

1714

# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to  $30.6 = 32.6$ . For slopes of 1 on 1½ see inside of back cover.  
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# 1714

## CITY ENGINEER'S OFFICE

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

X-Sec.	Alley BIK. 17, Lexington Park	2
"	Alley BIK. H #15 " "	5
"	Alley BIK. 25 " "	10
"	Alley E-W. BIK. 25 " "	10
"	Alley BIK. 13 " "	13
"	Alley BIK. 16 " "	16
"	Tuberose, Poplar St. S'ly to Primrose Lane	22
"	Alley BIK. 12, Lexington Park	36
"	Alley BIK. 319 & 322, Reed & Daley Addition	39

1/3 sec alley 15' wide

Blk. 17 Lexington Park

Note! Sta. on Nby Line alley  
Plotted a.m.

1195-51.

B.M. RR. SPIK  
NEW CAN. RR. C.I.C. 301.56 295.40 Pepper Dr. Columbine

0+00 Sec. diag.

N	STUB	5.36	96.20
C		5.1	96.5
S		4.9	96.7

0+14.4

S	Beg. hedge = S-03	4.9	96.7
C		5.0	96.6
N		4.9	96.7

0+30

S ± 1X & 12" P.P.

0+50

N		4.5	97.1
C		4.3	97.3
S		4.1	97.5

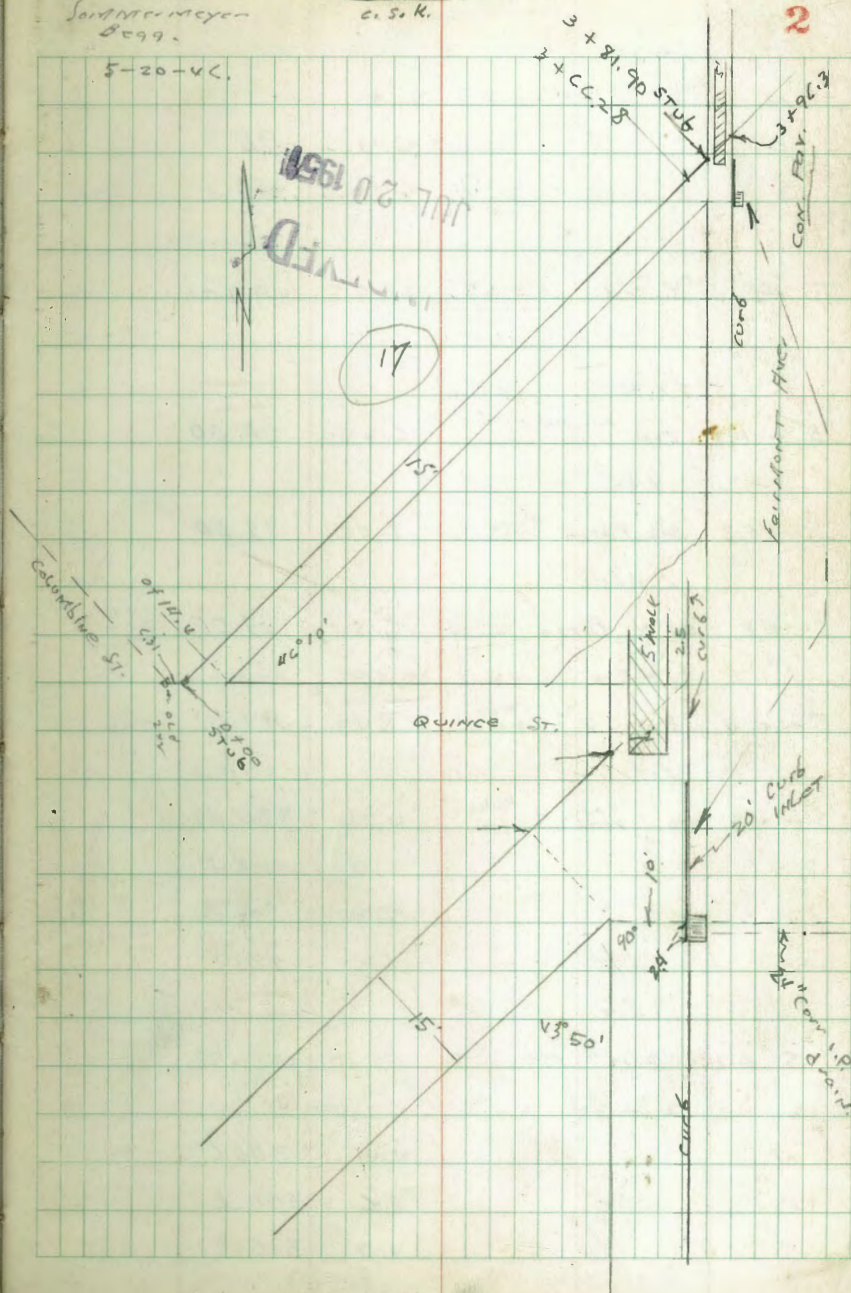
1+00

S		3.5	98.1
C		3.7	97.9
N		3.8	97.8

C. H. Moore  
S. M. Meyer  
1899.

Indexed  
C. S. K.

5-20-46.



301.56

1+30

N	2.6	99.0
C	2.7	98.9
S	2.5	99.1

T.P.	6.04	<u>305.05</u>	2.55	299.01
------	------	---------------	------	--------

1+30.5

S - 1.8	Top	N. end 4" Con. wall	6.25	98.80
---------	-----	---------------------	------	-------

1+42

S - 0.8	beg. Patio	Con. Floor	5.55	99.50
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1+55

S - 0.8	end Patio	"	5.55	99.50
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and  
beg.  
fence

1+64

S - 0.8	beg. 8" Con. wall		5.43	99.62	Top
---------	-------------------	--	------	-------	-----

1+82

S - 0.8	end wall	Con. Picket fence	4.74	300.31
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S	4.9	300.4
---	-----	-------

C	5.2	99.8
---	-----	------

N	5.0	99.0
---	-----	------

1+90

S + 1.2	8" PP	
---------	-------	--

2+30

N	4.4	300.6
---	-----	-------

C	4.6	300.4
---	-----	-------

S	4.7	300.3
---	-----	-------

305.05

3

2+70

S	5.2	99.8
C	4.8	300.2
N	4.7	300.3

3+00

N	5.6	99.4
---	-----	------

C	5.9	99.1
---	-----	------

S	5.6	99.4
---	-----	------

3+25

S	7.0	98.0
---	-----	------

C	7.3	97.7
---	-----	------

N	7.0	98.0
---	-----	------

T.P.	4.20	<u>302.91</u>	6.34	298.71
------	------	---------------	------	--------

3+44

S + 1' @ 14" PP	
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3+50

N	5.1	97.8
---	-----	------

C	4.9	98.0
---	-----	------

S	5.2	97.8
---	-----	------

3+64.5

C	M.H. P.M	5.24	97.67
---	----------	------	-------

30291

3+6628

S	5.2	97.7
C	5.4	97.5
N	5.4	97.5

3+8190 Sec. diag. on W.L. FAIRMONT

N	4.7	98.2
C	4.9	98.0
S	5.2	97.7

3+963 H.C.B. FAIRMONT

S-20	Tap creek	5.21	97.70
S-11	" "	5.13	97.78
S	" "	5.19	97.72
C	" "	5.02	97.89
N	" "	4.76	98.15
+20	" "	4.32	98.59

3+963 - gutter pan

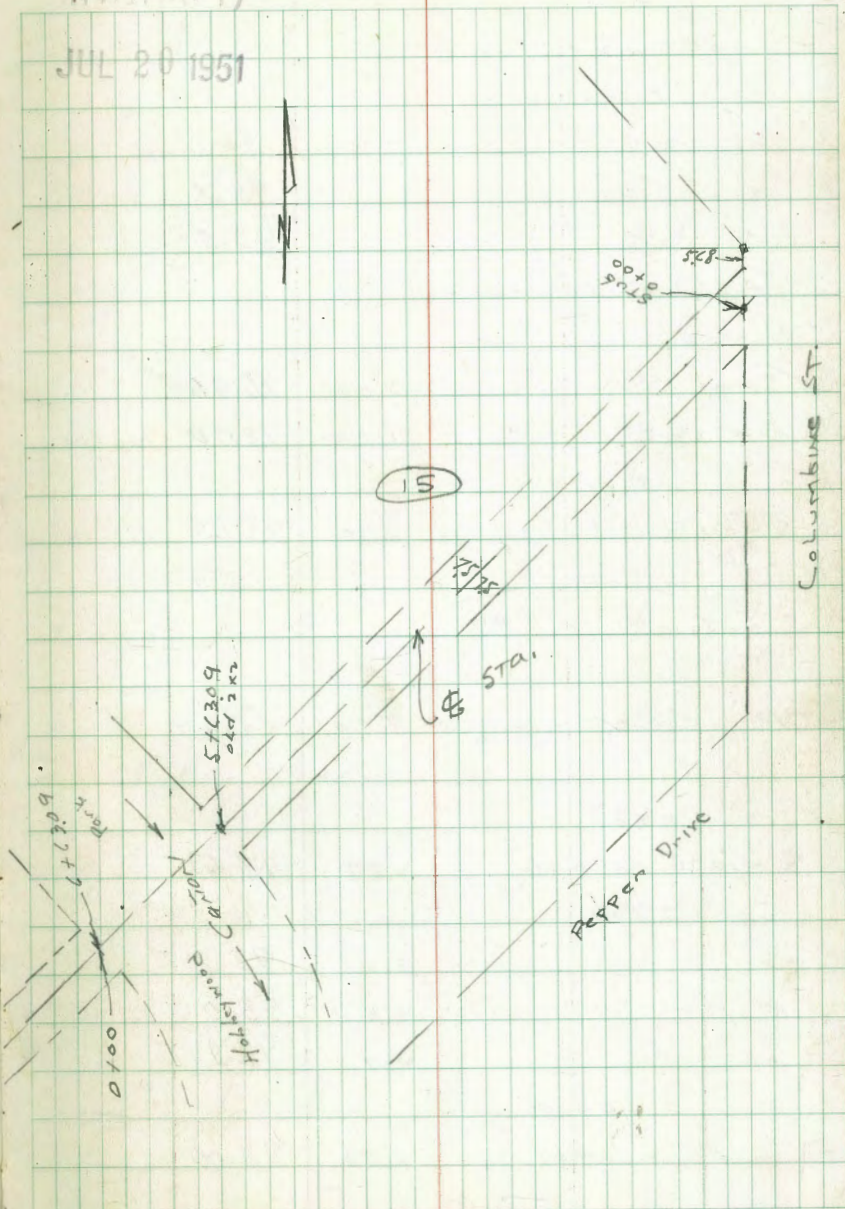
N-20		4.94	97.97
N		5.49	97.42
C		6.02	96.89
S		6.20	96.71
S+11	ON GRATING	6.17	96.74
"	FL. Box + 24" Cass. I.P. of 014	12.80	90.11
S+20		6.15	96.76

J.P. 0.88 201.25 2.14 300.77

check to orig. B.M. 6.24 295.1 295.00

INDEXED

JUL 20 1951



C 9m  
5-21-46

X sec alleys 15' wide

Bks. 15 and 14 Lexington Park.

Note! To STA, Columbine to Snowdrop

Plotted a.m.

RR 1/2" PP 5.15 300.55 295.40 Pepper & Columbine

0.100 = Alley + H.L. Columbine. Sec. diag.

N 4.7 95.8

C 5.1 95.4

S 4.8 95.7

0.107.81

S 4.8 95.7

C 5.2 95.3

N 4.7 95.8

0.124

S + 0.8 & 14" PP

0.150

N 5.5 95.0

C 5.9 94.6

S 5.8 94.7

1.100

S 6.7 93.8

C 6.7 93.8

N 6.4 94.1

OSTE  
1/2" PP  
1/2" PP

300.55

1+23

S-0.5 N.E. Cor. House

1+44

N 6.5 94.0

C 7.0 93.5

S 7.0 93.5

+0.3 N.W. Cor. House

1+48

S-0.0  $\Phi$  2.5 Con. Wall 7.07 93.48

N-13.2 E Sin. g.c. 6.65 93.90 Con. floor

1+57

S-0.4  $\Phi$  Sin. g.c. 6.70 93.85 Con. floor

1+62

S+1.5 E 1x" PP

T.P. 3.53 296.58 7.50 293.05

1+87

S-13 E do. g.c. 2.89 93.69 Con. floor

2+00

S 3.4 93.2

C 3.6 93.0

N 3.7 92.9

2+09.7

E Rim MH. 3.58 93.00

296.58

6

2+50

N 4.6 92.0

C 4.8 91.8

S 4.7 91.9

3+00

S 5.3 91.3

C 5.2 91.4

N 5.4 91.2

3+50

N 6.0 90.6

C 6.3 90.3

S 6.4 90.2

3+63

S+0.8 E 1x" PP

4+00

S 6.9 89.7

C E Rim MH. 7.07 89.51

N 7.2 89.4

4+03

S-0.0 Beg. Con. wall fence 6.60 89.98 Top

4+00

S-0.0 end fence + Beg. Shed

4+18

S-0.0 end shed + Beg. fence



296.58

4+43  
 S-0.8 end fence wall and 7.55 89.03  
 4+50  
 N 8.5 88.1  
 C 8.6 88.0  
 S 8.6 88.0

4+82  
 S+12 9 10" P.P.

T.P. 1.42 288.63 9.37 282.21

5+00  
 -5 4.4 84.2  
 S 3.1 85.5  
 C 2.3 86.3  
 N 1.9 86.7

5+15  
 -1 Beg. Top Con Wall 1.61 87.02  
 N ground 2.3 86.3  
 C 3.1 85.5  
 S 4.9 83.7  
 +5 5.8 82.8

5+39  
 -10 11.6 77.0  
 S 8.2 80.4  
 C 5.3 83.3

288.63

N 4.4 84.2  
 +1 Top end Con Wall 1.55 87.08

S+309 = E.L. Hollywood Park

N 5.9 82.7  
 C 7.3 81.3

+ 1.5 ± 10" P.P.  
 S 9.0 79.6  
 +15 12.2 76.4

5+80  
 -15 15.1 73.5  
 S 9.8 78.8  
 C 7.3 81.3  
 N 5.2 83.4

C+10  
 N 9.3 79.3  
 C 9.4 79.2  
 S 10.4 78.2  
 +15 14.0 74.6

C+25  
 -15 17.2 71.4  
 S 16.1 72.5  
 C 15.9 72.7  
 N 15.2 72.7  
 +15 14.5 74.0

28863

C#35

-15	14.1	72.5
N	16.0	72.6
C	15.8	72.8
S	16.0	72.6
+15	16.1	72.5

C#309 = W.L. Hollywood Park 20+00 alley in BLK. 14

-15	6.8	81.8
S	7.3	81.3
C	7.4	81.2
N	6.8	81.8
+15	8.1	80.5

6+14  
0+31

S#1.3 &amp; 12" P.P.

T.P. 9x6 294.08 4.01 284.62

7+19  
0+50

N	8.6	85.5
C	8.9	85.2
S	8.9	85.2

7763  
1+00

S	6.1	88.0
C	5.9	88.2

+71 Beg. wire fence

N	5.7	88.4
---	-----	------

29408

7+82

1+19

N end wire fence

7+87

1+24

N-30	E. Side gar.	4.56
	8+13	
	1+50	

N	4.1	90.0
---	-----	------

C	4.2	89.9
---	-----	------

+6.2 &amp; 12" P.P.

S	4.0	90.1
---	-----	------

8463  
2+00

S	3.4	90.7
---	-----	------

C	3.4	90.7
---	-----	------

N	3.3	90.8
---	-----	------

9+10  
2+47

N	3.8	90.3
---	-----	------

C	3.7	90.4
---	-----	------

S	3.9	90.2
---	-----	------

S+0.3	E. edge Con. walk	3.81	90.27
	9+12		
	2+47		

S	& 2' Con. walk	3.73	90.35
---	----------------	------	-------

S+5	"	3.77	90.31
-----	---	------	-------

9+16  
2+53

S-0.3	Wedge Con. walk	3.70	90.32
	9+18		
	2+53		

S-3.0	E. edge do. gar.	3.52	90.56	Cow floor
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S-1.3	" "	3.77	90.31
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ALLEY

BLK. 14

Lexington Park

Plotted a.m.

89.52 Con. floor

8

	$\frac{9+336}{2+70.5}$	$\frac{294.08}{2}$		
S - 3	Wedge d. gar	3.53	90.55	
S - 1.3	" " Cor. apron	3.83	90.25	
S		3.9	90.2	
+ 0.8	E 12" R.P.			
C		4.0	90.1	
N		3.9	90.2	

T.P. 3.08  $\frac{292.78}{2}$  4.38 289.70

$\frac{9+63}{2+00}$

N		3.2	89.6
C		3.0	89.8
S		3.1	89.7

$\frac{9+73}{2+10}$

S - 0.8 Reg. wire fence  
 $\frac{9+95.6}{2+32.5}$

N ± 3	E 2' Cor. walk	3.42	89.36
N	on "	2.95	89.83

$\frac{9+97}{2+34}$

N S.E. Cor. Bd gar. w. entrance  
 $\frac{10+13}{3+50} = E.L.$  Snowdrop St.

S 3.8 89.0

top end wire fence

C 3.9 88.9

+ 7.3 Sw. Cor. Bd gar. w. entrance

N See X sec. on Snowdrop St. 4.0 88.8

292.78

check to B.M. 3/4" pipe 3.60 289.18 289.14  
 S.E. Cor. Snowdrop 0.94  
 and Poplar

Xsec E-W 15' alley  
Blk 25 Lexington Park Plotted A.M.

SE Cor. 3/4" Pipe 2.05 291.19 289.14 Snowdrop  
Paplan

0+00 = W.L. Snowdrop St.

N 3.7 87.5

C 4.0 87.2

S Hub 4.1 87.1

0+52

-S 2.0 84.2

S 6.3 84.9

C 5.7 85.5

N 5.2 86.0

+29 SE Car House

0+62

N Line SE Car porch 4.5 86.54 floor EL.

N " on ground 5.7 85.5

C 6.0 85.2

S 6.6 84.6

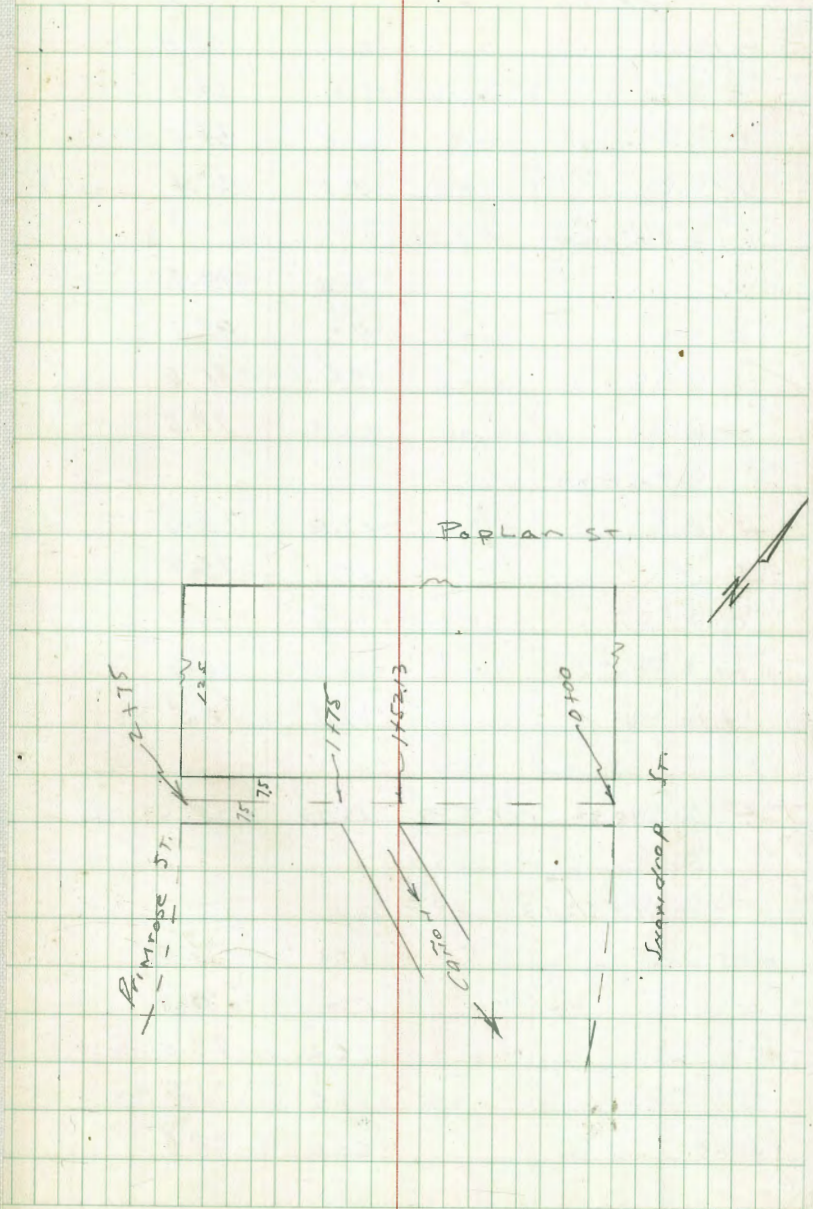
+10 8.9 82.3

0+74

N Line SW Car porch and House

0+89

S+0.8 E 14" P.P.



		<u>291.19</u>		
	1+00			
-10		10.4	80.8	
S		6.8	84.4	
C		6.6	84.6	
N		5.8	85.4	
	1+20			
N		7.0	84.2	
C		7.5	83.7	
S		9.6	81.6	
+10		12.6	78.6	
	1+40			
-15		12.4	73.8	
S		15.3	75.9	
C		15.1	76.1	
N		12.4	78.6	
+10		14.7	79.5	
T.P	10.92	<u>289.39</u>	12.72	278.47
	1+52.13			
-15		17.4	72.0	
N		17.0	72.4	
C		16.4	73.0	
S		17.5	71.9	
+15		20.6	68.8	

		<u>289.39</u>		11
	1+63			
-15		24.6	64.8	
S		20.0	69.4	
C		19.4	70.0	
N		19.2	70.2	
+15		20.0	79.4	
	1+75			
-15		20.3	69.1	
N		20.8	68.6	
C		20.4	69.0	
S		20.4	69.0	
+15		19.9	69.5	
	2+07			
-5	feet wall	8.3	81.1	
-5	top	5.0	84.4	
-1.5	" <sup>COLL</sup> <sub>WALL</sub>	4.9	84.5	
-1	feet " "	7.7	81.7	
S		7.7	81.7	
C		8.4	81.0	
N		9.0	80.4	
+15		7.7	79.5	
	2+13			
S-1	ground	6.1	83.3	
S-1.5	top end wall	4.7	84.7	

28939

	2+25			
-S	ground	5.0	84.4	
-S	Top wall concrete	3.5	85.9	
N	ground	4.9	84.5	
N	Top wall	3.4	86.0	S. end wall and beg. fence
+0.5	"	3.2	86.0	
"	ground	4.9	84.5	
C		4.1	85.3	
S		4.0	85.4	

2+32

S-3	H.E. Carr House	2.74	86.65	floor elev
"	"	3.6	85.8	ground
S		3.5	85.9	
C		3.2	86.2	
N		3.6	85.8	

2+53

S-3	H.E. Carr House			
	2+55			
N		2.9	86.5	
C		2.9	86.5	
+6.1	concrete beg. concrete wall	2.7	86.92	Top
S		2.5	86.9	

2+75 = Ely Palmrose St.

S		2.8	86.6	
+1.2	end top wall	2.83	86.56	

28939

12

C		3.4	86.0	
+7.3	end fence	3.1	86.3	
N		3.1	86.3	
T.P.	4.54	293.48	2.47	286.92
check to 0-19 B.M.				
Paplar & Swandrap	4.34	289.14		289.14

X sec 15' Alley

BLK 13 Lexington Park Plotted area

S. line = Sta. Baseline

B.M. SPIKE				Snowdrop
S.E. Cor. P.P.	10.53	290.58	280.05	Sycamore

0+00 = Ely Snowdrop

S 6.8 83.8

C 6.7 83.9

N Beg. wire fence 6.0 84.6

0+10

N 6.0 84.6

C 6.0 84.6

S 6.2 84.4

0+41

N end fence

0+47

S 4.6 86.0

C 4.3 86.3

+5.5 E 8' Con apron 4.00 86.58

+6.5 " " " 3.84 86.74

N " " " 3.84 86.74

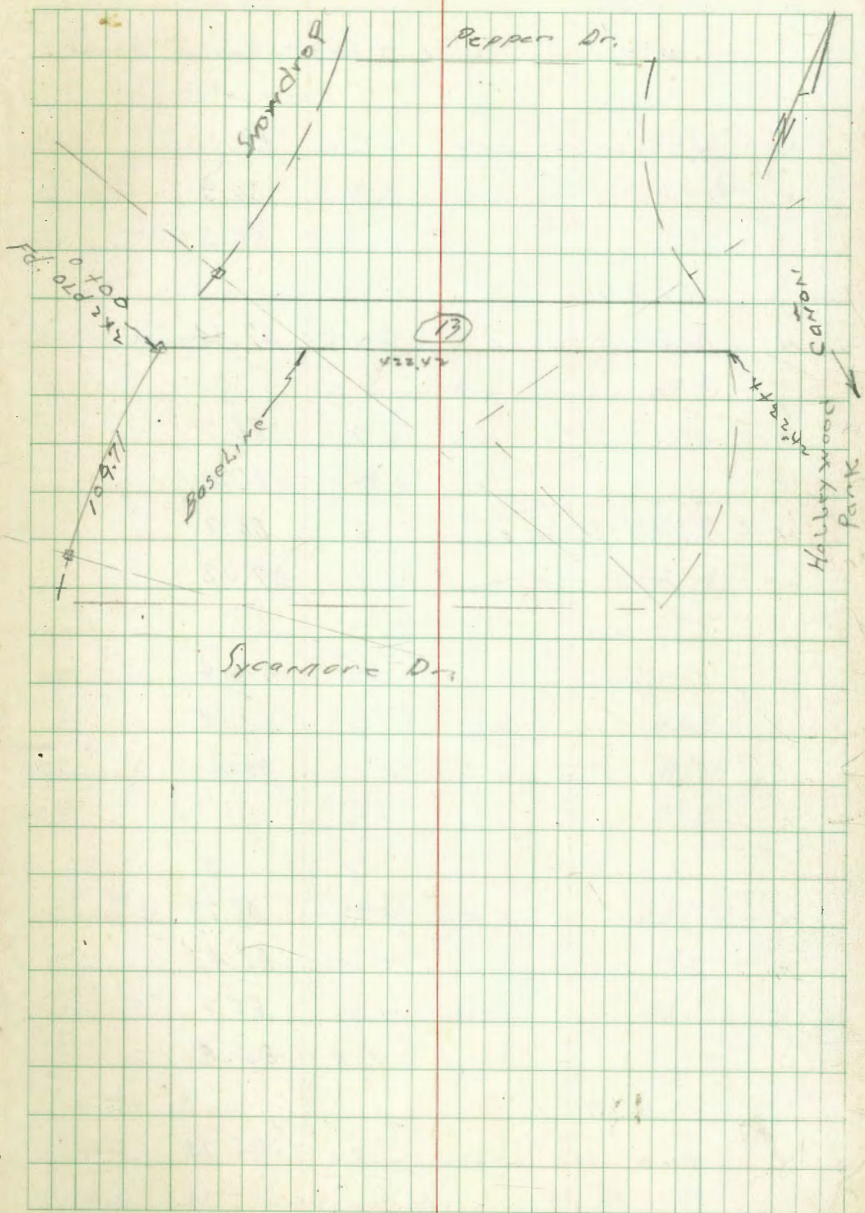
+7.2 E S.W. 900 3.84 86.74 Con floor

0+65

N Beg. wire fence

indexed  
C.S.K.

13



0+82

N end wire fence + beg. lattice fence

1+03

N \$ 3' Con. walk 3.32 87.26

C 3.7 86.9

S 4.0 86.6

1+11

N Beg. Con. slab 3.09 87.54

1+25

S 3.9 86.7

C 3.8 96.8

N End Con. slab  
End lattice fence  
& SW Cor. House 3.7 86.9

N Top. Con. Fd. 3.1 87.42

1+40

N SE Cor. House 3.44 87.14 Con. Fd.

" Beg. Con. slab 3.44 87.14 Con.

" " Bd. fence 4.0 86.6 ground

1+56

N-V Con. walk slab 3.85 86.73 3' gate

N " " " 4.15 86.43

C 4.5 86.1

S 4.8 85.8

1+69

N end <sup>Top</sup> Con. wall 3.84 86.74

N " Bd fence + Beg. wire fence

1+85

S + 1.5 E 14" PP.

2+00

S 6.4 84.2

C 5.6 85.0

N 5.3 85.3

2+26

N end wire fence 6.0 84.6

C 6.6 84.0

S 7.0 83.6

2+50

S 7.1 83.5

C 7.0 83.6

N 6.7 83.9

2+70

N 6.8 83.8

C 6.9 83.7

S 7.2 83.4

3+00

S 6.7 83.9

C 6.5 84.1

N 6.5 84.1

3+07

S + 1.5 E 14" PP.

3+07.5

N + 1.0 Beg. Lath fence



3 + 25

N	5.8	84.8
C	5.9	84.7
S	6.1	84.5

3 + 50

S	5.2	85.4
C	5.3	85.3
N	5.4	85.2

3 + 97

N	6.5	84.1
---	-----	------

+7 end fence

C	6.1	84.5
S	6.1	84.5

4 + 22.42 w/L Hollywood Park

S	Sec. at 90°	7.8	82.8
C		8.3	82.3
N		9.0	81.6

Xsec ALLEY 15' wide  
Blk. 10 Lexington Park

Plotted A.M.

Nly Line alley = Sta. B.L.

RR SPIKE P.P. New Can.	1.06	<u>296.46</u>	295.40	Pepper Columbine
---------------------------	------	---------------	--------	---------------------

0+00 = Nly Columbine ST.

N		5.1	91.4
C	on arc	5.8	90.7
S +1	89.4 <sup>wire</sup> distance	6.0	90.5
	0+13 Sec 90°		
S		6.0	90.5
C		4.0	90.5
N		5.6	90.9

0+23

S +0.9 E 1x" PP

0+50

N		7.3	89.2
C		7.4	89.1
S		7.3	89.2

0+73

S		8.2	88.3
C		8.4	88.1
N		8.5	88.0

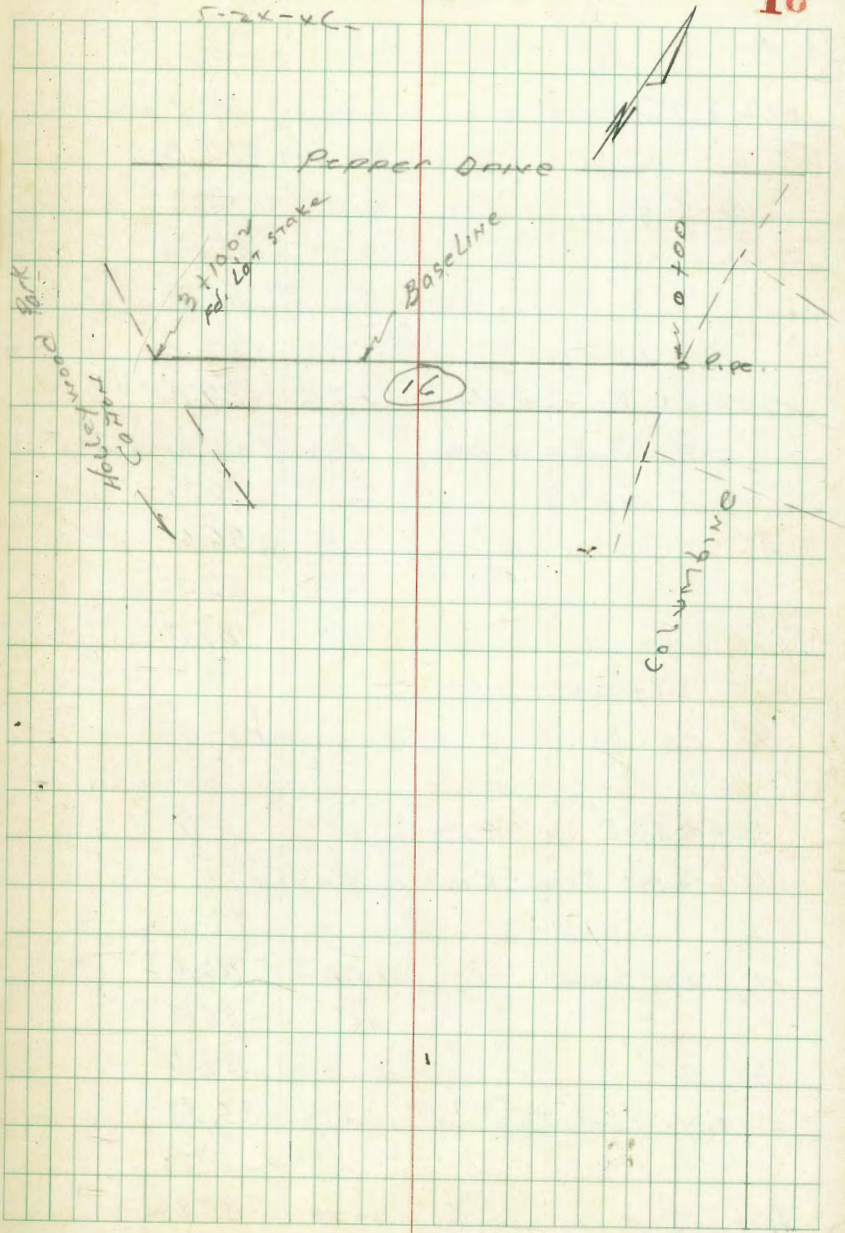
N +1 <sup>wire</sup> Beatenie and  
Cobble wall

	7.2	89.3
--	-----	------

Top

C. Moore  
Somerset Ave  
5-24-46

Indexed  
C.S.K.



296.46

	1+00		
N-0.7	Break Top	7.7	88.8
"	Cobble wall	8.7	87.8
N		9.2	87.3
C		9.3	87.2
S		9.4	87.1

1+04

N-0.7	Top end wall	8.7	87.8
"	S.E. Cor. gar North entrance		

1+15

S		9.9	86.6
C		9.8	86.7
N		9.5	87.0

1+21.4

N-0.9 S.W. Cor. 460 x 400

1+23

S+0.8 E 12" P.P.

N-0.9 Beg. Lat 4 fence

1+25

N		10.1	86.4
C		10.2	86.3
S		10.6	85.9

S-1.3 Beg. <sup>chicken</sup> con. walk 10.43 85.83

1+51

S-1.5 <sup>chicken</sup> A in walk 10.73 85.73

296.46

17

Don't try to match  
these chicken walks

	1+53.5		
S-4.0	A in <sup>chicken</sup> walk	10.9	85.6
	1+55		
N-0.7	Beg 6" wire	9.55	86.91 Top
	1+70		
S-3.6	end <sup>chicken</sup> con. walk	11.05	85.41
	1+73		
N-1.2	end fence		
N-0.3	" 6" wall	9.92	86.54 Top
S-1.3	end fence		
	1+80		

S 11.4 85.3

C 10.9 85.6

N 10.9 85.6

2+00

N 11.0 85.5

C 11.3 85.2

S 11.7 84.8

T.P. 1.96 287.80 10.52 285.84

2+22.5

N #1 Beg. wire fence

2+24

S/L E 10" P.P.

287.80

	2+32		
S		3.0	84.8
±4'	20" di. pepper tree		
C		2.7	85.1
N		2.4	85.4
	2+42		
N	-0.4 E and S edge 3x4 wood porch	0.6	87.2
"	ground	2.5	85.3
	2+74		
N		3.5	84.3
±1.4	end wire fence		
C		4.1	83.7
S		4.8	83.0
±5		5.4	82.4
	2+90		
-10		11.6	76.2
S		8.7	79.1
C		7.7	80.1
N		5.6	82.2
	3+10.5 = Ely Hollywood Park Sec. at 90°		
N		12.3	75.5
C		13.7	74.1
S		15.3	72.6
+10		18.6	69.2
	±60 about center of canyon and 25 ± lower		

287.80

18

T.P. 10.53 296.94 2.29 285.51  
 check to 0.19 B.M. 0.64 295.40 295.40

x sec of 15' alley

BLK 11 Lexington Park

BM. 2" pipe  
SE corner 3.70 292.84 289.14 Poplar  
Snowdrop

T.P. 4.14 290.34 C.L.X 286.70

SW corner  
SET SPIKE B.M. P.P. Poplar + Tuberosa 6.32 284.02 ✓

0+00 WLY Tuberosa ST

N 3.9 86.4

C 4.3 86.0

S 4.5 85.8

0+15

S 4.9 85.4

C 5.2 85.1

N 4.6 85.7

0+30

N 4.4 85.9

C 4.3 86.0

S 4.7 85.6

0+50

S 4.2 86.1

C 4.3 86.0

N 4.4 85.9

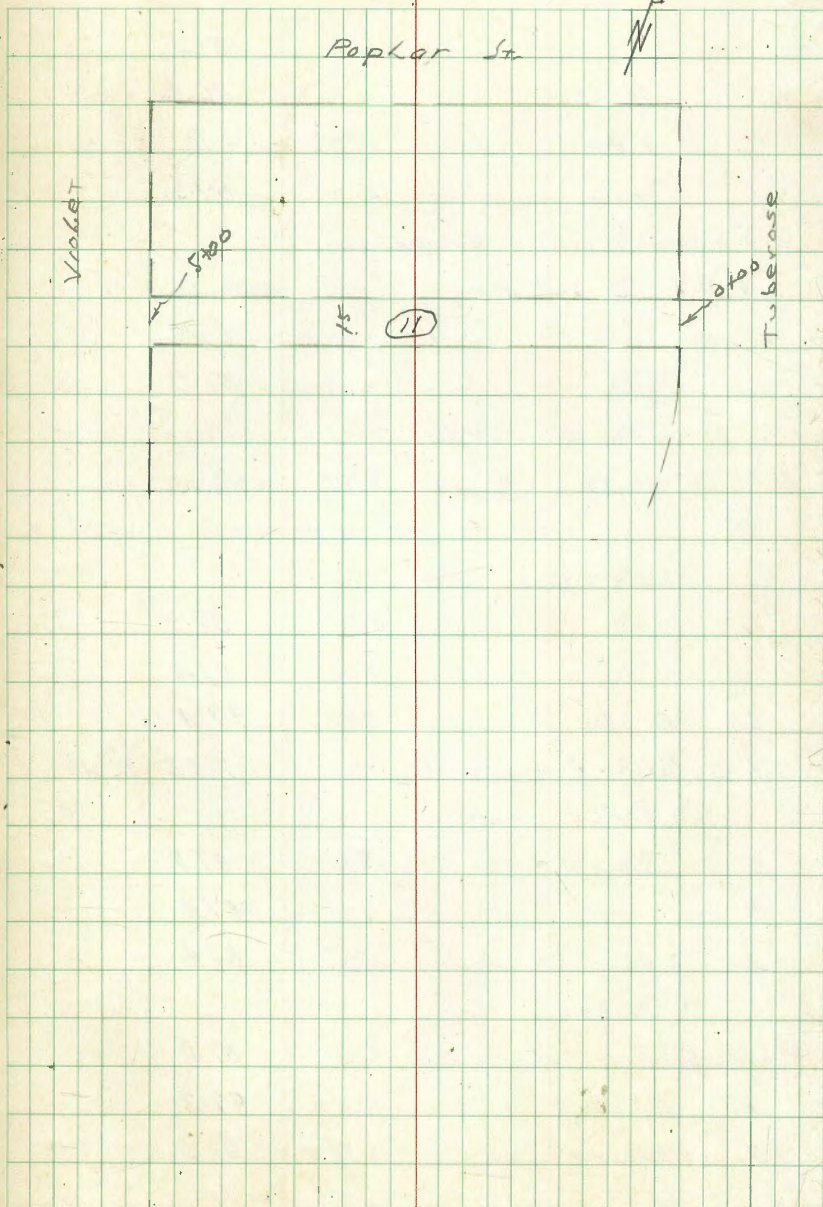
0+75

N 3.5 86.8

Indexed  
C.S.K.

19

Poplar St



C			3.2	86.7	
S			3.8	86.5	
	1+01				
S			3.0	87.3	
S+0.7	beg. Bd. fence				
S+0.8	E 12" P.P.				
C			3.1	87.2	
N			3.3	87.0	
T.P.	5.35	<u>292.64</u>	3.05	287.29	
	1+25				
N			5.3	87.3	
C			5.0	87.6	
S	fence		5.2	87.4	
+4	E 2'-8" doorsill		5.01	87.63	to House
	1+60				
S	fence		5.2	87.2	
C			5.2	87.4	
N			5.2	87.4	
	2+00				
N			5.6	87.0	
C			5.3	87.3	
S	fence		5.1	87.5	

			2+20		
S	end Bd. fence	beg. wire fence	5.7	86.9	
	+0.8	E 12" P.P.			
C			6.1	86.5	
N			5.6	87.0	
			2+60		
N			6.1	86.5	
C			6.8	85.8	
S			6.4	86.2	
			3+00		
	S-end wire fence				
S			7.0	85.6	
C			7.2	85.4	
N			7.0	85.6	
			3+20		
N			6.8	85.8	
C			7.2	85.4	
S			7.3	85.3	
			3+40		
S			6.3	86.3	
C			6.3	86.3	
N			6.4	86.2	
T.P.	3.85	<u>289.81</u>	6.73	286.41	

	3+50		
N-0.7	Req. wire fence		
	3+75		
N		4.6	85.3
C		4.8	85.1
S		4.9	85.0
	3+80		
S	Req. Picket fence		
	3+86		
S	end fence		
S+0.3	N.E. Car house		
	3+99		
S+2	apricot tree		
	4+00		
S+0.3	House	4.9	85.0
C		5.1	84.8
N+0.7	end wire fence	5.0	84.9
	4+05.7		
S+0.3	N.W. Car house		
	4+14		
S+0.5	E 10' Con. apron	5.31	84.55
S-2.4	" Sin. gar <sup>CON.</sup> floor	5.5	84.71
	4+20		
S-0.7	Req. Bd fence		

	4+27		
S-0.7	end Bd fence		
S-0.7	N.E. Car. Car. S. entrance		
	4+35		
S-0.7	N.W. Car. gar.		
S-0.7	Req. Bd fence		
	4+36		
S+1	E 12' P.P.		
	4+40		
N-4	E Sin. gar.	4.0	85.26
N		4.8	85.1
C		5.2	84.7
S		5.0	84.9
	4+50		
N-0.5	S.E. Car. Shed Garage		
	4+68		
N-0.5	sw Car. shed gar.		
	4+73		
S-0.7	end fence		
S		5.5	84.4
C		5.5	84.4
N		5.1	84.8
	5+00 = E.L. Violet St.		
N		5.8	84.1
C		6.3	83.6
S		6.3	83.6
	1628-49		
	check to SW Top F.H. Poplar + Violet	7.3	286.43
			286.40 0.03

x sec. Tuberosse St. <sup>50' wide</sup>  
 10' curbs  
 Poplar St. Sly to  
 Printrose Lane. Plotted C.M.

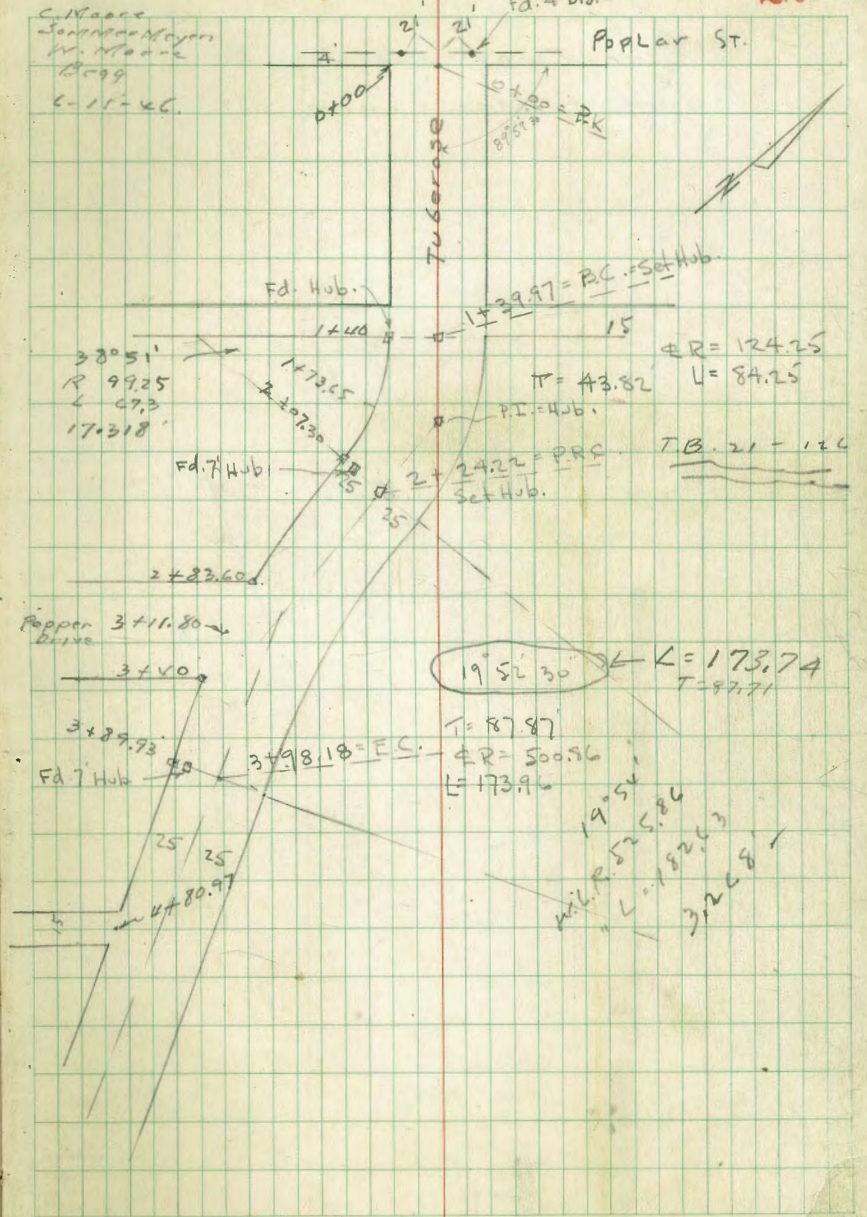
Note 1 Station on Widening of St.

P. 19  
 Spike  
 SW.P.P. C.37 290.39 284.02 Pepper & Tuberosse

0+00 = Sly of Poplar St.

W.L.	2.5	86.9
w c6	3.4	87.0
+4	3.9	86.5
C	3.9	86.5
EC6	4.1	86.3
E.L	3.8	86.6
0+40		
E	4.1	86.3
c6	4.0	86.4
C	4.0	86.4
+11	4.6	85.8
c6	3.7	86.7
w	3.7	86.7
0+72		
w	3.9	86.5
c6	3.8	86.6
+4	4.9	85.5

Contd. P. 24



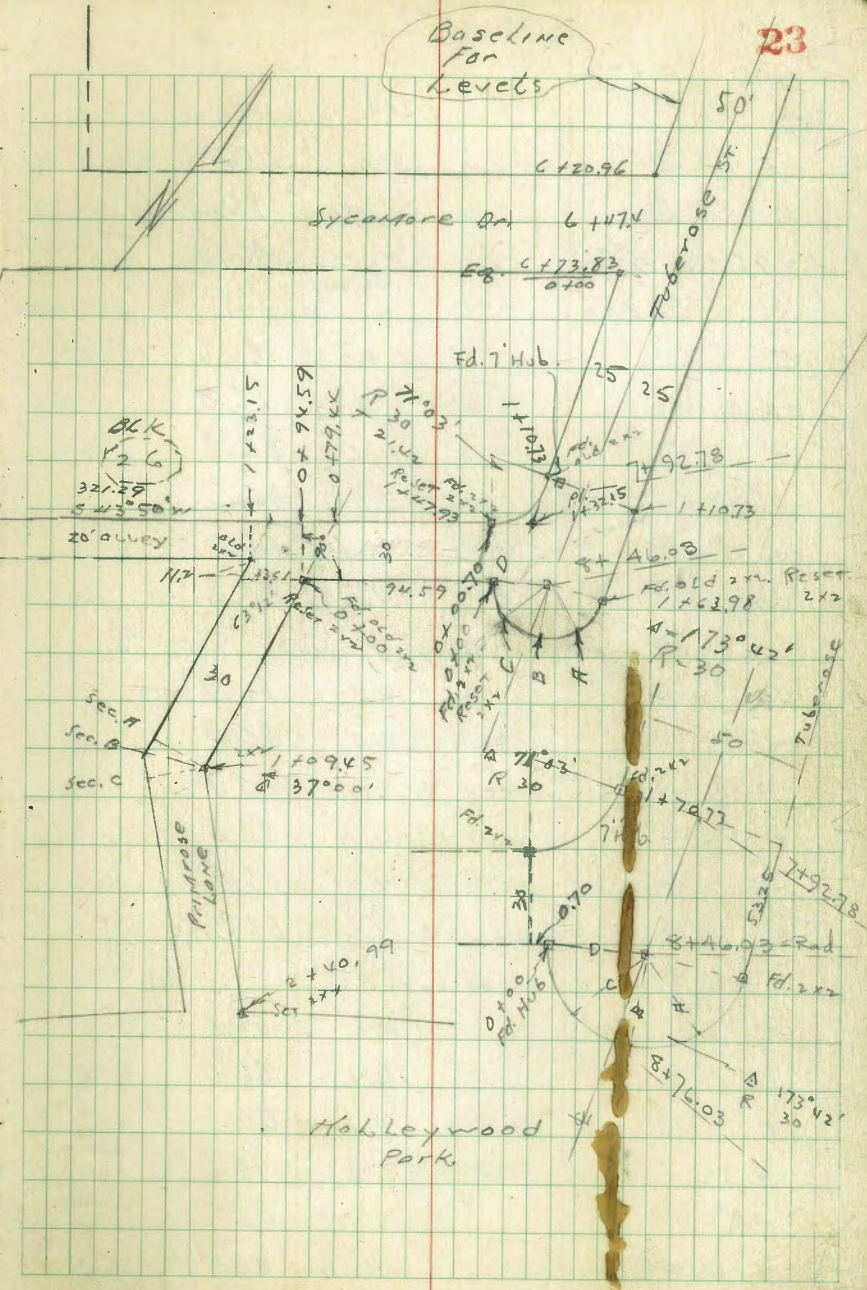
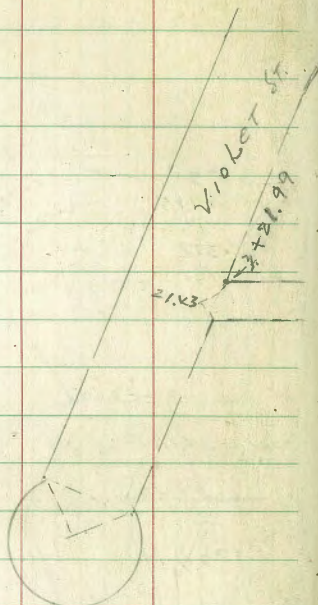


1/2 sec Tuberose St  
and Primrose Lane

163.98  
10.73  

---

53.25



D+72

C		4.1	86.3
CB		3.9	86.5
E		3.9	86.5
+29.5	do. Cor. FL.	4.2	86.13
	1+00		
E		3.8	86.6
CB		4.1	86.3
C		4.6	85.8
+11		5.1	85.3
CB		4.3	86.1
W		4.2	86.2
	1+25 N. Alley		
W		4.1	86.3
CB		4.5	85.9
+4		5.3	85.1
C		4.9	85.5
CB		4.4	86.0
E		4.2	86.2
	1+40 S. L. alley = B.C.		
E		4.0	86.4
CB		4.4	86.0
C		4.8	85.6
+12		5.6	84.8
CB		4.7	85.7
W		4.8	85.6

	1+43		
E +0.5	E 7' Cor. drive	4.09	86.30
E -22.5	" Sen. 900. Cor	3.77	86.62
	1+56.82 = 1+65.30		
	1461.06		
W		5.1	85.3
+5		5.1	85.3
+7		6.3	84.1
CB		6.1	84.3
C		4.6	85.8
+10		4.8	85.6
CB		4.3	86.1
+6	end 3' Cor. walk	4.10	86.29
E	on walk	4.10	86.29
	1+73.55 = 1+90.60		
E		4.5	85.9
CB		4.4	86.0
+4		5.7	84.7
C		5.4	85.0
CB		6.2	84.2
+5		6.5	83.9
+7		5.2	85.2
W		5.2	85.2
	1+90.47 = 2+15.90		
W		5.7	84.7
+3		5.7	84.7

290.39

W + 5	7.0	83.4
cb	6.9	83.5
C	6.0	84.4
+ 11	6.1	84.3
cb	5.2	85.2
E	5.0	85.4

1+98

E - 11.2 End <sup>8.3</sup> Drive 5.9 84.5

2+07.3 = P.R.C. = 2+41.20

E 3/4" pipe 2+24.24	6.0	84.4
cb	6.0	84.4
+ 5	6.4	84.0
C	6.5	83.9
cb	7.0	83.4
+ 3	7.1	83.3
+ 5	6.3	84.1
W	6.3	84.1

2+37 = 2+68.62

W	2+53.10	7.0	83.4
cb		7.3	83.1
C		6.7	83.7
+ 7		6.5	83.9
+ 10		7.4	83.0
cb		7.7	82.7
E		8.4	82.0
+ 5		8.4	82.0

290.39

Tubercose

25

2+60 = 2+89.43

- 12	2+15.01	16.0	74.4
E		17.1	73.3
cb		13.0	77.4
+ 9		7.0	83.4
C		7.1	83.3
cb		7.5	82.9
+ 2		7.5	82.9
+ 3		7.2	83.2
W		7.1	83.3

2+71 = 2+99.38

W	2+85.28	7.0	83.4
+ 7		7.2	83.2
+ 8		7.6	82.8
cb		7.5	82.8
C		7.2	83.2
+ 6		7.1	83.3
cb		12.8	77.6
E		19.4	71.0
+ 10		23.2	67.2
+ 20		19.3	71.1

2+83.6 m.c. Pepper Dr. = 3+10.78

- 25	2+97.48	23.1	67.3
- 15		25.3	65.1
E		21.1	69.3
cb		12.5	77.9

290.39

cb + 7	25.52	7.7	82.7
C		7.3	83.1
cb		7.4	82.8
W		7.0	83.4

3 + 14.8 E Pepper = 3 + 36.30

W	3 + 24.34	6.9	83.5
---	-----------	-----	------

cb		7.3	83.1
----	--	-----	------

C		7.8	82.6
---	--	-----	------

+ 8	25.52	7.9	82.5
-----	-------	-----	------

cb		11.2	79.2
----	--	------	------

F		13.2	76.5
---	--	------	------

+ 15		18.5	71.9
------	--	------	------

3 + 40 S.L. Pepper = 3 + 61.82

- 10	3 + 51.20	13.8	76.6
------	-----------	------	------

E		11.4	79.0
---	--	------	------

cb		9.9	80.5
----	--	-----	------

+ 4	22.67	8.2	82.2
-----	-------	-----	------

C		7.8	82.6
---	--	-----	------

+ 13		7.8	82.6
------	--	-----	------

cb		7.1	83.3
----	--	-----	------

W		6.5	83.9
---	--	-----	------

3 + 65 = 3 + 84.44

W	3 + 75.01	6.3	84.1
---	-----------	-----	------

cb		6.8	83.6
----	--	-----	------

+ 2		7.9	82.5
-----	--	-----	------

290.39

Tuberose 26

C		7.8	82.6
+ 10	22.56	8.0	81.8
cb		9.4	81.0
F		10.6	79.8
+ 10		12.7	77.7

3 + 89.93 EC = 4 + 07.00

- 10	3 + 98.75	11.2	79.2
------	-----------	------	------

F		10.1	80.3
---	--	------	------

cb		8.8	81.6
----	--	-----	------

C		7.8	82.6
---	--	-----	------

+ 13		7.9	82.5
------	--	-----	------

cb		6.5	83.9
----	--	-----	------

W		6.1	84.3
---	--	-----	------

T.P.	4.64	287.17	7.91	282.48
------	------	--------	------	--------

4 + 0.65

E - 5.5 E Sugar	5.3	81.8	Wood FL
-----------------	-----	------	---------

E diar drive	5.3	81.8	
--------------	-----	------	--

4 + 13 = 4 + 30.07

W	4 + 21.82	2.7	84.4
---	-----------	-----	------

cb		3.2	83.9
----	--	-----	------

+ 3		4.8	82.3
-----	--	-----	------

C		4.6	82.5
---	--	-----	------

cb		5.2	81.9
----	--	-----	------

287.14

E C6	+ 2.5 = N. end + 3' W. edge of walk	5.05	82.07
E	on walk to house	5.8	82.04
+ 5.3	" " " "	5.0	82.02
	4 + 4.3 = 4 + 60.07		
E	4 + 51.82	5.6	81.5
+ 7.7	S. end and W. edge of 3' concrete	5.07	82.05
C6		5.1	82.0
C		4.8	82.3
+ 1.2		4.9	82.2
C6		3.2	83.9
W		2.8	84.3
	4 + 80.97 = 4 + 98.04		
W	4 + 89.79	3.1	84.0
C6		4.2	82.9
+ 4		4.8	82.3
C		5.0	82.1
C6		5.5	81.6
E		6.5	80.6
+ 5		7.1	80.0
	4 + 94 = 5 + 11.07 = 5 + 102.82		
E - 15.7	& S. end 99' wood FL.	5.7	81.4
E - 1	& do. 2' concrete	6.5	81.07
E		6.1	81.0
C6		5.9	81.2
C		5.2	81.9

287.12

27

C	+ 1.7	5.2	81.9
C6		3.8	83.3
W		3.4	83.7
	5 + 0.9 = 5 + 26.07 = 5 + 17.82		
E + 2	& 2' concrete walk	4.36	80.76
	5 + 26.4		5 + 35.22
W - 0.5	& 2.5 concrete walk	3.97	83.15
W		4.0	83.1
C6		4.6	82.5
+ 3		5.6	81.5
C		5.0	81.5
+ 1.0		6.1	81.0
C6		6.8	80.3
E		8.0	79.1
+ 5		8.5	78.6
	5 + 50 = 5 + 62.07 = 5 + 58.82		
- 5		8.7	78.4
E		8.4	78.7
C6		7.3	79.8
+ 4		6.6	80.5
C		6.0	81.1
+ 1.2		6.0	81.1
C6		5.1	82.0
W		4.5	82.6

287.12

Tuberose

$$C+00 = 6+17.07 = 6+08.82$$

W	5.6	81.5
cb	5.9	81.2
+3	6.8	80.3
C	6.8	80.3
+11	7.3	79.8
cb	7.2	79.2
E	8.2	78.3
L7	9.3	77.8

$$C+20.96 N.L. Sycamore Dr. = 6+38.03$$

-7	6+29.78	10x	76.7
E		9.7	77.4
cb		8.5	78.6
+5		7.6	79.5
C		7.0	80.1
+13		7.1	80.0
cb		6.3	80.8
W		5.9	81.2

$$C+474 E Sycamore 6+64.47$$

W	6+56.22	7.0	80.1
cb		7.0	80.1
C		7.6	79.5
+11		8.4	78.7
cb		9.1	78.0
E		9.9	77.2
+10		10.8	76.3

287.12

28

$$\begin{array}{r} C+73.81 = 6+90.90 \\ \text{S.L. Sycamore Dr.} \\ \hline 0+00 = 6+82.65 \end{array}$$

E-10	11.1	76.0
E	10.7	76.9
cb	9.5	77.6
+4	9.1	78.0
C	8.3	78.8
+13	8.7	78.9
cb	7.5	79.6
W	7.4	79.7

$$\begin{array}{r} \text{Gully} \\ \text{T.P. spike} \\ \text{SW P.P. } 4.8 \end{array} \quad \begin{array}{r} 284.65 \\ 7.5 \end{array} \quad \begin{array}{r} 279.97 \\ \text{Tuberose} \\ \text{Sycamore} \end{array}$$

$$\begin{array}{r} \text{check to SE spike P.P.} \\ \text{Snowdrop + Sycamore } 4.58 \end{array} \quad \begin{array}{r} 280.07 \\ 280.5 \\ \hline 0.02 \end{array}$$

$$0+40 \quad 7+13.85 = 7+30.90$$

W	7+22.65	5x	79.2
cb		5.6	79.0
+4		6.7	77.9
C		6.5	78.1
cb		7.2	77.4
E		8.2	76.4
+10		9.1	75.5
	0+80	7+53.03 = 7+70.90	
E-10	7+62.65	9.0	75.0

0 + 80

E		8.4	76.0
c6		8.1	76.5
C		7.3	77.3
+11		7.5	77.1
c6		6.4	78.2
W		6.2	78.4
T.P.	2.49	<u>284.38</u>	6.76 277.89

$$L+10.73 \quad 7+84.56 = 8+01.63 = 7+93.38$$

W	B.C. W.L. ST. Hub	<sup>old</sup> 2.5	77.9
c6		2.8	77.6
+4		3.9	76.5
c		3.6	76.8
c6		4.3	76.1
E		5.0	75.4
+0.9	s.l. 3' Com walk	4.93	75.45
+10	" " " "	5.67	74.71

$$L+32.15 \quad 8+05.98 = 8+23.05 = 8+14.80$$

-10		6.9	73.5
E		5.5	74.9
c6		4.9	75.5
C		4.2	76.1
+14		4.5	75.8
+17		3.0	77.4

c6		3.0	77.4
C + 2.5 P.L.		3.1	77.3
W C.T.C. Curve		2.9	77.4
			$1+63.98 = 8C \text{ on } E.L. \quad 8+37.81 = 8+54.89 =$
30' R		5.2	75.2 8+46.63
R + 20		6.8	73.6
R + 30 = E.L. B.C. Hub	<sup>old</sup>	7.5	72.8
R + 40 = 10' out		8.9	71.5

Sec. A. Curve in 4 equal parts

30' R		5.2	75.2
R + 20		7.1	73.3
R + 30 E.L.		8.1	72.3
R + 40 10' out		9.4	71.0

Sec. B

30' R		5.2	75.2
R + 20		6.5	73.9
R + 30		7.5	72.9
R + 40		8.5	71.9

Sec. C

30' R		5.2	75.2
R + 20		6.0	74.4
R + 30		6.3	74.1
R + 40 10' out		6.8	73.6

280.38

Sec. D. = 0100 for alley &amp; sec

30' R	5.7	75.2
R+20	5.0	75.4
R+30 = E.C. <sup>Fd. old Hub</sup>	5.0	75.4
0100 for alley		

indexed  
C.S.M.

30

1/2 sec of 30' to 20' alley

IN BLK. 2 C. LEXINGTON PARK

280.38

Sketch p. 23

0100 = F.C. on S.L. 30' alley

S-10	5.7	274.68
S Fd. old Hub	5.0	275.38
C	4.2	276.18
N	3.4	277.00

0100.70

N Fd. old Hub	3.4	277.00
C	4.2	266.18
S	5.0	275.38
+10	5.7	274.68

0128

-10	6.4	274.00
S	5.8	274.58
C	5.0	275.38
N	2.8	276.58

0154

N	5.1	275.28
C	6.1	274.28
S ground	6.7	273.68
#04 N.E. Cor. XIXIX wood cabin	6.55	273.83
+10 ground	7.0	273.38 AL. EL.



280.38

0+65

S	against CABIN	7.2	273.06
C		7.2	273.18
N		6.3	274.08

T.P. Rock <sup>ON</sup> 6.33 276.87 9.84 270.54 ✓

0+79.44 Sec at 90°

N-10		2.5	274.37
N	on stub	6.25	270.62
+10		6.4	270.47
C	E 30' alley	5.9	271.06
S		5.7	271.17
+10		6.4	270.47

0+94.59 to 0+179.44 = line of Primrose Lane produced NLY

S	on Hub Cabin	11.66	265.21 ✓
C	E 30' alley	9.5	267.37
+9		9.0	267.87
N	on stub	6.25	270.62

0+94.59 Sec at 90°

N-10		3.8	273.07
N		8.7	268.17
+8		12.11	264.77
C	E 30' alley	13.11	263.77
S	on Hub on	11.66	265.21 ✓

E-L Primrose Lane  
and S.E. of 30' alley.

276.87

alley Blk 2C  
Lex. PK.

31

1+07

S.L.	30' alley	19.8	257.07
C	" "	13.8	263.07
N	" "	7.1	269.77
+10		5.0	271.87

1+23.15 = Beg. of 20' wide alley

N-10		5.1	271.77
N		7.5	269.37
C		10.0	266.87
S	Ed. old Hub	13.4	263.47

1+52

-10		15.1	261.77
S		12.0	264.87
C		9.9	267.00
N		7.5	269.37
+10		6.1	270.77

1+82

-10		6.3	270.57
N		7.5	269.37
C		9.1	267.77
S		10.8	266.07
+10		13.8	263.07

2+13

-10		14.2	263.67
S		10.9	266.00

276.87

C		9.1	267.77
N		7.1	269.77
+10		5.8	271.07
	2+30		
-10		5.6	271.27
N		7.3	269.57
C		9.3	267.57
S		11.8	265.07
+10		15.2	261.67
	2+40		
-10		18.2	258.67
S		14.2	262.67
C		9.8	267.07
N		6.8	270.07
+10		5.7	271.17
	2+53		
-10		5.4	271.47
N		6.4	270.47
C		9.5	267.37
S		13.1	263.77
+10		14.6	262.27
	2+73		
-10		7.4	269.47
S		6.7	270.17
C		6.0	270.87
N		5.4	271.47

alley Blk 2C  
Lexington Park

32

276.87

N +10		4.5	272.37
	3+00		
N		4.0	272.87
C		4.6	272.27
S		5.3	271.57
	3+21.99 = on Elk VIOLET ST		
S		4.5	272.37
C		4.2	272.67
N		3.9	273.00

Xsec of Prismatic lens, 30' wide

Com  
T.P. Hub 0.74 265.95 265.21 P. 31

0 + 00 = S.L. of 30' alley, sec. diag.

E on Hub 0.74 265.21  
C 9.3 257.65  
W 6.0 259.95  
+10 5.2 260.75

0 + 15.15 Sec. at 90°

W 6.0 259.95  
+11 12.1 253.85  
C 9.0 256.95  
E 3.8 262.15  
+10 +1.0 266.95

0 + 35

-10 3.4 262.55  
E 6.2 259.75  
+6 8.5 257.45  
C 14.1 251.85  
+5 12.1 248.85  
W 15.0 250.95  
+10 11.6 254.35

T.P. 1.18 258.89 8.24 257.71  
on Rock

258.89

Indexed  
c.s.k.

33

0 + 00

-10 1.3 257.59  
E 6.1 252.75  
C 12.5 246.39  
+10 18.2 240.69  
W 16.3 242.59  
+15 5.2 253.69

0 + 25

-15 9.0 249.89  
W 18.2 240.69  
+7 22.2 236.69  
C 18.7 240.19  
E 10.4 248.49  
+6 4.6 254.29  
+12 2.0 256.89

T.P. 0.62 247.23 12.28 246.61

0 + 95

-15 +4.7 251.93  
E 3.7 242.53  
C 12.5 239.73  
+6 15.0 232.23  
W 11.5 235.73  
+15 10.7 236.53

247.23

/ +09.45 Sec. A

-20	15.3	231.93
W	16.4	230.83
+12	17.1	230.13
C	14.7	232.53
E	Hub A 37°LT. Cx8	240.75

/ +09.45 Sec. B

SPLIT

-15	+0.9	248.13
F	Cx8	240.75
C	15.9	231.33
LC	20.8	226.43
+12	20.4	226.83
W	19.4	227.83
+15	11.3	235.93

/ +09.45 Sec. C

-15	12.1	235.13
W	19.4	227.83
LC	21.5	225.73
C	15.2	232.03
E	6x8	240.75

T.P. 0.53 = 239.74 8.02 239.21

/ +50

-10	+0.5	240.24
E	K.C	235.14

239.74

Primrose Lane 34

C	12.7	227.04
+13	18.4	221.34
W	18.4	221.34
+15	8.8	230.94
	1+9K	

-15	13.4	226.34
W	21.5	218.24
+2	22.1	217.64
C	14.6	225.14
F	9.0	230.74
+15	4.5	235.24

T.P. 1.45 228.57 12.67 227.12

2425

-15	3.5	225.67
F	8.0	220.57
C	11.9	216.67
+10	10.1	212.47
W	12.8	215.77
+15	4.6	223.97

2 + 40.99 = 44.4 Holleywood Park

-15	2.0	226.56
W	8.8	219.77
C	10.0	212.57

228.57

C + 2			17.6	211.00	
C + 7			12.7	210.87	
E			14.3	214.27	
+ 15			9.2	219.37	
T.P.	12.50	239.62	1.45	227.12	
T.P.	12.30	251.39	0.59	239.03	
T.P.	12.66	263.23	0.82	250.57	
T.P.	13.12	275.62	0.73	262.50	
T.P.	7.12	281.95	0.83	274.81	
check to	Spr spike P.P. Tuberosc + Sparrow		1.98	279.97	279.97 ✓

X sec 15' Alley

Blk. 12 Lexington Park

Plotted Q.M

C.M.  
C.S.  
K.M.  
E.B.  
6-19-40

S.E. Cor.  
TOP E.H.  
P. 41      0.78      287.18      286.40      Poplar  
Violet

T.P      5.27      284.89      7.56      279.67

0 ± 00 Fly Violet St

N      5.0      79.9

C      5.3      79.6

S      5.1      79.8

0 ± 00.5

N - 0.8 TOP Cor. 5" wall      4.43      80.46

0 ± 12.5

N - 0.4 end Top wall 5"      4.36      80.53

0 ± 25

S      5.0      79.9

C      4.9      80.0

N      4.8      80.1

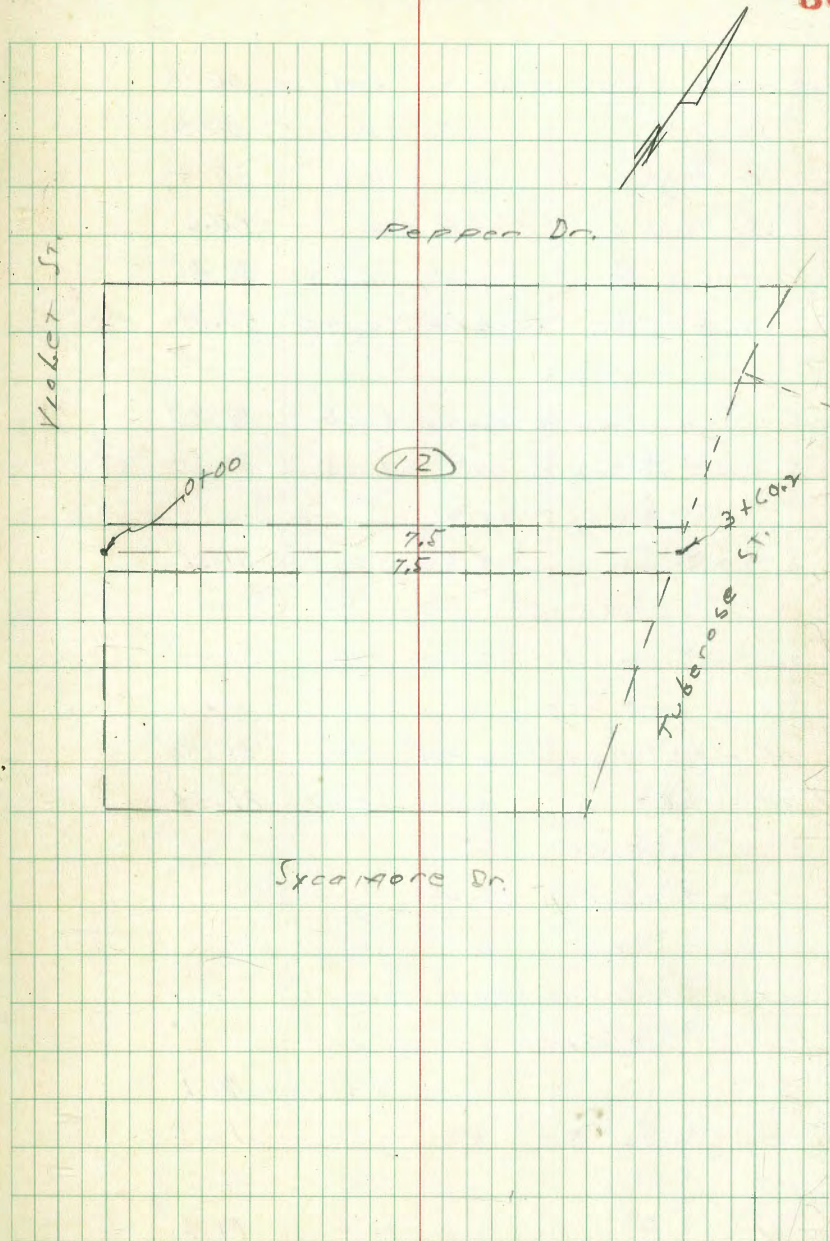
0 ± 42

N - 0.7 wedge slab con.      4.27      80.62

N - 2.9 Ramped up      3.88      81.01

0 ± 48

N - 2      con slab      3.86      81.03



N-0.7	Con. slab	4.11	80.78
N		4.1	80.8
C		4.0	80.9
S		4.3	80.6
+ 2.3	± 2' Con. dg.	4.43	80.46
+ 3.3	± Sin. 90°	4.55	80.34
	CON. FL.		
	0 + 53		
S-6.7	Top 4" Con wall	3.50	81.29
S-3.0	4 Top " " "	3.50	81.29
	0 + 56.5		
S + 0.5	" " " "	3.53	81.26
	0 + 58.5		
S + 0.5	end " " "	3.50	81.33
	0 + 60		
N-0.1	Edge Con slab	3.97	80.92
N-1.8	" " " "	3.85	81.04
	0 + 61		
N-0.9	Sw. Con Shed		
	0 + 79		
N-0.9	SE. Con. Shed		
	0 + 80		
S		3.2	81.7
+ 1	± 12" P.P.		
C		3.4	81.5
N		3.5	81.4

		1 + 00		
N			3.1	81.8
C			3.0	81.9
S			3.2	81.7
T.P.	8.41	<u>290.57</u>	7.93	281.96
		1 + 26.5		
S-4'	± Sin. 90° <sup>new</sup> dwelling		8.10	82.27
	CON. APRON <sup>9.5 wide</sup>		8.25	82.12
S			7.8	82.6
C			7.7	82.7
N			7.7	82.7
		1 + 50		
N			7.4	83.0
C			7.4	83.0
S			7.5	82.9
		1 + 75		
S			7.0	83.4
C			6.9	83.5
N			6.7	83.7
		2 + 00		
N			5.8	84.6
C			6.1	84.3
S	± 12" P.P.		6.1	84.3

2 + 15			
- 25		6.8	83.6
S		5.5	84.9
C		4.9	85.5
N		5.0	85.4
+ 20		5.2	85.2
2 + 50			
- 20		5.4	85.0
N		5.4	85.0
C		5.6	84.8
S		5.8	84.6
+ 25		6.4	84.0
2 + 80			
- 25		5.9	84.5
S		5.8	84.6
S + 0.3	beg. picket fence		
C		5.7	84.7
N		5.6	84.8
3 + 00			
N		5.4	85.0
C		5.5	84.9
+ 7.3	2' Cor. walk	5.92	84.45
S		5.92	84.45
+ 10	ON WALK	6.14	84.23

3 + 30			
S - 10	in yard	6.3	84.1
S		6.3	84.1
+ 2		5.6	84.8
C		5.6	84.8
N		5.3	85.1
2 + 60? w/ly Tuberosa ST.			
N		6.3	84.1
C		6.4	84.0
S	end picket fence	6.6	83.8
check to spike SW RR			
Tuberosa + Sycamore		10.40	279.95
			279.97
			P.35
			0.02



39

← sec. Ellzey's 20' wide

Blks. 319 and 322

contour Reed and Dakey Add.

Son Mein Meyer  
W. Hance  
Begg  
L. 2144

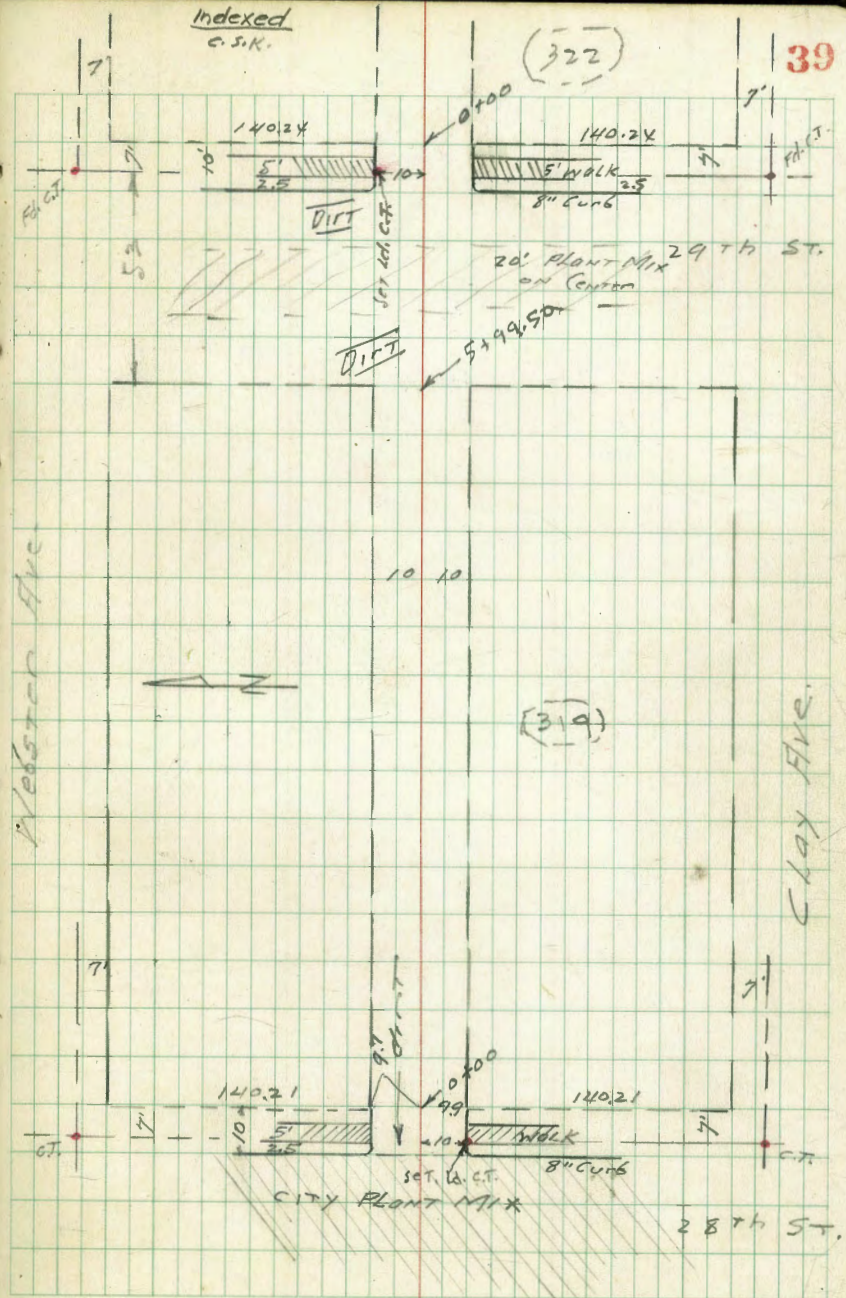
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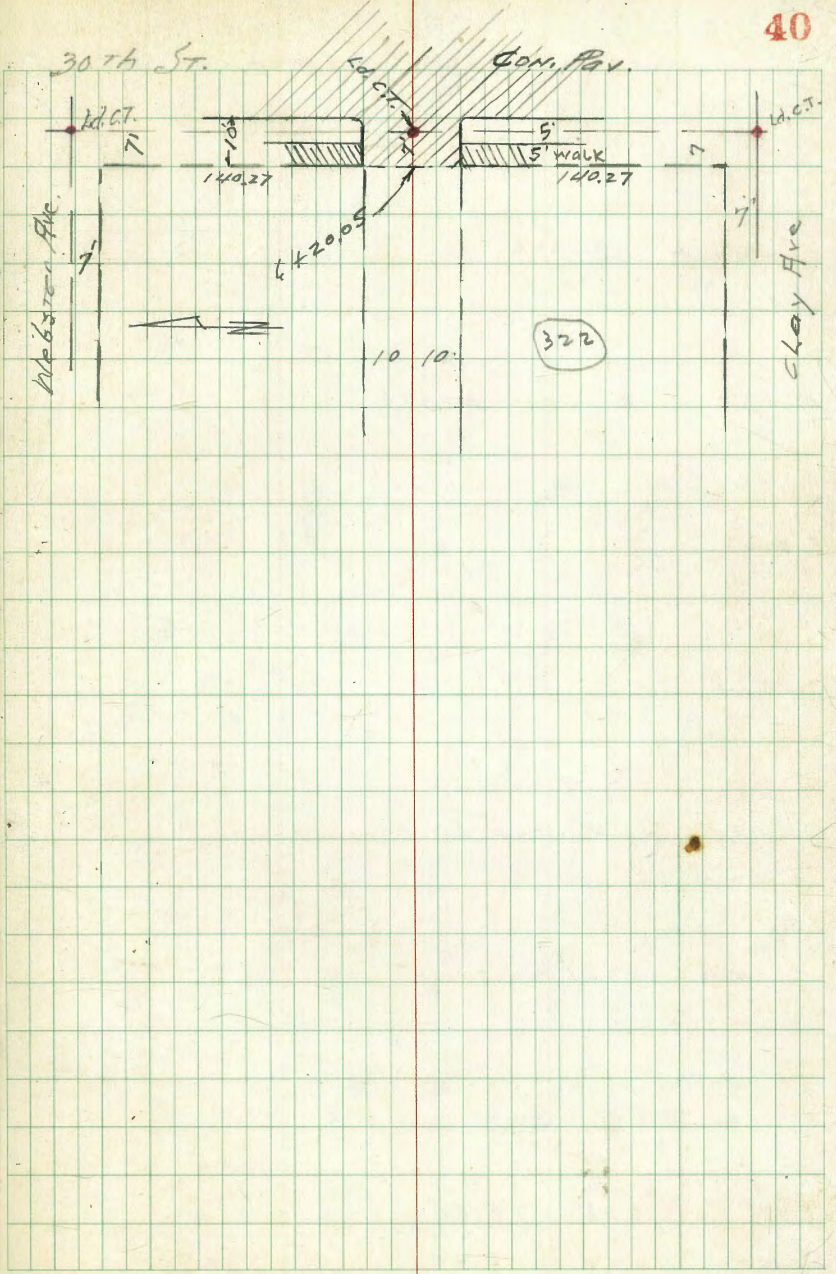
Levels Checked May 6, 17

H. J. Sizer

Indexed  
C.S.K.

39





Xsec alley Blk 319 Reed and Daley

0 + 50 73.7  
5.2  
70

0 + 42.5

0 + 40 3' Con. Wall

0 + 30

0 + 07.8

0 + 02 end, top 6" Con. Wall

0 + 00 E.L. 2874

0 - 10 E.C. 2874

T.P	3.88	78.89	328	7501
S.E.P.R	0.24	78.29		78.05

7974 + Chay

LT = N      E      RT = S

<sup>73.9</sup> Bd. F 9.9	<sup>73.8</sup> end Fence 9.1	<sup>73.8</sup> 5.1 8	<sup>73.7</sup> 5.2 ✓	<sup>74.0</sup> 4.9 10
---------------------------------	----------------------------------------	-----------------------------	--------------------------	------------------------------

#18" P.P. 9.5  
End Picket F 11

<sup>73.80</sup>  
5.09  
10

<sup>73.8</sup> 5.1 ✓ 10	<sup>73.8</sup> 5.1 ✓ 10	<sup>73.1</sup> 5.8 ✓	<sup>73.9</sup> 5.5 10	<sup>73.8</sup> 5.1 ✓ 10
--------------------------------	--------------------------------	--------------------------	------------------------------	--------------------------------

<sup>73.78</sup> end 8" Wall 5.1 9.8	<sup>73.78</sup> Picket Beg. fence 9.5	<sup>71.1</sup> 7.0 9	<sup>71.1</sup> 7.1	<sup>71.3</sup> 6.5 8	<sup>73.8</sup> 5.1 10
--------------------------------------------	----------------------------------------------	-----------------------------	------------------------	-----------------------------	------------------------------

<sup>73.84</sup>  
5.05  
9.9  
Top and beg. Picket fence

<sup>73.75</sup> 5.1 ✓ 9.7 Top 5" Con. Wall	<sup>71.6</sup> 7.25 9.7 6	<sup>71.5</sup> 7.4 9.7	<sup>71.4</sup> 7.5	<sup>71.9</sup> 7.0 9.9	<sup>71.95</sup> 6.9 ✓ 9.9 6	<sup>73.84</sup> 5.05 9.9 Top 6" Con. Wall
------------------------------------------------------	-------------------------------------	-------------------------------	------------------------	-------------------------------	---------------------------------------	-----------------------------------------------------

<sup>71.34</sup> 7.55 9.7 6	<sup>70.82</sup> 8.07 9.7	<sup>71.04</sup> 7.85	<sup>71.15</sup> 7.7 9.8	<sup>71.18</sup> 7.2 ✓ 9.8	<sup>71.18</sup> 7.18 9.8 6 Ret
--------------------------------------	---------------------------------	--------------------------	--------------------------------	----------------------------------	---------------------------------------------

78.89

1+10 & Sing. Gar. Dirt floor

1+00

0+92.5 & Single garages

0+87

0+75

0+69 & Sing. gar. dirt fl.

0+63

0+59 & Sing. gar. dirt fl.

78.89

LT. No

¢

R. No.

42

<sup>78.9</sup>  
Req. board Fence  $\frac{5.2}{10.3}$   
10

<sup>78.8</sup>  
5.1 ✓

<sup>78.5</sup>  
 $\frac{5.1}{10}$

<sup>78.9</sup>  
5.6  
 $\frac{10.9}{10.9}$   
Dirt floor

<sup>78.0</sup>  
Cold lay floor  
 $\frac{4.9}{16}$

End. Bd. F.  
10.9

Req. Bd. F.  
10.1

<sup>78.1</sup>  
5.7  
10.2

<sup>78.2</sup>  
End Fence  
10.2

<sup>78.8</sup>  
 $\frac{5.1}{10}$

78.89

1+60      \$ 19' board garage

1+56

1+50

1+40      \$ -20' Board garage dirt floor

1+41

1+36

1+26      \$ 2' Conc walk

1+16      Beg. board fence

78.89

-T

E

R

43

$\begin{array}{r} 78.6 \\ \sqrt{5.3} \\ 10.2 \end{array}$

Beg. Board Fence  
10

$\begin{array}{r} 78.6 \\ \sqrt{5.3} \\ 10 \end{array}$

78.9  
-5.0 ✓

$\begin{array}{r} 78.0 \\ \sqrt{4.9} \\ 10 \end{array}$

End board Fence  
10.6

$\begin{array}{r} 78.5 \\ \sqrt{5.4} \\ 10.1 \end{array}$

\$ 16" P. P. 6.  
9.3

End board  
Fence  
10.5

$\begin{array}{r} 78.24 \\ \sqrt{5.60} \\ 10.6 \end{array}$

Beg. fence  
16

78.89

2+29 4" C.I. plumbing vent

✓2+25 End slat fence

✓2+04 Reg slat fence

✓2+00

1+99

1+86 4 Sing. Bar dirt floor

✓1+80 End board fence on line

✓1+69

78.89

LT

E

R

44

4 vent  
10.1

End fence  
10.2

Reg. fence  
10.2

<sup>73.4</sup>  
5.3  
10

<sup>73.9</sup>  
5.0 ✓

<sup>73.9</sup>  
5.0  
10

<sup>73.6</sup>  
5.3  
10

this to be rebuilt further back

<sup>73.1</sup>  
5.8  
10

this to be rebuilt further back

Reg. board fence  
10.2

78.89

2+93  $\Phi$  Single Gar. dirt floor

12+88 10<sup>E</sup> Rt = End board fence

12+85 Man hole rim

12+79 S.E. Cor. board dwelling

12+66.5 9.4 Rt to  $\Phi$  14" P. Pole

12+50

S.W. Cor.

Board dwelling

4.23 + an. slab

4.1

4.2

Fence

9.7 End board fence

10

10.5

+ Conc. slab.

12+40 Beg. board fence + <sup>conc.</sup> slab walk

4.52

10

12+34  $\Phi$  Sing. Gar. dirt floor

4.7

10.2

78.89

78.89

Lt

←

Rt

45

3.8  
14.7

End fence

4.07

End dwelling 9.7  
Beg. board fence 9.6

7.66

4.5

4.7

9.7

10

10.5

4.37

4.52

10

4.7

10.2

√377A 8.8 Lt. Beg. board fence

√3767 E Sing. Gar. dirt floor

√3762 10.2 Rt.  
S.E. Cor. board shed. Beg. board fence

√3750

$\begin{array}{r} 7A5 \\ 4.4 \\ \hline 8.0 \end{array}$	$\begin{array}{r} \text{board} \\ \text{End Fence} \\ \hline 8.0 \end{array}$	4.3	$\begin{array}{r} 7A6 \\ 4.3 \\ \hline 10 \end{array}$	$\begin{array}{r} \text{NW. Cor. shed} \\ \hline 10.6 \end{array}$
---------------------------------------------------------	-------------------------------------------------------------------------------	-----	--------------------------------------------------------	--------------------------------------------------------------------

√3725 8.8 Lt. - Start board fence

√3716 E Sing. Gar. Dirt Floor.

$$\begin{array}{r} 7A7 \\ 4.2 \\ \hline 13.5 \end{array}$$

√3700

$\begin{array}{r} 7A8 \\ 4.1 \\ \hline 10 \end{array}$	4.1	$\begin{array}{r} 7A9 \\ 4.2 \\ \hline 10 \end{array}$
--------------------------------------------------------	-----	--------------------------------------------------------

√2798 End board fence

$$\begin{array}{r} \text{End Fence} \\ \hline 9.3 \end{array}$$

78.89

78.89



✓ 4+10 =  $\phi$  Sing Car. dirt floor

✓ 4+0A 10.4 RT = End board fence

✓ 4+02 9.9 Lt. = End board fence.

T.P. 4.03  $\frac{78.71}{78.89}$  4.21 74.68

✓ 4+00

✓ 3+98.5 9.1 RT =  $\phi$  14" P. pole

✓ 3+94 10.4 RT End shed. Beg board fence

✓ 3+82 10.4 RT End board fence. Beg board shed.

78.89

Lt.  
North

$\phi$

RT  
south

47

$\frac{74.6}{4.1}$   
10.6

78.91

$\frac{78.9}{5.0}$   
10

$\frac{74.4}{4.1}$   
6

$\frac{74.6}{4.3}$

$\frac{74.7}{4.2}$   
10

78.99

Lt.

±

Rt.

✓ A+67 9.6 Lt S.E. Cor Frame dwelling

✓ A+52 9.8 Lt. S.W. Cor. Frame dwelling

✓ A+50 9.6 Lt. End Cor. Iron fence

✓ A+49 9.9 Rt End Cor Iron + start board fence

✓ A+30 10.3 Rt. End Board shed - start Cor. Iron fence

✓ A+22 9.8 Lt Beg. Corr. Iron fence.

✓ A+16 10.6 Rt. Beg. board shed

✓ A+12 ± double Board Gar. dirt floor.

78.71

<sup>74.1</sup>  
4.6  
10

<sup>74.6</sup>  
4.15

<sup>74.6</sup>  
4.1  
10 12

<sup>74.2</sup>  
4.5  
10

78.71

√5+49 8.2 Rt = \$ 16" Mulberry tree -

√5+42 9.7 Rt = End board & Bag slat Fence

√5+30 8.6 Rt = \$ 14" P. pole

√5+21 8.3 Lt = Bag. board fence

√5+10 \$ Double Gar. dirt floor

√5+00

√4+93 \$ Single Gar. Ceno floor

√4+87 10. Lt. End board fence

√4+71 10. Lt Start board fence

78.71

Lt.

Rt

49

Save. Circle with paving

$\begin{array}{r} 1.3 \\ 4.9 \\ \hline 10.5 \end{array}$

$\begin{array}{r} 1.3 \\ 4.4 \\ \hline 10 \end{array}$

$\begin{array}{r} 1.1 \\ 4.0 \\ \hline \end{array}$

$\begin{array}{r} 1.1 \\ 4.1 \\ \hline 10 \end{array}$

$\begin{array}{r} 1.37 \\ 4.34 \\ \hline 10 \end{array}$

78.71

0+00 = E.L. 29<sup>th</sup>

Begin  
good board  
Fence  
9.9

0+00 - 10 = East Cb. line 29<sup>th</sup>

S.E.B.R. 29<sup>th</sup>  
+ Clay

SS

0.66 78.05 ok.

78.71

6+00 0.4 RT = ctr. Man Hole

5+99.5 8.9 Lt. = End board fence  
W. Line 29<sup>th</sup> st.

15+92 9.6 RT = End stat fence

15+75

15+50

78.71

Lt

Rt

50

73.51  
5.20  
9.9  
7.6 d.

73.2  
5.5  
dirt

73.2  
5.5

73.7  
5.2  
10  
dirt

74.1  
4.60  
Top Cb. 10.9  
Boj board Fe

73.92  
5.29  
Top C. rot  
10

72.9  
6.4  
10 dirt

72.6  
6.1

72.9  
5.8  
10 dirt

73.8  
4.88  
Top C. Rot.  
10

74.1  
4.60  
0.14 - 0.07 2.17 10

73.5  
5.2  
10

74.1  
4.5

73.8  
4.9  
10

74.4  
4.3  
10

74.3  
4.7

74.2  
4.5  
7

74.7  
4.0  
10

74.5  
4.2  
10

74.6  
4.1 ✓

74.7  
4.0  
10

78.71

✓ 0+81 11.1 Rt = End board shed.

✓ 0+67 10.9 Rt = End board fence start shed

✓ 0+50

✓ 0+49

✓ 0+47 9.0 Lt = End shed start board fence

✓ 0+33 9.5 Lt Beg. board shed

✓ 0+29.5 = 9.5 Lt = End board fence

10+10

78.71

Lt.

Rt.

51

Levels checked  
May 7-17  
H. Sisson

<sup>73.9</sup>  
4.9  
10

<sup>74.2</sup>  
4.5  
7

<sup>74.1</sup>  
4.6  
7

<sup>73.9</sup>  
4.8  
8

<sup>74.19</sup>  
4.2  
10

<sup>74.3</sup>  
4.4  
10

ctr. 12" pepper tree  
9.8

<sup>73.9</sup>  
4.8  
10

<sup>74.1</sup>  
4.6  
7

<sup>74.1</sup>  
4.6  
7

<sup>73.4</sup>  
5.3  
7

<sup>74.2</sup>  
4.5  
10

<sup>73.7</sup>  
5.0  
10

<sup>73.5</sup>  
4.9  
7

<sup>73.9</sup>  
4.8  
7

<sup>73.3</sup>  
5.4  
9

<sup>74.4</sup>  
4.3  
10

centroid

78.91

✓1741 8.4 Lt. start board fence.

✓1731 @ Doorway Sing. Gar. dirt floor 16' wide

✓1725 8.8 End Fence

✓1712 9.0 Lt. start board fence

✓1705 @ Sing. Gar. dirt floor

T.R 4.53 79.12 4.12 74.59  
78.71

✓1700

✓17091 = @ Sing. Gar. dirt floor.

78.71

Lt.

Rt.

52

<sup>12.6</sup>  
5.1  
8.7

<sup>73.7</sup>  
5.0  
9.2

77.12

<sup>14.0</sup>  
End board fence  
8.8

<sup>14.5</sup>  
4.7  
8

<sup>14.5</sup>  
4.2 ✓

<sup>14.5</sup>  
4.2  
10

Start board fence  
10.6

<sup>14.5</sup>  
3.9  
15.0

78.71

✓ 1+89 8.6 Lt. = End of board fence

1+88  $\Phi$  15" wide conc walk

✓ 1+81  $\Phi$  Sing. Gar. Conc. Floor

✓ 1+73 9.3 Lt. = start board fence

✓ 1+73 End Conc. Apron + Garage. North + So. Polts

✓ 1+52 start conc. drive - doub. Garage

✓ 1+50

✓ 1+48.5 85 Rt =  $\Phi$ -1A" P. Pole

✓ 1+47 End Fence start Conc. Gar. Apron

79.12

Lt.

Rt.

53

74.44  
4.68  
9.4

72.07  
5.05  
9.1  
Floor

74.24  
4.88  
13.2

74.10  
5.02  
9.3  
Apron

74.44  
4.68  
10.2  
Apron

74.68  
4.44  
15.6  
Gar.  
Floor

74.50  
4.62  
10.7  
Apron

74.68  
4.44  
15.6  
Gar

74.1  
5.10  
10

74.4  
4.7  
✓

End board  
Fence  
9.9

74.4  
4.7  
10

74.27  
4.85  
13.2

74.05  
5.04  
9.3

Gar. Floor

Apron

79.12

✓ 2+36 Encl. Apron + Double Bar Conc. Floor

2+28.5 8.9 Lt = S.W. cor board shed

✓ 2+25 8.9 Lt = S.E. Cor Gal. Iron shed

✓ 2+22 Start apron + Double Bar Conc. Floor

✓ 2+12 8.7 Lt = S.W. Cor. Gal. Iron shed.

✓ 2+06 E. Sing Bar dirt floor

✓ 2+00

✓ 1+90 9.4 Rt = start slat fence.

79.12

<sup>74.76</sup>	<sup>75.10</sup>
<u>4.36</u>	<u>4.02</u>
8.8	12.3
Apron	Cor. floor

<sup>74.70</sup>	<sup>75.05</sup>
<u>4.42</u>	<u>4.07</u>
8.7	12.1
Apron	Cor. floor

<sup>75.1</sup>
<u>4.0</u>
11.5

<sup>74.2</sup>
<u>4.9</u> ✓
10.

<sup>74.4</sup>
<u>4.7</u> ✓

<sup>74.4</sup>
<u>4.7</u>
End Board
Fence
<u>9.6</u>
10

79.12



3+50 9.5 Rt. start board fence

T.P. 4.33 80.08 3.37 75.75

3+47 9.7 Lt. start chicken wire fence

3+36  $\Phi$  old double garage (Board) dirt floor

3+00

2+62 9.1 Lt = End board fence

2+52 9.2 Rt. =  $\Phi$  16" P. pole.

2+50

2+46.5 9.1 Lt = S.E. Cor board shed + start

79.12

Lt  
(North)

$\Phi$

Rt  
(South)

55

<sup>75.8</sup>  
4.3  
10

<sup>75.7</sup>  
4.4

<sup>75.6</sup>  
4.3  
10

80.08

<sup>75.1</sup>  
4.0  
10.5

<sup>75.1</sup>  
4.0  
10

<sup>75.0</sup>  
4.1

<sup>75.1</sup>  
4.0  
10

<sup>74.8</sup>  
4.7  
10

<sup>74.9</sup>  
4.2

<sup>74.9</sup>  
4.2  
10

board fence.

79.12

✓ 4+37 9.9 Lt. = start board fence.

✓ 4+31 9.7 Lt =  $\Phi$  Sing Gar. dirt floor

✓ 4+25 10.0 Rt = End board fence

✓ 4+10 9.2 Rt. start board fence

✓ 4+02 12.0 Rt. =  $\Phi$  double Gar. dirt floor

✓ 3+92 9.2 Rt = End board shed

✓ 3+78 8.6 Rt =  $\Phi$  16" p. pole.

✓ 3+75 9.6 Lt. = End chicken wire fence.  
9.3 Rt End board fence start board shed

80.08

Lt.

$\Phi$

Rt

56

$\begin{array}{r} 14.8 \\ 5.3 \\ \hline 9.7 \end{array}$

$\begin{array}{r} 15.3 \\ 4.8 \\ \hline 10 \end{array}$

$\begin{array}{r} 15.4 \\ 4.7 \end{array}$

$\begin{array}{r} 15.3 \\ 4.8 \\ \hline 10 \end{array}$

$\begin{array}{r} 15.3 \\ 4.8 \\ \hline 12.0 \end{array}$

$\begin{array}{r} 15.6 \\ 4.5 \\ \hline 10 \end{array}$

$\begin{array}{r} 15.7 \\ 4.4 \end{array}$

$\begin{array}{r} 15.9 \\ 4.2 \\ \hline 10 \end{array}$

80.08

T.P. 4.67 79.45 5.30 74.78

✓ 5+27 10.1 Rt = End board fence.

✓ 5+25 10.45 conc. walk

✓ 5+02 8.9 Rt = 16" R. pole

✓ 5+00 10° Lt start good picket fence

✓ A+7A 10.4.0 Single Gar. Conc. floor

✓ A+88 10° Lt End board fence

✓ A+75.5 10.2 Rt = start board fence

✓ A+50

✓ 4+48.5 10.4 conc. walk

80.08

Lt  
North

±

Rt  
South

57

75.13  
4.95  
10.6

74.8  
5.3  
10 ✓

75.1  
5.0  
10 ✓

75.1  
5.0  
10 ✓

74.73  
5.35  
10

75.2  
4.9  
10 ✓

75.2  
4.9  
10 ✓

75.2  
4.9  
10 ✓

75.20  
4.88  
10.4 on walk

80.08

6+20.05 = W. line 30<sup>th</sup> Conc. paving

✓ 6+17

✓ 6+12 9.5 Rt = 8" Telephone pole

✓ 6+00

✓ 5+75 10' Lt. = End board fence

✓ 5+60 = Ctr. M.H.

✓ 5+50

✓ 5+45 End. conc. apron + double Cur.

✓ 5+28 Start conc. Apron + double Cur. Conc. Fl.

79.45

LT 50.

Rt No

58

$\begin{array}{r} 72.41' \\ 7.04 \\ \hline 9.98 \\ \hline \text{ct.} \end{array}$

$\begin{array}{r} 72.25' \\ 7.20 \\ \hline 9.95 \\ \hline \text{Enter} \end{array}$

$\begin{array}{r} 71.93' \\ 7.52 \end{array}$

$\begin{array}{r} 72.21' \\ 7.24 \\ \hline 10 \text{ cut.} \end{array}$

$\begin{array}{r} 72.34' \\ 7.11 \\ \hline 10 \text{ cut.} \end{array}$

$\begin{array}{r} 73.5' \\ 6.0 \\ \hline 10 \end{array}$

$\begin{array}{r} 72.3' \\ 7.2 \\ \hline 6 \end{array}$

$\begin{array}{r} 72.2' \\ 7.3 \end{array}$

$\begin{array}{r} 72.5' \\ 7.0 \\ \hline 6 \end{array}$

$\begin{array}{r} 73.8' \\ 5.7 \\ \hline 10 \end{array}$

$\begin{array}{r} 74.2' \\ 5.3 \\ \hline 10 \end{array}$

$\begin{array}{r} 73.5' \\ 6.0 \\ \hline 6 \end{array}$

$\begin{array}{r} 73.5' \\ 6.0 \end{array}$

$\begin{array}{r} 73.4' \\ 6.1 \\ \hline 5 \end{array}$

$\begin{array}{r} 74.3' \\ 5.2 \\ \hline 10 \end{array}$

$\begin{array}{r} 74.5' \\ 5.0 \\ \hline 10 \end{array}$

$\begin{array}{r} 74.4' \\ 5.1 \end{array}$

$\begin{array}{r} 74.5' \\ 5.0 \\ \hline 10 \end{array}$

$\begin{array}{r} 74.75' \\ 4.70 \\ \hline \text{on rim} \end{array}$

$\begin{array}{r} 74.9' \\ 4.6 \\ \hline 10 \end{array}$

$\begin{array}{r} 74.8' \\ 4.7 \end{array}$

$\begin{array}{r} 74.8' \\ 4.7 \\ \hline 10 \end{array}$

$\begin{array}{r} 75.08' \\ 4.37 \\ \hline 9.9 \\ \hline \text{Apron} \end{array}$

$\begin{array}{r} 75.42' \\ 4.03 \\ \hline 14.8 \\ \hline \text{Bar. Floor} \end{array}$

$\begin{array}{r} 75.13' \\ 4.32 \\ \hline 9.9 \\ \hline \text{Apron} \end{array}$

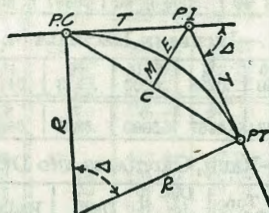
$\begin{array}{r} 75.45' \\ 4.00 \\ \hline 14.8 \\ \hline \text{Bar. Floor} \end{array}$

79.45

⊕

# DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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### CURVE FORMULAS

- Radius— $R = \frac{50}{\sin \frac{D}{2}}$  (1) Degree of Curve— $D$  and  $\sin \frac{D}{2} = \frac{50}{R}$  (2)
- Tangent— $T = R \tan \frac{\Delta}{4}$  (3) Length of Curve— $L = 100 \frac{\Delta}{D}$  (4)
- Middle ordinate— $M = R(1 - \cos \frac{\Delta}{2})$  (5)  $= R \text{vers} \frac{\Delta}{2}$  (6)
- External— $E = T \tan \frac{\Delta}{4} = R + \cos \frac{\Delta}{2} - R$  (8)  $= R \text{exsec} \frac{\Delta}{2}$  (9)
- Long Chord— $C = 2 R \sin \frac{\Delta}{2}$  (10)  $\Delta$ —Central Angle

### EXPLANATION AND USE OF TABLES

**Stations.**—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T.  $\Delta = 62^\circ 10'$   $D = 8^\circ 20'$ . From Table IV for  $1^\circ$  curve  $T = 3454.1$  and  $\div 8 \frac{1}{3} = 414.49$  ft. From Table V correction—.36 or  $T = 414.85$  ft. P. C.—Sta. P. I.— $T = 157 + 45.50$ . Also from (4)  $L = 746.00$  and P. T.—Sta. P. C. +  $L = 164 + 91.50$ .

**Offsets.**—Tangent offsets vary (approximately) directly with  $D$  and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.—7.27 ft. Distance— $158 - \text{Sta. P. C.} = 54.50$ , hence offset— $7.27 (54.50 \div 100)^2 = 2.16$  ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus  $(54.50)^2 \div (2 \times 688.26) = 2.16$  ft.

**Deflections.**—Deflection angle— $\frac{1}{2} D$  for 100 ft.,  $\frac{1}{4} D$  for 50 ft., etc. For  $c$  ft.—(in minutes)  $.3 \times C \times D^\circ$  or—defl. for 1 ft. from Table III  $\times C$ . For Sta. 158 of above curve—.3  $\times 54.5 \times 8 \frac{1}{3} = 136.2'$  or  $2^\circ 16.2'$ , or— $2.50 \times 54.5 = 136.2'$  from Table III. For Sta. 159 deflection angle— $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$ , etc.

**Externals.**—May be found in similar manner to tangents. Thus  $E$  for curve above is 115.37. For from Table IV for  $1^\circ$  curve  $E = 960.6$  for  $8^\circ 20' = 960.6 \div 8 \frac{1}{3} = 115.27$  and from Table V correction—.10 or  $E = 115.37$  ft. Or suppose  $\Delta = 32^\circ$  and  $E$  is measured and found to be 42 ft. What is  $D$ ? From Table IV  $E = 230.9$  and  $\div 42 = 5.5$  or  $D = 5^\circ 30'$ .

+      H1      -      BM

S.E. B.R. 29th + Clay.				
Orig B.M. <u>Sta. H. 48.05</u>		2.98		78.06
5.56	81.04	4.01		75.48
T.P.	4.41	79.49	4.37	75.08
		<u>79.45</u>		

C+30 = W. Cl. 30th	7.08	7.48	7.53	7.59	7.16
	7.37	7.77	7.92	7.86	7.29
	10 T.P. curb	10 Cutler		10 Cutler	10 curb
	<u>79.45</u>		⊕		
		<u>79.45</u>			

6° 28' 30"  
 12° 57'  
 19° 25' 30"  
 1° 59' 30"  
 3° 58' 45" X 30" X  
 5° 58' 15"  
 7° 57' 30"  
 9° 57'

71 03  
 33 31 30

22.66



DISTANCES FROM CENTER OF ROADWAY FOR  
 CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½  
 For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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