

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6 + (20 - 16) ÷ 2 or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.
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1727

CITY ENGINEER'S OFFICE

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.

1917
CITY ENGINEER'S OFFICE

The right page of the notebook is covered in a green grid pattern. A vertical red line is drawn down the right side of the grid, creating a margin. The grid consists of small squares, and the red line is positioned approximately one-fifth of the way from the right edge of the page.

Blk C 8 P. Loma Hrs

0 + 51 E 12" PP, 9.3 Rt

0 + 50

0 + 20

0 + 17 ctr. 10" P. pole.

0 + 05

0 + 00 Ely Santa Barbara

0 - 10

BM.
NXP BP 11.24 201.41
Newport
Santa Barbara

189.97

ht = nly

2

P

3

Levels checked
Jan 17-47
S. Sisson

201.41

199.6	199.4	198.9	198.9	200.6
1.8 ✓	2.0	2.523	2.5	0.8
$\frac{10}{10}$	$\frac{8}{8}$		$\frac{2}{2}$	$\frac{10}{10}$
1982	197.1	196.9	196.8	199.3
3.1	4.3	4.5	4.6	3.1
$\frac{10}{10}$	$\frac{8}{8}$		$\frac{8}{8}$	$\frac{10}{10}$
196.9	195.5	195.4	195.4	197.2
4.5	5.9	6.0	6.0	4.2
$\frac{10}{10}$	$\frac{8}{8}$		$\frac{8}{8}$	$\frac{10}{10}$
196.8	194.8	194.8	194.9	193.97
4.6	5.6	5.6	5.5	7.44 = Top end CB.
$\frac{10}{10}$	$\frac{8}{8}$		$\frac{10}{10}$	
1981	193.6	193.6	193.8	193.84
8.3	7.8	7.8	7.6	7.57
$\frac{10}{10}$			$\frac{10}{10}$	$\frac{10}{10}$
dirt			dirt	Top CB. Ret.
		201.41		

2401 F 12" PP B.V R_r

1+50

1+21 E.L. Com. Apron & do gar

1+05 W.L. Com. apron & do gar

1+00

0+69 E.L. Com. apron & do gar

0+53 W.L. Com. apron & do gar

T.P. 11.73 213.03 0.11 201.30

201.41

L_r

8

R_r

4

205.9	205.0	205.1	206.4	7.0
<u>7.1</u>	8.0 ✓	<u>7.9</u>	<u>2.0</u> ✓	<u>4.0</u>
10		7	10	40

204.86	202.96
8.17	9.07
25.6	11
9.00	AP.

204.81	202.92
8.27	10.11
25.6	11
9.00	A

202.2	201.6	201.8	203.1	9.9
<u>10.8</u> ✓	11.1 ✓	<u>11.2</u>	<u>9.9</u>	<u>9.9</u>
10		7	10	40

201.92	201.30
<u>11.2</u>	<u>11.73</u>
25	13

201.75	200.53
<u>11.28</u>	<u>12.50</u>
25	13
gar	apr.

213.03

213.03

2+5A W.L. Conc. Apr. + dec gas.

2+50

2+22

2+04 W.L. Conc apr + dec gas.

T.P. 10.50 ~~223.70~~ 0.33 21270

2+01

1+75

21303

LT

R

P

5

21592

7.28
Apr

21529

17.91
Apr 17

2142

9.0 ✓
10

2135

9.7 ~~98~~

2131

10.1
5

2136

9.5 ✓ 8.5 2.4
10 20 40

22320

21385

9.85

25.3
Apr

21385

9.85

21.3
Apr

21268

10.52

14
Apr

21324

9.95

25.3
Apr

21321

9.99

20.5
Apr

21182

11.38

14
Apr

223120

2101

2.9 ✓
10

2093

3.7 ~~8.6~~

2085

4.2
5

2099

3.1 ✓
10

4.5
10

21303

2078

5.7
10

2071

5.9
5

2070

6.0
5

2080

5.0
10

5.9
40

21303

3+54 W.L. Con apron + gar

3+50

3+38 9' do. gar. Con fl.

3+20^E E.L. Conc. Apron + Do. Gar.

3+20 10' Rt. & sewer lat.

3+04 W.L. Conc. Apr. + Do. Gar.

3+00

2+70 E.L. Conc. Apr. + Do. Gar.

223.20
213.03

Lr

±

R

6

221.41

1.79

21

gar

219.9

3.3
10

220.22

2.98

10.2

apr.

219.5

3.7
7

219.1

4.1

219.0

4.7
6

12.1
9.0

220.2

3.0
10

219.88
3.32
13.9
gar fl.

218.53

4.07

24.2

218.46

4.7x

22.7

218.51

4.67

Gar 24.2

218.46

4.80

22.7 apr.

217.0

5.2 ✓
10

215.99

7.21

24.4

gar

216.7

6.5
8

215.70

7.50

13.3

Apron

217.03

6.7
N.H. Riv

216.5

6.7
6

217.4

5.9 5.9
10

5.5
10

223.20
213.03

5+01 9" Rt. = ϕ 8" P.P.

5+00

T.P. 4,37 232.76 1.51 228.39

A+97 E.L. Conc. Apron + Do. Gar

A+79 W.L. Conc Apron + Do. Gar

A+50

A+486 ϕ 3' Conc. Walk

229.90

226.8

6.0
10

226.2

6.6
7

226.3

6.5 ✓

226.7

6.1
10 ✓

232.76

227.08

2.82
Gar 20.9

226.70

3.20
Apron 10.9

227.08

2.82
Gar 20.8

226.13

3.77
Apron 10.9

224.7

5.2
10

224.3

5.6

224.2

5.7
7

224.8

5.1
10

224.53

5.37
10.3

229.90

S. Wly. B.R.
Venice + Newport

Error - 0.02
shown as 230.14 ✓
2.64 230.12

6+10⁵⁰ Wly. Curb line Venice

6+00⁵⁰ Wly. Line Venice

5+60

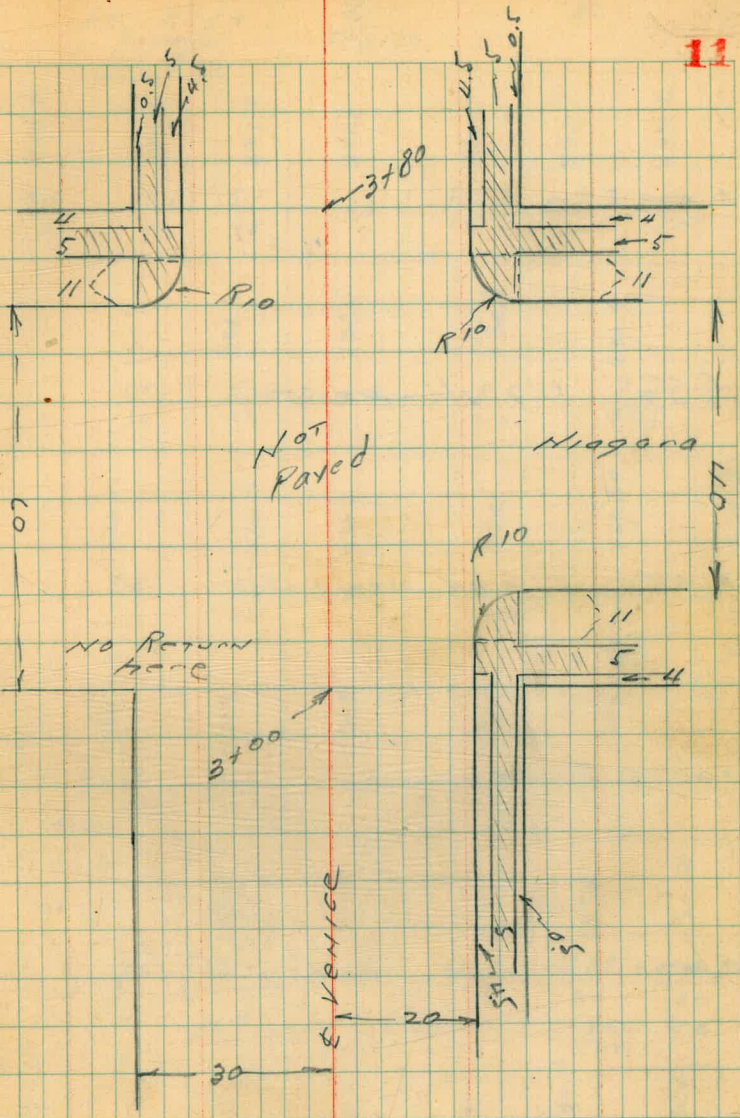
5+35 20.8 Lt = ϕ 18' Do Gar. Conc. Floor

5+25 E.L. Conc. Apron & Do. Gar.

5+05 W.L. Conc. Apron & Do. Gar.

232.76
X

228.7	227.8	227.4	226.5	227.2
$\frac{4.1}{30}$	$\frac{5.0}{10}$	5.4	$\frac{6.3 \checkmark}{10}$ Ground	$\frac{5.34}{10}$ Top Cl. Ret.
	228.0	227.7	227.4	227.69
	$\frac{4.8 \checkmark}{10}$	5.152	$\frac{5.4}{10}$ Ground	$\frac{5.07}{10}$ Top Cl.
	228.1	228.15	227.8	227.9
	$\frac{4.745}{10}$	$\frac{4.61}{10}$ M.H. Rim	$\frac{5.0}{6}$	$\frac{4.9 \checkmark}{10}$
228.76	227.6	227.4	227.3	227.5
$\frac{4.00}{20.8}$ Gar. Floor	$\frac{5.52}{10}$	5.455	$\frac{5.5}{6}$	$\frac{5.3 \checkmark}{10}$
228.67	227.72			
$\frac{4.07}{20.7}$ Gar. Apron	$\frac{5.04}{11}$ Apron			
228.71	227.26			
$\frac{4.05}{20.7}$ Gar. Apron	$\frac{5.50}{10.8}$ Apron			
				232.76



Check to Dr. B. A., 559 230.14 230.14

T.P. 1128 235.73 203 224.45

3 + 80 Sly Niagara

3 + 70

226.45

3 + 60 Sly of Niagara

3 + 40 E Niagara

226.48

L

Denise

R

15

217.0	216.78	215.7	215.8	215.6	217.04	217.2
9.5	9.70	10.8	10.7	10.9	9.44	9.3
30	20	20	20	20	20	30
30	06	97		97	06	
	217.19	216.1	216.2	216.1	217.11	
	9.29	10.4	10.1	10.4	8.97	
	20	20	20	20	20	
	708	97		97	708	
	06				06	
217.25	217.2	216.7	216.9	216.5	216.9	217.63
9.23	9.13	8.8	9.6	10.0	9.6	8.85
30	30	20	20	20	30	30
708	97				97	708
06					06	
217.6	217.8	217.9	217.9	217.9	218.1	
8.9	8.7	8.6	8.6	8.6	8.4	
30	20	20	20	20	30	

226.48

X-Section of 15' Alley in Block H - Bet.
 45th + West - N. of Logan - See sketch

0+75

0+50 - 6.8 Lt. = ϕ P. pole

0+49 - 15' Lt. = S.E. Cor. store gar. Conc. floor opening S.

0+33 - 11' Rt. = Med. House

0+10

0+00 = N.L. Logan - edge of Conc. pave = 0+00.2

0-10 = N. cb of Logan - Paved - Conc.

BM.

793

92.95

85.02

Disk ϕ Logan
 + 45th

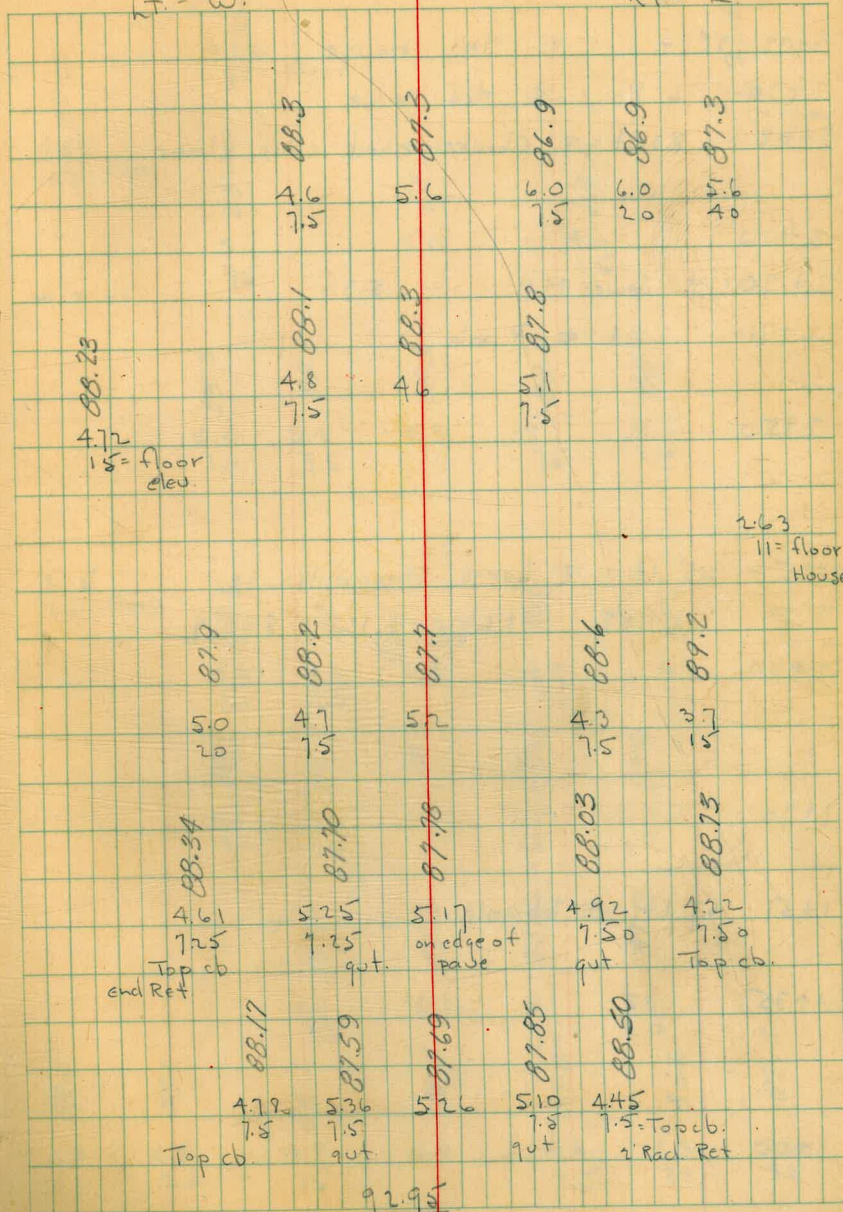
Indexed
 C.M.K.

ϕ

17

Lt. = W.

Rt. = E



3+32 - 88 Lt. = \$ Med. House
 3+30 - 76 Rt. = \$ Med. House
 3+08 - 8.3 Lt. = \$ Chicken shed - conc. floor

3+00

2+90 = \$ Sewer M.H. 5.30 on rim

2+71 - 7.2 Lt. = \$ P. pole

2+50

2+25 - 65 Lt. = \$ Large Stucco House

T.P. 4.88 93.67 4.16 88.79

2+00

1+70

1+51 6.7 Lt. = \$ Tel. pole

1+35

1+00

Alley Bk. H

18

	LT			Rt.	
29.00	3 92.45				92.05
158	88.0				76.2
83 = floor					76 = Floor
	1 88.0			1 89.1	
	0 1			0	
	1 88.3			1 88.6	
	0 4			0 1	
	1 88.3			1 88.0	
	0 5			0 1	
	1 88.4			1 88.6	
	0 3			0 1	
3.15					
65 = floor					
	1 88.6			1 88.6	
	0 3			0 3	
	1 88.2			1 88.6	
	0 0			0 0	
	1 88.3			1 88.8	
	0 6			0 0	
	1 88.6			1 87.9	
	0 3			0 0	
	1 87.8			1 87.0	
	0 1			0 0	
	1 88.1			1 86.6	
	0 1			0 0	
	1 88.0			1 87.3	
	0 1			0 0	
	1 88.5			1 87.8	
	0 1			0 0	
	1 88.0			1 86.6	
	0 1			0 0	
	1 88.0			1 87.3	
	0 1			0 0	

92.95

T.P. 5.89 93.28 ct of Alley B
+ E O.U.

Check BM. 13.69 85.48 85.44 ct. 45' + Ocean U.
+ + to W.

6+20.28 - E Alley and S. edge of 20' strip Conc. pave.

6+00.28 = S.L. Ocean View

5+98

5+80

5+78 - 7' Rt. = E Tel. pole

5+77 - 7' Rt. = E Tel. pole

5+50

	Lt.	±	Rt.
	90.6	90.20	90.36
	8.6 20	8.97	8.81 5
	90.6	92.0	92.2
	8.4 2	9.11 5	8.91 5
	93.1	92.3	91.7
	93.2	92.5	91.9
	93.3	92.6	91.9
	93.7	92.7	91.9
	93.7	92.8	91.9
	93.7	92.9	91.9
	93.7	93.0	91.9
	93.7	93.1	91.9
	93.7	93.2	91.9
	93.7	93.3	91.9
	93.7	93.4	91.9
	93.7	93.5	91.9
	93.7	93.6	91.9
	93.7	93.7	91.9
	93.7	93.8	91.9
	93.7	93.9	91.9
	93.7	94.0	91.9
	93.7	94.1	91.9
	93.7	94.2	91.9
	93.7	94.3	91.9
	93.7	94.4	91.9
	93.7	94.5	91.9
	93.7	94.6	91.9
	93.7	94.7	91.9
	93.7	94.8	91.9
	93.7	94.9	91.9
	93.7	95.0	91.9
	93.7	95.1	91.9
	93.7	95.2	91.9
	93.7	95.3	91.9
	93.7	95.4	91.9
	93.7	95.5	91.9
	93.7	95.6	91.9
	93.7	95.7	91.9
	93.7	95.8	91.9
	93.7	95.9	91.9
	93.7	96.0	91.9
	93.7	96.1	91.9
	93.7	96.2	91.9
	93.7	96.3	91.9
	93.7	96.4	91.9
	93.7	96.5	91.9
	93.7	96.6	91.9
	93.7	96.7	91.9
	93.7	96.8	91.9
	93.7	96.9	91.9
	93.7	97.0	91.9
	93.7	97.1	91.9
	93.7	97.2	91.9
	93.7	97.3	91.9
	93.7	97.4	91.9
	93.7	97.5	91.9
	93.7	97.6	91.9
	93.7	97.7	91.9
	93.7	97.8	91.9
	93.7	97.9	91.9
	93.7	98.0	91.9
	93.7	98.1	91.9
	93.7	98.2	91.9
	93.7	98.3	91.9
	93.7	98.4	91.9
	93.7	98.5	91.9
	93.7	98.6	91.9
	93.7	98.7	91.9
	93.7	98.8	91.9
	93.7	98.9	91.9
	93.7	99.0	91.9
	93.7	99.1	91.9
	93.7	99.2	91.9
	93.7	99.3	91.9
	93.7	99.4	91.9
	93.7	99.5	91.9
	93.7	99.6	91.9
	93.7	99.7	91.9
	93.7	99.8	91.9
	93.7	99.9	91.9
	93.7	100.0	91.9

99.17

T.P. 5.91 98.20 8.39 92.29 Hub. E +
St. T

6+02 = 7.5 Rt. = end picket fence

6+00.59 = S.L. T St. - Dirt Graded - cb. from Alley E.

5+96 = 5.6 Lt. = P. pole

5+75 = 12' Lt. = Med. House under Const.

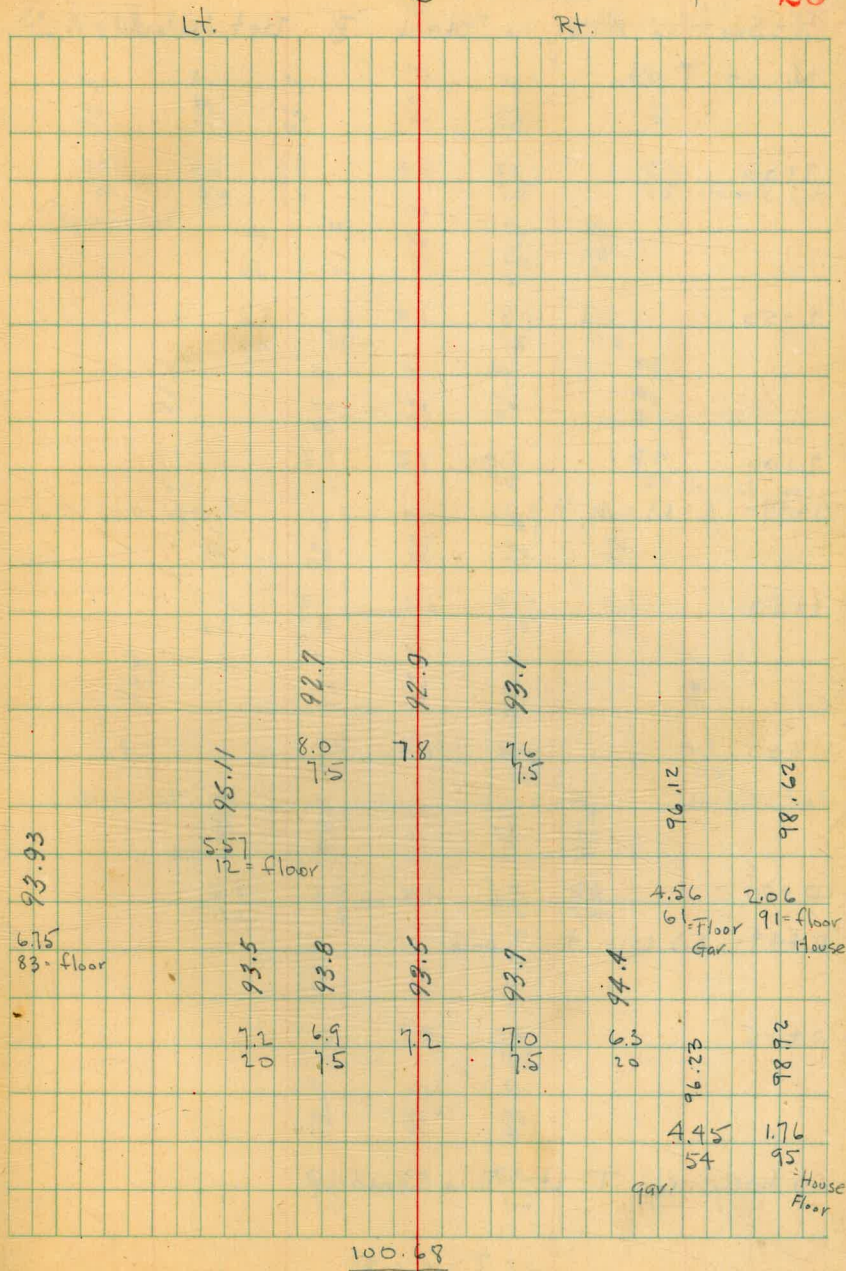
5+74 = Rt. = Med. House + 6' Lt. = Gar. Conc. floor + Tubs

5+70 = 83 Lt. = Med. House under Const.

5+50

5+22 = 95 Rt. = Med. House + 5' Rt. = Gar. Conc. floor + Tubs

5+02 = 7.4 Rt. = Beg. picket fence



X-Sect 15 Alley in Block "B" Bet. West + 46th
N. of T St.

3+00

2+50

2+00

1+99 - 5.3 ft. = P. pole

1+50

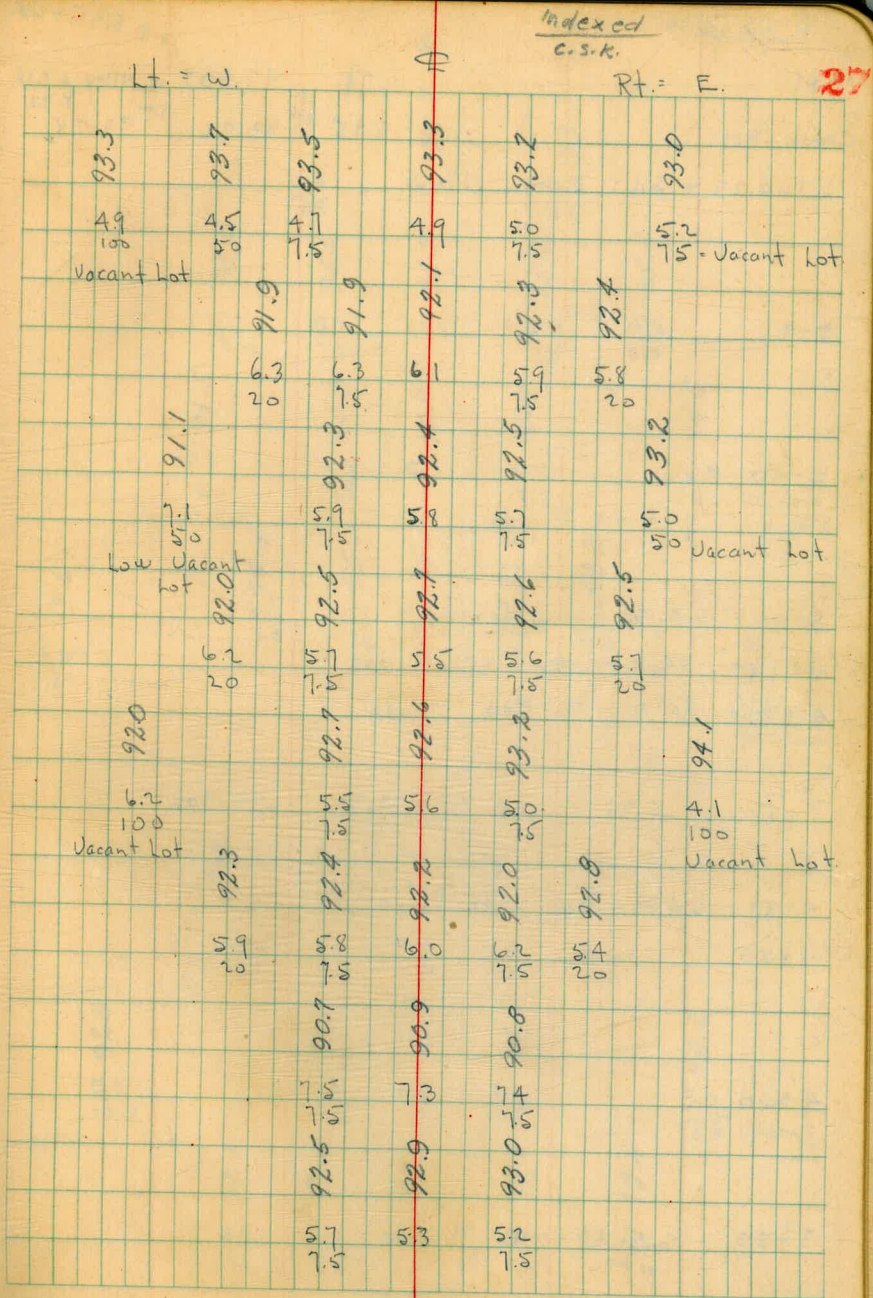
1+00

0+50

0+49 - 5.3 ft. = P. pole

0+05

0+00 = N.L. T St - Dirt Graded.



B.M.

2.71

97.50

ct. \neq BIK C + 0.0

\neq Alley + 0.0
ct. P. 22
93.28

Check B.M.

6.95

93.26

6+00.23 = S.L. Ocean View

5+97

5+50

5+01 - 7 Lt = \neq P. pole

5+00 - 6.0 Rt = end fence

4+76 - 84 Lt = \neq Med. House

4+75 - 94 Rt = \neq Med. House

T.P. 5.31 100.21 3.30 94.90

4+51 - 6.4 Rt = bee wire fence

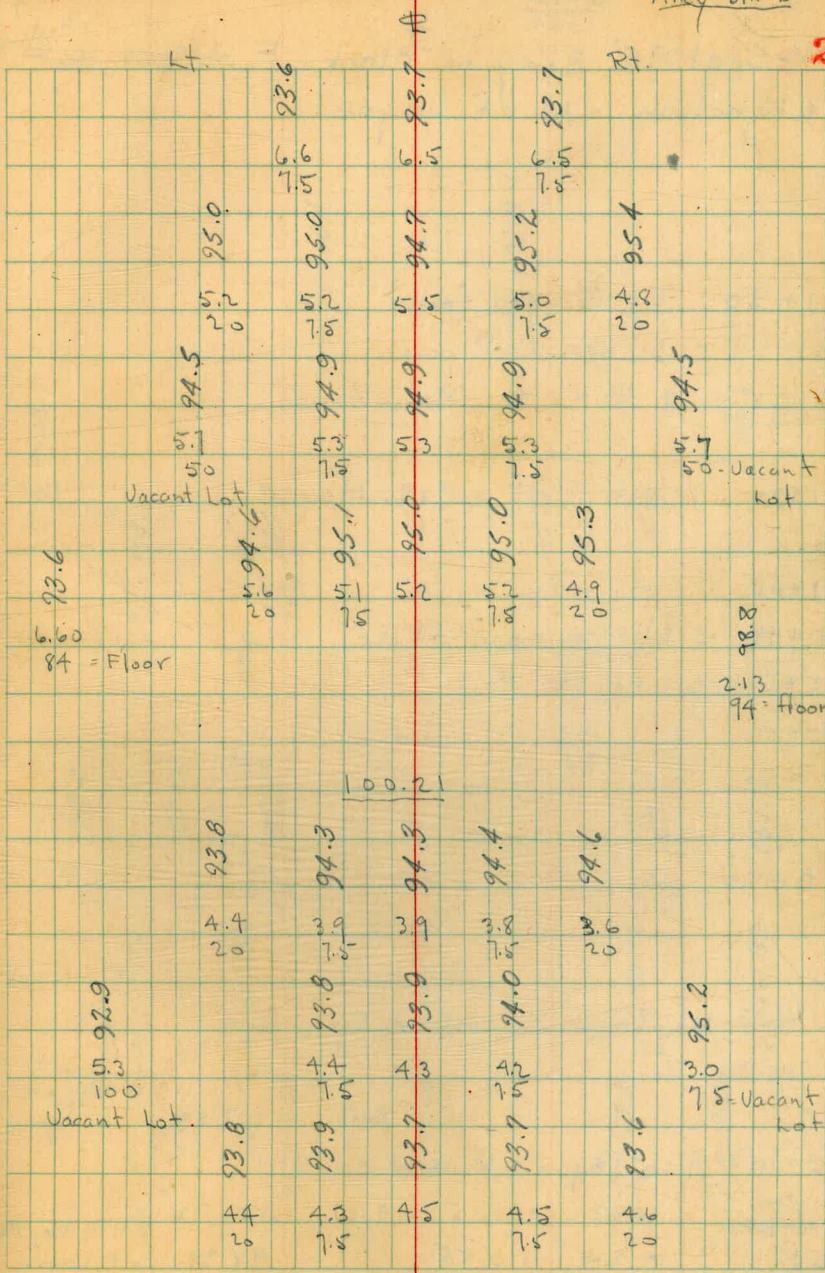
4+50

4+00

3+50 - 6.5 Lt = \neq P. pole

Alley BIK B

28



98.20

Lt.

R

Rt.

T.P. 11.76 109.26 0.50 108.76 ct. Alley Blk D
 + \$ O.V.
 use this
 Check B.M. ct. on \$ Alley + \$ O.V. 5.93 97.48 ✓ 97.50 R28

6+00.32 = S.L. Ocean View

5+85 - 11' Rt. = \$ Doub. Gar. Conc. floor

5+70 = \$ House on Rt. - Conn.

98.0	98.1	98.4	
5.4	5.3	5.0	
75		75	
98.9	99.0	99.1	
4.4	4.4	4.3	4.15 floor
75		75	11 Gar.

103.41

X-Sect. 15 Alley in Block E. Bet. Pynchan
 & 47th N. of Logan

1+48- 6.4 Rt. - Φ P. pole

1+25- 6.7 Rt. = Φ Med. house

T.P. 9.79 123.55 5.99 113.76

1+00

0+84- 8.3 Rt. = Φ Good shed - wood floor

0+60

0+59- 8.1 Rt. = Φ Shed. - dirt floor

0+49- 6.4 Lt. = Φ P. pole

0+30- 7.3 Rt. = Φ Med. House

0+11- 8' Rt. = Φ of Comb. shed + Gar. wood floor - openings to Logan.

0+00 = N.L. Logan = 0.25 ahead of edge of Conc. pave

Rods on pave

T.P. 0.84 119.75 0.94 118.91

0-10 = N. cb. of Logan - paved - Conc.

0.84

N.W. 2P 47th & Logan

0.94

118.91

1660-P40
118.83

B.M.

12.31

119.85

107.54

7.0
8-2746

indexed
C.S.K.

35

	Lt.	Φ	Rt.	
				126.18
				263 67 = floor
	109.4	12.2	123.55	13.7
	10.4	8.3	113.0	
	7.5	20	6.8	6.1
vac. lot.		7.5		7.5
		13.3		14.4
			11.2	
				4.10 = floor 83
	7.9	6.5	5.6	5.4
	20	7.5		7.5
				5.3 8.1 = floor
		12.6	11.4	14.0
				121.07
	7.9	7.1	6.4	5.8
	20	7.5		7.5
				11.32 = floor 73
				3.95 11 = floor
	4.98	5.6	5.42	5.1
	8	2		7.0
Top cb. end of Ret.	114.63	114.10	114.33	114.60
	5.1	5.5	5.42	5.1
	7.5	9.0		7.5
				4.5
				114.22
				119.75
				114.21
				5.5
				114.21
				5.37
				7.5
				4.80
				114.99
				7.5
				Top cb. 2 Rod. Ret.
				119.79

Lt.

Rt.

6+00.34 = S.L. T st. 4.78 117.01 on Hub.

5+75

5.7	17.4	117.6	18.2
20	4.4	4.2	3.6
	7.5		7.5
	18.0	118.6	10.8
	3.8	3.2	3.0
	7.5		7.5

121.79

curb + Gutter levels on Logan
 from 45th to 47th - Paved - Conc +
 Conc. curbs + sidewalks in. 60' st. 10' cbs.
 See sketch P. 16. for exact Dist. thru blocks.

T.P. 11.42 103.27 1.18 91.85 Disk # Logan
 + West

2+65 = W.L. West. St.

2+00

1+50

for Alley Ret. on Lt. - See Alley x-Sept.

1+00

0+50

0+00 = E.L. of 45th to N. - Conc. strip pave

B.M. 8.01 93.03 85.02 Disk # Logan
 + 45th

8-28-46

7.0.

Lt. = N.

⊕

Indexed
 C.S.K.

Rt = S. 42

91.23	90.67	91.10	90.65	91.24
1.80 20=cb.	2.36 gut.	1.93	2.38 gut.	1.79 20=cb.
89.83	89.16	89.58	89.17	89.81
3.20 20=cb.	3.87 gut.	3.45	3.86 gut.	3.22 20=cb.
88.75	88.13	88.59	88.04	88.74
4.28 20=cb.	4.90 gut.	4.44	4.99 gut.	4.27 20=cb.
87.68	87.13	87.49	87.09	87.72
5.35 20=cb.	5.90 gut.	5.54	5.94 gut.	5.31 20=cb.
86.57	86.02	86.42	86.06	86.65
6.46 20=cb.	7.01 gut.	6.61	6.97 gut.	6.39 20=cb.
^{x10} 85.63	^{x10} 85.16	^{x10} 85.14	^{x10} 84.94	^{x10} 85.66
7.40 20	7.87 gut.	7.89	8.09 gut.	7.37 20=Top cb. PC. Ret.
Top cb. - end of cb.				
		93.03		

T.P. 9.60 112.48 0.39 102.88

2+00

1+50

1+00

0+50

3+25 = E. L. of West St. = 0+00 ahead.

3+15 = E. cb. West.

2+95 = Φ West.

2+75 = w. cb. line of West st. to the N.
No. Ret. on S.

8-29-46
7.0.

Lt.

Φ

Rt.

43

101.47	100.87	101.29	100.97	101.54
1.80	2.40	1.98	2.30	1.73
20=cb.	got.		got.	20=cb.

99.25	98.62	99.07	98.71	99.27
4.02	4.65	4.20	4.56	4.60
20=cb.	got.		got.	20=cb.

97.01	96.38	96.70	96.30	96.87
6.26	6.89	6.57	6.97	6.40
20=cb.	got.		got.	20=cb.

94.70	94.14	94.49	94.04	94.69
8.57	9.13	8.78	9.23	8.58
20=cb.	got.		got.	20=cb.

92.57	91.95	92.66	92.23	92.88
10.70	11.32	10.61	11.04	10.39
20=cb.	got.		got.	20=cb.

92.56	91.97	91.69	92.35	91.97	92.61
10.71	11.30	11.58	10.92	11.30	10.66
20=Top cb.	got.	20		20	20=cb.
end Ret.				got.	

95.67	91.25	91.85	91.47	91.05	(92.05)
7.60	12.02	11.42	11.80	12.22	102.22
30	20		got.	20=cb.	
on N. edge of	in Cross				
pass	got.				

91.39	90.89	90.88	91.41	90.87	91.49
11.88	12.38	12.39	11.86	12.40	11.78
30	30	20		20	20=cb.
Top cb.	got.			got.	
end Ret.					

103.27

0+14 = Brk. to inlet in gut on Rt.

0+05 = € 10' Curb inlet on Rt.

3+45 = E.L. 46th = 0+00 ahead.

3+40 = opp. Brk. in gut on Rt. to cb. inlet

3+31 = E. cb. 46th Ret. opp. same as other 13' Rad.

3+05 = € 46th

2+79 = W. cb. Line 46th - apprx. a 13' Rad. on Ret. as near as can meas.

2+65 = W.L. 46th to N. Dirt - old cbs. broken up. No Ret. on S.

Lt.		€	Rt.		
105.70 6.78 20 = cb.	104.95 7.53 gut.	105.58 6.90	105.13 7.35 gut.	105.70 6.78 20 = cb.	
105.54 6.94 20 = cb.	104.99 7.49 gut.	105.44 7.04	104.63 7.85 20 on grate	105.60 6.88 20	
105.52 6.96 20 = cb.	104.99 7.49 gut.	105.38 7.10	104.65 7.83 gut.	105.55 6.93 20 = cb.	
105.64 6.84 20.9 cb. on Ret.	104.93 7.55 gut.	105.30 7.18	104.80 7.60 gut.	105.45 7.03 20 = cb.	
105.73 6.75 33.3 Top cb. end Ret.	105.07 7.41 33.3 gut.	104.88 7.60 20	105.20 7.28	104.60 7.68 gut.	105.28 7.20 20 = cb.
104.76 7.72 33.4 N. edge of Pave	104.52 7.96 20 = in cross gut.	104.80 7.68	104.80 7.68	104.36 8.12 gut.	104.94 7.54 20 = cb.
104.80 7.68 33.4 Top cb. - attend of Ret.	104.16 8.32 33.4 gut.	104.04 8.44 20	104.40 8.08	103.92 8.56 gut.	104.47 8.01 20 = cb.
104.48 8.00 20 = cb. P.C. Ret.	103.60 8.68 gut.	104.08 8.40	103.58 8.90 gut.	104.15 8.33 20 = cb.	
112.48					

2+03 = P.C. of cb. Ret. on Rt.

1+83.5 = E. cb. of st.

1+66.5 = \pm St. to S

1+49.5 = W. cb. line of Navy Housing St. Paved A.C.

1+30 = P.C. of Ret. on Rt.

1+00

0+50 = opp brk. in gut. to inlet on Lt.

0+24 = \pm 10' cb. inlet on Lt.

logan

45

Lt.

\pm

Rt.

108.75 3.73 20=cb.	108.16 4.32 gut.	108.63 3.85	108.22 4.26 gut.	108.74 3.74 20=cb.
--------------------------	------------------------	----------------	------------------------	--------------------------

108.42 4.06 20=cb.	107.83 4.65 gut.	108.26 4.22	107.96 4.52 20	108.05 4.43 40 gut.	108.51 3.97 40 Top cb. P.C. of Ret.
--------------------------	------------------------	----------------	----------------------	------------------------------	--

108.18 4.30 20=cb.	107.68 4.80 gut.	108.02 4.46	107.65 4.83 20	108.26 4.22 40 end Conc + brk A.C. Pave
--------------------------	------------------------	----------------	----------------------	---

107.88 4.60 20=cb.	107.41 5.07 gut.	107.77 4.71	107.39 5.09 20 in Cross gut.	107.97 4.51 40 gut.	108.45 4.03 40 Top cb P.C. Ret.
--------------------------	------------------------	----------------	---------------------------------------	------------------------------	---

107.01 5.47 20 in Alley	107.46 5.02	107.09 5.39 gut.	107.86 4.82 20=cb.
----------------------------------	----------------	------------------------	--------------------------

107.03 5.45 20=cb.	106.58 5.90 gut.	106.98 5.50	106.62 5.86 gut.	107.04 5.44 20=cb.
--------------------------	------------------------	----------------	------------------------	--------------------------

106.13 6.35 20=cb.	105.69 6.79 gut.	106.09 6.39	105.73 6.75 gut.	106.19 6.29 20=cb.
--------------------------	------------------------	----------------	------------------------	--------------------------

105.90 6.59 20=cb.	104.93 7.55 20=on grate	105.77 6.71	105.29 7.19 gut.	105.75 6.73 20=cb.
--------------------------	----------------------------------	----------------	------------------------	--------------------------

112.48

1+50

1+00

0+50

T.P. 9.31 120.37 142 111.06

3+25 E.L. Pyncheon = 0+00 ahead.

3+15 E. cb. line

2+95 = E Pyncheon

2+75 = W. cb. line

2+65 = W.L. Pyncheon st. to N. no Ref. on S.

Logan

46

Lt.

Rt.

115.21

114.67

115.05

114.53

115.09

5.16
20=cb

5.60
gut.

5.32

5.84
gut.

5.28
20=cb.

113.63

113.21

113.51

112.95

113.49

6.74
20=cb.

7.16
gut.

6.86

7.42
gut.

6.88
20=cb.

112.01

111.55

111.95

111.56

112.11

8.36
20=cb.

8.82
gut.

8.42

8.81
gut.

8.26
20=cb.

110.54

110.11

120.37
110.64

110.39

110.92

1.94
20=cb.

2.37
gut.

1.84

2.09
gut.

1.56
20=cb.

110.67

110.10

109.91

110.94

110.19

110.70

1.81
30
Top cb. end
Ret.

2.38
30
gut.

2.57
20

2.04

2.29
gut.

1.78
20=cb.

109.89

109.58

110.08

109.73

110.23

2.59
30=edge of
Conc. Pavt.

2.90
20

2.40

2.75
gut.

2.25
20=cb.

109.62

109.25

109.18

109.77

109.40

109.91

2.66
30
Top cb. end
Ret.

3.23
30
gut.

3.30
20th Cross
gut.

2.71

3.08
gut.

2.57
20=cb.

109.63

109.04

109.65

109.25

109.77

2.85
20=cb.

3.44
gut.

2.83

3.23
gut.

2.71
20=cb.

FB 2037-47
R. B.C. 109.55 cb
109.97 gut

112.48

Elevation Sewer Man Hole
Colony Road + 70th St. La Mesa

BM 3.23 467.49 464.26 ^{SMBP} Elevation 70th

TP 9.03 469.01 7.51 459.98

TP 1.62 468.13 2.50 466.51

Existing Sewer MH 3.99 464.14 ^{at Rim}
" " " 16.79 451.34 ^{Bottom + Set of} Channel E + M

TP 0.89 467.87 1.15 466.98

TP 6.97 466.97 7.87 460.00

BM 2.71 464.26 ^{SMBP} Elevation 70th
464.26

Indexed
C.S.R.

Oct. 17-46

48

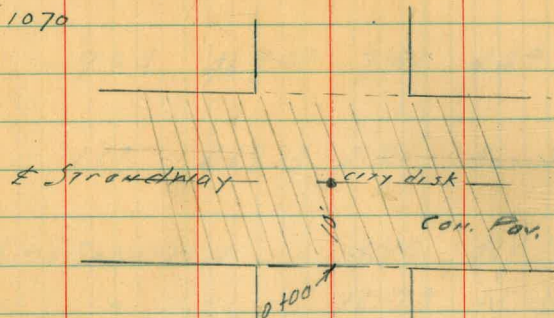
Sisson
McCoy
Haddell
Ellen
H.O. 1907

C. Moore
 Soren Meyer
 W. F. M.
 E. B.

Cross Sec. alleys Blks 175 & 176
 Mission Beach

10-31-46

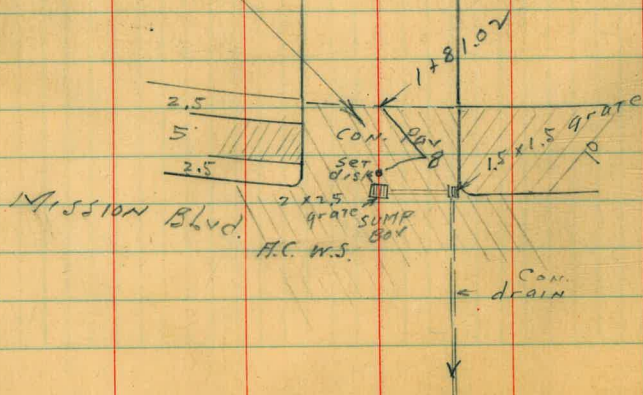
W.O. # 1070



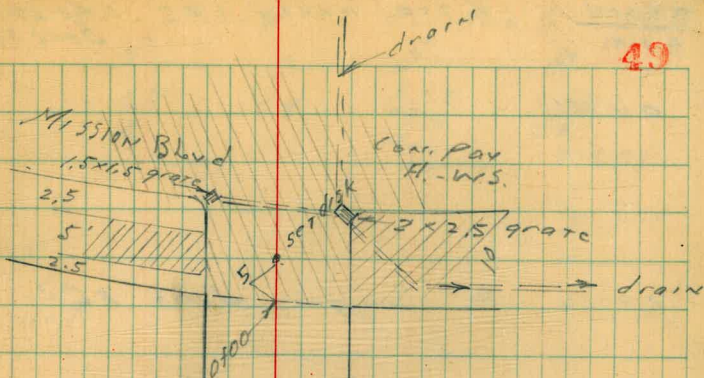
BLK 175

8 8

Art. P.O. asks,
 can this con. pav.
 be removed &
 lowered to drain
 thru low pt?



49

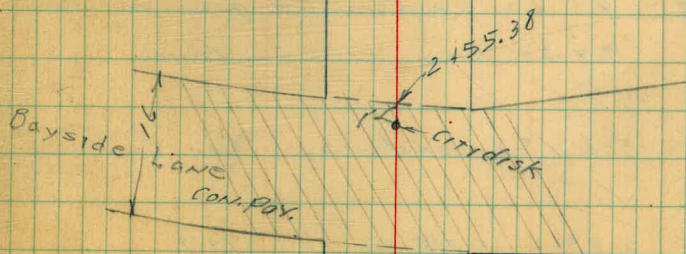


11-5-46

Notes Reduced & Henry

8 8

BLK 176



Indexed
C.S.K.

X sec alley 175 MISSION
Beach

0146

0144 E Singac, dirt FL.

0136.5 W. edge Con. apron da. gar.

0136 9.2 Rt end fence

0135.5 end of Bd. fence

0129 9.6 Rt end picket + Beg. Bd fence

0125

0121 9.2 Lt. SE Cor Bd. gar. + Beg. ^{WIND} PICKET fence

0106

0105 9.1 Lt SW Cor Bd. gar. W. door

0101 9.4 Rt. Beg. picket fence

0100 = E.L. Strandway Con. Pav.

BM.B.P.

2.89

10.08

7.19

Santa Clara Pl.
and Seawall

Lt = N

5.9
6.7
8

6.4

6.25
7.9
Con.
apron

50
6.22
9.8
gar FL

6.0
11.7

5.93

7.8
apron

6.20
7.8
gar FL.

6.9

4.2
8

6.5

4.6
8

6.0

5.1

6.6

4.0
8

6.7

3.4
8

6.5

3.5

6.9

3.2
8

6.06

3.12
8

6.5

3.51

6.95

3.13
8

10.08

0+98 9.5 RT E 20 wide Frame Bldg

0+85 7.4 RT E 10" PP

0+80

+75 9.5 LT SE Con Stucco Bldg

0+64

0+56 Bag Brick wall 9.8 RT

SW Con Stucco Dwelling 9.4 LT
0+55 = E edge apron + gap on RT

0+53 E 3.7 Con. walk on LT.

10.08

LT

E

RT

51

8	1.1	1.1	1.1	1.35	9
$\frac{9.3}{14}$	$\frac{9.0}{8}$	9.0	$\frac{9.0}{8}$	8.75	9.2
				9.8	10
				Bot. door	inside dirt floor

1.9	1.8	1.9
$\frac{8.2}{8}$	8.3	$\frac{8.2}{8}$

2.68
$\frac{6.40}{10}$
end Top Base of wall
Patio inside

2.8	2.6
$\frac{7.3}{8}$	7.5

2.6	3.2	3.68
$\frac{7.5}{8}$	$\frac{6.9}{8}$	6.39
		9.9
		4" walk thru wall
2.68	$\frac{6.40}{10}$	9.8 = Top Con Base of wall

2.58	$\frac{6.70}{8}$	3.36	$\frac{6.72}{10}$
	apron		gap

2.5
$\frac{6.57}{8.1}$

2.45	2.86
$\frac{6.63}{8}$	$\frac{6.22}{10}$
Con apron	9 on fl.

10.08

X Sec alley BLK 17C Mission
Beach

0+45.5 wedge do gar con FL + apron

0+44 7.9 LT end Stucco + SW Cor
wall + SW Frame Bldg

0+41 10 ft NE Cor Brick Bldg

0+34.5 8 LT Beg. Stucco wall

0+33 9 3' Con Walk

0+31 8 LT SE Cor Stucco Bldg

0+25

0+20 10 ft NW Cor Brick Bldg

0+20 E.L. Mission Bldg
8 LT SW Cor
Stucco Bldg

0-10 E CB Line Mission Bldg

T.P. 5.10 4.85 5.33 -0.25
5.08
P.52

LT = N.

E.

Rt = S

53

Indexed
c.s.Ki

-0.2
5.0
8

-0.2
5.0

-0.3
5.1
8

-0.08
4.93
8.9
Apron

13
4.72
11.8
gar.

-0.04
4.89
8.9 = WL + 1' Con
Walk

-0.02
4.87
8

-0.4
5.2
8

-0.4
5.2

-0.4
5.2

-0.23
5.08
7.7
CB

-0.84
5.67
7.7
Par

-0.17
5.62
7.7
Par

-0.85
5.70
8.1
Par.

-0.26
5.11
8.1
CB

-0.21
5.14
8
CB

-0.17
5.62
8
9.97c

-0.10
5.55
7.7
Par.

-0.83
5.68
8
9.97c

-0.33
5.18
8
CB

4.85

0 + 98.5 E 3' CON WALK

0 + 93 9.4 LT Beg. Picket Fence

0 + 89.5 9.3 RT E Low framed structure
7' wide

0 + 73 E Sin 900 dirt Floor

0 + 66 7.5 RT E 10" P.P.

0 + 65 E edge of 900 + apron

0 + 63 9.3 LT. CON, door sill 2.8' wide
to tile floor patio
Bd fence ends here

0 + 54 7.7 LT SE Cor Bldg. + 9.1 LT Beg Bd
Fence

4.85

Lt

E

RT

54

0.50	0.11
5.35	4.96
8.6	11
↑	↑
	walk

0
4.8
9.3

0.2
5.0
8

0.2
5.0

0.2
5.0
8

0.13
4.98
9
apron

.11

4.74
12
900 FL

38

4.47
9.3

4.85

1761,5 E 2,5 Con walk
 1759,5 7,8 RT 10" P.P.
 1759 8,8 RT Beg picket fence
 1757 E 2' con walk

 1755 9,9 LT SW Cor Dwelling + gar.
 1748 E Singar. Con apron 10' wide
 1738,5 8,8 RT end Bd. fence
 1732 E 2' door sill of dwelling

 1728 end apron + Beg Bd fence 8,5 Pn.

 1717 E edge do. gar, apron CONTINUED
 E Ly
 1704 9,7 LT end picket fence
 1700 W edge do. gar + apron

4,85

LT *

-0,53 RT
5,38
 8,7 **55**

-0,91
5,76
 7,5

-0,6
5,4
 8

-0,7
 5,5

-0,93
5,78
 7,8
 apron

-0,77
5,62
 9
 gar

Con Fl.

-0,12
4,73
 11
 sill

-0,45
5,30
 8,5
 apron

-0,23
5,08
 11
 apron +
 walk

-0,4

-0,3

-0,5

-0,5

-0,44

-0,16

E do. gar
dirt floor

5,0
11,3

5,1
 8

5,3

5,3
 8

5,29
 8,5
 apron

5,01
 11
 gar. Fl.

-0,3

-0,4

-0,5

-0,51

-0,10

5,1
 8

5,2

5,3
 8

5,36
 8,6
 apron

4,95
 11
 gar.

4,85

2 + 25 Beg. Lark fence 9.9 LT

2 + 06 end picket fence 9.4 LT
" CON. PATIO also Edge apron + gar on Rt on LT

1 + 91 Beg. picket fence + Cor patio

1 + 89.5 W. edge con. apron + do. gar.

T.P. 4.40 3.86 5.39 - 0.54

1 + 86 E Sim gar Cor. floor 10' wide

1 + 83 8.7 Pt end picket fence

1 + 75 SE Cor. Bd Dwell + gar 9.7 LT

1 + 68.5 E Sim. gar. Con apron = 7' wide

4.85

LT = 11

E

RT = 5

1.1	1.2	1.2	1.1	
<u>5.0</u>	<u>5.1</u>	5.1	<u>5.0</u>	56
9.9	8		8	

0.84	0.8	1.0	1.1	0.18	0.37
<u>4.70</u>	<u>4.7</u>	4.9	<u>5.0</u>	<u>4.64</u>	<u>4.23</u>
9.3	8		7	7.4	10.4
Con				apron	gar FL

0.84	0.8
<u>4.70</u>	<u>4.7</u>
9.3	9.0
Con	Fence

0.18	0.9	0.9	0.9	0.26	0.38
<u>4.64</u>	<u>4.8</u>	4.8	<u>4.8</u>	<u>4.72</u>	<u>4.24</u>
9.3	8		7	7.4	10.3
gar FL				apron	gar. FL

3.86

0.18
<u>5.63</u>
9.2

0.31	0.59
<u>5.16</u>	<u>5.54</u>
9.7	9
gar	apron

4.85

check to orig. BM, 106 7.18 7.19
0.01

T.P. 7.60 8.24 3.22 0.64

2+55.38 W.L. Bayside Line

2+43 E Six. gars. + 8' wide Cen. apron

2+36 E 2' Cen. walk

2+35 end last fence 9.86

3.86

L7-N

±

Px 57

1.01	1.13	.98
4.87	4.99	4.84
8	8	8
Par	Par	Par

.86	0.99	1.1	1.1	1.1	1.5
4.72	4.85	5.0	5.0	5.0	5.4
11.1	8.8	8	8	8	15
gar.	apron				

1.8
4.94
10.7

3.86

Proposed Sewer Line Wood St.
Pringle St to Existing Man Hole North
of Mission Hills Blvd

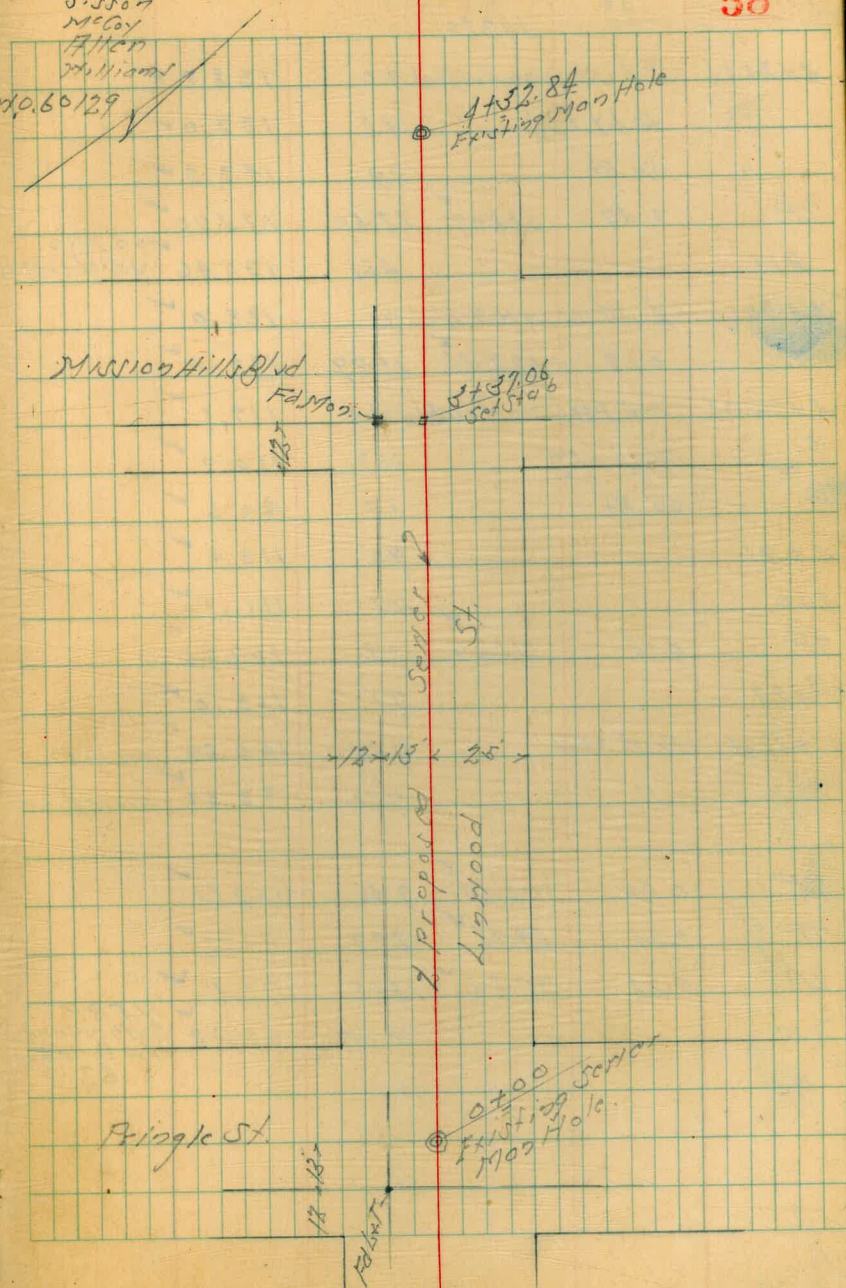
BM	0.45	196.91	196.46	13' Lt Pringle + 50'
TP	0.19	184.50	12.80	184.11
TP	0.35	171.62	13.03	171.27
BM			7.30	164.53 13' Lt Pringle + 51' Wood
0+0	Existing Man Hole Pringle + Linwood		6.08	165.54 27 Rim
"			10.20	161.42 Floor Line
+25	1/4 Pringle + 1/4 Parry		6.56	165.06
+50			7.1	164.5
+70			8.0	163.6
+04	4 1/2 Lt of 1/2 = Fly 3 Car Garage Apt. Above		9.98	161.64 on Conc Floor
+50			8.4	163.2
"	40' Lt of 1/2 = Bldg Line to South		14.5	157.1
+2+0			7.7	163.9
"	45' Lt of 1/2		15.3	156.3 on Basement Floor
+08	38.5 Ft of 1/2 = 1/2 + 1/4 Apartments		6.13	165.49
+40			7.8	163.8
TP	0.30	159.10	12.82	158.80
+60			1.9	157.2
"	50' Lt of 1/2		7.0	152.1
+80			6.6	152.5
+70			12.2	145.9
"	50' Lt of 1/2		17.1	142.0
TP	0.83	147.20	12.72	146.37
+18			8.0	139.2

June 18-47
Sisson
McGoy
Allen
Williams

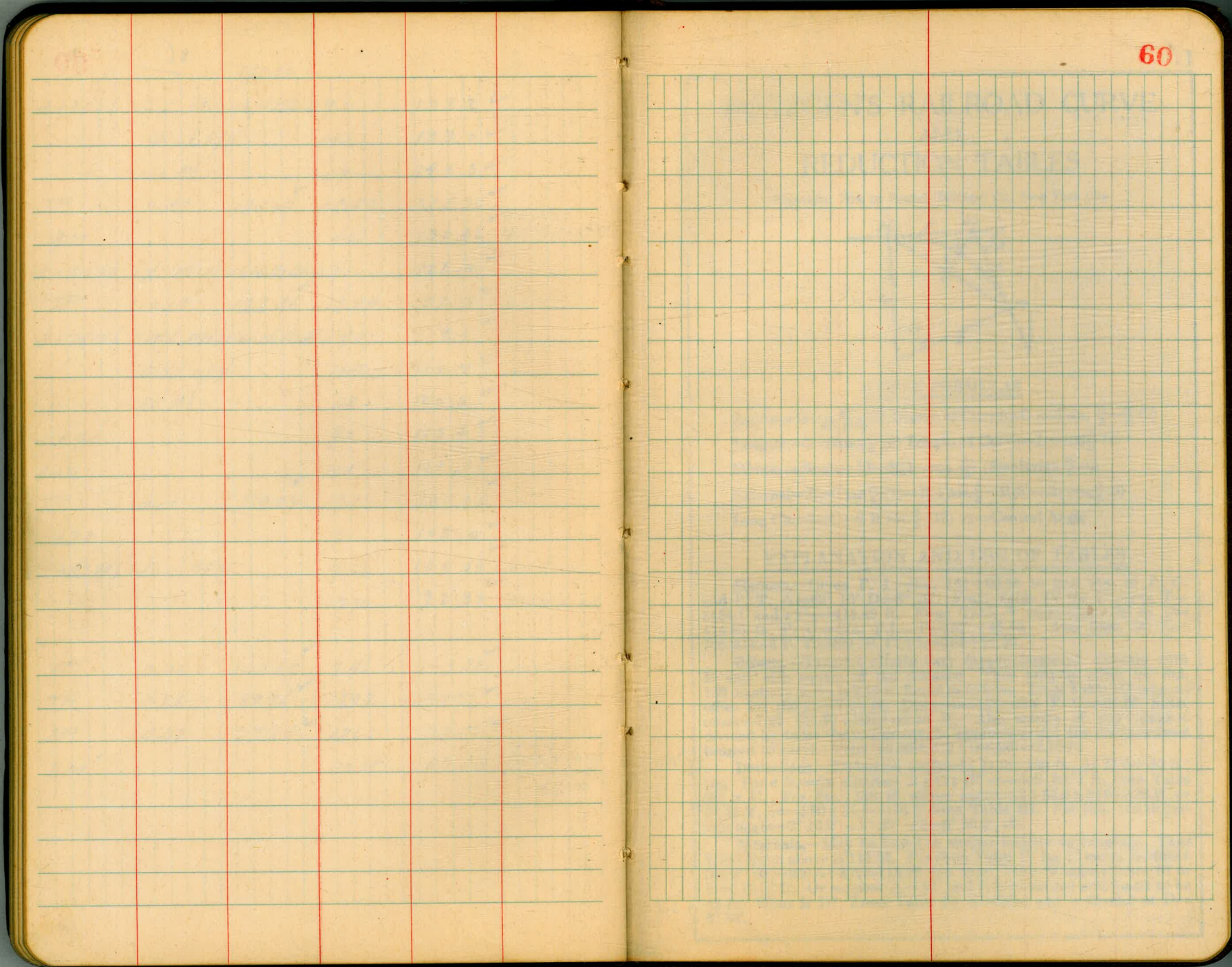
110.60/29

Indexed
C.S.K.

58



14720			
3+25.06	= S-L Mission Hills Blvd	9.0	138.2 ✓
"	50 Lt of 1/2	14.2	133.0 ✓
"	50 Rt " "	3.9	143.3 ✓
TP	0.37	135.07 ✓	12.50 134.70 ✓
BM		4.61	130.46 ✓ on Mon 13270/313706
3+50.06	= 1/2 Mission Hills Blvd	7.1	128.0 ✓
TP	0.18	122.36 ✓	12.89 122.18 ✓
3+75.06	= 1/2 Mission Hills Blvd	8.3	119.1 ✓
"	50 Lt of 1/2	11.7	110.7 ✓
"	50 Rt " "	1.8	120.6 ✓
3+90		9.0	113.4 ✓
4+0		11.5 ✓	111.1 ✓
TP	0.14	110.09 ✓	12.41 109.95 ✓
+23		7.1	103.0 ✓
+32.89	= Front MH	9.55	100.54 ✓ on Rim
"	" " "	17.70	92.39 ✓ Flat Line
TP	0.06	102.69 ✓	7.46 102.63 ✓
TP	0.24	89.96 ✓	12.97 89.72 ✓
TP	0.22	77.53 ✓	12.65 77.31 ✓
BM		10.15	67.38 ✓ NERP Suberland #20 Sottafre 67.19



1. V / V 2

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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