

1745

MS

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FRANK

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# 1745

CITY ENGINEER'S OFFICE

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CHICAGO

Pages

1-6 - X-sec. 69<sup>th</sup> - Saranac - N.

7-62 - Survey for Prop. Drain 41<sup>st</sup> - Univ. to  
Wightman + Marlborough + Univ.

63 - Loc. Ties + Improvements - National - 40<sup>th</sup> to 41<sup>st</sup>

64-66 Cross Sec Federal Blvd South 1/2 17<sup>th</sup> to 48<sup>th</sup> St.

~~68~~ 73 X Section Alley 3 Eastgate

73 Proposed Drain Mt. View Park.

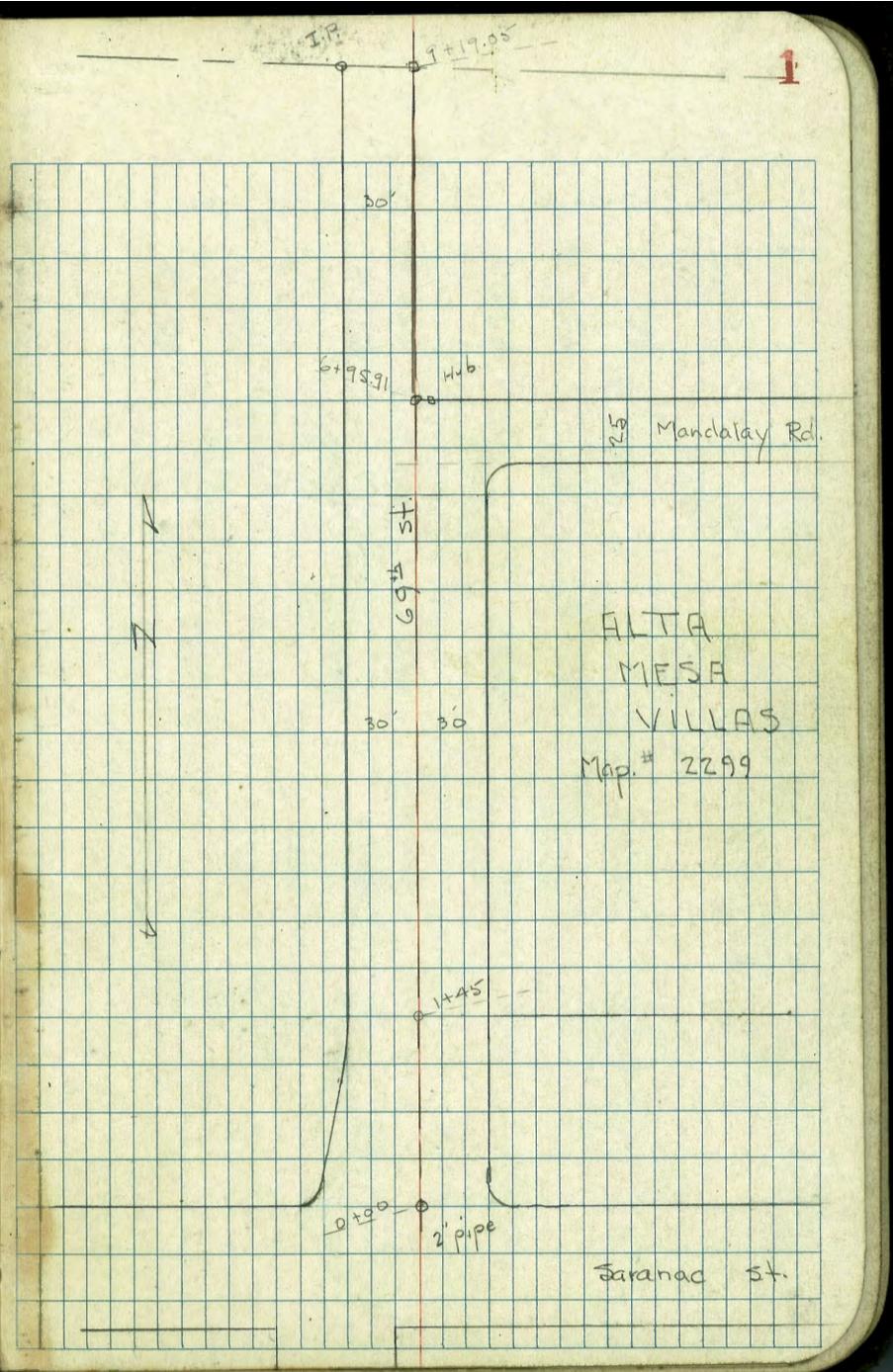
Indexed  
C.S.K.

# X-Section 69th - Saranac - North

# 591  
W.D. 230

10-30-46  
Osborne  
Hardin  
Worrell  
Smith

See 2893-B for opening Det.



X- Sect. 69<sup>th</sup> St. 60' wide Saranac  
N. to Mandalay Rd. - 30' for Rest of  
Way.

1+09.2 = opp. P.C. on W.L.

0+60

0+25

0+00 = N.L. Saranac.

0-30 =  $\Phi$  Saranac.

B.M.

3.19  
1.64

464.00  
466.39

5.58

460.81  
464.75

Top Hyd. s.E.  
Saranac + 6.42  
Top Hyd. s.W.  
Manauk + 1.04

L.		R.	
455.2	455.7	454.6	455.0
8.8 40	8.0 30	7.1 40	7.0 30
456.2	457.7	456.5	457.4
7.8 30	6.7 20	6.3 30	6.6 30
457.3	457.8	457.7	458.4
6.7 20	6.6 20	6.3 30	6.6 30
458.0	458.6	458.9	459.5
6.0	5.4	5.1	4.6
458.3	458.7	459.2	460.1
5.7 20	5.3 20	4.8 20	3.9 20
459.9	460.5	460.9	461.8
4.1 25	3.8 25	3.6 30	2.2 30
460.0	460.8	463.3	463.6
4.0 30	3.1 30	2.0 30	1.4 30
460.4	461.4	465.7	
3.6 30	2.6 30	1.1 30	
Approx. W.L.		Approx. W.L.	
Prop. P.C.		Prop. P.C.	
464.00			

4+00

3+50

3+00

2+50

2+09. 21.7 Lt. ← P. pale

2+00

1+50.52 - opp. E.C. on w.l.

455.2	455.1	455.0	454.9	455.3	455.6	455.6
455.8	455.7	455.4	455.6	455.6	455.6	455.6
457.0	456.8	456.0	456.5	455.9	456.1	456.1
457.1	456.5	456.1	455.9	455.8	455.8	455.8
457.6	457.0	456.5	456.5	456.1	456.3	456.3
458.3	458.9	457.9	457.1	456.9	456.7	456.7
459.3	458.8	457.7	457.1	456.8	457.0	457.0
459.5	459.0	457.8	457.3	457.0	457.1	457.1
459.8						

164.00



9+19.05

9+16 - 0.3' Rt. = end fence

9+02 - 7' Lt. = # 3" Euc.

9+00

8+65 - 10" Lt. = 14" Euc.

8+60 - 9.5' Lt. = # 10" Euc.

8+50

8+30 - 0.5' Lt. = # 8" Tree

8+29 - 7.7' Lt. = # 14" Euc.

8+20 - 3' Lt. = # 10" Euc.

8+16 - 20.4' Lt. = # P. pole

8+00 - 29.5' Lt. = 12" Euc.

7+68 - 22' Lt. = # 14" Euc.

7+50

7+38 - 0.8' Rt. = wire fence

7+14 - 3.7' Rt. = Begin tall wire fence

7+00 - 3.4' Lt. = R 8" Fruit tree

N. of Here only 30' wide - W. of # Produced.

6+95.91 = N.L. Mandalay and Nib. Sub.

.385 50%

457.26	456.86	456.26	454.26	451.36
457.26	457.26	456.66	454.26	451.96
457.56	457.96	456.36	454.16	450.86
458.56	458.16	456.86	454.56	450.66
458.36	456.66	456.06	453.96	449.86
458.26	457.66	456.16	453.96	449.86
458.86	457.46	456.06	453.36	449.66
458.66	457.46	456.06	453.36	449.66
459.06	457.46	456.06	453.36	449.66

starting B.M.	2.12	464.72	75'
T.P.	9.92	466.84	5.34
		456.92	

9+50

448.56  
 3 2  
 30

446.56  
 158

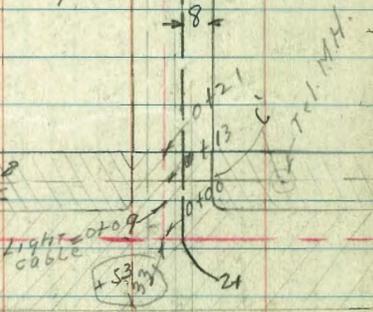
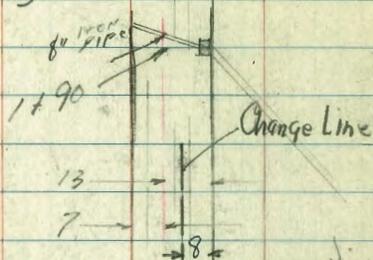
446.96  
 5 9  
 30

462.36

Proposed Storm Drain  
41st and Univ. Ave.

W.O. #203

ALL CB R=10



check up on Sewer  
M.H. in this alley

Note! old ESD pipes

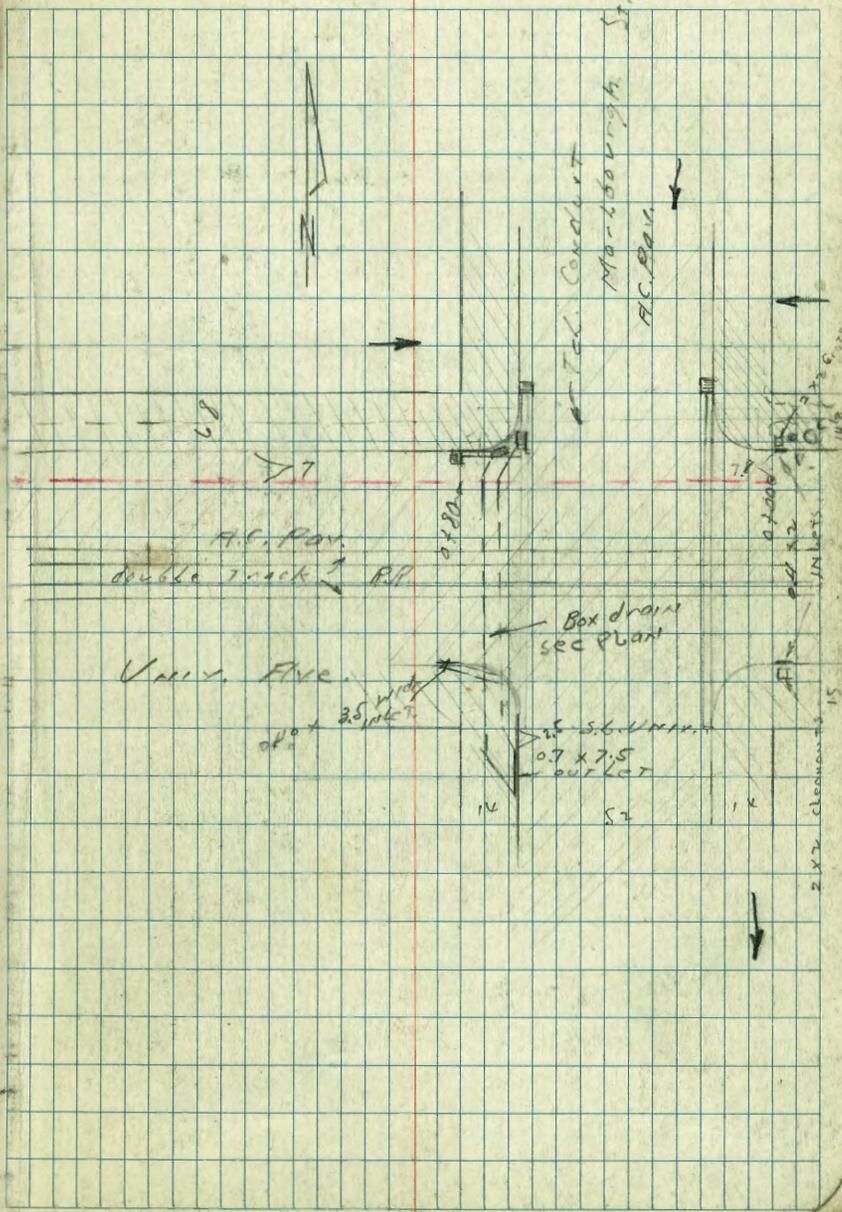
at Marlborough + 41st

C. Moore  
S. Moore  
W. R. M.  
B. C. G.

11-8-46.

INDEXED  
C.S.M.

7







Location of Ornamental Lights  
Pinned Poles, Palms etc.

1+186	9 RT.	P.P.			
+383	"	"	O. Light		
2+415	"	"	P.P.		
+71.1	"	"	O. Light		
3+77	"	"	"	"	
3+80.5	"	"	P.P.		
5+04	S. edge	drain outlet	7' RT.		
+042	11 RT.	14" di.	coco palm		
+31	"	12"	"	"	"
+61	"	"	"	"	"
+95	"	"	"	"	"
6+18	"	8"	"	"	"
+40	"	9"	"	"	"
+74	"	6"	"	"	"
7+08	"	10"	"	"	"
+35	"	8"	"	"	"
+55	"	12"	"	"	"
+83	"	"	"	"	"
8+06	"	8"	"	"	"
+24	"	6"	"	"	"
9+25	"	16"	Fern Palm		

Drain Levels  
 in Alley Blk. 42 E. S. D.  
 Betw. 41st & Markbonough

0 + 21 N.L. UNIV. edge Pav.

0 + 13 Intersect Tel. Conduit

0 + 09 Intersect Light cable

0 + 07 N gutter on UNIV.

2 + 33 on UNIV. 0 + 00

FOUND  
 NWBP 5.00 352.63

TP. 4.15 357.63 4.19 353.48

NWBP 5.7X 357.67  
 UNIV. and  
 CENTRAL 351.93

353.37 Lt = West

RT = TO EAST

353.37	424	4.30	353.20	4.37	353.38
	76	Pav.	443	13	13
			Pav.	Pa	25
			END		56
			352.97		
			471		
			352.82		
			481		
			352.77		
			486		
			353.13		
			450		
			357.63		
			UNIV. Ave & Markbonough		
			(S.E. C'd. CT. ON UNIV.		
			7" " ON 41ST.		







3700

775

750

2740

2733 = line front alley

2720

T.P.

474

357.91

416

353.17

357.33

L7

353.57

4.39

11.4

353.170

4.51

11.4

353.38

4.62

11.4

353.38

4.53

11.4

353.36

4.55

11.5

353.32

4.59

11.4

Roll

353.56

4.35

11.4

353.198

4.43

11.4

353.35

4.50

11.4

353.29

4.62

11.4

353.27

4.64

11.4

353.18

4.73

11.4

353.39

4.52

11.4

353.29

4.62

11.4

353.21

4.70

11.4

353.15

4.76

11.4

353.12

4.79

11.4

353.06

4.85

11.4

352.18

4.93

11.4

352.95

4.96

11.4

352.96

4.95

11.4

352.76

4.95

11.4

352.78

4.94

11.4

352.68

4.93

11.4

353.39

4.57

11.4

353.32

4.59

11.4

353.21

4.70

11.4

352.97

4.94

11.4

352.78

4.94

11.4

352.96

4.95

11.4

R7

15

357.91 ✓

3 + 93.84

3 + 93.84

26 Returns + Pay.

3 + 79.84 E.L. 41 ST

S.E.  
T.P.C. ST.  
WISCONSIN

4.26 357.74 4.43 353.48

3 + 50

3 + 25

357.91 ✓

352.18	353.82	353.32	353.28
5.50	4.30	4.40	4.46
59	59	59	45
FL. outlet	66	Pay 91	

353.29	353.01
4.45	4.73
45	45
06	92

353.22	353.22	353.83	353.83
4.52	5.52	4.91	4.11
65	65	91	24
96	97	91	66
353.65	353.71	353.58	353.85
4.05	4.03	3.90	4.89
38	22	14	21
FL. outlet	66	Pay 91	FL. outlet
353.19	353.82	353.65	353.58
4.55	4.40	4.09	4.16
55	55	24	24
91	66	66	91
353.52	353.73	353.19	353.59
4.20	4.01	4.55	4.15
38	101	91	06
FL. outlet	66	Pay 91	66
353.75	353.65	353.12	353.52
4.16	4.20	4.77	4.39
14	101	91	66
FL. outlet	66	Pay 91	66
353.63	353.50	353.11	353.50
4.28	4.41	4.80	4.41
14	101	91	66
FL. outlet	66	Pay 91	66
357.91			



+75

+50

+25

5+00.8 9 5' drain outlet on R

LT 97.84 SL V NIV

CTR SW Pct.

357.74

LT = EAST 9

R

18

352.55	352.23	357.75	352.39
5.19	5.51	5.99	5.35
10		7	7
		97.	06
352.86	352.57	352.18	
4.86	5.17	5.00	
10		7	
		97	14 da
353.38	353.09	352.55	
4.50	4.73	5.19	
10		7	
		97 in dr.	
353.61	353.51	352.68	353.65
4.13	4.23	5.10	4.09
10		7	7
		97	06
		72. outlet	
353.71	353.67	352.99	353.68
4.03	4.07	4.75	4.06
10		7	7
		97	70p06
		353.72	
		4.07	
		Top06	
		353.78	
		4.00	
		P0V1	
	357.74		

Lr

R

+25

T.P. 242 352.64 752 350.22 ✓

7+00

+75

+50

+25

6+00

357.74 ✓

2 138  
10 350.26

2 71  
10 350.93

2 14  
10 350.50

2 54  
10 350.10

10 350.65  
10 350.39

352.44 ✓  
10 350.39

10 350.96  
10 350.80

10 351.05  
10 350.78

10 350.26  
10 350.85

10 351.59  
10 351.22

10 350.69  
10 351.19

10 351.76  
10 351.49

10 350.97  
10 351.51

32.17  
10 351.85

10 351.98  
10 351.39

10 351.93  
10 351.81

357.74 ✓



+25

10+00

T.P. 2.03 341.87 12.80 339.80

+75

+50

+25

9+00

352.64

385 50%

L

R

P

21

339.15  
2.72  
10

390.18  
16.9  
10

391.38  
11.30  
10

392.82  
10.22  
10

393.56  
9.98  
10

394.72  
7.90  
10

338.69  
3.18

339.75  
2.12

341.87  
11.74  
389.90

391.97  
10.67

393.17  
9.87

394.38  
8.40

338.28  
3.59  
7

339.37  
2.50  
7

340.88  
12.14  
7

391.58  
11.06  
7

392.77  
9.87  
7

393.83  
8.81  
7

338.72  
2.90

339.88  
1.89  
7

391.12  
11.50  
7

392.26  
10.38  
7

393.80  
9.24  
7

394.90  
8.24  
7

352.64





+ R.I. - EV.

check to	NW BP				
	CNNI + Central	4.03	351.92	351.93	
T.P.	5.91	355.95	0.94	350.04	
T.P.	7.66	350.98	1.34	343.32	343.56
T.P.	9.47	344.66	1.68	335.19	335.49
					0.30

23.8 S of SL WIGHTMAN S. end inlet

15.5 S of SL WIGHTMAN = E curb inlet

7.3 S of SL WIGHTMAN

SL WIGHTMAN

S.F. RETURN + SW RET

341.87

LT R 24

= NW BP Central + Highman  
= NWBP 41st + Highman

	335.09	333.99
	1.78	7.88
	06	97. INLET
	335.25	333.87
	1.17	8.00
	06	9.00 TC
	335.88	332.01
	1.39	7.86
	06	97. INLET
	334.82	335.72
	7.03	1.13
	97	06
	335.89	335.87
	5.98	1.60
	CR Ret	CR Ret
	Tap 6	Tap
	341.87	

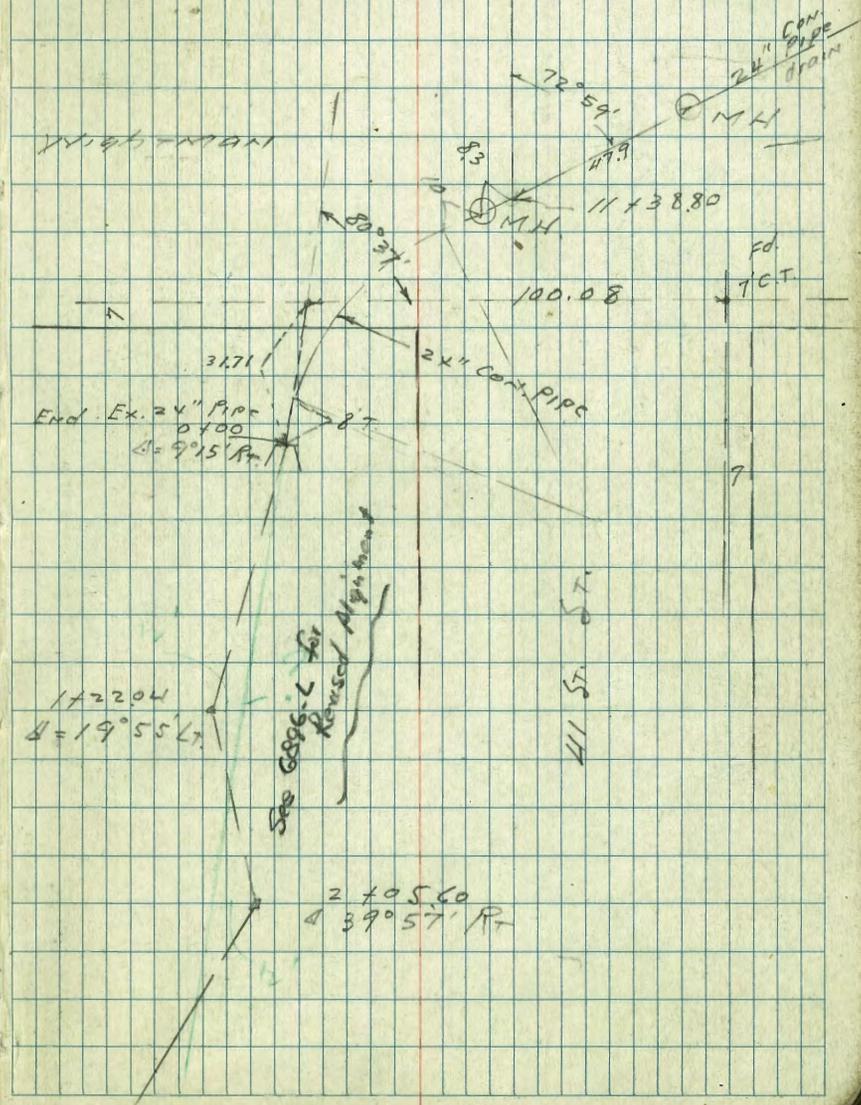
Survey STORM drain  
 from 41<sup>st</sup> & WIGHTMAN  
 to 40<sup>th</sup> S. of Landis St.

110-203

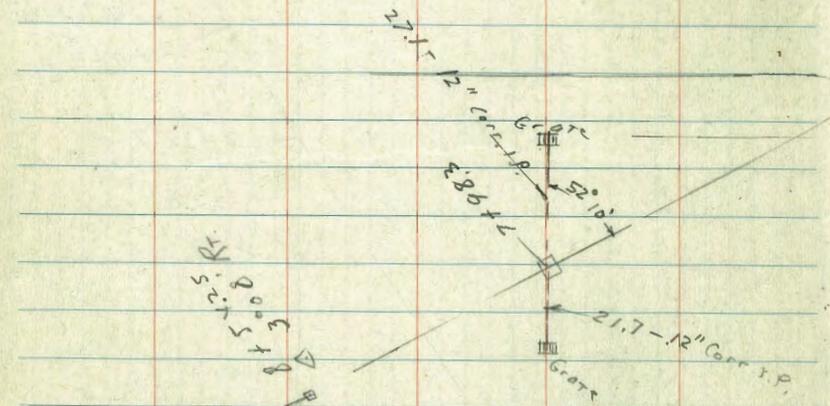
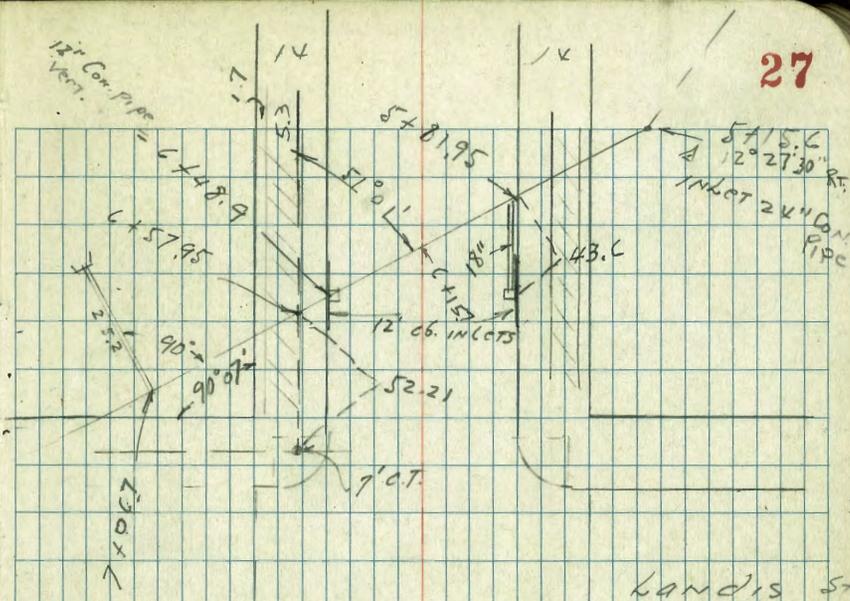
INDEXED  
 C.S.K.

21

25







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 99  
 100



Drain Levels Sketch P. 25

0 + 96 E 3' x 9' Foot bridge over creek

0 + 80 old wire fence

+ 75

0 + 45

0 + 29

0 + 04.5

0 + 00 F.b. outlet 24" Cor. Pipe

I.P. 1.5 326.39 12.2 325.24

MWB 2.17 337.36 ✓ 335.19 ← P. 25

VIST Highman

LT = To EAST

Pt

29

			310.7	
			11.7	
			FL Creek	
			315.1	
			11.3	
			315.8	
			10.6	SE Con Chickyard
				4.7
			315.9	
			10.5	NE Con Chickyard
				7.3
	322.6			
		319.1		
	3.8	7.3	317.3	
	10.5	10.5	9.1	6.1
	F.b. 30" pipe	ground		5
	outlet			
			316.57	
			9.72	
				326.39 ✓

150

2105.6  $\Delta$  39°57' RT

2100

1154.5 E 3.5 x 10 Foot bridge

1127 to 1132 Cobble wall 2.3 Ft.

T.P. 4.31 317.94 12.70 313.63

1122.04  $\Delta$  19°55' LT

326.39

LT

RT

RT

30

311.5  
21.2  
0

311.5  
K

311.6  
0.1  
0

313.1  
0.5  
0.5  
0.5  
0.5  
K

311.9  
0.0  
0.0  
K

312.8  
0.1  
0.1  
K

18' Dist. fence

1127  
2.0  
1132

317.94

13.7  
313.2

326.39

4 + 85

150

4

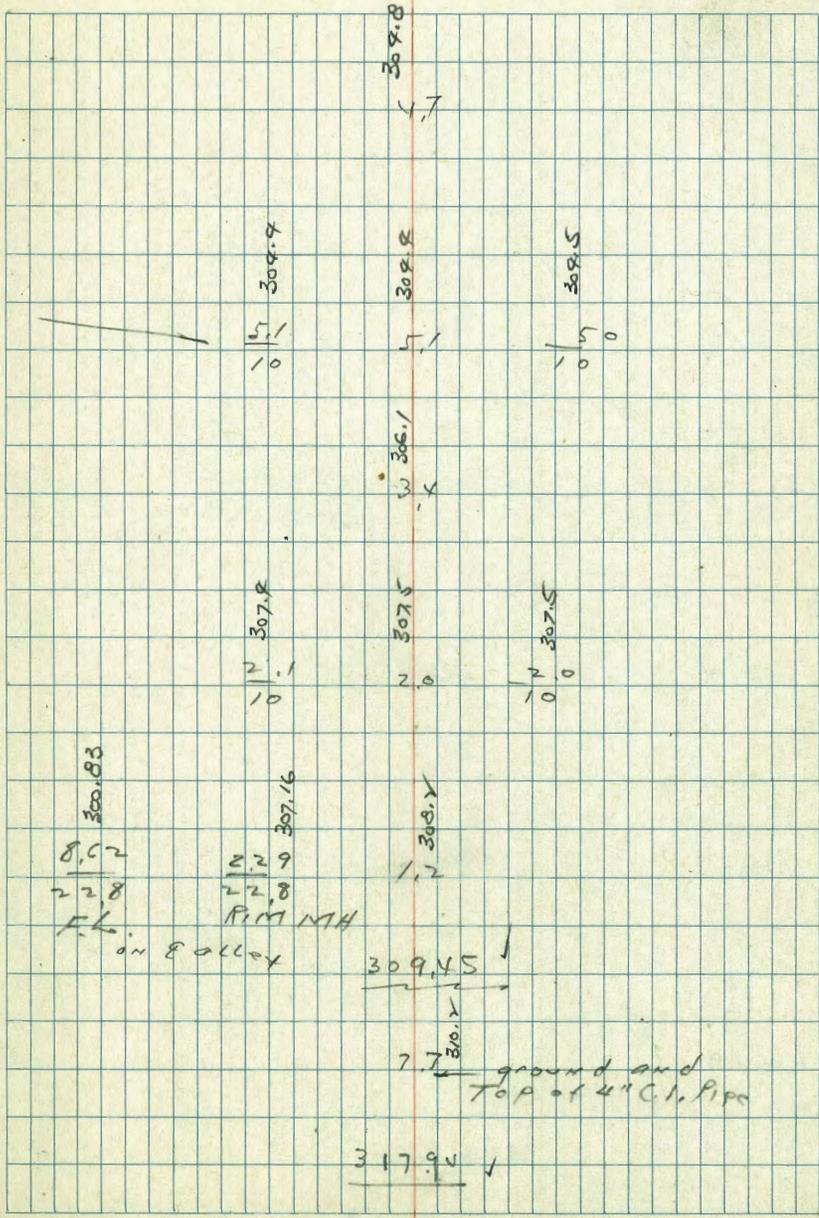
150

3 + 28.7 Intersect Sewer in alley

T.P. 0.70 309.45 9.19 308.75

2 + 95.7 Cross Sewer Lat.

317.94



5+63

T.P. 12.57 332.44 0.28 319.87

T.P. 10.81 320.15 0.11 309.34

5+16

5+156 Δ 12° 27' 30" R.

5+10

5+00

4+89

309.45

27.

Rx 32

324.0

C.K. Shoulder FILL

332.44 ↓

4.9 304.6

Top FILL

308.34

300.95

6.13

Top hdwall

9.00

FL. INLET 24" CON. PIPE

C.K. 303.1

C.K. 303.1

C.K. 303.4

309.45 ↓



9+43 Top FILL

9+43

T.P. 0.2 ~ 308.24 12.45 307.62

T.P. 1.06 320.07 12.45 219.01

B+50 Shoulder FILL

check to <sup>M+BP</sup> north of Landis 1.18 330.28 330.28  
0.00

7+98.3 M.H. cleanout

7+50

7+30

331.45

9  
12.8 285.8

7.4 300.6

308.74 ✓

5.0 326.5

322.21

328.87

321.20

326.50

319.60

325.53

320.35

9.25  
21.7  
Bot. Box

6.59  
21.7  
Top 9-47c

10.70  
2  
R.L. 12" from S.

4.96  
2  
R.L. 12" from N.  
38.80  
R.L. 20" pipe Box

11.80  
2  
R.L. 12" from N.

5.93  
27.1  
Top grate

11.11  
27.1  
Bot. Box

5.7 325.8

5 327.0

331.45 ✓

7 61

7 40

10

9 185

9 183

9+60.27  $\Delta = 12^{\circ} 32' 30''$  LT

T.P.	0.25	<u>295.65</u>	12.84	295.40
		308.24		

Revised - See pg 40

282.0  
13.7

282.6  
11.1

288.0  
7.5

288.8

289.88  
8.8

287.75  
7.90

R.C. outlet  
2" pipe

295.65 |

12100

12450

12100

+74

+50

+26

11420

T.P. 128 284.41 12.52 28313

11403.48 Δ 28°18'R

295.65

Revised  
See Pg. 40

Scobed  
M.H.  
R.K.  
D.S.  
200.83

276.7  
87

276.3

279.0

280.6

281.8

280.8

284.51

13 X 282.7

295.65 ✓

Notes Referred. 1248-96  
Pg. 11 to 35A





LT = E

\$  
41.57.

R<sub>T</sub>

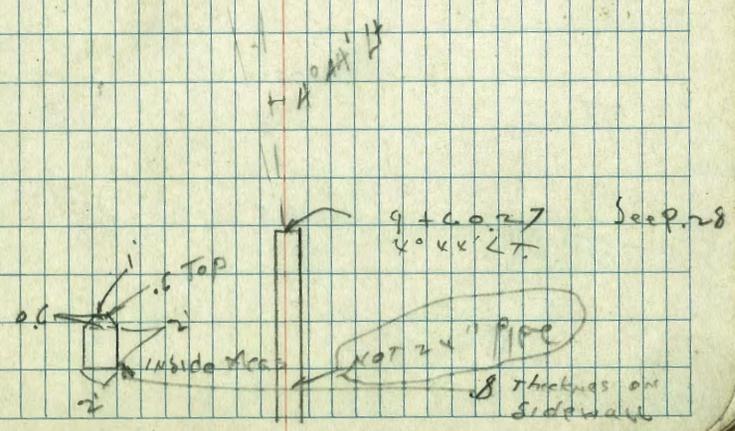
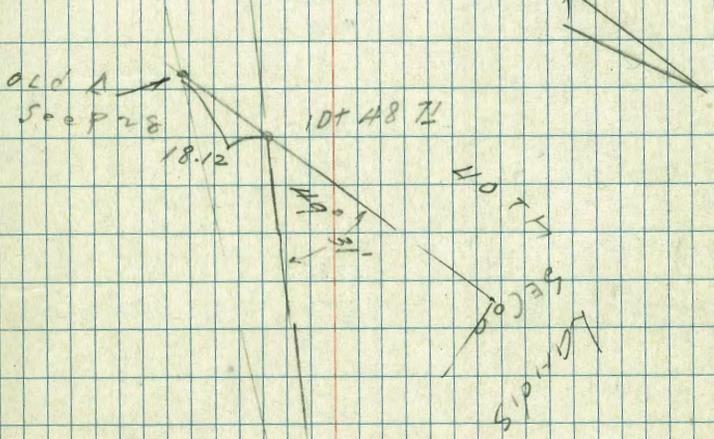
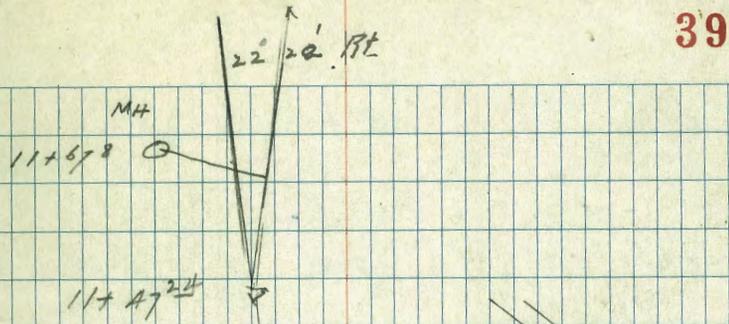
38

Elevations  
0.3 low  
~~Add~~

0 + 31	335.41 4.64 26.66	335.91 5.34 26	335.96 4.79 13	335.63 4.62 13	335.22 5.01 13	335.22 6.01 26.35	335.91 5.34 26	335.51 4.64 32.1 SW
0 + 24	335.59 4.76 26	335.88 5.41 26	335.88 4.91 13	335.60 4.65 13	335.25 5.00 13	335.93 6.32 26.2	335.09 5.16 26	
0 + 16	335.26 4.99 26	335.59 5.56 26	335.81 4.84 13	335.53 4.72 13	335.23 5.02 13	335.85 6.40 26.15	335.25 5.00 26	
0 + 11	335.29 4.96 26	335.68 5.57 26	335.81 4.84 13	335.56 4.69 13	335.17 5.08 13	335.89 6.36 26.1	335.36 4.39 26	335.83 4.42 32.8 SW
0 + 07.6	335.31 4.94 26	335.65 5.60 26	335.81 4.84 13	335.55 4.70 13	335.15 5.10 13	335.01 6.24 26.1	335.98 4.77 26	
0 + 00	335.81 4.84 26	335.23 6.02 26	335.89 4.76 13	335.55 4.90 13	335.22 5.03 13	335.88 5.37 25.92	335.75 4.57 26	335.01 4.22 32.5 SW
- 07	335.87 4.28 26	335.75 5.50 26.3	335.29 4.96 13	335.58 4.67 13	335.55 4.90 13	335.88 4.77 26	335.85 4.80 26.4	
	5.06	340.25			335.19			

NW BP  
Whiteman  
4-11

335.49



285.3

+63

52

282.5

+60

70

283.5

+50

70

284.7

+45

5.8

285.5

10+20

50

286.0

10+0

4.5

287.6

+75

2.9

286.8

9+65

37

HI ↓

9+60+7

290.48

2.73

287.75 ↓

FL of col/kert p 35

	+	#1	-	E1
12+50	6.8 32	277.0	7.8 276.0	7.0 276.8 48

12+0	52 44	278.6	6.3	277.5 48 279.0 6.8
------	----------	-------	-----	-----------------------------

11+67.8	MH 3.02 8.7L	280.80	277.9 5.9	
---------	--------------------	--------	--------------	--

3.59 283.82 #1

290.48 10.25 280.25 ✓

11+47.24 Δ 10.23 280.75

11+344		281.0	9.5	Pier 4.5
--------	--	-------	-----	-------------

11+205	Pier 4.5	282.0	8.5	
--------	-------------	-------	-----	--

11+0		283.6	6.9	
------	--	-------	-----	--

10+85		283.4	7.1	
-------	--	-------	-----	--

290.48 ✓

Notes Reduced. 1.28.57

283.82	
3.02	
280.80	

+ HI  
Check Levels ✓

2.46 332.74 330.28 R34

12.76 319.98

2.30 322.28

12.68 309.60

0.42 310.02

12.32 297.70 ✓

0.92 298.62 ✓

7+60.27  
Culvert  
11+67.8  
HM

42

40<sup>th</sup> Lardin NW BP

- 10.90

287.72 ✓

Flowline

- 7.84

290.78 ✓

Top of Culvert

- 17.84

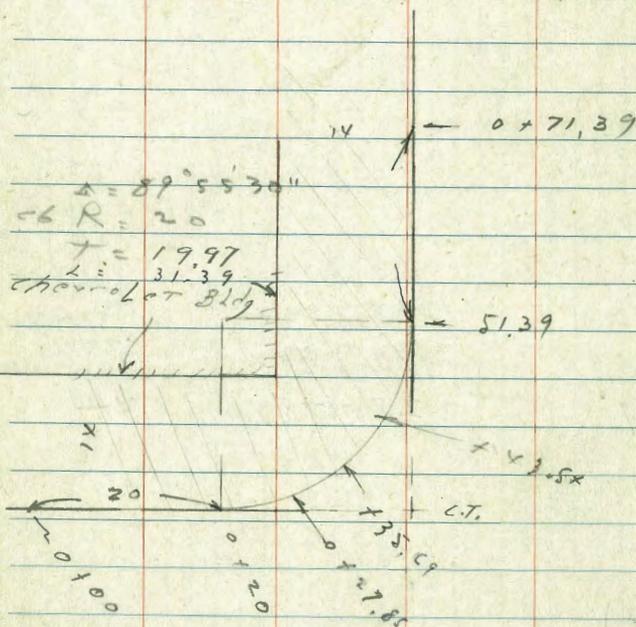
280.78 ✓

MH

80.80 R9-11

N.W. 20' c.b. R. Returns  
 Markborough & Univ.  
 as proposed

Full width walk



Note: Used existing curb  
 lines for  $\Delta$  of Returns

also 6' Ld. C.T. at intersections

" chiseled crosses at

P.C.'s & P.C.'s & on curve 1/5

BM  
 N.W. B.P. 4.52      357.15      352.63 ✓  
 Markborough  
 and Univ. Ave

26  
 21145  
 2

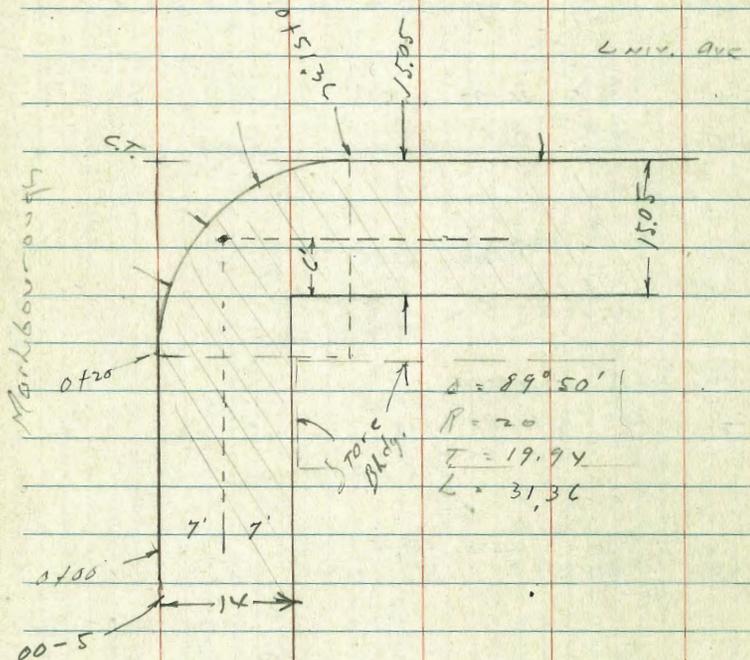
117

43

	352.67	352.11	352.66	353.05
0 + 71.39	4.48	5.04 97	4.49 7	4.10 15
	352.69	351.94	352.54	353.04
0 + 51.39 C.S.	4.51	5.23 97	4.56 7	4.11 15
	352.63	352.57	352.84	352.73
0 + 43.54	4.52	4.58 1.7	4.83 1.8	4.42 7
	352.56	352.55	352.23	352.46
0 + 35.69	4.59	4.60 4.2	4.92 4.3	4.69 7
	352.5	352.5	352.18	352.66
0 + 27.85	4.65	4.65 7.1	4.97 7.2	4.50 7
	352.46	352.44	351.36	352.63
0 + 25	4.69	4.71 0.5	5.79 0.6	4.52 7
	352.39	351.84	352.36	352.74
0 + 20 P.C.T.	4.76	5.31 0.1	4.59 7	4.36 12
	352.38	352.38	352.03	
0 + 15	4.77	5.12 0.1		
	352.05			
0 + 10			5.10 = P.V. in drive	
	357.15 ✓			



Proposed S.E. Return  
 Marlborough & Univ. Ave



SE. Cap. TR. IS ON  
 C' Line on Univ. Ave  
 7' " " Marlborough

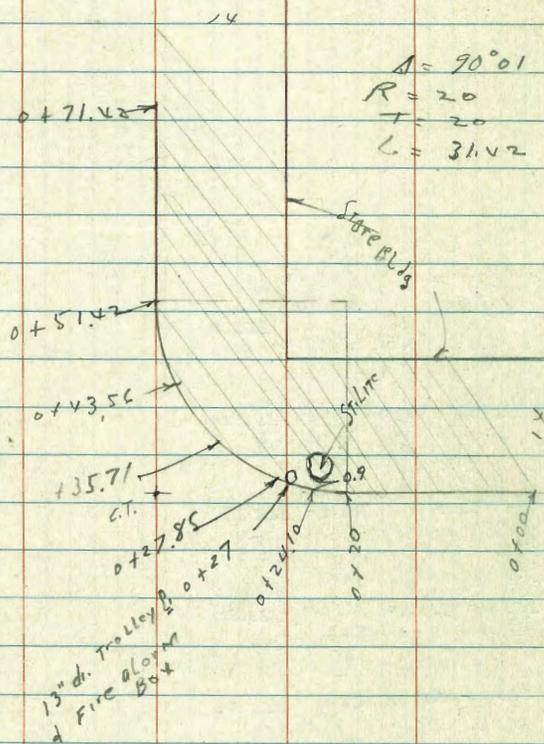
	352.52	352.80	352.72	
D+71.3C	3.41 15	3.75 7	4.43 97	353.15
				362.96
	353.32	353.29	352.90	
D+51.3C	3.81 15	3.91 7	4.49 97	42.5
D+49.2	353.31	352.79		
	3.84 15	4.00 7	4.36 97	352.87 352.99 4.16
	353.09	352.72	352.89	352.93
D+35.8	4.00 15	4.43 7	4.76 97	4.72
				Ex. 6. + Pav. TOP of CLEAR OUT
	352.99	352.89	352.85	
D+27.8X	4.16 15	4.26 7	4.30 97	352.89 4.26
				Ex. 6. + Pav.
	352.89	351.37	351.70	352.72
BC P D+20	4.31 15	4.78 7	5.45 97	4.43
D+20				= behind car
	352.62	352.23	351.69	352.88
D+5	4.53 15	4.92 7	5.46 97	4.17
				357.15 ✓

1.3 di. Power +  
 1.6 P<sub>1</sub> Trolley Pole





Proposed N.E. Ret.  
41st + Univ. Ave.



385 50%

LT

66

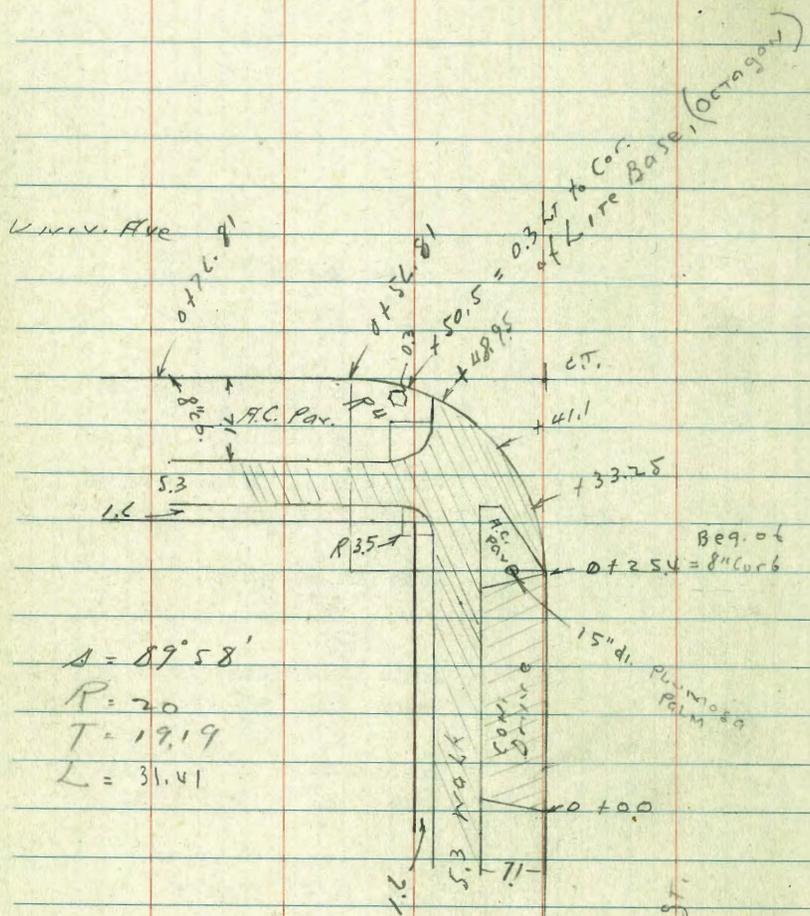
48

	353.86	353.19	353.80
+ 71.42	4.69	5.41	4.75
	15	97	
	353.95	353.60	352.91
E.C.	4.60	4.95	5.64
+ 57.42	15	7	97
	353.85	353.49	352.78
+ 43.50	4.70	4.86	4.77
	15	7	16
	353.81	353.52	352.61
+ 35.71	4.74	5.03	4.94
	15	7	4
	353.80	353.59	353.26
+ 27.85	4.75	5.01	5.29
	15	7	16
	353.76	353.53	352.16
0 + 20	4.79	5.02	5.40
	15	7	97
	353.73	353.15	353.54
0 + 0	4.82	5.40	5.01
	15	97	

358.55 ✓



S.W. Ret.  
 41 ST. + Union Ave.



$\Delta = 89^{\circ}58'$   
 $R = 20$   
 $T = 19.19$   
 $L = 31.41$

	353.89	353.00	353.59	
0 + 76.81	5.06	$\frac{5.55}{97}$	$\frac{4.96}{75}$	
F.C. + 50.81	353.60	353.15	353.59	353.71
	4.95	$\frac{5.40}{97}$	$\frac{5.01}{7}$	$\frac{4.84}{15}$
	353.66	353.65	353.84	353.59
+ 48.95	4.89	$\frac{4.90}{17}$	$\frac{5.13}{97}$	$\frac{4.95}{7}$
	353.78	353.73	353.69	353.74
+ 41.1	4.87	$\frac{4.87}{3.76}$	$\frac{4.86}{7}$	$\frac{4.83}{15}$
	353.74	353.70	353.98	353.59
+ 33.25	4.83	$\frac{4.85}{1.6}$	$\frac{5.07}{1.6}$	$\frac{4.96}{7}$
	353.63	352.58	353.28	353.57
89. + 25.4	4.92	$\frac{5.97}{97}$	$\frac{5.7}{7}$	$\frac{4.98}{15}$
	353.10	352.57	353.15	
0 + 00	5.45	$\frac{5.98}{97}$	$\frac{5.40}{15}$	

358.55 ✓

Add. Levels at  
NW cor. 41st + Wightman

10 + 97.68 = <sup>N.L.</sup> Wightman

195.7

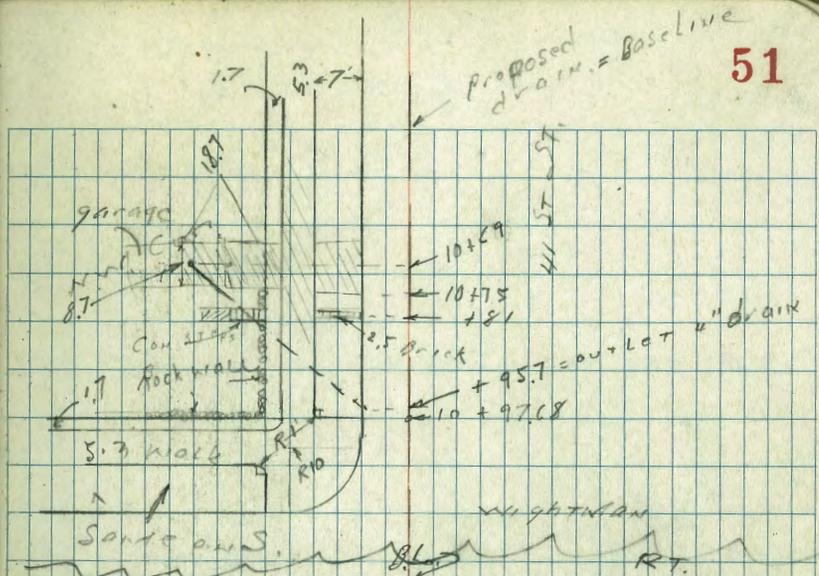
10 + 88.7

10 + 75 = From P. 22 ← could Beg. here with const.

10 + 69.0 = E drive

NW BP 6.66 341.85  
41st Wightman

335.19



335.02 335.31 335.31  
6.83 6.54 6.54  
7 14 19.3

335.29 335.02 335.59 335.13  
6.61 6.83 7.60 7.26 6.77  
5.7 Pav 7 7 7 14  
Fl. u. dra.

add  
0.3

335.53 334.94 335.76 335.90 335.92  
6.37 6.91 6.09 5.95 5.91  
7 7 14 19.3

336.27 336.01 336.67 336.79 336.85  
5.58 5.84 5.18 5.06 5.00  
7 7 14 19.3

336.56 336.35 336.43 337.15 336.83  
5.29 5.50 5.42 4.70 4.76  
7 7 19.3 28 38 39.7  
341.85 drive dr. 23.3 28 38 39.7  
Sum 401.4

6.558



Levels on 41st St  
 from 2405.7 S of SL, see  
 Nightman NLY to Landis P37

4400 ± N.L. Landis - end Paving.  
 F.V. N.W. BP 41st + Landis 428 336.98 ✓  
 I haven't got this in my Bk.  
 +50

5400  
 4453  
 T.P. 4.29 341.26 3.95 336.77

4400  
 4450

3401

2450

N.W. BP 5.53 340.72  
 N.W. BP  
 N.W. BP  
 335.19

Lt = E. side €

add 0.3 53

337.39	336.79	337.24	337.32	337.07	336.27	336.96
3.87	4.47	4.04	3.92	4.24	4.99	4.30
26	26	13	13	13	26	26
337.18	336.63	337.10	337.23	336.94	336.28	336.83
4.08	4.63	4.14	4.03	4.34	4.98	4.43
26	26	13	13	13	26	26
337.16	336.48	337.04	337.11	336.77	336.19	336.66
4.10	4.78	4.24	4.15	4.49	5.12	4.60
26	26	13	13	13	26	26
336.92	336.30	336.81	336.91	336.64	335.93	336.51
4.34	4.96	4.45	4.35	4.64	5.33	4.75
26	26	13	13	13	26	26
			<u>341.26</u> ✓			
336.77	336.17	336.68	336.79	336.39	335.78	336.39
3.95	4.55	4.04	3.93	4.33	4.94	4.33
26	26	13	13	13	26	26
336.64	336.05	336.50	336.60	336.26	335.63	336.29
4.10	4.67	4.22	4.12	4.46	5.09	4.48
26	26	13	13	13	26	26
336.52	335.89	336.86	336.98	336.14	335.50	336.13
4.20	4.84	4.36	4.24	4.60	5.22	4.59
26	26	13	13	13	26	26
336.39	335.68	336.18	336.27	335.96	335.29	336.01
4.33	5.04	4.54	4.45	4.76	5.43	4.71
26	26	13	13	13	26	26
4.06						4.06
			<u>340.72</u> ✓			

Line change of drain  
FROM P. 25 + P. 29

0100 to 2 + 50

0 + 75

+CC

+55

0 + 45

+42

0 + 32

0 + 29

T.P. 0.35 326.63 10.62 326.28

N.W.B.P. 1.71 336.90 ✓ 335.19

41 St. Whigham

? 335.19

322.3	317.2	315.2		316.9	316.2
$\frac{4.3}{15}$	$\frac{9.4}{5}$	$\frac{11.4}{3}$	15'	$\frac{10.2}{2}$	$\frac{10.7}{12}$

Peach  
 $\frac{10}{10}$

PLUM  
 $\frac{9}{9}$

Peach  
 $\frac{11}{11}$

PLUM  
 $\frac{10}{10}$

318.9	318.6	316.1		318.3	319.3	320.2	320.5
$\frac{7.7}{15}$	$\frac{8.0}{7}$	$\frac{10.5}{3}$	15'	$\frac{8.3}{2}$	$\frac{7.3}{5}$	$\frac{6.4}{6}$	$\frac{6.1}{10}$

Peach  
 $\frac{11}{11}$

Peach  
 $\frac{13}{13}$

320.0	319.7	316.8		319.5	320.2
$\frac{4.4}{10}$	$\frac{6.9}{2}$	$\frac{9.8}{2}$	15'	$\frac{7.1}{3}$	$\frac{6.4}{8}$

326.63 ✓

1+34

T.P. 1.55 317.93 1025 316.38

1+24

1+2204  $\Delta$  Sec. on split

1+14

0+98

0+96

0+88

0+85

326.63

L+

4" di.  
cedar

4

4" to 5" di.  
cedar

4

9

55

cedar

10

cedar  
12

317.93 ✓

Peach  
4

315.2

315.3

313.2

12 1/2

312.2

315.2

315.2

11.4

11.3

13.4

14.4

11.4

11.4

12

3

2

1

3

15

Peach  
2

PLUM  
5

Peach  
5

316.8

316.9

315.0

312.8

316.0

316.0

orange  
15

3/4 Hyd 9.8  
85 1.3

9.7

11.6

14 1/2

11.8

10.6

10.6

85

1.3

4

3

2

4

11

orange  
6

orange  
12

320.43 ✓

1+68

1+64

1+61

1+58

1+54.5

1+52

1+48

1+46

1+38

1+37

317.93

L + 8" di Eucal

R 56

Orange  $\frac{1}{2}$  Rose  $\frac{1}{2}$  Tree  $\frac{1}{2}$

cedar  $\frac{1}{4}$  Shrub and Rock  $\frac{1}{2}$  Shrub  $\frac{1}{8}$  Rose  $\frac{1}{17}$

48" di. Eucal.  $\frac{1}{2}$

Shrub  $\frac{1}{5}$

319.0	319.0	319.3	313.0	8	313.3	319.6	318.9	313.9	317.9
$\frac{2.9}{20}$	$\frac{3.9}{10}$	$\frac{2.6}{5}$	$\frac{4.9}{2}$		$\frac{11.6}{2}$	$\frac{3.3}{3}$	$\frac{4.0}{10}$	$\frac{11.0}{23}$	$\frac{0.0}{28}$

Quince  $\frac{1}{20}$

Rose  $\frac{1}{8}$

Shrub  $\frac{1}{8}$

Shrub  $\frac{1}{8}$

Shrub  $\frac{1}{8}$

Shrub  $\frac{1}{10}$

Macasia  $\frac{1}{2}$

2 + 50

2 + 10

2 + 0.56 Δ Sec. on split

2 + 00

1 + 89

1 + 80

1 + 74

1 + 71

31793 ✓

311.3

$\frac{6.5}{15}$

311.5

14

311.6

$\frac{6.7}{15}$

oak  
12

312.4

$\frac{5.5}{15}$

13'

313.0

$\frac{4.9}{1}$

312.1

$\frac{5.8}{2}$

312.1

$\frac{5.8}{4}$

313.2

$\frac{4.7}{8}$

313.9

$\frac{0.92}{12}$

315.9

$\frac{2.5}{11}$

$\frac{2.5}{25}$

312.7

$\frac{5.7}{15}$

313.2

$\frac{4.7}{2}$

312.9

$\frac{5.5}{1}$

11'

312.1

$\frac{5.8}{4}$

312.9

$\frac{5.0}{2}$

319.9

$\frac{3.0}{17}$

316.7

$\frac{1.7}{25}$

apple  
Peach  
7

scrub  
oak tree  
14

8'd. Cedar  
12

cacti + Flowering  
shrubs

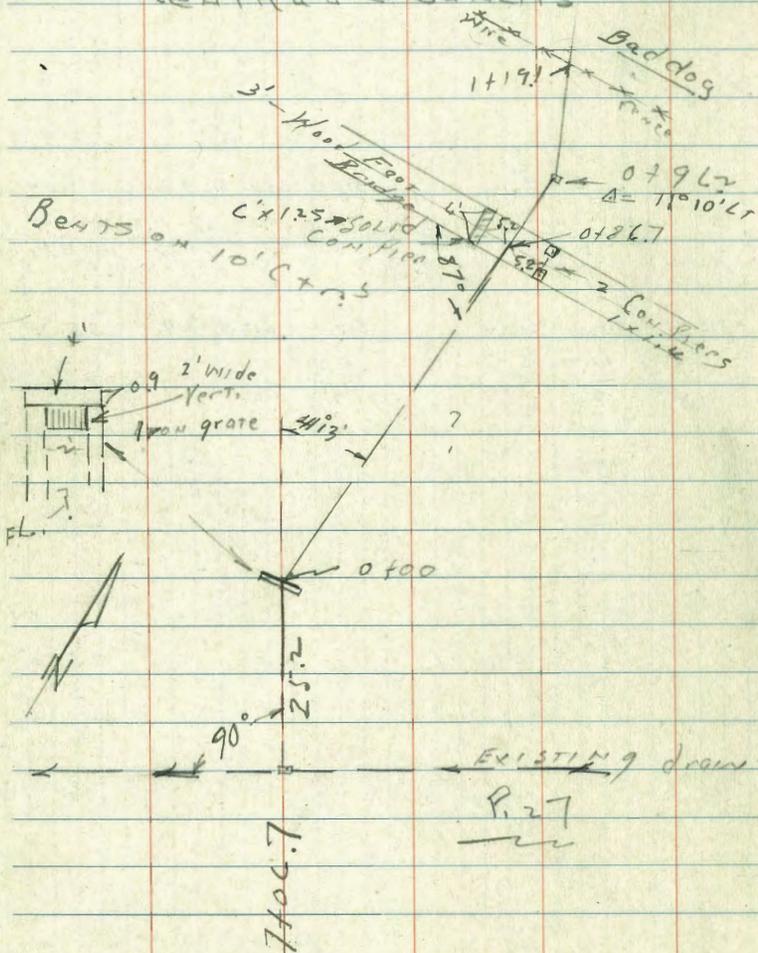
Shrub  
11

Peach  
6

Add. Levels on  
N branch drain  
at NW Cor. of  
Central + lands

P. 27 & 34

Levels P. 59



1+191 95 wide fence

0+767  $\Delta$  Not planned to fill  
N. of Foot Bridge

0+867

0+70

0+35

0+12

0+01

0+00 Top hd wall

T.P. 1.28 320.53 1225 319.25  
B.M. NIALBP 122 331.50 ✓ 330.28 40<sup>th</sup>

310.0 309.3 311.2  
 $\frac{18.5}{15}$  11.2  $\frac{9.3}{15}$

311.7 309.2 311.3 313.9  
 $\frac{8.8}{15}$  11.3  $\frac{9.2}{15}$   $\frac{7.1}{20}$

311.2 308.8 307.8 307.6 310.1  
 $\frac{9.3}{5.2}$   $\frac{11.7}{4.5}$  12.7  $\frac{12.9}{5}$   $\frac{10.4}{15}$

Top  
P. 100

312.3 308.5 307.9 307.1 311.2  
 $\frac{6.7}{15}$  12.0  $\frac{13.1}{3}$   $\frac{13.4}{9}$   $\frac{9.3}{20}$

311.7 306.9 306.4 307.1 310.0  
 $\frac{8.8}{15}$   $\frac{14.1}{2}$  14.1  $\frac{13.4}{16}$   $\frac{10.5}{20}$

306.9 305.0 309.4 305.9 310.9  
 $\frac{13.6}{2.4}$   $\frac{15.5}{12}$  16.1  $\frac{15.1}{11}$   $\frac{10.1}{20}$   
Top on slope

308.7 308.5 308.03  
 $\frac{11.8}{15}$  16.0  $\frac{12.5}{15}$   
on slope Top slope

306.09 305.09 298.13  
Top hd wall 14.44 15.44 22.4  
Top grate Bot. Box  
if narrow  
1600's

and lands

Addl. drain Levels

10 + 00 to 12 + 50 <sup>see P. 40</sup>

+ 60

+ 50

+ 47

+ 45

+ 20

10 + 00

BM.  
FL. outside  
of drain

5.6

292.91

287.75

9 + 60.27 P. 35

8

R.T

60

289.0 285.8 290.3

8.4 7.1 2.6  
1 3 25

284.3 287.0

8.4 5.9  
12 25

286.9

6.0  
25

286.0 289.2

6.9 3.5  
6 25

285.8 286.7 290.3

7.1 6.7 2.4  
2 3 25

286.9 286.2 288.4 290.7

7.0 6.4 4.5 2.7  
4 8 11 25

292.91 ✓

+47.2 x <sup>old</sup> Δ on split

11 + 3 + 4

T.P. 6.00 289.39 9.40 282.79

116

10.5

11

10 + 85

T.P. 7.28 292.19 8.00 284.91

292.91 = H. Fwd.

Rt 61

282.4	287.8
<u>6.0</u>	<u>1.6</u>
14	25

282.8	289.7
<u>6.9</u>	<u>0.3</u>
10	25

289.39 ✓

282.4	285.4	289.7	289.8
<u>9.6</u>	<u>6.8</u>	<u>2.45</u>	<u>2.4</u>
	14	23	25

Top of  
C.M. Pier

283.5	285.96	285.5	290.9
87	<u>6.73</u>	<u>6.7</u>	<u>1.3</u>
	13.8	18	25

Top of  
C.M. Pier  
at 30 ground

285.7	290.6
<u>6.5</u>	<u>1.5</u>
12	25

283.5	289.5	290.9
<u>8.7</u>	<u>7.7</u>	<u>1.3</u>
✓	✓	25

292.19 ✓

12 + 50

12

11 1078

Notes Reduced. 3-10-07  
 R. 03662

276.0	276.8	278.9	281.2
13.4	$\frac{12.6}{4}$	$\frac{11.0}{15}$	$\frac{8.2}{25}$
		780 SLOPE	

277.4	277.8	279.2	279.2	281.4
12.0	$\frac{11.6}{2}$	$\frac{10.2}{7}$	$\frac{10.2}{14}$	$\frac{8.0}{25}$

279.1	280.1	285.4
$\frac{10.3}{2}$	9.3	$\frac{11.0}{25}$
	13	

28939 ✓

Locate Tie points + check Ext. Improvements  
National - 40<sup>th</sup> to 41<sup>st</sup> + Vicinity

W.D. 210

4-11-47

Osborne  
Hardin  
Smith  
Warvell

← 60' →

T.P. Book 24 - 42 + 47

T.P. sheets - 374 + 388

Logan Ave.

Fd. Mon.

± 5'

20.07 (meas)

27'

fence online

Vacant Lots  
Here - Nothing  
To define Line  
of St.

Very old

Improvements on Alley  
Seem to be in proper position

± 1'

0

7'

fence online

Lot lines Here  
Seem to be in Correct  
Position

14' 5' 45'

40'

Fd. 7' ct.

National Ave

617.04 (T.P.)

Fd. cts. in pave

40'

5' 14' 4.5'

27'

7'

Alley Location Correct, as defined by Ties shown

Fd Mon.

INDEX  
DISK

Fd. Mon.  
T.P. 24-48

63

← 60' →

80'

Mon. Fd spike in pave

Pueblo Line

229.06

Fd 2" pipe filled  
with Conc. with  
Nail 0.04 W. of line

fences Here  
in position

17'

367.00 (Tie P)

51'

41'

old fence

277.64

0 end of

43'

± 7'

0 21'

Fd. Disk

Fd. Disk

Fd. old fence  
Post-Cor. fits  
Lines

17'

Lot lines as occupied in  
this Block are 2' west of correct  
position

Cross Section Federal Blvd. South Partion  
47th St to 48th St.

Sketch #1182-2

Indexed  
C.S.R.

May 9-47  
H.S. Johnson  
17<sup>th</sup> Coy  
Job 6507  
H.O. 25001  
64

1+50

230.31	230.03	229.77	229.82	230.06
179	5.07	5.33	5.28	5.04
	18	37 on Pk.	50 on Pk.	75 on Pk.

1+21 = 174 HC. Paving to South

230.07	229.71	229.64	229.64	230.02
503	5.39	5.56	5.46	5.08
	18.5 HC. Paving	37 on Pk.	50 on Pk.	75 on Pk.

1+23 38 Rt of L = 54 Power Pole #273972

1+0

229.80	229.45	229.4	229.7	230.2
5.30	5.65	5.7	5.4	1.9
	18.5 HC. Paving	37 on Pk.	50 on Pk.	75 on Pk.

0+64.4

229.38	229.10	229.2	229.17	229.29
5.72	6.00	5.9	5.93	5.81
	18.5 HC. Paving	37 on Pk.	50 on Pk.	75 on Pk.

0+28

228.99	228.72	228.7	228.99	228.91	228.20
6.11	6.32	6.2	6.11	6.09	5.20
	18.5 HC. Paving	37 on Pk.	50 on Pk.	50 on Pk.	75 on Pk.

0+0 = East Line 47th St to South

228.65	228.37	228.34	228.5	228.5	228.33	228.45
6.45	6.79	6.76	6.6	6.6	6.77	6.65
	18	21.5 HC. Paving	37 on Pk.	50 on Pk.	75 on Pk.	90 on Pk.

8.17 7.05 235.10 228.05  
4.247 Federal Blvd #41125

385 5072

Federal Blvd  
47th to 48th Sts.

3750

3710 = CB EC on Rt

2780 = E-L Alley to South

2765 =  $\frac{1}{2}$  Alley to South

2750 = 0+0 #1682-35  
375' Pa/2 = Sky Power Pole #178213 Sta S3-224

270

23510

2

Rt. South

65

231.60	231.20	231.2	230.22	230.40	229.83	230.16
350	390	39	488	470	537	494
	18	37	43	56	75	76
			43-HX Pa		75-Gutter	76-CB

231.53	231.19	231.3	230.48	230.60	230.19	230.97
357	391	38	452	450	491	451
	18	37	43	56	75	76
			43-HX Pa		75-Gutter	76-CB

231.73	231.06	231.4	230.90	230.79	230.73	230.27	230.59
367	404	37	430	431	437	483	437
	18	37	43	56	75	75	75
			43-HX Pa		75-Gutter	75-Gutter	75-CB

231.32	230.98	231.3	230.87	230.75	230.66
378	417	38	433	435	411
	18	37	43	56	70
			43-HX Pa		70-SHTC

231.25	230.85	230.58	230.51	230.65
385	425	457	459	445
	18	37	56	75
				75-FHTE Pa

230.75	230.39	230.21	230.24	230.46
435	471	489	486	444
	18	37	50	75
			50-Gutter	75-SHTC Pa

23510

Federal Blvd.  
49th to 48th Sts.

4735 = 1/2 48th St to South

4719 = W Cb Line 48th St

4712 2919/10/7 = Sky Port Pole 2916.26 Sta 5-3-239

4705

3790

235.10

2

R/S

231.52	231.12	231.11	229.82	229.85	229.51
3.58	3.98 18	4.0 37	5.28 13-H/B	5.25 88	5.59 75
231.60	231.16	231.11	229.85	230.01	229.62
3.50	3.94 18	4.0 37	5.25 73	5.09 58	5.48 75
231.65	231.16	231.11	229.86	230.15	229.22
3.45	3.94 18	4.0 37	5.24 73	4.95 56	5.38 80
231.58	231.17	231.11	229.96	230.17	229.49
3.52	3.93 18-SW/COM	4.0 37	5.11 13-H/B	4.91 58	5.31 75
235.10					

July 18, 1947 Elev's. Pipe Across 8th Ave.

Hendricks So. of Robinson

W. Moore

Sherman

NO# 60135

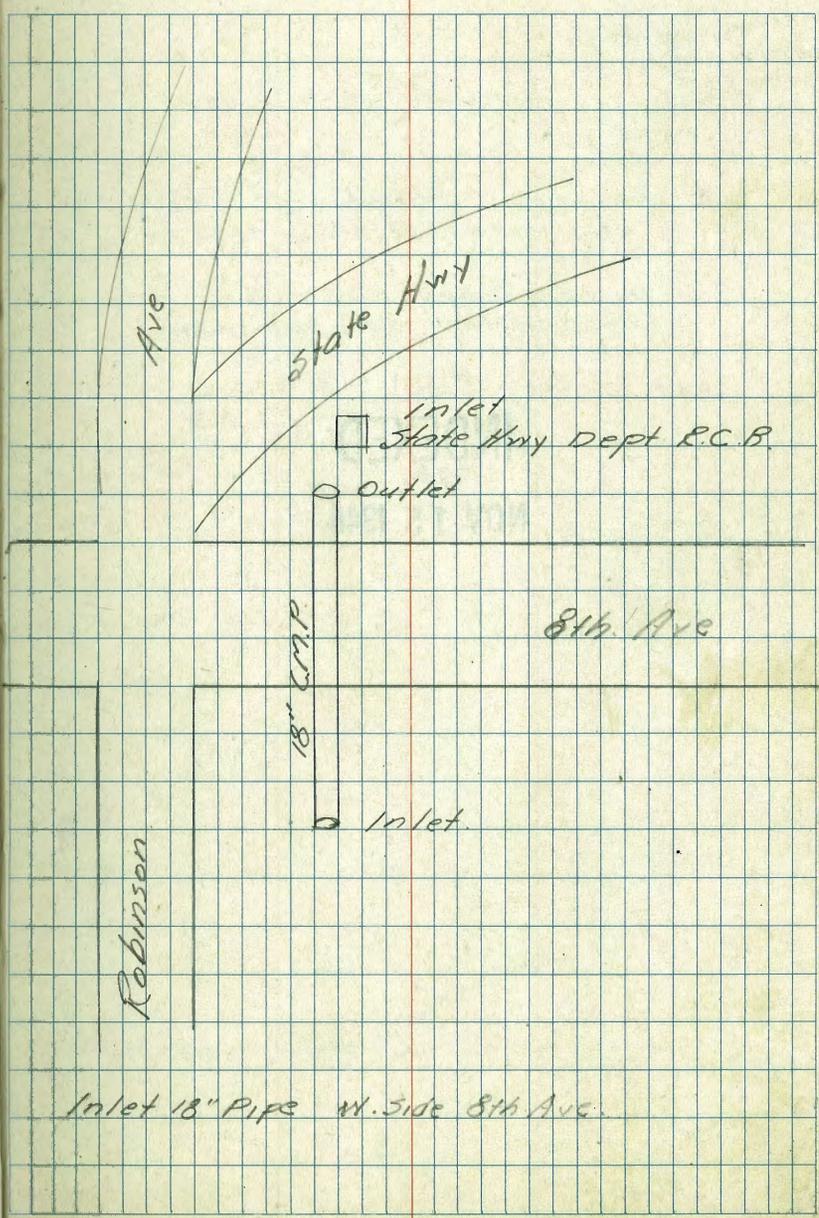
+ 41 - Elev

INDEXED

WK

NOV 15 1948

Set. Nail in sheeting	15.12	99.39	
at Outlet of City Pipe	15.12	99.39	RCB
	19.39	95.12	Outlet
	0.52	114.51	
TP.		10.56	113.99
	12.18	124.55	
TP		0.69	112.37
	13.06	113.06	100.00 Assumed

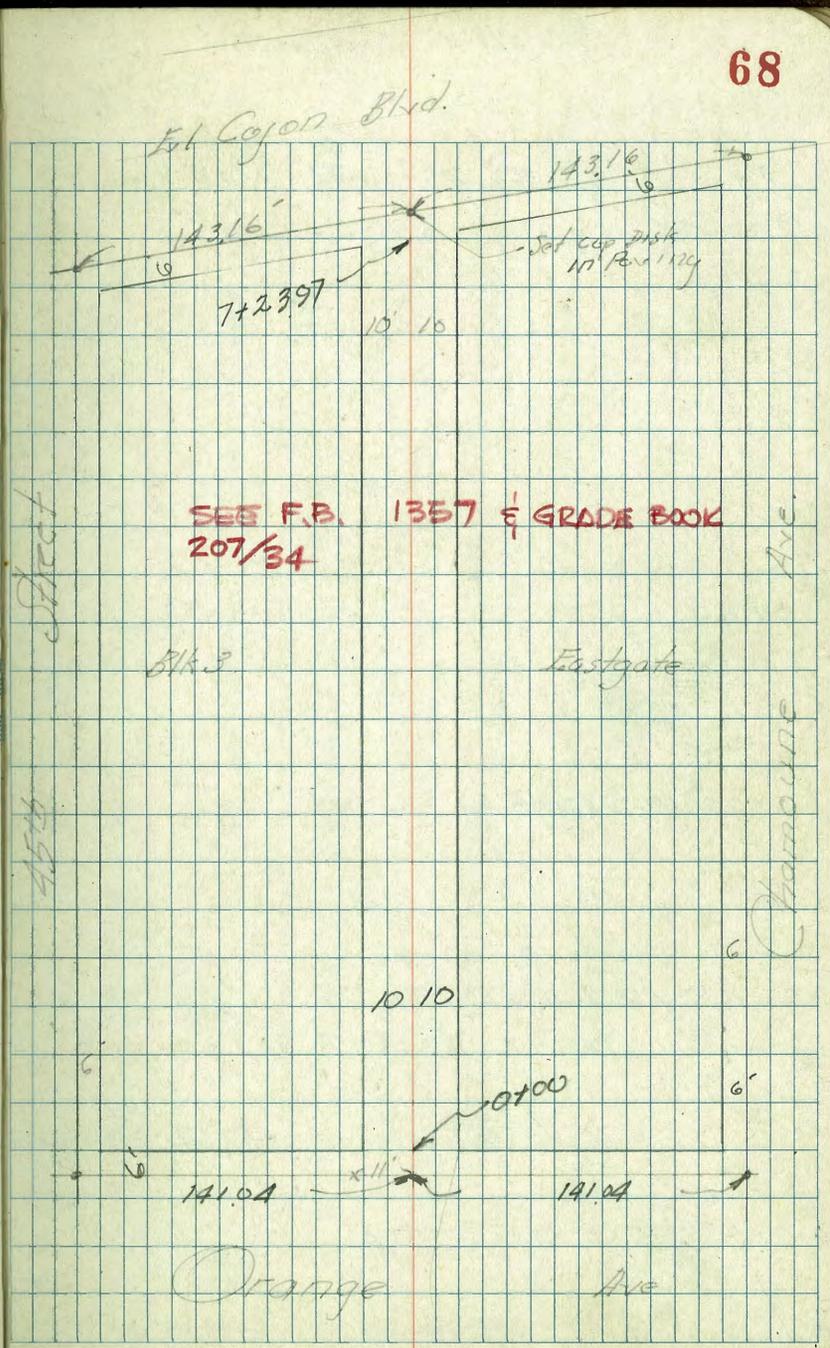


Inlet 18" Pipe W. Side 8th Ave.

check Cross Sections -  
 Walker  
 Hendricks  
 Becker  
 Johnson  
 10-10-47  
 Alley Blk. 3 - Eastgate  
 Between 45th and Chamourne Sts  
 from Orange Ave to El Cajon Blvd.  
 Original Sections FB 1357-76

Note:  
 Location & Elevations Garages  
 etc. in FB 1357. Pages 76 to 79  
 (No New Improvements)  
 Since original notes were taken.

INDEXED  
 WK  
 NOV 15 1948







Alley Blk 3 - Eastgate  
Check Cross Sections

4.

8

Rt.

71

TP 555 36274 3.28 357.19

5+50

30 18	32 10	36 7	37	36 6	32 10	39 11
----------	----------	---------	----	---------	----------	----------

5+00

36 15	38 10	41	40 6	39 10	40 15
----------	----------	----	---------	----------	----------

4+60

36 10	38 10	39 6	44	45 10	45 15
----------	----------	---------	----	----------	----------

4+27

43 15	44 10	46 5	46	49 5	44 10	44 15
----------	----------	---------	----	---------	----------	----------

4+24 blk. N end Conc. Drive } Oble. Garage  
4+08 = South " " "

436  
10

4+00

47 15	47 10	49 7	48	46 10	45 15
----------	----------	---------	----	----------	----------

360.47

360.47

7+37

357.74	357.24	357.26	357.57	357.98
500	550	5.48	5.17	4.76
6	10		10	10
	cut		cut	cut

7+31.9

358.03	357.82	357.48	357.64	357.89
471	472	5.26	5.10	4.85
10	10		10	10
cut	cut		cut	cut

7+23.97 = Skine E. / Cajon Dig Section

358.05	357.95	357.59	357.83	357.93
469	479	5.15	4.91	4.81
996	996	on Pav.	10	10
cut	on Pav.		cut	cut

7+00

358.5	358.2	358.4	358.8	358.7
4.2	4.5	4.3	3.9	4.0
10	10	10	10	15

6+41 N edge Dble Garage on Rt North Dirt Entrance Floor

358.5	358.5	358.4	358.5	358.3	358.4
4.2	4.2	4.3	4.4	4.8	4.3
10	10	10	10	15	2.5
			cut	cut	Garage

6+00

357.7	357.7	357.8	357.9	358.1
50	50	4.9	4.8	4.6
10	10		10	15

362.74

362.74

Alley Blk 3 East Gate

73

$\frac{0.02}{357.95}$   
 $\frac{4.81}{357.93}$   
 Chk E Top cb 7+23.97 FB 1357  
 79

Section on Conc. Paving.  
 7+50 = S edge Conc. Paving E. I. Cajon Blvd.

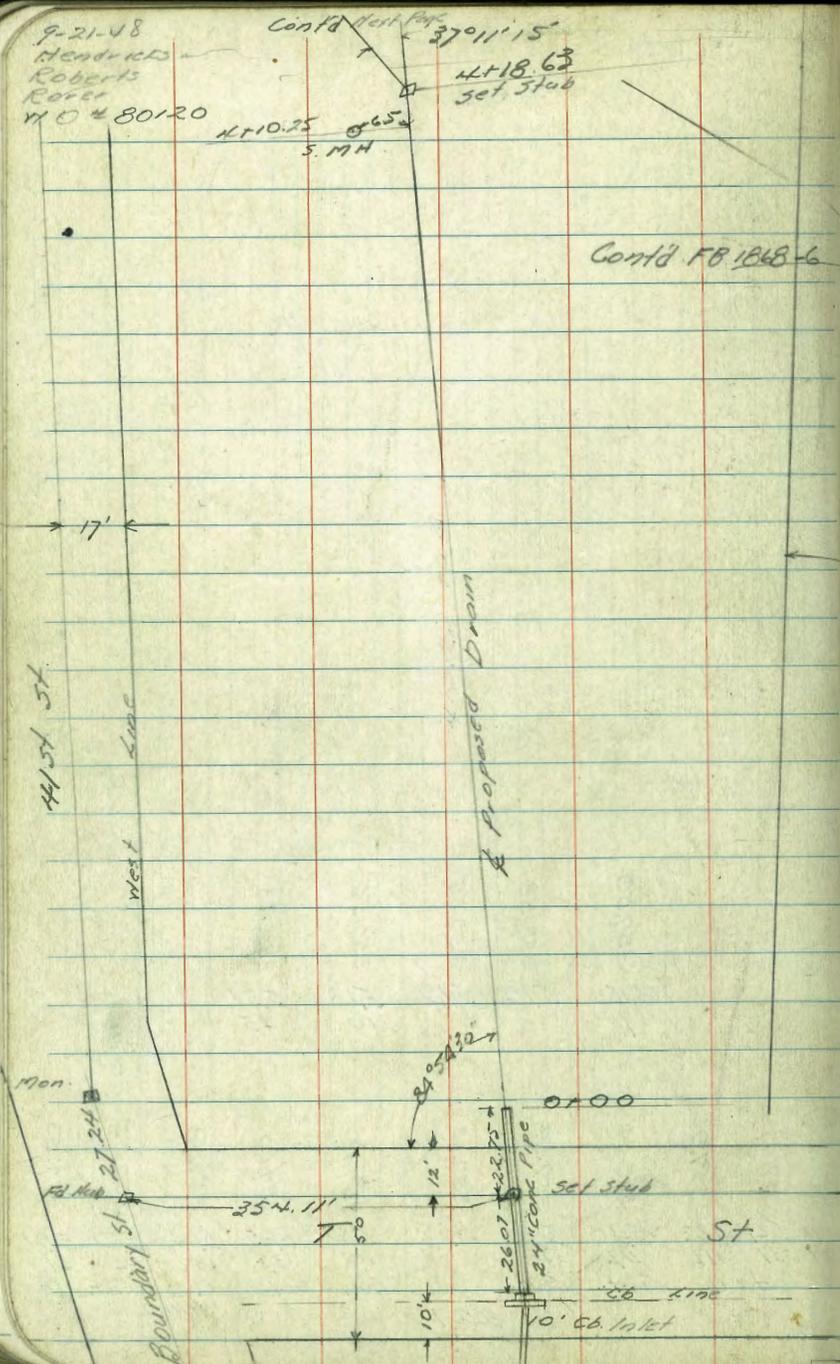
7+40.2 = S. cb. E. I. Cajon  
 7+32.4

$\frac{362.74}{4}$

357.84	357.59	357.58	357.55	357.56	357.43
470	515	516	519	518	531
37	67	10		10	45
cb	Gut.	Gut.		Gut.	Gut.
357.92	357.84	357.34	357.18	357.13	357.09
482	540	540	556	561	565
116	116	10		10	13.8
cb	Gut.	Gut.		Gut.	Gut.
357.70	357.05	357.53	362.74		
504	569	571			
139	34	34			
cb.	Gut.	cb			
Return					

9-21-48  
Hendricks  
Roberts  
Rorer  
M.O. # 80120

Cont'd Mt. Park  
37°11'15"  
441863  
set stub  
5.74

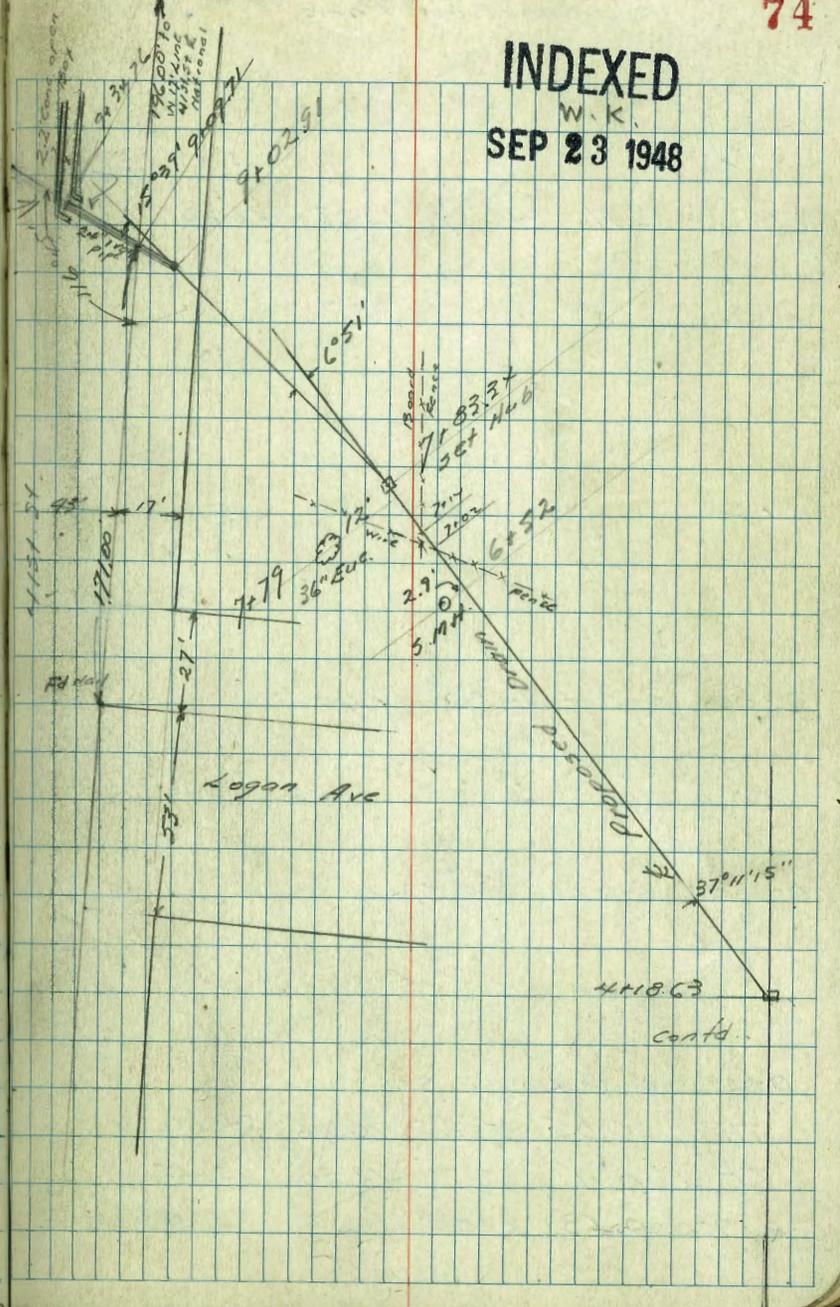


Cont'd FB 1868-6

Proposed Drain Mountain View Park

74

INDEXED  
W.K.  
SEP 23 1948



441863  
cont'd.

Levels Proposed Drain  
Mountain View Park

1+50

T.P. 2.91 46.29 12.27 43.38

1+00

0+50

0+00 Outlet 24" Conc. Pipe

0-26.07 Inlet 24" Conc. Pipe

0-28 No. ch. line T St.  
 T.P. 0.85 55.65 10.76 54.80  
 T.P. 0.11 65.56 12.38 65.45  
 B.M. 0.63 77.82 77.20

47.13  
 47.0  
 46.29  
 44.6  
 43.2  
 43.4  
 43.4  
 43.0  
 11 12 12 12 10  
 37 21 4 16

44.6  
 11

46.25  
 13.47  
 FL

47.73  
 7.2  
 Grate FL

47.74  
 47.75  
 48.70  
 48.68  
 47.24  
 7.21 6.80 6.85 6.87 8.01  
 5 5 5 5 5  
 6 6 6 6 6  
 Grate

N.W.R.B. TRUCK & 40th St.

5+00

39.4 31.2 30.0 28.0 26.0  
11 23 25 25 35  
26 10 10 25

4+55

38.6 36.6 34.4 32.0  
07 29 31 35  
18 11 15

TP. 192 39.47 8.75 37.54

one Hub + 118.63

39.47 35.4 34.4 32.0 31.0  
40.5 5.5 9.4 9.4 8.75 2.2 11.0  
42 27 4 4.0 15

4+18.63 L Lt. Rt Angles to Back Tank

4+10.25 Sewer M.M. 6.5 Lt.

37.1 (8.5) 35.1 33.3 32.8  
8.5 9.2 8.0 10.3 11.5  
28 5 2 17

4+00

3+78

39.4  
19

3+50

38.5 38.4 35.9 34.5 33.5  
7.8 7.5 6 5.8 5.8  
40 20 4 14

3+00

33.1 29.9 30.0 30.2 34.6  
3.2 6.5 6.2 6.1 1.7  
28 20 13 24

2+50

41.0  
100

2+00

43.6 41.7 41.8 41.7 44.5  
28 4 4 4 1.8  
20 15 23 22

46.29

46.291

7+23 8" Mulberry Tree 7.5H

7+21

7+14 Board fence

7+03 wire fence

T.P. 4.15 4003 3.59 35.88

7+00

6+52 Sewer MH 2.9H.

6+12

6+00

5+83

5+71

5+40

3947

8 <sup>31.1</sup>	9 <sup>31.0</sup>	9 <sup>31.0</sup>	8 <sup>31.4</sup>
15	15	15	15

4003 ✓

Nail North Side 36" Eng 13.4 7+79

35 <sup>31.4</sup>	36 <sup>31.0</sup>	37 <sup>31.0</sup>	38 <sup>31.4</sup>
18	18	18	18

50 <sup>31.9</sup>	51 <sup>31.3</sup>	52 <sup>31.6</sup>	53 <sup>31.1</sup>	54 <sup>31.6</sup>
21	21	21	21	21

60 <sup>31.1</sup>	61 <sup>31.2</sup>	62 <sup>31.2</sup>	63 <sup>31.2</sup>
21	21	21	21

5<sup>31.2</sup>

60 <sup>31.5</sup>	61 <sup>31.1</sup>	62 <sup>31.4</sup>	63 <sup>31.9</sup>	64 <sup>31.1</sup>
20	20	20	20	20

50 <sup>31.1</sup>	51 <sup>31.4</sup>	52 <sup>31.1</sup>	53 <sup>31.9</sup>
21	21	21	21

39 <sup>31.6</sup>	40 <sup>31.4</sup>	41 <sup>31.7</sup>	42 <sup>31.6</sup>	43 <sup>31.0</sup>
20	20	20	20	20

3947 ✓

B.17

478

35.25 35.25

9+3476 Outlet 24" Iron Pipe

9+0291 Inlet 24" Iron Pipe

8195

8190

8175

8150

8100

7+8334 L L1

7+58

7+37

40.03

NWBP Hist & National

Continued 78  
1868-C

12 24 21.79  
FK

28.76  
11 27  
FK

31.5	31.4	20.0	31.0	31.3	31.3
8 5	8 4	10 0	10 0	7 7	7 0
11 2	2	2	2	20	
31.5	31.3	31.1	31.1	31.9	31.3
8 5	7 9	7 7	7 7	7 1	6 8
B 5	4 2			14	

31.6	31.6	31.6	31.6	31.4	31.8
5 4	5 4	5 4	5 4	6 6	6 2
23	7	4	2		18

31.4	31.8	31.0	31.5	31.0	31.7
4 8	5 2	9 2	9 2	6 0	5 7
25	7	2		1	20

31.4	31.0	31.3	31.1	31.5
4 8	5 0	9 7	4 9	4 1
25	7		6	23

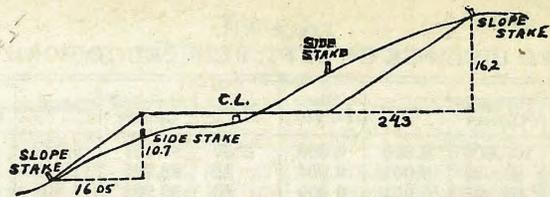
31.4	31.0	31.4	31.5	31.7
4 8	5 0	9 5	5 5	5 1
26	7	4 0	5	14

31.1	31.9	31.2	31.2	31.4
4 9	5 1	9 8	9 8	9 5
21	10	3		15

31.3	31.5	31.6	31.5	31.0
5 7	5 7	9 2	9 2	9 0
29	11	4		15
			40.03	

Notes Reduced 10-8-88

724580  
30 20 45



740971

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

179-60  
63.45  
176.45

464.75	76.65	HWP Test & 4011
<u>16.4</u>	<u>0.63</u>	
466.39	77.28	
<u>5.88</u>	<u>12.38</u>	
460.81	64.90	
<u>3.19</u>	<u>0.11</u>	
464.00	65.01	
<u>7.70</u>	<u>10.76</u>	
456.30	54.25	
<u>6.06</u>	<u>0.85</u>	
462.36	55.10	
<u>5.34</u>	<u>12.27</u>	
456.92	42.83	
<u>9.92</u>	<u>2.91</u>	
466.84	45.74	
<u>2.12</u>	<u>8.75</u>	
464.72	36.99	
	<u>1.92</u>	
	38.92	
	<u>3.57</u>	
	35.33	
	<u>4.49</u>	
	39.82	
	<u>5.14</u>	
	34.68	
	<u>2.5</u>	
	32.18	

51.85  
902.91  
934.76

Mohawk + 69 <sup>th</sup>	S.W Hyd.	464.75
" 70 <sup>th</sup>	S.E. "	476.12
El Cajon + 69 <sup>th</sup>	SWBP	456.75
70 <sup>th</sup> + Saranac	Φ L+T	460.34

367  
196  
171

95.91  
55  
40.91

555  
45  
69.591