 = 10² Lt. = End board fence +
 A+45

7.9
 $\frac{5.2}{10}$ 7.5
 5.6 7.9
 $\frac{5.2}{10}$

A+14 10 Lt. - start board fence

A+07³ Φ Conc. Apron. Sing. Gar.

7.61 7.47
 $\frac{5.47}{10}$ $\frac{5.61}{6}$
 Floor Apron

A+00 10' Lt. = End board fence

7.4 7.4 7.0 6.8
 $\frac{5.7}{10}$ $\frac{5.7}{4}$ 6.1 $\frac{6.3}{10}$

3+96 { 13² Rt. = End Broken up Curb. Ret.
 8⁵ Lt. = ctr. 18" Eucalyptus
13.08

6.8
 $\frac{6.3}{13.4}$

13.08

5+26 21° Rt. = Φ Double Gar. Conc. Floor

9.03

9.33

$\frac{4.05}{17.5 \text{ Apron}}$

$\frac{3.75}{21 \text{ Floor}}$

5+10

8.74

8.44

8.3

8.6

4.34

4.64

4.8

4.5

9.6

9.2

10

Gar. Floor

Edge Apron
+ ground

5+00 Start 4 unit Gar. Bldg. ^{Bldg} on line

8.66

8.51

4.42

4.57

10

9.4

Floor

Apron

4+99 9.3 Lt. = N. side pole. Bay for #5022

4+93 8.7 Lt. = Rough Conc. Apron.
10 Lt. = Φ Sing. Gar.

8.79

8.3

4.79

4.8

10

8.7

Floor

4+91 9.6 Rt. = S. Edge pole # 5022
7.9 Lt. = End board Fence.

4+88 8.9 Rt. = End picket Fence

+80 12° Rt. = 10" pepper tree Limbs in alley

4+74 10° Rt. = start Picket Fence
13.08

8.3

8.1

8.4

4.8

5.0

4.7

9.9

10

13.08

6410 10² Lt. = End Rail fence

	8.0	1.4	8.0
	5.1	5.7	5.1
	<u>10</u>		<u>10</u>

6400 10 Lt = Fence

8.1	8.4	1.0	1.8	8.0
5.0	4.7	5.3	5.3	5.1
<u>10</u>	<u>7</u>		<u>7</u>	<u>10</u>

5486 8⁰ Lt. = Wly. Edge poles with down conduit # P.A. 5005

5475 9² Lt. = Fence

8.2	8.4	8.3	8.2	8.5
4.9	4.7	4.8	4.9	4.6
<u>10</u>	<u>5</u>		<u>8</u>	<u>10</u>

5460 9³ Lt = start Rail fence.

5449 10² Lt. = End. 4 Unit. Car

8.95	8.04	8.6	8.7
4.13	4.24	4.5	4.4
<u>10.4</u>	<u>8.6</u>		<u>10</u>
Car #ker	Apr 17		

5436.93 = B.C. Rt.

8.93	8.86	8.5	8.6
4.15	4.22	4.6	4.5
<u>9.9</u>	<u>9.3</u>		<u>10</u>
	Edge Apr 17 4		
	Ground		

13.08

13.08

Cross Section Champlain

" " Alley BIKs {¹⁹⁰₁₉₁₁₉₂}

Ocean Bay Beach Sub.

Summermeier
W. Moore
L. Melton

orig. B.M. Page. 63
Abbott +
Vallairs (247)

6.32 2.45 - Error (0.02)

T.P. 2.03 8.77 6.97 6.74

T.P. 6.12 13.71 5.49 7.59

13.08

6+25.61 = W. Line Bacon No curb Ret on North
taken along W. Line Bacon.

5+16 Radial to intersection of Nly. Line
Alley + paving

13.08

Court.

±

72

7.16	7.16	7.16	7.04	7.39	7.64	7.71
5.52	5.83	5.92	6.04	5.69	5.44	5.37
17.8	17.3	15.1	15.1	11.1	15.1	23
walk	N. Edge	Par	Par	cutter	S. Line	at walk
	par			+ walk		Back
				Drive		Edge

7.16	7.16	7.9
5.92	5.9	5.2
10		70
Edge Par.		

13.08

July 9, 1947 69th St. from City Limits North

X Section 9+50 to 12+17

Rainer
Nieman
Baker

Indexed
over

Lefts

±

Rights

73

10+50

4.5 5.9 7.8 11.4
25 15 6 85 20

10+24

3.6 4.0 6.4 9.5
25 13 4 6.7 20

10+00

1.2 0.9 3.5 4.5 4.6 8.7
25 21 3 1 39 10.5 20

9+89

1.3 1.5 4.7
21 11 3.8 20

9+86

1.1 4.5
20 3.5 20

1.28 447.69

TR #2

12.43 446.41

9+79

fence crossing end N.S. Fence ^{1.0E}

9+50

9.7 9.8 10.5 12.5
36 26 20 12.3 20

0.64 458.84

TR #1

3.43 458.20

0.82 461.63

B.M. Top of H. St. ^{FB 1745 P2} Saranac + 69th

460.61

69th St. from City Limits North
 X Sections 9+50 to 12+17

Left C Right

BM.P. 73 0.28 460.82 Corr. 460.81

8.21 461.10

T.P.#5 0.09 452.89

12.05 452.98

T.P.#A 0.00 440.93

12+17

14.6	15.2	19.4		23.2	28.6
25	16	9	19.7	10	22

12+00

10.4	12.0	15.6		19.6	24.7
25	15	8	14.4	12	25

11+83

10.6

11+50

0.6	2.1	4.5	7.5		9.8	12.4
25	15	10	7	6.7	9	20

11+00

10.7	10	2.2	3.8		5.4	8.9
25	11	9	8	3.8	9	24

3.77 440.93

T.P.#3 10.55 437.14

447.69

Levels on Prop Sewer on Lisbon St.

from Φ Pidgeon to E. 3-16-48

W.O. 21001

7.0

9' Lt = Ground at loc. of Prop. House

7' Rt = Ground at loc. of Prop. House

8+60 = To serve prop New Houses

304.28
298.50
5.78

6+60 = Φ Prop M.H.

4.19

306.33
297.00

F.L. Sewer
297.00

T.P.

19.05

310.52

0.16

300.47

133' Rt. of Φ = Φ House

3+60 = Φ Prop. M.H.

6.00

294.63

F.L. Sewer.
288.17

2+54 = D.E. of Present Plan

0+00 = Φ Lisbon + Pidgeon = $\frac{7}{9}$ + 39.76 - P. 16

13.00 300.63

287.63

spt Φ Pidgeon
+ Lisbon
P. 16

300.63

309.7

0.8

9.0

ground.
Loc. House

9.33

304.28

6.24

301.4

9.1

7.0 = ground
loc. House

310.52

285.0

15.6

133

ground

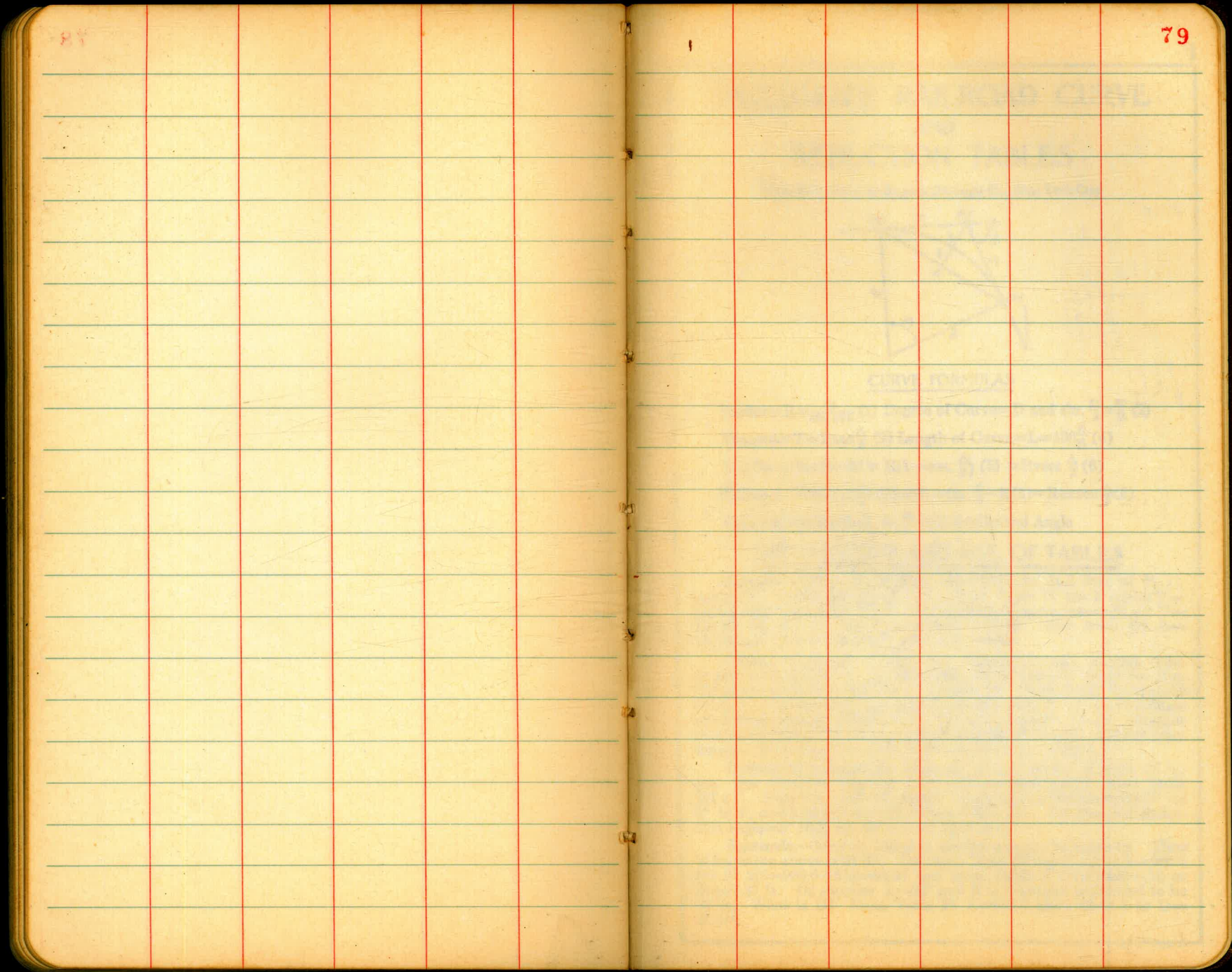
296.74

13.85

133

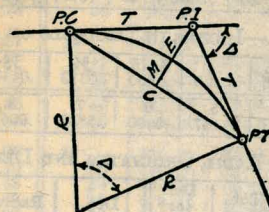
floor.

The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. Vertical red lines create margins on both sides of each page. The right page has the number '77' printed in red in the upper right corner. The notebook is bound in the center, and the pages appear slightly aged with some minor discoloration and faint smudges. The notebook is set against a dark background.



DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



350

212
1379
1167.21
350
1517.21
1379
138.21

CURVE FORMULAS

- Radius= $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve= D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)
- Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)
- Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2})$ (5) $= R \text{vers} \frac{\Delta}{2}$ (6)
- External= $E = T \tan \frac{\Delta}{4}$ (7) $= R \div \cos \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)
- Long Chord= $C = 2 R \sin \frac{\Delta}{2}$ (10) $\Delta = \text{Central Angle}$

1379
140
1519

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{2} = 414.49$ ft. From Table V correction=.36 or $T = 414.85$ ft. P. C.—Sta. P.I.— $T = 157+45.50$. Also from (4) $L = 746.00$ and P. T.—Sta. P. C. + $L = 164+91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = $158 - \text{Sta. P. C.} = 54.50$, hence offset = $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^\circ$ or = def. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8\frac{1}{2} = 136.2'$ or $2^\circ 16.2'$, or $= 2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 91.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{2} = 91.27$ and from Table V correction=.10 or $E = 91.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

11+67
 3.50
 15+17
 08
 49

727
 84
 473

360
 300
 660

3+70 on w

1342
 1167
 175

16+96.46
 7+39.76
 9.5670

533

325

1291 -17
 1595.53

86° 53' 30"

98° 34'

25.63

179.42

5142
 22530
 27672

300.63
 0.16
 300.47
 10.05
 310.52

DISTANCES FROM CENTER OF ROADWAY FOR
 CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
 For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20-16)+2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.