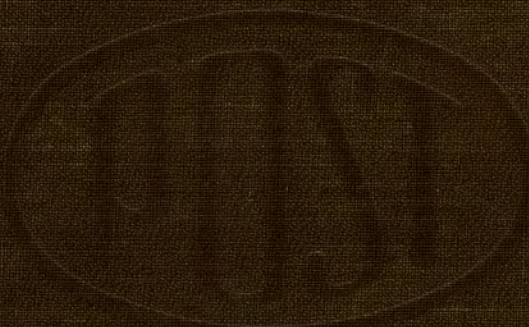


1740



1740

CITY ENGINEER'S OFFICE

MICROFILMED
DEC 29 1964

MADE IN U. S. A.

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THE FREDERICK POST CO.

ENGINEERING and DRAFTING SUPPLIES

P. O. Box 803

CHICAGO

Sewer Location	Riley Cauby	1
"	" Scott + Talbot	2
Cross Section	Alley Blk 3 Venice Park	4-7
Survey	M.H.W. Line Terry Pines Beach	10-28
Cross Section	Lacust St. Pos to Russell	29-39
Tie Points	Goodyear St.	40
Cross Section	Goodyear St. Barton to National	41-45
Storm Drain	Market St 43 rd + Genby St	46-60
Cross Section	Maude Ave. 31 st St to 32 nd St	61-76
Pakemere Sewers	{ Lots 39 to 52 } incl. { " 55 to 62 }	77-

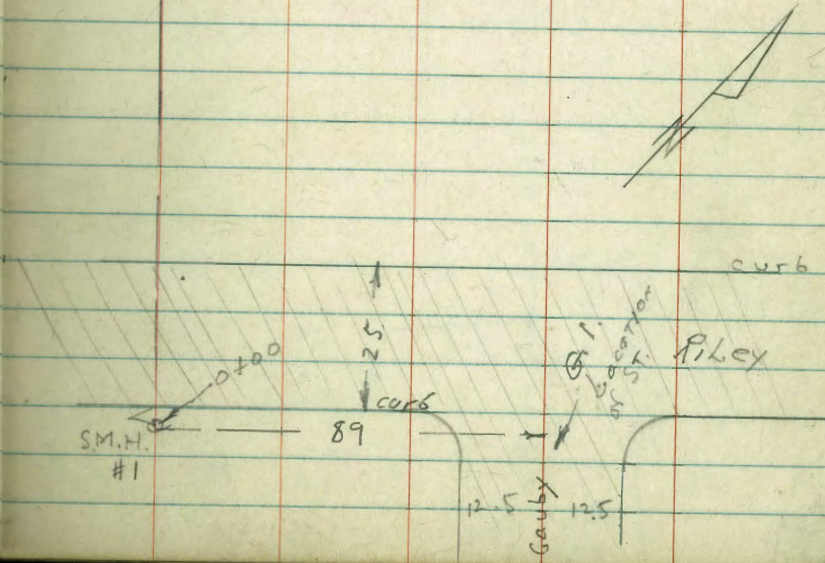
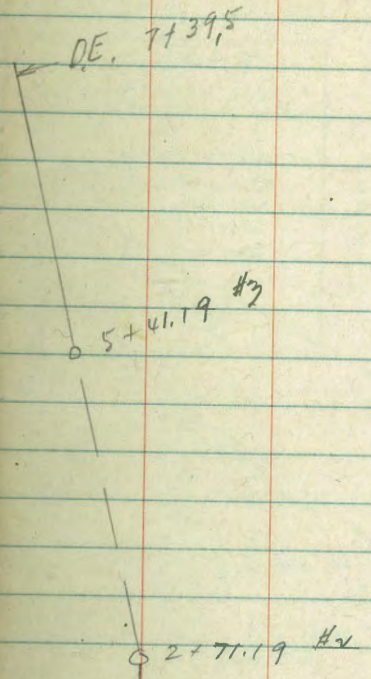
Location & E.L. of
G.I. Sewer at
Riley & Cauby W.O. #10

CS Moore
Johann Meyer
W.F.M.
E.B.
10-14-46

Indexed
C.S.K.
GRH

Inspector says, don't
check F. lines of
this sewer

7+39.5 D.E.	4.7x	2.76	Top Iron Plug
8+41.19 M.H. #3	4.56	2.94	RIM
T.P.	5.3x	<u>7.50</u>	4.59 2.16
2+71.19 M.H. #2 Δ approx 45° LT	4.67	2.08	RIM
0+00 M.H. #1	4.39	2.36	RIM
BM. Freeland SW. Top FH. Riley & Cauby	176	<u>6.75</u>	4.99

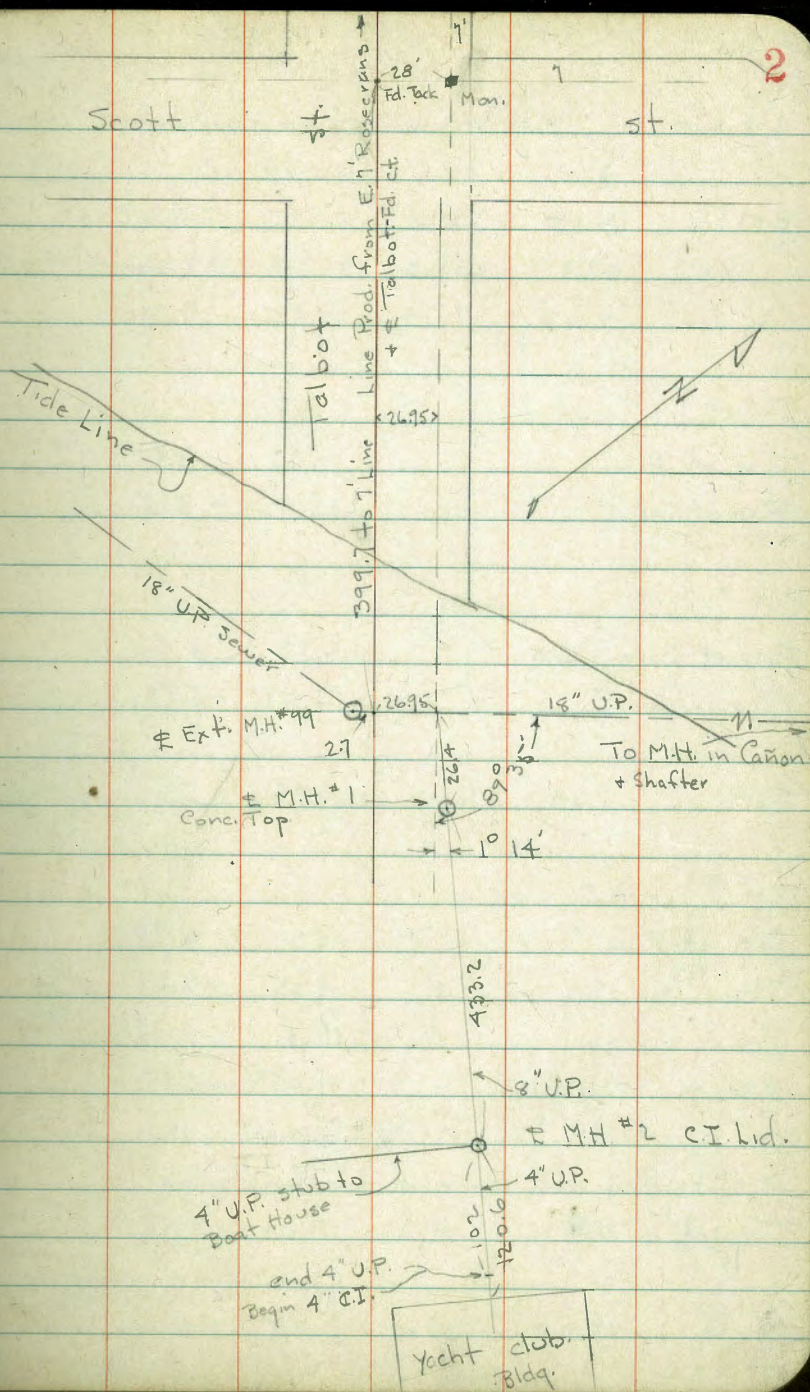


Indexed
C.S.K.

Location of Sewer put in by
Heilbron for the Yacht Club, at the
foot of Talbot St.

567
W.O. 210

10-27-46
Osborne
Hardin
Wornell
Smith



Levels on M.H.'s on Sewer to Yacht Club.

B.M.	2.14	30.19	28.05	13.86
	1.61	20.66	11.14	19.05
	2.03	9.74	12.95	7.71

M.H. B.P.
Rosecrans
+ Bessemer

T.P. 12.07 25.22 0.71 13.15

6.72 30.82 1.12 24.10

check starting B.M. 2.80 28.02 28.05

M.H. # 99

Top of Rim	6.77	2.97
Flow line	18.42	-8.68

M.H. # 1

Top of Conc. lid	6.23	3.51
Flow line	18.57	-5.83

T.P.	1.54	6.84	5.30	7.44	5.30
------	------	------	------	------	------

6.84
ok
5.30
6.84

✓ bolt in pile
opp M.H. #99

M.H. # 2 - C.I. lid

Top of Rim	5.94	0.90
Flow line - Beginning of 8"	9.15	-2.31
F.L.	9.01	-2.17
F.L. 4" stub to S.	9.05	-2.21

102 E. of M.H. # 2 on Main line to club - end at

4" vitrified and begin 4" C.I. soil pipe

Top of 4" V.P.	7.01	-0.17
----------------	------	-------

T.P.	8.56	13.86	1.54	5.30
------	------	-------	------	------

X-Sect. 15' Alley in Block 3
Venice Park

614

W.O. 230

11-7-46

Osborne
Hardin
Worrel
Smith

Indexed
C.S.N.

4

Pac Beach Dr.

168.09
Dirt Graded.

270.18

6-12-82

Set Hub

2.381

Mon

46'

Mon

23487

Morell St
Narrow Road - Poorly oiled.

Block
3
Venice Park
Map # 991

15

Pr.

Dirt Graded.

Crown Pt

46
Mon

133.29

112

Mon.

Fortuna Ave
Dirt Graded

N

X- Sect. 15' Alley in Block 3 - Venice Park

Lt = W

Rt = E

1+50

13.6
8.7
7.5

14.5
7.8
7.5

14.6
7.7

14.3
8.0
7.5

2+00

13.6
8.7
7.5

12.7
9.6
7.5

12.6
9.1

12.6
9.1
7.5

12.5
9.0

1+97 - 6.5' Lt. = P. pole

1+50

11.6
10.1
7.5

11.6
10.7

11.3
11.0

1+13 = ± M.H. on Alley 11.02

on Rim

1+00

12.7
9.6
7.5

11.4
10.9
7.5

11.4
11.4

10.7
11.6
7.5

10.5
11.8
7.5

0+50

0+47 - 7.5 Lt = P. pole

0+00 = N.L. Fortuna

11.8
10.5
7.5

10.9

11.4
10.9
7.5

12.7
9.6
7.5

12.6
9.7
7.5

12.7
9.6

12.5
9.8
7.5

11.9
10.4
7.5

0-35 = Fortuna - for Profile of Road.

11.8
7.5
7.5

13.3
9.0

12.3
10.0
7.5

in Road.

in intersection of Roads.

T.P. 4.86 22.32 7.45 17.46

B.M. 1.38 24.91 23.53

SW 7 Mon
Moffet +
Pac. Beach
Dr.

22.32

4+50

4+00

3+98 - 96 Lt. = \$ 4" Pine

3+97 - 6' Lt = \$ 4" shrub

3+92 - 14 Rt = end row of shrubs

3+90 - 9' Lt = \$ 12" Pepper

3+84 - 29 Lt. = \$ 2" Pine tree

3+84 - 14 Rt = Beg row of shrubs - 6' High

3+79 = \$ 3' x 1.5' Small brick incinerator

3+69 - 11.9 Lt = \$ 12" " "

3+69 - 7.6 Lt = \$ 6" Evergr. Tree

3+68 - 18' Lt = \$ Small shed 2.99

Wood floor

3+67 - 10.6 Lt = \$ 6" " Tree

3+67 - 4.5 Lt = \$ 8" Evergreen stump

3+50

3+46 - 6.2 Lt = \$ P. pole

3+43 = \$ Sewer M.H. on \$ 5.76

on Top.

3+00

Lt.

Rt.

19.6

19.7

19.1

2.7
75

2.6

3.2
75

20.2

19.5

18.9

18.8

18.9

2.1
202.8
75

3.4

3.5
753.4
20

18.1

17.4

17.4

4.2
75

4.9

4.9
75

16.5

16.1

16.1

15.8

15.7

5.8
206.2
75

6.2

6.5
756.6
2022.32

check B.M. 2.78 23.55 ✓

T.P. 8.69 26.33 4.68 17.64

6+42.90 = \pm Pac. Beach Dr. - for Profile of road.

6+12.82 = S.L. Pac. Beach Dr.

6+00

5+94- 0.3 Rt = \pm 6" Gate stand

5+50

5+00

4+95-6.8 Lt. = \pm P. pole

Lt. Φ Rt.

18.8	16.3	12.6
2.45 50	6 0	9.7 50
19.3	18.7	18.1
3.0 20	3.6 7.5	4.2 7.5
19.5	18.6	18.7
2.8 20	2.7 7.5	3.2 7.5
19.7	19.5	18.9
2.6 7.5	2.8 7.5	3.4 7.5
20.0	19.8	18.4
2.3 20	2.1 7.5	2.9 7.8
	19.8	18.4
	2.1 7.5	2.9 7.8
		22.32

check

T.P.

$6 + 42$

$6 + 12$

$6 + 0$

$5 + 9$

$5 + 5$

$5 +$

$4 + 9$

ched

T.P

6 + 4

6 + 1

6 +

5 + 9

5 +

5 +

4 + 9

Survey M.H.W. Line
 Torrey Pines Beach
 N. Cor. San Diego at Del Mar
 Sly to S.L. of P.L. 132V

Used 4.91 U.S.C. & G. datum

0 + 00 on City Boundary
 LINE

Levels

T.P. 0.16 13.44 2.08 13.28

check T.P. 0.05 15.36 1.87 15.31

6 + T.P. Rock Below 1.52 17.18 12.04 15.66

check to State B.M. #16 5.39 22.31

6 + T.P. Rock 12.04 27.70 9.40 15.66

6 + check to State disk 2.56 22.50

5 + T.P. 11.03 25.06 1.63 14.03

5 + 4.52 15.66 11.04 =

5 - CITY BM BP 11.04 + 9.01 = 2.03 ✓ CITY DAT.

↑
 NOW ON
 U.S.C. & G.
 DATUM

C. Moore C.P. Marks indexed
 SUMNER MOYER INST. C.S.K. 10
 W. Moore H. Chain
 E. Beag P "

1-7-47. clear little wind
 W.O. 247 TJ High Tide
 -2.0 Low "

Note!
 Shore Bench (dry sand) approx. El. 13.5
 Toe Hwy. Emb. " " 15.0
 1-7-47 High Pt wave wash "

Used Wye Levels to 6 + 00
 thence Transit after a
 good check up.

checked X
 SW Cor Hwy Bridge 22.31
 TOP of SW B.M. #16 13.27 -13.27
 9.04
 dif. on dat = 9.01
 0.03 error

U.S.G.S. H 53-1938 = 22.50
 19.49
 3.01
 2.89
 0.12 error

U.S.C. & G. datum 11.45 = Walker - 11.04 11.08
 0.575 dif

on Sly wing of Sly Bubbld of Santa Fe
 overhead xing on old Torrey Pines Rd.
 mouth of Sarcenito Creek near Ocean

Ref. Books
 1285-1407-1410- 1408-1423
 4711 6
 WILLIAMS MAP of Pueblos

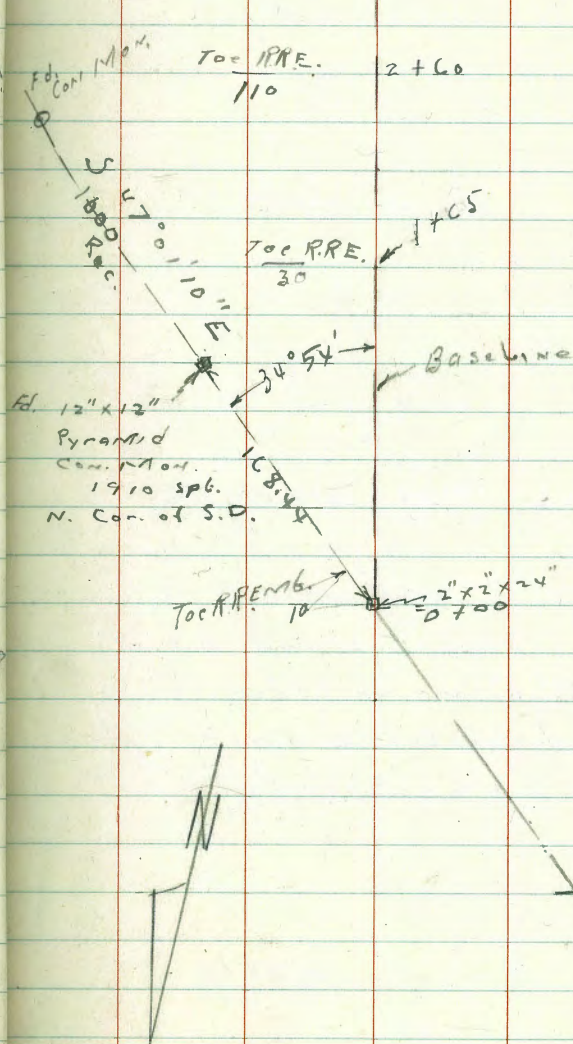
Note!

Ed. Williams Con. Man,
 Top 3" knocked off by flow,
 assumed 4d. c.t. was centered.
 Next 2 Moni to S. 4d. c.t. gone
 by salt erosion of Con. in Moni,
 when Exposed to elements,
 Time was essence, so used,
 45 Ed. Possible to be off
 0.10 for line at Beg.

1-7-47. 9:00 AM. Saw 2 state Eagles
 engaged in current drift survey
 of Sta. 50 + 00 inside Phunge Line

13.44

LT.
 Base Cliff
 on R. Breakwater



R.
 M.H.W.
 8.53
 4.91
 116

11

Lt

Rt

T.P. 3.57 15.41 4.68 11.80

Toe Hwy Em. 15+00
60

11.61
130

Toe Hwy Em. 12+00
50

11.61
120

Toe Hwy Em. 9+00
40

11.61
100

Toe Hwy Em. 7+50
40

11.61
49

6+00

8.53
107

Toe Hwy E. 5+50
80

Toe R.P. Emb. 4+40
125

49 ← M.H.W.

Beachline

T.P. 3.25 16.57 0.17 13.27

Note! offsets shown at
all Δ's are on Spher.
except at Bsq. and end
which are on Phot Lines

13.44

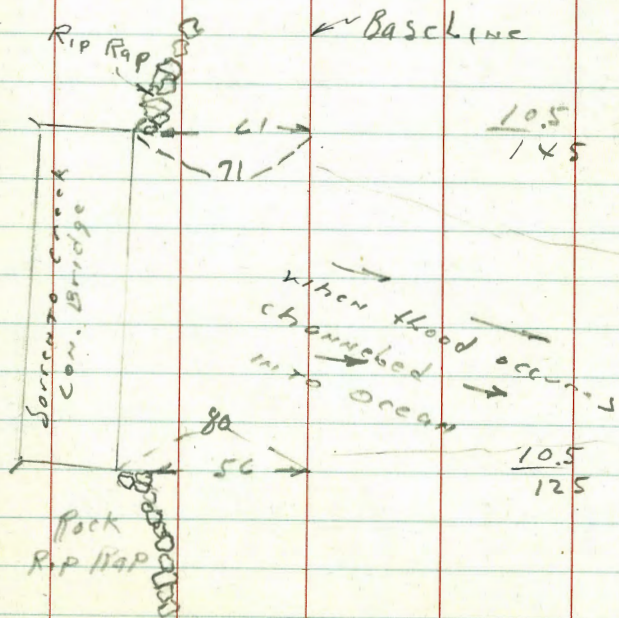
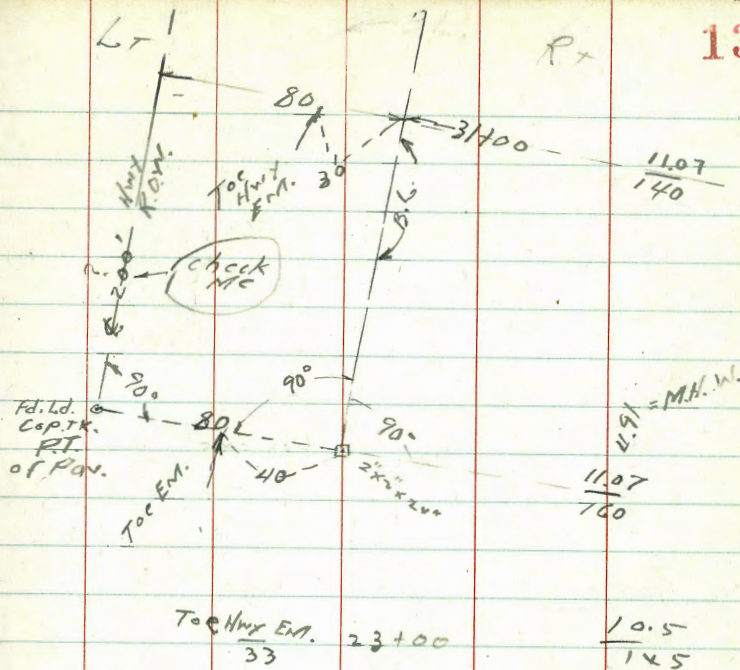
24+80.45 A 5°25' RT.

T.P. 4.37 15.98 3.80 11.61

20+96

18+00

15.4



47+00

T.P. 5.00 17.32 3.61 12.32

44+00 5' Lt. Beg. City Rock ^{RIP}_{RIP}

43+00

36+24.60 Δ 0° 45' 30" LT

36+24.60
24 81.45
<u>1138.15</u> ✓

T.P. 4.65 15.93 4.70 11.28

15.98

Lt.

Bk. 56

Rt.

14

Top EM.
2

Top EM.
5

Top EM.
6

Fd. Id. Ct.
Rt.

80

90°

Top EM.
2

Top EM.
24

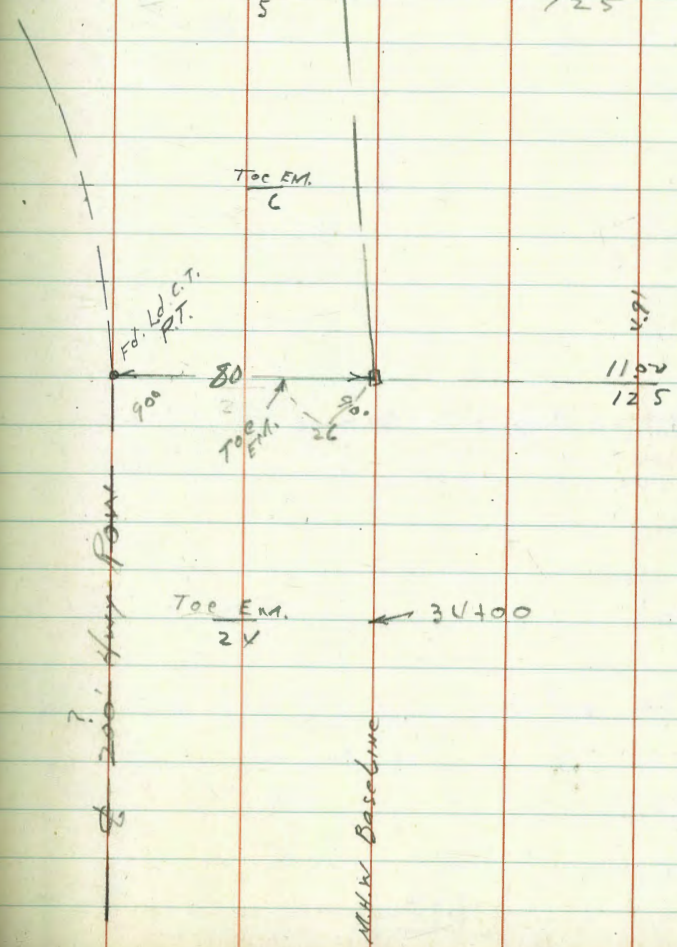
36+00

2nd Hwy Row

Highway Baseline

49'

11.02
125



Quit here 5:00 PM 1-7-47

T.P. on Hub
52+94.8 1.07 13.59 4.80 12.57 =
D.P.T.
2"x2"x2"x2"

52+94.80 Δ C°30 RT 2"x2"x2"x2"

51+30

50+25

49+80 Beg. of Natural Chiffs

49+00

48+50 20' Lt. end of Cox Rip Rap

48+10 12' Lt. Toe Rip Rap

47+85

1732

LT.

RT

Hide 75

15

High Pt. of Wave Wash 1-7-47

Variable
at div. pts.
at Beach
acct. of wave slope
of foreshore and
outward tidal
Toe Cliff
3

Toe Cliff
5

Foot Cliff
20

Toe cliff
30 and Rd. to Beach from
Rd. FOOT of old Torrey
PINE Grade. Auto
Parking Area

Toe EM.
24

Toe
20

Toe
16

Toe EM
5

49
= 12.41
137

LT

B.l.

RT

16

69 + 93

$$\begin{array}{r} \text{Toe cliff} \\ 37 \end{array}$$

68

$$\begin{array}{r} \text{Toe cliff} \\ 22 \end{array}$$

$$\begin{array}{r} 7.62 \\ 72 \end{array}$$

65

$$\begin{array}{r} \text{Toe cliff} \\ 30 \end{array}$$

$$\begin{array}{r} 7.62 \\ 80 \end{array}$$

63 + 90

$$\begin{array}{r} \text{Toe cliff} \\ 20 \end{array}$$
T.P. 2.67 12.53 3.08 9.91
$$\begin{array}{r} \text{Toe cliff} \\ 27 \end{array}$$

$$\begin{array}{r} 8.68 \\ 100 \end{array}$$

62

Note! See City Carrans of
this cliff.

Notes taken for possible Hwy.

59

by BRISSELL + Sisson

also Yeager

$$\begin{array}{r} \text{Toe cliff} \\ 21 \end{array}$$

$$\begin{array}{r} 8.68 \\ 95 \end{array}$$

56 + 63 Beg. here 7.7 tide wets ft. of cliff

$$\begin{array}{r} \text{Toe cliff} \\ 6 \end{array}$$

$$\begin{array}{r} 8.68 \\ 109 \end{array}$$

13.54

This might settle thru tidal action

chiseled cross top rock Δ 2.99 6.15

76 + 37.45 $\Delta = 4^{\circ} 21' LT$ chiseled \times Top 5' di. Rock

74

73 + 65

73 + 40

73 + 10

T.P. 0.18 9.64 3.07 9.46

71

12.53

LT

Toe cliff and sand beach $\frac{3.5}{17}$

$\frac{T.C.}{27}$

$\frac{T.C.}{21}$

$\frac{T.C.}{12}$

Toe cliff $\frac{27}{27}$

Toe cliff $\frac{30}{30}$

Rt.

17

$\frac{4.73}{26}$

$\frac{4.73}{58}$

baseline

$\frac{7.67}{60}$

T.P. 4.58 11.18 3.04 6.60

84 + 32

83

82

80

79

78 + 23

9.64

LT

RT

18

Toe cliff
27

Toe cliff
35

4.73
36

Toe cliff
55

Toe cliff
50

4.73
54

T.C.
50

T.C.
24

93+30

$$\frac{\text{Toe cliff}}{30}$$

92+55

$$\frac{\text{Toe cliff}}{75}$$

92

$$\frac{\text{Toe cliff}}{72}$$

$$\frac{627}{9 \text{ hr}}$$

↙ Baseline

91

Mouth of wash trail up
to Top cliff

$$\frac{\text{Toe cliff}}{80}$$

89

$$\frac{\text{Toe cliff}}{62}$$

$$\frac{627}{12}$$

86

$$\frac{\text{Toe cliff}}{40}$$

$$\frac{627}{30}$$
11.18

96+67.15 Δ 27°18'30" Rt. chisel X ^{CTP} 3" X C Rock

Toe cliff

$\frac{5.33}{40}$

95+70

Toe cliff

$\frac{5.33}{80}$

Base line

94+25

Toe cliff

94+10 Sedge Rock Bench

4.91

5.33 sand

OH
T.P. Lag screw 1.76 10.2X 2.70 8.48 8.915
93+90.50 2.435

IN: F.B. 1408-44

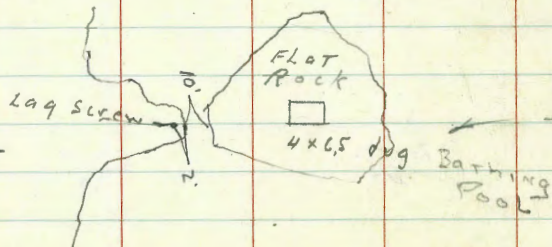
Quit here 1-8-47

See F.B. 1285-10

93+90.50 Δ 42°05'30" Lt. Fd. Lag Screw

Δ 42°05'30" Lt. Fd. Lag Screw

93+75



Toe cliff

Base line

14.

107 + 25 Mouth Wash

106

104

T.P., 1.70 9.44 2.50 7.7x

103

101 + 45

100 + 80

100

1024

Lr

Bla.

Rr

21

Top cliff
50

Top cliff
45

4.53
30

Top cliff
60

Top cliff
50

5.33
30

Top cliff
35

Top cliff
45

Top cliff
40

5.33
30

approx.
 To A
 Main cliff
 400
 200' above
 MHW
 approx.

Toe
 Main cliff
 370
 15' above
 MHW
 approx.

Wedge
 Plateau
 750
 60' above
 MHW

Toe Sec'dy
 cliff
 75
 ↓

Lt.
 Highest
 Wave Wash
 60
 15

R7
 ← Beg. Rock out crop

115+00

and Beg.

Toe cliff
 60

6.04
 18

T.P. 2.85 10.95 1.34 8.10

112+00 Δ 12°31'00" R.

Toe cliff
 33

4.53
 54

110+80

Toe cliff
 33

110+30

Toe cliff
 25

109

Toe cliff
 24

4.53
 30

108+10

Toe cliff
 28

9.44

128

125

124 + 50

124

123

TP 4.09 10.08 4.96 5.99

121 + 98.90 Δ 1800' LT

fd. hole in 8' di. Flat Rock

50' di. disk (conv) this might be same
App. of 1928

120

10.95

LT

Toe 2nd cliff
50

491
517
22

Toe 2nd cliff
Shoreline
130

Toe 2nd cliff
100

Toe 2nd cliff
Shoreline
75

Toe
Secondary cliff
28
Shoreline

Toe cliff
50

Shore
line

P+

23

x.91
517
40

Baseline

SIT ← Sedge Rock Beach

SIT west edge Rock
30 = N.H.W.

60 x 10 = 600 Rocks

← Sed disk
18000' LT

60 x 90
PT Rocks

Baseline

T.P. 3.78 12.55 3.89 8.77

132

133

132 + 70 = Cr. Wash from E,

130 + 60 = S. end of secondary cliffs

129 + 73.50 Δ 1649'30" Pt. Chisel X
Small Rock
on Small Rock Pt.

T.P. 6.53 12.66 3.95 6.13

10.08

Lr

Top cliff
130

Top cliff
120

Top Main
Cliff
80

Top 2nd cliffs
Shore line
75

Baseline

Δ Chisel
Cross
1649'30" Pt.

← Baseline

Rr

24

775
100

775
90

7.75
0.5

162 + 14.30 Δ 1428' Pt

T.P. 7.23 15.06 2.49 8.23

160 + 00

154 + 00

T.P. 0.71 10.92 3.65 10.71

N.B.
T.P. 75' 3.48 14.36 1.67 10.88

145 + 00 P.O.T.

102

139

12.55

LT

Toe cliff
75
Beg. Indian Trail & Bar. wash

Part stake in sand

Pt
10.55
1.80

Toe cliff
55

6.01
1.55

Toe cliff
75

6.01
1.30

Baseline

Pt

75

Toe cliff
75
110

75

B.M.
10.88

Toe cliff
115

7.68
1.00

7.64
1.10

Toe cliff
125

7.64
8"

177+50

175+80

Note! M.H. W. as shown only approx.
 den. by 13.5 = High line wave wash
 5.0
 8.5 7.25 8.71

172+77.80 Δ 9°42' LT.

169+00

166+00

162+50

15.46
2

LT

Toe cliff
120

Toe cliff
55

found
here
South

used hand level

TIME + TIDE AWAITS NO MAN.

Toe cliff
20
CENTRAL GIANT
slide

Toe cliff
32

Toe cliff
45

Toe cliff
7

RT

26

M H
85

4.9 = Elev. M.H.W.
80 here So.

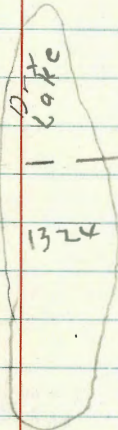
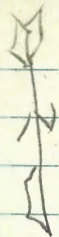
Small
of Rock 10.55
80

Baseline

10.55
90

10.55
100

Fd. Gran. Mon.



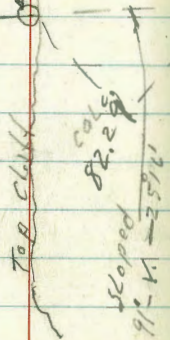
F.T. Seapp Est.

CITY
Trolley Races Park

Fd. Com. Mon. by N.O.G.

OK for line
No Rec. and as
time was short
did not check

Fd. Com. Mon.
Ser Williams
Map of Ploors



End Job

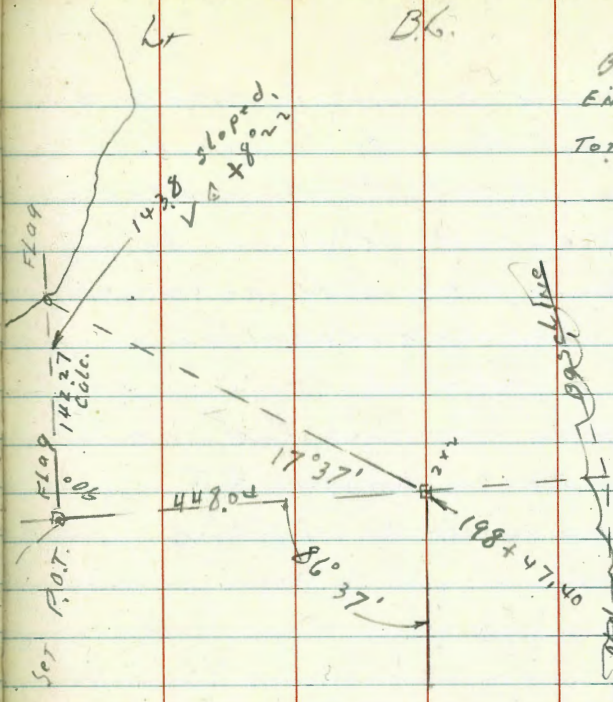
198 + 47.40

Taken on P.L. produced wire

194

190 + 16.77 Δ 7°41' Δ 222

185



B.G.

Rt 27
Beg. 1-7-47
End 1-11-47

Total Hours
OVERTIME
at all times
weather clear
Mod. wind.
(over)

approx. EL. + 6.0
U.S.G. & G.
Tide Book

Top cliff
 $\frac{125}{50}$

M.H.
50

Top cliff
 $\frac{90}{90}$

M.H.
115

Top cliff
 $\frac{40}{40}$

M.H.
135

T. cliff
 $\frac{50}{50}$

M.H.
110

Orders were to locate
Top of Hwy fills and
Base of cliffs but also
I located M.H.W. to
show the diff between
this present date and
1928 M.H.W. Line.

The Scripps Int. at
La Jolla might be
interested in this
CS 74

Indexed
S.S.K.

X-Sect. of Locust St. - 70' st. + 18' cbs.
from S.L. Poe to N.L. Russell st.

Also from Newell to Poe - location and
elev. of improvements

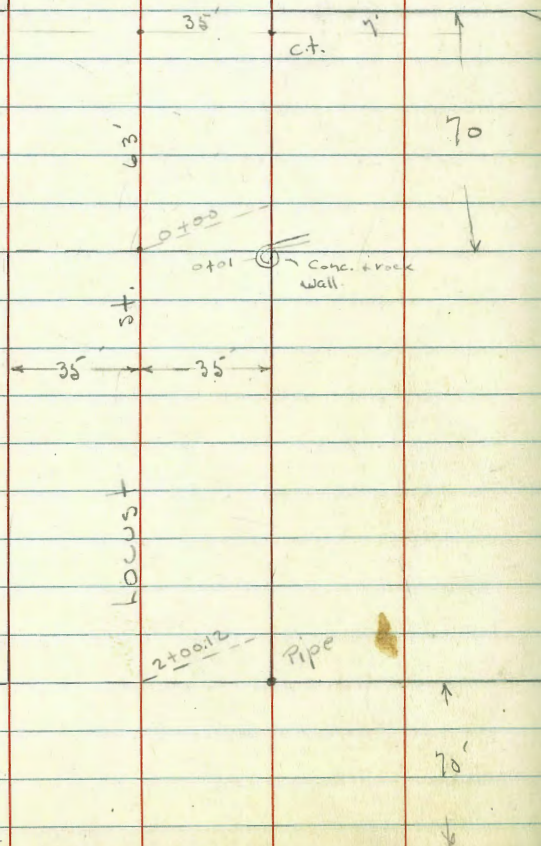
738

W.O. 230

1-31-47

Osborne
Hardin
Smith

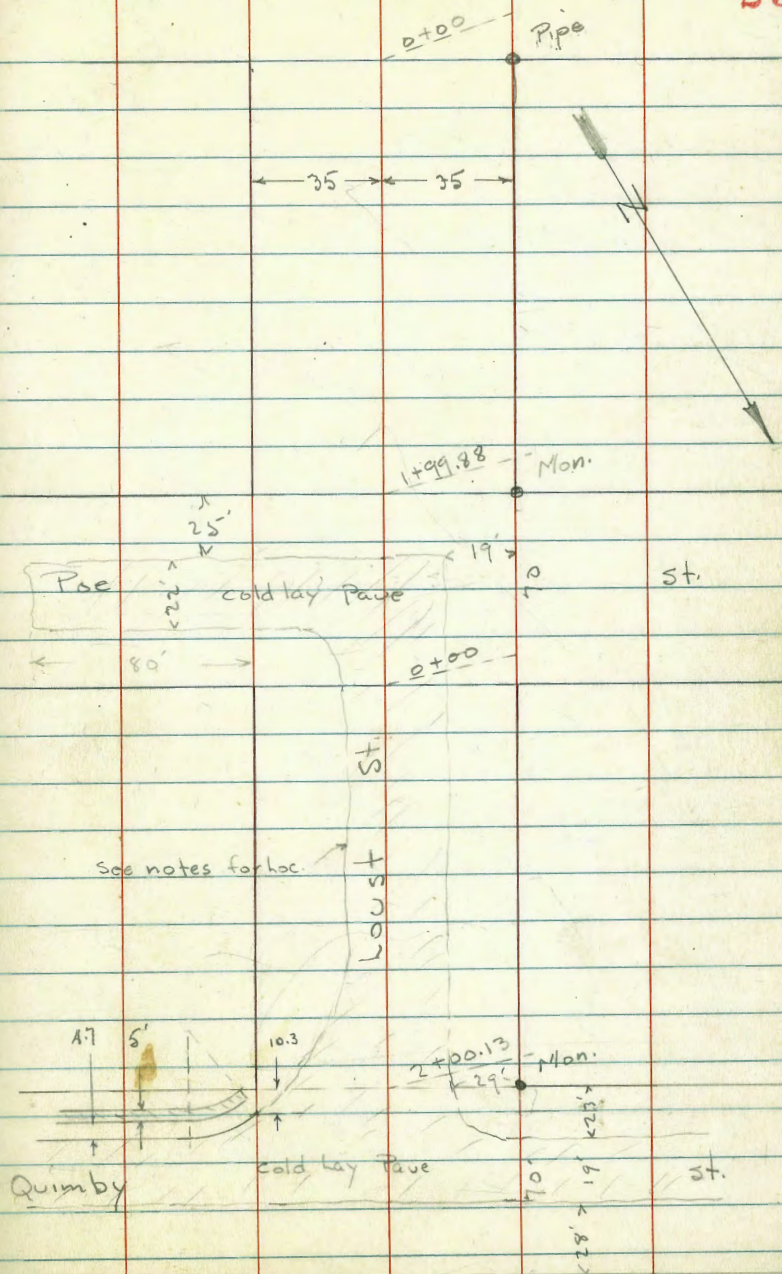
Newell St.



Oliphant St

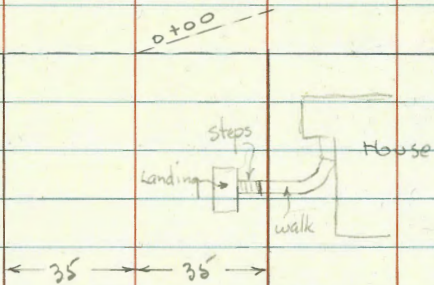
Oliphant St.

29



Quimby

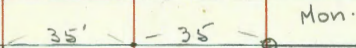
St.



Russell

70'

St.



Locust St.

Location + elev. of Improvements on
Locust St. from Newell to Poe.

± is base line.

1+63- 32.5' Rt = Beg. w side 2' Hedge 3' High

1+62- 35' Rt = end fence

1+55- 7.8 Rt = ± Tel. pole

1+00- 35.1 Rt = Beg. picket fence

1+00- 30.9 Lt = ± P. pole

partition to House 35.4 Lt.

0+97- 32.5 Lt = ± 2.6' Conc. walk to door of

0+78- 36.2 Lt = S.E. Cor. House

0+63- 30' Lt = ± 3.5' Conc. walk

0+54- 35.5 Lt = ± 2.5' Conc. walk

0+23- 4.6 Rt = ± Tel. pole

wall around plant.

0+01- 32.5 Lt = ± 5' Diam. round 6" Rock + Conc.

0+00 = N.L. Newell

7'ct. on N.W. Newell + Locust. 5.96 15.31

3.31 21.27 4.29 17.96

8.85 22.25 12.45 13.40

B.M. 3.00 25.85 22.85

S.E. 7' Mon.
Jarvis +
Evergreen

Lt. = W.

Rt. = E.

17.53
3.74
3.44
floor House

17.22
4.05
3.54
walk

17.14
4.13
3.25 = walk

13.8
7.5
100 - Vac.
lot

17.11
4.16
3.5
walk

17.66
3.6
3.5

16.84

4.43
3.25
Top wall

17.05
4.22
3.0
Top walk

16.6
4.7
3.0
ground

3.6
3.5 = on walk

15.3

6.0
3.25
ground

21.27

Locust. (Cont.)

Lt.

⌘

Rt.

32

1+99.88 = S.L. Pole

S.W. Prop. Man

8.81

14.43

12.00

11.93

12.50

1+47- 35.6 Rt. = ⌘ 3.5 Conc walk to House

11.24

11.31

9.74

35.6 = walk
47 = walk
50 = floor
at steps
to House
House

11.74

11.81

1+27- ⌘ Sing Gar. on Rt. - Conc. floor Apron

11.50

11.43

35.3
apron

47 = floor

0+98- 31' Lt. = ⌘ P pole

12.08

12.49

0+93- Rt. = ⌘ Sing Gar. Conc. floor + apron

11.16

10.75

36.6
apron

46.5 = floor

0+85- 35.1 Rt. = end fence

T.P.

10.29

23.24

8.32

17.95

23.24

0+05- 84 Rt. = ⌘ Tel. pole

0+00- 35.1 Rt. = Beg. pickett fence

2+70.12 = N.L. Oliphant = 0 too ahead

2+01- 34 Rt. = end W. side 2 Hedge

2+00.12 = S.L. Oliphant - 70' st.

21.27

Beq. Regular X-Sect. of Locust - from
S.L. Poe to N.H. Russell. 70' st. 18' obs.

0+00 = N.L. Poe

0-18 = N. cb.

0-22 = N edge Ch. on Rt

0-35 = † Poe

0-52 = S. cb.

0-65 = 30.9 Lt. = P pole

0-70 = S.L. Poe = 1+99.88 - P. 32

	Lt.	A	Rt.
	18.2	17.9	17.3
	5.0	5.3	5.9
	50	35	17
			16.9
			6.3
			7.0
			12
			edge Ch.
			6.8
			16.4
			7.2
			10-edge
			Ch.
			6.8
			13
			7.1
			17
			16.4
			16.1
			7.9
			35
			15.3
			8.2
			50
			15.0
			14.7
			12.8
	18.9	16.7	16.3
	4.3	6.5	6.9
	85	35	17
			16.3
			6.9
			16.3
			7.6
			15.6
			13
			7.5
			15.7
			8.5
			17-edge
			Ch.
			8.2
			25
			15.0
			14.7
			10.4
			8.5
			12.8
			16.6
			6.6
			35
			7.2
			16.0
			7.8
			14
			edge Ch.
			7.6
			15.6
			8.3
			17
			14.9
			8.9
			25
			14.3
			9.2
			35
			14.0
			12.3
			16.4
			6.8
			35
			7.4
			15.8
			8.1
			16-edge
			Ch. (Cold lay)
			8.2
			15.0
			8.6
			17
			14.6
			9.2
			35
			14.0
			10.9
			80-end
			Ch.
			12.3
	18.0	15.4	15.4
	5.2	7.8	7.8
	85	35	23
			8.5
			17
			14.7
			14.3
			8.9
			13.4
			9.8
			17
			13.4
			10.1
			35
			13.1
			11.5
			85: for
			Profile
			11.7
			14.6
			14.1
			13.4
			9.1
			9.8
			9.8
			17
			13.4
			10.1
			35
			12.7
			23.2
			4 - P. 32

1+50

1+22 - 31.6 Rt. - 5.5 Conc. slab for garbage cans

1+19 - 35.2 Rt. = Beg picket fence

1+10 - 17.2 Rt. = 15' Conc. Dr. to Doub. Gar. - Conc. floor

1+00

T.P. 11.23 33.81 0.66 22.58

0+91 - Double Gar. on Rt. - Conc. floor + apron

0+82 - 35 Rt. = end. fence

0+54 - 35 Rt. = Beg. picket fence

0+50

0+35 - 39 Rt. = Medi. House - Conc. found.

27.3

6.5
50

26.8

3.7
35

25.5

8.3
-1

25.1

8.1
-10

23.7

10.1
6

edge CL.

23.7

10.1

23.2

10.6
15

edge CL.

Rt.

23.2

10.6
17

23.1

10.7
37

21.6

12.2
50

21.06

12.75 slab
31.6 = edge

21.34

12.47

17.2 edge
Dr.

21.61

12.20

19.2
Brk in
Dr.

20.78

13.03

29 = Brk
in Dr.

20.51

13.30

39
floor
Gar.

24.3

9.5
50

23.7

10.1
35

22.9

10.9
-1

22.4

11.4
-9

21.4

12.4
7

edge CL.

21.4

12.4

21.0

12.8
15

edge CL.

21.0

12.8
17

19.7

14.1
35

33.81

19.31

39.3

35 = apron

19.25

39.9

39 floor

21.3

1.9
50

20.7

2.5
35

19.8

3.4
-1

19.5

3.9
-1

18.7

4.5
10

edge CL.

18.8

4.4

18.5

4.7
12

edge CL.

18.8

4.4
17

17.5

5.7
356.4
39
ground
at House

18.44

4.80

39 = floor

23.24

35' N. = ± on Sewer M.H. = Section C.L. pave

18' N. = S.cb.

a line radial

10.3 N. of SL. - 35' Rt. = end of cb. - walk ends on

02' N. = 314 Lt. = ± P pole

7.11 36.77

Prop. Mon. S.W. Cor.

4.15 29.66

2+00.13 = S.L. Quimby.

1+76-35.6 = ± Near partition to Stucco House

1+69-35.2 Rt. = end fence

26.2
0.6
4.5
on C.L.

35.3
1.5
8.5

32.3
4.5
3.5
on C.L.
Pave

31.3
5.5
3.5

30.9
5.9
17

29.7
7.1
17

29.74
7.03
Rivet
M.H.

28.1
8.7
17

28.3
8.5
17

26.9
9.9
17

25.77

11.00
34' Top
end cb.

26.8
10.0
3.5

24.92
10.8
3.5
Top-Rt.
43' Rad
Ret.

25.88

10.89
outside
edge
walk
47' Back of cb.
on Radial
line

23.5
13.3
8.5

24.3
12.5
6.0
6.0
9.7

26.00

10.77
inside edge
97' Back

30.9
2.9
5.0

30.2
3.6
3.5

28.4
5.4
17

28.0
5.8
5.8
edge C.L.

27.0
6.8
6.9

26.9
6.9

26.1
7.7
17

25.8
8.0
2.2
edge
C.L.

25.7
8.1
3.5

24.3
9.5
5.0

24.3

9.5
35.6
ground
at house

25.59

8.22
35.6
floor

33.81

Lt.

Rt.

Rt.

2-3-47

7.0.

36

0+75

Nearest part of House at 0+27 is 37 Lt.

Conc. steps + 3.5 Conc walk on top to House.

0+52 - 19.7 Lt. = ± 7.7 Conc. landing for 3.5 wide

0+50

T.P. 8.89 45.65 0.01 36.76

70' N. = N.L. Quimby = 0+00 ahead.

52' N. = N. cb.

49' N.

	Lt.				#	Rt.				
	43.1	42.7	42.5	39.6		38.1	38.8	34.0	32.9	30.7
	2.6	3.0	3.2	6.1		6.7	6.9	11.7	12.8	15.0
	50	35	30	21		17	6	7	35	50
	45.09	42.80	42.62	37.86		37.73				
	0.56	2.85	3.03	7.19		7.92				
	50	35	30.4	23.4		19.7				
	floor on walk		Top	Bot		step edge landing				
	House		step.							
	43.4	42.8	42.7	37.8		37.3	36.2	37.1	33.1	31.4
	2.3	2.9	3.0	7.9		8.4	9.5	8.6	12.6	14.3
	50	35	33	23		17		6	7	35
	along									
	House									
	42.2	41.5	34.5	33.5		33.2	33.0	31.0	29.7	28.3
	+5.4	+4.7	2.3	3.3		+3.6	4.7	3.8	5.8	5.1
	50	35	21	17		2	7	7	35	50
	36.1	33.7	32.1	30.6		29.6	29.8	28.4	27.4	
	0.7	3.1	4.7	6.2		7.2	7.0	8.4	9.4	
	50	35	17			12	7	35	50	
	34.4	32.9	31.7	30.5		29.0	27.3	26.1		
	7.4	3.9	5.1	6.3		7.8	9.5	10.7		
	50	35	17			7	35	50		
						36.77				

1+65

48.6	43.2	47.0	44.60 Lt.	42.5	41.7	40.9	41.3	36.7	36.3	24.9	32.9
+2.9	25	+1.3	10.5	3.2	4.0	4.8	4.4	9.0	9.4	10.8	12.8
45.4	37	35	27.3	27.3	17	6	6	14	17	35	50
ground at house			Top of Base wall								

1+31- end of C.L. on Lt.

42.5	48.3	43.2	44.63	42.6	41.8	40.8	41.0	36.3	35.9	34.4	32.5
3.2	+2.6	+2.5	1.02	3.1	2.9	4.9	4.7	9.4	9.8	11.3	13.2
50	37	35	27.5	27.5	17=edge	6	6	15	17	35	50
			Top wall	C.L. at wall	C.L.						

1+22- 27' Lt. = Rock steps + Angle in wall

43.05	42.5
2.60	3.2
37	27' at
Top of steps	Bot. step

1+18- 35.7 Lt. = Reg. Rock + Conc. wall.

1+09 = Double Gar. on Lt. Conc. floor + C.L.

42.56	41.3
30.9	14
35.7	17
floor gar.	edge C.L.

1+01 25.4 Rt. = P. pole

42.4	40.8	39.9	40.1	35.5	35.3	33.7	32.4
3.3	4.9	5.8	5.6	10.2	10.4	12.0	13.3
35	17	17	17	35	35	50	50
Back C.L.	edge C.L.						

1+50

0+98 - N. side Conc. apron on Lt.

42.37	40.7
3.28	5.0
35.4	17=edge
edge apron	C.L.

0+82 = S. side Conc. apron + Coldlay approach for Doub. Gar. on Lt.

43.11	29.4
2.54	6.3
49.8	17
floor Gar.	edge apron edge C.L.

45.65

Lt.

Rt.

			3.92	15.31	sw. 7' ct. Newell
	4.80	19.23	9.22	14.43	NW Mon Poc
T.P.	0.13	23.65	13.00	23.52	
			6.87	29.65	sw. Prop Mon. Quimby
T.P.	0.06	36.52	12.69	36.46	
Mon. on N.W. Cor.			7.76	41.39	

70' N. = N.L. Russell = end.

52' N. = N. cb

43.0	41.6	39.9	38.2	36.4	34.4	32.8
6.2	7.6	9.3	11.0	12.8	14.8	16.4
50	35	17		17	35	50
45.4	42.7	40.5	39.0	37.3	35.1	33.7
3.8	6.5	8.7	10.2	11.9	14.1	15.5
50	35	17	49.15	17	35	50

Tie Points - Groodyear St.

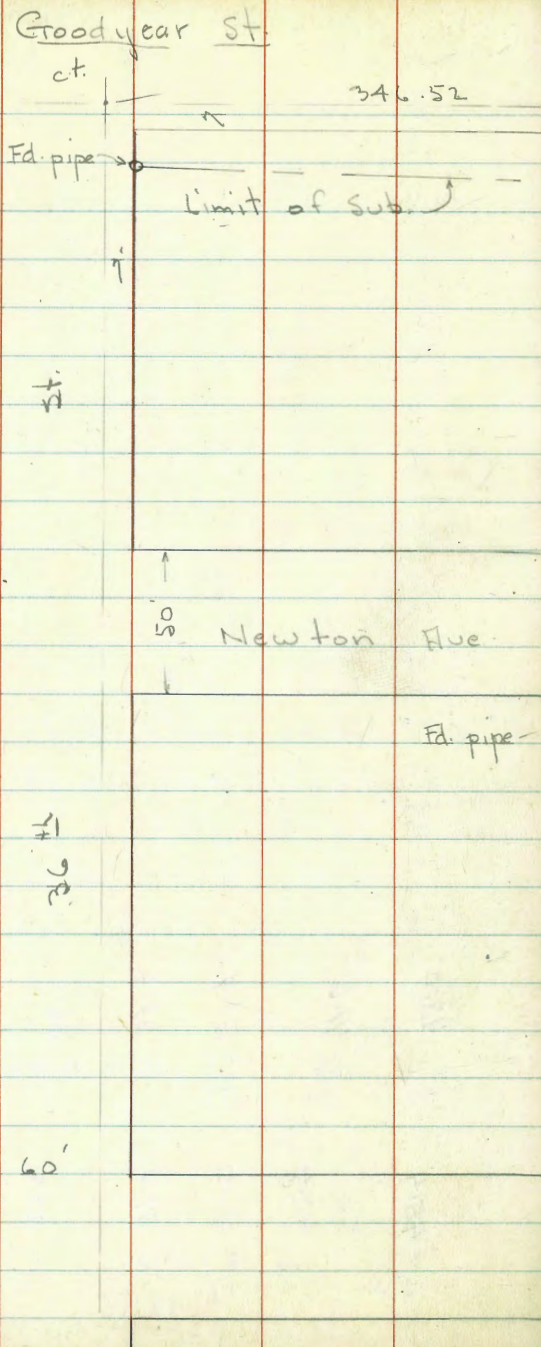
For X-Sect.

Groodyear from Boston to Natl.

2-27-47 Osborne Hardin Smith
800

W.O. 230

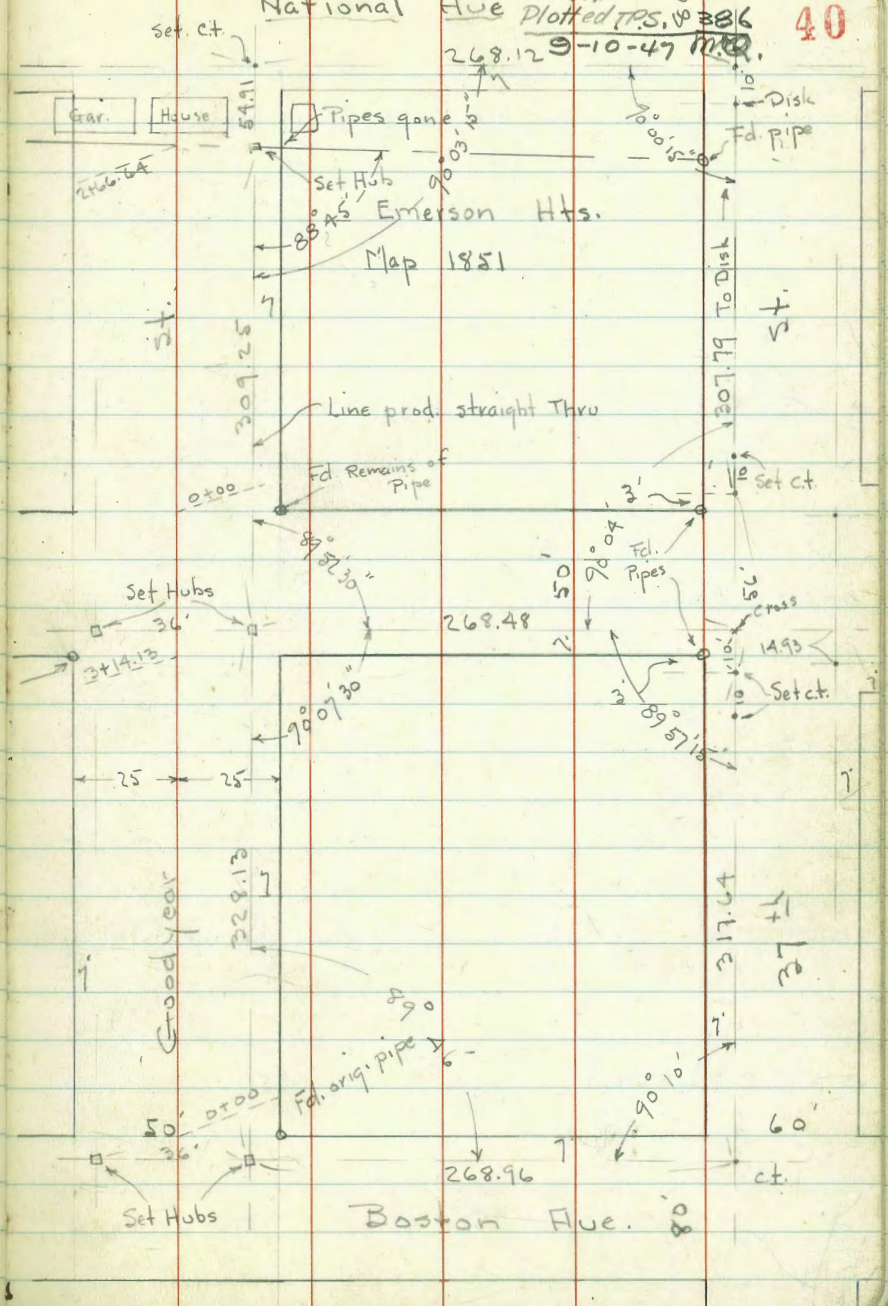
N



National Ave

Inboxed
C.S.H.
Plotted P.S. 80
268.12
9-10-47

40



X-Section. Goodyear St. 50' + 10' cbs.
from S.L. Boston to S.cb. National.

0+45

	Lt. = W.				Rt.		F
	11.0	8.6	7.2	6.3	5.1	4.2	4.0
	40	32	28	18	18	25	40
		26.0	21.3	18.2	29.4	30.3	30.5

0+13 = 39.6 Rt. = R House - Conc. found

44.4 ground
39.6 at found
19.3 floor
39.6 = floor

0+00 = N.L. Boston

	11.3	10.1	9.1	7.1	5.6	5.2	4.7
	40	25	25	1	15	25	40
	23.2	24.4	25.4	27.4	28.9	29.3	29.8

0-14 = N.cb.

	13.2	11.0	10.1	9.5	7.0	5.2	5.1
	50	25	25	25	15	25	40
	21.0	23.5	24.4	26.0	27.6	28.0	28.4

0-40 = S - Outs along Boston for profile

	22.1	13.0	11.2	10.2	8.5	8.2	8.2
	100	25	25	18	15	25	50
	12.4	21.5	23.0	24.3	26.0	25.9	26.2
	16	25	18	10	15	25	100
	18.0	21.5	23.0	24.3	26.0	25.9	26.2

0-80 = S.L. Boston

	17.2	12.2	12.2	12.2	12.2	12.2	12.2
	25	25	25	25	25	25	25

B.M.	5.55	34.45	8.18	28.90	N.E. Pipe slut 7' ct. Boston + 37th	34.45
	34.3	37.08		33.65		

0+43 51 Rt = \neq House

0+20

50' N. = N.L. Newton = 0+00 ahead.

T.P. 7.90 37.19 5.16 29.29

40' N. = N. cb.

25' N. = \neq - Newton has been X-Sectioned

10' N. = S. cb.

3+14.13 = S.L. Newton - 50' st. 10 cbs.

2+90

6.57
40

6.53
25

6.52
15

5.58

4.58
15

2.53
25

2.53
40

5.53
50

2.59
25

2.56
15

1.59

1.59
15

1.58
25

1.52
50

2.56
25

1.57
15

0.34
3

0.34
15

2.00
25

7.34
40

5.50
25

4.51
15

2.55

2.53
15

2.56
25

2.57
40

4.57
40

6.53
25

5.53
15

2.59

2.56
15

2.55
25

2.54
40

29.9

32.2

33.1

34.7

34.9

34.7

34.5

4.57
40

6.53
25

5.53
15

2.59

2.56
15

2.55
25

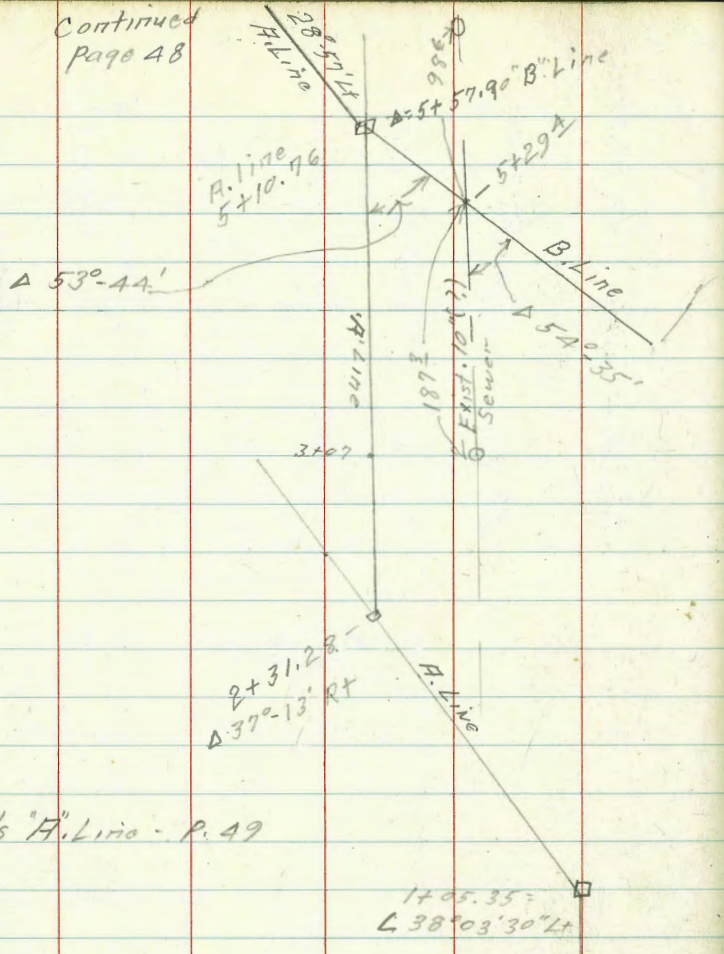
2.54
40

0.37
0.01
Floor

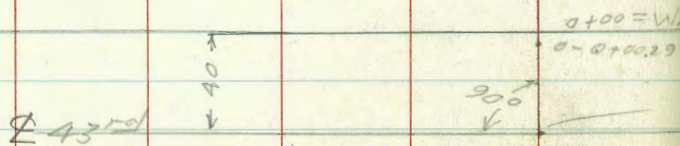
43

34.45

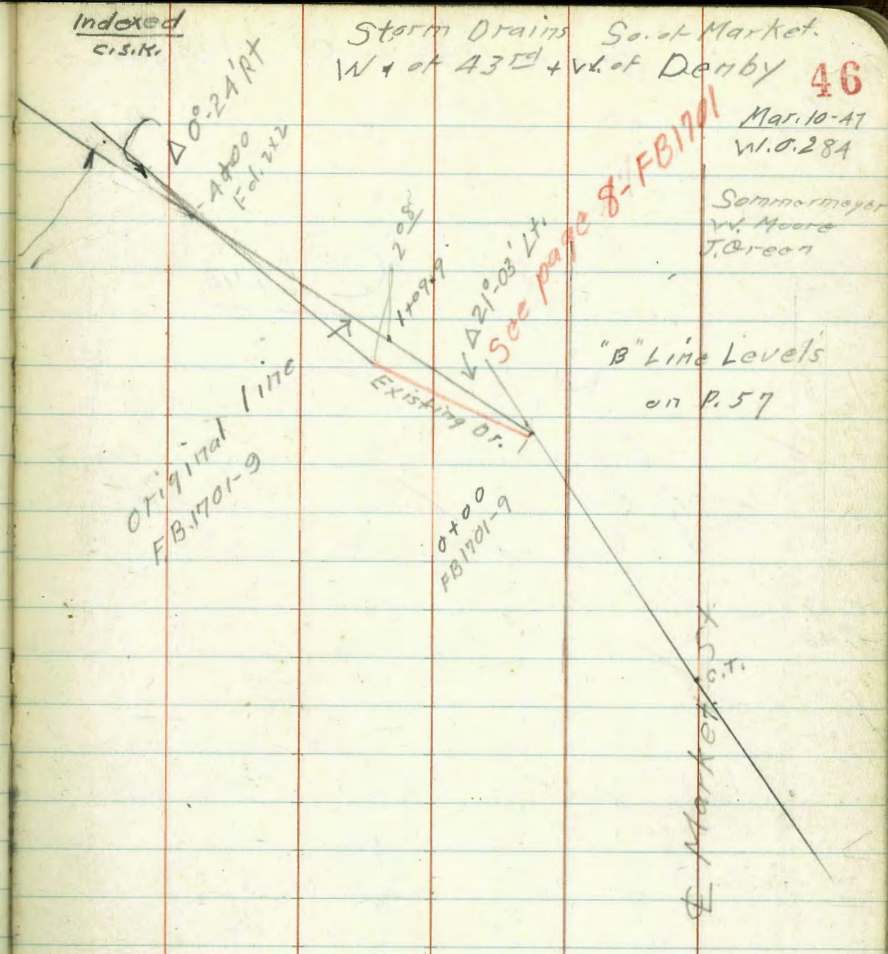
Continued
Page 48



Levels "H. Line" - P. 49



Indexed
C.S.K.



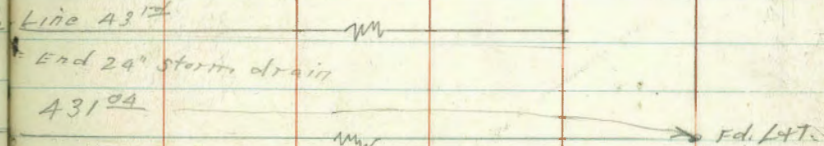
Storm Drains So. of Market
W. of 43rd + v. of Denby **46**

Mar. 10-47
W.O. 284

Sommarmayer
vt Moore
J. Green

"B" Line Levels
on P. 57

← 40' →

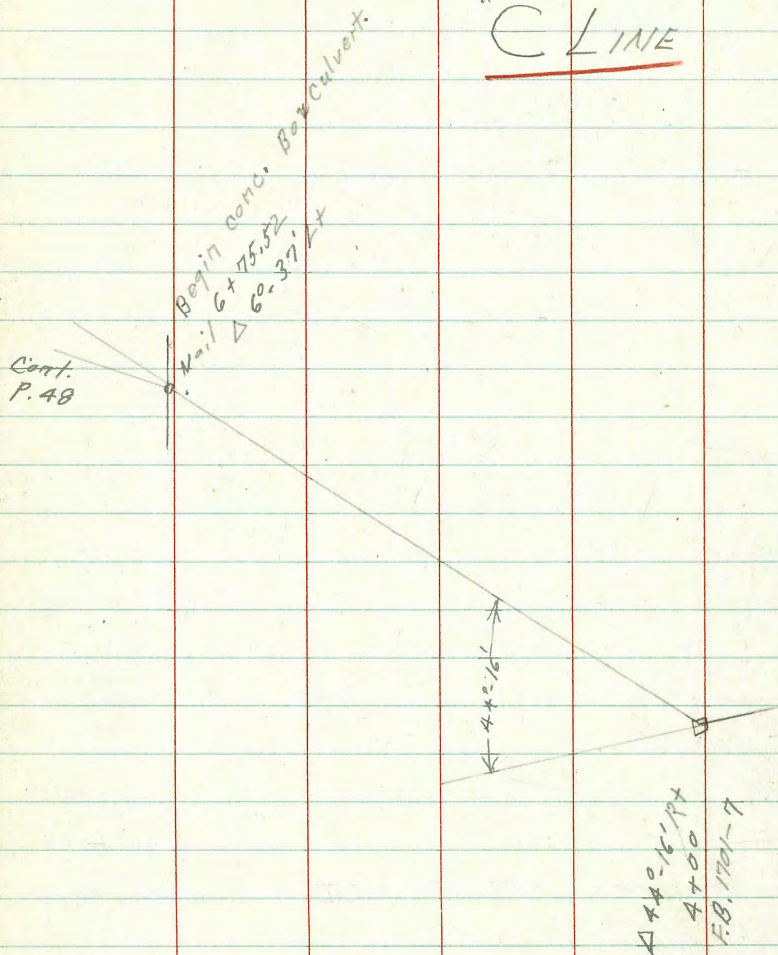


Storm Drain S. of Market - W. of Morrison = "C" Line.

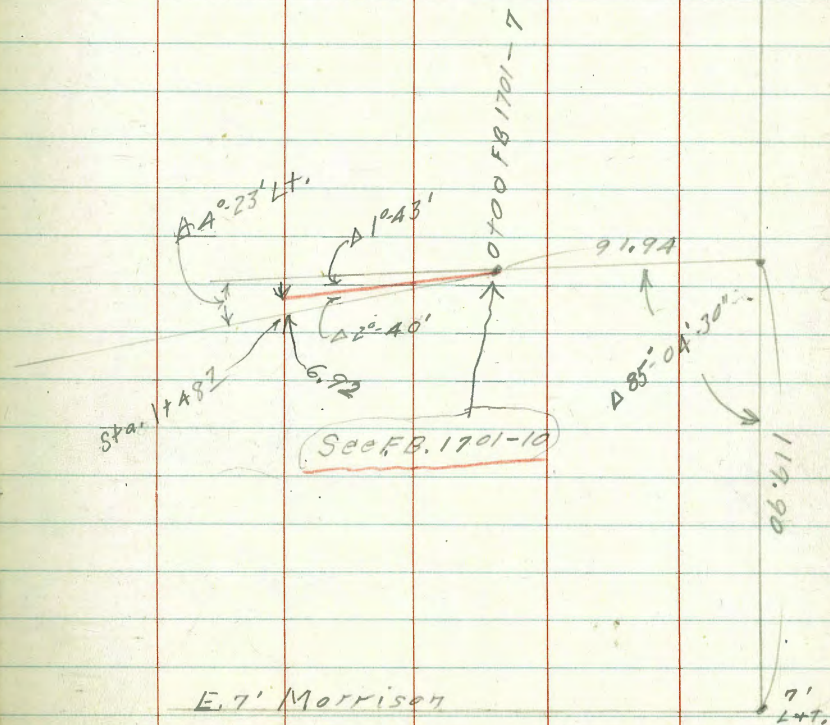
3-10-47
Summer, 1947

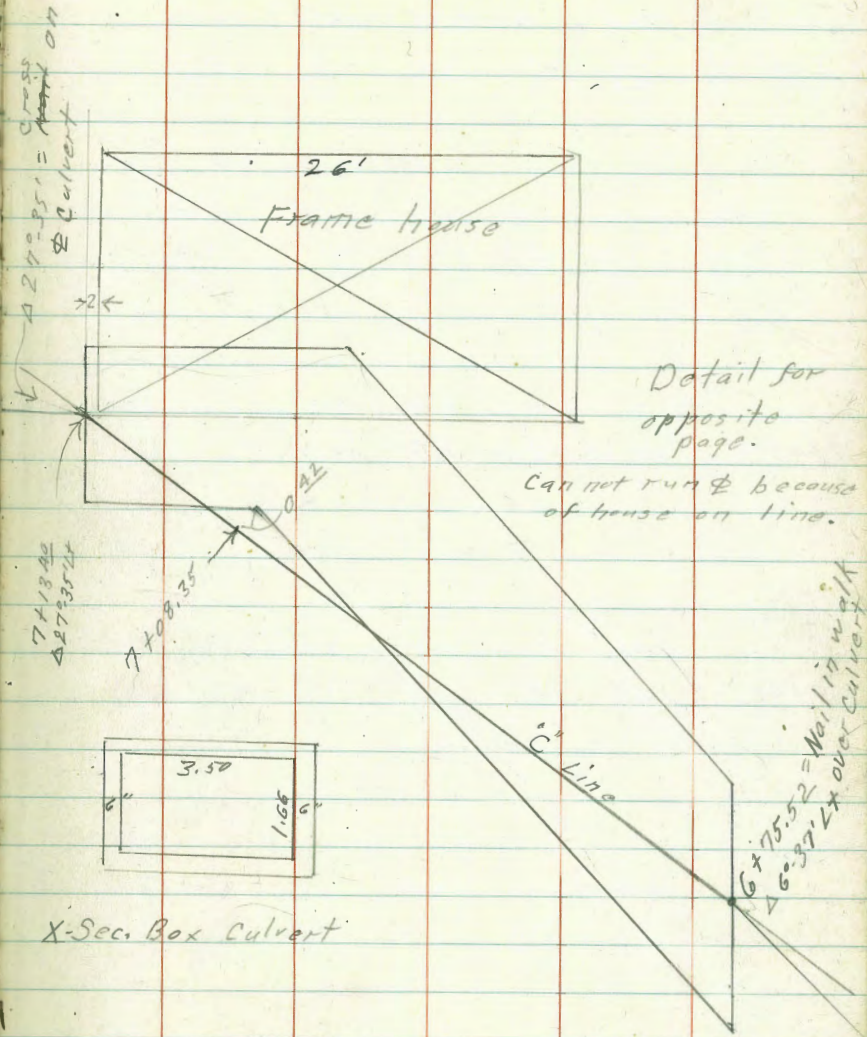
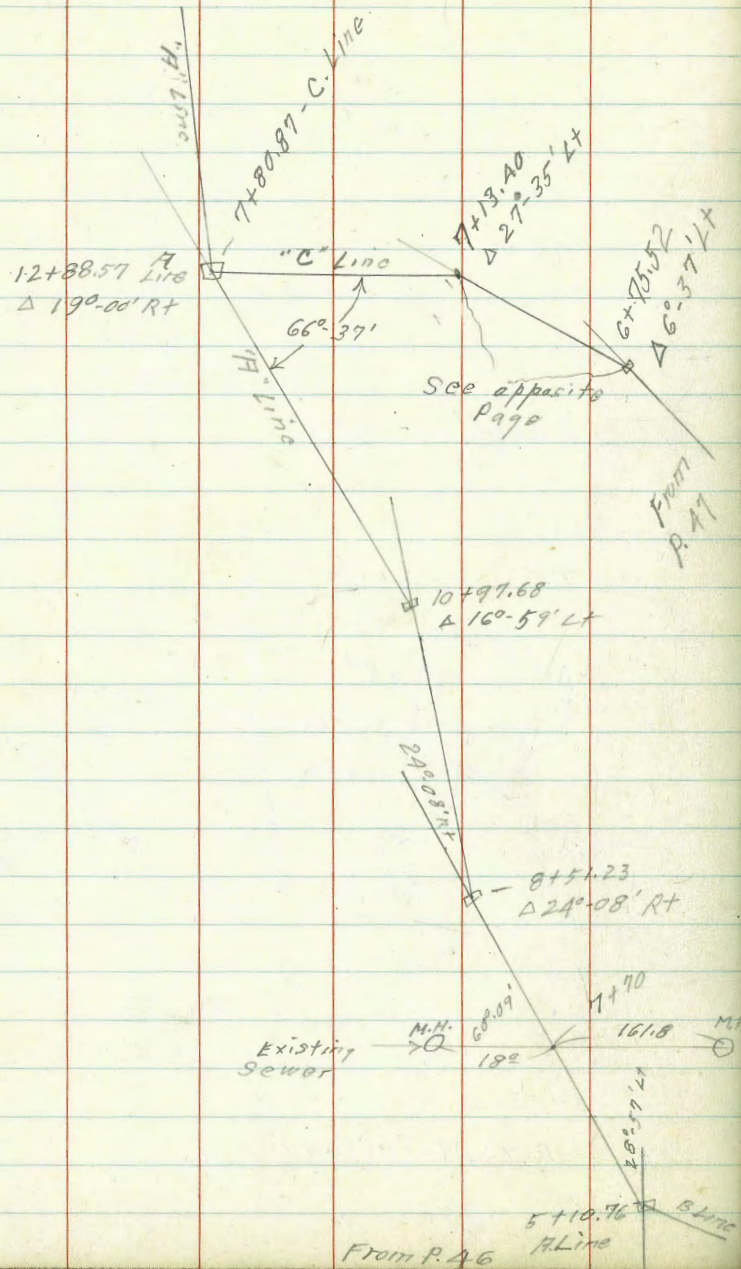
Work Order 284

"C" LINE



Levels on P58





Levels "A" Line Storm drain
 Marsena park.
 0+00 = W.L. 43rd - Sketch P. 46.

Summary of
 W Moore
 Green 3/1/47 **49**

T.P.	3.06	120.41	111.2	117.35	LT	BL	118.3	48.3	121.8	123.9	129.8
2+00					8.0 50	10.9 6	10.2 5	10.2 5	6.7 20	4.6 35	3.7 70

1+50					8.3 50	8.0 2	7.3 2	8.4 2	5.1 30	1.8 50	
------	--	--	--	--	-----------	----------	----------	----------	-----------	-----------	--

1+05.35	$\Delta 38^{\circ} 03' 30''$ Lt.	takey on split			120.7 7.8 20	120.6 7.7 10	120.8 7.7	121.0 7.5 10	122.3 6.2 20		
---------	----------------------------------	-------------------	--	--	--------------------	--------------------	--------------	--------------------	--------------------	--	--

0+60					122.9 5.6 15	123.5 5.0 4	122.5 6.0 2	121.2 7.3	122.6 5.7 2	129.3 4.2 10 40	
------	--	--	--	--	--------------------	-------------------	-------------------	--------------	-------------------	--------------------------	--

0+00					126.8 1.7 20	126.3 2.2 6	121.9 6.6	127.0 1.5 8	127.2 1.3 20		
------	--	--	--	--	--------------------	-------------------	--------------	-------------------	--------------------	--	--

0-0.29 = End Exist 24" Conc. pipe

9 E.B.R 43 & Market.	2.04	128.47	7.32	126.43							
	6.21	133.75	—	127.54							

122.03
6.22
114.07
128.47 ✓

LT

BL

RT

4+00

116.9	119.0	113.5	113.8	112.7	119.3
$\frac{3.5}{40}$	$\frac{6.4}{15}$	6.8	$\frac{6.6}{30}$	$\frac{6.7}{60}$	$\frac{6.1}{100}$

3+50

119.1	115.6	115.0	115.0	116.7	117.0
$\frac{1.3}{30}$	$\frac{4.8}{10}$	5.1	$\frac{5.4}{30}$	$\frac{3.7}{55}$	$\frac{3.4}{100}$

3+15

120.4	117.1	115.6	116.5	117.5	125.7
$\frac{0.0}{40}$	$\frac{3.3}{25}$	$\frac{4.8}{10}$ Wash	3.9	$\frac{3.1}{20}$	$\frac{+4.8}{80}$

3+07

20² Rt = M.H. (See sewer plan)

116.7	117.98	108.98
4.2	$\frac{2.43}{\text{M.H.}} / \text{Rim}$	$\frac{11.43}{\text{Invert}}$

2+90

118.9	116.9	115.7	117.0	117.6	120.1
$\frac{1.5}{30}$	$\frac{4.0}{20}$	$\frac{4.2}{6}$ Wash	3.4	$\frac{2.8}{2}$	$\frac{0.3}{40}$

2+31.28 - A

37°-13' Rt.

Taken on split

120.3	119.3	117.3	117.0	118.6	122.1	126.2
$\frac{0.1}{20}$	$\frac{1.1}{10}$	3.1	$\frac{3.4}{14}$ Wash	$\frac{1.9}{22}$	$\frac{+2.7}{40}$	$\frac{+5.8}{90}$
		120.41 ✓				

120.41 ✓

T.P. 4.33 113.72 110.2 109.39

6+00

LT	BL	RT
112.8	112.2	109.9
$\frac{5.6}{20}$	$\frac{8.2}{12}$	$\frac{11.0}{8}$
		$\frac{11.4}{12}$
		$\frac{9.5}{30}$

5+76

116.2	109.7	111.9	111.0
$\frac{4.2}{27}$	$\frac{10.7}{10}$	8.5	$\frac{9.4}{30}$

5+60

115.9	109.9	108.6	111.0	111.9	111.7
$\frac{5.0}{22}$	$\frac{10.5}{15}$	$\frac{11.8}{10}$	$\frac{9.4}{3}$	9.0	$\frac{8.7}{30}$
					$\frac{1.9}{10}$

5+46

115.3	111.5	111.9	112.0
$\frac{5.1}{22}$	$\frac{8.9}{16}$	9.0	$\frac{8.4}{30}$

5+10.76 Δ 28° 57' Lt. Also junction "B" line
Taken on split A

119.5	112.4	112.07	112.8	115.9
$\frac{0.9}{60}$	$\frac{8.0}{30}$	$\frac{8.34}{30}$	$\frac{9.6}{30}$	$\frac{4.5}{60}$
		EXL 345		

4+50

120.41

116.2	113.0	112.5	113.0
$\frac{4.2}{50}$	$\frac{7.4}{30}$	7.9	$\frac{7.4}{30}$
		120.41 ✓	

L+

B.L

R+

7+50

109.1	108.1	6.0	107.9	107.1	108.3	108.1
4.6	5.6	6.3	5.8	6.6	5.4	5.6
<u>40</u>		<u>15</u>	<u>45</u>	<u>5.6</u>	<u>60</u>	<u>75</u>
				Wash		

7+18 L IN wash

110.6	108.5	109.2	108.2	107.1	108.3	108.7
3.1	5.2	4.5	5.5	6.6	5.4	5.0
<u>30</u>		<u>15</u>	<u>92</u>	<u>95</u>	<u>98</u>	<u>110</u>
				Wash		

7+00 L IN wash

111.1	109.6	109.2	107.2	108.9	109.7
2.6	4.1	4.5	6.5	4.8	4.0
<u>20</u>		<u>84</u>	<u>92</u>	<u>100</u>	<u>120</u>
			Wash		

6+70

112.2	111.6	110.7	110.2	107.9	108.7	109.7
1.5	2.1	3.0	3.5	6.3	5.0	4.0
<u>25</u>	<u>15</u>		<u>3.6</u>	<u>41</u>	<u>45</u>	<u>6.0</u>
				Wash		

6+25

112.7	112.1	107.9	109.7	110.1
0.0	1.6	5.8	4.9	3.6
<u>15</u>		<u>6</u>	<u>10</u>	<u>30</u>

6+15

113.7	112.0	107.7	107.9	109.5	110.9
0.0	0.7	6.0	5.8	4.2	2.8
<u>15</u>	<u>8</u>		<u>5</u>	<u>7</u>	<u>90</u>

113.72 ✓

113.72 ✓

T.P. 4.69 110.54 7.87 105.85

8+70

107.9 105.2
 $\frac{6.3}{55}$ $\frac{8.5}{46}$

102.3 100.6 103.3 105.2 105.9 106.1 108.1
 $\frac{10.4}{44}$ $\frac{13.1}{32}$ $\frac{10.4}{25}$ $\frac{8.5}{20}$ $\frac{8.3}{20}$ $\frac{7.6}{20}$ $\frac{5.6}{40}$
 wash

8+51.23 = Δ 24°-08' RT Taken on split

106.2 106.4 102.9 102.9 105.6 105.8 107.7 107.7 109.3
 $\frac{7.5}{35}$ $\frac{8.3}{25}$ $\frac{10.8}{22}$ $\frac{10.8}{13}$ $\frac{8.1}{10}$ $\frac{7.9}{20}$ $\frac{6.0}{20}$ $\frac{6.0}{40}$ $\frac{4.4}{50}$

8+07 Just of 3 washes

167.2 106.5 103.8 109.2 105.7
 $\frac{6.5}{15}$ $\frac{7.2}{7}$ $\frac{7.9}{10}$ $\frac{9.5}{10}$ $\frac{8.0}{20}$

8+00 June'

107.0 106.9 109.0 106.5 109.0 109.8 105.7
 $\frac{6.7}{20}$ $\frac{6.8}{10}$ $\frac{9.9}{\text{side wash}}$ $\frac{7.2}{5}$ $\frac{9.7}{\text{side wash}}$ $\frac{8.7}{20}$ $\frac{8.0}{100}$
 Side Draw

7+80 L in wash

107.3 105.9 107.0 106.9 106.2 106.9
 $\frac{6.4}{20}$ $\frac{7.8}{10}$ $\frac{6.7}{12}$ $\frac{6.8}{10}$ $\frac{7.5}{3}$ $\frac{6.8}{10}$
 Side wash INwash

7+70 Ent. " sewer 60°-09' Lt to line
 113.72 ✓

101.01 107.26 107.3 110.14 103.16
 $\frac{12.71}{\text{INVERT}}$ $\frac{6.96}{18}$ $\frac{6.4}{\text{Rim}}$ $\frac{3.58}{\text{Rim}}$ $\frac{10.56}{\text{INVERT}}$

113.72 ✓

T.P. 5.57 106.18 ✓ 9.63 100.91

10+97.68 L 16"-59" Lt. taken on split

10+55

10+33 L in wash

10+00 L in wash

9+50

9+00

110.54 ✓

LT

B.L

RT

101.3 100.9 98.8 100.8 107.0

$\frac{7.2}{30}$ $\frac{7.6}{13}$ $\frac{11.7}{10}$ 9.7 $\frac{3.5}{15}$
wash

102.9 101.8 99.0 101.9 105.9

$\frac{8.1}{40}$ $\frac{8.7}{13}$ $\frac{11.5}{1}$ 9.1 $\frac{5.1}{10}$
wash

103.0 101.9 100.9 99.8 101.9 105.8

$\frac{7.5}{35}$ $\frac{8.6}{12}$ $\frac{10.1}{8}$ $\frac{10.7}{1}$ $\frac{8.6}{1}$ $\frac{4.7}{15}$

105.0 109.0 101.6 101.6 101.5 102.7 109.7

$\frac{5.5}{60}$ $\frac{6.5}{47}$ $\frac{8.9}{4.7}$ $\frac{8.7}{35}$ $\frac{7.0}{20}$ 7.8 $\frac{5.8}{15}$

105.7 100.7 100.5 102.6 103.1 109.3 106.0

$\frac{4.8}{63}$ $\frac{7.8}{59}$ $\frac{10.0}{54}$ $\frac{7.7}{53}$ $\frac{7.4}{11}$ 6.2 $\frac{4.5}{15}$
wash

110.5 107.6 102.2 109.9 109.2 107.1

0.0 $\frac{2.7}{70}$ $\frac{8.3}{62}$ $\frac{5.6}{57}$ 6.3 $\frac{3.4}{40}$ $\frac{3.4}{15}$
wash

110.54 ✓

12+00

LT	B.L.	RT
100.9	100.5	97.8
<u>5.6</u>	<u>6.0</u>	<u>8.7</u>
15	7	6
		7.7
		<u>5.6</u>
		6
		100.9
		100.7
		<u>5.8</u>
		15

11+80

101.6	101.9	97.9	97.8	97.9	100.9	101.1
<u>4.8</u>	<u>4.6</u>	<u>8.6</u>	<u>8.7</u>	<u>8.6</u>	<u>5.6</u>	<u>5.4</u>
10	5	3		4	9	15

11+71 7⁵RT = ctr. 16" Eucalyptus

11+52 = Top 4" Sewer Lat. ←

11+52 = Int. 3/4" Water service tied to

11+51 = Φ Bridge 1" deck 4XA stringers
4-2XA post on Φ 4-2XA posts 11²RT

11+51 = Int. of a 1 1/2" pipe line ?

11+35

103.7	102.7	99.2	97.7	97.7	103.8	103.5
<u>2.8</u>	<u>2.8</u>	<u>2.2</u>	<u>8.8</u>	<u>8.8</u>	<u>3.1</u>	<u>3.0</u>
15	7	1		1	10	15

11+28 3⁵LT = ctr. 1" Eucalyptus11+26 3⁵RT = ctr. 1" Eucalyptus

11+17

101.6	99.3	98.1	97.9	101.6	103.2
<u>4.9</u>	<u>7.2</u>	<u>8.4</u>	<u>8.6</u>	<u>4.9</u>	<u>3.3</u>
12	5	2		5	10

106.48

106.48 ✓

Lt

B.L.

Rt

56

T.P. 2nd 12+88.57 4.41 97.82 ✓

13+75

98.9

96.5

97.9

 $\frac{9.8}{10}$

5.7

 $\frac{4.8}{10}$

13+65 7' Lt = ctr. A" Eucalyptus

13+25

99.9

97.9

97.1

97.9

98.7

 $\frac{2.3}{12}$ $\frac{4.8}{8}$ $\frac{5.1}{5}$

4.8

 $\frac{2.5}{10}$ T.P. 4.41 102.23 8.66 97.82 ✓102.23 ✓13+00 7th Lt = ctr 2' Eucalyptus

12+88.57 = A 19° 00' Rt. Also Junct. "C" Line

100.9

100.2

97.3

97.82

 $\frac{5.6}{15}$ $\frac{6.3}{9}$ $\frac{7.2}{4}$ $\frac{8.66}{2 \times 2 \div 1.5}$

12+81 10' Lt = ctr. A" Eucalyptus

12+78 6' Rt. = ctr 2' Eucalyptus

12+71 13' Lt = ctr 3' stump (dead)

12+40

100.9

99.8

98.2

98.5

99.6

100.0

 $\frac{5.6}{20}$ $\frac{6.7}{10}$ $\frac{8.3}{6}$

8.0

 $\frac{6.9}{6}$ $\frac{6.5}{15}$

106.48

106.48 ✓

Levels "B." Line sketch P. 46

LT

BL

RT

57

T.P. $\frac{0.01}{112.07}$
 should be
 A 5+10.76 Paq051 H Line 5.64 112.08

5+57⁹⁰ = Junction with H. Line at
 H. Line Sta. of 5+10.76

112.08
5.64

5+29² = Int. "Sewer Δ 54² 35' Rt.

112.7 111.31 105.05
 see P. 50 for El. 5.0 $\frac{0.41}{98.6}$ $\frac{12.67}{1177}$
 187.3 Invert

5+00

112.8 112.7 112.0 112.5 113.9
 $\frac{4.9}{20}$ 5.0 $\frac{5.7}{3}$ $\frac{5.2}{7}$ $\frac{4.3}{25}$

4+50

113.9 112.7 112.1 112.8 118.5
 $\frac{4.3}{35}$ $\frac{5.0}{7}$ $\frac{5.6}{4}$ 4.7 $\frac{3.2}{20}$

2 x 2 stub.
 A+00 4.75 117.72 — 112.97
 FB1701-AG +2.12

Flow Line - Outlet 42" Pipe. 115.09

Levels "C" Line - Sketch P 47

T.P. 3.70 106.56 8.19 102.66
6+50

5+85

5+50

5+38

4+75

4+20

2x stub = 4+00
FB1701-P 8

5.44

110.85

105.41

+5.11

58

LT	BL	RT	
103.0	101.0	101.8	109.8
$\frac{7.8}{25}$	9.8	$\frac{9.0}{15}$	$\frac{6.1}{25}$

105.9	102.9	101.8	100.8	101.6	105.6
$\frac{5.0}{10}$	8.0	$\frac{9.1}{18}$	$\frac{10.1}{19}$	$\frac{9.3}{20}$	$\frac{5.3}{30}$

105.2	103.9	101.8	105.2
$\frac{5.7}{10}$	7.5	$\frac{9.0}{9}$	$\frac{5.7}{20}$

102.6	103.0	102.2	102.6	103.6	105.0
$\frac{6.2}{10}$	$\frac{7.9}{3}$	8.6	$\frac{8.2}{2}$	$\frac{7.3}{70}$	$\frac{5.9}{15}$

106.8	103.6	105.2	107.8	108.6
$\frac{4.1}{36}$	$\frac{7.3}{24}$	$\frac{5.6}{19}$	3.0	$\frac{2.2}{5}$

107.6	106.8	107.8	107.0	109.6
$\frac{3.3}{25}$	$\frac{4.0}{10}$	$\frac{6.0}{5}$	3.9	$\frac{1.3}{20}$

FLMC. 24" Pps : 110.52

7+13.40 End box culvert start Wood
side flume rough conc. floor
3.8 wide

	L+		BL		R+	
	100.8	100.8	98.8	98.8	98.8	100.6
	$\frac{5.8}{7}$	$\frac{5.8}{2}$	$\frac{7.8}{1.9}$	7.78	$\frac{7.8}{1.9}$	$\frac{6.0}{2}$
						$\frac{6.1}{10}$

7+13.40 = Top culvert box

	100.5	100.7	101.11	101.1	101.1
	$\frac{6.1}{15}$	$\frac{5.9}{2}$	5.45	$\frac{5.5}{2}$	$\frac{5.5}{7}$

6+75.52

	101.8		101.61		102.1
	$\frac{4.8}{15}$		4.95 Top of box		$\frac{4.5}{15}$

6+75.52 = Beg. culvert (P. 40)

99.30
7.20
invert

6+74

	101.8	101.9	99.6	99.5	99.6	102.1	102.2
	$\frac{4.8}{15}$	$\frac{4.7}{5}$	$\frac{7.0}{3}$	7.1	$\frac{7.0}{3}$	$\frac{4.5}{6}$	$\frac{4.2}{15}$

6+65

	101.9	101.7	101.0	101.6	102.1
	$\frac{4.7}{10}$	$\frac{4.7}{4}$	5.6	$\frac{5.0}{5}$	$\frac{4.5}{15}$

106.56 ✓

106.56 ✓

Marsceme Park
Storm Drain

3/12/47

Sommermaye
W Moore
J Green

LT

BL

RT

60

BE

Notes Reduced. 3-20-47

T.P.

A Line Page 56 9.73
+ 12+88.57

should be

$\frac{0.01}{97.82}$

97.83 ✓

7+80.87 Junction with "A" Line
"A" Line sta. 12+88.57

97.83

8.73

7+67

Ground.

100.0

100.0

98.6

98.5

98.5

99.8

100.1

$\frac{6.6}{10}$

$\frac{6.6}{2}$

$\frac{8.0}{1.8}$

8.1

$\frac{8.1}{1.8}$

$\frac{6.8}{2}$

$\frac{6.5}{10}$

7+67

End Wood Flume + App. End of
rough conc. Flume Floor

97.6

97.59

97.6

$\frac{9.0}{1.8}$

8.97

$\frac{9.0}{1.8}$

106.56

106.56 ✓

Cross Section Meade Ave.
35th St. to W.L. 3rd St.
B.M. #1296-79

Indexed
c.s.k.
W.O. 60108

4.25

2

Rt. N

April 17-47
Sisson
McCoy
Allen
Becker
61

0+0 = W.L. 35th St

386.78	386.38	386.54	386.86	386.82	386.89	387.19
5.58 28.26	5.08 28.64	5.92 14	5.50	5.54 14	5.57 27.4 9d	5.27 27.46

0-12 = W.C. 35th

386.76	386.15	386.27	386.39	386.45	386.61	386.68	386.70	387.20
5.70 28.26	5.71 28.64	5.19 28	5.07 14	5.01	5.85 14	5.78 27.4	5.76 28.64	5.21 28.64

0-26

386.75	386.87	386.96	387.06	387.18	387.23	387.28
5.71 28	5.59 28	5.50 14	5.40	5.29 14	5.23 27.4	5.18 28

0-40 = W.C. 35th St

386.92	387.00	387.01	387.07	387.25	387.37	387.51
5.54 28	5.46 28	5.45 14	5.39	5.21 14	5.09 27.4	4.95 28

0-54

386.88	386.92	386.97	387.06	387.14	387.23	387.31
5.58 28	5.54 28	5.49 14	5.40	5.29 14	5.23 27.4	5.15 28

0-68 = F.C. of 35th St

386.85	386.26	386.41	386.40	386.66	386.76	386.68	386.74	387.07
5.41 28.64	6.20 28.64	6.05 28	5.06 14	5.80	5.70 14	5.78 27.4	5.72 28.64	5.39 28.64

For Fast Line 35th St See #1768 Page 25

B.M. 5.29 392.46

387.17

N.Y.S.P.
Meade Ave.
35th St.
#1768-25

392.46 ✓

Notes Reduced & Checked
by R.E. Coburn 4/24/47

1+75

387.45	386.86	387.30	387.64	387.56	387.26	387.87
5.01	5.60	5.16	4.82	4.90	5.20	4.59
28.03	28.54	14	14	14	27.4 = 54	27.4 = 54

1+43.5 = W L Alley South

387.49	387.20	387.39	386.85	387.05	387.29	387.49	387.22	387.68
4.97	5.11	5.07	5.61	5.11	5.13	4.97	5.24	4.78
40.03	40.03	28.03	28.03	14	14	14	27.4	27.4

1+33.5 = E L Alley South

387.20	386.89	387.04	387.30	387.51	387.19	387.65
5.26	5.57	5.12	5.16	4.95	5.24	4.81
40	28	14	14	14	27.4	27.4

1+23.5 = E L Alley South

387.54	387.34	387.34	386.86	387.03	387.21
4.92	5.12	5.15	5.60	5.13	5.25
40.03	40.03	28.03	28.03	14	14

1+0

387.21	386.63	387.04	387.23	387.28	387.03	387.44
5.25	5.83	5.12	5.23	5.18	5.18	5.02
28	28	14	14	14	27.4	27.4

0+80

386.90	386.50	386.73	387.01	387.06	386.97	387.34
5.51	5.96	5.73	5.15	5.10	5.19	5.12
28.03	28.03	14	14	14	27.4 = 54	27.4 = 54

39216 ✓

39216 ✓

3713 = WCB Swift South

2795 = Z Swift to South

2729 = ECB Swift to South

2762 = ECB of Swift to North

2750 = EL Swift to North

270

392.46 ✓

LT	Z	RT
387.27 519 10-cb	386.82 554 94	386.86 560 28
387.16 530 40	387.24 532 28	387.25 531 19
387.79 467 40-cb	387.19 537 40 94	387.34 512 28 14
387.78 468 28-cb	387.14 533 28 94	387.44 502 14
387.80 466 28	387.14 533 28	387.43 503 14
387.57 489 28-cb	386.94 552 28 94	387.23 523 14
		387.97 547 14
		387.11 535
		387.10 534 14
		387.07 533 27.4
		387.14 532 40
		387.41 505 STOP SWIFT H
		387.51 495 14
		387.66 480 27.4
		387.79 467 40
		387.50 496 14
		387.75 471 27.4
		388.08 458 40
		387.53 493 14
		387.75 471 27.4
		387.66 481 40-cb 94
		388.20 456 40-cb
		387.62 481 14
		387.6 485 27.4
		388.13 433 27.4
		387.47 499 27.4 = 94
		388.07 459 27.4-cb

392.46 ✓

1+33.5 = F. H. Hiller South

4.	Z	PT.
385.91	385.46	385.64
385.82	385.71	385.58
386.16		
5278 70	423 28	405 14
5287	398 14	4.11 27.4-60
		3.53 27.4-66

1+23.5 = F. L. Hiller South

386.49	386.28	386.19	385.60	385.70	385.92	385.78	385.60	386.22
530 70-6	391 40-44	5.50 28-63	4.09 28-50	599 14	5.77	391 14	4.09 27.4	3.47 27.4

1+0

386.36	385.70	385.89	386.21	386.11	385.85	386.66
533 28	599 28	580 14	5.48	538 14	5.84 27.4	5.03 27.4

TP 2.57 389.69 5.34 387.12

389.69 ✓

386.70	386.19	386.42	386.62	386.57	386.29	387.09
576 28	527 28	604 14	5.81	5.89 14	6.17 27.4	5.03 27.4

0+50

0+0 J
3+257 = H. L. Striff to South

387.34	386.74	386.92	387.06	387.04	386.74	387.29
522 28	572 28	554 14	5.10	5.42 14	5.72 27.4-60	5.17 27.4-66

3+18 = H. C. Striff North

387.41	386.82	386.98	387.10	387.06	386.91	386.78	387.29
505 28-6	554 28-60	578 14	5.56	5.40 14	5.53 27.4	5.68 40-60	5.17 40-66

392.46 ✓

392.46 ✓

2+9565 = 2 34^{1/2} St to South

384.28	384.16	384.16	384.21	384.16	384.01	384.45
5.1/10	5.53/28	5.55/14	5.28 17 South 17.5 N.H.S.	5.53/14	5.68/27.4	5.31/10

2+78 = FC6 34^{1/2} St to South

384.67	384.04	384.22	384.33	384.50	384.60	384.13	384.38
5.03/10	5.65/25.4	5.47/28	5.36/14	5.19	5.29/14	5.56/27.4	5.01/10

2+67 = FC6 34^{1/2} North

384.81	384.25	384.39	384.61	384.42	384.20	384.24	384.96
4.88/28	5.44/28 9.4	5.30/14	5.08	5.27/14	5.49/27.4	5.45/10 9.4	4.98/10 9.4

2+50 = 10^{1/2} North 4 1/2 x 2 S.D. Gas Main Hole 5.17

384.52

TOP M.H.

385.02	384.29	384.59	384.81	384.67	384.32	384.87
4.67/28	5.40/28	5.10/14	4.88	5.08/14	5.37/27.4	4.88/27.4

2+0

385.48	384.69	384.95	385.28	385.24	384.90	385.39
4.21/28	5.00/28 5.01	4.74/14	4.41	4.45/14	4.79/27.4	4.30/27.4

1+135 = 17^{1/2} North South

386.16	385.99	385.86	385.31	385.50	385.70	385.60	385.55	386.12
2.53/10	3.70/10 6.4	3.83/28 10.4	4.38/28 6.4	4.19/14	3.99	4.09/14	4.44/27.4 6.4	3.57/27.4 6.4

38969 ✓

38969 ✓

1+23.5 = E to Hilley South

TP 2.41 386.60 ✓ 6.50 383.19 ✓

1+0

0+50

0+0
3+25.657 = W-L 34'6" to South

BM 5.47 384.22 ✓ NWBP
Wooden 34'
384.12

3+23 WCB 34'6" North

3+13.65 WCB 34'6" S to South

389.69 ✓

Lt. Δ Rt

383.45 383.35 383.08 382.52 382.57 382.86 382.80 382.33 382.73

3.5 3.25 3.52 4.08 4.03 3.74 3.80 4.27 3.87
28-6 10-9 27.7-6 27.7-6 14 14 27.7 27.7
541 541 541

383.04 382.44 382.85 383.11 382.90 382.56 383.15

6.65 7.25 6.84 6.58 6.79 7.12 6.54
27.7 27.7 14 14 14 27.7 27.7

383.66 383.05 383.40 383.51 383.34 383.01 383.68

6.03 6.64 6.59 6.18 6.55 6.68 6.01
27.7 27.7 14 14 14 27.7 27.7

384.17 383.62 383.82 383.94 383.75 383.65 384.10

5.52 6.07 5.87 5.75 5.94 6.04 5.59
27.7 27.7 14 14 14 27.7 27.7-6
541

384.19 383.66 383.88 383.97 383.79 383.67 383.70 384.22

5.50 6.00 5.81 5.72 5.90 6.03 5.90 5.47
28-6 28-6 14 14 14 27.7 27.7-6 10-6

384.12 383.71 383.81 383.94 384.05 383.94 383.93 384.18

5.57 5.28 5.88 5.75 5.74 5.75 5.71 5.51
10-6 10-6 28 14 14 14 27.7 40

389.69 ✓

Meade Ave.

Lt.

L

Rt.

67

2+72 = E.C. Felton North

381.44	381.00	381.11	381.25	381.12	380.85	380.86	381.42
516 277-13	560 277-6ul	549 14	535	548 14	525 277	574 10-5ul	578 10-15

2+64.8 = E.L. Felton to South

381.52	381.00	381.13	381.35	381.20	380.97	381.52
508 277-13	560 277-6ul	547 14	525	540 14	563 277-6ul	508 277-13

2+50

381.68	381.12	381.31	381.52	381.38	381.07	381.61
492 277	548 277	539 14	508	539 14	555 277	499 277

2+0

382.22	381.63	381.83	382.06	381.88	381.54	382.13
438 277-13	477 277-6ul	477 14	454	472 14	506 277	447 277

1+43.5 = H.L. Hill South

382.92	382.83	382.65	382.23	382.40	382.76	382.49	382.05	382.78
468 40-15	377 40	395 277-6ul	407 277-6ul	420 14	384	411 14	455 277	382 277

1+37

S.P. 1/4 - 25x25
50.605 RP

391

382.69

Tap M.H.

383.11	382.28	382.49	382.81	382.69	382.20	382.80
379 40	425 277	44 14	379	391 14	410 277-6ul	380 277-13

1+32.5 = H.L. Hill South

386.80 ✓

386.60 ✓

0714 = N L Falton North

381.06	380.43	380.65	381.07	380.99	380.54	381.15
554 277 17	517 277 64	595 17	553	561 14	606 277 64	545 277 68

0702 = N C6 Falton North

380.98	380.92	380.63	380.64	381.23
562	568 14	599 277	591 40 501	537 40 66

0700 }
372487 = N L Falton South

381.06	380.53	380.76	380.97
554 277 63	607 277 64	584 14	563

3713 = N C6 Falton South

381.18	380.87	380.79	380.93	381.08	380.96	380.64	381.04
592 40 63	571 40 64	581 277	567 14	552	564 14	596 277	556 40

27948 = N Falton South

381.18	381.06	381.06	381.15	381.00	380.70	381.03
547 40	554 277	554 14	515	560 14	590 277	557 40

2777 = N C6 of Falton South

381.41	380.78	380.97	381.07	381.19	381.10	380.80	380.93
519 40 63	582 40 64	563 277	552 14	541	580 14	580 277	567 40

386.60 ✓

386.60 ✓

210

TP 4.13 383.72 701 379.59

1+425 = H.L. Alley South

1+335 = H.L. Alley South

1+235 = F.L. Alley South

1+0

0+50

379.44	378.88	379.16	377.52	379.35	378.99	379.56
4.38 27.7	4.84 27.7	4.58 19	4.20 19	4.37 19	4.73 27.7	4.16 27.7
			580.72			

380.10	380.07	379.94	379.44	379.68	380.00	379.80	379.60	380.19
6.80 40.05	6.53 40.05	6.66 27.7	7.16 27.7	6.92 19	6.60 19	6.80 19	7.00 27.7	6.41 27.7

380.14	379.46	379.67	380.06	379.94	379.64
6.46 40	7.14 27.7	6.23 19	6.51	6.66 19	6.96 27.7

380.30	380.05	380.20	379.65	379.79	380.21	380.01	379.71	380.31
6.30 40.05	6.55 40.05	6.40 27.7	6.95 27.7	6.81 19	6.39 19	6.39 19	6.89 27.7	6.29 27.7

380.30	379.75	380.06	380.38	380.29	379.92	380.46
6.30 27.7	6.85 27.7	6.84 19	6.22	6.27 19	6.68 27.7	6.14 27.7

380.74	380.26	380.39	380.76	380.51	380.25	380.93
5.86 27.7	6.34 27.7	6.21 19	5.84	6.09 19	6.35 27.7	5.67 27.7

586.60

586.60

2+19.15

378.37	378.36	378.29	378.49	378.52	378.58	378.63
$\frac{535}{40}$	$\frac{536}{277}$	$\frac{533}{14}$	$\frac{533}{14}$	$\frac{520}{14}$	$\frac{511}{277}$	$\frac{509}{40}$

2+05.15 = 2nd 33rd St

378.46	378.46	378.46	378.55	378.64	378.72	378.83
$\frac{536}{40}$	$\frac{536}{277}$	$\frac{536}{14}$	$\frac{517}{14}$	$\frac{508}{14}$	$\frac{500}{277}$	$\frac{489}{40}$

2+9.15

378.56	378.33	378.26	378.42	378.41	378.60	378.70
$\frac{516}{40}$	$\frac{539}{277}$	$\frac{521}{14}$	$\frac{520}{14}$	$\frac{521}{14}$	$\frac{513}{277}$	$\frac{503}{40}$

2+77.15 = E.C. 33rd St

378.70	377.99	378.07	378.09	378.12	378.16	378.30	378.35	379.02
$\frac{502}{40-6}$	$\frac{528}{40-54}$	$\frac{535}{277}$	$\frac{565}{14}$	$\frac{560}{14}$	$\frac{556}{14}$	$\frac{543}{277}$	$\frac{537}{40-54}$	$\frac{470}{40-6}$

2+65.15 = E.L. 33rd St

378.70	378.29	378.14	378.41	378.43	378.46	379.02
$\frac{503}{277}$	$\frac{543}{277}$	$\frac{538}{14}$	$\frac{531}{14}$	$\frac{539}{14}$	$\frac{526}{277}$	$\frac{470}{277-6}$

2+50

378.85	378.40	378.57	378.96	378.64	378.91	379.07
$\frac{487}{277-6}$	$\frac{522}{277-54}$	$\frac{515}{14}$	$\frac{486}{14}$	$\frac{508}{14}$	$\frac{531}{277-54}$	$\frac{465}{277-6}$

38872 ✓

38872 ✓

2+24 16' top of 22nd 586
509a.M.R.

2+0

1+50

1+0

0+50

0+0
3+15.15 = N.L. 33rd St

B.M.

3+33.15 = N.C. 6 of 33rd St

383.72 ✓

LT	2	PA
378.05	377.60	377.95
567 276-cl	519 276-5ul	577 14
378.20	378.26	378.06
552 14	546 14	568 277
378.12	377.72	378.07
560 276	500 276	565 14
378.37	378.37	378.39
535 276	535 14	538 14
378.37	377.92	378.25
535 276	580 276	547 14
378.45	378.44	378.17
537 14	538 14	555 277
378.61	378.56	378.17
505 14	516 14	515 277
378.04	378.00	378.97
568 14	572 276-5ul	525 277-cl
378.13	377.96	377.91
589 14	576 277	581 14
378.17	378.22	378.34
565 14	550 277	538 40-5ul
378.13	377.91	378.99
589 14	576 277	581 14

383.72 ✓

N.M. 80
Meade + 33rd
378.96

Sub-
Driv

TP 3.83 381.98 557 378.15

2+13 = WCB 33rd Place North

2+899 = 33rd Place North

2+844 = 34th Place North 592 377.80

2+66 = E.C. 33rd Place North

2+549 = E.L. 33rd Place North

2+41 = E.C. 33rd Place South

2+28 = C.B. BC Lt

383.72 ✓

Lt S Pt

377.55 377.25 377.50 377.73 377.79 377.64 377.69 378.10
617 647 622 599 593 608 603 562
276-26 276-90 14 14 277 40-90 40-26

377.72 377.32 377.66 377.87 377.83 377.64 378.13
600 646 606 585 589 608 559
276-26 276-90 14 14 277 10

377.91 377.47 377.25 377.72 377.96 378.18 378.16 377.89 377.89 378.47
581 625 647 600 576 554 556 583 582 575
40-26 40-90 276 14 14 9.5-90 14 277 40-90 40-26

377.78 377.31 377.69 378.07 378.23 378.01 378.50
599 641 603 565 549 571 522
48 276 14 14 277 277-26

378.12 377.75 377.58 377.32 378.02 378.14 377.94 378.50
560 597 614 570 570 558 578 532
40-26 40-90 276 14 14 277 277

378.03 377.53 377.90 378.12 378.22 377.96 378.54
569 619 582 560 553 576 518
276-26 276-90 14 14 277 277-26

383.72 ✓

17712 = F.L. Bancroft South

376.94	376.45	376.54	376.55	376.68	376.75	376.88
5.04 27.8	5.53 27.6	5.11 14	5.43	5.30 14	5.29 27.7	5.10 40

1765 = E.C. Bancroft North

376.91	376.46	376.58	376.64	376.68	376.76	376.80	377.31
5.07 27.8	5.52 27.8	5.10 14	5.54	5.30 14	5.29 27.7	5.18 40-50	4.67 40-50

17532 = F.L. Bancroft North

376.89	376.53	376.79	376.95	376.97	376.92	377.30
5.09 27.8	5.45 27.8	5.19 14	5.03	5.01 14	5.06 27.7	4.68 27.7

170

377.23	376.79	377.14	377.36	377.33	377.11	377.47
4.25 27.6	5.19 27.8	4.81 14	4.62	4.65 14	4.87 27.7	4.51 27.7

0450

376.91	377.22	377.48	377.47	377.28	377.79
5.07 27.6	4.36 14	4.50	4.51 14	4.20 27.7	4.19 27.7

040 J
272197 = W.L. 3rd Place North

377.14	377.45	377.72	377.80	377.59	378.06
4.81 27.6	4.53 14	4.26	4.18 14	4.39 27.7	3.97 27.7

38198 ✓

38198 ✓

0750

410	474	437	408	404	430
276	276	14	14	14	277
CB	Gul				Gul

0714 1766 of 2-25-2 490 377.08

0753 2-7312) = W.L. Bancroft Souths

377.09	376.65	377.04	377.18	377.28	377.13	377.65
489	523	494	480	470	485	433
276	276	14	14	14	277	277
CB	Gul					

21175 = W.C.B. Bancroft Souths

377.07	376.42	376.56	376.68	376.84	376.98	376.86	377.77
491	556	542	536	514	500	511	461
276	276	14	14	14	14	277	277
CB	Gul						

2+13 = W.L. Bancroft Norths

376.56	376.58	376.61	376.71	376.65	376.88	376.80	377.39
542	540	533	527	523	519	518	459
276	276	14	14	115	119	277	277
				50	50	50	277
				CB	CB	CB	CB

BM 436 377.42 ✓ H.W.B. Bancroft 37736

2+012 = 1/2 Bancroft Souths 1/2 W.C.B. Norths

376.63	376.71	376.66	376.87	376.79	376.80	376.77	377.40
533	527	532	511	519	510	525	458
276	276	14	14	14	277	276	276
						14	14
						CB	CB

1+94 6 1/2 of 1 = Server 522 376.76 Mah. Hole

376.84	376.36	376.39	376.55	376.66	376.87	376.96	377.00
510	567	547	543	532	511	503	498
40	276	276	14	14	14	277	276
CB	Gul						

1+83 = F.C.B. Bancroft Souths

38198 ✓

38198 ✓

210

379.47 379.10 379.40 379.58 379.55 379.27

5.48 5.85 5.55 5.37 5.40 5.68
276.43 276.56 14 14 277.56

TP

5.39 384.95 242 379.56

384.95 ✓ 379.56 ✓

1+56

378.79 378.50 378.80 379.08 379.00 378.64 379.16

3.19 3.18 3.19 2.90 3.28 3.34 3.82
278 278 14 14 277.94 277.56

1+22 = W.L. Hill North

378.14 378.48 378.73 378.66 378.50 378.92 378.97 379.16

3.84 3.50 3.25 3.32 3.48 3.26 3.05 2.82
276.56 14 14 277.56 277.56 277.56 277.56

1+145 = E. Hill North

378.37 377.99 378.40 378.65 378.60 378.39 378.77

3.65 3.99 3.68 3.33 3.38 3.39 3.21
276 276 14 277.56 277 277 40

1+07 = E.L. Hill North

378.25 377.95 378.36 378.61 378.50 378.38 378.87 378.80 378.95

3.73 4.02 3.62 3.37 3.48 3.60 3.11 3.18 3.03
276 276 14 14 277.56 277.56 277.56 277.56

1+0

378.17 377.89 378.25 378.47 378.40 378.24

3.81 4.09 3.73 3.51 3.58 3.24
276 276 14 14 277.56 277.56

381.98 ✓

381.98 ✓

3+069 - H.L. 32nd St.

B.M.

4.54 380.41

H.W.B.P.
Meady
380.41
41296

2+194.9 - H.C. 32nd St.

2+76.9 - L. 32nd St.

2+58.9 = F.C. 32nd St.

2+46.9 = F.C. 32nd St.

38495 ✓

380.25	379.81	379.82	380.01	380.13	380.05	380.46	
470 27.6-cb	5/4 27.6-54	5/3 14	494	488	490 27.7-54	499 27.7-cb	
380.20	379.70	379.79	379.81	379.80	379.84	379.97	
425 40-cb	5/5 40-54	5/6 27.6	5/4 14	5/5	5/1 14	498 27.7	501 40-54
380.11	380.14	380.15	380.19	380.30	380.30	380.37	
484 40	481 27.6	480 14	476	465 14	465 27.7	458 40	
380.18	379.75	379.85	379.91	379.87	379.88	379.78	
477 40-cb	5/20 40-54	5/10 27.6	5/9 14	5/8	5/7 14	5/7 40-54	475 40-cb
380.08	379.73	379.84	380.01	379.93	379.71	380.25	
487 27.6-cb	5/22 27.6-54	5/11 14	491	502 14	5/24 27.7	470 27.7-cb	

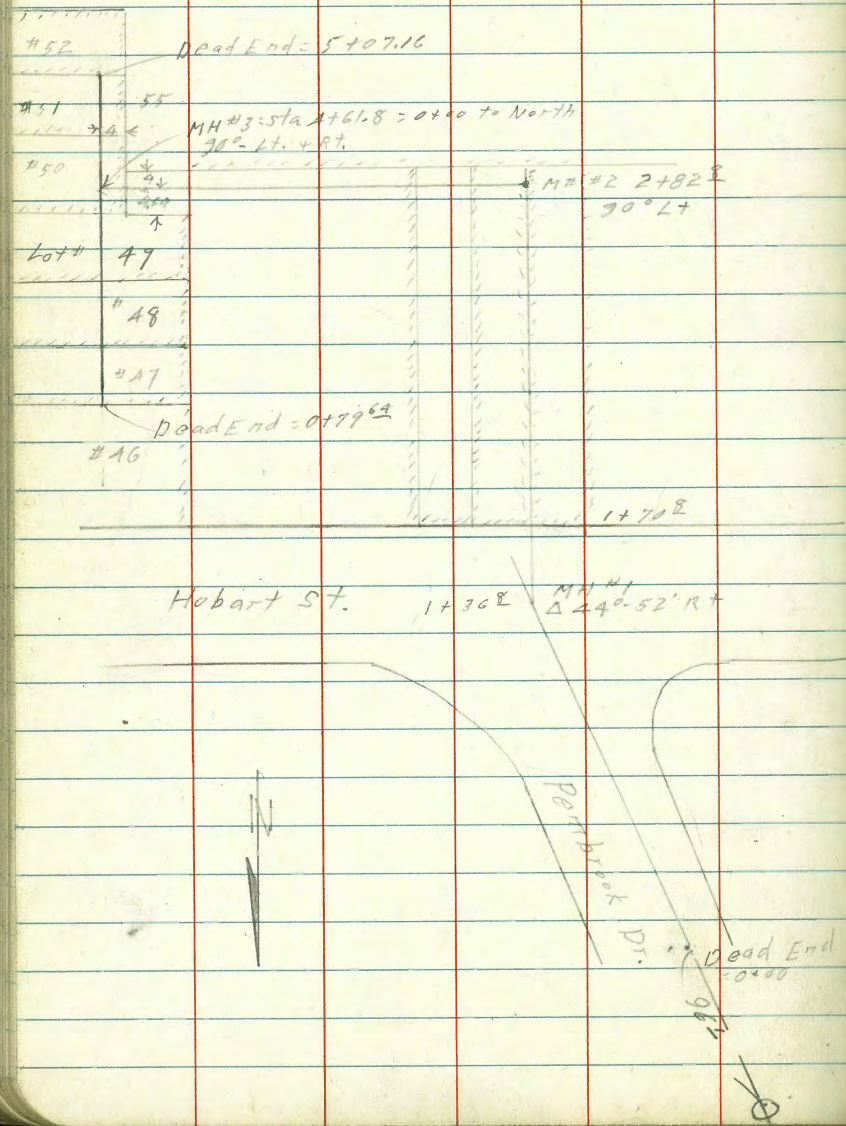
38495 ✓

Oakmere (Lots 39 to 52 + 55 to 62)
Sewer.

Profile

Indexed
C.S.R.

77



Station	Profile	Index	C.S.R.	Notes
1.16	469.82	—	465.66	N.M. B.P. 63 rd + E.1 Cajon
T.P.	3.67	467.37	6.12	463.70
T.P.	5.45	466.97	5.85	461.52
0-96'	Existing M.H.	13.74	453.23	INVERT
0+00:	Existing D. End	Ord.	8.2	458.8
+45		8.1	458.9	
+90		8.1	458.9	
1+36 ⁸	M.H. #1	7.9	459.1	
T.P.	3.67	466.52	4.12	462.85
1+50		6.6	459.9	
+60		4.4	462.1	
+80		4.3	462.2	
2+00		6.7	459.8	
+50		5.3	461.2	
+82 ⁸	M.H. #2	5.0	461.52	
3+00		4.9	461.6	
+50		5.2	461.3	
4+00		4.5	462.0	
+45		4.4	462.1	
4+61.8	M.H. #3	4.2	462.32	

466.52

5+07¹⁵ = D.E. 4.3 462.22v 80° Lt = ^{Ord} Cor. House 3.8 462.72

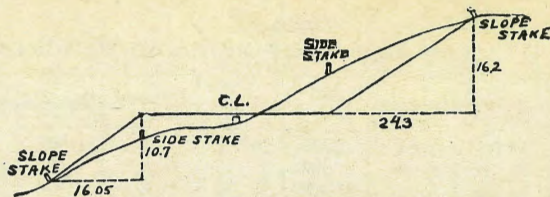
" " " Floor. 2.40 464.12

4+61² = From MH 23
0+00 = Going North 4.2 462.3

+A0 3.6 462.9

+79⁶⁹ = D.E. 3.8 462.72" 30° RT = ^{Ground at} Cor. H-430 3.7 462.8

" 30° " = Floor House 3.0 463.5



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
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42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
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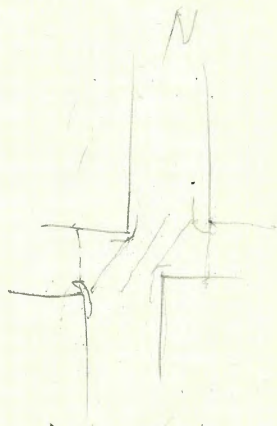
Computed by L. Leland Locke.

106.48
 9.66
 97.82
 4.41
 102.23

106.48
 9.66
 97.82

117.72
120.41
8.34
112.07
5165

6.41
626
1267



Δ 7° 41' RT.

