

1711

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS.

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \times 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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8960
7731
1129
1711

10204
7
71428

CITY ENGINEER'S OFFICE

INDEXED
completely

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

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X-Sept. of 15' Alley in Block 21
Lexington Park.

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140 287.90 10.44 286.50

163 296.94 6.17 295.31

B.M. Quince 4.29 301.48 297.19 S.E. BP
Fairmount

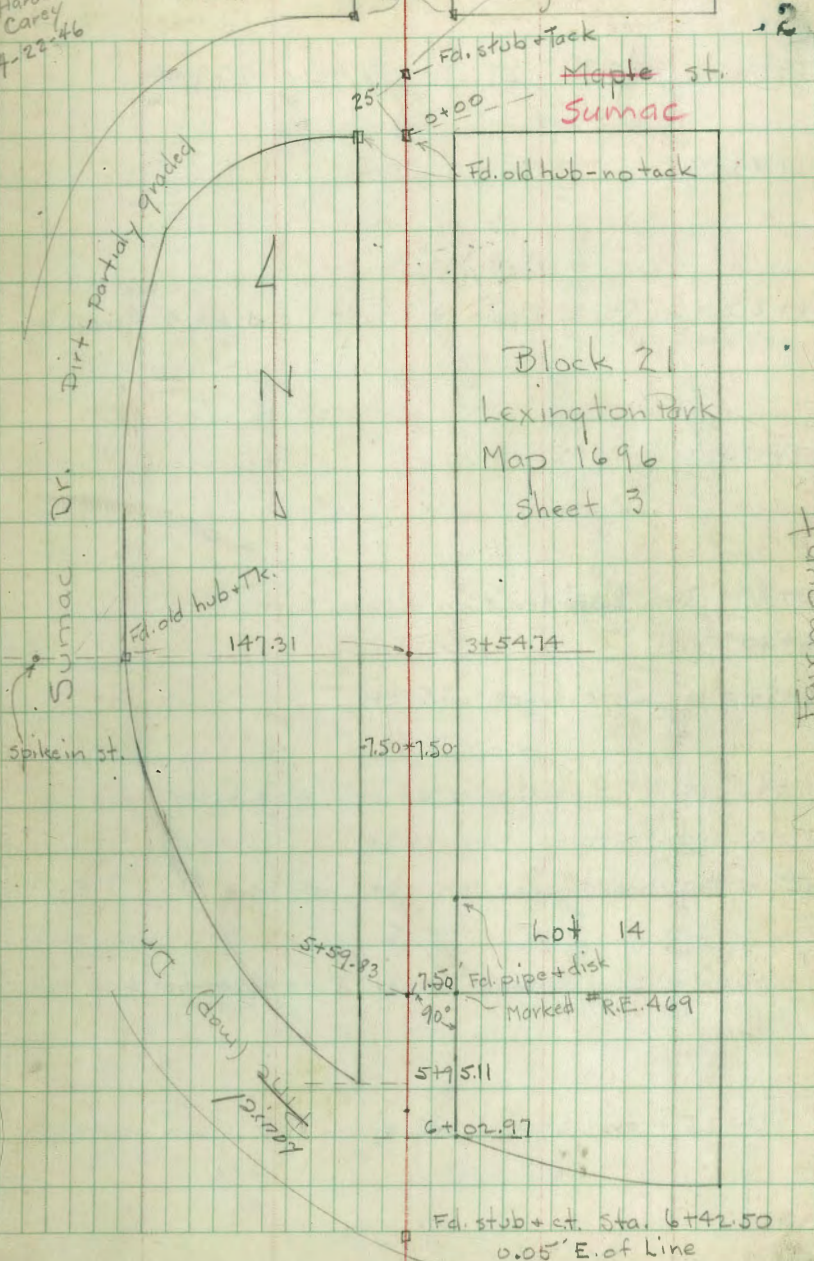
F. Osborne
Hardin
Carey
4-22-46

Indexed
C.S.K.

Fd. hubs

Tied out No. on E of
Ally 50' & 100' N.

2



Block 21
Lexington Park
Map 1696
Sheet 3

Fairmount

5+75

5+60

5+59.6 - 7.6 Lt. = " " " " " " " " " " " "

5+20 - 7.6 Lt. = Wedge of 3" pipe 4' high - set in Conc.

5+15

5+00 - 5.6 Rt. = P. pole

4+80 = S. end Conc. slab on Rt. = Driveway to gar. set way back

4+68 - 7.1 Rt. = end picket fence

4+42 = N. end Conc. slab on Rt.

4+39 - 7.1 Rt. = end of board + begin picket fence

T.P. 2.27 274.59 9.39 272.32

4+01 - 6.2 Rt. = P. pole

4+00 - 6.2 Rt. = beg. board fence

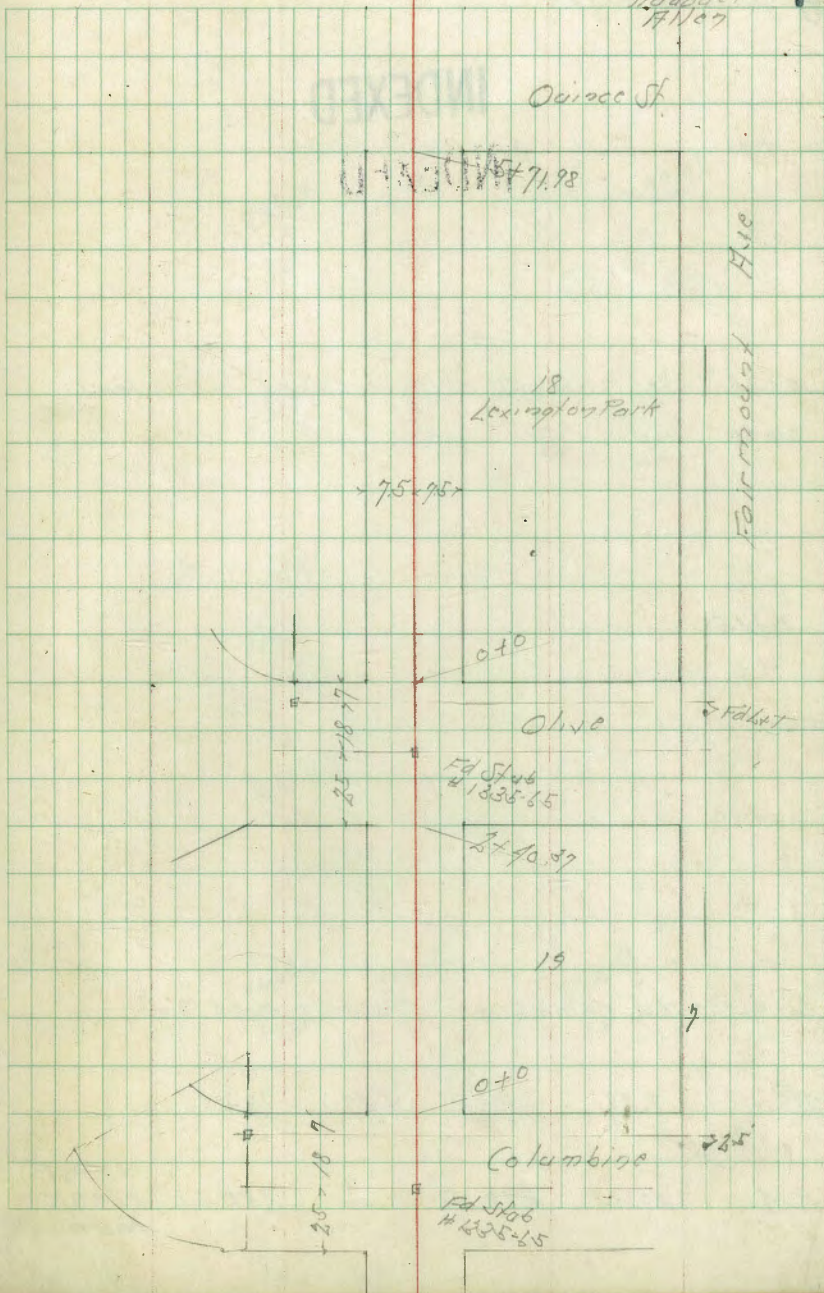
70.1	69.9	68.3	68.1	68.4	69.5
4.5 12	4.5 20	5.3 4	5.1 01	4.7 68.4	4.9 69.5
	70.1		59.9	69.4	69.8
	4.5 20		4.9 01	4.7 69.4	4.9 69.8
	70.1		70.1	69.8	69.5
	4.5 5		4.5	4.8 5	5.1 5
	71.2		71.1	71.29	71.19
	3.4 7.5		3.5	3.30 7.2	3.40 6
	72.3		72.3	72.39 58 for slab	72.34 on conc.
	2.3 7.5		2.3	2.37 7.2	2.51 19
			274.59	N.E. Cor. conc. slab	N.W. Cor. slab - side of House
	73.5		73.3	73.6	73.6
	4.8 6.5		5.4	4.8 5	4.8 5
			281.71		

Cross Section Alley's Block 18 x 19
Lexington Park
Levels next page

INDEXED

Indexed
C.S.K.

April 26 - 46
S. 1107
110000
110000
110000



Cross Section Alley Block 19 Lexington Park
 From Columbine to Olive West of Fairmount.
 Sketch Page 7

INDEXED

+91 7' Lt of 2" NY Wire Fence

+80

0+74 7' Lt of 2" NY Picket Fence + 5' Wire Fence

0+50

0+45

0+30

0+0 2" L. Columbine 7' Lt of 2" Picket Fence

TP 8.22 293.36 5.27 285.14

BM 10.34 290.51 280.17 NY BP
 Maple +
 Fairmount

Lt: N

S

Rt: E

8

288.9
 4.5
 7.5

288.6
 4.8

288.9
 4.5
 7.5

290.61
 4.75
 8.25

288.1
 5.3
 7.5

287.6
 5.8

288.1
 5.3
 7.5

288.0
 5.4
 8.0

288.12
 5.24
 7.5

287.81
 5.55
 7.5

287.43
 5.03
 7.5

286.2
 7.1
 7.5

286.0
 7.4

286.0
 7.4
 7.5

292.88

1+91

+80

+62

+60

+59

+52

1+50

+40

1+25

1+0

5.3 Lt of 2 - W/4 Wire Fence

6' Lt of 2 - W/4 10' Euc Tree

6' Lt of 2 - W/4 10' Euc Tree

5.2 Lt of 2 - S/4 Wire Fence

6' Lt of 2 - W/4 Power Pole

Lt. W

2

Rt. E

290.5

29

8.5 Euc Tree
Dist Floor

290.4

30

8.5 Euc Tree
Dist Floor

291.0

24

8.5 Barren
Dist

292.30

1.06

8.5 W/4 Euc Tree
Dist

290.8

26

7.5

290.7

27

291.2

22

7.5

292.33

1.08

8.5 Top of
Dist

289.9

35

20

290.3

21

7.5

290.3

21

290.6

28

7.5

292.08

1.28

7.5 Top of
Dist

289.3

20

289.4

20

7.5

289.3

21

289.6

28

7.5

291.20

2.16

7.5 Top of
Dist

292.36

JP 6.47 297.02 2.81 290.58 ^{on 25th} Oliver Alley

2+40.37 = 56.01 sec

+21

2+0

293.36

21-11

Pl. 2

10

290.8
2.6
7.5

290.9
2.5

291.1
2.3
7.5

292.09

291.0

291.0

291.0

1.37

3.4

5.4

2.4

10.6-14 hour
6.7-11.5
6.7-11.5
6.7-11.5
6.7-11.5

290.6
2.8
7.5

290.9
2.5

291.0
2.4
7.5

291.8
1.8
7.5

292.36

Cross Section Alley Block 18
Lexington Park
Sketch Page 7

indexed
C.S.K.

INDEXED

1785

1750

1710

0781

76 Lt of 2-Wly Pattern Pale

0750

0700 - M.L. Olive

297.02 of Ford

Lt: W

Z

P. 2.5

11

$\frac{291.7}{5.8}$
20

$\frac{292.0}{5.0}$
25

$\frac{292.0}{5.0}$
25

$\frac{292.3}{4.9}$
25

$\frac{293.2}{5.8}$
20

$\frac{290.2}{5.8}$
20

$\frac{291.3}{5.7}$
25

$\frac{291.5}{5.5}$
25

$\frac{292.1}{4.9}$
25

$\frac{292.5}{5.5}$
25

$\frac{293.1}{5.9}$
20

$\frac{289.9}{7.1}$
20

$\frac{291.1}{5.9}$
25

$\frac{291.2}{5.8}$
25

$\frac{291.6}{5.1}$
25

$\frac{292.2}{4.8}$
20

$\frac{292.5}{4.5}$
20

$\frac{291.2}{5.8}$
20

$\frac{292.1}{4.9}$
25

$\frac{292.3}{4.7}$
25

$\frac{292.8}{4.2}$
25

$\frac{293.5}{4.5}$
20

$\frac{291.3}{5.7}$
20

$\frac{291.9}{5.1}$
25

$\frac{291.9}{5.1}$
25

$\frac{292.3}{4.7}$
25

$\frac{293.7}{5.2}$
20

$\frac{290.7}{6.8}$
20

$\frac{291.2}{5.8}$
25

$\frac{291.4}{5.6}$
25

$\frac{291.8}{5.2}$
25

297.02

INDEX

3+40

+32 7.5 L of 2 = 5/4 Fence

2+0

2+80

IP 558 301.20 1.40 295.62

+51 6.9 L of 2 = 1/4 Power Pole

2+50

2+30

2+0

297.02

$\frac{295.37}{5.80}$
7.5

$\frac{295.28}{5.91}$
7.5 = 1/4 1/4
Conc. Floor

$\frac{296.2}{5.0}$

$\frac{296.2}{5.0}$
7.5

$\frac{297.19}{5.01}$
7.5 = 1/4 1/4
Conc. Floor

$\frac{295.8}{5.1}$
7.5

$\frac{295.9}{5.3}$
7.5

$\frac{295.8}{5.4}$

$\frac{295.9}{5.3}$
7.5

$\frac{296.0}{5.3}$
7.5

$\frac{295.7}{5.50}$

7.5 = 1/4 1/4
Conc. Floor

30/20

$\frac{294.7}{2.00}$
7.5

$\frac{295.1}{1.9}$
7.5

$\frac{294.9}{2.1}$

$\frac{295.1}{1.9}$
7.5

$\frac{295.6}{1.5}$
7.5

$\frac{294.2}{2.8}$
7.5

$\frac{294.4}{2.6}$
7.5

$\frac{294.3}{2.7}$

$\frac{294.5}{2.5}$
7.5

$\frac{295.4}{2.6}$

$\frac{292.8}{4.2}$
7.5

$\frac{292.9}{4.1}$
7.5

$\frac{292.5}{4.5}$

$\frac{292.9}{4.1}$
7.5

$\frac{293.6}{3.4}$
7.5

297.02

38M 594 297.23 SE 8P. Quince + Falmouth 297.19

5+72.0 = 5/8 Quince 7.2 ft of 1/2 = Ely CKC Clot 400 Post

5+35

5+0

TP 6.29 303.17 4.32 296.88

+92 6.8 ft of 1/2 = Wly Paper Pole

+59

+50 7.7 ft of 1/2 = Picket Fence

+21 7.2 ft of 1/2 = 1/4 Fence

+11 7.2 ft of 1/2 = 5/8 Fence

4+02

+96 8.1 ft of 1/2 = 1/4 Fence

3+71 8.2 ft of 1/2 = Fence
7.2 ft of 1/2 = Wly Paper Pole

30120

11-24

297.9
5.8
7.5

298.1
5.7
7.5

298.4
5.8
7.5

297.3
5.9
7.6

297.5
5.7
7.5

297.7
5.8
7.5

297.9
5.8
7.0

297.23
5.9
7.5

297.10
6.1
7.6

297.2
6.0
7.6

297.3
5.9
7.5

297.3
5.8
7.0

296.55
4.6
7.6

296.43
4.7
8.3

296.2
5.0
7.0

296.4
4.8
7.8

296.3
4.9
7.9

296.5
4.7
7.5

296.9
4.8
7.0

296.3
4.9
7.5

296.2
5.0
7.5

296.5
4.7
7.7

296.6
4.6
7.5

296.8
4.4
7.0

296.3
4.9
7.5

296.2
5.0
7.0

296.4
4.8
7.5

30120

Cross Section A/ley Block A Swans 2nd Add

From Maple to Olive

Sketch Page 14

INDEXED

see also
Pg 57
this Book

2+0 9.9 Lt of 1/2 - W/ly Picket Pole

TP 6.03 297.52 0.05 291.49

1+50 10.4 Rt of 1/2 - W/ly Fence

+46 9.9 Lt of 1/2 - W/ly Wire Fence

1+0 9.9 Rt of 1/2 - Fence 9.5 Lt of 1/2 - Wire Fence

0+90 9.5 Lt of 1/2 - W/ly Picket Pole

0+72

Reduced
J. Barrett
4-19-49
McClaman
5-5-49

0+50

0+48 9.9 Lt of 1/2 - Sty Wire Fence

0+31 9.8 Lt of 1/2 - W/ly Picket Fence

0+0 = N.L. Maple 10.2 Lt of 1/2 - Sty Picket Fence

0-4 10 Rt of 1/2 = Sty Lath Fence

BM 11.27 291.54

280.17

11.11 6P
Maple +
Fairmount

April 27 46

S. 0307
Lt. W
M. 194
H. 100
H. 100

Rt. E

15

290.9 291.4 291.5 291.8 292.0
4.6/30 6.1/10 6.0 6.7/10 5.5/30

290.2 290.4 297.52 290.7 291.2 291.4
1.6/30 1.0 0.8 0.6 0.0

289.9 290.1 290.1 290.5
1.6/10 1.4 1.6/10 1.0/30

289.68 288.7 288.4
1.86/10 2.8/10 3.1

287.1 287.2 287.3
4.4/10 4.5 4.2/10
10 - 800 1515
Coed. 19 10/10

291.54

410 97' H of $\frac{1}{2}$ - W/4 Parter Pole

3750

3712

370

486 10.6' H of $\frac{1}{2}$ - N/4 Wire Fence

2768

2750

2744 10.8' H of $\frac{1}{2}$ - S/4 Wire Fence
297.52

293.0
1.5
20

293.3
1.8
20

293.3
1.2
20

293.7
3.8
20

293.7
5.8
20

292.7
1.8
20

292.8
1.7
20

293.0
1.5
20

293.3
1.2
20

293.5
1.0
20

292.5
5.0
20
136.7
100.0

292.5
1.7
20

292.5
5.0
20

292.9
4.6
20

293.0
4.6
20

292.50
5.0
114.4
100.0

292.56
1.96
11.4
100.0

292.0
1.7
20

291.9
5.7
20

292.2
5.6
20

297.52

BM

6700.77

5725 97 Lt of 1/2 = 1/4 Power Pole

5750

5746

570 92 Lt of 1/2 = 1/4 Power Pole

4794

TP 6.43 300.51 2.14 294.08

4750

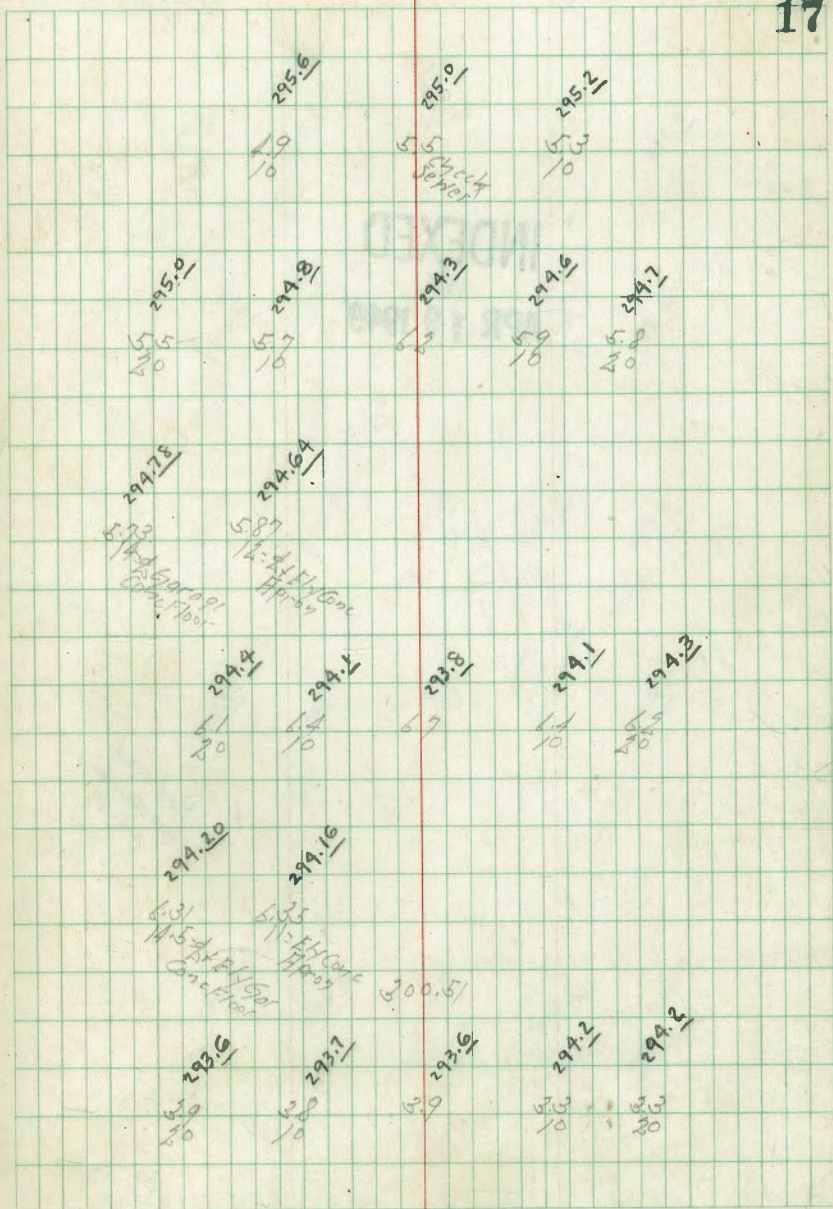
297.52

Lt.: 1/2

4

Rt.: 1/2

17



Cross Section Alley Block 13 Swan's Hdd
 From Maple South
 Sketch Page 14

INDEXED
 C.S.K.

INDEXED
 WK
 APR 19 1949

2+0

1+50

1+0

0+50

0+04 9' Pt 1/2 - Nly Anchor

0+0 - 5' Maple

BM 11.06 291.23

280.17

NK 80
 Maple
 Fairmount

Note!
 Ed. No change

Reduced
 meclanor
 5-5-49

April 29-49
 Si 3102
 77 added
 11/10

Lt = E

5

Rt = W

18

283.3	283.1	283.2	282.7	282.4
79 20	81 10	80	85 10	88 20

284.5	283.9	283.7	283.7	283.0
67 20	76 10	75	79 10	82 20

285.4	285.0	284.8	284.3	283.8
65 20	67 10	64	60 10	57 20

286.5	286.0	285.5	285.4	284.9
47 20	52 10	57	58 10	62 20

286.8	286.5	286.4	285.8	285.8
44 20	47 10	48	54 10	51 20

291.23

Slope Continues Down

4+30 No change

4+0 900 d

TP 0.20 269.90 12.96 269.70

3+75

3+68.70 POT 7.02 00 Stub

3+50

3+0

TP 0.36 282.66 8.93 282.30

2+50

291.23

252.4	252.5	249.2	252.6	257.4	260.5
17.5 20	17.4 10	20.7 6	17.5	12.5 10	9.1 20
266.5	265.2	263.7	263.0	268.8	269.8
2.4 20	4.7 15	6.2 10	6.9 8	4.3	1.1 10
			269.90		
276.2	275.5	274.5	274.9	275.5	
6.5 20	7.2 10	8.2	7.8 10	7.2 20	
278.0	277.5	277.4	277.2	277.1	
4.7 20	5.2 10	5.5	5.5 10	5.2 20	
280.5	280.2	280.2	279.7	279.4	
7.2 10	2.5 10	2.5	5.0 10	5.0 20	
		282.66			
282.0	281.8	281.6	281.2	281.0	
9.2 20	9.1 10	9.6	10.0 10	10.2 20	

Cross Section Laurel/St Fairmount to Sumac
 Sumac Dr. Laurel/St to Fairmount H.H.
 Flipped + Sketch 1335-13

indexed
 C.S.K.

INDEXED

2+0

+50

+36 206 ft of 7 - Sly Porryer Pole

+14 217 ft of 8 - Sly Anchor Pole

1+0

0+50

0-0 = B.C.R. = N.L. Fairmount

0-20 = W.C. Line Fairmount to North = Sly Paving

B.M. 8.25 270.18

261.92 1335-62

May 6. 46
 Station
 1000 ft
 1110

Rt. N

20

44 51 49 48 47 45 40 37
 35 25 22 15 15 19 31 25

43 48 53 52 48 47 40
 35 20 18 15 15 15 25

42 48 51 51 52 53 48 29
 35 21 18 15 15 15 19 25

51 51 59 58 55 57 52 48 40
 25 20 19 15 15 15 19 25 25

56 68 66 62 63 58 47
 35 21 15 15 15 16 25

663 640 634 622 597 592 585 541
 35 25 15 15 15 15 15 15
 270.18 137 130.06

+25 142 Rt of 2 - Fly Power + Tel pole
 4+05 = Case 5 steps + 1014 07 Rt

+82

+68 31.4 Lt of 2 - Fly Power Pole

+50

TP 5.37 272.74 2.81 267.37

3+35 146 Rt of 2 - S Fly Harbor Pole

2+98.28 - P.R.C Lt

2+50

270.18

Lt

Rt

Rt

61 35	54 25	48 15	44	440 1.5 Fly Pole	410 1.5 Fly Pole	2.30 12-Top Steps	2.2 15	1.7 15
----------	----------	----------	----	---------------------------	---------------------------	-------------------------	-----------	-----------

65 35	51 25	57 20	54 15	46	460 1.5 Fly Pole	440 1.5 Fly Pole	2.00 15-Top Steps	2.51 25-Top Steps
----------	----------	----------	----------	----	---------------------------	---------------------------	-------------------------	-------------------------

81 50	62 25	54 15	52	272.74	515 1.5 Fly Pole	3.84 15-Top Steps	3.07 2.5 12-Top Steps
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52 50	28 25	53 15	30	282 1.5 Fly Pole	1.45 15-Top Steps	0.63 2.5 12-Top Steps
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60 35	59 25	38 20	44 20	4.2 15	3.8	3.8 12	3.4 15	3.0 2.5
----------	----------	----------	----------	-----------	-----	-----------	-----------	------------

81 35	64 25	49 18	47 15	1.2	1.2 15	1.27 15
----------	----------	----------	----------	-----	-----------	------------

270.18

6+50

6+0

+5524 BCRT

IP 8.39 278.76 2.27 270.57

5+0

4+7124 - EC

4+34

272.74

LT-11

Z

RT-F

22

11.3 8.5 6.4 5.9 5.6 5.5 5.1 2.9
3.5 2.5 1.5 1.3 8 1.5 2.5

12.2 10.1 8.3 7.6 7.2 7.2 5.2 5.0 4.2
3.5 2.5 1.5 1.3 7.2 1.2 1.5 2.5

14.1 12.1 8.8 8.2 8.0 6.3 6.1 5.3
3.5 2.5 1.5 8 1.3 1.5 2.5

278.76

9.8 6.3 5.4 5.7 2.9 3.0 1.2 2.3
3.5 2.5 2.1 1.5 7 1.2 2.5

8.1 5.5 4.0 3.8 3.6 1.4 1.3 2.2
7.3 2.5 1.5 2.5 7 1.3 1.3 2.5

9.3 8.8 6.0 4.6 4.0 4.1 2.8 1.3
3.5 3.0 2.5 1.5 1.9 1.6 2.5

260.74
260.74
260.74

272.74

8782.08

8739.86

TP 11.03 287.70 2.09 276.67

7497.64 = BC. Pt.

+50

+25.73 FC

7+0

278.76

67

81

Pt

23

81 76 74 81 81 72 70 71
35 25 15 9 11 15 25

131 122 112 107 106 104 95 94 83
35 25 15 11 10 12 15 25

287.70

89 72 56 56 54 33 27 27 16
35 25 15 11 11 13 15 25

111 86 65 40 42 4.25 4.0 2.9
35 25 15 9 11 11.50 oil 2.5
oil

110 82 59 43 45 4.65 4.20 2.30
35 25 15 10 11 9.50 oil 2.50 oil
oil

108 85 62 50 48 4.8 2.8 2.1
35 25 15 11 10 1.5 2.5

278.76

174 Rt of 2 = Sky Port or Poll
 10 + 59.33 = W.L. Fairmount = Sky Curst + Pav = 79

10 + 20

10 + 0

9 + 80

9 + 50

9 + 24.29 = E.C. = W.L. Hiley 14 Rt of 2 = Sky Port or Poll

287.70

7.1
2.5
7.38
1.5 = Ob Top
7.93
1.5 = Gutter
8.16
8.65
1.5 = Gutter
8.95
1.5 = Ob Top
7.4
2.5

6.3
2.5
6.3
1.5
7.3
1.4
7.1
6.9
9
6.1
1.5
6.9
2.5

5.5
2.5
5.3
1.5
6.0
1.4
5.8
5.9
9
5.3
1.2
5.9
1.3
4.6
2.4 = 11.24 = 10.7
Hills

4.6
2.5
4.3
1.5
5.0
1.4
5.0
5.1
9
4.6
1.1
4.5
1.5
4.7
2.5

4.2
2.5
4.9
1.5
4.7
1.3
5.3
5.3
11
4.8
1.3
4.9
2.5
4.8
2.9 = 11.24 = 10.7
Dirt Floor

5.9
2.5
5.1
1.5
5.4
1.3
6.1
6.0
1.0
5.3
1.2
5.3
1.3
5.1
2.5

287.70

BM

7.42 280.27

NW 8P
Maplet
Fairmount
280.17

10 + 7933 = N/C1/Curb Line Fairmount

10 + 6933 = C6 BC R1 + 21

287.70

7.46 25=C6	7.97 25=90Hr	8.16 15	8.40	8.60 15	8.71 15=90Hr	8.18 15=C6
---------------	-----------------	------------	------	------------	-----------------	---------------

7.71 25	7.48 15=C5Top	8.09 15=90Hr	8.28	8.58 15=90Hr	8.10 15=C5Top	8.05 15
------------	------------------	-----------------	------	-----------------	------------------	------------

287.70

Sketch page 26

INDEXED

1+50

1+0

0+90

IP 10.10 272.55 139 262.45

0+50

0+14

0+0 = E.L. Survey

Taken on Diagram

B.M. 11.79 262.84

252.05

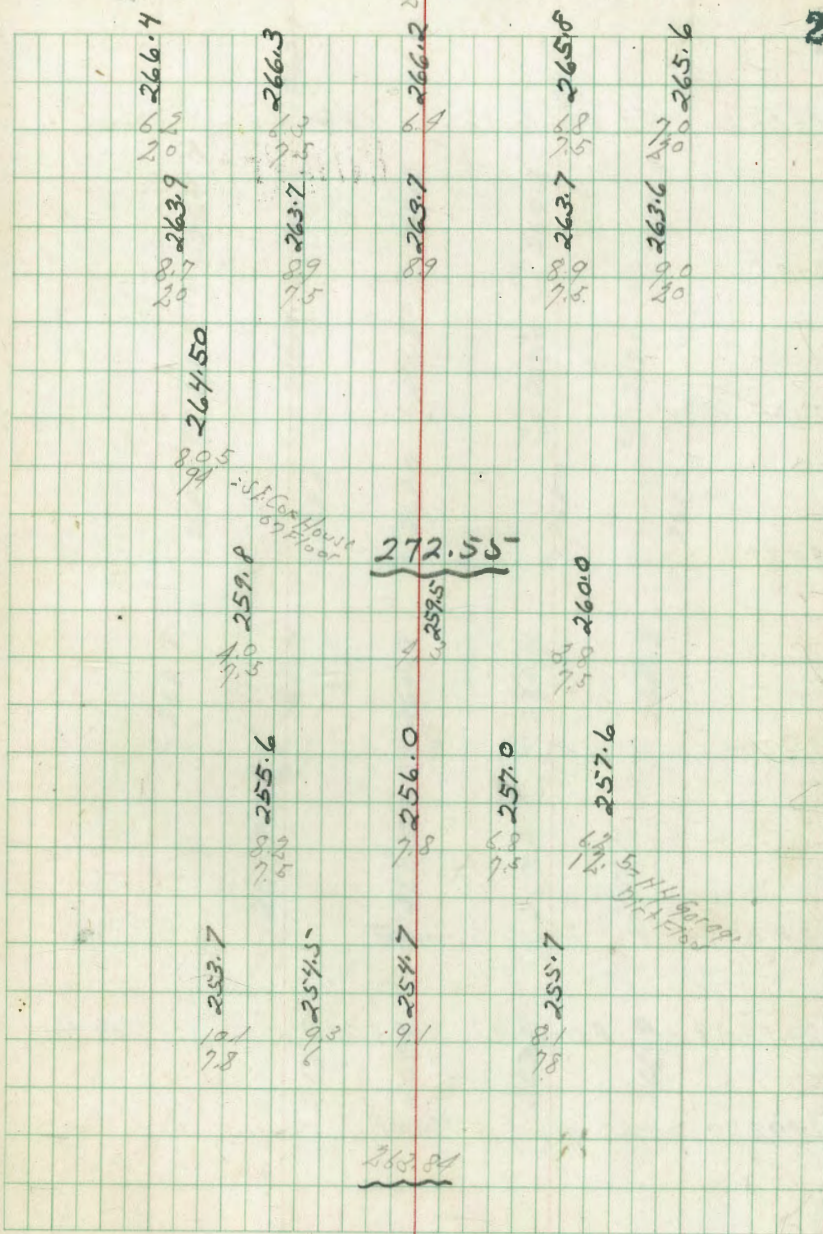
0.00 ft
1.93%
Slope of
1335-75

Lt. H

indexed
C.S.K.

Rt. S

27



370.31 = H.L. Madesto Taken on diagonal

3735

370

2780

2750

2707.89 = F.L. H & S #11 of "B"

2700.39 = 1/2 #11 of "B" 5.21

1792.89 = H.L. H & S #11 of "B"

27255

Lt

268.7	268.3	266.6	264.7	262.1	261.51
1.2	1.5	1.8	2.1	2.4	2.7
20%	15%	10%	5%	0%	0%
267.7	266.1	264.9	264.2	264.1	262.4
1.9	1.5	1.8	2.1	2.4	2.7
15%	10%	5%	0%	0%	0%
267.5	266.0	266.8	264.2	264.1	262.4
5.1	5.8	6.5	7.2	7.9	8.6
5%	10%	15%	20%	25%	30%
267.5	267.6	267.3	264.4	264.1	262.4
5.1	5.0	4.9	4.8	4.7	4.6
5%	5%	5%	5%	5%	5%
266.9	267.1	267.1	264.3	264.1	262.4
5.1	5.0	4.9	4.8	4.7	4.6
5%	5%	5%	5%	5%	5%

27255

2+9678 = ~~L~~ Alley C 5.23

07% Hub

2+8928 = SL Alley C

2+45

2+0

1+97

275.26

Lt=H

L

Rt=E

30

270.91

5.25
20

269.8

5.25
20

270.3

5.25
20

270.3

270.7

4.6
7.5

270.7

4.8

270.5

4.6

270.7

4.9

270.4

4.6
7.5

270.7

4.6
7.5

270.9

5.0
7.5

270.3

4.6
20

271.0

4.6
20

271.0

4.35
14 = 14.75
0.40
17.10

275.26

Cross Section Alley C - Block 23
 Lexington Park
 Sketch Page 26

BM 13.44 261.82

1785.18 = W.L. Modesto Taken on Diagonal

1740

140

0+91.91 = F.L. Alley "B"

0+76.91 = W.L. Alley "B"

0+40

0+0 = F.L. Sumac Taken on Diagonal

INDEXED

275.26 Rt. Ford

L.F.N

Rt. 5

21.2

269.0 268.8 265.9

270.0 270.3

270.0

265.2

269.8

270.5

264.89

269.8

270.6

264.7

269.7

270.7

270.1

270.2

270.7

266.7

262.1

270.3

266.7

266.7

261.9

266.3

266.4

261.8

269.9

269.8

270.1

269.6

269.0

268.8

265.9

270.0

270.3

270.5

269.8

269.7

264.7

269.8

270.6

261.9

266.3

266.4

261.8

269.9

269.8

270.1

269.6

269.0

268.8

265.9

275.26

Cross Section Juniper St.
Sumac St to Fairmount Place
Sketch Page 26

Indexed
C.S.K.

May 16 4
St. Hwy
Hedge
1/2 in
Ht. 11

170

INDEXED

0+73.67 = BC on H

0+38

See FB 222
53

0+51.96 = E.L. Sumac to North

0+25.98 = Sumac to North

0+10 4.5 ft of $\frac{1}{2}$ = 11y Parva Pole

0+0 = N.L. Sumac to North

B.M. 12.75 265.59 252.84
Ht. 11 1/2
Sumac
13.5-74

408	264.51	30	259.1	68	259.2	68	259.4	68	259.5
165	260.1	30	259.0	68	257.9	68	259.6	68	259.9
165	259.3	30	256.5	68	257.3	68	259.6	68	259.9
165	259.2	30	256.1	68	257.4	68	259.4	68	260.1
165	255.9	30	256.1	68	257.4	68	259.4	68	260.1
165	255.3	30	256.1	68	257.4	68	259.4	68	260.1
165	251.2	30	256.1	68	257.4	68	259.4	68	260.1
165	252.1	30	256.1	68	257.4	68	259.4	68	260.1
165	252.84	30	256.9	68	258.4	68	258.0	68	258.4
165	253.4	30	256.1	68	257.4	68	258.0	68	258.4
165	254.0	30	256.1	68	257.4	68	258.0	68	258.4

10+17.97 = 5+63.70 Prop. Service	6.40	171.91	07 Stub
TP	1.36	178.31	12.03
For Check		5.34	183.64
10+0		9.8	
TP	0.32	188.98	12.88
9+50		19	
TP	0.14	201.54	12.59
9+17.43 = FL Fairmount Place		2.83	07 Hub
TP	0.47	213.99	12.68
9+0		8.9	
TP	0.65	226.20	12.68
8+50		8.8	
TP	0.86	238.23	12.91
8+0		6.6	

7+89.71 = FL Fairmount Place

TP	1.02	250.31	12.88
----	------	--------	-------

7+50

262.17

249.7	243.9	244.8	246.13	246.4	246.4	248.5	249.1
1.33	64	55	4.18	3.9	3.9	1.30	1.30
0.33	30	15	07 May	15	20	20	00
252.2	253.4	255.6	255.5	255.4	256.7	256.7	256.2
1.30	8	6.6	250.31	6.8	2.1	8.6	0.6
0.30	15	15	07 May	15	20	20	00

262.17

INDEXED 4-11

R-5

2+7141 = W. L. Fairmount Place

TP 1.22 228.53 12.61 227.31

2+35

239.92

159 20	212.6	114 7.5	217.1	873 675.64	219.80	67 7.5	221.8	91 20	224.4
18 20	221.3	139 7.5	226.0	228.55 220.2	229.80	98 7.5	230.1	8 20	236.0
									20 Total Fall
					<u>239.93</u>				

Proposed Sider Fairmount Ave.
Home Ave. to Laurel St.

INDEXED

B.M.	12.79	160.84	148.05	8 P.P. Cor. Box Culvert Fairmount Home Ave
0+0	- Existing Ditch	10.74	150.10	27 Rim
+11	Edge Oil Paving	10.12	150.72	
+65	Edge " "	6.96	153.88	
+76.42	627° 57' 30" Rt	3.51	155.23	as Stub
+170		8.6	157.2	
"	10 ft Edge Conc Pav	2.95	157.89	
+21		1.7	159.1	
TP	12.19	172.90	0.13	160.71
+23		11.8	161.1	
+30		9.3	163.6	
2+0		3.8	169.1	
"	10 ft of 2" Edge Pav	3.19	169.73	
TP	12.93	185.70	0.18	172.72
+50		11.0	174.7	
2+0		4.8	180.9	
"	10 ft of 2" Edge Pav	4.55	181.15	
+18	2 1/2 ft of 2" Fly 18"	2.28	183.42	27 Top
"	2 1/2 ft of 2" Fly 18" Corp. Iron Culv.	4.84	180.86	Fly 18" Corp.
+25		1.9	183.8	
+26	= Bottom of Side Ditch	3.5	182.2	
+38	" " "	2.3	183.4	
+39		0.5	185.2	
TP	12.43	197.94	0.19	185.51
+50		11.2	186.7	

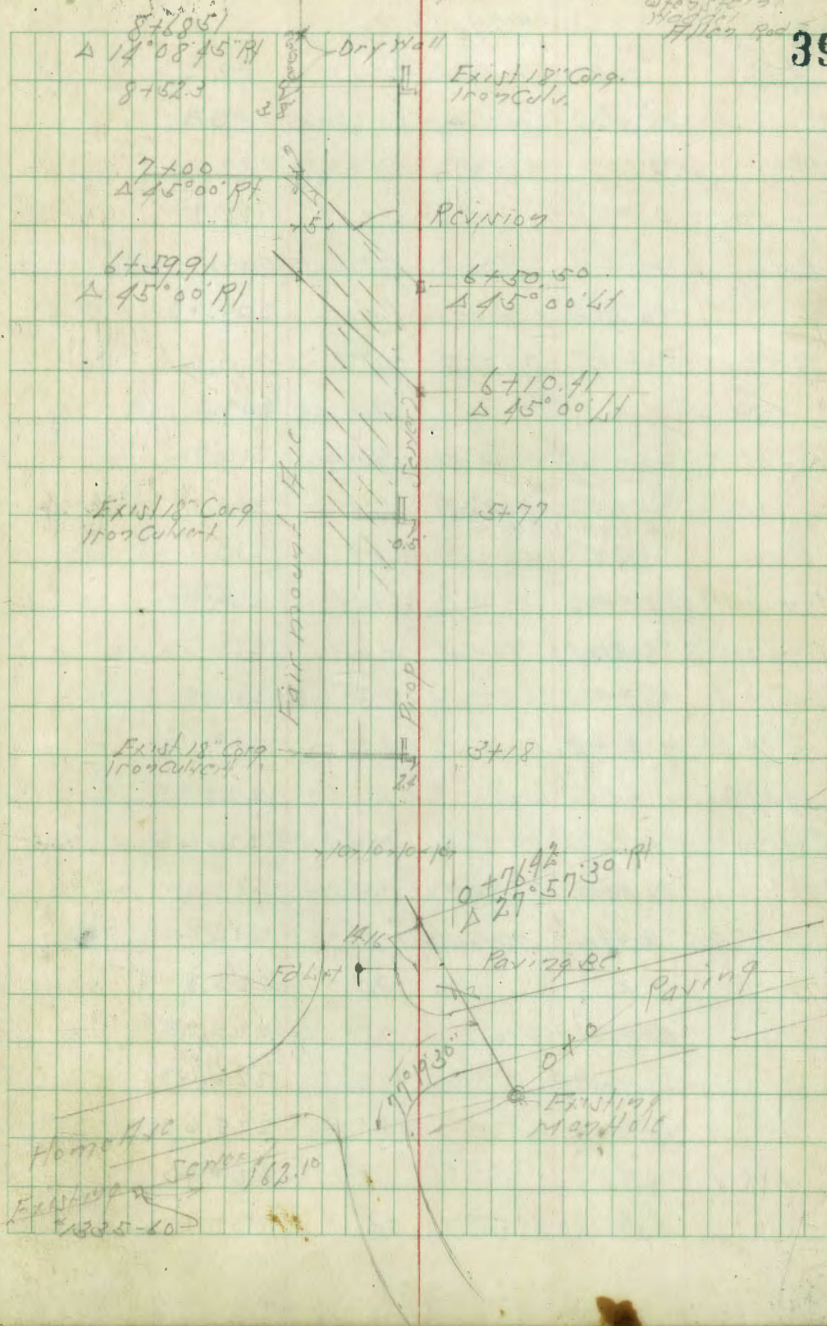
Indexed
e.s.k.

Cont Page 1

May 30-48

S. P. Co.
S. P. Co.
S. P. Co.

39



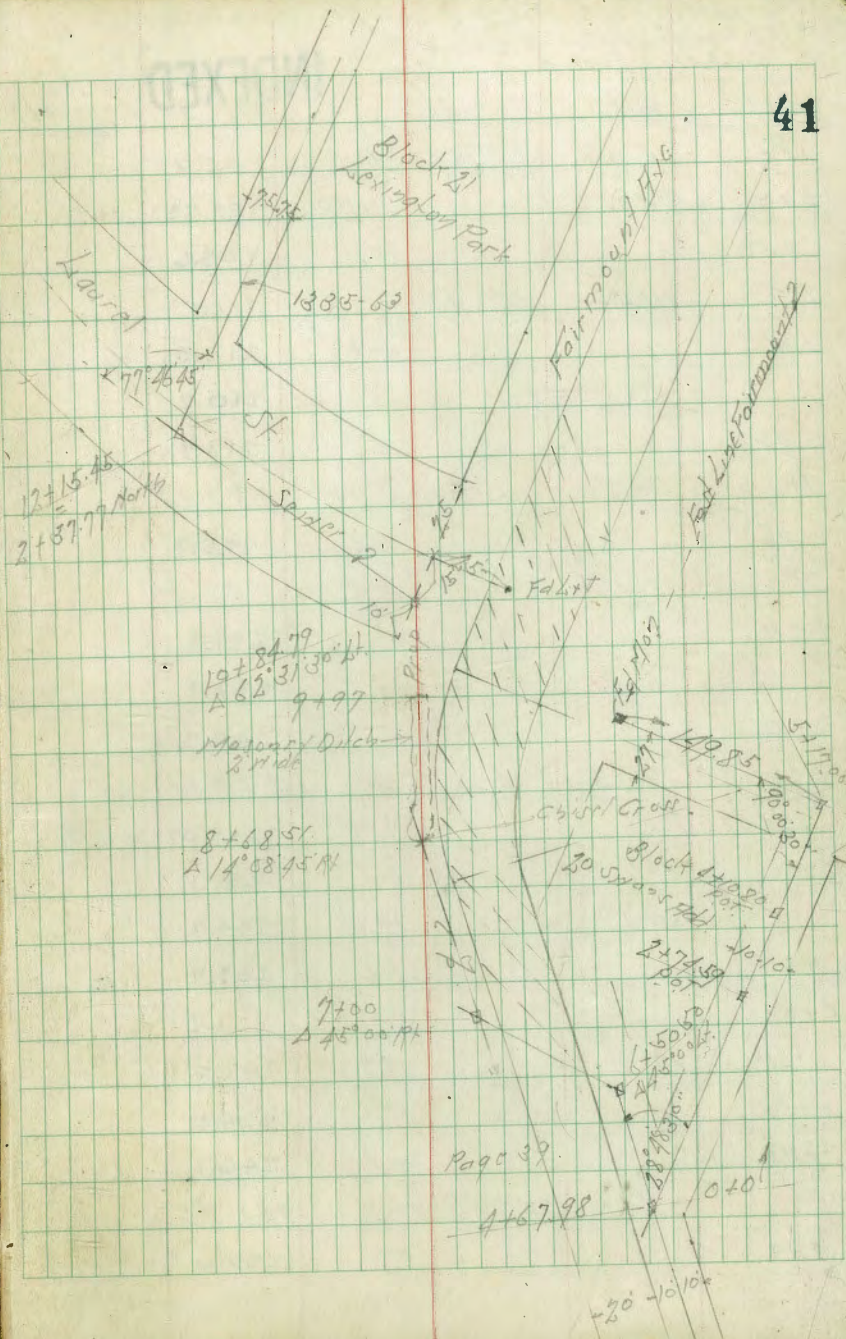
19794				
4+0			5.7	192.2
"	10' Lt of $\frac{1}{2}$ Edge Pav	4.0		193.3
TP	12.65	210.49	0.10	197.84
+50			12.8	197.7
5+0			6.8	203.7
"	10' Lt of $\frac{1}{2}$ Edge Pav	6.06		204.43
TP	11.87	222.08	0.28	210.21
+50			12.3	209.8
+77	0.5' Lt of FH H. Wall	9.34		212.74
"	4.4' Lt " " " " " "	12.29		209.79
6+0	Corp Iron Culvert	4.0		218.1
+10.41	Δ 45° 00' Lt	3.69		218.40
"	8' Rt of $\frac{1}{2}$ = Top Cut	+1.5		223.6
+13		5.3		216.8
+24.45	= Edge Paving	3.96		218.12
+52.83	" " "	1.53		220.55
+59.91	Δ 45° 00' Rt	0.43		221.65
TP	11.98	232.63	0.42	221.65
+59.91	15' Lt of $\frac{1}{2}$ on Full Slope	22.2		211.4
7+0			8.3	225.3
"	53 Rt of $\frac{1}{2}$ = Edge 1	7.88		225.75
"	1' Lt of $\frac{1}{2}$	7.0		226.63
"	15' Lt " "	8.0		225.63
+18		6.2		227.4
"	4' Lt of $\frac{1}{2}$ = Top Cut	0.5		233.1

23363				
7+50			2.5	231.1
"	4' Lt of $\frac{1}{2}$ = Top Cut	+2.4		236.0
TP	12.95	246.46	0.12	233.57
8+0			8.7	237.5
"	53 Rt of $\frac{1}{2}$ Edge Paving	9.93		237.03
"	7' Lt " "	9.1		237.4
"	15' Lt " " on Full Slope	12.0		234.5
+25	27' Lt of $\frac{1}{2}$ = $\frac{1}{2}$ Box Pole			
+50			5.7	242.8
"	7' Lt of $\frac{1}{2}$	11.8		234.7
"	15' " " "	15.7		230.8
+52.3	38' Lt of $\frac{1}{2}$ - 11' 18" Corp Iron Culvert	8.17		238.29
+68.51	Δ 11° 08' 45" Rt	1.42		245.04
"	1' Lt = Bottom Nails	3.4		243.1
"	6' Lt	3.1		243.4
TP	13.39	258.40	0.45	246.01
9+0	Bottom 4' Masonry	10.67		247.43
"	42' Rt of $\frac{1}{2}$ = Edge Pav	10.07		248.33
"	6' Lt of $\frac{1}{2}$ = Top Cut	+1.8		260.2
+50	= 5' Lt Bottom 2' Masonry Ditch	4.7		253.7
"	3' Lt of $\frac{1}{2}$	4.7		253.7
"	6' Lt of $\frac{1}{2}$ = Top Cut	+5.7		264.1
TP	10.17	268.51	0.06	258.34
+97	M/M Masonry Ditch	9.88		258.63
10+0		9.8		258.7

268.51

10+0	6' Rt of 1/2 - Edge Pav	9.11	259.40	
"	5.5 ft	0.0	268.5	
+50		5.7	262.8	
"	9' Lt of 1/2	5.2	263.3	
+71	48 Rt of 1/2 - 1/2 Post or Pole			
+84.79	62° 31' 30" Lt	5.05	263.46	on Stake
11+0		4.6	263.9	
+50		3.9	264.6	
12+0		3.7	264.8	
+15.25		3.71	264.80	264.85 1335-14
2+37.77	to rock			

Level Revision 6+10.41 to 7+00				
B.M.	9.56	227.96	218.40	6+10.41
			224.67	
6+50.50	Δ 45° 00'	3.69	3.69	on Stake
	6' Rt of 1/2 - Top of	+5.8	233.8	
+65.4	Edge Pav	5.30	222.60	
+93.7	"	2.85	225.11	
7+0	Δ 45° 00'	2.08	225.88	on Stake



S:

X SEC of Grape St. = 75' wide
12' curbs
12.75 1/4"

INDEXED

29th to 30th St. W.L.O. # 1035

Rush!

SW BR	0.55	275.57	✓	275.02	Grape and 30th
T.P.	0.71	263.34	✓	12.94	262.63
T.P.	2.54	255.59	✓	10.29	253.05

Fd. B.P. OUT. only Ed. table
N.W. Cor. of 29th & Grape
4.57
251.02
250.92
0.10
Curb bulged up

W.L. of 29th - 95'

N CB	12.85	243.14	✓
95	12.98	242.61	✓
1/4	12.65	242.94	✓
C	12.72	242.86	✓
1/4	13.38	242.21	✓
95	14.26	241.33	✓
S CB	13.62	241.97	✓

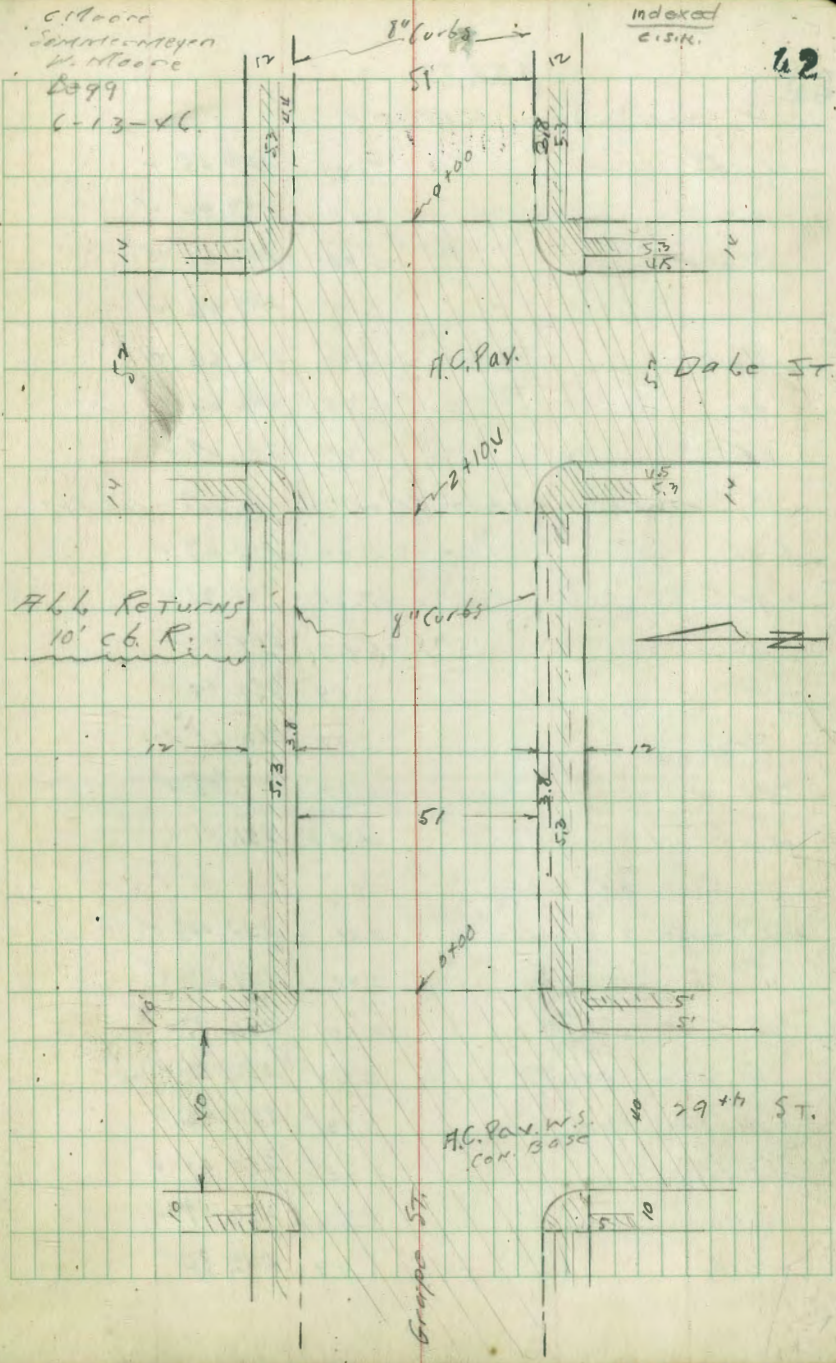
W.L. 29th - 50'

S CB	10.31	245.28	✓
95	10.90	244.69	✓
1/4	9.90	245.69	✓
C	9.10	246.49	✓
1/4	9.04	246.55	✓
95	9.27	246.32	✓
N CB	8.75	246.84	✓

C. Moore
Sammelen
W. Moore
1899
6-13-46

Indexed
C.S.K.

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W.L. 29th - 10'

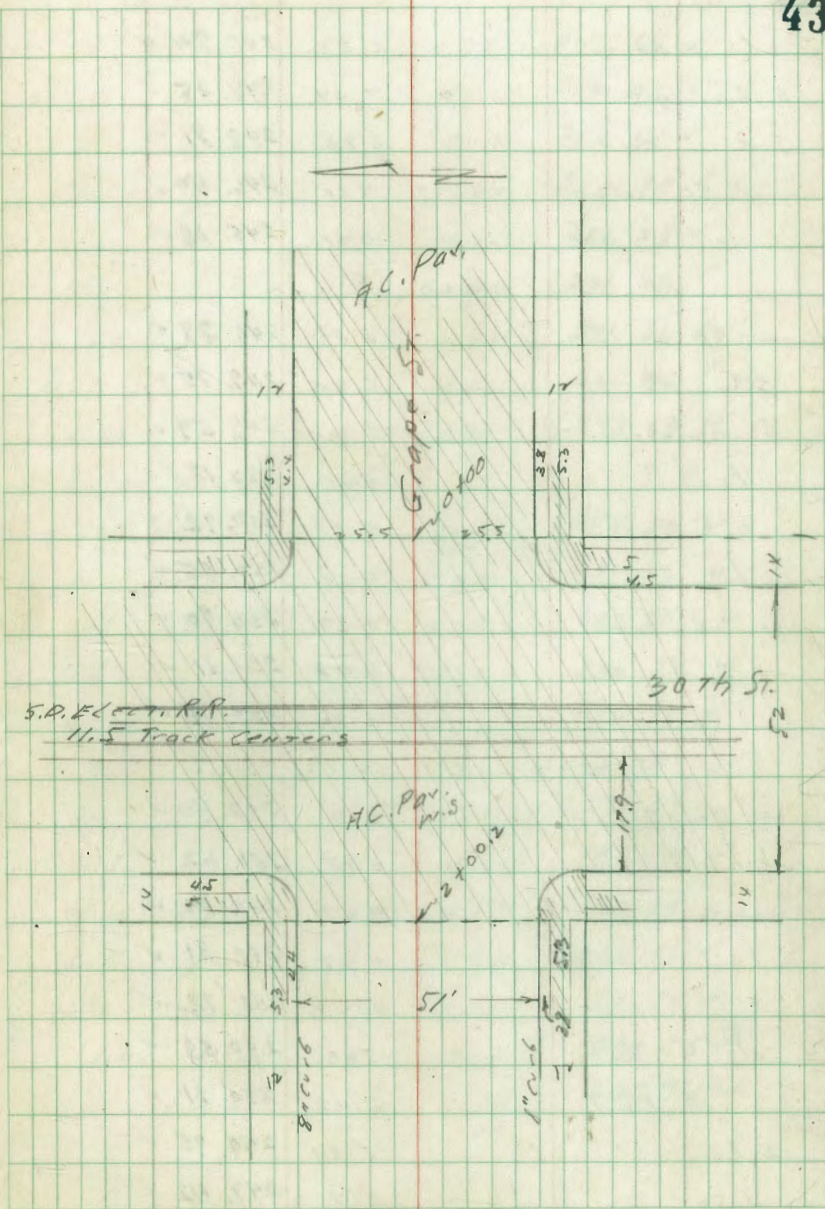
N.C.B.	5.44	250.15 ✓
9T	6.15	249.44 ✓
1/4	5.98	249.61 ✓
c	6.17	249.42 ✓
1/4	6.93	248.66 ✓
9T	7.93	247.66 ✓
S.C.B.	7.52	248.07 ✓

W.L. 29th = 60' wide, 10' cbs 10' 1/2"

S.C.B.	6.92	248.67 ✓
9T	7.38	248.21 ✓
1/4	6.19	249.40 ✓
c	5.59	250.00 ✓
1/4	5.38	250.21 ✓
9T	5.57	250.02 ✓
N.C.B.	4.58	251.01 ✓

W.L. 29th

N.L. - 50' curb	3.11	252.48 ✓
" " 9T	3.71	251.88 ✓
N.L. curb	4.62	250.97 ✓
N.L. 9T	5.28	250.31 ✓
N.C.B. Pav.	5.13	250.46 ✓
1/4 "	4.98	250.61 ✓
c "	5.20	250.39 ✓
1/4 "	5.79	249.80 ✓



255.59

S. cb Pav	6.85	248.74 ✓
S.L. 9T	7.34	248.25 ✓
S.L. curb	6.78	248.81 ✓
+ 50 curb	9.10	246.49 ✓
" 9T.	9.71	245.88 ✓
W 1/4 of 29th		
- 50	8.81	246.78 ✓
S.L.	6.44	249.15 ✓
S. cb Line	6.00	249.59 ✓
1/4	5.41	250.18 ✓
c	4.87	250.72 ✓
1/4	4.64	250.95 ✓
N. cb. Line	4.69	250.90 ✓
N.L.	4.48	251.11 ✓
+ 50	2.84	252.75 ✓
E 29th St.		
- 50	2.19	253.40 ✓
N.L.	3.97	251.62 ✓
N. cb. Line	4.29	251.30 ✓
1/4	4.28	251.31 ✓
c	4.47	251.12 ✓
1/4	5.06	250.53 ✓
S. cb. Line	5.48	250.11 ✓
S.L.	5.84	249.75 ✓
+ 50	8.17	247.42 ✓

255.59

E-4th St

44

E 1/4 29th		
- 50	7.94	247.65 ✓
S.L.	5.51	250.08 ✓
S. cb Line	5.18	250.41 ✓
1/4	4.84	250.75 ✓
c	4.31	251.28 ✓
1/4	3.99	251.60 ✓
N. cb. Line	3.93	251.66 ✓
N.L.	3.63	251.96 ✓
+ 50	1.90	253.69 ✓
E. cb. of 29th		
- 50 cb	1.04	254.55 ✓
" 9T	1.83	253.76 ✓
N.L. curb	2.75	252.84 ✓
" 9T	3.36	252.23 ✓
N. cb Pav	3.63	251.96 ✓
1/4	3.72	251.87 ✓
c	4.12	251.47 ✓
1/4	4.54	251.05 ✓
S. cb Pav	5.16	250.43 ✓
S.L. 9T	5.58	250.01 ✓
S.L. curb	4.75	250.84 ✓
+ 50 curb	7.04	248.55 ✓
" 9T	7.83	247.76 ✓

255.59

0 + 100 = E. Co. 7957 = Pav. edge

S cb	4.69	250.90	✓
9T	5.16	250.43	✓
1/4	4.30	251.3	✓
c	3.82	251.77	✓
1/4	3.45	252.14	✓
9T	3.45	252.14	✓
N cb	2.66	252.93	✓
0 + 10			
N cb	2.03	253.56	✓
9T	3.0	252.6	✓
1/4	2.9	252.7	✓
c	3.7	252.4	✓
1/4	3.8	251.8	✓
9T	4.6	251.0	✓
S cb	4.04	251.55	✓

T.P. 12.60 266.50 1.69 253.90 ✓

0 + 50

S cb	12.4	254.36	✓
9T	12.8	253.7	✓
1/4	12.0	254.5	✓
c	11.3	255.2	✓
1/4	11.0	255.5	✓

266.50

Graps St.

45

N 9T	10.9	255.60	✓
N cb	10.24	256.26	✓
0 + 88			
N cb	7.70	258.80	✓
9T	8.4	258.1	✓
1/4	8.0	258.5	✓
c	8.2	258.3	✓
1/4	9.3	257.2	✓
9T	9.9	256.6	✓
S cb	9.60	256.90	✓
1 + 10			
S cb	8.09	258.41	✓
9T	8.4	258.1	✓
1/4	7.8	258.7	✓
c	6.7	259.8	✓
1/4	6.4	260.1	✓
9T	6.8	259.7	✓
N cb	6.27	260.23	✓
1 + 50			
N cb	3.57	262.93	✓
9T	4.1	262.4	✓
1/4	3.4	263.1	✓
c	3.6	262.9	✓
1/4	4.7	261.8	✓
9T	5.7	260.8	✓
S cb	5.06	261.44	✓

266.50

1 ± 96.4

S cb	1.58	264.92 ✓
9T	2.11	264.4 ✓
1/4	1.14	265.1 ✓
C	0.7	265.8 ✓
1/4	0.8	265.7 ✓
9T	1.0	265.5 ✓
N cb	0.36	266.14 ✓

T.P. 6.93 272.41 ✓ 4.02 265.48 ✓

10.4
2 + 0.4 = W.L. Dale St. 80' wide
For edge 14' curbs
13' 1/4"

N cb	5.33	267.08 ✓
9T	6.09	266.32 ✓
1/4	5.90	266.51 ✓
C	6.07	266.34 ✓
1/4	6.36	266.05 ✓
9T	6.93	265.48 ✓
S cb	6.43	265.98 ✓

W cb, Dale

- 50 curb	8.88	263.53 ✓
" 9T	9.38	263.03 ✓
S.L. curb	6.39	266.02 ✓
" 9T	4.91	265.50 ✓
S cb Dale Pav	6.53	265.88 ✓

272.41

Grape

46

S 1/4	5.85	266.56 ✓
"	5.48	266.93 ✓
N 1/4	5.43	266.98 ✓
W. L. Dale Pav.	5.64	266.87 ✓
N.L. 9T	5.82	266.59 ✓
N.L. curb	5.30	267.11 ✓
+ 50 curb	4.24	268.17 ✓
" 9T	4.77	267.64 ✓

W 1/4 Dale

- 50	3.77	268.64 ✓
N.L.	4.80	267.61 ✓
cb.	4.95	267.46 ✓
1/4	4.92	267.49 ✓
C	5.08	267.33 ✓
1/4	5.30	267.11 ✓
cb.	5.66	266.75 ✓
S.L.	5.88	266.53 ✓
+ 50	8.39	264.02 ✓

E Dale

- 50	7.72	264.69 ✓
S.L.	5.27	267.14 ✓
cb	5.03	267.38 ✓
1/4	4.85	267.56 ✓
C	4.71	267.70 ✓
1/4	4.50	267.91 ✓

272.41

N cb	4.30	268.11 ✓	
N.L.	4.16	268.25 ✓	
+ 50	3.00	269.37 ✓	
E 1/4 Dale			
- 50	2.85	269.56 ✓	
N.L.	4.03	268.38 ✓	
N cb Line	4.25	268.16 ✓	
1/4	4.40	268.01 ✓	
C	4.54	267.87 ✓	
1/4	4.68	267.73 ✓	
S cb Line	4.88	267.53 ✓	
S.L.	5.10	267.31 ✓	
+ 50	7.61	264.80 ✓	
E cb Dale			
- 50 cb	6.88	265.53 ✓	
- 50 9T	7.64	264.77 ✓	
S.L. cb	4.42	267.99 ✓	
S.L. 9T	5.25	267.16 ✓	
check to S.E.B.P. Grape + Dale	Curb Outdged out	4.40	268.01 267.95 0.06 High
S.L. cb Line par.	5.03	267.38 ✓	
S 1/4	4.83	267.58 ✓	
C	4.64	267.77 ✓	
N 1/4	4.50	267.91 ✓	

272.41

Grape

47

N cb Line, Par	4.34	268.08 ✓
N.L. 9T	4.12	268.29 ✓
N.L. cb	3.36	269.05 ✓
+ 50 cb	2.23	270.18 ✓
" 9T	3.00	269.41 ✓
0 + 100. = E.L. Dale ST. Par. edge		
N cb	3.32	269.09 ✓
9T	4.16	268.25 ✓
1/4	4.17	268.24 ✓
C	4.33	268.08 ✓
1/4	4.63	267.78 ✓
9T	5.02	267.39 ✓
S cb	4.34	268.07 ✓
0 + 14 dirt Roadway row		
S cb	3.96	268.45 ✓
9T	4.17	267.7 ✓
1/4	4.0	268.4 ✓
C	3.6	268.8 ✓
1/4	3.5	268.9 ✓
9T	3.8	268.6 ✓
N cb	2.92	269.49 ✓
0 + 50		
N cb	1.66	270.75 ✓
9T	2.7	269.7 ✓
1/4	2.3	270.1 ✓

272.41

C	2.2	270.2 ✓
S 1/4	2.9	269.5 ✓
9T	3.5	268.9 ✓
S CB	2.71	269.70 ✓

T.P.	8.17	279.69 ✓	0.89	271.52 ✓
------	------	----------	------	----------

0 + 85

S CB	8.70	270.99 ✓
9T	9.6	270.1 ✓
1/4	8.8	270.9 ✓
C	8.3	271.4 ✓
1/4	8.4	271.3 ✓
9T	8.6	271.1 ✓
N CB	7.69	272.00 ✓

1 + 15

N CB	6.70	272.99 ✓
9T	7.6	272.19 ✓
1/4	7.2	272.5 ✓
C	7.3	272.4 ✓
1/4	7.9	271.8 ✓
9T	8.3	271.4 ✓
S CB	7.68	272.01 ✓

1 + 50

S CB	6.45	273.25 ✓
------	------	----------

279.69

Grape

48

S 9T	7.2	272.5 ✓
1/4	6.5	273.2 ✓
C	6.0	273.7 ✓
1/4	6.1	273.6 ✓
9T	6.5	273.2 ✓
N CB	5.41	274.28 ✓

1 + 86.2

N CB	4.18	275.51 ✓
9T	5.1	274.6 ✓
1/4	4.7	275.0 ✓
C	4.7	275.0 ✓
1/4	5.2	274.5 ✓
9T	5.7	274.0 ✓
S CB	5.12	274.57 ✓

2 + 00.7 = W.L. 30 TH =
For edge.80' wide
14' curb
13' 1/4"

S CB	4.65	275.04 ✓
9T	5.17	274.52 ✓
1/4	4.57	275.12 ✓
C	4.23	275.46 ✓
1/4	4.23	275.46 ✓
9T	4.38	275.31 ✓
N CB	3.73	275.96 ✓

W.L. CB, 30 TH

N - 50 curb	3.08	276.61 ✓
" " 9T	3.17	276.02 ✓

279.49

N.L. curb	3.71	275.98 ✓
" 9T	4.28	275.41 ✓
N. of Line Pav.	4.14	275.55 ✓
1/4	3.93	275.76 ✓
C	4.00	275.69 ✓
1/4	4.22	275.36 ✓
S. of Line Pav.	4.78	274.91 ✓
S.L. curb	4.71	274.98 ✓
" 9T	5.07	274.62 ✓
+ 50 curb	5.84	273.85 ✓
" 9T	6.32	273.37 ✓
W 1/4 3074		
- 50	5.42	274.23 ✓
S.L.	4.40	275.29 ✓
cb. Line	4.19	275.50 ✓
1/4	4.03	275.66 ✓
C	3.86	275.83 ✓
1/4	3.72	275.97 ✓
cb. Line	3.55	276.14 ✓
N.L.	3.46	276.23 ✓
+ 50	2.88	276.81 ✓
W. rail of W. Track		
- 50	2.75	276.94 ✓
N.L.	3.38	276.31 ✓
C	3.83	275.86 ✓

279.69

Grape

49

S.L.	4.28	275.41 ✓
+ 50	5.40	274.29 ✓
E. rail of W. Track		
- 50	5.41	274.28 ✓
S.L.	4.30	275.39 ✓
C	3.83	275.86 ✓
N.L.	3.36	276.33 ✓
+ 50	2.76	276.93 ✓
W. rail of E. Track		
- 50	2.77	276.92 ✓
N.L.	3.32	276.37 ✓
C	3.75	275.94 ✓
S.L.	4.19	275.50 ✓
+ 50	5.26	274.43 ✓
E. rail of E. Track		
- 50	5.27	274.42 ✓
S.L.	4.19	275.50 ✓
C	3.77	275.92 ✓
N.L.	3.33	276.36 ✓
+ 50	2.74	276.95 ✓
E 1/4 3074		
- 50	2.88	276.81 ✓
N.L.	3.50	276.19 ✓
N. of Line	3.50	276.13 ✓
N 1/4 3074	3.68	276.01 ✓

279.69

C	3.77	275.90	✓
S 1/4	3.85	275.84	✓
S. of Line	4.01	275.68	✓
S. L.	4.17	275.52	✓
+ 50	5.34	274.35	✓
E. of 30th			
- 50 curb	4.85	274.84	✓
" 9T	5.58	274.11	✓
S. L. curb	3.67	276.07	✓
" 9T	4.44	275.25	✓
S. of Line pass	4.10	275.59	✓
1/4	3.76	275.93	✓
C	3.55	275.14	✓
1/4	3.57	276.12	✓
N. of Line pass	3.69	276.00	✓
N. L. 9T	3.73	275.96	✓
N. L. curb	3.08	276.61	✓
N. L. curb ^{Break}	3.18	276.51	✓
+ 50 9T	3.16	276.53	✓
" curb	2.45	277.25	✓
0 to 0. E. L. 30th			
N. of	3.17	276.52	✓
N. 9T	3.88	275.81	✓
1/4	3.58	276.11	✓
C	3.43	276.36	✓

279.69

Grape

50

S. 1/4	3.70	275.99	✓
9T	4.15	275.54	✓
S. curb	3.63	276.06	✓
T.P. ^{orig. 8.2%} SWBP 5.77 <u>280.78</u> ✓ 4.68 275.01 ^{30th + Grape} <u>275.02</u> _{0.01}			
0 + 14			
S. curb	4.98	275.80	✓
9T	5.42	275.36	✓
1/4	4.87	275.91	✓
C	4.58	276.20	✓
1/4	4.67	276.11	✓
N. 9T in drive	5.13	275.65	✓
0 + 30			
N. 9T in drive	5.40	275.38	✓
1/4	4.90	275.88	✓
C	4.78	276.00	✓
1/4	5.14	275.64	✓
9T	5.72	275.06	✓
S curb	5.38	275.40	✓
0 + 50			
S. curb	5.70	275.08	✓
9T	6.13	274.65	✓
1/4	5.49	275.29	✓
C	5.16	275.62	✓

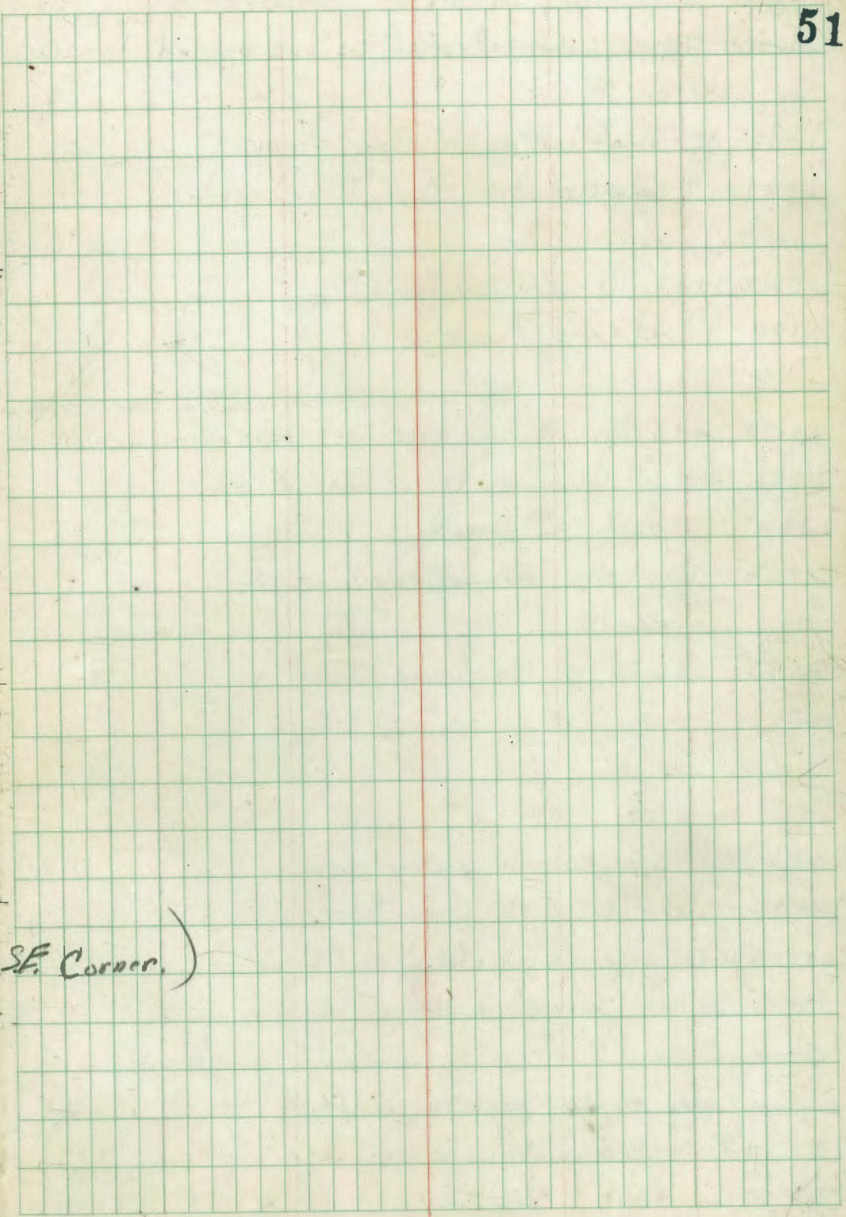
280.78

N 1/4	5.22	275.56	✓
97	5.55	275.23	✓
N curb	4.88	275.90	✓
1102			
N curb	5.66	275.12	✓
97	6.33	274.45	✓
1/4	6.06	274.72	✓
C	6.03	274.75	✓
1/4	6.41	274.37	✓
97	7.09	273.69	✓
S curb	6.67	274.11	✓

orig. B.M. 5.77 275.01 275.02

9-14-55 - Roberts - W.O.# 31035
 0+00 = E.L. 29th St.
 0+00 to 0+55 on Lt bad curb.
 1+56 to 1+66 on Rt bad curb
 1+89 to 2+10.4 on Lt bad curb
 2+10.4 = West Line Dale
 0+00 = East Line Dale
 N.E. Corner Dale & Grape Walk in bad shape. Also S.E. Corner.)
 0+35 to 0+41 on Rt bad curb
 0+57 to 0+61 on Lt bad curb
 0+59 on Lt bad bump in walk. 6' wide
 0+87 to 0+90 on Rt bad curb
 1+44 to 2+00.2 on Rt bad curb.
 1+87 to 2+00.2 on Lt bad curb.
 2+00.2 = West Line 30th St.

INDEXED



4+00 - 8.4 Lt. = # P. pole

3+50

3+01 - 9.2 Lt. = # P. pole

3+00

2+50

T.P. 8.81 373.46 1.57 364.65

2+17 - 10.4 Lt. = end pickett fence

2+17 - 10' high wire fence for school grounds E + W.

2+00

1+83 - 8.8 Lt. = # P. pole + 9.8 Lt. = Beg. pickett fence

1+74.89 = N.L. of 25' opening to E.

1+62.39 = E to E. 3.48 362.74 on Hub.

1+55 - 9.8' Lt. = end fence

1+49.90 = S.L. opening to E

1+36 - 10.4 Lt. = beg. Lath fence

1+27 - # Sing. on Rt. Conc. floor + apron

1+20 - 11.2 Lt. = # Doub. Gar. - Conc. floor

Lt.		Rt.	
367.3	367.0	367.2	367.6
6.2	6.5	6.3	5.9
30	0	10	30
	366.4	366.6	366.7
	7.1	6.9	6.8
	10		10
365.8	365.8	365.9	365.8
7.1	7.7	7.6	7.5
30	10	10	30
	364.8	365.0	364.9
	8.7	8.5	8.6
	10		10
		373.46	
	364.1	363.9	363.9
	2.1	2.3	2.3
	10		10
	363.2	363.2	363.3
	3.0	3.0	2.9
	10		10
362.9	362.9	362.7	362.0
3.3	3.3	3.5	3.2
20	10		10
362.32			362.22
3.90			4.00
11.2 = floor			11.3
			apron
			362.25
			3.97
			12.3
			Floor
		366.22	

Check B.M. 9.75 361.54 361.55 ✓

T.P. 1.81- 371.29 6.11 369.48

6+06.08 = S. cb Line Polk

Note: Ret. are approx. 1' off - checked split of block and is app. o.k.

5+99.58 = S.L. Polk. edge of A.C. pave

T.P. 5.43 375.59 3.30 370.16 end Ret. on Lt.

5+70

5+47.4

5+41.4 = S. side of 6' Conc. E+W. walk

5+00

4+98-88 Lt. = P. pole

4+50

369.84	370.06	369.67	369.61	369.63	370.01	369.40
5.75 5.0 9ut.	5.53 8.5 Top cb.	5.92 8.5 9ut.	5.98	5.96 10.9 9ut.	5.58 10.9 Top cb.	6.19 5.0 9ut.
					2' Rad. Ret.	
370.16	370.01	369.96	370.12	370.29		
5.43 8.5 Top cb.	5.58 8.5 9ut.	5.63	5.47 10.9 9ut.	5.30 10.9 Top cb. end Ret.		
			375.59			
	370.1	370.0		369.6		
	3.4 10	3.5		3.9 10		
	369.66	369.81		369.88	369.8	
	3.80 10 walk	3.65		3.58 10 walk	3.7 10 ground.	
370.15	369.57	369.72		369.84		
3.31 2.0 edge walk	3.89 10	3.74		3.62 8.2 = angle in walk	3.59 10 walk	3.69 3.9 10 ground
369.73	368.6	368.6		368.8	369.0	
4.2 3.0	4.9 10	4.9		4.7 10	4.5 3.0	
	367.9	368.0		368.0		
	5.6 10	5.5		5.5 10		
			373.46			

Levels on 25' lot opened for Pub. Drive
To Wilson from 15' Alley - See sketch P. 60

INDEXED

1+419 = W. edge of 5.3' Conc. side walk - left in for Dr.

1+40.04 = W.L. Wilson St - 133 Lt. = end High fence

1+00 = House on Rt

0+69 - 154 Rt = Med. House

0+65

0+58 - 12.4 Rt = end lath fence

0+20

0+03 - 13.3 Lt = Beg. 10' Wire fence to school grounds

0+03 - 12' Rt = beg. lath fence

0+00 = E.L. of 15' N+S. Alley

R.M. 5.89 368.63

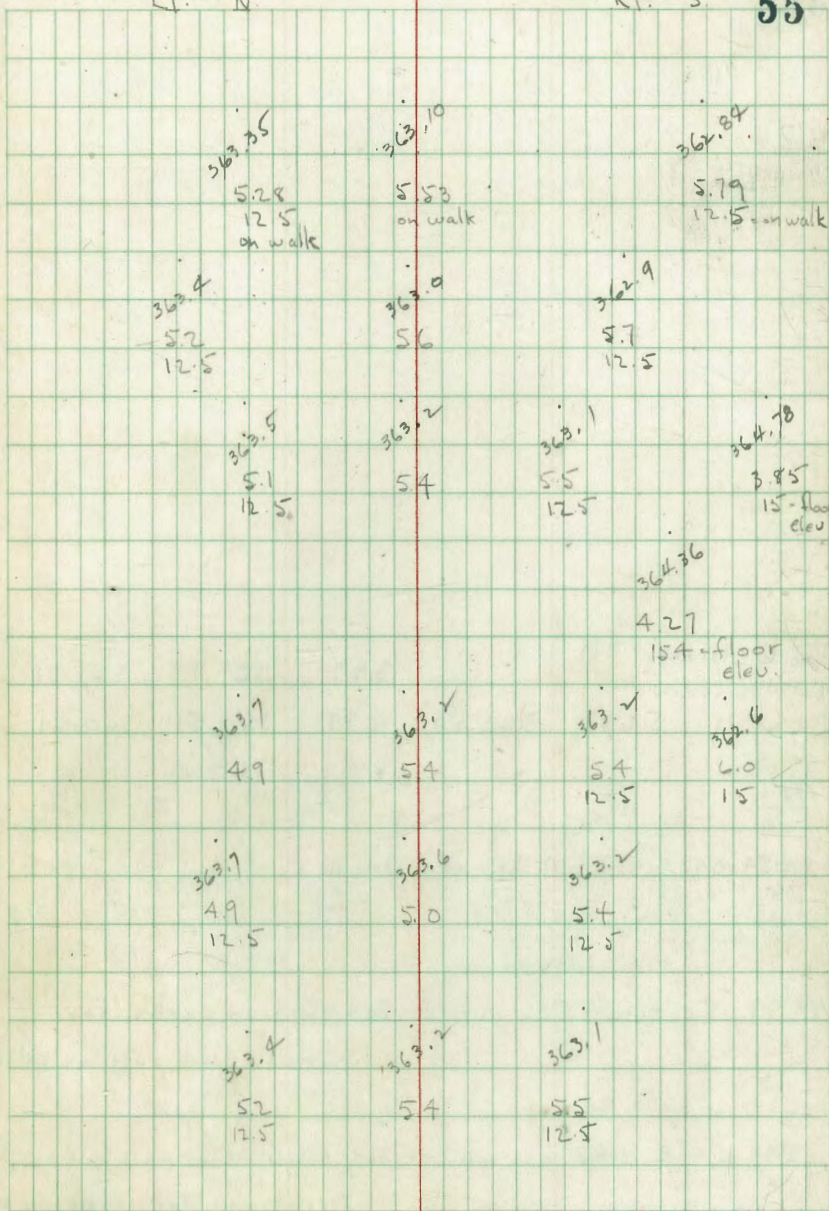
on 25' lot
362.74 1+62.39
P. 53

Lt. = N

of 25' lot.

Rt. = S

55



368.63

check Starting D.M. NW Wilson & Univ.		3.97	361.53	361.55
check B.M. 5.28	365.50	4.99	360.51	360.61
T.P.		8.41	360.22	

1+54.04 = W. cb line of Wilson

1+49.05 = opp. P.C.'s of 5' Rad Ret. in curbs for Drive. Same outs as below

1+47.2 = E edge of walk + Beg solid Conc slab for Drive - inside curbs

362.94	362.99	362.46	362.99	362.28	362.05	361.89	362.35	361.43
5.49	5.64	6.17	6.14	6.35	6.58	6.74	6.28	7.20
50 gut	17.5	17.5	12.5		12.5	17.6	17.6	50
	Top cb PC. of 5' Rad Ret	gut. + end of Conc slab.	gut		gut	gut	Top cb PC. of 5' Rad. Ret.	gut

363.11	362.99	362.69
5.52	5.69	5.94
12.5		12.6
face-beg Ret. for Drive		12.6 = face of beg. Ret. for Drive

368.63

Re-4sec alley Blk 13 Swan's Add.

See P. 14 and 18

Moore
B-99
SHEPHERD
D. J. 5304
4-18-49

INDEXED

0+78.5

Reduced
McClain
6-5-49

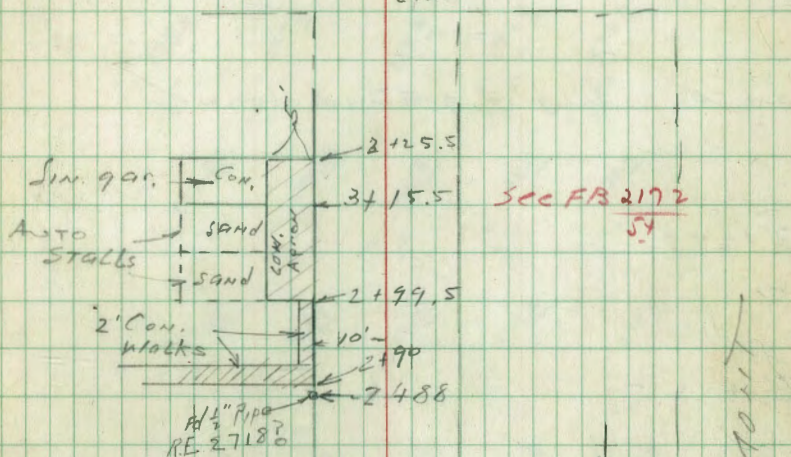
LT = E

RT 57

285.9 4.8 28	285.6 7.1 10	285.3 7.6	284.80 5.5K 102 CON.	284.34 2.40 38 garage
--------------------	--------------------	--------------	-------------------------------	-----------------------------

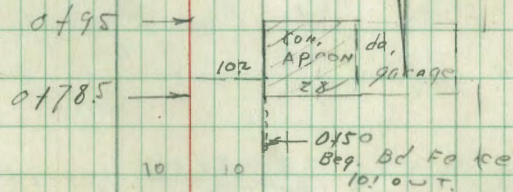
290.74
400

Laurel ST.



SEE FR 2172
57

FAIRMONT



0+00
S. Maple

NW BF 10.57 290.74 280.17
Maple
FAIRMONT

T.P. 0.45 ^{259.20} 259.90 1290 258.75

4+00

T.P. 0.99 271.65 1201 270.66

3+75

3+50 slight ground change

3+25.5

3+15.5

2+99.5

2+90

TD 4.51 282.17 1258 278.10

0+95

290.74

See p 19

276.2
1.5
25

278.0
4.7
25

280.65
2.0
15
CON.

280.68
1.99
15
CON.

280.67
2.00
15
CON.

280.80
1.87
10
CON.

285.6
1.7
25

285.3
1.4
10

271.65
8.2
10

277.4
5.3
10

278.8
3.9
10

279.2
3.5
10

280.0
2.7
10

280.4
2.3
10

282.67
5.7
10

290.74

274.8
7.5
10

277.2
5.5
10

278.6
4.1
10

279.0
3.7
10

279.4
3.3
10

279.7
3.0
10

284.87
6.7
10

275.5
7.2
25

277.0
5.7
25

278.4
4.3
25

278.6
4.1
25

279.2
3.5
25

279.4
3.3
25

284.36
6.38
28

APON

F. OSBORNE 8-1-46

MCCOY

HARDIN Polk

WADDELL

Ave Paved A.C. ct.

157.15

Fd. tack 313.29

5499.58

7 Block

33

School Prop.

closed (Dotted section)

609.61

N

1790.86

162.39

Set hub

125

125

Opened

89° 29' 30"

10'

10'

0+00

1440.00

168.39

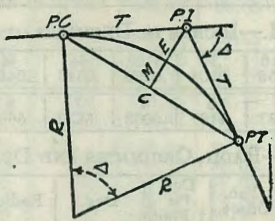
312.91

Set ct. 155.75

Univ. Ave Paved A.C.

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

- Radius— $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve— D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)
- Tangent— $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve— $L = 100 \frac{\Delta}{D}$ (4)
- Middle ordinate— $M = R(1 - \cos \frac{\Delta}{2})$ (5) $= R \text{vers } \frac{\Delta}{2}$ (6)
- External— $E = T \tan \frac{\Delta}{4}$ (7) $= R \div \cos \frac{\Delta}{2} - R$ (8) $= R \text{exsec } \frac{\Delta}{2}$ (9)
- Long Chord— $C = 2 R \sin \frac{\Delta}{2}$ (10) Δ —Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{3} = 414.49$ ft. From Table V correction—.36 or $T = 414.85$ ft. P. C.—Sta. P. I.— $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T.—Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.—7.27 ft. Distance—158—Sta. P. C.—54.50, hence offset— $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle— $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft.—(in minutes) $.3 \times C \times D^\circ$ or—defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve—.3 $\times 54.5 \times 8\frac{1}{3} = 136.2'$ or $2^\circ 16.2'$, or— $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle— $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 115.27$ and from Table V correction—.10 or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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