1713

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

1713

CITY ENGINEER'S OFFICE

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

Levels for County Parking Lot.
West of Existing Center Lane

Ely Harbor Drive → 84°01'30"
R=1600

C. Moore
Sanitary Engr.
Bldg.

4-29-46.

3+04.81
B.C. L.T.

Ed. State
Con. Man.

90°
58'30"
95°

0+59.27

Δ 99°42'
R=50
T=59.27
L=87.00

0+00
To East
and North

Page 3

indexed
6'5.14

2

35'

84.80

100

4+83

100'
B.C. Pav.

50 50

Reshapes dirt
for present

Center Lane

Existing

Cold lay Pav.

4+02

3+75

3+48

Paved Parking Lot

Δ = 84°42'
R = 30
T = 27.71
L = 33.07

2+57.24
2+50.33

Δ = 21°11'
R = 50
T = 9.35
L = 18.49

Δ = 64°55'
R = 50
T = 31.00
L = 56.65

1+93.48

1+45.68

1+43.57

1+19.03

3+00

2+57.24

2+50.33

C.91

Spike in Pav.

Date St.

Spike

In Pav.

25

Spike

25.5

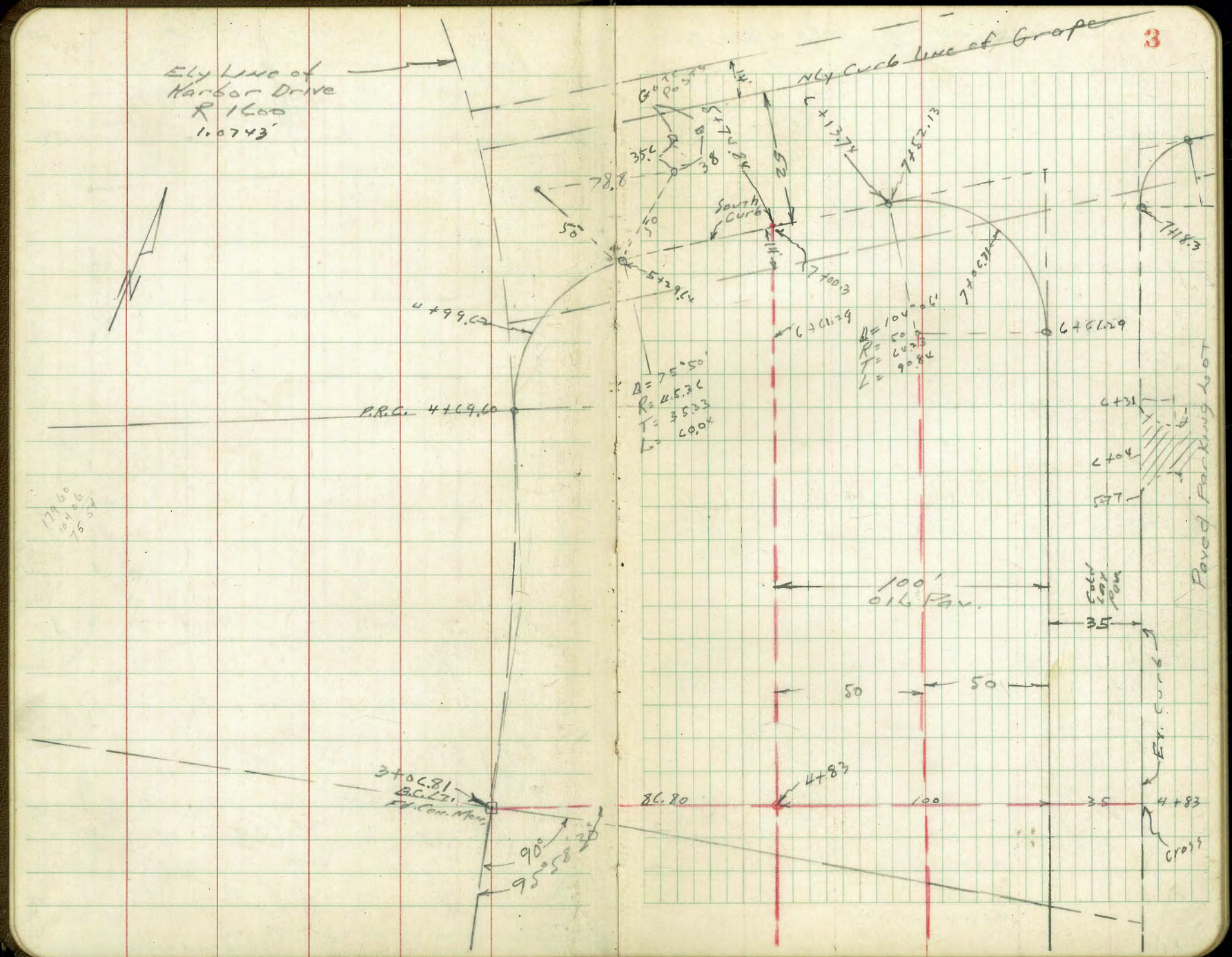
N ½ Cold lay Pav.

50.

Existing Curb

Cross on curb on a split.

Chiseled + on Curb


Ely Line of Harbor Drive
R 1600
1.0743'
NLy Curb Line of Grape
78.8
50'
South Curb
7+00.3
7+52.13
7+18.3
7+13.74
7+13.74
5+29.64
4+99.60
P.R.C. 4+69.60
Δ = 75°50'
R = 45.36
T = 35.33
L = 69.04
Δ = 104°-00'
R = 50.00
T = 64.28
L = 90.84
6+61.29
6+61.29
6+31
6+04
5+77
100' Of. Fav.
35
50
50
Ex. Curb
Paved Parking Lot
Road Fold
3+06.81
B.C.L.I.
Ex. Con. Mon.
90°
90°
B.C. 80
100
35
4+83
4+83
Cross

Levels on Co. Park Lot.

1 + 13.57 = E.C.

1 + 45.08 B.C.L.T.

1 + 19.03 = 100' Line

/

0 + 59.27 = E.C.

0 + 00 = P.I.

999
assumed
H.I.

N.C.6. Date.

B.L.
N.L. Date

4

Grade

999 5.30 4.69 ✓	4.94 5.05	5.01 4.38 25	5.10 4.89 50
999 5.20 4.79 ✓	4.72 5.27	5.67 5.32 25	5.82 5.32 50
999 5.07 4.92 ✓	4.76 5.23	5.25 5.33 25	5.05 5.90 50
999 4.97 5.02 ✓	4.50 5.49	5.57 4.42 25	5.05 4.96 50
476 5.23 ✓	4.43 5.56	5.00 4.49 25	4.84 5.16 50
999 4.44 5.55 ✓	4.30 5.70	4.80 5.19 25	4.70 5.30 50
9.99			

	100' Line	℄ 50' Line of Park Lot 1
3+48	5.26 / 4.73	5.20
3+00	5.20 / 4.79	4.94
2+57.24 E.C. on IPt. 5	5.14 / 4.85	Center lane 4.64
2+50.33 = EC on WL	5.10 / 4.89	999 / 4.70 / 582 / 4.60
2+22 ℄ Curve		999 / 4.54 / 5.45
1+93.68 BC Lt.		999 / 4.91 / 5.08

W.L. Lane

5.37 / 4.67 / 100

5.24 / 4.75 / 50

4.10 / 5.89

3.64 / 6.34 / 17.5

5.20 / 4.79 / 100

4.80 / 5.19 / 50

3.97 / 6.02

3.70 / 6.29 / 17.5 Hold

4.48 / 6.51 / 35 = Top grate

4.74 / 5.24 / 100

4.40 / 5.39 / 50

4.00 / 5.99

3.74 / 6.23 / 17.5

4.17 / 5.72 / 100

4.60 / 5.39 / 50

4.20 / 5.79

3.90 / 6.09 / 17.5

4.57 / 5.42

4.26 / 5.73 / 25

11:40 1 Hr

4.59 / 5.09 / 45

4.39 / 5.39

4.54 / 4.45 / 25

4.96 / 5.05 / 50

9.99

Hill Lane

		100' Line	℄ 50' ℄ Lot		
5+77		4.68 / 5.31	5.30		
5+38		4.92 / 5.07	5.50		
5+00		5.10 / 4.89	5.58		
4+83	Cross	5.15 / 4.84	5.57	on State Con. Mon. SCT B.M.	assumed 30.5 — C.9x / 186.80
4+42.5		5.24 / 4.75	5.54		
4+02		5.28 / 4.71	5.41		

4.86 / 5.13 / 100	5.40 / 4.59 / 50	4.73 / 5.26	4.50 / 5.39 / 175
4.88 / 5.11 / 100	5.60 / 4.39 / 50	4.54 / 5.37	4.55 / 5.14 / 175
5.07 / 4.92 / 100	5.59 / 4.40 / 50	4.43 / 5.54	4.43 / 5.56 / 175
5.06 / 4.93 / 100	5.33 / 4.83 / 50	4.38 / 5.41	4.50 / 5.59
5.16 / 4.83 / 100	5.70 / 4.29 / 50	4.23 / 5.56	4.21 / 5.78 / 175
5.30 / 4.69 / 100	5.54 / 4.35 / 50 / stub	4.30 / 5.49	3.98 / 5.01 / 175

999 / 2

50' Line & Lot.

= 100' Line = Sch. Grape

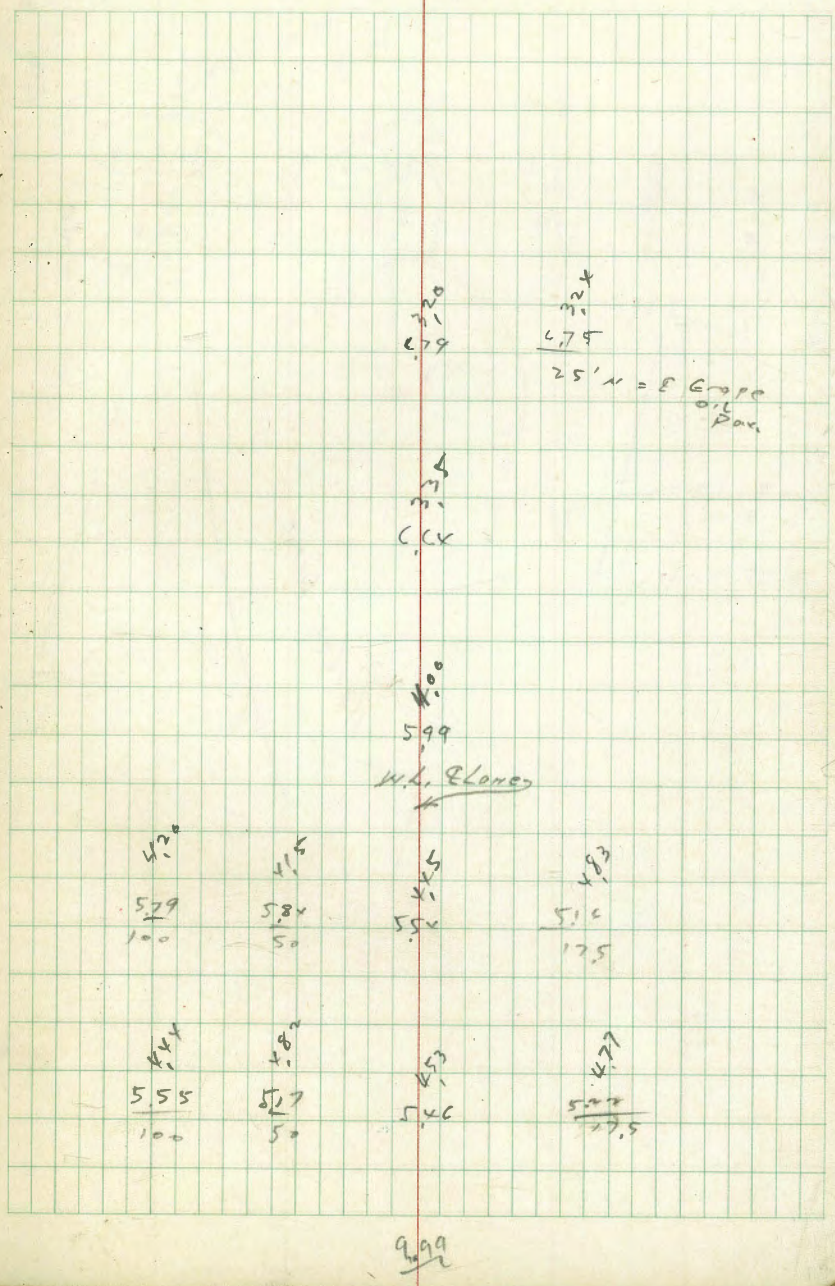
7 + 52.13 = C + 137 x = E.C. Sch Grape

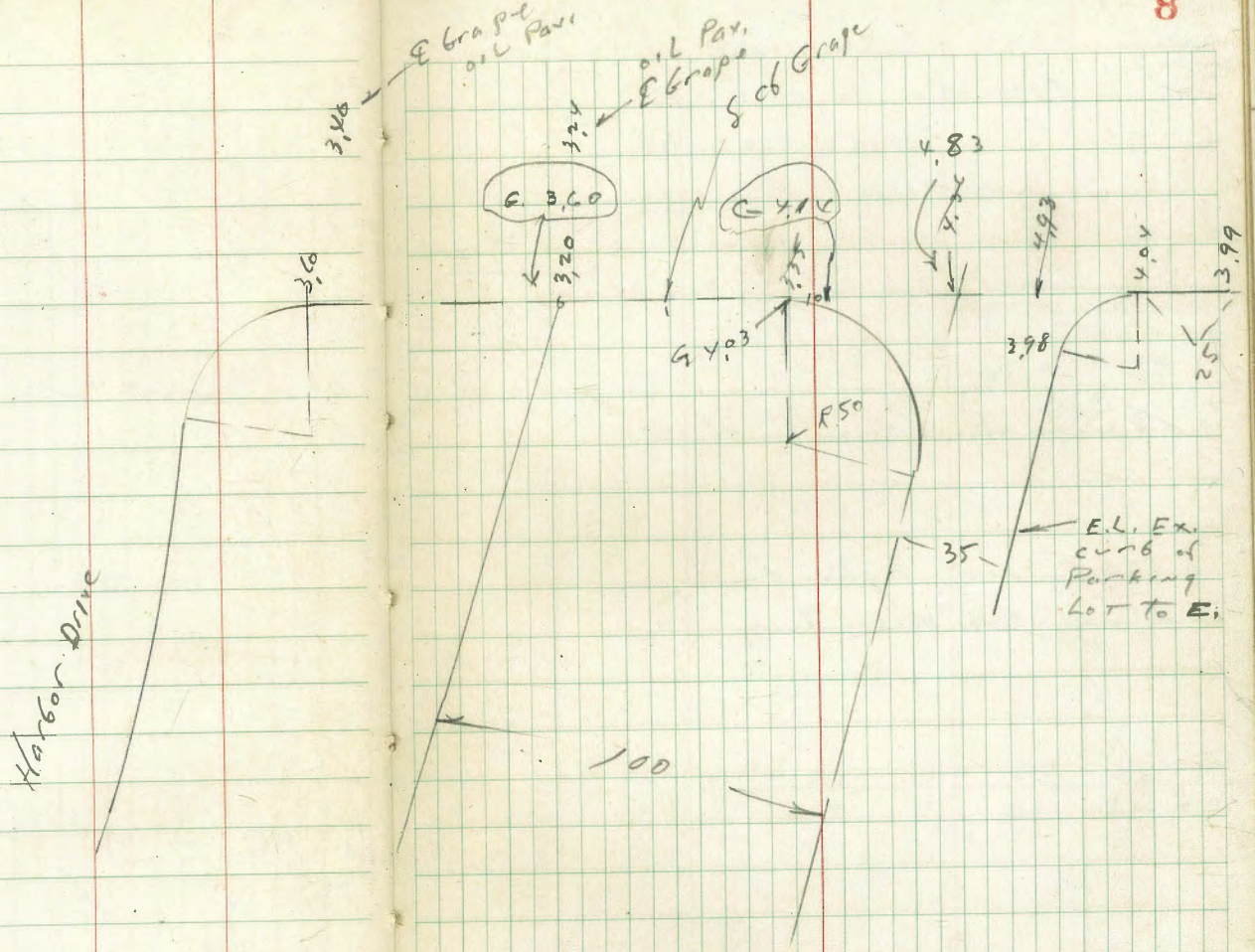
7 + 06.71 ℄ Curve Lt.

	100' Line	50' Line
6 + 41.79 B.C. on Lt. of ℄ Line	4.10 / 5.89	4.63
6 + 31	4.32 / 5.67	4.80

Sch. Line Grape

7




℄ Grade
o.L Pav.
3.40
Harbor Drive
3.10
℄ Grade
o.L Pav.
℄ of Grade
3.24
E 3.60
3.20
G 4.13
4.83
4.93
4.04
3.99
3.98
25
G 4.03
F.50
35
E.L. Ex.
curb of
Parking
Lot to E.
100

C. Moore
Sam Merrixcox
Begg

× sec of Emerson St. 70' wide 18" c65

Rosecrans to W. C Low

5-4-46. See Sketch 1605-39.

no change of Rosecrans

0+97 See Sketch, 1592-37 also P. 47

W. edge triple Conc. Blk. Dr.

0+83 E. edge of Triple Conc Blk. dr.

0+80 End Picket fence

0+57 Beg. Picket fence

0+50

0+27 See 1605-39

0+00 = W'ly Rosecrans

T.P.	1.41	15.63	12.57	14.22
Set Spike B.M.	Sely Con Tel. P. Evergreen + Emerson	6.85		19.94 ✓
Sw. B.P.	1.68	2.79		25.11

Evergreen Fenelon

Indexed
C.S.K.

LT ℄ RT.

9

6.69
8.94
35

0+97 → 1.9
3.5
0+83 → 1.9

6.84
8.77
35

Fence
34.5

Fence
33.6

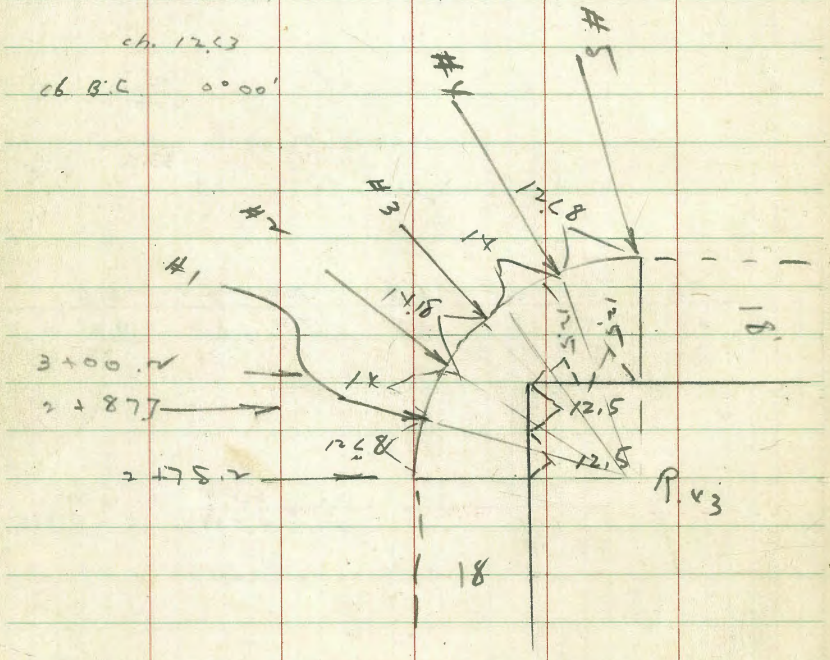
7.2	7.2	6.5	6.9	6.0	6.7	6.6
8.4	8.4	9.1	8.7	9.6	8.9	9.0
35	25	12		10	18	35

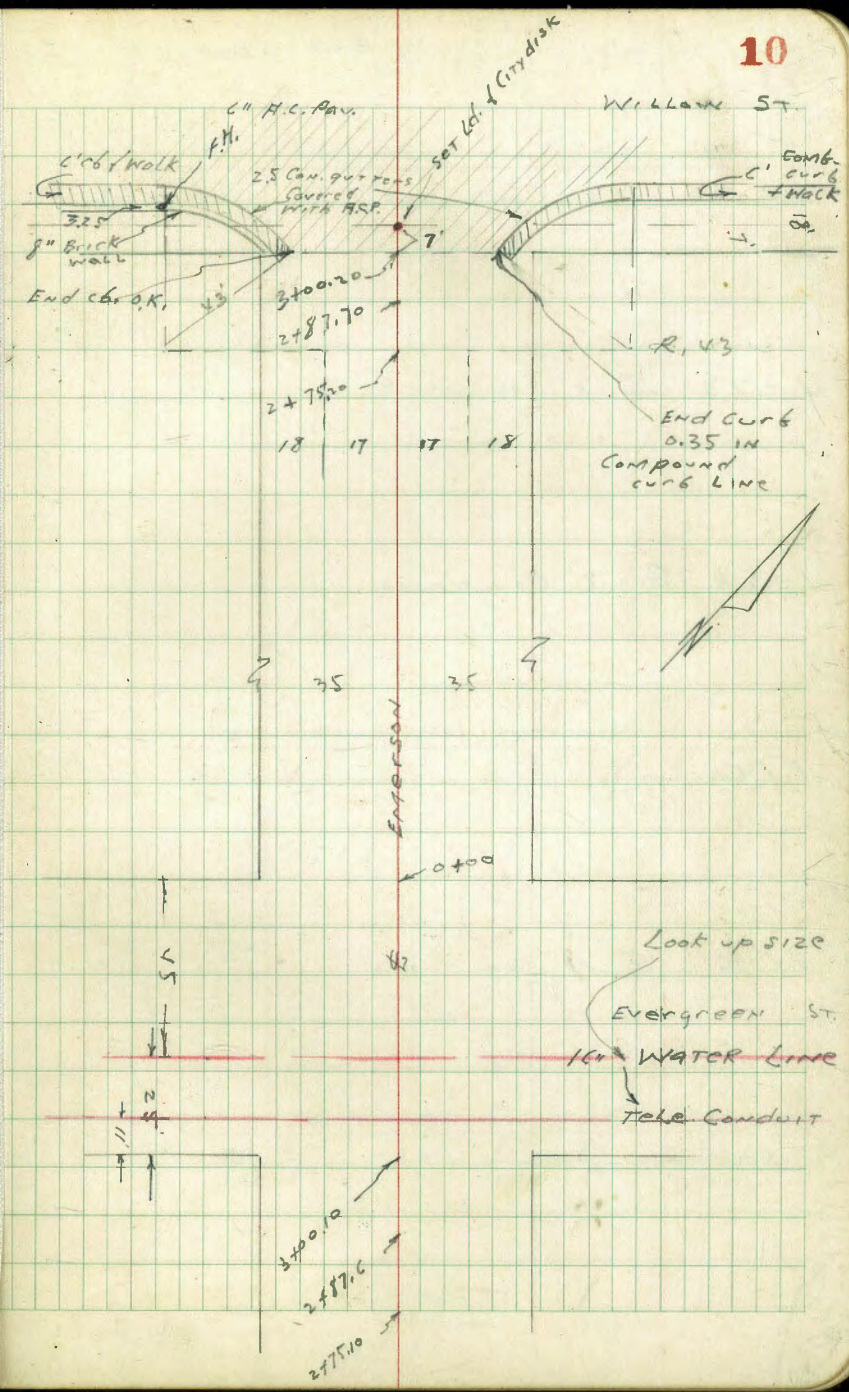
7.02
8.61
18
06

6.04
9.59
18
06

15.63

5 — E.C. 45°00.0
ch. 12.63
4 — 30°33.0
ch. 13.91
3 — 27°13.33
ch. 14.14
2 — 17°41.50
ch. 13.91
1 — 8°21.87
ch. 12.63
cb B.C. 0°00'





EMERSON

2+00

1+73 ℄ 3' Con walk

1+58 ℄ 7' Con. drive

1+50

1+05 ℄ 10' Con. drive

1+00

15.63

LT ℄ RT

8.7	9.1	8.6	9.0	8.7	7.7	8.8
5.9	6.5	7.0	6.6	6.4	6.4	6.8
35	17	10		11	14	35

8.51
7.17
35

8.08
7.55
35

8.4	8.2	8.0	8.1	7.8	7.8	7.8
7.7	7.K	7.4	7.5	7.8	7.8	7.8
35	20	17		12	25	35

8.06
7.57
35.5

8.0	7.9		7.4	7.6	7.3	7.5	7.1
7.6	7.7	RR	8.7	8.0	8.3	8.1	8.5
35	25	24.6	17		16	17	35

15.63

2 + 75.18 ch B.C.

2 + 71 ℄ 3' Con. walks Both sides

2 + 50 Beg. Picket fence

2 + 48

2 + 41.7 ℄ 7' Con. Dr.

2 + 22 ℄ 3' con. walks Both sides

1563

Lt ℄ Rt. 12

11.6	11.4	10.1	10.5	10.0	10.8	10.3
4.0	4.2	5.5	5.1	5.4	4.8	5.3
35	18	10		13	18	35

12.01
3.62
35.2

10.44
5.19
35

35.2

11.1	10.8	9.9	10.1	9.5	9.9	10.19
4.5	4.8	5.7	5.5	5.1	5.7	5.44
35	20	12		16	20	35.2 ℄ 14' Con. Dr.

11.11
4.52
35.5

10.71
4.92
36.1

9.46
5.17
34.8

1563

Emerson

Wly 1/4

℄ Loc ST

Ely 1/4

Ely c6. Lowest

E.6. + 9' Cor. picket fence or 9' in ST.

3+00.18 = Ely Lowest ST = 70' w, de / 18' c&g / 8.5 1/2 s

2+77

+5.43

Lt ℄ Rt

12.0	11.8	12.0	12.0	12.0
3.6 / 35	3.8 / 16	3.6	3.6 / 16	3.6 / 35
11.8	11.5	11.8	11.8	11.8
3.8 / 35	4.1 / 16	3.8	3.8 / 16	3.8 / 35
11.3	11.0	11.6	11.5	11.6
4.3 / 35	4.6 / 16	4.0	4.1 / 16	4.0 / 35

12.73	12.4	12.1	11.0	11.4	11.0	11.6	11.5
3.90 / 135 Top Curb End	3.7 / 35	3.5 / 17	4.6 / 11	4 ~	4.6 / 13	4.0 / 19	4.1 / 35

Fence Cor. 34.5

12.2	11.2	10.5	10.9	10.6	11.1	10.8
3.8 / 35	4.8 / 12	5.1 / 10	4.7	5.0 / 13	4.5 / 15	4.8 / 35

P.P. 21.8

15.63

Elevation

0 + 50 — Top of end 5" Conc. Wall → 1.28 / 35.3

0 + 30 — ℄ 2' Conc. Walk on S ℄ of 4.5 Conc. Walk

0 + 25

W c/y Locust = 0+00

W c6. + 15.5 = 35.1 Lt. to Beg. picket fence
W c6. + 13.5 = 30' Lt. to P.P.

W/y Curb. Locust

W c/y 1/4 + C

15.43

Lt ℄ Rt

14

	13.9	13.5	13.0	13.4	13.0	13.2	14.25	13.5
End fence	1.7	2.1	2.6	2.7	2.6	2.4	1.38	2.1
35.3	35	14	13		12	13	29	35

Top S end 5" Conc. Walk

	13.93		13.60
one N.	1.70		2.03
	35.2		29.9

13.7	13.3	12.5	13.1	12.6	13.2	13.4
1.9	2.3	3.1	2.5	3.0	2.4	2.2
35	16	14		12	14	35

13.2	12.9	12.0	12.5	12.2	12.5	12.8
2.4	2.7	3.6	3.1	3.4	3.1	2.8
35	16	17		11	12	35

13.41	12.9	12.7	11.8	12.2	12.2	12.1
2.22	2.7	2.9	3.8	3.4	3.4	3.5
135	35	18	13		16	35

Top Curb End.

12.0	11.8	12.1	12.1	12.0
2.6	3.8	3.5	3.5	3.6
35	16		12	35

15.43

Emerson

1+27 ℄ 3' Conc. walk

1+09.6 ℄ do. Conc. Pedestrian 7' wide over all

1+06 ℄ 11' Conc. Dr.

T.P. 7.28 21.81 1.10 14.53

1+00

0+88 ℄ 3' Conc walk

0+57.5 ℄ 8' Conc. Dr.

15.63

Lt ℄ Rt. 15

14.94
6.87
35

14.88
6.93
35

14.54
7.27
35.2

14.54
7.17
35.2

21.81

14.4		14.2	14.2	13.7	14.0	14.3
1.2	P.P.	1.4	1.4	1.9	1.6	1.3
35	20	14		12	13	35

14.48
1.15
35

14.25
1.38
35

15.63

Emerson

2+00

1+87 ℄ 3' Con. walk

1+72.5 ℄ 3.8 Con. walk

1+52.5 ℄ 7.5 Con. dr.

1+54 ℄ 7.5 Con. drive

1+50

21.81

Lt ℄ Rt

16.5		16.7	16.2	16.6	16.2	16.7	17.2	17.98
5.3	P.P.	5.1	5.6	5.4	5.6	5.1	4.4	3.83
35	22.7	14	12		12	14	35	35

5. end ℄ Con. wall

16.20
5.61
35.7

16.50
5.31
35

15.39
6.42
35.8

16.02
5.79
35

15.2	15.3	14.8	15.2	15.0	15.8	
6.6	6.5	7.0	6.6	6.8	6.0	CH Con. wall
35	13	14		15	35	35

21.81

5. end Con. wall 22" High

Nail Tel. Pole
SE. Evergreen
Evergreen

T.P.	9.00	28.94	1.87	19.94	19.94

2 + 00.10 = EL'y Evergreen = 70' wide
18' c6.5
8.5 1/4's

+ 89 21.2 Lt to Tel. P.

2 + 75.10 c6 B.C.

2 + 50 Rt, end Top 7" Con. Wall → 3.3 x / 35

2 + 33.5 ℄ 3' Con walk

2 + 10 ℄ 7' Con. dr.

2 + 01.5 ℄ 8.7 Con. dr.

21.81

Lt	℄	Rt

20.1	20.1	19.5	19.8	19.3	20.3	20.9
1.7 / 35	1.7 / 20	2.3 / 11	2.0	2.5 / 14	1.5 / 17	0.9 / 35

18.8	18.8	18.5	18.9	18.7	19.4	19.7
3.0 / 35	3.0 / 15	3.3 / 13	2.9	3.1 / 13	2.4 / 20	2.1 / 35

17.8	18.0	17.5	17.9	17.8	18.2	s. end	18.7
3.0 / 35	3.8 / 16	4.3 / 13	3.9	4.0 / 17	3.6 / 14	Hedge 25	3.1 / 35

17.13
4.58
35.7

17.70
4.11
34.2

16.75
5.06
37.7

21.81

Emerson

W 1/L

E Evergreen

E 1/L

E cb #7 Top 16" Water Line

E cb

E.L. Evergreen ± 11' Top Tel. Cond.

28.94

Lt. ℄ Rt. 18

20.4	20.5	20.8	21.1	21.2
8.5	8.4	8.1	7.8	7.7
35	18		18	35

20.2	20.3	20.6	20.7	20.8
8.7	8.6	8.3	8.2	8.1
35	18	MH. Rim	18	35

20.1	20.0	20.3	20.2	20.6
8.8	8.9	8.4	8.7	8.3
35	18		18	35

17.33
11.61
10

20.4	19.8	20.2	19.9	20.4	20.5
8.5	9.1	8.7	9.0	8.5	8.4
35	15		15	20	35

16.73
12.21
10

28.94

ENTERSON

0 + 98 24' Lt. P.P.

0 + 95

0 + 79

0 + 50

0 + 25 cb E.C.

Wly Evergreen = 0 + 00

W cb Evergreen.

28.94

Lt ℄ Rt

27.0	27.1	26.0	26.0	26.7	26.50	
1.9	1.8	1.9	2.9	2.7	2.4x	Com. dr.
35	20	7		18	34.7 ← W. edge	

26.2	26.0	25.8	25.0	24.8	25.5	26.51	
2.7	2.9	3.1	3.9	4.1	3.4	2.3	Com. dr.
35	25	7	4		10	34.7 ← E. edge	

24.3	23.9	24.2	23.2	23.2	24.1	24.1	25.2	25.1
4.6	5.0	4.7	5.7	5.7	4.8	4.8	3.7	3.8
35	17	5	3		10	24	28	35

23.1	23.0	23.3	22.1	22.3	23.0	23.1	23.8	24.2
5.8	5.9	5.6	6.8	6.6	5.9	5.8	5.1	4.7
35	18	4	2		9	28	31	35

4' Wide Brick Walk

22.3	22.3	22.1	21.5	21.5	22.0	22.2	23.1	22.9
6.6	6.6	6.8	7.x	7.x	6.9	6.7	5.8	6.0
35	25	10	5		18	27	29	35

20.5	20.5	21.1	21.2	21.5
8.4	8.4	7.8	7.7	7.4
35	18		18	35

28.9x

Elmerson

1+16.5 E 3' Con. walk

L+15

L+12.5 Beg picket fence

L+10.2 ℄ 4" Con walk

L+10

T.P. 8.01 36.66 0.29 28.65

L+04 Beg. picket fence 35' Lt.

L+03

28.94

Lt ℄ Rt

29.62
7.0 V
33

29.6 29.6 28.3 27.3 27.5 27.1 28.8 29.11 29.11 29.2
7.1 7.1 8.4 9.4 9.2 8.6 7.9 7.55 7.55 7.5
35 25 10 5 16 29 29 31 35
Con. walk

Fence
33

8.2 8.08
32 35
Top Con. wall at w edge dr.

29.7 29.5 28.0 26.9 27.1 27.7 28.2 28.31
7.0 7.2 8.7 9.8 9.6 9.0 8.50 8.35
35 25 10 5 18 29 35
w. edge Con. dr.

36.66

28.4 28.7 27.8 27.2 26.2 26.6 27.1 27.99 28.17
+0.5 +0.2 1.1 1.7 2.7 2.3 1.8 0.95 0.77
35 25 18 7 3 17 29 35
E. edge Con. dr.

28.94

2+60 30' Lt. 5" dia. Acacia tree
2+50 " " " " "

		Lt	℄	Rt
		38.8	38.7	
2+45		7.7	7.8	
		25	18	
		37.3		
2+25		9.2		
		55		
2+05	30' Lt = 12" dia Acacia tree			
2+00	End wire fence 35' Lt.			
T.P.	14.33	46.48 ✓	1.51	35.15 ✓
1+75				
1+50	End 8ft fence on lot line 33' Rt			
1+44	end picket fence			
1+29.5	end picket fence			
		36.66		

		42.9	46.0	46.1	45.4	41.7	41,3	44.3	44.3	38.9	38.2	37.9
		3.6	0.5	+0.4	1.1	4.8	5.2	2.2	2.2	7.6	8.3	8.6
		35	20	18	4		4	10	15	30	35	55
		37.2	37.9	42.1	41.4	40.1	38.6	39.3	37.2	36.4	37.0	
		9.3	8.6	4.4	5.1	6.4	7.9	7.7	9.3	10.1	9.5	
		37	35	20	18	5		16	20	35	55	
		35.2	35.2	35.2	34.8	35.4	35.0	34.1		34.3		
		11.3	11.3	11.3	11.7	11.1	11.5	12.4		12.2		
		45	35	22.5 P.P.	11		20	35		45		
		46.48										
		33.5	33.3	32.9	32.6	33.1	32.6	32.3		32.4		
		2.7	3.4	3.8	4.1	3.6	4.1	4.4		4.3		
		45	35	20	7		20	35		45		
		31.0	31.0	30.3	30.5	30.4	29.6					29.6
Reg. Wire fence		5.7	5.7	6.4	6.2	6.3	7.1	Grass Free		7.1		
		35	20	7		18	25	26	32	35		
Fence												
35												
Fence												
33												
		29.45	29.45	29.44								
		7.21	7.21	7.17								
		28.7	30.7	35								
		end Con. walk										
				Wedge 3.3 Conc. walk								

EMERSON

LT ℄ RT

3 + 09.7 on Pav.

3 + 00.7 = Ely Welcome St. on Pav.

2 + 99.9

2 + 87.7

T.P. 7.5 59.97 ✓ 1.67 52.45 ✓

℄ + 75.20 ch. B.C. M.L. House

℄ + 57

T.P. 8.05 54.17 ✓ 0.41 46.07 ✓

YC. 48

ON CONC. SUN Porch

44.98
9.14
53

54.88 54.71 54.47 54.17 54.13 53.93 53.70
5.09 5.26 5.50 5.70 5.84 6.04 6.27
25 17 8.5 8.5 17 25

54.49 53.82 53.72 53.53 53.39 53.15 52.86 52.60 53.17
5.48 6.15 6.25 6.48 6.58 6.87 7.11 7.37 6.80
25 25 17 8.5 8.5 17 25 35
06 97. 97. 06

55.1 55.1 54.0 53.9 54.0
4.9 4.9 6.0 6.1 6.0
35 25 25 35

55.5 55.4 55.2 53.9 53.1 52.5 52.9 48.5 48.5 47.0 44.9
4.5 4.6 4.8 6.1 6.9 7.5 7.1 11.5 11.5 13.0 15.1
X0 35 28 18 13 26 35 36 45 55

59.97

48.4 49.5 50.1 52.3 51.3 51.4 47.6 47.5 50.9 44.6 42.1 41.6
5.7 4.6 4.0 1.8 2.8 2.7 6.5 2.6 2.7 9.5 13.0 12.5
53 50 35 17 6 10 14 23 35 40 55

43.0 44.4 42.4 42.4 45.4 49.5 47.7 44.1 46.8 45.4 39.7 39.4 38.5
11.1 9.7 11.7 11.7 5.7 4.6 10.0 7.3 8.7 14.4 14.7 15.6
52 50 35 36 22 13 9 15 24 35 45 55

54.12

2 - BM. BH on SW Cy CB. Ret. → 1.C5 → 1,79 — 7C,X5 = 7C,X4 — 7C,31 = 7C,30

Willow + Dickens

T.P.	5.82	73.10	0.C3	7.2.28	
T.P.	13.05	72.91	0.11	59.8C	
		59.97			

3 + 18.2 = E C6 Willow on Pav.

59.97

Lt ℄ Rt

23

Ex. C6 Ret. and guttering

F.C. #5 — C6. gut — 1.48 — 2.45 — 58.29 — 57.52

Ex. C6 Ret. and guttering

E.C. — C6 gr — 5.75 — C.53 — 54.22 — 53.44

#4 — C6 gut — 2.C0 — 3.38 — 57.37 — 54.59

C6 gr. — 5.41 — C.08 — 54.56 — 53.89

#3 — C6. gut. — 3.8X — 4.5C — 56.13 — 55.41

C6 gr — 5.C2 — 6.23 — 54.35 — 53.74

#2 — C6 gr. — 5.X8 — C.15 — 54.49 — 53.82

C6 gr — 4.80 — 7.37 — 53.17 — 52.60

#1 = C6 gut, dist

dist

55.69	55.45	55.20	55.04	54.89	54.68	54.47
4.28	4.52	4.77	4.93	5.08	5.29	5.50
25	17	8.5		8.5	17	25

59.97

Lt. ℄ Pt.

Lgm Fd. Levels on
5-15-46. Con. drives on Emerson St.
Rosecrans To Willow

2+41.7 ℄ 7' Con. dr.

T.P. 5.53 1.502 3.09 9.x 9

1+58 ℄ 7' Con dr. no garage

1+05 ℄ 10' Con. dr.

0+97 W. edge Rib. dr.

0+83 E. edge Con Rib. drive

W.L. Rosecrans = 0+00

Top cb end 5.56 12.58 7.02
SW Emerson
& Rosecrans
P. 9

11.69 | 11.52
3.33 | 3.50
63,5 | 60
gal. | dr.

1.502

7.64
4.9 x
85
dr.

9.15 | 8.67 | 8.39
3.x3 | 3.91 | 4.19
10 5.5 | 87.5 | 60
gal. | dr. | dr.

6.72 | 7.02
5.86 | 5.56
41 | CK
Rib | gal.

6.90 | 7.02
5.70 | 5.56
41 | CK
Rib | gal.

12.58

ERICSON

L + 56.5 ℄ 7.5 Con. dr.

L + 54 ℄ 7.5 Con. dr.

T.P. 4.09 20.27 2.46 16.18

L + 09.0 ℄ do. con. 16. dr. 7' overall 2" risers

L + 06 ℄ 11 Con. drive No garage

0 + 57.5 ℄ 8' Con. dr.

T.P. 4.99 18.6x 1.37 13.65

0 + 00 = WLy Lowest St

2 + 48 ℄ 14' Con. dr.

15.02

L + ℄ Rt.

15.81
44.6
8.47
dr.
1 gar.

16.66 17.80
3.61 2.47
85 106.5
dr. gar.

20.77

15.13 14.89
3.51 3.75
60 57
gar. 16. dr.

15.03
3.61
85
dr.

15.03 14.75
3.51 3.89
79.0 76.0
gar. dr.

18.6x

9.46 9.65
5.96 5.37
85 117
dr. gar.

15.02

Emerson

1+10	W. edge Con dr.			
1+03	E. edge Con. dr.			
0+95	W edge con. dr.			
0+79	E edge Con dr.			
Spike B.M.	4.74	31.68	19.94	
	W Ly Evergreen = 0+00			
T.P. on B.M. Spike, P.P. S.E. Emerson Evergreen		2.03	19.95	19.94 / 0.01
2+10	E 7' Con. dr.			
2+06.5	E 8.7 Con. dr.			
T.P.	5.23	21.98	3.52	16.75
		20.27		

Lt ℄ Rt

31.68
3.70
27.98 = 27.99.
0.01
P. 20

28.75 29.89
2.93 1.79
47 117
dr. gar.

28.66 29.89
3.02 1.39
47 117
dr. gar.

26.75
4.93
44.7
dr. + gar.

26.72
4.90
44.7
dr. + gar.

31.68

18.12 18.40
3.80 3.58
58 61.5
dr. gar.

16.50 16.43
5.48 5.55
105 102
gar. dr.

21.98

Indexed
C.S.K.

Levels on Locust St. St. = 70' Width
18' C&S
8.5 1/4 S

Dickens to Fenelon

C.S.
5-18-46.

1 + 37.2 ℄ 8' Conc. Apron

1 + 24.4 S. edge Conc. Apron

1 + 00

0 + 25

0 + 00 = Wly Dickens - edge Pav.

T.P.	3.65	17.29	6.99	13.64	Emerson Evergreen
S.E. Spike on P.P.	0.64	20.63		19.94	

Lt = Wly ℄ Rt

27

2.45 / 42.3 / 90 / Ft.

3.08 / 35

3.19 / 30

4.54 / 25.4

4.58 / 35

4.45 / 45.7 / 90 Ft.

13.41

3.88 / Topend Ex. C6

4.2 / 9T

3.9 / 8

4.0

4.3 / 8

4.5 / 9T

12.76

4.53 / Top end Ex. C&G

2.26 / 17 / Top C6

3.12 / 9T

3.4 / 8.5

3.3

3.4 / 8.5

3.6 / 9T

2.87 / 17 / Top C6

1.80 / 25 / C6

2.29 / 25 / 9T

2.28 / 12.5

2.39

2.59 / 12.5

2.85 / 25 / 9T

2.43 / 25 / C6

17.29

Contd. P.30

D +39.5

0 +25

0 +20

0 +12

0 +00 = Nly Emerson St.

1 +74.5 = 25.5 S of S.L. Emerson

1 +38.2 N. edge Con. Apron

17.29

Lt ℄ Rt

4.05
37.8
Con. Con.
Walk

4.2 / 35 | 5.1 / 17 | 5.4 / 8 | 5.5 | 5.8 / 8 | 6.0 / 17 | 6.5 / 35

5.97
3 K.C
Con. Walk

5.8 K
39.1

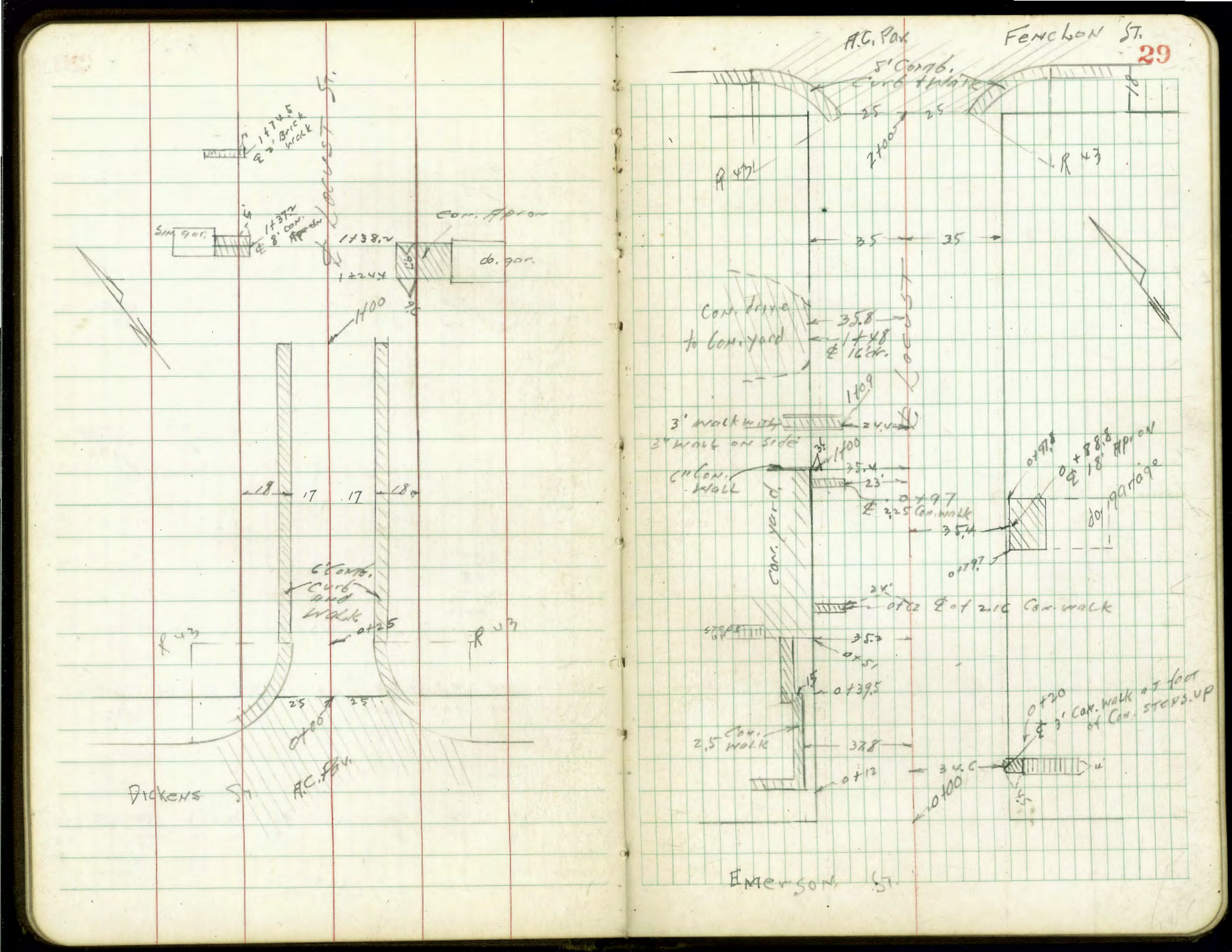
3.95
37.8
Con. Con.
Walk

3.63
35
Brick Walk

3.76 / 33 Brick Walk | 4.1 / 17 | 4.9 / 14 | 4.9 / 8 | 4.9 | 5.3 / 8 | 5.6 / 14 | 4.4 / 17 | 4.16 / 35

3.08 / 35 Conc. Apron | 3.8 / 19 | 4.6 / 97 | 4.4 / 8 | 4.4 | 4.6 / 8 | 4.8 / 12 | 4.0 / 14 | 4.55 / 25.3 | 4.56 / 35 apron | 4.41 / 45.3 gar

17.29


A.C. Pav.
Fencion St.
5' Conc. Curb & Gutter
25
25
Z+00
R 43
R 43
35
35
Conc. drive to Con. yard
35.8
1+48
℄ 16 Con.
1+09
3' walk with 3" walk on side
24'
1+00
35.4
23'
0+97
℄ 2.5 Con. walk
Con. yard
0+47.5
0+88.8
℄ 18' Apron
do. 90 to 90°
35.4
0+79.7
24'
0+62 ℄ of 2.16 Con. walk
Steps up
35.7
0+51
15'
0+39.5
0+20
℄ 3' Con. walk at foot of Con. steps up
2.5 Con. walk
32.8
0+12
3 4.6
0+00
Emerson St.
Conc. Apron
1+38.2
1+24.4
do. gar.
Sim gar.
1+37.5
℄ 3' Brick walk
8' Conc. Apron
1+00
18
17
17
18
6' Conc. Curb and Walk
0+25
R 43
R 43
25
25
0+00
Dickens St.
A.C. Pav.

L+00				
T.P.	5.18	16.79	5.68	11.61
0+97.8	N edge Con. apron			
0+97				
0+79.7	= S Edge Con apron			
0+60				
0+51				
		17.79		

LT & RT

3.89 / 35.4 / end Con. Walk

3.47 / 31.4 / To A end Wall

5.0 / 17

5.1 / 8

5.3

16.79

5.6 / 8

5.7 / 17

6.2 / 35

6.33 / 35.4 / Con. apron

6.28 / 44.2 / gar. fl.

4.95 / 23 / Con. Walk

35.4 / Con. Walk

6.36 / 35.4 / Con. apron

6.27 / 44.2 / gar fl

4.38 / 35.2 / Con. Walk

4.86 / 24 / Con Walk

5.5 / 17

5.6 / 8

5.8

6.0 / 8

6.3 / 17

6.7 / 35

4.28 / 35.2 / Con. Con. Walk

17.79

check to SW BP	Evergreen Fenelon	1.58	x5.11	25.11	0.00
T.P.	11.58	24.69	1.68	15.11	
		16.79			

2+00 S.L. Fenelon St. edge Pav.

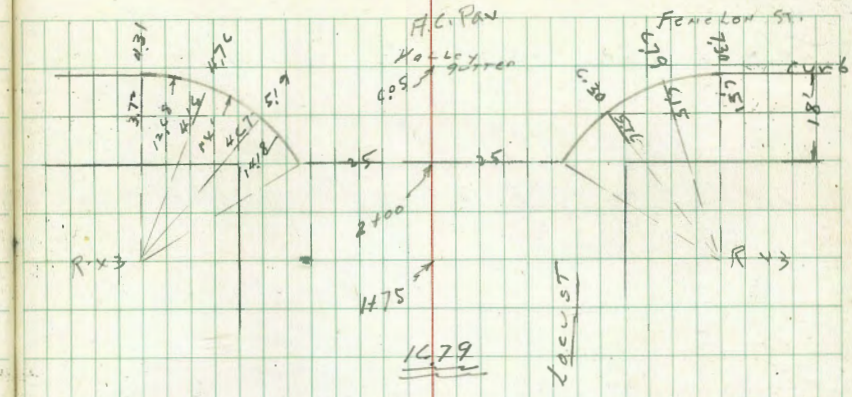
1 x 75

1+48 ℄ 16' Con. drive

1+09 ℄ 3' Con walk

16.79

Lt ℄ Rt



16.79

Fenelon St.

4.81 / 25 / 06 Top

5.33 / 25 / 97

5.45 / 12.5

5.59

5.83 / 12.5

6.11 / 25 / 97

5.07 / 25 / top 06.

3.6 / 35

4.7 / 17

4.8 / 8

x 8

5.0 / 8

4.6 / 17

5.5 / 35

3.08 / 57.8 & do. Dan.

3.38 / 45.8 Co approx.

4.46 / 35.8

5.0 / 17

4.9

5.7 / 8

5.3 / 17

5.5 / 35

4.46 / 35 on Con walk

4.70 / 24.4

16.79

Walker
Hendricks
Hunley
Cure
6-24-46

CROSS SECTION - GEORGIA ST.

80' Wide
20' Curbs 10'-4"-5

From Myrtle St. South.

				B.M. NW. BP Myrtle Indian
	3.65	297.70		294.05
T.P.	2.59	292.98	7.31	290.39
	0-25			
W			2.7	290.3
cb.			2.92	290.06
Gut.	on Paving		3.58	289.40
¼	" "		3.47	289.51
½	" "		3.50	289.48
¼	" "		3.96	289.03
Gut.	" "		4.74	288.25
Top Cb.			4.14	289.85
E.			3.9	289.1

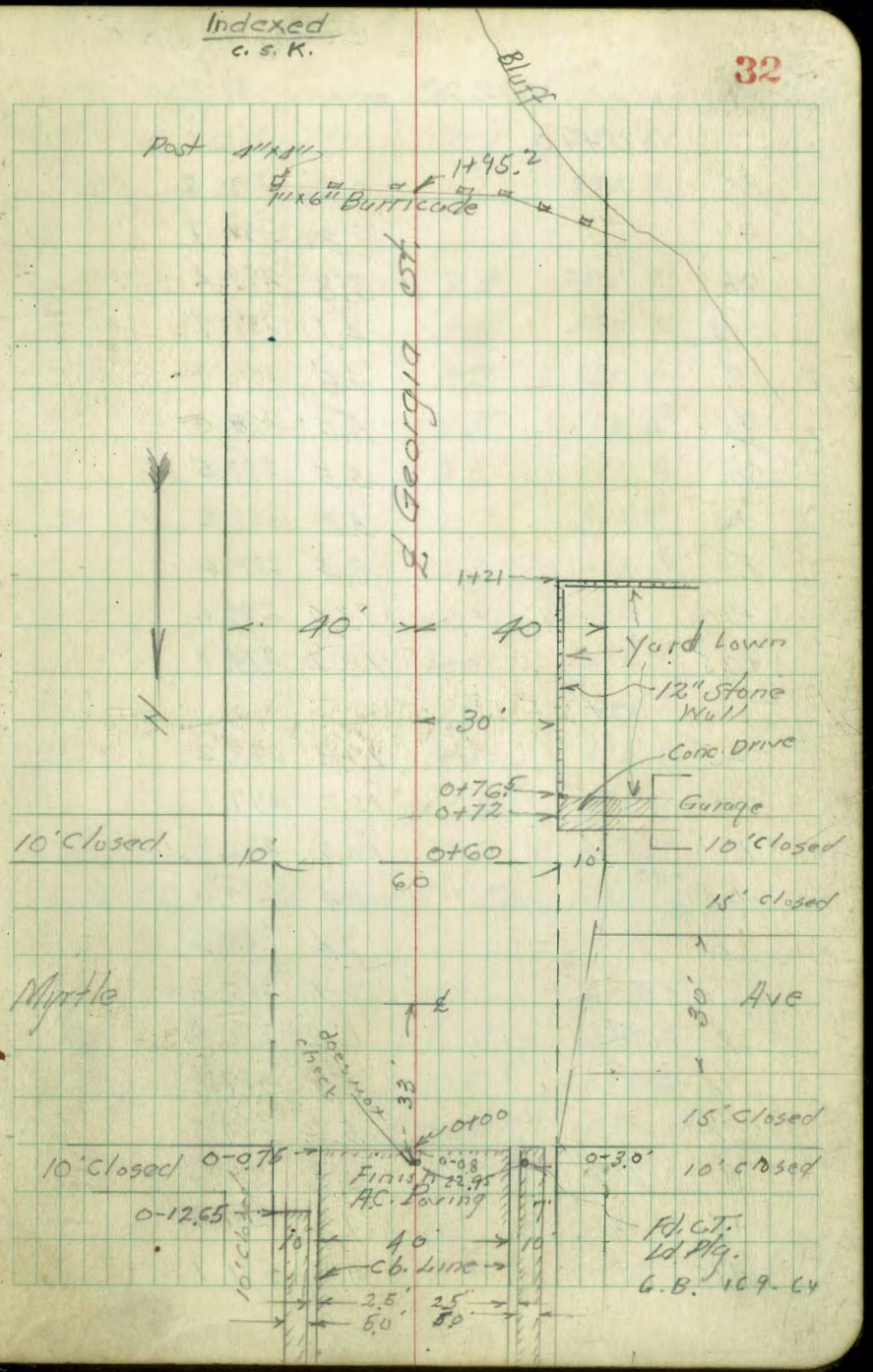
Sections → This Intersection 60' 10'cbs 10'-4"-5.

0-0.8 = South edge Paving

E. on Ground		7.3	285.7
" " Wall		3.87	289.11
cb = 0.75'		3.93	289.05
Gut.	on Pav.	4.50	288.48
¼	" "	3.82	289.16
½	" "	3.39	289.59
¼		3.21	289.77
Gut.		3.32	289.66
+25	on Walk	2.61	290.37
+75		2.47	290.51
W		1.9	291.1
+10		+0.7	292.8

Indexed
C. S. K.

32



Georgia St

292.98

0+10

W-10	+0.2	292.8
W	1.3	291.7
cb.	3.8	289.2
1/4	4.1	288.9
℄	4.6	288.4
1/4	5.0	288.0
cb.	5.5	287.5
+4	5.8	287.2
E	8.4	284.6
+10	13.9	279.6
+25	18.2	274.8

0+25

-25	19.8	273.2
-10	15.2	277.8
E	10.2	282.8
+4	8.4	284.6
cb.	7.4	285.6
1/4	7.1	285.9
℄	6.6	286.4
1/4	5.9	287.1
cb.	5.2	287.8
W	2.2	290.8
+5	1.3	291.7
+10	1.1	291.9

292.98

33

0+30.2 = N. edge Conc. Ret 12" wall on W 2' Buck

on 12" wall

Ground at wall

0+50

-10	11.1	291.87
W	2.7	290.3
-10	7.3	285.7
W	7.8	285.2
+2	7.9	285.1
+5	9.5	283.5
cb.	9.8	283.2
1/4	10.1	282.9
℄	10.8	282.2
1/4	10.9	282.1
cb.	11.6	281.4
+4	11.9	281.1
E	14.7	278.3
+9	17.5	275.5
+25	19.3	273.7

0+52.5 35'W of ℄ = Elec. Pole (Fx. Lamp)

0+56

-75	19.6	273.4
-7	17.7	275.3
E.	14.8	278.2
cb.	12.2	280.8
1/4	11.9	281.1
℄	11.8	281.2
1/4	11.2	~~278.8~~ 281.8

		29.98 Georgia St.		
cb.			11.0	282.0
+3			10.9	282.1
W			8.8	284.2
+10			8.3	284.7
TP	1.42	281.47	12.93	280.05 ✓
	0+59			
-25			1.8	279.7
W			0.5	281.0
cb.			0.1	281.4
¼			0.4	281.1
℄			0.9	280.6
¼			1.1	280.4
cb			1.2	280.3
E			4.2	277.3
+7			6.3	275.2
+25			8.2	273.3
	0+72 = ℄		Conc. Drive on W. 10' inst 8' wide	
	0+70		20' cbs 10' ¼ from Here - South	
-20'			2.5	272.0
E.			7.7	273.8
+10			6.7	274.8
cb.			4.1	277.4
¼			3.6	277.9
℄			3.0	278.5

		281.47		
¼			2.2	279.3
cb			1.9	279.6
+10 on Drive			2.56	278.91
+20			2.51	278.96
	0+76.5 = beg. 12" Stone wall on W 10' inst.			
on w/all			1.87	279.60
Base "			2.4	279.1
	1+00			
-5 in yard			2.8	278.7
W " "			2.8	278.7
+10			2.9	278.6
" on w/all			2.38	279.09
+14			5.0	276.5
+20 = cb			5.6	275.9
¼			5.9	275.6
℄			6.6	274.9
¼			7.0	274.5
cb			7.6	273.9
E			8.9	272.6
+10			9.9	271.6
+18			12.4	269.1
+20			14.5	267.0
	1+21.3 = End Above 12" Stone Wall 9' in St.			
on w/all			3.06	278.41

	1+25			
-25			16.0	265.5
-15			12.3	269.2
E			10.6	270.9
cb.			9.2	272.3
¼			8.7	272.8
℄			8.4	273.1
¼			8.1	273.4
cb.			8.2	273.3
W			8.5	273.0
+10			8.7	272.8
	1+50			
-10			10.8	270.7
W			10.3	271.2
cb.			9.9	271.6
¼			10.0	271.5
℄			9.9	271.6
¼			10.1	271.4
cb.			10.3	271.2
E			10.9	270.6
+6			12.0	269.5
+25			17.5	264.0
	1+75			
T.P.	2.59	271.64 ✓	12.47	269.05 ✓
T.P.	3.23	272.28 ✓	2.59	269.05 ✓ on Rock

Note: Section 1+90 P-56

1+75		
-25	9.3	263.0
E	3.3	269.0
cb.	2.2	270.1
¼	2.1	270.2
℄	1.8	270.5
¼	1.5	270.8
cb	1.5	270.8
W	1.9	270.4
+10	3.1	269.2
2+00		
W in Canyon	22.0	250.3
+78 on Bluff	6.5	265.8
cb.	4.9	267.4
¼	4.0	268.3
℄	3.6	268.7
¼	3.7	268.6
cb.	4.0	268.3
E	4.7	267.6
+25	10.4	261.9
2+25		
-25	12.0	260.3
E	7.7	264.6
cb.	7.4	264.9
¼	6.9	265.4
+6	6.7	265.6

27228 Georgia St.

℄		7.4	269.9	
1/4		8.6	263.7	
cb.		11.8	260.5	
+2	on Bluff.	13.5	258.8	
+3	in Canyon	28.5	248.8	
T.P.	12.96 284.63	0.61	271.67	
T.P.	12.78 295.82	1.59	283.04	
chk starting B.M.		1.78	294.04	

Walker & Party

7-3-46 Additional Sections - Georgia St.

B.M. on Rock P. 35

	1.28 270.33		262.05	
chk. Ground ℄ 2+00		1.6	268.7	
	2+09			
-25'		2.0	261.3	
E.-3'		4.2	~~264.5~~	266.1
E		3.8	~~264.9~~	266.5
cb.		3.0	~~265.7~~	267.3
1/4		2.5	~~266.2~~	267.8
℄		2.6	~~266.1~~	267.7
1/4		3.6	~~265.1~~	266.7
cb		5.0	~~263.7~~	265.3
+10	on Bluff	6.1	~~262.6~~	264.2
+11	in Canyon	22.1	~~246.6~~	248.2
	2+19			
W+13	in Canyon	22.1	~~246.6~~	248.2
+14	on Bluff	9.1	~~259.6~~	261.2

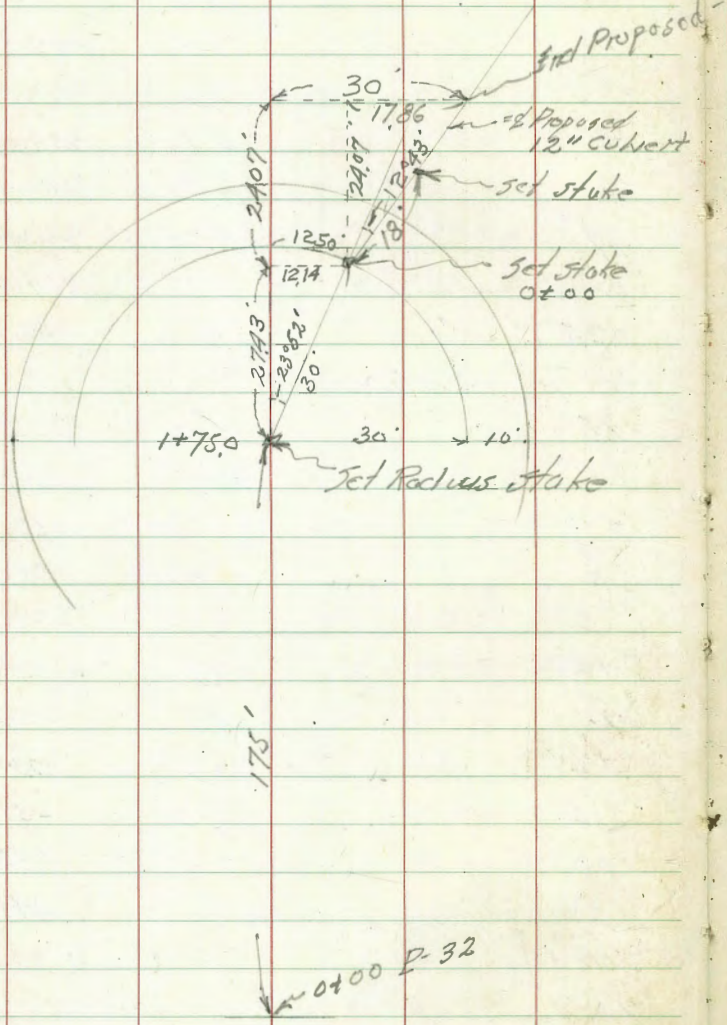
2+19 27033

W cb.		7.2	~~261.5~~	263.1
W 1/4		5.5	~~263.2~~	264.8
℄		4.4	~~264.3~~	265.9
+2		3.9	~~264.8~~	266.4
1/4		4.1	~~264.6~~	266.2
cb.		4.3	~~264.4~~	266.0
~~1/4~~		5.0	~~263.7~~	265.3
E		4.7	~~264.0~~	265.6
+25		9.9	~~258.8~~	260.4
	2+50			
-25		13.0	~~255.7~~	257.3
E		10.6	~~258.1~~	259.7
+10		10.0	~~257.7~~	259.3
cb.		10.4	~~258.3~~	259.9
1/4		10.1	~~258.6~~	260.2
+6		13.9	~~254.8~~	256.4
℄		14.5	~~254.2~~	255.8
+2		14.9	~~254.8~~	255.4
1/4		17.3	~~251.4~~	253.0
+8 = Bluff.		19.6	~~249.1~~	250.7
+9 = Canyon 10' East of ℄ 2+50		27.6	~~241.1~~	242.7
on Axis Transit		6.41	263.92 HI Transit	

VΔ	Slope	Horiz.	Diff Elev	Stake Elev.
-19°10' Rod 4.41	77.09	72.8	25.21 - 4.41 Rod = 20.80	234.30

Above Stake 22.8' West of W Line at Sta. 2+50

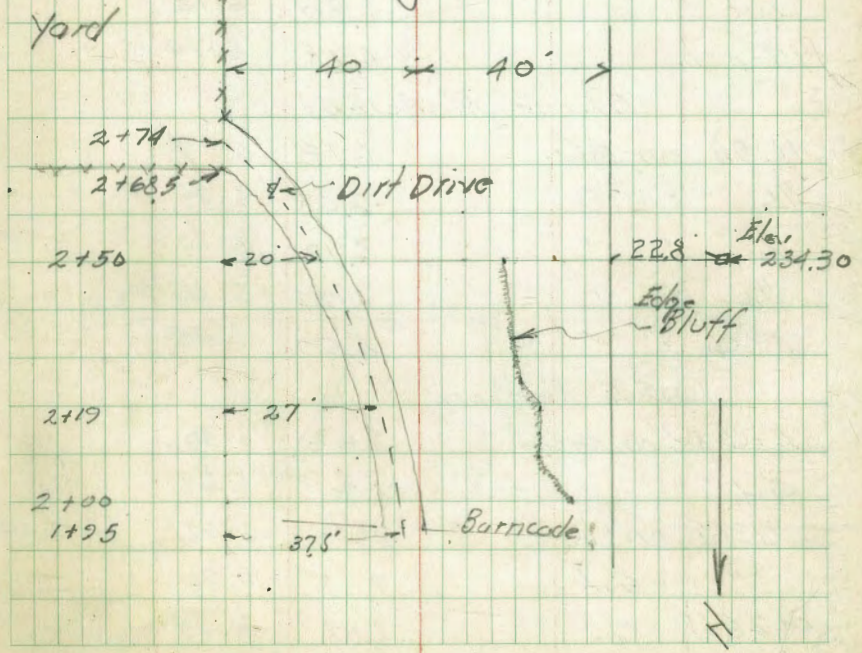
Georgia St.
Cont. from P-36



12" Pipe

Profile Proposed 12" Culvert

	3.62	272.67	269.05 Rock P-36
0+00		5.1	267.6
+16		9.1	263.6
+14.8		10.2	262.7
+18 on stake		9.82	
*22 = edge Bluff		12.8	259.9
Obs. ℄ Ground	2+09	5.0	267.7



Walker
Hendricks
Hunter
Carey

1-3-46

Cross Section - Keats St.

70' Wide
18" Cbs. 8.5' 1/4 5'

	6.11	8.86		2.75	B.M. SW Br. Rosecrans & Garrison
T.P.	7.12	12.63	3.35	5.51	Ld. & Disk
T.P.	6.26	12.92	5.97	6.66	W.Y.L.Y Cor. Rosecrans & Keats

27' E, E.L.Y. Line Rosecrans = End cb. Returns

S. Top cb.	6.62	6.30
" Gut. on Paving.	7.23	5.69
1/4 " "	6.91	6.01
℄ " "	6.75	6.17
1/4 " "	6.72	6.20
Gut " "	6.80	6.12
N Top cb	6.18	6.74

E. Line Rosecrans

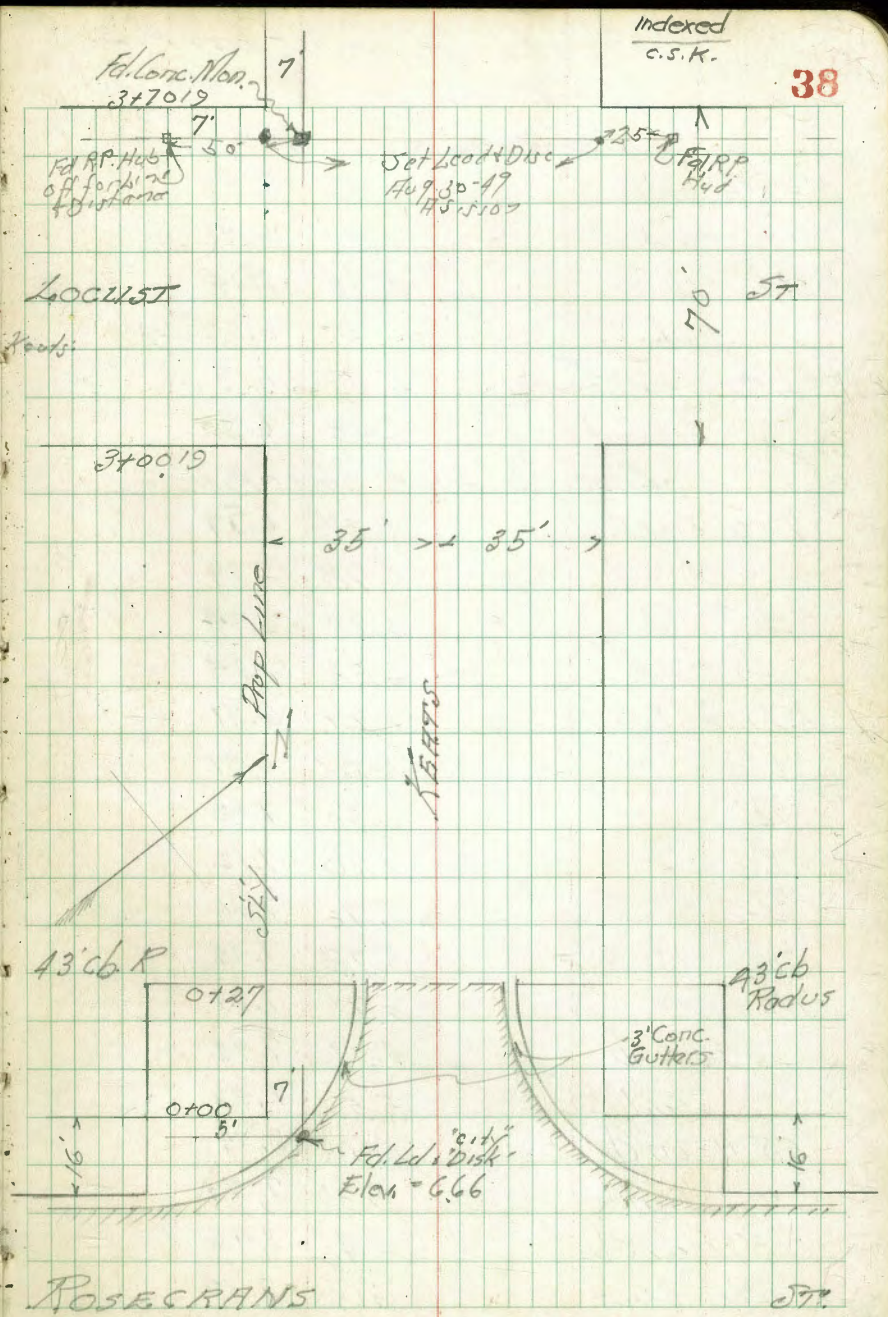
N cb on Par.	6.13	6.79
1/4 " "	6.08	6.84
℄ " "	6.12	6.80
1/4 " "	6.24	6.68
S cb " "	6.50	6.42

S E Return

B.C. cb Rd. on Keats.	6.62	6.30
Gut	7.23	5.69
+12.68 on cb.	6.40	6.52
" " Gut	7.02	5.90
+26.68 " cb.	6.08	6.84
" " Gut.	6.72	6.20

Indexed
C.S.K.

38



Keats St. Cont. from P. 38

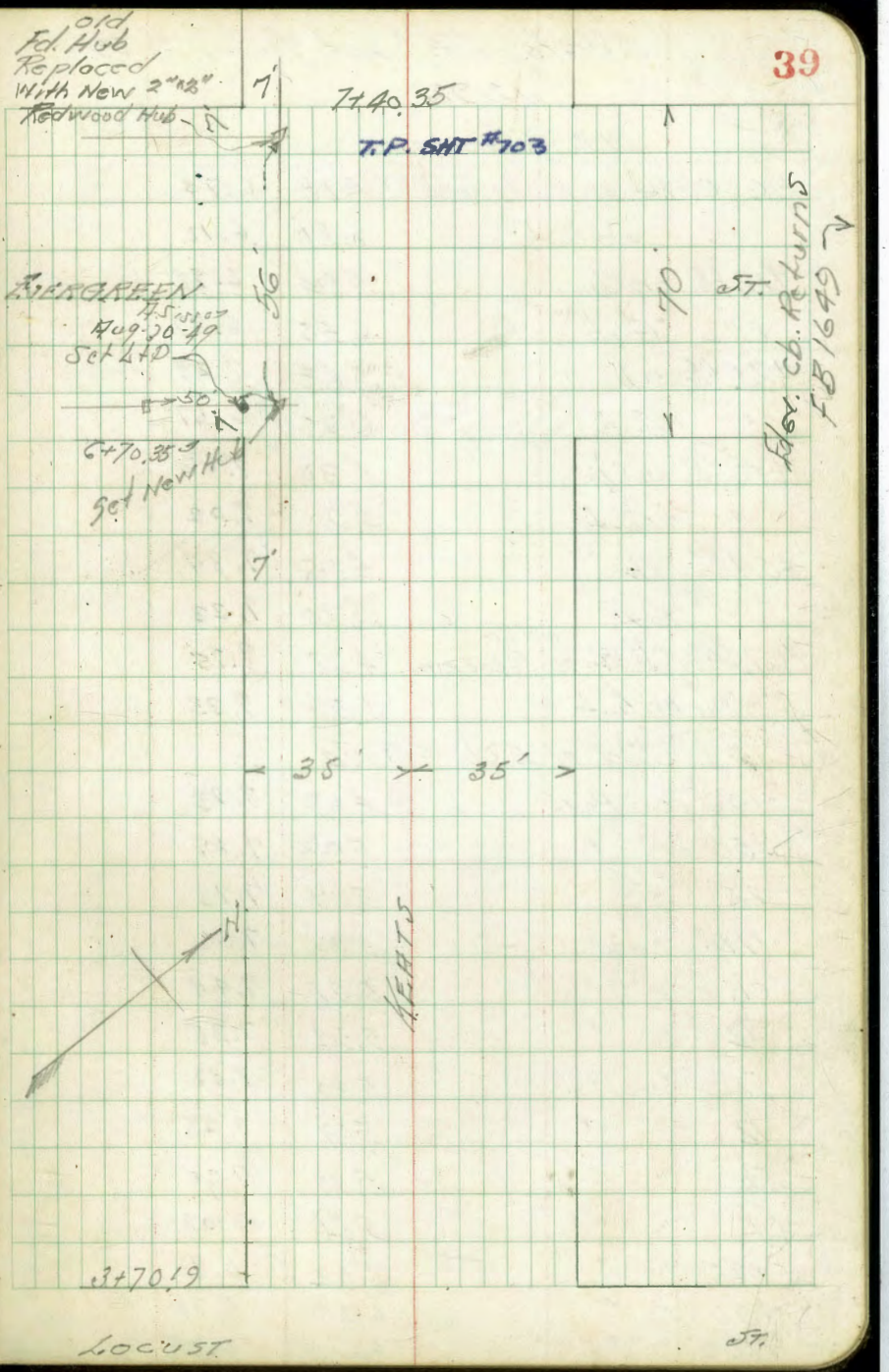
12.92

S.E. Return Cont. from P. 38

7+40.86	on cb.	5.89	7.33
"	"Gut.	6.51	6.91
7+54.86	" cb	5.78	7.14
"	"Gut. on cb.	6.40	6.52
7+67.54	= E.C. on Rosecrans	5.79	7.13
"	on Gut.	6.42	6.50

East cb Line Rosecrans

-100'	on cb	6.33	6.59
"	"Gut.	6.93	5.99
-50'	" cb	5.98	6.94
"	"Gut.	6.58	6.34
S. Line	Pav.	6.21	6.71
cb.	"	6.01	6.91
1/4	"	5.90	7.02
℄	"	5.80	7.12
1/4	"	5.76	7.16
cb	"	5.73	7.19
N.L.	"	5.71	7.21
cb	E.C. cb	4.97	7.95
	Gut	5.59	7.33
50' N	on cb	4.78	8.14
"	" Gut	5.38	7.54
100' N	on cb.	4.46	8.46
"	" "Gut.	5.05	7.87

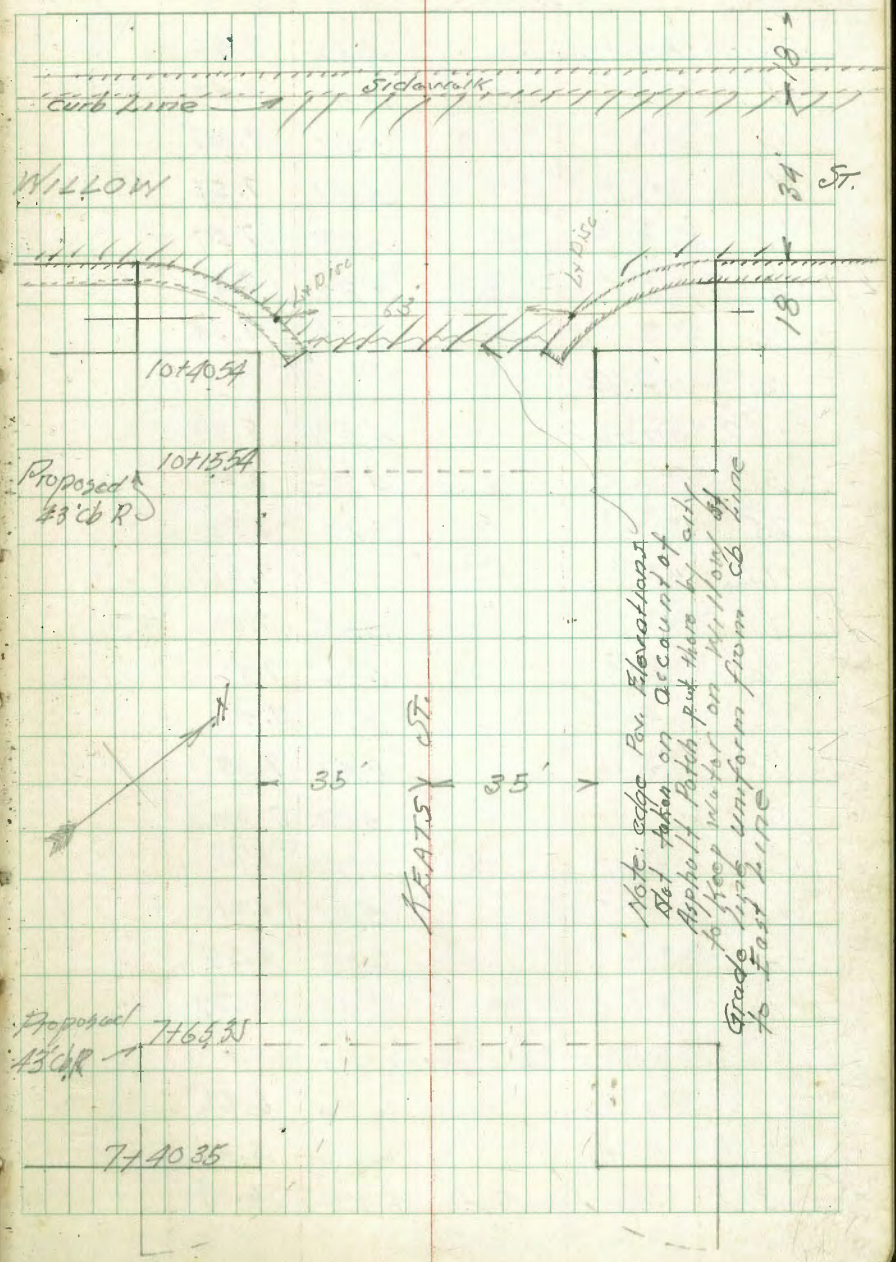


Keats St. Cont. from P. 39

12.92

N.E. Return

B.C. cb	Rot. on Keats on cb	6.18	6.74
"	on Gut.	6.80	6.12
7+12.68	on cb	5.94	6.98
"	" Gut.	6.55	6.37
7+26.68	" cb	5.63	7.29
"	" Gut.	6.25	6.67
7+40.68	on cb.	5.30	7.62
"	" Gut	5.90	7.02
7+54.86	" cb	5.08	7.84
"	" Gut	5.70	7.22
7+67.54	= cb EC. on Rosecrans on cb	4.97	7.95
"	on Gut.	5.59	7.33
	17' W of E cb. = E ½		
-100'	on Por.	4.69	8.23
-50'	" "	5.03	7.89
-25'	" "	5.19	7.73
NL.	" "	5.36	7.56
cb	" "	5.48	7.44
¼	" "	5.54	7.38
℄	" "	5.60	7.32
½	" "	5.67	7.25
cb	" "	5.72	7.20
SL.	" "	5.84	7.08
+25	" "	6.02	6.90
+50'	" "	6.20	6.72
+100'	" "	6.53	6.39



	12.92	Keats St.	
	E. Rosecrans		
Eline	on Pav.	5.66	7.26
cb	" "	5.52	7.40
½	" "	5.45	7.47
℄	" "	5.41	7.51
½	" "	5.35	7.57
cb.	" "	5.30	7.62
NL.	" "	5.18	7.74
	N ½		
-100'	on Pav.	4.59	8.33
-50'	" "	4.92	8.00
-25'	" "	5.10	7.82
N.L.	" "	5.24	7.68
cb.	" "	5.40	7.52
½	" "	5.46	7.46
℄	" "	5.52	7.40
½	" "	5.57	7.35
cb	" "	5.62	7.30
SL	" "	5.74	7.18
+25'	" "	5.91	7.01
+50'	" "	6.08	6.84
+100'	" "	6.43	6.39
	West cb. Rosecrans		
-100'	on cb.	6.30	6.62
"	" Gut.	6.90	6.02
3' E	" Edge Conc. Gut.	6.83	6.09

	12.92	Keats St.	
	W. cb. Rosecrans Cont. from Opp. Page		41
-50'	on cb	6.01	6.91
"	" Gut	6.61	6.31
3' E	on "	6.51	6.41
SL	" Pav.	6.11	6.81
cb.	" "	5.96	6.96
½	" "	5.87	7.05
℄	" "	5.81	7.11
½	" "	5.75	7.17
cb	" "	5.71	7.21
NL.	" "	5.58	7.34
+50'	on cb.	4.84	8.04
"	" Gut	5.44	7.48
3' E	" "	5.37	7.55
+100'	" cb.	4.51	8.41
"	" Gut.	5.11	7.81
3' E	" "	5.03	7.89
	N.W. Ref. on cb.		
B.C.	on Rosecrans	4.98	7.94
	" Gut.	5.60	7.32
	3' E	5.44	7.48
B.C.	+12.68 on cb.	5.03	7.89
	" " Gut	5.66	7.26
	3' SL. on "	5.60	7.32
	+26.68 on cb.	5.13	7.79
	" " Gut	5.76	7.16
	3' SL. " "	5.68	7.24

12.92 Keats St

NW Ret. Cont. from P. 41

+40.86 on Cb	5.23	7.69
" " Gut	5.87	7.05
3'Lt "	5.84	7.08
+54.86 on Cb	5.17	7.75
" " Gut	5.80	7.12
on Cb. 3'Lt →	6.78	7.14
+67.54 Cb EC. on Keats →	5.12	7.80
" on Gut.	5.76	7.16
3'Lt.	5.69	7.23

SW Ret.

EC. on Rosecrans on Cb	5.77	7.15
" Gut.	6.44	6.48
3' Rt	6.34	6.58
+12.68 on Cb	5.76	7.16
" " Gut.	6.39	6.53
3' Rt "	6.29	6.63
+26.68 on Cb.	5.79	7.13
Gut.	6.46	6.52
3'R	6.22	6.70
+40.68 on Cb	5.75	7.17
" " Gut	6.34	6.58
3'R "	6.17	6.75
+54.86 on Cb.	5.71	7.21
Gut	6.34	6.58
3' R "	6.12	6.80

12.92

SW. Ret. Cont.

Cb EC. Cb.	5.62	7.30
Gut.	6.23	6.69
3'R	6.12	6.80
0+00 = NLY Line Rosecrans		
E	5.0	7.92
Cb. on Pov.	5.78	7.14
1/4 " "	5.87	7.05
1/2 " "	5.95	6.97
1/4 " "	5.99	6.93
Cb. " "	6.07	6.85
SLine	5.6	7.3
0+27		
-5	5.1	7.8
SL.	4.9	8.0
Cb.	5.62	7.30
Gut. on Pov	6.23	6.69
1/4 " "	5.94	6.98
1/2 " "	5.81	7.11
1/4 " "	5.74	7.18
Gut.	5.76	7.16
Cb.	5.12	7.80
N	4.5	8.4
45	4.4	8.5
0+50		
-5	4.0	8.9
N	4.0	8.9

		12.92	Heats St.	
Cb.			4.2	8.7
+4			4.0	8.9
+5			4.5	8.4
1/4			4.3	8.6
℄			4.2	8.7
1/4			4.4	8.5
+3			4.7	8.2
Cb.			4.4	8.5
SL.			4.8	8.1
+5			5.0	7.9
	1+00			
-5			3.5	9.4
SL			3.5	9.4
+11 = Power Pole				
Cb.			3.5	9.4
+3			3.1	9.8
1/4			3.1	9.8
℄			2.9	10.0
1/4			2.9	10.0
+3			3.0	9.9
+4			2.7	10.2
Cb			3.6	9.3
NL.			3.1	9.8
+5			2.8	10.1
T.P.	802	18.60	2.34	10.58
	1+50			
-5			7.2	11.4
N			7.4	11.2

	1+50	18.60
N Cb.	8.1	10.5
+4	7.9	10.7
+5	8.2	10.4
1/4	8.1	10.5
℄	8.1	10.5
1/4	8.3	10.3
Cb.	8.3	10.3
SL.	8.5	10.1
+5	8.6	10.0
1+81 = ℄ 3' Conc. Walk on South Line		
SL Line on Walk	8.20	10.4
10'S " "	8.20	10.4
1+90.5 = ℄ 8' Conc. Drive on South on Line		
SL Line on Drive	8.35	10.25
4.5' " " at Gutter	8.20	10.40
2+00		
-5	8.2	10.4
5	8.2	10.4
Cb.	8.0	10.6
1/4	7.8	10.8
℄	7.7	10.9
1/4	7.7	10.9
+2	7.7	10.9
+3	7.1	11.5
Cb.	7.5	11.1
N	7.0	11.6
+5	7.0	11.6

18.60 Keats St.

2+50 - ℄ Power pole on South 10.5' in St.

-5	6.5	12.1
N	6.5	12.1
cb.	7.0	11.6
+6	6.8	11.8
1/4	7.2	11.4
℄	7.3	11.3
1/4	7.3	11.3
cb.	7.6	11.0
o.L.	7.7	10.9
+5	7.8	10.8

2+75.19 - B.C. Proposed 43' Radius cb

-5	7.0	11.6
o.L.	7.1	11.5
cb.	7.1	11.5
1/4	7.0	11.6
℄	6.9	11.7
1/4	7.0	11.6
+1	6.5	12.1
cb.	6.6	12.0
N	6.2	12.4
+5	6.2	12.4

3+00.19 - ℄ Lane Locust St.

-5	5.7	12.9
N	5.9	12.7
cb	6.1	12.5
+6	5.9	12.7
1/4	6.6	12.0

3+00.19 18.60

℄	6.5	12.1
1/4	6.6	12.0
+6	6.9	11.7
cb.	6.6	12.0
o.L.	6.9	11.7
+5	6.9	11.7

3+18.19 - ℄ cb. Locust

-5	6.4	12.2
5	6.3	12.5
cb.	6.2	12.4
+2	6.6	12.0
1/4	6.2	12.4
℄	6.0	12.6
1/4	6.0	12.6
+1	5.7	12.9
cb.	5.7	12.9
N	5.4	13.2
+5	5.4	13.2
+200' on cb Rot. at Lowell ℄	2.94	15.66 SE Rot. Lowell
SE. Rot on cb	1.99	16.61

3+26.69

-5	5.3	13.3
N	5.4	13.2
cb	5.6	13.0
1/4	5.8	12.8
℄	5.8	12.8
1/4	6.0	12.6

		18.60	Keats St.	
	3+26.69			
¼+6			6.5	12.1
cb.			6.2	12.4
S			6.4	12.2
+5			6.6	12.0
	3+35.19			
-5			6.7	11.9
S			6.6	12.0
cb.			6.3	12.3
¼			5.9	12.7
℄ on Rim Sewer MH			5.46	13.14
¼			5.5	13.1
cb.			5.6	13.0
N			5.4	13.2
+5			5.4	13.2
	3+43.69			
-5			5.3	13.3
N			5.2	13.4
cb.			5.4	13.2
¼			5.2	13.4
℄			5.4	13.2
¼			5.8	12.8
cb			6.1	12.5
S			6.5	12.1
+5			6.8	11.8
	3+52.19			
-5			6.6	12.0
S			6.4	12.2

	18.60	Keats St.	
Scb.		6.0	12.6
¼		5.7	12.9
℄		5.4	13.2
¼		5.1	13.5
cb.		5.2	13.4
N		4.9	13.7
+5		4.8	13.8
	3+70.19 = WLY Line Locust St		
-5		3.3	15.3
N		3.4	15.2
+10		4.7	13.9
cb.		4.8	13.8
+7		4.5	14.1
¼		4.9	13.7
℄		5.2	13.4
cb.		5.5	13.1
+3		5.6	13.0
S		6.1	12.5
+5		6.2	12.4
	3+64 Power Pole on South 4.5' in St.		
	3+85 = ℄ 3' Conc. on South, on Line		
	S. Line on Walk	6.02	12.58
	+10' " "	6.11	12.49
	4+12 = ℄ 7' Conc. Drive		
	S. Line on Drive	5.46	13.16
	+25' " " at Garage	6.10	

18.60 Keats St.

	4+00		
-5		5.7	12.9
S		5.7	12.9
+13		5.1	13.5
cb.		5.4	13.2
½		5.1	13.5
℄		4.8	13.8
¼		4.6	13.8
+1		4.2	14.4
cb.		4.3	14.3
+15		3.8	14.8
N on Lawn		3.1	15.5
+5 " "		2.9	15.7
	4+25		
S Line on 2' Conc. Ribbon		5.42	13.18
+25 " Drive		5.90	12.70
	4+30		
S Line on 2' Conc. "		5.41	13.19
+25 " " Drive		5.84	12.76
	4+50		
-5		2.3	16.3
N		2.3	16.3
cb.		3.2	15.4
¼		3.3	15.3
+2		3.8	14.8
℄		3.9	14.7
¼		4.2	14.4
cb.		4.5	14.1
+8		4.1	14.5

18.60

+7	4.6	14.0
S Lawn	4.9	13.7
+5 "	5.0	13.6
4+54 = ℄ 3' Conc. Walk on S		
S Line on Walk	4.70	13.90
+10 " "	4.76	13.84
T.P. 10.92 25.40	4.12	14.48 W
4+85.7 = ℄ 3' Conc. Walk on South		
S Line on Walk	10.49	14.91
+10 " "	10.68	14.82
5+00		
-5 on Lawn	10.3	15.1
S " "	10.2	15.2
+15	9.9	15.5
cb	10.2	15.2
¼	9.7	15.7
℄	9.5	15.9
+6	9.5	15.9
¼	9.1	16.3
cb.	8.6	16.8
N on Lawn	7.9	17.5
+5 " "	7.7	17.7
4+86.8 = ℄ 3' Conc. Walk on N		
N on Walk	8.26	17.14
+10 " "	7.78	17.62
5+12.5 = ℄ 2.5' Conc. Drive on N. Line		
N. Line on Drive	7.77	17.63
+28.5 " " at Curve	6.50	18.90

5+18 = ℄ Power Pole on S 10.3 Lt ℄		
5+11 = ℄ 2' Conc. Ribbon on South		
SL on Drive	9.77	15.63
+15 " " ℄ 2' "	10.22	15.18
5+16 = ℄ " "		
SL + 2.5 S.S. Line on Ribbon	9.77	15.63
+ 15 " " "	10.21	15.19
5+25 = ℄ 2' Ribbon on South		
SL +2 on Ribbon	9.46	15.94
+15	9.66	15.74
5+30		
SL. on Ribbon	9.31	16.09
+15 " "	9.57	15.83
5+54.5 = ℄ 3' Conc. Walk on S		
SL +0.3 on Walk	8.28	17.12
" +10' " "	8.41	16.99
5+50		
-5	6.4	19.0
S ℄	6.6	18.8
cb.	6.7	18.7
+7	6.8	18.6
½	7.1	18.3
+1	7.7	17.7
℄	7.6	17.8
½	7.7	17.7
cb.	8.0	17.3
+3	7.7	17.7

+7	8.3	17.1
SL.	8.4	17.0
+5 on Lawn	8.6	16.8
5+86 = ℄ 3' Conc. Walk on S 0.1' Back		
SL +0.1' on Walk	7.18	18.22
+10	7.57	17.83
6+00		
-5 on Lawn	6.7	18.7
S " "	6.6	18.8
+13 " "	6.1	19.3
cb.	6.3	19.1
½	5.8	19.6
℄	5.6	19.8
+7	5.5	19.9
½	5.1	20.3
cb	4.8	20.6
N	4.5	19.9
+5	4.5	19.9
6+11 = ℄ 2' Conc. Ribbon on SL		
SL. on Ribbon	5.86	19.54
+15 " "	6.50	18.90
6+16 ℄ 2' Conc.		
SL. on Ribbon	5.88	19.52
+15 " "	6.40	19.00
6+20 = ℄ 2' Conc. Ribbon on South		
SL. on Ribbon	5.89	19.51
+3.5' " " Back	5.96	19.49
+15' " "	6.37	19.03

	6+25 - ℄ Conc. Ribbon		
SL-	on Ribbon 25.40	5.77	19.63
+15	" "	6.31	19.09
	6755 = ℄ 3' Conc Walk on South		
SL.	on Walk	5.00	20.40
+10	" "	5.13	20.27
	6+40 = ℄ 3.4' Conc Walk	4.4' in ℄ on N.	
N+4.6'	on	2.86	22.54
5.4 N	N.L.	2.61	22.79
	6+45.35		
-5	on Lawn	2.5	22.9
N	" "	2.6	22.8
Cb.		3.5	21.9
+5		3.4	22.0
½		4.2	21.2
℄		4.3	21.1
½		4.6	20.8
Cb.		5.0	20.4
+2	Lawn	4.8	20.6
SL	on "	5.3	20.1
+5	" "	5.4	20.0
	6+70.35 = ℄ Pine Evergreen		
-5	on Lawn	4.8	20.6
5	" "	4.7	20.7
+16	" "	4.1	21.3
Cb.		4.4	21.0
½		3.8	21.6
℄		3.4	22.0

	25.40	Keats	
½		3.2	22.2
N		2.9	22.5
Cb.		2.8	22.6
N	on Lawn	2.3	23.1
+5	" "	2.2	23.2
	6+88.55 Cb		
-5		1.6	23.8
N		1.7	23.7
Cb.		1.8	23.6
+5		1.9	23.5
½		2.6	22.8
℄		2.8	22.6
½		3.3	22.1
Cb.		3.6	21.8
+2		3.4	22.0
SL		3.7	21.7
+5		3.8	21.6
6+79.7 = ℄ Power Pole		10.7 in ℄	on South
	6+96.85 ½		
-5		3.8	21.6
5		3.6	21.8
Cb.		3.2	22.2
½		2.9	22.5
℄		3.6	22.8
½		2.3	23.1
Cb		2.0	23.4
N		1.4	24.0
+5		1.3	24.1

2540

Keats St.

7+05.35 = ℄ Evergreen.

-5			0.8	24.6
N			0.9	24.5
cb.			1.5	23.9
1/4			1.9	23.5
℄			2.2	23.2
1/4			2.5	22.9
cb.			2.9	22.5
S			3.2	22.2
+5			3.3	22.1
	7+13.85 = 1/4			
-5			3.0	22.4
S			2.9	22.5
cb.			2.5	22.9
1/4			2.1	23.3
℄			1.8	23.6
1/4			1.7	23.7
cb.			1.4	23.9
N			1.1	24.3
+5			1.0	24.4
	7+22.35 cb			
-5			0.4	25.0
N			0.7	24.7
cb.			0.9	24.5
+6			1.2	24.2
1/4			1.7	23.7

2540

℄		1.4	24.0
1/4		1.7	23.7
cb.		2.3	23.1
+2		2.1	23.3
5L.		2.2	23.2
+5		2.4	23.0
T.P. 10.50	34.79	11.1	24.29
B.M.	Elec.		SE. Locust & Evergreen
chk. Spike in Pole		12.54	22.25 FB 1649:47
			22.23
			0.02 diff.
7+40.35 W.L.Y. Line Evergreen			
-5		10.6	24.2
S		10.5	24.3
+16		10.3	24.5
cb.		10.8	24.0
1/4		10.1	24.7
℄		10.0	24.8
1/4		10.1	24.7
cb.		9.3	25.5
N on		8.3	26.5
+5		8.1	26.7
~~7+65.35~~		7+57.83' Conc. Walk.	
N Line on Walk		6.86	27.93
+10 " "		6.47	28.32
7+65.35			
-5' on Lawn		6.3	28.5
N " "		6.4	28.4

N +12			6.5	28.3	
N cb.			7.2	27.6	
+7			8.5	26.3	
1/4			8.5	26.3	
℄			8.3	26.5	
1/4			8.5	26.3	
cb.			8.8	26.0	
+6			7.2	27.6	
SL			7.3	27.6	
+5			7.2	27.6	
	8+00 = 0.8' East of ℄				on North 7' Conc. Drive
-5			5.2	29.6	
SL.			4.9	29.9	
+12			4.3	30.5	
+16			6.0	28.8	
cb.			5.9	28.9	
1/4			5.9	28.9	
℄			5.8	29.0	
1/4			5.8	29.0	
cb.			4.8	30.0	
N			3.4	31.4	
+1' on Drive			3.35	31.44	
+18" "	"		2.04	32.75	
T.P.	8.10	41.99	0.90	33.89	Hunt Pole
	8+40.5 = Power Pole on S.		10.1	in St.	
	8+61.5 = ℄ 3' Conc. Walk on South				
S. Line	on Walk		2.74	32.25	
+10	" "		9.89	32.10	

8+86 ℄ 7' Conc. Drive on South 0.2' Back

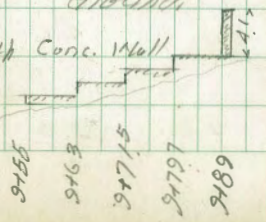
S +0.2 on Walk	8.70	33.29
+20 " "	9.31	32.68
8+50		
-5' on Lawn	10.2	31.8
SL + "	10.2	31.8
+11	10.1	31.9
cb.	10.5	31.5
1/4	10.1	31.9
℄	9.8	32.2
1/4	10.0	32.0
+7	8.8	33.2
cb.	8.6	33.4
+5 Lawn	7.7	34.3
N on "	7.0	35.0
+5 " "	6.9	35.1
8+45.2 ℄ 8' Conc. Drive		
N +0.5 Drive	7.26	34.73
+15 on "	6.83	35.16
8+66 = ℄ 3' Conc. Walk on N 11' in St.		
-10' on Walk	6.13	35.86
N " "	6.51	35.48
+11 " East "	6.87	35.12
8+96 = ℄ 7' Conc. Walk on N 0.6 Back		
N-0.6 on Drive	5.07	36.92
-15 " "	4.65	37.34

4.1.99 — Keats St.

	9+165 & 3' Conc. Walk on N on Line		
N	on Walk	4.45	37.54
+10	" "	4.05	37.94
	9+00		
-5	on Lawn	4.8	37.2
N		5.0	37.0
+16		6.3	35.7
cb.		6.6	35.4
+8		7.5	34.5
1/4		7.2	34.8
℄		7.0	35.0
1/4		7.4	34.6
cb.		7.8	34.2
+3	on	7.6	34.4
+9		7.9	34.1
S.L.		8.1	33.9
+0.4	on ℄ 7' Conc. Drive	8.05	33.95
+15	" Drive	8.35	33.65
	9+50		
-5		5.7	36.3
S		5.6	36.4
+10		5.2	36.8
+15		4.4	37.6
cb.		4.8	37.2
1/4		4.0	38.0
℄		3.7	38.3
1/4		4.0	38.0

4.1.99

1/4 +4'	4.3	37.7
N cb.	3.7	38.3
N on Lawn	2.8	39.2
+5 " "	2.6	39.4
9+46 & 7' Conc. Drive	0.8' Back on N	
N+0.8 on Drive	2.78	39.21
+15' " "	2.36	39.63
9+67 = ℄ 3' Conc. Walk on N		
N+0.5	1.59	40.40
+10	1.21	40.78
T.P. 11.98 51.79 ✓	2.18	39.81 N
9+90 = Power Pole on S 2.7' in St.		
9+55 = Beginning 6" Conc. Wall on South 1' Back		
9+55 on Wall	13.84	37.95
" Ground	14.9	36.9
9+63 on Wall	17.76	37.03
" Ground	14.3	37.5
9+71.5 on Wall	11.75	40.04
" Ground	13.3	38.5
9+79.7 on Wall	11.11	40.68
" " Ground	12.6	39.8
9+89 " Wall	11.03	40.76
" Ground	11.6	40.2



5179 Keats Cr.

-5	10.6	41.2
N	10.8	41.0
cb.	11.5	40.3
+2	11.8	40.0
+5	12.3	39.5
1/4	12.0	39.8
℄	11.7	40.1
1/4	12.6	39.8
cb.	12.7	39.1
+3	12.0	39.8
S	12.3	39.5
9+90		
-5 on Lawn	11.0	40.8
S	10.9	40.9
+12'	10.7	41.1
cb.	11.5	40.3
1/4	10.8	41.0
℄	10.6	41.2
1/4	10.9	40.9
+2	11.0	40.8
+5	10.2	41.6
cb.	10.3	41.5
N on Lawn	10.2	41.6
+5	10.2	41.6
10+00		
-5	8.8	43.0

5179

52

N	8.7	43.1
cb.	8.7	43.1
+2	9.0	42.8
+5	10.1	41.7
1/4	10.1	41.7
℄	9.8	41.9
1/4	10.1	41.7
℄	10.7	41.1
+2	9.9	41.9
S on Lawn	10.2	41.6
+5 " "	10.1	41.7
10+15.54		
-5 on Lawn	9.1	42.7
S	9.1	42.7
+16	8.9	42.9
cb.	9.4	42.4
1/4	8.9	42.9
℄	8.6	43.2
+6	8.6	43.2
1/4	9.0	42.8
cb	7.9	43.9
+3	7.5	44.3
E	7.8	44.0
+5	7.9	43.9
10+40.54 = E Line w/Lawn		
-5	5.6	46.2
N	6.1	45.7

51.79

Keats St.

+25 on Walk	6.10	45.7
cb. Rot	6.41	45.38
Gut.	7.21	44.58
cb on Ground	7.1	44.7
¼	6.9	44.9
℄	7.1	44.7
¼	7.3	44.5
cb.	7.7	44.1
+ Gut.	8.33	43.46
+ = cb Rot.	7.62	44.17
cb +94 on Walk	7.40	44.39
S	7.4	44.4
10+47.54		
S cb. on Por	7.50	44.29
¼ " "	7.82	44.47
℄ " "	7.11	44.68
¼ " "	6.93	44.86
N cb " "	6.81	44.98 ✓
NE Return Keats × Willow		
B.C. on Willow on cb	5.08	46.71
" Gut	5.86	45.93 ✓
+12.68 on cb	5.43	46.36
" " Gut	6.21	45.58
+26.68 " cb	5.74	46.05
" " Gut.	6.45	44.34

51.79

53

SE Rot.

8℄ on Willow on cb	7.98	43.81
" " Gut.	8.80	42.99
+12.68 on cb.	7.59	44.20
" " Gut.	8.38	43.41
+26.68 " cb	7.39	44.40
" " Gut	8.04	43.75
10+58.54 = E cb Willow		
-100' on cb.	3.13	48.66
" " Gut.	3.96	47.83
-56' on cb.	4.43	47.36
" " Gut	5.19	46.60
N " Por	6.09	45.70
cb " "	6.40	45.39
¼ " "	6.59	45.20
℄ " "	6.77	45.02
¼ " "	6.89	44.90
cb " "	7.10	44.69
S " "	7.64	44.15
+50' on cb	8.94	42.85 ✓
" " Gut.	8.77	42.02
+100 " cb. N Drive		
" " Gut.	11.68	40.11
10+67.04 - E ¼		
-100' on Por.	11.00	40.79
-50 " "	9.06	42.73

10+67.84 5179 Keats St.

-25' on Pav.	8.09	43.70
S " "	7.37	44.42
cb. " "	6.85	44.94
1/4 " "	6.68	45.11
℄ " "	6.57	45.22
1/4 " "	6.35	45.44
cb " "	6.17	45.62
N " "	5.76	46.03
+25' " "	5.25	46.54
+50' " "	4.67	47.12
+100' " "	3.44	48.35

10+75.84 = ℄ Willow

-100' " "	3.11	48.68
-50' " "	4.28	47.51
-25' " "	4.92	46.87 ✓
N " "	5.56	46.23
cb " "	5.94	45.85
1/4 " "	6.14	45.65
℄ on Rim MH	6.31	45.48
1/4 " Pav.	6.46	45.33
cb " "	6.65	45.14
S " "	7.16	44.63
+25' "	7.75	44.04
+50 "	8.65	43.14
+100' " "	10.62	41.17

10+84.4 = W 1/4 5179

-100 on Pav.	10.37	41.42
50 " "	8.47	43.32
+25 " "	7.54	44.25
S " "	6.98	44.81 ✓
cb " "	6.60	45.19
1/4 " "	6.39	45.40
℄ " "	6.16	45.63
1/2 " "	5.97	45.82 ✓
cb. " "	5.78	46.01
N " "	5.38	46.41
+25' " "	4.71	47.08
+50 " "	4.10	47.69
+100' " "	2.90	48.89

10+92.54 = W. cb. Willow

-100' on cb	2.17	49.62
" " Gut.	3.02	48.77
-50' on cb.	3.36	48.43
" " Gut.	4.23	47.56
-25' " cb. in Drive	~~4.81~~	
" " Gut	4.84	46.95 ✓
N " cb	4.68	47.11
" " Gut.	5.39	46.40
cb. " cb	5.00	46.79
" " Gut.	5.74	46.05
1/4 " cb.	5.22	46.57
" " Gut	5.90	45.89

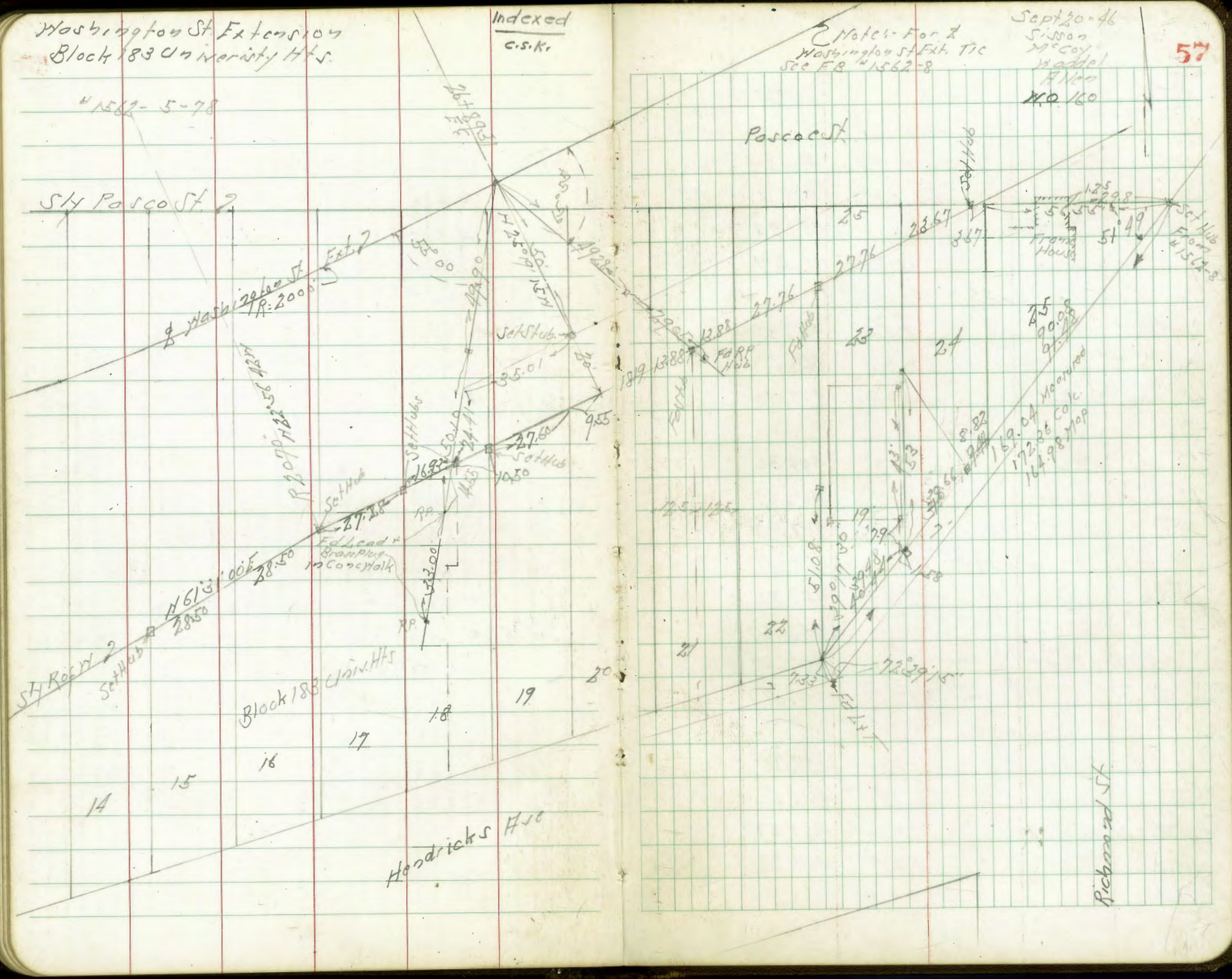
		51.79	Keats St.	
℄	on cb.		5.44	46.35
	" Gut		6.15	45.64
½	" cb.		5.60	46.19
	Gut		6.29	45.50
cb	on cb.		5.80	45.99
	" Gut.		6.47	45.32
S.L	" cb		6.21	45.58
"	" Gut.		6.24	44.85
+25'	on cb		6.76	45.03
	" Gut.		7.55	44.24
+50'	" cb		7.75	44.04
"	" Gut.		8.56	43.23
+100'	on cb		9.64	42.15
"	" Gut.		10.48	41.31
T.P.		0.67 39.29 ✓	12.47	39.32 ✓
T.P.		2.74 30.04 ✓	12.69	27.30 ✓
Chk Spike in Pole			7.78	22.26 ✓
SE Keats & Evergreen P.O.				22.23
				0.03

~~Field Work~~
Completed 7-5-46

Walker Georgia St.
Hendricks
Becker
9-4-46

Cont. from P-35

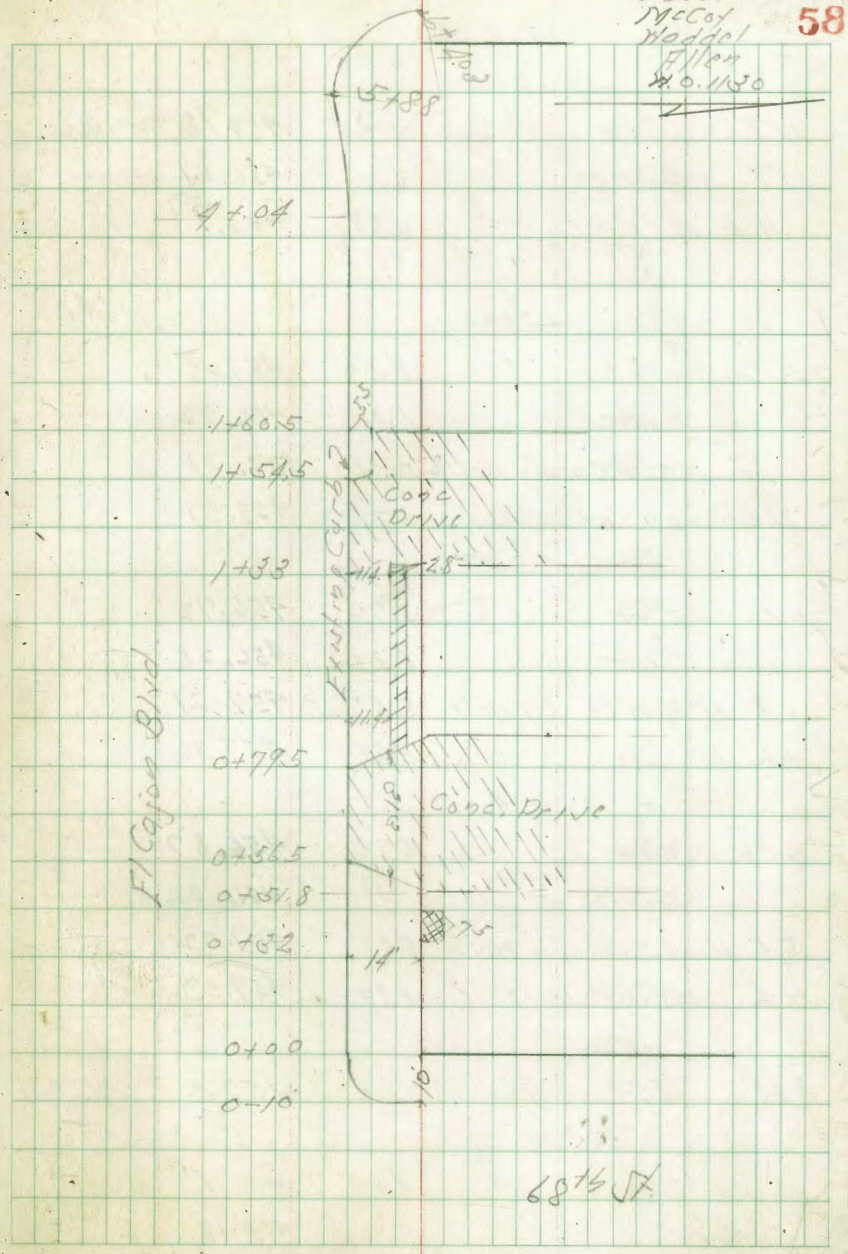
		π Hand Level		
	5.15	274.2	269.05	
Chk. Ground at 00 culvert		6.7	267.5	P-37
E-15		9.3	264.9	
E		6.0	268.2	
+10		5.1	269.1	
+20		5.0	269.2	
+30		4.8	269.4	
thc=℄		4.6	269.6	
℄+10		4.9	269.3	
+20		4.2	270.0	
+30		5.0	269.2	
+35		5.4	268.8	
6' South = Bluff		6.7	267.5	
℄+40 = W.L.		5.8	268.4	
6' South = Bluff.		7.3	266.9	
WL+5'		6.5	267.7	
6' South "		9.1	265.1	
WL+10		8.3	265.9	
6' " "		10.5	263.7	
WL+34		17.1	257.1	
7' " "		21.1	253.1	


Washington St Extension
Block 183 University Hts.
Indexed
C.S.K.
#1562-5-78
S'ly Pasco St.
Washington St.
R:200.
Ext 7
Set Stub
Set Hub
Fd Lead & Brass Plug in Conc. Walk
Fd Hub
Fd RR Hub
RP
Block 183 Univ. Hts.
Hendricks Hse
Pasco St.
Note:- For Z Washington St Ext. Tie See F.B. #1562-8
Sept 20-46
Simon McCoy Waddel & Allen
Frame House
Fd Nail
Fd Cut
Fd Pin
Macadam Road
Richmond St.
57

Levels North Curb Line of El Cajon Blvd West of 68th St 67th St.

BM	5.28	462.68		457.40	S.W. BP El Cajon 68th St.
		0-10 = N Cb 68th St.			
14'	N of N Cb El Cajon		5.74	456.94	= Top Cb
		0+00 = N.L. 68th St.			
N Cb	= Top Curb		5.14	457.54	
"	= Gutter		5.84	456.84	
		0+32			
N Cb	= Top Curb		5.34	457.34	
"	Gutter		5.98	456.70	
N.L. El Cajon			4.98	457.70	on Conc Wall
		0+51.8			
N Cb	= Top Cb		5.32	457.36	
"	Gutter		6.00	456.68	
N L	= El Cajon Drive		4.91	457.77	
		0+56.5			
N Cb	= Top		5.33	457.35	
"	Gutter		6.01	456.67	
5.8	N of N Cb		5.06	457.62	
N L			4.91	457.77	
		0+79.5			
N Cb	= Top		5.42	457.26	
"	" Gutter		6.12	456.56	
5.8	N of N Cb		5.11	457.57	
N L			4.95	457.73	

67th St. Dec. 2-46
Sisson
McCoy
Waddell
Fuller
No. 11830



El Cajon Blvd	68th to 67th St.				
	462.68				
	0+85				
NCb	Top		5.44	457.18	Add 0.06
"	Gutter		6.11	456.51	
11.4	N of NCb - Conc Walk		4.88	457.74	
	1+33				
NCb	Top		5.57	457.05	
"	Gutter		6.30	456.32	
11.4	N of NCb - Conc Walk		5.31	457.31	
NL	on Conc Walk		5.25	457.37	
	1+54.5				
NCb	Top		5.70	456.92	
"	Gutter		6.34	456.28	
5.5	N of NCb - Conc Walk		5.41	457.21	
NL			5.26	457.36	
	1+60.5				
NCb	Top		5.75	456.87	
"	Gutter		6.36	456.26	
5.5	N of NCb - Conc Walk		5.40	457.22	
NL	on Conc Drive		5.29	457.33	
BM	3.93	461.33		457.40	STA BR El Cajon & 68th St
	2+0				
NCb	Top		4.52	456.81	
Gutter			5.16	456.17	

	461.33		
	2+50		
NCb	Top	4.77	456.56
Gutter		5.37	455.96
	3+0		
NCb	Top	4.97	456.36
Gutter		5.37	455.96
	3+50		
NCb	Top	5.01	456.32
Gutter		5.70	455.63
	4+04 = Approx. Cb BC.		
NCb	Top	5.21	456.12
Gutter		5.82	455.51
	4+50		
NCb		5.40	455.93
Gutter		6.01	455.32
	5+05		
NCb		5.74	455.59
Gutter		6.30	455.03
NCb		5.91	455.42
Gutter		6.55	454.78
	5+88 = PRC		
NCb		6.22	455.11
Gutter		6.78	454.55

Notes Reduced 12-4-46
C.A. Smith

		461.33			
		6+14			
Cb	Top		6.64	454.69	
Gutter			7.26	454.07	
TP	4.40	460.07	5.66	455.67	
		6+40.3 = N/ Cb			
Cb	Top		6.43	453.64	
Gutter			7.11	452.96	
BM			6.81	453.76	SW. BP. Elev 460.57 +6.81 453.76
B.M.			2.70	457.37	SW BP. Elev 460.57 +6.81 453.76

TABLE VI.—CORRECTIONS FOR SUB-CHORDS AND LONG CHORDS.

D	FOR SUB-CHORDS ADD 10	20	30	40	50	60	70	80	90	Excess of arc per 100 ft.
4°	.00	.00	.01	.01	.01	.01	.01	.01	.00	.02
6	.00	.01	.01	.02	.02	.02	.02	.01	.01	.05
8	.01	.02	.02	.03	.03	.03	.03	.02	.01	.08
10	.01	.02	.03	.04	.05	.05	.05	.04	.02	.13
12	.02	.04	.05	.06	.07	.07	.07	.05	.03	.18
14	.02	.05	.07	.08	.09	.10	.09	.07	.04	.25
16	.03	.06	.09	.11	.12	.12	.12	.09	.05	.33
18	.04	.08	.11	.14	.15	.16	.15	.12	.07	.41
20	.05	.10	.14	.17	.19	.20	.18	.15	.09	.51
22	.06	.12	.17	.21	.23	.24	.22	.18	.10	.62
24	.07	.14	.20	.25	.28	.28	.26	.21	.12	.74
26	.09	.17	.24	.29	.32	.33	.31	.25	.15	.86
28	.10	.19	.27	.34	.37	.38	.36	.29	.17	1.00
30	.11	.22	.31	.39	.43	.44	.41	.33	.19	1.15
32	.13	.25	.36	.44	.49	.50	.47	.38	.22	1.31
34	.15	.28	.40	.50	.55	.57	.53	.43	.25	1.48
36	.17	.32	.45	.56	.62	.64	.59	.48	.28	1.66
38	.18	.36	.51	.62	.70	.71	.66	.53	.31	1.86
40	.21	.40	.56	.69	.77	.79	.73	.59	.35	2.06
42	.23	.44	.62	.76	.85	.87	.81	.65	.38	2.28
44	.25	.48	.68	.84	.94	.96	.89	.72	.42	2.50
46	.27	.52	.75	.92	1.02	1.05	.98	.78	.46	2.74
48	.30	.57	.81	1.00	1.12	1.14	1.06	.86	.50	2.99
50	.32	.62	.89	1.09	1.21	1.24	1.15	.93	.55	3.24
52	.35	.67	.96	1.18	1.31	1.35	1.25	1.01	.59	3.52
54	.38	.73	1.04	1.28	1.42	1.46	1.35	1.09	.64	3.80
56	.41	.78	1.12	1.38	1.53	1.57	1.46	1.17	.69	4.09
58	.44	.84	1.20	1.48	1.65	1.69	1.57	1.20	.74	4.40
60	.47	.91	1.29	1.59	1.76	1.81	1.68	1.35	.80	4.72

D	LONG CHORDS 200	300	400	500
1	199.99	299.97	399.92	499.85
2	199.97	299.88	399.70	499.39
3	199.93	299.73	399.32	498.63
4	199.88	299.51	398.78	497.57
5	199.81	299.24	398.10	496.20
6	199.73	298.90	397.26	494.53
7	199.63	298.51	396.28	492.57
8	199.51	298.05	395.14	490.31
9	199.38	297.54	393.86	487.75
10	199.24	296.96	392.42	484.90
12	198.90	295.63	389.12	478.34
14	198.51	294.06	385.22	470.65
16	198.05	292.25	380.76	461.86
18	197.54	290.21	375.74	452.02
20	196.90	287.94	370.17	441.15
22	196.32	285.44	364.06	429.30
24	195.63	282.71	357.43	416.53
26	194.87	279.76	350.30	402.89
28	194.06	276.59	342.69	388.42
30	193.18	273.20	334.61	373.20
32	192.25	269.61	326.08	357.28
34	191.26	265.81	317.12	340.73
36	190.21	261.80	307.77	323.61
38	189.10	257.60	298.03	305.99
40	187.94	253.21	287.94	287.94
42	186.72	248.63	277.51	269.54
44	185.44	243.87	266.78	250.85
46	184.10	239.93	255.78	231.95
48	182.71	233.83	244.51	212.92

NOTE.—When a chord of less than 100 ft. is used the corrections given in the above table should be added to the nominal length of chord to get the length which should be used in order that the 100 ft. points will check with those obtained by using the standard 100 ft. chord. Thus in locating a 14° curve by 25 ft. chords measure 25'.06 for each chord. Long chords are useful in passing obstacles.

TABLE VII.—MIDDLE ORDINATES FOR RAILS IN FEET.

Deg. of Curve	LENGTH OF RAILS 32	30	28	26	24	22	20
1°	.022	.020	.016	.013	.011	.009	.008
2	.045	.038	.034	.029	.025	.021	.017
3	.067	.058	.051	.044	.037	.031	.026
4	.089	.079	.069	.060	.050	.042	.035
5	.112	.099	.086	.074	.063	.053	.044
6	.134	.117	.102	.088	.076	.064	.052
7	.156	.137	.120	.104	.088	.074	.061
8	.179	.158	.137	.119	.100	.085	.070
9	.201	.175	.153	.133	.112	.095	.078
10	.223	.196	.171	.148	.125	.106	.087
11	.245	.216	.188	.163	.139	.117	.096
12	.268	.236	.206	.179	.151	.128	.105
13	.290	.254	.222	.192	.163	.138	.113
14	.312	.275	.239	.207	.175	.148	.122
15	.334	.295	.257	.223	.188	.159	.131

Deg. of Curve	LENGTH OF RAILS. 32	30	28	26	24	22	20
16°	.356	.313	.273	.236	.200	.170	.139
17	.378	.333	.290	.252	.213	.180	.148
18	.400	.351	.306	.265	.225	.190	.156
19	.423	.371	.324	.280	.238	.201	.165
20	.445	.392	.341	.296	.250	.212	.174
21	.466	.410	.357	.309	.262	.222	.182
22	.487	.430	.375	.325	.275	.233	.191
23	.509	.450	.390	.338	.287	.243	.199
24	.531	.469	.408	.354	.299	.253	.208
25	.552	.486	.424	.367	.311	.263	.216
26	.573	.506	.441	.382	.323	.274	.225
27	.594	.524	.457	.396	.335	.284	.233
28	.618	.545	.475	.411	.348	.294	.242
29	.638	.564	.491	.424	.361	.303	.250
30	.660	.583	.508	.438	.374	.313	.259

SLOPE REDUCTIONS.

When distances are measured on a slope they may be reduced to the equivalent horizontal distance by the following approximate rule:—subtract from the slope distance the square of the rise divided by twice the slope distance. Thus for a slope distance of 250.3 ft. and a rise of 15 ft. correction=$15^2 \div 2 \times 250.3$=.45 (by slide rule) or horizontal distance=250.3—.45=249.85. When vertical angle=V. A. is measured horizontal distance=slope distance—slope distance (1—Cos. V. A.). Thus for slope distance of 248.7 ft. and V. A. of 4° 20′ from Table VIII Cos=.99714 and correction=1—.99714=.00286 per foot or total of .286× 2½ (near enough)=.57 and horizontal distance=248.7—.57=248.13 ft.

TRIGONOMETRICAL FORMULAS.

See fig. (a).

sin. $A=\frac{a}{c}$

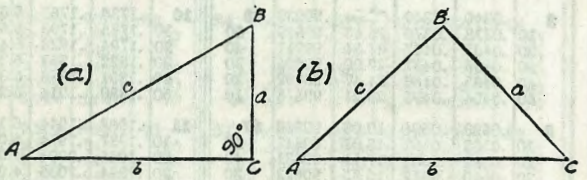
cos. $A=\frac{b}{c}$

tan. $A=\frac{a}{b}$

cot. $A=\frac{b}{a}$

sec. $A=\frac{c}{b}$

cosec. $A=\frac{c}{a}$



FORMULA FOR SOLVING TRIANGLES.

Given	Sought.	Right triangles. See fig. (a).
a, c	A, B, b	$\sin. A=\frac{a}{c}$, $\cos. B=\frac{a}{c}$, $b=\sqrt{(c+a)\,(c-a)}$
a, b	A, B, c	$\tan. A=\frac{a}{b}$, $\cot. B=\frac{a}{b}$, $c=\sqrt{a^2+b^2}$.
A, a	B, b, c	$B=90°-A$, $b=a \cot. A$, $c=\frac{a}{\sin. A}$.
A, b	B, a, c	$B=90°-A$, $a=b \tan. A$, $c=\frac{b}{\cos. A}$.
A, c	B, a, b	$B=90°-A$, $a=c \sin. A$, $b=c \cos. A$
Given	Sought.	Oblique triangles. See fig. (b).
A, B, a	b	$b=\frac{a \sin. B}{\sin. A}$
A, a, b	B	$\sin. B=\frac{b \sin. A}{a}$
a, b, C	$A-B$	$\tan. \frac{1}{2}(A-B)=\frac{(a-b) \tan. \frac{1}{2}(A+B)}{a+b}$
a, b, c	A	If $s=\frac{1}{2}(a+b+c)$, $\sin. \frac{1}{2}A=\sqrt{\frac{(s-b)\,(s-c)}{b\,c}}$, $\cos. \frac{1}{2}A=\sqrt{\frac{s\,(s-a)}{b\,c}}$, $\tan. \frac{1}{2}A=\sqrt{\frac{(s-b)\,(s-c)}{s\,(s-a)}}$, $\sin. A=\frac{2\sqrt{(s-a)\,(s-b)\,(s-c)\,s}}{b\,c}$
A, B, C, a	area	$\text{area}=\frac{a^2 \sin. B \sin. C}{2 \sin. A}$
A, b, c	area	$\text{area}=\frac{1}{2} b\,c \sin. A$
a, b, c	area	$s=\frac{1}{2}(a+b+c)$, $\text{area}=\sqrt{s\,(s-a)(s-b)(s-c)}$

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20—16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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