

EUGENE DIETZGEN CO.
DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on 1½ see inside of back cover.
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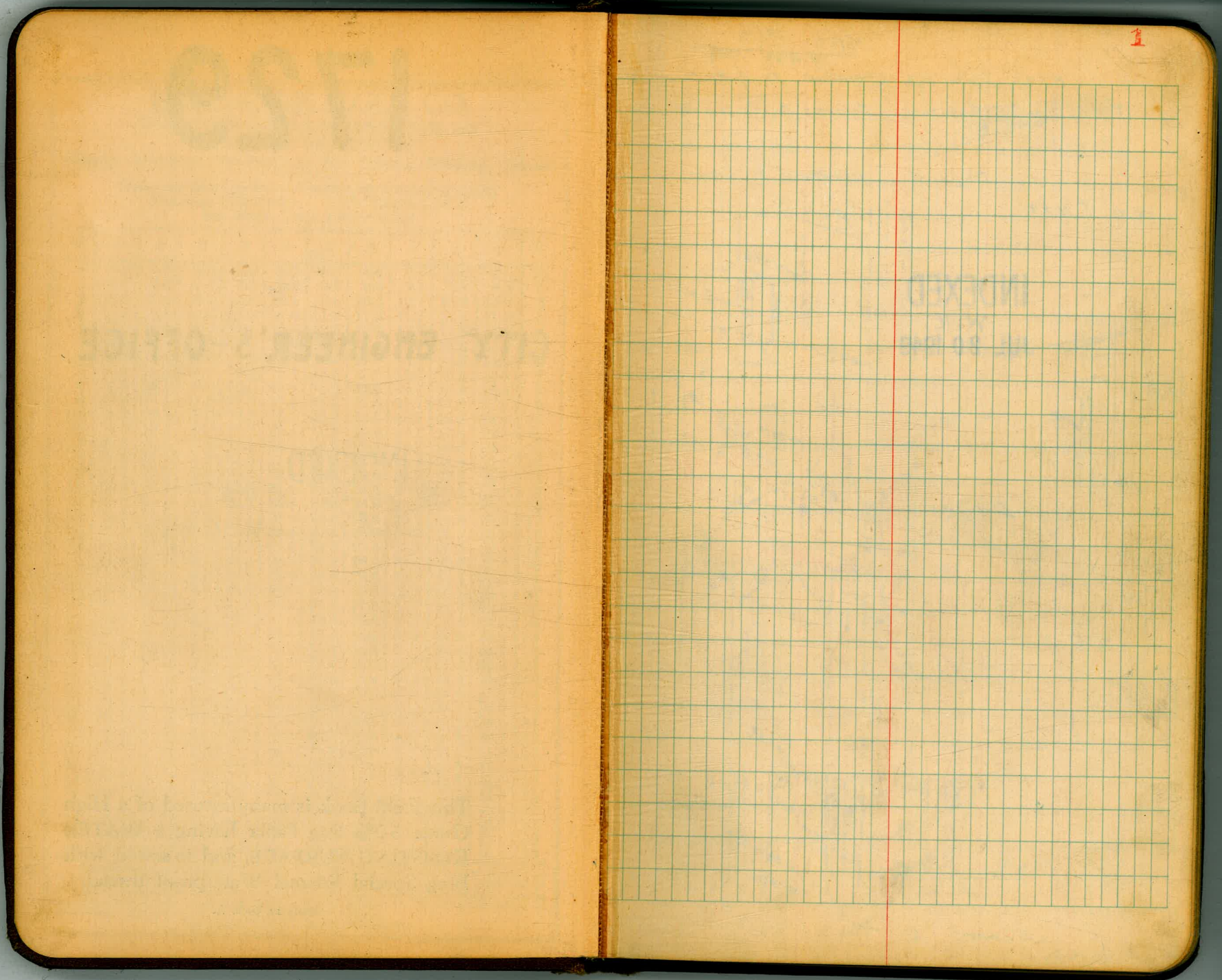
1729

CITY ENGINEER'S OFFICE

INDEXED
to page # 43
except pages 45 to 48

This Field Book is manufactured of a High Grade 50% Rag Paper having a WATER RESISTING SURFACE, and is sewed with Bing Special Enamel Waterproof thread.

Made in U. S. A.



T.P.S. 1762

9-4-50 MHO

X sec Dawes, Diamond to Lane

" Missouri, Everett to Ocean Blvd.

" Chalcedony " " " "

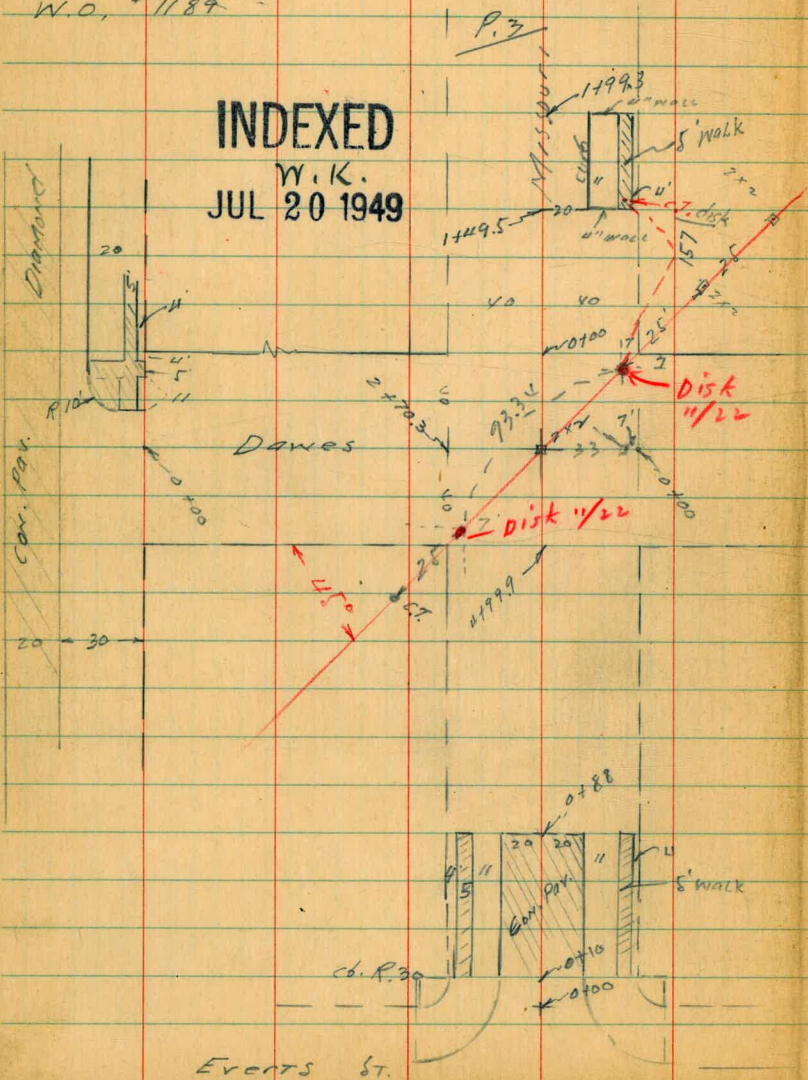
" Bayard, Diamond to Lane

W.O. # 1189

INDEXED

W.K.

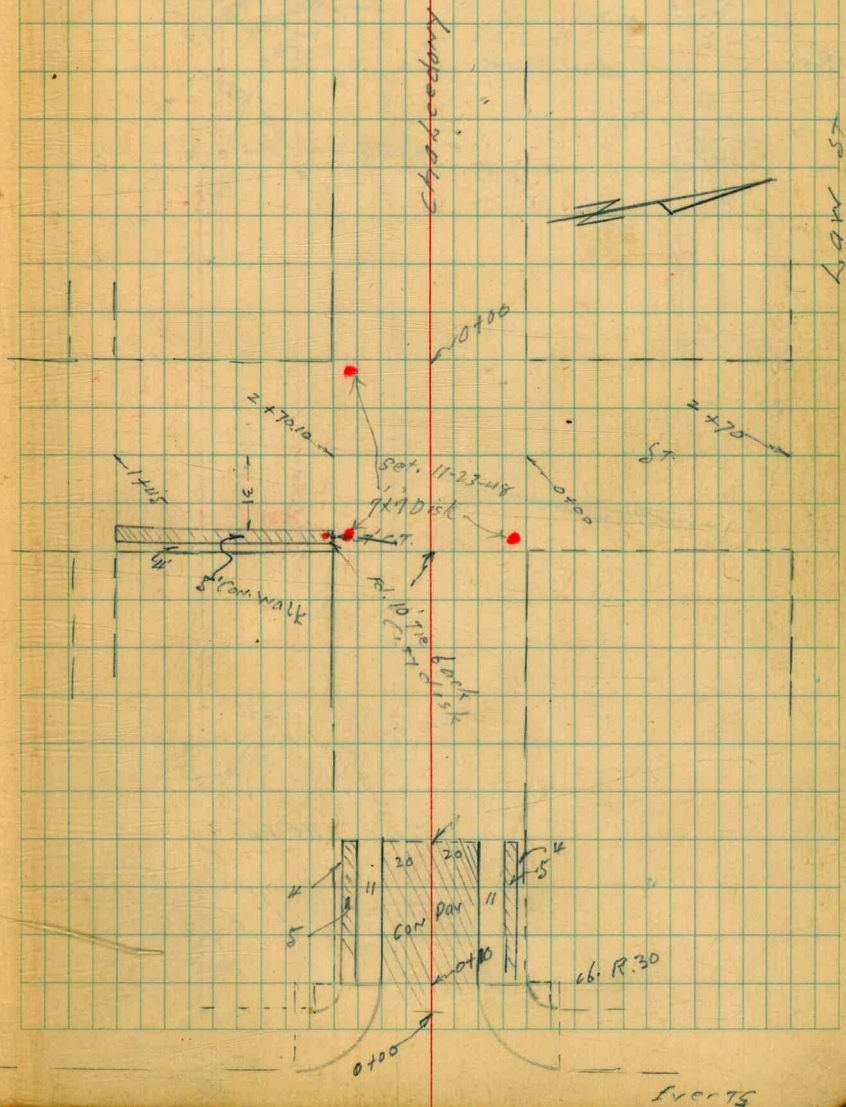
JUL 20 1949



C. Moore
Sergeant
8099
Allen
7-2-46

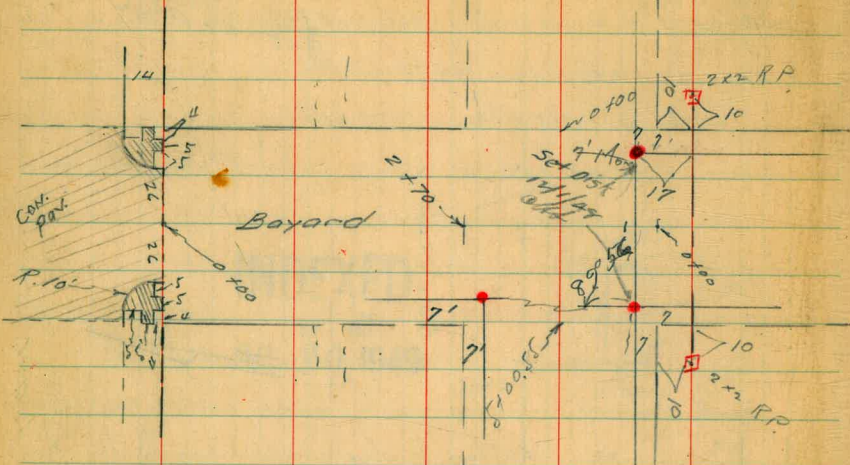
T.P. BK. #20

T.P.S. 1773
9-5-50 MHO



o = set disk

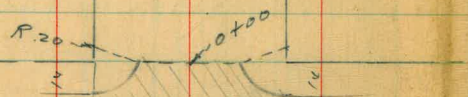
T.P.S. 1764
9-4-50 M.C.



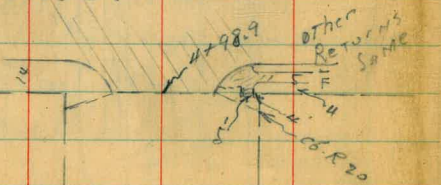
Diamond



Mission

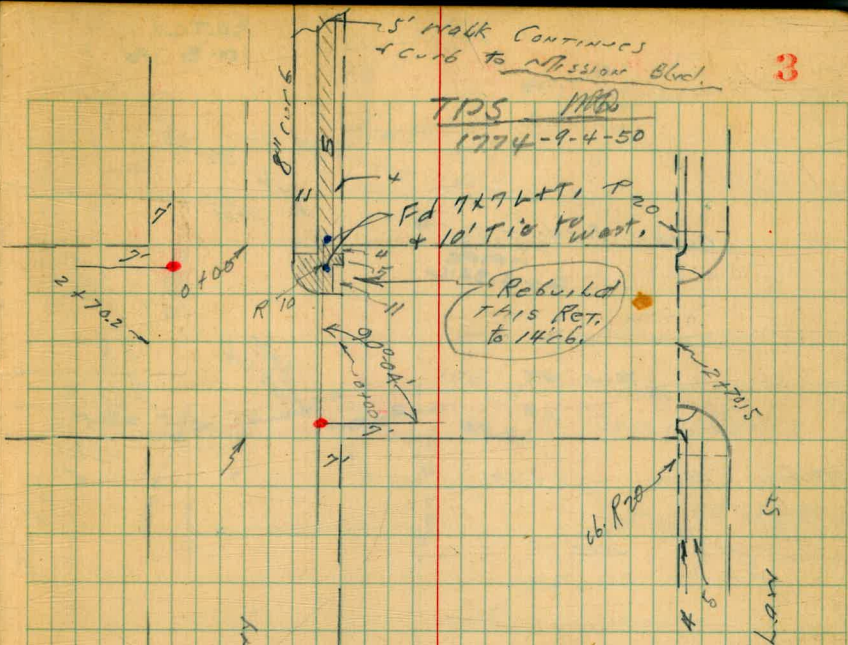


Cross St. R.C. Pav.



3

T.P.S. 1766
1774-9-4-50



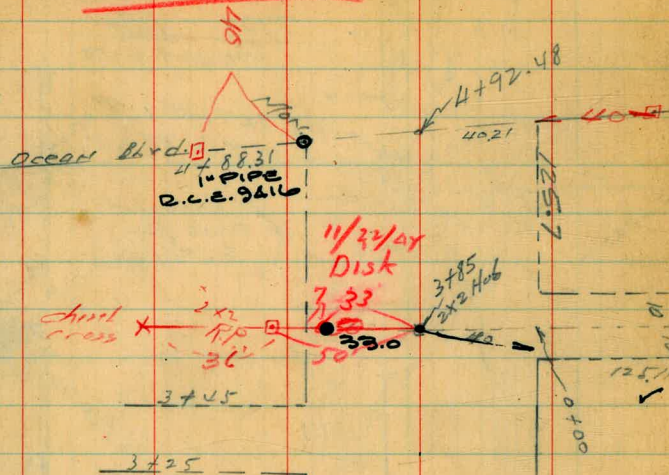
Chalcedony

Low St



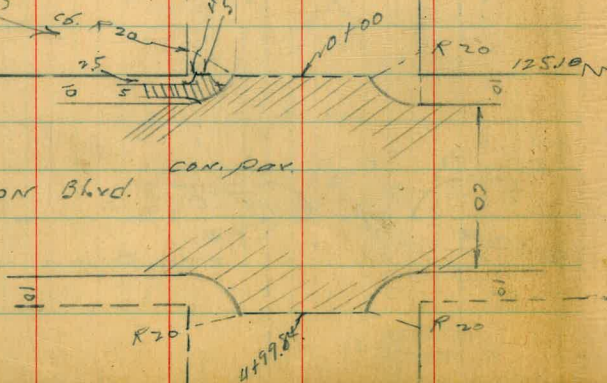
● = set disk

KATCH
10-8-75

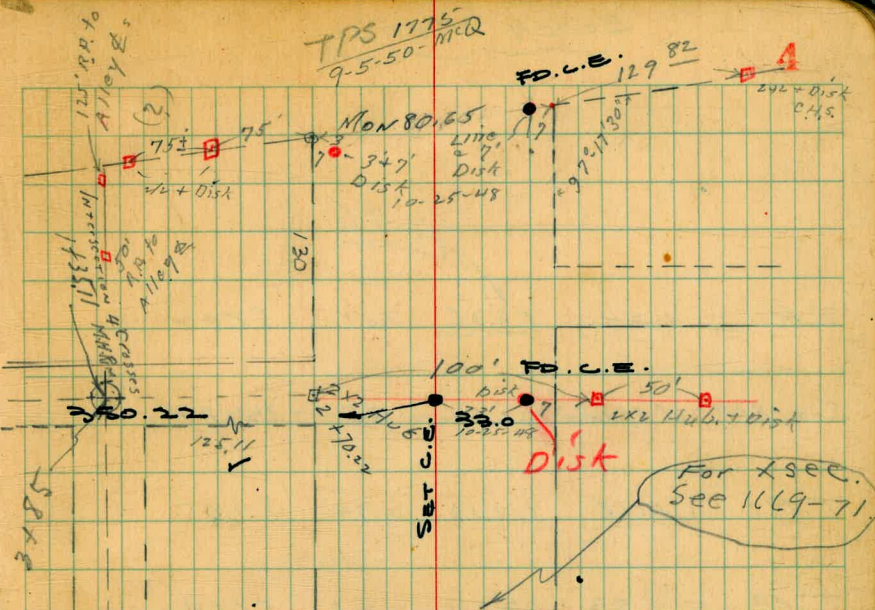


Other Returns
SAME

Mission Blvd.



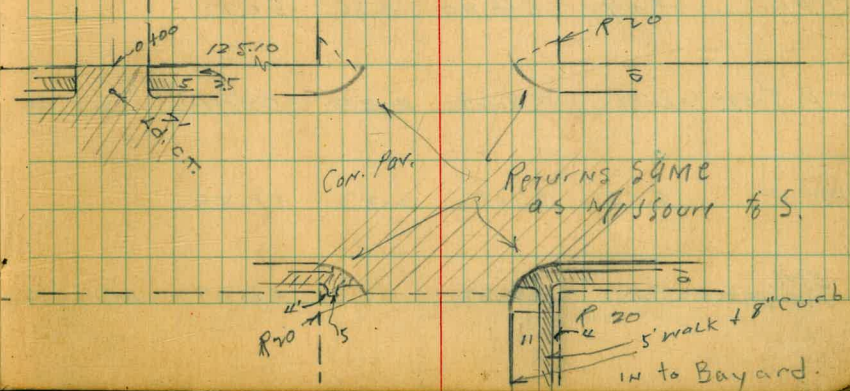
TPS 1775
9-5-50-MQ



BLK 117

Chalcedony

For X see
See 1669-71



Returns SAME
as Missouri to S.

5' walk + 8" curb
14" to Bayard.

Bench Marks

H.P.C.

T.P. 1.34 58.36 7.11 57.02

Set B.M. 30° spike Tel. Pole 1.95 62.18 ✓

T.P. 4.18 64.13 2.72 59.95

T.P. 6.53 62.67 2.26 56.14

Set B.M. 6.88 51.52 S.W. 7' Ld. C.T. Missouri and Cass St.

T.P. 3.92 58.46 9.52 54.48

Set B.M. 4.45 59.55 S.W. 7' Ld. C.T. Chalcedony and Cass St.

T.P. 5.19 64.00 0.86 58.81

T.P. 7' C.T. 6.91 59.67 4.39 52.76 ^{Set B.M.} N.W. 7' Ld. C.T. Chalcedony and Bayard St.

T.P. 5.66 57.15 2.83 51.49

BM. N.E. B.P. 5.83 54.37 48.49 Mission Blvd. and Chalcedony orig. by order

BM. City disk 10 RP
SE Con Chalcedony
Dawes

6872 5

N.E. Con. Missouri and Dawes

7' Ld. C.T. Missouri and Cass St.

Ld. C.T. Chalcedony and Cass St.

Ld. C.T. Chalcedony and Bayard St.

Mission Blvd. and Chalcedony orig. by order

X sec Dawes
Diamond to Law.

W.O. #1189

INDEXED

0 + 10

0 + 02 20' LT. Beg. Hedge

0 + 00 = N.L. DIAMOND ST

0 - 20 N. CB DIAMOND

51.91
645
40
TOP
CURB

0 - 30 N. edge Pav.

0 - 40 E DIAMOND

0 - 50 S. edge Con. Pav.

58.36
P. 5

LT = WEST \$ INDEXED C.S.K. P.F. = F 6

53.26	53.54	53.18	52.86	52.26	54.54	54.56
5.0	4.8	6.2	5.5	6.1	3.9	3.8
40	23	15		16	21	20
52.16	52.10	51.98	52.46	51.86	52.56	52.26
6.7	6.2	6.38	5.9	6.5	5.8	6.1
40	31	20	20	15	15	15
	E. edge - Schr.	TOP CURB				
51.56	51.94	51.76	51.56	51.86	52.16	52.36
6.8	6.42	6.6	6.8	6.5	6.7	6.0
40	30	30	20	10	17	17
	TOP CURB					
52.65	51.46	51.56	51.66	51.78	51.91	52.07
7.73	6.90	6.80	6.70	6.58	6.45	6.29
100	40	30	20	10		10
52.64	51.46	51.60	51.71	51.84	51.99	52.13
7.72	6.90	6.76	6.65	6.54	6.37	6.23
100	40	30	20	10		10
52.07	51.23	51.50	51.62	51.73	51.83	52.00
7.85	7.03	6.80	6.74	6.63	6.53	6.30
100	40	30	20	10		10
52.18	52.32	52.45	53.48			
6.18	6.04	5.91	4.88			
20	30	40	100			
52.21	52.26	52.43	53.41			
6.15	6.00	5.93	4.87			
20	30	40	100			
52.09	52.29	52.36				
6.27	6.07	6.01				
20	30	40				

58.36

Darries

LT=W

✱

59.25 RT=E

2+20 25.5 RT TEL. Pole end Fence 40.2 RT

2+00

T.P. 9.2 C 65.85 1.77 56.59

1+50 Beg. Fence 40.3 RT.

1+45 29' RT P.P.

1+07 £ Con. porch

1+00

0+75 \$ 7.5 Con. drive + 900.

0+69 27.5 LT. end Fence

0+50 39' LT. CTR. C'du clump BANANA TREES

0+38 26' LT. end hedge + Beg. wire fence

58.36

57.25 8.5 40	57.85 8.0 22	56.75 9.1 15	57.65 8.7	56.65 9.0 15	58.05 7.8 20	58.45 7.4 40	LEAN TO door SILL TOOL SHED
55.96 2.4 40	56.36 2.0 20	55.86 2.5 16	56.46 1.9	55.76 2.0 15	56.56 1.8 19	57.16 1.7 40	
57.66 0.80 41 Con. Porch		55.26 4.1 41 ground					
55.46 2.9 40	55.56 2.8 23	54.56 3.8 15	55.06 3.3	54.36 4.0 15	55.76 2.0 18	56.26 2.1 40	
54.72 3.6x 4x.5 900.	54.72 3.5x 40 drive	54.67 3.09 27.3 drive			12" TEL. POLE 29		
54.36 4.0 40	54.66 3.7 23	53.16 5.2 15	54.06 4.3	53.36 5.0 16	55.06 3.3 21	55.26 3.1 40	
							58.36

Dawes
 33' Rt 14" di. Eucal. tree
 1+25 40' Lt end picket fence

1+21

0+97

0+81 40.2 Rt. end fence ^{Bd.}

0+64 40' Lt. Beg. picket fence

0+50

0+22 29.5 Rt P.P.

0+18 29.5 Rt. Tel Pole

0+00 N.L. Missouri

2+70.3 S.L. Missouri St.

2+35

65.85

Lt=W

8

Rt=E

8

63.95 1.9 40	64.45 1.2 20	63.85 2.0 16	64.35 1.5	63.75 2.1 15	64.95 0.9 19	65.05 0.8 40	65.20 0.25 end 41.8 Can. Yard
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63.15 2.7 40	63.65 2.2 20	63.75 2.1 15	63.25 2.3	63.85 3.0 15	63.85 2.0 20	63.65 1.2 40	65.10 0.75 Beg 41.8 Can Yard
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61.95 3.9 40	62.15 2.2 18	61.45 2.2 15	62.25 3.0	61.95 2.9 12	62.25 2.1 19	62.55 2.3 40
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60.65 5.2 40	61.05 4.8 20	60.55 5.3 15	61.25 4.0	60.85 5.0 12	61.45 4.4 18	61.75 4.1 40	87 40.2 8d fence
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59.85 6.8 40	59.65 6.2 20	58.85 7.0 12	59.45 5.2	58.95 6.9 15	59.85 6.0 22	60.35 5.5 40
--------------------	--------------------	--------------------	--------------	--------------------	--------------------	--------------------

58.05 7.8 40	58.75 7.1 20	57.85 8.0 15	58.65 7.2	57.85 8.0 12	59.15 6.7 22	59.65 6.2 40
--------------------	--------------------	--------------------	--------------	--------------------	--------------------	--------------------

65.85

Doves

2+35

2+07 3' Cor. walk

2+00

1+91 2 do. 1.5 Cor. Rib. drive 7' overcall

1+85 N end 6' Cor. Ret wall

1+45 28.5 ft. P.P.

T.P. 7.47 72.67 0.65 65.20
15.85

LT=W

E

RT=E

9

66.97	67.87	66.47	67.47	69.17	67.87	67.75	68.47
5.7	4.8	6.2	5.2	5.5	4.8	4.92	4.2
40	21	14		15	19	30	40

E. edge
5' walk

66.92	66.60	68.07
5.75	5.07	4.60
30	40	50

E. edge
5' walk 2' walk 3' walk

66.37	66.67	67.47	66.47	67.87	66.87	66.77	67.47
6.3	6.0	7.2	6.2	5.8	5.8	5.96	5.2
40	21	14		15	20	30	40

E. edge
5' walk

66.47	67.17	67.57
6.20	5.5	5.1
30	40	50

E. edge
5' walk Low Bet.
Ribbons

66.32	67.25
6.35	5.42
30	30

5' walk
E. edge Top wall

64.67	64.97	64.47	65.07	64.67	65.37	65.42	66.61	66.65	65.95
8.0	7.8	8.2	7.6	8.0	7.3	7.25	6.0	6.07	6.7
40	18	14		17	23	30	30	40	40

E. edge
5' walk 30' top
Ret. wall

72.67

0+76 E 14' Con. apron + 900. Con FL.

0+50

T.P. 5.94 77.84 0.77 71.90

0+32.5 E Con. steps

0+100 N.L. Chalcedony

2+70.1 S.L. Chalcedony 28' to P.P.

7+48 E 3' Con. walk

72.67
✓

572.22
5.24
40.00
900

772.00
1.84
38.5
900

71.34
5.5
40

71.54
5.3
23

70.54
7.3
10

71.34
5.5

71.14
5.7
15

70.34
7.5
17

72.64
5.2
19

72.74
5.1
20

77.84

71.36
1.31
47.4
Top
Con. steps

70.87
1.8
42.4
ground

70.17
2.5
40

70.27
2.0
22

69.27
2.4
14

70.37
2.3

70.07
2.5
17

71.37
1.0
19

71.37
1.3
20

67.97
4.7
40

68.77
3.9
21

67.27
5.4
15

68.77
4.5

67.67
4.0
15

68.67
4.0
19

68.87
3.81
30

69.57
3.1
40

E edge
and at end
5' Con. walk

68.11
4.50
30
E edge
5' walk

68.80
3.87
40

69.25
3.44
50

3' walk

72.67
✓

Dawes

P. 5

Check to spike BM, NE Con.

Missouri + Dawes 8.28 6.19 6.18

T.P. 1.11 70.47 8.48 69.36

2 + 70 S.L. LAW ST.

2 + 35

2 + 07 P 14.5 Con. apron + 900.

2 + 00

1 + 50

1 + 00

77.84

LTN

+

P = E

11

74.74
3.1
40

74.14
3.7
16

75.04
2.8

74.44
3.6
15

75.24
3.6
20

75.74
3.1
40

74.24
3.6
40

73.84
4.0
17

74.54
3.3

74.04
3.8
16

74.74
3.1
18

75.04
2.8

74.01
38.3
49.3
900

73.93
39.3
Apron

73.94
4.0
40

73.64
4.2
19

73.24
4.5
16

74.14
3.7

73.04
4.6
16

74.54
3.3
19

74.64
3.2
40

73.04
4.8
40

72.84
4.9
17

72.64
5.2
15

72.84
4.5

72.84
4.9
16

74.24
4.6
20

74.34
4.4
40

73.04
5.8
40

72.04
5.8
19

71.44
6.4
15

72.84
5.5

71.94
5.9
15

70.74
7.1
17

72.04
6.8
40

72.04
6.4
40

77.84

x sec. Missouri St.

Excavations to Ocean

W.O. #1189

1+15

3' con. walk

1+00

INDEXED

W.K.

JUL 20 1949

0+88

end pav. obs etc

0+10

Curb Ret. E.C.

0+00

W.K. Events

set BM. SW. 7' LD. CT.

Missouri and Events

446

4701

T.P.

5.63

71.47

0.70

65.84

71.47

BM spike

4.36

66.54

62.8

Missouri
DAMES

Tel. P. W. E. Co.

LT = South

♀

Rt = A

12

66.67

4.8
40

66.67

4.8
23

66.67

5.8
15

66.77

4.7

67.37

4.1
19

67.67

3.8
30

68.83

2.44
39.8

walk

66.77

4.7
40

66.77

4.7
24

65.87

5.6
15

66.67

4.0

67.27

4.2
20

68.77

2.7
40

66.77

4.7
40

66.93

4.54
20

66.77

4.15
20

66.99

5.48
10

66.28

5.19

66.40

5.07
10

66.19

5.28
20

66.88

4.59
20

67.27

4.2
35

68.77

2.7
210

67.00

4.67
20

66.28

4.13
20

66.90

4.57
10

67.20

4.17

67.45

4.02
10

67.29

4.18
20

67.81

3.00
20

3+50

3+42 E 7' Con. dr.

T.P. 2.89 66.39 7.97 63.50

3+00

2+91 E 7.5 Con. drive

2+50

2+38 E 3' di. PALMA 30' Pt

2+41 E 7.5 Con. drive

2+25 E 3.3 Con. walk

2+00

1+91 E 6.5 Con. drive

1+50

71.47

LT=5

RT=N

13

62.39
4.0
40

62.59
3.8
30

62.99
3.5
12

62.39
4.0
7

62.59
3.8

62.89
3.5
20

62.79
3.0
30

62.99
2.0
40

62.69
3.70
39.8

62.87
8.0
40

62.67
7.8
11

62.17
8.0
5

66.39

62.37
8.1

62.97
7.5
20

64.87
6.0
40

62.87
7.0
40

64.27
7.1
13

62.87
7.0
11

64.47
7.0

64.97
6.5
20

65.87
5.0
30

66.57
4.9
40

66.407
7.40
40

64.47
7.0
40

65.17
6.3
16

64.67
6.8
15

65.17
6.3

65.57
7.9
20

66.68
35.3
walk

66.37
7.1
35

66.37
6.4
40

66.68
4.79

66.70
4.77

65.87
5.0
40

66.07
5.4
16

65.87
5.0
15

66.17
5.3

66.67
4.8
20

67.68
3.79
33

67.37
3.0
40

71.47

0718

0700
4+99.9 = E.L. Davies

4+91 E 7.5 Con, dn.

4+77 25' LT 5" di. PALM

4+56 E 4' Con. WALK

4+50

4+40 E 7.5 Con. down

4+00

2+90 E 7' Con. down

11.39

$\begin{array}{r} 60.89 \\ 5.1 \\ \hline 55.79 \end{array}$	$\begin{array}{r} 60.09 \\ 5.3 \\ \hline 54.79 \end{array}$	$\begin{array}{r} 60.09 \\ 5.3 \\ \hline 54.79 \end{array}$	$\begin{array}{r} 60.29 \\ 5.1 \\ \hline 55.19 \end{array}$	$\begin{array}{r} 60.69 \\ 5.1 \\ \hline 55.59 \end{array}$	$\begin{array}{r} 61.29 \\ 5.1 \\ \hline 56.19 \end{array}$	$\begin{array}{r} 61.39 \\ 5.1 \\ \hline 56.29 \end{array}$
$\begin{array}{r} 60.29 \\ 6.1 \\ \hline 54.19 \end{array}$	$\begin{array}{r} 60.29 \\ 5.8 \\ \hline 54.49 \end{array}$	$\begin{array}{r} 60.19 \\ 6.1 \\ \hline 54.09 \end{array}$	$\begin{array}{r} 60.19 \\ 5.2 \\ \hline 54.99 \end{array}$	$\begin{array}{r} 60.79 \\ 5.1 \\ \hline 55.69 \end{array}$	$\begin{array}{r} 61.49 \\ 5.9 \\ \hline 55.59 \end{array}$	$\begin{array}{r} 61.69 \\ 4.7 \\ \hline 56.99 \end{array}$

$\begin{array}{r} 60.79 \\ 5.1 \\ \hline 55.69 \end{array}$	$\begin{array}{r} 61.39 \\ 5.2 \\ \hline 56.19 \end{array}$	$\begin{array}{r} 61.19 \\ 5.1 \\ \hline 56.09 \end{array}$	$\begin{array}{r} 61.09 \\ 5.3 \\ \hline 55.79 \end{array}$	$\begin{array}{r} 61.09 \\ 5.3 \\ \hline 55.79 \end{array}$	$\begin{array}{r} 61.79 \\ 5.1 \\ \hline 56.69 \end{array}$	$\begin{array}{r} 62.19 \\ 5.2 \\ \hline 56.99 \end{array}$
---	---	---	---	---	---	---

$\begin{array}{r} 61.12 \\ 5.7 \\ \hline 55.42 \end{array}$

$\begin{array}{r} 61.49 \\ 4.7 \\ \hline 56.79 \end{array}$	$\begin{array}{r} 61.99 \\ 4.4 \\ \hline 57.59 \end{array}$	$\begin{array}{r} 61.69 \\ 4.7 \\ \hline 56.99 \end{array}$	$\begin{array}{r} 61.79 \\ 4.0 \\ \hline 57.79 \end{array}$	$\begin{array}{r} 61.79 \\ 4.0 \\ \hline 57.79 \end{array}$	$\begin{array}{r} 62.59 \\ 5.0 \\ \hline 57.59 \end{array}$	$\begin{array}{r} 62.99 \\ 5.0 \\ \hline 57.99 \end{array}$
---	---	---	---	---	---	---

$\begin{array}{r} 61.95 \\ 4.4 \\ \hline 57.55 \end{array}$

11.39

0 + 50 Bag. picket fence 30' RT.

B.M.

0.39 62.57 62.18

check to BM Daws
1120 62.19 62.18
0.01

$\frac{0+00}{0+80} = W.L. Daws$

0 + 60

0 + 54

0 + 40 = Daws

0 + 24

66.39

LT=5
58.67
3.9
40
2
58.17
4.0
11
58.57
4.0
20
59.19
3.2
20
R₂=N
60.99
1.4
40

62.57

59.09
7.3
40
10.59.59
11.8
11
58.17
2.2
8
59.29
7.1
20
60.09
1.3
20
60.59
5.5
40

59.79
6.6
40
59.79
6.6
30
60.19
5.2
15
59.89
7.5
20
59.79
6.6
20
60.29
5.1
20
60.99
5.2
40
61.19
5.7
40

58.89
11.8
50
59.49
11.8
20
59.99
6.5
20
60.09
5.3
20
60.59
5.7
40

59.39
5.0
20
59.89
6.5
20
60.39
6.0
20
60.89
5.7
20
61.2
5.2
40

59.09
7.3
40
59.59
6.8
27
59.59
6.8
20
58.89
6.5
20
60.59
5.9
20
61.09
5.3
33
61.29
5.7
40

66.39

2 + 50

1 + 99.3

1 + 49.5

1 + 39

E do. 2' Com. Rib. Dr. 7' wide access

1 + 00

0 + 94 E 7.5 Con. do.

0 + 90 End Picket fence 36 RT

L 25

$\begin{array}{r} 55.07 \\ 7.5 \\ \hline 40 \end{array}$	$\begin{array}{r} 55.67 \\ 7.9 \\ \hline 46 \end{array}$	$\begin{array}{r} 55.67 \\ 7.5 \\ \hline 43 \end{array}$	$\begin{array}{r} 55.87 \\ 7.2 \\ \hline 48 \end{array}$	$\begin{array}{r} 55.99 \\ 8.0 \\ \hline 20 \end{array}$	$\begin{array}{r} 56.37 \\ 8.7 \\ \hline 22 \end{array}$	$\begin{array}{r} 56.57 \\ 8.0 \\ \hline 40 \end{array}$
--	--	--	--	--	--	--

$\begin{array}{r} 55.57 \\ 7.0 \\ \hline 40 \end{array}$	$\begin{array}{r} 55.57 \\ 7.6 \\ \hline 46 \end{array}$	$\begin{array}{r} 55.67 \\ 7.1 \\ \hline 43 \end{array}$	$\begin{array}{r} 55.97 \\ 7.1 \\ \hline 48 \end{array}$	$\begin{array}{r} 56.37 \\ 7.7 \\ \hline 20 \end{array}$	$\begin{array}{r} 57.09 \\ 5.48 \\ \hline 20 \end{array}$	$\begin{array}{r} 57.07 \\ 5.5 \\ \hline 40 \end{array}$
--	--	--	--	--	---	--

$\begin{array}{r} 56.17 \\ 6.4 \\ \hline 40 \end{array}$	$\begin{array}{r} 56.57 \\ 6.0 \\ \hline 46 \end{array}$	$\begin{array}{r} 56.17 \\ 6.4 \\ \hline 41 \end{array}$	$\begin{array}{r} 56.37 \\ 6.2 \\ \hline 48 \end{array}$	$\begin{array}{r} 56.87 \\ 5.7 \\ \hline 20 \end{array}$	$\begin{array}{r} 57.87 \\ 4.74 \\ \hline 20 \end{array}$	$\begin{array}{r} 57.77 \\ 4.8 \\ \hline 40 \end{array}$
--	--	--	--	--	---	--

$\begin{array}{r} 57.74 \\ 4.83 \\ \hline 36 \end{array}$	$\begin{array}{r} 57.74 \\ 4.83 \\ \hline 40 \end{array}$
---	---

$\begin{array}{r} 57.07 \\ 5.5 \\ \hline 40 \end{array}$	$\begin{array}{r} 57.47 \\ 5.1 \\ \hline 31 \end{array}$	$\begin{array}{r} 57.27 \\ 5.3 \\ \hline 43 \end{array}$	$\begin{array}{r} 56.77 \\ 5.8 \\ \hline 41 \end{array}$	$\begin{array}{r} 57.57 \\ 5.3 \\ \hline 48 \end{array}$	$\begin{array}{r} 57.77 \\ 4.8 \\ \hline 20 \end{array}$	$\begin{array}{r} 58.47 \\ 4.1 \\ \hline 40 \end{array}$
--	--	--	--	--	--	--

$\begin{array}{r} 58.03 \\ 3.74 \\ \hline 36 \end{array}$	$\begin{array}{r} 58.96 \\ 3.61 \\ \hline 40 \end{array}$
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L 25

4+35.5 Bcg. Can. BLK. WALL 40' LT

4+34 E 3' Can walk

4+00

3+64 E do 2' Can Rib. dr.

3+50

3+45 E 3' Can walk

3+19 E 2' do Can Rib. Dr. 7' overall

3+00

T.P. 247 58.26 680 55.77
62.57

LT=5

8

R=N

1

40	53.26	53.06	53.03	53.16	54.16	54.56
X0	53.26	53.06	53.03	53.16	54.16	54.56
	4.8	4.8	4.8	4.1	5.8	3.7
	20	20	17	20	21	40

40	53.66	54.26	53.46	54.26	55.06	55.86
X0	53.66	54.26	53.46	54.26	55.06	55.86
	4.8	4.9	4.8	4.8	4.8	4.8
	20	21	17	20	25	40

35	55.89	56.10
X0	55.89	56.10
	2.2	2.1
	35	50

34	56.16	56.22
X0	56.16	56.22
	2.0	1.9
	34	40

40	54.36	54.96	54.26	54.96	55.56	56.06
X0	54.36	54.96	54.26	54.96	55.56	56.06
	3.9	3.8	4.0	3.8	2.7	1.7
	40	17	15	33	20	50

58.26

0+27 13' oil drive + gas

0+00 W.L. Cass St.

0-14 W. 26. Cass St

T.P. SW. 7/67

Man + Cass 373 54.75 6.7x 51.54 51.54

5+129 = E 26 Cass

4+989 E.L. Cass St. Pav. edge
and end Con. Blk. wall 40' LT

4+50

5826

LT-5

51.45	51.48	51.15	51.56	51.89	51.97	51.83	52.46	52.85
33	327	260	219	282	278	292	229	1.9
40	20.9	20.9	10	10	10	20.9	20.9	40
	06	97				97	97	
51.34	50.91	51.52	51.79	52.06	52.27	52.38	52.54	52.89
41	382	323	272	219	248	237	221	1.80
40	40	20	10	10	10	20	20	40
06	97					97	97	06

51.95	51.12	51.57	51.72	51.94	52.12	52.28	52.55	52.88
6.31	714	6.09	6.54	6.32	6.14	5.98	5.51	4.78
40	40	20	10	10	10	20	10	40
06	97						97	06

52.06	52.43	51.92	52.19	52.35	52.44	52.46	53.05	53.46
5.7	5.83	6.34	6.07	5.91	5.87	5.80	5.21	4.8
40	20.9	20.9	10	10	10	20.9	20.9	40
	06	97				97	06	

52.56	52.96	52.26	52.86	53.56	53.86
5.7	5.3	5.9	4.5	4.7	4.4
40	20	19	40	20	40

5826

51.75
20
10
06

R-5245-11
2.3
40
06

52.37
1.38
22.4
900
06

54.75

1479 E 3' Con. walk

1459 E do. v. con. rib. 7' wide

1450

1431 E 3' Con. walk

1409 E v. do. Con. Rib. Pa. 7' Wide

1400

0+52 E 2.5' Con. walk

54.75

L=5

E

5027
452
R_T-N

19

49.65 C.1 40	49.75 5.0 15	49.45 4.7 11	49.75 5.0	49.65 5.1 12	50.25 4.8 18	50.45 4.3 40
--------------------	--------------------	--------------------	--------------	--------------------	--------------------	--------------------

5027
4.0
39.8

51.05
3.70
40

50.55 5.2 40	50.05 4.7 18	49.95 4.8 11	50.25 4.5	50.35 4.4 14	51.05 3.7 40
--------------------	--------------------	--------------------	--------------	--------------------	--------------------

50.25 4.5 40	50.75 4.0 17	50.65 4.1 12	50.95 3.8	51.05 3.7 14	51.65 3.1 18	51.85 2.90 208	52.32 2.43 40
--------------------	--------------------	--------------------	--------------	--------------------	--------------------	----------------------	---------------------

54.75

work

No.

L = S

F

R = N

20

3 + 00

49.65
5.1
40

49.45
7.0
42

49.25
7.5
41

49.05
7.2
42

48.75
7.0
41

48.25
5.5
41

48.75
5.0
40

2 + 80 F 3' Con. walk

49.17
5.5
40

2 + 59 F do. 2nd Con. Rib. do 7 wide

49.34
5.7
40

2 + 50

49.25
7.5
40

48.25
5.5
42

48.05
5.7
41

48.25
5.5
42

48.15
5.0
45

48.65
5.1
40

49.25
7.5
40

2 + 09 F do. 2nd Con. Rib. do 7 wide

49.93
5.8
40

2 + 00

49.05
5.7
40

48.95
5.8
41

48.75
5.0
41

49.05
5.7
42

48.95
5.8
45

49.65
5.1
41

49.95
5.8
40

54.75

54.75

4117 Q 3' CON WALK

rNo.

4109 Q do. 27' Con Rib Dr. 7' wide

4100 END CON. BRICK WALL 40' RT.

3198 END LATH FENCE 40, LT

3179 Q 3' CON. WALK

3175 Beg. LATH FENCE 40 LT

3158 Q 8.5' CON. DRIVE

3150 Beg. CON. BRICK WALL 40' RT

3109 Q do. 27' Con Rib, dr. 7' wide

T.P. 291 50.55 7.10 47.65

54.75

LT=5 46.40

5.16

42

R=N

21

46.76

4.8

40

46.76

4.5

15

46.26

4.3

8

46.46

4.1

46.36

4.2

10

47.06

3.5

21

47.56

3.0

40

47.48
3.08
39.5

47.48
3.08
39.5

47.93
2.53
40

46.06

4.5

40

46.86

3.7

11

46.76

3.8

9

46.96

3.5

46.96

3.6

17

47.46

3.1

22

47.66

2.9

40

48.57
1.99
40

50.55

Mo.

5 + 25.55

5 + 14.55

5 + 00.55 E.L. Bayard St

4 + 06 @ 3' Con. walk

4 + 50

4 + 30 @ 3' Con. walk

50.56

L = S

@

R = N

22

44.16
10

45.76
10

44.76
10

44.76
10

45.06
10

45.76
10

46.06
10

44.46
10

45.26
10

44.76
10

45.06
10

45.76
10

45.76
10

46.16
10

44.46
10

45.16
10

44.96
10

45.26
10

45.26
10

45.76
10

46.36
10

46.96
10

44.96
10

45.86
10

45.76
10

45.96
10

45.96
10

46.26
10

46.96
10

47.39
10

50.56

M.O.

$\frac{0+00}{5+80.55} =$ w.L. Bayard St. Beg. Lark fence
39.5 Ft.

5+60.55

5+60.5

5+40.55 E Bayard

5+33.5

5+28.55

50.56

L = S

R

R = N

23

$\frac{44.86}{5.7}$ 40	$\frac{44.46}{5.1}$ 15	$\frac{44.26}{5.3}$ 5	$\frac{44.26}{5.2}$ ✓	$\frac{44.86}{5.7}$ 20	$\frac{45.26}{5.0}$ 22	$\frac{45.76}{4.8}$ 8
---------------------------	---------------------------	--------------------------	--------------------------	---------------------------	---------------------------	--------------------------

$\frac{44.06}{5.5}$ 40	$\frac{44.66}{5.9}$ 15	$\frac{44.16}{5.2}$ 5	$\frac{44.26}{5.2}$ ✓	$\frac{44.66}{5.7}$ 20	$\frac{45.66}{5.9}$ 22	$\frac{45.76}{5.8}$ 8
---------------------------	---------------------------	--------------------------	--------------------------	---------------------------	---------------------------	--------------------------

$\frac{44.86}{5.7}$ 40	$\frac{44.26}{5.3}$ 15	$\frac{44.16}{5.2}$ 5	$\frac{44.16}{5.2}$ ✓	$\frac{44.46}{5.6}$ 20	$\frac{44.86}{5.7}$ 22	
---------------------------	---------------------------	--------------------------	--------------------------	---------------------------	---------------------------	--

$\frac{44.26}{5.2}$ 40	$\frac{43.96}{5.5}$ 15	$\frac{44.56}{5.0}$ 5	$\frac{44.56}{5.0}$ ✓	$\frac{45.06}{5.7}$ 20	$\frac{45.46}{5.9}$ 22	
---------------------------	---------------------------	--------------------------	--------------------------	---------------------------	---------------------------	--

$\frac{43.66}{5.9}$ 40	$\frac{44.16}{5.2}$ 15	$\frac{44.66}{5.7}$ 5	$\frac{44.66}{5.7}$ ✓	$\frac{44.96}{5.9}$ 20	$\frac{45.36}{5.7}$ 22	
---------------------------	---------------------------	--------------------------	--------------------------	---------------------------	---------------------------	--

$\frac{44.46}{5.3}$ 40	$\frac{44.26}{5.3}$ 15	$\frac{44.46}{5.1}$ 5	$\frac{44.46}{5.1}$ ✓	$\frac{44.86}{5.7}$ 20	$\frac{45.06}{5.9}$ 22	
---------------------------	---------------------------	--------------------------	--------------------------	---------------------------	---------------------------	--

50.56

170.

T.P. 390 46.93 7.53 43.03

1+26 End Picket fence 28.8 LT.

1+21 E 40" Cypress 30 LT

1+15 E 18" Cypress 30 LT

1+09 E 12" Cypress 30 LT.

1+04 E 18" Cypress 30' LT.

1+00 End Lark fence 40' RT

0+94 E 3.5 Con. Walk

0+50 Beg. Picket Fence 30' LT.

0+17 E 3' Brick Walk

Fd. & Set BM, Con. Man. S.W. Con.
Missouri & Bayard50.56

L-25

P-N

24

$\begin{array}{r} 43.16 \\ 7.4 \\ \hline 40 \end{array}$	$\begin{array}{r} 43.26 \\ 7.3 \\ \hline 29 \end{array}$	$\begin{array}{r} 43.26 \\ 7.2 \\ \hline 18 \end{array}$	$\begin{array}{r} 43.26 \\ 7.3 \\ \hline 8 \end{array}$	$\begin{array}{r} 43.26 \\ 7.0 \\ \hline 20 \end{array}$	$\begin{array}{r} 43.86 \\ 5.7 \\ \hline 20 \end{array}$	$\begin{array}{r} 44.56 \\ 5.0 \\ \hline 27 \end{array}$	$\begin{array}{r} 44.76 \\ 5.8 \\ \hline 20 \end{array}$
--	--	--	---	--	--	--	--

$\begin{array}{r} 43.15 \\ 7.41 \\ \hline 40 \\ \text{Walk} \end{array}$	$\begin{array}{r} 43.22 \\ 7.14 \\ \hline 29.3 \\ \text{Walk} \end{array}$
--	--

$\begin{array}{r} 43.26 \\ 7.3 \\ \hline 40 \end{array}$	$\begin{array}{r} 43.56 \\ 7.0 \\ \hline 30 \end{array}$	$\begin{array}{r} 44.16 \\ 6.4 \\ \hline 10 \end{array}$	$\begin{array}{r} 43.76 \\ 6.2 \\ \hline 8 \end{array}$	$\begin{array}{r} 43.96 \\ 6.0 \\ \hline 20 \end{array}$	$\begin{array}{r} 44.36 \\ 5.2 \\ \hline 20 \end{array}$	$\begin{array}{r} 44.06 \\ 5.5 \\ \hline 27 \end{array}$	$\begin{array}{r} 44.56 \\ 5.0 \\ \hline 20 \end{array}$
--	--	--	---	--	--	--	--

$$\begin{array}{r} 45.63 \\ 4.93 \\ \hline 39.5 \end{array}$$
50.56

170.

4

+50 End LatA fence 21.7 LT.

3

Boq. LatA fence 22 LT.

+50

1

+50

46.93

4-5

4

Pt=N

25

40.73	41.53	41.03	41.33	41.43	42.43
5.2	5.2	5.9	5.2	5.5	5.5
80	10	8	5	15	10
41.13	41.73	41.53	41.53	41.83	42.63
5.8	5.2	5.6	5.4	5.1	5.0
40	17	7	7	20	10
41.43	42.03	41.73	41.93	42.03	42.53
5.5	5.0	5.2	5.0	5.0	5.2
10	10	5	5	10	8
41.53	42.43	42.03	42.23	42.53	43.33
5.2	5.0	5.0	5.2	5.0	5.0
40	10	7	7	15	10
42.03	42.83	42.43	42.53	42.83	43.53
4.9	5.1	5.5	5.2	5.1	5.0
40	10	7	4	10	10
42.33	43.13	42.83	43.03	42.43	43.73
4.6	3.8	5.1	3.9	3.5	3.2
40	10	8	3	17	19
			46.93		

Mo.

0-10 W. cb. Line Mission Blvd.

N.W. 7' CT.

T.P. 2.67 43.16 40.49 ✓

N.E. Con. Mission
check to BMBP & Choleady 0.57 48.49 48.49
0.00

7' T.P. CT. 8.52 49.01 6.44 40.49 ✓ T. Id +

? 5' 10" 10'?

✓ E. cb Line Mission Blvd.

4 + 99.84 E.L. Mission Blvd. edge Pav.

4 + 80

4 + 50

40.93

L7-5

±

RT = N

39.47	38.91	39.19	39.37	39.50	39.60	39.69	39.98	39
3.73	4.25	3.97	3.83	3.66	3.55	3.47	3.18	2.61
40	40	20	10	10	10	20	40	40
cb	9T						9T	cb

43.16

39.95	39.26	39.26	39.80	39.92	40.08	40.19	40.40	41.08
6.98	7.57	7.27	7.13	7.01	6.85	6.76	6.53	6.29
40	40	20	10	10	10	20	40	40
cb	9T						9T	cb

40.03	40.14	39.60	40.04	40.29	40.36	40.38	40.98	41.13
6.9	6.79	7.23	6.89	6.64	6.57	6.55	6.95	6.78
40	20	20	10	10	10	20	20	40
		9T				9T	9T	

40.33	40.73	40.13	40.47	40.77	41.17	41.83
6.6	6.3	6.6	6.5	6.2	6.5	6.1
40	20	20	20	20	20	40

40.53	41.23	40.63	40.87	41.03	41.53	41.83
6.7	6.7	6.3	6.1	6.9	6.4	6.1
40	20	20	20	20	20	40

40.93

M10.

1450

1448 E 3' Con. walk

1434 7.5 wide
E Con. & gran + 992. Confl.

1400

0450

0410

0400 W.L. Mission Blvd. paved edge

43.10

L=5

2

R=N

27

57.7 50	58.16 11	57.76 5	57.76 7	58.16 19	58.46 22	58.76 50
57.66 50	58.16 13	57.76 12	58.46 11	58.86 18	59.26 21	59.56 50
57.8 40	58.26 15	58.86 12	59.06 11	59.46 17	59.86 15	59.96 50
59.26 50	59.66 20	59.46 16	59.56 15	59.96 18	40.36 22	40.46 50
59.46 37	59.70 36	59.77 22.7	59.85 10	59.87 10	59.90 22.7	40.44 22.7
40	36	77	43.10	40	40	40.66 50

3 + 45

3 + 25

2 + 85 con. walk
T.P.

4.14

42.02

57.8

37.88 ✓

3 + 00

2 + 85 E 2 con. walk

2 + 50

2 + 00

43.16

L = S

X

R = N

28

36.72

5.9
40

36.72

5.3
20

37.02 ✓

5.0
20

37.02

5.0
20

37.42

5.4
20

37.62

4.4
40

37.22

4.8
22

36.72

5.3
18

36.72

5.3
10

36.82 ✓

5.2
10

36.92

5.1
20

37.52

5.5
20

36.56

6.6
40

37.06

6.1
11

36.76

6.1
10

37.02 ✓

5.3
20

37.06

6.1
20

37.56

5.6
20

37.87

5.9
20

36.56

6.6
40

37.16

6.0
11

37.06

6.1
9

37.06 ✓

6.1
23

37.06

6.0
23

37.86

6.8
20

36.86

6.3
40

37.36

6.8
11

37.26

5.9
9

37.36 ✓

5.8
21

37.76

5.6
21

38.06

6.8
20

43.16

43.16
60
6.56

1 sec Mo.

5+14 edge cliff sec, diag

5+07 sec. diag.

4+92.48 E.L. Ocean Blvd. Sec. on diag.

4+50

4+90

3+85 Bayley to N

4207

LT = 9

A

R = N

29

36.02	36.62	37.82	36.72	37.32
C.0	5.4	5.2	9.3	9.7
40.2	20		20	40.21

35.82	36.22	36.52	36.92	38.02
5.7	5.8	5.5	5.1	4.0
40.21	20		20	40.21

35.82	36.02	36.42	36.82	37.42
C.2	6.0	5.6	5.2	4.6
40.21	20		20	40.21

36.02	35.82	36.02	36.52	37.12
5.0	5.1	5.0	4.9	5.9
40	15		20	50

36.22	37.02	36.52	36.72	37.22
5.8	5.0	5.4	5.3	4.8
40	20	15	20	50

36.12	36.62	36.52	37.12	37.42
5.9	5.4	5.5	4.9	4.5
40	8	15	20	50

4207

x sec Missouri

5+22.6 x W by Ocean Blvd. cliff

5+19 edge cliff

42.02

29.32

$\frac{12.7}{40.2}$

28.42

$\frac{13.6}{20}$

27.72 ✓

14.3

27.72

$\frac{18.3}{20}$

27.92

$\frac{14.1}{40.2}$

36.72

$\frac{5.3}{40.2}$

37.02

$\frac{5.0}{30}$

37.62

$\frac{4.4}{11}$

35.72 ✓

6.3

29.52

$\frac{12.5}{24}$

28.82

$\frac{13.2}{40.2}$

42.02

Sketch P.4

X sec N + S alley
BLK 117 Pacific Beach

1 + 45.11

1 + 35.11 E E + W alley

1 + 27 9.5 L. 9" R.R.

1 + 25.11

1 + 00

0 + 50

0 + 00 N.L. Missouri St.

T.P. 2 + 85

Con. walk

P. 28

5.91 43.79

37.88

W.O. #1189

L.T. = to west

$\frac{4.1}{10}$

39.39

3.9

$\frac{10}{10}$

39.89

3.7

$\frac{10}{10}$

40.09

4.5

$\frac{10}{10}$

39.29

5.5

$\frac{10}{10}$

38.29

6.6

$\frac{10}{10}$

37.19

0.5m

0.5

S.H.

E.B.

Indexed

c.s.k.

7-8-46

R.T.

4.4

$\frac{9}{10}$

39.39

3.89

12.8 R.R.

39.90

4.0

$\frac{10}{10}$

39.79

4.5

$\frac{10}{10}$

39.29

5.0

$\frac{10}{10}$

38.19

6.8

$\frac{10}{10}$

37.39

43.79

4.6

$\frac{9}{10}$

39.19

4.2

$\frac{10}{10}$

39.59

3.8

$\frac{10}{10}$

39.99

4.3

$\frac{10}{10}$

39.49

5.3

$\frac{10}{10}$

38.49

Cor. Rail fence

859' rail fence

N + S alley 117 P.B.

2 + 70.22 S.L. Chabcedoxy

2 + 60

2 + 40

2 + 00

1 + 85

43.79

L.T. = to West ←

Rt. 1/4

32

9.5	9.5	9.4	10.3
10		4	10
34.29	34.29	34.39	33.49

16.4	9.4	9.4	9.2	6.6
33	15	10	10	10
27.39	34.59	34.29	34.59	37.19

27.09	8.8	8.8	8.6	8.5	4.1	1.7	1.7
33	13	10		8	10	10	20
20	34.89	34.99	35.19	35.29	39.69	42.09	42.09

26.99	8.7	6.7	6.7	6.7	6.5	2.7	2.7
38	17	11	10		8	11	15
20	35.09	37.09	37.09	37.09	37.29	41.09	41.09

3.3	3.3	5.8	6.2	6.1	2.8	2.7
20	11	10		9	12	15
40.49	40.49	37.99	37.59	37.69	40.99	41.09

43.79

8 Xsec E & W alley. Sketch
Blk 117 Pac. Beach Pl

0 + 98.5 E 900. Break in Fl. elev.

0 + 77 E.L. Comp. approx + Future gas
on Rt.

0 + 50 W.L. Comp. approx + Future gas
on Rt.

0 + 11 E.L. Comp. approx + Future gas
on Rt.

0 + 00 W.L. Mission Blvd. Comp. pav. edge

0 - 10 = W of line Mission Blvd.

NEBP 0.66 49.15

48.49 Chalcedony
Mission
Blvd

LT = to South

Indexed
c.s.k.

Rt.

33

7.4 10 41.75	7.1 42.05	7.0 10 42.15	6.53 12.9 99.00 42.62	5.94 19.8 900 E.L. 43.21	5.41 19.8 990 W.L. 42.74
--------------------	--------------	--------------------	--------------------------------	--------------------------------------	--------------------------------------

7.1 10 42.05	6.9 42.25	6.7 10 42.45	6.34 16.9 99.00 42.81	5.94 19.8 900 43.21
--------------------	--------------	--------------------	--------------------------------	------------------------------

6.9 10 42.25	6.7 42.45	6.5 10 42.65	6.04 16.8 99.00 43.11	5.59 19.8 900 43.56	FL
--------------------	--------------	--------------------	--------------------------------	------------------------------	----

6.4 10 42.75	6.5 42.65	6.3 10 42.85	5.94 16.8 99.00 43.21	5.63 19.7 FL 43.52
--------------------	--------------	--------------------	--------------------------------	-----------------------------

5.99 10 43.16	6.17 10 42.98	6.27 42.88	5.74 10 43.41	5.58 10 43.57
---------------------	---------------------	---------------	---------------------	---------------------

6.31 10 42.84	6.67 10 42.48	6.48 42.67	6.29 10 42.86	5.60 10 43.55
---------------------	---------------------	---------------	---------------------	---------------------

42.84 49.15

2+25 Beg. Bd. Fence 10' LT.

2+17 € Sim. gar. Con. Fl. on LT.

1+93.5 End Con. yard slab and Beg. Con. apron + Car gar. on Rt.

1+80.5 € 1.5 sq. Bank chimney, ^{Now} Badly cracked

1+75 W.L. Con. apron + gar. also Beg. Con. yard on Rt.

1+50 9' LT. to € 9" R.P.

1+33 F.L. Con. apron + 11 Car gar. on Rt.

T.P. 3.97 45.54 7.58 111.57

1+19 W.L. Con. apron + Future gar. on Rt.

49.15

5.16
13.9
40.38

5.0 4.8 4.6 4.03 3.71
10 10 10 16.8 19.8
40.54 40.74 40.94 apron 90r
+ slab 41.83
41.51

4.96
10.5 10
made up chimney 40.58
Con. Base

5.00 4.4 4.5 4.7 3.69 3.31
10 5 10 10 16.8 19.9
40.54 41.14 41.04 41.34 apron 90r
also slab 42.23
41.85

4.3 4.0 3.9 3.48 3.29
10 10 10 16.7 19.5
41.24 41.54 41.64 42.06 42.25

45.54

7.7 7.4 7.2 6.81 6.44
10 10 10 16.0 19.8
41.45 41.75 41.95 42.34 42.71

49.15

check to RIM M.H. 5.6 39.90 39.90
P.31

3+75 E.F.L. of H + S alley

3+47 Beg. Fence 9.7 LT.
H.W. Cor. Dwelling 2 1/2 wide 11' LT.

3+40

3+24 end Bd. Fence 9.8 LT.

3+00 also Beg. Bd. Fence 9.8 LT.
8" P.P. 9.8 LT.

2+88 19' Dwelling Cor. F.L.

2+74 End Bd fence 10.3 LT.

2+50

2+35.5 W.L. Cor. apron + 4 Car gas on R

45.54

5.6	5.0	5.1
<u>10</u>		<u>10</u>
39.94	39.54	39.44

5.7	5.7	5.3
<u>10</u>		<u>10</u>
39.84	39.84	40.24

5.0	5.0	4.5
<u>10</u>		<u>10</u>
40.54	40.54	41.04

5.11
<u>13.2</u>
40.43

5.4	5.1	4.8
<u>10</u>		<u>10</u>
40.14	40.44	40.74

5.3	5.1	4.7	4.05	3.66
<u>10</u>		<u>10</u>	<u>14.8</u>	<u>19.8</u>
40.24	40.44	40.84	apron	900
			41.04	41.88
			<u>45.54</u>	

X sec alley Blk 170 Pac Beach

W.O. # 1189

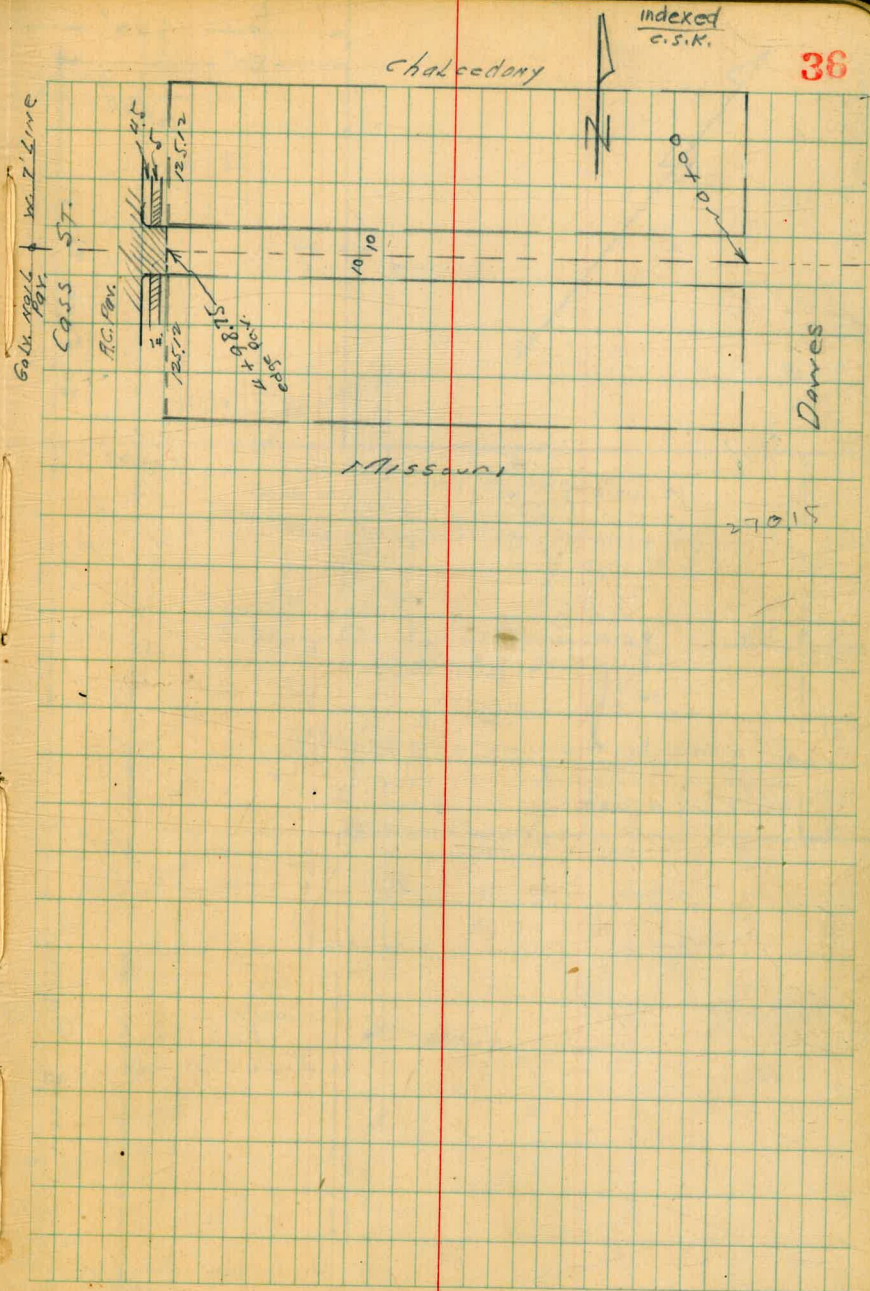
See notes in 1723/2

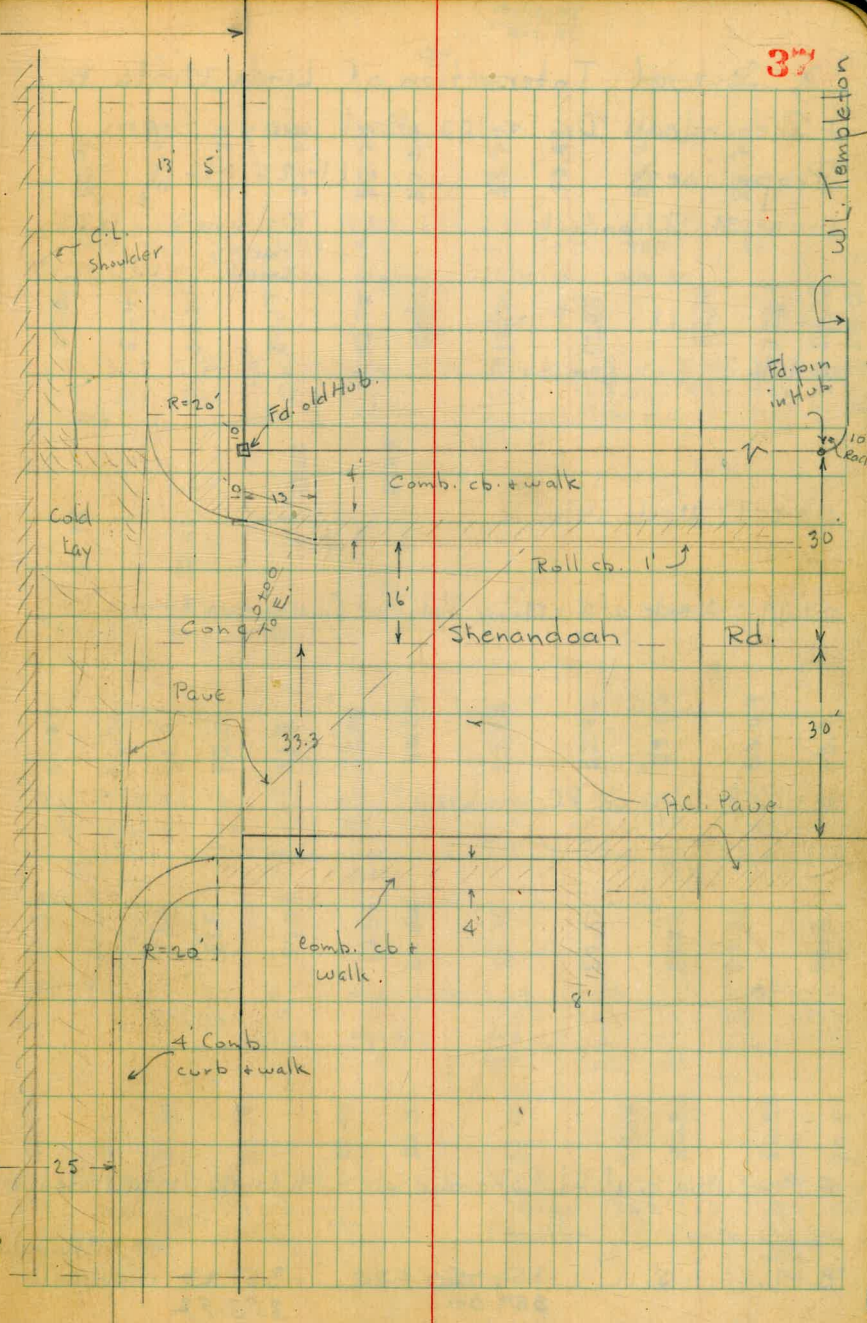
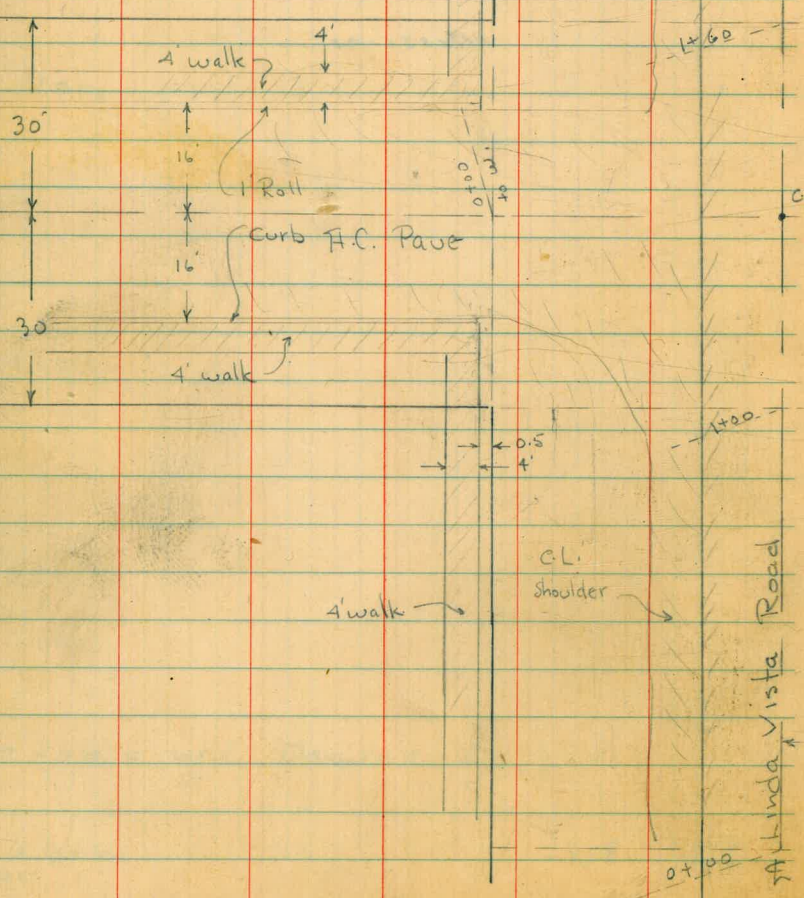
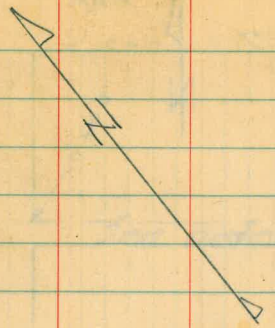
0 + 00 = W.L. Dawes St.

N.E. Spike
RP
Dawes and
170.

62.18

P. 5





377
Templeton

1+10

1+70 = opp. PC. on Rt.

1+60 = N.L. Shenandoah

1+54 = 4.3 Rt. = Tel. pole

1+50 = opp. PC. Cb. return on E.

1+46 = N. cb. - Top of Roll - E. + W.

1+30 = Shenandoah

1+14 = Top of Roll cb. to W.

52.90	52.78	52.73	52.72	52.94	52.99	53.34
6.14	6.26	6.31	6.32	6.10	6.05	5.10
57.5	57.5	57.5	57.5	57.5	57.5	57.5
CL	walk	Cor. walk	edge walk	CL	CL	CL
53.58	53.50	53.42	53.03	53.65	53.65	54.09
5.46	5.54	5.62	5.71	5.17	5.17	4.9
15	16	17	30	15	15	15
CL	edge	edge	edge	edge	edge	edge
53.84	53.75	53.72	53.59	53.87	53.87	54.33
5.20	5.19	5.32	5.32	5.17	5.17	4.11
9.9	10	10	10	10	10	9.8
edge	edge	edge	edge	edge	edge	edge
53.91	53.8	53.80	53.61	53.96	53.96	54.39
5.13	5.20	5.14	5.43	5.08	5.08	4.65
13	20	14	43	8	8	6.5
edge	edge	edge	edge	edge	edge	edge
53.74	53.68	53.64	53.48	53.84	53.84	54.20
5.30	5.36	5.40	5.56	5.20	5.20	4.84
10.1	10	10	16	10	10	9.1
edge	edge	edge	edge	edge	edge	edge
53.40	53.37	53.28	53.21	53.80	53.80	54.04
5.64	5.72	5.76	5.83	5.24	5.24	5.00
29.7	29.1	29.6	28.6	18.5	18.5	17
Conc.	Conc.	Conc.	Conc.	Conc.	Conc.	Conc.
53.44	53.49	53.31	53.24	53.44	53.44	53.8
5.60	5.55	5.53	5.52	5.60	5.60	5.2
33.1	34.1	33.3	32.2	33.1	33.1	30.2
edge	edge	edge	edge	edge	edge	edge
53.98	54.01	54.02	54.02	53.93	53.93	54.30
5.66	5.70	5.70	5.70	5.66	5.66	5.1
33.1	34.1	33.3	32.2	33.1	33.1	30.2
Top cb.	Top cb.	Top cb.	Top cb.	Top cb.	Top cb.	Top cb.
54.04	54.11	54.02	54.02	54.06	54.06	54.47
5.00	4.93	4.93	4.93	4.98	4.98	4.5
43.1	43.1	43.1	43.1	43.1	43.1	43.1
walk	walk	walk	walk	walk	walk	walk
54.11	54.12	54.12	54.12	54.12	54.12	54.52
4.92	4.92	4.92	4.92	4.92	4.92	4.5
43.1	43.1	43.1	43.1	43.1	43.1	43.1
walk	walk	walk	walk	walk	walk	walk
54.0	54.0	54.0	54.0	54.0	54.0	54.34
5.0	5.0	5.0	5.0	5.0	5.0	4.7
5.0	5.0	5.0	5.0	5.0	5.0	5.0

2+60 = 100' N. of N.H. = end

2+36 - 3.2' Rt. = Φ Tel. pole

2+35 - 3.5' Rt. = Φ Tel. booth 3.6' x 3.6' Conc. base

54.17	54.22	54.14	54.2	54.67	54.71	54.80	54.68	54.54	54.2	54.81	54.99	55.00	54.9
4.87	4.22	4.8	4.8	4.37	4.33	4.24	4.36	4.50	4.8	4.23	4.5	4.4	4.1
54.5	55	54.0	54.0	54.0	54.0	54.0	54.0	54.0	54.0	54.0	54.0	54.0	54.0
				Cl. edge	Conc.		Conc. edge	Cl.	got	Top cb.	Walk		50

359.04

52.33
40.2
3.5
Top conc.
base

Lt

Rt

Rt.

40

1+60 = end.

54.3

4.9
30

54.24

1.99
20
walk

54.18

50.5
6
top

53.57

5.5
6
top

53.83

5.40

53.90

5.33
0

54.05

5.18
0

54.19

5.04
27.1 = edge
A.C.

359.23

Lt.

#

Rt.

42

Shenandoah from W.L. Linda Vista Rd. to
 100 W. - Φ of 60 St = base Line
 0+00 = W.L. Shenandoah

INDEXED

1+00 = end.

0+50

0+15

0+04.5 = W. side of Walks

0+00.5

= E. edge of walk along
 Linda Vista Rd.

Lt = S.

Rt = N.

43

6.88 30	6.54 20	6.59 15	6.59 15	6.51 8	6.56 8	6.54 8	6.51 8	6.50 8	6.44 20	6.47 30
walk	walk	Top	Top	Top	Top	Top	Top	Top	walk	walk
50.43	50.69	50.64	50.28	50.52	50.66	50.51	50.41	50.73	50.79	50.5
51.3	51.61	51.57	51.16	51.46	51.67	51.46	51.34	51.78	51.86	51.9
walk	walk	walk	walk	walk	walk	walk	walk	walk	walk	walk
51.8	52.19	52.21	51.91	52.21	52.45	52.85	52.17	52.52	52.55	52.6
walk	walk	walk	walk	walk	walk	walk	walk	walk	walk	walk
52.39	52.58	52.84	52.23	52.46	52.59	52.50	52.39	52.73	52.78	52.86
w edge walk	w edge walk	Top	Top	w edge walk	w edge walk	w edge walk	w edge walk	w edge walk	w edge walk	w edge walk
52.43	52.71	52.34	52.54	52.67	52.59	52.52	52.73	52.93		
on E. edge walk	Top Roll out cb + Cor. walk	Top Roll out	on E. edge walk	on E. edge walk	on E. edge walk	on E. edge walk	on E. edge walk	on E. edge walk		

Proposed, drain Betw.
 Copeland Place
 and
 VISTA ST.

MOORE

Begg

Roberts

#

W.O. 21027

Ties chgd. to # 25001

INDEXED

W.K.

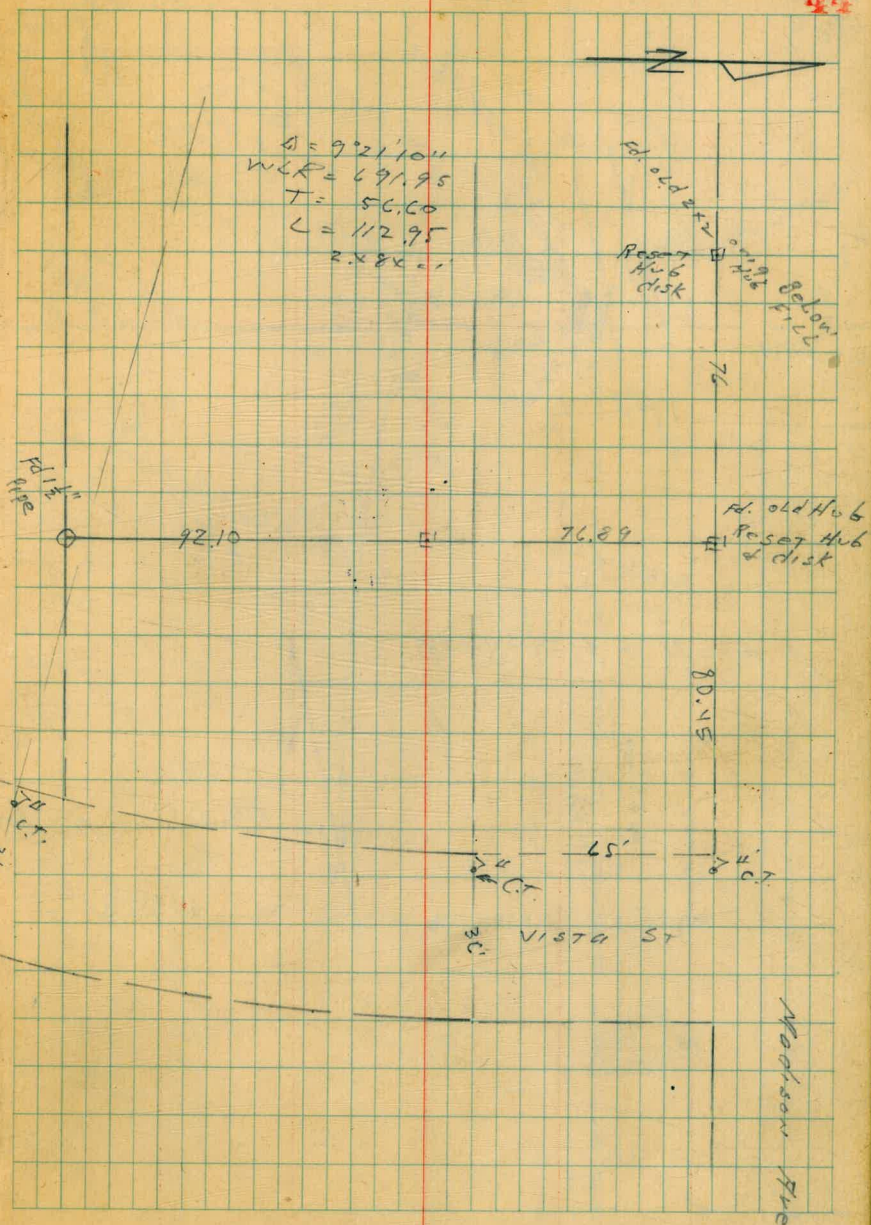
JUL 20 1949

1/2 CT.

30'

$d = 921.10''$
 $WLR = 731.95$
 $T = 59.47$

44

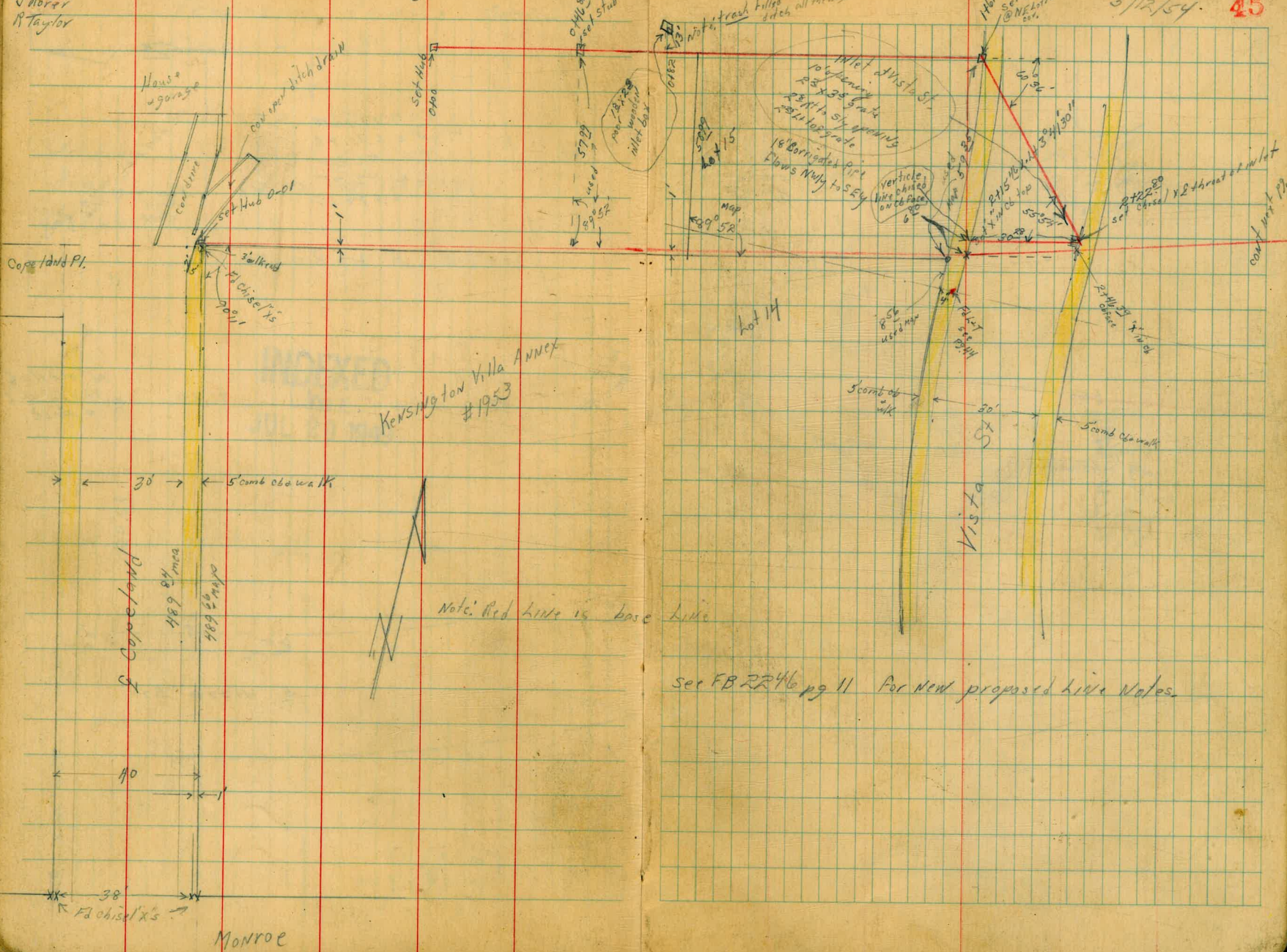


D. Smith
J. Morar
R. Taylor

Survey Vista St Area

Storm Drain

NO. 20123
5/12/54. 45



See FB RR 46 pg 11 For New proposed line Notes.

4	48.96
3	3761
<hr/>	
	110.95

Cont. May 30 to 31

Set Hub & Rt 391730
5+3761

10' cbs
5' walk
4' parking

10' cbs
5' walk
4' parking

4448 46
set Hub

4508 87
set Hub

90° Elong

Van Dyke St

POCKET PROP. 80
5' drive
Prop. Rad.
12' Lot

POCKET PROP. 85
5' drive

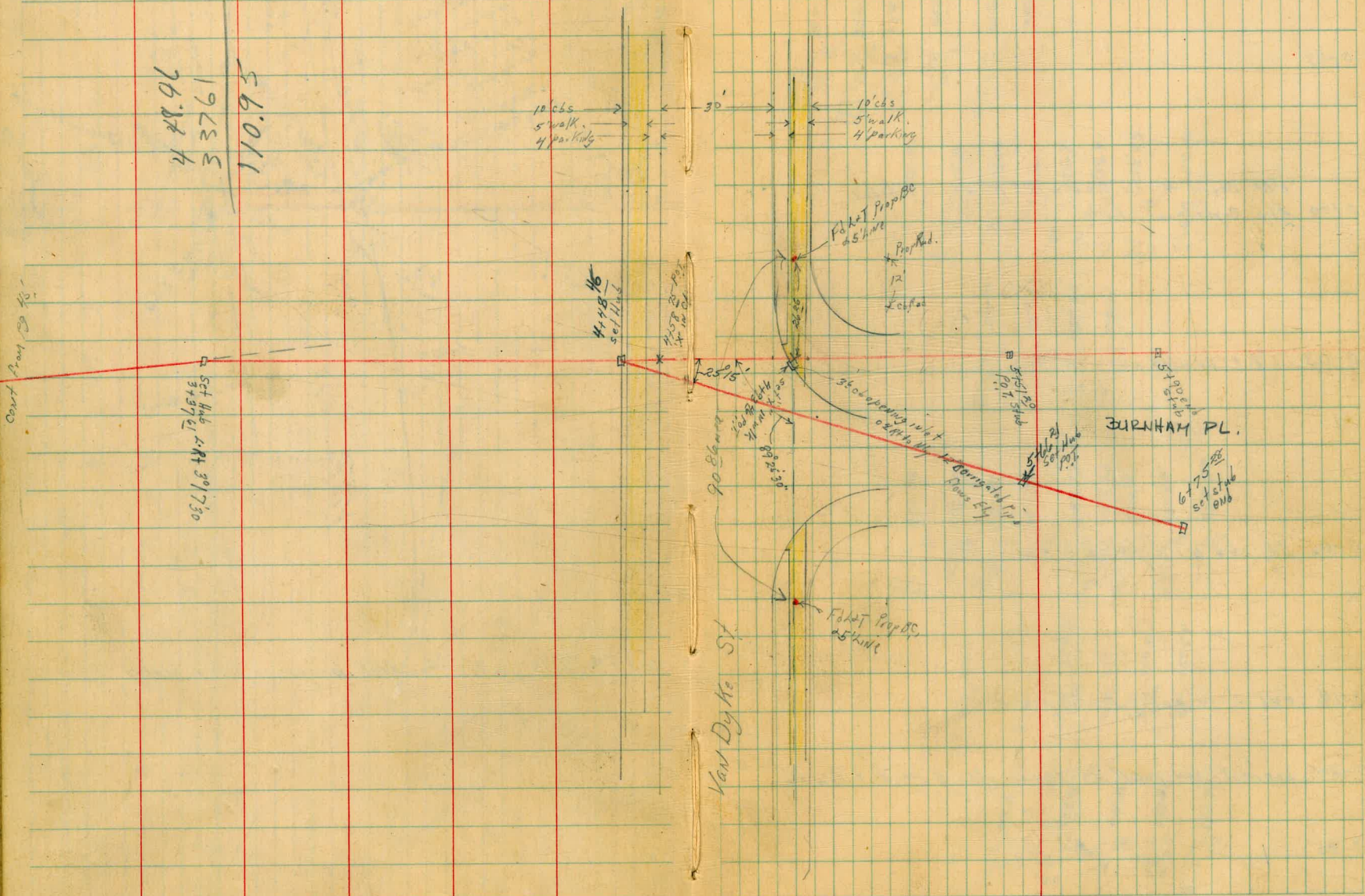
5718 85
set Hub

5708 85
set Hub

BURNHAM PL.

5728 85
set Hub

5775 85
set Hub



0+10 E crosses 4' high 2' wide hedge

0+06 5⁵ Lt E 6" Magnolia trees

0+03

1st Rt Begin 4" cov wall + 2nd Rt Begin 3' hedge

0+00 Ely Copeland Ave

0-03 1st Rt + C6 walk exp

0-05 Ely ob. line Copeland Ave

0-14 end 5" cov wall = picket fence

0-34 begin 5" cov wall on live also 3' picket fence

0-35

BM

466

363⁷⁰

359⁰⁴

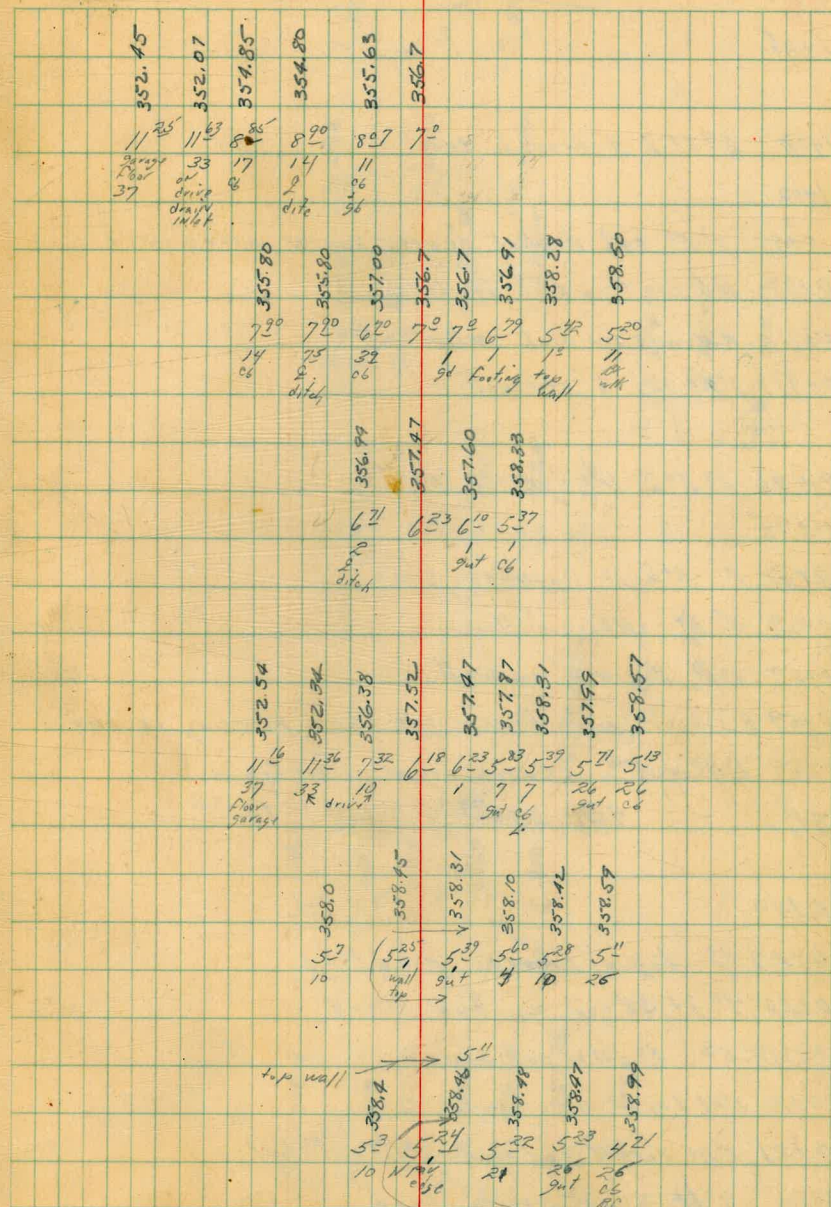
SWBP
Copeland Ave
Copeland Pl

Lt-Nly

Base
1111

Rt-Sly

47



1725

1718 5⁴ Lt 2 4" Avocado tree

1700

0799 1^o At end Picket fence begin wire fence

0799 NE cor 8' cov slab on lime

0791 NW cor 8' cov slab on lime

0791 1^o At end 6" cov wall

0776 2^o At 12" Cypress tree

0775

0771 2^o At 10" Cypress tree

0759 5^o At NE cor House

0759 1^o At begin 6" cov wall

0759 2 crosses wire fence end flower planting on lime

0759 1^o At end wire fence begin picket fence

TP 4⁷² 358³⁴ 10²⁸ 353⁶²

0750

0727 1^o 2 begins flower planting

0722 9^o Lt SE cor wooden shed

0721 5^o At NW cor house

0721 1^o At begin wire fence

0721 1^o At end 4' cov wall + 2^o At end hedge

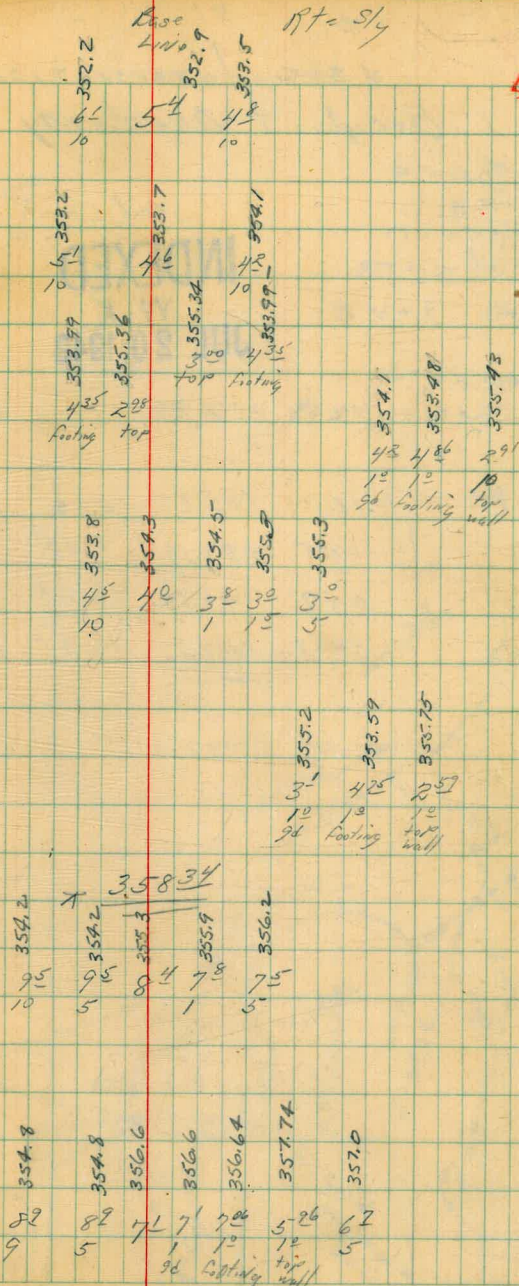
0715 9^o At SW cor wooden shed

Lt = Nly

base
line

Rt = Sly

48



71 363²⁰

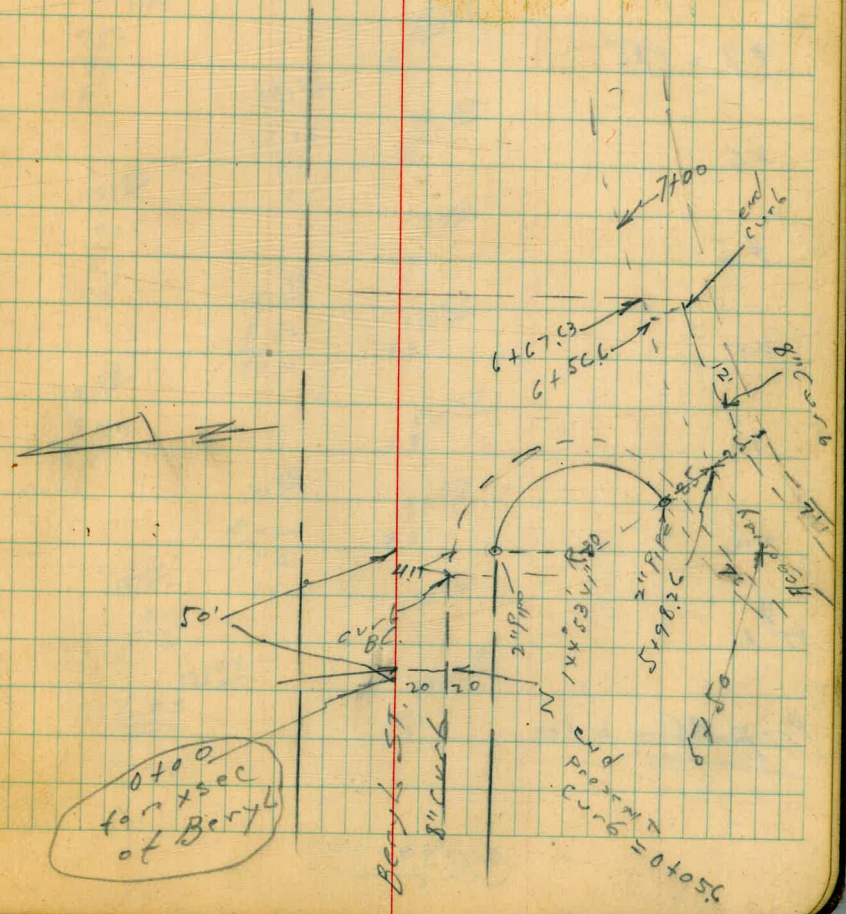
+ #1 -
X SEC Intersection of
Beryl & Academy Sts

Moore
Beag
Green
Roberts
2-9-48

W.O.P. 25001
INDEXED
W.K.
JUL 20 1949

10' RP. C.T.
on S.W. cor 1253 154.89 14236 Low 2
Lament

T.P.	1077	165.37	0.29	151.60
	1.45	158.17	8.65	156.72
	0.49	146.38	12.28	145.89
	5.20	140.27	11.31	135.07



Levels on Swby Ret.
 $\Delta 144^\circ 53' 41''$ $R = 30'$
 P.L. curve in 7 08. P.T.S.
 P.L. = Base Line

#7 = PXC

#6

#5

#4

#3

#2

#1
PT 1

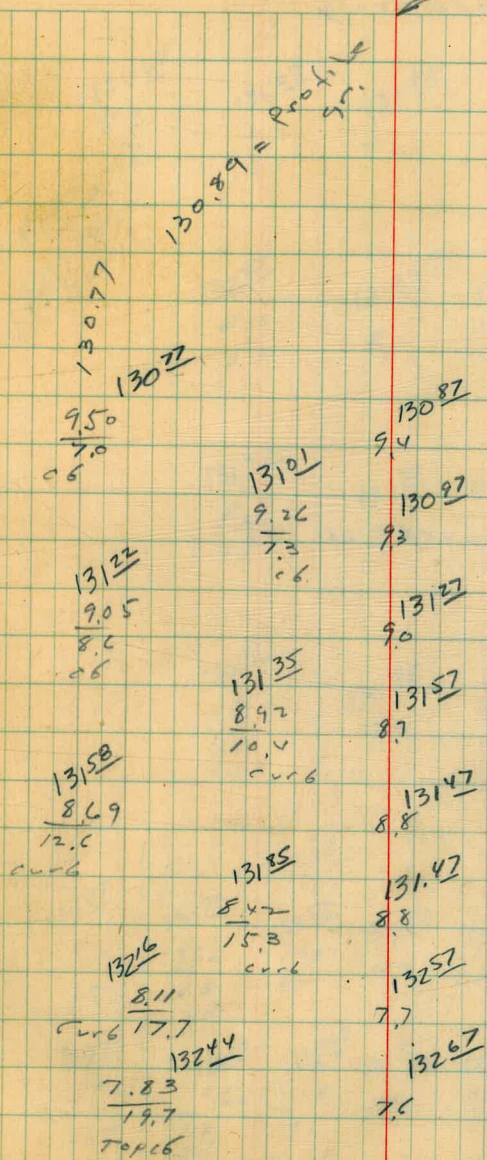
Prop. BC = 0.100

140.27

L7 = CURB

Prop. Line = Base Line

50



140.27

1500 Academy

7+00

6+67.63

6+56.6 = end curb on RT.

6+33.8

5+98.24 = PRC

5+50

L+

EST

R+

51

134⁶⁷
56
38
dirt
4 PPH
S.B. Bent L

136⁰⁷
42
25

137⁸⁷
+2.4

133¹²
+ 7.1
25

132²⁷
8.0
25

133⁸⁷
6.4

136²²
3.5
13

139²²
+0.5
25

131⁴⁷
8.8
25

132²²
7.5

132⁸⁷
7.4
17.7

134¹³
6.14
17.7
6. end

138⁵⁷
1.7
25

130¹²
10.1
25
dirt

130⁸⁷
9.3

131²⁷
9.0
18

132¹⁵
7.84
18
66
Top

137²²
2.5
25
dirt

130⁸⁷
9.4
25

130²⁷
7.5
18
66

129⁶⁷
10.6
18

129⁸⁷
10.4

129⁶⁷
10.4
18

130⁶²
9.65
18
66

132⁵⁷
7.7
25

129²⁷
10.5
25

129⁶⁷
10.6
18
66
Top

129⁶⁷
11.6
18
dirt

128⁵⁷
11.7

128⁵⁷
11.7
18
dirt

129⁶³
10.64
18
66
Top

129⁶⁷
10.6
25

140²⁷

2 sec Beryl
at Academy

2 + 00

1 + 40

1 + 00

0 + 80

0 + 50 = P.L. B.C. on South on RT,

0 + 05.4

LT: North

♀

R7

52

137²⁷
+ 3.0
40

136¹²
+ 4.1

133²⁷
+ 7.0
40

136⁵⁷
+ 3.7
40

135²⁷
+ 5.0
30

134⁸²
+ 5.4

133²⁷
+ 6.5
40

133¹²

132²⁷

135²⁷

134⁰⁷

132²⁷

132²⁷

130²⁷

7.1
40

8.0
22

6.5
18

6.7
3

7.5
3

7.5

9.3
40

133⁴⁷

132⁵⁷

134⁶⁷

134¹²

132²⁷

132²⁷

130²⁷

6.8
40

7.7
19

5.6
15

6.1
3

7.3
3

8.0

9.5
30

9.7
21.7

133⁵⁷

133⁶⁷

135²⁷

134⁵⁷

132²⁷

132²⁷

131⁴⁷

132⁴⁷

132⁶⁷

6.7
40

6.6
20

4.3
14

5.7
3

7.3
3

8.0

8.8
20.3
9.1

7.83
20.3

7.6
40

130²⁷
+ 10.0
40

136⁰⁷
+ 4.7
16

133⁶⁷
+ 6.6

132⁶⁷
+ 7.6
20

133⁷⁸
+ 6.49
20
curb
end

133⁹⁷
+ 6.3
40

140.27

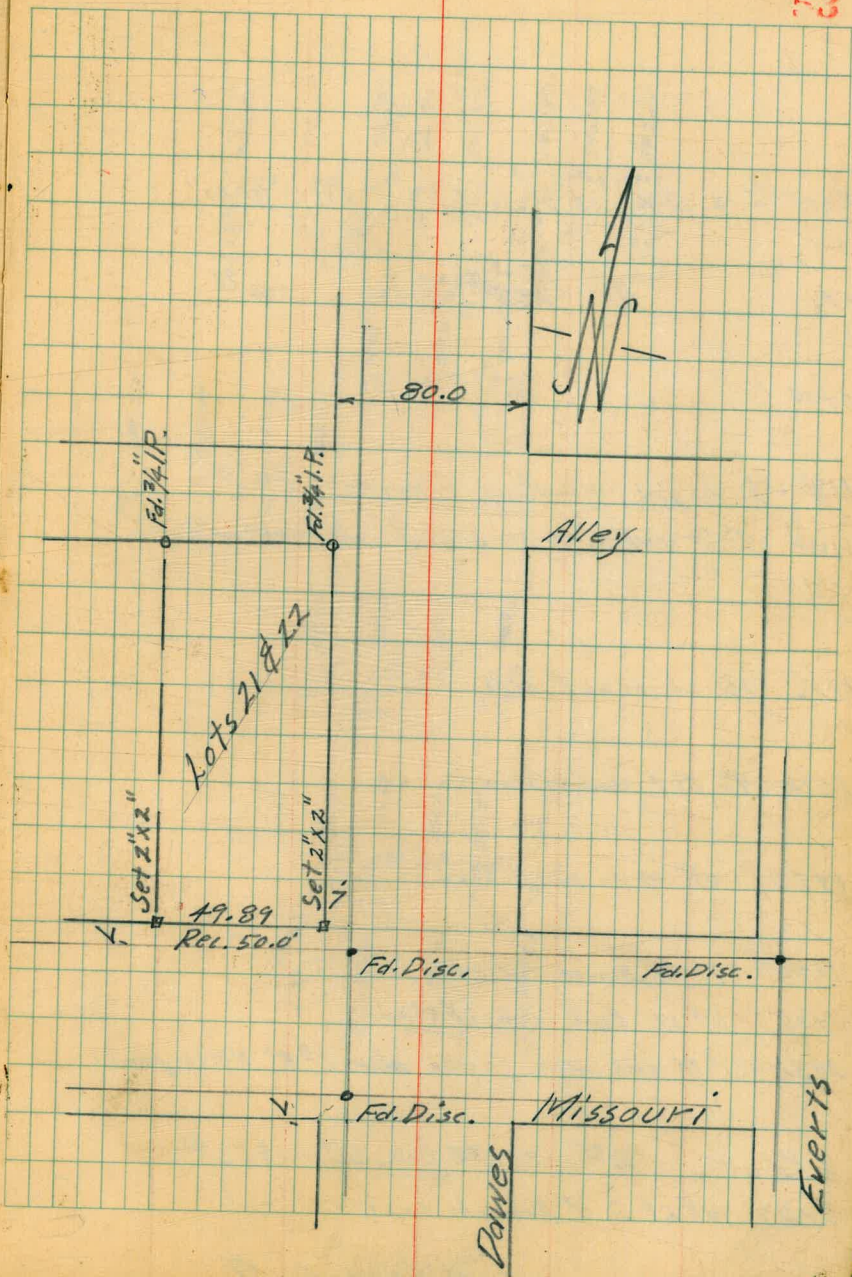
7/19/49

Garper
Cota
Chavez

Replaced two stakes
Lots 21 & 22 Bk 120
Pacific Beach

INDEXED
W. K.
JUL 20 1949

53



4425

4400

3499 3rd Rt NE cor garage

TP5 5⁵⁷ 340⁷¹ 6²⁰ 335¹⁴

3479 on E Begin flower planting

3479 4th Rt NW cor garage

3478 0th Rt begin 3' rail fence

3478 1st Lt SE cor garage

3477 1st Rt End 5' Board fence

3452⁵ 2nd Lt SW cor garage

3451 0th Rt NW cor ^{begin 11 to line} diagonal fence ^{5' board}

3450

3441 10th Rt to Wly cor diag 5' board fence

TP4 2⁸⁰ 341⁸⁴ 12⁵⁹ 339⁰⁴

3437⁶ L Rt 3' 17' 30" 5th Rt end 4' Picket fence

3434 E crosses 4' Picket fence

3433 1st Rt E 3" Canada tree

Lt-Nly

335.07	Base	335.52	335.5	335.5	335.5
564	1.1W	56	02	41	40
24	56	335.3	335.4	336.4	337.8
25		335.2			
26		08	1	42	
27				43	
28				44	
29				45	
30				46	
31				47	
32				48	
33				49	
34				50	
35				51	
36				52	
37				53	
38				54	
39				55	
40				56	
41				57	
42				58	
43				59	
44				60	
45				61	
46				62	
47				63	
48				64	
49				65	
50				66	
51				67	
52				68	
53				69	
54				70	
55				71	
56				72	
57				73	
58				74	
59				75	
60				76	
61				77	
62				78	
63				79	
64				80	
65				81	
66				82	
67				83	
68				84	
69				85	
70				86	
71				87	
72				88	
73				89	
74				90	
75				91	
76				92	
77				93	
78				94	
79				95	
80				96	
81				97	
82				98	
83				99	
84				100	

56

340⁷¹

335.53	335.5	335.4
631	64	64
18		
1600		

336.8	336.7	336.7	337.3	337.3
50	49	49	45	45
10	3	3	5	10

341⁸⁴

342.8	342.7	342.7	342.3
68	69	69	11
10		50	8

351⁶³

5109^E & crosses road drive way Wly edge

TP 004 337⁶³ 31_R 337⁵² Top Fire Hqd 75° at

4497^S bk of w/k

4493⁴⁰ 2³ & 3⁵ ob throat opening only inlet 12" corrug

4488¹⁰ Fly ob line Van Dyke

4473⁰⁰

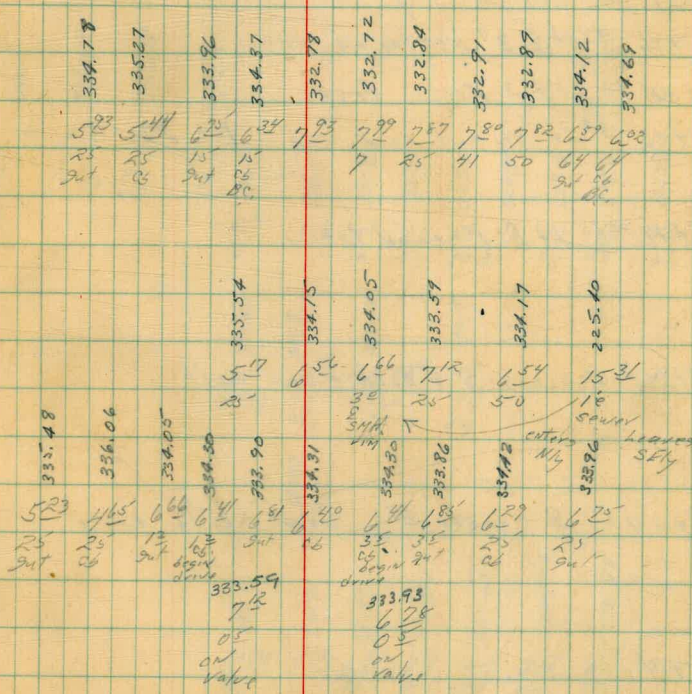
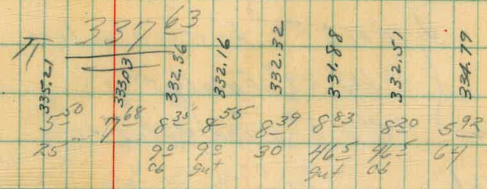
4458²⁵ & crosses Wly ob Van Dyke st.

4457 0⁵ at RT & water meter boxes

4448⁵ 1⁴ at end 3' rail fence & planting

Lt. Nly Base Line Rt. Sly

337.99
564



340.71

5466 27° RT & 4" 18" corrugated tapeper drain for posts

5463 { 19° RT & 36" Eucalyptus tree
10° RT & 24" Eucalyptus tree
8° RT & 24" Eucalyptus

5463 1° RT & 8" Eucalyptus tree

5461

TP 087 326³² 12¹⁸ 325⁴⁸

5451 2° LT & 2" Fig tree

246 92° RT & 3" Nectarine tree

5445 1° LT & 3" Peach tree

5443 3° LT sly end con wall ⊥ to line

5441 6° LT & 1" hemod tree

5426³ & crosses 8" rock + con wall

5424⁵ & crosses Ely con drive edge

5414

Lt = Nly

Base
LINE

RT = Sly

58

320.04
27
10

320.4
59
10
323.4
69
10
320.8
55
10
322.6
30
23
324.4
12
45

326³²

330.4	328.69	322.71	332.3	332.7	332.0	331.8	331.5	329.0	327.9	328.6	329.8	333.6
78	894	486	53	49	56	58	64	86	92	80	78	110
91	32	30	9d	10	10	10	27	29	33	43	50	60
Ely	Footng	top wall	top wall	top wall								
331.47	331.8	333.23	332.8	331.47	331.83	331.8	333.23	332.8	331.8	331.8	331.8	331.8
616	58	435	51	616	631.83	58	435	51	58	58	58	58
Footng	top wall	top wall	top wall	Footng	Footng	Footng	Footng	Footng	Footng	Footng	Footng	Footng
333.10	331.91	331.80	330.42	333.10	331.83	331.8	333.23	332.8	331.8	331.8	331.8	331.8
453	572	623	721	453	572	623	721	819	739	739	739	739
115	10	10	215	115	10	10	215	30	123	123	123	123
Spring			9d	Spring			9d					
door			11	door			11					

33763

BM starting

481

359⁰²

359⁰² ✓

TP₄

6⁵¹

363⁸³

481

357³²

TP₁₀

12²³

362¹³

6²⁸

349²⁰

TP₉

11⁹⁵

349⁵⁸

0²²

337⁶³

TP₈

11⁴⁵

337⁸⁵

0²²

326¹⁰

6400

5787 approx E. canyon

5776 3⁵ RT & 12" corrugated pipe out let. From Van Dyke

5770 10³ RT & 14" cast iron pipe out let

Lt = My

Base
4110

RT = S/Ly

59

318.4

6¹⁹

10

315.0

11³

10

315.7

10²

10

319.8

6¹⁵

10

318.7

11⁶

10

316.4

9²

10

319.5

6¹⁶

10

314.3

12⁶

10

316.6

9²

20

313.6

12²

25

316.4

9⁹

50

314.79

11⁵³

10

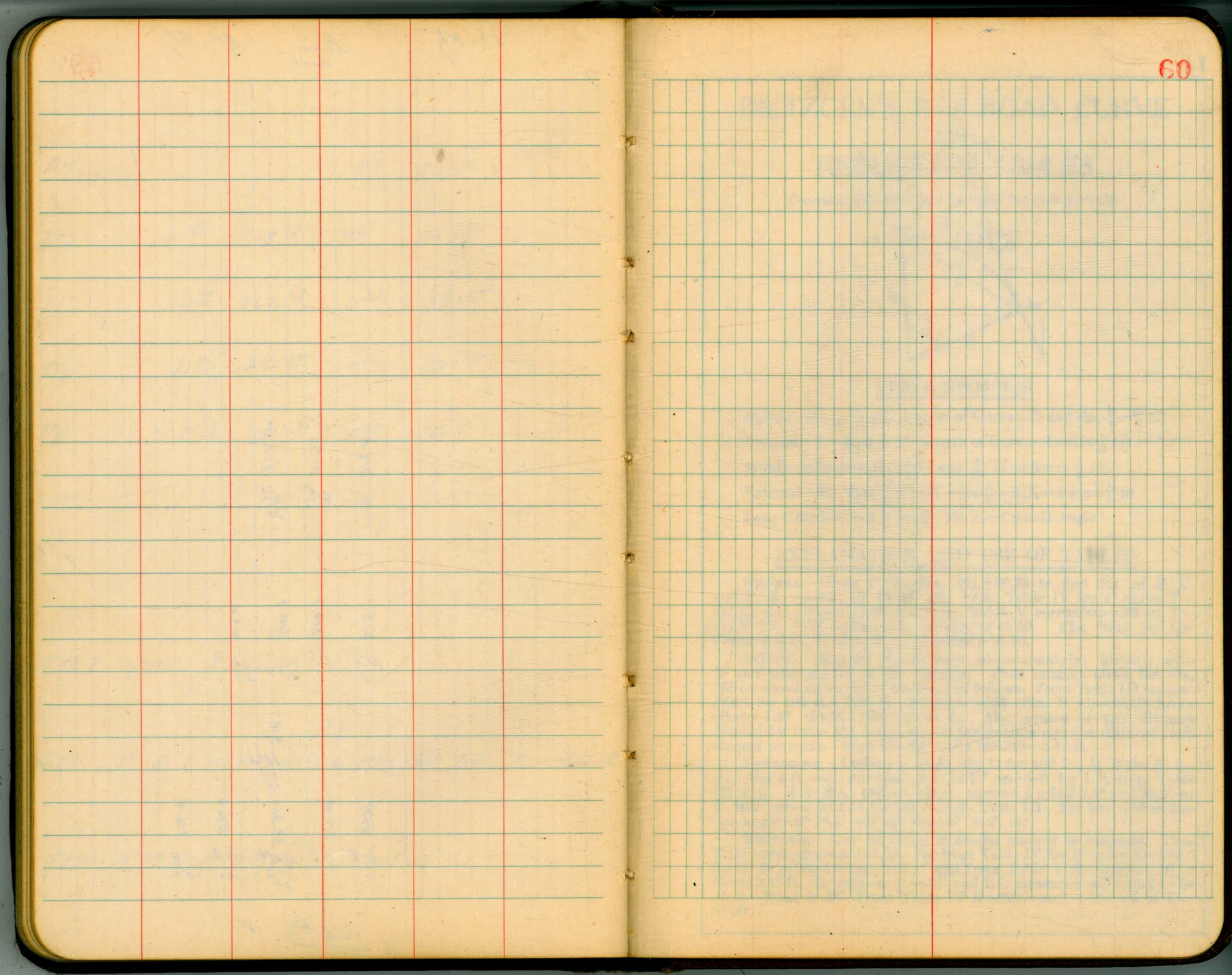
316.34

9⁹⁸

10

326³²

1



+ 8.88

9613

79

86517

60294

729427

$$M = \frac{C^2}{8R}$$

$$R = \frac{C^2}{8M}$$

2500

8 * 7.8

7.8) 312 (40
312

1.0142
8
173136

79 @ 16°

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9 + (20-16) * 2 or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

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