

1725

EVANS' BOOKS
FIELD BOOK
No. 404

1725

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

CITY ENGINEER'S OFFICE

016

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.
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This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

Lilac Park	41
X sec High Ave	51
" Bluebird Lane	43

Relocate Prop. Sewer At end of Ozark st

0+00 = Sta. 6+25.90 on old line.

B.M.	2.93	143.57	140.64	on Hub. 3+86.63 1673-P.2
0+00 - on new stub	2.40	141.17		
0+50	3.2	140.4		
1+00	3.4	140.2		
-65 Lt.	12.1	131.5		
1+50	3.2	140.4		
2+00	2.9	140.7		
2+10 - 8' Rt. = ± Small frame house	+10.30	153.87	Floor	
2+50	2.3	141.3		
-70' Lt. = Vac. lot.	10.5	133.1		
2+95.92 Ang 2°00'30" Lt.	2.80	140.8	on stub	
3+00	3.0	140.3		
10' to w. end.				
3+25 = E. end 8" Cobble wall	2.70	140.9	Top wall	
	3.9	139.7	ground.	
3+34 - 8' Lt. = Beg. Holly Tree Hedge - av. 8' cc.				
3+46 - 68' Rt. = ± Med	1.10	142.47	Floor	
Frame House - Note: Toilet + Wash house in back is 38' lower than House floor.		138.7	Floor	
3+50	5.7	137.9		
4+00 - ±	12.0	131.6		
-131' Lt. = ± Large frame House	16.48	127.09	Floor	

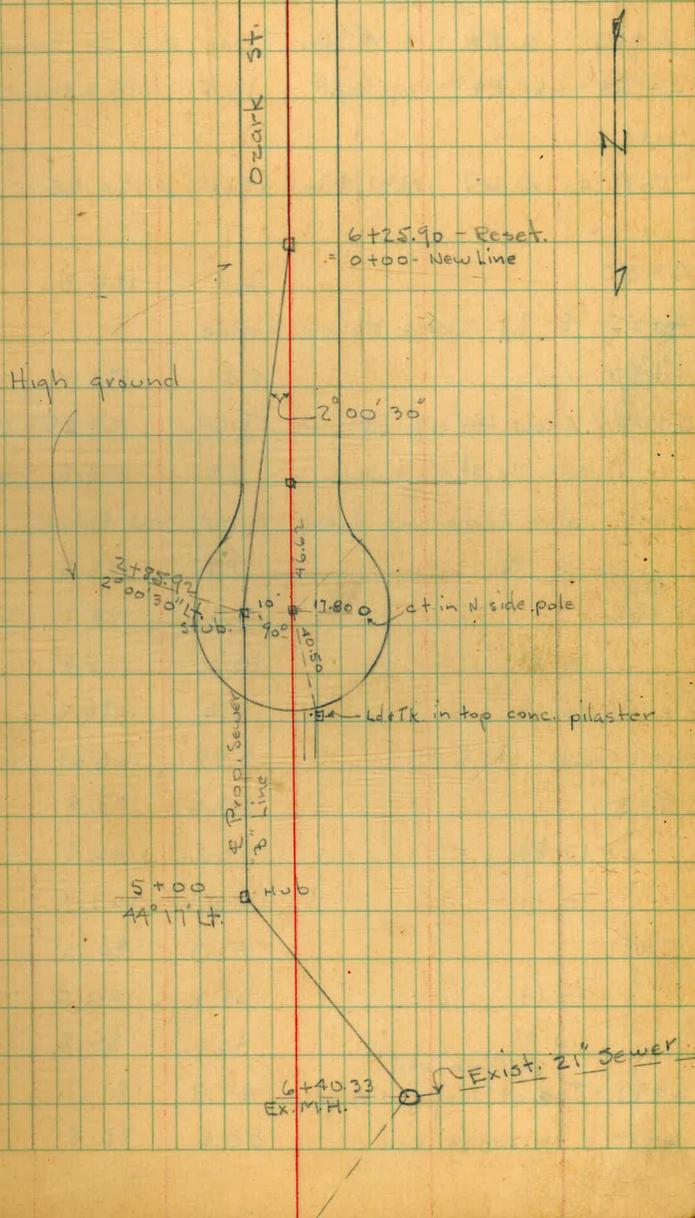
7-7-46

Deborne
McCoy
Hardin

Indexed
c.s.M.

8+68.10 P.O.T.
Fd. stub.

2



143.57

4+10 - 6' Rt. = 4" fir Tree			
4+30 - 65' Rt. = Prop Bld. site	13.5	130.1	
T.P. - 0.67	131.42	12.82	130.75
			stub 15" Rt 4+25
4+50	3.1	128.3	
4+55 - 8' Lt. = end Holley Hedge			
4+90	4.8	126.6	
5+00 = Angle 44° 17' Lt.	7.09	124.33	on Hub.
10.2 Lt. at 90° to back	5.6	125.8	on Ground.
Tang. = Wire fence and E. end - 15' Rt.	E+W slat fence 7.9	123.5	
5+17	8.3	123.1	Top of bank
10 Rt.	14.6	116.8	
10 Lt.	6.0	125.4	
check Hub. 1+25.79	5.95	125.47	1673-P2 125.49
5+50	27.6	103.8	
10 Rt.	30.6	100.8	
10 Lt.	23.6	107.8	
5+72	41.3	90.1	
10 Lt.	31.4	100.0	
10 Rt.	45.6	85.8	
5+97 = Toe of slope + edge of Creek bed.	49.7	81.7	
6+13 - in. creek bed	50.6	80.8	

131.42

6+40.33 = 2 Ext. M.H. - Top sealed.			
on ground at M.H.	48.4	83.0	1673 P.2
B.M. on shoulder M.H.	46.1	85.3	85.27

Turned down with Hand Level - had check on M.H.

Location of Prop. Sewer + New Easement Lines N. of Imp. + Bet 50th + Euclid.

8-6-46
Osborne
McCoy
Hardin
Waddel

B.M. 11.63 179.82 168.19 Stub. 27+21.14 1673-P7

30+40 = end of old line 7.19 172.63 on stub

30+50 = Beg. wire fence on line

30+68 - R 6.6 173.2

28.3 Rt. = Small house 0.96 178.86 on floor

30+82 - 76.8 Rt. = Large stucco House + 5.40 185.22 floor
No plumbing

Conc floor of basement 2.89 176.93

30+97 = end of E+W. fence on line + Cross Wire fence

31+00 6.3 173.5

31+49.14 = Ang. 90° Rt. 6.41 173.41 on stub

100 Lt. = N. along Lot line 14.0 165.8

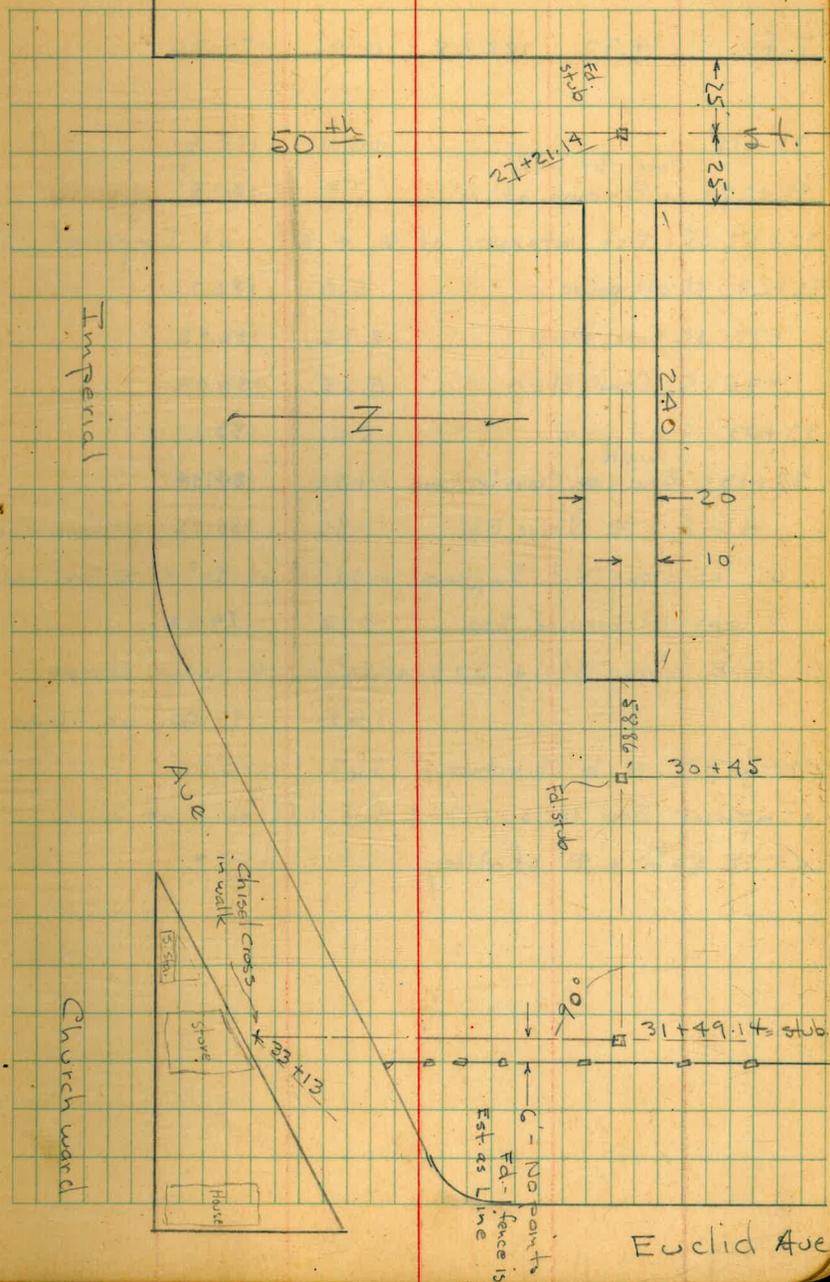
32+00 2.1 177.7

22.3 Lt. = Med. stucco House + 2.60 182.4 Floor
no plumbing

Conc floor of Basement 5.79 174.03

Elev. of Approx floor 3.7 176.1 Floor

of Prop. Bld. - Just found forms in - 10' E of Ang. pt.
= of Bld.



T.P	9.32	188.68	0.46	179.36
32+15			10.4	178.3
Conc. Ret. wall				
32+27 =	on Remains of 6"		7.9	180.8
32+52.05 = Est. intersect of Φ + N.L. of Imperial				
32+68 =	N. oil pave		6.0	182.7
+77 =	N. Conc strip		5.76	182.92
+95 =	S. Conc Strip		5.65	183.03
33+03 =	S. oil pave walk		5.6	183.1
33+13 =	End. on Cross in Conc		4.34	184.34
4.6 S. =	Φ Store Bld.		3.96	185.72 on Conc. floor
61' W. along S.L. Imperial + 22' S. at 90° = Φ Ser. Sta				
Floor of Service Sta			3.76	184.92
70' E along St. + 30' S. at 90° = Φ Large Stucco				
			1.68	187.00 on Floor
Check BM. S. cb. Churchward			3.63	185.05
*Imperial See 1673 - P. 7+7 for diff. elev. of Stub				
at Φ 50 th + Φ of Alley				

8-6-46
7.0.

Loc. and floor elev. of houses in
Area N. of Imperial - Euclid to Escuellast.

H = House - See 1673 - P.I. for sketch

Ozark St.

B.M.						
	5.30	160.16	154.86	1.8+68.10	studs	
6+45	62 Rt. = ± Med. H.	15.20	144.96		Floor	
7+50	66 Rt. = ± Med. H.	2.83	157.33		"	
7+74	49' Lt. = ± Med. H.	4.01	156.15		"	
8+32	80' Lt. = ± Med. H.	1.00	159.00		"	
8+49	66' Rt. = ± Med. H.	1.26	158.90		"	
9+10	85' Rt. = ± Med. H.	0.0	160.16		"	
	136' Rt. - ^{Rear} Small H. in	2.1	158.1		"	
9+95	51' Lt. = ± Large H.	0.64	159.52		"	
10+75	57' Lt. = ± Med. H.	+ 0.70	160.86		"	
T.P.	8.88	165.45	3.59	156.57		
12+95	43 Rt. = ± Med. H.	3.57	161.88		"	

Nogal St.

B.M.						
	7.93	83.30	75.37	E 7' 4 1/4"	± Nogal	
Small H. on S.E. Cor		6.9			= Floor	
47 th ± Nogal						
3+44	95' Rt. = ^{abandoned H.} Small	8.8			"	
4+90	45 Lt. = ± Med. H.	3.20			"	
4+91	40 Rt. = ± Med. H.	+ 0.30			"	
T.P.	12.90	95.45	0.75	82.55		
5+40	39 Rt. = ± Med. H.	10.66			"	
5+70	90 Lt.		81.57		"	
5+80	40 Rt. = ± Med. H.	9.63			"	
6+20	42' Lt. = ± Med. H.	10.30			"	
6+40	42 Rt. = ± Med. H.	6.93				
6+75	55 Lt.		87.83			
7+43	52' Lt. = ± Med. H.	4.08				
7+78	48' Lt. = ± Med. H.	3.24				
Vacant lots on Rt. - Higher						
T.P.	13.17	108.04	0.58	94.57		
	12.30	120.25	0.09	107.95		

120.25

10+20 - 44' Lt = ± Med. H.	6.38			Floor
10+80 - 44' Lt = ± Med. H.	5.42			"
11+35 - 45' Lt = ± Med. H.	3.54			"
12+00 - 75' Rt.	0.4			"
12+02 - 44' Lt = ± Med. H.	2.26			"
12+75 - 45' Lt = ± Med. H.	0.26			"
T.P. 13.22	<u>132.94</u>	0.53	119.72	
13+50 - 75' Lt.	18.8			
75' Rt.	6.4			
14+42 - 31.5' Lt = ± Med. H.	6.60			"
T.P. 12.77	<u>145.56</u>	0.15	132.79	
16+40 - 54' Lt = ± Med. H.	1.36	144.20		"
1				
17+00 - 75' Rt.	6.7	138.9		
T.P. 9.33	<u>154.73</u>	0.16	145.40	
17+30 - 125' Lt = ± Small H.	3.35	151.38		"

154.73

18+10 - 140' Lt = ± Sm. H.	+1.00	155.73		Floor
20+90 - 89' Rt = ± Med. H.	1.58	153.15		"
21+00 - 89' Lt = ± Med. H.	0.40	154.33		"
T.P. 12.31	<u>165.30</u>	1.74	152.99	
21+55 - 155' Rt = ± Med. H.	6.33	158.97		"
23+50 - 75' Rt. = Vac. Lot.	1.8	164.5		
Elect. shop - May have plumb.				
24+40 - 8.6' Rt. = ±	0.45	164.85		"
24+60 - 148' Rt. = ± Med. H.	+4.60	169.90		"
T.P. 10.45	<u>174.57</u>	1.18	164.12	
25+35 - 134' Rt. = ± Med. H.	1.85	172.72		"
25+80 - 89' Rt. Ely. Small H.	4.45	170.12		"
-116' Rt. ± Med. H.	0.85	173.72		"
27+70 - 10' Lt = ± Sm. H.	4.08	170.49		"

From Ozark to 50th and on 50th to Imp.

D.M. 6.28 174.26 167.98 ^{Stub 9+8290} 1673 P 4

6+75-88' Rt. = Φ Med. H. 11.16 163.10 Floor.

6+83-62' Lt. = Φ Med. H. 12.00 162.26 "

6+90-114' Lt. = Φ Sm. H. 11.10 163.16 "

7+46 101' Lt. = Φ Sm. H. 9.30 164.96 "

7+46-61' Lt. = Φ Sm. H. 9.10 165.16 "

7+85 60' Lt. = Φ Med. H. 9.10 165.16 "

8+42 59' Lt. = Φ Med. H. 6.86 167.40 "

8+45 44' Rt. = Φ Med. H. 7.73 166.53 "

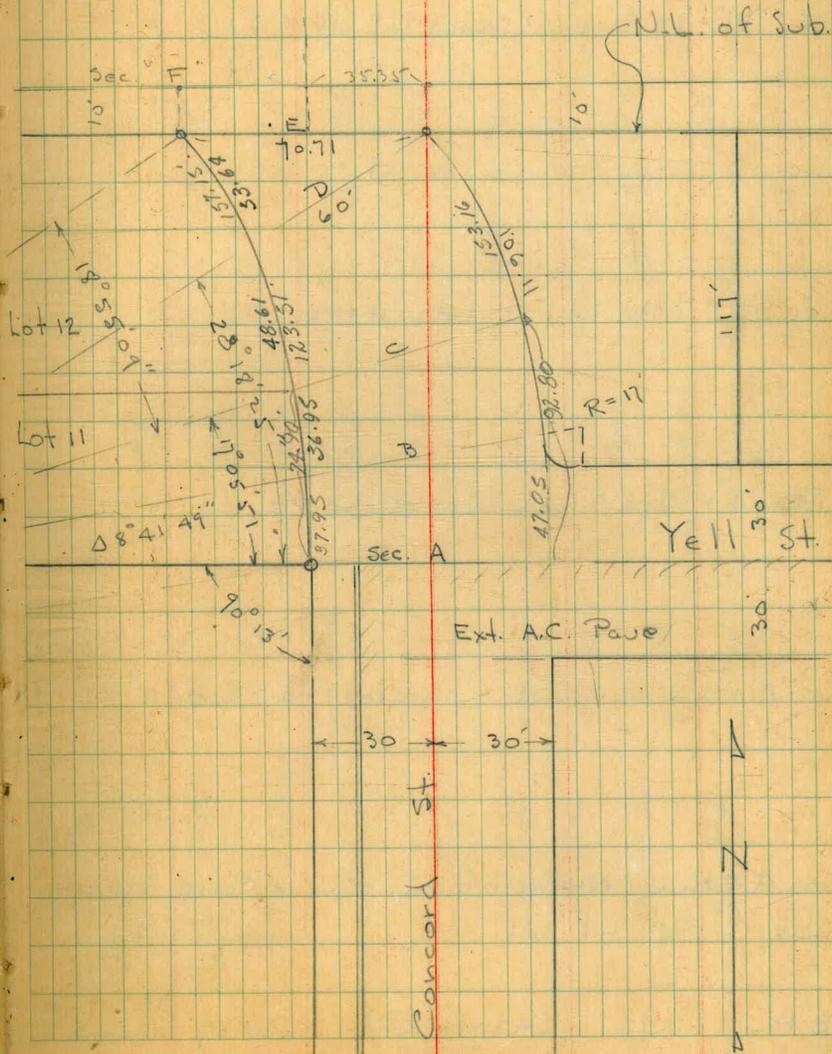
9+25-51' Lt. = Φ Sm. H. 3.13 171.13 "

10+80-41' Lt. = Φ Med. H. +5.20 179.46 "

10+84 28' Rt. = Φ Med. H. +0.90 175.16 "

X-Sect. Concord - from E Yell - N. to
 N.L. of Subdivision Sections taken
 as shown by Letters.

Information shown by Private Eng.
 Profile sheet - No. Number



Sec. "F" - 10' N. at 90° to show rise at end.
+ Paralell to Sub. line

Sec "E" - on Diagonal, along N.L. of Sub.

Sec "D" - opp Prop. Cor. on Rt.

Sec. "C" Thru. Cor of Lots 11+12

Sec. "B" - Opp 17' Rad. Prop. PC. on Rt.

Sec A' = 3' N. of Sec. "A" - Paralell to Sec. "A"

Sec. "A" along N. edge of AC. Pavc + Comb curb + walk. + PC. of W.L.

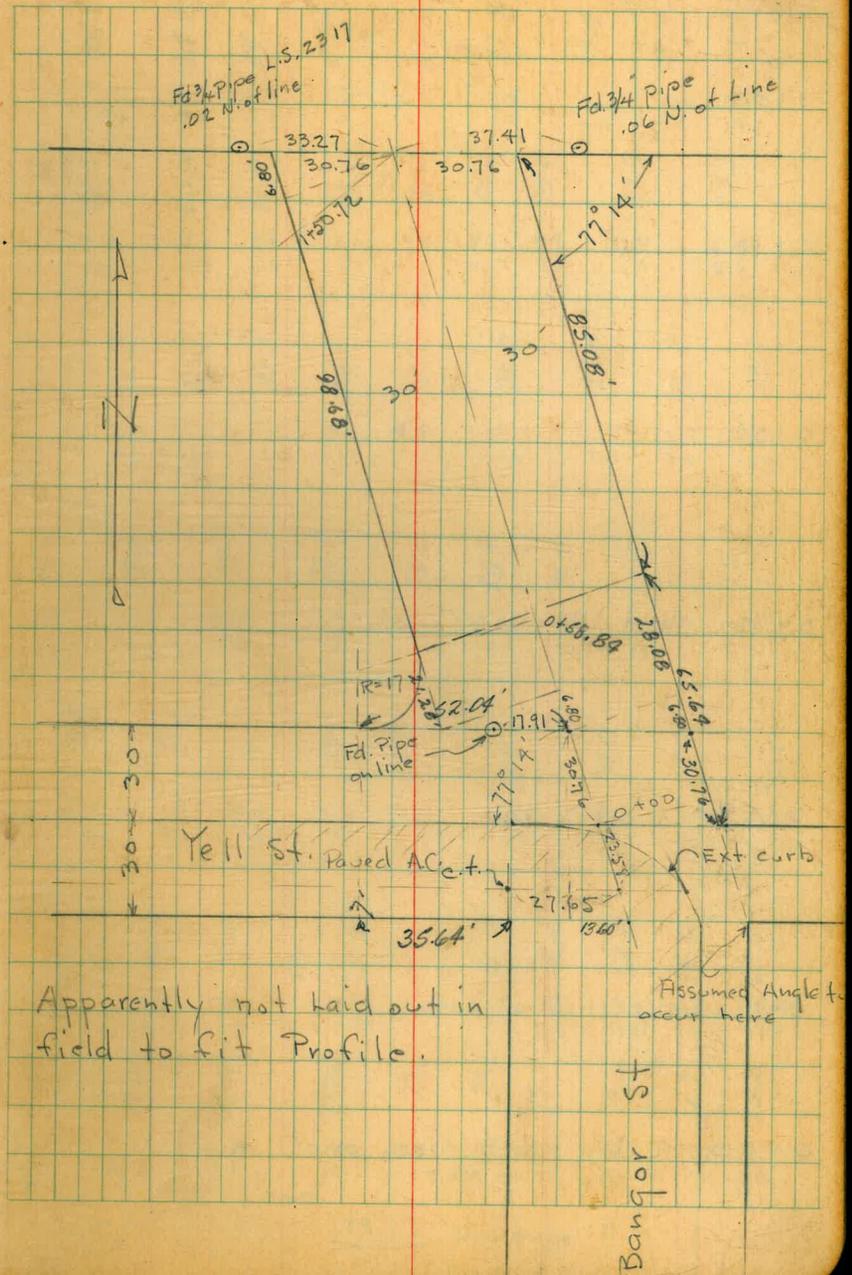
B.M. 7.93 243.20 235.27 SE.B.P. Yell + Concord

36.0	36.8	36.25	36.17	35.68	35.88	35.97	35.78	35.52	35.22	34.71
726	469	362	703	752	787	723	742	719	798	844
50	30	22	17	17	0	0	0	0	30	55
	Wedge		To curb	cut						
	walk		end.							
35.9	34.5	33.5	35.2	34.7	36.2	37.0	38.1	38.3	38.7	39.6
713	517	515	550	520	570	562	571	589	571	576
72	16	15	10	20	20	11	10	19	10	16
										Top of Hill
36.9	34.5	33.5	35.2	35.7	36.2	37.0	38.1	38.3	38.7	39.6
658	517	515	550	520	570	562	571	589	571	576
703	16	15	10	20	20	11	10	19	10	16
										Top of Hill
36.17	36.6	33.5	35.2	35.7	36.2	37.0	38.1	38.3	38.7	39.6
103	658	515	550	520	570	562	571	589	571	576
17	16	15	10	20	20	11	10	19	10	16
										Top of Hill
35.68	37.3	33.5	35.2	35.7	36.2	37.0	38.1	38.3	38.7	39.6
752	658	515	550	520	570	562	571	589	571	576
17	16	15	10	20	20	11	10	19	10	16
										Top of Hill
35.88	37.8	33.5	35.2	35.7	36.2	37.0	38.1	38.3	38.7	39.6
787	658	515	550	520	570	562	571	589	571	576
0	16	15	10	20	20	11	10	19	10	16
										Top of Hill
35.97	37.6	33.5	35.2	35.7	36.2	37.0	38.1	38.3	38.7	39.6
723	658	515	550	520	570	562	571	589	571	576
0	16	15	10	20	20	11	10	19	10	16
										Top of Hill
35.78	38.3	33.5	35.2	35.7	36.2	37.0	38.1	38.3	38.7	39.6
742	658	515	550	520	570	562	571	589	571	576
0	16	15	10	20	20	11	10	19	10	16
										Top of Hill
35.52	39.1	33.5	35.2	35.7	36.2	37.0	38.1	38.3	38.7	39.6
719	658	515	550	520	570	562	571	589	571	576
0	16	15	10	20	20	11	10	19	10	16
										Top of Hill
35.22	39.4	33.5	35.2	35.7	36.2	37.0	38.1	38.3	38.7	39.6
798	658	515	550	520	570	562	571	589	571	576
30	16	15	10	20	20	11	10	19	10	16
										Top of Hill
34.71	40.5	33.5	35.2	35.7	36.2	37.0	38.1	38.3	38.7	39.6
844	658	515	550	520	570	562	571	589	571	576
55	16	15	10	20	20	11	10	19	10	16
										Top of Hill

243.20

X-Sept Bangor St. from ϕ of Yell
N. about 150 to N.L. of Sub.

B.M.	2.18	237.45		235.27	SE. Yell + Concord
	0.44	224.86	13.03	224.42	
	0.51	212.36	13.01	211.85	
	0.16	200.03	12.49	199.87	
	1.43	188.73	12.73	187.30	
	12.78	201.27	0.24	188.49	
	12.88	213.75	0.40	200.87	
	12.85	226.49	0.11	213.64	
	12.89	239.15	0.23	226.26	
Check B.M.			3.89	235.26	



1+00

0+70

0+50

0+32 = about N. edge of wash

0+25 = ± of wash

0+17 = S. edge of Small wash

0+00 = ♀ Yell - Sect. taken on Diag.

86.1	84.3	82.5	81.5	81.1	80.1	80.0	79.9	79.9	78.5	74.9
26 40	44 40	62 40	72 30	76 20	86 10	97 10	107 10	117 20	129 30	156 40
85.2	83.6	81.5	81.1	80.1	78.9	78.0	77.0	75.8	73.1	
35 30	51 30	72 30	76 20	86 10	97 10	107 10	117 20	129 30	156 40	
84.4	82.9	81.1	80.1	78.9	78.0	77.0	75.8	73.1		
43 20	58 20	76 20	86 10	97 10	107 10	117 20	129 30	156 40		
83.4	82.1	80.1	78.9	78.0	77.0	75.8	73.1			
53 10	66 10	86 10	97 10	107 10	117 20	129 30	156 40			
82.2	81.0	80.1	78.9	78.0	77.0	75.8	73.1			
65 10	77 10	86 10	97 10	107 10	117 20	129 30	156 40			
81.2	80.1	79.0	77.9	77.0	75.8	73.1				
55 05	86 10	97 10	107 10	117 20	129 30	156 40				
79.9	79.9	77.9	77.0	75.8	73.1					
88 20	102 30	140 50								
81.2	80.1	79.0	77.9	77.0	75.8	73.1				
55 05	86 10	97 10	107 10	117 20	129 30	156 40				
82.2	81.0	80.1	78.9	78.0	77.0	75.8	73.1			
65 10	77 10	86 10	97 10	107 10	117 20	129 30	156 40			
80.0	77.8	77.3	76.8	76.5	75.4	74.4	73.7	72.0		
87 40	109 30	114 20	119 10	122	133 10	143 20	150 30	167 40		
78.9	77.0	76.5	76.5	75.3	74.7	74.0	72.1	70.5		
9.8 40	11.7 30	12.2 20	13.2 10	13.4	14.0 10	14.7 20	16 30	18.2 50		
80.8	78.5	78.7	77.9	76.3	75.6	74.4	74.8	74.0	69.7	
84 40	102 30	100 20	108 10	124	131 10	143 20	139 30	147 40	170 50	
81.4	79.0	78.0	77.9	77.6	77.1	75.7	74.9	74.7	62.0	
7.28 50	9.72 30	10.63 20	10.80 10	11.1	11.6 10	13.0 20	13.8 30	14.0 38	26.7 60	
on edge Pavc	Wk on edge Pavc	Wend of Curb.	oncb.	1.4 N. of cb. face						
				189.73	See page 11					

6.15 #
 5.15 177.30
 5.85 176.60
 5.58 176.87
 5.62 176.83
 5.36 177.09

4.5 ✓ 182.45

177.93

See P. 11 for check to starting B.M.

Elev. on N. end of cb. inlet to show check on levels

1+70 - Taken normal to # to show ground ^{away} falling

1+50.72 = N.L. of Sub. - Sect. taken along line of Sub.

1+25

Gutter -
 curb at B.c. Return 18
 on catch basin -
 back of walk 15' - 2nd - on # Bangor
 5 - curb line 1st on # Bangor
 next to Curb on # Bangor -
 on Curb 10' W of # @ 0+00 See page 12 -

177.56
 177.42
 Profile

11.17

80.2	78.3	77.6	76.7	75.9	75.2	74.0	72.9	69.7
8.5 50	10.4 30	11.1 20	12.0 10	12.8	13.5 10	14.7 20	15.8 30	19.0 50
81.6	80.5	79.9	79.3	78.7	77.8	77.2	76.3	74.7
7.1 50	8.2 30.76	8.8 20	9.4 10	10.0	10.9 10	11.5 20	12.4 30.76	14.0 50
85.3	84.2	83.1	82.2	81.3	80.3	78.8	77.5	75.0
8.4 40	9.1 30.25	9.6 20	10.5 10	11.4	12.4 10	13.9 20	15.2 30	19.7 50

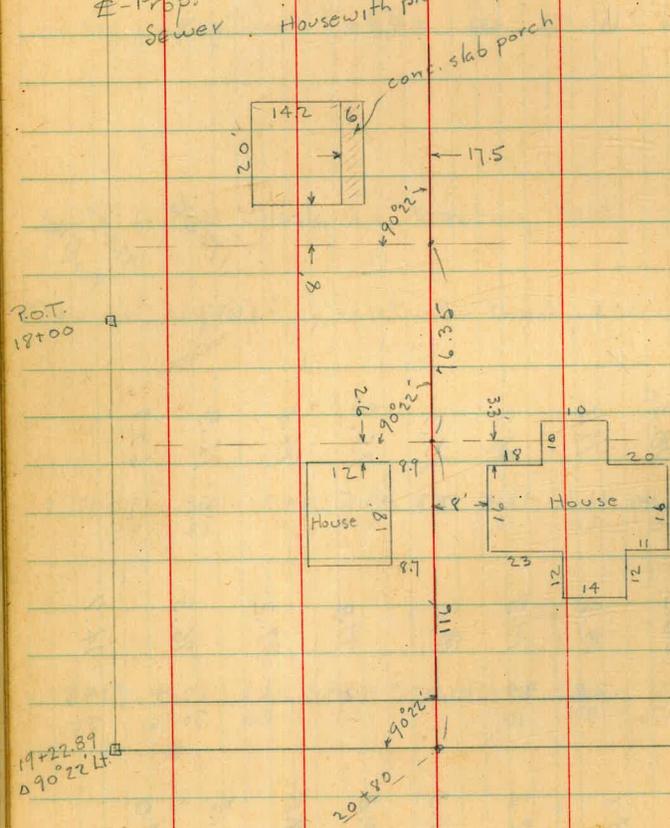
182.93

Prop. Sewer Loc. lot 42 - Hortons Pcr.
 Ozark to 50th - 1673 - P. 1.
 Loc. of Houses for District

8-22-46

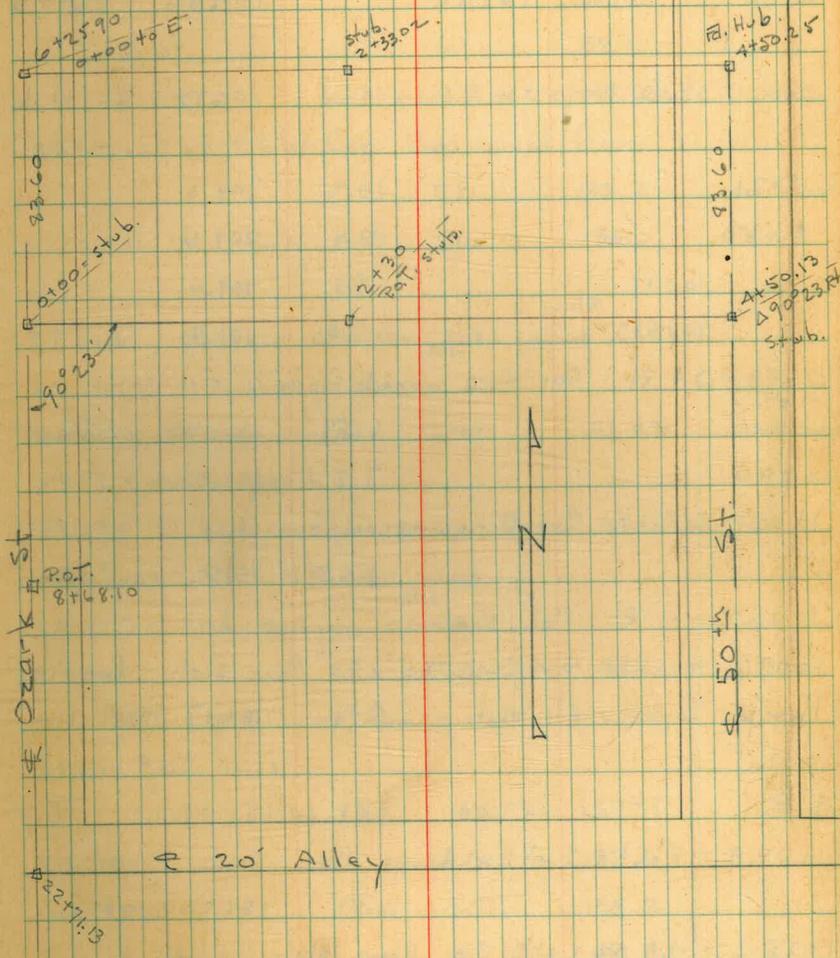
F.O.

E-Prop. Sewer House with plumbing
 conf. slab porch



Indexed
 C.S.K.

14



Levels on Prop. New location.

D.M.	3.92	158.78	154.86	stub. 8+68.10 1673- P3
0+00	stub. = 7+09.50 on E Ozark 1204		146.74	on stub.
0+21		10.3	148.5	
0+50		9.2	149.6	
	10 - Lt.		9.8	149.0
	10 - Rt.		7.4	151.4
0+89	3.4 Rt = Cor. shed. ^{NW.} - wood floor		6.59	152.19 on floor
1+00		7.5	151.3	
1+05	6.8 Lt = Cor. Conc apron to shed.		7.60	151.2 on apron
1+05.2	4' Rt = Cor. shed ^{NE.}			
1+09.7	4.1 Rt = NW. Cor. 15.5' x 7.8' Conc slab - for Gas Pump - Tanks under slab.		5.91	153.87 Top slab
T.P.	7.97	159.04	7.71	151.07
1+09.9	8' Lt = S.W. Cor. Large shed - Conc. floor		6.82	152.22 on floor.
1+25.2	4.6 Rt = N.E. Cor. Conc. slab.		6.17	152.87 on slab
1+30.4	8.4 Lt = S.E. Cor. shed.			

1+50		5.6	153.4	
	15' Lt.		6.9	152.1
	15 Rt.		4.5	144.5
1+52	10.9 Lt = S.W. Cor. shed - wood floor		5.8	153.2 on floor
1+70	11.1 Lt. S.E. Cor. shed		5.0	154.0 on E
1+77.5	W. side chicken shed ^{5' wide} good. Const.			
2.2 Lt. of E	= N. edge porch			
0.5 Rt. = N. edge shed.	2.61	156.43		^{Porch} floor shed
1+84.6	= end of porch			
1+86.9	= W. side pigeon coop. from shed N. 9.3'			
1+99.7	2.2 Rt. = N.E. Cor. shed.			
2+01.3	= end pigeon coop			
2+05		3.4	155.6	
2+25.7	= Cross wire fence - 3.1 Lt. = Cor.			
2+30	= P.O.T. stub.			
T.P.	3.86	161.85	1.05	157.99 on stub
2+50		4.3	157.6	
	15' Rt.		3.7	158.2
	15 Lt.		4.7	157.2
2+98.5	= Cross wire fence - 2.7 Lt. = E+W. fence			
3+00		3.7	158.2	
3+50		4.1	157.8	

161.85

4+00

5.5

156.4

4+25.1 = Cross Wire fence - 216 Lt. - E. + W. fence

4+30

6.6

155.3

4+50.13 = Ang. 90° 23' Rt. 8.33 153.52 on stub.

= 5+33.85 on E 50th

check on Hub - 4+50.25

11.98

149.87

149.84

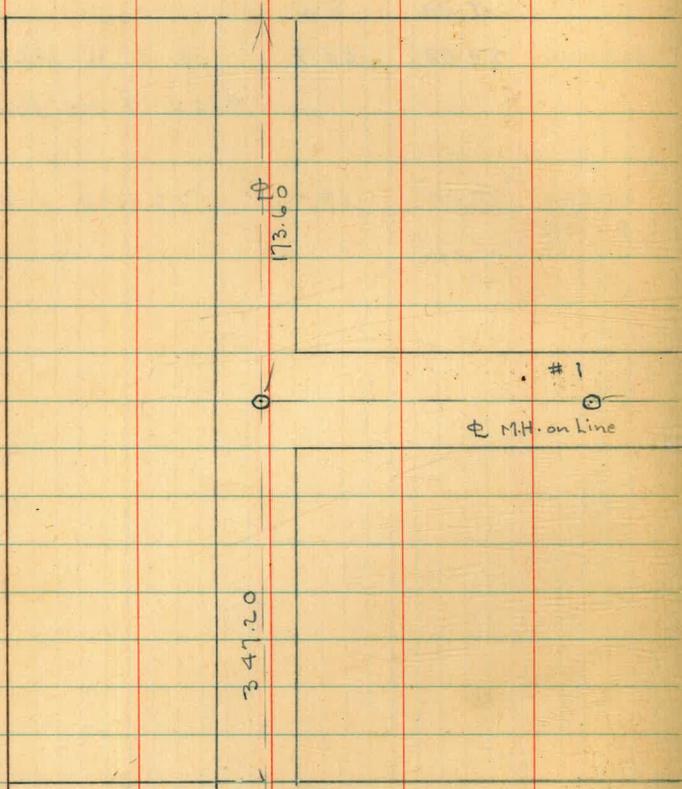
1673-P3

Location of M.H.'s in Alley W. of Draper

± E. of Draper - N. of Nautilus St.

See B 1650 for line on Draper

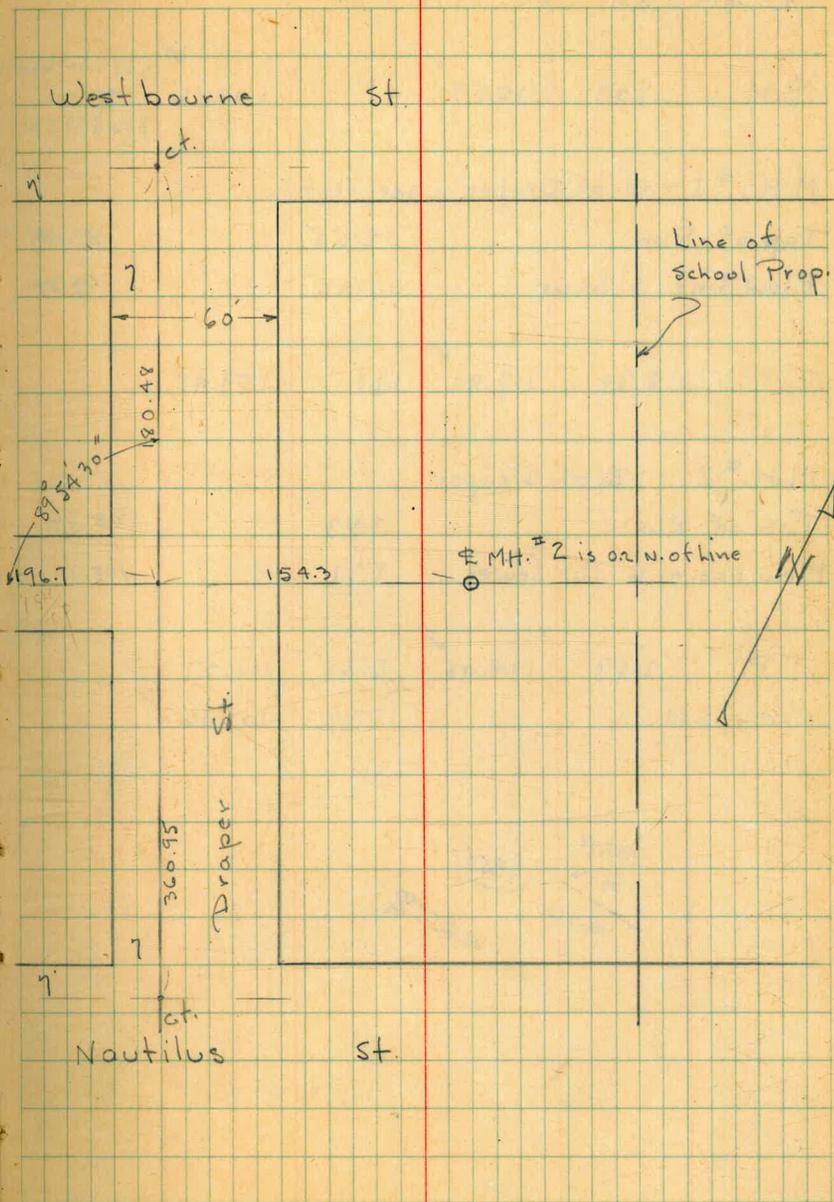
10-21-46
Osborne
Hardin
Worrell
D. Smith



568
W.O. 210

Indexed
C.S.K.

17



Levels on Ext. M.H.'s

B.M.	7.43	110.59 ✓	103.16 ✓	sw. westbound + Draper B1650-56
------	------	----------	----------	---------------------------------------

M.H. # 1 - W. of Draper - see sketch.

Top of Rim		12.55		98.02
Flow line 6" Sewer		17.92		92.77

T.P.	8.34	117.82 ✓	1.11	109.48
------	------	----------	------	--------

M.H. # 2 - E. of Draper

Top of Rim		3.83		113.99
Flow line of 6" U.I. Sewer		8.71		109.11

T.P.	2.87	114.08 ✓	6.61	111.21
check B.M.		10.92	103.16 ✓	

$$\begin{array}{r} 109.11 \\ 92.77 \\ \hline 16.34 \end{array}$$

$$\begin{array}{r} 351 \\ 4.655 \end{array}$$

Wulker
Becker
Greer
11-4-46
Preliminary Levels for
Proposed Sewer on S. 68th St.
from Amherst
to Canyon South of Amherst

Notes: 40' N of St. Amherst = 0+00

0+00	1.57	458.92	8.0	451.0
0+40			8.1	450.9
1+00			10.1	448.9
+50			12.0	447.0
2+00			13.2	445.8
+50			13.6	445.4
3+00			13.6	445.4
+50			13.9	446.1
4+00			11.8	447.7
TP	13.04	460.70	11.31	447.66
4+50			10.6	450.1
5+00			8.5	452.2
+69	Fd Pipe	20' Rt.	6.0	454.7
6+00			5.2	455.5
+50			4.7	456.0
7+00			4.0	456.7
+50			3.1	457.6
8+00			2.6	458.1
+50			1.5	459.2
9+00			0.3	460.4
TP	1.66	462.07	0.29	460.41
9+50			1.5	460.6

462.07

10+00			1.9	460.2
+50			3.1	459.0
11+00			4.4	457.7
+50			5.9	456.2
12+00			7.2	454.9
+50			7.9	454.2
13+00			8.4	453.7
+50			8.8	453.3
14+00			9.5	452.6
+50			10.1	452.0
15+00			10.7	451.4
TP	4.73	456.09	10.71	451.36
(14+45)	Lt on Top Tr. Hqd.	2.93		454.06
15+50			5.6	450.5
+75	Per E. West St.		6.0	450.1
16+00			6.8	449.3
+50			8.2	447.9
17+00			8.6	447.5
+50			7.6	448.5
18+00			6.5	449.6
+50			5.7	450.4
19+00			5.3	450.8
+50			5.1	451.0
20+00			5.7	450.9
+50			5.5	450.6

Cont. P-20

456.09

21+00		6.0	450.1	
+50		6.1	450.0	
22+00		6.0	450.1	
+50		5.6	450.5	
23+00		5.2	450.9	
+50		5.1	451.0	
24+00		4.8	451.3	
T.P.	1.99	453.11	4.27	451.12
24+50		2.0	451.1	
25+00		2.7	450.4	
+50		3.6	449.5	
26+00		4.9	448.2	
+50		6.7	446.4	
27+00		10.6	442.5	
T.P.	0.88	440.17	13.02	440.09
27+50		2.7	437.5	
28+00		3.1	432.1	
+50		12.1	428.1	
T.P.	0.28	428.02	12.43	427.74
+78		1.4	426.6	
+80		1.2	426.8	
+90		5.6	422.4	
29+00		7.5	420.5	
T.P.	0.55	416.12	12.45	415.57
29+50		1.8	415.3	
30+00		7.0	409.1	

two Nails
in Pole
SW. Cor. St.

416.12

20

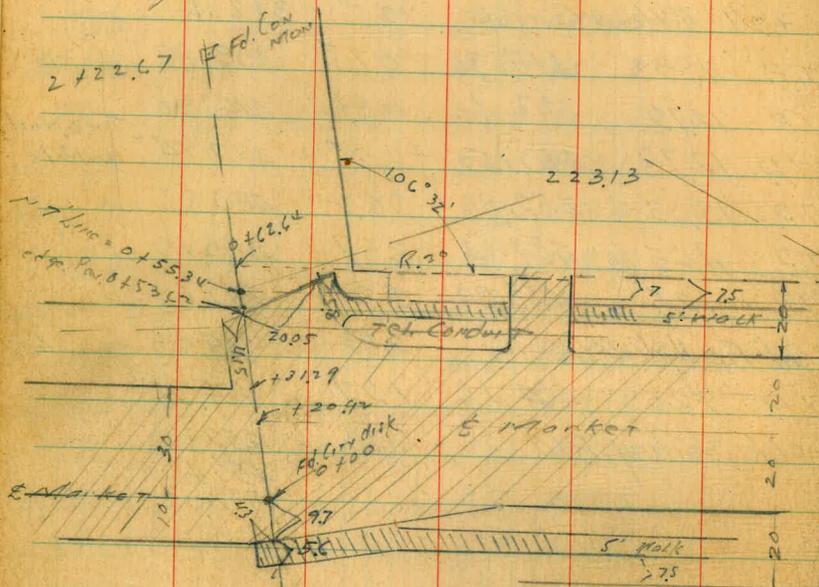
30+50		11.9	404.2	
T.P.	0.75	404.63	12.24	403.88
31+00		4.6	400.0	
+50		8.2	396.4	
32+00		10.4	394.2	
+21=Bottom Canyon		12.5	392.1	
T.P.	11.85	415.71	0.75	403.88
T.P.	12.79	427.69	0.81	414.90
T.P.	12.78	440.52	+0.05	427.74
T.P.	13.03	452.86	0.62	439.83
T.P.	4.65	454.84	2.67	450.19
T.P.	7.25	456.88	5.21	449.63
chk Fire Hyd 14+45		2.85	454.03	-0.34 corr
T.P.	9.25	464.16	1.97	454.91
chk starting B.M.		6.78	457.38	
			457.40	
			0.02	

Two Nails
in Pole

xsec of Boundary St.
Market to Hilltop

C. Moore
C.S.
W.M.
E.B.
12-13-46

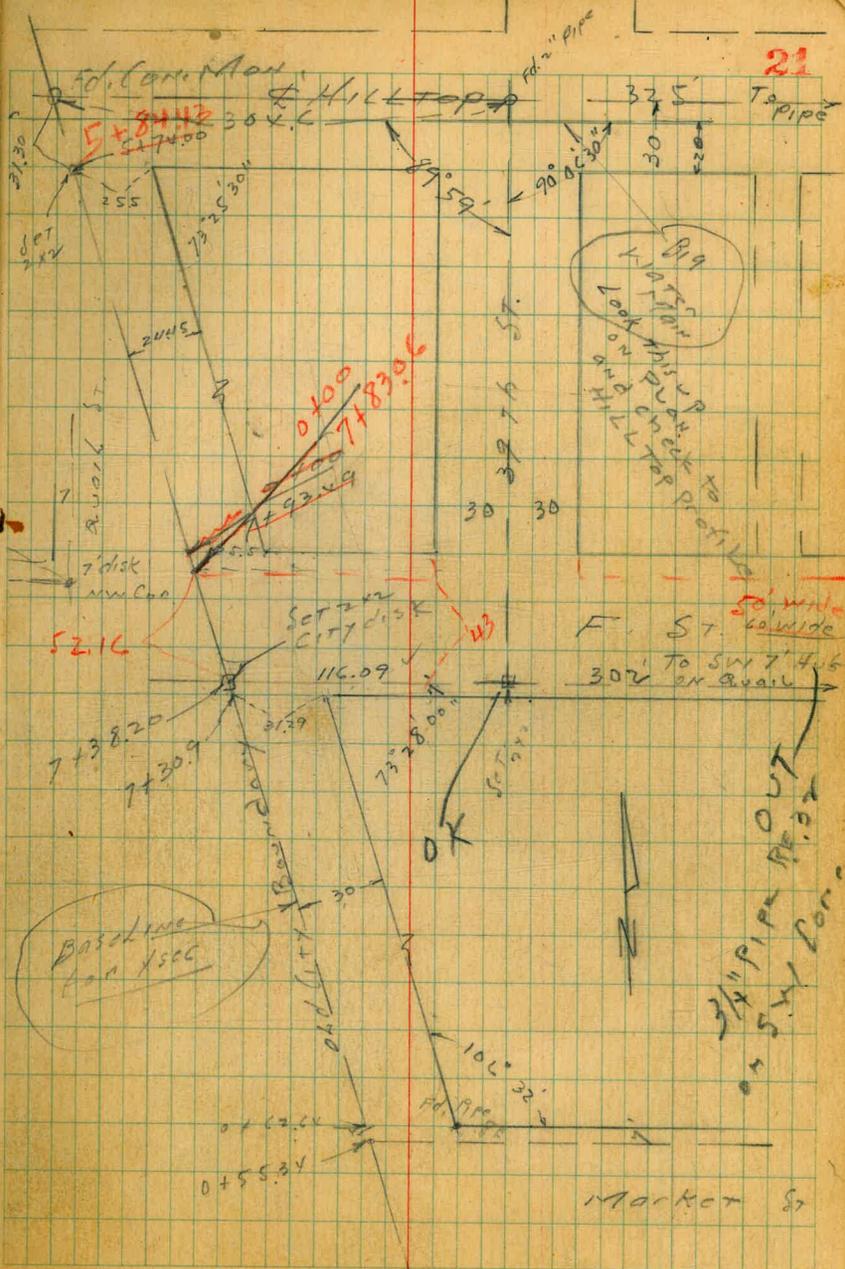
W.D. # 230



12-10-47 CSW
checked this work
and fd 1 was in
error of 10 in
width of FST

574
10.43
584.43

Big pipe
Main



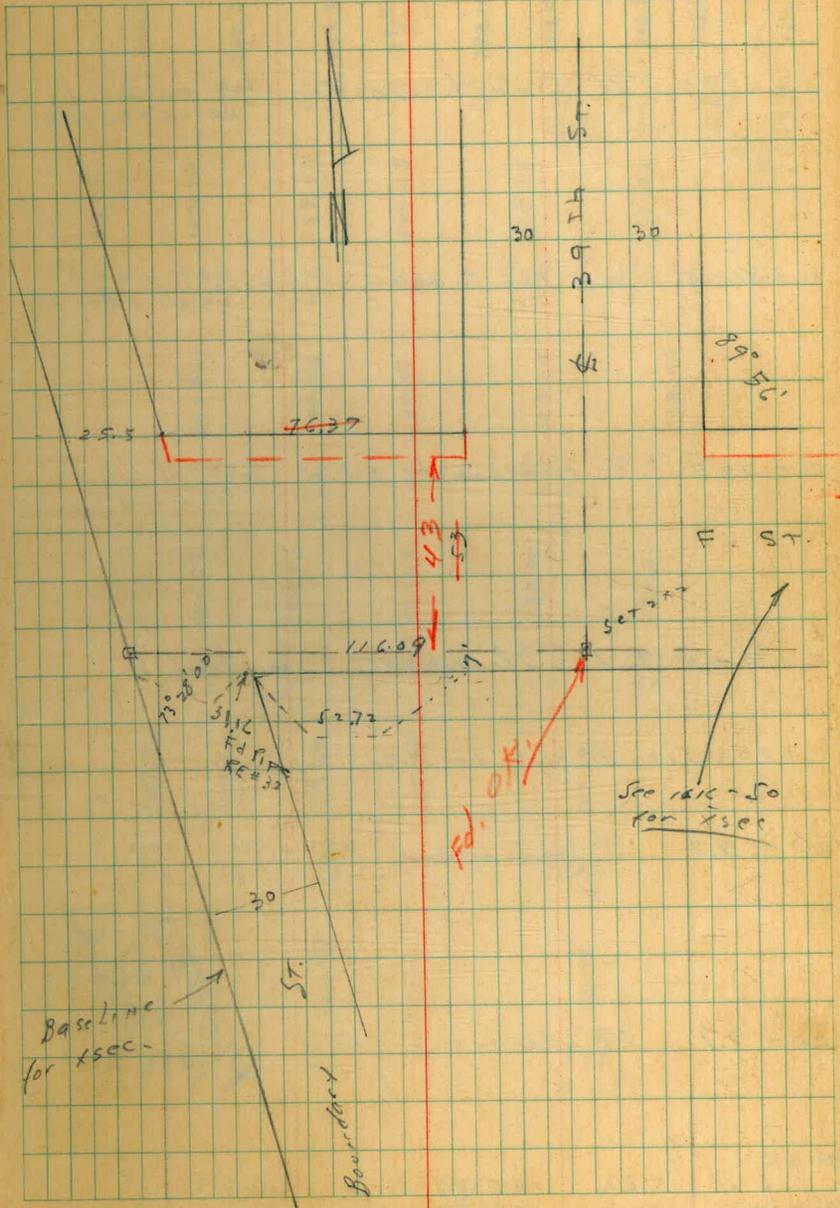
99
Water Main
Load check to
and Hilltop profiles

F. St. 50' wide
40' wide
To SW 7' 4.6
30' or avail

Baseline
for xsec

3/4" PIPE OUT
on 5" CON.

Market St



0 + 41.73 = 66 Line to East Sec parallel
with Market

0 + 31.29 = N L Pav. to West Parallel
with Market

0 + 29.92 E Market to East Sec. parallel
with Market

0 + 10.43 E Pav to West Sec. parallel
with Market

0 + 00 = City disk See sketch

00 - 9.7 S gutter on Market

00 - 9.7 = Seb Market to East

PROTECTED
12-12-47
J. M. [unclear]

B.M.G.P.
in Seb of
Market on
old City
Boundary
5.87 145.79 139.92

Lt = 70 West

	141.29	140.29	139.31	138.21	138.10	137.04	136.52	135.78	135.17
	4.5	5.5	6.8	5.8	7.69	8.75	9.7	12.9	12.67
	60	30	42	18	39	29	29	66	907
						66% approx	907		
	141.46	140.46	139.54	139.43	137.28	137.28	134.53		
	4.32	5.13	6.25	6.0	8.51	11.26			
	60	30	43	20	30	60			
		141.84	140.73	139.56	137.28	134.45			
		3.95	5.06	6.33	8.51	11.34			
		60	30	30	30	60			
		141.79	140.83	139.68	137.00	134.11			
		5.80	4.96	6.11	8.29	11.68			
		60	30	60	60	60			
	141.33	140.41	139.29	139.09	133.34				
	4.66	5.28	6.50	6.70	12.45				
	60	37.5	42		58.5				
			140.05	139.69	133.79				
			5.74	6.10	11.80				
			42		58.5				
					4.66				

145.79

0 + 00

0 + 75

0 + 65 Sec. ^S now at 90°

0 + 62.54 NE Marker to East Sec. parallel ^{with} Marker

T.P. ^{BM} 2.86 142.78 5.87 139.92

0 + 53.62 N edge Pav. Sec. to NE Cor. approx 90°

0 + 52.32 = NE Marker to West ^{same as} 0 + 46

0 + 46 Sec. parallel w. 75° Marker

145.79

142.8	141.8	140.9	139.2	139.0	137.0	137.5	133.5	131.8
<u>0.0</u>	<u>1.9</u>	<u>1.9</u>	<u>2.4</u>	<u>0.8</u>	<u>1.8</u>	<u>1.5</u>	<u>9.3</u>	<u>11.9</u>
40	30	20	20	2	5	30	37	50
143.8	142.5	141.3	139.4	138.2	137.8	137.7	134.6	133.3
+ 1.0	1.5	1.5	2.4	1.6	1.0	1.1	8.4	9.5
<u>40</u>	<u>30</u>	<u>20</u>	<u>20</u>	<u>2</u>	<u>30</u>	<u>30</u>	<u>37</u>	<u>50</u>
144.5	143.1	142.3	138.6	138.4	136.3	133.7	134.6	133.3
+ 1.7	0.5	0.5	4.2	1.4	6.5	4.1	8.4	9.5
<u>40</u>	<u>30</u>	<u>20</u>	<u>20</u>	<u>2</u>	<u>30</u>	<u>30</u>	<u>37</u>	<u>50</u>
144.5	143.1	141.8	138.6	138.4	138.2	136.4	134.6	133.3
+ 1.7	1.0	1.0	4.2	1.4	4.6	6.4	8.4	9.5
<u>40</u>	<u>30</u>	<u>20</u>	<u>20</u>	<u>2</u>	<u>31.3</u>	<u>30</u>	<u>37</u>	<u>50</u>
143.89	140.89	139.39	139.19	139.08	138.50	137.53	137.84	138.29
7.9	4.9	6.4	6.60	6.71	7.29	8.26	7.95	7.5
<u>40</u>	<u>18</u>	<u>9</u>	<u>4.2</u> Pav.	<u>2</u>	<u>12.5</u>	<u>25</u> 97	<u>25</u> 66	<u>30</u>

145.79

2 + 50

2 + 22.47 Cor

2 + 00

1 + 70

1 + 35

1 + 13

142.78

27

Base Line

RT

25

50	142.6	2.0	140.5	5.0	137.8	6.1	136.7	8.7	136.6	5.7	132.6
30	141.5	4.0	139.3	5.0	137.2	8.0	136.1	8.0	136.0	8.0	137.1
20	140.4	2.0	138.2	6.0	136.7	2.0	135.5	2.0	135.4	2.0	134.6
47	138.6	7.2	135.6	7.0	135.8	9.0	133.8	9.89	133.89	7.0	135.2
27	137.1	8.0	134.8	7.5	135.4	9.0	133.6	9.0	133.8	2.8	134.6
4	135.9	7.9	134.9	8.8	134.0	9.2	133.3	9.0	133.8	8.0	133.9
23	136.1	9.1	133.7	8.9	133.9	9.5	131.5	2.0	132.7	8.0	132.6
28	133.9	9.5	133.3	10.0	132.5	11.0	129.5	10.1	132.7	5.0	130.4
30	133.8	10.9	131.9	12.7	130.1	13.3	129.5	12.8	130.4	5.0	129.4
50	131.3	11.5	131.9	5.0	130.1	13.3	129.5	12.8	130.4	5.0	129.4

142.78

5 + 00

4 + 50

4 + 00

3 + 50

T.P. 12.39 152.61 2.56 140.22

3 + 00

2 + 70

142.78

L

50.1	147.5	147.5	150.5	149.9	148.6	148.0	147.2	147.3	146.8	146.1	144.4
<u>50</u>	<u>20</u>	<u>20</u>	<u>10</u>	<u>20</u>	<u>20</u>	<u>10</u>	<u>20</u>	<u>20</u>	<u>13</u>	<u>20</u>	<u>50</u>
147.5	147.1	146.8	146.3	145.6	145.6	145.6	145.2	145.4	144.2	143.2	
<u>50</u>	<u>20</u>	<u>20</u>	<u>10</u>	<u>20</u>	<u>20</u>	<u>10</u>	<u>20</u>	<u>20</u>	<u>13</u>	<u>15</u>	<u>30</u>
146.2	145.8	145.0	143.6	143.8	143.3	144.1	142.9	142.0	140.7	140.4	
<u>20</u>	<u>30</u>	<u>12</u>	<u>20</u>	<u>20</u>	<u>15</u>	<u>17</u>	<u>30</u>	<u>41</u>	<u>42</u>	<u>50</u>	<u>12.5</u>
143.3	142.8	141.8	140.4	140.7	140.4	141.1	140.0	139.1	138.7	138.5	138.4
<u>50</u>	<u>30</u>	<u>20</u>	<u>10</u>	<u>20</u>	<u>20</u>	<u>18</u>	<u>20</u>	<u>35</u>	<u>50</u>	<u>20</u>	<u>50</u>
140.8	140.4	140.0	139.2	137.4	152.61	137.1	137.8	136.7	136.5	135.4	
<u>20</u>	<u>20</u>	<u>20</u>	<u>10</u>	<u>20</u>	<u>20</u>	<u>19</u>	<u>20</u>	<u>25</u>	<u>30</u>	<u>50</u>	<u>20</u>
139.1	138.5	138.0	136.4	136.4	135.7	135.3	134.1				
<u>50</u>	<u>20</u>	<u>20</u>	<u>20</u>	<u>20</u>	<u>19</u>	<u>20</u>	<u>25</u>	<u>50</u>			
142.78											

142.78

7 + 52

$$\begin{array}{r} 7 + 30.9 \\ \underline{26.08} \\ 7 + 56.98 \end{array}$$

7 + 30.9 = SL F ST and ^{Sec.} parallel with F

7 + 00 Last Sec. at 90°

6 + 50

6 + 00

T.P. 11.33 161.50 2.44 150.17

5 + 50

152.61

152.0	152.0	153.7	155.4	156.2	157.8	159.2	161.50	148.4	148.8	148.9	147.6	147.7
0.6	1.8	3.1	4.9	7.7	9.0	11.0	148.8	4.2	8.8	10.9	145.7	13.9
20	20	20	20	20	20	20	20	20	20	20	20	20
150.8	149.5	148.7	148.4	152.4	153.9	154.9	157.0	151.0	151.5	151.4	150.4	149.9
1.8	3.1	4.9	7.7	9.0	11.0	12.6	154.9	10.5	10.0	10.1	10.4	12.9
20	20	20	20	20	20	20	20	15	16	5	30	50
153.7	152.4	151.2	152.8	153.9	154.9	156.2	155.5	152.2	152.7	152.7	150.6	149.2
7.8	9.1	10.3	11.5	12.6	13.8	14.7	155.5	9.3	8.8	9.8	10.9	11.7
40	20	8	2	7	3	2	7	17	18	30	50	10
152.0	148.8	148.7	148.4	152.4	153.9	154.9	157.0	151.0	151.5	151.4	150.4	149.9
0.6	1.8	3.1	4.9	7.7	9.0	11.0	148.8	10.5	10.0	10.1	10.4	12.9
20	20	20	20	20	20	20	20	15	16	5	30	50
153.7	152.4	151.2	152.8	153.9	154.9	156.2	155.5	152.2	152.7	152.7	150.6	149.2
7.8	9.1	10.3	11.5	12.6	13.8	14.7	155.5	9.3	8.8	9.8	10.9	11.7
40	20	8	2	7	3	2	7	17	18	30	50	10
152.0	148.8	148.7	148.4	152.4	153.9	154.9	157.0	151.0	151.5	151.4	150.4	149.9
0.6	1.8	3.1	4.9	7.7	9.0	11.0	148.8	10.5	10.0	10.1	10.4	12.9
20	20	20	20	20	20	20	20	15	16	5	30	50

9+83.49
2+0.43
~~1+90~~

23.2 Rt 4.9 Con walk

9+43.49
1+60.43
~~1+50~~

PLEASE CONTACT
STA OK-FIXED

9+41.49
1+58.43
~~1+48~~

24' Rt P.P. & 25' Rt Beg. wire fence

9+18.49
1+35.43
~~1+25~~

T.P. 12.97 176.35 8.98 163.38

8+93.49
1+10.43
~~1+00~~

8+68.49
0+85.43
~~0+75~~

8+43.49
0+60.43
~~0+50~~

172.36

LT

BL

R

29

172.4	171.1	169.8	167.4	166.2	164.7	165.3	165.31	165.33
3.9 40	3.0 30	6.5 20	9.0 4	10.1	11.4 7	11.0 20	11.04 23.2 4.9 walk	11.02 24.5 walk
173.1	171.6	170.2	167.1	164.8	163.1	163.4	164.0	163.9
3.7 40	3.0 30	6.1 20	9.2 3	11.5	13.2 2	12.9 19	12.3 20	12.4 24.5
173.5	171.6	169.8	166.5	163.2	162.2	162.1	163.0	163.0
2.8 40	3.0 30	6.5 20	9.8 4	13.1	14.1 3	14.2 21	13.3 22	13.3 24.5
171.3	170.1	168.9	166.4	163.6	161.35	161.2	162.5	163.0
1.1 40	3.0 30	3.9 20	6.0 4	8.8 163.6	11.4 3	11.7 22	9.9 23	10.4 24.5
170.0	168.7	167.4	164.9	162.4	159.8	160.0	161.1	161.0
5.4 40	3.0 30	5.0 20	7.5 3	10.0	12.0 3	12.4 22	11.3 23	11.3 24.5
168.4	166.9	165.5	164.1	161.1	158.4	158.2	159.2	160.2
4.0 40	3.0 30	6.9 20	8.3 5	11.3	14.0 3	14.2 22	13.2 24.5	12.2 30
167.4	166.1	164.1	161.1	158.4	158.2	159.2	160.2	160.1
4.0 40	3.0 30	6.9 20	8.3 5	11.3	14.0 3	14.2 22	13.2 24.5	12.2 30

172.36

11 + 63.49
~~3 + 80.43~~
~~3 + 70~~

48.7 Rt Con. drive 8' wide

11 + 43.49
~~3 + 60.43~~
~~3 + 50~~

T.P. 7.24 179.76 3.83 172.52

10 + 93.49
~~3 + 10.43~~
~~3 + 00~~

10 + 53.49
~~2 + 70.43~~
~~2 + 60~~

10 + 13.49
~~2 + 30.43~~
~~2 + 20~~

10 + 06.49
~~2 + 23.43~~
~~2 + 13~~

24.5 Rt end wire fence

176.35

Lt

Bl.

Rt

30

175.1	175.2	175.4	174.7	173.1	171.5	171.8	172.6	172.7
4.7	4.4	4.5	4.7	8.3	8.0	7.2	7.1	
40	30	20	30	19	24.5	35		
175.5	175.0	174.5	173.6	179.76	169.4	169.3	170.7	170.5
0.8	1.8	2.7	5.0	6.9	7.0	5.4	5.8	
40	30	20	30	19	24.5	35		
	172.4	171.7	171.1	168.6	167.5	167.8	168.5	168.6
	3.9	5.7	7.7	8.8	8.5	7.8	7.7	8.3
	40	30	20	2	19	21	24.5	35
171.9	170.8	169.7	169.0	167.2	167.1	164.9	166.5	167.0
4.4	6.5	7.3	9.1	9.7	10.4	9.8	9.3	9.4
40	30	20	15	9	2	18	19	24.5
								10.5
								33
								garage
								dirt

176.35

12+93.49
~~5+10.43~~
~~5/00~~

12+57.49
~~5+04.43~~
~~4+94~~

END 6" CON. WALL

12+65.49
~~4+82.43~~
~~4+72~~

3.4 wide CON STEPS THRU WALL

12+43.49
~~4+60.43~~
~~4+50~~

12+33.49
~~4+50.43~~
~~4+40~~

24.8 FT BEG. 6" CON. WALL

11+93.49
~~4+10.43~~
~~4/00~~

179.76

Lt

BL

Rt

31

173.5	174.4	175.3	175.7	174.0	174.2	174.7	176.0
6.3		4.5	4.1	5.8	5.6	5.1	5.8
40	30	20	30	21	24.5	24.5	35

IN DIRT DRIVE

176.81
~~2.95~~
~~278~~
 TOP WALL

174.60
~~5.16~~
~~27.2~~
 TOP OF BOX STEP

172.4	173.7	174.8	176.0	173.6	174.0	174.1	176.21
7.4		5.7	3.8	6.2	5.8	5.7	3.55
40	30	22	2	24.5	27	27	27

TOP WALL

176.12
~~3.24~~
~~22.8~~
 TOP WALL

174.0	174.3	174.6	174.4	173.4	172.9	173.2	173.9	174.8
5.8		5.7	5.4	6.4	6.9	4.6	5.9	5.0
40	30	20	2	23	24.5	24.5	35	35

179.76

13 + 62.49
~~5 + 79.43~~
~~5 + 69~~

end Coggle wall

13 + 37.49
~~5 + 54.43~~
~~5 + 44~~

2.5 wide Con steps

13 + 22.49
~~5 + 39.43~~
~~5 + 29~~

Beq. Cen. Coggle wall with
Batten

13 + 17.49
~~5 + 34.43~~
~~5 + 24~~

E. Singan dirt floor

13 + 10.49
~~5 + 27.43~~
~~5 + 17~~

28.3 Rt End Con wall

12 + 97.49
~~5 + 114.43~~
~~5 + 104~~

28.1 Rt Beq. 4" Con wall

179.76

Lt

Bl.

Rt

32

175.0	175.9	176.1	175.3	175.6	175.1	174.4	174.6	175.9	177.07
4.8	3.7	4.5	4.7	4.7	5.4	5.2	5.2	2.9	2.69
40	28	15	2	2	2	2	22	28.6	29.7
								ground	Top wall
								174.6	175.31
								175.0	
								4.8	4.5
								24.5	26
									Top Bot. STEP
								175.5	
								4.3	2.70
								26	27.8
								Bot. ground	Top
								176.9	
								2.9	
								56	
								177.16	
								2.60	
								28.3	
									Top wall
								176.96	
								2.80	
								28.1	
									Top wall

179.76

14 + 17.49
6 + 34.43
~~6 + 24~~

14 + 15.49
6 + 32.43
~~6 + 22~~

13 + 99.79
6 + 15.73
~~6 + 05.5~~ E Hilltop Drive

13 + 88.49
6 + 05.43
~~5 + 9.5~~

13 + 73.49
5 + 90.43
~~5 + 80~~

13 + 71.99
5 + 88.93
~~5 + 78.5~~

13 + 67.49
5 + 84.43
~~5 + 74~~

SL. Hilltop Drive Sec. parallel Hilltop Drive with

179.76

OK For Position
BUT STA. should be 5 + 84.43
~~(OK-FITED) for~~

33

L
167.94
11.9
50
30
20
163.2
167.1
168.8
170.7
8.1
5.1750
4.8
25.5

163.7
16.1
50
30
20
167.1
168.8
171.0
8.8
5.3
25.5

164.0
15.8
50
30
20
167.3
169.0
171.6
8.2
5.4
25.5

163.7
16.1
50
30
20
167.3
168.6
170.5
9.3
5.2
25.5

P. Pole
4

TCL Pole
2
167.5
12.3
50
168.7
11.0
40
170.1
8.3
30
171.5
5.4
20
174.4
4.8
8
175.0
4.6
25.5
176.1
3.7
30
177.07
2.69
30.7
Top
Wall

179.76
2

BM. ϕ pipe
 check to ~~Trail~~ Hilltop 4.23 171.15 171.13
 F.B. 1608-48

T.P. 0.44 175.38[✓] 4.84 174.92

Set B.M. Con. Moni on
 Boundary line to Hilltop
 Drive 9.01 170.75

14 + 30.09
~~6 + 47.03~~
~~6 + 36.6~~ = N.L. Hilltop + parallel

179.74

27

80.

R.

34

169.6	171.8	172.9	173.7	175.9
10.2		2.9	61	3.9
50	80	20		25.5

179.74

Sommermeier
W. Moore.
J. Green.

CROSS SECTION of
For Grade Est.

From Van Nuys to a point 226'
north of N.L. Pueblo lot 1783.

Left = to West

Right = to East

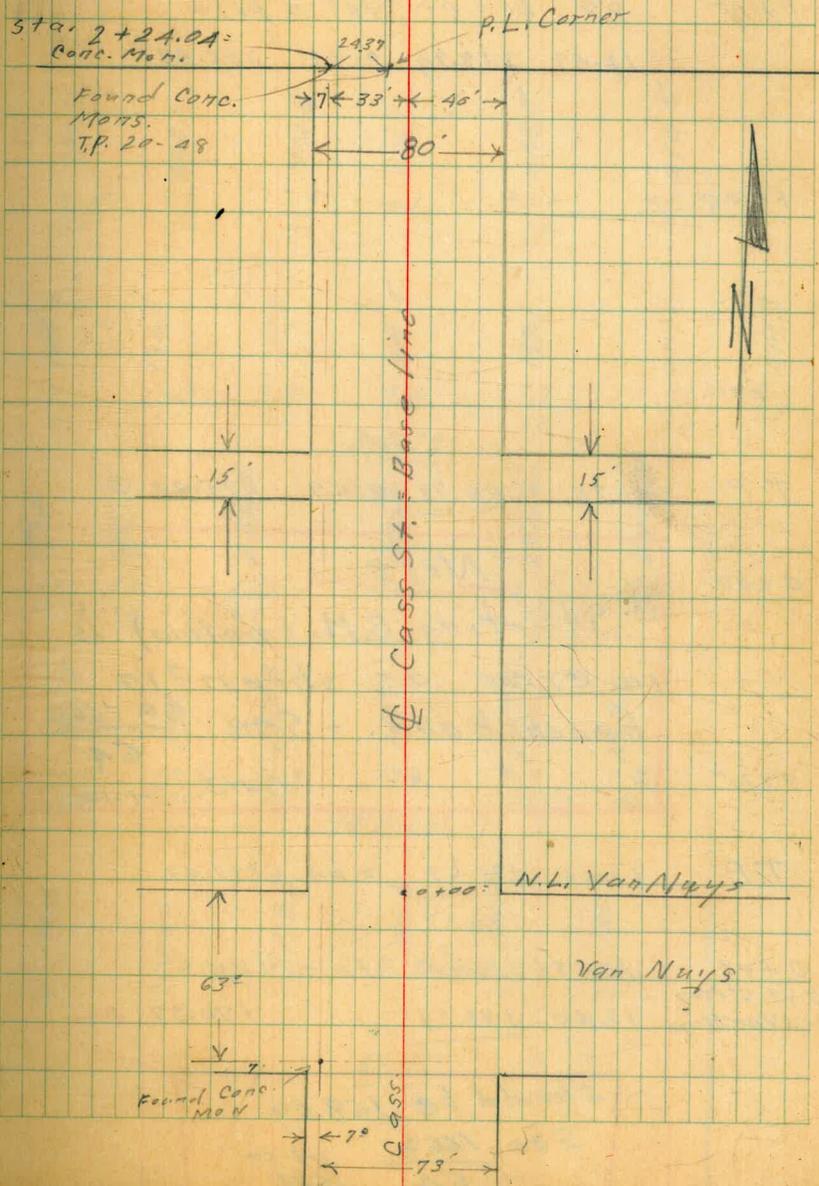
⊕ = ⊕ Cass.

See FB 2020 3/1/50
5A C.H.S.

Cass Street

W.O. #230 2/17/47 36

P.L. 1781 Indexed
e.s.k.



1+15 28' Lt. = Cts. 16" R. pole
 12.47 218.94 0.31 206.47

1+00

+75

T.P. 11.78 206.78 0.69 195.00

0+50

Note
 Starting B.M. (below) is
 in error as shown in
 bench book. - See F.B. 1662
 64
 C.H.S. 3-1-50

0+25

T.P. 12.66 195.69 0.24 183.03
 183.27

0+00 = North line Van Nuys
 S.W. 7' Mon
 Cass + Van Nuys 12.40 183.27 170.87

should be 168.59
 See 1662 3-1-50
 64

W

⊕
Cass

E

37

199.3	202.5	204.2	206.7	209.5	210.5
$\frac{7.5}{60}$	$\frac{4.3}{40}$	$\frac{2.6}{20}$	0.1	$\frac{+2.7}{20}$	$\frac{+3.7}{40}$
191.6	194.5	197.0	199.5	199.1	201.7
$\frac{15.2}{60}$	$\frac{12.3}{40}$	$\frac{9.8}{20}$	7.3	$\frac{7.7}{20}$	$\frac{5.1}{33}$
185.6	187.2	189.0	191.1	192.6	194.6
$\frac{10.1}{60}$	$\frac{8.5}{40}$	$\frac{6.7}{20}$	4.8	$\frac{3.1}{20}$	$\frac{1.1}{40}$
180.7	181.8	183.3	185.1	187.0	188.5
$\frac{15.0}{60}$	$\frac{13.7}{40}$	$\frac{12.4}{20}$	10.6	$\frac{8.7}{20}$	$\frac{7.2}{40}$
176.8	177.9	179.5	180.8	181.1	180.8
$\frac{6.5}{60}$	$\frac{5.7}{40}$	$\frac{3.8}{20}$	2.5	$\frac{2.2}{12}$	$\frac{3.0}{40}$
			195.69		
				183.27	

Set. B.M. Conc. Mon. W. 7' Cars + Pueblo line 6.77 237.27

2+24⁰⁴ = Pueblo line

2+00

1+75

T.P. 12.70 244.04 0.32 231.34

1+55

1+35

T.P. 12.93 231.66 0.21 218.73

1+17.5± = Φ Alley

218.94

W

Φ

E

38

222.8	236.4	240.1	243.9	245.8	246.9
$\frac{11.8}{60}$	$\frac{7.6}{40}$	$\frac{3.9}{20}$	0.1	$\frac{1.8}{20}$	$\frac{12.9}{40}$
228.7	231.5	235.8	238.6	240.6	242.8
$\frac{15.3}{60}$	$\frac{12.5}{40}$	$\frac{8.9}{20}$	5.4	$\frac{3.4}{20}$	$\frac{1.2}{20}$
219.5	226.0	228.7	231.1	233.6	235.5
$\frac{20.5}{60}$	$\frac{18.0}{40}$	$\frac{15.3}{20}$	12.9	$\frac{10.4}{20}$	$\frac{8.5}{40}$
			<u>244.04</u>		
217.5	220.4	223.3	226.1	229.0	230.7
$\frac{14.2}{60}$	$\frac{11.3}{40}$	$\frac{8.5}{20}$	5.6	$\frac{2.7}{20}$	$\frac{1.0}{20}$
210.6	213.7	216.1	219.7	222.1	225.3
$\frac{2.1}{60}$	$\frac{18.0}{40}$	$\frac{15.6}{20}$	12.5	$\frac{9.6}{20}$	$\frac{6.4}{40}$
			<u>231.66</u>		
204.7	207.4	210.1	215.0	215.8	217.5
$\frac{14.2}{60}$	$\frac{11.5}{40}$	$\frac{8.8}{20}$	5.9	$\frac{3.1}{20}$	$\frac{1.4}{40}$
			<u>218.94</u>		

A+25

$$\frac{11.3}{60}$$

A+00

3+85

$$\frac{21.7}{67}$$

3+55

3+00

2+40

244.04

227.7	227.7	225.0	231.4	233.6	236.8	240.0
$\frac{16.3}{60}$	$\frac{16.3}{40}$	$\frac{19.0}{26}$	$\frac{12.5}{12}$	$\frac{10.4}{9}$	$\frac{7.2}{20}$	$\frac{4.0}{40}$
219.5	222.9	229.5	235.2	239.9	243.6	246.5
$\frac{24.5}{58}$ IN WASH	$\frac{21.1}{40}$ IN WASH	$\frac{14.5}{20}$	8.8	$\frac{4.1}{20}$	0.4	$\frac{0.4}{40}$
227.5	230.2	233.8	238.3	242.6	246.5	246.5
$\frac{16.5}{60}$	$\frac{13.8}{40}$	$\frac{10.2}{20}$	5.7	$\frac{1.9}{20}$	$\frac{2.5}{40}$	
234.0	234.9	236.3	239.9	242.2	243.6	243.6
$\frac{100}{80}$	$\frac{9.1}{40}$	$\frac{7.7}{20}$	4.1	$\frac{1.8}{20}$	$\frac{0.4}{40}$	$\frac{0.4}{40}$
224.3	237.9	241.6	244.5	246.4	247.8	247.8
$\frac{9.7}{60}$	$\frac{6.1}{40}$	$\frac{2.9}{20}$	+0.5	$\frac{2.9}{20}$	$\frac{3.8}{40}$	

244.04

				- 0.03
				170.87
orig B.M. Should be	(170.87)	12.38	170.84	
TP	0.26	183.22	12.48	182.96
TP	0.28	195.44	12.02	195.16
TP	0.28	207.18	12.75	206.90
TP	0.68	219.65	12.95	218.97
T.P.	0.51	231.92	12.63	231.41
		244.04		

Ground rises to north

A+50

244.04

236.8	236.2	234.7	232.3	236.3	238.4
8.2	7.8	7.3	11.7	7.7	5.6
60	40	20		20	10

244.04

Xsec Lilac Path

Map # 1489 Auraca Hts

Moore
Boyer
Green
Roberts
H. 12.47

W.O. # 230

Set 2x2 RW 4x6

Lilac Path

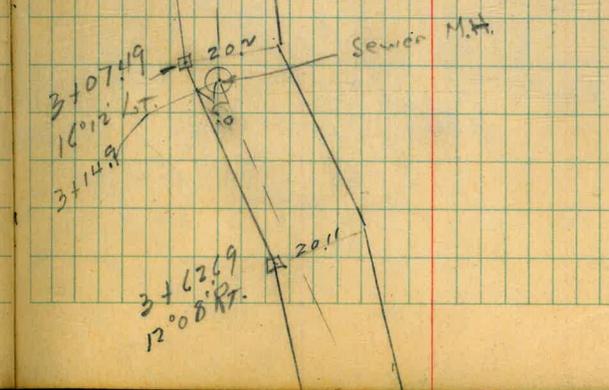
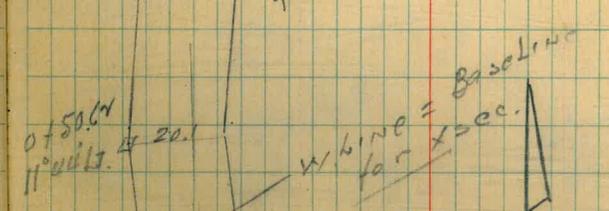
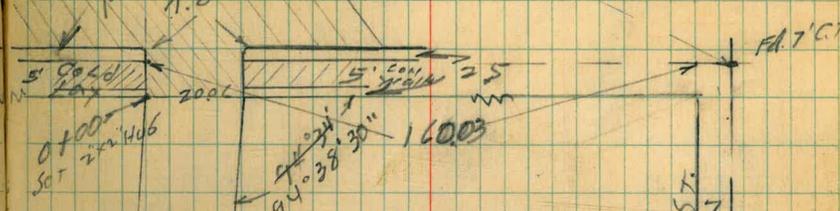
indexed
C.S.H.

41

290.30

Palm St.

90°
1.8" A.C. Pav.



W.L. 30.75 ST.

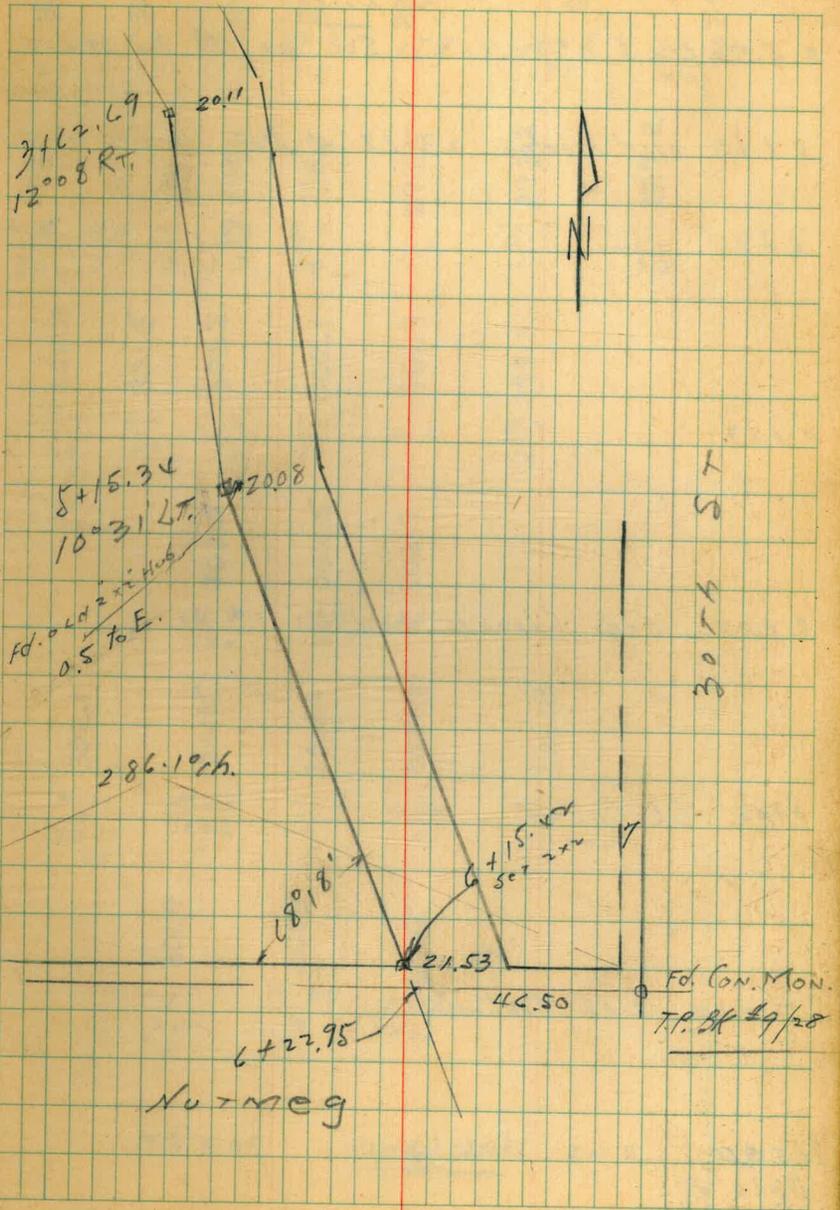
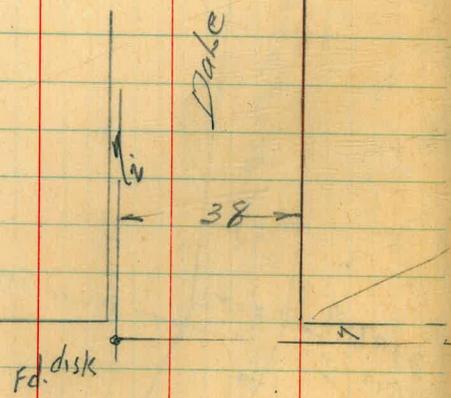
147' CT.



9°
18'18"
21°42'

1.07627
20
215254°

1.07627
7
753389



x sec Lilac Path

Note!

0 + 50.62 @ 11° 44' Lt

Sec: at D^s on split.

0 + 45 end hedge 23 Lt. of Beg. Lattice fence

0 + 35

0 + 27

0 + 06 Beg. Cypress hedge 19' Lt.

0100 SL PALM

0-10 SOB PALM

NEBP.

2.66

306.53

303.87

Dole +
PALM

	23	20	17	14	11	8	5	2
301.3								
300.5 = East								
297.3								
295.2								
290.7								
Baseline								
274.7								
302.1								
301.6								
299.3								
299.3								
298.1								
297.5								
292.2								
287.2								
302.3								
301.5								
300.2								
302.1								
301.9								
298.3								
303.0								
302.5								
302.7								
302.0								
302.18								
302.1								
301.5								
301.86								
301.55								
302.0								
302.18								

1+50

1+41 17.5 LT Tol. P. 46439 H

T.P. 0.51 284.78 11.76 284.27

1+25

1+00

1+03 end fence 24' LT.

1+07 19 LT 7" Eucal

0+99 20 LT 3" Eucal

0+96 22 LT 5" Eucal

0+93 16' LT 3" Acacia tree

0+90 22 LT 3" Eucal.

0+87 15' LT 4" Acacia 20' LT 5" di. Eucal.

0+81 20.5 LT 4" di. Eucal

0+77 20' LT 4" di. Eucal. tree

0+75

T.P. 2.40 294.03 12.90 293.63

30653

170 291.8

150 290.2 LT

130 287.8

110 281.3

90 274.8

75 269.7

60 257.8 P

45 257.4

25 257.4

wash

20 296.0

20 293.0

20 286.6

20 285.0

20 284.2

20 270.7

20 265.2

20 262.2

20 296.5

20 294.5

20 289.5

20 288.8

20 287.0

20 276.7

20 269.9

20 264.9

20 264.5

20 296.5

20 294.5

20 289.5

20 288.8

20 287.0

20 276.7

20 269.9

20 264.9

20 264.5

40 300.2

40 298.2

40 295.2

40 293.2

40 292.7

40 289.5

40 283.0

40 269.4

40 268.5

40 269.0

40 300.2

40 298.2

40 295.2

40 293.2

40 292.7

40 289.5

40 283.0

40 269.4

40 268.5

40 269.0

Bot. wash

296.03

Loc

3 + 07.49 @ 10' 12' LT

14.5
23
247.8

2 + 89 10' 47 Tchl. P. 95996 H

2 + 75

T.P. 1.97 261.97 12.68 260.00

2 + 50

217.9
+ 5.2
25

2 + 25

2 + 00

T.P. 0.21 272.68 12.31 272.47

1 + 75

284.78

15.5 14.8 15.2 14.3 14.5 14.5 11.2
25 20 18 10 14.5 5 13
Bot. Wash

256.0	254.8	253.8	252.9	253.2	249.8	248.5	249.6	251.4
15.5	14.8	15.2	14.3	14.5	14.5	11.2	11.2	11.2
25	20	18	10	14.5	5	13	13	13
267.3	265.3	261.1	258.5	261.97	250.5	250.3	252.3	251.4
15.5	14.8	15.2	14.3	14.5	14.5	11.2	11.2	11.2
25	20	18	10	14.5	5	13	13	13
272.7	271.9	266.6	265.4	265.9	259.6	253.0	253.0	253.3
15.5	14.8	15.2	14.3	14.5	14.5	11.2	11.2	11.2
25	20	18	10	14.5	5	13	13	13
284.7	280.2	277.8	272.7	271.5	266.1	264.7	258.0	254.4
15.5	14.8	15.2	14.3	14.5	14.5	11.2	11.2	11.2
25	20	18	10	14.5	5	13	13	13
287.8	284.5	281.5	276.5	272.68	266.0	255.8	258.4	258.4
15.5	14.8	15.2	14.3	14.5	14.5	11.2	11.2	11.2
25	20	18	10	14.5	5	13	13	13
284.78								

4+50

4+25

T.P. 2.60 242.90 / 0.30 240.36

4+00

11.0
30

3+62.69 d

3+50

8.0
27

3+25

3+15

T.P. 0.09 250.66 11.40 250.57
261.97

236.2	239.6	238.3	244.7	241.0	245.5	236.2
20	20	20	30	20	30	20
233.7	236.5	237.9	241.8	240.5	243.4	233.7
20	20	20	20	20	20	20
235.0	238.2	239.8	240.0	244.5	246.5	235.0
20	20	20	20	20	20	20
239.0	240.2	241.6	243.0	244.7	246.3	239.0
20	20	20	20	20	20	20
239.8	241.0	242.0	243.7	245.9	246.7	239.8
20	20	20	20	20	20	20
246.0	245.3	247.2	243.7	249.6	250.0	246.0
20	20	20	20	20	20	20
248.3	247.4	248.1	245.2	248.1	248.1	248.3
20	20	20	20	20	20	20

M.H. King

250.66

1320-20

check to top old curb
N.W. corner Nutmeg
and Date

	8.54	249.91	269.94	0.03
T.P.	8.20	278.45	0.49	270.25
T.P.	12.21	270.74	0.29	258.53
T.P.	12.45	258.82	0.54	246.37
T.P.	12.66	246.91	0.33	234.25

6x15.42 = N.W. Nutmeg Section Line

6+00

$\frac{10.4}{33}$ $\frac{12.5}{28}$

5+50

$\frac{8.5}{34}$ $\frac{9.8}{26}$
Wash

T.P. 2.56 234.58 10.94 232.02

5+15.34 $\Delta 10^{\circ}31'17''$

$\frac{14.0}{40}$

4+75

$\frac{10.3}{30}$ $\frac{12.7}{27}$
Wash

242.96

L

x/6

R

47

224.0	220.1	218.6	219.5	223.1	224.0	226.6	228.9
14.4	15.0	15.1	11.5	10.6	8.0	5.7	
21.5	19	10	7	7.8	3	10	
220.3	221.2	224.8	224.9	226.8	231.1	231.1	
14.3	13.4	9.8	7.7	7.8	10.5	10.5	
20	11	10	1				
225.2	226.9	229.3	229.6	230.0	232.8	237.6	
9.4	7.7	5.2	5	15.6	1.8	13.0	
20	7.6	13	10	5	1.8	10	
227.0	231.5	233.2	234.2	234.6	239.0	241.9	244.3
16.0	11.5	9.8	8.8	8.4	4.0	1.1	1.3
35	20	15	10	7	7.0	5	10
232.4	233.1	237.6	237.6	238.0	240.2	243.3	247.6
10.6	9.9	5.6	5.4	15.0	2.8	1.30	4.6
20	18	12	10	3		10	

242.96

Survey drain Ext. thru
 Lot 1 Blk 3 Valencia Park
 Cont'd. from FB, 1696-78

1100

0 + 75.38 Δ 15° 28' R Sec. on split

0 + 35

0 + 12 Δ 17° 30' R

0 + 09.3 F.L. inlet 36" pipe

175.96

LT

\$

R

48

$\frac{3.7}{10}$	$\frac{6.0}{19}$	$\frac{9.3}{8}$	10.0	$\frac{10.0}{5}$	$\frac{7.2}{12}$	$\frac{5.8}{20}$
1723	1700	1667	1640	1600	1688	1692

$\frac{4.4}{20}$	$\frac{7.1}{15}$	10.8	$\frac{10.8}{2}$	$\frac{6.2}{7}$	$\frac{5.2}{20}$
1716	1689	1652	1652	1698	1698

$\frac{1.8}{10}$	$\frac{9.0}{23}$	$\frac{11.1}{15}$	11.1	$\frac{11.1}{2}$	$\frac{5.3}{10}$
1692	1670	1649	1649	1649	1708

11.3

$\frac{8.5}{30}$	$\frac{9.2}{15}$	11.93	$\frac{10.0}{7}$	$\frac{5.0}{17}$
1675	1668	162.03	166.0	171.0

175.96

3 + 20 Δ 30° ~ 3' L7 Sec. on Spd 17

3 + 00

2 + 50

TP 8.40 184.04 0.37 175.64

2 + 00

1 + 50

1 + 20

17596

L7

8

17

49

6.0	9.4	10.8	9.8	3.3
^{178.0}	^{174.6}	^{173.2}	^{174.2}	^{180.7}
30	15	Wash	10	30

6.2	10.1	11.1	11.5	10.8	8.5	5.0
^{177.8}	^{173.9}	^{172.9}	^{172.5}	^{173.2}	^{175.5}	^{179.0}
30	10	Wash	12	21	28	

6.2	12.6	13.4	11.0	9.4
^{177.8}	^{171.4}	^{170.6}	^{173.0}	^{174.6}
30	11	Wash	22	30

0.4	3.5	4.2	5.4	7.0	5.2	4.2
^{175.6}	^{172.8}	^{171.8}	^{170.6}	^{168.4}	^{170.8}	^{171.8}
25	16	4	10	15	30	

2.7	4.0	5.9	9.0	6.8	5.9
^{173.3}	^{172.0}	^{171.1}	^{167.0}	^{169.2}	^{170.1}
30	13	10	23	33	

4.6	6.0	9.4	9.6	6.5	5.1
^{171.4}	^{169.4}	^{166.6}	^{164.4}	^{169.5}	^{169.8}
30	11	10	15	30	

17596

check to E Ld. C.T. 189x5
 San Jacinto 4.38 189.47 189.47
 and Churchward

T.P. 8.27 193.85 0.82 185.58

on disk
 T.P. 12.16 186.40 9.80 174.24 174.24
 811.

5700

4750

4700

3751

18404

Notes Reduced. 7-14-47
~~88~~

$\frac{1.0}{12} 182.4$ $\frac{2.0}{2} 181.7$ $\frac{1.0}{5} 182.6$ $\frac{0.0}{10} 184.0$

$\frac{1.0}{11} 182.7$ $\frac{0.5}{4} 180.3$ $\frac{1.0}{2} 180.7$ $\frac{0.8}{15} 183.2$

$\frac{1.0}{15} 178.0$ $\frac{1.0}{12} 176.8$ $\frac{1.0}{15} 177.2$ $\frac{2.0}{15} 182.0$

$\frac{8.2}{17} 175.7$ $\frac{8.8}{9} 175.2$ $\frac{8.48}{11} 175.4$ $\frac{8.9}{8} 175.1$ $\frac{8.7}{8} 175.3$ $\frac{5.0}{15} 178.4$
 M.H.
 P.M.
 18404

Cross Section High Ave.

Torrey Pines Rd. to Virginia Way

Ed. 7' CT⁵

Moore
Green
Roberts

Set 2"x2" R.M. hub. disk
W.O. 31141

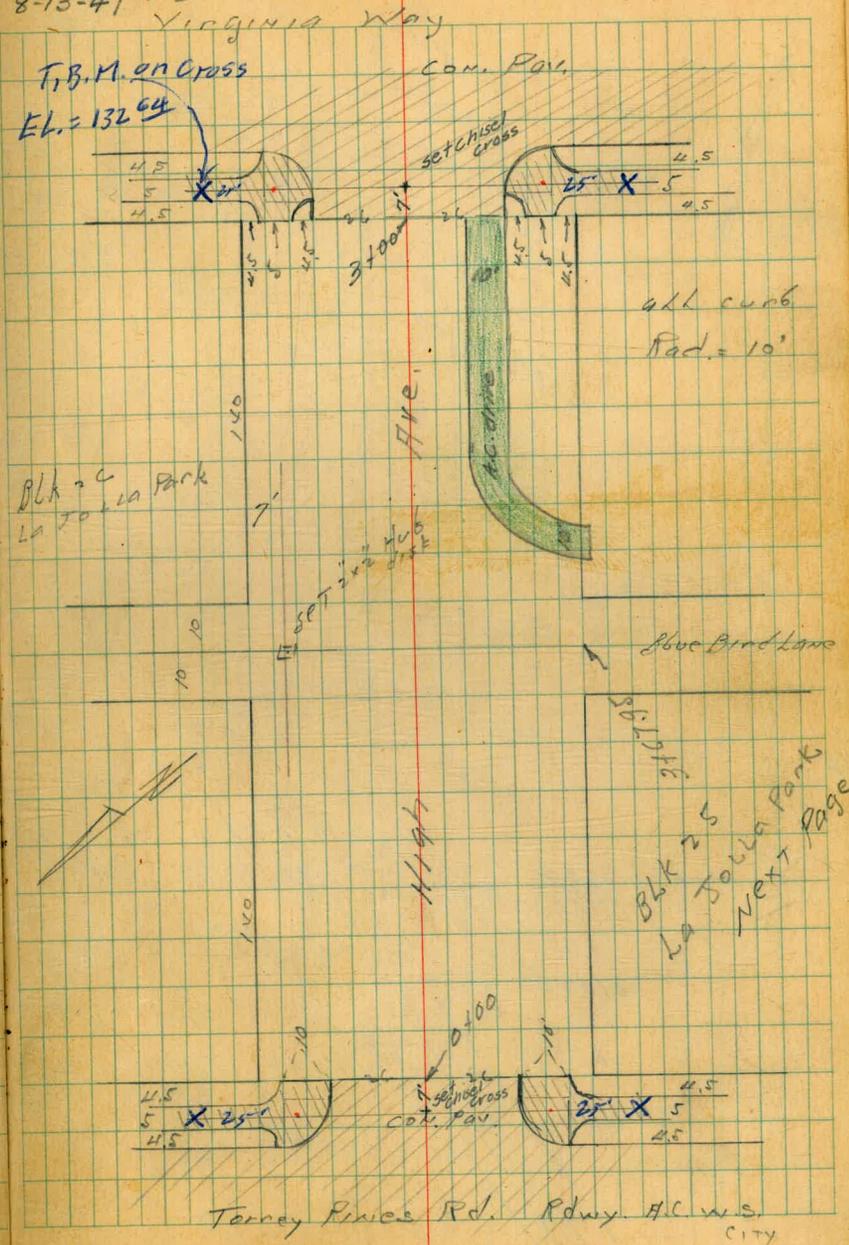
8-C-47

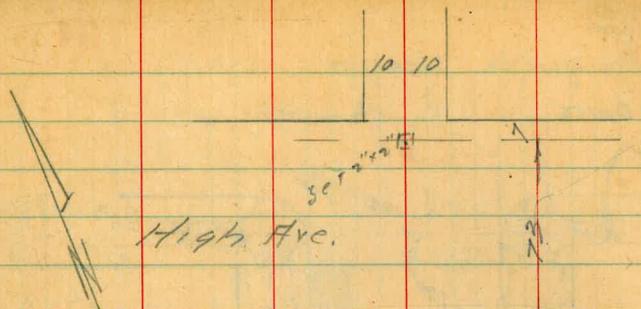
X = CROSS = 25' TIC to 7' L&T.

Cut 6-29-56 - CHD

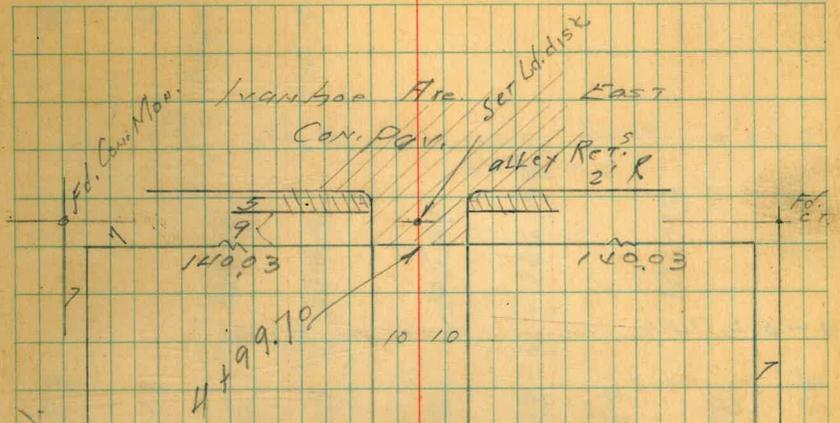
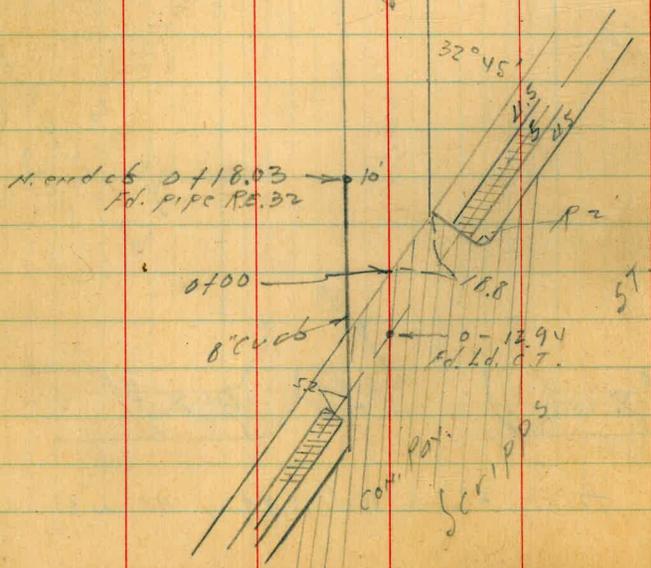
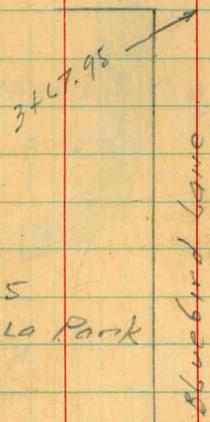
Indexed M2
8-13-47

51





Blk 25
La Jolla Park



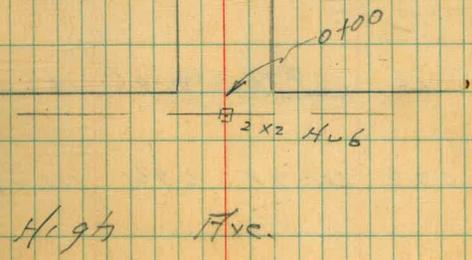
Tarrey Pines Rd.

Now paved
4" with
A.C. Pav.

Blk 26
La Jolla Park

Bluebird Lane

Virginia Hwy



04683 Top step

04683 step on walk

04637 Sedge 27 ^{Con.} walk // with alley

0450

0435

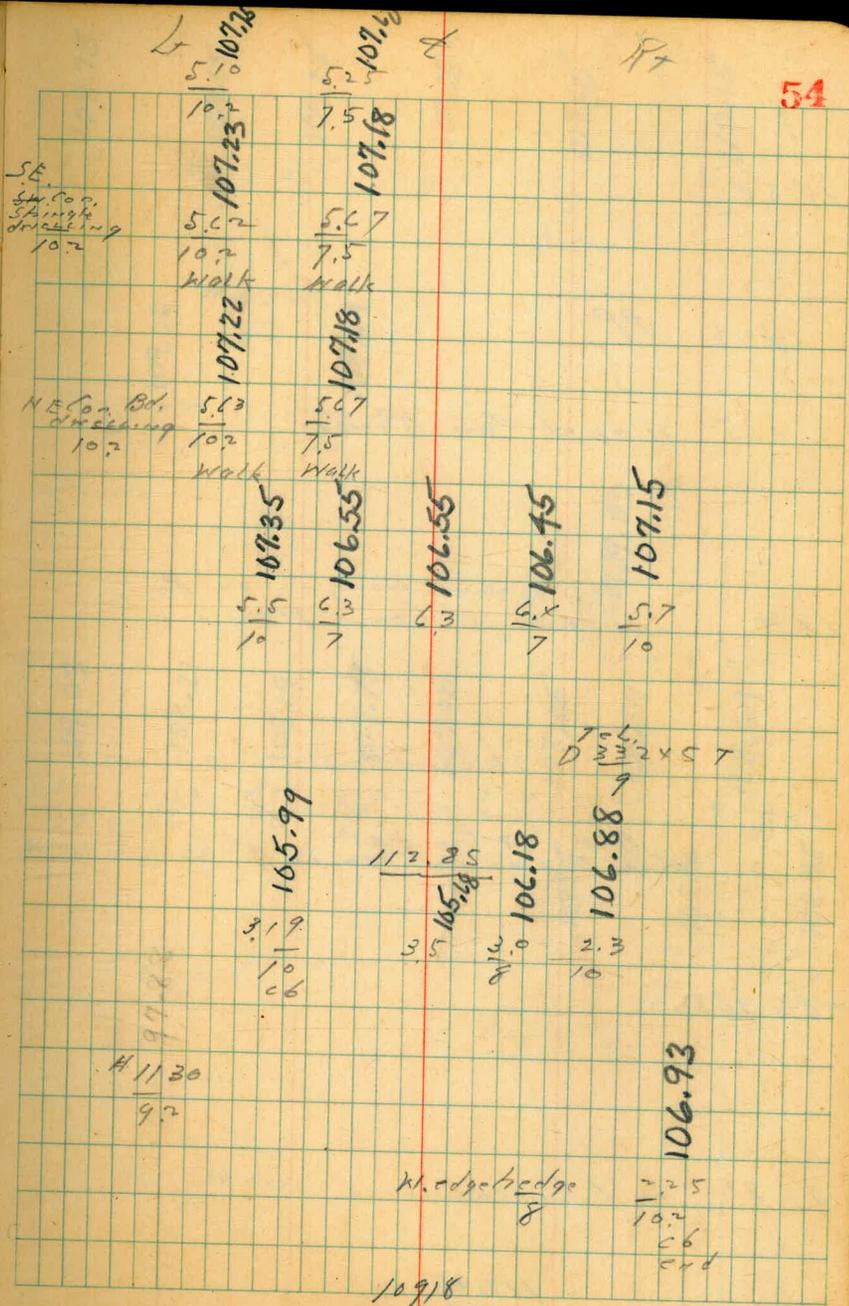
T.P. 708 112.85 341 105.77

0418 end ck. on W. + SE loc. Bd. + Bat. dwelling on line

0417 P.P.

0416 Beg. Cypress hedge

10918



1450

+42 PP

+15 N end Con Ramp

1411

beg. Cypress hedge on Rt.
N. end of Con apron " "

139 Lt S.E. Con Shingle dwelling

1400

S.L. Con apron on Rt
End 2.7 Con walk " Lt
also beg. of Con Ramp

0 + 96.5

0 + 81

end Cypress hedge

112.85

20 109.75

3.2 109.65

3.4 109.25

5 109.25^{fx}

3.3
8 hedge 109.65

1.2 110.15

55

3.79
13.8 #1150
8.6

N.E. Con
shingle dwelling

4.21
10 108.64

W. edge
hedge 3.87
10 apron + 90'

109.03

109.03

108.21

108.19

109.75

109.65

108.05

108.59

108.64

3.82
13.9
107

4.64
10
walk

4.66
7.0
walk

4.51
11

5.2

5.6
10
107.95

4.20
10
108.40

4.21
14.5
108.45

N.E. Con. shingle
dwelling
107

W. edge hedge
11

5.6
10
107.95

4.20
10
108.40

4.20
12.9
108.45

112.85

2+05 S end Con apron

2+04 7' Pt end + wedge hedge

2+00

1+96 7.6 Pt = Bay ^{West edge} Cypress hedge

1+87 E S. M. gar.

1+81.5 S. L. Con apron

1+78 end hedge on Pt.

TP 6.17 115.81 3.21 109.64
112.85

L+

R

56

4.5
20
111.31

5.0
10
110.81

5.3
10
110.51

5.1
110.71

4.7
7
111.11

4.4
10
111.77

4.2
9.9
111.58

4.2
10
111.61

4.23
10.1 = Mk. apron

4.35
10.7
111.76

4.28
10.3
111.53

4.41
10.2
111.40

Wedge hedge
7

115.81

3100

2195 10 LT end Lark fence

2182 N end Con. drive

2171 8' B. end of Hedge ^{Cypress} hedge

T.P. 786 120.16 351 11230

2169 99' end wire fence and Beg. Lark fence

2150

2120 Beg. Cypress hedge

2119 10.5 LT. Beg. wire fence

211 9 do. gas. Con. Dr.

11581

LT

5.5
10 114.66

5.7
10 114.96

5.7
10 114.46

5.2
10 114.96

57

6.4
10 113.76

7.2
10 112.96

6.30
10 113.86

5.7
10.1 114.42

5.2
10 114.42
5.2 end.
Con. drive

120.16

2.9
10 112.91

pp. 1170
5.5
10 112.31

6.0
10 112.11

6.7
10 112.61

112.13

W. edge
B. edge
8.5

3.58
10 Row
N end apron

111.86

3.95
10.1
apron

112.06

3.75
18.7
gas

11581

Set
T.P.
Nail
Cor.
fence

0.8 119.8 ✓

3 + 67.95 = S.L. High Ave.
= 10.4 LT end Bd. fence

+ 67 10 Pt. Tel. P. 432483 H

3 + 50

3 + 18 11.3 Ft Ctr. Cypress tree hedge
10.1 Lt Beg. Bd fence

3 + 13.5 N. edge Com drive

3 + 11 Sin gar dirt floor

3 + 02.5 S edge Com drive

120.6

L

R

R

58

$\begin{array}{r} 2.4 \\ 10 \\ \hline 117.76 \end{array}$

$\begin{array}{r} 1.9 \\ 10 \\ \hline 117.26 \end{array}$

$\begin{array}{r} 3.0 \\ 10 \\ \hline 117.16 \end{array}$

$\begin{array}{r} 2.9 \\ 10 \\ \hline 117.26 \end{array}$

$\begin{array}{r} 1.3 \\ 10 \\ \hline 117.86 \end{array}$

115.66

$\begin{array}{r} 4.5 \\ 11.4 \end{array}$

$\begin{array}{r} 4.3 \\ 10.4 \\ \hline 115.83 \end{array}$

115.21

$\begin{array}{r} 4.95 \\ 9.9 \end{array}$

120.6

End Cypress
Trees

Sketch P. 51

W.O. 31141 Xsec High Ave

Torrey Pines Rd. to Virginia Pt. ^{Way}

0130

0123 end 8" Cornwall 40 ft
and Beg. Bd. Fence

0107

0105 Beg. 8" Cornwall

0100 E. La. Torrey Pines Rd. 40' 17' Beg. Picket
fence

0-14 E. C6 Line

0-40 E Torrey Pines Rd.

T.P. Nail 861 128.09
P. 58

119.28

L₄ = 216
Indexed - 8-13-47

35/40 124.59
4.9/12 123.19

3.8/40 124.29
5.5/9 122.49

5.5/7 121.59

6.3/70 121.09
6.3/70 121.79

8.0/29 120.09

8.7/50 119.39

120.37

7.7/40 Topwall

4.6/40 123.49

5.2/36 122.87

6.17/26 121.92

6.67/13 121.42

6.69/70 121.40

7.07/70 121.02

7.7/13 120.35

8.79/26 119.30

8.27/26 119.82

8.20/56 119.89

8.2/50 119.69

3.48/75 124.41

4.21/75 123.98

5.18/40 122.91

5.79/40 122.30

6.36/26 121.71

7.40/70 120.69

8.6/26 119.47

9.20/26 118.79

8.7/26 119.37

11.38/75 116.71

10.80/75 117.29

1.71/100 126.38

4.37/50 123.72

6.26/70 121.83

8.23/40 119.86

11.45/100 116.64

128.09

59

1762

1760

1744

T.P. Nail 1266 13214 861 11948

1740

139.6 40' Rt end fence

1700

0750 40' Lt. end Picket. Bag. Bd. Fence

128.09

L

R

R

0

125.14
40

123.54
60

122.84
30

120.04
80

123.04
50

122.34
20

120.54
110

118.24
210

122.89
50

122.29
20

120.84
110

118.24
210

end fence 40

124.59
40

122.19
20

121.99
110

121.69
60

120.29
29

118.79
40

118.09
45

124.19
40

123.29
20

122.49
110

121.89
60

121.59
29

118.49
40

118.09
45

128.09

3.00 W.L. Virginia Way

T.P. 6.78 134.93 1.99 130.15

2.75

2.50

2.00

1.8x

132.14

5	131.53
40	5.89
	35.5
	WALK
6.3	131.04
20	6.63
66	130.30
20	7.24
97	129.69
13	7.25
13	129.68
747	129.46
73	7.96
26	128.97
91	8.1
66	128.32
26	8.24
35.5	128.89
40	8.70
40	128.73
	8.6
	128.33

6.3	125.84
40	7.3
38	124.84
26	8.2
14	123.94
26	8.1
20	124.04
10.1	123.04
29	122.04
30	11.3
30	120.84
30	11.7
40	121.24
40	120.54
45	120.44
5	130.64
40	1.5
10	3.0
33	4.1
4.9	127.24
27	7.5
40	8.3
45	8.7
40	128.14
5.7	126.44
5	6.0
5	126.14
5	123.84
5	123.44
5	123.84
5	120.74
5	120.44

132.14

check to N.W. BP curb
Kline + transit 0.69 128.05 128.09
0.00

NOIL T.P.
P. 58 9.26 128.74 119.48

check to NOIL T.P.
P. 58 8.93 119.48 119.48

T.P. 7.81 128.41 11.33 125.60

3740 E Virginia

3714

136.93

L E R 82

2.09	134.84	134	135.59
100	134.28	100	132.27
40	131.49	134	130.63
26	130.99	40	129.09
40	130.49	630	127.90
20	129.92	7.84	128.41
701	128.63	50	125.71
20	127.90	11.17	
903	128.41	100	
50			
97			
1101			
100			

136.93

1000 Bluebird Lane
 W.D. 31141 Blk 2C La Jolla Park

1+02 Tel.P. 8.4 RT 300044H End picket fence 10RT

1+00 End Bd. Fence beg. picket 10 Lt

0+97 N.L. Conc. Apron Beg. Bd. Fence 9.9 Lt

0+91 Center Apron and Garage

0+85 10LT end Bd fence + S. edge Con. Apron

T.P. 726 139.95 111 130.69

0+85 10 LT end Bd fence + S. edge

0+75 Beg. Picket fence 10 RT

0+51 PP 9.7 LT #1216

0+50 Beg. Bd fence 10.7 Lt

0+45 N.L. apron + garage

128 S.L. Con apron on Lt. Do. gar

125 end Con. wall + fence

+01 Tel.P. 9.5 RT. 432484 H

0+00 N.L. High

T.P. nail
 10' W of
 3+6795
 P. 58
 1232 131.80 119.48

Lt. Wly
 Indexed - 8-13-47

R. 63
 130.82

7.86 22.4 Gar.	129.27 8.12 10.4	8.68 10.5 9.03 10.5 To Conc. AP.	129.95 8.0 10 129.77 8.1 129.85	130.09	130.36 7.13 10.1 7.6 10 S. edge Con apron
5.23 22.4 9.25 126.53	5.67 10 Coll. 125.05	6.75 9.9 apron	126.57 126.18 59 125.90	126.57	126.20 127.00 127.40
5.25 22.5 9.07 123.80	6.75 9.9 apron		123.10 122.90	123.80	123.40 123.90
8.0 10 101	8.0 10 7	2.7 2.9	131.80	8.0 10 7	7.9 10

1+97 Tol. P. 9.3 Rt # 432485 H

1+89 E S. H. gar. Con Fl.

1+75 10 Rt Beg. Bd. fence

1+72 N edge Con apron

T.P. 6.48 143.47 0.96 136.99

1+64 E do. gar. Con.

1+57 S edge Con apron

+50 P.P. 9.5 Lt # 1230

1+49 N edge Con apron

1+44 10.7 Rt end Con. Blk wall

1+40 E do. gar

1+30 S edge Con apron

1+25 N edge apron + Beg. Con. Blk wall

1+13 E do. gar. or Rt

137.95

138.66

4.81
20.13

1.00 136.95

1.12

133.66

4.79
20.00
94.00

end fence 10.7

5.8

137.95

1.80 136.15

1.10

3.54
10.50
apron

133.72

4.23
10.50
apron

133.72

143.47

2.15
135.55

3.60
134.35

132.88

5.07
10.20
apron

5.8

136.72
1.75
10.00
135.95

2.10
10.00
135.89

3.15
10.00
137.55

137.85

5.35
10.20
131.54

131.54
5.93
10.00
apron

136.95
7.02
11.00
apron

11.50
20.60
135.89

3.10
12.70
137.85

137.85

132.60

5.93
25.10
gar.

132.60

136.95

136.80

136.80

136.80

132.88

132.60

132.60

+ 35 10.4 Lt end Rock wall

T.P
CON.
W.L. 9.22 151.13 156 141.91

+ 25 N edge Con apron 102 Rt Beg.

+ 24 N edge Con apron

2+14 E do 940 Rt + Lt

+ 106

+ 102.5

+ 102 S edge con apron on Rt

+ 102 end Bd fence 101 Rt

2+100 S edge con apron on Lt

143.47

143.87
7.26 8.05 8.27 8.5
10.4 10 8 8.5
TOP WALL 151.13

Bd fence

142.22
140.92
140.69
140.96
140.79
140.31
140.47
2.55 2.78 2.51 2.88
25 18 12 10.5
do 940 apron

3.6
12.1
Con apron

outlet
FL 3" drain 3.78
14. Con apron 11.5
140.25
3.2 3.85 4.1
12.3 10.3 10
apron apron

139.62
139.37
139.07

143.47

142.63
142.93
141.82
141.02
16.5
10 2.45
14.5

140.67
140.55
140.96
2.8 2.92 2.51
10 11.8 18.5
apron

139.01

4.0 FL outlet
9.7 4" drain

139.71
139.27
139.07
138.07
139.07
4.4 4.4 4.4
7 8.8 9.1 10.1

3+50 Beg. fence wire 11.8 ft & hedge
 End fence 10' LT
 3+43 ♀ Sin gar. Con Floor

+38 10' LT P.P. #1270
 3+29 11.7 ft end fence

T.P. 7.01 155,842.30 148.83

3100 7.01 P. 9.5 ft D 304777 J.P. 1267.

+90 ♀ Sin gar. Con apron. 1.5 wide

+83.5 ♀ Sin gar. Floor

+77 10.8 LT end Picket

+75 end of fence below

+53 end Bd Fence + ^{Beg. Lattice fence} with cow Robble wall

+50 9.5 LT P.P. #1250
 11' LT. Beg. Picket fence

2+41 ♀ Sin gar. Con. Floor ^{Con apron}

151.13

1" app REV 8
 150.24
 150.04
 150.24
 150.44
 5.1
 14.7
 200

Beg. Wire fence
 148.53
 2.0
 148.33
 2.0
 147.13
 3.5
 147.03
 147.13
 148.03
 155.8x
 148.23

Beg Picket
 11.6 Fence

147.13
 2.5
 147.17
 3.96
 24.7

144.72
 144.51
 145.03
 143.61
 144.53
 144.03
 141.00
 141.33
 141.33
 141.33

141.33
 141.33
 141.33

151.13

+50
 +49 10.3 Rt Tel. P. D 3047 LT
 +42.5 10.9 Lt 8 Bd. Bar. shed
 +39 10.9 Lt end barb fence

 +12 Beg. Barb fence 10.8 Lt

 4 +07 8 Sin gan + Con apron

 +02 end wire fence 12 Lt

 4+00

 +915 Sin gan Con apron
 +82 12 Lt Beg. wire fence
 +79 12.3 Rt end wire fence + hedge

 3+73 Sin gan Con Floor

 3+61 8 Sin gan Con apron

 155.84

67

27
 153.67
 2.17
 97

 152.40
 3.4
 12
 900

 152.35
 3.4
 99
 apron

 151.99
 3.9
 0
 152.04

 151.31
 4.53
 151.10
 4.7
 11.9
 900

 151.04
 4.8
 11.2
 apron

 153.54
 2.30

 153.88
 1.96
 pav.

 153.94
 1.9
 10
 dirt on
 pav.

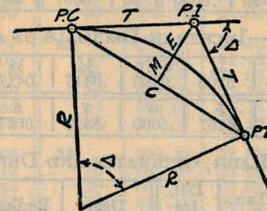
 152.14
 3.4
 152.39
 3.4
 151.39
 1.8
 0
 151.39

 152.51
 3.4
 152.39
 3.4
 151.39
 3.4
 151.39
 3.4
 151.39

155.84

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

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CURVE FORMULAS

- Radius— $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve= D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)
- Tangent— $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve— $L = 100 \frac{\Delta}{D}$ (4)
- Middle ordinate— $M = R(1 - \cos \frac{\Delta}{2}) = R \text{vers} \frac{\Delta}{2}$ (5) (6)
- External— $E = T \tan \frac{\Delta}{4} = R \div \cos \frac{\Delta}{2} - R$ (7) (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)
- Long Chord— $C = 2 R \sin \frac{\Delta}{2}$ (10) $\Delta = \text{Central Angle}$

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{3} = 414.49$ ft. From Table V correction = .36 or $T = 414.85$ ft. P. C.—Sta. P.I.— $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T.—Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = $158 - \text{Sta. P. C.} = 54.50$, hence offset = $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^\circ$ or = defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8\frac{1}{3} = 136.2'$ or $2^\circ 16.2'$, or = $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 115.27$ and from Table V correction = .10 or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

367-87

11.8
15.8

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1 1/2
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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