

1715

ENGINEER'S  
LEVEL BOOK  
No. 4107

# EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and  
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning  
Roadway 16 feet wide. Side Slopes 1 on 1.  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be  $30.6 + (20 - 16) \div 2$  or 2 ft. added to  $30.6 = 32.6$ . For slopes of 1 on 1½ see inside of back cover.  
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# 1715

## CITY ENGINEER'S OFFICE

INDEXED

W.R.

MAR 31 1950

Completely

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

X sec Herrick Blvd to Jewell 41

Proposed drain in Herrick to

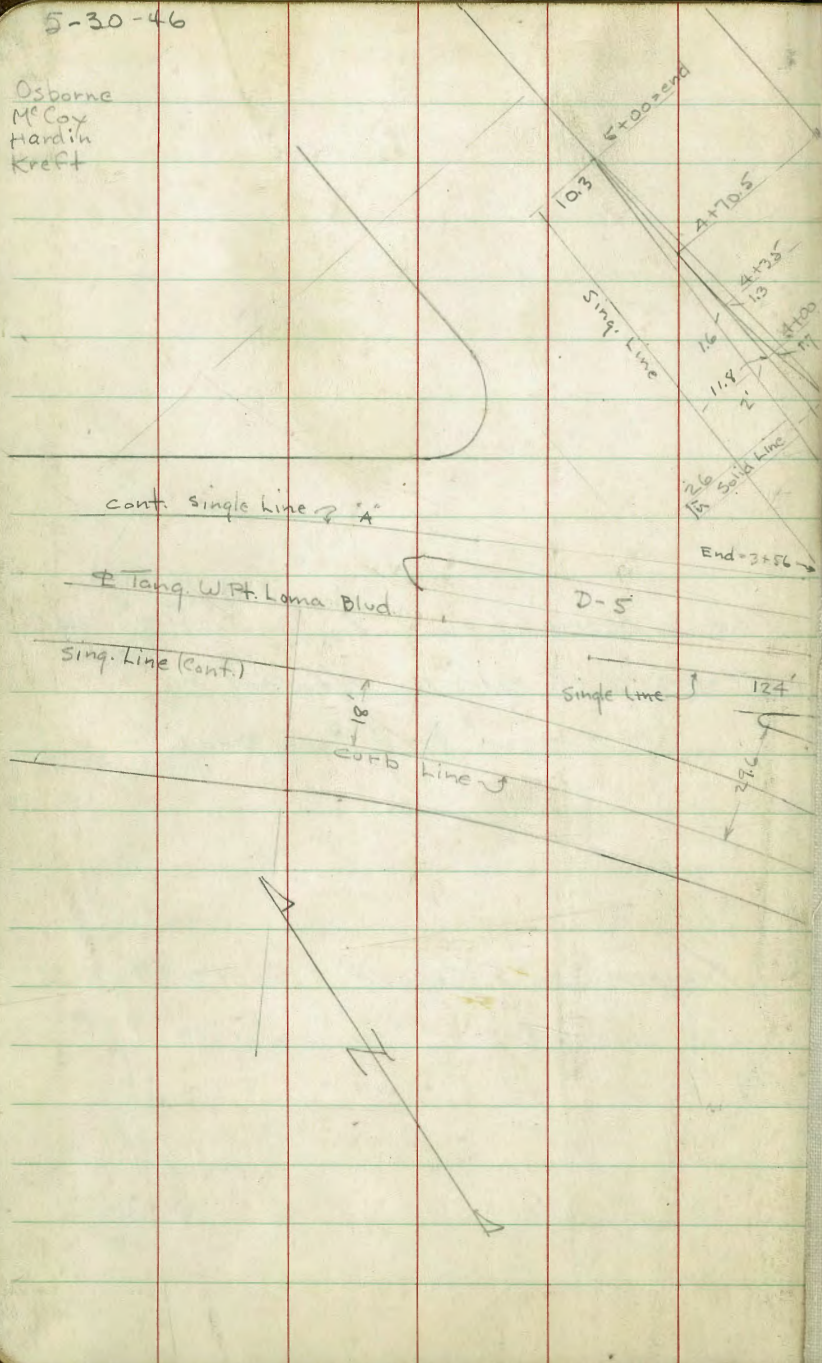
South of Bird Rock add. - 47

Proposed Sewer El Cajon Blvd East of 70<sup>th</sup> St 67-68

X sec Landis, 47th to Euclid 69

5-30-46

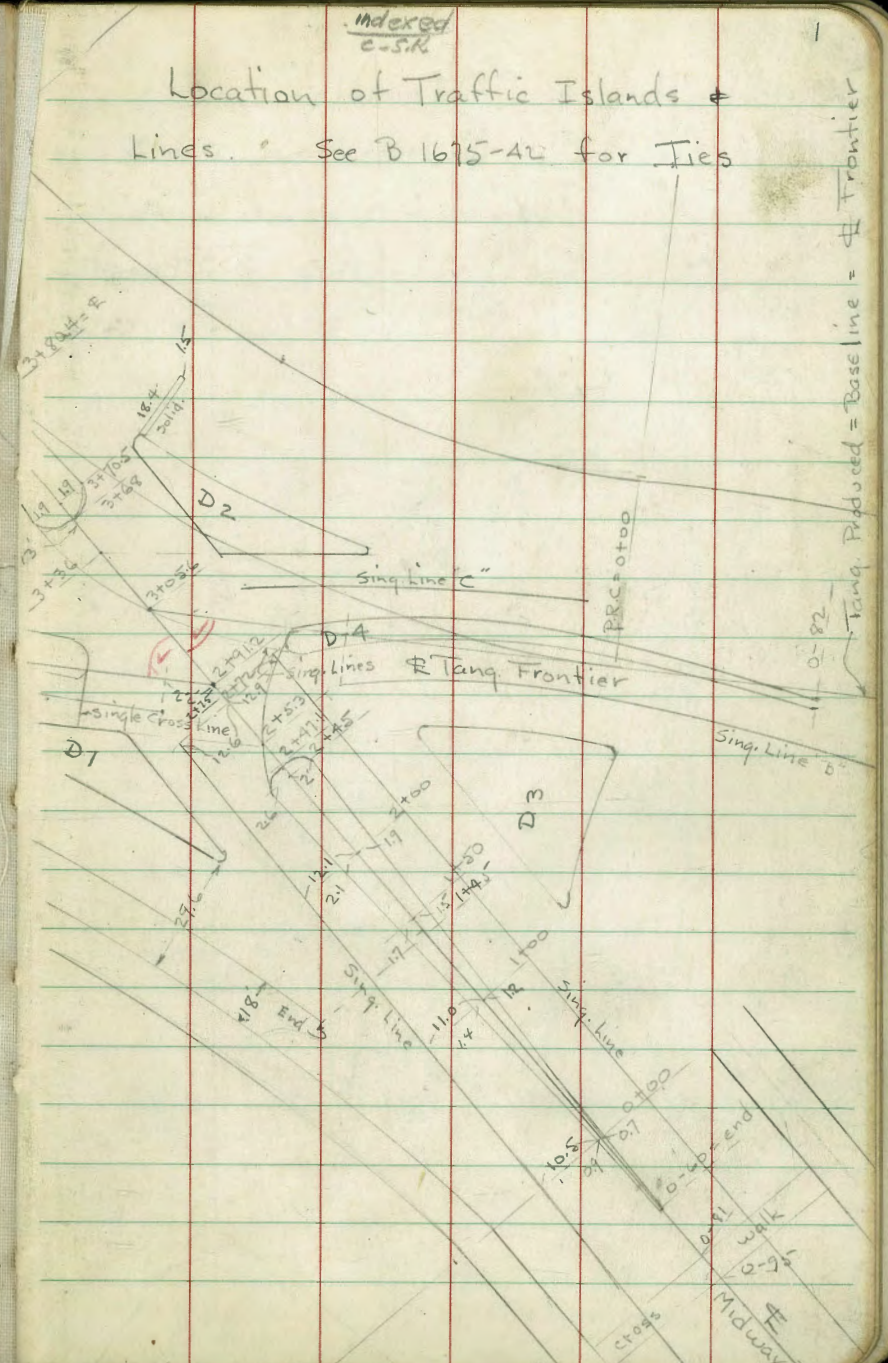
Osborne  
McCoy  
Hardin  
Kreft



Indexed  
C-S.R.

1

Location of Traffic Islands &  
Lines. See B 1675-42 for Ties



Tang. Produced = Base line = Frontier

0-82

Sing. Line b

Tang. Frontier

Sing. Line C

PRC = 0+00

D3

D1

D2

D4

D5

D6

D7

D8

D9

D10

D11

D12

D13

D14

D15

D16

D17

D18

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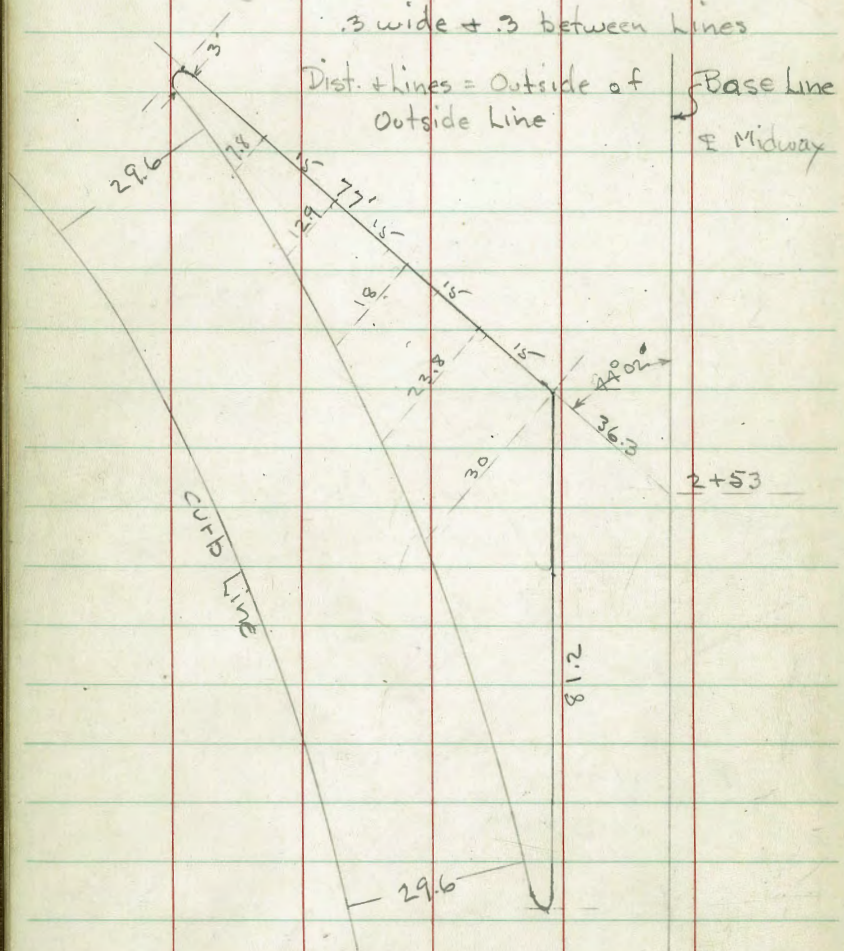
Detail - for loc. of Islands

D-1 - See P.

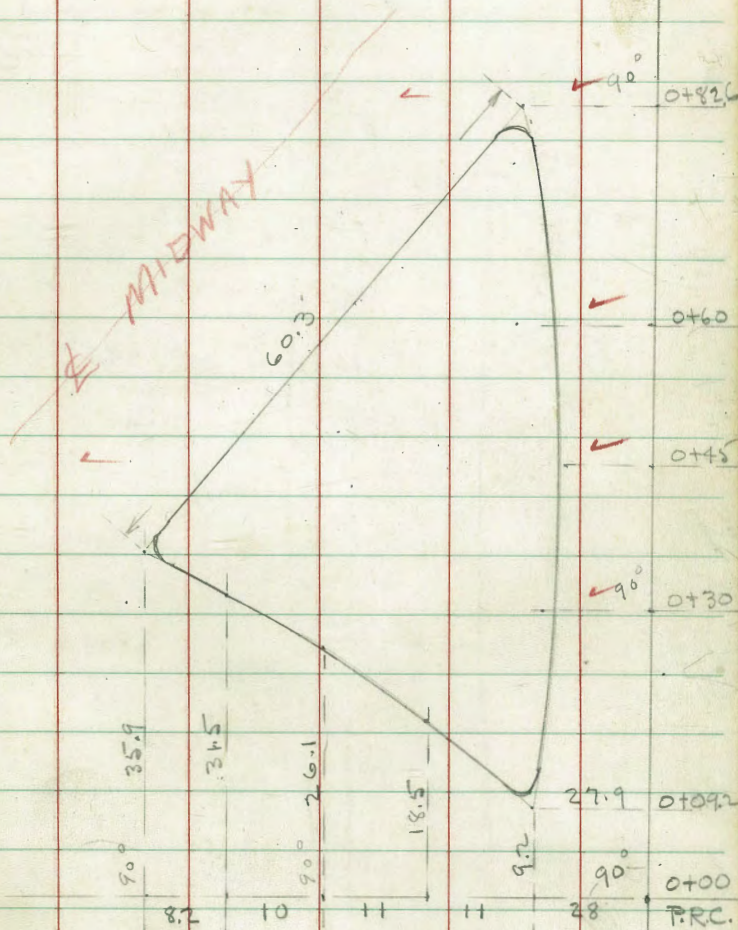
Islands Have Double Lines

.3 wide + .3 between Lines

Dist. + Lines = Outside of Base Line  
Outside Line  
Midway



D-3

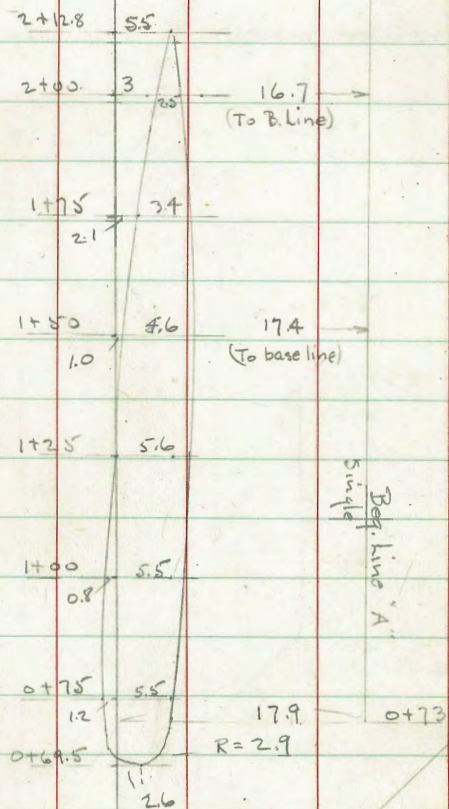


Base line =  $\frac{1}{2}$  Tang.  
of Frontier prod.



D-5

Base Line =  $\neq$  Tang. w. Pt.  
Loma Blvd.



2+91.2

4

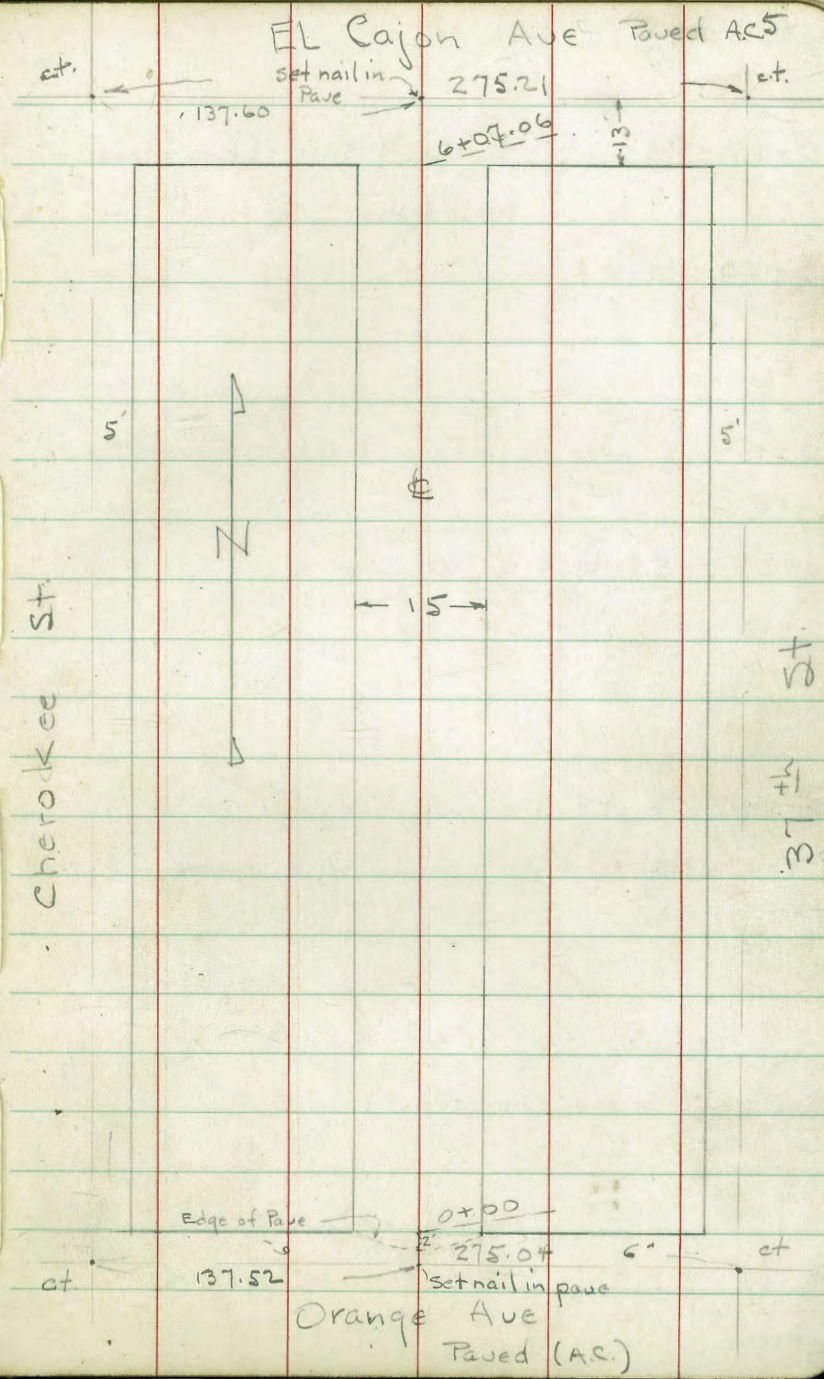
Indexed  
C.S.K.

X-Sect. 15 Alley in BIK 33

Terralta Ties B. 23-P. 13

sub. H&I  
6-6-46

Osborne  
McCoy  
Hardin





0+67 - 30.2 Lt. -  $\Phi$  12'x9' shed - Conc. floor + Wash tubs

0+50

0+39 = 8' Lt. =  $\Phi$  3.5' Conc. Porch for back door

0+24 - 5.8 Lt. =  $\Phi$  Tel. pole

0+12

0+08 6 Lt = Deadman for guy

0+00 = N.L. Orange - Reg. Wire fence 7.1 Lt.

0-14 = N. cb. line Orange

B.M.  
N.W. R.P. Wilson  
+ Orange

3.54

376.67

7.89

373.13

3.97

381.02

377.05

372.73

W  
Lt.

$\Phi$

E.  
Rt.

6

30.2

on Conc floor  
Shedi

372.57

4.1  
7.5

372.57

4.1

372.47

4.2  
7.5

372.27

4.4  
3.0

372.78

3.94

Top Conc walk  
along house

372.79

2.88

Top of  
conc. porch

372.07

4.6  
7.5

371.97

4.8

371.97

4.7  
7.5

371.18

5.49  
7.1

Top cb  
end ret.

370.71

5.96  
7.1

gut

370.53

6.14

on edge of  
pave 2' S.  
see sketch

370.65

5.87  
7.5

gut

370.97

5.70  
7.5

Top cb end ret.

371.56

5.31  
6.0

Top cb

370.69

5.98  
6.0

gut

370.95

5.74  
7.5

Top cb  
Alley Ret.  
2' Rad.

370.35

6.32  
7.5

gut

370.22

6.45

on pave

370.17

6.50  
7.5

gut

370.86

5.81  
7.5

Top cb

370.47

6.20  
6.0

Top cb

369.96

6.11  
6.0

gut

376.67

2+06 =  $\Phi$  Single gar. on Rt. Dirt floor

T.P. 5.32 378.29 3.70 372.97

1+75

1+50 - 7.2 Lt. = end board fence

1+03 - 7.2 Lt. edge of post-board fence (angle in fence)

1+01 - 6 Lt. =  $\Phi$  P. pole

1+00

0+88 - 5.2 Lt. = dead man for guy

0+75 = 7' Lt. = end wire fence - 7.5 Lt. = beg. board fence

0+65 =  $\Phi$  Single gar. on Rt. Conc. floor & apron

Lt.  $\Phi$  Rt.

5.3 7.5 <sup>372.99</sup>  
5.2 <sup>373.09</sup>  
5.4 7.5 <sup>372.89</sup>  
5.6 12.4 <sup>372.69</sup> Floor Gar.

378.29

3.8 30x <sup>372.87</sup>  
3.9 10 <sup>372.77</sup>  
3.5 7.5 <sup>373.17</sup>  
3.7 <sup>372.97</sup>  
3.5 7.5 <sup>373.17</sup>  
4.2 10 <sup>372.47</sup>  
4.4 50 <sup>372.47</sup>

3.6 7.5 <sup>373.07</sup>  
4.0 <sup>372.67</sup>  
4.0 7.5 <sup>372.67</sup>

3.2 20 <sup>373.47</sup>  
3.7 7.5 <sup>372.97</sup>  
4.0 <sup>372.67</sup>  
4.1 7.5 <sup>372.57</sup>  
4.5 25 <sup>372.17</sup>

4.36 8 <sup>372.31</sup> edge Apron  
4.10 20 <sup>372.57</sup> floor

376.67

3+50

3+05 = £ Gar. on Rt. Conc. floor + apron

Note - using drive to 37<sup>th</sup> thru another gar.

3+00

2+83 = £ Single gar. on Rt. Conc. floor (not used)

2+58 = £ Single Gar. on Rt - Conc. floor (not used)

2+50 - 6' Lt. = £ P. pole

5.0 1.5	572.19 Lt.	4.9 1.5	572.29	4.9	572.29	5.0 1.5	572.19 Rt.	5.0 1.5	572.29
------------	------------	------------	--------	-----	--------	------------	------------	------------	--------

5.10 7.6	572.19	5.00 15.7	572.29
edge Apron		Conc. floor	

5.0 1.5	572.29	5.1 7.5	572.19	4.9	572.29	5.1 7.5	572.19	5.5 8.0	572.79
------------	--------	------------	--------	-----	--------	------------	--------	------------	--------

5.32  
16.6 = Conc. floor gar.

5.23  
16.4 - Floor gar  
on conc.

5.1 2.0	572.19	4.7 7.5	572.51	5.0	572.29	5.4 7.5	572.09	5.7 2.5	572.59
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378.29

4+19 - on Conc. slab

4+12 = Approx. beg. of Rough irregular Conc. slab in Alley

4+04 = S. end 3 car Gar. on Lt. - Conc. floor

4+03 = E 4' Rough Conc. walk on Lt.

4+00 - 6 Lt. = P. pole

3+91 = Single Car. on Lt. - Conc. floor (not used)

3+60 = Single Car. - Conc. floor - on Lt. (not used)

Lt. 374.19  
4.1  
12 = W. edge  
E 374.09  
4.2  
Rt. 374.29  
4.0  
8 = E. edge

373.99  
4.3  
w. edge 2  
374.09  
4.2  
374.09  
4.2  
8 = E. edge

374.21  
4.08  
15.8  
Floor  
Gar.

374.07  
4.22  
6.4 = edge of walk

373.49  
4.8  
2.0  
373.79  
4.5  
7.5  
373.79  
4.5  
7.5  
373.69  
4.6  
7.5  
373.49  
4.8  
2.0

373.79  
4.50  
14.7  
Floor  
Gar.

373.60  
4.69  
12.6  
Floor  
Gar.

378.29

5+25 - 7.2 Lt = E P. pole

5+10

5+02 - 7.7 Lt = end wire fence - beg board fence

5+00.5 7.7 Rt = Beg. Conc. Bld. on Rt.

4+93 - 6.8 Lt = wire fence

4+75

4+70 - 10.5 Rt = 2' Conc. walk

4+52 - 7.6 Lt = beg. wire fence

4+40 = End. Conc. Slab.

4+34 - on slab.

4+32 = N. end of Gar. on Lt. Conc. floor

Lt. E Rt.

375.39  
 2.9  
 10

374.29  
 4.0  
 7.5

374.59  
 3.7

374.59  
 3.7  
 7.5

373.99  
 4.4  
 15

373.99  
 4.3  
 7.5

374.09  
 4.2

374.59  
 3.7  
 7.5

374.09  
 4.2  
 20

374.23  
 4.07  
 10.5 = on walk

373.69  
 4.6  
 16

374.19  
 4.1  
 7.5 = wedge

374.19  
 4.1  
 on Conc.

374.19  
 4.1  
 5 = E. edge

374.19  
 4.0  
 7.5

374.29  
 4.2  
 20

374.39  
 3.9  
 W. edge 12

374.19  
 4.10  
 15.9  
 Floor  
 Gar.

378.29

check B.M. 3.17 377.07 377.05

8.21 380.24 7.21 372.03

T.P. 2.75 379.24 3.34 376.49

S.W. BR  
Cherokee +  
El Cajon

6+27.06 = S. cb. line El Cajon

6+07.06 = S.L. El Cajon - 7.5 Lt = end Stucco Bld  
7.6 Rt. = end Conc. Bld.

T.P. 5.17 379.83 3.63 374.66

5+85

5+70 - 7.4 Lt = end board fence - beg. Stucco Bld.

5+50

5+31

Lt.

Rt.

4.67	5.04	4.91	5.30	5.40	5.46	5.11	6.04	5.41
4.5	4.5	7.5	7.5		7.5	7.5	7.0	7.0
Topcb.	gut.	Topcb.	gut.		gut	Topcb	gut	Top
						Alley Ret.		cb.
						2 Rad.		

4.60	4.70	5.06	5.11	4.91
7.5	7.5		7.6	7.6
			gut.	Topcb. endot
				Alley Ret.

3.0	2.9	2.9
7.4		7.5

3.1	3.5	3.5	3.5
12	7.5		7.5

2.7	3.4	3.2	3.3
10	7.5		7.5

378.29

X-Sect Evergreen - from Jarvis to Ingelow

9-25-46

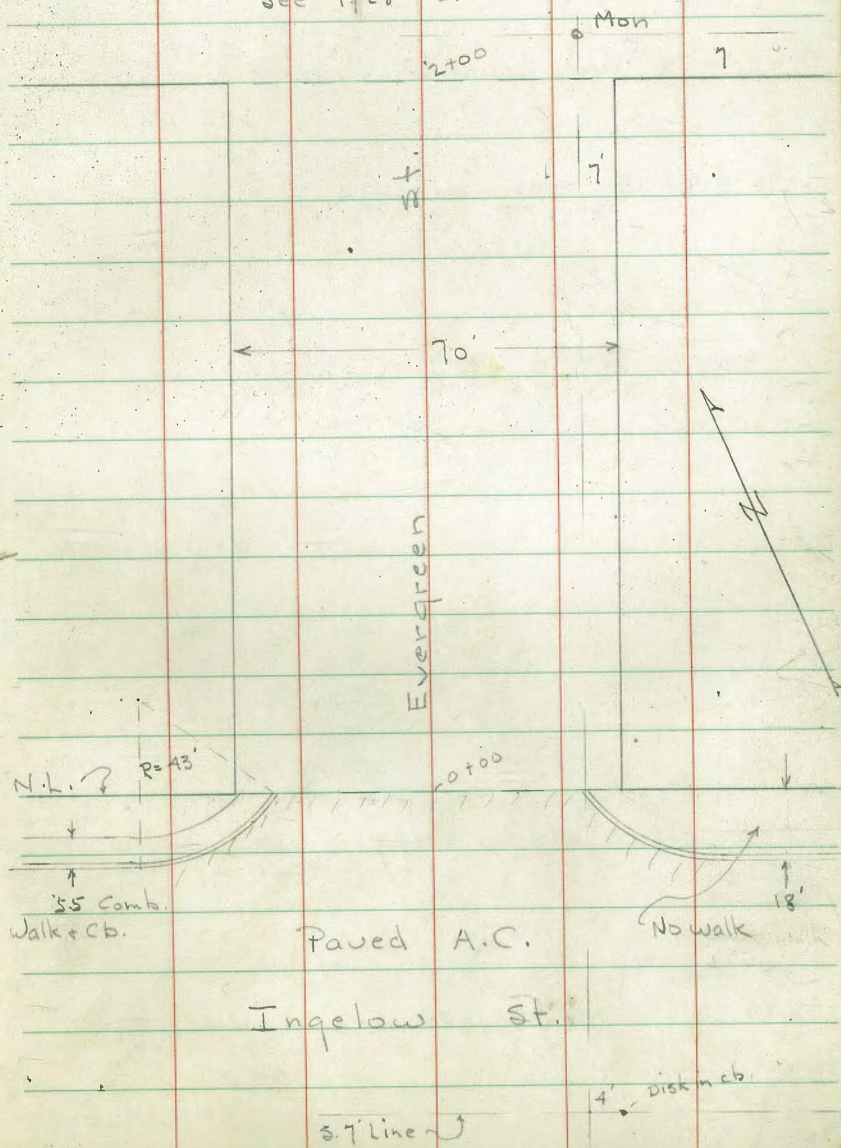
Osborne  
Hardin  
Worrell

Indexed  
C.S.K.

12

Jarvis St. - Dirt - Graded

See 1728 - 21







Lt.

C

Rt.

2+00 = S.L. Jarvis = end.

1+90 - 34.6 Lt = end fence

1+58 - 34.7 Lt = Bog Lath fence

1+50

1+40 34.6 Lt = end fence

1+00 - 34.6 = Lt = Bog picket fence

26.1	25.0	24.6	24.2	23.1
5.0	6.1	6.5	6.9	8.0
35	17		17	35

27.1	26.8	25.4	24.7	23.5	22.9
4.0	5.3	5.9	6.4	7.6	8.2
35	17		17	35	50

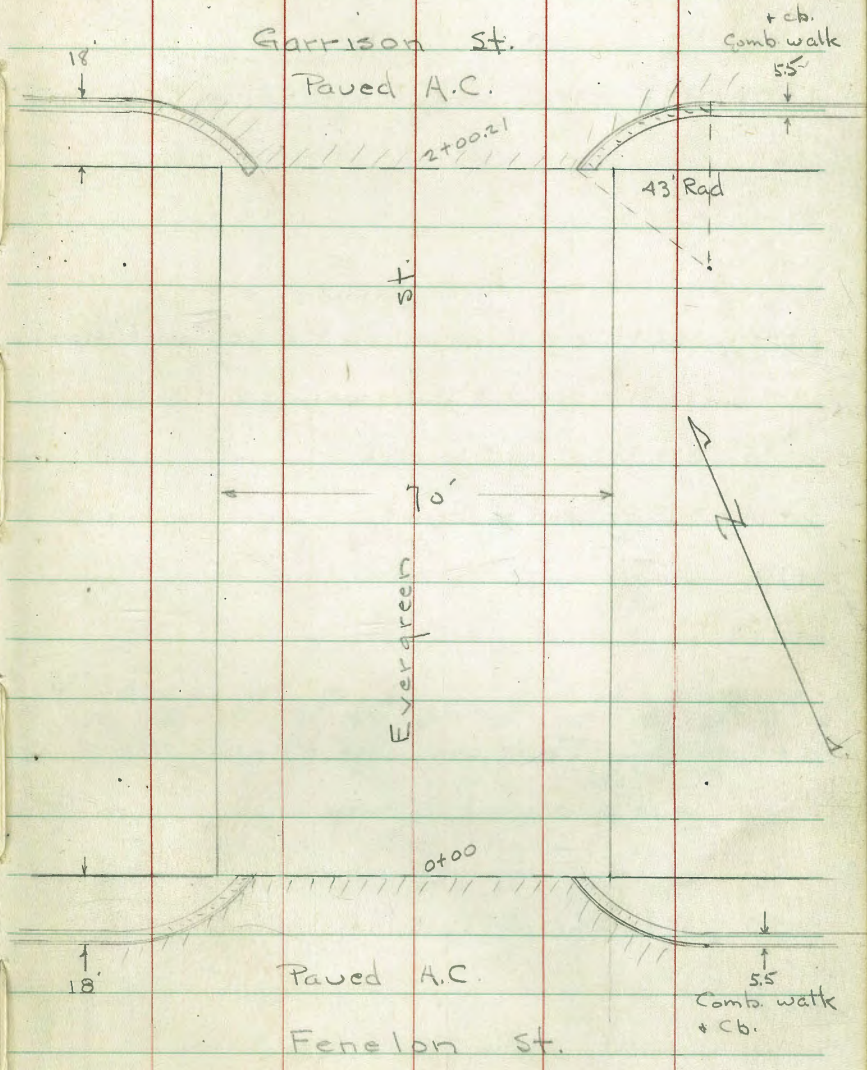
27.2	26.5	26.0	25.6	25.1	25.2	24.4
3.9	4.6	5.1	5.5	5.0	5.9	6.7
35	17		10	17	35	50

31.14

X-Sect. Evergreen - Fenelon to Garrison

Osborne - 9-25-46

Indexed  
e. s. r.



X-Sect. Evergreen - 70' st. - 18' cbs.

Lt = W.

Rt = E.

with basement  
 0+57 - 31' Lt = 3' Conc walk - + 39.4 Lt. Side of large house

30.1  
 2.4 3.1 4.0 4.5 5.0 5.3 6.3  
 3.5 2.7 2.3 1.7 5.0 5.3 3.5

30.45  
 39.94  
 26.79  
 2.02 + 1.95 5.68  
 31 39.4 39.4  
 on walk  
 Floor elev of House  
 abo floor basement

House  
 0+40 - 34.2 Rt = end Stucco wall - + 37.8 S.W. Cor. of offset in

27.22  
 5.25  
 37.8 = Floor of House

0+18 - 34' Rt = Second 8" Stucco wall - 5.5' High

0+15 - 33.8 Rt = 1.5' Conc. Walk

26.22  
 6.25  
 33.8  
 on walk

0+14 - 31.7 Rt = end of Hedge

0+10

29.22  
 3.3 3.5 6.1 6.4 6.6 7.0 6.8 6.5  
 3.5 3.0 2.2 1.7 1.0 1.7 3.5

0+00 = N.L. Fenelon = edge of pave

26.5 25.29 26.12 25.60 25.52 25.42 25.31 25.18 22.97 22.69 25.33 25.58 25.5  
 6.0 6.18 6.33 6.87 6.95 7.05 7.16 7.29 7.50 7.78 7.14 7.09 7.0  
 3.5 3.05 2.5 2.5 1.7 8 8 17 17 24.8 24.8 30.3 3.5  
 back edge walk Top-end gut Ret. Top end Ret. Backedge of walk

0-01 = 31.7 Rt = W. edge of 1.5' Hedge - 2' High

27.95 27.41 25.87 25.09 24.69 24.33 24.13 23.38 27.00  
 4.52 5.06 6.60 7.38 7.93 8.14 8.34 9.09 8.47  
 6.0 6.0 3.5 1.7 1.7 3.5 6.0 6.0  
 Top cb. gut Top cb. gut top cb. PC Ref.

0-18 = N. cb. line of Fenelon

4.37 32.47 4.19 28.10

32.47

T.P. 5.51 32.29 4.36 26.78

B.M. 8.29 31.14 22.85 P. 13

1+50

Lt.		Φ		Rt.	
19	25	4.3	4.6	4.7	5.7
35	26	17	17	17	35
					50

1+70 27.5 Lt. = N. side apron + 39.4 Lt. = floor of Gar.

31.39	30.00
1.08	2.47
39.4	27.5 = apron
floor	

1+05 24.9 Lt. = N. side of slab + 27 Lt. = S. side Conc. apron to

Doub. Gar. conc. floor

2.41	2.66
27	24.9 = N. side slab
S. side apron	

1+00

2.09	2.83	4.2	4.5	5.1	5.7	6.9
35	24.8	17	17	17	35	50
on slab.	edge slab.					

Aprons to garages

0+99 = 24.8 Lt. = N. side of apron + S. side of slab walk between

2.86	3.22
24.8	24.8
Top + S. side of slab.	edge of N. side apron

0+87 = 25 Lt. = S. side of 12 Conc. apron to Sing gar. - Conc. floor

2.47	3.22
39.3	25 = edge Apron
floor gar.	

0+92 37.8 Rt. = Φ Double gar. - Conc. floor

6.07	22.41
37.8	6.00
Floor	37.7
	walk

0+60 = 37.7 Rt. = Φ 2' Conc. walk along N. edge of house

32.47



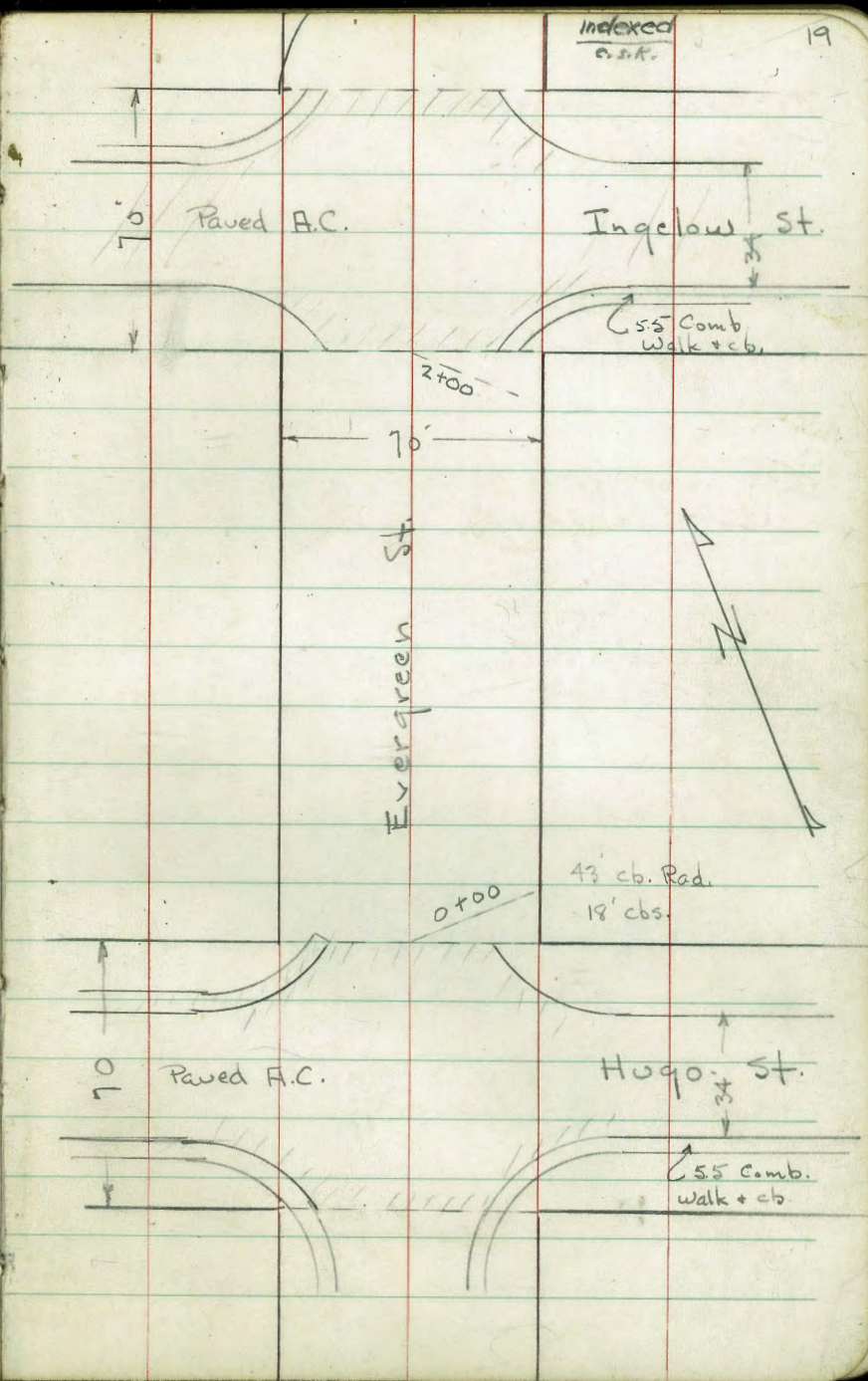
X-Sect. Evergreen - 70' St. 18' cbs.  
 from S.L. Hugo to N.L. Ingelow.

# 603

W.O. 1283

11-4-46

Osborne  
 Hardin  
 Dorrell  
 Smith



X-Sect. Evergreen

0+00 = N.L. Hugo = edge of A.C. pave

0-18 = N. cb. line Hugo

0-35 = E Hugo

T.P. 4.41 31.88 3.79 27.47

0-53 = S. cb. line Hugo

0-70 = S.L. Hugo - on A.C. pave

B.M. 8.41 31.26

22.85

S.E. 1/4 Mon  
Jarvis & Evergreen

Lt = W.

E

Rt = E

27.4	27.30	26.70	26.54	26.26	25.96	25.65	25.30	24.99	25.43	26.1
AS	4.58	5.16	5.45	5.62	5.92	6.23	6.58	6.99	6.45	5.8
35	25	25	17	8	8	7	25	25	38	
	Top cb.	gut.					gut.	Top cb.	end. ret.	
end. ret.										

28.54	27.94	27.05	26.30	25.74	25.12	24.48	23.42	23.94		
3.34	3.94	4.83	5.88	6.14	6.76	7.40	8.46	7.94		
60	60	35	18		18	35	60	60		
	Top cb.	gut.								
P.C. 43 Rad										
Ret.										

28.16	27.09	26.45	25.81	25.22	24.61	23.58				
3.71	4.79	5.43	6.07	6.66	7.27	8.30				
60	35	18	04 MH.	18	35	60				
			Top							

31.88

			26.06	25.45	24.83					
3.01	3.54	4.44	5.20	5.81	6.43	7.06	8.10	8.63		
60	60	35	18		18.	35	60	60		
	Top	gut.					gut	Top. cb.		
P.C. Ret.										
43 Rad										

26.78	26.09	25.51	24.39	24.96						
4.48	5.17	5.75	6.87	6.30						
24.7	24.7		24.7	24.7						
Top.	gut.		gut.	Top						

31.26

+ 26.9 Lt. = end picket fence  
 1+31 - Doub. gar. on Rt. - Conc. floor & apron  
 1+21 - 17.6 Rt. = end pickett fence  
 1+18 - 31.6 Lt. = nearest edge of Conc. slab. <sup>Patio</sup> for barbeave  
 1+12 - 32' Lt. = Nly. Cor. Barbecue - wing  
 wings 2' High - stack 6' High  
 1+05 - 34.8 Lt. = Sly. Cor. Barbeave oven - Brick  
 1+00 - 27.4 Rt. = beg. picket fence

0+81 - 26.1 Lt. = beg. picket fence  
 0+75 = ± Sing. Gar on Lt. - Conc. floor & apron  
 0+70 - 33.8 Lt. = N.E. Cor. Tile  
 0+70 - 26.8' Lt. = end Hedge  
 0+53 - ± Sing. gar. on Rt. - Conc. floor & Apron  
 0+53 - 33.8 Lt. = S.E. Cor. Tile patio  
 0+53 - 27.3 Lt. = beg. 2' Hedge - 4' high

0+50

0+15

31.9

Lt.

±

Rt.

28.84

3.04

31.6 = Top slab.

28.5	28.0	27.1	26.7	26.2	26.6	26.1	25.4
34	3.9	4.8	5.2	5.7	5.3	5.8	6.5
35	17	13		14	17	35	50

29.94

29.26

1.94

2.62

29.39

49.6 =

34.4 = edge

2.49

floor

apron

33.8

gar.

26.13 26.17

5.75 5.71

36.3 38.7 = floor

edge apron

29.35

2.53

33.8

on Tile

28.8	27.8	27.3	26.8	26.3	26.7	25.4
3.1	4.1	4.6	5.1	5.6	5.2	6.5
35	17	14		13	17	35

28.7

27.5

27.1

26.7

26.1

26.6

26.5

3.2

4.4

4.8

5.2

5.8

5.3

5.4

35

17

15

16

17

35

on lawn

on lawn

31.88



2+18 = S. cb. Line Ingelow

= S.L. Ingelow + edge AC. pave

2+00 = 28.3 - Lt. = end picket fence

1+97

1+84 - 27.9 Lt. = end rock wall + beg. picket fence

1+80

1+65 - 27.8 Lt. = 4' Conc. walk

1+50

around good lawn.

1+46 - 26.6 Lt. = N. side drive + beg. low rock wall

1+38 - Doub. gar. on Lt. - Conc. floor + 17' Conc. Drive

I.P. 2.67 31.40 3.15 28.73

Evergreen 22

31.40

28.04	27.45	26.28	25.55	24.98	24.44	23.90	22.98	23.45
3.36	3.95	5.12	5.85	6.42	6.96	7.50	8.42	7.95
60	60	35	17		17	35	60	60
Top		gut.					gut.	Top
PC	Ret.						PC	Ret.

43' Rad.

28.1	26.40	25.85	25.65	25.30	24.80	24.34	24.74	24.7
3.3	5.00	5.55	5.75	6.10	6.80	7.06	6.66	6.7
35	24.7	24.7	17		17	25.3	25.3	35
	Top	gut.				gut.	Top	end
	end	Ret.				Ret.		Ret.

28.3	28.0	26.3	25.8	25.6	25.0	25.1	25.6	25.5
3.1	3.4	5.1	5.6	5.8	6.4	6.3	5.8	5.9
35	26	23	17		13	17	25	35

28.7	27.5	26.8	26.3	25.6	26.2	25.4
2.7	3.9	4.6	5.1	5.8	5.2	6.0
35	17	13		12	17	35

28.29

3.11

27.8 = edge walk

28.9	27.6	27.1	26.8	26.1	26.2	25.6
2.5	3.8	4.3	4.6	5.3	5.2	5.8
35	17	12		14	17	35

28.15

3.25

26.6

40.14 26.21 27.69

1.26

3.19

3.71

61.8

26.6

20.6 = edge of

Floor

edge of

rough Conc. slab.

gar.

Reg. dr.

out side of dr.

31.40

check B.M.

8.54 22.86 ✓

2+70 = N.L. Ingelow = edge A.C. pave

2+53 = N. cb. Line

2+35 = #

53

31.40

25.97	25.47	25.34	24.74	24.43	23.83	24.34
5.43	5.93	6.06	6.66	6.97	7.57	7.06
25	25	17		17	25	25
Top-end gut					gut.	Top-end
Ret.						Ret.

27.48	27.01	26.06	25.42	24.86	24.26	23.59	22.48	22.97
3.92	4.39	5.34	5.98	6.54	7.14	7.81	8.92	8.43
60	60	35	17		17	35	60	60
Top		gut.				gut.	Top	
P.C. Ret.							P.C. Ret.	

27.56	26.26	25.52	24.90	24.35	23.83	23.01
3.84	5.14	5.88	6.50	7.05	7.51	8.39
60	35	17	on M.H.	17	35	60
			hid.			

31.40

X-sect. Evergreen - Jarvis to Keats

70' st. 18' obs.

# 630

W.O. 1283

11-18-46

Osborne  
Hardin  
Wopell  
Smith

indexed  
C.S.K.

24

Keats st.

2+00.32 Hub.

7

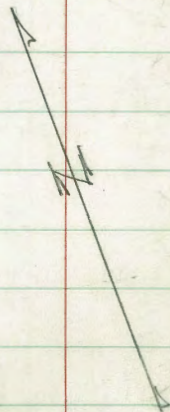
70'

7

← 35' → 35' →

st.

Evergreen



0+00

Jarvis st.

Mon. BM. 12.95

7

X-Sect Evergreen

0+83 - 35.4 Lt =  $\Phi$  7' Conc. slab

0+75

0+69 - Double Gar on Rt. Conc. floor + Apron

0+50

0+31 - 40' Rt =  $\Phi$  Med. Stucco House

0+25

0+00 = N.L. Jarvis

B.M. 5.24 28.09

22.85

S.E. 7' Mon.  
Jarvis + Evergreen

Lt = W

$\Phi$

Rt. = E

308.26  
35.8  
Top slab.

24.0  
4.1  
3.5

23.0  
5.1  
1.7

22.5  
5.6  
1.1

21.1  
7.0  
8

20.9  
7.2  
1.7

20.2  
7.9  
1.7

19.3  
8.8  
3.5

18.27  
8.82  
36.2 = apron

18.24  
8.80  
40.2 = Floor

23.9  
3.2  
4.5

24.4  
3.7  
3.5

23.1  
5.0  
1.7

22.7  
5.4  
1.1

21.9  
6.2  
9

21.6  
6.5  
1.7

20.6  
7.5  
1.7

19.4  
8.7  
3.5

18.9  
9.2  
5.0

24.4  
3.5  
3.5

23.5  
4.6  
1.7

23.3  
4.8  
1.1

22.7  
5.4  
1.0

22.5  
5.6  
1.7

21.6  
6.5  
2.2

22.1  
6.0  
1.4

22.0  
6.1  
1.7

21.5  
6.6  
2.5

20.0  
8.1  
3.5

21.9  
6.90  
40  
Floor Elev

24.7  
3.4  
3.5

24.0  
4.1  
1.7

23.1  
5.0  
1.7

22.7  
5.4  
1.7

22.6  
5.5  
2.1

21.0  
7.1  
3.5

28.09

check B.M.

5.24 22.85 ✓

2+00.32 = s.l. Keats

1+72 = 38.8 Rt. = Med. Stucco House

1+60

1+59 - 34.9 Rt. = end fence

1+30

1+00 - 35.2 Rt. = Beg picket fence

5.8 24.3

5.0 4.0 24.1

5.0 3.5 4.0 23.4

5.0 3.5 4.0 22.5

5.0 3.5 4.0 21.9

5.0 3.5 4.0 21.3

5.0 3.5 4.0 21.2

5.0 3.5 4.0 20.8

5.0 3.5 4.0 20.1

5.0 3.5 4.0 19.5

3.2 24.9

3.5 4.0 23.6

3.5 4.0 22.3

3.5 4.0 21.6

3.5 4.0 20.7

3.5 4.0 20.8

3.5 4.0 20.3

3.5 4.0 17.2

2.6 25.5

3.0 24.2

3.0 22.6

3.0 21.9

3.0 20.8

3.0 20.7

3.0 20.2

3.0 19.3

3.0 19.0

28.09

Lt

Rt

Rt.

24.0  
35

23.1  
35

22.1  
35

21.6  
35

20.6  
35

6.321.70  
Floor

X-Sect. Roselawn - Euclid to Landis

# 652

W.O. 230

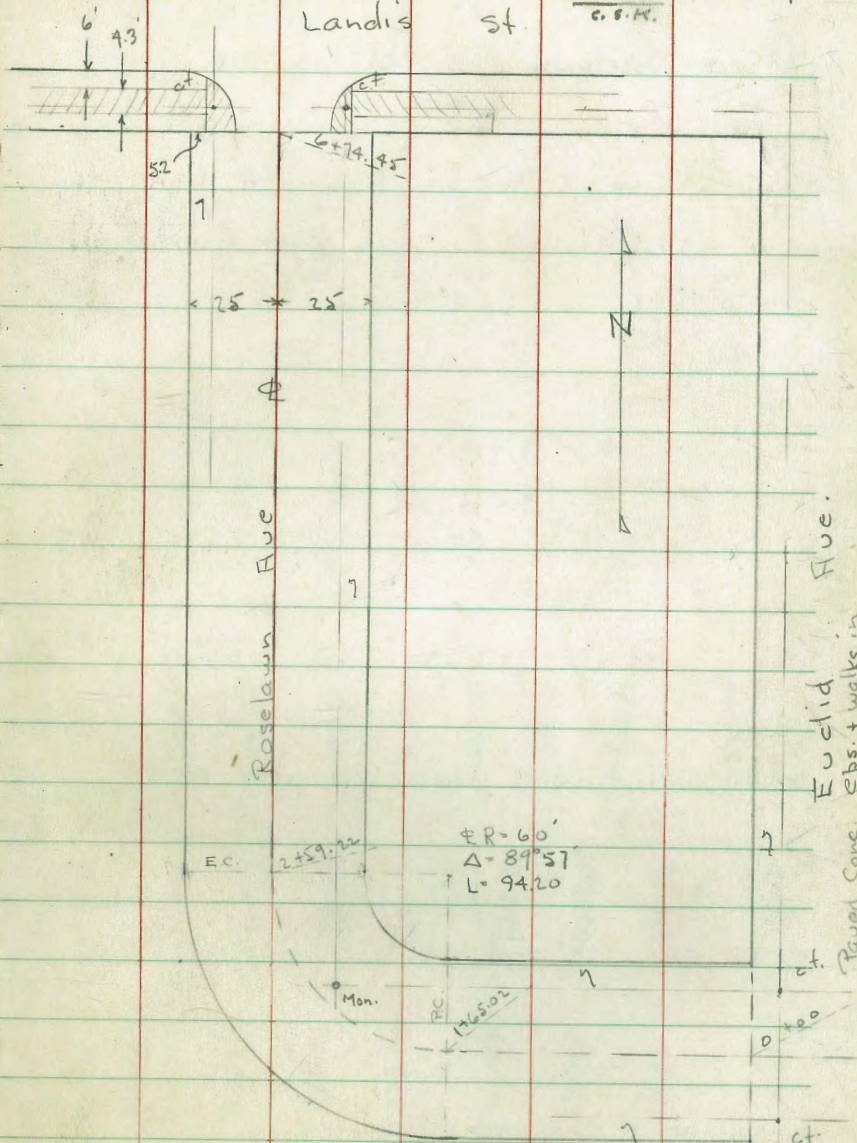
11-29-46

Osborne  
Hardin  
Worrell  
Smith

Landis St.

Indexed  
C. S. M.

27









2+95 = 25' Lt. =  $\Phi$  4' Conc. walk +  $\Phi$  Small House

2+92 = 25.5 Rt. =  $\Phi$  3' Conc. walk

T.P. 7.54 341.00 4.16 333.46

2+74 = 24.5 Lt. = beg. Fly. 4" Conc. wall - flush with hqr

31' S - 39.2 Lt. =  $\Phi$  Sing. Gar. - Conc. floor

41' S. - 36.9 Lt. =  $\Phi$  Sing. Gar. - wood floor  
used for chickens

53' S. of E.C. - 35.4 Lt. =  $\Phi$  Sing. Gar. - wood floor

Note - for accuracy + ease of plotting will show Garages  
on W. side of Curve - from Tangent prod. back from E.C.

2+59.22 = E.C. = end of wall on Rt.

to House - E. + to.

2+31 = 21 Rt = edge of wall opp.  $\Phi$  of 2.5' Conc. walk

2+27.82

335.00  
6.00  
41  
floor House

339.35 Lt.  
6.65  
25

A

Rt.

335.27  
05.71  
25.5 = walk

339.32

341.00

330  
24.5

332.55

332.62

332.65

5.07  
38.2 floor

4.97

36.9 floor

5.00  
35.4 floor

333.69

333.2

333.5

333.4

333.3

333.9

338.7

339.72

339.9

3.93  
48 =  
floor, small  
House

4.4  
40

4.1  
25

4.2  
15

4.3  
13

4.2  
15

2.90  
25.3 = Top  
end + w. side wall

4.0  
40

332.8  
4.8  
40

332.9  
4.7  
25

333.1  
4.5  
15

333.1  
4.5  
13

333.0  
4.6  
15

333.4  
4.2  
15

333.96  
3.66  
20.2 = Top  
s. wall

339.23  
3.39  
25 on  
walk

339.8  
2.8  
40

337.62

4+24.2 - 0.1 Rt =  $\Phi$  Sewer M.H.

4+11 - 23.5 Lt =  $\Phi$  2.5' Brick walk

4+01 = 25' Lt =  $\Phi$  2-2' Conc. strip Drive

4+00

3+64 - 24.8 Rt =  $\Phi$  2.5' Conc. walk

3+63 - 27' Rt =  $\Phi$  3' Conc. walk

3+56 - 56' Lt =  $\Phi$  Small House

3+50

3+35 - 26.6 Rt =  $\Phi$  8' Conc. Dr.

3+31 - 46' Lt =  $\Phi$  Sing. Gar. Conc. floor

3+18 - 46' Lt =  $\Phi$  Sing. Gar. Conc. floor

3+14 - 25' Lt = end wall

3+00

	Lt.	A	Rt.
335.25	5.7		5.6
335.44	2.5		0.1 = Rim M.H.
335.0	6.0		
335.2	5.8		
334.9	6.1		
335.0	6.0		
335.2	5.8		
335.8	5.7		
336.22			4.78
			2.9
			walk
334.3	6.7		
334.5	6.5		
334.3	6.1		
334.7	6.3		
334.6	6.4		
335.1	6.9		
335.8	6.2		
335.9	6.1		
336.16			4.84
			26.6
			Top conc.
333.98	7.02		
333.97	46		
	floor		
	7.03		
	46 = floor		
334.53	6.47		
334.42	6.58		
333.7	7.3		
334.1	6.9		
334.2	6.8		
334.1	6.9		
334.6	6.4		
335.1	6.9		
	2.5		
	on wall		
			341.00

5+62 - 27 ft. 23.5 Lt. = 2.8 Conc. walk

5+54 - 1 1/2 Drive - 2 - 17 Conc. strips

5+50

5+41 - 17.9 Lt. = beg. 2" wood curb.

5+40 - 24.8 Rt. = 1/2 of 2.3 Conc. Step to Conc. walk

5+36 - 81 Lt. = 1/2 Sing. Gar. - Dirt floor (Prop. Conc.)

5+25 - 17.9 Lt. = end wood curb

5+25 - 24.9 Rt. = W. end of 6" Conc. wall

5+09 - 25 Lt. = 1/2 3' Conc. walk

5+06 - 29.8 Rt. = 1/2 3' Conc. walk

5+00

4+90 - 18' Lt. = beg. 2" Wood curb.

T.P. 4.51 344.45 1.06 339.94

s.w. 7' of  
Lands +  
Rose lawn

4+50

338.47

5.98  
23.5

Lt.

Rt.

Rt.

32

337.82

6.63

6.6  
81

Floor

337.75

6.70

25 = walk

337.3

7.1  
25

337.05

7.40  
18

336.2

4.8  
40

336.3

4.7  
25

336.0

5.0  
18

335.5

5.5  
25

335.7

5.3  
25

335.8

5.2  
25

336.2

4.8  
18

336.8

4.2  
20

337.0

4.0  
25

341.00

338.2

6.2  
25

338.0

6.4  
18

337.3

7.1  
25

337.7

6.7  
25

337.6

6.8  
25

338.5

6.9  
25

338.90

5.5  
24.8

1/2 step

339.69

4.7  
24.9

1/2 wall

337.8

5.6  
25

339.45

5.0  
26.0

Top walk

339.09

5.36  
29.8 = walk

339.49

4.96

27.8 Top Dr.







2+00

1+93 = ± 10' Dr. on Lt

1+82 = ± 10' Dr. on Rt.

1+75

1+50

1+49 = ± 9' Dr. on Rt

1+36 = ± of 10' Dr. on Lt.

1+15 = ± of 9' Dr. on Rt.

1+00

0+83 = ± 9' Dr. on Rt.

0+74 = ± 10' Dr. on Lt.

0+50

341.53  
341.03  
walk Dr.

341.37  
4.06  
15  
Top

341.18  
4.25  
15  
Top

341.13  
4.30  
17.5  
walk

340.65  
4.78  
17.5  
Top Dr.

341.03  
4.40  
15  
Dr.

341.0  
4.4  
15  
Top

340.8  
4.6  
15  
Top

340.43  
5.00  
15  
Dr.

339.97  
5.46  
15  
Bot Dr.

341.56  
3.87  
15  
Top

341.0  
4.4  
15  
Top

340.8  
4.6  
15  
Top

340.78  
4.65  
15  
Top

340.44  
4.99  
15  
Top

341.2  
4.2  
15  
Top

340.8  
4.6  
15  
Top

340.8  
4.6  
15  
Top

340.3  
5.1  
15  
Top

340.0  
5.4  
15  
Top

341.1  
4.3  
15  
Top

340.9  
4.5  
15  
Top

340.7  
4.7  
15  
Top

340.4  
5.0  
15  
Top

340.2  
5.2  
15  
Top

341.1  
4.3  
15  
Top

340.9  
4.5  
15  
Top

340.7  
4.7  
15  
Top

340.4  
5.0  
15  
Top

340.2  
5.2  
15  
Top

341.0  
4.4  
15  
Top

340.9  
4.5  
15  
Top

340.7  
4.7  
15  
Top

340.3  
5.1  
15  
Top

340.1  
5.3  
15  
Top

340.8  
4.6  
15  
Top

340.8  
4.6  
15  
Top

340.7  
4.7  
15  
Top

340.63  
4.80  
15  
Top

339.7  
5.5  
15  
Top

342.20  
3.23  
15  
Top

341.07  
4.36  
15  
Top

340.28  
5.5  
15  
Top

340.63  
4.80  
15  
Top

340.30  
5.13  
15  
Top

340.43  
5.00  
17.5  
Dr.

340.43  
4.25  
17.5  
walk

340.90  
4.53  
17.5  
walk

340.01  
5.42  
15  
Dr.

340.73  
4.70  
17.5  
walk

340.56  
4.87  
17.5  
walk

Lt=N

Rt=E

341.13

345.43

3+50

3+39 - ± 11' Dr. on Lt.

3+32 - ± 10' Dr. on Rt.

3+25

T.P. 3.84 343.69 5.58 339.85

3+00

2+84 - ± 10' Dr. on Rt.

2+82 - ± 10' Dr. on Lt.

2+75

2+50

2+48 - ± 10' Dr. on Rt.

2+38 - ± 10' Dr. on Lt.

2+25

2+16 - ± 10' Dr. on Rt.

339.77  
339.06

3.92 4.63  
17.5 15  
walk Dr.

340.10  
339.4  
339.7  
339.6  
339.5

340.91  
340.1  
340.4  
343.69  
340.3

341.36  
340.63  
4.07 4.80  
17.5 15  
walk Dr.

340.71  
341.1  
341.0  
341.0  
340.9

341.79  
341.12  
3.64 4.31  
17.5 15  
walk Dr.

341.71  
341.3  
341.2  
341.2  
341.1  
341.1  
341.35

3.72 4.1  
15 15  
Top gut

4.40 15  
5.0 5.0

340.10  
339.4  
339.7  
339.6  
339.5

340.91  
340.1  
340.4  
343.69  
340.3

341.36  
340.63  
4.07 4.80  
17.5 15  
walk Dr.

340.71  
341.1  
341.0  
341.0  
340.9

341.79  
341.12  
3.64 4.31  
17.5 15  
walk Dr.

341.71  
341.3  
341.2  
341.2  
341.1  
341.1  
341.35

3.72 4.1  
15 15  
Top gut

4.40 15  
5.0 5.0

340.10  
339.4  
339.7  
339.6  
339.5

340.91  
340.1  
340.4  
343.69  
340.3

341.36  
340.63  
4.07 4.80  
17.5 15  
walk Dr.

340.71  
341.1  
341.0  
341.0  
340.9

341.79  
341.12  
3.64 4.31  
17.5 15  
walk Dr.

341.71  
341.3  
341.2  
341.2  
341.1  
341.1  
341.35

3.72 4.1  
15 15  
Top gut

4.40 15  
5.0 5.0

340.10  
339.4  
339.7  
339.6  
339.5

340.91  
340.1  
340.4  
343.69  
340.3

341.36  
340.63  
4.07 4.80  
17.5 15  
walk Dr.

340.71  
341.1  
341.0  
341.0  
340.9

341.79  
341.12  
3.64 4.31  
17.5 15  
walk Dr.

341.71  
341.3  
341.2  
341.2  
341.1  
341.1  
341.35

3.72 4.1  
15 15  
Top gut

4.40 15  
5.0 5.0

340.10  
339.4  
339.7  
339.6  
339.5

340.91  
340.1  
340.4  
343.69  
340.3

341.36  
340.63  
4.07 4.80  
17.5 15  
walk Dr.

340.71  
341.1  
341.0  
341.0  
340.9

341.79  
341.12  
3.64 4.31  
17.5 15  
walk Dr.

341.71  
341.3  
341.2  
341.2  
341.1  
341.1  
341.35

3.72 4.1  
15 15  
Top gut

4.40 15  
5.0 5.0

340.10  
339.4  
339.7  
339.6  
339.5

340.91  
340.1  
340.4  
343.69  
340.3

341.36  
340.63  
4.07 4.80  
17.5 15  
walk Dr.

340.71  
341.1  
341.0  
341.0  
340.9

341.79  
341.12  
3.64 4.31  
17.5 15  
walk Dr.

341.71  
341.3  
341.2  
341.2  
341.1  
341.1  
341.35

3.72 4.1  
15 15  
Top gut

4.40 15  
5.0 5.0

340.10  
339.4  
339.7  
339.6  
339.5

340.91  
340.1  
340.4  
343.69  
340.3

341.36  
340.63  
4.07 4.80  
17.5 15  
walk Dr.

340.71  
341.1  
341.0  
341.0  
340.9

341.79  
341.12  
3.64 4.31  
17.5 15  
walk Dr.

341.71  
341.3  
341.2  
341.2  
341.1  
341.1  
341.35

3.72 4.1  
15 15  
Top gut

4.40 15  
5.0 5.0

340.10  
339.4  
339.7  
339.6  
339.5

340.91  
340.1  
340.4  
343.69  
340.3

341.36  
340.63  
4.07 4.80  
17.5 15  
walk Dr.

340.71  
341.1  
341.0  
341.0  
340.9

341.79  
341.12  
3.64 4.31  
17.5 15  
walk Dr.

341.71  
341.3  
341.2  
341.2  
341.1  
341.1  
341.35

3.72 4.1  
15 15  
Top gut

4.40 15  
5.0 5.0

340.10  
339.4  
339.7  
339.6  
339.5

340.91  
340.1  
340.4  
343.69  
340.3

341.36  
340.63  
4.07 4.80  
17.5 15  
walk Dr.

340.71  
341.1  
341.0  
341.0  
340.9

341.79  
341.12  
3.64 4.31  
17.5 15  
walk Dr.

341.71  
341.3  
341.2  
341.2  
341.1  
341.1  
341.35

3.72 4.1  
15 15  
Top gut

4.40 15  
5.0 5.0

340.10  
339.4  
339.7  
339.6  
339.5

340.91  
340.1  
340.4  
343.69  
340.3

341.36  
340.63  
4.07 4.80  
17.5 15  
walk Dr.

340.71  
341.1  
341.0  
341.0  
340.9

341.79  
341.12  
3.64 4.31  
17.5 15  
walk Dr.

341.71  
341.3  
341.2  
341.2  
341.1  
341.1  
341.35

3.72 4.1  
15 15  
Top gut

345.43



I.P. 6.24 341.03 8.90 334.79

4+77.5 =  $\Phi$  inlet on Lt. = Same Dimensions  
16" R.C. Culvert across Road and to East along curb.

4+76 =  $\Phi$  of inlet on Rt. = 2' x 2.5' box + grate + 6 opening

4+75

4+50

4+39 =  $\Phi$  9' wood Dr. on Lt. - curb not broken - wood in st.

4+38 =  $\Phi$  8' Dr. on Rt.

4+27 =  $\Phi$  10' Dr. on Lt. = Not used - High wall at prop

4+25

4+21 =  $\Phi$  11' Dr. on Rt.

4+00

3+83 =  $\Phi$  9' Wood Dr. on Lt. - curb not broken - wood in st.

3+75

8.70 1.5 Top cb.	334.99	11.34 1.5 FL. Box	332.35	9.51 1.5 Top grate	334.18	9.30 1.5 12.5 = edge grate	334.39	9.60 1.5 12.5 = edge Grate	333.89	10.03 1.5 9.4 = Top Grate	333.66	11.91 1.5 1.5 = Top of box	331.78	9.18 1.5 15 = Top cb	334.51
8.65 1.5 Top	335.04	9.14 1.5 Top	334.3	8.9 1.5 Top	334.8	9.0 1.5 Top	334.7	9.9 1.5 9.4 = on conc. of inlet	334.6	7.13 1.5 15 = Top cb.	333.71	7.13 1.5 15 = Top cb.	331.78	334.51	
7.8 1.5 Top	335.87	8.3 1.5 Top	335.4	8.3 1.5 Top	335.4	8.4 1.5 Top	335.3	8.6 1.5 Top	335.1	9.0 1.5 Top	334.7	8.38 1.5 Top	335.37	335.74	
7.0 1.5 Walk Dr.	336.69	7.6 1.5 Walk Dr.	336.77	7.6 1.5 Walk Dr.	336.08	7.5 1.5 Walk Dr.	336.2	7.5 1.5 Walk Dr.	336.2	7.7 1.5 Walk Dr.	336.0	7.7 1.5 Walk Dr.	335.69	336.24	
6.92 1.5 walk	337.60	7.6 1.5 walk	336.77	7.6 1.5 walk	336.08	7.5 1.5 walk	336.2	7.5 1.5 walk	336.2	7.7 1.5 walk	336.0	7.7 1.5 walk	335.69	336.24	
6.09 1.5 Top	337.60	6.09 1.5 Top	337.60	6.09 1.5 Top	337.60	6.09 1.5 Top	337.60	6.09 1.5 Top	337.60	6.09 1.5 Top	337.60	6.09 1.5 Top	337.60	337.60	
5.28 1.5 Top	338.41	5.28 1.5 Top	338.41	5.28 1.5 Top	338.41	5.28 1.5 Top	338.41	5.28 1.5 Top	338.41	5.28 1.5 Top	338.41	5.28 1.5 Top	338.41	338.41	
5.1 1.5 Top	338.1	5.1 1.5 Top	338.1	5.1 1.5 Top	338.1	5.1 1.5 Top	338.1	5.1 1.5 Top	338.1	5.1 1.5 Top	338.1	5.1 1.5 Top	338.1	338.1	
5.1 1.5 Top	338.0	5.1 1.5 Top	338.0	5.1 1.5 Top	338.0	5.1 1.5 Top	338.0	5.1 1.5 Top	338.0	5.1 1.5 Top	338.0	5.1 1.5 Top	338.0	338.0	
5.1 1.5 Top	338.0	5.1 1.5 Top	338.0	5.1 1.5 Top	338.0	5.1 1.5 Top	338.0	5.1 1.5 Top	338.0	5.1 1.5 Top	338.0	5.1 1.5 Top	338.0	338.0	
5.1 1.5 Top	337.8	5.1 1.5 Top	337.8	5.1 1.5 Top	337.8	5.1 1.5 Top	337.8	5.1 1.5 Top	337.8	5.1 1.5 Top	337.8	5.1 1.5 Top	337.8	337.8	
5.1 1.5 Top	337.4	5.1 1.5 Top	337.4	5.1 1.5 Top	337.4	5.1 1.5 Top	337.4	5.1 1.5 Top	337.4	5.1 1.5 Top	337.4	5.1 1.5 Top	337.4	337.4	
5.1 1.5 Top	337.94	5.1 1.5 Top	337.94	5.1 1.5 Top	337.94	5.1 1.5 Top	337.94	5.1 1.5 Top	337.94	5.1 1.5 Top	337.94	5.1 1.5 Top	337.94	337.94	
5.1 1.5 Top	343.69	5.1 1.5 Top	343.69	5.1 1.5 Top	343.69	5.1 1.5 Top	343.69	5.1 1.5 Top	343.69	5.1 1.5 Top	343.69	5.1 1.5 Top	343.69	343.69	

Rt. = E

6+35.32 = opp S. end of 34 Conc gut. on Lt. (poor Cond)

335.40  
5.15  
16.7  
Top gut.  
cb. Ret.

336.11  
4.92  
20  
edge walk

335.39  
5.64  
13.5  
outside gut.

336.01  
5.10  
10.2  
Top PC.  
Ret.

335.4  
5.16  
7.8

336.2  
4.8

335.9  
5.1

335.7  
5.1

336.50  
4.53

336.65  
4.38  
20 = edge walk

6+27.32 = S.L. Landis

6+00

5+67 = \$ 10' Dr. on Rt.

335.56  
5.47  
17.5  
walk

334.95  
6.08  
9.5

335.40  
5.10  
7.8

335.2  
5.10  
7.8

335.2  
5.10  
7.8

335.5  
5.10  
7.8

335.6  
5.10  
7.8

335.5  
5.10  
7.8

336.13  
5.10  
7.8

335.02  
6.01  
Dr.

335.71  
6.32  
20  
on walk

5+62 = \$ 11' Dr. on Lt.

5+50

5+21 = \$ 10' Dr. on Lt.

335.22  
5.81  
17.5  
walk

334.61  
6.42  
5

335.46  
5.10  
7.8

334.7  
5.10  
7.8

334.8  
5.10  
7.8

335.0  
5.10  
7.8

335.0  
5.10  
7.8

334.8  
5.10  
7.8

335.33  
5.10  
7.8

5+00

4+84 = \$ 10' Dr. on Rt.

335.08  
5.81  
17.5  
walk

334.61  
6.42  
5

335.08  
5.10  
7.8

334.3  
5.10  
7.8

334.7  
5.10  
7.8

334.77  
5.26  
7.8

334.4  
5.10  
7.8

334.2  
5.10  
7.8

334.69  
5.10  
7.8

334.13  
6.90  
Dr.

334.57  
6.46  
17.5  
walk

341.03



Cross Sec. Hornblend  
Ingraham to Jewell  
to establish grade.

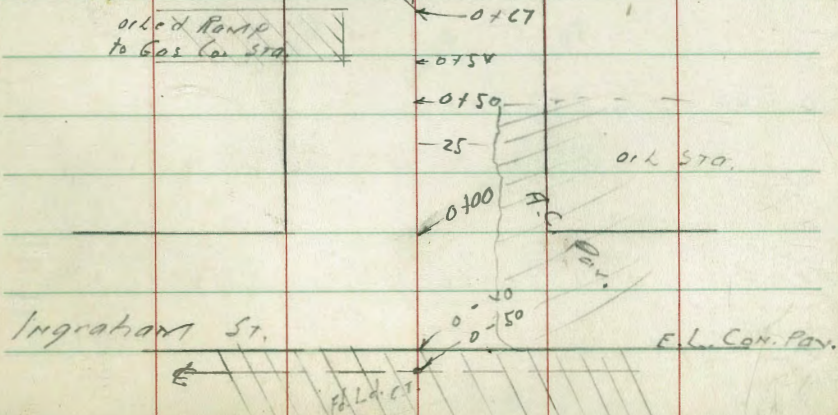
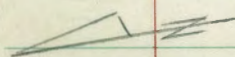
C. Moore  
Begg  
Cress  
Roberts

W.D. # 270 2-20-47

Indexed  
C.S.K.

41

Jewell



10' R.  
Returns in  
same as  
5' R. Con.

Curve  
Line

4+99.5

40 - 20'

3+99.6

R.10

50'  
50'

11' W  
MARKS

4+00 = Cypress Tree

20'

0-00 = E.L. Ingraham

T.P. 8.18 69.44 270 1076

0-06

0-20

0-30

0-40 = E.L. Cox Pay.

NEBP 7.61 63.46 5585

Grand and  
Ingraham

LT. = Month

\$

P<sub>1</sub>

42

L.O	8.4	9.7	9.7	2.59	9.32
40	33	16		20	40
63.4	61.0	59.7	59.7	edge Pay	Pay
				59.85	60.12

69.44

60.6

2.8  
40

60.0

3.4  
20

59.9  
3.5

59.6  
3.50

60.08

3.38  
40

59.9

2.5  
40

59.6

3.8

59.9

3.67

59.6

3.50

61.5

3.5  
40

59.9

3.5

59.9

3.71

59.62

3.84

60.38

3.08  
40

60.12

2.34

59.87

3.59  
40

63.46



2+00

1+91 25 LT 1x" di Pop. 2000

1+26 26 RT 18" di Pop. 2000

1+55 25 LT 1x" di Pop. 2000

1+50

1+46 26 RT 1x" di pop. 2000

1+16 24 LT 1x" di pop. 2000

1+05 25 RT P.P.

1+00

0+91 24 LT olive tree

0+77 8 18" Bank Walk

L944

68.7	65.8	65.9	64.9	64.8	64.1	64.4	64.5
0.7	3.6	3.9	3.5	4.5	4.6	5.8	4.9
40	35	20	15	10	17	21	20

65.5

69.0	68.6	68.5	68.0	68.94	68.3	68.1	68.4
2.4	4.0	3.9	5.4	5.5	5.1	5.6	4.0
40	37	20	11	5	18	22	20

65.6	64.3	64.2	62.9	62.84	62.4	62.4	62.7
3.8	5.1	5.2	6.5	6.5	7.0	6.0	5.7
40	38	20	11	5	18	29	20

62.90  
5.24  
41

L944

3 + 50

$\frac{1.6}{40}$	$\frac{2.1}{30}$	$\frac{2.6}{20}$	$\frac{3.3}{11}$	$\frac{4.2}{7}$	$\frac{5.5}{18}$	$\frac{6.3}{24}$	$\frac{6.5}{40}$
------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------

3 + 48 26 Lt 12" di. Pop. tree

$\frac{1.6}{40}$	$\frac{2.1}{30}$	$\frac{2.6}{20}$	$\frac{3.3}{11}$	$\frac{4.2}{7}$	$\frac{5.5}{18}$	$\frac{6.3}{24}$	$\frac{6.5}{40}$
------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------

3 + 00

+ 75 25 Lt 12" di. Pop. tree

+ 70 25' Pt 12" Pop. tree

T.P. 3.44 66.97 5.91 63.53

$\frac{3.1}{36}$	$\frac{4.5}{20}$	$\frac{5.0}{15}$	$\frac{5.7}{11}$	$\frac{6.2}{7}$	$\frac{6.7}{17}$	$\frac{7.3}{35}$	$\frac{7.8}{60}$
------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------

2 + 50

$\frac{2.4}{40}$

+ 35 26 Pt 12" di. Pop. tree

2 + 33 25 Lt 10" di. Pop. tree

2 + 06 25' Pt 15" di. Pop. tree

69.44

69.44



Check to BM BP NW Cor.  
Grand Jewell

8.91 51.8x 51.80  
0.00

T.P. 1.58 6.75 7.80 5.97

E.L. Jewell

E. c. b. Line Jewell

Jewell = 40' betw. Curbs

5+19.5 W. c. b. Line Jewell

4+99.5 W.L. Jewell

+53 26 LT 30" di. Fan Palm

4+50

4+16 26 LT 30" Fan Palm

31996 <sup>old</sup> 809 curb + walk on RT

66.97

LT

R

R

46

61.85  
5.12  
20  
Top  
Curb

60.5  
6.4  
20

60.2  
6.7

59.1  
7.8  
20

59.9  
7.02  
20  
Top  
c. b.

61.83  
5.14  
40  
Top  
Ret.

59.9  
7.09  
40  
Top  
c. b. Ret.

59.9  
6.98  
40  
Top  
c. b. Ret.

62.3  
4.6  
40

61.9  
5.0  
20

60.8  
6.1  
11

60.5  
6.4  
20

59.5  
7.4  
20

60.0  
6.97  
20  
Top  
Curb

60.2  
6.7  
40

63.1  
3.8  
40

62.7  
4.6  
20

61.5  
5.7  
9

61.0  
5.9  
20

60.0  
6.9  
20

60.6  
6.31  
20  
Top  
c. b.

60.9  
6.0  
40

63.9  
3.0  
40

63.4  
3.5  
38

63.3  
3.6  
15

62.1  
4.8  
11

61.6  
5.3  
20

60.6  
6.3  
20

61.34  
5.63  
20  
Top  
c. b.

61.5  
5.1  
40

66.97

Survey for drain  
 South of Bird Rock Add.  
 Ocean to La Jolla Mesa Dr.  
 South of COLIMA Ave.

Indexed  
 c.s. No.

417

MOORE  
 3599  
 GREER  
 ROBERTS  
 5-21-47

La Jolla Blvd

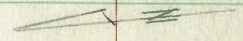
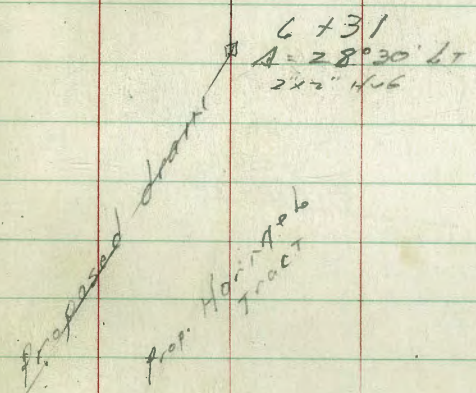
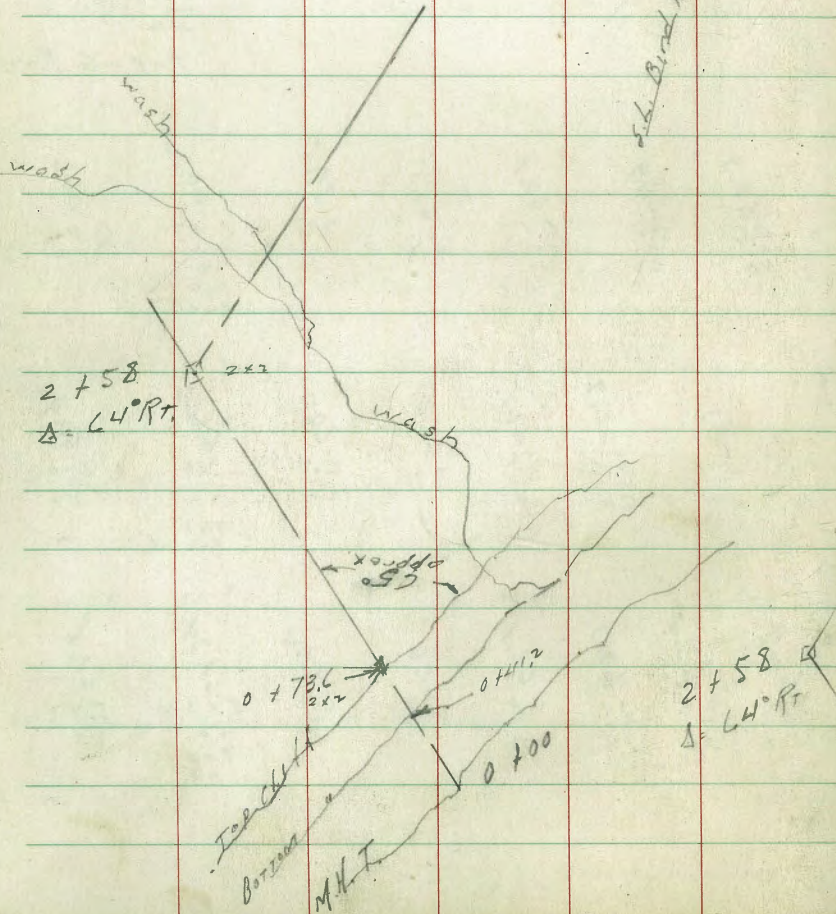
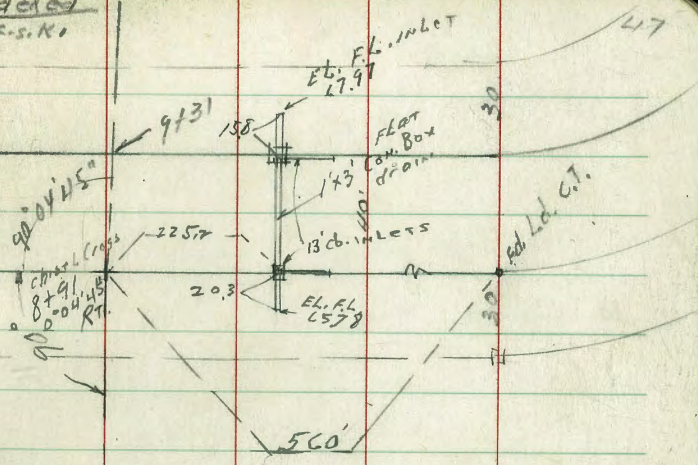
W.O. 90041

Rd. Bird Rock  
 Rd. Gran Moron

E. Curb

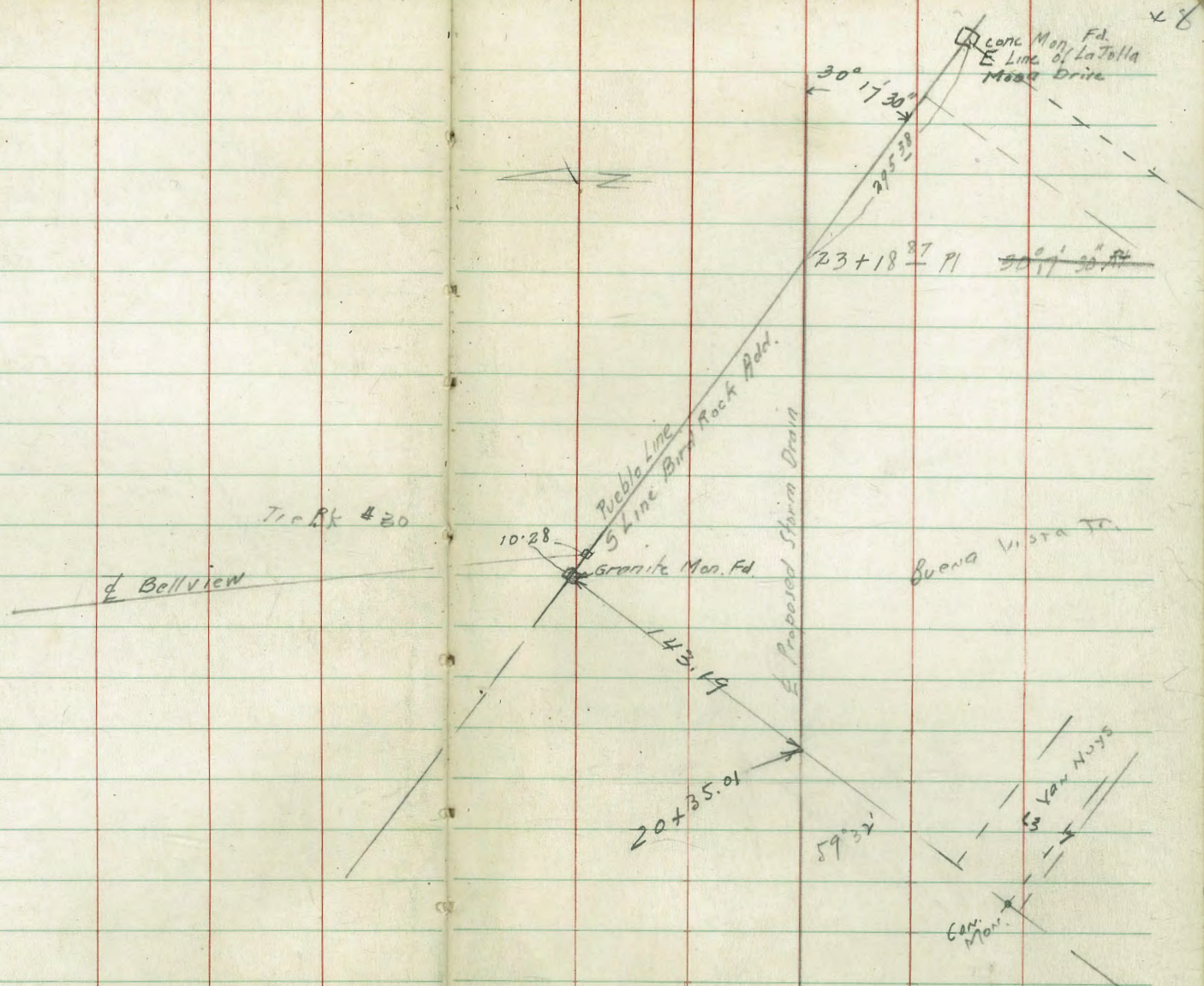
W. Curb

m



73.99  
 8.21  
 65.78 output

73.99  
 6.02  
 67.97 INLET



Conc Mon. Fd.  
E Line of La Jolla  
Mass Drive

30° 17' 30"

275.38

23 + 18 87 71

~~209' 30"~~

Twp Rk 420

10.28

Pueblo Line  
E Line of Bird Rock Add.  
Granite Mon. Fd.

Bellview

Suena Vista Tr.

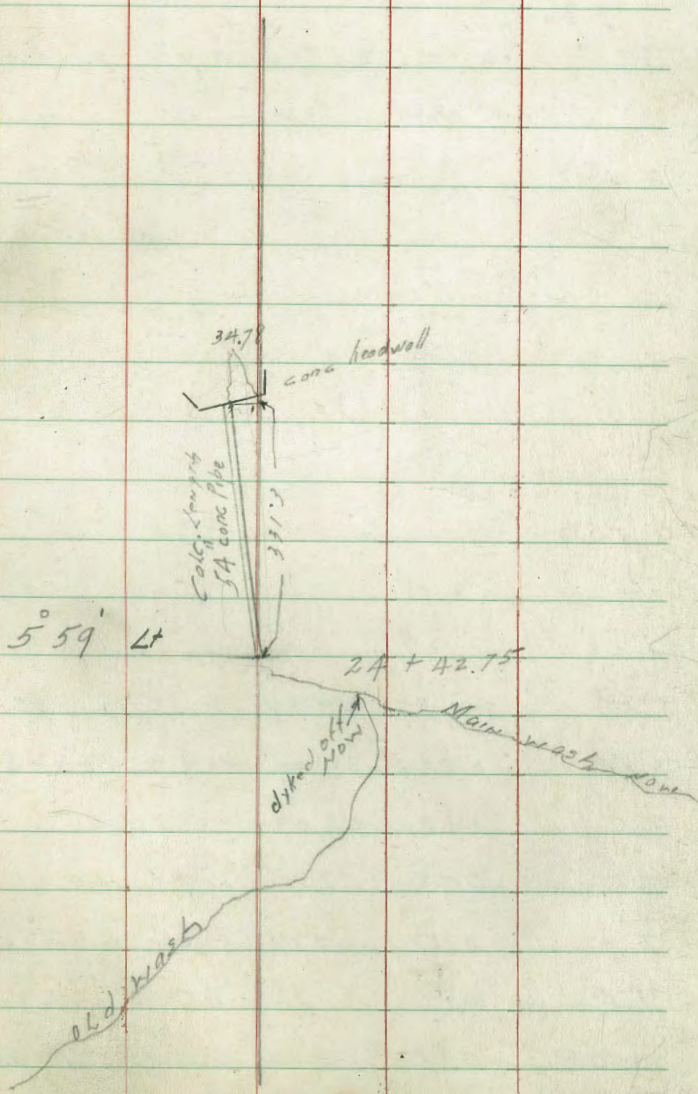
20 x 35.01

143.19

59.21

23 Van Nuys

Conc Mon.



Draw Levels

LT = 114

\$

Rt

50

0 + 73.6

38.8	<del>26.7</del>	30.3	26.2	29.6	13.6	-0.2	-6.5
<u>712.1</u>	<u>+10.9</u>	<u>+3.6</u>	0.5	<u>2.1</u>	<u>13.1</u>	<u>27.1</u>	<u>33.2</u>
81	50	32			25	46	96

fence

Top of Cliff  
Main of Wash

T.P. 2.10 24.70 ✓ 0.44 24.60

24.70 ✓

0 + 41

280	170	0.9	-3.0
<u>+3.0</u>	<u>8.0</u>	<u>24.1</u>	<u>28.0</u>
43	50	83.5	80

Top of Cliff  
fence

0 + 20

1.2	0.4	-2.2	-6.0
<u>23.8</u>	<u>24.6</u>	<u>28.2</u>	<u>31.0</u>
78	50		100

80.5  
Cliff

0 + 00 Sec. at 90°

-2.4	-3.8	-2.4	-7.5
<u>27.4</u>	<u>28.8</u>	<u>29.4</u>	<u>32.5</u>
100	50		100

T.P. 2.19 25.04 ✓ 11.95 22.85

25.04 ✓

T.P. 0.86 34.80 ✓ 12.55 33.94

T.P. 1.48 46.59 ✓ 12.39 45.11

T.P. 0.25 57.50 ✓ 12.54 57.25

T.P. 0.42 69.79 ✓ 4.34 69.37 ✓

Top of N. of 8 + 91

T.P. 4.14 73.71 ✓ 8.77 69.59

SxxBP 0.38 78.36 ✓ 77.98 old City datum

La Jolla Blvd & Colima

1+90

1+67

T.P. 10.60 35.20 2.10 24.60

1+55

1+28

This wash is to be filled up,  
lim. told.

1+05

0+85

26.70

L

E

R

51

93.1	92.6	39.6	27.2	16.1	16.2	25.7	28.6	25.8
+7.9	+7.4	0.6	8.0	19.1	19.0	9.5	6.6	3.1
100	42	24		15	21	38	63	76
				Wash				

91.7	92.9	92.9	30.7	29.3	21.9	19.1	13.1	15.0	22.9	32.6
+6.5	+7.2	+7.2	4.5	5.9	13.8	2.1	22.1	20.7	12.8	2.0
70	43	40	17		25	35	40	50	80	100
	Fence				Wash					

35.20

91.7	92.2	31.9	30.2	29.0	20.3	11.3	11.5	28.3	22.7
+15.0	+15.5	+4.7	+3.5	2.7	6.4	15.4	15.2	+1.6	4.0
57	36	16		35	46	72	77	83	107
	Fence				Wash				
								Top	Cliff

90.9	91.8	91.8	30.2	28.5	29.5	14.9	6.6	6.6	16.9
+14.2	+15.1	+15.1	+3.5	+1.8	2.2	11.8	20.1	20.1	60.9
100	70	39	14		17	33	22	49	68
	Fence					Wash			Top
									Cliff

90.7	91.1	39.9	29.7	26.7	9.2	9.2	15.0	9.2	-0.9
+14.0	+14.4	+12.7	+3.0	0.0	22.5	22.5	11.7	17.5	27.1
100	82	33	15		28	32	27	78	82
					Wash			Top	Beach
								Cliff	

39.8	38.8	30.5	20.7	18.9	2.2	-0.3	-0.5	-5.3
+13.1	+12.1	+3.0	0.0	8.3	24.5	27.0	27.2	37.0
100	81	37	17	16	34	50	65	100
	Fence				Wash			Top
	St. Mary							Cliff
	Gun School							on Beach
					<u>26.70</u>			

3+07

3+07

2+93

2+87

2+80 Sec. 90°

2+58 A 64° R Sec. on split A

T.P 11.92 45.94 1.18 34.02

2+30 Sec. 90°

35.20

Lt

ε

R

52

36.7  
9.7  
6.5

36.6	31.6	27.2	31.7	27.9	22.8	27.7	36.9	39.2
9.3	14.3	18.7	14.7	10.	23.1	18.7	9.5	6.7
87	57	xx Wash	33		8 sly Wash	14	38	50

47.9	23.7	20.8	21.9	39.8	39.6	36.6
+2.0	22.2	25.1	24.5	11.1	6.3	10.3
87	33	Wash	15	3.5	52	70

47.7	45.3	23.7	20.9	19.8	32.6	38.5	35.2
+1.8	0.6	22.2	25.0	26.1	13.3	7.4	10.7
87	63	22	Wash	16	34	52	71

47.9	42.0	33.2	28.8	19.2	30.8
+2.0	1.9	12.5	17.1	26.5	15.1
100	46	16		20	32

45.9	45.3	35.9	19.2	19.2	34.7	36.9
0.0	0.6	18.0	26.7	26.7	14.2	9.0
100	16		28	33	41	67
			Wash			

45.94 ✓

44.6	49.7	49.2	28.7	17.6	17.5	30.9	39.2
+9.4	+9.5	+9.0	6.5	17.6	17.7	4.8	0.8
100	57	26		17	20	32	45
				Wash			

35.20 ✓

4+50

4+20

3+80

T.P. 7.16 5.118 1.97 4.402

3+58

3+30

3+16

4594

53

LT                      ♀                      RT

51.0	49.6	49.9	48.8	48.8
0.2	1.6	1.8	7.4	7.4
100	50		50	90

48.8	47.9	49.3	45.9	46.9	48.8	38.9	39.0
2.4	3.8	1.9	5.3	4.8	6.4	12.3	12.7
100	92	50		34	50	82	100

49.0	38.9	46.3	43.9	42.3	42.8
2.2	12.8	4.9	7.3	8.9	8.4
100	73	50		50	80

sly wash

5.118

47.7	46.2	38.2	37.0	39.9	41.8	41.3	39.3	38.7
11.8	0.7	11.7	8.9	6.0	4.1	4.6	6.6	7.7
100	76	44	41	24		35	50	76

Wash

49.9	48.9	39.7	28.8	32.6	33.5	38.3	37.0	36.6
1.5	2.0	11.7	17.1	13.3	12.4	7.6	8.1	9.3
66	56	27	18	12		30	50	76

Wash

30.9	30.3	37.1	29.2	25.9	30.1	37.9	39.2	36.6
15.0	15.6	8.8	16.7	20.5	15.8	8.0	6.7	9.3
100	78	45	11	Wash	6	37	50	63

sly Wash Wash

4594



7+00

6+50

6+31 @ 28°30' Lt Sec on split

6+00

T.P. 920 44.32 0.85 5717

+50

5+00

T.P. 773 57.97 0.94 5024

5118

Lt

£

Pt

60.2 60.3 60.6 60.2 59.7  
6.1 6.0 5.7 6.1 6.6  
100 50 50 100

57.7 57.9 58.2 58.0 57.8  
8.6 8.4 8.1 8.3 8.5  
100 50 50 100

58.1 57.8 57.5 56.5 55.9  
8.7 8.5 8.8 9.8 10.4  
100 50 50 100

58.1 57.1 56.3 55.8 53.7  
8.7 9.2 10.0 11.5 12.6  
100 50 50 100

66.32 ✓

56.8 58.7 58.2 57.9 52.2  
1.7 3.3 3.8 5.1 5.8  
100 50 50 96

55.2 53.5 52.8 50.9 48.1 43.6  
2.8 4.5 5.6 7.1 9.9 14.4  
100 50 25 50 92

57.97 ✓

65.11  
 8 + 91 w/ly gutter  
 4 0"0" x 5" R<sub>r</sub> La Jolla Blvd.  
 F.L. outlet  
8.88

8 + 91 w/ly cb. line  
 La Jolla Blvd.

8 + 61 w/ly La Jolla Blvd.

8 + 50

T.P. 777 7399 010 66.22

8 + 00

7 + 50

66.32

55

	65.20	67.90	68.98	68.99	69.06	69.15	69.19	68.92	65.92
	8.79	6.09	5.05	5.00	4.93	4.84	4.80	5.05	8.05
	472.9	472.9	100	50	50	50	100	225.2	225.2
	F.L. Box	grate					grate		F.L. Box

	68.85	69.33	69.37	69.25	69.55	69.62	69.92
	5.14	4.66	4.62	4.54	4.24	4.37	4.07
	472.9	100	50	50	50	100	225.2
	C.P. inlet						Top cb.
	Top curb						

	66.8	66.6	66.8	67.0	66.7
	7.7	7.4	7.2	7.0	7.3
	100	50		50	100

	66.2	66.1	66.3	66.7	65.9
	7.8	7.9	7.7	7.3	8.1
	100	50		50	100

73.99

	62.5	62.2	62.2	62.6	62.5
	1.8	2.1	2.1	1.7	1.8
	100	50		50	100

	62.2	62.2	62.5	62.2	61.9
	4.1	4.1	3.8	3.9	2.4
	100	50		50	100

66.37

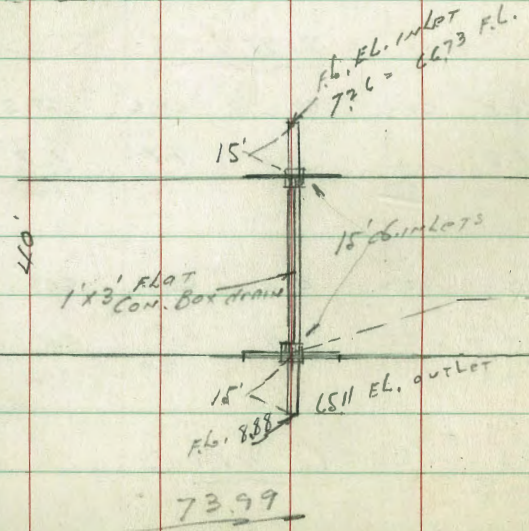
9+61 E.L. to Jolla Blvd.  
 9+41 68 ft 8" d. Eucaly.  
 9+37.6 14' LT PP. 132 68 ft PP. 131

check to T.P. Top curb  
 P. 50 461 69.38 69.37

9+31 Ely curb La Jolla Blvd.  
 464  
 472.9  
 CTR. Inlet  
 Top cb

9+31 E. gut Blvd.  
 66.72 68.54  
 7.28 5.45  
 472.9 472.9  
 FL. Box 9997c

La Jolla  
 4+11 E Blvd.



LT	E	PT
71.6	71.3	71.1
2.4	2.7	2.9
100	50	50
		71.7
		72.0
		2.0
		100

69.87	69.99	70.01	70.10	70.21	70.98
4.17	4.00	3.98	3.89	3.78	3.51
100	50	50	100		225.4
					Top ob.

69.12	69.16	69.22	69.27	69.36	69.55	69.69
4.85	4.83	4.75	4.72	4.63	4.44	6.10
100	50	50	100	225.2	225.2	
				grate		FL. Box

69.61	69.65	69.73	69.82	69.92
4.38	4.34	4.26	4.17	4.05
100	50	50	100	

472.9

8+91  
 1=0.0445K  
 chisel  
 cross Top cb.  
 73.99 ✓

Ely Curb  
 La Jolla Blvd.  
 wly curb

12 + 50

T.P. 1231 95.59 0.58 8328

12 + 35 101 R, RP J.R. 5308  
33 L, PP J.P. 5318.

12

+ 50

11

+ 50

10 + 00

T.P. 1232 83.86 2.49 71.50

73.99

Lt

¢

Rt

57

89.5 89.3 89.2 89.6 83.8 78.9 77.0 89.9

11.1 11.3 11.4 11.0 11.8 14.7 16.6 11.7  
100 50 50 93 95 99 100  
ditch

95.59 ✓

80.8 80.6 80.7 81.0 81.6 76.4 77.7 81.9  
3.1 3.3 3.2 2.9 2.3 7.7 6.7 2.5  
100 50 50 70 92 99 100  
ditch

78.5 78.5 78.5 78.7 78.7  
5.4 5.4 5.4 5.7 5.7  
100 50 50 100

76.2 76.2 76.4 76.7 76.7  
7.4 7.5 7.7 7.7 7.2  
100 50 50 100

75.2 74.2 74.9 74.9 75.0  
8.7 9.7 9.5 9.0 8.9  
100 50 50 100

73.1 72.5 72.2 72.9 73.3  
10.8 11.4 11.7 11.0 10.6  
100 50 50 100

83.86 ✓

150

101.3	100.2	99.9	99.0	98.3
5.7	6.8	7.1	8.0	8.7
100	50		50	100

15

97.5	97.9	96.8	96.2	95.9
9.5	9.6	10.2	10.4	11.6
100	50		50	100

T.P. 1250 10702 1.13 94.46

10702 ✓

150

95.9	99.6	93.8	93.3	92.8
0.2	1.0	1.8	2.3	2.8
100	50		50	100

14

91.3	91.1	90.5	90.3	90.9
4.3	4.5	5.1	5.3	4.7
100	50		50	100

150

89.2	88.8	88.9	88.3	88.3
6.4	6.8	7.2	7.3	7.3
100	50		50	100

13

86.9	86.3	86.0	86.0	86.2	86.5	86.0	86.3
9.2	9.3	9.6	9.6	9.4	9.1	14.6	9.3
100	50		50	100	120	124	127

95.59

95.59 ✓

ditch goes  
sly from  
here

+50

T.P. 12.30 128.91 0.17 116.55

1.8

+50

17

T.P. 70.89 116.72 11.9 105.83

+50

16

107.02

116.5	116.8	116.5	116.9	116.3
12.3	12.5	12.4	12.0	12.6
100	50		50	100

128.91

113.6	113.2	113.6	113.7	113.0
3.1	3.5	3.1	3.0	3.7
100	50		50	100

110.5	110.6	110.7	110.3	109.9
6.2	6.1	6.0	6.4	6.8
100	50		50	100

108.3	108.2	108.0	107.9	106.8
8.4	8.5	8.7	9.3	9.9
100	50		50	100

116.72

106.9	105.8	105.1	104.7	104.0
0.6	1.2	1.9	2.3	3.0
100	50		50	100

103.9	102.8	102.3	101.6	100.9
3.1	4.2	4.7	5.4	6.1
100	50		50	100

107.02

LT

E

R

130.5	130.9	128.6	131.6	132.5	133.9	133.2	133.3
8.1	8.2	10.0	10.3	7.0	6.1	5.7	5.4
100	100	100	100	100	100	100	100
	93	88	83	75	50	50	50
	old wash						

21

129.5	130.9	130.5	130.1	130.6
9.1	8.2	8.1	8.5	8.0
100	50	50	50	100

T.P. 9.87 1.3859 0.19 128.72

1.3859 ✓

±50

127.6	127.7	127.3	127.3	127.5
1.3	1.2	1.6	1.6	2.4
100	50	50	50	100

20

125.0	125.2	129.7	125.1	125.9
3.9	3.7	4.2	3.8	2.5
100	50	50	50	100

±50

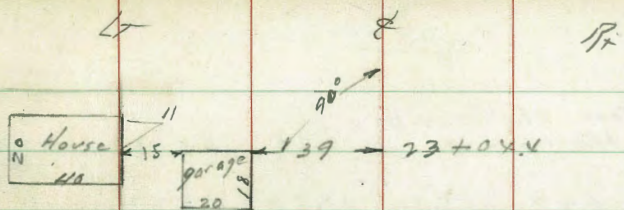
121.8	122.1	121.9	121.8	121.1
7.1	6.8	7.0	7.1	7.8
100	50	50	50	100

19

119.7	119.2	119.0	118.9	118.3
9.2	9.7	9.9	10.0	10.2
100	50	50	50	100

12891

12891 ✓



23

140.6	141.0	142.2	138.7	140.9	141.9
4.7	6.3	7.1	9.1	6.4	5.4
40		43	53	65	100
			ditch		

150

140.5	136.9	137.0	139.7	138.5	139.9
6.8	10.4	10.3	12.6	8.8	7.9
70	50		13	40	100
			ditch		

138

135.7	135.9	136.1	139.9	137.9	138.3
11.6	11.4	11.2	12.9	9.9	9.0
83	50	13	ditch	12	50
					100

128

135.0	135.1	135.3	139.0	136.2	137.8	137.9	137.8
12.3	12.2	12.0	12.2	11.1	9.5	9.4	9.5
100	50	79	10		22	50	100
			ditch				

22

133.9	133.9	132.9	131.7	133.6	134.9	135.8	135.7	136.3
13.4	13.4	10.4	15.6	13.7	12.4	11.5	11.6	11.0
100	50	29	25	70	6		50	100
			ditch					

T.P.

1123 147.29 2.53 136.06  
138.59 ✓

147.29 ✓



overs

check to Mon. E.L. Mission Blvd.  
 S 7' of Archer St. 12.44 123.06 123.28  
 T.P. 0.29 135.50 12.68 135.21  
 T.P. 0.64 147.89 12.64 147.25  
 T.P. 0.70 159.89 13.04 159.19  
 inlet of 54" Con. Pipe 11.01 161.22 INVERT  
 T.P. 3.62 172.73 1.82 168.61  
 T.P. 12.72 170.43 0.70 157.71  
 24 + 42.75 outlet Ex. 11.32 147.19 INVERT  
 54" Con. Pipe

#15

24

T.P. 11.74 158.41 0.62 146.67

23 + 50

147.29

L7

8

R7

62

152.6 152.9 198.5 199.8 199.9 153.0  
 5.8 5.5 99 8.6 8.5 54  
 30 15 det 3 13 29  
 filled

150.0 151.0 192.8 193.9 195.2 192.7

8.4 74 14.0 15.0 13.2 10.7  
 50 50 8.2 85 100  
 new  
 wash

198.7 199.3 199.9 192.2 199.3 193.7

9.7 9.1 13.5 16.2 14.1 14.7  
 50 50 7.5 84 100  
 new  
 wash

158.41

199.1 199.8 199.0 191.2 192.3 193.3

3.2 29 3.3 6.1 5.0 4.0  
 50 27 42 46 100  
 old  
 ditch  
 end

147.29

135.50 ✓

T.P. 2.34 126.85 ✓ 10.99 124.51

T.P. 2.14 116.95 ✓ 12.04 114.81

T.P. 0.61 104.75 ✓ 12.81 104.14

T.P. 0.55 94.72 ✓ 10.58 94.17

T.P. 2.65 86.75 ✓ 10.62 84.10

T.P. 5.56 80.15 ✓ 12.16 74.59

check to orig. B.M. 2.15 78.00 ✓ 77.98

Notes Reduced Pgs. 50 to 63  
P. 6.2.87



Grades Alley Between 37th St & Cherokee & Orange & El Cajon

Sta.	+	H. I.	Lt.	Elev.	Elev.	Cut. Lt.	Rod. Rt.	Elev.	Elev.	Cuts. Rt.
CR W. Ch. 50	L. El Cajon		Stakes	Grade Lt.			Stakes Rt.	Grade Rt.		
6+00			4.49	374.87	(374.92) (P. 11)	0.55 ✓	3.80	375.52	374.65	0.91 ✓
5+50			3.77	375.59	375.04					
5+20			4.28	375.08	374.45	0.63 ✓	3.53	375.83	374.16	1.67 ✓
5+00			4.03	375.33	374.10	1.23 ✓	3.39	375.97	373.86	2.11 ✓
4+80	B.R.K.		5.19	374.17	373.90	0.27 ✓	3.92	375.44	373.69	1.75 ✓
4+50			5.48	373.88	373.78	0.10 ✓	4.71	374.65	373.58	1.07 ✓
4+100			5.52	373.84	373.66	0.18 ✓	5.09	374.27	373.46	0.81 ✓
3+50			5.54	373.82	373.46	0.36 ✓	5.91	373.45	373.26	0.19 ✓
3+150			6.02	373.34	373.26	0.08 ✓	6.06	373.30	373.06	0.24 ✓
TP.	6.06	379.36	4.97	373.30						
3+100			5.36	372.91	373.06	0.15 ✓	5.22	373.05	372.86	0.19 ✓
2+50			5.14	373.13	372.86	0.27 ✓	5.38	372.89	372.66	0.23 ✓
2+00			5.19	373.08	372.66	0.42 ✓	5.38	372.89	372.46	0.43 ✓
TP.	5.32	378.27	4.55	372.95						
1+50			4.04	373.46	372.46	1.00 ✓	4.55	372.95	372.26	0.69 ✓
1+00	B.R.K.		4.17	373.33	372.26	1.07 ✓	4.95	372.55	372.06	0.49 ✓
0+80			4.24	373.26	372.13	1.13 ✓	5.10	372.40	371.94	0.46 ✓
TP.	4.90	377.50	4.43	372.60						
0+60			4.28	372.75	371.91	0.84 ✓	4.43	372.60	371.76	0.84 ✓
0+40			4.41	372.62	371.59	1.03 ✓	4.51	372.52	371.50	1.02 ✓
0+20			4.61	372.42	371.17	1.25 ✓	4.84	372.19	371.17	1.02 ✓
0+00			5.68	371.35	370.71	0.64 ✓	5.88	371.15	370.80	0.35 ✓
TP.	3.30	377.03	6.92	373.73						
B.M.	3.60	380.65		377.05						

N.W.B.P. Wilson & Orange



Proposed Sewer E/Cajon Blvd. East of 73rd St.  
To Serve Lot 5 La Mesa Colony

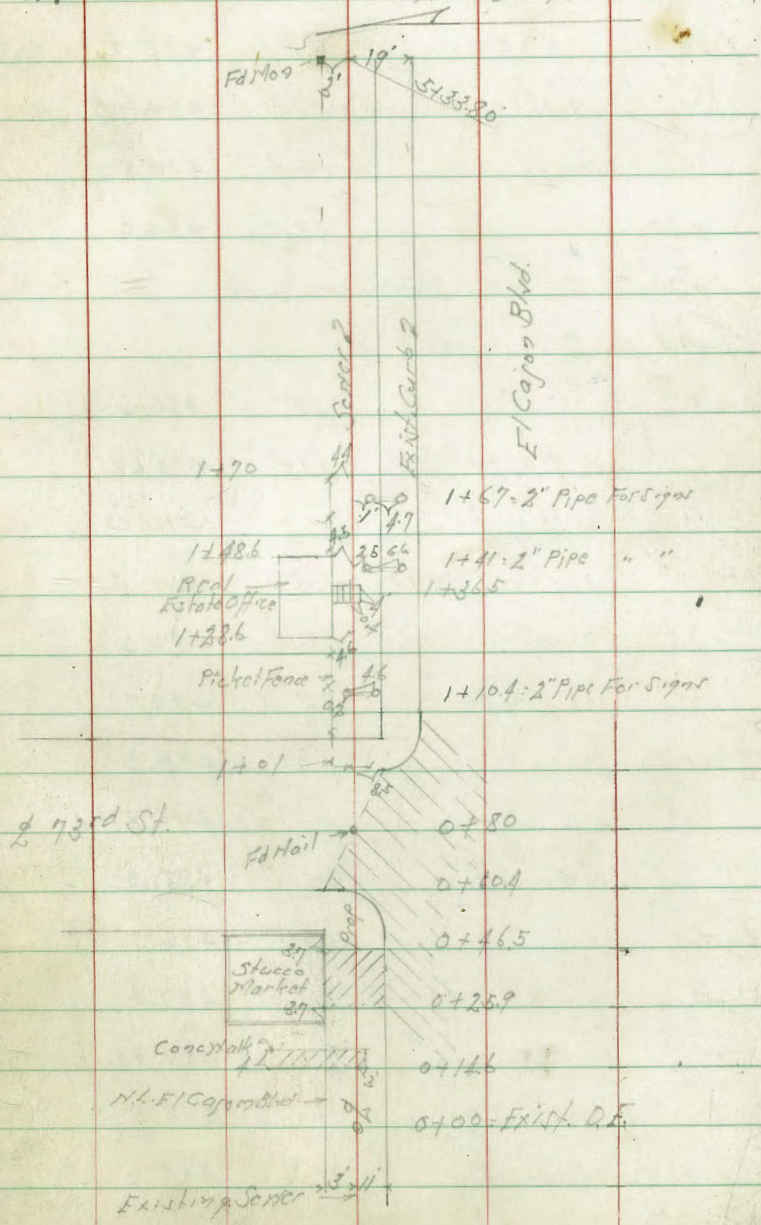
INDEXED

JPB

Nov. 3-47  
S. S. 503  
McCoy  
7160  
80077

67

B.M.	Description	Elevation	Notes
9.41	189.76	180.25	SMBP E/Cajon Blvd + 73rd St
0+0	Existing DE	10.4	479.4
+14.6	1/4 Conc. Walk	10.02	479.74
+25.9	1/4 Conc. Slab	9.61	480.15
+41.5	Fly "	9.25	480.51
+60.4	Curb Top	9.25	480.51
"	Gutter	9.73	480.03
+80	1/2 73rd St	9.07	480.69 on Nail
1+0		8.1	481.7
"	25 ft of 1/4 Conc. Rd.	8.24	481.52
+36.5	4.6 ft of 1/2 Reol Est.	4.68	485.08 office on floor
+50		6.6	483.2
+77		6.0	483.8
2+0		4.8	485.0
"	19 ft of 1/2 Curb	6.76	483.00
"	100 ft "	0.5	489.3
+16	2 ft of 1/2 Cluster Gravel Burbs		
+50		4.4	485.4
+55	1 ft of 1/2 5" Pipe Top		
+77	1/2 12" Diam Century Plant		



489.76

497.59

3+0		46	485.2
"	19' Pt of $\frac{1}{2}$ " Carb	484	484.92 Top
"	100' Lt " "	+0.4	489.80
+50		38	486.0
+70	2.2' Lt of $\frac{1}{2}$ " 2-3" Guava Bush		
+94	2 " " " 4' " "		
4+0		32	486.6
"	19' Pt of $\frac{1}{2}$ " Carb	214	486.62
"	100' Lt of $\frac{1}{2}$ "	+0.2	490.0
TP	11.14	497.59	3.31 486.45
+35		11.0	486.6
"	100' Lt of $\frac{1}{2}$ "	77	489.9
"	200' " " "	43	493.3
"	250' " " "	58	491.8
"	300' " " "	93	488.3
4+50		10.9	486.7
5+0		10.2	487.4
"	19' Pt of $\frac{1}{2}$ " Carb	916	488.43
"	100' Lt of $\frac{1}{2}$ "	91	488.5
+338	Fly Lot 5	96	488.0

B.M.

9.52

488.07

07 Mon  
3' Lt 5733.8

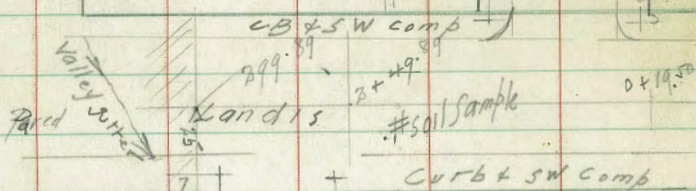
INDEXED  
NOV 2 1950

X Section

Landis

47 St  
60

Memo



60

47 St

INDEXED

MAR 31 1950

see 2034/18

Moore Landis 47 & Euclid

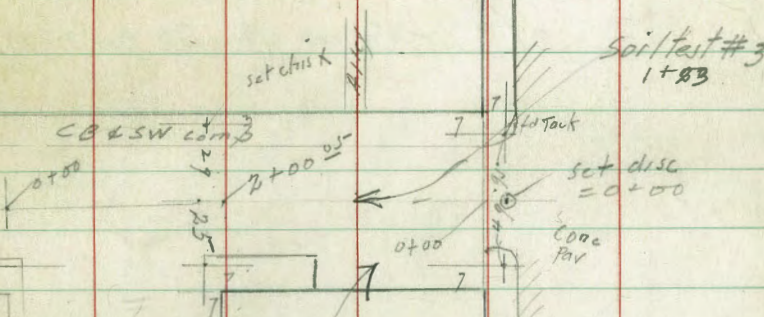
Begg Roselawn Landis &

Sherman 3/28/50 WD 31830

Crawford

Roselawn

69



50

Rose Lawn

no cb  
no SW

Euclid



0 + 99 21.3 Lt NW cor Bell Toll Box 3.2 x 1.7

0 + 50

343.1	343.2	343.5	342.8	343.92	(343.24)
5.5	5.4	5.1	5.8	5.19	
30	30	19.5		26	

0 + 20

343.7	343.8	343.2	343.9	343.4	343.95	(343.7)
4.9	4.8	5.4	4.9	5.2	4.66	
30	20	19		19.5	19.5	

0 + 00

343.5	343.92	342.03	343.60	343.93	344.32	344.00
	5.19	5.58	5.01	4.68	4.29	4.29
	26	9	19.5	26		
	20.4					

Reduced by C. Lawrence  
4-50

0 - 12 ob line Euclid

342.96	342.06	343.35	342.93	343.09	343.41	343.63	343.67	344.15	342.79	342.19
6.15	5.55	5.26	5.68	5.52	5.20	4.98	4.94	4.46	5.22	5.22
cb	92.4	cb	BC	20.4		19.5	22.6	cb	9	cb

348.61

8 15 348.61

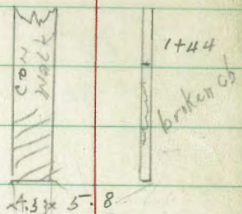
340.46

Lantana Dr & Euclid NE BP

1+44 beg curb lt  
 broken curb to gar 1+40  
 1+35 beg sidewalk lt

1+34 MH

1+35



1+355 EC 221 line of alley to 19

1+33 BC of cb Rt

TP 2.23 344.37 .6.47 347.14

1+00

348.61

341.19 340.8 341.2  
 3.18 3.5 3.1  
 20.5 9  
 341.54 341.48  
 8.83 2.39  
 30.63 26.3

341.80  
 2.57

342.21

342.43

2.76 1.94  
 2.21 3.14

341.6 341.7 341.2 341.8 341.5 342.19  
 2.7 2.6 3.1 2.5 2.8 2.1 P (342.13)  
 30 21 19 19.6 19.6

344.37

Top of Hydrant Rose lawn & Lardis

342.3 342.2 342.0 342.5 341.9 342.56 (342.48)  
 6.3 6.4 6.6 6.1 6.7 6.05  
 30 20 28 19.6 CB 19.6  
 18

348.61

1.81 343.95 2.23 342.14 H<sub>1</sub>

2+0005 Rose lawn

1+83  $\frac{1}{2}$  driveway 6' wide

1+47 EC cb

1+45 line of Alley to A

34A 37

340.37	339.8	<u>343.95</u>	339.9	340.91
4.00	4.5	4.1	4.4	3.46
cb	203		19.8	cb
203				

340.60	340.1	340.5	340.5	340.60	341.33
3.77	4.2	3.8	3.8	3.77	3.04
203			198	conc	25.7
			198		

341.74  
2.63  
196  
cb

341.10	340.8	341.2	341.1	341.85	342.03
3.27	3.5	3.1	3.2	2.52	2.33
cb	30.5		196	21.6	316
	9			cb	

344 37

0 + 0 - 0  
25 + 50 - 05

Rose lawn W Line

2 + 40

2 + 25 - 05

Rose lawn

2 + 10 - 05

cb line

343.95

73

339.84

339.2

339.7

339.5

340.20

4.11

4.7

4.2

4.6

3.75

202

20.2

19.9

19.9

cb

9

9

cb

339.85

339.2

339.4

339.8

339.5

340.31

4.10

4.7

4.5

4.1

4.4

3.64

cb

32.2

2.0

19.9

cb

32.2

17.9

339.7

339.9

339.9

339.7

340.56

4.2

4.0

4.0

4.2

3.39

30

20

19.9

cb

340.41

339.6

339.8

340.1

339.9

340.75

3.54

4.3

4.1

3.8

4.0

3.20

cb

30.4

20

19.8

cb

E

3

17.8

343.95

0+34 cont'd

0+34

0+34 BC curb on H7th

0+195 E line H7 to North

343 95

H12

340.83  
312  
cb  
86.7

340.22  
3.73  
86.7  
9

339.33

4.62  
cb  
20.2

338.7

5.2  
2

339.2

4.7

339.2

4.7  
19.9

339.38

4.57  
3.17  
cb  
of Br.

339.89

4.06  
cb  
31.7

339.50

4.45  
cb  
20.2

338.7

5.2  
20.2

339.3

4.6

339.2

4.7  
19.9

339.87

4.38  
cb

339.54

4.41  
cb  
20.2

338.8

5.1  
20.2

339.3

4.6

339.1

4.8  
19.9  
2

339.94

4.01  
cb

343 95

0+64.5 cont

0+64.5 curb line

0+49.5  $\phi$  47 to N

0+48.5  $\phi$  driveway 7 wide

343 95

340.17  
378  
108  
87  
75  
339.61  
4.34  
9

338.93	338.4	338.9	338.3	338.61	339.07
5.02	5.5	5.0	5.6	5.34	4.88
CB	20.2		20	9	CB
20.2				32	

338.59	338.9	339.2	339.31	340.33
5.36	5.0	4.7	4.64	3.62
20.2		20	32	87
			edges	
			for	

339.35	338.59
4.60	5.36
26.2	20.2

343 25

1+49 Driveway Pt.

1+40

1+23 MH

1+00

0+79.5 W line 47 St to N 8' Drive to left

343.95

338.0	337.87	338.51
5.9	6.08	5.74
	19.8	25.7

337.91	337.4	338.0	337.7	338.50
6.04	6.5	5.9	6.2	5.45
cb	20.2		19.8	cb
				19.8

338.4  
5.5

338.47	337.8	338.4	338.0	338.82
5.48	6.1	5.5	5.9	5.13
cb	20.2		19.8	

338.93	338.20	338.7	338.3	339.04
5.02	5.75	5.2	5.6	4.91
262	20.2		19.8	cb
	driveway			19.8

343.95

2+49<sup>29</sup> E line A7 to S

336.40  
5.02  
cb  
20.2  
336.0  
5.4  
9  
336.7  
4.7  
336.7  
4.7  
337.51  
3.91  
cb  
19.9

2+25 W Line Alley to N

336.73  
4.69  
cb  
20.2  
336.1  
5.3  
337.0  
4.4  
336.9  
4.5  
20  
337.74  
3.68  
cb  
ret  
337.92  
3.50  
337.82  
3.60  
dirt  
32

2+50 MH

337.4  
4.0

2+05 East line Alley to N - T driveway to L

337.17  
4.25  
26.2  
336.47  
4.95  
20.2  
on drive  
337.3  
4.1  
337.2  
4.2  
19.8  
337.95  
3.47  
2.2  
cb  
338.20  
3.22  
3.2  
cb  
dirt

333 341.42 5.86 338.09

341.42

1+63 Driveway on Lt 7" wide

337.95  
6.20  
26.2  
337.10  
6.85  
20.2  
337.8  
6.1  
337.5  
6.4  
9.198  
338.33  
5.62  
cb

343.95

343.95



3+15 on Paving

336.38	335.62	335.87	336.22	336.34	336.30	336.96	78
5.04	5.80	5.55	5.20	5.08	5.12	4.46	
cb	20.2	10		10	19.8	cb	
						19.8	

2+99<sup>89</sup> W Line 47 to S

335.98	335.38	335.98	336.47	336.68	336.45	337.10
5.44	6.04	5.44	4.95	4.74	4.97	4.32
cb	20.2	10		10	19.8	cb
			edge of Paving			19.9

2+89<sup>89</sup> cb line 47 to S

335.81	335.28	335.98	335.47	335.6	336.5	336.3	337.18
5.61	6.04	5.44	5.95	5.8	4.9	5.1	4.24
cb	50.1	cb	32	20		19.9	cb
		32	par				

2+74<sup>89</sup> d 47 to S

335.72	336.03	336.1	336.6	336.5	337.29
5.70	5.39	5.3	4.8	4.9	4.13
50	32	20		19.9	cb

2+59<sup>89</sup> E cb line 47 to S

336.18	335.70	336.49	335.95	335.8	336.7	336.7	337.91
5.24	5.72	4.99	5.47	5.6	4.7	4.7	4.01
cb	50	cb	32	20		19.9	cb
		cb	par				

341.42

341.42

		7.67	340.45	340.46
TP	9.55	348.12	2.85	338.57

Lanton & Euclid

341.42

379.36  
 4.44  
 374.87  
 379.36  
 4.74  
 374.62  
 379.36  
 4.96  
 374.40

379.38  
 4.21  
 375.15

DISTANCES FROM CENTER OF ROADWAY FOR  
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½  
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.