

1728

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.
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1728

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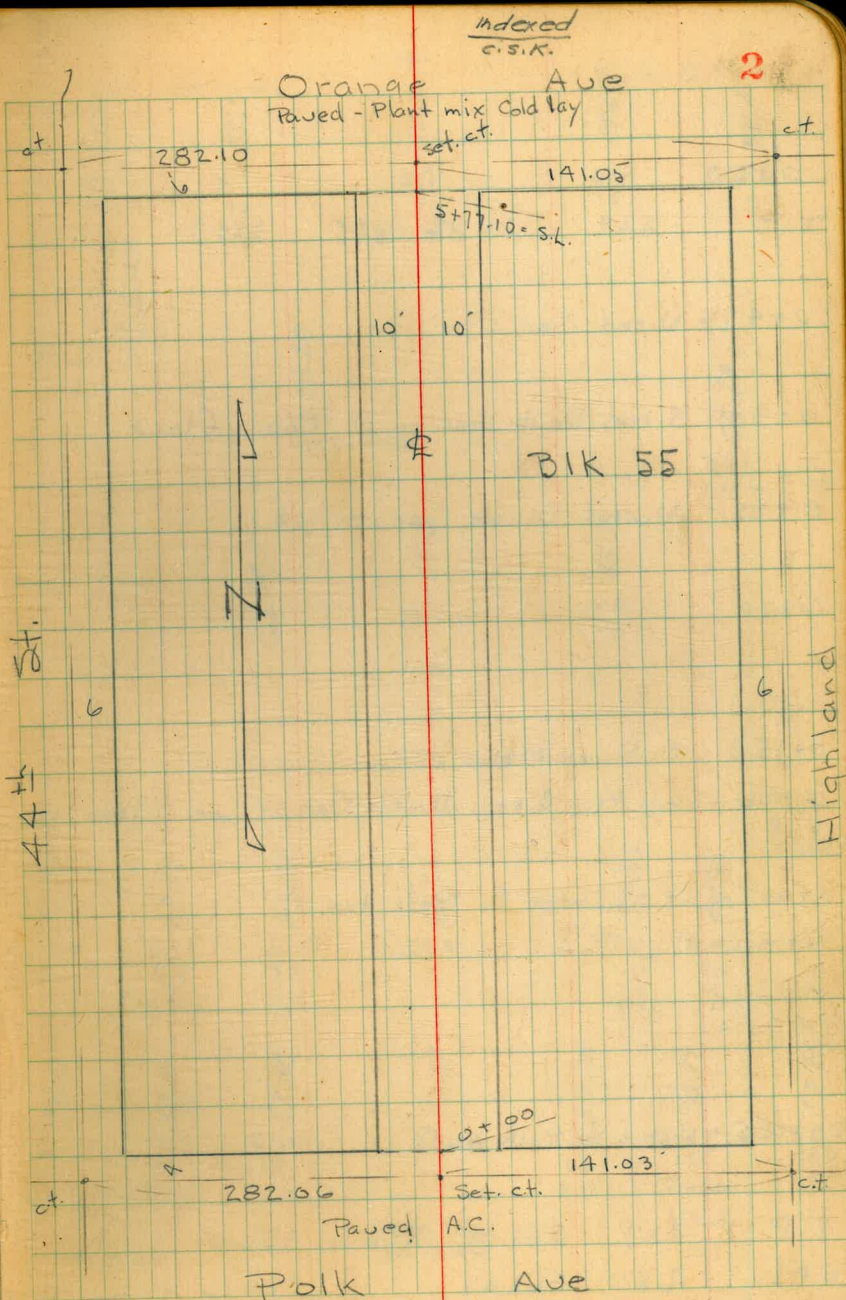
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HIGH ABILITY

X-Sect. 20' Alley in Blk 55 -
Fairmount Add. Map 1035

7-10-46

Osborne
McCoy
Hardin
Widdel



check B.M. 8.13 354.18 354.16

5+91.10 = S. cb. Line Orange

T.P. 6.12 362.31 5.70 356.19

5+77.10 = S.L. Orange Ave. - 10' Lt. = end 2' Conc. walk
Joins cb. for grade

5+76 - 9.3 Rt. = tel. pole

5+61 = Break in grade in walk on Lt.
under house is lower

5+55 - 12.1 Rt. = Vent. in Foundation of House - Ground

5+50

5+34 - 10' Lt. = beg. 2' N. + S. Conc. walk - slab on S. end

5+31 - Sing. Gar. on Lt. - Conc. floor + apron

5+27 - Sing. Gar. on Rt. - Conc. floor + apron

	Lt.	Rt.
	55.96	
	5.93 got	
	5.85 Top cb 2 Rad. Ret	
	56.04	
	6.38 10 got	
	55.51	
	6.54 got	
	55.35	
	6.69 10 = got	
	56.20	
	6.18 10 cb.	
	55.91	
	7.32 5.00 got	
	54.59	
	362.31	
	56.71	
	5.18 Top cb at end Alley Ret.	
	56.33	
	5.56 9.8 got Pave rolled up to Curb - rod = Ave. pave Cold Lay.	
	56.49	
	5.70 got	
	56.28	
	9.61 9.9 Pave rolled. rod = Ave.	
	56.44	
	9.9 10 cb.	
	57.23	
	4.66 12.1 Bot. of Vent. on Conc.	
	57.1	
	4.8 10 of walk	
	57.09	
	4.80 10 walk	
	56.92	
	4.97 9.5 Apron	
	57.08	
	5.21 14 Apron	
	56.68	
	5.18 7.2 Floor	
	56.91	
	361.89	

0+51 - 6.8 Rt. = Tel. pole.
 0+50 - 5.6 Lt. = Pole + 5.8 Rt. = end Hedge (w. edge)

0+36 - 6.8 Lt. = end 28 Slab.

0+31 - 8.1 Lt. end 16 Walk + req. 2.8 Conc. Slab. for step to Med. frame House

0+15

T.P. 5.78 390.94 3.97 385.16

0+01 - 4' Lt. = Gas Co. Gate Cover

0+00 = N.L. Madison - on edge A.C. pave + 7.8 Lt.
 = req. E. edge 16 Conc Walk + 5.6 Rt. = w. side 4.5' Cypress Hedge 6' High

Note: Alley Ret. are in poor Concl. should be repaired
 Paving
 0-12 = N. cb. Line Madison Ave. on A.C. Pave

B.M. 4.42 389.13 5.80 384.71
 4.72 390.51 385.79 S.E. 32nd Adams

in B.M. - Books 385.80 wherry -

9

Lt. = W. Rt. = E.

385.6	385.9	386.0	386.3	
5.3	5.0	4.9	4.6	
2.0	7.5		7.5	
387.60	385.98			
3.34	4.96			
Floor House	6.8 = Cor. Slab.			
386.99	385.99			
4.95	4.95			
8.1	6.8 = edge slab			
edge walk				
385.82	385.5	385.6	385.7	
5.12	5.4	5.3	5.2	
8.1	7.5		7.5	
edge walk				
		390.94		
		385.20		
		3.93		
		4 = Top Cover		
385.48	385.39	385.25	385.10	385.12
3.65	3.74	3.88	4.03	4.01
7.8	7.2	7.2		7.4
edge walk				
389.36	385.13	384.66	384.67	384.61
4.27	4.00	4.47	4.46	4.52
4.0	7.5	7.5		7.5
gut.	Top cb.	gut.	gut.	Top cb.
				2 Rad. Ret
				389.94
				4.69
				4.0
				gut.
				389.13

3+00

2+50

2+49-56 Lt. = P. pole + 6.9 Rt. = Tel. pole
2+31-8.3 Rt. = N. end Conc Slab + S. end 2 Car Gar.
opening to S. on slab. and drive out to 32nd

2+00 - 8.3 - Rt. = end 6' slab + 8.7 Rt. = S. end 21' wide Conc slab

1+85 - 8.3 Rt. = S. end 6' Conc. Slab.

1+50 - 7.4 Lt. = end fence + 7' Rt. = Tel. pole

1+49 - 56 Lt. = P. pole

1+00 - 7.4 Lt. = beg. pickett fence

0+90 = 8.4 Rt. = E. of back of good Gar. or house

0+73 = 8.2 Rt. = N. end shed.

0+51 - 8.2 Rt. = S. end shed or house

384.7 Lt
6.2
20

384.7
6.2
7.5

384.6
6.3

384.7
6.2
7.5

Rt. 384.9
6.0
20

10

384.9
6.0
7.5

384.6
6.3

384.9
6.0
7.5

384.7
6.2
30

385.47
5.47
8.3

385.39
5.55 = on slab.
21.6 = E. Door. Gar.

385.9
5.0
30

385.2
5.7
7.5

385.1
5.8

385.1
5.8
7.5

385.33
5.61
8.3 = edge
6' slab

385.24
5.70
8.7 = edge
4.9 slab

385.28
5.66
30
on slab

385.8
5.1
30

385.5
5.4
7.5

385.5
5.4

385.5
5.4
7.5

385.4
5.5
30

385.48
5.51
8.3 = slab

385.9
5.0
30

385.7
5.2
7.5

385.7
5.2

386.0
4.9
7.5

386.1
4.8
20

386.37
4.57
8.4 = Floor Elev.

387.23
3.71 = floor.
8.2

390.94

Lt. = Rt.

386.2	385.8	385.3	385.3	385.0
3.8	4.2	4.7	4.7	5.0
2.0	7.5		7.5	2.0
385.7	384.9	384.9	385.0	384.9
4.3	5.1	5.1	5.0	5.1
3.0	7.5		7.5	2.0
387.9				
2.97 = floor elev.				
386.2				
12.9 = bot. of vent.				
383	385.0	384.9	384.9	
12.9 = vent.	5.0	5.1	5.1	
	7.5		7.5	
385.29				
4.80				
8 = edge walk				
385.11				
4.93				
8.2				
edge walk				
385.22				
1.82				
7.8 = edge walk				
381.07	386.37			
2.97	3.17			
10.3	7.2 = edge			
Floor Elev	Top porch	390.04		
384.9	384.8	384.7	384.8	
6.0	6.1	6.2	6.1	
7.5	390.94	7.5	2.0	

5+02 - 7.3 Rt = beg. pickett fence
 5+00 - 7.4 Lt = end fence
 4+52 - 6 Lt = P. pole + 7.7 Lt = beg pickett fence
 4+51 - 6.6 Rt = Tel. pole
 4+50

4+26 12.9 Lt = E back of large Stucco Court

4+16 - 12.9 Lt = E Vent. in Conc found. to above ct.

4+00 - 7.4 Lt = end board fence

3+94 - 8 Lt = end slab walk

3+78 - 7.4 Lt = end lath + beg. board fence

3+59 - 7.8 Lt = bot. steps + beg. 2' Conc. slab. walk along bid.

Apt. house
 3+56 = 7.8 Lt + 3 x 2.5 Conc. porch to back door 2 story stucco
 T.P. 5.48 390.04 6.38 384.56

3+51 - 5.7 Lt = P. pole

3+50 - 7.3 Lt = beg. lath fence + 6.8 Rt = Tel. pole

T.P. 5.25 392.41 2.88 387.16

6+50.61 = sil. of E.+W. 15' Alley = end.

6+50 = 6.9' Rt. = end board fence

6+30

6+27 = 6.3 Rt. = Tel. pole

6+01 = 5.6 Lt. = P. pole

6+00 = 7.6 Rt. = beg. high board fence

5+52 = 7.8 Rt. = end fence

5+50

5+29 = N. end 2' walk on Lt.

5+21 = N. end Gar. + beg. 2' Conc. walk joins apron.

5+05 S. end Doub. gar. on Lt. Conc. floor + apron

Lt. E Rt.

386.9	386.6	386.6
3.1	3.4	3.4
7.5		7.5

386.2	386.2	386.2
3.8	3.8	3.8
7.5		7.5

386.2	386.9	386.2	385.7	385.6
3.8	3.6	3.8	4.3	4.4
2.0	7.5		7.5	2.0

386.0	385.9	385.6	385.6	385.7
4.0	4.1	4.4	4.4	4.3
2.0	7.5		7.5	2.0

385.77
4.27
9.8 = end walk

385.98	385.81
Floor 4.06	4.23
11.8	9.8 = apron + walk
385.91	385.77
4.13	4.32
11.8	9.8 = apron
Floor	
Gar.	

390.04

2+20 - 8.2 Rt. = end of Conc. Slab. Drive
 2+05 - 7.8 Rt. = N.E. Cor Sing. Gar. opening to E.
 Conc. floor + Slab drive to 32nd

2+00

1+81 - 8.2 Rt. = \pm shed on back of Gar. Conc. floor

1+50

1+33.1 - 0.6 Lt. = \pm Sewer M.H.

1+32.72 = Int. Φ + Φ of N. & S. Alley

1+27 - 5.7 Rt. = \pm P. pole

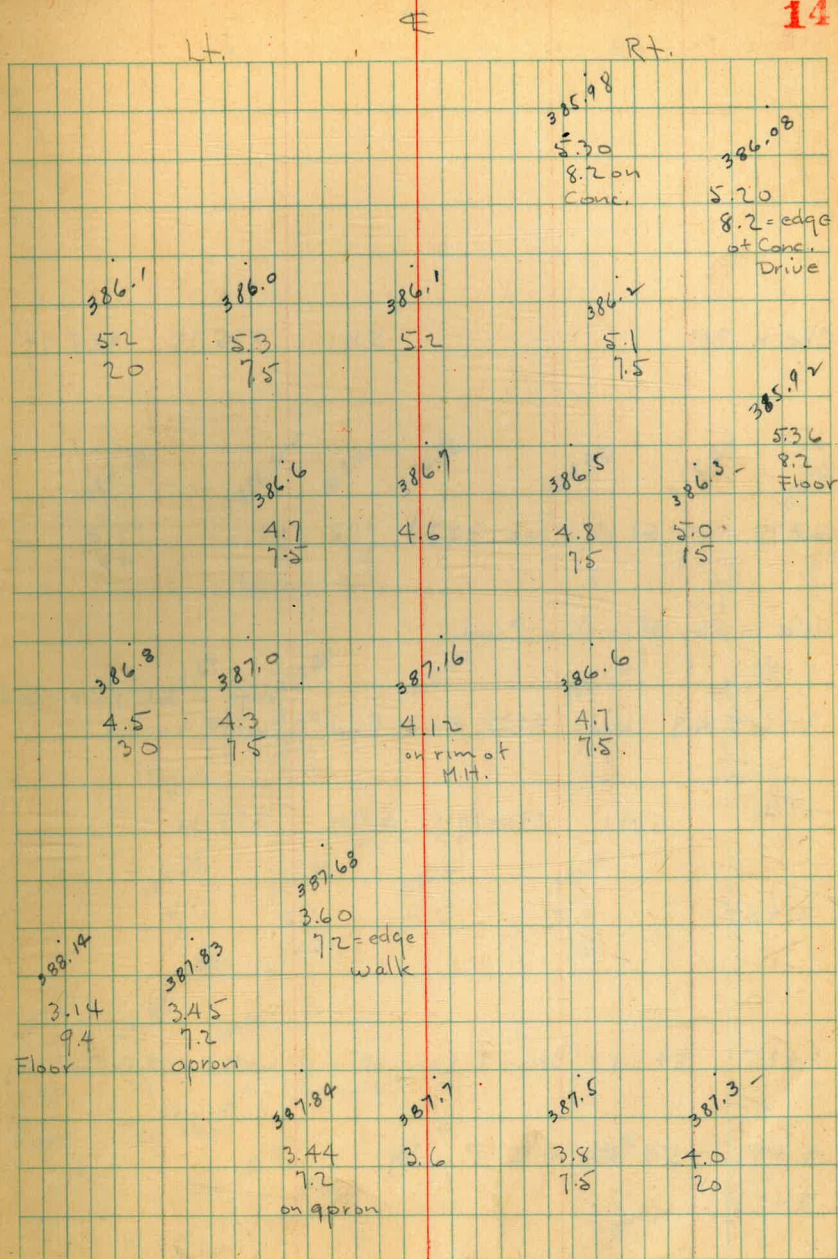
1+09 = 7.2 Lt. = Fly. 2'5" Conc. walk - N & S. - Joins apron

1+06 = N. end Gar. on Lt.

1+05 - 6.7 Rt. = Dead man

1+00

0+99 - 5.7 Rt. = Dead man for Pole



check B.M. 5.01 385.78 385.79 ✓

2+77.43 = W. cb. Line 32nd

Curbs in Alley Ret. in fair Cond.

2+65.43 = W.L. 32nd + End 2' walk on Lt. edge of A.C. pave-good

T.P. 5.41 390.79 5.90 385.38

2+55

2+35 - 9.4 Lt. = Req. 2' Conc. E+W. Walk + 3.5' Conc. steps
to house

2+32 - 5.9 Rt. = E P. pole

2+25

Lt.

E

Rt.

15

384.90	385.62	385.00	384.96	384.92	385.40	384.78
5.89	5.17	5.79	5.83	5.87	5.39	6.01
5.0	7.5	7.5		7.5	7.5=Top	5.0
	Top cb.	gut.		gut.	cb. 2' Rad.	gut.
					Ret.	

385.59	385.80	385.37	385.54	385.76
5.20	5.39	5.34	5.17	5.03
7.6	7.6		7.9	7.9
Top cb.	gut.		gut.	Top cb.
				end Ret.

385.57	385.6	385.8	385.9
5.71	5.7	5.5	5.4
9.3	7.5		7.5
edge walk			

387.51	386.98	385.81
3.77	4.30	5.47
13	13	9.4 - edge walk
Floor house		
	Top. steps	

385.8	385.9	385.8
5.5	5.4	5.5
		7.5

391.28

Levels on Gresham

Garnet N.Ly.

N.O. #210

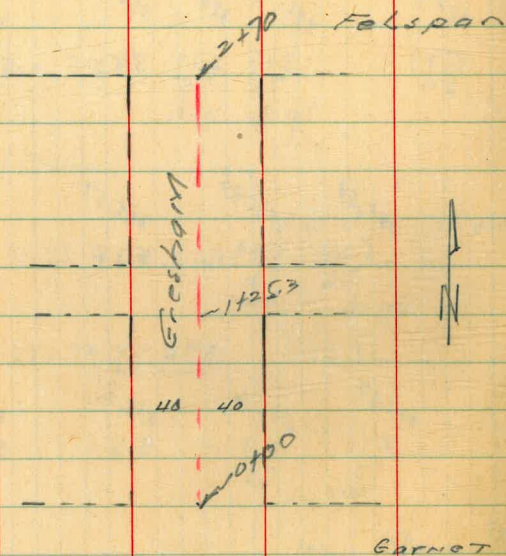
C. Moore
Santamoya
Hardie
Visham
9-30-46

indexed
C.S.K.

16

For possible curb + walk
on E. Side

Levels p. 17



Hot! here's a tough one!

1+25.7 S. edge and N. edge Con. apron

and Back Bldg. 49

4.5 3.14 2.93
20 33 40
 Con. apron

1+15 E doorway

5618 5648
3.27 2.97
33 40
Con. apron FL. EL.

1+06 S. edge Con. apron

5609 5644
52 3.36 3.01
20 33 40
 Con. apron

59.45

59.45

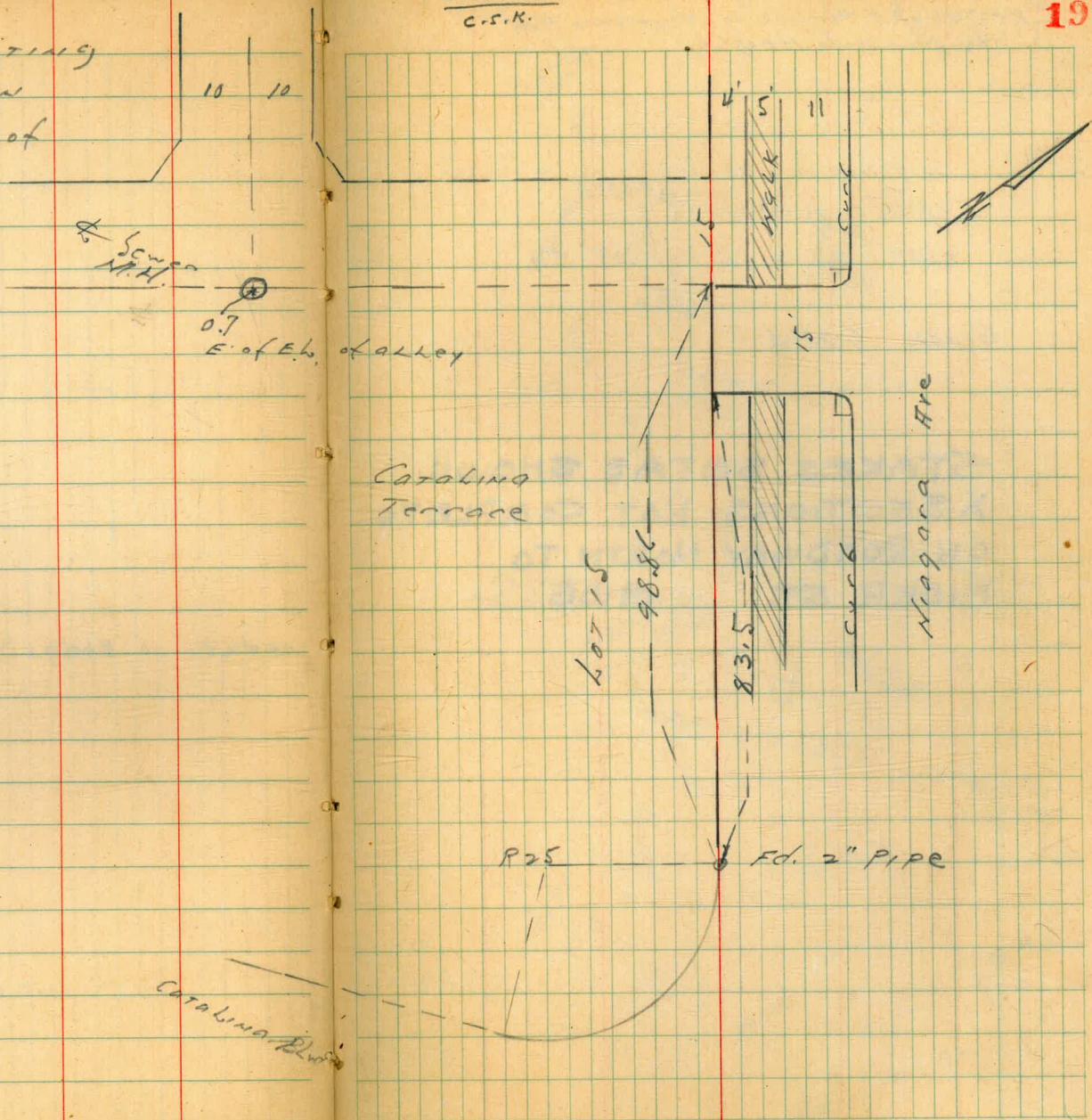
57

Rt.

18

Location of Existing
alley Returns on
Niagara wly of
Catalina Blvd.

C. Moore
Sons of Meyer
Hardin
W Moore
8-30-46



Jarvis st. Sections

B.M.	0.70	41.97	41.27	SE. 7 th Propriet. Inglens + Willow. 1177-63
Levels around Ret "A" - see sketch - 40.8 around				
From P.C. to E.L. of willow - 4 parts 10.2 each				
P.C. = E. cb. line Willow.	Top cb.	4.00	37.97	Top cb.
	gut	4.83	37.12	gut
10.2	Top.	4.32	37.65	
	gut	5.17	36.80	
20.4	Top	4.76	37.21	
	gut	5.58	36.39	
30.6	Top	5.03	36.92	
	gut	5.72	36.25	
40.8 = end of cb. = E.L.	willow Top	5.46	36.51	
	gut.	6.22	35.75	

Levels around Ret. "B" - 40.8 around - 4 parts - 10.2

P.C. = E. cb. line of	willow Top	5.40	36.57
	gut.	6.23	35.72
10.2	Top.	5.45	36.52
	gut.	6.20	35.77
20.4	Top	5.54	36.23
	gut	6.26	35.71
30.6	Top	5.64	36.33
	gut.	6.45	35.52

9-24-46
70.

41.97

40.8 = end of cb at E.L.	- Joins inlet curb.	
Top	5.86	36.11
gut.	6.74	35.23

X- Sect of Jarvis - 70' wide - 18' cbs.

Also for Storm Drain

0+80

0+43 - 34.6 Rt = beg. wire fence

0+35

0+29 - 20.8 Lt = Φ Tel. pole

0+16.7 - opp. end of 36" steel pipe

0+05

0+00 = E.L. of Willow = edge of Pave - Note face of Inlet curb is 0.3 E of E.L.

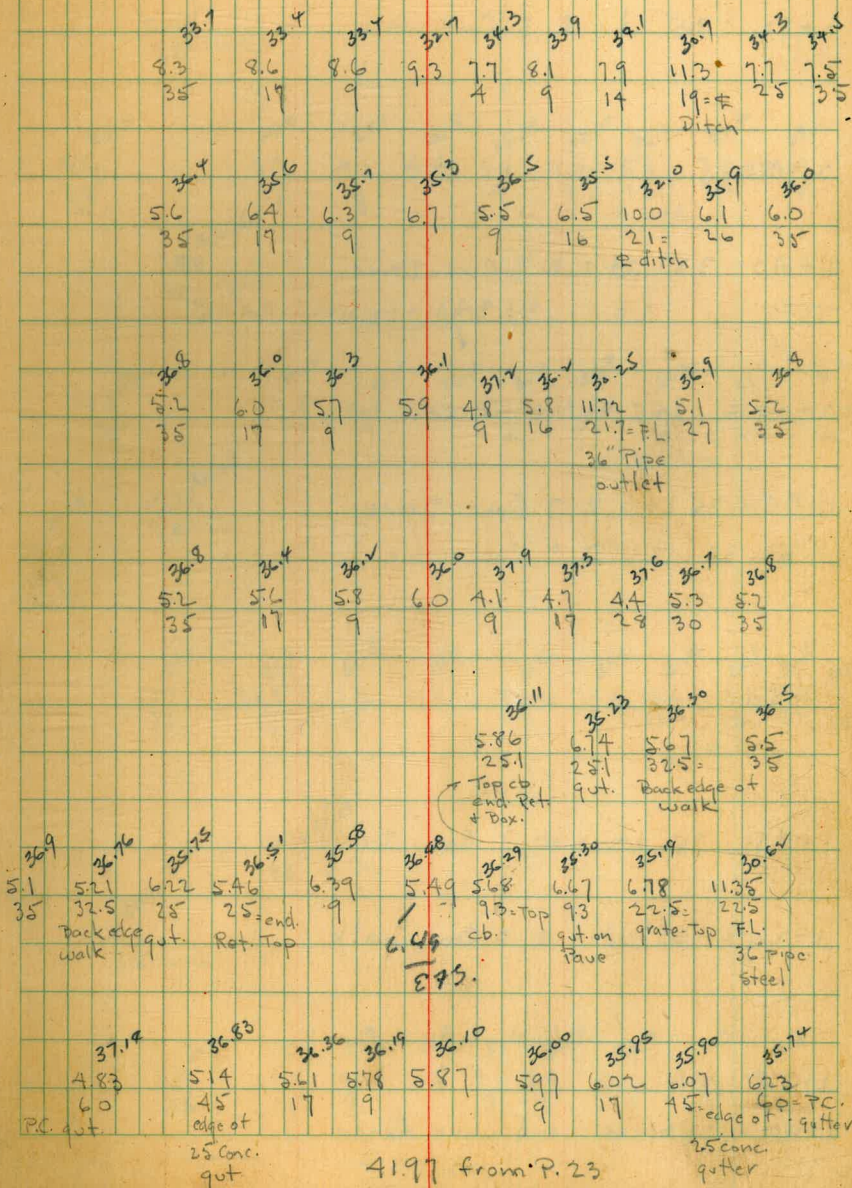
0-18 = E. curb line of Willow - on A.C. Pave

Jarvis St.

Lt. = N.

E

Rt. = S - 24



2+72 - 35' Lt. = 3' Conc. walk

2+50

2+40 - 35.1 Lt. = 7' Conc. Drive

T.P. 12.9 31.24 12.02 29.95

2+00 - 24.5 Rt. = P. pole

1+95 - 35' Lt. = 7' Conc. Drive

1+75 - 35' Lt. = 3' Conc. walk

1+50

1+45 - 35' Lt. = 7' Conc. Drive

1+24 = 35' Lt. = 3' Conc. walk

1+20

1+00 - 35.2 Rt. = end wire fence

Jarvis St
Rt. 25

Lt. =
26.23
5.01
35' walk

27.0 27.0 27.1 26.8 28.4 27.7 25.4 27.4 28.5
4.2 4.2 4.1 4.4 3.0 4.0 5.8 3.8 2.7
3.5 17 9 4 4 9 18 23 3.5

27.76
34.8
35.1 - Dr.

31.24 ✓

29.4 29.4 29.4 28.7 30.1 29.8 25.9 27.9 30.0
12.8 12.8 12.8 13.3 11.9 12.2 15.1 12.2 12.0
3.5 17 9 13.3 4 9 18 22 3.5

30.23
11.74
35' walk

31.1 31.1 30.8 30.4 31.8 31.6 31.6 28.9 31.5 31.7
10.9 10.9 11.2 11.6 10.2 10.4 10.4 13.1 10.5 10.3
3.5 17 9 11.6 3 9 11 18 27 3.5

31.18
10.79
35' on Dr.

31.91
10.06
35' walk

32.1 32.0 31.8 31.5 32.9 33.4 30.0 32.7 32.8
9.9 10.0 10.2 10.5 9.1 8.6 11.0 9.3 9.7
3.5 17 9 3 9 18 24 3.5

41.97 ✓

4+03 - 35' Lt = Φ 3' Conc. walk.

4+00

3+70.08 = E.L. Evergreen

3+58 = opp. Conc. box = 12x12 in Ditch. dont know what is in it - parallell to Evergreen

3+52.08 = E. cb.

3+35.08 = Φ Evergreen

3+18.08 = W. cb. of Evergreen

3+00.08 20.3 Lt. = Φ Tel. pole = W.L. Evergreen

Jarvis 26

18.71	Lt.	Φ	Rt.
12.53 35 on walk	15.6 12.6 35	19.0 12.2 17	19.7 12.0 9
			19.7 12.0 9
			20.1 11.1 4
			16.9 14.3 13
			21.3 9.9 22
			21.9 9.3 35
			Φ Ditch
19.44	20.9	22.0	21.8
11.8 50	10.3 35	9.2 17	9.4 9
			21.9 9.3
			22.7 8.5 6
			18.9 12.3 15
			22.6 8.6 24
			23.1 8.1 35
			Φ Ditch
			20.60 10.64 10-Top box
			20.59 10.65 20-Top box
22.7	23.7	23.1	23.1
8.5 35	8.0 17	8.1 9	8.1
			23.8 7.4 9
			21.8 9.4 18
			Φ Ditch
			24.1 7.1 22
			24.7 7.0 35
23.1	23.9	23.8	23.8
8.1 35	7.3 17	7.4 9	7.4
			25.6 5.6 9
			22.3 8.9 18
			Φ Ditch
			24.8 6.4 22
			24.7 6.5 35
23.7	24.4	24.7	24.7
7.5 35	6.8 17	7.0 9	7.0
			24.4 6.8 3
			23.1 8.1 9
			23.1 8.1 18
			Φ Ditch
			24.9 6.3 22
			25.0 6.2 35
24.6	25.1	24.9	24.7
6.6 35	6.1 17	6.3 9	6.5
			24.9 6.3 5
			24.5 6.7 9
			23.8 7.4 18
			25.8 5.4 22
			26.3 4.9 35
			Φ Ditch

31.24 ✓

5+30 - 35.1 Lt. = \$ 8' Drive - double 2.5' Conc. strips

5+20 - 20.2 Lt. = \$ Tel. pole

5+17 - 12.6 Rt. = inlet 24" steel culvert - under dirt Drive ^{Poor Cond.}

5+11 - 35.3 Lt. = \$ 8' Drive - double 2.5' Conc. strips

5+00 Level out
4+91 - 35.2 Lt. = \$ 3' Conc. walk

4+65

4+54 - 35.3 Lt. = \$ 3' Conc. walk

4+35

4+29 - 35.1 Lt. = \$ 8' Dr. = Double 2.5' Conc. strips

4+20 - 21.9 Rt. = \$ P. pole

1.79 21.07 ✓ 11.66 19.58

B.M. on S.E. 7' Mon. 8.39 22.85 ✓

Lt.	\$	Rt.
14.98	15.0	15.4
6.09	6.1	5.7
35.1	20	17
on Dr.		
	15.3	15.8
	5.9	5.3
	9	9
	15.9	15.5
	5.2	5.6
	17	35
		16.39
		416.8
		50 = Conc.
		floor Sing. Grav.
	15.6	15.9
	5.5	5.2
	4	9
		15.6
		15.79
		15.7
		5.4
		5.4
		35
		12.6
		19
		Philippa
15.49	15.6	15.6
55.9	15.6	16.3
35.3	16.2	16.0
	16.4	16.1
	14.7	16.1
	5.1	5.0
	4.7	6.7
	4	9
		13
		Ditch
		5.0
		16.1
		5.0
		35
	16.1	16.4
	5.0	4.3
	35	17
		16.8
		16.8
		4.3
		9
		16.6
		17.0
		4.1
		3
		4.5
		9
		16.6
		15.3
		5.8
		15
		Ditch
		4.1
		19
		17.0
		3.9
		35
		17.1
		17.1
		17.6
		17.6
		17.0
		16.0
		17.7
		3.4
		22
		Ditch
		18.1
		2.9
		35
		17.36
		37.1
		35.1
		on Dr.
		21.07 ✓
		31.24

6+88.27 = W. cb. locust

6+75 = 31.3 Rt = E P. pole

6+70.27 = W. h. locust

T.P. 2.32 13.52 9.87 11.20

6+54 - 35' Lt. = 3 Conc. walk

6+50

6+29 - 35.1 Lt. = 8' Dr. - 2.5 Conc. strips

6+15 - 11.9 Rt. = outlet of 24" Culvert

6+11 - 35.1 Lt. = 8' Drive - double 2.5 Conc. strips

6+00

5+91 - 35' Lt. = 3' Conc. walk

5+71 - 24.4 Rt. = P. pole

5+60

5+53 - 35' Lt. = 3' Conc. walk

Lt.

R

Rt.

10.8	10.9	11.0	11.0	11.8	11.3	9.9	11.3	10.9
2.7	2.6	2.5	2.5	1.7	2.2	3.6	2.2	2.6
35	17	9		3	7	10	17	35
						Ditch		

11.3	11.3	11.4	11.4	11.6	11.4	10.3	11.4	11.4
2.2	2.2	2.1	2.1	1.7	2.3	3.2	2.1	2.1
35	17	9		3	9	11	17	35
						Ditch		

11.77
9.30
35
on walk

11.8	11.9	11.9	11.8	12.1	11.3	10.8	11.9	11.9
9.3	9.2	9.2	9.3	9.0	9.8	10.3	9.2	9.2
35	17	9		3	9	14	17	35
						Ditch		

8.57
35.112.59
8.48
35.1 on Dr.

12.8	13.5	12.9	10.89	12.9	12.9
9.3	7.6	8.5	10.18	8.2	8.2
	3	9	11.9	17	35

13.45
7.62
35
walk

13.0	13.3	13.3	13.4	13.8	13.3	13.4	13.3
8.1	7.8	7.8	7.9	7.3	7.8	7.9	7.8
35	17	9		3	9	17	35

14.4	14.5	14.6	14.4	14.4	14.5	14.5
6.9	6.6	6.5	6.7	6.7	6.6	6.6
35	17	9		9	17	35

14.38
6.69
35 on walk

21.07

9+65 - 35.5 Rt. = N.W. Cor. of ext. of House
 9+55 - 10.3 Rt. = Outlet of 24" steel Culvert (changes
 in there somewhere)

9+52

9+48 - 34.7 Rt. = Φ Sing. Gar. - Conc. floor + Apron9+41 - 23.8 Rt. = Φ P. pole + 18.5 Lt. = Φ P. pole9+35 - 34.5 Rt. = Φ 8.7 Conc. Dr.9+32 - 35' Lt. = Φ 9' Conc. Dr.

9+20

9+16 = 11.1 Rt. = inlet 18" RC. Culvert under dirt Drives

9+06 - 35' Lt. = Φ 3' Conc. walk9+05 - 33.4 Rt. = Φ 3.5' Conc. walk

9+00

Lt.

 Φ

Rt.

6.8 1.3 6.0¹ 1.5 1.3 6.9 6.7
 6.7 6.2 8.45 6.0 6.2 6.7 6.8
 8 10.3 14 17 25 35
 F.L. 24" pipe

1.1 6.6 6.6 6.9 7.3 1.7 1.3 6.9 6.7
 6.4 6.9 6.9 6.6 6.2 5.8 6.2 6.7 6.8
 35 17 9 5 14 17 27 35

6.74 6.94
 32.4 = edge Apron
 34.7 = floor.

7.18
 6.34
 35 = Dr.

6.31 1.21
 34.5 =
 Dr.

6.9 6.8 6.8 6.6 6.7 1.6 1.7 1.7
 6.6 6.7 6.7 6.9 6.8 5.9 6.3 6.3
 35 17 9 3 9 17 35

1.0 6.8 6.8 6.7 6.7 1.4 5.6⁴ 1.3 1.3 1.7
 6.5 6.7 6.7 6.8 6.5 6.1 7.88 6.2 6.2 6.3
 35 17 9 3 7 11.1 15 17 35
 F.L. 18" Pipe

7.7²
 5.80
 35 on walk

7.46
 6.26
 33.4 walk

1.7 1.0 1.0 6.9 7.5 1.6 6.0 1.5 1.1 7.5
 6.5 6.5 6.5 6.6 6.0 5.9 7.5 6.0 6.7 6.0
 35 17 9 3 9 11 13 17 35

 Φ ditch

13.52 f

10+40.70 = w.l. Posecrans

Top of ♀ Grate on Inlet on Lt. 6.63 4.26
See sketch - 10' opening

F.L. of Box + 18" Conc. pipe 8.99 2.80

10+13.70 = Edge of Pavc + P.C. 43' Rad. Curb Ret.

10+10

T.P. 5.77 10.89 8.40 5.12 ♀ Inlet.

9+90

9+79 - 35.5 Rt. = N.E. Cor. ext. of House

9+75

Lt.					Rt.				
5.9	5.52	4.89	4.94	4.99	5.00	4.87	4.68	4.44	5.05
5.0	5.57	6.00	5.95	5.90	5.89	6.02	6.21	6.45	5.94
35	26.6	26.6	17	9	9	17	26.5	26.5	35
		Top of cb. on Ret.	got				got	Top of cb. on Ret.	

3.00
7.89
25.2 =
Top of wier - See Detail

6.4	5.32	4.60	4.82	4.87	4.69	4.36	4.97	5.11	0.35
4.5	5.57	6.23	6.07	6.02	6.20	6.53	5.92	5.78	10.54
35	17	17	9	9	9	17	17	25.2	25.2
	Top of cb. end	got.				got.	Top of cb.	♀ Inlet	F.L. of box at curb

7.5	5.9	4.9	5.1	5.2	5.0	4.9	3.5	3.5	6.2
2.4	5.0	6.0	5.8	5.7	5.9	6.0	7.4	7.4	4.7
35	20	17	9	9	9	17	23	25	30
							In Ditch		

10.89 ✓									
7.2	6.7	5.4	6.0	6.3	6.2	6.8	3.8	6.5	4.5
6.3	6.8	8.1	7.5	7.2	7.3	6.7	9.7	6.9	7.0
35	17	11	6	9	9	14	17 =	25	35
							In Ditch		

6.8	6.4	5.8	6.6	6.7	6.7	7.1	3.9	6.1	6.5
6.7	7.1	7.7	6.9	6.8	6.8	6.4	9.6	6.8	7.0
35	17	12	5	6	6	12	17	23	35
							In Ditch		

13.52 ✓

8.47
5.05
35.7 =
Floor
lev.

Lt.

#

Rt.

Inglew + Rosecrans
check B.M. S.W. 7+5' Disk

7.60

3.29

3.34

1177-64

Notes Reduced. 9.25.06

10 + 56.70 = W. cb. line of Rosecrans = 16' cbs.

	5.06	5.46	5.33	5.28	5.19	5.10	4.89	4.66	5.26
Top cb.	1.83	5.43	5.56	5.61	5.70	5.79	6.00	6.23	5.63
9ft.	60	60	35	17		17	35	60	60
PC. of Ret.					10.89 ✓				PC. of Ret.

X-Sept 20' Alleys in Block 9 - Alhambra
Park - Map 1488

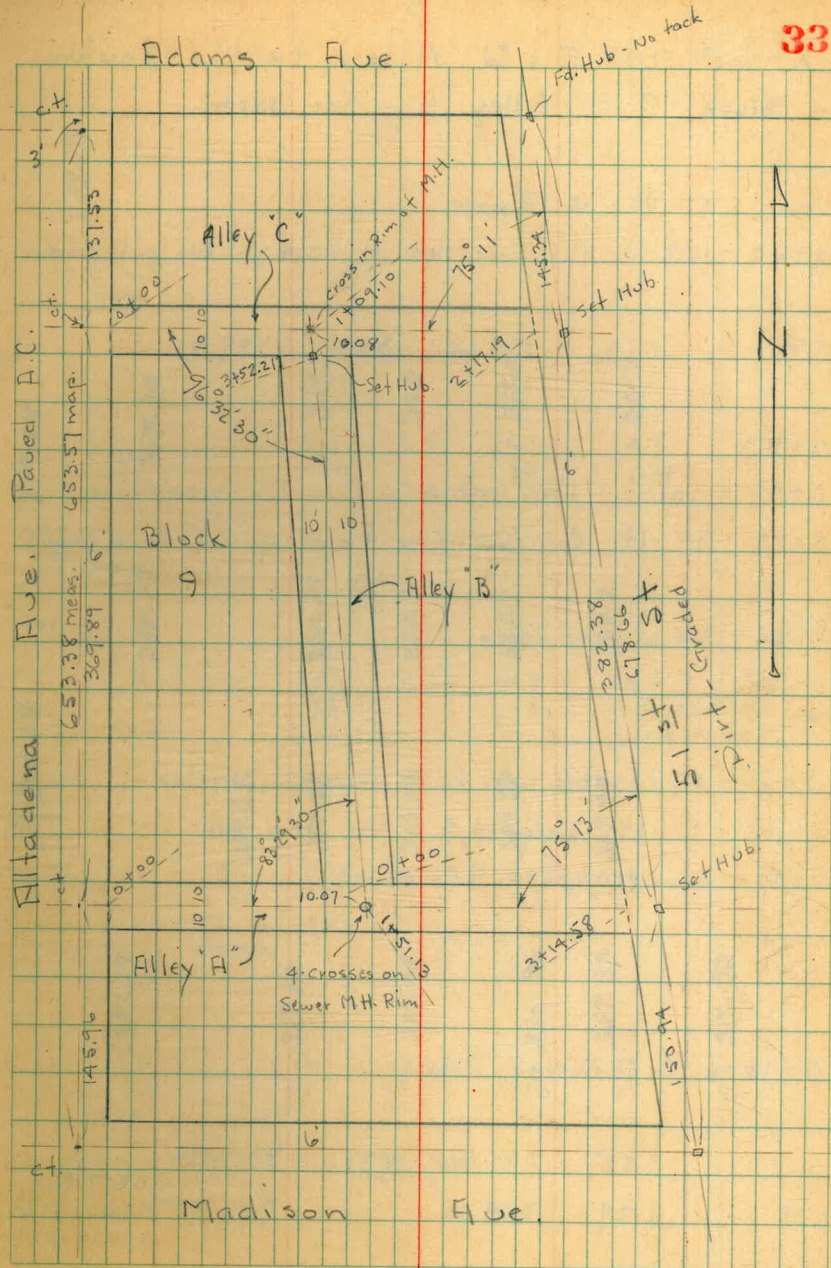
11-25-46

11-26-46

622.

W.O. 230

Osborne
Hardin
Worrell
Smith



X-Sect. 20' E. + W. Alley to the South
in Block 9 - Alley "A" - See sketch.

0+60 - 9.3 Rt = # P. pole

0+60 - 10.2 Lt = Cor. Conc slab + 10.4 Lt = beg. picket fence

T.P. 5.19 394.60 3.55 389.41

0+50

0+49 - 10.1 Lt = Cor. Gar. + Cor. Conc Slab - board fence along edge

0+27 - 9.9 Lt = Cor. Gar. - Conc. floor + apron - drive joins apron.
opens W.

0+26 - 5.6 Lt = end fence

0+15

0+03 - 5.7 Lt = beg. wire fence along small Hedge

0+00 - 11' Lt = S. edge of S. 2' Conc strip Dr.

0+00 = E.L. + edge of A.C. pave.

0-12 = E. cb. Line Altadena

3.55 392.96 4.71 389.41

B.M.

7.29 394.12

386.83

SE. 7 tack.
Madison + 51st
81679-P37

Lt = N.

Rt = S.

34

389.13					
547					
10.2 = on Conc.					
389.05	394.60				
389.30	389.3				
3.66	3.7				
10.1 on Conc. Slab.	0				
391	388.87	388.8	388.8	388.8	388.7
9.9	4.09	4.2	4.1	4.3	4.3
floor	11	10	11	0	20
Gar.	On Dr.				
388.19	387.65	387.48	387.29	387.28	387.2
4.78	5.31	5.48	5.67	5.88	4.8
11	0	0	0	0	16.9 = Cor Gar. open to W. - dirt floor
Top Dr.	Top cb. end Ret.	gut.			
387.27	387.10	387.08	386.96	387.97	386.72
5.69	5.86	5.88	6.00	5.57	6.24
gut	gut.		gut.	Top cb	gut.
	Note: cb out for corner Drive			2 Rd. Ret.	
		392.96			

Levels on Alley "B" - 20' N+S Alley in Block 9.

2+53 - 8.7 Lt. = Beg. picket fence

1+51 - 6.3 Lt. = ± P. pole

2+50 - 10' Rt. = Picket fence

2+02 = 10.2 Lt. = end picket fence

T.P. 5.22 395.56 4.26 390.34

2+00

1+51 - 10' Rt. = beg. picket fence

1+50

1+26 - 7.2 Lt. = ± P. pole + 10.2 Lt. = picket fence

1+00

0+77 - 10' Lt. = beg. picket fence

0+50

0+00 = ± + N.L. of E. + W. Alley "A" - Sect. along
N.L. of Alley "A"

Lt. = W.

⊕

Rt. = E.

4.7 20	4.6 10	5.2 0	5.0 0	2.5 0
389.9	390.1	390.4	390.3	389.8
4.7 20	4.6 10	4.2 0	4.3 0	4.6 20
389.8	390.0	390.4	390.4	389.6
5.1 10.05	5.1 0	5.2 0	5.1 0.05	
389.5	389.6	390.6	389.5	
4.6 10	4.7 0	4.2 0	4.1 0	4.6 20
390.0	389.9	390.9	389.9	389.6
4.6 10	4.6 0	4.2 0	4.3 0	4.6 20
391.1	391.0	390.4	390.3	390.1
4.7 20	4.6 10	5.2 0	5.0 0	2.5 0
391.1	391.0	390.4	390.3	390.1
4.7 20	4.6 10	4.2 0	4.3 0	4.6 20
391.1	391.0	390.4	390.3	390.1
5.1 10.05	5.1 0	5.2 0	5.1 0.05	
391.5	391.6	392.6	391.5	
4.6 10	4.7 0	4.2 0	4.1 0	4.6 20
390.0	389.9	390.9	389.9	389.6
4.6 10	4.6 0	4.2 0	4.3 0	4.6 20
391.1	391.0	390.4	390.3	390.1
4.7 20	4.6 10	5.2 0	5.0 0	2.5 0
391.1	391.0	390.4	390.3	390.1

T.P. 5.06 395.46 5.16 390.40

3+52.21 = S.L. of Alley "C" - Sect. along S.L. Alley "C"
9.5 Lt = ± P. pole

3+30

3+01 - 8.2' Lt. = end fence

3+00

2+99 - 10.2 Rt. = end fence

2+58 - 10' Lt. = Φ of 6" Conc. slab for clothes lines

Lt.

#

Rt.

37

4.1 391.5
10.05

4.4 391.2

4.05 391.1
0.05

4.3 391.3

4.4 391.2

4.5 391.1

4.8 390.8

4.1 390.9

4.4 391.2

4.8 390.8

4.8 390.8

4.5 390.5

4.1 390.3

4.38
10.0 on slab

395.50

check starting B.M. 7.26 386.84 386.83
 T.P. 6.52 394.10 6.63 387.58

2+17.19 = w.l. 51st - Sect. along w.l.

2+00

1+80 - 14.7 Lt. = \pm frame House

1+55 - 8.7 Lt. = \pm 3.3 Conc. walk

1+50

1+38 - 12.9 Lt. = \pm Doub. Gar. Conc. floor (rough)

T.P. 339 394.21 4.64 390.82

Lt.

Rt.

39

to the road
 15.47
 389.6

389.6
 4.6
 10.35

389.3
 4.9

389.3
 4.9
 10.35

390.2
 4.0
 20

389.6
 4.6
 10

389.6
 4.6

389.5
 4.7
 0

389.4
 4.8
 0

390.42

390.46

391.59

3.79
 14.7
 walk at gate

3.76
 8.7
 edge walk

2.62
 14.7 = floor

390.4
 3.8
 10

390.4
 3.8

390.6
 3.6
 0

390.6
 3.6
 0

390.51

3.70
 12.9
 floor.

394.21

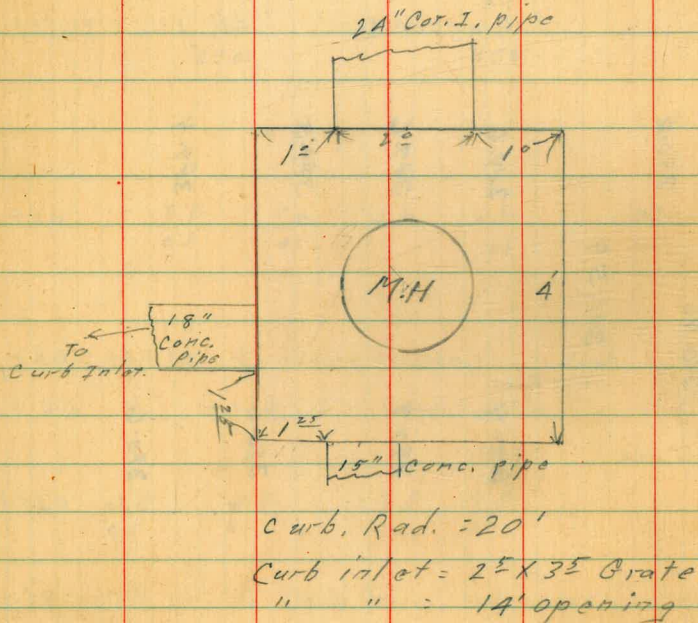
2-6-47

NOEL & HANCOCK

Seminar Meyer
W Moore
J Green

CROSS SECTION FOR DRAIN

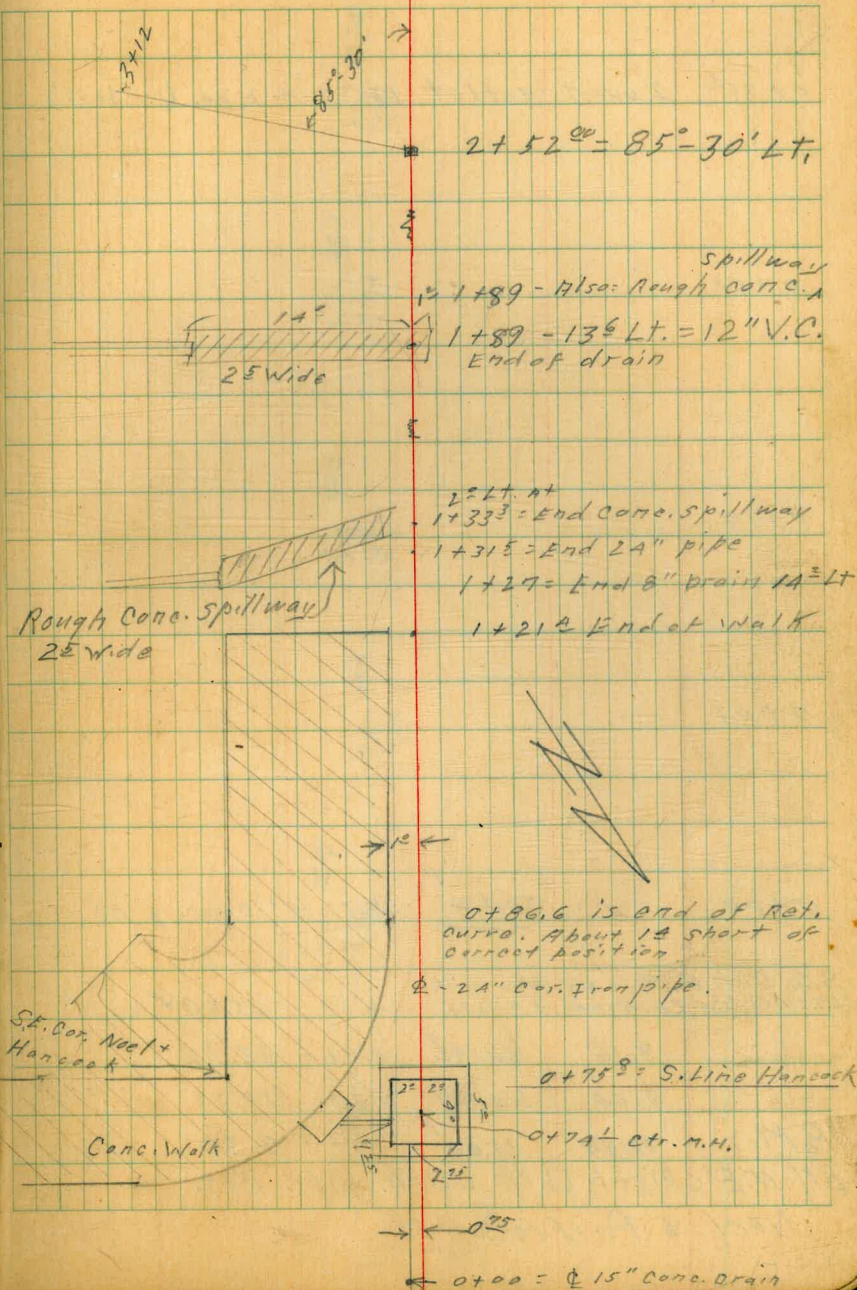
& Locate present drain



Work Order # 38

Included
C.S.M.

40



0+72¹ Invert-outlet 15" C.M. pipe. (in box)

22.28
8.14
0.75

0+50

25.1
5.3
0.75

0+17

26.3
4.1
0.75

0+01

27.6
2.8
0.75

0+00

30.42 ✓ N.E. 15" C.M. pipe

25.09
5.33
0.75

S.S. Set B.M. on copper disk
(L.S. 2286) S.W. Cor. Hanson & Noel

4.82 25.60 ✓

8.16 30.42¹ 2.71 22.26

9.64 24.97¹ 0.33 15.33

B.M. = 12.30 15.66¹ — 3.36

B.M. N.E. chisel □ in curb. ctr. Ret.

Noel & Pacific.

30.42 ✓

T.P. 1.86 2253 9.75 2067

1+50

1+33² = ϕ 2⁵ Wide rough conc. spillway

1+31^E End 24" Cor. Iron pipe

1+27 14' Lt: ϕ 8" Conc drain outlet

1+21^A End of Walk

0+86^E E.C.

30.42

22.0	21.8	18.5	18.6	21.9	21.7
8.4	8.6	11.0	11.8	7.5	8.7
10	2		2	6	13

21.5	18.3
8.9	11.6
2	

21.6	18.9	18.51	18.9	23.2	22.9
8.8	11.5	11.91	11.5	7.2	7.5
2	1	11 INVERT	1	5	10

21.87	23.2	23.2
8.55	7.2	7.3
14 INVERT		5

23.69	23.89	23.5	23.5	23.92
6.73	6.93	6.7	6.9	6.5
15	10	10		5
Edge Walk	Top Ch.	Top.		

25.26	24.97	24.72	24.7	24.1
5.16	5.45	5.7	5.7	6.3
15	10	10		5
inside walk	Top Ch.	Ground		

30.42 |

2+37

2+25

2+04 3rd Lt. = Ctr. 16" power pole

1+93

1+89 } { Φ 2^{1/2} wide rough corr. spill way }
13th Lt. Φ 12" v.c. drain (P. 40)

1+86

22.53

22.53

44

18.9	20.1	17.2	20.5	17.5
$\frac{3.6}{10}$	$\frac{2.4}{6}$	5.3	$\frac{2.0}{6}$	$\frac{4.6}{10}$

18.5	19.1	17.5	19.5	18.5
$\frac{4.0}{10}$	3.4	$\frac{5.0}{3}$	$\frac{2.6}{9}$	$\frac{4.0}{12}$

20.2	19.9	18.1	19.4	19.8
$\frac{2.3}{10}$	2.6	$\frac{4.4}{2}$	$\frac{3.1}{4}$	$\frac{2.7}{10}$

18.99	18.18	18.08	18.1	19.7
$\frac{4.04}{13.6}$	$\frac{4.35}{2.70}$	$\frac{4.25}{1.2 \text{ corr.}}$	$\frac{4.4}{4}$	$\frac{2.8}{7}$

20.2	20.0	18.1	19.9	19.5
$\frac{2.3}{10}$	2.5	$\frac{4.4}{3}$	$\frac{2.6}{8}$	$\frac{2.6}{10}$

22.53

Error 0.01
 orig 3.36 orig B.M.
 9.00 3.37 P A1

T.P. 1.86 12.37 12.02 10.51
 3+12 22.53 End of Profile

2+92 12^{ft} Lt. = S.W. Corn Bldg

2+70

2+58

2+52⁰⁰ = L 85°-30' Lt. Section taken on split

2+46

22.53

⊕

45

22.5
 $\frac{9.0}{7}$ 17.7 18.1 18.4
 4.8 4.3 4.1

21.3 21.0 17.8 18.9 18.8
 $\frac{1.2}{12.5}$ $\frac{1.5}{3}$ 4.7 $\frac{3.6}{3}$ $\frac{4.1}{10}$

18.6 17.6 18.7 21.1
 $\frac{3.9}{5}$ 4.9 $\frac{3.8}{5}$ $\frac{1.3}{10}$

17.1 21.0 12.3 16.7
 $\frac{5.4}{7}$ 1.5 $\frac{5.2}{12}$ $\frac{5.8}{20}$

17.0 21.3 18.5 17.4 17.6
 $\frac{5.5}{11}$ $\frac{1.2}{4}$ 4.0 $\frac{5.1}{10}$ $\frac{4.7}{15}$
 IN ditch

19.0 17.1 20.1 17.3
 $\frac{3.5}{10}$ $\frac{5.4}{6}$ 2.3 $\frac{5.2}{8}$

22.53

Notes Reduced 2-7-07

Elevations + Ties for Prop Entrance
to Golf Club. - No grading done outside of
Prop. Line.

798
W.O. 262

2-21-47
Osborne
Hardin
Smith
Worrell

154 + 47.99 = E.C.
156 + 47.62 = P.O.T.

123'

Fd. 2" pipe
L.S. 2236

193.12

Fence

Graded

Baseline

60' RC

c.l. Drive

CL. Drain
5' wide

62'

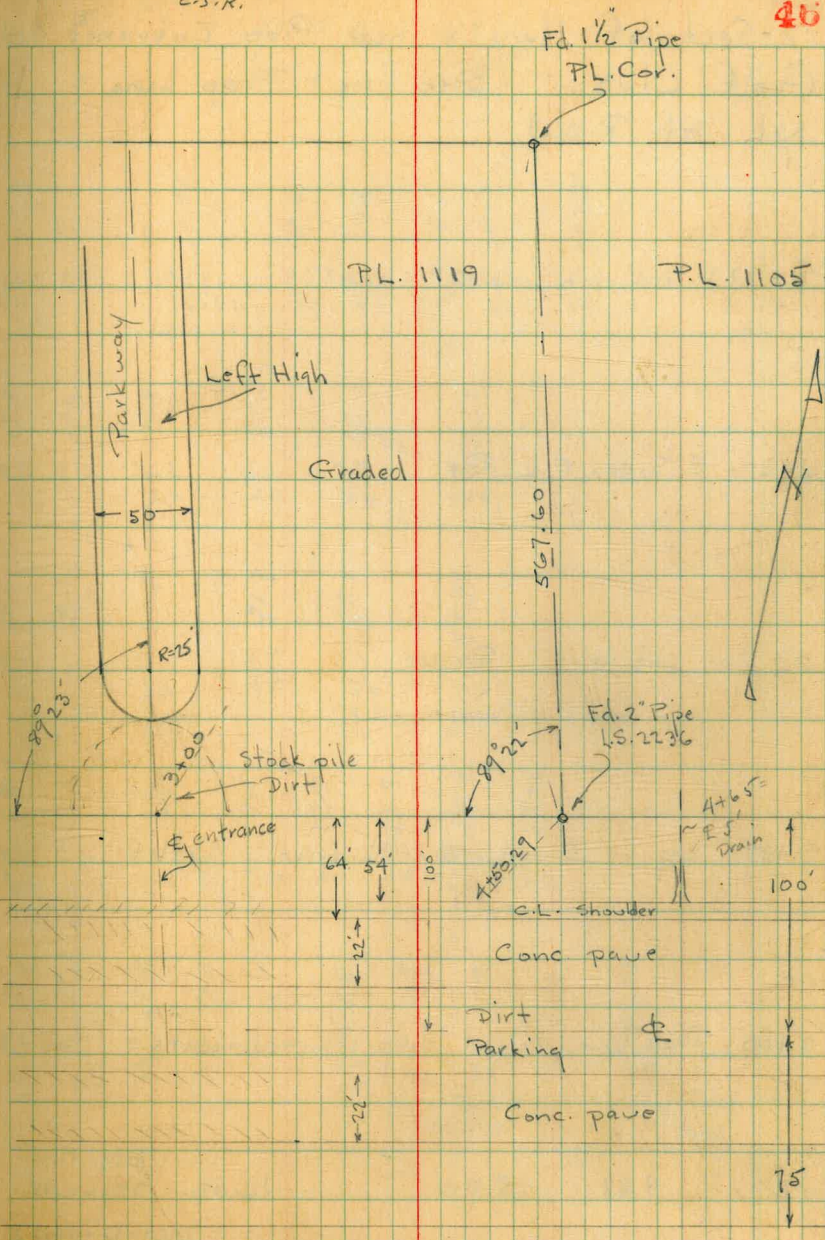
13'

36'

29 + 16.80
1670.749
Elev. 1634

Indexed
C.S.K.

46



X-Section of Hwy + near Prop Entrance to Golf Club. - Base line = Prop line = N.L. of R.O.W.

Base Line = N.L. Row.

Lt = N.

Rt = S

27

0+77 = End. 60" Culvert = inlet

0+63 = E Side C.L. Dr.

0+50 = W. side C.L. Drive

0+37 = Beg 60" Culvert under C.L. Drive = Outlet.

0+00 = Prop. Line = Wend Prop. Improvements

15.9	11.5	11.71	18.8	19.6	22.8	22.3	22.58
100	84	14.19	7.1	6.3	3.1	3.6	3.32
10		15 = FL 60" pipe	30	40	54 100 Roll	56	64
17.1	17.9	19.8	21.3	22.2	22.51		
0	20	6.20	4.6	3.5	3.3	6.4	
			4.0	5.6	6.4		
17.6	18.3	19.8	21.2	22.1	22.57		
0	20	6.20	4.7	3.8	3.3	6.4	
			4.0	5.6	6.4		
				1.4	edge Conc		
16.3	17.8	18.9	19.1	19.9	22.2	22.54	
9.6	8.1	15.01	6.8	6.0	3.2	3.7	3.36
0		15 = FL 60" Culvert.	30	40	54	64	64
17.6	17.2	17.3	17.1	17.1	16.8	22.7	22.55
8.3	8.7	8.6	14.8	14.8	9.1	3.2	3.35
0		5.6	13	20	27	54	64
						Top Cl. Roll	edge Conc. Pave

9.88 25.90

16.02 B.M. Mon.
35+62.48

1061-D-sheet 4

5+00

4+65 = C.L. Drain 5 wide

4+50.29 = P.L.

4+00

3+75

3+50

3+25 = E. Side Parkway

To W.
Top
bank

16.8

16.2

16.2

17.3

9.1

9.7

9.7

8.6

75

75

50

30

16.3

9.6

16.4

9.5

15.9

10.0

16.3

9.6

16.0

9.9

16.3

9.6

16.8

16.2

16.2

17.3

Lt.

49

B.L.

92
10

17.3

8.8
5

17.1

13.2
10

12.7

12.9
17

13.0

9.0
24

16.9

17.2

23.6

23.1

23.82

98
10

17.1

8.4
5

17.5

12.6

12.6

17.1

8.2
43

23.6

23.0

23.24

23.6

23.1

23.82

93
4

16.6

8.6
5

17.3

12.9

12.7

16.8

8.6
43

23.4

22.9

23.04

23.30

22.0

23.26

91
4

16.8

8.0
5

17.9

13.1

13.0

17.2

8.1
43

23.4

22.8

23.06

23.26

21.9

23.22

68
15

19.1

8.3
5

17.6

12.6

12.6

17.4

7.7
44

23.3

22.7

22.99

23.20

21.9

23.16

92
10

17.3

8.8
5

17.1

12.7

12.9
17

13.0

9.0
24

16.9

17.2

23.6

23.1

23.82

98
10

17.1

8.4
5

17.5

12.6

12.6

17.1

8.2
43

23.6

23.0

23.24

23.6

23.1

23.82

93
4

16.6

8.6
5

17.3

12.9

12.7

16.8

8.6
43

23.4

22.9

23.04

23.30

22.0

23.26

91
4

16.8

8.0
5

17.9

13.1

13.0

17.2

8.1
43

23.4

22.8

23.06

23.26

21.9

23.22

68
15

19.1

8.3
5

17.6

12.6

12.6

17.4

7.7
44

23.3

22.7

22.99

23.20

21.9

23.16

92
10

17.3

8.8
5

17.1

12.7

12.9
17

13.0

9.0
24

16.9

17.2

23.6

23.1

23.82

98
10

17.1

8.4
5

17.5

12.6

12.6

17.1

8.2
43

23.6

23.0

23.24

23.6

23.1

23.82

93
4

16.6

8.6
5

17.3

12.9

12.7

16.8

8.6
43

23.4

22.9

23.04

23.30

22.0

23.26

91
4

16.8

8.0
5

17.9

13.1

13.0

17.2

8.1
43

23.4

22.8

23.06

23.26

21.9

23.22

68
15

19.1

8.3
5

17.6

12.6

12.6

17.4

7.7
44

23.3

22.7

22.99

23.20

21.9

23.16

Bottom
Drain

Top
Drain

Bottom
Drain

Top
Drain

Bottom
Drain

Top
Drain

Bottom
Drain

Top
Drain

Bottom
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Bottom
Drain

Top
Drain

edge
Conc.

edge
Conc.

edge
Conc.

edge
Conc.

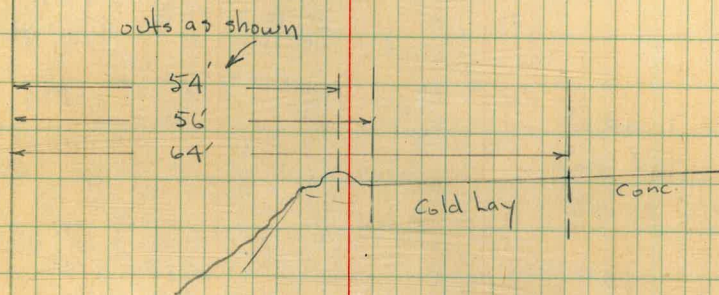
edge
Conc.

Lt.

Bl.

Rt.

Detail of Cold Lay Shoulder Const.



6+00 = end.

5+50

9.6	16.13	16.6	9.3	16.6
0	16.4	16.8	0	16.8
9.4	16.5	16.7	9.2	16.7
5	16.2	13.2	5.2	13.2
12.7	13.1	13.5	12.7	13.5
12.8	16.5	17.0	12.4	17.0
9.4	16.4	17.4	8.9	17.4
23	23.7	23.7	25	23.7
9.5	23.2	23.3	8.5	23.3
22	23.3	23.53	4.3	23.53
54			54	
56			56	
56			56	
64			64	

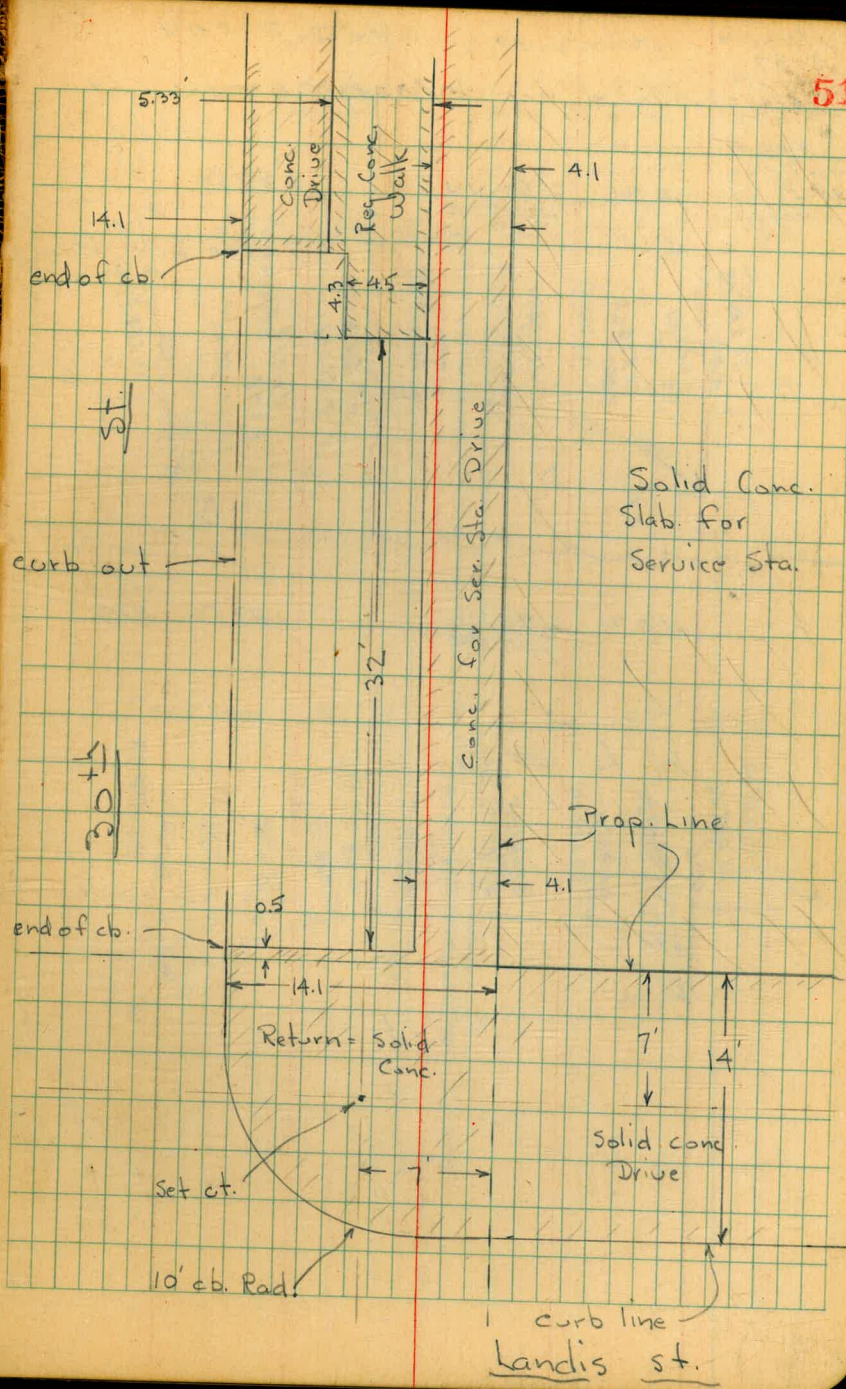
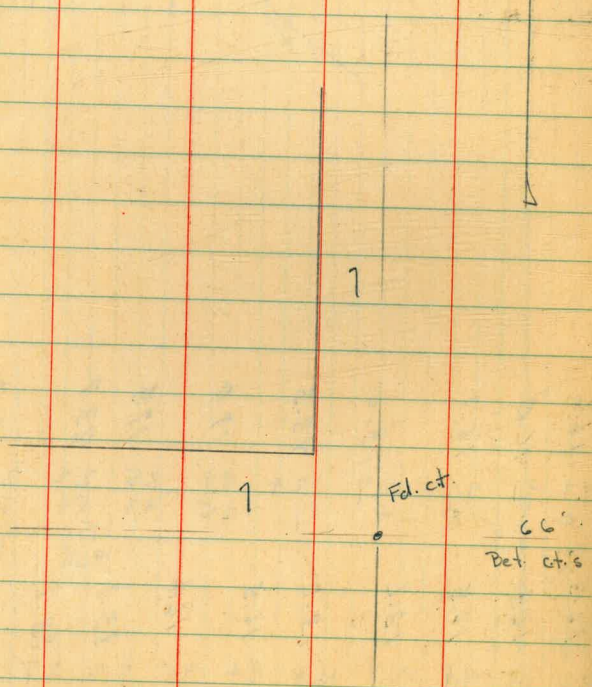
Top of Roll put
64 = edge Conc.

Measurements of Broken out Walk-curb +
 Driveway at NE Cor. of Landis + 30th
 3701 - 30th St. - a Service Sta.

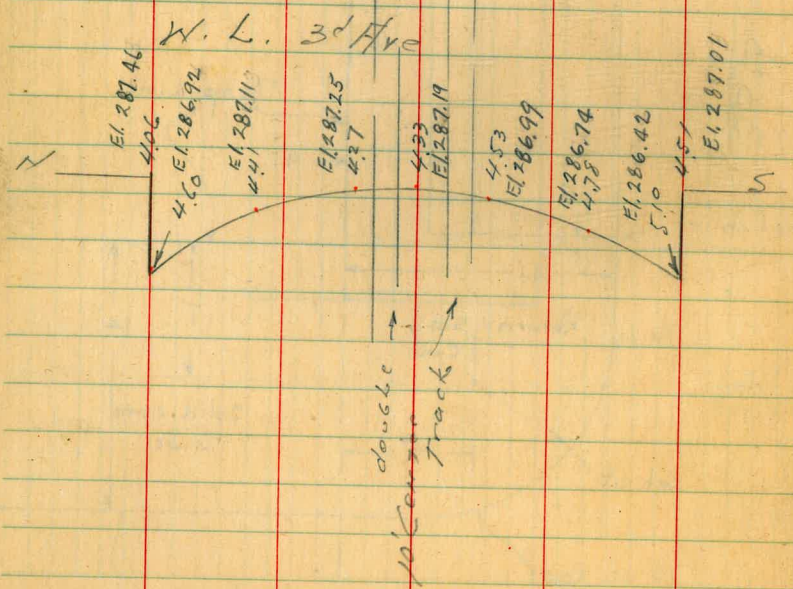
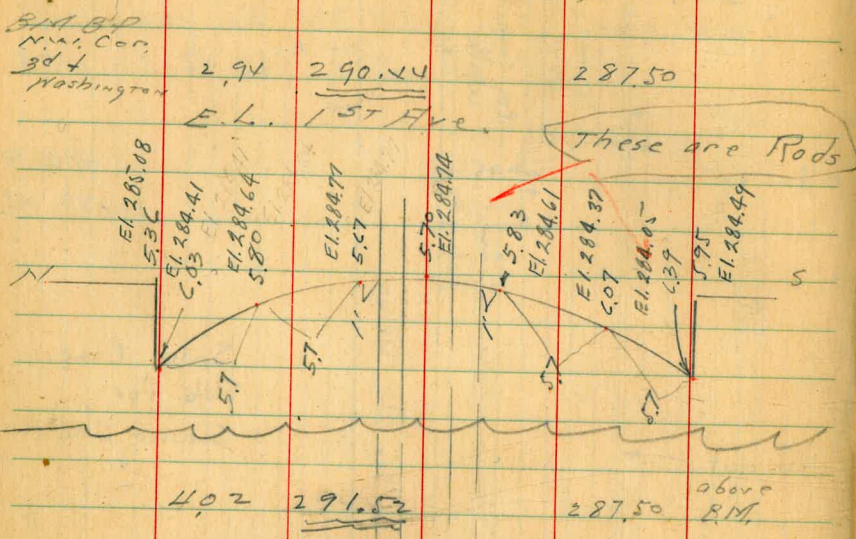
1094
 W.O. 25001

5-21-47
 Osborne
 Hardin
 Smith
 Worrell

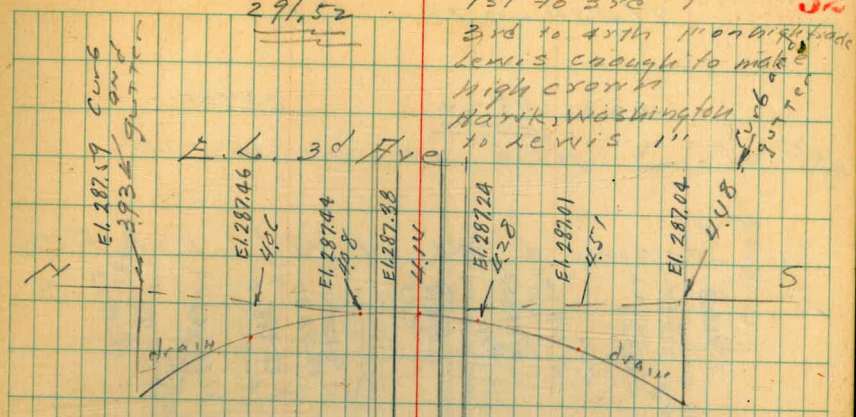
N



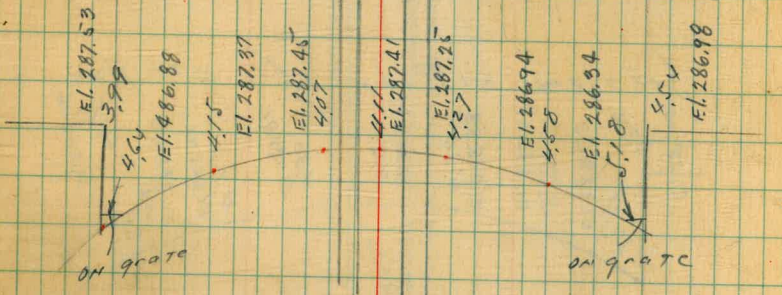
Moore 10-23-27, W.O. 21004
 Bogg
 Green
 Roberts Levels on Washington St



Washington St.
 291.52 1st to 3rd 11" 52
 3rd to 4th 11" on bridge grade
 Lewis enough to make
 high cross to
 Mark Washington
 to Lewis 11"



SECTION 4.5 F of E.L. 3d Ave

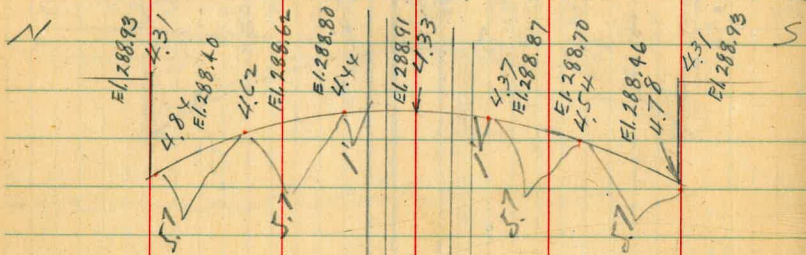


Washington St.

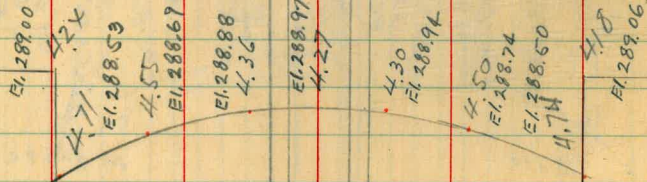
4.23 293.24

289.01

SECTION C'W of W.L. 4th Ave



SECTION ON E.L. of 4th Ave

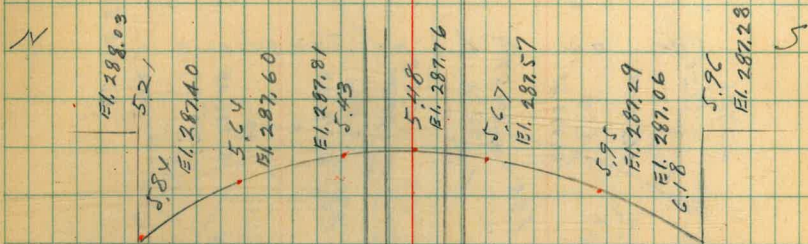


Double Track
Centers

293.24

53

SECTION ON W.L. alley E. of 4th Ave

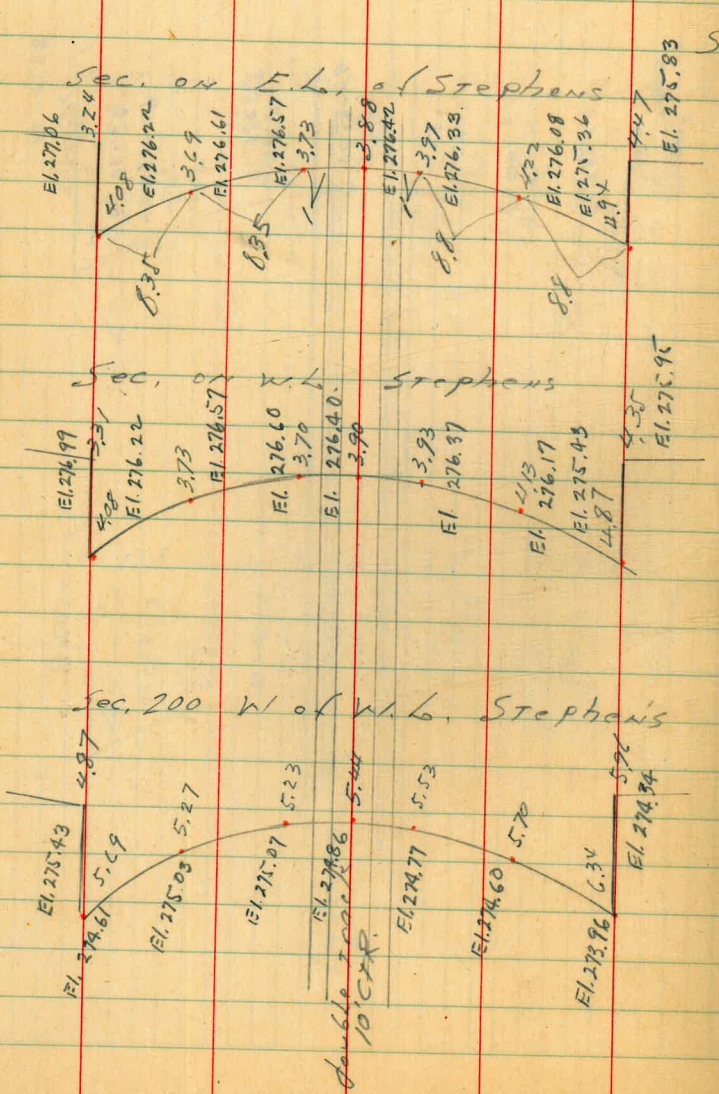


10' Track Centers

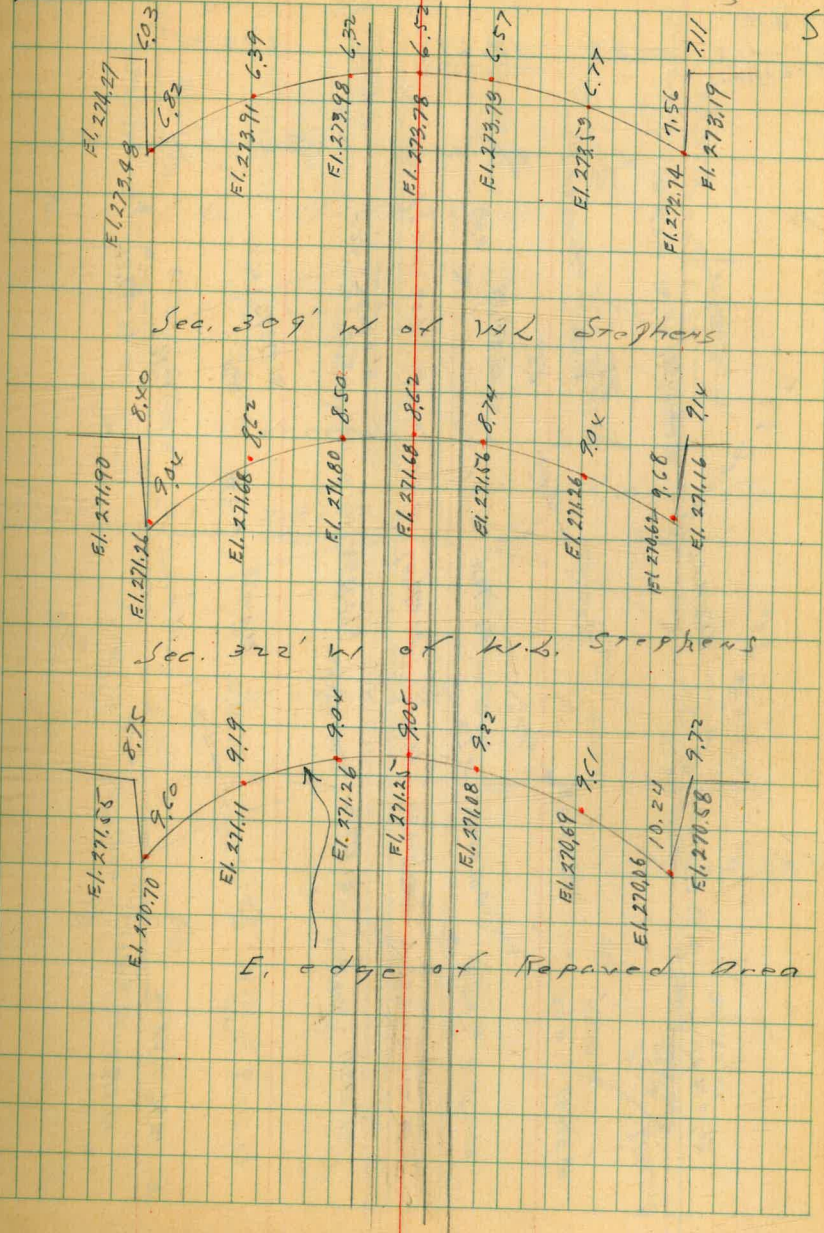
Levels on Lewis St.

SE8P
Lewis &
Stephens

4.52 280.30 275.78



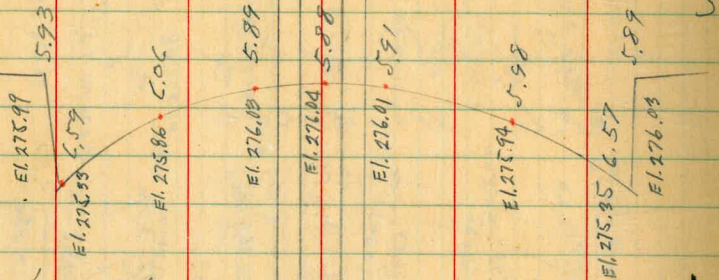
280.30
Sec. 250' W of W.L. Stephens 54



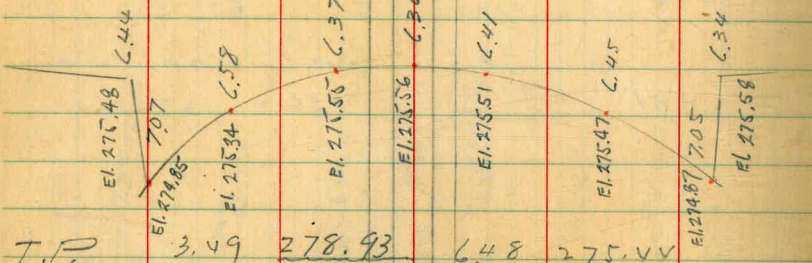
281.92

W.L. Ingalls

N.



E.L. Ingalls

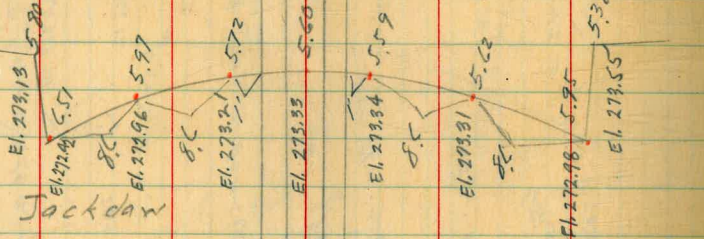


T.P

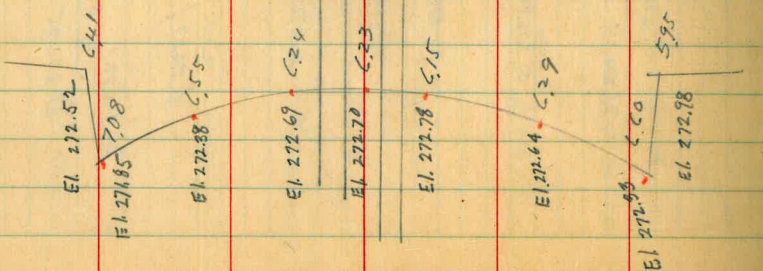
3.49 278.93

6.48 275.44

W.L. Jackdaw



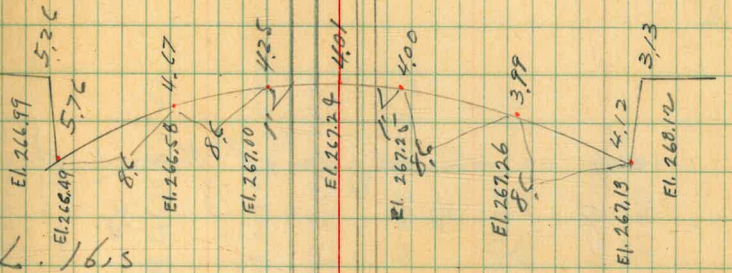
E.L. Jackdaw



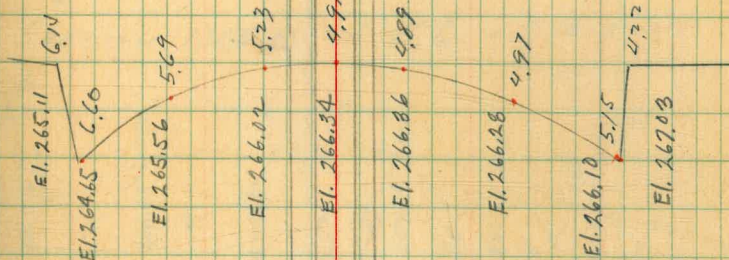
T.P 081 271.25 8.49 270.44

W.L. 16.5

N



E.L. 16.5



Lewis St.

271.25

section on W. edge of Repaved Area

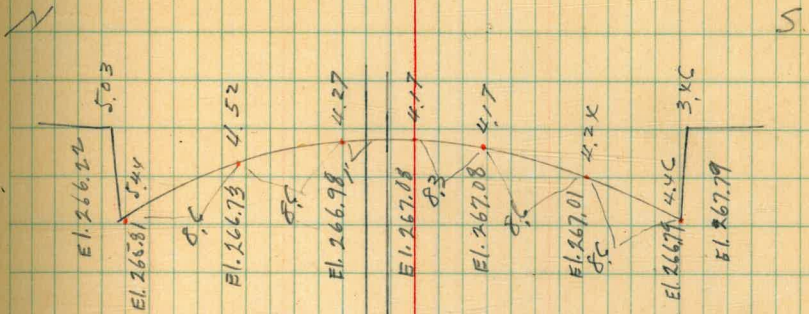
check to S.W. B.P.
Lewis & Hawk

330 267.95 267.97

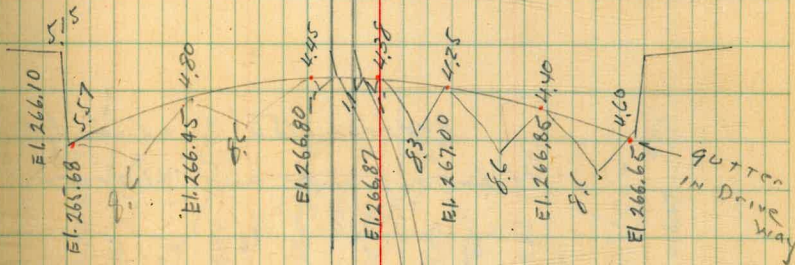
57

271.25

Section 127' E of E.L. of 1615 St



Section 106.5 E of E.L. of 1615 St



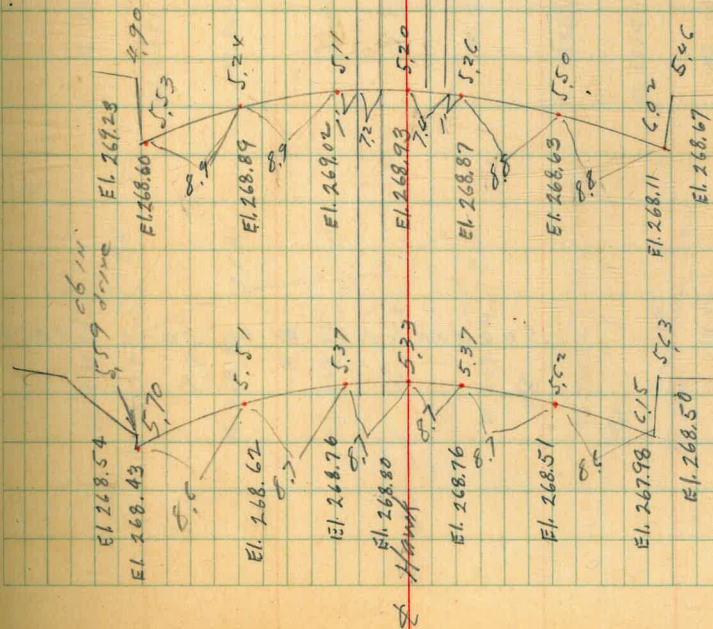
ST.

Levels on Hawk St.

SWBP
Lewis &
Hawk 6.16 274.13 267.97

Section 155' S of S.L.
of Lewis = N end W track

SECTION 115' S of
S.L. Lewis St =
N end E track



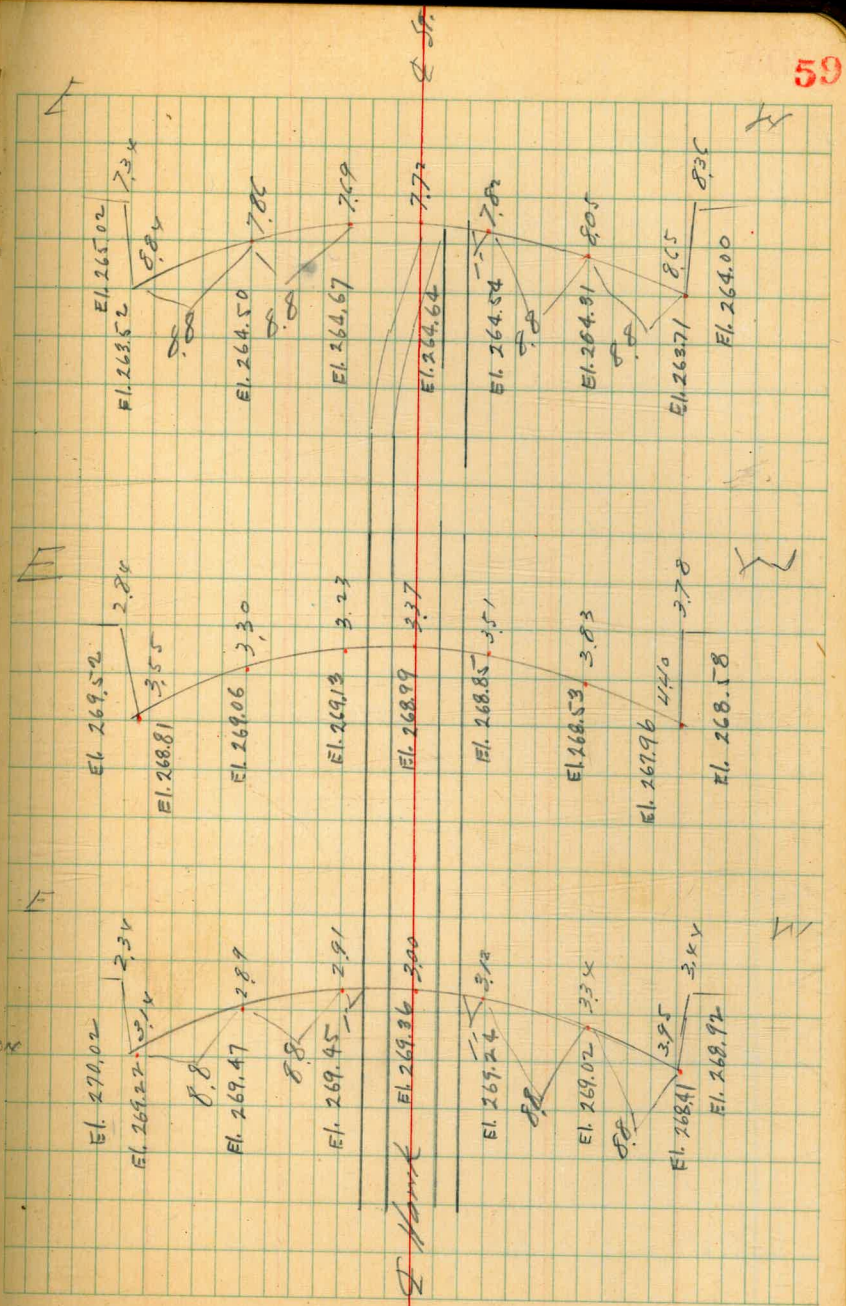
Levels on Hawk St

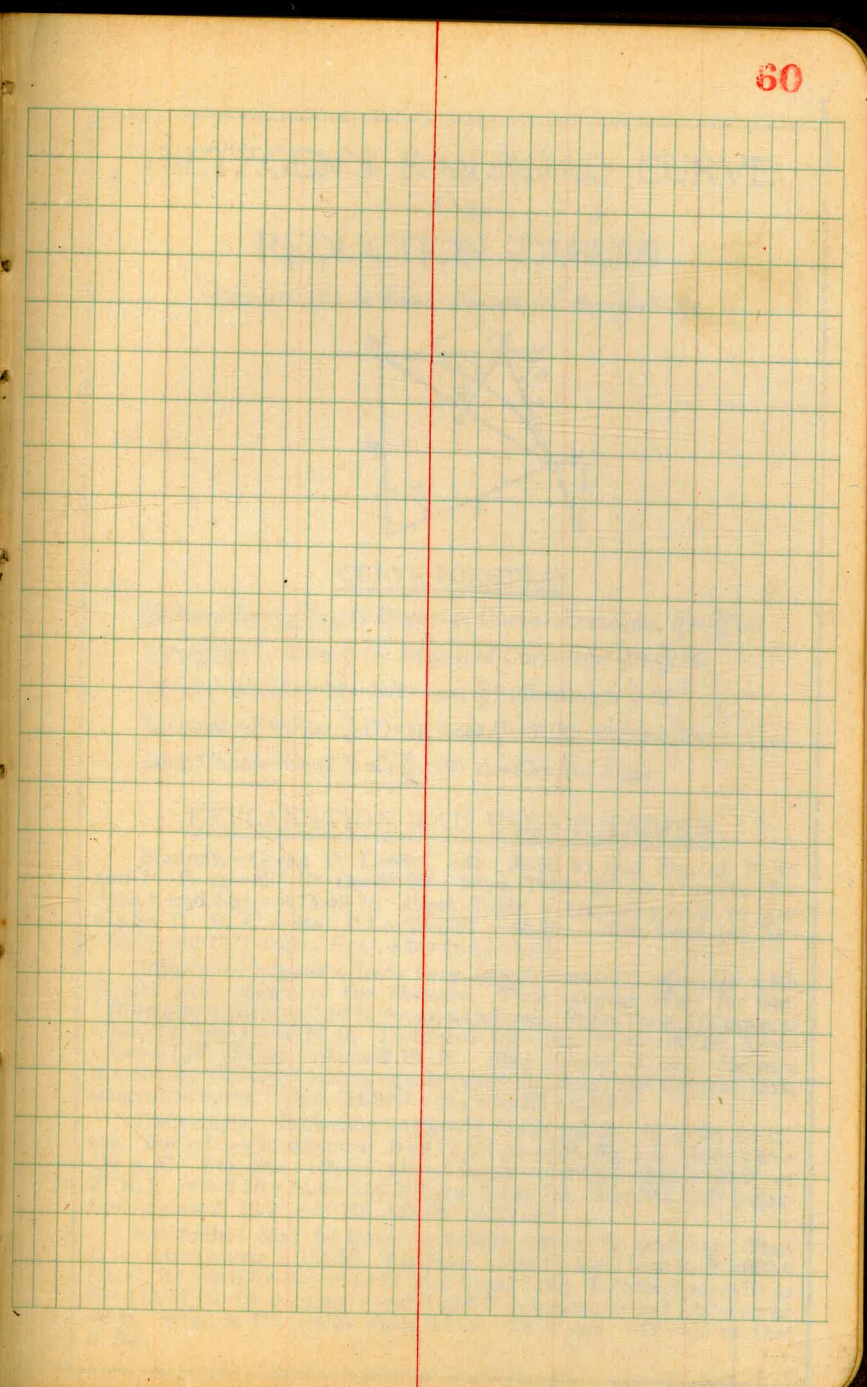
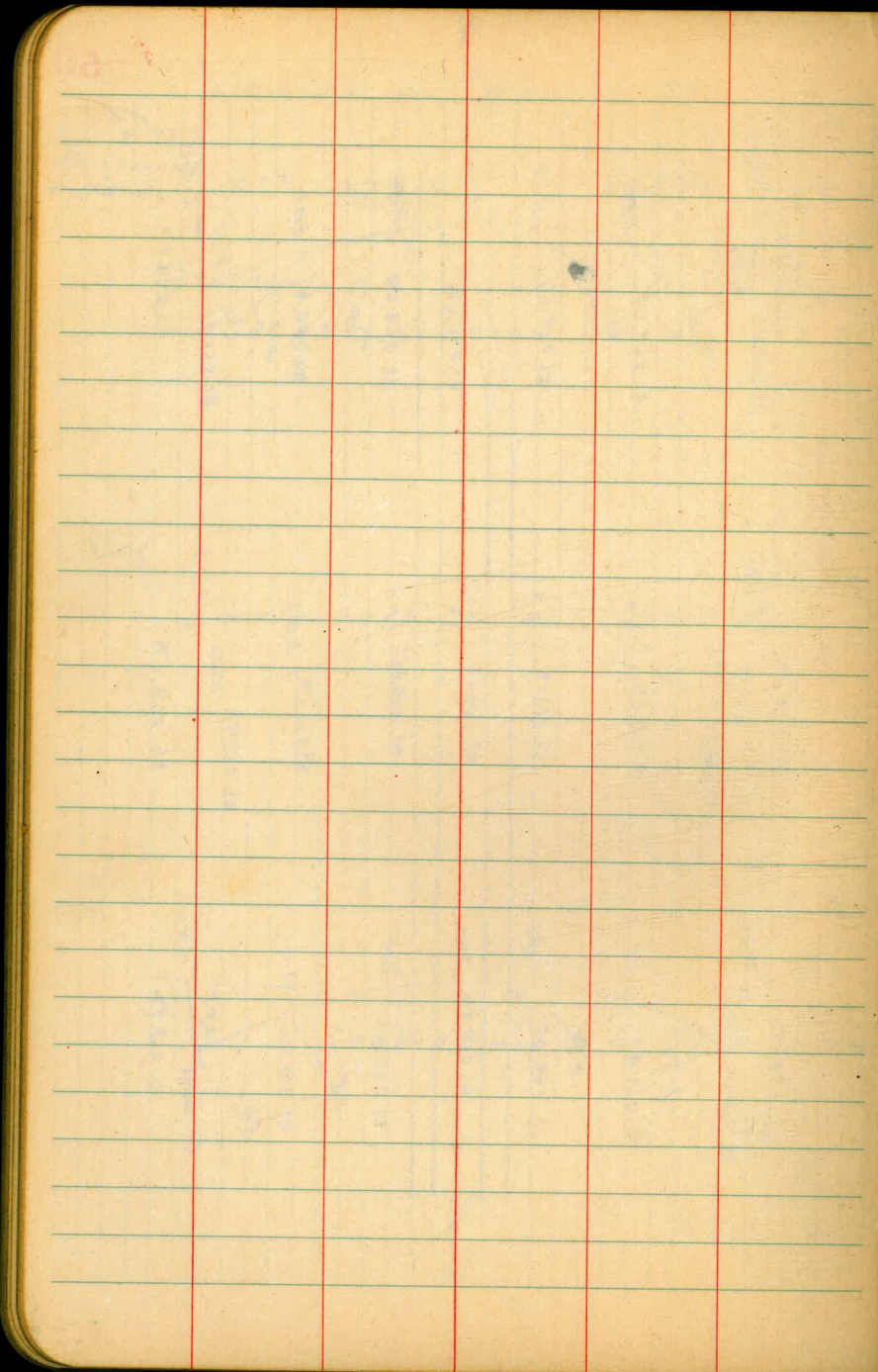
new B.P.
 Ft. Stockton 342 272.36 268.94
 Hawk

SECTION 204'S. of S.E. of FORT STOCKTON
 N. edge Repaved area

SECTION ON S.E. FORT STOCKTON

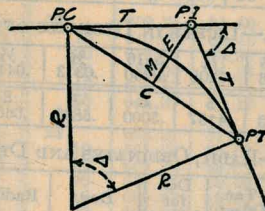
SECTION ON N.E. FORT STOCKTON





DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

- Radius= $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve= D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)
 Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)
 Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2})$ (5) $= R \text{vers } \frac{\Delta}{2}$ (6)
 External= $E = T \tan \frac{\Delta}{4} = R \div \cos \frac{\Delta}{2} - R$ (8) $= R \text{exsec } \frac{\Delta}{2}$ (9)
 Long Chord= $C = 2 R \sin \frac{\Delta}{2}$ (10) $\Delta =$ Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{1}{3} = 414.49$ ft. From Table V correction = .36 or $T = 414.85$ ft. P. C.—Sta. P.I.— $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T.—Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft. = 7.27 ft. Distance = 158—Sta. P. C. = 54.50, hence offset = $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle = $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft. = (in minutes) $.3 \times C \times D^\circ$ or = defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve = $.3 \times 54.5 \times 8\frac{1}{3} = 136.2'$ or $2^\circ 16.2'$, or $= 2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle = $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37. For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{1}{3} = 115.27$ and from Table V correction = .10 or $E = 115.37$ ft. Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

3280

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20 - 16) ÷ 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.