

1719

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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1719

CITY ENGINEER'S OFFICE

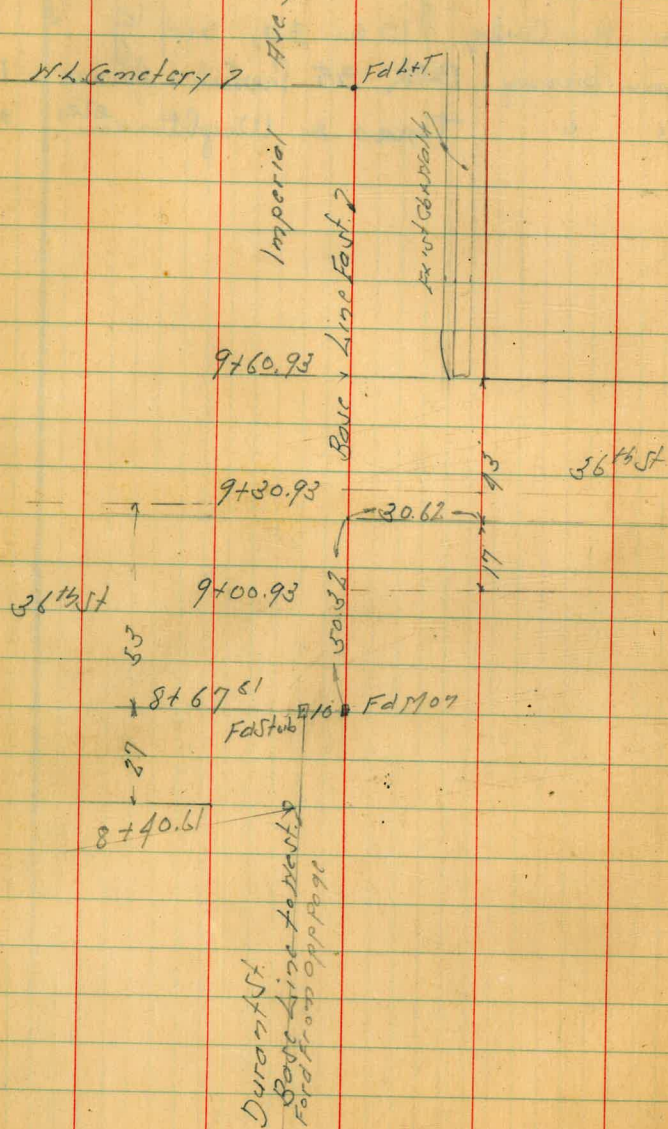
515507

This Field Book is manufactured of a High
Grade 50% Rag Paper having a WATER
RESISTING SURFACE, and is sewed with
Bing Special Enamel Waterproof thread.

Made in U. S. A.

Cross Section Durant St
 Francis St to East of 36th St

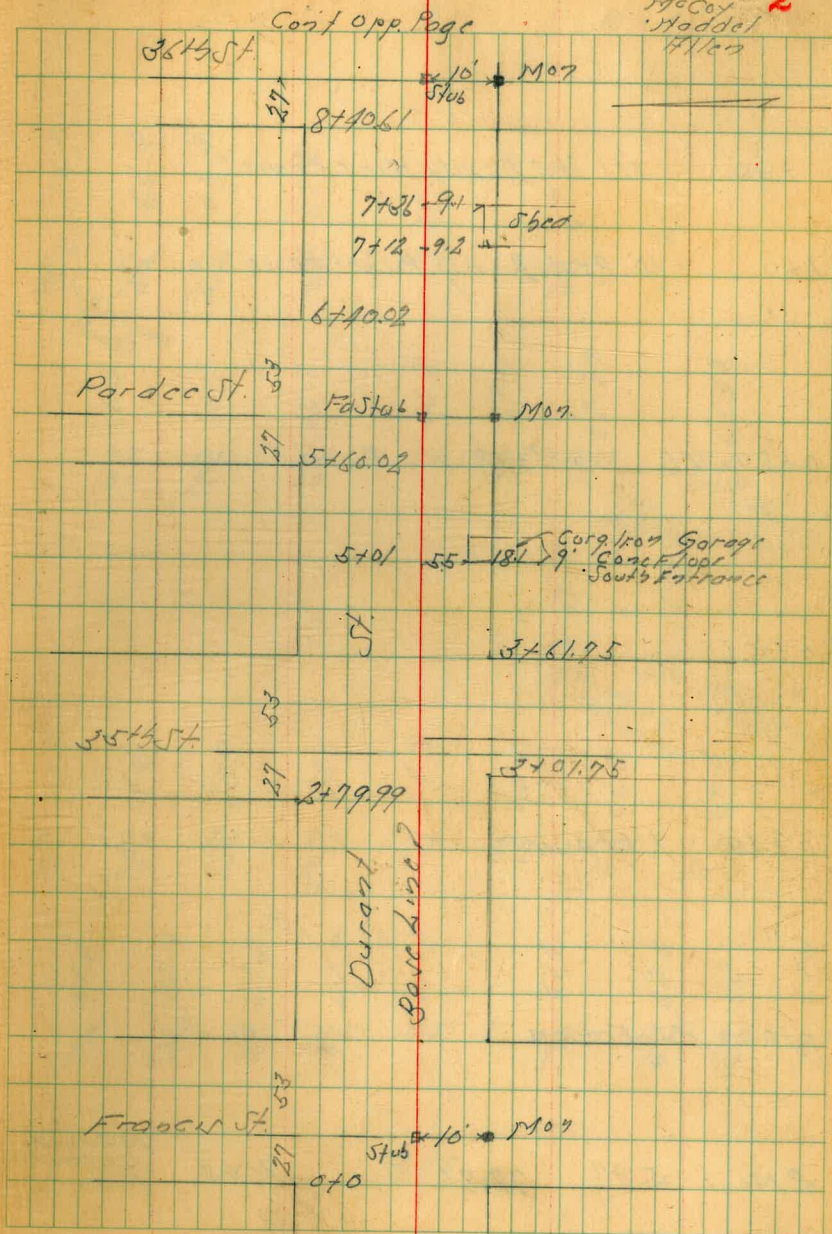
Levels next page



Indexed
 C.S.K.

Sept. 4-46
 S. 1507
 190 Coy
 Model
 1912

2



Durant St Francis St to 36th St

+30 22.6 Lt of R = Wly Wick Fence

1+0 10' Rt of R = Fly Picket Fence

0+80 = E.L. 10' Rt of R = Wly Picket Fence

0+56

0+40 = R Francis

0+0 = W.L. Francis

8M

5.87

72.85

66.98

13' Meas
Durant +
Francis

H.M.

R

Rt = S

3

66.0	66.4	66.9	67.0	67.1	67.1	65.9
5.8 10 285 = Fly Picket House	6.1 10	5.9 10	6.5 10	5.7 10	5.7 10	5.9 10
65.3	65.9	66.7	66.7	67.0	67.37	65.44
5.7 10	5.9 10	6.1 10	6.1 10	5.8 10	5.48 10 = Fly Cobble Wall	7.1 10 = Fly Cobble Wall
67.19	67.19	67.19	67.19	67.19	67.19	67.19
5.6 10	5.6 10	5.6 10	5.6 10	5.6 10	5.6 10	5.6 10
65.7	64.8	65.9	64.6	64.9	65.1	64.5
9.1 10	8.8 10	6.9 10	8.2 10	7.9 10	7.7 10	8.2 10
61.4	62.0	62.2	61.3	61.3	61.4	62.3
11.4 10	10.8 10	10.6 10	11.5 10	11.5 10	11.4 10	10.5 10
61.1	63.1	61.1	61.1	61.1	61.1	61.1
11.7 10	9.7 10	11.7 10	11.7 10	11.7 10	11.7 10	11.7 10
72.85						

Durant St.

+7999 - W.L. 35th St. to North

+50

+20

+02 217 Lt of B = A Picket Fence

+01 10' Rt of B = Fly Wire Fence

270

+92 26 Lt of B = W/L Picket Fence

+87

+82 26 Lt of B = Fly Wire Fence

+65 227 Lt of B = A Wire Fence

+52 103 Rt. of B = W/L Wire Fence

1+50

72.85

St.

69.7
70.1

69.5
70.3

69.2
69.6

69.1
69.2

68.8
68.6

68.5
68.4

69.7
70.1

69.5
69.6

69.2
69.3

69.1
69.2

68.8
68.6

68.5
68.5

67.5
67.5

69.0
69.0

69.2
69.2

69.2
69.3

69.3
69.3

68.2
69.5

67.9
69.1

67.5
67.3

67.1
67.1

68.7
68.7

68.9
68.9

69.0
69.0

68.9
68.9

68.7
68.7

67.5
67.5

68.75
68.75

68.80
68.80

68.1
68.1

68.1
68.1

67.9
67.9

67.5
67.5

66.5
66.5

67.2
67.2

67.8
67.8

68.1
68.1

68.1
68.1

67.9
67.9

66.6
66.6

66.5
66.5

26.0 - Approx
26.0 - Approx
26.0 - Approx

21.5 - Approx
21.5 - Approx
21.5 - Approx

72.95

4

470

+86

20.3 H of B = 5 1/4 Tol Pole

+74

10.4 Rt of B = W 1/4 Board Fence

3761.75 = EL 35th to South

+55

26.5 H of B = 5 1/4 Tol Pole

TP

11.36 83.46 0.75 72.10

431.75 = 2 35th St to South

3701.75 = W 1/4 35th St to South 22 H of B = F4 Pocket Fence

47

8

Rt

5

	6.8 30	6.8 20	7.5 19	7.7 5	7.7 76.8	7.8 71.7	7.7 20
		8.0 30	9.0 18	9.6 5	8.0 75.2	8.1 75.4	8.0 20
		8.8 20	10.0 18	10.4 5	10.1 73.4	10.3 73.2	10.2 20
		9.1 30	9.6 20	10.9 18	11.2 5	10.7 72.9	11.6 20
			70.3	70.9	71.1	83.46	
		70.7	70.6	70.1	69.9	70.9	70.1
		71.7	70.6	70.1	69.9	69.9	69.7
		71.7	70.6	70.1	69.9	69.9	69.7

Durant St.

6+0008: $\frac{1}{2}$ Pardee

+60.02 = W.L. Pardee St

TP 12.56 94.74 1.28 82.18

+34 19.3 Lt of $\frac{1}{2}$ = Sly Tail Pole

+30

+01 11 Rt of $\frac{1}{2}$ = Fly Wire Fence

5+0

+70 98 Rt of $\frac{1}{2}$ = Fly Board Fence + Fly Wire Fence

+50

4+12

83.46

Lt.

Rt

6

86 30	88 20	91 14	84.8 5.2 67.6	86 5	83 2	82.1 10	81 20
105 30	102 20	103 15	117 14	119 5	118 1	113 10	116 10
19 30	20 20	20 17	23 15	25 5	28 0	15 10	25 20
37 30	37 20	42 16	43 5	56 5	55 5	50 10	26 20
56 30	56 20	61 18	58 5	55 5	55 5	55 10	57 20

84.5
91.5
72.8
77.9
77.0
78.0

94.74
94.74
80.0
80.0

6.2
10 = Fly Wire Fence

83.46

+98 17.6 Lt of $\frac{3}{8}$ = Fly Picket Fence
 +83 16.7 Lt of $\frac{3}{8}$ = Fly Tel Pole
 +80

 +50
 +36 9.1 Rt of $\frac{3}{8}$ = W/4 Board + Picket Fence
 +12 9.2 Rt of $\frac{3}{8}$ = Fly Wire Fence 19.5 Lt of $\frac{3}{8}$ = W/4 Picket Fence
 +07
 TP 9.51 102.69 1.56 93.18

 710 27 Lt of $\frac{1}{2}$ = Fly Fence on North

 +87 8.5 Rt of $\frac{3}{8}$ = W/4 9' Popper Tice
 +85 8.6 Rt of $\frac{3}{8}$ = W/4 Wire Fence
 +70
 +55 17.8 Lt of $\frac{1}{2}$ = Fly Tel Pole
 +15 10.4 Rt of $\frac{3}{8}$ = Fly Wire Fence

 6 + 40.02 = E. L. Pordee to North
 +38 21.2 Lt of $\frac{3}{8}$ = W/4 Wire Fence
 6 + 12 10.4 Rt of $\frac{3}{8}$ = W/4 Wire Fence
 9474

7

	LT	RT	RT
	937 30	537 10	40
	99.0	98.8	93.3
	4	5.9	1.0
	98.4	97.6	91.0
	4.13 30	1.3 10	5.5
	20.2 30	92.5	9.1
	81 30	81 30	102.69
	94.3	93.3	90.7
	0.4 30	1.3 11	1.7
	91.4	90.7	91.6
	5.5 30	4.3 12	4.9
	91.2	90.7	91.6
	1.9 30	6.4 12	6.4
	99.2	88.1	88.1
	5.7 30	5.7 10	5.5
	99.0	99.0	99.0
			9474

20.2 = W/4
 81 = W/4
 92.5 = W/4
 102.69 = W/4
 90.7 = W/4
 91.6 = W/4
 99.0 = W/4
 9474 = W/4

Durant St.

9+0093 = W L 36th to South

188

TP 3.47 9.594 10.22 92.47

+ 80.61 = 1/2 36th St to North

+ 56 157 Lt of B = Sly Anchor Pole

+ 50 163 Lt of B = Sly 6" Pepper Tree

+ 44 4.6 Rt of B = 1 1/4 Light Pole

+ 40.61 = W L 36th St to North

+ 19 15.9 Lt of B = 5 1/4 28" Euc. Tree

+ 17

+ 07 8.9 Rt of B = Fly Board at Picket Fence

8+0

102.69

Lt.

B

Rt.

8

837 500m Par	715 300m Par	676 176 422m Par	51	1.8	2.12	1.30
88.14	91.7	91.0	94.0	94.7	94.7	94.7
80 93.8 Sly 17.10m	4.4 2.0	4.9 1.6	1.9	1.9	1.7	1.8
17.2	92.3	92.7	95.94	97.2	97.2	97.2
15.23 1.5 Sly 17.10m	10.1 3.0	10.0 2.0	92.1	94.7	94.7	94.7
94 70-Top	91.4	91.5	95.4	95.4	98.2	98.2
7.3 1.50	6.1 2.0	7.9 5.6	7.0	7.0	5.0	4.5
	91.9	91.6	99.6	99.6	99.9	99.9
4.0 3.0	4.8 2.0	4.3 3.0	4.1	4.1	1.8	1.8
					100.9	100.9

102.69

1.8 = 2 + 1/4 Dia
6" Pepper Tree

BM 4.65 97.93 5.8P
 1m partial +
 South look
 97.91

16+86 = Approx H.L. Filley

7P 7.61 102.58 0.97 94.97

10+26

786

+60.93 = E.L. 36th to South

+30.93 = 1/2 36th to South

9+14

9594

Lt.	S	Rt.
56.93 5.8P 16=H/Por	101.01 5.50	97.08 5.50 10=Guller
104.5 11.57=H/Por	102.58 9.32 0.62	97.79 5.09 20=Cb 76.06 0.15=Cb
62.7 9.5 2.8=H/Por	0.82 2.63 2.24	93.96 1.98 200 203=Guller 94.65 1.28 203=Cb
52.7 26.1/21 Por	41.15 4.16 1/20 Por	93.03 2.91 281 2.23=Guller 2.30 2.23=Cb End
7.57 4.15=H/Por	81.06 5.76 1/20 Por	90.90 4.49 1/20 Por
8.36 8.50=Por	80.06 5.86 1/20 Por	90.02 5.14 1/20 Por
		4.23 4.0 4.0 4.17=H/Por
		3.5 3.0
		1.5 1.8 = F/L Core Valued mkr

9594

Survey for Drain on S. side of
 Laurel St. E. of Pacific Hwy. *Indirect*

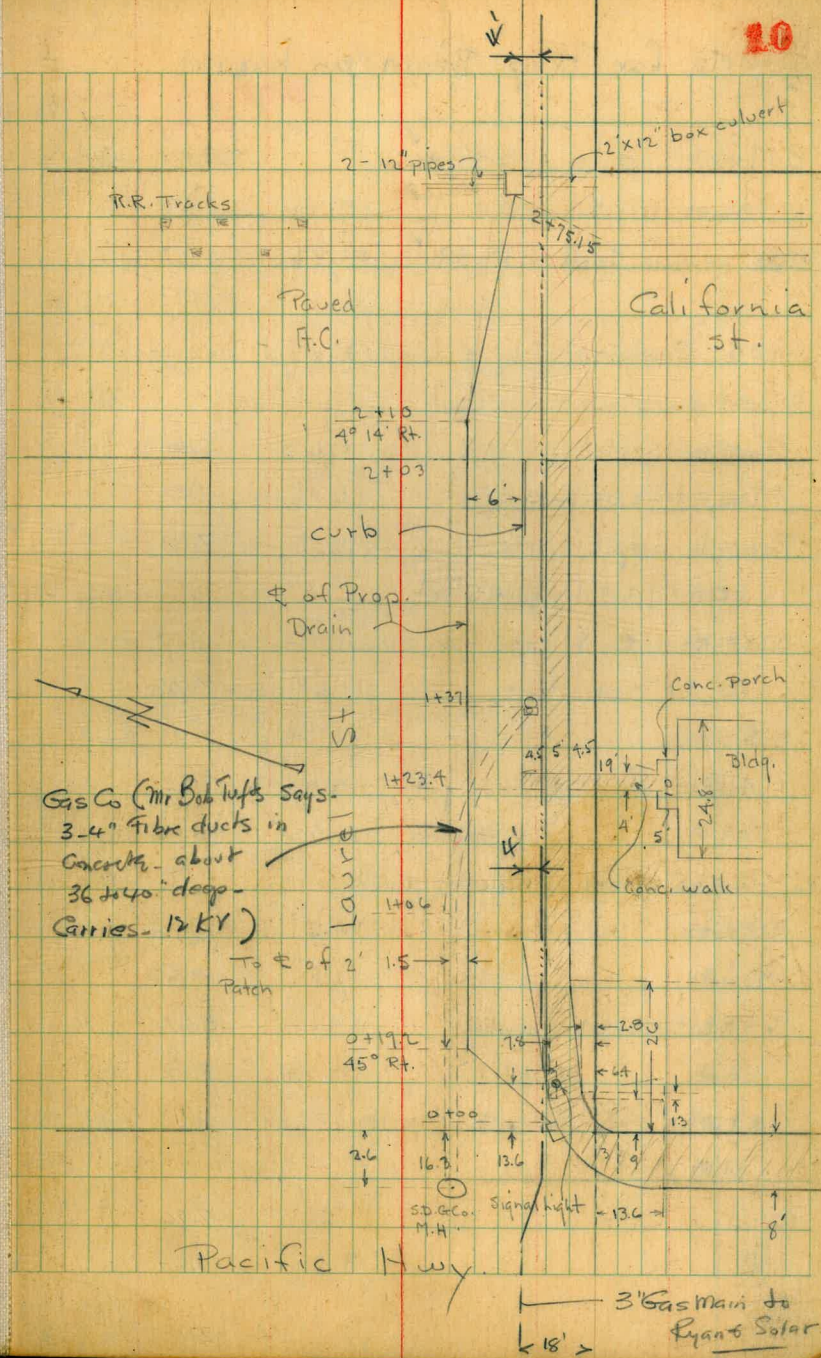
604

W.O. 209 ✓

11-8-46

Osborne
 Hardin
 Worrell
 Smith

1+06 = P.C. in ditch for conduit - High tension
 Cable (Looks like)



Levels for Prop. Drain on Laurel. ??

BM Record Shows -

B.M.	0.10	32.94	✓	32.97	SE BP Laurel + Kettner
	1.37	22.17	✓	12.14	20.80
	9.27	19.47	✓	11.97	10.20

0+00 = Center of Ely. side of 2' x 3.5' Box for G

type curb inlet

Top of grate 12.67 6.80

Flow line of box 16.98 2.89

Top cb. opp. 11.59 7.88

0+19.2 = Ang. 45° Rt.

13.3 Rt = ± 8" base for Signal Control box

10' Lt = on Pavc 11.69 7.78

± 12.04 7.93

11.4 Rt = face cb in gut 12.28 7.22

" " top cb 11.42 8.05

0+65 = opp. angle in curb.

10' Lt. 10.51 8.96

± 10.81 8.66

6' Rt. = curb - gut. 10.86 8.61

Top 10.30 9.17

0+67.5 - 8' Rt = ± P. pole

1+00

10' Lt. 9.51 9.96

± 9.50 9.97

19.47 ✓

11

6' Rt. = gut. 9.50 9.97

Top cb. 9.09 10.38

1+37 = opp 2' x 1' Conc base for High tension conduit along P. pole. - just back of cb.

1+50

10' Lt. 8.00 11.97

± 8.07 11.80

6' Rt = gut. 8.16 11.31

Top 7.57 11.90

10.5 Rt = edge walk 7.48 11.99

15.5 " = " " 7.50 11.97

1+94 = low point in gutter

1+97 - 79' Rt = ± Crossing sign post 8' x 8' 6.23 13.28

6' Rt. gut. 6.45 13.02

Top cb. 5.53 13.98

A.C. Pavc

2+03 = W.L. California St. + end of cb. + walk + base.

10' Lt. 5.40 14.07

± 5.43 14.08

6' Rt. = gut. 5.60 13.87

Top cb. - end. 5.17 14.30

10.5 Rt = edge walk - end. 5.03 14.88

15.5 " = " " " 4.86 14.61

19.47 ✓

2+10 = Angle	4° 14'	Rt.		
10' Lt.		5.13	19.32	
Φ		5.07	19.40	
6' Rt.		5.05	19.42	
10' Rt. on H.C. pave		4.78	19.69	
18' Rt. = edge pave		4.84	19.63	
2+15 = 19' Rt. = Φ P. pole				
2+51 = W. rail of W. track				
10' Lt. - on rail		3.27	16.10	
Φ on rail		3.40	16.07	
17' Rt. along rail - edge pave		3.49	15.98	on rail
2+70 = E. rail of				
10' Lt. on rail		3.34	16.13	
Φ " "		3.41	16.06	
16 Rt. " "		3.45	16.02	
2+75.15 = W. side of 3.5' x 1.8' box for				
grate inlet				
Top of Grate		3.18	16.29	
Flow line box		5.20	19.27	
T.P.	13.85	33.23	0.09	19.38
check B.M.		0.40	32.83	✓

Notes Reduced. 11-29-42

Levels for Sunken Curb on W. side
30th - G St. south.

605

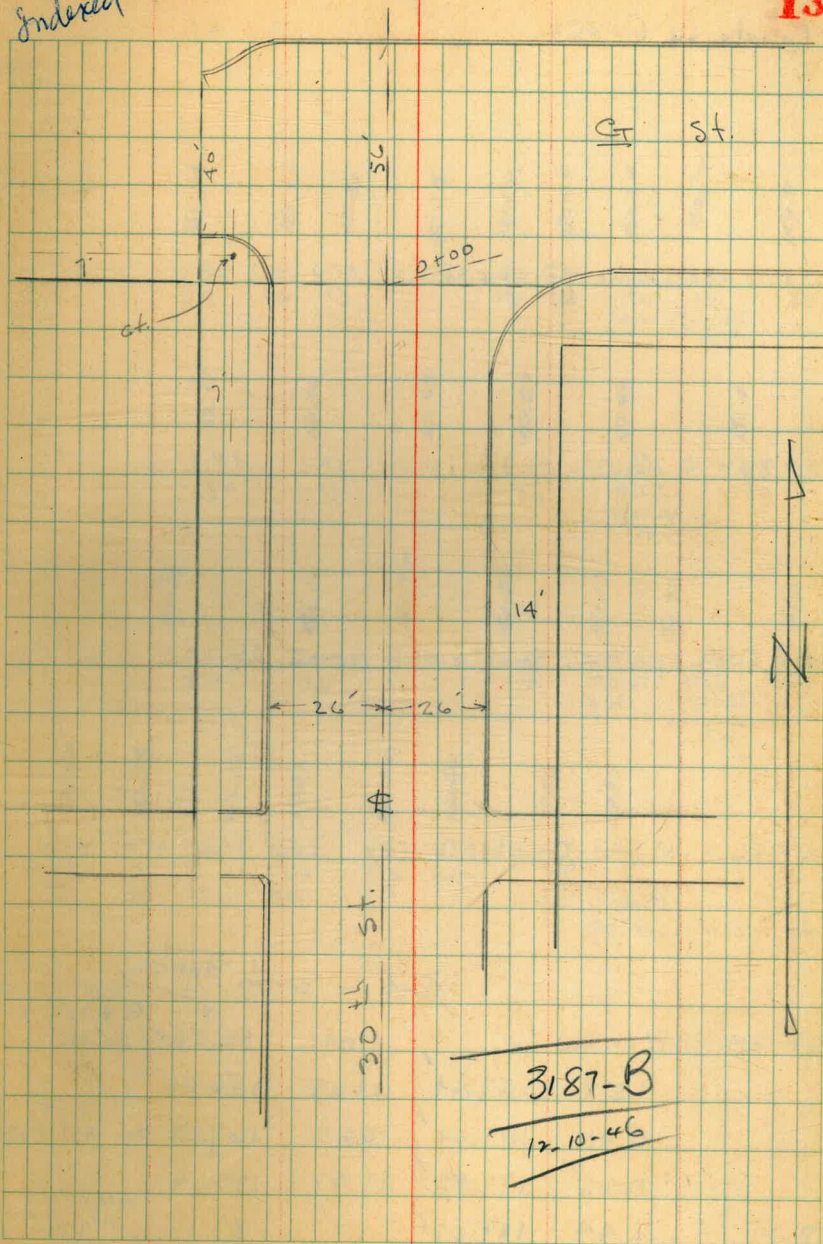
W.O. 208

11-12-46

Osborne
Hardin
Worrell
Smith

Indexed

13



Levels on G St.

0-10 = s.cb. line G to W.

0-30 = Φ G St.

0-50 = opp. E.C. Rev. Curve in cb. on Rt.

0-56 = N. cb. G St.

Past in Bench Book

Set BM. - B.P. on S.W. Cor.	7.09	150.55	Φ + 30 th to South.
1.58	157.64	11.63	156.06
0.40	167.69	10.60	167.29 inside cor. Ret. S.W. F + 30 th
0.25	177.89	11.43	177.64
B.M.	1.44	189.07	187.63 NW B.P. 30 th + E

Lt = Ft.

Rt. W. 14

151.28	151.22	151.31	151.28	151.14	150.68	150.28	150.72	149.8
6.40 50	6.42 26	6.33 13	6.36	6.52 13	7.00 26	7.40 40 put.	6.92 40 Top EC. Ret.	8.72 50
152.17	151.72	151.68	151.57	151.98	150.8			
5.47 50	5.90 26	6.00	6.07 26	6.20 40.2. edge Conc. Pave	7.2 50			
152.33	152.00	151.72	151.55	151.17	151.79			
5.31 50	5.64 26	5.92	6.09 26	6.47 40.6 put.	5.85 40.6 Top EC. + edge pave			6.15 50
152.80	152.32	152.36	151.99	152.02	151.66	151.85	151.97	
4.84 50 Top.	5.30 50 put.	5.28 26 Top	5.65 26 put.	5.62 Top	5.98 put.	6.19 25 put.	5.67 25 Top cb.	PC. Rev. curve in cb.

157.64

0+35

0+27

0+20 = opp PC Ret on ht. + 36.3 Rt. = end porch + 39.6 Ft = S.E. Cor House

0+16 - 28.2 Rt = Φ 4" pipe guard

0+15

0+14.5 - 27.8 = Rt = Φ F.H.

0+12.5 - 27.2 Rt = base of 4" pipe guard for F.H.

0+10.6 - 27.6 Rt = Φ P. pole

0+00 - 36.3 Rt = Reg. porch to house - 39.6 Rt = N.E. Cor. House

0+00 = S.L. G St. to W. = end walk on Rt.

0-04 = S. cb. G to E.

	H	Rt.
151.25	150.81	149.87
6.39	7.33	7.77
5.3	3.1	3.6
6.81	150.82	149.02
5.0	149.63	149.59
6.92	149.82	149.59
2.6	150.36	149.71
6.54	150.38	149.7
6.76	150.56	149.85
13	150.15	149.87
26.6	149.61	149.82
9.0	149.82	149.7
20.0	149.82	149.85
10.0	149.82	149.85
40	149.82	149.85
157.64		

PC Ret.

Top cb. Ret.

Top cb. on Ret.

39.6 = Floor
Porch + House

36.6 = edge
walk

1+25

1+00

0+97 - 40' Rt. = S.E. Cor. House - Conc porch out to walk level

0+83 - 40' Rt. = N.E. Cor. small House

0+80

0+60

0+57 - 40' Rt. = S.E. Cor. House - Conc. Porch out to edge of walk

0+43 - 40' Rt. = N.E. Cor. small House

0+40 = Beg. walk on Rt.

Lt.

Rt.

8.36 31	8.26 31	8.13 13	8.02 31	8.36 13	8.26 26	8.13 13	8.02 31	8.36 13	8.26 26	8.13 13	8.02 31	8.36 13	8.26 26	8.13 13	8.02 31	8.36 13	8.26 26	8.13 13	8.02 31
149.28	148.51	148.99	149.62	149.85	148.18	148.71	148.80	148.97	149.0	149.03	148.30	148.88	148.81	149.05	149.8	149.62	149.12	149.19	149.59
148.74	148.99	148.98	148.65	148.27	147.82	148.38	148.57	148.68	148.68	148.27	147.82	148.38	148.57	148.68	148.68	148.27	147.82	148.38	148.57
9.90	9.26	9.06	8.99	9.37	9.52	9.26	9.07	9.07	8.96	9.37	9.52	9.26	9.07	9.07	8.96	9.37	9.52	9.26	9.07
in Dr.	in Dr.	in Dr.	in Dr.	Top	Top	Top	Top	Top	Top	Top	Top	Top	Top	Top	Top	Top	Top	Top	Top
150.03	149.20	149.52	149.73	149.32	148.67	149.12	149.12	149.12	149.12	149.32	148.67	149.12	149.12	149.12	149.12	149.32	148.67	149.12	149.12
157.64	157.64	157.64	157.64	157.64	157.64	157.64	157.64	157.64	157.64	157.64	157.64	157.64	157.64	157.64	157.64	157.64	157.64	157.64	157.64

157.64

side walk

w. side

floor of house + porch

40' floor house

149.83

check BM.

			1.66	187.63	187.63
	10.58	189.29	0.48	178.71	
	11.90	179.19	0.45	167.29	
T.P.	11.68	167.74	1.58	156.06	

2+50

2+00

1+70 = S.L. Alley

1+60 = Alley

1+50 = N.L. Alley

1+48 - 40' Rt. = S.E. Cor. House - Conc. porch out to walk

1+34 = N.E. Cor. House

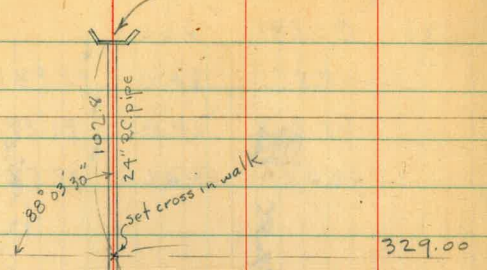
Notes Reduced. 11-29-86

188.16	187.62	188.06	188.22	187.93	187.38	188.08	188.31	187.29
9.44	10.02	9.58	9.42	9.21	10.26	9.60	9.33	10.35
26	26	13		13	26	26	2.3	40
Top cb.	out.			out.	Top	1 Rad. ret.	edge Conc. Pavement Alley Ret.	on oil pave
2 Rad ret.								

188.81	185.58	186.13
12	12	11
26	26	26
9.4	9.6	9.5
		Top
187.00	187.62	187.39
10.6	10.02	10.25
26	26	22.3
out.	Top	
187.14	187.42	187.04
10.55	10.22	10.60
26	32.3	40

157.64

Elev. 146.75 = Flowline inlet



329.00

Culvert # 1
See Detail

1° 36'

Block

Prop Drain

1+17.77
Hub

11° 29'

1+39
24.6

Shed
Conc. found.

1+60
16.9

4.5
2+15

Garage
10.1

10.1
2+32

See Detail

cross at 2+96

263.22

Culvert # 2
24" RC pipe

2.7
95° 30'

71° 57'

314.05 Bet. 7 lines at 26th

To ct.

80'

Survey for storm Drain

Indexed

Broadway

ct.

80'

35

Loomis

Parrish

Map 288

314.13
27th

E St.

ct.

6820-L
3188-B
(over)

Survey for Storm Drain thru Block 35

Parnish + Loomis.

606

W.O. 207

11-14-46

Osborne
Hardin
Worrell
Smith

B.M.	11.39	191.40		180.01	sw.B.P. 27 th + E
	0.88	191.80	0.48	190.92	N.W. B.P. 27 th + B.W.D.
	0.54	179.64	12.70	179.10	
	1.64	171.07	10.21	169.43	
	0.88	159.36	12.59	158.48	
	3.10	149.98	12.48	146.88	

Inlet of Culvert #1 - under Broadway is built up with Rock + Conc. rubble + Covered with Corrugated Iron sheets. Took flow line + Dist. to original Headwall

Flow line of inlet - 24" pipe 146.75 Elev. [?]

0+00 = face of Headwall - outlet 24" Culvert #1

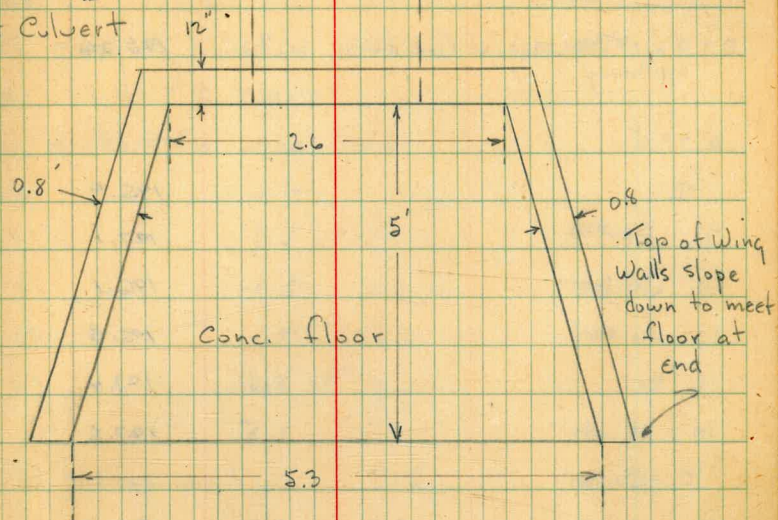
See Detail - opp. page - Note: filled in with dirt.

Top Headwall	3.10	146.88
Flowline pipe	6.68	143.30
Ground	3.4	146.6
10' Lt.	1.7	148.3
10' Rt.	0.0	150.0

Detail - outlet

Culvert #1

+ Inlet Culvert #2



149.98 ✓

0+05 - Top edge of Conc. floor spillway	6.72	193.26
0+25		
⊕	4.6	195.4
7' Lt.	2.9	197.1
10' Lt.	3.9	196.1
15' Lt.	4.2	195.8
6 Rt.	2.6	197.4
10 Rt.	2.5	197.5
0+50		
⊕	5.3	199.7
10' Lt.	5.1	199.9
5' Rt.	3.1	196.9
10' "	2.4	197.6
1+00		
⊕	6.1	193.9
10 Lt.	6.5	193.5
10 Rt.	3.8	196.2
1+09 - 14 Lt. = inlet 24" steel Culvert		
Flow line	7.50	192.48
1+17.77 = Angle 11° 29' Lt. = ⊕ Alley - oil strip		
⊕ on Hub.	5.25	199.73
10' Lt.	5.2	199.8
50' Lt along ⊕ Alley	3.5	196.5

149.98 ✓

20

10' Rt.	4.9	195.1	
40' Rt. along ⊕ Alley	1.6	198.8	
1+24 - 8.8 Rt. = ⊕ P. pole			
1+25 - 9' Rt. = Cor. wire fence			
1+30			
⊕	5.7	199.3	
10' Lt.	5.0	195.0	
10 Rt.	5.8	199.2	
1+53 = 4.6 Lt. = outlet 24" pipe			
⊕	7.3	192.7	
4.6 Lt. = Flow line	9.15	190.83	
10 Lt.	7.8	192.2	
10' Rt.	7.3	192.7	
17.8 Rt. = line wire fence	6.9	193.1	
1+94 - 7.2 Rt. = Near Cor. low picket fence			
2+00			
⊕	9.7	190.3	
5 Lt.	9.4	190.6	
15 Lt.	6.7	193.6	
10 Rt.	8.3	191.7	
T.P. 7.44	149.42	8.00	141.98
2+36			
⊕	9.0	190.4	
10' Lt.	7.0	192.4	

149.42

2+36 Cont.

3' Rt.	9.9	139.5	
8.7 Rt. = Near edge Conc. foundation wall 6" wide	7.9	141.5	ground.
	7.08	142.34	Top wall
Conc. floor of Car. on Rt. - shown in sketch			
	7.21	142.21	floor.

2+50

±	9.9	139.5	
10' Lt	7.4	142.0	
3' Rt.	10.0	139.4	
7' Rt.	7.5	141.9	
13.6 = Conc. wall	7.05	142.37	Top wall

2+66.9 = Edge of Spillway floor (See Detail P. 19)

± on Conc. edge	11.84	137.52	
± on Ground (filled in)	11.0	138.4	
6' Lt. = base loose Rubblewall	9.9	139.5	
6' Lt. = Top " "	7.9	141.5	
10' Lt.	7.5	141.9	
2' Rt.	11.0	138.4	
10' Rt.	7.5	141.9	

2+71.9 = face of Headwall - inlet 24" RC Culvert

FL. Pipe	11.90	137.52	
Top Headwall	8.19	141.23	

Flow line of Pipe at inlet (Grate ±) on N. cb. of E. St. (see sketch.) Note: Pipe in first - so just broke holes for connection

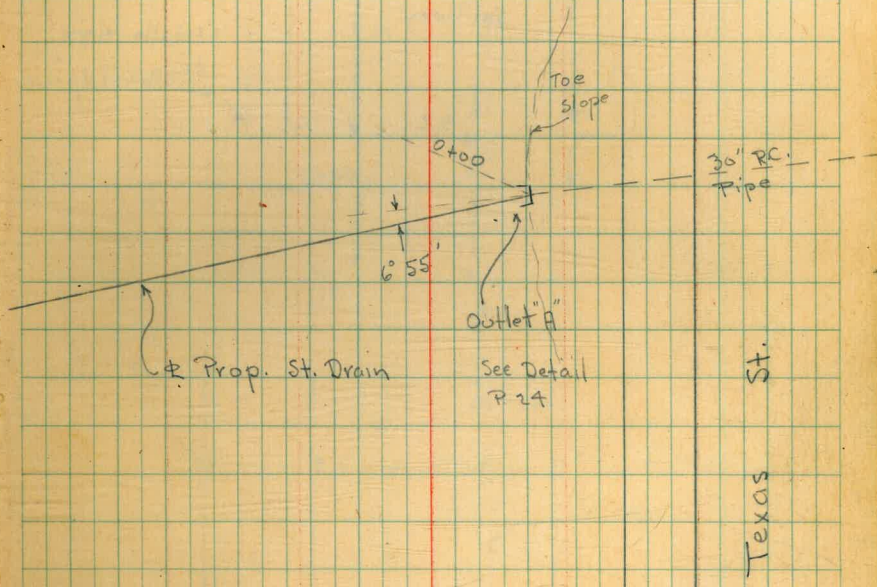
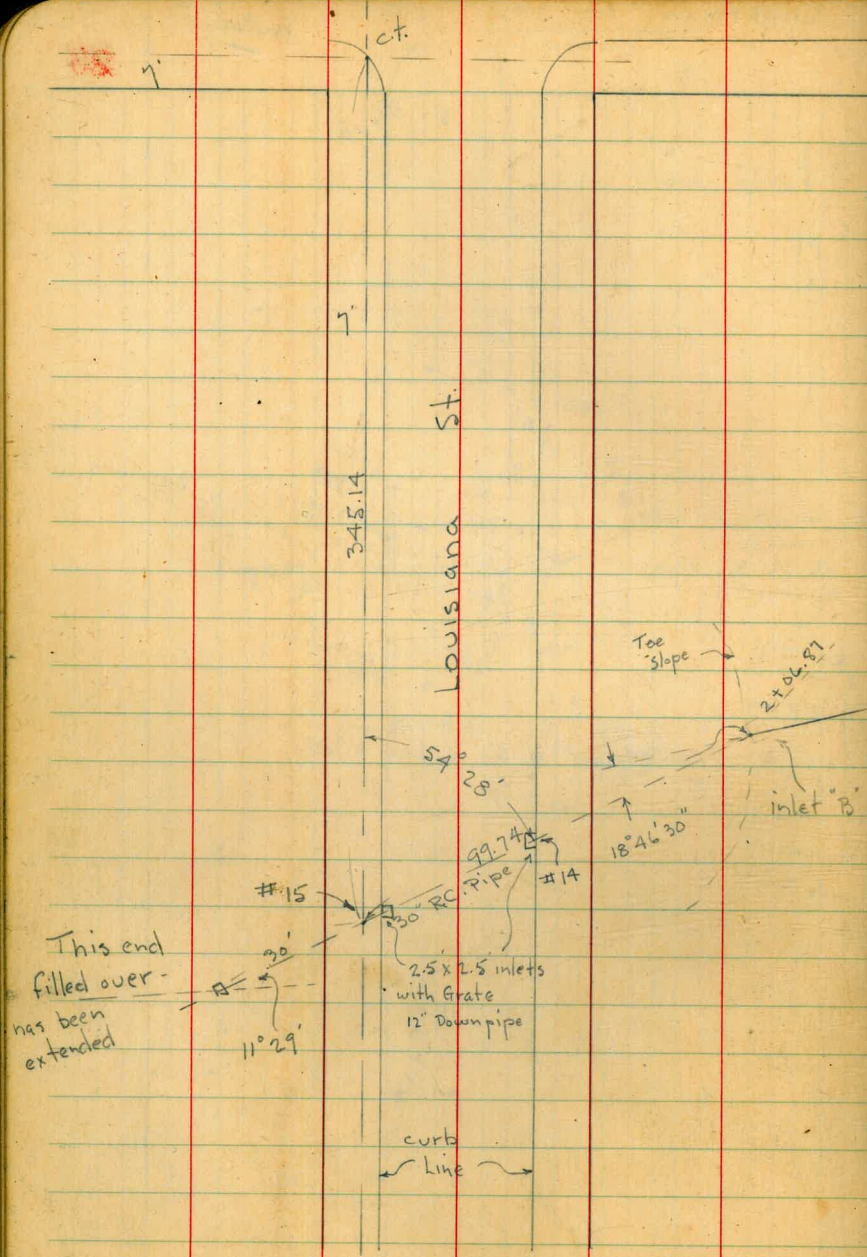
	12.25	137.17	FL pipe
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149.42

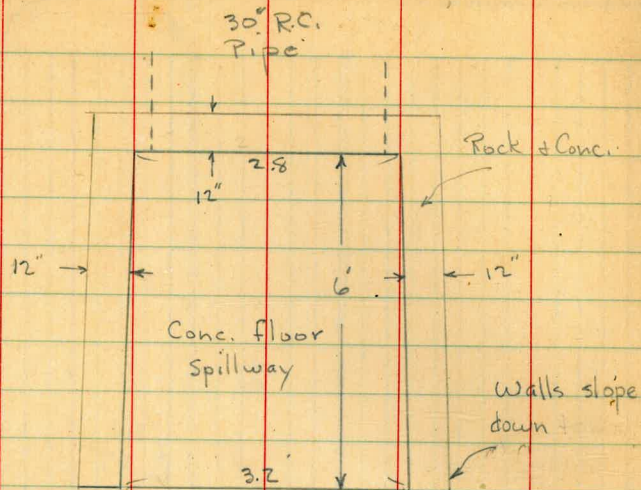
Approx. flow line of 24" pipe - 2.9' W. of E. 3.5' x 2' Grate inlet. (on S. cb. of E. St.)

	13.61	135.81	FL.
TP 12.44	141.09	0.77	148.65
12.27	173.16	0.20	160.89
11.67	184.00	0.83	172.33
check starting B.M.	3.99		180.01 18001

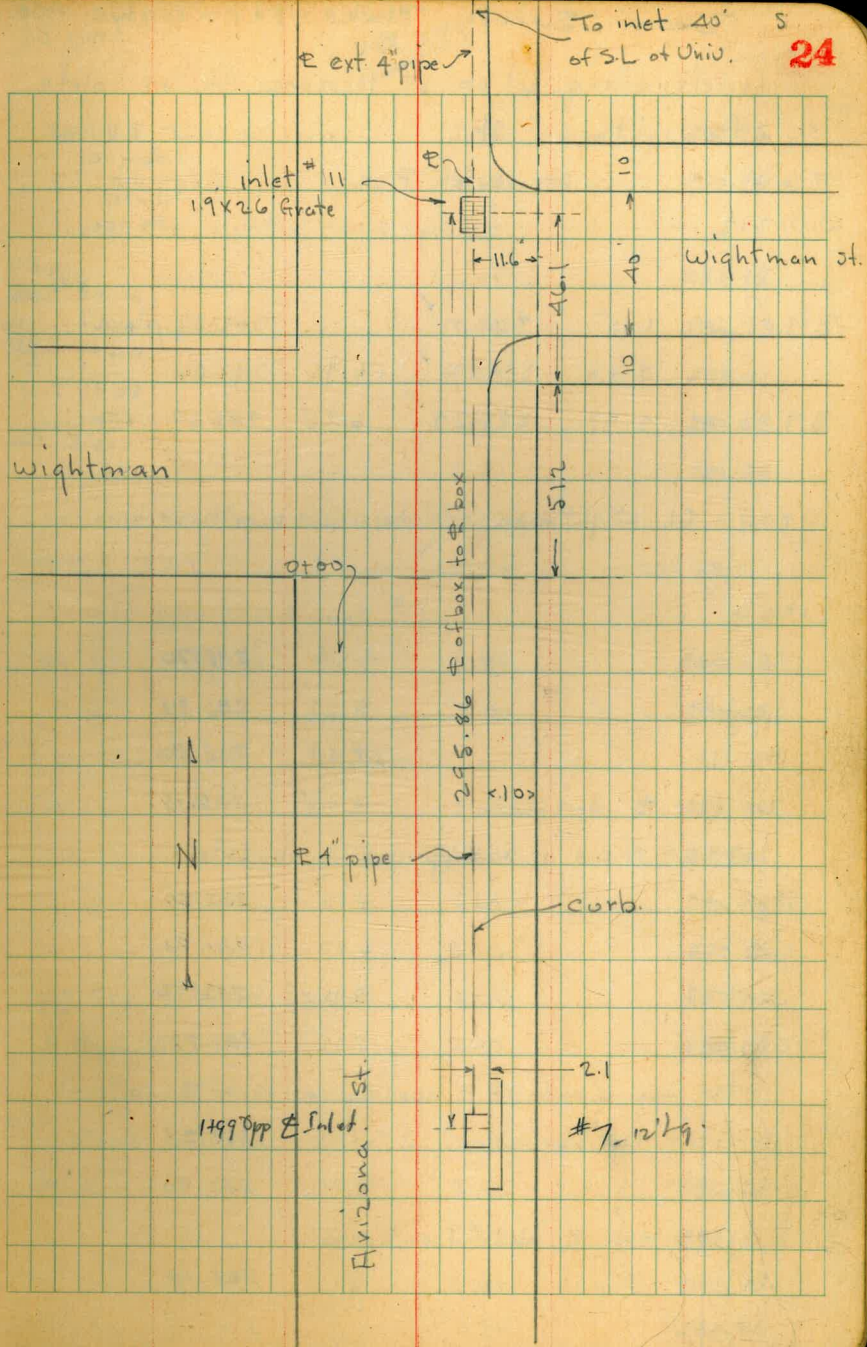
Notes Reduced. 11.29.96



Detail
Outlet "A"



ext 4" pipe
To inlet 40' S of S.L. of Univ. **24**



Drain Survey Blocks - 8+7 - Pauly's Add.
Map 65

Levels along W. cb of Arizona St. at inlets

S. of Wightman St.

#607

see sketch P 22

W.O. 212

11-21-46

Osborne
Hardin
Worrell
Smith

BM	1.15	304.02 ✓		302.87	SE B.P. Texas Landis - plug out took +.01 ch lead
	0.46	291.52 ✓	12.96	291.06	
BM	2.97	288.24 ✓	6.25	285.27	SE B.P. Landis + Arizona 285.31 = Book

0+00 = S.L. Wightman - face of curb is base line

1+50

Top cb	4.54	283.70
gut	5.27	282.97
10' Lt.	4.44	283.80
20' Lt. = E. Arizona	4.05	282.19

1+89.6 = N. end of 20.5 opening curb Inlet

Top	5.85	282.39
gut	6.83	281.91
10' Lt.	5.78	282.96
20' Lt.	5.25	282.99

1+93 = opp N. end of 12' opening inlet on E. cb

40' Lt. = Top cb	5.03	283.21
40' Lt. = gut.	5.84	282.80

1+99 = opp. E. inlet #7 on E. cb.

40' Lt. Top cb.	5.10	283.19
-----------------	------	--------

288.24

25

40' Lt. = gut-on grate	5.98	282.26	
F.L. of box	8.08	280.16	
1+99.7 = E. inlet #5 (20.5 opening)			
Top	6.05	282.19	
gut-on grate	7.46	280.78	
F.L. box	9.23	279.01	
10' Lt.	6.21	282.03	
20' Lt.	5.51	282.73	
2+02.3 = Beg. Conc. slab bet Pb. & walk			
T.P. 5.48	287.66 ✓	6.06	282.18
2+05 = opp. S. end inlet #7			
40' Lt. = Top cb	4.58	283.08	
" " gut.	5.40	282.26	
2+10.1 = S. end Inlet #5			
Top cb.	5.62	282.09	
gut	6.66	281.00	
10' Lt.	5.61	282.05	
20' Lt.	5.06	282.60	
27 Rt. = E. edge of 53 walk	5.62	282.08	
8' Rt. = W. " " " "	5.47	282.19	
2+10.7 = end Conc. slab.			
2+31.8 = N. end Inlet #6 (20.5 opening)			
Top	5.46	282.20	
gut	6.48	281.18	
10' Lt.	5.48	282.18	
20' Lt.	4.91	282.75	

287.66 ✓

2+318 Cont.		
2.7 Rt = E. edge walk	5.46	282.20
8 Rt. W. " "	5.43	282.23
2+42 - Φ Inlet #6		
Top cb.	5.46	282.20
gut. on Grate	6.66	281.00
F.L. box	8.45	279.21
10' Lt.	5.50	282.16
20 Lt.	4.92	282.88
2.7 Rt = E. edge walk	5.40	282.26
8 Rt = W. " "	5.35	282.31
2+52.3 = S. end opening #6		
Top cb.	5.35	282.31
gut.	6.34	281.32
10' Lt.	5.44	282.22
20' Lt = on Sewer M.H.	4.68	282.98
2+75		
Top cb.	5.17	282.49
gut.	6.01	281.65
10' Lt.	5.09	282.57
20 Lt.	4.55	283.11
3+00		
Top cb.	4.94	282.72
gut.	5.68	281.98
10' Lt.	4.88	282.78
20' Lt.	4.40	283.26

end.

26

levels on line of 24" Corrugated Iron pipe - culvert # 2 in sketch. also Φ for proposed new culvert (base line for levels)
 Note: ext. pipe bends to the north in the middle - not straight thru.

287.66 ✓ - opp Page

0-4.93 = face of cb. at E of inlet #6

Top cb.	5.46	282.20
gut. on Grate	6.66	281.00
F.L. box	8.45	279.21
0-02.2 = E. edge walk		
Φ on walk	5.40	282.26
0+00 = W. 5' Line Arizona (see sketch.)		
Φ	5.36	282.30
10' Lt. on walk	5.30	282.36
10' Rt. on walk	5.43	282.23
0+03 = W. edge walk	5.32	282.39
0+15		
Φ	5.0	282.7
10' Lt.	5.0	282.7
10' Rt.	5.1	282.6
0+22.8 - 42 Rt = Cor. 3 1/2" Conc. curb for border		
Top cb.	5.06	282.60
0+30.9 - 2.3 Lt = req. Cor. 2' Conc. walk along house		
Cor. walk	5.47	282.19

287.66 ✓

0+32.7 - 5.9 Rt. = S.E. Cor. House

Floor elev. 3.77 283.89

0+33.2 - 4.2 Lt. = N.E. Cor. House

Floor elev. 4.67 282.99

2+36.1 = Cross pickett fence + Solid Conc. slab bet. Houses

± Top slab 5.82 281.89

5.3 Rt. = N. side slab at cb. 5.50 282.16

3.9 Lt. = slab. ^{2' Conc. walk} along house + end 5.53 282.13

0+36.6 - 5.2 Rt. = end 3/2" cb. at Brick chimney

Top end. 4.99 282.67

0+43.2 = 1.5 Rt. = ± inlet 3" drain pipe in slab

± on Conc. slab 7.30 280.36

1.5 Rt. = F.L. drain 7.74 279.92

0+44.5 = Point of roll down in slab. ?

± 7.12 280.52

3.8 Lt. = slab along house 6.79 280.87

6.6 Rt. = " " " 6.86 280.80

T.P. 3.47 282.38 8.75 278.91

0+46.8 = end solid slab

± 3.14 279.22

1' Lt. = beg. Conc. slab along ^{House} 2.87 279.51

3.6 Lt. = slab at House 1.80 280.58

4.1 Rt. = beg. Conc. slab along ^{House} 3.47 278.91

6.8 Rt. = slab at House 2.26 280.12

282.38 ✓

27

0+51.2 - 2' Lt. = end Conc. slab.

2' Lt. = slab 3.32 279.06

3.2 Lt. = " at House 2.32 280.06

0+55

± 4.2 278.2

0+65.7 - 2.4 Lt. = N.W. Cor. House + beg. 1' Rock wall

± 4.4 278.0

2.4 Lt. Ground at House 4.1 278.3

Floor elev. of basement. 7.2 275.2 Dirt floor

2.4 Lt. = Top wall 2.60 279.8

5.7 Rt. = edge of jrg in slab 4.25 278.13

8' Rt. slab at House 3.94 278.42

0+66.4 - 4' Rt. = Edge slab. 4.43 277.95

0+67.4 - 8.1 Rt. = S.W. Cor. House

Floor elev. Basement - dirt floor. 6.69 275.69

0+69 - 5' Rt. = beg. Conc. Ret. wall 8" with wire fence ^{on top}

± 4.8 277.0

1.6 Lt. = base wall 4.8 277.6

Top wall 4.12 278.26

2.6 ^{lt} ground at wall 6.2 276.2

10' Lt. 6.4 276.0

5 Rt. = base wall 4.8 277.6

Top wall 3.12 275.26

10' Rt. 3.9 278.5

282.38 ✓

0+80 - 1.9 Rt. = Φ of Top 24" Cor. pipe (shows curve to N.)		
Φ	5.8	276.6
1' Lt. - base wall	5.8	276.6
Top "	3.75	278.63
2' = base wall	6.1	276.3
10' Lt.	6.3	276.1
1.9 Rt. = Top pipe	6.10	276.28
5.9 Rt. = base wall	5.9	276.5
Top "	4.08	278.30
7. Rt. =	4.8	277.9
0+86 - 1.4 Rt. = Φ Conc. slab over pipe at joint		
1.4 Rt. = Top slab	5.96	276.82
0+91 - 0.5 Lt. = end Rock wall		
0.5 Lt. = base wall	6.4	276.0
Top "	5.31	277.07
1+00		
Φ	6.5	275.9
10' Lt.	6.7	275.7
7.3 Rt. = base wall	6.6	275.8
Top wall	4.09	278.29
1+01.3 - 2.4 Lt. = Cor. 5.5 Arbor. (2x4 posts)		
1+13 - 1' Lt. = Cor. Arbor.		
1+18.5 - .6 Lt. = Φ of CI Cover to cleanout M.H. - 40" x 40"		
0.6 Lt. = Rim of M.H.	7.46	279.92
FL. of Box	10.71	271.67

282.38 ✓

28

1+21.58 = Ang. 27° 25' Rt. top 30" culvert # 3		
Φ	7.5	279.9
10' Lt. on split	7.8	279.6
9.8 Rt. = base wall	7.3	275.1
= Top "	4.12	278.26
1+34.8 = Cross wire fence		
1+39.5 - 4.1 Lt. = Φ of 1' down drain in N. end of 5' x 2'		
Conc. box with Heavy wire Cover - fastened on. # 9		
4.1 = Top grate	9.59	272.79
1+40 - 1.5 Rt. = end + Cor. Conc. wall		
Φ	8.6	273.8
3' Lt. = Conc. edge at inlet	9.60	272.8
10' Lt.	9.4	273.0
1.5 Rt. = base wall	8.4	279.0
= Top wall	4.20	278.18
1+45		
Φ	8.3	279.1
2' Lt. = Φ ditch	9.5	272.9
3' Lt.	8.5	273.9
10' Lt.	8.3	279.1
4' Rt.	5.8	276.6
10' Rt.	6.0	276.4
1+48 = Φ 4" steel pipe		
Φ on Top pipe	9.10	273.28

282.38

1+52.14 - E edge of 36" x 30" Conc. box inlet with grate on top. - Rock + Conc. wing walls + Head wall Vertical around opening

± Top grate - ± E. edge 9.81 272.57

E.L. box wall 12.66 269.72

1.25 Lt. = grate at base wing 9.81 272.57

" " Top wing wall 5.65 276.73

10' Lt 5.9 276.5

1.25 Rt. = grate at base wall 9.81 272.57

" " Top wing wall 6.40 275.98

10' Rt. 6.1 276.3

1+55.14 - W. edge box + face Head wall

± on grate 9.82 272.56

" on top Head wall 5.28 277.10

T.P. 12.75 295.08 ✓ 0.05 282.33

6.39 300.81 ✓ 0.66 294.42

0.64 296.01 ✓ 5.44 295.37

1.20 284.78 ✓ 12.43 283.58

2.92 275.08 ✓ 12.62 272.16

Levels for Prop. Drain Between Texas + Louisiana - S. of Wightman - See sketch P 23

275.08 - opp. page

0+00 = ± Face of Headwall = ± outlet "A" of 30" culvert under Texas.

Top ± Headwall 8.84 266.28

F.L. Pipe + floor spillway 13.57 261.51

0+06 = edge of wing walls + spillway

± on edge of Conc. 13.83 261.25

1.6 Rt. = Top of end of wing wall 12.24 262.89

10' Rt. 9.4 265.7

16 Lt. = 12.43 262.65

10' Lt. Top end wing wall 9.1 266.0

Note: Seems to be a slab of Conc. about 4' ahead of edge - underwater Cant locate

0+10 = apparent top of Conc. Slab. ✓

± 13.97 261.11

0+15

± 11.8 263.3

10' Lt. 10.2 269.9

10' Rt. 9.8 265.3

0+50

± 10.2 264.9

10' Lt. 11.4 263.7

275.08 ✓

0+50 Cont.

4' Rt. = \pm Ditch	13.3	261.8
10' Rt.	10.6	269.5
0+90		
\pm	11.8	263.3
10' Lt.	11.9	263.2
5' Rt.	11.2	263.9
10' Rt. = \pm ditch	13.7	261.8
20' Rt.	12.4	262.7
1+10		
\pm	12.2	262.9
10' Lt.	12.6	262.5
4' Rt. = \pm ditch	12.6	262.5
8' Rt. Toe of Fill	12.1	263.0
15' Rt. = on New Lot fill	8.9	266.2
1+40		
\pm	10.6	267.5
10' Lt.	9.4	265.7
5' Rt. = \pm Ditch	13.3	261.8
7' Rt. = Toe fill	12.5	262.6
15' Rt.	5.1	270.0
1+75		
\pm	12.2	262.9
10' Lt.	10.4	269.7
4' Rt. = \pm ditch	14.2	260.9
8' Rt. toe fill	12.5	262.6
15' Rt. on fill	6.7	268.8

Notes Reduced. 11-29-86

30

275.08 ✓

1+95		
\pm	11.8	263.3
10' Lt.	9.0	266.1
4' - Rt = \pm ditch	15.7	259.8
7' Rt. = toe fill	14.5	260.6
15' Rt.	9.4	265.7
2+06.87 = Inlet "B" = end 30" R.C. pipe (no wing walls or Headwall)		
Flow Line pipe	17.60	257.98
10' Lt.	9.7	265.8
10' Rt.	9.9	265.2

T.P.	12.65	286.52	12.1	273.37
check B.M. SE. BP. Louisiana			0.60	285.92
				285.88
				Bench book

276
259.4
15

15
Add. Notes for Inlets - pipes etc + walks
on Arizona St

B.M. 4.08 289.35 ✓
R-25
S.E. Lands
+ Arizona

F.L. of 18" pipe in Inlet #7 - 2.5 out from cb.

F.L. + Bottom of box 9.20 280.15

F.L. 4" Conc pipe from N. 8.73 280.62

F.L. of Outlet of 18" Pipe from #7 to #5

F.L. pipe - 1.9 out from cb face 10.30 279.05

Inlet #7 Grate on opening is 4' long (along cb) and
2.3' wide (grate in 2 sections 2' x 2.3')

Inlet #5 - Grate is 3.4' long (along cb) and 2.4'
wide (in 2 sect. 1.7' x 2.4')

Inlet #6 - Grate - 4.9' long x 2.8' wide (2-sect. 2.45' x 2.8')

Elev. of E. edge of Side walk on W. side
of Arizona - adjacent to Inlet #6

Same Sta. + baseline as previous notes on P 15'
+ 26 - edge of walk 2.7' from face of cb.

1+89.6 - edge walk 2.7' 7.01 282.38

7.0.
12-26-46

289.35 ✓

31

2+00 - 2.7 Rt. - Low point 7.25 282.00

2+02.3 " " 7.33 282.02

2+10.7 " " 7.33 282.02

2+20 = Top cb 7.29 282.06

2.7 Rt. - low point 7.31 282.08

2+52.3 - 2.7 Rt. 7.00 282.35

2+75 - " " 6.75 282.60

3+00 6.55 282.80

T.P. 8.81 293.70 ✓ 4.46 284.89

F.L. 4" pipe + Box Inlet #11 4.63 289.07

F.L. 4" pipe to N. 4.66 289.08

F.L. + Grate elev. of Inlets # 12 + 13 on Texas st.

B.M. 2.77 305.64 ✓ 302.87 S.E. Texas + Landis

Top Grate in gut Inlet # 12 on E side of Texas
 Top grate 11.41 299.23
 flow line pipe 41.93 263.71

Inlet # 13 on W. side

Top Grate 12.76 292.88
 flow line pipe 42.95 262.79

B.M. 1.14 287.02 ✓ 285.88 S.E. Landis + Louisiana

Inlets # 14 + 15 on Louisiana

Inlet # 14 on E. Side
 Top Grate - gut 11.45 275.57
 flow line pipe 31.37 255.65

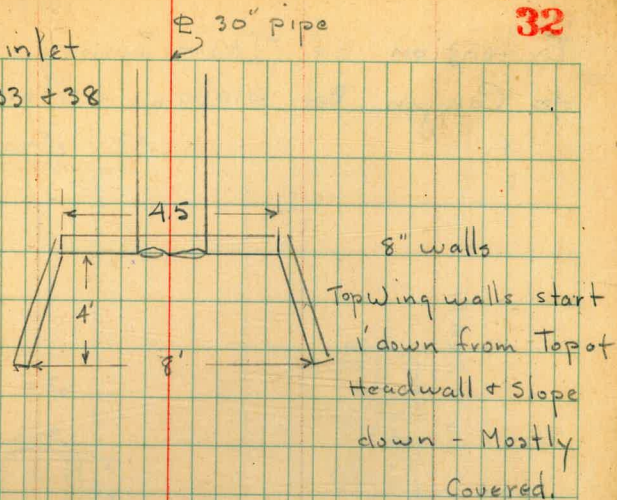
Inlet # 15 on W. Side

Top Grate in gut 12.30 279.72
 flow line pipe 32.50 259.52

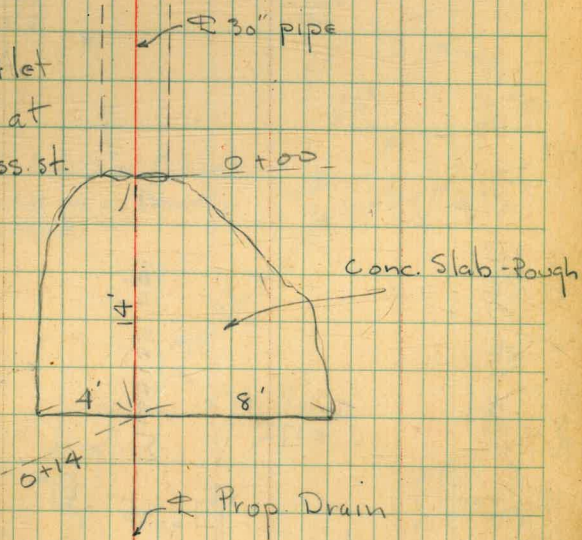
T.P. 12.03 274.99 ✓ on Rock

32

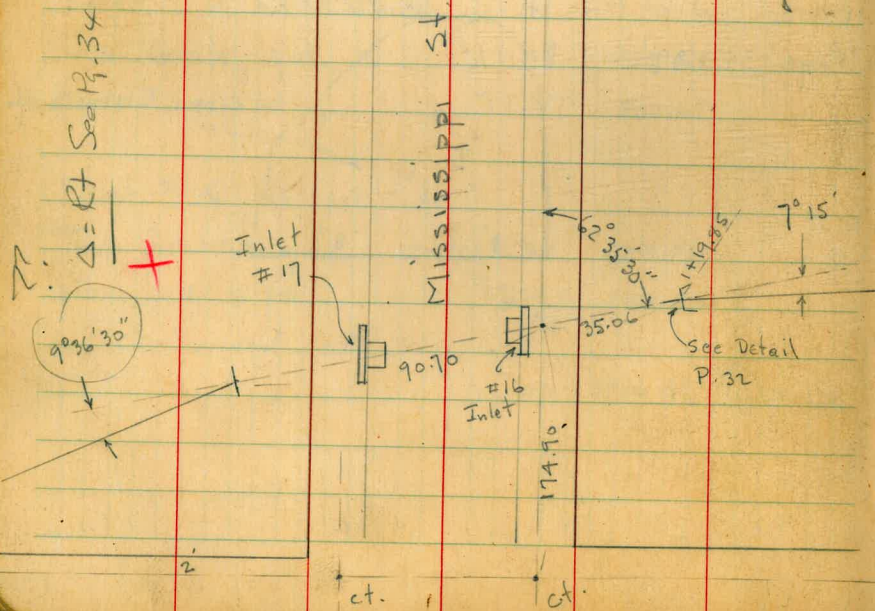
Detail of inlet
 Sta. 1+19.85 - P 33 + 38



Detail of Outlet
 and Conc. Slab at
 0+00 - -W. of Miss. st.
 Page 34 + 39



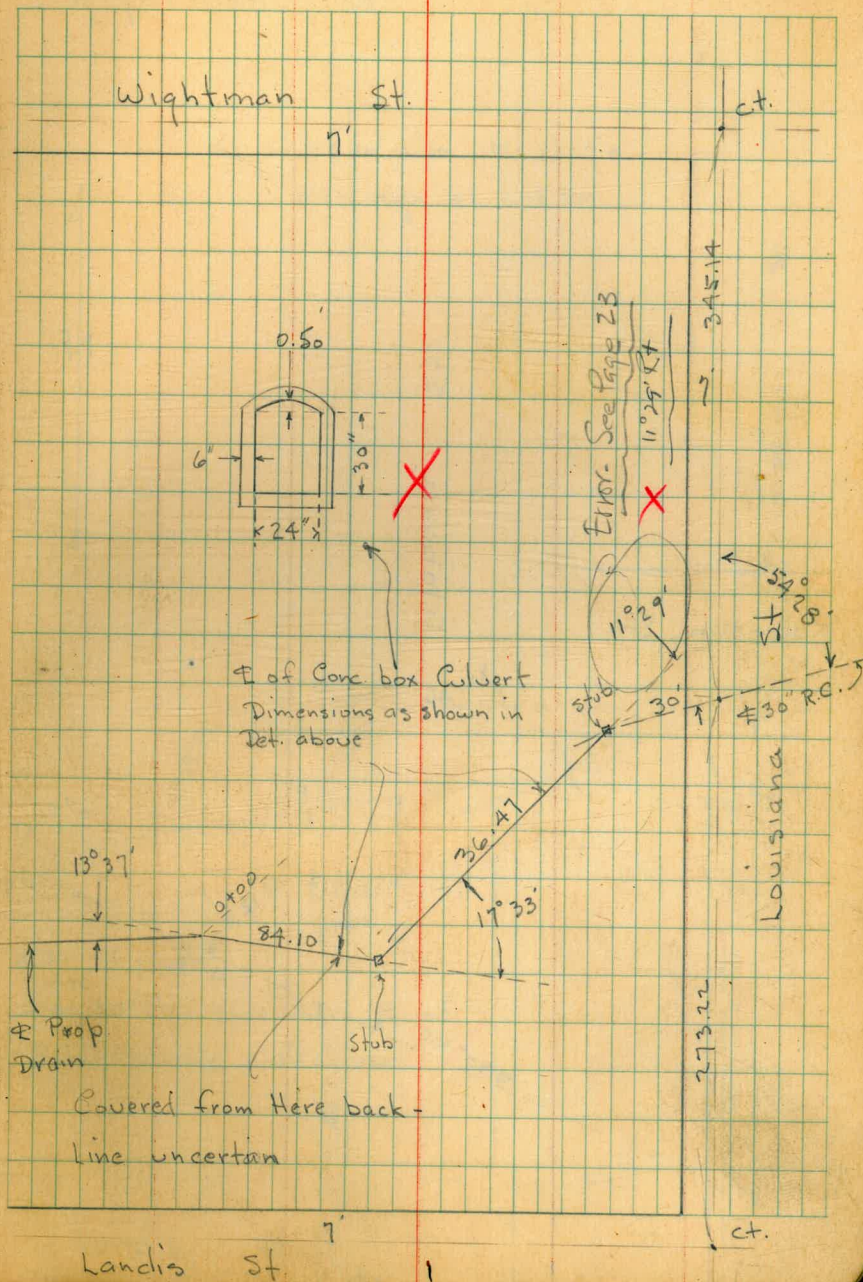
Extension of Drain Survey from Louisiana
to Canyon Bet. Alabama + Florida.



12-26-46
F.O.

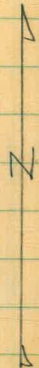
indexed
c.s.K.

33



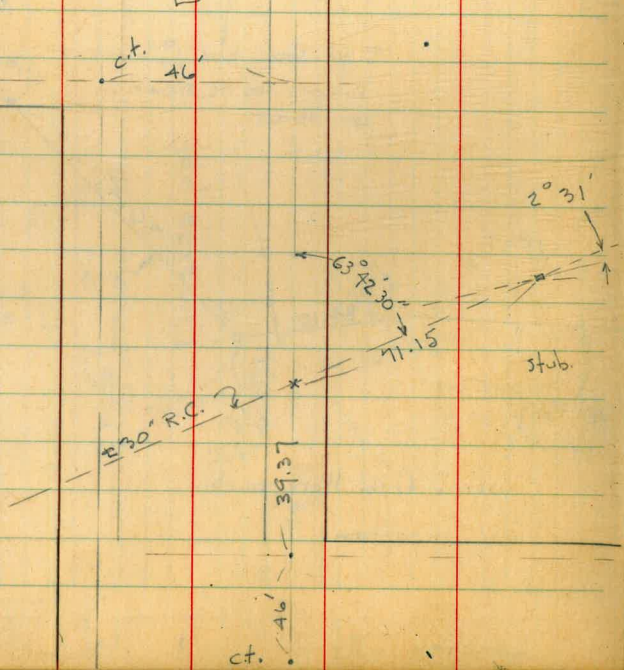
Robinson St.

Alabama St.



7'

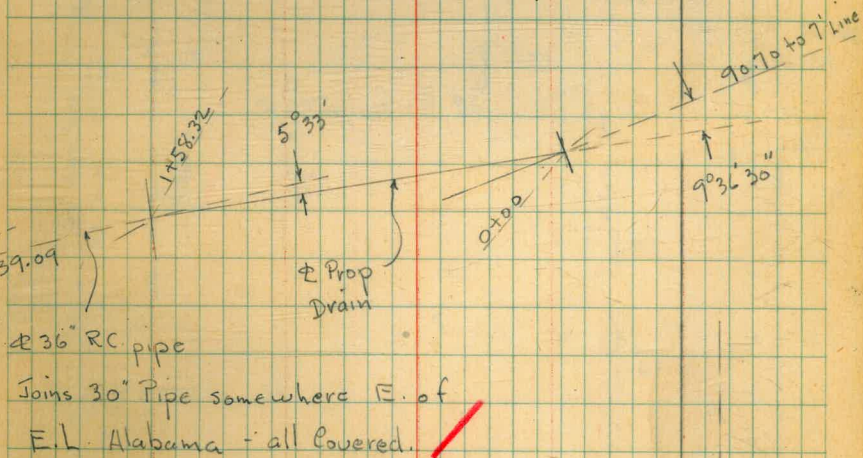
ct. 46'



Wightman St.

Water in pipe 12-27-46
0.20 High at 2:15 PM.

Mississippi St.

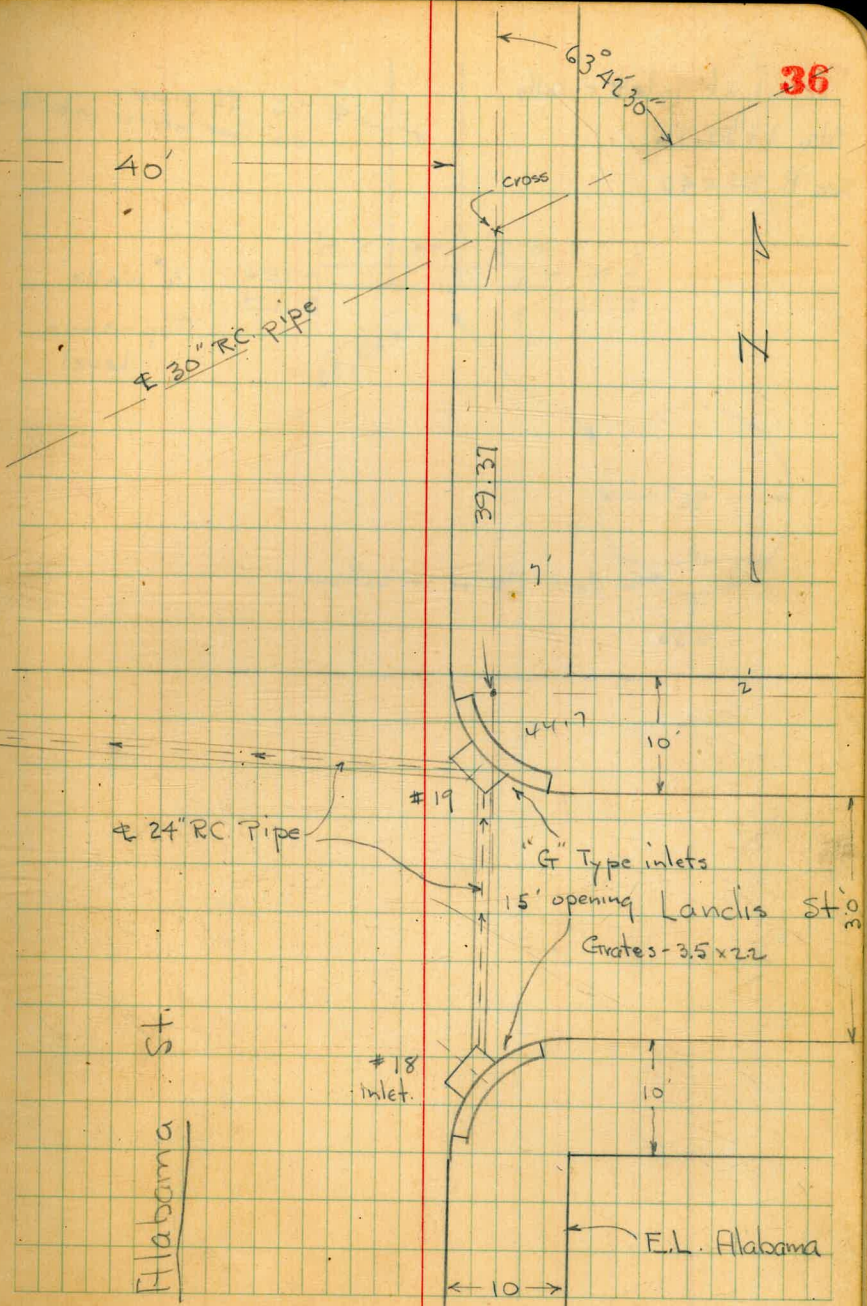
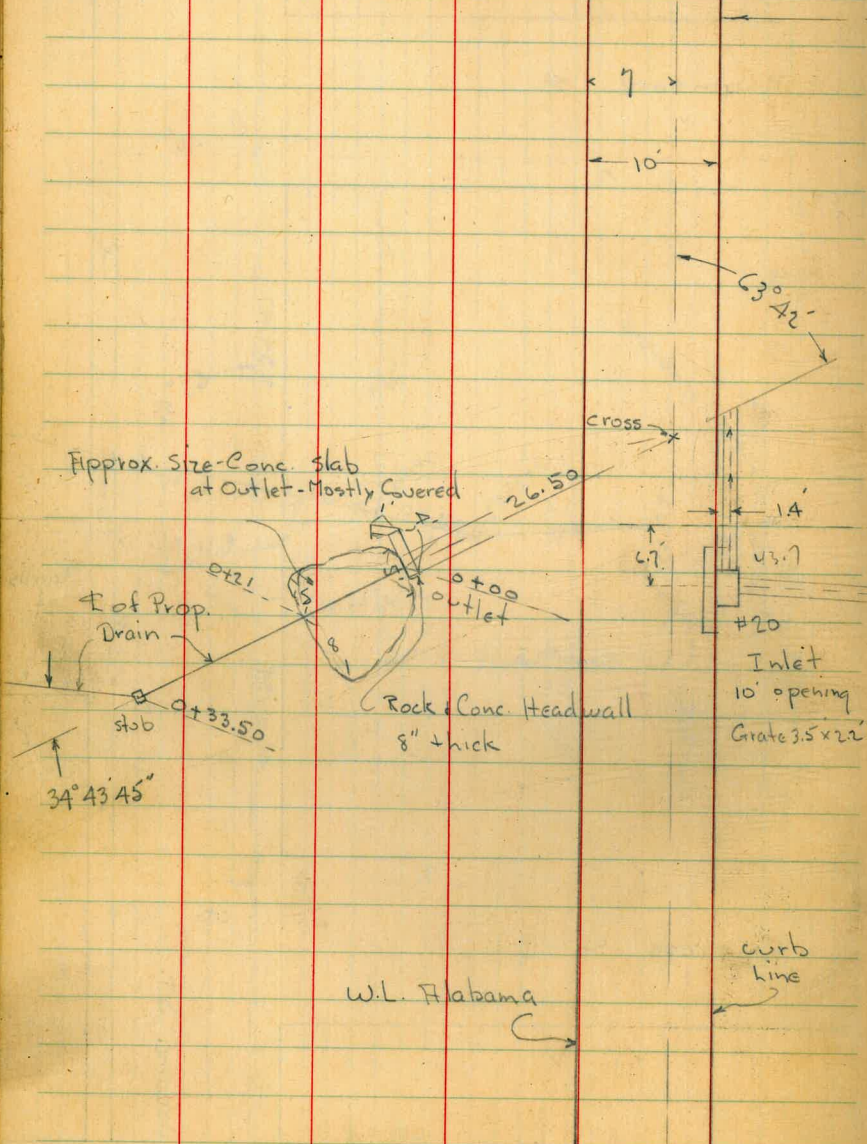


36" RC pipe

Joins 30" Pipe somewhere E. of
E.L. Alabama - all Covered.

Landis St.

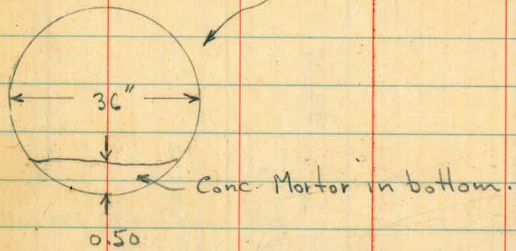
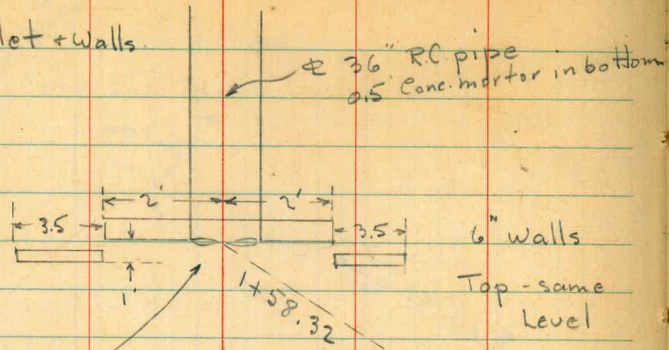
12 Detail of Intersection
to Show Inlets + Culverts



Detail of inlet + walls

Sta. 1+58.32

Sec P. 34 + 40



Levels on Prop. Drain Bet Louisiana & Mississippi.

T.P. P.32	1.48	276.47		274.99
	0.35	263.80	13.02	263.45
	2.98	<u>257.93</u>	8.85	254.95

0+00 = Outlet of Private built Box Culvert - See

Page 33

± = F.L. Culvert		7.02		250.91
6' Lt.		6.4		251.5
10 Lt.		4.3		253.6
10 Rt.		5.3		252.6
0+30				
±		6.4		251.5
5 Lt. = ± ditch		6.9		251.0
10 "		6.0		251.9
10 Rt.		6.1		251.8
0+50				
±		7.1		250.8
2' Lt. = ± Ditch		8.7		249.2
4 "		7.1		250.8
10 Lt.		6.5		251.4
20 "		7.6		250.3
6 Rt. = Toe slope		6.6		251.3
20 " - on fill		+ 3.1		261.0

12-30-46

7.0.

38

257.93

0+80				
± = Toe fill		7.3		250.6
5' Lt. = ± Ditch		9.4		248.5
9 Lt.		7.5		250.4
5 "		8.2		249.7
15 Rt		+ 0.5		258.4
1+05				
± = Toe fill		8.7		249.2
5' Lt.		10.6		247.3
10 "		9.2		249.7
15 "		8.0		249.9
5 Rt.		6.6		251.3
15 "		0.5		257.4
1+19.85 = Inlet of 30" RC pipe + face of Headwall				
± = flow line 30" pipe		12.04		245.89
± Top of Headwall		8.35		249.58
10 Lt.		6.9		251.0
10 Rt.		3.2		254.7
T.P. 12.68		<u>270.39</u>	0.22	257.71

Levels on Inlet # 16 on E. curb of Mississippi
 6.2 opening - 2.4 x 2.5' grate - 12" pipe down to 30" pipe
 F.L. 30" pipe 25.46 245.03
 Top Grate in gut. 4.90 265.49

270.39 ✓

Levels on Inlet # 17 - on w. curb Miss. St.

Same Dimensions as # 16

FL 30" Pipe	26.83	283.56
Top Grate in Gut	5.51	269.88
T.P. 1.46	258.85	13.00 257.39
3.14	249.31	12.68 246.17

Levels on Prop Drain - Bet. Mississippi + Alabama St.

0+00 = outlet of 30" Pipe on W. side of Miss St.
for Detail of Conc. Slab See P 32

⊕ on FL 30" pipe	6.66	282.65
10' Lt.	1.3	288.0
2' Rt. - edge of Conc. Slab	6.5	282.8
6' Rt.	3.4	285.9
10 "	2.5	286.8
0+14 = end Conc. Slab		
⊕ - on Slab	7.56	281.75
8' Lt. = edge Conc.	7.32	281.99
15 "	4.5	288.8
4' Rt. - edge Conc.	7.26	282.05
15 "	2.8	286.8
0+25		
⊕	7.5	281.8

249.31 ✓

5' Lt. = ⊕ Ditch	7.7	281.6
10 "	6.7	282.6
15 "	5.7	283.6
6' Rt.	3.5	285.8
10 "	2.4	286.9
0+40		
⊕	6.3	283.0
7' Lt. = ⊕ Ditch	8.7	280.6
10 "	7.9	281.8
20 "	5.6	283.7
3' Rt.	4.7	289.6
20' Rt.	2.8	286.5
0+70		
⊕	8.3	281.0
4' Lt. = ⊕ Ditch	9.0	280.3
8' "	6.4	282.9
15 "	7.5	281.8
3' Rt.	6.3	283.0
10 "	5.5	283.8
20 "	3.4	285.9
0+74 - 5' Lt. = ⊕ 2" Euc. Tree		
1+00		
⊕	9.2	280.1
2' Lt.	11.2	238.1
4' Lt.	9.0	280.3

39

249.31		
7' Lt. = in Berry Bushes	7.9	241.2
20 "	8.0	241.3
6' Rt.	7.7	241.6
20' Rt.	8.5	240.8
1+14 - 8.7 Rt. = ϕ 18" Cottonwood		
1+15 - 8.5 Lt. = ϕ P. pole		
1+25		
ϕ = ϕ Ditch	10.6	238.7
5' Lt.	8.1	241.2
10 "	8.3	241.0
20 "	6.6	242.7
5' Rt.	8.4	240.9
20 "	9.1	240.2
1+56 = edge of Conc. Slab at inlet		
ϕ on Conc.	10.88	238.93
1.5 Lt. = edge Conc.	10.72	238.59
6' Lt.	7.5	241.8
9.7 Lt. = ϕ 3' Pepper tree		
1.5 Rt. = edge Conc.	10.73	238.58
5' Rt.	9.0	240.3
10 "	8.8	240.5
1+58.32 = Inlet 36" RC pipe + Headwall - See Detail		
P. 37		
ϕ = F.L.	10.78	238.53
Top Headwall	7.40	241.90

249.31				
T.P.	5.49	248.45	6.35	242.96
	4.31	251.77	0.99	247.46
check B.M. S.E. Landis + Alabama			6.26	245.51
	1.89	247.41		245.52
Levels on Inlets #18-19+20 at Int of Landis + Alabama - See Detail P. 36				
# 18 - "G" Type on S.E. Ret.				
Flow line of Box	7.70			239.71
Top of grate in Gut.	3.01			244.80
# 19 - "G" on N.E. Ret.				
F.L.	9.45			237.96
Top Grate	2.68			244.73
# 20 - "A" Type on W.cb.				
F.L.	12.29			235.12
Top grate	3.75			243.66
T.P.	4.73	239.74	12.40	235.01
Begin Levels on Prop. Drain W. of Alabama to creek E. of Florida St.				
0+00 = outlet of 30" RC pipe - See Detail P. 36				
ϕ = F.L. 30" pipe	8.01			231.73
ϕ Top Headwall	3.96			235.78
2.5 Lt. = edge Conc. slab.	7.90			231.82
10' Lt.	0.9			238.8

0+100 Cont

239.74 ✓

25 Rt. = edge Conc.	8.46	231.28
10 Rt.	0.4	239.3
0+12		
Φ - on Conc. slab.	10.18	229.56
Φ on Dirt	9.2	230.5
7' Lt.	9.4	230.3
15 "	3.2	236.5
20 "	+ 1.2	240.9
9' Rt. (Slab Covered to deep.)	8.1	231.6
25' Rt.	+ 1.0	240.7
0+21 = end of Conc. Slab (approx.)		
Φ on slab.	10.62	229.12
Φ on Dirt	8.4	231.3
9' Lt.	7.9	231.8
15 "	1.7	238.0
20 "	0.7	239.0
7' Rt.	7.7	232.0
20 Rt.	+ 0.9	240.6
0+33.50 = Ang. pt. (outs on split of Ang.)		
Φ	9.1	230.6
8' Lt.	9.5	231.2
12 "	5.2	237.5
10 "	4.5	235.2
4 Rt.	8.0	231.7

239.74 ✓

41

20 Rt.	0.0	239.7
0+50		
Φ	10.3	229.4
13 Lt.	10.1	229.6
15 Lt.	7.6	232.1
20 "	7.2	232.5
4 Rt.	8.6	231.1
20 Rt.	0.0	239.7
0+65		
Φ - Φ Ditch	12.1	227.6
3' Lt.	11.1	228.6
5 "	8.8	230.9
20 "	8.1	231.6
3 Rt.	10.7	229.0
20	1.0	238.7
0+89 - 11' Rt. Φ 8" Pine		
1+00		
Φ	13.1	226.6
9 Lt.	13.2	226.5
11 "	9.8	229.9
20 "	9.2	230.5
6 Rt.	11.9	227.8
10 "	9.8	229.9
20 "	7.2	232.5
TIP 288	232.89	9.73
		230.01

232.89 ✓

1+16 = 12.2 Rt. = ± 8" Pine.		
1+20		
±	4.0	228.9
20' Lt.	3.5	229.4
2' Rt. = in ditch	6.9	226.0
8' " " "	7.6	225.3
10 "	3.7	229.2
20 "	2.8	230.1

1+33 = 11.5 Rt = 7" Pine

1+40		
±	4.3	228.6
20 Lt.	4.5	228.2
1 Rt. = in Ditch	7.7	225.2
7' " " "	7.7	225.2
10 "	4.0	228.9
20	4.2	228.7
40' Rt. = E. side of Small House	1.80	231.09 floor.

1+45 = 10' Rt. = ± 3' Pine

1+50		
± = in Ditch	8.0	227.9
1' Lt.	4.6	228.3
20 "	4.6	228.3
6' Rt.	7.6	225.3
9' Rt.	4.3	228.6
20 "	4.6	228.3

232.89 ✓

42

1+67 = 9' Rt. = ± 4" Pine

1+75		
± in Ditch	8.4	227.5
4 Lt.	7.9	225.0
6 "	5.5	227.2
20 "	4.9	228.0
5 Rt.	8.0	227.9
7 "	5.5	227.2
20' Rt.	5.3	227.6

1+80 = 9' Rt. = ± 3" Pomegranite

1+88 = 19' Lt. = ± 3' Eve. Tree

2+00		
±	9.4	223.5
4' Lt.	8.9	222.0
6 "	6.5	226.2
20 "	6.1	226.8
4' Rt.	9.0	223.9
6 "	5.7	227.2
20 "	5.9	227.0

2+05

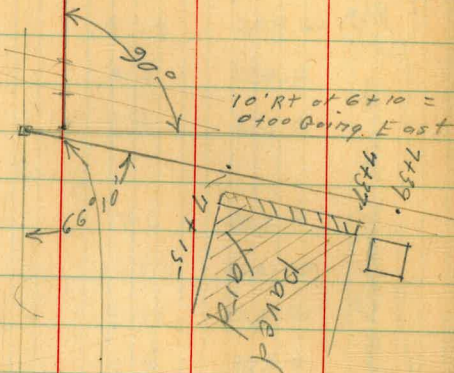
±	9.7	223.2
6' Lt.	9.6	223.3
8' "	7.2	225.7
20 "	7.1	225.8
10' Rt. = in N. + S. Creek	8.7	222.2

		✓		
		232.89		
2+11-	Beq. Conc Ramp on Lt.			
±		10.6	222.3	
14.4 ft.	Cor. Conc.	8.28	222.61	Notes Reduced 1-3-87
20 Lt. =		8.0	222.9	
20 Rt. =	in Creek	9.4	223.5	
2+25-	Cor. - end of Ramp			
±		10.6	222.3	
3' Lt. =	Cor. Ramp	10.82	222.07	
18' Lt. =	S. edge Ramp	9.48	223.21	
20 "		10.5	222.2	
6 Rt.		9.2	223.7	
20 Rt.		8.6	224.3	
2+32 =	± 15" Conc. Box - Covering Sewer line			
± -	Top box	9.48	223.02	
2+35				
±		9.9	222.9	
20' Lt.	in Creek	11.0	221.9	
20 Rt.		7.4	225.5	
2+49.02 =	Stub. = end.			
± on	Stub.	6.17	226.72	
20' Lt.		7.0	225.9	
20 Rt.		5.4	227.5	
T.P.	13.08	245.37	0.60	232.29
check B.M.		+ 0.15		245.52 ✓

DRAINAGE LEVELS
South side Frontier St.

Frontier

6+103 1x1 stub L.
L=113°-50' Lt



605.58

50 ← → 40 → 10

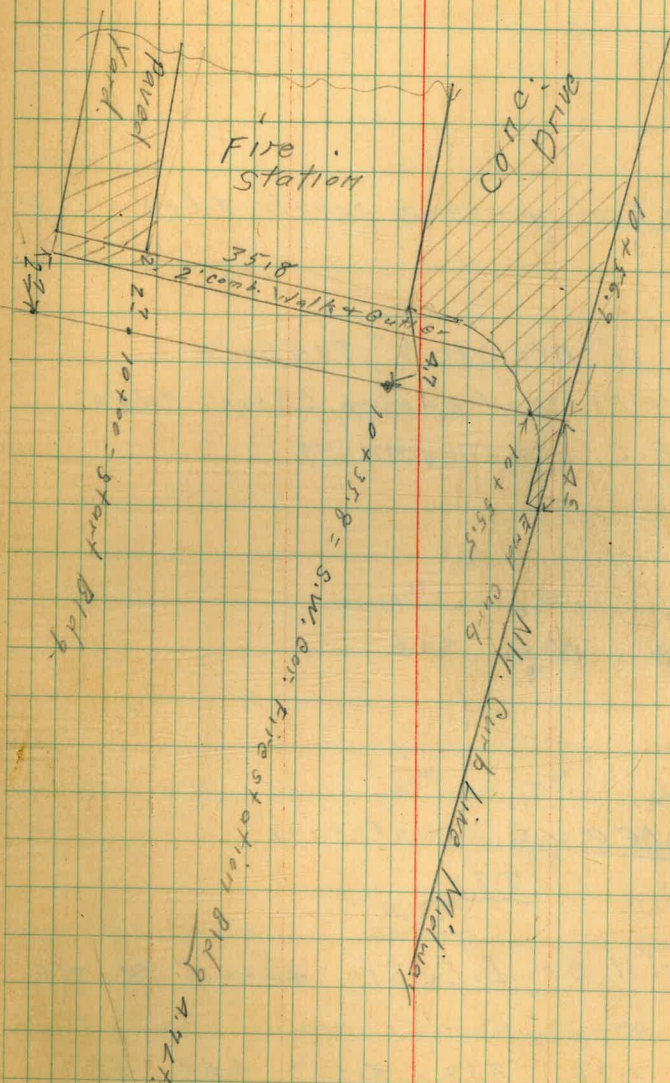
0+00 = E.C. 42+65.80 FB. 1579 page 20
5' Fd. 1/2 Hub

F.d. 2/2 Hub

Sommermeier
in Moore
J. Green

Work Order
210

2-13-47 44



0+10 End paving rough edge

0+06.5 11' Rt = ctr. 9" Tel. pole

0+02 10' Rt = End paving (Rough edge)

0+00 = E.C. on paving

(0+0) - 50

(0+0) - 100 on paving

7.38

0+00 will be E.C. Sta. 42+65.80 -

B.P. in Culvert	2.78	7.38	5.52	4.60
Head Wall	7.22	10.12	—	2.90
850' West of W. Dr. Loma				
on Midway Drive.				

2.10	2.1	2.9
4.68	$\frac{5.3}{8}$	$\frac{4.5}{12}$

2.89	2.44	2.83
4.47	$\frac{4.94}{7}$	$\frac{4.55}{12}$

3.35	2.10	3.23
4.03	$\frac{4.48}{9}$	$\frac{4.05}{12}$

3.86	3.37	3.60
3.52	$\frac{4.06}{13}$	$\frac{3.78}{18}$

7.38

FB 1679-P.20.

B.L. = Base line = 10' North of
So. line Frontier.

1+75

1+50

1+47

12' Rt. = Ctr. 9" Tel. Pole

1+25

1+00

0+75

+50

0+25

7.38
x

21	20	25
5.3	<u>5.4</u>	<u>4.9</u>
	5	15

21	21	21
5.3	<u>5.3</u>	<u>5.3</u>
	6	10

22	21	23
5.2	<u>5.3</u>	<u>5.1</u>
	6	10

23	22	23
5.1	<u>5.2</u>	<u>5.1</u>
	6	10

24	23	25
5.0	<u>5.1</u>	<u>4.9</u>
	6	10

25	23	21
4.9	<u>5.1</u>	<u>4.7</u>
	7	12

25	21	26
4.9	<u>5.3</u>	<u>4.8</u>
	7	10
		5.4

7.38

Frontier

+ 25

3 + 00

+ 75

2 + 50

T.P. 5.36 $\frac{7.54}{7.38}$ 5.20 2.18

+ 25

2 + 00

7.38

BL.

47

2.0 1.6 2.4
5.5 $\frac{5.9}{10}$ $\frac{5.1}{12}$

2.0 1.6 2.2
5.5 $\frac{5.9}{10}$ $\frac{5.3}{12}$

2.0 1.7 2.3
5.5 $\frac{5.8}{10}$ $\frac{5.2}{12}$

1.8 1.5 2.5
5.7 $\frac{6.0}{10}$ $\frac{5.0}{12}$

2.0 2.0 2.9
5.4 $\frac{5.4}{10}$ $\frac{4.5}{15}$

2.0 2.1 2.0
5.4 $\frac{5.3}{10}$ $\frac{4.8}{15}$
7.38

4 + 75

4 + 50

+ 25

4 + 00

+ 75

3 + 50

7.54

51	21	2.0	1.6	2.4	2.9
$\frac{4.4}{2.0}$	$\frac{4.8}{1.0}$	5.5	$\frac{5.9}{1.0}$	$\frac{5.3}{1.2}$	$\frac{4.6}{5.0}$
Par.					

2.0	1.7	2.3
5.5	$\frac{5.8}{1.0}$	$\frac{5.2}{1.2}$

2.0	1.7	2.3
5.5	$\frac{5.8}{1.0}$	$\frac{5.2}{1.2}$

2.0	1.5	2.5
5.5	$\frac{6.0}{1.0}$	$\frac{5.0}{1.2}$

1.9	1.5	2.7
5.6	$\frac{6.0}{1.0}$	$\frac{4.8}{1.2}$

1.9	1.6	2.6
5.6	$\frac{5.9}{1.0}$	$\frac{4.9}{1.2}$
	S.A. 10	

7.54

B.L.

T.P. 4.31 6.20 5.65 1.89 $\frac{2.6 \times 10}{113^\circ 50' RT}$

7.54

6+10 L: $113^\circ 50'$ RT.

6+00

+75

+50

+25

5+00

7.54

3.0 2.5 1.89
 $\frac{4.5}{20}$ $\frac{5.0}{10}$ 5.65 - on stub
 Pav.

3.0 2.5 1.9 1.5 2.0
 $\frac{4.5}{20}$ $\frac{5.0}{10}$ 5.6 6.0 5.5
 Pav. 12

3.1 2.5 1.9 1.6 2.0 3.1
 $\frac{4.4}{20}$ $\frac{5.0}{10}$ 5.6 5.9 5.5 4.4
 Pav. 12 10

3.1 2.6 2.0 1.6 2.5 3.0
 $\frac{4.3}{20}$ $\frac{4.9}{10}$ 5.5 5.9 5.0 4.5
 Pav. 10 12 10

3.1 2.7 2.0 1.6 2.2 3.5
 $\frac{4.3}{20}$ $\frac{4.8}{10}$ 5.5 5.9 5.3 4.0
 Pav. 10 12 60
 on floor
 Cataparch

3.1 2.6 2.1 1.5 2.1 3.1
 $\frac{4.3}{20}$ $\frac{4.9}{10}$ 5.4 6.0 5.4 4.4
 Pav. 10 12 50
 S. Lino

7.54

Φ AS TUN = B.L. Φ

7+44.5 = 3rd RT. = start picket fence

7+39 3.4 RT. = Φ 4' x 4' Inerator
Brick on Conc. Base

7+37 - 2.5 RT. = End 8" Conc. Wall

7+15⁷ - 2.5 RT. = start 8" conc wall

7+00

6+90

6+50

6+21

6+20⁹³ = S. Line. Frontier.

6.20

1.1	1.7	3.0
$\frac{4.5}{5}$	4.5	$\frac{3.2}{5}$

1.9	2.8	2.9	2.9
$\frac{4.3}{10}$	$\frac{4.4}{5}$	3.3	$\frac{3.3}{5}$

2.3	2.2	2.3
$\frac{3.9}{5}$	4.0	$\frac{3.9}{5}$

2.1	2.2	2.1
$\frac{2.1}{5}$	4.0	$\frac{2.1}{5}$

1.6	1.6	1.6
$\frac{4.6}{5}$	4.6	$\frac{4.6}{5}$

Φ
6.20

9+90³ 2.7 Lt = N.W. Cor. paved Fire station yard.

9+84 1.0 Rt = start 2XA - Rail fence
3.3 Rt = End. picket fence

9+50

9+20 4.3 Lt = End row of 5" poplars

T.P. 4.17 $\frac{6.06}{6.20}$ 4.31 1.89

9+00

8+50

8+00

7+75 5' Lt = start row of 7 poplar trees
5" trunk diam.

7+50

6.20

E

2.09

$\frac{3.97}{2.9}$

1.8

$\frac{4.3}{5}$

1.1

5.0

2.4

$\frac{3.7}{4}$

9

6.06

1.6

$\frac{4.6}{5}$

1.1

5.1

1.1

$\frac{5.1}{2}$

2.1

$\frac{4.1}{4}$

1.9

$\frac{4.3}{5}$

1.8

4.4

1.8

$\frac{4.4}{2}$

2.8

$\frac{3.4}{4}$

1.8

$\frac{4.4}{5}$

1.6

4.6

1.6

$\frac{4.6}{2}$

3.4

$\frac{2.8}{4}$

1.7

$\frac{4.5}{5}$

1.6

4.6

1.6

$\frac{4.6}{2}$

3.4

$\frac{2.8}{4}$

6.20

T.P.

5.38

7.39

4.99

2.01

7.00

6+00

5+00

4+00

3+00

2+00

1+00

7.00

B.L.
S. Line Frontier

33

2.0

5.0

1.7

5.3

1.8

5.2

1.6

5.4

1.7

5.3

1.6

5.4

7.00

BL
S.L. Frontier

54

T.P. 5.62 8.47 4.54 2.85

7.39

12+00

11+00

10+00

9+00

8+00

7+00

7.39

2.6
—
4.8

2.7
—
4.7

2.5
—
4.9

2.1
—
5.3

1.9
—
5.5

1.9
—
5.5

7.39 ✓

18+00

2.9

5.6

17+00

2.8

5.7

16+00

3.0

5.5

15+25

3.2

5.3

14+69 Apex of Fordham

2.9

5.6

1A+00

2.9

5.6

13+00

2.8

5.7

8.47

8.47 ✓

29+00

23+00

22+00

21+00

T.P. 4.33 7.23 5.57 2.90

20+00

8.47

19+00

8.47

2.1

5.1

2.4

4.8

2.4

5.0

2.3

4.9

7.23 ✓

2.5

6.0

2.6

6.0

8.47

28+00

27+17 Approx Φ Reliant St.

T.P. 494 7.48 A.69 2.54
7.23

27+00

26+00

25+00 stationing on S. Line Frontier

24+85.66 = B.C. RT

7.23

B.L.

57

23

5.2

24

5.1

7.48 ✓

23

4.9

20

5.2

21

5.0

22

5.0

7.23

T.P. 4.98 7.46 5.00 2.48

7.48

33+00

32+00

31+00

30+00

29+00

28+64.19 = EC

7.48

2.4
5.1
5
IN OUT

2.7
4.8

2.0
5.5

2.4
5.3

2.1
5.3

2.3
5.2

2.3
5.2

7.48

S.W.B.P.
Kurtz +
Rosecrans

7.46

4.50

2.96

2.97 - correct E.L.
2.97

34 + 38.4 = start state paving ^{FB} 1679-8

3A100

7.46

B.L.
So. Line
Frontier

38

2.9 3.0
4.6 4.5
11
07 Pav.

2.9 3.4 2.8
4.6 4.1 4.7
10 6

7.46

Summer Mayer
W. Moore
J. Green

2-18-47

W.O. #210

Elevation Top of
La Playa & Haines

0+60 = 50' So.-So. line La Playa

N.E.B.R. La Playa + Frontara

12.41 31.86 — 19.45

0+00 top pipe 6.07 25.79

" Ground 3.3

0+50 so. line La Playa

1+04 top pipe 5.25 26.61

" Ground 3.6

Notes Reduced -

2-25-47 - Wheeny -

16" Water line 1+04

60

So. Line La Playa 0+50

54'

23'

50'

0+00

East line Haines

16" Water line

23'



Re Survey Lot 4 Block 76 Homestead Union

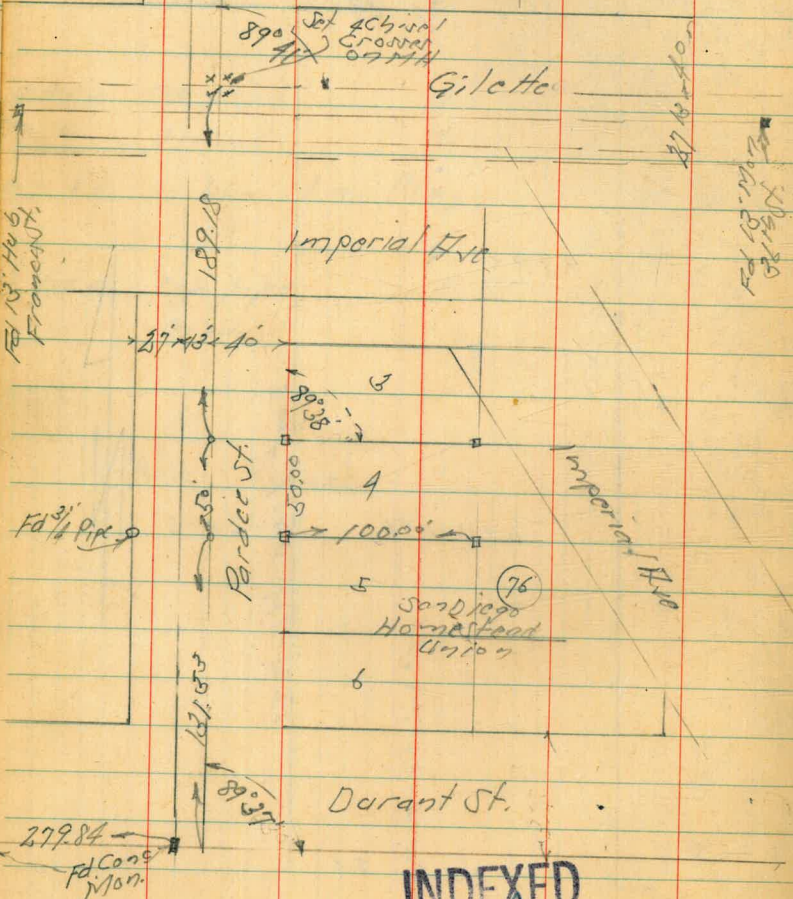
For Ogden

Falst
B. Tompkins
H.A. Bardea

Indicator
Hub & Disc Set

Nov 20-50
H.S. 5509
Garber
Rorer
Pulley

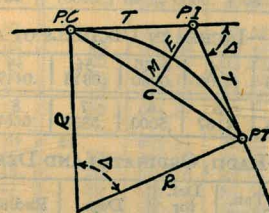
N.O. 22009



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DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

- Radius $= R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve $= D$ and $\sin \frac{D}{2} = \frac{50}{R}$ (2)
- Tangent $= T = R \tan \frac{\Delta}{2}$ (3) Length of Curve $= L = 100 \frac{\Delta}{D}$ (4)
- Middle ordinate $= M = R(1 - \cos \frac{\Delta}{2})$ (5) $= R \text{vers} \frac{\Delta}{2}$ (6)
- External $= E = T \tan \frac{\Delta}{4}$ (7) $= R \div \cos \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)
- Long Chord $= C = 2 R \sin \frac{\Delta}{2}$ (10) $\Delta =$ Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I. = Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $+8\frac{1}{2} = 414.49$ ft. From Table V correction $= .36$ or $T = 414.85$ ft. P. C. = Sta. P. I. $- T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T. = Sta. P. C. $+ L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = 158 - Sta. P. C. = 54.50, hence offset = $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle $= \frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^\circ$ or = defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve $= .3 \times 54.5 \times 8\frac{1}{2} = 136.2'$ or $2^\circ 16.2'$, or $= 2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle $= 2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{2} = 115.27$ and from Table V correction $= .10$ or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

**DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.**

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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