

1743



1743

CITY ENGINEER'S OFFICE

MICROFILMED
DEC 29 1964

MADE IN U. S. A.

76 of 25

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- No. 380 LEVEL BOOK. Left and Right Hand Page
the same as Left Hand Page
of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this
Book, Right Hand Page 4x4
to the inch, Center Line Red.
- No. 384 MINING TRANSIT
BOOK. Left Hand Page as in this
Book, Right Hand Page 8x8
to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this
Book, Right Hand Page 8 ver-
tical and 4 horizontal lines to
the inch, Center Line Red.

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ENGINEERING and DRAFTING SUPPLIES

P. O. Box 803

CHICAGO

INDEX

Page

X-Alley Blk 4-Ocean Villa Trust — 67
Alicia Drive 6

Sewer Levels on
Perry St.
Betw. San Antonio
and Roscorans St

C. Moore
San Antonio Mex
W. Moore
B999
10-28-46

| | | | | |
|------|------|--------------|------|-----------------------|
| SWBP | 119 | 579 | 460 | McCull San Antonio |
| T.P. | 1174 | 1209 | 5.00 | 0.35 |
| T.P. | 1.26 | <u>11.60</u> | 175 | 10.34 |

set B.M. Perry and
S.W. 7' C.T. San Antonio 7.98 3.62

| | | | |
|------|------------------|-------|-------|
| 0+00 | M.H. RIM | 9.00 | 2.60 |
| " | " Invert | 15.83 | -4.23 |
| " | " Comp. Step | 14.65 | -3.05 |
| 0+15 | edge Pav. | 9.05 | 2.55 |
| 0+25 | w/ly San Antonio | 7.6 | 4.0 |
| 0+45 | | 2.4 | 9.2 |

T.P. 1306 24.36 0.30 11.30

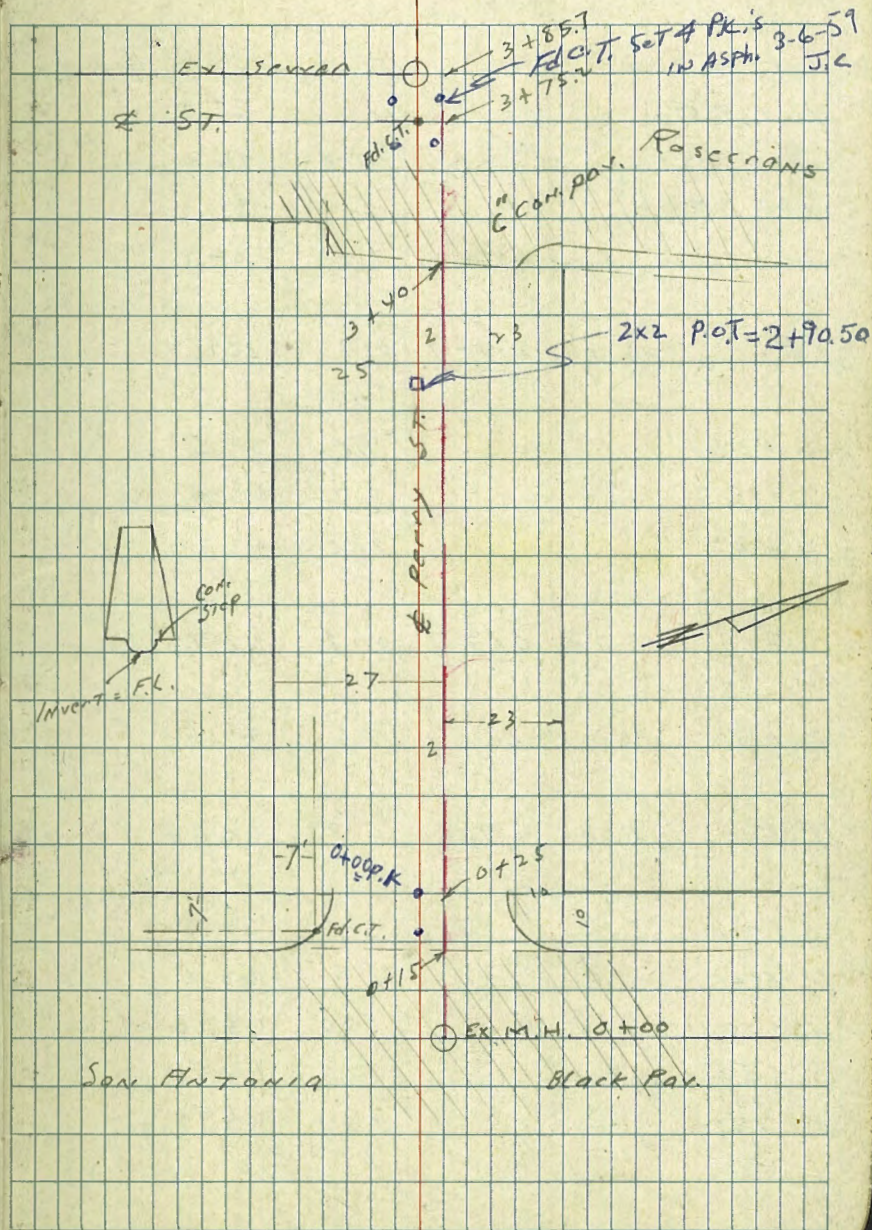
| | | | |
|------|--|------|------|
| 0+60 | | 12.9 | 11.5 |
| 0+80 | | 8.8 | 15.6 |
| 1+00 | | 5.6 | 18.8 |
| 1+25 | | 1.0 | 23.4 |

T.P. 1247 36.34 0.44 23.92

W.O. 199

indexed
C.S.K.

1



30.34

| | | | |
|--------|--|------|------|
| 1 + 40 | | 10.3 | 26.0 |
| 1 + 55 | | 11.1 | 25.2 |
| 1 + 60 | | 10.3 | 26.0 |
| 1 + 85 | | 5.2 | 31.1 |
| 2 + 10 | | 1.4 | 34.9 |

| | | | | |
|------|-------|-------------|-----|------|
| T.P. | 12.91 | <u>4907</u> | 018 | 3016 |
|------|-------|-------------|-----|------|

| | | | |
|--------|--|-----|------|
| 2 + 35 | | 9.6 | 39.5 |
| 2 + 55 | | 5.7 | 43.4 |
| 2 + 80 | | 1.4 | 47.7 |

| | | | | |
|------|-------|-------------|-----|-------|
| T.P. | 12.28 | <u>6127</u> | 008 | 48.99 |
|------|-------|-------------|-----|-------|

| | | | |
|--------|----------|------|------|
| 2 + 90 | Toe FILL | 11.5 | 49.8 |
|--------|----------|------|------|

| | | | | |
|------|-----|-------------|------|-------|
| T.P. | 908 | <u>6946</u> | 0.89 | 60.38 |
|------|-----|-------------|------|-------|

| | | | |
|----------|-----------|------|-------|
| 3 + 08 | | 5.9 | 63.6 |
| 3 + 20 | | 6.3 | 63.2 |
| 3 + 40 | edge Pav. | 5.26 | 64.20 |
| 3 + 50 | Pav | 5.16 | 64.30 |
| 3 + 75.7 | " | 4.53 | 64.93 |

6946

2

| | | | | |
|----------|-------------|-------|-------|------|
| 3 + 85.7 | Pav. | 4.49 | 64.97 | |
| " | 2' S E M.H. | 4.47 | 64.99 | P.M. |
| " | " " " " | 14.50 | 54.96 | F.L. |

check to NEBP

| | | | |
|--------------------|------|-------|-------|
| Perry + Passerelli | 5.30 | 64.16 | 64.15 |
|--------------------|------|-------|-------|

Curb elevations + location of
 Driveways - on Altadena - El Cajon
 to Trojan - for sketch and previous
 X-sect. See Book 1672 - P. 5

611 11-6-46

W.O. 1086 Osborne
 Hardin
 Worrell
 Smith

1+50

1+25

1+10 = end dr. on Rt.

1+00

0+84 = Beg. Conc. dr. on Rt.

0+75

0+50

0+35 = end Dr. on Lt.

0+20

0+00 = opp. prop. Cor. on Rt. - See sketch

0-11 = Beg. Dr. to Ser. Sta on Lt. - also new walk

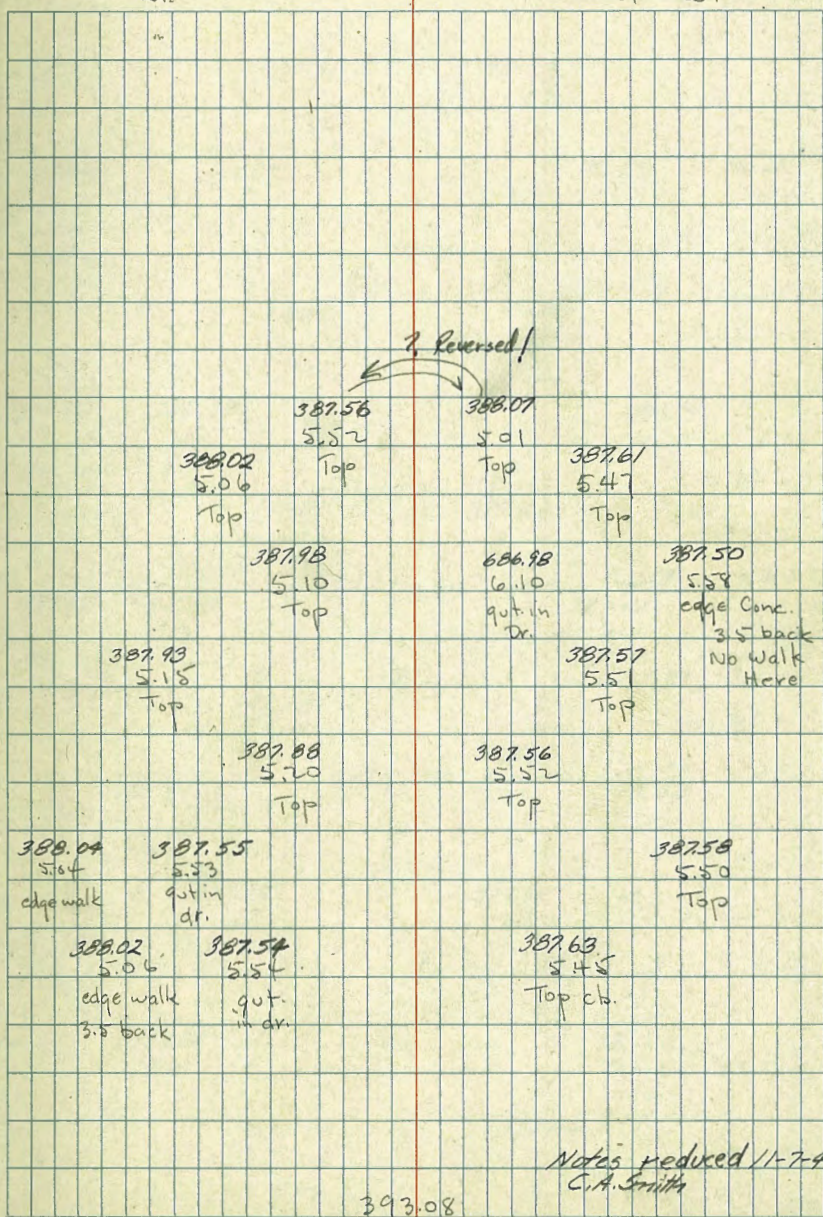
| | | | | | |
|------|------|--------|------|--------|---------------------------------|
| J.P. | 5.54 | 393.08 | 2.19 | 387.54 | S.E. Hyd. |
| B.M. | 3.63 | 389.73 | | 386.10 | 50 th + EL Cajon. |

Indexed
 C.S.K.

3

Lt = E.

Rt = W.



4+25

4+00

3+98.5 = ± 9' Conc. Dr. on Lt.

3+96.5 = ± 10' Conc. Dr. on Rt.

3+75

3+50

3+48 = ± 10' Conc. Dr. on Lt.

3+25

3+03 = ± 10' Conc. Dr. on Lt.

3+00

2+98 = ± 10' Conc. Dr. on Rt.

2+75

2+62 = ± 10' Conc. Dr. on Lt.

2+50

2+25

2+19 = ± 9' Dr. on Lt.

2+14 = ± 10' Dr. on Rt.

2+00

1+75

Lt.

Rt.

4

385.58

7.50

Top

385.50

7.58

Top

386.10

6.98

edge Dr.
3.5' back

385.45

7.63

cut in
Dr.

385.52

7.56

cut in
Dr.

386.02

7.06

edge Dr.
3.5' back

386.43

6.65

Top

386.38

6.70

Top

386.90

6.18

edge walk

386.28

6.80

cut in
dr.

386.72

6.34

Top

387.21

5.87

Top

387.22

5.86

Top

387.65

5.43

edge walk
3.5' back

387.09

5.99

cut in
Dr.

387.02

6.06

cut in
dr.

387.56

5.52

edge Dr.
3.5' back

387.72

5.36

Top

387.57

5.51

Top

387.71

5.37

Top

387.48

5.60

Top

387.85

5.23

Top

387.58

5.50

Top

388.05

5.03

Top

387.57

5.51

Top

388.03

5.05

Top

387.64

5.44

Top

388.08

5+87.5 = Brk. on Lt.

5+90 = Brk. on Rt.

5+80 = Brk. on Rt.

5+75

5+74 = Brk. on Rt.

5+62 = Brk. on Lt.

5+59 = Brk. on Rt.

5+54 = Brk. on Lt.

5+53.5 = ± 12' Conc. Dr. on Rt.

5+50

5+48.7 = ± 10' Conc. Dr. on Lt.

5+35 = Brk. in cb. on Rt.

5+25

T.P. 6.94 383.13 10.89 382.19

5+00

4+98.5 = ± 10' Conc. Dr. on Rt.

4+75

4+53.2 = Beg. cb. on Lt.

4+50

4+49 = ± 11' Conc. Dr. on Rt.

4+43.3 = end cb. on Lt. broken out for Dirt Dr.

385 50%

Lt.

±

Rt.

375.42

7.71
Top

376.16
6.97
Top

379.04
6.09
Top

378.30
4.83
Top

378.95 378.08
4.18 5.25
Dr. 3.5' back gut in Dr.

380.93
2.20
Top

382.67
10.41
Top

384.08
9.00
Top

384.96
8.17
Top-end

385.21
7.87
Top-end

375.65
7.48
Top

378.04
5.09
Top

379.39
3.74
Top

383.13

384.85
11.23
gut in Dr.

384.23
8.85
gut in Dr.

393.08

374.76
8.37
Top

376.78
6.35
Top

378.21
4.92
gut in Dr.

380.48
2.65
Top

378.85
4.28
Dr. 3.5' back

382.71
10.37
edge Dr. 3.5' back

384.02
9.06
Top

384.99
8.09
edge Dr. 3.5' back

check BM. on Disk N.W. end cb. 12.57 70.56 70.54

6+57.96 = N.L. Trojan

6+50

6+29 = Brk. on Rt. = S. edge Dr.

6+25

6+11 = Brk. on Rt. = N. edge Dr.

6+09 = Brk. on Lt. on S. side Dr.

6+04 = ± 10' Conc. Dr. on Lt.

6+00

369.33
13.80
Top end cb

370.11
13.02

372.14
10.99
Top.

373.49
9.64
Top

374.31
8.82
Dr. 35' back

373.82
9.31
cut in
Dr.

383.13

370.55
12.58
Top end cb

371.19
11.94
Top

372.53
10.58
Top

373.96
9.17
Top

372.36
10.77
cut in
Dr.

374.52
8.61
Top

372.76
10.17
edge Dr.
35' back

Alicia Dr. Alignment
Tennyson St. to Catalina Blvd.

~~Indexed~~
B

Added Notes, FB # 7835-36

Nov. 20-46

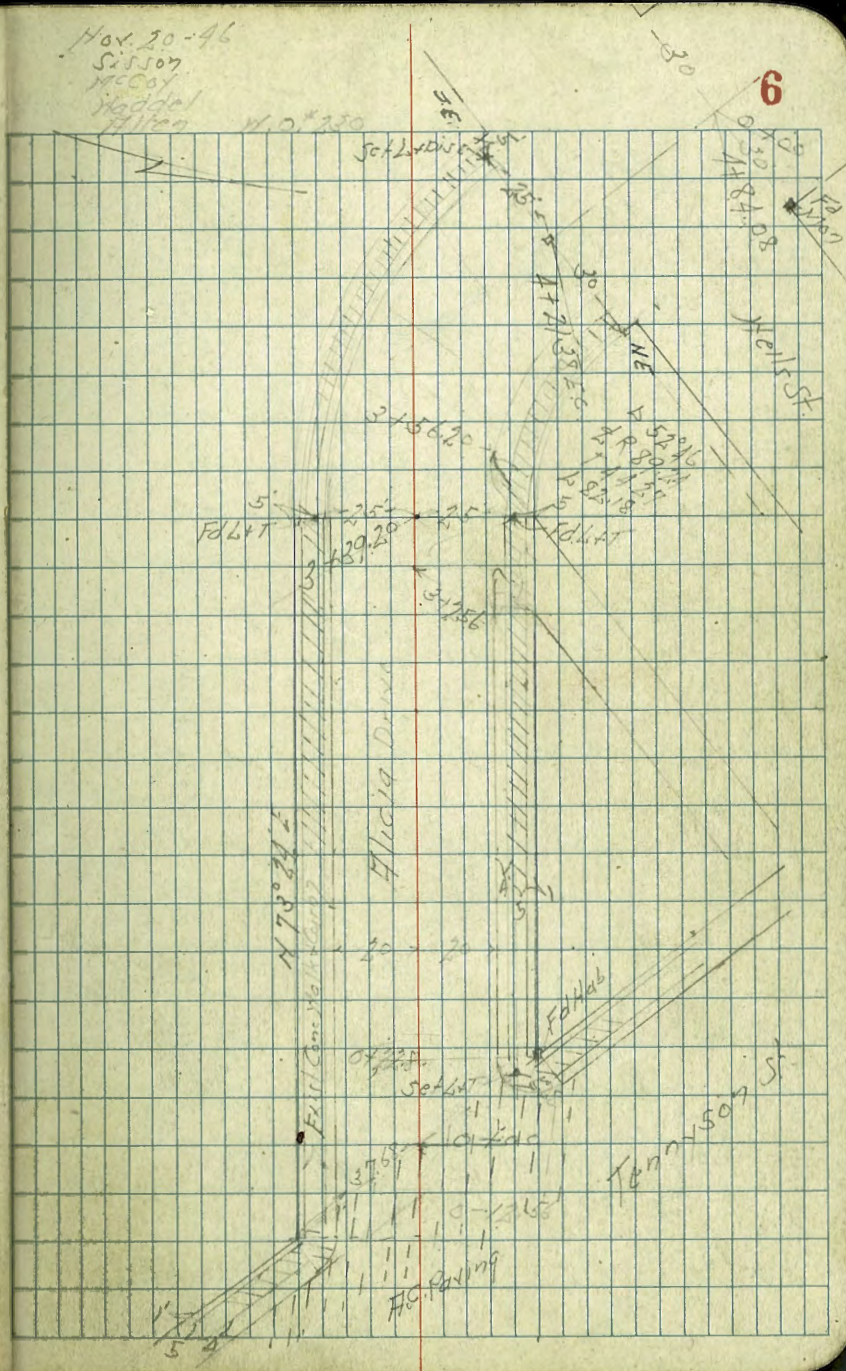
Sisson

McCoy

Waddell

Allen

4107330



Cross Section Alicia Drive
Tennyson to Catalina Blvd

Sketch page 6

Lt. 5

Dg

Rt. 11.

8

| | | | | | | | | | | | |
|------------------------------------------------|-------|--------|-------|-------|------------------------|------------------------|-------------------------|-------------------------|----------------|-------------------------|------------------------|
| | | | | | 6.21 20.1-d | 6.7 20.1 | 6.8 10 | 6.6 | 6.6 10 | 6.8 20 | 6.5 20.1-cb |
| +1.50 | | | | | | | | | | | |
| +22.8 | | | | | 8.68 19.9 | 9.44 19.9 | 8.6 10 | 8.4 | 8.5 10 | 8.4 19.9 | 7.92 19.9-cb |
| | | | | | 93.69 | 93.16 | 93.71 | 94.30 | 94.87 | 95.91 | 96.03 |
| 0+0 = N.L. Tennyson Taken on Dip | | | | | 6.55 13.2 | 11.07 25.2 | 10.53 12.54 | 9.93 | 9.36 12.58 | 8.74 27 | 8.26 27.7-cb |
| | | | | | | | | | | | |
| 0-12.56 = N. Ch. Line of Tennyson Taken on Dip | | | | | 92.86 11.37 33.8 | 92.23 12.09 33.8 | 92.57 11.66 35.12 | 93.05 11.88 37.58 | 93.46 10.77 | 93.93 10.39 12.88 | 94.39 9.84 25.18 |
| | | | | | | | | | | | |
| BM set | | 8.48 | 95.75 | | | | | | | | |
| TP | 12.27 | 104.22 | 0.96 | 91.96 | | | | 104.23 | | | |
| TP | 5.53 | 92.92 | 9.99 | 87.29 | | | | | | | |
| BM | 0.73 | 97.38 | | 96.65 | | | | | | | |

SW 81
Tennyson
El. 100

SW 81
Tennyson
El. 100

95.67
8.56
L.S. 10

+25.6

TP 12.71 128.03 0.76 115.32

3+0

+50

2+0

+50

TP 12.63 116.08 0.18 104.05

1+0

104.23

| | | | | | | | | |
|----------------|-------------|-------------|-------------|-------------|-------------|----------------|-------------|-------------|
| 16.39 | 15.7 | 15.7 | 15.8 | 15.8 | 15.8 | 16.0 | 16.61 | 16.81 |
| 1164 203-03 | 1237 203 | 1237 203 | 1237 203 | 1237 203 | 1237 203 | 1237 203 | 1112 203 | 1122 203 |
| 14.41 | 13.8 | 13.8 | 13.9 | 14.0 | 14.0 | 14.72 | | |
| 167 203 | 225 203 | 225 203 | 225 203 | 225 203 | 225 203 | 225 203 | 225 203 | 225 203 |
| 10.97 | 10.4 | 10.6 | 10.5 | 10.6 | 10.7 | 11.29 | | |
| 511 201-06 | 57 201 | 55 201 | 56 201 | 55 201 | 54 199 | 479 199-06 | | |
| 07.68 | 06.9 | 07.4 | 07.4 | 07.1 | 07.4 | 07.97 | | |
| 840 201-03 | 92 201 | 87 201 | 87 201 | 90 201 | 87 201 | 811 201-06 | | |
| 04.51 | 03.7 | 04.1 | 04.0 | 03.9 | 03.8 | 04.69 | | |
| 1157 201-03 | 124 201 | 120 201 | 121 201 | 124 201 | 123 199 | 1139 199-06 | | |
| 01.32 | 00.5 | 00.8 | 01.1 | 00.8 | 00.5 | 01.45 | | |
| 291 201-06 | 37 201 | 34 201 | 31 201 | 34 201 | 37 201 | 378 201-03 | | |

104.23

1+3408 - cb Linn Wallr

1+2138 - EC

+9398

Taken Radial

+6659

Taken Radial

+562

Taken Radial

3+3920 - BC RT

128.03

| | | | | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 126.4 | 126.9 | 126.6 | 125.7 | 125.3 | 124.8 | 124.4 | 124.2 | 123.5 | 123.5 | 123.6 |
| 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 |
| 122.92 | 121.7 | 121.8 | 121.4 | 121.2 | 121.3 | 121.99 | 121.99 | 121.99 | 121.99 | 121.99 |
| 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 |
| 120.06 | 119.3 | 119.1 | 118.9 | 119.1 | 119.2 | 119.2 | 119.2 | 119.2 | 119.2 | 119.2 |
| 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 |
| 19.21 | 18.5 | 18.2 | 18.2 | 18.4 | 18.4 | 18.4 | 18.4 | 18.4 | 18.4 | 18.4 |
| 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 |
| 17.31 | 16.5 | 16.5 | 16.75 | 17.0 | 17.2 | 17.2 | 17.2 | 17.2 | 17.2 | 17.2 |
| 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 | 50 |
| 128.03 | 128.03 | 128.03 | 128.03 | 128.03 | 128.03 | 128.03 | 128.03 | 128.03 | 128.03 | 128.03 |

128.03

140

TP

+72

+750

0400
+724.08 = W.L. Wells

+74.08 = Ch Line Wells

TP

+754.08 = W. Wells

128.05

4

6

pt.

| | | | | | | | | | |
|--------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 6.00 100 | 136.1 | 134.0 | 134.3 | 135.3 | 134.5 | 134.0 | 133.4 | 132.4 | 132.7 |
| 11.00 100 | 132.7 | 132.2 | 131.3 | 131.3 | 131.0 | 131.0 | 131.1 | 131.2 | 131.2 |
| 12.00 100 | 130.6 | 130.2 | 129.6 | 129.6 | 128.8 | 128.8 | 128.6 | 127.1 | 127.1 |
| 13.00 100 | 127.8 | 127.1 | 126.3 | 126.3 | 125.5 | 125.5 | 125.0 | 125.0 | 125.0 |
| 14.00 100 | 127.7 | 127.1 | 126.0 | 126.0 | 125.2 | 125.2 | 124.3 | 123.4 | 123.4 |
| 15.00 100 | 127.2 | 126.5 | 125.8 | 125.8 | 125.1 | 125.1 | 124.5 | 123.9 | 123.9 |

1109 H.W.
Proo. Cor.
Wells 510

125.84
125.59

125.84
125.59

128.05

+50

+25

370

+50

270

+50

145.00

| | | | | | | | | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 138.2 | 139.6 | 141.4 | 140.1 | 139.0 | 137.4 | 137.0 | 137.1 | 137.6 | 137.9 | 140.0 | 139.7 | 139.9 | 139.9 | 138.0 | 135.7 |
| 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 |
| 136.5 | 138.5 | 139.9 | 139.8 | 139.5 | 137.4 | 137.2 | 137.1 | 137.4 | 137.9 | 140.0 | 139.7 | 139.9 | 139.9 | 138.0 | 135.7 |
| 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 |
| 135.6 | 137.9 | 139.5 | 139.4 | 139.5 | 137.9 | 137.2 | 137.1 | 137.4 | 137.9 | 140.0 | 139.7 | 139.9 | 139.9 | 138.0 | 135.7 |
| 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 |
| 134.9 | 137.2 | 139.2 | 139.0 | 139.2 | 137.9 | 137.2 | 137.1 | 137.4 | 137.9 | 140.0 | 139.7 | 139.9 | 139.9 | 138.0 | 135.7 |
| 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 |
| 135.7 | 138.2 | 139.5 | 139.7 | 139.5 | 137.9 | 137.2 | 137.1 | 137.4 | 137.9 | 140.0 | 139.7 | 139.9 | 139.9 | 138.0 | 135.7 |
| 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 |

145.00

TP 1.72 111.72 11.41 110.01

+50

6+0

TP 0.48 121.42 12.09 120.94

+50

5+0

+50

TP 0.12 133.02 12.10 132.90

4+0

145.00

Lt

Lt

Rt

13

| | | | | | | | | | | | |
|------|-------|------|-------|------|-------|------|-------|------|-------|------|-------|
| 6.00 | 135.1 | 6.00 | 130.0 | 6.00 | 124.7 | 6.00 | 121.2 | 6.00 | 117.8 | 6.00 | 113.0 |
| 1.00 | 134.4 | 1.00 | 130.2 | 1.00 | 124.6 | 1.00 | 120.6 | 1.00 | 116.2 | 1.00 | 112.0 |
| 1.00 | 133.6 | 1.00 | 129.0 | 1.00 | 123.9 | 1.00 | 119.7 | 1.00 | 115.2 | 1.00 | 111.9 |
| 1.00 | 133.7 | 1.00 | 129.2 | 1.00 | 124.0 | 1.00 | 119.7 | 1.00 | 115.6 | 1.00 | 111.9 |
| 1.00 | 134.0 | 1.00 | 129.4 | 1.00 | 124.6 | 1.00 | 120.4 | 1.00 | 116.2 | 1.00 | 111.9 |
| 1.00 | 133.7 | 1.00 | 128.9 | 1.00 | 124.5 | 1.00 | 120.4 | 1.00 | 115.9 | 1.00 | 111.7 |
| 1.00 | 133.5 | 1.00 | 128.3 | 1.00 | 123.9 | 1.00 | 119.7 | 1.00 | 115.4 | 1.00 | 111.2 |
| 1.00 | 134.5 | 1.00 | 129.9 | 1.00 | 125.5 | 1.00 | 121.3 | 1.00 | 117.0 | 1.00 | 113.1 |
| 1.00 | 136.3 | 1.00 | 130.1 | 1.00 | 125.3 | 1.00 | 121.2 | 1.00 | 118.8 | 1.00 | 114.5 |

145.00

TP 6.05 70.59 996 64.54 ^{SF Top of Blv} Catalina _{Voltaire}

TP 1.35 74.50 1144 73.15

TP 0.26 84.59 1274 84.33

B.M. 9.83 87.24 ^{90 N E C 6} _{Voltaire}

TP 0.35 97.07 1270 96.72

TP 0.43 109.42 274 108.99 ^{SF Top of Blv} Catalina _{Voltaire}

+3515 = Cb Line of Catalina Blvd Taken on Diag.

+3593 = E.L. Catalina Blvd Taken on Diag.

+25 = End Return on Lot

7+0

111.73

B.M. 4.58 86.59 ^{H. H. B.P.} _{Voltaire} _{Baltasar} _{86.50}

TP 9.25 91.11 0.16 81.88

TP 11.53 82.04 0.08 70.51

70.595 B-Food

| | | | | | | | | |
|-------|--------|--------|--------|--------|--------|--------|--------|--------|
| 109.4 | 106.98 | 106.63 | 104.75 | 104.33 | 103.88 | 103.38 | 102.66 | 103.14 |
| 2.4 | 2.75 | 5.10 | 6.98 | 7.40 | 7.85 | 8.35 | 9.07 | 8.59 |
| 30 | 20 | 15.4 | 11 | 11 | 11 | 22 | 595 | 575 |
| | | | | | | | | |
| 108.6 | 106.98 | 106.06 | 104.75 | 104.33 | 103.88 | 103.38 | 102.66 | 103.14 |
| 3.0 | 4.75 | 5.67 | 6.98 | 7.40 | 7.85 | 8.35 | 9.07 | 8.59 |
| 20 | 15.5 | 15.4 | 11 | 11 | 11 | 22 | 595 | 575 |
| | | | | | | | | |
| 107.4 | 106.34 | 106.06 | 104.75 | 104.33 | 103.88 | 103.38 | 102.66 | 103.14 |
| 6.3 | 5.39 | 5.67 | 6.98 | 7.40 | 7.85 | 8.35 | 9.07 | 8.59 |
| 15 | 21.5 | 15.4 | 11 | 11 | 11 | 22 | 595 | 575 |
| | | | | | | | | |
| 107.2 | 106.34 | 106.06 | 104.75 | 104.33 | 103.88 | 103.38 | 102.66 | 103.14 |
| 4.5 | 5.39 | 5.67 | 6.98 | 7.40 | 7.85 | 8.35 | 9.07 | 8.59 |
| 10 | 21.5 | 15.4 | 11 | 11 | 11 | 22 | 595 | 575 |
| | | | | | | | | |
| 107.3 | 105.9 | 105.55 | 104.75 | 104.33 | 103.88 | 103.38 | 102.66 | 103.14 |
| 4.4 | 5.8 | 6.18 | 6.98 | 7.40 | 7.85 | 8.35 | 9.07 | 8.59 |
| 10 | 10 | 11 | 11 | 11 | 11 | 22 | 595 | 575 |
| | | | | | | | | |
| 107.1 | 105.6 | 105.55 | 104.75 | 104.33 | 103.88 | 103.38 | 102.66 | 103.14 |
| 4.6 | 6.1 | 6.18 | 6.98 | 7.40 | 7.85 | 8.35 | 9.07 | 8.59 |
| 10 | 10 | 11 | 11 | 11 | 11 | 22 | 595 | 575 |
| | | | | | | | | |
| 107.3 | 106.0 | 105.55 | 104.75 | 104.33 | 103.88 | 103.38 | 102.66 | 103.14 |
| 4.4 | 5.7 | 6.18 | 6.98 | 7.40 | 7.85 | 8.35 | 9.07 | 8.59 |
| 20 | 20 | 22 | 22 | 22 | 22 | 22 | 595 | 575 |
| | | | | | | | | |
| 109.3 | 106.6 | 105.55 | 104.75 | 104.33 | 103.88 | 103.38 | 102.66 | 103.14 |
| 3.4 | 5.1 | 6.18 | 6.98 | 7.40 | 7.85 | 8.35 | 9.07 | 8.59 |
| 30 | 30 | 22 | 22 | 22 | 22 | 22 | 595 | 575 |

111.73

Tie out of Mon. in Block 42
Point Loma Hts

Nov 21-26

S. Brown
McCoy
Maddal
Ellen

15

NO. 910

FdL+T-7

181.8

FdL+Disc 1930/4
RE 1847

Redondo

St.

Chapel Coast
02 61/6

8/01

147.97

FdL

17

Fd Mon

16

3 4

Block 42
Point Loma
Hts

15

14

W. Wood Road

Tennyson St. Alignment
Horden St to Catalina Blvd.

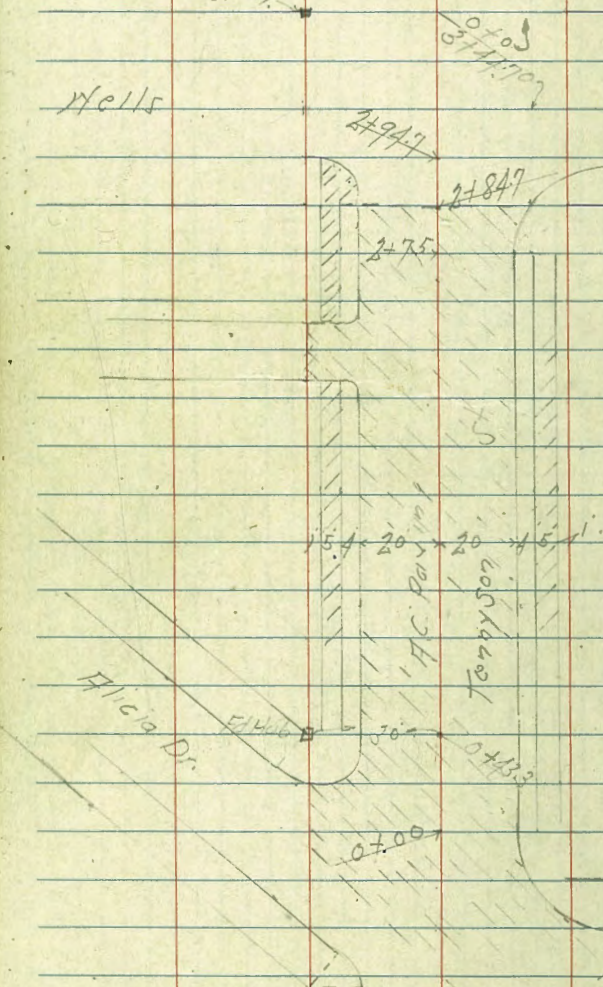
Levels next page

Catalina Page

Added Notes
FB #1835-44

Fd. Mon.

Wells

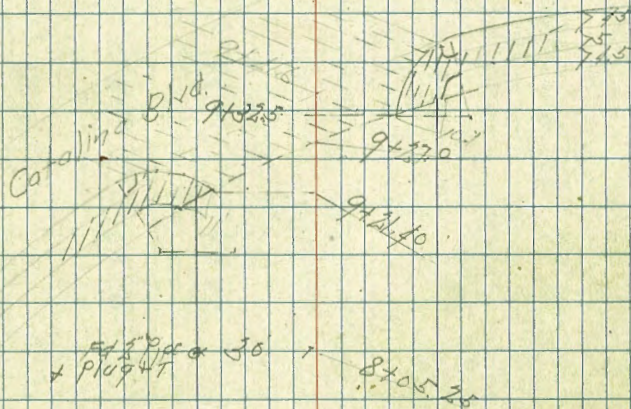


385 50%

Nov 22-46
Sisson
McCoy
Hoddel
Allen

#1372
#2227

16



Alley in 2076
42
2/29/50
CAR

Tennyson St

San Clemente
Not Graded

Mon. Out

B.A. Ford

Cross Section Tennyson St.
 Morden St to Catalina Blvd.

+20.3 = F.L. Alley on St

2+0

+50

1+0

0+43.3

0+0 = C.B. Morden St

BM 9.96 105.71

95.75

NXBP
 Tennyson
 Catalina
 Page 8

| St. Elevation | 102.23 | 102.12 | 101.59 | 101.52 | 101.42 | 101.21 | 101.13 |
|---------------|--------|--------|--------|--------|--------|--------|--------|
| 58-05 | 54.8 | 53.59 | 47.3 | 47.8 | 47.29 | 45.0 | 45.58 |
| 20-56 | 101.45 | 100.80 | 100.82 | 100.71 | 100.45 | 99.91 | 100.43 |
| 20-06 | 99.60 | 98.98 | 99.04 | 98.88 | 98.51 | 98.06 | 98.54 |
| 20-06 | 97.75 | 97.14 | 97.18 | 97.05 | 96.64 | 96.17 | 96.71 |
| 20-06 | 95.71 | 95.11 | 95.04 | 94.93 | 94.64 | 94.16 | 94.71 |
| 20-06 | 93.46 | 93.51 | 93.44 | 93.04 | 92.46 | 92.98 | |
| 20-06 | 105.91 | | | | | | |

Lt.S

20

pt-H

17

RM

9.76 106.92

31X Cor. No. 1
Tennison
4 Wells

+34.7 = W.C.B. Line W.C. St.

2+14.7 = 2

+94.7 = F.C.B. Line Wells

TP 11.42 116.68 0.45 105.26

+84.7 = E.L. Wells St. = W.H. A.C. Parking

+75 = C.B. BC. on Rt

2+35 = W.L. Alley on Lt

105.91

27

28

18

| | | | | |
|---------------|-------------------|-------------------------|------------|------------|
| 102.91 | 104.24 | 105.26 | 106.1 | 106.5 |
| 2.80 30-55 | 1.47 20-CB | 11.42 30-CB 50-FH | 1.06 30 | 1.07 30 |
| 102.79 | 103.60 | 104.6 | 105.4 | 106.1 |
| 2.91 20-CB | 2.11 20 | 1.11 50 | 1.13 20 | 1.06 20 |
| 102.17 | 103.90 | 104.3 | 104.8 | 105.5 |
| 2.51 20-CB | 1.81 20-Gutter | 1.24 20 | 1.19 20 | 1.12 20 |
| 102.11 | 103.64 | 104.3 | 104.8 | 105.5 |
| 2.60 20 | 1.74 20 | 1.24 20 | 1.19 20 | 1.12 20 |
| 102.01 | 103.48 | 104.0 | 104.56 | 105.4 |
| 2.70 20 | 1.85 20 | 1.27 20 | 1.24 20 | 1.13 20 |
| 101.71 | 103.18 | 103.7 | 104.5 | 105.1 |
| 2.00 20 | 2.22 20 | 1.18 20 | 1.22 20 | 1.16 20 |
| 101.23 | 102.75 | 104.1 | 104.4 | 105.2 |
| 4.48 20 | 2.80 20 | 1.26 20 | 1.24 20 | 1.15 20 |
| 101.68 | 103.25 | 103.24 | 103.9 | 105.2 |
| 4.53 20-CB | 2.16 20-CB | 1.24 20-CB 50-FH | 1.28 30 | 1.15 30 |

105.91

+50

2+0

TP 12.32 128.85 0.15 116.55

+65 $\frac{1}{2}$ - $\frac{1}{2}$ Scher M.H. 1.46 67 R.L.M.

+50

1+0

+54 right of $\frac{1}{2}$ -Sly Harbor Pole

+50

+07 224 Rt of $\frac{1}{2}$ -NW Tal Pole

+04 223 Lt of $\frac{1}{2}$ -Sly Power Pole

0+00
3744.7 = W.L. Hall St.

116.68

4+

4+

| | | | | | | | | |
|----|-------|-------|-------|-------|-------|-------|-------|-------|
| 67 | 121.2 | 120.6 | 119.4 | 119.5 | 119.3 | 119.0 | 118.9 | 118.5 |
| 66 | 118.8 | 118.0 | 116.9 | 116.9 | 116.6 | 115.8 | 116.2 | 116.0 |
| 65 | 115.6 | 115.3 | 114.2 | 114.2 | 114.2 | 113.5 | 113.7 | 113.2 |
| 64 | 112.6 | 112.3 | 111.4 | 111.5 | 111.1 | 110.5 | 111.2 | 110.9 |
| 63 | 109.8 | 108.2 | 108.6 | 108.6 | 108.6 | 108.0 | 108.2 | 108.6 |
| 62 | 107.3 | 106.6 | 105.9 | 105.9 | 105.9 | 105.6 | 105.8 | 105.8 |
| 61 | 104.9 | 104.6 | 104.6 | 104.6 | 104.6 | 104.0 | 104.2 | 104.6 |
| 60 | 102.5 | 102.3 | 102.4 | 102.5 | 102.5 | 102.5 | 102.5 | 102.5 |
| 59 | 100.1 | 100.1 | 100.1 | 100.1 | 100.1 | 100.1 | 100.1 | 100.1 |
| 58 | 97.7 | 97.7 | 97.7 | 97.7 | 97.7 | 97.7 | 97.7 | 97.7 |
| 57 | 95.3 | 95.3 | 95.3 | 95.3 | 95.3 | 95.3 | 95.3 | 95.3 |
| 56 | 92.9 | 92.9 | 92.9 | 92.9 | 92.9 | 92.9 | 92.9 | 92.9 |
| 55 | 90.5 | 90.5 | 90.5 | 90.5 | 90.5 | 90.5 | 90.5 | 90.5 |
| 54 | 88.1 | 88.1 | 88.1 | 88.1 | 88.1 | 88.1 | 88.1 | 88.1 |
| 53 | 85.7 | 85.7 | 85.7 | 85.7 | 85.7 | 85.7 | 85.7 | 85.7 |
| 52 | 83.3 | 83.3 | 83.3 | 83.3 | 83.3 | 83.3 | 83.3 | 83.3 |
| 51 | 80.9 | 80.9 | 80.9 | 80.9 | 80.9 | 80.9 | 80.9 | 80.9 |
| 50 | 78.5 | 78.5 | 78.5 | 78.5 | 78.5 | 78.5 | 78.5 | 78.5 |
| 49 | 76.1 | 76.1 | 76.1 | 76.1 | 76.1 | 76.1 | 76.1 | 76.1 |
| 48 | 73.7 | 73.7 | 73.7 | 73.7 | 73.7 | 73.7 | 73.7 | 73.7 |
| 47 | 71.3 | 71.3 | 71.3 | 71.3 | 71.3 | 71.3 | 71.3 | 71.3 |
| 46 | 68.9 | 68.9 | 68.9 | 68.9 | 68.9 | 68.9 | 68.9 | 68.9 |
| 45 | 66.5 | 66.5 | 66.5 | 66.5 | 66.5 | 66.5 | 66.5 | 66.5 |
| 44 | 64.1 | 64.1 | 64.1 | 64.1 | 64.1 | 64.1 | 64.1 | 64.1 |
| 43 | 61.7 | 61.7 | 61.7 | 61.7 | 61.7 | 61.7 | 61.7 | 61.7 |
| 42 | 59.3 | 59.3 | 59.3 | 59.3 | 59.3 | 59.3 | 59.3 | 59.3 |
| 41 | 56.9 | 56.9 | 56.9 | 56.9 | 56.9 | 56.9 | 56.9 | 56.9 |
| 40 | 54.5 | 54.5 | 54.5 | 54.5 | 54.5 | 54.5 | 54.5 | 54.5 |
| 39 | 52.1 | 52.1 | 52.1 | 52.1 | 52.1 | 52.1 | 52.1 | 52.1 |
| 38 | 49.7 | 49.7 | 49.7 | 49.7 | 49.7 | 49.7 | 49.7 | 49.7 |
| 37 | 47.3 | 47.3 | 47.3 | 47.3 | 47.3 | 47.3 | 47.3 | 47.3 |
| 36 | 44.9 | 44.9 | 44.9 | 44.9 | 44.9 | 44.9 | 44.9 | 44.9 |
| 35 | 42.5 | 42.5 | 42.5 | 42.5 | 42.5 | 42.5 | 42.5 | 42.5 |
| 34 | 40.1 | 40.1 | 40.1 | 40.1 | 40.1 | 40.1 | 40.1 | 40.1 |
| 33 | 37.7 | 37.7 | 37.7 | 37.7 | 37.7 | 37.7 | 37.7 | 37.7 |
| 32 | 35.3 | 35.3 | 35.3 | 35.3 | 35.3 | 35.3 | 35.3 | 35.3 |
| 31 | 32.9 | 32.9 | 32.9 | 32.9 | 32.9 | 32.9 | 32.9 | 32.9 |
| 30 | 30.5 | 30.5 | 30.5 | 30.5 | 30.5 | 30.5 | 30.5 | 30.5 |
| 29 | 28.1 | 28.1 | 28.1 | 28.1 | 28.1 | 28.1 | 28.1 | 28.1 |
| 28 | 25.7 | 25.7 | 25.7 | 25.7 | 25.7 | 25.7 | 25.7 | 25.7 |
| 27 | 23.3 | 23.3 | 23.3 | 23.3 | 23.3 | 23.3 | 23.3 | 23.3 |
| 26 | 20.9 | 20.9 | 20.9 | 20.9 | 20.9 | 20.9 | 20.9 | 20.9 |
| 25 | 18.5 | 18.5 | 18.5 | 18.5 | 18.5 | 18.5 | 18.5 | 18.5 |
| 24 | 16.1 | 16.1 | 16.1 | 16.1 | 16.1 | 16.1 | 16.1 | 16.1 |
| 23 | 13.7 | 13.7 | 13.7 | 13.7 | 13.7 | 13.7 | 13.7 | 13.7 |
| 22 | 11.3 | 11.3 | 11.3 | 11.3 | 11.3 | 11.3 | 11.3 | 11.3 |
| 21 | 8.9 | 8.9 | 8.9 | 8.9 | 8.9 | 8.9 | 8.9 | 8.9 |
| 20 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 | 6.5 |
| 19 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 | 4.1 |
| 18 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 | 1.7 |
| 17 | -0.7 | -0.7 | -0.7 | -0.7 | -0.7 | -0.7 | -0.7 | -0.7 |
| 16 | -3.1 | -3.1 | -3.1 | -3.1 | -3.1 | -3.1 | -3.1 | -3.1 |
| 15 | -5.5 | -5.5 | -5.5 | -5.5 | -5.5 | -5.5 | -5.5 | -5.5 |
| 14 | -7.9 | -7.9 | -7.9 | -7.9 | -7.9 | -7.9 | -7.9 | -7.9 |
| 13 | -10.3 | -10.3 | -10.3 | -10.3 | -10.3 | -10.3 | -10.3 | -10.3 |
| 12 | -12.7 | -12.7 | -12.7 | -12.7 | -12.7 | -12.7 | -12.7 | -12.7 |
| 11 | -15.1 | -15.1 | -15.1 | -15.1 | -15.1 | -15.1 | -15.1 | -15.1 |
| 10 | -17.5 | -17.5 | -17.5 | -17.5 | -17.5 | -17.5 | -17.5 | -17.5 |
| 9 | -19.9 | -19.9 | -19.9 | -19.9 | -19.9 | -19.9 | -19.9 | -19.9 |
| 8 | -22.3 | -22.3 | -22.3 | -22.3 | -22.3 | -22.3 | -22.3 | -22.3 |
| 7 | -24.7 | -24.7 | -24.7 | -24.7 | -24.7 | -24.7 | -24.7 | -24.7 |
| 6 | -27.1 | -27.1 | -27.1 | -27.1 | -27.1 | -27.1 | -27.1 | -27.1 |
| 5 | -29.5 | -29.5 | -29.5 | -29.5 | -29.5 | -29.5 | -29.5 | -29.5 |
| 4 | -31.9 | -31.9 | -31.9 | -31.9 | -31.9 | -31.9 | -31.9 | -31.9 |
| 3 | -34.3 | -34.3 | -34.3 | -34.3 | -34.3 | -34.3 | -34.3 | -34.3 |
| 2 | -36.7 | -36.7 | -36.7 | -36.7 | -36.7 | -36.7 | -36.7 | -36.7 |
| 1 | -39.1 | -39.1 | -39.1 | -39.1 | -39.1 | -39.1 | -39.1 | -39.1 |
| 0 | -41.5 | -41.5 | -41.5 | -41.5 | -41.5 | -41.5 | -41.5 | -41.5 |

89.11

7+0

7+50 22467 of 2 - Sky Power Pole

TP 2.14 120.67 10.32 118.53

6+04

7+75

7+53

5+50

128.85

| | | | | | | | | | | | | | | | | | | |
|-----------|-------|-----------|-------|-------|-----------|-------|-------|-----------|-------|-------|-----------|-------|--------|-------|--------|-----------|-------|-------|
| 6.4 30 | 114.3 | 6.4 30 | 127.7 | 119.6 | 6.4 30 | 126.8 | 124.4 | 6.4 30 | 124.2 | 124.2 | 6.4 30 | 125.7 | 126.3 | 125.0 | 128.52 | 6.4 30 | 126.3 | 127.6 |
| 8.9 20 | 113.8 | 8.9 20 | 127.3 | 118.7 | 8.9 20 | 126.3 | 123.4 | 8.9 20 | 124.2 | 124.2 | 8.9 20 | 125.7 | 126.3 | 125.0 | 128.52 | 8.9 20 | 126.3 | 127.6 |
| 8.9 7 | 111.8 | 8.9 7 | 125.2 | 117.4 | 8.9 7 | 124.1 | 121.2 | 8.9 7 | 124.2 | 124.2 | 8.9 7 | 125.7 | 126.3 | 125.0 | 128.52 | 8.9 7 | 126.3 | 127.6 |
| 8.8 10 | 111.5 | 8.8 10 | 125.7 | 117.7 | 8.8 10 | 124.4 | 121.7 | 8.8 10 | 124.2 | 124.2 | 8.8 10 | 125.7 | 126.3 | 125.0 | 128.52 | 8.8 10 | 126.3 | 127.6 |
| 8.6 | 112.1 | 8.6 | 125.8 | 117.4 | 8.6 | 124.2 | 121.8 | 8.6 | 124.2 | 124.2 | 8.6 | 125.7 | 126.3 | 125.0 | 128.52 | 8.6 | 126.3 | 127.6 |
| 8.8 10 | 111.9 | 8.8 10 | 125.7 | 117.0 | 8.8 10 | 124.2 | 121.5 | 8.8 10 | 124.2 | 124.2 | 8.8 10 | 125.7 | 126.3 | 125.0 | 128.52 | 8.8 10 | 126.3 | 127.6 |
| 8.9 20 | 112.5 | 8.9 20 | 126.3 | 117.5 | 8.9 20 | 125.0 | 122.2 | 8.9 20 | 125.0 | 125.0 | 8.9 20 | 126.3 | 127.6 | 125.0 | 128.52 | 8.9 20 | 126.3 | 127.6 |
| 7.9 30 | 112.8 | 7.9 30 | 127.6 | 117.0 | 7.9 30 | 126.8 | 123.3 | 7.9 30 | 126.8 | 126.8 | 7.9 30 | 127.6 | 128.52 | 125.0 | 128.52 | 7.9 30 | 126.8 | 127.6 |

128.85

0.6 = 3/5
5.3 = 11/20
4.6 = 23/5
3.2 = 16/5
127.15
128.52 = 127.15 + 1.37
128.52 = 127.15 + 1.37

BM

9.79

87.24

Don't Excl
End of
Curb End
Trolley
87.24 P/A

9+27 = El. Catalina Blvd + Fly Paving Taken on Day

+21.4 = Curb End on Lt.

9+0

TP 0.82 97.03 12.16 96.21

+50

+05 228 ft of 7-5/8 Power Pole

8+0

TP 0.20 108.37 12.50 108.17

7+50

120.67

Lit.

Rt.

22

| | | | | | | | | |
|-----------|------------|-------------|------------|--------|------------|--------------|-------------|------------|
| 89.6 | 89.53 | 88.89 | 88.55 | 88.05 | 87.40 | 86.73 | 87.23 | 87.13 |
| 71 30 | 750 248 | 8.14 248 | 8.48 11 | 8.98 | 9.63 11 | 10.30 207 | 9.80 207 | 9.9 214 |
| 89.6 | 89.53 | 88.89 | 88.55 | 88.05 | 87.40 | 86.73 | 87.23 | 87.13 |
| 71 30 | 750 248 | 8.14 248 | 8.48 11 | 8.98 | 9.63 11 | 10.30 207 | 9.80 207 | 9.9 214 |
| 93.2 | 93.0 | 91.2 | 91.1 | 90.7 | 90.6 | 90.0 | 90.5 | 91.4 |
| 63 30 | 40 20 | 52 17 | 50 10 | 6 3 | 6 10 | 7 15 | 6 20 | 5 30 |
| 98.2 | 97.7 | 96.2 | 95.7 | 95.7 | 95.6 | 95.7 | 96.3 | |
| 102 30 | 127 20 | 122 17 | 127 10 | 127 | 128 10 | 127 20 | 127 30 | |
| 103.2 | 102.4 | 101.3 | 100.9 | 100.7 | 100.7 | 101.3 | 101.7 | 102.6 |
| 57 30 | 60 20 | 71 15 | 75 10 | 77 | 77 10 | 76 20 | 77 27 | 78 30 |
| 109.0 | 108.2 | 106.2 | 106.1 | 106.6 | 106.1 | 106.5 | 106.8 | |
| 117 30 | 125 20 | 145 17 | 146 10 | 141 | 145 10 | 147 20 | 139 30 | |

120.67

9 + 416 = F Cb Line of Catalina Take in Dior

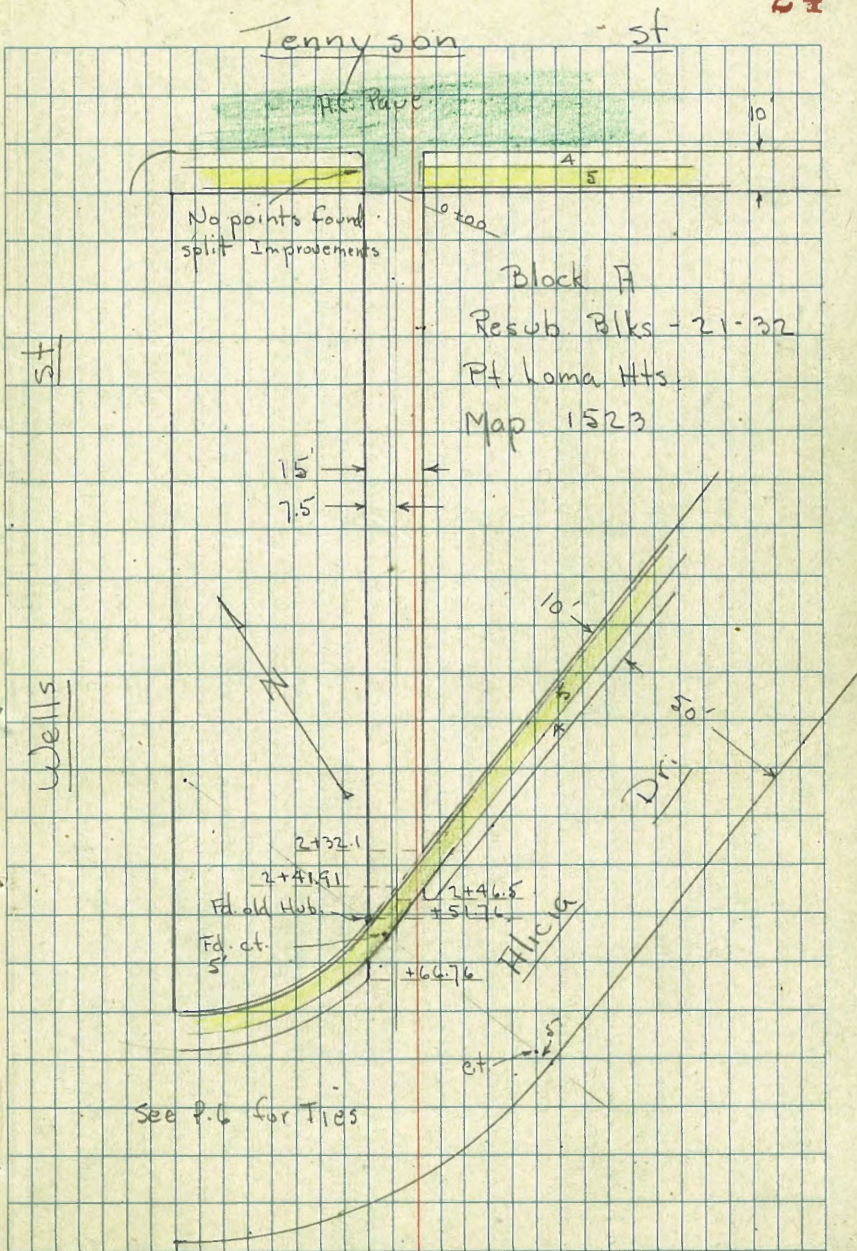
97.03

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 89.67 | 89.05 | 87.89 | 87.96 | 86.98 | 86.40 | 85.95 | 85.28 | 85.89 |
| 7.38 | 7.98 | 9.11 | 9.57 | 10.05 | 10.63 | 11.08 | 11.75 | 11.14 |
| 19.1 | 19.1 | 22 | 11 | | 11 | 23 | 37 | 37 |
| | | 110.5 | | | | | 110.5 | 110.5 |

97.03

X-Sect. 15' Alley in Block F -
See Page 72 for Notes

W.O. 25001



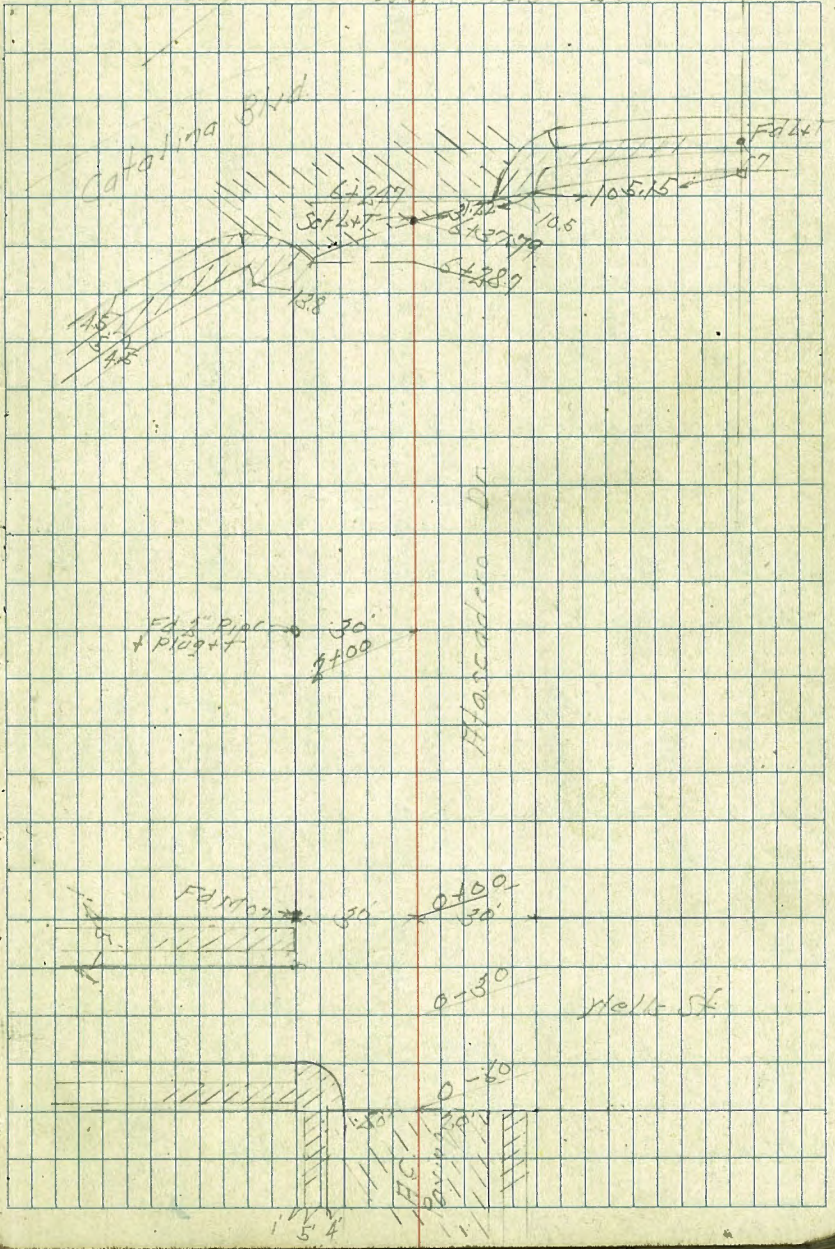
Hascadero Drive Alignment
Hells St. to Catalina Blvd.

Level next page

Additional X Sections FB[#]2015-24

Nov. 25-46
Sisson
McCoy
Hordel
Allen

Mark Order #330



| | |
|------|------------------------------------------------------|
| +60 | |
| +30 | |
| +10 | |
| | |
| +75 | |
| +50 | |
| +42 | 22 Pt of $\frac{1}{2}$ - $\frac{1}{2}$ 12" Euc. Trce |
| 0+35 | |

16039

| | |
|--|-----------------------------------------------------|
| | 6.24 / 57.7 / 56.3 |
| | 6.24 / 57.3 / 56.1 |
| | 6.24 / 56.4 / 55.1 |
| | 6.24 / 56.3 / 54.9 |
| | 6.24 / 56.4 / 55.1 |
| | 6.24 / 56.3 / 55.1 |
| | 6.24 / 56.4 / 55.1 |
| | 6.24 / 56.3 / 55.1 |
| | 6.24 / 56.2 / 54.7 |
| | 6.24 / 57.0 / 55.9 |
| | 6.24 / 57.4 / 56.1 |
| | 6.24 / 58.2 / 56.3 |
| | 6.24 / 57.1 / 56.2 |
| | 6.24 / 56.7 / 56.0 |
| | 6.24 / 56.6 / 56.0 |
| | 6.24 / 56.2 / 56.0 |
| | 6.24 / 56.2 / 55.6 |
| | 6.24 / 57.9 / 55.2 |
| | 6.24 / 55.8 / 55.8 |
| | 6.24 / 55.8 / 55.8 |
| | 6.24 / 55.0 / 55.0 |
| | 6.24 / 55.8 / 55.8 |
| | 6.24 / 55.0 / 55.8 |
| | 6.24 / 55.0 / 55.8 |

16039

~~6.24~~ / ~~58.0~~ / ~~58.0~~

+50

TP 0.78 136.98 12.43 136.20

40

+50

20

TP 0.78 148.63 12.54 147.85

+50

20

160.39

| | | | | | |
|-------|-------|-------|-------|--------|-------|
| 132.4 | 137.6 | 141.6 | 144.7 | 149.31 | 152.7 |
| 132.1 | 136.4 | 140.1 | 144.5 | 149.21 | 153.0 |
| 132.0 | 135.3 | 139.5 | 143.5 | 147.39 | 152.1 |
| 131.0 | 135.6 | 139.8 | 144.0 | 148.0 | 152.2 |
| 132.1 | 136.2 | 140.0 | 144.2 | 148.3 | 152.2 |
| 131.2 | 135.6 | 140.0 | 144.1 | 148.0 | 152.0 |
| 131.9 | 135.1 | 140.0 | 143.8 | 147.9 | 151.5 |
| 132.4 | 136.6 | 141.1 | 145.5 | 147.3 | 152.7 |
| | | | | | 153.3 |

160.39

BM 7.76 108.99

TP 2.67 116.75 10.98 114.08

+52 = F.C. Line of Catalina

BM 8.22 116.84

+37.79 = F.L. Catalina Blvd. Taken ending

+28.7 = Cb End on Lt.

640

TP 1.02 135.06 12.94 124.04

+50

540

136.98

SF Top of Hd
5/16/10
Catalina
10899
Page 14

SF RPT'd
Flascondore
4/24/10

Lt.

Rt.

29

| | | | | | |
|-------|-------|--------|--------|-------|--------|
| 128.4 | 121.0 | 117.7 | 116.79 | 8.27 | 29.00 |
| 128.3 | 120.6 | 117.83 | 116.17 | 8.89 | 41.50 |
| 128.1 | 120.4 | 117.17 | 115.69 | 9.37 | 54.00 |
| 126.6 | 119.6 | 117.18 | 115.45 | 9.61 | 66.00 |
| 127.5 | 119.9 | 117.8 | 115.38 | 9.68 | 78.00 |
| 127.7 | 119.8 | 117.8 | 115.09 | 9.97 | 90.00 |
| 127.6 | 119.8 | 117.6 | 114.97 | 10.09 | 102.00 |
| 127.0 | 119.3 | 117.1 | 114.97 | 10.30 | 114.00 |
| 128.2 | 121.0 | 118.7 | 114.76 | 10.30 | 126.00 |
| 128.8 | 120.9 | 118.0 | 115.31 | 9.95 | 138.00 |
| 128.4 | 125.1 | 117.7 | | 9.25 | 150.00 |
| 128.3 | 124.8 | 117.7 | | 9.25 | 162.00 |
| 126.6 | 122.9 | 117.3 | | 9.25 | 174.00 |
| 127.5 | 124.0 | 117.8 | | 9.25 | 186.00 |
| 127.7 | 123.5 | 117.6 | | 9.25 | 198.00 |
| 127.6 | 122.9 | 117.1 | | 9.25 | 210.00 |
| 128.2 | 125.2 | 118.7 | | 9.25 | 222.00 |
| 128.8 | 125.1 | 118.0 | | 9.25 | 234.00 |

136.98

Cross Section C. Calcedony St.
Lamont St. to Academy St.

index of
C.S.R.

Lt. = 11

8

Rt. = 5

31

Sketch page 50

+99 20.5 ft of $\frac{1}{2}$ - 5/4 Perce. Pale

+50

+20 21.7 ft of $\frac{1}{2}$ - 1/4 Tel Pale

+0.5

0+0 - East line of Lamont St.

0-20 = East Carb Line of Lamont St.

| | | | | | |
|----|-------|--------|------|--------|-------------------------------------|
| BM | 466 | 130.88 | 4.80 | 126.22 | SE of 1 C. Calcedony + Lamont |
| TP | 12.56 | 131.02 | 0.18 | 118.76 | |
| BM | 12.69 | 118.64 | | 105.95 | SW of P D. Lamont + Acad |

| | | | | | | | |
|-----------|-----------|-----------|--------|-----------|----------|------------|-----------|
| 128.9 | 128.1 | 127.9 | 126.3 | 126.4 | 126.2 | 125.4 | 124.8 |
| 20/40 | 28/35 | 30/40 | 46/40 | 45/40 | 47/40 | 47/40 | 51/40 |
| 130.0 | 128.7 | 126.7 | 126.5 | 126.3 | 126.0 | 126.3 | 126.0 |
| 27/40 | 38/30 | 42/37 | 44/40 | 46/40 | 49/40 | 46/40 | 49/40 |
| 127.5 | 127.13 | 126.46 | 126.53 | 126.33 | 125.92 | 125.52 | 126.06 |
| 14/40 | 27.5/49.0 | 41.3/39.0 | 43/40 | 45.1/40 | 49.1/40 | 51.36/50.2 | 48.1/20.7 |
| 127.18 | 126.64 | 126.38 | 126.10 | 125.61 | 125.33 | 126.05 | |
| 37.0/40.0 | 4.24/10.0 | 4.53/3.0 | 4.78 | 5.27/40.0 | 5.5/40.0 | 4.83/40.0 | |
| | | | | | | | 130.88 |

TP 317 126.72 7.33 123.55

+50

+14 167 ft of $\frac{1}{2}$ - Sky Tel Pole

340 192 ft of $\frac{1}{2}$ - Sky Paper Pole

+50

+25 198 ft of $\frac{1}{2}$ - Sky Wire Fence

240

+52 196 ft of $\frac{1}{2}$ - Sky Tel Pole

+50

+20 203 ft of $\frac{1}{2}$ - Sky Wire Fence

140

130.88

385 50%

64

44

44

32

~~127.5~~
124.5

~~125.7~~
124.2

~~125.5~~
123.9

~~125.5~~
123.9

~~125.3~~
123.7

~~126.4~~
124.5

~~126.4~~
124.0

~~125.1~~
123.2

~~124.5~~
122.9

~~126.5~~
126.5

~~126.1~~
126.1

~~126.0~~
126.0

~~125.7~~
125.7

~~125.5~~
125.3

~~126.4~~
126.4

~~125.8~~
125.8

~~125.6~~
125.6

~~125.1~~
124.5

~~126.7~~
126.7

~~126.0~~
126.1

~~125.2~~
126.0

~~125.2~~
125.7

~~125.0~~
125.5

~~125.5~~
126.0

~~125.8~~
125.8

~~124.3~~
125.6

~~124.1~~
125.1

~~126.8~~
126.8

~~125.9~~
126.0

~~125.3~~
125.2

~~125.2~~
125.2

~~125.1~~
125.0

~~124.7~~
125.5

~~123.5~~
126.0

~~122.9~~
124.3

~~122.7~~
124.1

~~127.9~~
127.9

~~126.6~~
126.6

~~126.3~~
126.3

~~125.5~~
125.5

~~125.5~~
125.2

~~125.5~~
125.1

~~125.8~~
124.7

~~124.3~~
123.5

~~124.1~~
122.9

~~123.6~~
122.7

130.88

Chalcedony st.

TP 2.32 117.46 115.58 115.14
37 Caped P.P.
40 41 42
5780.77

+50

540

+75

+50

+11

470

126.72

41.

4

ft.

33

| | | | | | | | | |
|--|-------|-------|-------|-------|-------|-------|-------|-------|
| | 120.4 | 119.2 | 119.0 | 118.5 | 118.0 | 117.5 | 116.6 | 116.2 |
| | 77 | 75 | 77 | 82 | 87 | 92 | 101 | 105 |
| | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
| | 122.1 | 121.6 | 121.5 | 121.5 | 120.6 | 120.1 | 119.9 | 119.3 |
| | 46 | 51 | 51 | 52 | 61 | 66 | 70 | 80 |
| | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
| | 123.7 | 123.4 | 123.4 | 122.9 | 122.4 | 121.9 | 120.5 | 119.9 |
| | 40 | 50 | 50 | 58 | 48 | 40 | 30 | 20 |
| | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
| | 125.2 | 124.9 | 124.1 | 123.5 | 123.3 | 122.8 | 121.0 | 120.2 |
| | 15 | 20 | 26 | 32 | 40 | 49 | 57 | 65 |
| | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |

123.5 = 123.4 + 0.1
Bitch 1/11

126.72

+50 = 2.5 wide to bottom
open ditch Taken on Diagonal

+45

740

750

640

5480 40' Pt of 1/2 - 1 1/4 Rail Fence

117.46

| | | | | | | | | | |
|-------------|-------------|-------------|-------------|-------------|--------------|--------------|--------------|--------------|--------------|
| 8.5 21.5 | 8.6 22.8 | 8.8 21.4 | 9.4 20.0 | 9.9 21.4 | 10.3 21.4 | 11.2 22.8 | 11.2 22.8 | 11.5 25.0 | 11.5 25.0 |
| 108.0 | 108.9 | 108.7 | 108.1 | 108.1 | 107.2 | 106.3 | 106.2 | 106.2 | 106.2 |
| 112.8 | 112.9 | 112.8 | 112.0 | 112.3 | 112.3 | 111.6 | 109.1 | 108.8 | 108.7 |
| 47 60 | 47 60 | 49 60 | 51 60 | 51 60 | 51 60 | 51 60 | 51 60 | 51 60 | 51 60 |
| 112.8 | 112.8 | 112.4 | 112.5 | 112.4 | 112.4 | 112.3 | 109.1 | 109.0 | 108.9 |
| 47 60 | 47 60 | 49 60 | 49 60 | 49 60 | 49 60 | 49 60 | 49 60 | 49 60 | 49 60 |
| 113.2 | 112.9 | 112.7 | 112.8 | 112.6 | 112.4 | 112.5 | 109.9 | 109.6 | 109.5 |
| 47 60 | 46 60 | 48 60 | 47 60 | 49 60 | 49 60 | 49 60 | 49 60 | 49 60 | 49 60 |
| 113.6 | 113.0 | 112.5 | 112.4 | 112.3 | 112.7 | 112.1 | 110.7 | 110.6 | 110.1 |
| 47 60 | 45 60 | 45 60 | 47 60 | 48 60 | 48 60 | 47 60 | 48 60 | 49 60 | 47 60 |
| 116.8 | 115.2 | 113.3 | 112.8 | 112.4 | 112.1 | 111.1 | 111.2 | 110.4 | 110.4 |
| 47 60 | 47 60 | 48 60 | 47 60 | 47 60 | 47 60 | 47 60 | 47 60 | 47 60 | 47 60 |

117.46

BM 9.48 118.63 5.7. P. 60
Lap 11 Academy
St 2579

TP 11.52 128.11 0.87 116.59

8+15.44 = L Academy St to North

7+90.44 = X L Academy St to North

7+70

117.46

| | | | | | |
|---------|--------|-------|-------|-------|-------|
| 55/60 | 112.9 | 48/50 | 112.7 | 30/40 | 114.5 |
| 46/50 | 112.9 | 53/50 | 112.5 | 29 | 114.6 |
| 50/50 | 112.5 | 55/50 | 112.4 | 30/30 | 114.4 |
| 52/50 | 112.2 | 55/50 | 112.1 | 31 | 114.4 |
| 56/50 | 111.9 | 55/50 | 112.0 | 31 | 114.4 |
| 67/50 | 110.8 | 55/50 | 112.0 | 36/30 | 114.9 |
| 46/50 | 110.9 | 50/50 | 111.5 | 38/30 | 114.7 |
| 25.2/50 | 107.0 | 46/50 | 110.9 | 41/30 | 113.4 |
| 10.5/50 | 108.26 | 55/50 | 111.4 | 51/50 | 112.4 |
| 10.5/50 | 106.2 | | | | |

117.46

Bench Levels Lamont St.
Diamond to Hilber

| | | | | | |
|----|-------|--------|------|--------|------------------------------------------|
| BM | 12.67 | 118.62 | | 105.95 | 574 BP Diamond + Lamont |
| TP | 12.58 | 131.04 | 0.16 | 118.46 | |
| BM | | | 4.82 | 126.22 | SE 7 2+7 Cholcedony + Lamont |
| TP | 12.82 | 141.57 | 2.29 | 128.75 | |
| BM | 13.00 | 153.22 | 1.35 | 140.22 | SE 7 2+7 Lamont |
| TP | 12.95 | 164.20 | 1.97 | 151.25 | |
| BM | 12.15 | 174.43 | 1.92 | 162.28 | SE 7 2+7 Beryl + Lamont |
| TP | 12.95 | 187.06 | 0.32 | 174.11 | |
| BM | | | 0.81 | 186.25 | SE 7 2+7 Hilber + Lamont 186.29 |

385 50%

4730

410

3150

310

2150

TP 2.26 138.02 897 13576

2111 27' S of S = E of Masonry Wall

210

144.73

54

27

PT

| | | | | | | | | | |
|-------|-------|-------|-------|-------|-------|--------|-------|-------|-------|
| 136.5 | 133.9 | 133.9 | 134.6 | 135.1 | 136.5 | 135.8 | 134.8 | 134.1 | 133.5 |
| 132.9 | 133.4 | 133.9 | 134.6 | 135.1 | 136.4 | 135.8 | 134.8 | 134.1 | 133.5 |
| 132.4 | 132.9 | 133.4 | 133.9 | 134.7 | 135.9 | 135.9 | 134.8 | 134.1 | 133.5 |
| 132.2 | 132.2 | 132.3 | 133.2 | 134.1 | 134.9 | 135.02 | 134.8 | 134.1 | 133.5 |
| 132.0 | 131.8 | 132.0 | 132.7 | 133.5 | 134.5 | 134.8 | 134.8 | 134.1 | 133.5 |
| 131.9 | 131.9 | 131.6 | 132.4 | 133.2 | 134.8 | 134.8 | 134.8 | 134.1 | 133.5 |
| 131.5 | 130.7 | 131.1 | 131.8 | 132.6 | 134.6 | 134.6 | 134.6 | 134.1 | 133.5 |

136.5
136.4
135.9
135.8
134.8
134.1
133.5

144.73

6415

640

5445

5435

TP 1.94 127.76 12.20 125.82

540

445

13802

69
1027
1022
1018
10107
1079
10

120.9

125.1

125.5

126.0

127.3

130.1

27
1516
2522
1522
15109
2571
25

120.3

123.2

127.5

125.0

127.1

130.9

80
1563
1541
1538
15111
1571
15

119.4

121.5

123.7

124.0

126.9

130.6

80

77

52

44

113

71

119.8

120.1

122.6

123.4

126.7

130.6

80
1579
1544
1538
15107
1568
15

119.4

119.9

121.4

124.0

127.5

131.2

86
2580
2571
2540
2598
2570
25

119.2

119.3

120.7

123.8

128.2

131.0

93
1090
1075
1036
1087
1066
10

118.6

118.8

120.5

124.2

129.3

131.4

13802

B.M. 8.19 133.35

on Hub 40/R
9+88.80
Bar y 1st.

TP 3.75 141.54 0.69 137.79

TP 11.43 138.48 0.71 127.05

B.M. 9.12 118.64

SW Pipe
LAWY
7cademy
5E202519
118.63
Page 35

7+64.75 = Prop BC on Rt

7+40

7+15

6+85

6+50

127.76

Lt.

2

Rt.

40

| | | | | | | |
|------------------|------------------|------------------|-------|------------------|------------------|------------------|
| 121.3 | 121.0 | 120.6 | 120.3 | 119.7 | 119.2 | 118.7 |
| $\frac{6.5}{10}$ | $\frac{6.8}{25}$ | $\frac{7.2}{15}$ | 7.5 | $\frac{8.1}{15}$ | $\frac{8.6}{25}$ | $\frac{9.1}{40}$ |
| 121.6 | 121.0 | 120.6 | 119.3 | 118.8 | 118.6 | 118.0 |
| $\frac{6.9}{10}$ | $\frac{6.8}{25}$ | $\frac{7.1}{15}$ | 8.5 | $\frac{9.0}{15}$ | $\frac{9.1}{25}$ | $\frac{9.8}{10}$ |
| 122.3 | 122.1 | 121.7 | 121.3 | 121.0 | 120.7 | 119.9 |
| $\frac{6.6}{10}$ | $\frac{6.7}{25}$ | $\frac{6.1}{15}$ | 6.5 | $\frac{6.8}{15}$ | $\frac{7.1}{25}$ | $\frac{7.9}{10}$ |
| 122.4 | 122.1 | 122.0 | 121.3 | 121.1 | 120.9 | 120.8 |
| $\frac{6.4}{10}$ | $\frac{6.5}{25}$ | $\frac{6.8}{15}$ | 6.5 | $\frac{6.7}{15}$ | $\frac{6.9}{25}$ | $\frac{7.0}{10}$ |
| 120.9 | 120.3 | 120.1 | 119.9 | 119.0 | 118.7 | 118.5 |
| $\frac{6.9}{10}$ | $\frac{7.5}{25}$ | $\frac{7.7}{15}$ | 8.4 | $\frac{8.8}{15}$ | $\frac{9.1}{25}$ | $\frac{9.3}{10}$ |

127.76

Cross Section Beryl St
Lamont to Academy St

Sketch Page 30

Indexed
C.S.M.

Dec 18 46
S. 300
1960
Haddel
Allen Lt. 11

Rt. 5 41

1+45

1+05

1+0

+99

+79

+59

0 +50

+39

+27

0+0

0-20 = ECB Line of Lamont

BM 2.78 165.06

162.28

1/2 1/2 1/2
Beryl +
Lamont
Page 36

| | | | | | |
|--------|--------|--------|--------|--------|--------|
| 162.13 | 162.13 | 161.82 | 161.5 | 164.0 | 162.9 |
| 161.57 | 162.11 | 161.52 | 160.89 | 161.3 | 161.0 |
| 161.22 | 161.99 | 160.8 | 160.1 | 160.3 | 160.0 |
| 161.05 | 161.39 | 160.8 | 160.1 | 160.0 | 159.6 |
| 160.85 | 161.19 | 160.5 | 160.0 | 160.0 | 159.5 |
| 160.63 | 160.63 | 160.1 | 159.6 | 159.5 | 158.9 |
| 160.26 | 160.07 | 159.9 | 159.1 | 159.0 | 158.5 |
| 159.81 | 160.58 | 159.93 | 159.41 | 159.24 | 158.70 |
| 160.61 | 160.9 | 160.2 | 159.2 | 159.2 | 159.0 |

2+50

1+26

1+32

2+0

+79 233 Rt of St = 1/4 4" Fuel Tree

1+70

1+50 = Fly Curb + Walk on Rt

165.06

Li:

Rt

42

| | | | | | | | |
|--------|-------|--------|-------|--------|-------|--------|-------|
| 41/10 | 160.7 | 41/10 | 162.2 | 41/10 | 160.7 | 41/10 | 160.8 |
| 46/25 | 160.5 | 46/25 | 161.3 | 46/25 | 160.2 | 46/25 | 158.3 |
| 55/30 | 159.6 | 55/30 | 160.6 | 55/30 | 160.3 | 55/30 | 158.2 |
| 56/30 | 159.5 | 56/30 | 160.5 | 56/30 | 160.5 | 56/30 | 159.0 |
| 57/30 | 159.4 | 57/30 | 160.2 | 57/30 | 160.7 | 57/30 | 159.9 |
| 61/10 | 158.9 | 61/10 | 159.7 | 61/10 | 160.9 | 61/10 | 158.3 |
| 66/20 | 158.5 | 66/20 | 159.2 | 66/20 | 160.9 | 66/20 | 158.2 |
| 67/20 | 158.6 | 67/20 | 159.5 | 67/20 | 160.9 | 67/20 | 158.2 |
| 70/20 | 158.9 | 70/20 | 159.7 | 70/20 | 160.9 | 70/20 | 158.3 |
| 71/20 | 158.9 | 71/20 | 159.7 | 71/20 | 160.9 | 71/20 | 158.3 |
| 72/20 | 158.9 | 72/20 | 159.7 | 72/20 | 160.9 | 72/20 | 158.3 |
| 73/20 | 158.9 | 73/20 | 159.7 | 73/20 | 160.9 | 73/20 | 158.3 |
| 74/20 | 158.9 | 74/20 | 159.7 | 74/20 | 160.9 | 74/20 | 158.3 |
| 75/20 | 158.9 | 75/20 | 159.7 | 75/20 | 160.9 | 75/20 | 158.3 |
| 76/20 | 158.9 | 76/20 | 159.7 | 76/20 | 160.9 | 76/20 | 158.3 |
| 77/20 | 158.9 | 77/20 | 159.7 | 77/20 | 160.9 | 77/20 | 158.3 |
| 78/20 | 158.9 | 78/20 | 159.7 | 78/20 | 160.9 | 78/20 | 158.3 |
| 79/20 | 158.9 | 79/20 | 159.7 | 79/20 | 160.9 | 79/20 | 158.3 |
| 80/20 | 158.9 | 80/20 | 159.7 | 80/20 | 160.9 | 80/20 | 158.3 |
| 81/20 | 158.9 | 81/20 | 159.7 | 81/20 | 160.9 | 81/20 | 158.3 |
| 82/20 | 158.9 | 82/20 | 159.7 | 82/20 | 160.9 | 82/20 | 158.3 |
| 83/20 | 158.9 | 83/20 | 159.7 | 83/20 | 160.9 | 83/20 | 158.3 |
| 84/20 | 158.9 | 84/20 | 159.7 | 84/20 | 160.9 | 84/20 | 158.3 |
| 85/20 | 158.9 | 85/20 | 159.7 | 85/20 | 160.9 | 85/20 | 158.3 |
| 86/20 | 158.9 | 86/20 | 159.7 | 86/20 | 160.9 | 86/20 | 158.3 |
| 87/20 | 158.9 | 87/20 | 159.7 | 87/20 | 160.9 | 87/20 | 158.3 |
| 88/20 | 158.9 | 88/20 | 159.7 | 88/20 | 160.9 | 88/20 | 158.3 |
| 89/20 | 158.9 | 89/20 | 159.7 | 89/20 | 160.9 | 89/20 | 158.3 |
| 90/20 | 158.9 | 90/20 | 159.7 | 90/20 | 160.9 | 90/20 | 158.3 |
| 91/20 | 158.9 | 91/20 | 159.7 | 91/20 | 160.9 | 91/20 | 158.3 |
| 92/20 | 158.9 | 92/20 | 159.7 | 92/20 | 160.9 | 92/20 | 158.3 |
| 93/20 | 158.9 | 93/20 | 159.7 | 93/20 | 160.9 | 93/20 | 158.3 |
| 94/20 | 158.9 | 94/20 | 159.7 | 94/20 | 160.9 | 94/20 | 158.3 |
| 95/20 | 158.9 | 95/20 | 159.7 | 95/20 | 160.9 | 95/20 | 158.3 |
| 96/20 | 158.9 | 96/20 | 159.7 | 96/20 | 160.9 | 96/20 | 158.3 |
| 97/20 | 158.9 | 97/20 | 159.7 | 97/20 | 160.9 | 97/20 | 158.3 |
| 98/20 | 158.9 | 98/20 | 159.7 | 98/20 | 160.9 | 98/20 | 158.3 |
| 99/20 | 158.9 | 99/20 | 159.7 | 99/20 | 160.9 | 99/20 | 158.3 |
| 100/20 | 158.9 | 100/20 | 159.7 | 100/20 | 160.9 | 100/20 | 158.3 |

165.06

+50 22.2 Rt of $\frac{1}{2}$ - NY Paper Pole

+31

+20 23.3 Rt of $\frac{1}{2}$ - NY 24" Euc Tree

+04

340

+95

+90 22.7 Rt of $\frac{1}{2}$ - NY 16" Euc Tree+70 21.4 Rt of $\frac{1}{2}$ - NY 14" Euc Tree

2769

165.06

161.2

 $\frac{39}{10}$

159.2

 $\frac{59}{20}$

158.5

 $\frac{66}{10}$

157.7

74

157.9

 $\frac{77}{14}$

156.1

 $\frac{98}{19}$

156.6

 $\frac{85}{10}$

154.7

 $\frac{104}{10}$

161.57

161.85

160.7

 $\frac{44}{10}$

160.0

 $\frac{51}{10}$

159.6

 $\frac{67}{10}$

159.4

 $\frac{65}{19}$

157.4

 $\frac{77}{19}$

158.9

 $\frac{64}{19}$

157.0

 $\frac{81}{10}$

161.81

 $\frac{53}{10}$ $\frac{55}{10}$ $\frac{57}{10}$ $\frac{59}{10}$ $\frac{61}{10}$ $\frac{63}{10}$ $\frac{65}{10}$ $\frac{67}{10}$ $\frac{69}{10}$ $\frac{71}{10}$ $\frac{73}{10}$ $\frac{75}{10}$ $\frac{77}{10}$ $\frac{79}{10}$ $\frac{81}{10}$ $\frac{83}{10}$ $\frac{85}{10}$

165.06

+82

+78 19.4 Pt of 2 - N 1/4 9" Euc Tree 157.0

+63 19.5 Pt of 2 - N 1/4 30" Euc Tree

+50 24.2 Pt of 2 - N 1/4 Power Pole 45
40

+44 21.2 Pt of 2 - N 1/4 18" Euc Tree

+41 18.6 " " " " 14" " "

+33 21.7 " " " " 13" Euc Tree

+32 " " " " " " "

+08

+0

+93 21.4 Pt of 2 - N 1/4 34" Euc Tree

TP 4.88 161.52 8.42 156.64

+87 18' Pt of 2 - N 1/4 12" Euc Tree

+80 14' Pt of 2 - N 1/4 18" Euc "

2x58

16506

| | | | | | | | | | |
|--------|-------|--------|-------|-------|-------|-------|-------|-------|-------|
| 156.0 | 155.6 | 155.1 | 154.8 | 154.2 | 153.5 | 152.5 | 152.9 | 151.1 | 150.1 |
| 20 | 17 | 15 | 16 | 23 | 10 | 17 | 20 | 10 | 14 |
| 157.52 | | | | | | | | | |
| | | 157.73 | | | | | | | |
| | | 158.6 | | | | | | | |
| | 160.1 | | | | | | | | |
| | | 158.6 | | | | | | | |
| | | 157.6 | | | | | | | |
| | | 156.8 | | | | | | | |
| | | 156.2 | | | | | | | |
| | | 155.5 | | | | | | | |
| | | 155.9 | | | | | | | |
| | | 153.7 | | | | | | | |
| | | 153.5 | | | | | | | |

161.18
160.69
161.53
161.53

161.18
160.69
161.53
161.53

161.18
160.69
161.53
161.53

16506

+50 40.3 Lt of 1/2 = E4 Picket Fence

+40

+93

TP 1.90 150.44 12.98 148.54

+50 24.5 Lt of 1/2 = My Partner Pole

+31 20' Rt of 1/2 = 11/4 34" Euc Tree

+40 40.4' Lt of 1/2 = My Picket Fence

+92 22.2' Rt of 1/2 = 11/4 18" Euc Tree

+490

151.52

| | | | | | | | | |
|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|--------------------|
| 198.6 | 197.1 | 196.5 | 195.1 | 195.9 | 194.9 | 193.0 | 190.7 | 190.2 |
| $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ |
| 151.5 | 150.3 | 149.6 | 149.1 | 148.7 | 147.9 | 148.5 | 147.9 | 146.8 |
| $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ |
| 155.1 | 152.9 | 151.8 | 151.3 | 150.5 | 150.8 | 149.9 | 148.7 | 148.0 |
| $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | $\frac{1.00}{100}$ |
| 157.57 | 156.59 | | | | | | | |
| $\frac{1.00}{100}$ | $\frac{1.00}{100}$ | | | | | | | |

151.52

6+80

7+10

7+35

+60

8+0

7+30

150.44

| | | | | | |
|--------|-------|-------|-------|-------|-------|
| 6.0/10 | 147.3 | 148.8 | 145.7 | 141.1 | 141.6 |
| 5.5/10 | 147.3 | 148.2 | 145.3 | 140.6 | 140.6 |
| 5.0/10 | 145.3 | 144.5 | 143.3 | 140.6 | 140.0 |
| 4.5/10 | 144.7 | 143.9 | 142.6 | 140.2 | 138.5 |
| 4.0/10 | 146.2 | 145.8 | 141.8 | 139.7 | 138.4 |
| 3.5/10 | 145.0 | 144.4 | 140.0 | 139.1 | 137.8 |
| 3.0/10 | 142.7 | 141.8 | 139.4 | 138.4 | 136.2 |
| 2.5/10 | 139.5 | 139.1 | 135.6 | 134.8 | 135.1 |
| 2.0/10 | 138.7 | 135.3 | 133.6 | 133.6 | 133.9 |

150.44

6+

7+

8+

46

9488.80 = S.L.B.C.

+70

+50

+25

TP 2.57 146.64 6.97 143.47 ^{2.90} 9+0

9+0

8+60

15044

67

8

Rt

47

| | | | | | | | |
|--|-------|-------|-------|-------|-------|-------|-------|
| | 139.0 | 138.0 | 150.0 | 151.8 | 148.6 | 195.3 | 139.0 |
| | 130 | 80 | 50 | 50 | 50 | 50 | 80 |
| | 133.8 | 137.5 | 148.1 | 150.9 | 146.5 | 192.7 | 133.8 |
| | 130 | 50 | 40 | 40 | 40 | 30 | 40 |
| | 133.9 | 140.4 | 147.1 | 149.5 | 146.5 | 191.4 | 133.9 |
| | 130 | 40 | 50 | 30 | 50 | 90 | 80 |
| | 134.8 | 140.7 | 142.3 | 143.2 | 143.3 | 190.1 | 134.8 |
| | 110 | 50 | 90 | 80 | 70 | 100 | 110 |
| | 135.7 | 139.4 | 140.5 | 140.7 | 141.7 | 137.8 | 135.7 |
| | 100 | 30 | 50 | 30 | 80 | 100 | 80 |
| | 133.3 | 137.7 | 137.9 | 137.9 | 137.5 | 137.6 | 133.3 |
| | 120 | 40 | 40 | 40 | 40 | 30 | 40 |
| | 131.5 | 133.6 | 135.4 | 136.2 | 135.6 | 134.8 | 131.5 |
| | 140 | 60 | 80 | 80 | 80 | 150 | 140 |

150.44

11+75

TP 12.71 158.10 0.07 145.39

11+30

11+0

10+80

10+35

TP 12.15 145.46 12.73 133.31

10+17

146.04

077065%
978880
13335
Page 20

385 50%

4.

20

Pt.

48

| | | | | | | | |
|-----|-------|-------|-------|-------|-------|--------|-------|
| 117 | 137.3 | 134.3 | 137.3 | 139.4 | 140.4 | 142.7 | 147.3 |
| 75 | 75 | 75 | 80 | 80 | 80 | 80 | 80 |
| 121 | 133.9 | 134.0 | 133.1 | 139.4 | 140.4 | 142.7 | 147.3 |
| 80 | 80 | 80 | 80 | 80 | 80 | 80 | 80 |
| 125 | 133.5 | 133.1 | 133.1 | 136.8 | 138.4 | 141.8 | 147.7 |
| 80 | 80 | 80 | 80 | 80 | 80 | 80 | 80 |
| 131 | 131.9 | 132.8 | 132.8 | 135.0 | 136.8 | 142.6 | 148.4 |
| 80 | 80 | 80 | 80 | 80 | 80 | 80 | 80 |
| 135 | 130.6 | 132.4 | 132.4 | 133.9 | 137.3 | 143.7 | 149.9 |
| 80 | 80 | 80 | 80 | 80 | 80 | 80 | 80 |
| 139 | 131.0 | 131.6 | 132.7 | 132.7 | 138.3 | 144.0 | 150.9 |
| 80 | 80 | 80 | 80 | 80 | 80 | 80 | 80 |
| 143 | 130.4 | 131.0 | 132.4 | 132.0 | 140.0 | 144.6 | 152.7 |
| 80 | 80 | 80 | 80 | 80 | 80 | 80 | 80 |
| 147 | 130.9 | 129.8 | 133.8 | 133.8 | 142.2 | 146.6 | 153.8 |
| 80 | 80 | 80 | 80 | 80 | 80 | 80 | 80 |
| 151 | 130.0 | 130.0 | 136.2 | 136.2 | 138.1 | 149.10 | |
| 80 | 80 | 80 | 80 | 80 | 80 | 80 | |

146.04

176
80
104
50%

B.M.

5.86

163.75

on 1/2 pipe to
40 ft of
12+37.08

156.4

12+37.08 = E.C. Academy St.

132
60

TP

12.17

169.61

0.66

157.44

12+0

158.10

157.8

148
10

150.2

155.8

138
33

151.3

156.3

133
20

149.8

155.9

137
11

150.4

160.7

89

169.61

153.9

162.6

7
50

155.6

163.6

60
40

157.1

164.9

58
50

157.8

158.10

4+03.73 = PCC

14.5
50

125.5

3+65

TP 12.41 140.03 3.50 127.62

117.0

3+25

14.1
17.0 = Bottom
Start

2+86.95 = P.R.C. on Lt

120.0

2+55.89

117

2+24.84 = B.C. Pt.

131.12

Lt

Rt

Rt

| | | | | | |
|-----------------------|-----------------------|-----------------------|---------------------------|-----------------------|-----------------------|
| 117.5 | 115.1 | 116.0 | 122.4 | 118.5 | 124.5 |
| 14.0 17.0 = Bottom | 14.0 17.0 = Bottom | 15.1 15.1 = Bottom | 15.8 15.8 = Bottom | 15.5 15.5 = Bottom | 15.5 15.5 = Bottom |
| 114.3 | 119.8 | 120.2 | 122.9 | 124.0 | 121.8 |
| 13.0 13.0 = Bottom | 14.5 14.5 = Bottom | 14.9 14.9 = Bottom | 16.0 16.0 = Bottom | 16.0 16.0 = Bottom | 18.2 18.2 = Bottom |
| 119.2 | 120.3 | 121.7 | 122.8 | 124.2 | 119.5 |
| 11.9 11.9 = Bottom | 10.0 10.0 = Bottom | 9.9 9.9 = Bottom | 8.0 8.0 = Bottom | 16.5 16.5 = Bottom | 16.5 16.5 = Bottom |
| 120.9 | 120.6 | 121.8 | 123.6 | 124.6 | 124.2 |
| 11.7 11.7 = Bottom | 10.5 10.5 = Bottom | 9.9 9.9 = Bottom | 7.5 7.5 = Bottom | 7.5 7.5 = Bottom | 15.8 15.8 = Bottom |
| 122.1 | 121.7 | 123.0 | 124.6 | 126.7 | 125.8 |
| 9.0 9.0 = Bottom | 8.1 8.1 = Bottom | 8.1 8.1 = Bottom | 140.03 140.03 = Bottom | 14.2 14.2 = Bottom | 14.2 14.2 = Bottom |
| 125.1 | 123.8 | 124.3 | 127.3 | 132.5 | 132.1 |
| 8.0 8.0 = Bottom | 6.8 6.8 = Bottom | 6.8 6.8 = Bottom | 6.0 6.0 = Bottom | 7.5 7.5 = Bottom | 7.5 7.5 = Bottom |
| 126.2 | 125.3 | 126.0 | 128.8 | 135.6 | 135.5 |
| 8.9 8.9 = Bottom | 7.8 7.8 = Bottom | 7.8 7.8 = Bottom | 7.0 7.0 = Bottom | 4.0 4.0 = Bottom | 4.0 4.0 = Bottom |
| 127.9 | 127.4 | 128.5 | 132.8 | 128.6 | 139.6 |
| 8.5 8.5 = Bottom | 8.0 8.0 = Bottom | 7.4 7.4 = Bottom | 6.7 6.7 = Bottom | 6.4 6.4 = Bottom | 6.0 6.0 = Bottom |
| 129.4 | 128.9 | 129.5 | 132.8 | 128.6 | 139.6 |
| 8.5 8.5 = Bottom | 8.0 8.0 = Bottom | 7.6 7.6 = Bottom | 6.7 6.7 = Bottom | 6.4 6.4 = Bottom | 6.0 6.0 = Bottom |

131.12

5+61.29

TP 11.94 145.24 6.73 133.30

5+24.26

5+10

5+0

4+87.23 = PRC 0741

4+45.48

140.03

0740640R4
9+88.80
Boryest
133.35
P09C40

131/50 126.9

135/50 126.5

141/50 125.9

385 5084

| | | | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 127.9 | 127.2 | 126.8 | 127.3 | 125.0 | 122.4 | 122.2 | 128.2 | 129.7 | 132.0 | 133.6 |
| 127.3 | 127.0 | 127.0 | 126.9 | 122.4 | 127.7 | 129.4 | 131.1 | 131.1 | 132.1 | |
| 126.8 | 127.1 | 122.4 | 122.5 | 126.8 | 129.2 | 131.0 | 133.1 | 133.1 | | |
| 126.7 | 126.4 | 122.1 | 122.3 | 126.3 | 127.0 | 132.1 | 133.7 | 133.7 | | |
| 126.3 | 126.1 | 120.7 | 120.4 | 126.0 | 126.4 | 127.7 | 133.9 | 137.3 | | |
| 126.0 | 126.0 | 126.0 | 126.0 | 126.0 | 126.0 | 126.0 | 126.0 | 126.0 | | |
| 126.4 | 126.4 | 126.4 | 126.4 | 126.4 | 126.4 | 126.4 | 126.4 | 126.4 | | |
| 126.0 | 126.0 | 126.0 | 126.0 | 126.0 | 126.0 | 126.0 | 126.0 | 126.0 | | |
| 127.7 | 127.7 | 127.7 | 127.7 | 127.7 | 127.7 | 127.7 | 127.7 | 127.7 | | |
| 133.9 | 133.9 | 133.9 | 133.9 | 133.9 | 133.9 | 133.9 | 133.9 | 133.9 | | |
| 137.3 | 137.3 | 137.3 | 137.3 | 137.3 | 137.3 | 137.3 | 137.3 | 137.3 | | |

140.03

TP 11.17 165.22 1.05 154.05

7+60

7+30

TP 12.09 155.10 2.23 148.01

6+85

6+46.98

6+20

5+98.31

130.2

15.0
5.0

145.24

Lt.

8

PL

53

| | | | | | | | | | |
|---------------------|---------------------|-------------|------------|------------|------------|------------|------------|------------|------------|
| 128.8 | 130.4 | 130.2 | 136.3 | 143.0 | 147.2 | 148.4 | 150.1 | 151.5 | 153.3 |
| 16.4 25 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 |
| 128.8 | 129.8 | 129.8 | 136.3 | 143.0 | 147.2 | 148.4 | 150.1 | 151.5 | 153.3 |
| 16.4 25 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 |
| 128.8 | 123.0 | 130.2 | 136.3 | 143.0 | 147.2 | 148.4 | 150.1 | 151.5 | 153.3 |
| 16.4 25 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 |
| 125.5 | 121.8 | 130.4 | 136.3 | 143.0 | 147.2 | 148.4 | 150.1 | 151.5 | 153.3 |
| 19.7 3.0 16.7 | 18.1 3.0 15.1 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 | 17.0 15 |
| 126.5 | 129.4 | 133.4 | 141.6 | 146.2 | 146.2 | 146.2 | 150.1 | 151.5 | 153.3 |
| 18.9 | 15.8 | 16.8 | 16.6 | 16.6 | 16.6 | 16.6 | 16.6 | 16.6 | 16.6 |
| 127.0 | 130.0 | 138.7 | 143.6 | 148.6 | 148.6 | 148.6 | 150.1 | 151.5 | 153.3 |
| 18.0 7 | 17.0 15 | 16.5 2.2 | 16.6 | 16.6 | 16.6 | 16.6 | 16.6 | 16.6 | 16.6 |
| 129.0 | 132.6 | 140.6 | 145.2 | 149.9 | 149.9 | 149.9 | 150.1 | 151.5 | 153.3 |
| 16.0 15 | 16.5 15 | 16.5 15 | 16.5 15 | 16.5 15 | 16.5 15 | 16.5 15 | 16.5 15 | 16.5 15 | 16.5 15 |
| 132.3 | 136.5 | 142.6 | 147.7 | 151.4 | 151.4 | 151.4 | 151.4 | 151.4 | 151.4 |
| 15.9 2.5 | 16.5 15 | 16.5 15 | 16.5 15 | 16.5 15 | 16.5 15 | 16.5 15 | 16.5 15 | 16.5 15 | 16.5 15 |
| 137.5 | 141.1 | 147.7 | 151.4 | 151.4 | 151.4 | 151.4 | 151.4 | 151.4 | 151.4 |
| 15.5 10 | 16.5 15 | 16.5 15 | 16.5 15 | 16.5 15 | 16.5 15 | 16.5 15 | 16.5 15 | 16.5 15 | 16.5 15 |

145.24

B.M

151

163.71

opp. P.P. + D.T.
15.8
151.8708
Bery 151
163.73
Page 49

7+9201 = P.C.C.

165.22

~~150.9~~

~~152.1~~

~~154.0~~

~~155.9~~

~~157.3~~

~~159.4~~

165.22

7-17-47

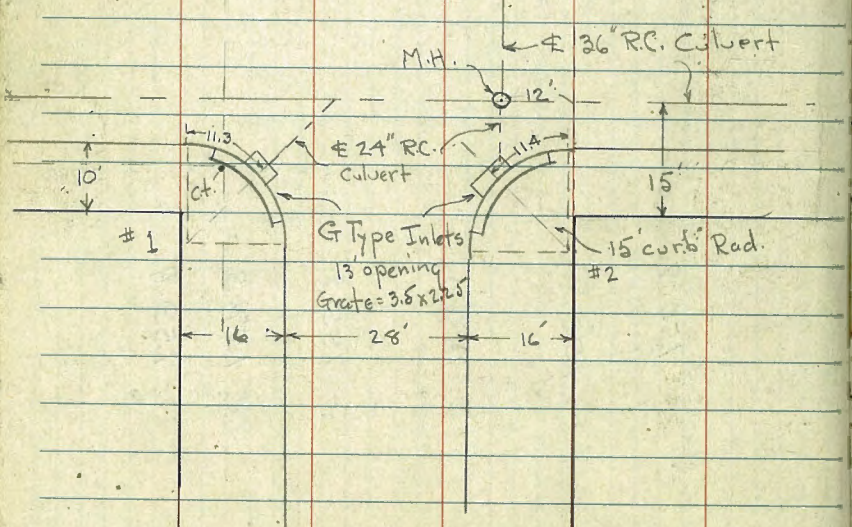
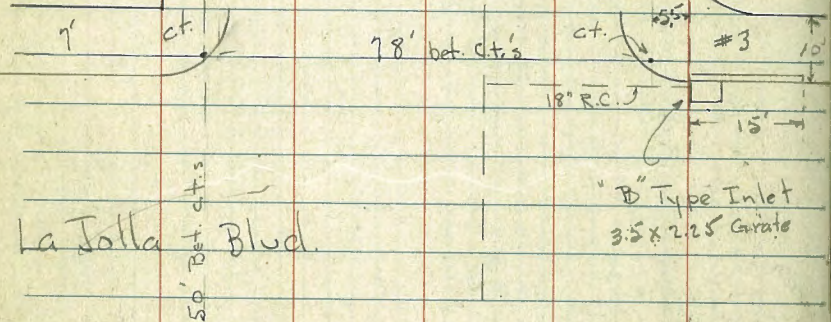
Osborne
Hardin
Smith
Worrell

788

W.O. 252

Fern
Glen

Fern
Glen



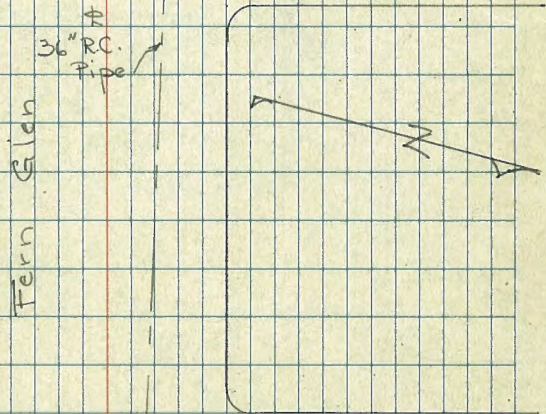
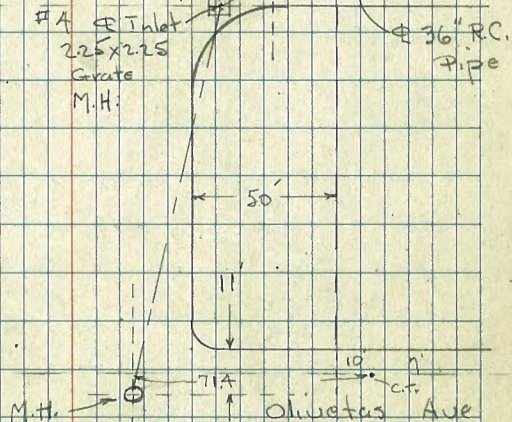
Fern Glen Drain

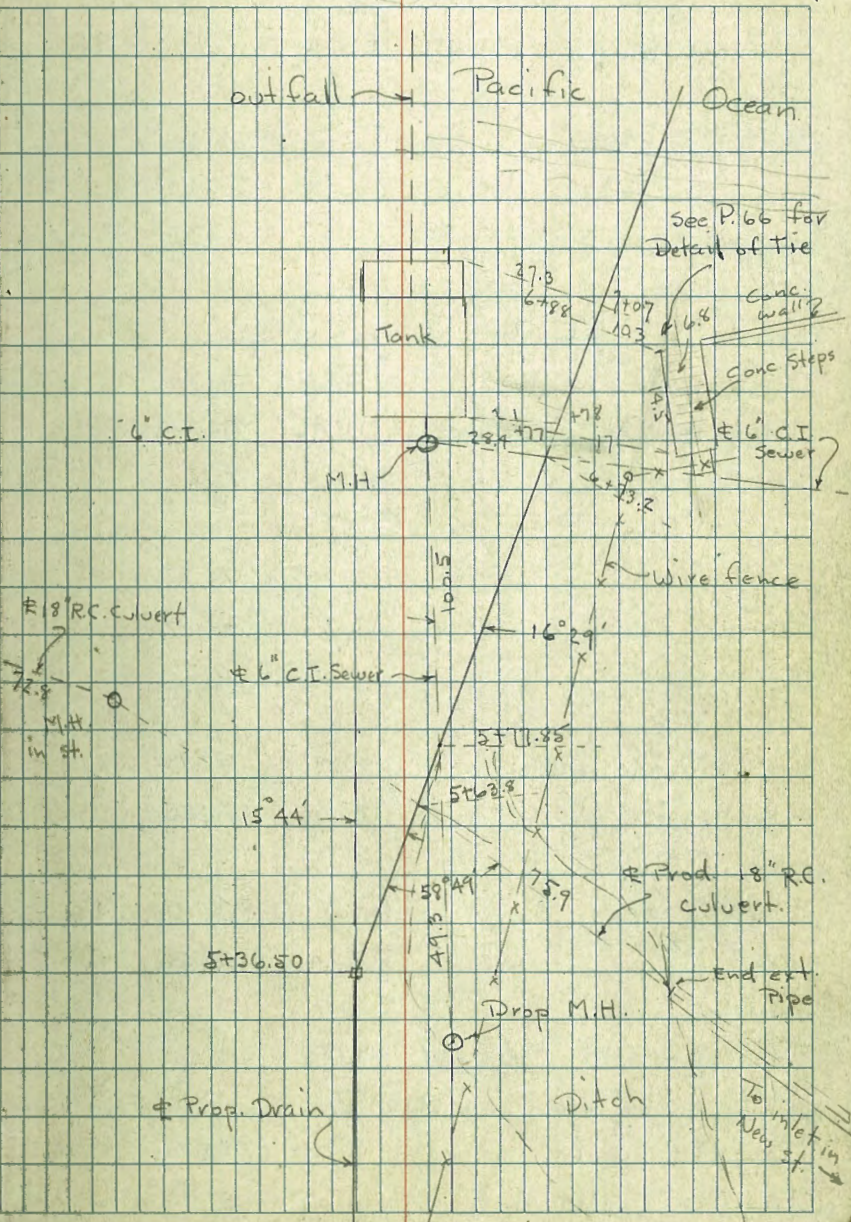
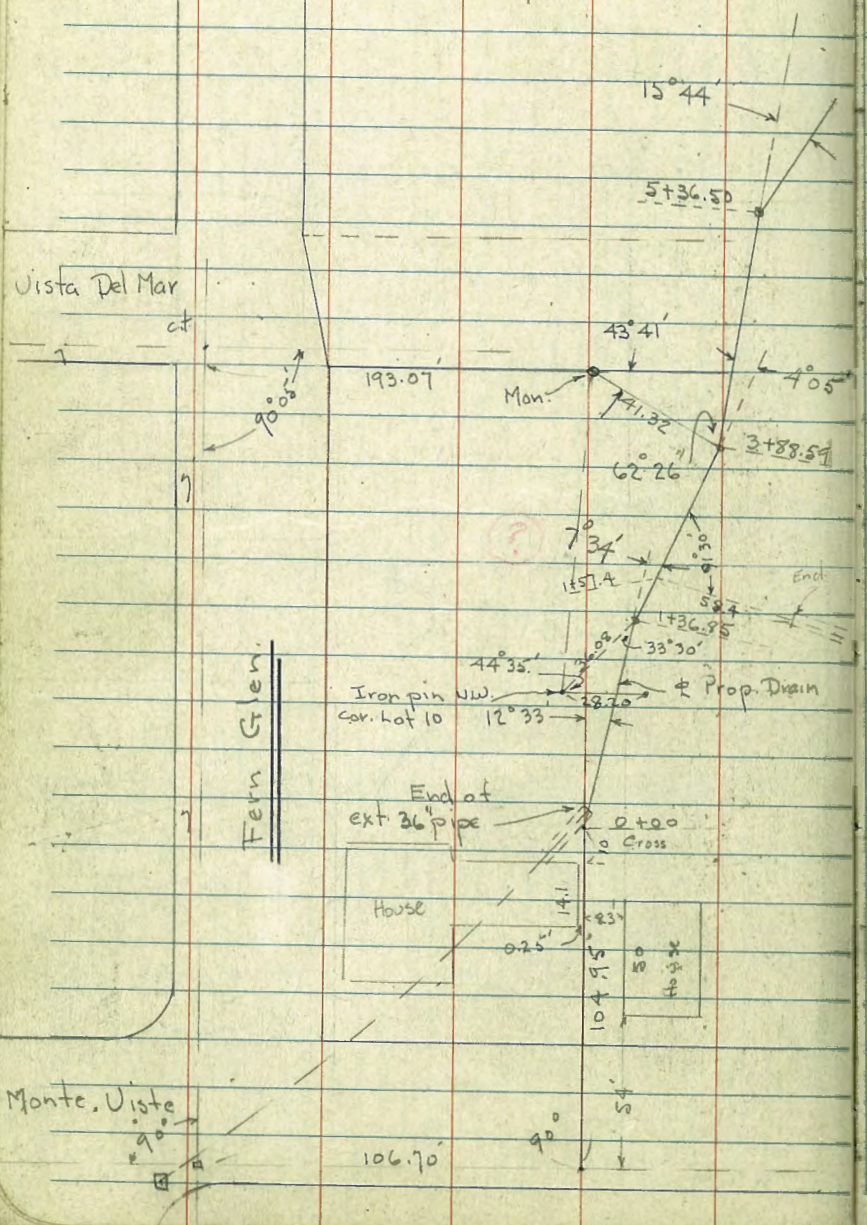
Indexed
C.S.R.

Inlet #5 **55**

Monte Viste

Man





Levels on Flow lines of Inlets and
Culverts at La Jolla Blvd. + Fern Glen.

| | | | | |
|------|-------|---------|-------|-----------------------------------------|
| B.M. | 12.28 | 71.80 ✓ | 59.52 | S.W. B.P. Delvedere + Monte Vista |
| | 3.88 | 75.50 ✓ | 71.62 | |

Inlet #1 - S.E. Cor. G⁺ Type 13' opening
next to cb.

| | | |
|----------------------------|-------|-------|
| Top of Grate at Φ box | 4.60 | 70.90 |
| Flow line 24" Pipe + box | 11.96 | 63.52 |

Inlet #2 - N.E. Cor. G⁺ Type - 13' opening

| | | |
|-----------|-------|-------|
| Top grate | 5.03 | 70.87 |
| F.L. | 12.51 | 62.99 |

Inlet #3

| | | |
|---------------------------|-------|-------|
| Top - Φ Grate at cb. | 5.78 | 69.72 |
| F.L. box + 18" pipe | 13.00 | 62.50 |

Flow line of 36" Pipe to W. in M.H. Near N.E. Cor.

| | | |
|------|-------|-------|
| F.L. | 15.94 | 59.56 |
|------|-------|-------|

I.P. 3.18 65.90 ✓ 12.78 62.72 ✓

M.H. on 36" Drain near N.W. Cor. Olivetas + Fern Glen

| | | |
|----------------------------|-------|-------|
| Top M.H. (2' Below ground) | 6.20 | 59.70 |
| F.L. 36" Pipe + M.H. | 14.07 | 51.83 |

| | | | |
|-------------------------------------------------------|---------|-------|---------|
| T.P. 0.12 | 53.52 ✓ | 12.50 | 53.40 ✓ |
| Inlet #4 - 2.25 x 2.25 Grate over M.H. - at N.E. Cor. | | | |
| Top Grate | | 4.96 | 48.56 |
| Flow line 36" Pipe + M.H. | | 12.22 | 41.30 |
| Inlet #5 at N.W. Cor. | | | |
| Top grate - Φ | | 7.95 | 45.57 |
| F.L. box and 20 x 20" Culvert | | 11.36 | 42.16 |
| T.P. 0.53 | 41.93 ✓ | 12.12 | 41.40 ✓ |

Begin levels on Prop Drain from end
of Existing 36" RC Pipe - W. to Ocean

41.93 - P 57

0+00 = Cross in Conc Slab above end of pipe

⊕ 4.60 37.33

7.7 Rt = ground at House 2.0 39.9

5' Lt. 4.0 37.9

0+03.6 = end pipe

Flow line 10.67 31.26

0.8 Rt. = bot. Limestone 10.6 31.3

3' Rt. 4.4 37.5

8' Rt. 2.0 39.9

2' Lt. = bot. Ditch 10.6 31.3

3' Lt. = Top bank 4.3 37.6

0+13

⊕ in bot. 10.9 31.0

12 Rt. 10.9 31.0

2' Rt. = Top 4.7 37.2

11' Rt. = fence 1.1 40.8

1' Lt. = bot. 10.9 31.0

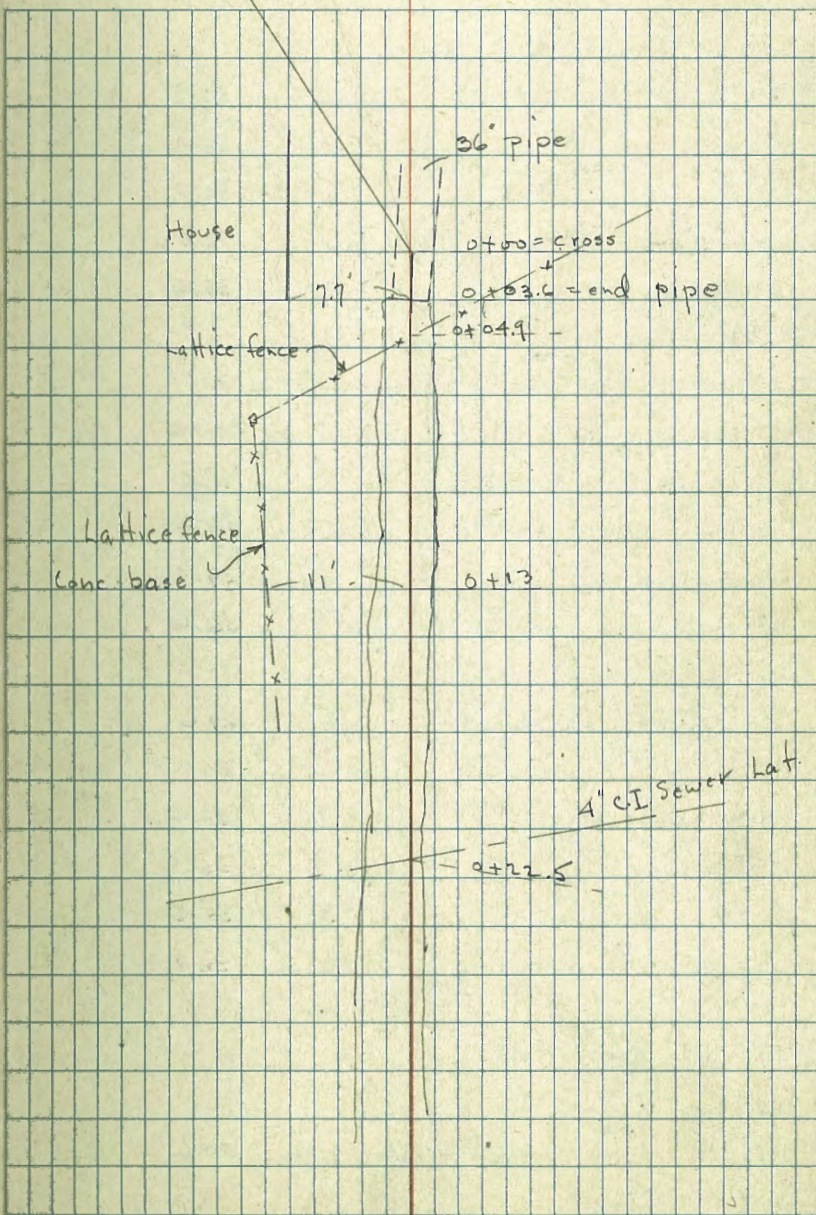
2' " = Top. 5.1 36.8

10 " 4.7 37.2

0+17 = 74 Lt. = ⊕ 2" Lemon.

0+22.5 = ⊕ 4" C.I. Sewer Lat.

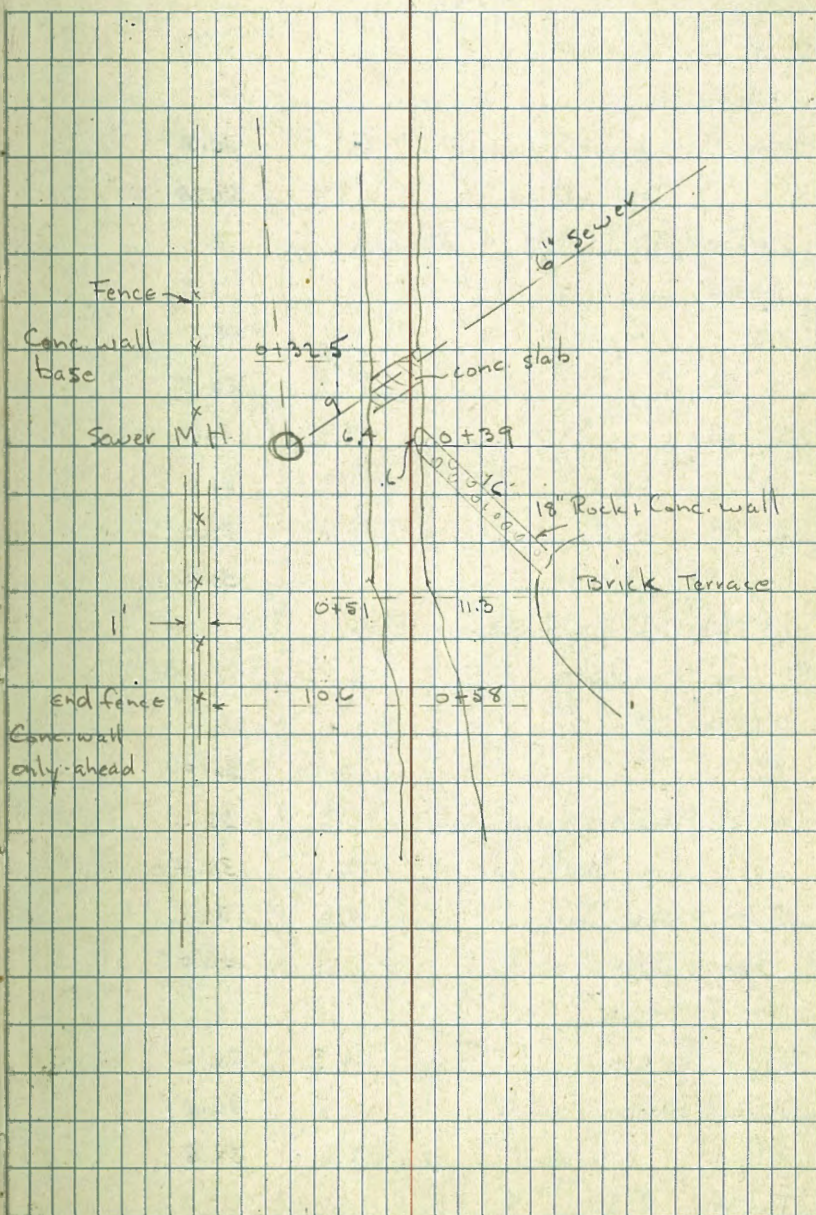
Top pipe 7.66 34.27



41.93

| | | |
|-------------------------------------------|-------|---------|
| 0+25- 56 Lt. = ϕ 3" peach | | |
| ϕ + .5 Lt + 2' Rt = bot. | 11.0 | 30.9 |
| 2' Lt. = top | 5.8 | 36.1 |
| 10' " | 5.5 | 36.2 |
| 3' Rt = Top | 5.6 | 36.3 |
| 10' Rt | 2.3 | 39.6 |
| 0+34- 28 Lt. = ϕ 6" Acacia | | |
| 0+31.5 = ϕ 2.5 Conc. slab over Sewer | | |
| ϕ = Top slab in Ditch | 11.17 | 30.76 |
| 0+39- 64 Rt = ϕ M.H. | | |
| Top | 6.29 | 35.62 |
| Flow line | 12.05 | 29.88 |
| 0.6 Lt. = Top Rock wall | 6.3 | 35.6 |
| 0+46 | | |
| ϕ + 1.5 Rt + 2.5 Lt = bot. ditch | 12.3 | 29.6 |
| 4' Lt. = | 10.2 | 31.7 |
| 9.8 Lt. = base wall | 4.3 | 33.6 |
| Top wall | 6.5 | 35.2 |
| 4' Rt. | 7.3 | 34.6 |
| 10.5 Rt. = at wall | 5.2 | 36.7 |
| T.P. 4.53 40.60 | 5.86 | 36.07 ✓ |
| 0+51 | | |
| 11.3 Lt. = base Brick Terrace | 6.0 | 39.6 |
| " " = Top " " | 3.2 | 37.4 |

59

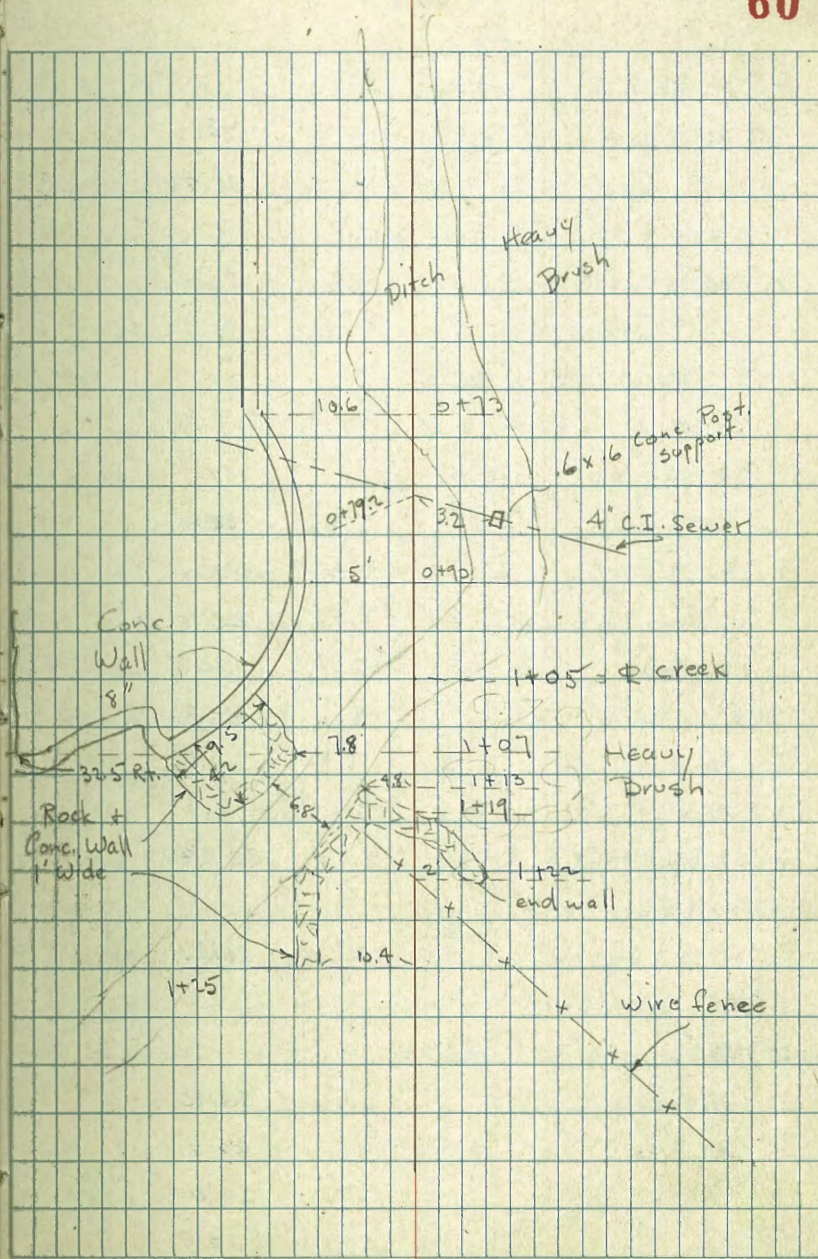


40.60 ✓

| | | | |
|-----------------------------|-------|-------|-------|
| 0+58 | | | |
| 10.6 Rt. = base Conc wall | 5.1 | 35.5 | |
| " " Top wall | 0.82 | 39.78 | |
| 0+64 - 9.9 Lt. = 4" Acacia | | | |
| 0+65 | | | |
| ± | 11.9 | 28.7 | |
| 5' Lt. | 11.9 | 28.7 | |
| 6' Lt. | 9.9 | 30.7 | |
| 10 " | 7.0 | 33.6 | |
| 3' Rt. | 11.6 | 29.0 | |
| 10.4 Rt. at wall | 6.1 | 34.5 | |
| 0+79.2 = 4" C.I. Sewer Lat. | | | |
| ± on top of pipe | 6.22 | 37.38 | |
| 0+90 | | | |
| ± | 10.2 | 30.9 | |
| 6' Lt. = ± Ditch | 14.3 | 26.3 | |
| 18 Lt. = Top bank | 2.2 | 38.9 | |
| 5' Rt. = base wall | 8.0 | 32.6 | |
| " " Top | 0.55 | 40.05 | |
| 1+05 | | | |
| ± = ± Ditch | 14.3 | 26.3 | |
| 10.2 = wall-ground. | 8.5 | 32.1 | |
| 17' Lt. = Top | 2.8 | 37.8 | |
| T.P. 9.54 | 40.81 | 9.33 | 31.27 |

✓ Pipe-lots
10 + 11

60



40.81

| | | | |
|------------------------------------------------|------|-------|---------|
| 1+07 - 7.8 Rt. = Cor. Rock wall | | | |
| 7.8 Rt. = base | 14.6 | 26.2 | |
| " " Top | 7.32 | 33.89 | |
| 1+13 - 4.8 Rt. = Cor Rock Wall | | | |
| 4.8 Rt. = base | 14.8 | 26.0 | |
| " " = Top | 7.10 | 33.71 | |
| 1+14 - 9.5 Lt. = Φ 4" Euc. | | | |
| 1+18 - 6.1 Lt. = Φ 4" Euc. | | | |
| 1+19 = face Rock Wall | | | |
| Φ = Top wall | 5.4 | 35.2 | |
| 9' Lt. = Top | 2.6 | 38.2 | |
| 9' Rt. = Top Rock wall | 8.06 | 32.75 | |
| " " base " | 12.8 | 28.0 | |
| 18' Rt. = Φ Ditch | 15.6 | 25.2 | |
| 30' Rt. | 7.2 | 33.6 | |
| 1+22 - 3' Lt. = Φ 2" Pine | | | |
| 1+22 - 2' Lt. = end Rock wall | 5.17 | 35.62 | Top-end |
| 1+23 - 9.5 Lt. = Φ 3" Pine | | | |
| 1+25 - 10.4 Rt. = end Rock wall | 8.60 | 32.21 | Top. |
| 1+28 - 6.3 Lt. = Φ 2" Pine | | | |
| 1+36.85 = Ang. Pt. 7° 34' Rt. - Sect on split. | | | |
| Φ - on Stub. | 2.66 | 38.15 | |
| 14' Rt. | 6.3 | 34.5 | |
| 18' Rt. = Φ Ditch | 16.2 | 28.6 | |
| 50' Rt. | 5.9 | 34.9 | |

40.81 ✓

61

| | | | |
|------------------------------------------------------------|-------|-------|--|
| 12.2 Lt. = fence | 0.8 | 20.0 | |
| 20' Lt. | +1.0 | 41.8 | |
| 1+57.4 = Int of Φ + Φ Prod. of 18" Drain from N. | | | |
| Φ FL 18" pipe end. | 3.5 | 37.3 | |
| 58.4 Rt. along Φ Prod. = | 11.42 | 29.39 | |
| 1+70 | | | |
| Φ | 3.9 | 36.9 | |
| 10' Lt. | 0.0 | 40.8 | |
| 10' Rt. | 4.9 | 35.9 | |
| 33.4 Rt. = Φ M.H. - Top | 11.65 | 29.16 | |
| 6" Flowline | 20.78 | 20.03 | |
| 46' Rt. = Φ Ditch | 18.6 | 22.2 | |
| 64' Rt. | 6.8 | 39.0 | |
| 2+00 | | | |
| Φ | 4.1 | 30.7 | |
| 22' Lt. | 0.0 | 40.8 | |
| 7' Rt. | 5.4 | 35.2 | |
| 28' Rt. = Φ Ditch | 21.6 | 19.2 | |
| 53' Rt. | 9.2 | 31.6 | |
| 2+20 | | | |
| Φ | 10.2 | 30.6 | |
| 26' Rt. = Φ Ditch | 21.9 | 18.9 | |
| 47' Rt. | 9.4 | 31.2 | |
| 25' Lt. | 1.8 | 39.0 | |

40.81 ✓

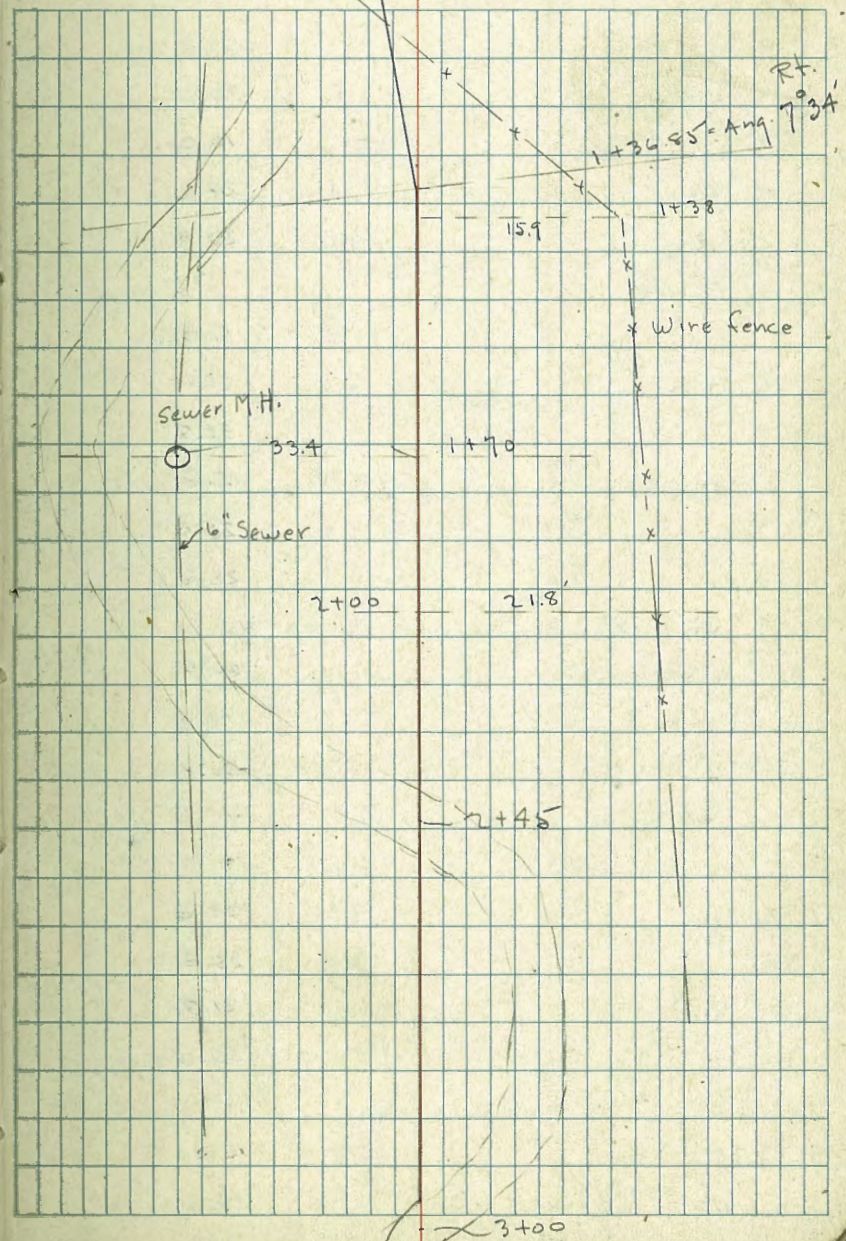
T.P. 2.00 31.55 ✓ 11.26 29.55 ✓

2+45
 ⌘ = ⌘ Ditch 13.1 18.9
 10' Lt. 6.4 25.2
 20' Lt. +2.2 33.8
 20' Rt. 2.1 29.9
 30 " 1.1 30.9
 2+70

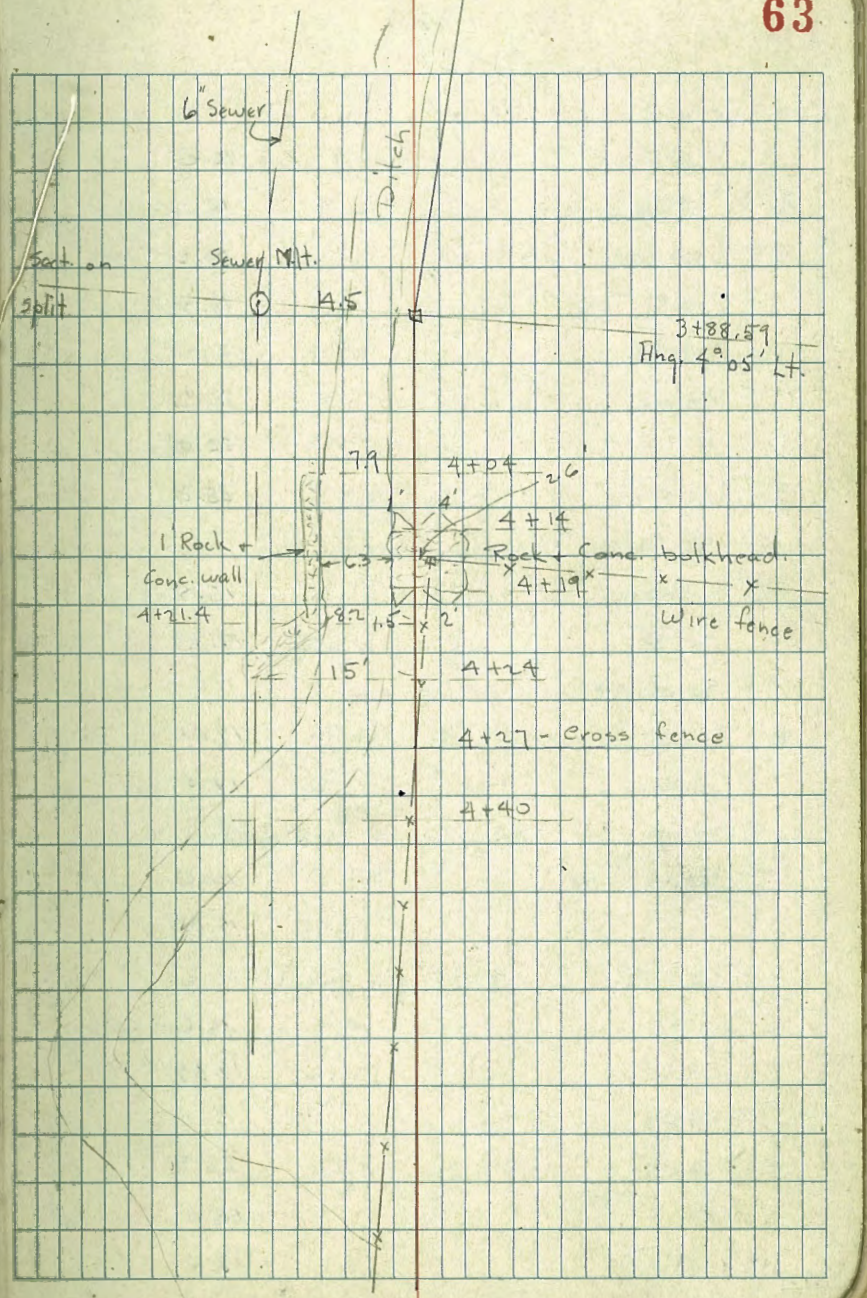
⌘ 7.0 28.6
 12' Lt. = ⌘ Ditch 13.9 17.6
 17' Lt. 9.2 22.9
 40 Lt. +4.0 35.6
 14' Rt. 2.9 28.6
 25 Rt. 2.2 29.9

3+00
 ⌘ = ⌘ Ditch 14.3 17.2
 5 Lt. 11.6 20.0
 13' Lt. 5.0 26.6
 25 +3.9 35.2
 16 Rt. 6.8 28.8
 35 Rt. 2.0 28.6

3+30
 ⌘ 10.7 20.8
 10' Lt. 6.7 28.8



| | | |
|------------------------------------|---------|-------|
| | 31.55 ✓ | |
| 25' Lt. | 1.7 | 29.8 |
| 35 Lt. | + 3.5 | 35.0 |
| 9' Rt. = Φ Ditch | 15.6 | 16.0 |
| 20' Rt. | 7.4 | 29.2 |
| 30' Rt. | 4.1 | 27.9 |
| 3+60 | | |
| Φ | 11.8 | 19.8 |
| 15 Lt. | 5.2 | 26.2 |
| 35 | + 1.9 | 33.2 |
| 7' Rt. = Φ Ditch | 16.0 | 15.6 |
| 23' Rt. | 6.5 | 25.0 |
| 35 | 5.9 | 25.6 |
| 3+88.59 = Ang pt. - Sect. on split | | |
| Φ on Stob. | 14.71 | 16.89 |
| 5' Rt. = Φ Ditch | 17.0 | 19.6 |
| 10' Rt. | 11.2 | 20.2 |
| 14.5 Rt. = Φ M.H. - Top | 9.81 | 21.79 |
| 6" pipe F.L. | 16.58 | 19.97 |
| 20 | 8.9 | 22.6 |
| 35 | 8.0 | 23.6 |
| 10' Lt. | 10.1 | 21.9 |
| 30' Lt. | + 1.7 | 33.2 |
| 4+04 - 7.9 Rt. - end Rock wall | | |
| 7.9 Rt. = base | 15.8 | 15.8 |
| Top wall | 12.5 | 19.0 |



31.55 ✓

| | | |
|--------------------------------------|-------|-------|
| 4+10 | | |
| ± | 14.8 | 16.8 |
| 4' Rt = ± Ditch | 16.3 | 15.2 |
| 7.3 Rt = base wall | 16.3 | 15.2 |
| " " Top " | 12.3 | 19.2 |
| 22 Rt. | 10.4 | 21.2 |
| 35' Rt. | 9.3 | 22.2 |
| 10' Lt. | 9.5 | 22.0 |
| 35' Lt. | +4.2 | 35.8 |
| 4+14 = edge Rock Bulkhead. | | |
| ± = base | 16.2 | 15.9 |
| " " Top | 11.62 | 19.93 |
| 4+19 = edge | | |
| ± = Top Rock | 11.74 | 19.81 |
| " " = base " | 17.2 | 18.8 |
| 4+21.4 = 8.2 Rt. = Ring in Rock wall | | |
| 8.2 Rt. = base wall | 17.0 | 18.6 |
| " " = Top " | 11.75 | 19.80 |
| 4+24 - 15' Rt. = end Rock wall | | |
| 15' Rt. = base | 14.9 | 16.6 |
| " " = Top | 12.16 | 19.39 |
| 4+40 | | |
| ± | 7.8 | 23.8 |
| 10' Rt. | 12.7 | 18.8 |
| 12' Rt. | 18.1 | 13.9 |

31.55 ✓

64

| Pipe - shows in Ditch | | | |
|-------------------------|-------|-------|----------|
| 13.7 Rt = ± 6" CI Sewer | 17.24 | 19.31 | Top pipe |
| 15' Rt. = ± Ditch | 18.0 | 13.6 | |
| 20' Rt. | 15.8 | 15.8 | |
| 35' Rt. | 13.2 | 18.9 | |
| 50' Rt. | 10.6 | 21.0 | |
| 12 Lt. | 2.7 | 28.8 | |
| 30 Lt. | +3.6 | 35.2 | |
| 4+85 | | | |
| ± | 2.5 | 29.0 | |
| 10 Lt. | +0.4 | 32.0 | |
| 25 Lt. | +0.1 | 31.6 | |
| 50 Lt. | +3.6 | 35.2 | |
| 13' Rt. | 10.9 | 20.6 | |
| 25 Rt. | 12.4 | 19.2 | |
| 57 Rt. | 16.4 | 15.2 | |
| 61 = ± Ditch | 21.4 | 10.2 | |
| 77 Rt. | 10.5 | 21.0 | |
| T.P. 116 | 22.71 | 10.00 | 21.55 ✓ |
| 5+10 | | | |
| ± | +1.2 | 23.9 | |
| 5' Lt. | +4.7 | 27.9 | |
| 25 Lt. | +5.9 | 28.6 | |
| 50 Lt. | +8.3 | 31.0 | |

22.71 ✓

| | | |
|---------------------------------------------------------|-------|-------|
| 17' Rt. | 4.3 | 18.9 |
| 30' Rt. | 12.5 | 10.2 |
| 53' Rt. | 12.5 | 10.2 |
| 72' Rt. | 2.9 | 19.8 |
| 5+27-11.8 Rt = ^{Drop.} Φ M.H. - Sec P. 56 | | |
| 11.8 Rt. - Top | 8.30 | 14.91 |
| " " Flow Line from E | 10.80 | 11.91 |
| " " F.L. To W. | 18.30 | 9.91 |
| 5+36.50 = Ang. 15° 44' Rt. - Sect. on Split | | |
| Φ on Stub: | 6.80 | 15.91 |
| 10' Lt. | 0.2 | 22.5 |
| 25' Lt. | +0.7 | 23.9 |
| 50' Lt. | +2.7 | 25.9 |
| 11 Rt. | 14.5 | 8.2 |
| 22' Rt = Wire fence | | |
| 50' Rt | 12.9 | 9.8 |
| 70' Rt. | 3.8 | 18.9 |
| 5+63.8 = Φ 18" RC Culvert - Produced. | | |
| Φ end 18" pipe. | 11.4 | 11.3 |
| 75.9 - Rt along line = F.L. | 12.15 | 10.56 |
| 5+85 | | |
| Φ | 12.7 | 10.0 |
| 10 Lt | 9.1 | 13.6 |
| 40' Lt | 7.5 | 15.2 |
| 6' Rt = Φ Ditch | 19.3 | 3.9 |

22.71 ✓

65

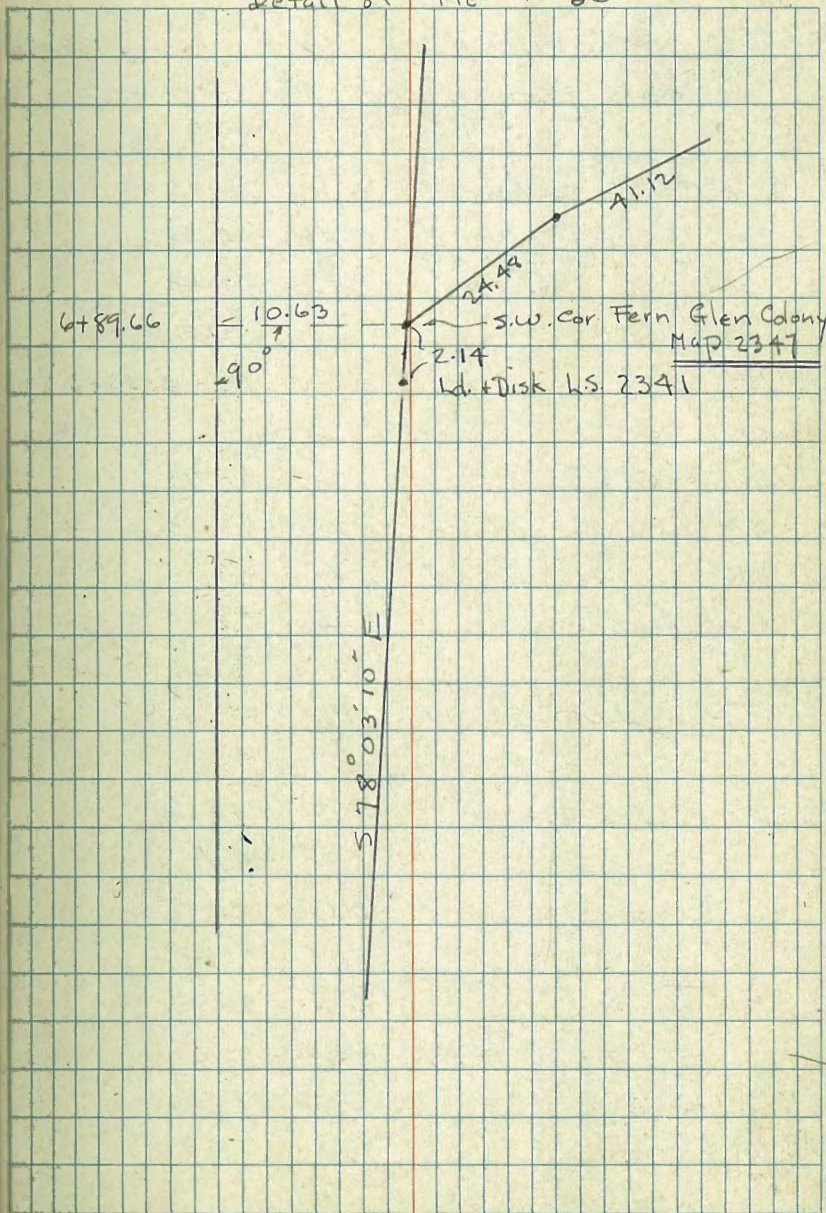
| | | |
|----------------------------------------|------|------|
| 15' Rt. | 11.2 | 11.5 |
| 35' Rt. | 6.5 | 16.2 |
| 50' Rt. | 5.8 | 15.9 |
| 6+10 | | |
| Φ | 23.0 | -0.3 |
| 10 | 11.1 | 11.6 |
| 25 | 8.2 | 14.5 |
| 50' Rt. | 7.3 | 15.9 |
| 4' Lt. | 17.8 | 9.9 |
| 20' Lt. | 11.0 | 11.7 |
| 40' Lt. | 8.6 | 4.1 |
| T.P. 4.75 ✓ <u>14.81</u> 12.65 10.06 ✓ | | |
| 6+50 | | |
| Φ | 13.5 | 1.3 |
| 4' Lt. | 7.3 | 5.5 |
| 15' Lt. | 5.5 | 9.3 |
| 25' Lt. | 3.2 | 11.6 |
| 50' Lt. | 0.7 | 12.1 |
| 7' Rt. | 8.7 | 6.1 |
| 25' Rt. | 2.3 | 12.5 |
| 50' Rt. | 1.5 | 13.3 |
| 6+70 1.4 Rt = Cor. Wire fence | | |

14.81 ✓

| | | | |
|-------------------------------|-------|---------|------------|
| 6+73.2 = Φ 6" C.I. Sewer | 11.16 | 3.65 | Top pipe |
| 284 Lt along the pipe = M.H. | | | |
| Top. | 7.87 | 6.92 | |
| Flow line | 11.90 | 2.91 | |
| 6+77-17' Rt = Cor. steps | 4.75 | 10.06 | Top |
| 6+78-21 Lt = Cor. Tank | 10.21 | 4.60 | Top |
| 6+88-10.3 Rt = Cor. steps | 7.92 | 6.89 | Top |
| 6+90 | | | |
| Φ RT | 13.8 | 1.0 | |
| 11.7 = Bottom step | 9.01 | 5.80 | |
| 18.1 RT = Top Ret. wall | -7.33 | 7.28 | |
| 40 RT. | 6.6 | 8.2 | |
| 10' Lt. | 11.6 | 3.2 | |
| 23.4 = edge Tank - Top | 10.26 | 2.55 | |
| 7+07-27.3 Lt = Cor. Tank | 10.29 | 2.52 | |
| 7+15 | | | |
| Φ - in Sand = end | 16.4 | -1.6 | |
| T.P. | 13.27 | 58.02 ✓ | 0.06 14.75 |
| | 12.32 | 40.33 ✓ | 0.01 28.01 |
| | 11.91 | 52.03 ✓ | 0.21 40.12 |
| | 9.45 | 61.08 ✓ | 0.40 51.63 |
| Check starting B.M. | 1.58 | 59.50 ✓ | 59.52 ✓ |

Notes Reduced 2-25-47

Detail of Tie P 56



6+89.66

10.63

90°

21.44
21.12
S.W. Cor Fern Glen Coony
Map 2347
2.14
Ld. + Disk W.S. 2341

578° 03' 10" E

Walter
Handicks
Baker
Johnson
4-24-47

Cross Section 15' Alley Blk. 4

Ocean Villa Tract

Between Sapphire Tourmaline
from Mission Blvd. R.R. Pt. of Way Lane

B.M. on Conc. Alon
600' West of Mission
on 11th Turnwise st 921 103.73

| | | | | |
|------------------------|------|-------|-------|--------------|
| TP #1 | 5.73 | 98.06 | 11.40 | 92.33 |
| chk curb NW Tourmaline | | 7.93 | | 90.13 |
| | | | | 89.09 Record |
| | | | | 1.13 diff. |
| TP #2 | | | 7.89 | 90.17 |

B.M. F.I.E. B.P.
Beryl St
+ Mission Blvd 11.02 71.77 60.75

| | | | | |
|-----------------|-------|-------|------|--------------------|
| TP | 11.56 | 82.61 | 0.72 | 71.05 |
| TP | 12.05 | 94.24 | 0.42 | 82.19 |
| chk Above TP #2 | | 5.14 | | 89.10 89.12 = P-71 |
| | | | | 20.17 |
| | | | | 4.07 |

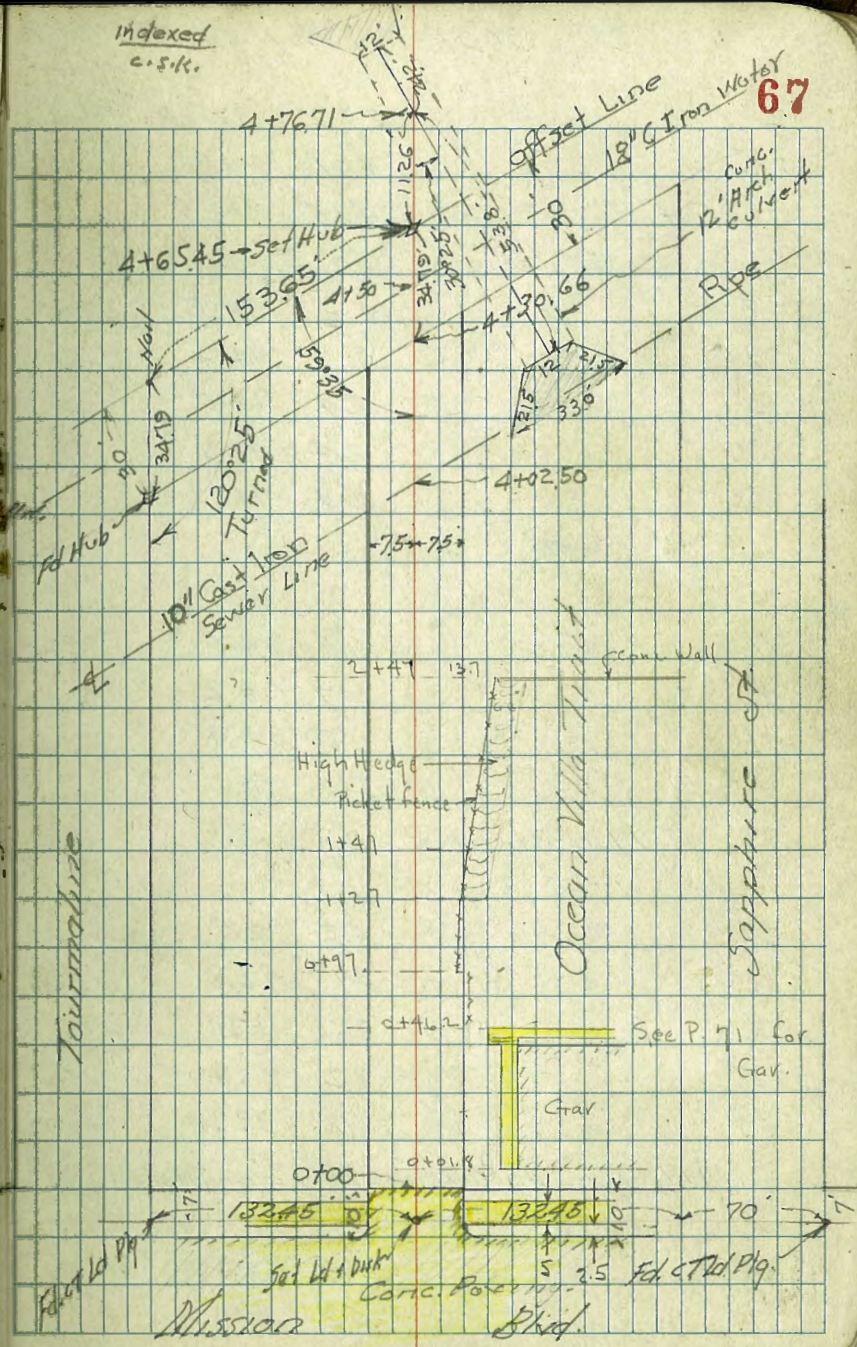
TP 416 76.91 1.42 92.75
0-10' West of Line Mission Blvd

| | | |
|-------------------------|------|-------|
| 5-3' = 80 3' cb R on cb | 4.17 | 92.74 |
| " " on Gut | 4.80 | 92.11 |
| L on Conc | 4.52 | 92.39 |
| +10.5' = 80 cb | 3.56 | 93.36 |
| " on Gut | 4.18 | 92.73 |

0+00 = W.P. Mission Blvd.
N.L. on cb 3.55 93.36
" " Gut 3.67 93.24

Cont. P-68

Indexed
c.s.k.



67

See P. 71 for
Gar.

Mission Blvd

Blvd

96.91

Alley Bk. A

| | | | |
|--------|-----|-------|------------------------------------------|
| Σ | 422 | 92.69 | New elev. for changed gravel Dr. + |
| SL. cb | 401 | 92.90 | gravel Grav. |
| + Gut. | 415 | 92.76 | |

0+15

| | | | |
|--------------------------------|-----|------|------|
| -5 | 2.6 | 94.3 | 93.8 |
| SL. Checked Sections | 2.3 | 94.6 | 93.7 |
| Σ No Change | 2.4 | 94.5 | 93.9 |
| SL. after 0+50 | 2.4 | 94.5 | 94.1 |
| N/G 7.0 4-9-48 | 2.4 | 94.5 | 94.1 |
| +5 | 2.4 | 94.5 | |
| 0+50 See P. 71. for 0+50 sect. | | | |

| | | | |
|----|-----|------|------|
| -5 | 1.9 | 95.0 | |
| N | 2.1 | 94.8 | |
| Σ | 2.7 | 94.2 | 94.6 |
| SL | 2.5 | 94.4 | |
| +5 | 2.8 | 94.1 | |

0+97 = Pole on 4 0.8' in Alley

1+00

| | | | |
|----|-----|------|--|
| -5 | 4.3 | 92.6 | |
| SL | 4.1 | 92.8 | |
| Σ | 3.8 | 93.1 | |
| N | 3.2 | 93.7 | |
| +5 | 3.2 | 93.7 | |

0+17 = Pole Anchor on 4 1.2' in Alley

1+50

| | | | |
|-----|-----|------|--|
| N-5 | 4.8 | 92.1 | |
| N | 4.8 | 92.1 | |

96.91

Chc

68

1+50

| | | | |
|----|-----|------|--|
| Σ | 4.9 | 92.0 | |
| SL | 5.1 | 91.8 | |
| +5 | 5.4 | 91.5 | |

0+97 to 1+50 Fence on N of 1st Alley

2+00

| | | | |
|----|-----|------|--|
| -5 | 7.3 | 89.6 | |
| Σ | 7.3 | 89.6 | |
| Σ | 7.6 | 89.3 | |
| N | 7.0 | 89.9 | |
| +5 | 6.8 | 90.1 | |

2+50

| | | | |
|----|-----|------|--|
| -5 | 8.1 | 88.5 | |
| N | 8.5 | 88.4 | |
| Σ | 8.9 | 88.0 | |
| Σ | 8.8 | 88.1 | |
| +5 | 9.1 | 87.8 | |

3+00

| | | | |
|----|------|------|--|
| -5 | 10.4 | 86.5 | |
| Σ | 10.1 | 86.8 | |
| Σ | 9.9 | 87.0 | |
| N | 9.6 | 87.3 | |
| +5 | 9.5 | 87.4 | |

TR 0.93 87.371047 86.44

3+17

| | | | |
|----|-----|------|--|
| -5 | 0.4 | 87.0 | |
| N | 0.5 | 86.9 | |

87.37 Alley Blk. 4

| | | | |
|---------------------|------|------|-------|
| L | 3+17 | 07 | 86.7 |
| SL | | 1.0 | 86.4 |
| +5 | | 1.1 | 86.3 |
| 3+22 = L Sewer M.H. | | | |
| on L Run | | 0.93 | 86.44 |
| 3+29 | | | |
| -5 | | 2.0 | 85.4 |
| SL | | 2.2 | 85.2 |
| L | | 2.6 | 84.8 |
| N | | 5.9 | 81.5 |
| +20 | | 7.0 | 80.4 |
| 3+39 | | | |
| -30 | | 14.0 | 83.4 |
| -8 | | 13.8 | 83.6 |
| NL | | 11.4 | 76.0 |
| L | | 7.8 | 79.6 |
| SL | | 3.4 | 84.0 |
| +10 | | 2.8 | 84.6 |
| 3+59 | | | |
| -10' | | 2.7 | 84.7 |
| -18' | | 6.5 | 80.9 |
| -10 | | 12.6 | 74.8 |
| SL | | 15.3 | 72.1 |
| L | | 17.8 | 69.6 |
| N | | 20.0 | 67.4 |
| +16 | | 21.9 | 66.1 |
| +41 | | 20.6 | 66.8 |

8737

69

| | | | |
|----------------------------------------|--|------|------|
| 3+70 | | | |
| -42' | | 26.0 | 61.4 |
| -21 | | 24.0 | 63.4 |
| N | | 20.8 | 66.6 |
| L | | 19.6 | 67.8 |
| SL | | 18.6 | 68.8 |
| +16 | | 13.8 | 73.6 |
| +29 | | 5.7 | 81.7 |
| +40 | | 4.0 | 83.4 |
| 4+02.5 = Int. 10" Cast Iron Sewer | | | |
| -37 | | 4.4 | 83.0 |
| -32 | | 4.9 | 82.5 |
| -3 | | 32.3 | 65.1 |
| SL | | 23.4 | 64.0 |
| L Ground | | 25.0 | 63.4 |
| L on Top 10" Sewer | | 17.4 | 70.0 |
| NL | | 25.9 | 61.5 |
| +27 | | 28.4 | 59.0 |
| +37 | | 30.2 | 57.2 |
| +50 in Channel | | 31.2 | 56.2 |
| East Wing Walls 12' x 13' Arch Culvert | | | |
| SE Top Wing Wall | | 28.5 | 59.9 |
| " Lip Conc. Apron | | 32.0 | 55.4 |
| NE Top Wing Wall | | 28.5 | 59.9 |
| " Lip Conc. Apron | | 32.0 | 55.4 |

87.37

Alley Bk 4

+47

306

4+30.31

| | | | |
|-----------------|------|------|------------------------|
| 27.24 | 164 | 71.0 | 12' x 13' Arch Culvert |
| " " " " " Flory | 32.7 | 54.7 | 12' x 13' Arch Culvert |
| N-12 | 20.3 | 67.1 | |
| NL | 19.0 | 68.4 | |
| L | 16.0 | 71.4 | |
| SL | 15.5 | 71.9 | |
| +16 | 10.7 | 76.7 | |
| +27 | 7.8 | 79.6 | |
| +42 | 6.3 | 81.1 | |

4+20

| | | | |
|-----|------|------|--|
| -30 | 5.0 | 82.4 | |
| SL | 24.5 | 62.9 | |
| L | 24.5 | 62.9 | |
| +20 | 26.5 | 60.9 | |

4+30.66

diag Section

| | | | |
|-------|------|------|--|
| -43 | 6.8 | 80.6 | |
| -28 | 6.9 | 80.5 | |
| -22 | 14A | 73.0 | |
| SL-13 | 15.9 | 71.5 | |
| SL | 16.0 | 71.4 | |
| L | 15.8 | 71.6 | |
| NL | 15.0 | 72.4 | |
| +26 | 18.1 | 69.3 | |
| +43 | 17.2 | 70.2 | |

87.37

70

4+50 Int. 18" Cl. Iron Water Main

diag Sec

| | | | |
|----------------|------|------|--|
| -43 | 6.9 | 80.5 | |
| -26 | 5.7 | 81.7 | |
| -11 | 10.5 | 76.9 | |
| N | 9.8 | 77.6 | |
| L | 10.8 | 76.6 | |
| SL | 11.0 | 76.4 | |
| +A on Top Pipe | 11.4 | 76.0 | |
| +14 " Top Pipe | 11.0 | 76.4 | |
| +20 | 10.8 | 76.6 | |
| +24 | 6.8 | 80.6 | |

4+58 diag Sec.

| | | | |
|-----|-----|------|--|
| -43 | 5.3 | 82.1 | |
| SL | 5.0 | 82.4 | |
| L | 4.9 | 82.5 | |
| N | 4.7 | 82.7 | |
| +20 | 3.0 | 84.4 | |

4+65.45 diag Section

| | | | |
|----------|------|-------|--|
| -20 | 4.1 | 83.3 | |
| N | 4.0 | 83.4 | |
| L on Hub | 5.14 | 82.23 | |
| S | 5.0 | 82.4 | |
| +20 | 5.1 | 82.3 | |

Cont p 71

8737 Alley Blk. 4

TP 11.53 96.69 2.21 85.16

chk B.M. Conc. Mon } 3.22 93.47
 600' West Mission Blvd }
 on N.E. Turquoise } 94.52
 +.05

No doubt this Mon is not the one shown in
 Bench Books This Particular Mon. should be
 THIS E. lev.

2.21 102.68

94.52 B.M. Starting
 93.47 Mon

TP #1 5.73 97.01 11.40 91.28

chk. N.W. Mission + Tourmaline 7.93 89.08

89.00 Profile
 0.08 Record

TP #2 Tack to Pk. N.E. Tourmaline
 W.T. Line Mission 7.89 89.12

0 + 35 = extra Sect for yardage
 Conc. Block wall

2 + 47 = 13.7 Rt. = end fence + Hedge at N + S

1 + 47 = 7.7 Rt = Pk in fence line

1 + 27 = 7.7 Rt = fence - Beg. Large Hedge behind fence

0 + 97 = 8' Rt = end board + 6.4 Rt = Beg. Picket fence

0 + 47.3 = 8' Rt = Beg. Board fence

0 + 46.2 = 11.7 Rt = end steps + Conc. walk to N.

0 + 42 = 11.7 Rt = Beg. 3.2 Conc. steps along Gar.

0 + 42 = 13.3 Rt = end Conc. Apron

0 + 01.8 = 13.3 Rt = Beg. Conc. Apron to 4 Car Gar - Conc. floor
 I.P. # 2

B.M. 9.78 98.88 89.10

Add. Notes on Imp. in Alley Blk 4 See P. 67

| | | | |
|-------|-------|--------------|-----------|
| 94.18 | 94.08 | 94.18 | 94.13 |
| 4.5 | 4.8 | 4.7 | 4.75 |
| 13.3 | 13.3 | 13.3 | 13.3 |
| | | | Apron |
| | | 95.38 | 95.67 |
| | | 3.50 | 3.21 |
| | | 11.7 | 11.7 |
| | | Steps + Walk | Walk |
| | | 94.11 | 94.29 |
| | | 4.77 | 4.64 |
| | | 13.3 | 13.3 |
| | | Top apron | floor |
| | | 94.09 | 94.25 |
| | | 4.81 | 4.63 |
| | | 13.3 | 13.3 |
| | | Car apron | floor |
| | | 98.88 | 97.65 |
| | | | 4.23 |
| | | | Car steps |

X-Sect. 15' Alley in Block A - Resub.

Pt. Loma Hts. - Map 1523

See P. 24 for Sketch

12-30-47

7.0

w.o. 25001

0+96-8.1 Rt. = Ely. P. pole # A 2075

0+70

0+60.5-7.5' Lt. = Beq. Lattice fence

T.P. 10.82 117.83 0.93 107.01

0+40

0+10

0+00 = S.L. Tennyson - edge A.C. Pavc

0-10 = S. cb. Tennyson

12.19 107.94

95.75

NW 8P
Tennyson
+
Hick
P. 8

Lt. = E.

⊙

Rt. = W.

72

INDEXED
JAN 28 1948

| | | | |
|--------|--------|--------|--------|
| 107.6 | 108.3 | 109.0 | 109.7 |
| 107.6 | 108.3 | 109.0 | 109.7 |
| 105.9 | 106.0 | 106.8 | 107.2 |
| 104.2 | 103.2 | 103.5 | 104.7 |
| 104.0 | 103.2 | 103.5 | 104.7 |
| 102.18 | 102.12 | 102.53 | 102.89 |
| 100.49 | 101.81 | 102.09 | 102.75 |
| 102.10 | 101.57 | 102.09 | 102.75 |
| 101.81 | 101.3 | 102.09 | 102.75 |
| 107.94 | 107.94 | 107.94 | 107.94 |

Lt.

±

Rt.

73

2+43.5 = Back edge of walk

2+41.91 = ± + N.L. Alicia

2+32.1 = E.L. Alley + N.L. Alicia

T.P. 6.48 123.34 0.97 116.86

2+20

1+80

1+77-6.8 Lt. = ± 4" Euc. Tree

1+40

Normal to Alicia - Dr. to Alicia

1+29.5 - 10.5 Lt. = Near Cor. Doub. Gar. - Conc. floor

1+28 - 7.5 Lt. = Beg. Lath fence

1+00 - 7.5 Lt. = end fence

| | | | | | | | |
|------|-----------|------------|-----------|--------|-------|-------|-------|
| | | | | | 6.18 | | |
| | 115.3 | 116.10 | 116.55 | 116.99 | 117.0 | 117.8 | 118.7 |
| 8.0 | 7.24 | 6.79 | 6.35 | 6.3 | 5.5 | 4.6 | |
| 12.6 | 12.6 | 7.5 | 1.5 | 6.3 | 7.5 | 1.5 | |
| | Top | outside of | edge walk | | | | |
| | of | walk | | | | | |
| | of | end of | | | | | |
| | 114.19 | 116.18 | 116.2 | 116.8 | 117.4 | 118.2 | |
| 9.15 | 7.26 | 7.1 | 6.5 | 5.9 | 5.1 | | |
| 33.8 | 8.8 | 1.5 | 7.5 | 1.5 | | | |
| | 1.5 along | edge | | | | | |
| | walk from | walk | | | | | |
| | here | | | | | | |
| | | 115.3 | 116.2 | 123.34 | | | |
| | | 2.5 | 1.5 | 116.5 | 0.170 | 0.178 | |
| | | 116.5 | 115.1 | 115.2 | 1.57 | 116.2 | |
| | | 3.3 | 2.1 | 2.6 | 2.1 | 1.6 | |
| | | 1.5 | 1.4 | 1.7 | 1.9 | 1.3.5 | |
| | | 111.5 | 112.6 | 112.7 | 112.9 | 113.5 | |
| | | 6 | 5.2 | 5.1 | 4.9 | 4.3 | |
| | | 111.69 | 112.6 | 112.7 | 112.9 | 113.5 | |
| | | 6.19 | 5.2 | 5.1 | 4.9 | 4.3 | |
| | | floor | 5.2 | 5.1 | 4.9 | 4.3 | |
| | | | 110.9 | 110.3 | 110.9 | 111.1 | |
| | | | 7.9 | 7.5 | 7.5 | 6.7 | |
| | | | 5.5 | 7.5 | 7.5 | 5.7 | |
| | | | | 117.83 | | | |

Lt. # Rt.

N.W. Mon - Wells + Alicia

✓ P-11 ✓
 4.42 124.73 124.74
 T.P. 8.63 129.15 2.82 120.52

See P. 10 for Alicia Sections.

2+66.76 = opp. pt. of 1' Rad. Ret. on Rt.

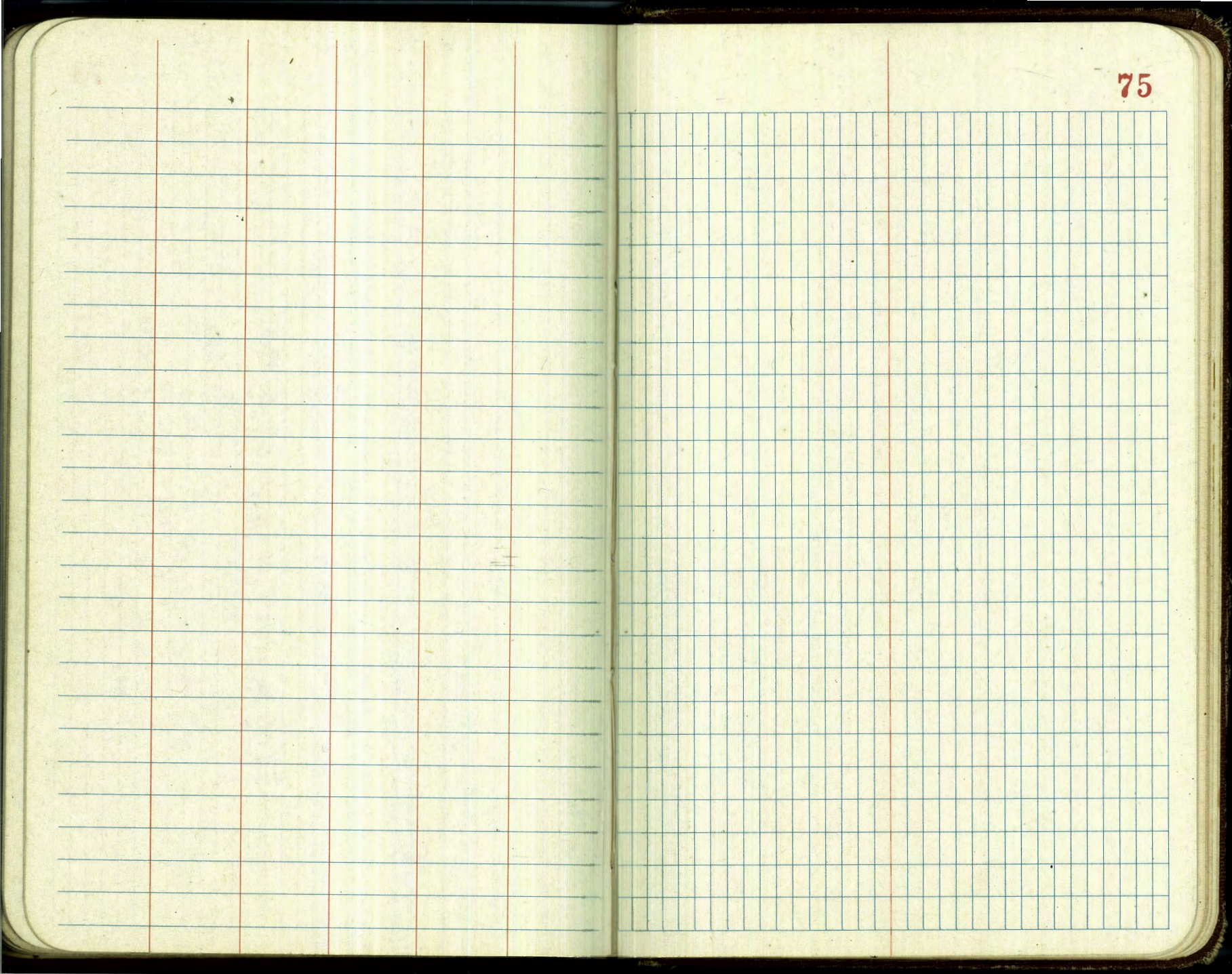
walk
 2+60.76 = opp end of Ret. on Rt. at edge of

outside of walk
 2+51.76 = W.L. Alley + N.L. Alicia - also # +

2+46.5 = opp. pt. of 2' Rad. Ret on Lt.

| | | | | | | |
|--|--------------------|------------------------------------|---------------------------|----------------------------------|---------------------------------|---------------------|
| | 116.2 | 116.7 | 117.3 | 118.72 | 119.28 | 120.8 |
| | 7.1 1.5 | 6.6 1.5 | 6.0 in gut | 4.62 1.5 end Ret + walk | 4.06 15.4 Back of walk | 2.51 2.5 gut. |
| | 115.8 | 118.2 | 117.61 | 118.06 | 118.1 | 119.1 |
| | 7.5 1.5 | 7.1 1.5 gut | 5.73 edge walk | 5.28 6.3 Back edge walk | 5.2 1.5 | 4.2 1.5 |
| | 114.77 | 113.9 | 116.1 | 116.8 | | |
| | 8.57 2.5 Top | 9.4 2.5 # along gut. Here | 7.2 1.5 gut on Ret. | 6.66 1.5 | | |
| | | | | | | 123.34 |

4.20
7.5
Top
1' Rad.
gut
Cb. from
Here



385 50%

A table with 5 columns and 20 rows. The columns are defined by vertical red lines, and the rows are defined by horizontal blue lines. The table is currently empty.

A table with 1 column and 20 rows. The column is defined by a vertical red line, and the rows are defined by horizontal blue lines. The table is currently empty.

A ledger page with 6 vertical red lines and 25 horizontal blue lines. The lines create 5 columns of varying widths. The columns from left to right are approximately: 1/3 of the page width, 1/3, 1/3, 1/3, and 1/3. The page is otherwise blank.

A ledger page with 1 vertical red line and a 20x20 grid of blue lines. The red line is positioned approximately 1/3 of the way from the left edge. The grid covers the remaining two-thirds of the page. The page is otherwise blank.

IMPROVED TABLES AND INFORMATION

HORIZONTAL STADIA CORRECTIONS

| | | |
|----------------|----------------|----------------|
| 2°-00' — 0.1 | 21°-00' — 12.8 | 33°-00' — 29.7 |
| 3°-00' — 0.3 | 21°-30' — 13.4 | 33°-15' — 30.1 |
| 4°-00' — 0.5 | 22°-00' — 14.0 | 33°-30' — 30.5 |
| 5°-00' — 0.8 | 22°-30' — 14.7 | 33°-45' — 30.9 |
| 6°-00' — 1.1 | 23°-00' — 15.3 | 34°-00' — 31.3 |
| 7°-00' — 1.5 | 23°-30' — 15.9 | 34°-15' — 31.7 |
| 8°-00' — 1.9 | 24°-00' — 16.5 | 34°-30' — 32.1 |
| 9°-00' — 2.5 | 24°-30' — 17.2 | 34°-45' — 32.5 |
| 10°-00' — 3.0 | 25°-00' — 17.9 | 35°-00' — 32.9 |
| 10°-30' — 3.3 | 25°-30' — 18.6 | 35°-15' — 33.3 |
| 11°-00' — 3.6 | 26°-00' — 19.2 | 35°-30' — 33.7 |
| 11°-30' — 4.0 | 26°-30' — 19.9 | 35°-45' — 34.1 |
| 12°-00' — 4.3 | 27°-00' — 20.6 | 36°-00' — 34.6 |
| 12°-30' — 4.7 | 27°-30' — 21.3 | 36°-15' — 35.0 |
| 13°-00' — 5.1 | 28°-00' — 22.0 | 36°-30' — 35.4 |
| 13°-30' — 5.5 | 28°-30' — 22.8 | 36°-45' — 35.8 |
| 14°-00' — 5.9 | 29°-00' — 23.5 | 37°-00' — 36.2 |
| 14°-30' — 6.3 | 29°-30' — 24.3 | 37°-15' — 36.6 |
| 15°-00' — 6.7 | 30°-00' — 25.0 | 37°-30' — 37.1 |
| 15°-30' — 7.2 | 30°-15' — 25.4 | 37°-45' — 37.5 |
| 16°-00' — 7.6 | 30°-30' — 25.8 | 38°-00' — 37.9 |
| 16°-30' — 8.1 | 30°-45' — 26.2 | 38°-15' — 38.3 |
| 17°-00' — 8.5 | 31°-00' — 26.5 | 38°-30' — 38.7 |
| 17°-30' — 9.0 | 31°-15' — 26.9 | 38°-45' — 39.1 |
| 18°-00' — 9.5 | 31°-30' — 27.3 | 39°-00' — 39.6 |
| 18°-30' — 10.1 | 31°-45' — 27.7 | 39°-15' — 40.0 |
| 19°-00' — 10.6 | 32°-00' — 28.1 | 39°-30' — 40.5 |
| 19°-30' — 11.2 | 32°-15' — 28.5 | |
| 20°-00' — 11.7 | 32°-30' — 28.9 | |
| 20°-30' — 12.3 | 32°-45' — 29.3 | |

Chains to Feet

| | |
|----------|-----|
| 1 | 66 |
| 2 | 132 |
| 3 | 198 |
| 4 | 264 |
| 5 | 330 |
| 6 | 396 |
| 7 | 462 |
| 8 | 528 |
| 9 | 594 |
| 10 | 660 |

Feet to Chains

| | |
|------------|--------|
| 100 | 1.515 |
| 200 | 3.030 |
| 300 | 4.545 |
| 400 | 6.060 |
| 500 | 7.575 |
| 600 | 9.090 |
| 700 | 10.606 |
| 800 | 12.121 |
| 900 | 13.636 |
| 1,000 | 15.151 |

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

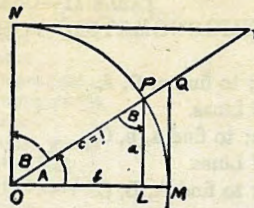


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

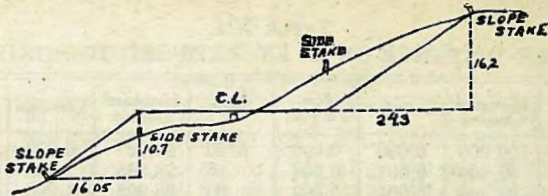
$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

| | 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 | |
|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|----|
| 0 | 0 00 | 0 15 | 0 30 | 0 45 | 0 60 | 0 75 | 0 90 | 1 05 | 1 20 | 1 35 | 0 |
| 1 | 1 50 | 1 05 | 1 20 | 1 35 | 1 50 | 1 65 | 1 80 | 1 95 | 2 10 | 2 25 | 1 |
| 2 | 3 00 | 3 15 | 3 30 | 3 45 | 3 60 | 3 75 | 3 90 | 4 05 | 4 20 | 4 35 | 2 |
| 3 | 4 50 | 4 65 | 4 80 | 4 95 | 5 10 | 5 25 | 5 40 | 5 55 | 5 70 | 5 85 | 3 |
| 4 | 6 00 | 6 15 | 6 30 | 6 45 | 6 60 | 6 75 | 6 90 | 7 05 | 7 20 | 7 35 | 4 |
| 5 | 7 50 | 7 65 | 7 80 | 7 95 | 8 10 | 8 25 | 8 40 | 8 55 | 8 70 | 8 85 | 5 |
| 6 | 9 00 | 9 15 | 9 30 | 9 45 | 9 60 | 9 75 | 9 90 | 10 05 | 10 20 | 10 35 | 6 |
| 7 | 10 50 | 10 65 | 10 80 | 10 95 | 11 10 | 11 25 | 11 40 | 11 55 | 11 70 | 11 85 | 7 |
| 8 | 12 00 | 12 15 | 12 30 | 12 45 | 12 60 | 12 75 | 12 90 | 13 05 | 13 20 | 13 35 | 8 |
| 9 | 13 50 | 13 65 | 13 80 | 13 95 | 14 10 | 14 25 | 14 40 | 14 55 | 14 70 | 14 85 | 9 |
| 10 | 15 00 | 15 15 | 15 30 | 15 45 | 15 60 | 15 75 | 15 90 | 16 05 | 16 20 | 16 35 | 10 |
| 11 | 16 50 | 16 65 | 16 80 | 16 95 | 17 10 | 17 25 | 17 40 | 17 55 | 17 70 | 17 85 | 11 |
| 12 | 18 00 | 18 15 | 18 30 | 18 45 | 18 60 | 18 75 | 18 90 | 19 05 | 19 20 | 19 35 | 12 |
| 13 | 19 50 | 19 65 | 19 80 | 19 95 | 20 10 | 20 25 | 20 40 | 20 55 | 20 70 | 20 85 | 13 |
| 14 | 21 00 | 21 15 | 21 30 | 21 45 | 21 60 | 21 75 | 21 90 | 22 05 | 22 20 | 22 35 | 14 |
| 15 | 22 50 | 22 65 | 22 80 | 22 95 | 23 10 | 23 25 | 23 40 | 23 55 | 23 70 | 23 85 | 15 |
| 16 | 24 00 | 24 15 | 24 30 | 24 45 | 24 60 | 24 75 | 24 90 | 25 05 | 25 20 | 25 35 | 16 |
| 17 | 25 50 | 25 65 | 25 80 | 25 95 | 26 10 | 26 25 | 26 40 | 26 55 | 26 70 | 26 85 | 17 |
| 18 | 27 00 | 27 15 | 27 30 | 27 45 | 27 60 | 27 75 | 27 90 | 28 05 | 28 20 | 28 35 | 18 |
| 19 | 28 60 | 28 65 | 28 80 | 28 85 | 29 10 | 29 15 | 29 40 | 29 45 | 29 70 | 29 75 | 19 |
| 20 | 30 00 | 30 15 | 30 30 | 30 45 | 30 60 | 30 75 | 30 90 | 31 05 | 31 20 | 31 35 | 20 |
| 21 | 31 50 | 31 65 | 31 80 | 31 95 | 32 10 | 32 25 | 32 40 | 32 55 | 32 70 | 32 85 | 21 |
| 22 | 33 00 | 33 15 | 33 30 | 33 45 | 33 60 | 33 75 | 33 90 | 34 05 | 34 20 | 34 35 | 22 |
| 23 | 34 50 | 34 65 | 34 80 | 34 95 | 35 10 | 35 25 | 35 40 | 35 55 | 35 70 | 35 85 | 23 |
| 24 | 36 00 | 36 15 | 36 30 | 36 45 | 36 60 | 36 75 | 36 90 | 37 05 | 37 20 | 37 35 | 24 |
| 25 | 37 50 | 37 65 | 37 80 | 37 95 | 38 10 | 38 25 | 38 40 | 38 55 | 38 70 | 38 85 | 25 |
| 26 | 39 00 | 39 15 | 39 30 | 39 45 | 39 60 | 39 75 | 39 90 | 40 05 | 40 20 | 40 35 | 26 |
| 27 | 40 50 | 40 65 | 40 80 | 40 95 | 41 10 | 41 25 | 41 40 | 41 55 | 41 70 | 41 85 | 27 |
| 28 | 42 00 | 42 15 | 42 30 | 42 45 | 42 60 | 42 75 | 42 90 | 43 05 | 43 20 | 43 35 | 28 |
| 29 | 43 50 | 43 65 | 43 80 | 43 95 | 44 10 | 44 25 | 44 40 | 44 55 | 44 70 | 44 85 | 29 |
| 30 | 45 00 | 45 15 | 45 30 | 45 45 | 45 60 | 45 75 | 45 90 | 46 05 | 46 20 | 46 35 | 30 |
| 31 | 46 50 | 46 65 | 46 80 | 46 95 | 47 10 | 47 25 | 47 40 | 47 55 | 47 70 | 47 85 | 31 |
| 32 | 48 00 | 48 15 | 48 30 | 48 45 | 48 60 | 48 75 | 48 90 | 49 05 | 49 20 | 49 35 | 32 |
| 33 | 49 50 | 49 65 | 49 80 | 49 95 | 50 10 | 50 25 | 50 40 | 50 55 | 50 70 | 50 85 | 33 |
| 34 | 51 00 | 51 15 | 51 30 | 51 45 | 51 60 | 51 75 | 51 90 | 52 05 | 52 20 | 52 35 | 34 |
| 35 | 52 50 | 52 65 | 52 80 | 52 95 | 53 10 | 53 25 | 53 40 | 53 55 | 53 70 | 53 85 | 35 |
| 36 | 54 00 | 54 15 | 54 30 | 54 45 | 54 60 | 54 75 | 54 90 | 55 05 | 55 20 | 55 35 | 36 |
| 37 | 55 50 | 55 65 | 55 80 | 55 95 | 56 10 | 56 25 | 56 40 | 56 55 | 56 70 | 56 85 | 37 |
| 38 | 57 00 | 57 15 | 57 30 | 57 45 | 57 60 | 57 75 | 57 90 | 58 05 | 58 20 | 58 35 | 38 |
| 39 | 58 50 | 58 65 | 58 80 | 58 95 | 59 10 | 59 25 | 59 40 | 59 55 | 59 70 | 59 85 | 39 |
| 40 | 60 00 | 60 15 | 60 30 | 60 45 | 60 60 | 60 75 | 60 90 | 61 05 | 61 20 | 61 35 | 40 |
| 41 | 61 50 | 61 65 | 61 80 | 61 95 | 62 10 | 62 25 | 62 40 | 62 55 | 62 70 | 62 85 | 41 |
| 42 | 63 00 | 63 15 | 63 30 | 63 45 | 63 60 | 63 75 | 63 90 | 64 05 | 64 20 | 64 35 | 42 |
| 43 | 64 50 | 64 65 | 64 80 | 64 95 | 65 10 | 65 25 | 65 40 | 65 55 | 65 70 | 65 85 | 43 |
| 44 | 66 00 | 66 15 | 66 30 | 66 45 | 66 60 | 66 75 | 66 90 | 67 05 | 67 20 | 67 35 | 44 |
| 45 | 67 50 | 67 65 | 67 80 | 67 95 | 68 10 | 68 25 | 68 40 | 68 55 | 68 70 | 68 85 | 45 |
| 46 | 69 00 | 69 15 | 69 30 | 69 45 | 69 60 | 69 75 | 69 90 | 70 05 | 70 20 | 70 35 | 46 |
| 47 | 70 50 | 70 65 | 70 80 | 70 95 | 71 10 | 71 25 | 71 40 | 71 55 | 71 70 | 71 85 | 47 |
| 48 | 72 00 | 72 15 | 72 30 | 72 45 | 72 60 | 72 75 | 72 90 | 73 05 | 73 20 | 73 35 | 48 |
| 49 | 73 50 | 73 65 | 73 80 | 73 95 | 74 10 | 74 25 | 74 40 | 74 55 | 74 70 | 74 85 | 49 |
| 50 | 75 00 | 75 15 | 75 30 | 75 45 | 75 60 | 75 75 | 75 90 | 76 05 | 76 20 | 76 35 | 50 |

Computed by L. Leland Locke.