

1746



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# 1746

## CITY ENGINEER'S OFFICE

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- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
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- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
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ENGINEERING and DRAFTING SUPPLIES

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CHICAGO

INDEXED

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Cross Sec Alley Bk 4 1<sup>st</sup> East to Ocean Spray 1-9

" " 26<sup>th</sup> St Opening Logport + Detroit 10-14

" " Meade Ave Fairmount to 15

Trias + Ft. Stockton 36

Cross Sec. Cuts - Hancock to Meade 40

" " Alley Bk 5<sup>B</sup> Pt. Lanza Hgts 45-55  
" " Catalina Manor

" " Statist Palen to Guinco 56-61

Cross Sec. 33<sup>rd</sup> St. 7<sup>th</sup> St to Date St. 62-71

" " Beech St. Bancroft to 33<sup>rd</sup> St. 72-74



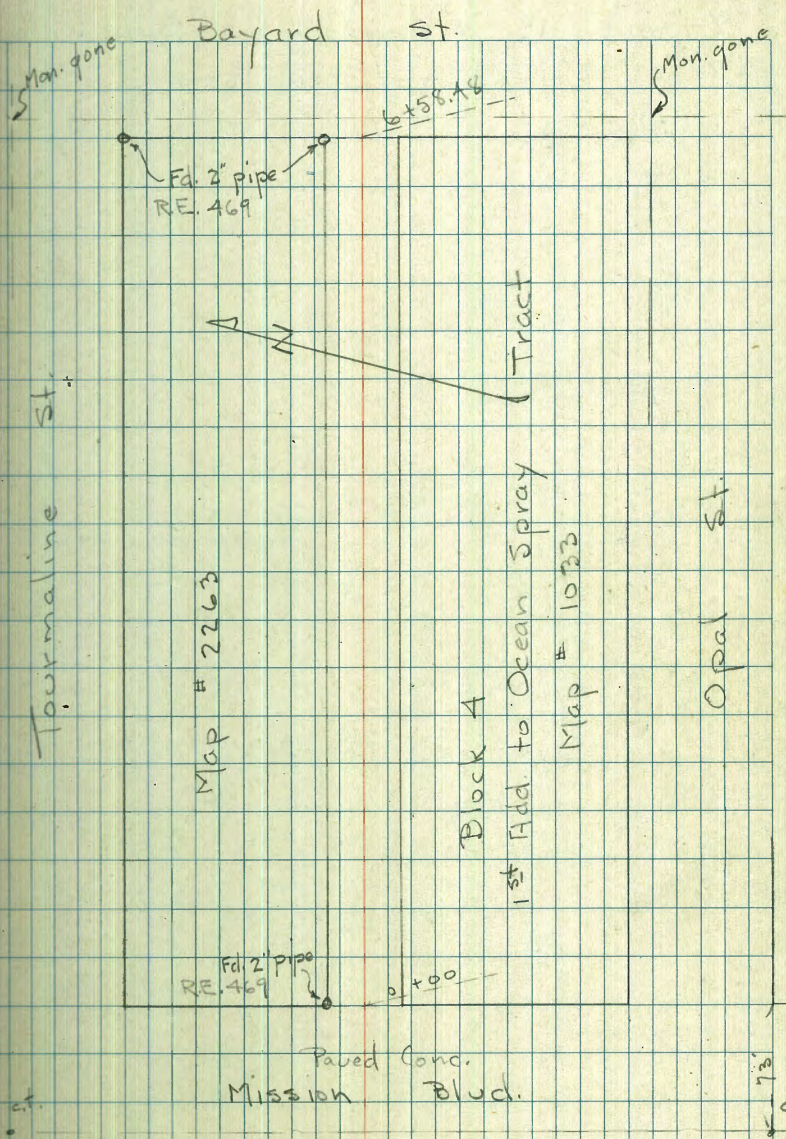
Indexed  
O.S.K.

1

X-Sect. Alley 20' wide N. of Block  
4 - 1<sup>st</sup> Add. to Ocean Spray Tract.

# 592  
W.O. 230

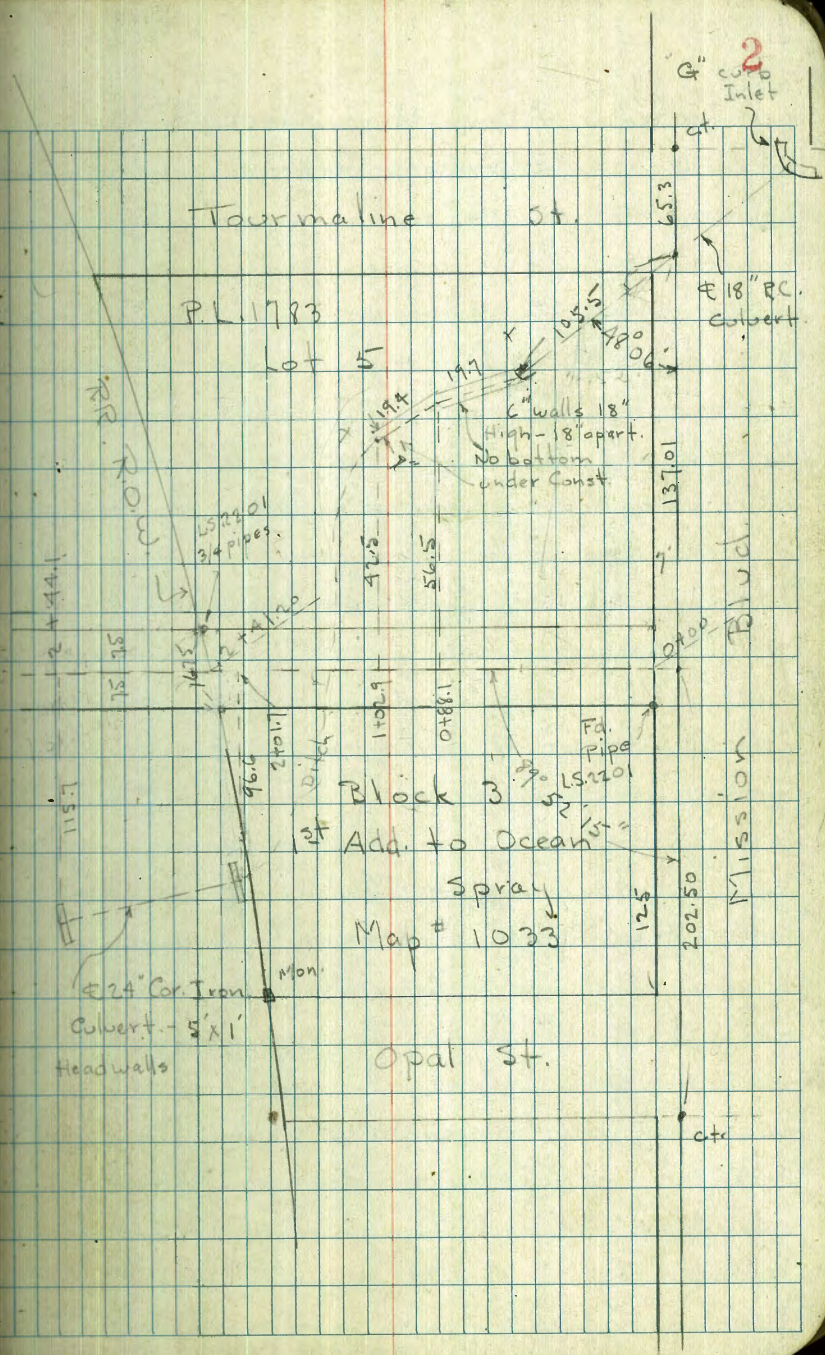
11-1-46  
Osborne -





X-Sect. 15' Alley N. of Block  
3 in 1st Add. to Ocean spray.

4+00



Tourmaline St.

P.L. 1783

Lot 5

G<sup>2</sup> curb Inlet

18" RC  
Culvert

18" walls  
High - 18" apart.  
No bottom  
under Const.

RR ROAD

LS2201  
34 Pipes

42.5

56.5

137.01

Mission Blvd.

142.5

175.7

192.9

210.1

227.5

244.1

Block 3  
1st Add. to Ocean  
Spray

Fd. Pipe

Map # 1033

12.5

202.50

Mission Blvd.

24" Cor. Iron  
Culvert - 5' x 1'  
Headwalls

Man.

Opal St.

ctd



X-Sect. 20' Alley N. of Block 4  
1st Add. to Ocean Spray Tract.

1+08 - 9.1 Rt = E P. pole

1+00

0+57 - 9.8 Lt = # 6' Rough Conc. Slab for incinerator

0+20

0+00 = E.L. Mission Blvd. = edge Conc. pave

0-10 = E. cb. Mission Blvd

B.M.		7.35	84.62	2" Pipe 10' Lt. 0+00
	12.05	91.97	0.16	79.92
B.M.	8.11	80.08		71.97
				sw Top Hyd. Lining + Mission Blvd

Lt = N.

Rt = S.

3

87.6

AA  
0

87.05

1.92  
9.8 Top  
edge Conc.

85.9

0

84.05

7.92

Top cb. + gut.  
end Ret.

83.77

8.20

2.5

gut.

83.42

8.55

1.0

gut.

87.7

AA

86.8

5.2

85.5

0

83.64

8.33

83.15

8.82

91.97

87.5

AA

86.6

5.4

85.7

0

83.51

8.46

Top cb. + gut.  
end Ret.

82.89

9.08

gut.

86.8

AA

86.6

5.4

85.7

0

83.51

8.46

Top cb. + gut.  
end Ret.

82.44

9.25

gut.



4+08 - 9.7 Rt. = ± P. pole

4+00

T.P. 8.90 100.48 0.39 91.58

3+50

3+00

2+59 - 9.4 Rt. = ± P. pole

2+50

2+00

1+50

92.4

8.1  
- 0

91.4

0.6  
- 0

90.9

1.1  
- 0

90.9

0.6  
- 0

89.6

2.4  
- 0

88.6

3.4  
- 0

92.6

7.9  
- 0

91.4

0.6  
- 0

90.7

1.3  
- 0

90.1

1.9  
- 0

89.4

2.6  
- 0

88.6

3.4  
- 0

92.5

8.0  
- 0

91.2

0.8  
- 0

90.4

1.6  
- 0

89.6

2.4  
- 0

89.1

2.9  
- 0

88.2

3.8  
- 0

91.3

9.2  
- 0

91.2

0.8  
- 0

90.4

1.6  
- 0

89.6

2.4  
- 0

88.5

3.6  
- 0

Level out

level out

91.97



check - 7.58 84.61 2" pipe at od.

3.21 92.19

T.P. 3.37 92.27 11.58 88.90

6+58.48 91 = W.L. Bayard - 9.5 ft = end fence

6+37-99 Rt = N.W. Cor. Conc. slab for Gar.

6+30

6+08-102 ft = beg board fence

6+00

5+58-93' Rt. = P pole

5+50

5+00

4+50

	7	8	Rt.
	98.2	98.3	97.70
	2.3 -0.1	2.3 -0.1	2.75 -0.05 = Cor. Conc. slab.
	97.9	97.0	97.1
	0.0 -0.1	0.0 -0.1	0.4 -0.1
	96.7	96.7	97.0
	0.0 -0.1	0.0 -0.1	0.4 -0.1
	95.8	95.7	95.9
	0.0 -0.1	0.0 -0.1	0.4 -0.1
	95.2	95.2	95.9
	0.0 -0.1	0.0 -0.1	0.4 -0.1
level out	93.7	93.7	94.8
	0.0 -0.1	0.0 -0.1	0.4 -0.1
	100.48		

97.71  
0.0  
-0.1 = Top  
conc.







1+62.7 - 4.8' Rt = S.W. Cor. of House - Conc. floor  
basement storeroom

1+50

1+30

1+26 - 9.9 Rt = S.E. Cor. frame House - Conc. found.  
wall + Conc. floor in little basement room.

1+22

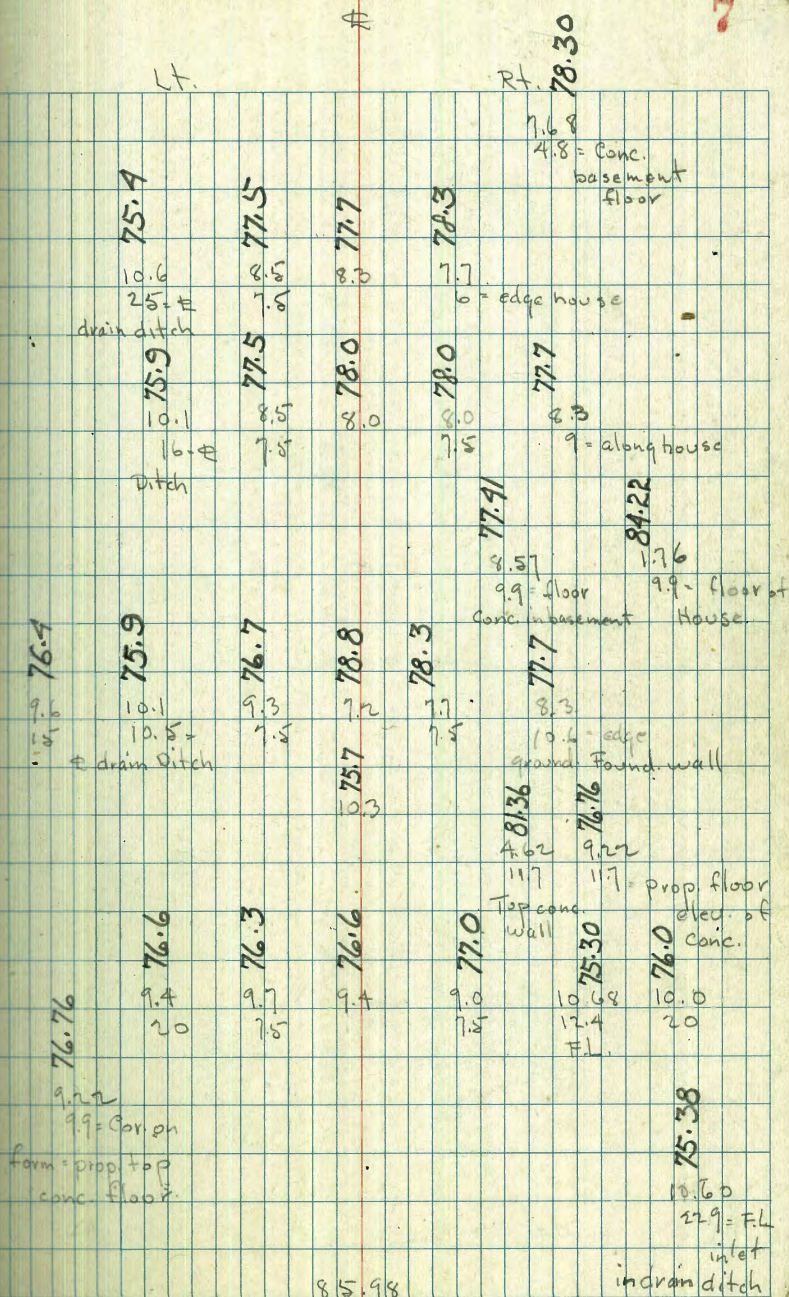
1+16 =  $\phi$  of drain ditch <sup>1/8" wide</sup> on  $\phi$  Alley

1+15 - 11.7 Rt = E. side of Conc. found. wall to  
prop. Gar.

1+11.5 - 12.4 Rt = outlet 12" culvert

1+09.8 - 9.9 Lt = N.W. Cor. prop. 4 car gar.

1+08 - 22.9 Rt = inlet of 12" transite pipe for culvert  
under approach to prop. Gar.





check starting B.M.

10.32 71.97

2+60 - for Profile beyond end of Alley

2+45 - opp. car. on Rt.

2+120 =  $\phi$  alley + E.L. RR. R.O.W.

2+37.5 = opp. car. on Lt.

2+15

2+03 - 2.6 Lt.  $\phi$  Sewer M.H.

2+00

T.P. 4.44 82.29 8.13 77.85

74.0	77.7	77.7	77.4	77.5	77.8	77.5	77.8
8.3 2.5	4.6 0	4.6 2.5	4.9	4.8 7.5	4.8 7.5	4.8 7.5	4.8 7.5
73.8	77.5	77.8	77.9	77.9	77.9	78.1	78.1
8.6 3.0	4.8 5	4.8 7.5	4.4	4.4 7.5	4.4 7.5	4.4 7.5	4.4 7.5
78.1	78.6	78.6	78.8	78.9	78.9	79.3	79.3
4.2 5	4.7 5	4.7 5	4.5	4.4 5	4.4 5	4.0 5	4.0 5
77.5	78.2	78.18	78.18	79.4	79.4	80.4	80.4
4.8 5	4.1 5	4.1	4.1	4.9 5	4.9 5	4.9 5	4.9 5
		82.29	82.29				
		85.98	85.98				



Additional Notes for Culverts  
near Alley in Block 3 - W. of Mission  
Blvd. also prod. & W. to 4+00 for  
add. x-sections - See sketch - P 2.

70.  
12-13-46 Lt.

Rt.

2+44.1 - 115.7 Lt. = & of outlet 24" CI Culvert

67.53  
10.94  
Top wall  
64.60  
13.87  
115.7 = FL pipe

2+01.7 - 96.6 Lt. & inlet of 24" Corr. Iron culvert  
& & of 1' Headwall - 5' Long

70.75  
77.2  
96.6  
Top wall  
67.99  
10.48  
96.6 = FL pipe

T.P. 2.40 78.47 10.98 76.07

78.47

Ditch runs from here to same as shown in  
first notes - P 7

42.5 Rt.

1+02.9 & walls under Const. only - N. wall in.

78.36  
86.9  
Top wall  
78.15  
8.90  
Top N. wall  
76.45  
10.6  
56.5 = Dirt  
Bottom  
76.05

0+88.1 - 56.5 Rt. = & - 2 6" walls - 18" apart.

FL of 18" RC pipe - outlet

95.5 = FL  
See sketch

B.M. 2.43 87.05

84.62 - 2' pipe  
N.L. Alley + E.L.  
Mission

87.05



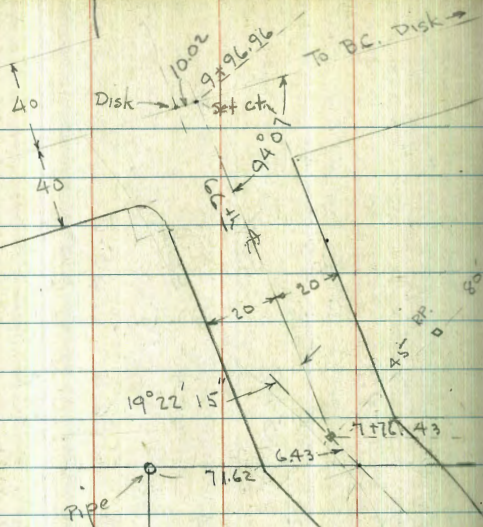




Indexed  
C.S.K.

sky line  
e

Dr.



See Drawing 6691-L

1687-63

T.P. 24-65

Location + X-Sept. of 66th + Opening  
To Leghorn + Leghorn. to Detroit. 10

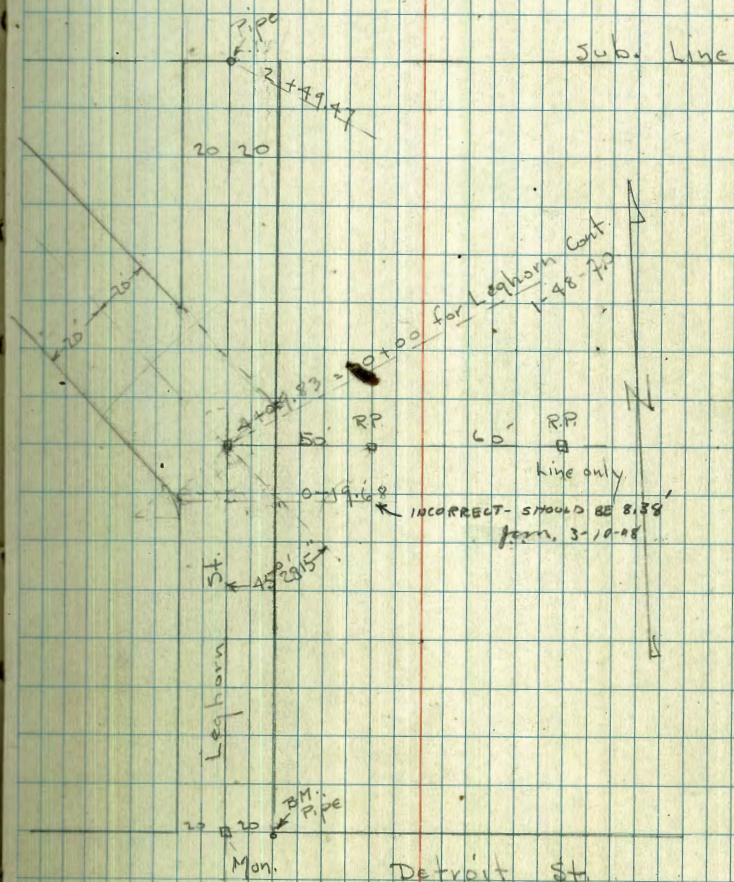
1-16+17-47

# 729

W.O. 210

Osborne  
Harwin  
Warrell  
Smith

RP  
Line only









4+09.83 = Ang. in  $\$$  Leghorn + Opening

3+94 = opp. PC. Prop. curve on Lt

3+88 = 25.2 Rt. = end  $\$$  Trees

3+50

T.P 13.07 404.91 4.71 391.84

3+00 = 26.6 Rt. = Beg.  $\$$  Line of Small trees

2+81 = 18 Rt.  $\$$  Guy

2+63 = 17.2 Rt. =  $\$$  P. pole

1+50 = Dirt Drive up Hill to Rt. for House

2+00

1+50

1+09 = 11.5 Rt. =  $\$$  P. pole

379.1	379.1	390.4	390.4	391.1	391.1
380.7	380.7	390.4	390.4	391.1	391.1
382.0	382.0	390.4	390.4	391.1	391.1
384.3	384.3	390.4	390.4	391.1	391.1
385.3	385.3	390.4	390.4	391.1	391.1
387.0	387.0	390.4	390.4	391.1	391.1
387.6	387.6	390.4	390.4	391.1	391.1
389.0	389.0	390.4	390.4	391.1	391.1
390.1	390.1	390.4	390.4	391.1	391.1
394.7	394.7	390.4	390.4	391.1	391.1
394.9	394.9	390.4	390.4	391.1	391.1
397.3	397.3	390.4	390.4	391.1	391.1
397.8	397.8	390.4	390.4	391.1	391.1
402.3	402.3	390.4	390.4	391.1	391.1
402.4	402.4	390.4	390.4	391.1	391.1
406.9	406.9	390.4	390.4	391.1	391.1
409.0	409.0	390.4	390.4	391.1	391.1
409.8	409.8	390.4	390.4	391.1	391.1
399.88	399.88	390.4	390.4	391.1	391.1
382.2	382.2	390.4	390.4	391.1	391.1
386.2	386.2	390.4	390.4	391.1	391.1
404.91	404.91	390.4	390.4	391.1	391.1
382.7	382.7	390.4	390.4	391.1	391.1
385.5	385.5	390.4	390.4	391.1	391.1
388.8	388.8	390.4	390.4	391.1	391.1
390.9	390.9	390.4	390.4	391.1	391.1
394.9	394.9	390.4	390.4	391.1	391.1
397.6	397.6	390.4	390.4	391.1	391.1
397.3	397.3	390.4	390.4	391.1	391.1

~~396.55~~







check Starting B.M. 9.46 389.50 389.49

T.P. 5.32 398.96 10.67 393.64

9+96.96 =  $\Phi$  Skyline

9+87.5 = S. side - 20' Strip Conc. pave.

9+74 - 4' Rt. = end - E. edge Cabbage patch

9+74 - 6.4 Rt. = Meter - end 1 1/2" pipe

9+57.8 = S.L. Skyline Dr. - Sect. on S.L. Skyline

9+50 - 6.6 Rt. = pipe + 5' Rt. = edge Cabbage patch

9+13 - 4.9 Rt. =  $\Phi$  2' Conc. walk

9+00 - 2' <sup>E. edge</sup> Rt. = 1/2 Cabbage patch - 4.8 Rt. = pipe

8+50 - 1' Rt. = pipe - on ground + edge Cabbages on  $\Phi$

8+46 - 1' Rt. = T. in stub below 6.64 Top  
from Main line

8+42 - 16.5 Rt. = end 1 1/2" stub 8.79 Top

8+00 - 5' Lt. = Beg. Cabbage patch + 2.7 Lt. = pipe

7+82 - 3.8 Lt. = Ang. in water pipe on ground

7+78.5 =  $\Phi$  1 1/2" Water pipe 9.41 Top pipe

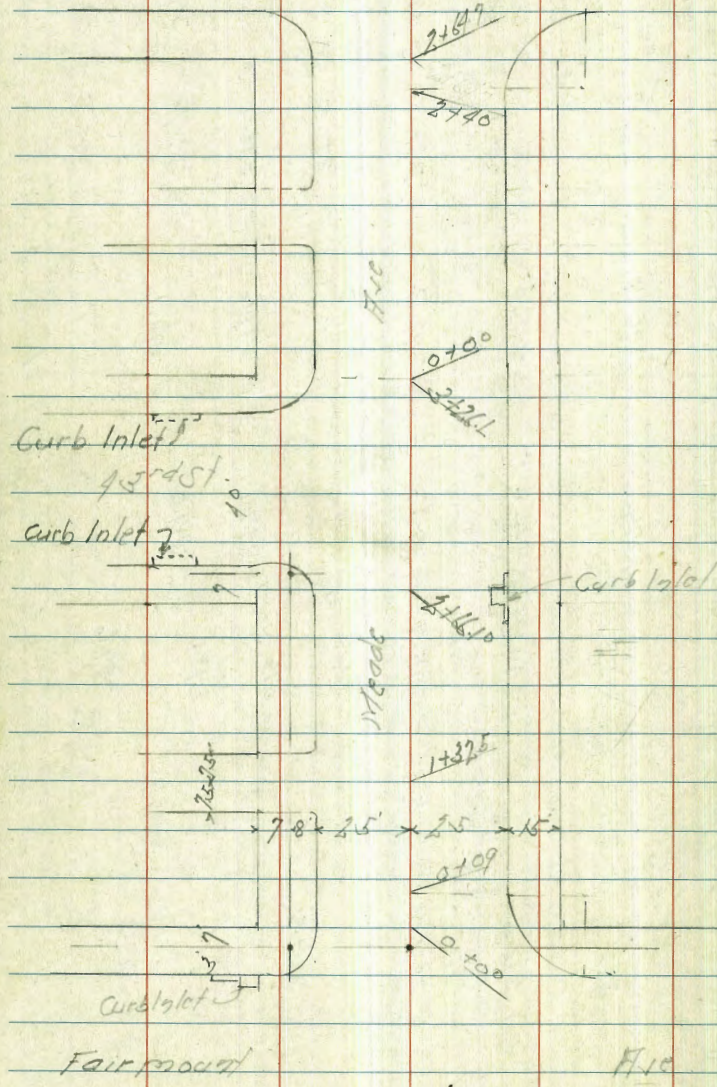
7+76.43 = Ang. in R - Sect. on split.

7+70 - 9' Lt. = end Tomatoes

396.06	Lt.	396.99	397.11	397.31	397.56	397.67	397.69
8.25		7.32	7.20	6.8	6.75	6.6	6.2
0		40	0	0	0	40	0
396.7		397.1	397.5	397.8	397.5	398.0	397.67
1.6		2.2	1.8	1.0	1.5	1.5	1.6
40		0	0	0	0	40	0
396.4		396.8	397.3	397.5	397.6	398.6	399.81
1.9		2.5	1.0	1.2	1.1	1.1	1.1
40		0	0	0	0	40	0
394.6		395.5	396.3	397.1	397.1	399.2	399.81
0.7		0.8	0.8	0.8	0.8	0.7	0.9
40		0	0	0	0	40	0
393.5		394.6	395.9	396.2	396.2	397.6	399.6
10.8		1.1	1.4	1.1	1.1	1.1	1.1
40		0	40	0	0	40	40
391.2		392.3	395.3	395.6	396.7	399.7	399.7
2.1		1.1	0	1.1	1.1	1.1	1.1
40		0	0	0	0	40	0
390.8		392.2	395.01	395.5	396.7	399.7	399.7
2.7		1.1	0	1.1	1.1	1.1	1.1
40		0	0	0	0	40	0
390.8		392.2	395.01	395.5	396.7	399.7	399.7
2.7		1.1	0	1.1	1.1	1.1	1.1
40		0	0	0	0	40	0
404.31							

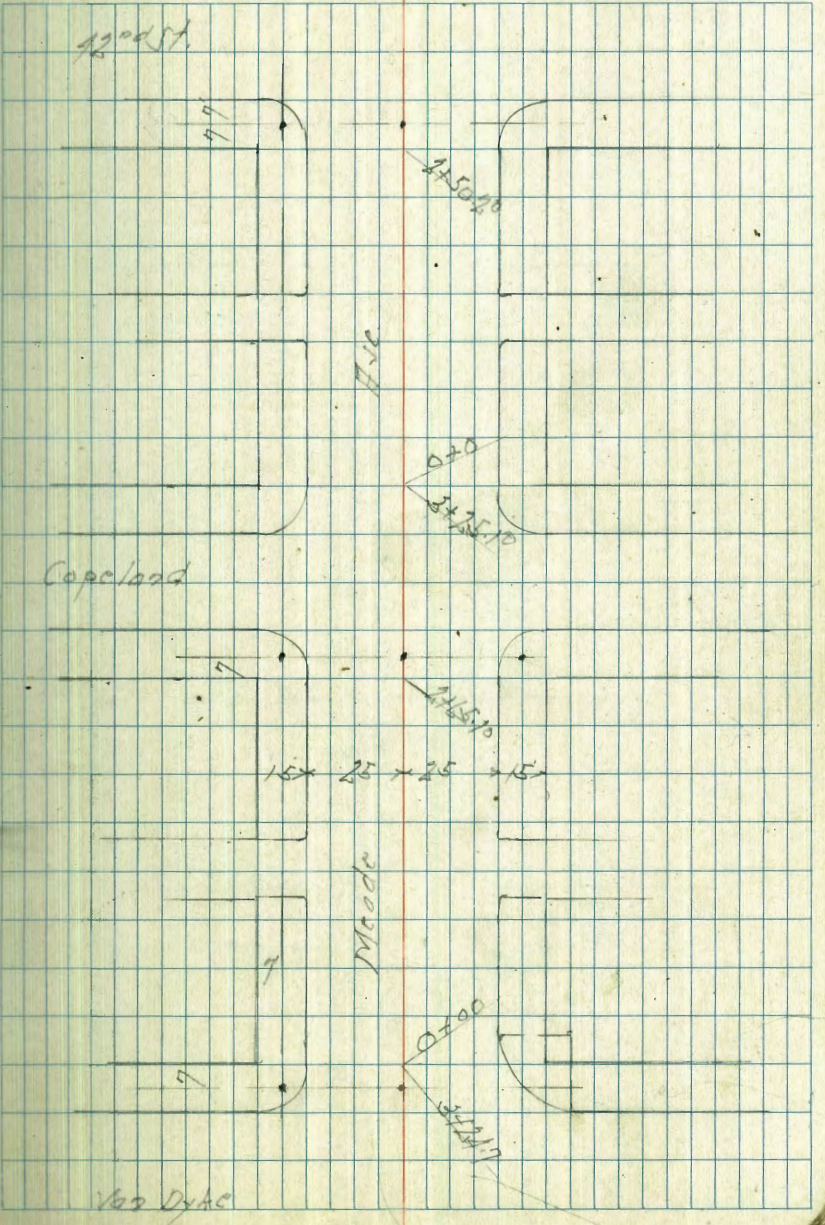


Cross Section Meade Ave.  
 Fairmount Ave. West  
 Levels Page 17  
 Van Dyke



Indexed  
 C.S.K.

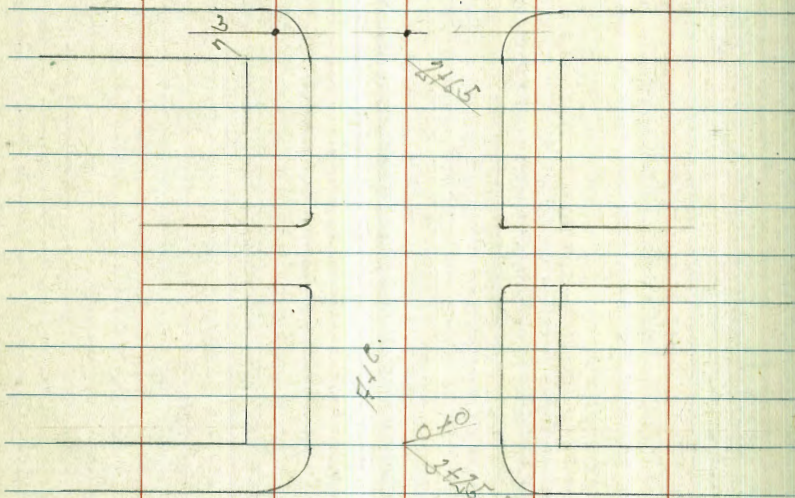
April 11-47  
 Sisson  
 McCoy  
 Haddad  
 Allen



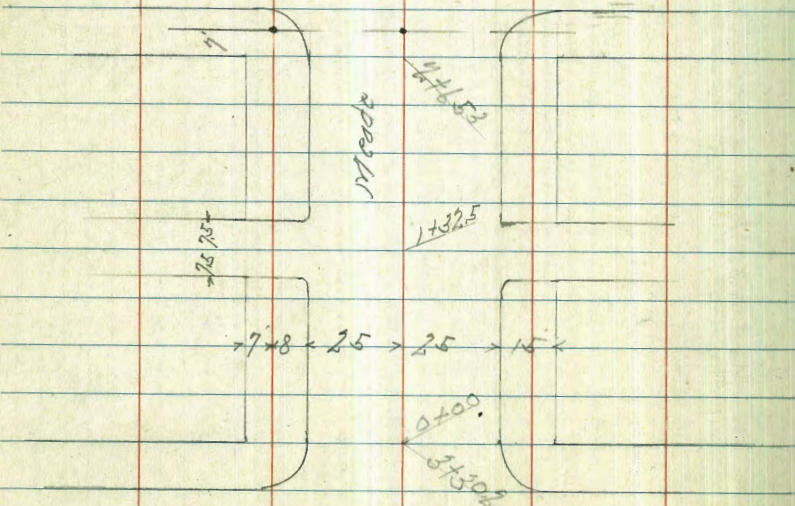


Moode Ave

41st St.

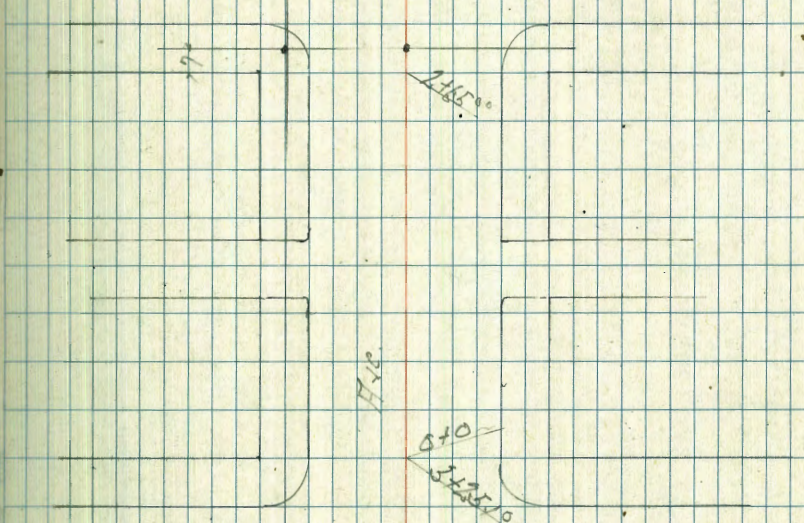


Marlborough

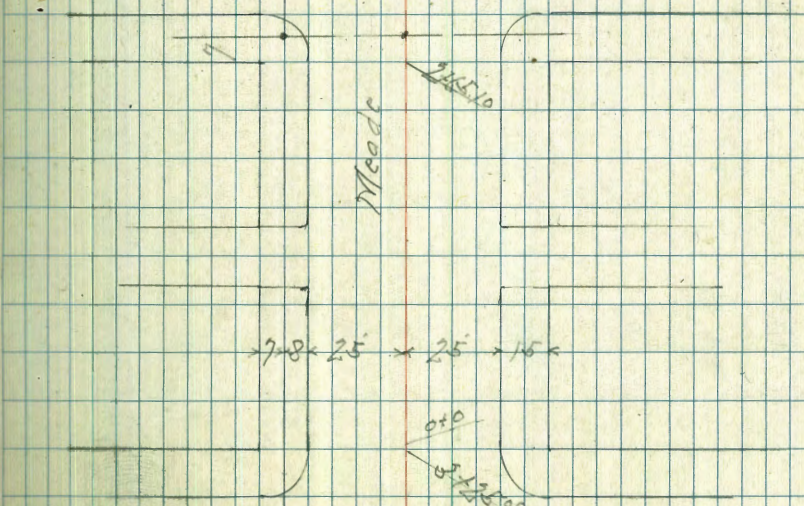


12th St.

41st St.



Central Ave



12th St.



Cross Section Meade Hvc.  
Fairmount Hvc. York

W.O. 60108

Sketch Page 15

1+25 = F.L. Alley to South

613  
90.03

1+0

0+50

0+09 = C.B.C. on Rt.

0+0 = H.L. Fairmount

0-10 = West Curb Line Fairmount Hvc.

BM 3.00 3.5540

3.52.90

H.M.B.P.  
Meade Hvc.  
Fairmount

21:5

648 90.03	649 90.03	650 90.03	651 90.03	652 90.03	653 90.03	654 90.03	655 90.03	656 90.03	657 90.03	658 90.03	659 90.03	660 90.03	661 90.03	662 90.03	663 90.03	664 90.03	665 90.03	666 90.03	667 90.03	668 90.03	669 90.03	670 90.03	671 90.03	672 90.03	673 90.03	674 90.03	675 90.03	676 90.03	677 90.03	678 90.03	679 90.03	680 90.03	681 90.03	682 90.03	683 90.03	684 90.03	685 90.03	686 90.03	687 90.03	688 90.03	689 90.03	690 90.03	691 90.03	692 90.03	693 90.03	694 90.03	695 90.03	696 90.03	697 90.03	698 90.03	699 90.03	700 90.03	701 90.03	702 90.03	703 90.03	704 90.03	705 90.03	706 90.03	707 90.03	708 90.03	709 90.03	710 90.03	711 90.03	712 90.03	713 90.03	714 90.03	715 90.03	716 90.03	717 90.03	718 90.03	719 90.03	720 90.03	721 90.03	722 90.03	723 90.03	724 90.03	725 90.03	726 90.03	727 90.03	728 90.03	729 90.03	730 90.03	731 90.03	732 90.03	733 90.03	734 90.03	735 90.03	736 90.03	737 90.03	738 90.03	739 90.03	740 90.03	741 90.03	742 90.03	743 90.03	744 90.03	745 90.03	746 90.03	747 90.03	748 90.03	749 90.03	750 90.03	751 90.03	752 90.03	753 90.03	754 90.03	755 90.03	756 90.03	757 90.03	758 90.03	759 90.03	760 90.03	761 90.03	762 90.03	763 90.03	764 90.03	765 90.03	766 90.03	767 90.03	768 90.03	769 90.03	770 90.03	771 90.03	772 90.03	773 90.03	774 90.03	775 90.03	776 90.03	777 90.03	778 90.03	779 90.03	780 90.03	781 90.03	782 90.03	783 90.03	784 90.03	785 90.03	786 90.03	787 90.03	788 90.03	789 90.03	790 90.03	791 90.03	792 90.03	793 90.03	794 90.03	795 90.03	796 90.03	797 90.03	798 90.03	799 90.03	800 90.03	801 90.03	802 90.03	803 90.03	804 90.03	805 90.03	806 90.03	807 90.03	808 90.03	809 90.03	810 90.03	811 90.03	812 90.03	813 90.03	814 90.03	815 90.03	816 90.03	817 90.03	818 90.03	819 90.03	820 90.03	821 90.03	822 90.03	823 90.03	824 90.03	825 90.03	826 90.03	827 90.03	828 90.03	829 90.03	830 90.03	831 90.03	832 90.03	833 90.03	834 90.03	835 90.03	836 90.03	837 90.03	838 90.03	839 90.03	840 90.03	841 90.03	842 90.03	843 90.03	844 90.03	845 90.03	846 90.03	847 90.03	848 90.03	849 90.03	850 90.03	851 90.03	852 90.03	853 90.03	854 90.03	855 90.03	856 90.03	857 90.03	858 90.03	859 90.03	860 90.03	861 90.03	862 90.03	863 90.03	864 90.03	865 90.03	866 90.03	867 90.03	868 90.03	869 90.03	870 90.03	871 90.03	872 90.03	873 90.03	874 90.03	875 90.03	876 90.03	877 90.03	878 90.03	879 90.03	880 90.03	881 90.03	882 90.03	883 90.03	884 90.03	885 90.03	886 90.03	887 90.03	888 90.03	889 90.03	890 90.03	891 90.03	892 90.03	893 90.03	894 90.03	895 90.03	896 90.03	897 90.03	898 90.03	899 90.03	900 90.03	901 90.03	902 90.03	903 90.03	904 90.03	905 90.03	906 90.03	907 90.03	908 90.03	909 90.03	910 90.03	911 90.03	912 90.03	913 90.03	914 90.03	915 90.03	916 90.03	917 90.03	918 90.03	919 90.03	920 90.03	921 90.03	922 90.03	923 90.03	924 90.03	925 90.03	926 90.03	927 90.03	928 90.03	929 90.03	930 90.03	931 90.03	932 90.03	933 90.03	934 90.03	935 90.03	936 90.03	937 90.03	938 90.03	939 90.03	940 90.03	941 90.03	942 90.03	943 90.03	944 90.03	945 90.03	946 90.03	947 90.03	948 90.03	949 90.03	950 90.03	951 90.03	952 90.03	953 90.03	954 90.03	955 90.03	956 90.03	957 90.03	958 90.03	959 90.03	960 90.03	961 90.03	962 90.03	963 90.03	964 90.03	965 90.03	966 90.03	967 90.03	968 90.03	969 90.03	970 90.03	971 90.03	972 90.03	973 90.03	974 90.03	975 90.03	976 90.03	977 90.03	978 90.03	979 90.03	980 90.03	981 90.03	982 90.03	983 90.03	984 90.03	985 90.03	986 90.03	987 90.03	988 90.03	989 90.03	990 90.03	991 90.03	992 90.03	993 90.03	994 90.03	995 90.03	996 90.03	997 90.03	998 90.03	999 90.03	1000 90.03
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355.40

Rt=11

April 17  
14:17  
**17**  
578.00  
378.00  
200.00  
278.00







140

150

0+0 }  
3+26.107 = 4<sup>th</sup> 43<sup>rd</sup> St to South

3+16.10 = WCB 43<sup>rd</sup> to South

2+96.10 = 2<sup>nd</sup> 43<sup>rd</sup> to South

2+77.10 = ECB 43<sup>rd</sup> St to South

35175

640 12.5	348.25	640 12.5	347.75	640 12.5	348.16	640 12.5	348.16
640 12.5	348.80	640 12.5	347.75	640 12.5	347.57	640 12.5	347.57
640 12.5	349.17	640 12.5	347.15	640 12.5	347.75	640 12.5	347.75
640 12.5	349.63	640 12.5	347.90	640 12.5	348.00	640 12.5	348.00
640 12.5	349.89	640 12.5	347.98	640 12.5	347.95	640 12.5	347.95
640 12.5	349.80	640 12.5	347.68	640 12.5	347.59	640 12.5	347.59
640 12.5	349.57	640 12.5	347.17	640 12.5	347.03	640 12.5	347.03
640 12.5	350.10	640 12.5	347.65	640 12.5	347.49	640 12.5	347.49

67

68

69

35145







0 + 23 = Cb EC 029A

020 J  
372477 = W.L. Van Dyke

RM

65 14  
599

359.15

5A 7247  
Moode  
Van Dyke

37147 = W.Cb Van Dyke

+ 747 = W. Van Dyke

+ 747 = F.Cb. Van Dyke

27647 = E.L. Van Dyke

36514

499	357.04	358.77	358.34	357.72	357.65	357.86	357.59	357.36	357.28
25	67	69	71	72	72	73	73	74	74
13	16	16	16	16	16	16	16	16	16
360.27	359.94	358.17	358.38	357.96	357.94	357.86	357.59	357.36	357.28
15	15	15	15	15	15	15	15	15	15
64	65	65	65	65	65	65	65	65	65
359.61	358.82	358.65	358.38	357.96	357.94	357.86	357.59	357.36	357.28
15	15	15	15	15	15	15	15	15	15
15	15	15	15	15	15	15	15	15	15
359.28	359.06	358.92	358.43	357.96	357.94	357.86	357.59	357.36	357.28
15	15	15	15	15	15	15	15	15	15
15	15	15	15	15	15	15	15	15	15
359.76	359.12	358.95	358.44	357.94	357.94	357.86	357.59	357.36	357.28
15	15	15	15	15	15	15	15	15	15
15	15	15	15	15	15	15	15	15	15
359.45	358.96	358.74	358.30	357.86	357.86	357.86	357.59	357.36	357.28
15	15	15	15	15	15	15	15	15	15
15	15	15	15	15	15	15	15	15	15
359.09	358.58	358.44	358.19	357.86	357.86	357.86	357.59	357.36	357.28
15	15	15	15	15	15	15	15	15	15
15	15	15	15	15	15	15	15	15	15
359.65	359.30	359.19	358.06	357.86	357.86	357.86	357.59	357.36	357.28
15	15	15	15	15	15	15	15	15	15
15	15	15	15	15	15	15	15	15	15
359.76	359.86	359.86	358.06	357.86	357.86	357.86	357.59	357.36	357.28
15	15	15	15	15	15	15	15	15	15
15	15	15	15	15	15	15	15	15	15

36514



















0.20 J  
2+30.207 = 274.92207

0 + 50

1 + 0

1 + 25 = F.L. 7/10/2

1 + 32.5 = 2. 7/10/2

1 + 40 = M.L. 7/10/2

270.29

365.78  
45  
40-cb

365.07	365.16	365.35	365.49	365.78	365.25
364.68	364.81	364.95	365.02	365.51	365.53
365.17	365.01	365.19	365.27	365.28	365.12
365.19	365.13	365.22	365.28	365.33	365.33
364.86	364.95	365.06	365.12	365.10	365.10
364.32	364.52	364.66	364.85	364.81	364.87
364.66	364.94	365.14	365.15	365.23	365.36
					365.35
					365.58



2 + 95.30 = 2 Marlborough

2 + 75.30 = ECB of Marlborough

2 + 65.30 = 2 Marlborough

2 + 50

2 + 0

1 + 50

370.39

134 10	366.04	366.05
135 15	365.48	366.04
136 15	365.66	366.09
137 15	365.94	
138 15	365.89	366.05
139 15	365.66	365.77
140 15	365.36	365.40
141 15	365.32	365.59
142 15	365.91	365.91
143 15	365.93	
144 15	365.63	
145 15	365.54	
146 15	365.15	
147 15	365.26	
148 15	365.96	
149 15	365.76	
150 15	365.91	

570.39  
10  
60  
DRIVE

570.39



1+32.5 = 2 Alley

1+25 = E.L. Alley

TP 1.50 372.87 4.02 366.37

1+0

0+50

0+0 J  
3725.307 = M.L. Marlborough

BM 4.37 366.82  
M.L. 87  
Mead +  
Marlborough  
366.01

3+15.36 = M.C. e/ Mar 160094

370.39

4.13 12.5	366.26	4.17 12.5	366.13	4.18 12.5	366.57	4.18 12.5	366.91	4.18 12.5	367.12	4.18 12.5	366.94
4.16 12.5	365.63	4.17 12.5	365.68	4.15 12.5	366.24	4.18 12.5	366.58	4.18 12.5	367.07	4.18 12.5	366.95
4.17 12.5	365.82	4.18 12.5	366.14	4.15 12.5	366.45	4.18 12.5	366.74	4.18 12.5	366.70	4.18 12.5	366.75
4.18 12.5	366.09	4.17 12.5	366.12	4.18 12.5	366.46	4.18 12.5	366.79	4.18 12.5	366.85	4.18 12.5	366.89
4.18 12.5	365.85	4.17 12.5	365.94	4.18 12.5	366.21	4.18 12.5	366.50	4.18 12.5	366.57	4.18 12.5	366.91
4.18 12.5	365.54	4.18 12.5	365.54	4.17 12.5	365.12	4.18 12.5	366.10	4.18 12.5	366.16	4.18 12.5	366.21
4.19 12.5	365.48	4.18 12.5	366.02	4.14 12.5	366.25	4.18 12.5	366.64	4.18 12.5	366.72	4.18 12.5	366.47
4.19 12.5	366.03	4.17 12.5		4.14 12.5		4.18 12.5		4.18 12.5	367.23	4.18 12.5	

370.39







TP 513 378.62 468 358.19

140

0+50

0+15

0+0 ↓  
3+257 = W.L. 41500

B.M. out

W.L. 41500  
367.74

3+15 = W.C. 6 of 41500

3+95 = 41500

378.87

4.

4

PT

30

119 40.55	367.07	517 40.55	367.74	511 40.55	367.76	511 40.55	367.74	513 40.55	367.74
538 40.55	367.49	538 40.55	366.89	538 40.55	366.89	538 40.55	366.89	538 40.55	367.62
515 40.55	367.72	515 40.55	366.96	515 40.55	366.96	515 40.55	366.96	515 40.55	367.71
490	367.97	490	367.05	490	367.05	490	367.05	490	367.67
509 40.55	367.78	509 40.55	367.08	509 40.55	367.08	509 40.55	367.08	509 40.55	367.62
537 40.55	367.50	537 40.55	367.17	537 40.55	367.17	537 40.55	367.17	537 40.55	367.65
458 40.55	367.99	458 40.55	367.22	458 40.55	367.22	458 40.55	367.22	458 40.55	367.65
			367.68		367.68		367.68		367.68

378.87



1+50

2+0

1+50

1+40 = 1/2 Hilly

1+325 = 1/2 Hilly

1+25 = 1/2 Hilly

36P.32

5.30  
10-C6

373.62

36P.11	5.13 10-C6	367.86	5.13 10-C6	36P.19	5.13 10-C6	367.99	5.13 10-C6	367.89	5.13 10-C6	367.82
36P.13	5.14 10-C6	367.60	5.14 10-C6	36P.08	5.14 10-C6	367.57	5.14 10-C6	367.42	5.14 10-C6	367.35
367.54	5.19 10-C6	367.60	5.19 10-C6	367.65	5.19 10-C6	367.80	5.19 10-C6	367.71	5.19 10-C6	367.66
367.79	5.23 10-C6	367.81	5.23 10-C6	367.85	5.23 10-C6	368.02	5.23 10-C6	368.03	5.23 10-C6	368.02
367.96	5.24 10-C6	367.93	5.24 10-C6	367.85	5.24 10-C6	368.02	5.24 10-C6	368.03	5.24 10-C6	368.02
367.78	5.28 10-C6	367.83	5.28 10-C6	367.84	5.28 10-C6	367.87	5.28 10-C6	368.03	5.28 10-C6	367.95
367.62	5.30 10-C6	367.62	5.30 10-C6	367.66	5.30 10-C6	367.67	5.30 10-C6	368.03	5.30 10-C6	367.95
36P.10	5.31 10-C6	367.60	5.31 10-C6	36P.15	5.31 10-C6	367.62	5.31 10-C6	367.81	5.31 10-C6	367.87
36P.04	5.32 10-C6	367.80	5.32 10-C6	367.95	5.32 10-C6	368.13	5.32 10-C6	368.29	5.32 10-C6	368.34
36P.21	5.33 10-C6	367.80	5.33 10-C6	56P.23	5.33 10-C6	56P.23	5.33 10-C6	56P.23	5.33 10-C6	56P.23







1+50

TP 478 373.42 498 368.64

1+40 = H.L. Filley

1+32.5 = H. Filley

1+25 = F.L. Filley

1+0

0+50

373.62

4.

2

Pt

33

181 125.60	36P.60	181 125.60	36P.60	181 125.60	36P.60	181 125.60	36P.60
510 125.60	36P.52	510 125.60	36P.52	510 125.60	36P.52	510 125.60	36P.52
511 125.60	36P.18	511 125.60	36P.18	511 125.60	36P.18	511 125.60	36P.18
512 125.60	36P.59	512 125.60	36P.59	512 125.60	36P.59	512 125.60	36P.59
477	36P.85	477	36P.85	477	36P.85	477	36P.85
479 125.60	36P.83	479 125.60	36P.83	479 125.60	36P.83	479 125.60	36P.83
489 125.60	36P.73	489 125.60	36P.73	489 125.60	36P.73	489 125.60	36P.73
418 125.60	36P.44	418 125.60	36P.44	418 125.60	36P.44	418 125.60	36P.44
513 125.60	36P.81	513 125.60	36P.81	513 125.60	36P.81	513 125.60	36P.81
514 125.60	36P.81	514 125.60	36P.81	514 125.60	36P.81	514 125.60	36P.81
515 125.60	36P.62	515 125.60	36P.62	515 125.60	36P.62	515 125.60	36P.62
516 125.60	36P.24	516 125.60	36P.24	516 125.60	36P.24	516 125.60	36P.24
517 125.60	36P.56	517 125.60	36P.56	517 125.60	36P.56	517 125.60	36P.56
483	36P.79	483	36P.79	483	36P.79	483	36P.79
494 125.60	36P.68	494 125.60	36P.68	494 125.60	36P.68	494 125.60	36P.68
418 125.60	36P.44	418 125.60	36P.44	418 125.60	36P.44	418 125.60	36P.44
418 125.60	36P.60	418 125.60	36P.60	418 125.60	36P.60	418 125.60	36P.60
445 125.60	36P.17	445 125.60	36P.17	445 125.60	36P.17	445 125.60	36P.17
481 125.60	36P.81	481 125.60	36P.81	481 125.60	36P.81	481 125.60	36P.81
480 125.60	36P.82	480 125.60	36P.82	480 125.60	36P.82	480 125.60	36P.82
511 125.60	36P.28	511 125.60	36P.28	511 125.60	36P.28	511 125.60	36P.28
512 125.60	36P.59	512 125.60	36P.59	512 125.60	36P.59	512 125.60	36P.59
170	36P.92	170	36P.92	170	36P.92	170	36P.92
483 125.60	36P.79	483 125.60	36P.79	483 125.60	36P.79	483 125.60	36P.79
494 125.60	36P.66	494 125.60	36P.66	494 125.60	36P.66	494 125.60	36P.66
433 125.60	36P.29	433 125.60	36P.29	433 125.60	36P.29	433 125.60	36P.29
418 125.60	36P.50	418 125.60	36P.50	418 125.60	36P.50	418 125.60	36P.50
418 125.60	36P.60	418 125.60	36P.60	418 125.60	36P.60	418 125.60	36P.60
515 125.60	36P.56	515 125.60	36P.56	515 125.60	36P.56	515 125.60	36P.56
516 125.60	36P.18	516 125.60	36P.18	516 125.60	36P.18	516 125.60	36P.18
517 125.60	36P.49	517 125.60	36P.49	517 125.60	36P.49	517 125.60	36P.49
183	36P.79	183	36P.79	183	36P.79	183	36P.79
487 125.60	36P.75	487 125.60	36P.75	487 125.60	36P.75	487 125.60	36P.75
503 125.60	36P.59	503 125.60	36P.59	503 125.60	36P.59	503 125.60	36P.59
428 125.60	36P.34	428 125.60	36P.34	428 125.60	36P.34	428 125.60	36P.34
418 125.60	36P.50	418 125.60	36P.50	418 125.60	36P.50	418 125.60	36P.50
418 125.60	36P.60	418 125.60	36P.60	418 125.60	36P.60	418 125.60	36P.60

373.62



2+05 = 40th St.

2+90

2+75 = E.C. of 40th St.

2+65.00 = E.C. of 40th St.

2+50

2+0

37812

4

29

pt

505 10	36P.26	505 10	36P.17	505 10	36P.16	505 10	36P.22	505 10	36P.39	505 10	36P.179	505 10	36P.90	505 10	36P.84	505 10	36P.50
487 5	36P.46	487 5	367.58	487 5	367.70	487 5	367.74	487 5	367.84	487 5	367.82	487 5	367.94	487 5	367.91	487 5	369.49
461 25	36P.70	461 25	367.80	461 25	36P.15	461 25	36P.29	461 25	36P.39	461 25	36P.15	461 25	369.02	461 25	36P.84	461 25	369.50
405	36P.77	405	36P.58	405	36P.78	405	36P.82	405	36P.79	405	36P.82	405	369.02	405	36P.84	405	369.50
412 25	36P.28	412 25	36P.80	412 25	369.00	412 25	369.02	412 25	36P.90	412 25	369.02	412 25	369.02	412 25	36P.84	412 25	369.50
387 5	36P.47	387 5	36P.94	387 5	36P.05	387 5	369.01	387 5	36P.84	387 5	369.01	387 5	369.01	387 5	36P.84	387 5	369.50
387 5	36P.65	387 5	369.10	387 5	369.57	387 5	369.49	387 5	369.50	387 5	369.49	387 5	369.49	387 5	369.49	387 5	369.50
387 5	36P.61	387 5	369.16	387 5	369.61	387 5	369.57	387 5	369.50	387 5	369.57	387 5	369.50	387 5	369.57	387 5	369.50

528 12



BM

3.54

369.88

11.21 7.25  
17.00  
4.00

0.20

37457 = W.L. 4015 St.

3435 = W.Cb of 4015 St.

3420

37342

367.89

5.53  
15.00

367.90

5.53  
15.00

368.07

5.53  
15.00

367.41

6.01  
15.40

367.34

6.01  
15.40

368.27

6.01  
15.40

368.09

5.53  
12.50

368.08

5.53  
12.50

368.55

4.87  
11.00

368.70

4.72

368.51

4.91

368.86

37343

369.01

4.41  
12.50

368.89

4.41  
12.50

369.18

4.41  
12.50

369.06

4.36  
12.50

369.06

4.36  
12.50

369.37

4.03  
11.50

369.64

3.78  
15.00

369.28

4.40  
15.00

369.64

3.78  
15.00







0+10 Cont.

0+10 = Ely. Cl. Trias

0+00 = E.L. Trias

0+75

0+50

0+25

0+00 = 100' E. East line Trias St

BM = NEBR.  
 Ft. Stockton  
 + Trias

1.65 276.71 — 267.06

264.38 2.33 1.35	264.18 6.53 85	266.51 5.20 95	265.94 5.77 95	266.57 5.14 95	267.68 4.63 95	267.09 4.62 95	267.59 4.12 95
266.00 5.23 77	266.46 5.25 31	266.87 2.84 10.5	266.90 4.81	266.97 4.74 10.5	266.62 5.07 81	267.10 4.61 10.5	
266.51 5.20 66	266.88 5.67 77	266.54 5.17 10.5	266.91 4.80	266.58 5.13 77	266.40 5.31 21	267.06 4.67 66	
266.02 5.67 66	265.45 6.16 21	266.23 5.48 10.5		266.37 5.84 10.5	265.94 5.77 21	266.61 5.10 66	
265.64 6.05 66	265.02 6.65 21	265.77 5.72 10.5	265.99 5.72	266.03 5.68 10.5	265.61 6.20 21	266.19 5.52 66	
265.23 6.48 66	264.67 7.04 21	265.45 6.26 10.5	265.60 6.11	265.61 6.10 10.5	265.16 6.55 21	265.84 5.57 66	
264.72 6.87 77	264.26 7.45 21	265.05 6.60 10.5	265.20 6.57	265.19 6.52 10.5	264.75 6.75 21	265.42 6.22 77	



0+40 Cont.

0+40 Cont.

0+40 Wly. C6. Trias

0+32.5 Wly 1/4 Trias

0+25 = E Trias

0+17.5 Ely 1/4 Trias

271.71

264.84	264.26	264.94	267.18	267.49	267.83
5.87 13.5 TAPCH	7.95 13.5	6.72 8.5	4.43 8.5	4.02 13.5	3.88 15.0
266.31	265.76	265.75	266.48	266.65	266.71
5.40 3.5 TAPCH	5.95 3.5	5.86 3.1	5.28 2.4 TAPCH	5.06 2.1 TAPCH	5.00 3.1
265.96	266.05	266.28	266.63	266.77	266.79
5.75 2.4 E.C. POT	5.69 2.1	5.43 1.4	5.08 1.7	4.94 1	4.92 1
264.65	264.86	266.15	266.73	266.81	266.85
7.06 13.5	6.85 8.5	5.56 3.5	5.08 2.1 10.5	4.90 10.5	4.86 10.5
264.79	265.06	266.3	266.91	266.21	268.15
6.72 13.5	6.65 12.4 E.C. POT	5.2 3.5 dist	4.8 12.4 dist	4.5 3.5 dist	3.56 12.4 S.C. POT
264.74	265.42	266.13	266.71	266.97	267.07
6.97 13.5	6.27 8.5	5.58 4.3 E.C. POT	5.00 10.5	4.79 10.5	4.64 4.2 8.5
					267.59
					267.98
					268.13
					3.78 13.5
					3.88 15.0



1+00

266.11	265.75	266.34	266.62	266.44	266.14
$\frac{5.60}{14}$	$\frac{5.95}{14}$	$\frac{5.77}{6.5}$	$\frac{5.09}{1}$	$\frac{5.27}{8.5}$	$\frac{5.57}{15}$
road	94x	$\frac{1}{4}$		$\frac{1}{16}$	94x in drive

0+75

266.22	265.82	266.53	266.71	266.61	266.22	266.59
$\frac{5.49}{14}$	$\frac{5.87}{14}$	$\frac{5.28}{6.5}$	$\frac{5.00}{1}$	$\frac{5.10}{8.5}$	$\frac{5.47}{16}$	$\frac{5.12}{14}$
oc	94x	$\frac{1}{4}$		$\frac{1}{16}$	94x	$\frac{1}{16}$

0+50 = Wly Line Trias

266.45	266.03	266.54	266.76	266.75	266.58	266.98
$\frac{5.20}{14}$	$\frac{5.68}{14}$	$\frac{5.17}{12}$	$\frac{4.95}{1}$	$\frac{4.96}{14}$	$\frac{5.13}{16}$	$\frac{4.77}{14}$
oc	94x	6.5	roadway	$\frac{1}{16}$	94x	oc



Cross Section Cauts St. (80' wide)  
Hancock to Moore

Sommermeier  
W Moore  
Melter  
Sherman 6/12/47

W.O. 25001

Sat. B.M. Ely 7' Mon  
Cauts + Hancock

1168 12.71

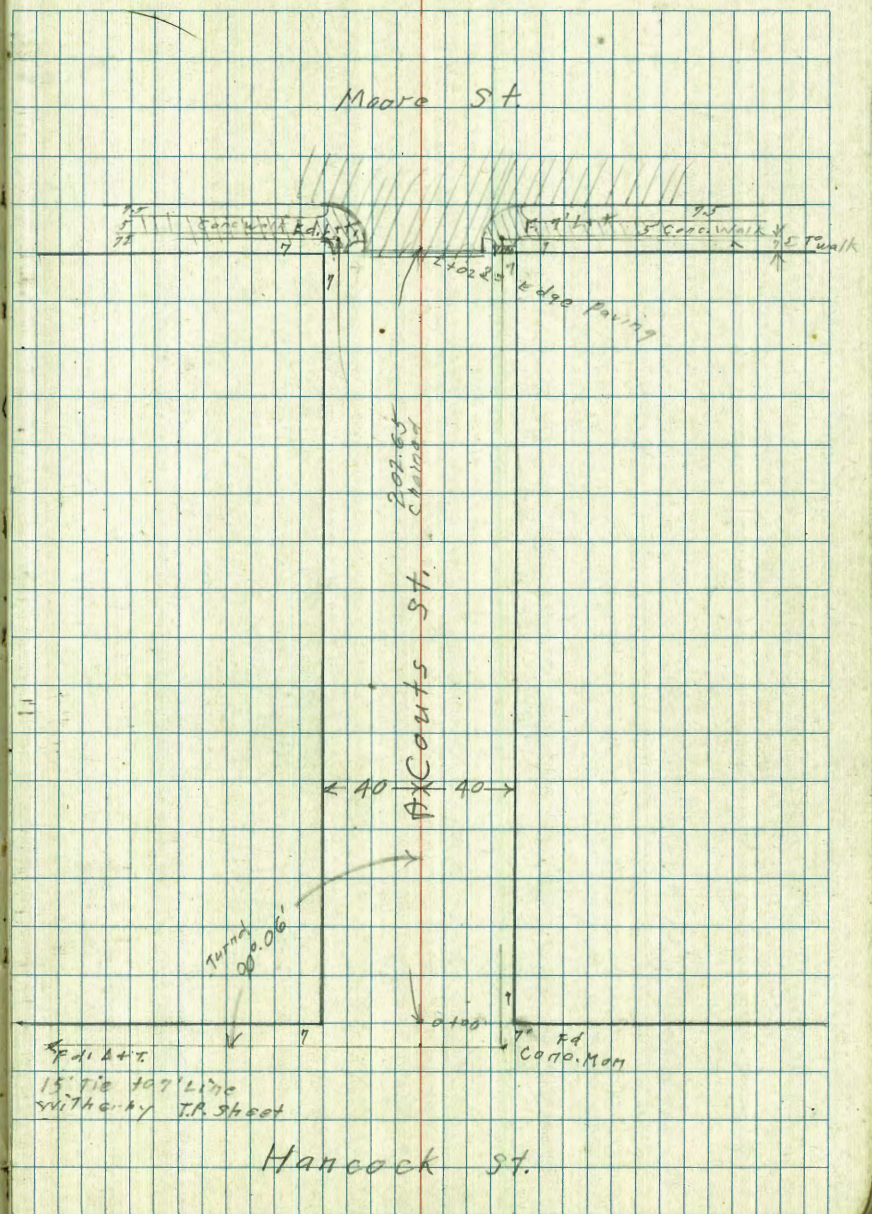
8.33 24.39 11.78 16.06

BM = B.P. in  
West curb near 0.11 27.84 — 27.73

B.C. Moore  
Witherby

indexed  
C.S.K.

40





LT.

♀

RT

Counts

41

0+65

 $\frac{5.6}{100} / 17.8$  $\frac{5.4}{40} / 19.0$  $\frac{5.7}{30} / 18.5$  $\frac{6.4}{30} / 17.6$  $\frac{7.4}{40} / 17.0$  $\frac{6.7}{100} / 17.7$ 

0+59

 $\frac{6.9}{100} / 17.5$  $\frac{6.4}{40} / 18.0$  $\frac{6.2}{30} / 18.2$  $\frac{6.4}{25} / 18.0$  $\frac{7.7}{40} / 16.7$  $\frac{7.3}{100} / 17.1$ 

0+50

 $\frac{8.7}{100} / 15.7$  $\frac{8.5}{40} / 15.9$  $\frac{8.1}{30} / 16.3$  $\frac{8.1}{40} / 16.3$  $\frac{7.5}{100} / 16.9$ 

0+40

 $\frac{9.7}{100} / 14.7$  $\frac{9.3}{40} / 15.1$  $\frac{9.3}{30} / 15.1$  $\frac{8.6}{40} / 15.8$  $\frac{9.6}{100} / 15.8$ 

0+00 = N. Ely, Line Hawk cock.

 $\frac{11.9}{100} / 12.6$  $\frac{11.6}{40} / 12.8$  $\frac{11.3}{30} / 13.1$  $\frac{11.9}{40} / 13.4$  $\frac{10.9}{100} / 14.0$ 

0-35

 $\frac{13.5}{100} / 11.1$  $\frac{12.9}{40} / 11.5$  $\frac{13.2}{30} / 11.2$  $\frac{13.1}{40} / 11.3$  $\frac{12.2}{100} / 12.2$ 

24.39

24.39







2+10 = start good curb on right

2+08<sup>55</sup> start good walk on Rt

2+02<sup>62</sup> Cont. - start walk on left.

2+02<sup>65</sup> S.W. by. Line Moore St Edge. H.C. Pav.

1+90

1+76

1+69

36.57

Lt.

Coats

Rt.

43

11.9 40	24.7	14.6 100	25.0	9.8 100	26.8	4.55 40 top. cl.	32.02	5.8 100	30.8	2.92	33.60	9.04 20 top. cl.	33.53
9.0 23	27.6	14.6 40	26.0	9.3 55	27.3	4.91 20 Bottom	31.66	4.58 100	30.8	2.92	33.60	9.04 20 top. cl.	33.53
6.9 16	29.7	14.6 32	26.4	8.6 27	34.0	4.34 19	32.23	4.58 100	30.8	2.92	33.60	9.04 20 top. cl.	33.53
10.2 36.57	26.4	14.6 33	33.0	9.0 16	32.6	3.99	32.58	4.58 100	30.8	2.92	33.60	9.04 20 top. cl.	33.53
11.3 8	25.2	14.6 33	33.0	9.4 36	33.2	3.70 13	32.87	4.58 100	30.8	2.92	33.60	9.04 20 top. cl.	33.53
11.5 40	25.1	14.6 33	26.5	9.4 40	29.2	3.66 13	32.91	4.58 100	30.8	2.92	33.60	9.04 20 top. cl.	33.53
		14.6 40	26.5	9.2 45	27.4	3.50 13 (Sunken)	33.07	4.58 100	30.8	2.92	33.60	9.04 20 top. cl.	33.53
		14.6 100	26.5	8.6 100	28.0			4.58 100	30.8	2.92	33.60	9.04 20 top. cl.	33.53

inside edge  
walk

Walk  
Sunken  
35.5

35.5 inside edge  
walk

2.92  
20  
Cut  
33.07



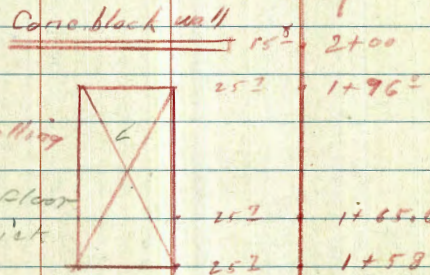




Alley BIK 58. Pt. Loma Hqts.

9-25-47

Sammer Meyer  
W. Moore  
E. Sherman



See page 53  
for levels

E. Line Venice = 0+00

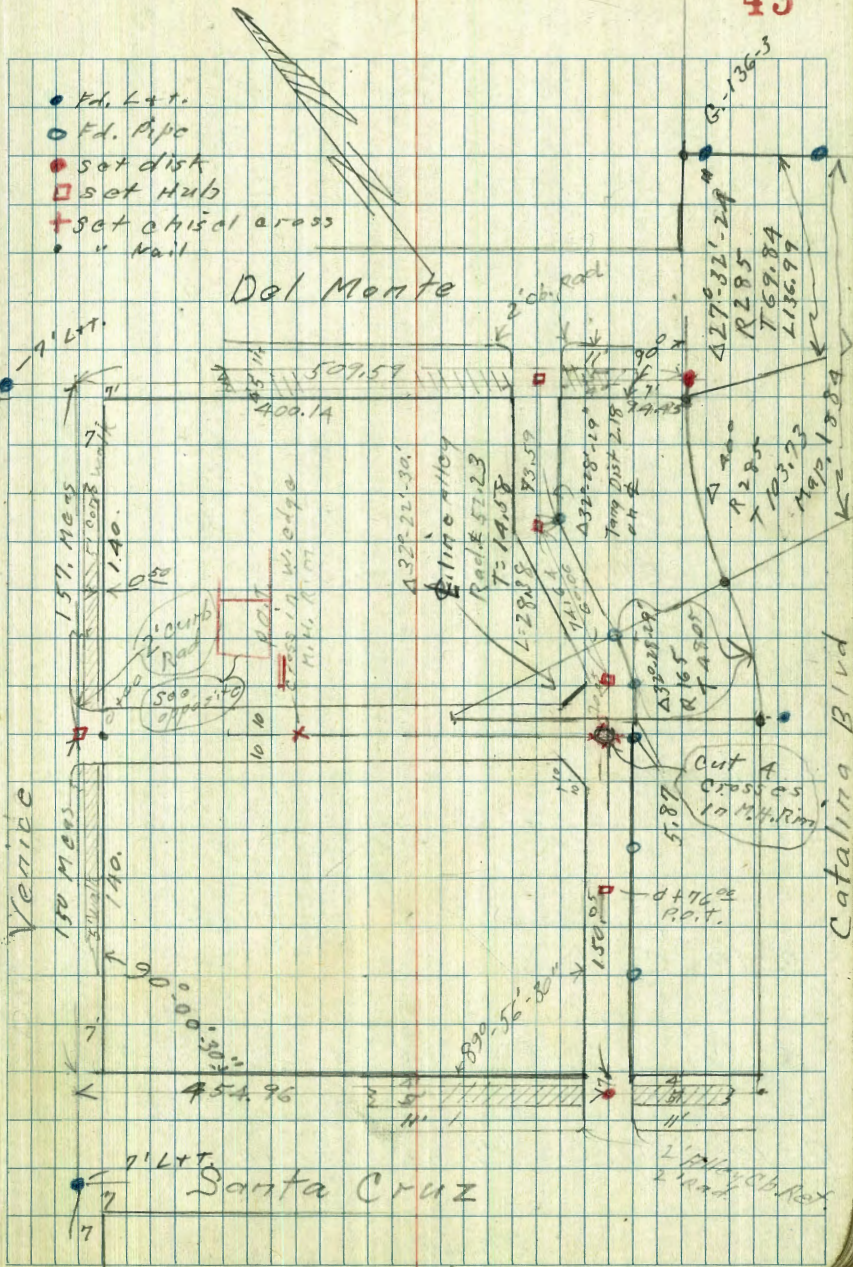
S.W. B.P. (Set. B.M.)  
Del Monte + Venice 3.10 217.39

T.P. 5.57 215.49 8.33 209.92

S.W. B.P.  
Venice + Niagara 0.53 218.25 — 217.72

Indexed  
C.S.K.

45





1+00 99 RT. = P. Pole # A 4282

0+50

0+00 = Ely. Line Venice

0-7

0-10 Cont

0-10 = Ely. Curbitine Venice

215.49

Lt.

A

Rt.

46

210.95	212.12	212.54	210.09	210.99	208.59	211.99	209.39
4.54 Top Cl.	2.95 9.9 Top Cl.	2.95 9.9	5.1 10	2.5	5.2 9	2.5 10	6.1 50
211.09	212.39	212.09	212.09	212.29	208.59	211.99	209.39
9.4 50 Ord.	3.1 9.9 Ord.	3.1 9.9	3.1	5.2	5.2 9	2.5 10	6.1 50
212.36	211.79	212.59	212.39	212.59	212.59	212.59	209.39
3.13 10 Top Cl. Ret.	3.75 50 Top Cl.	2.97 9.9 Top Cl.	3.1	2.9 9.9	2.9 9.9	2.9 9.9	6.1 50
211.09	211.99	212.09	212.39	212.59	212.59	212.71	212.83
3.8 10	3.5	3.4 10	5.2	2.9 9.9	2.9 9.9	2.9 9.9	2.66 9.9 Top Cl.
212.72	212.79	212.72	212.09	212.09	212.09	212.72	213.27
3.4 10 Top Cl. Ret.	3.8 50 Ord.	1.7 10 Ord.	3.4 10	2.9 9.9	2.9 9.9	2.9 9.9	2.22 50 Top Cl.
<u>215.49</u>							



3+95 7.7 Rt. P. pole # 174216

3+50

T.P. 0.20 191.27 12.55 191.07

3+00

2+50 9.5 Rt. = P. pole # 174254

T.P. 0.38 203.62 12.25 203.24

2+00

1+75

1+58 See additional notes P. 53

1+50

215.49

Lt.

\$

Rt.

47

186.17  
5.1  
10

191.92  
11.7  
50

191.52  
12.1  
70  
196.62  
4.0  
10

202.29  
13.2  
50

203.29  
12.2  
10  
205.39  
10.1  
10

207.29  
7.9  
10

186.57  
4.7  
191.27  
10

192.82  
11.8  
196.92  
6.7  
203.62  
10

203.89  
12.6  
10  
205.99  
9.5  
10

207.79  
7.7  
10

215.49

186.77  
4.5  
10

192.02  
11.6  
10

196.92  
6.7  
10

203.39  
12.1  
10

205.79  
9.7  
10

207.69  
7.9  
10

192.32  
11.3  
50

202.99  
12.5  
50



8.72 184.48 — 175.76

4+37.90 = P.O.T.

T.P. 2x2 Hub on  $\Phi$

6.82 175.76



4+40<sup>s</sup> 20' Pt. = End Flare on south.

4+39<sup>e</sup> 18<sup>18</sup> Lt. = End Flare, off north

4+30<sup>s</sup> = Start Flare in alley

T.P. 3.87 182.58 12.56 178.71

4+00

191.27

385 50%

Lt.

$\Phi$

Rt.

48

12.0 50	180.27	7.12 18.2	175.38	6.8	175.78	7.1 20	175.18
5.1 10	177.78	5.1 10	172.68	4.7	172.48	5.1 10	172.48
10.3 10	181.0	9.9	182.58	9.8 10	181.57	10.2 50	181.07
		191.27					



0+50 6<sup>2</sup> Rt. = Rpdle # 17-1712

0+25

0+05

0+00 = E. Line Santa Cruz

Set B.M. - Load + Disk

Galley - E 9' Line Santa Cruz 10.82 173.66

0-20 Cont.

0-20 = E. Cb. line Santa Cruz

184.48

LT.	RT.
181.08	171.38
2.4 30	13.1 45
178.98	175.78
5.5 15	8.7 7.5
177.28	171.38
2.2 7.5	13.1 45
176.48	170.98
8.1 6	14.8 55
174.08	179.08
8.2 7.5	17.2 15
173.88	175.88
8.1 6	8.7 7.5
171.38	174.18
10.1 3	10.3 5
174.84	174.48
9.6 7.5 66.799	10.0 7.5
174.48	174.78
10.00 7.5 Per	9.7 13
173.82	170.98
10.66	13.5 40
173.38	173.42
11.10 1.55 Per	10.3 5
165.16	173.42
11.10 1.55 Per	11.06 7.55 66.68 md
179.32	165.53
7.4 Per	18.95
172.79	173.09
11.69 7.55 Butter at 28 lbs	18.95 7.4 14.86
173.47	173.09
11.01	11.39 7.7 Cb. Per
174.24	
10.24 7.5 Butter at 28 lbs 1.70	
179.48	
11.01	

9' Rt. Rads  
Turned down  
with level +  
figured from T

184.48















Additional Levels  
 Alley B/K. 58 Pt. Larra Hgts.

block (North + South) wall.  
 2+00 15<sup>8</sup> Lt. = End 6" wide conc.

1+96° 25<sup>2</sup> Lt. = End Bldg.

1+65° 25<sup>2</sup> Lt. = End gar. door.

750 = start @ gar. door.  
 + Garage. Conc. Floor.  
 1+58 } 25<sup>2</sup> = start comb dwelling

0.20 212.74 — 212.54  
 B.M. = East End. of North Alley curb. 0+00  
 page 26

⊕  
 Alley

Additional Levels - See Page 45  
 47

206.9	202.1	203.2			
5.8	10.6	9.5			
15.8	15.8	15.8			
Top wall	Bottom wall	Ground			
204.96	204.5				
7.78	8.2				
25.7	25.6				
07 Floor	07.0				
204.94	204.94	206.0	206.9	207.2	
7.80	7.8	6.7	5.8	5.5	
25.7	25	10		10	
Gar. Floor					
204.90	205.24	206.04	207.34	207.54	207.54
7.84	7.5	5.9	5.4	5.2	5.4
25.2	25	10	5		10
8.91					
2100					
			212.74		







2+70 - for Profile + House on Lt.

D.M. on Pipe -  $\phi$  Leghorn U. end. 3.85 426.94

2+49.47 = End = N.L. Sub.

T.P. 11.14 430.79 0.49 419.65

2+00

1+50

429.06  
1.3  
30.2  
floor  
elev.

427.0  
3.8  
30.2  
along +  
house

427.6  
3.2  
20

428.6  
2.2

429.2  
1.5  
20

429.3  
1.5  
20

424.5  
6.2  
20

425.3  
5.5  
20

426.8  
4.0

427.9  
2.9  
20

427.8  
3.0  
20

417.1  
3.4  
410.8  
20

418.7  
2.4  
412.6  
20

430.79 ✓  
+ 420.7  
415.9  
4.2

420.14

+ 423.2  
2.1  
20

418.2  
- 1.9  
20

+ 423.8  
2.3  
20

419.1  
- 2.0  
20



X-Section State Street from  
Palm Street to Quince Street.

Johnson  
Pope  
Crawford  
9-14-49  
W.O. 25010

INDEXED  
W.K.  
SEP 19 1949

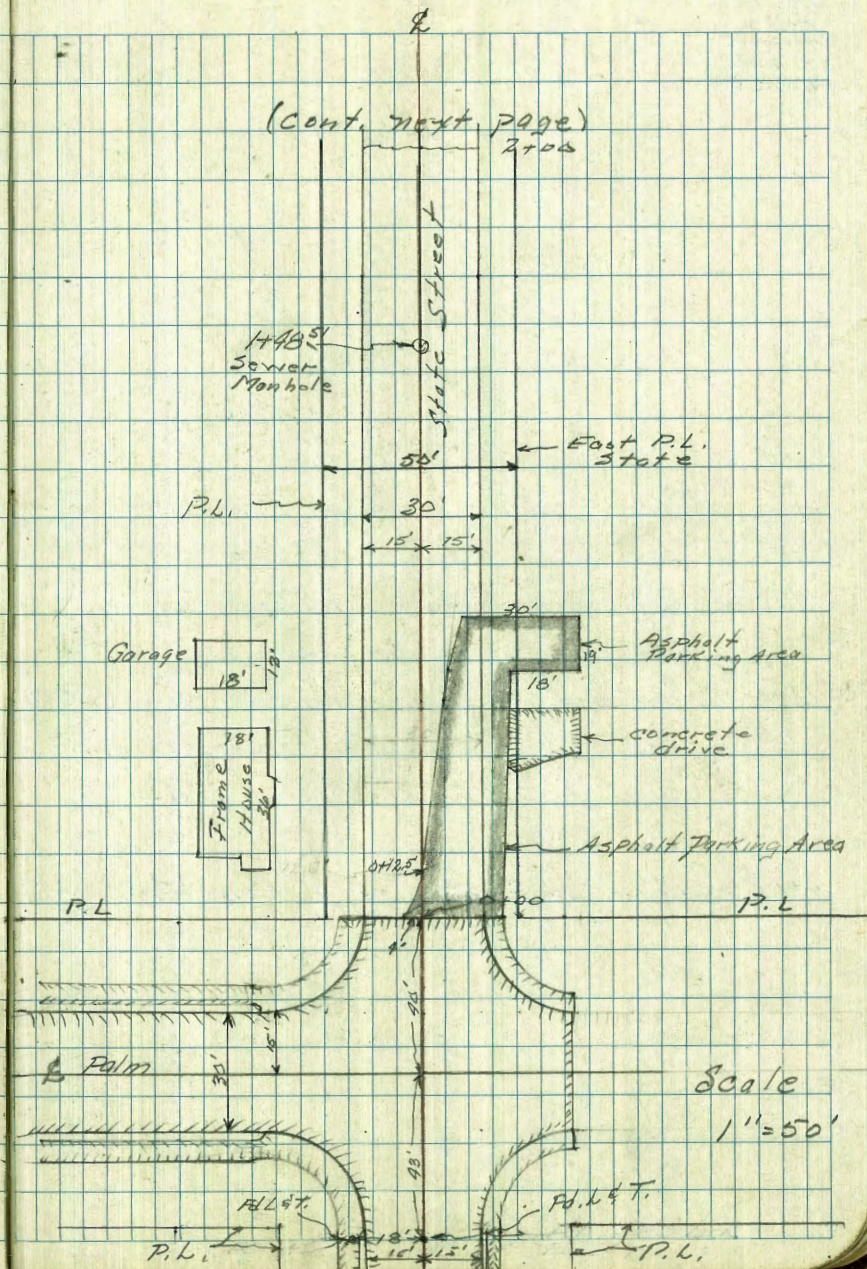
1+48.5 = Sewer M.H. & State

0+12.5 = Int. & State & Asphalt Parking

0+00 = North Prop. Line - Palm

0-40 = & State & Palm

0-80 = South Prop. line Palm

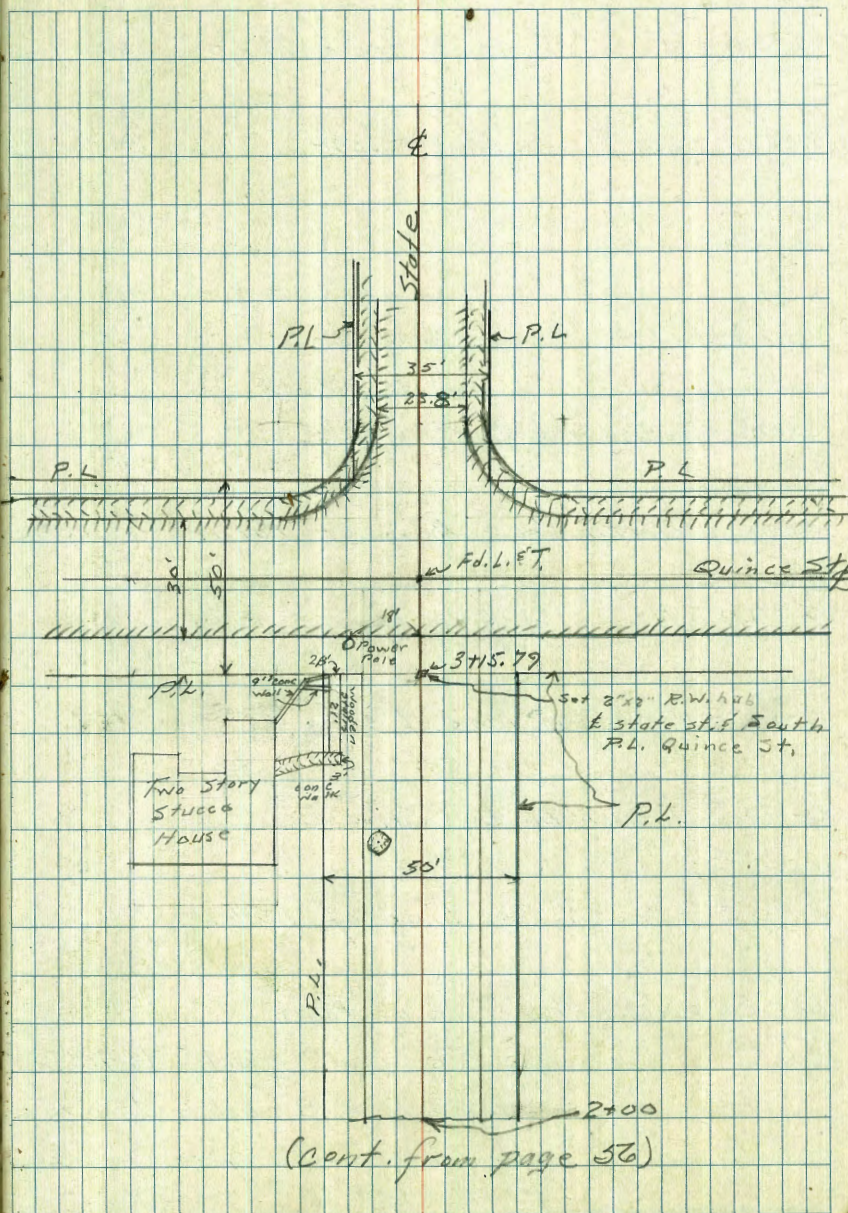




X-section State Street  
Palm to Quince

Johnson  
Pope  
Crawford  
4-14-49  
W.D. 25810

- 3+65.79 = North Prop. Line Quince
- 3+55.79 = North Curb Line Quince
- 3+40.79 = E State & Quince Streets
- 3+25.79 = South Curb Line Quince
- 3+15.79 = South Property line of Quince St.  
& E State St. Set City engineers  
disk & 2"x2"x8" Redwd Hub
- 2+72 = 16' ft to center of 6' conc. fish pond



(Cont. from page 56)



X-Section - State St. -  
Johnson Palm to Quince  
Pope  
Crawford  
9-19-49 Level Notes

0+59 - End of conc. drive 23' RT

0+39 - Start Conc. drive 22' RT

0+27

0+23

0+12.8 = Asphalt Int. with E

0+00 = North Prop. line of Palm

0-18

0-25 = North Cb line of Palm

0-40 = Int. Palm E & State E

0-55 = South Curb line of Palm

0-80 = South Prop line of Palm

T.P.	6.89	171.17	2.45	164.33
T.P.	10.63	166.78	0.06	150.15
T.P.	13.09	158.21	0.00	143.10
	12.86	143.12		130.26

Lt.      E      Rt.

217 65	203 35	196 25	176 225	147 185	138 135	24 7.5	59	554 5.5	490 15	436 23	128 41	Garage floor
203 35	191 34	183 26	123 19	145 12	104 11	6.0 2.6	6.2	591 34	523 18	463 22	434 26	2.5 36
200 37	169 34	166 26.5	109 19.5	106 15	9.9 11.5	7.8 8.5	6.3	639 18	580 15	510 22.5	51 25	3.0 34.5
197 37	162 36	158 22	130 21	91 15	71 8	6.5	650 7.5	600 15	526 22.3	53 25	3.0 37	
205 71	193 59	142 87	145 27	128 25	7.5 13.5	7.7 15	6.6	632 75	558 22	52 25	3.0 37.5	
178 43	143 43	118 58	117 27	9.3 24	6.65 22.5	6.84 15	7.53 7	6.71 6.71	6.42 15	6.05 15	Gut 06	
126 50	117 44.8	10.2 39	9.2 30	7.97 25	7.57 14.4	8.07 12.4	6.00	3.82 20.3	3.39 20.3	Gut 06		
12.20 50	12.88 50	10.65 35	7.65 7.5	5.74	4.00 75	2.93 37.2	0.53 37.2	1.10 43	1.81 47	Gut 06		
13.15 57	14.30 35	10.00 15	5.45	3.45 75	1.23 32.5	7.54 93	1.08 46					
13.72 57	13.8 37	9.54 35	9.95 35	7.19 75	5.34	3.53 75	0.64 37.8	0.25 37.8	1.09 47	1.15 47		
4.97 15	5.41 15	3.76	3.57 15	2.02 15								

S.W.B.P. Columbia & Palm



X-section - State Street  
Palm to Quince  
Level Notes

2+19 = 18' RT to 10" tree stump

2+17

T.P. 8.18 155.74 0.09 147.56

2+12 = 2' RT to 10" tree stump; 12' RT to 10" tree stump; 18' RT to 6" tree stump

2+04 = 18' RT to 6" tree stump

1+92 = 23' RT to 12" tree stump

1+82 = 10' RT to 10" tree stump

1+70 = 12' RT to 12" tree stump

1+67

1+56 = 22' RT to 10" tree

1+48.5 = Sewer N.H. on E side <sup>North Rim</sup> 8.16 139.49

1+41

T.P. 0.51 147.65 12.98 147.14

1+27 = power pole 24.3' Lt # P2930

1+05

1+00

T.P. 1.63 160.12 12.68 158.49

0+83

0+72 = End of Asphalt drive 10.5' RT

0+66 = E Garage 40' Lt & Dirt Floor

LT.

L

RT

59

9.9	14.4	15.1	9.4	8.0	5.4	4.0	4.0
5.0	2.5	1.5		3	1.5	2.5	3.0

155.74

7.5	6.7	11.6	0.5	+1.2	+4.0
5.0	3.4	7.4	1.5	2.5	3.7

16.2	19.8	11.5	8.0	4.0	2.9	9.0
5.0	2.5	1.5	9	1.5	2.5	3.7

16.6	12.9	13.2	9.2	7.2	4.3	0.9
4.5	2.5	1.5		1.5	2.5	3.7

Conc. Block wall

(Ring not level)

12.4	10.7	8.3	7.1	3.1	0.7	+2.8	7.5
5.0	4.3	2.5	1.5	5.2	1.5	2.5	5.0

147.65

Nail 5.55' high on Power Pole

23.4	19.0	17.3	15.1	12.7	11.9	6.8
5.0	2.5	1.5		1.5	2.5	5.0

19.3	13.8	12.7	10.2	8.3	7.5	3.1
5.0	2.5	1.5		1.5	2.5	5.0

16.9	12.0	11.3	7.0	6.5	6.3	2.4	+1.3
5.0	2.5	1.5		1.5	2.5	5.0	7.5

160.12

21.3	20.9	20.8	18.3	14.2	6.4	6.0	5.4	4.5
6.5	4.0	2.5	1.5		7	1.5	2.5	4.4

20.6	21.2	19.4	12.3	15.8	12.8	6.4	5.23	5.07	4.16
4.0	3.65	19.5	7.6	11.5	8	9	10.5	1.5	9.15

20.3

40

171.7



X-section - State St.  
Palm to Quince  
Level Notes

Gutter

3+55.79 - North Carb of Quince

3+90.79 = State & Quince

Gutter

3+25.79 = South Carb of Quince

3+17.79

3+15.79 = South Prop. line Quince St & State on hub

T.P. 5.20 185.27 0.24 180.07

T.P. 12.54 180.31 0.82 167.77

2+93 - 21' Lt to 2.3' conc. Walk

2+88 - 4' Lt to 4" tree

2+85

2+72 = 16' Lt to 6' Circular fish pond conc.

T.P. 12.99 168.59 0.14 155.60

2+67

2+59 = 7' Rt to 8" stump

2+50

2+27 = 4' Rt to 10" stump; 14' Rt to 8" stump

Lt.

¢

Rt.

60

1290 78	1400 50	9.07 40.3						488 36	234 50	199 100
1242 78	952 50	8.62 40.3	7.80 25	7.49 24.2 6.14	7.07 11.9	6.44	5.90 71.9	4.47 36	3.89 50	1.59 100
	1251 78	9.64 50	7.13 25	6.68 20.2 8.14	5.87	5.52 15	5.06 25	3.91 50	1.49 100	
	1309 78	10.27 50	7.90 25	7.26 17.5 6.14	6.63	6.09 15	5.69 25	4.51 50	1.95 100	
	1260 78	9.82 50	7.93 25	6.67 17.5 6.14	6.17	5.64 15	5.25 25	4.08 50	1.62 100	
		9.9 50	8.0 25	6.8 15	6.3 75	5.7 25	5.4 25	4.2 50		
		100 50	8.2 25	7.4 15	6.75	6.8 15	6.2 25	5.2 50		
					185.27					
					4 P. 1101				S.W. cor - State & Quince	
					rail in power pole 14' up from ground					
		5.78 37	5.49 25	5.19 21	6.3 15	5.9	6.5 15	6.2 25	5.4 40	
		8.3 36	9.0 25	14.5 12	13.4 12.0	13.4 7	11.0 17	9.9 25	7.3 39	
						168.59				
		7.12 38	6.3 25	6.9 15	2.4 6	4.7	2.0 10	1.5 25	1.0 36	
		6.9 50	3.5 25	5.0 15	8.3 5	8.6	8.3 5	3.0 13	2.6 25	
									1.0 37	
						155.74				



X-section - State St.  
 Palm to Quince  
 Level Notes

				0.01	
				130.26	
		6.47		130.25	
T.P.	4.31	136.70	12.57	132.41	
T.P.	0.39	144.98	12.94	144.59	
T.P.	1.00	157.53	13.09	156.53	
T.P.	0.50	169.62	13.09	169.12	
T.P.	2.14	182.21	5.20	180.07	
3+65.79 =	North P.L.	of Quince			

Lt.      Q      Rt.      61

S.W.B.P. Columbia & Palm.

Nail in	Power Pole	S.W. Cor.	State of	Quince	
6.93	7.15	6.85	5.53	5.45	5.10
15.1	15.1	11.9	5.94	11.9	13.4
Ob. Out.				Ob.	Ob.
		165.27			



Cross Section 33rd St.  
H St. to Datast.

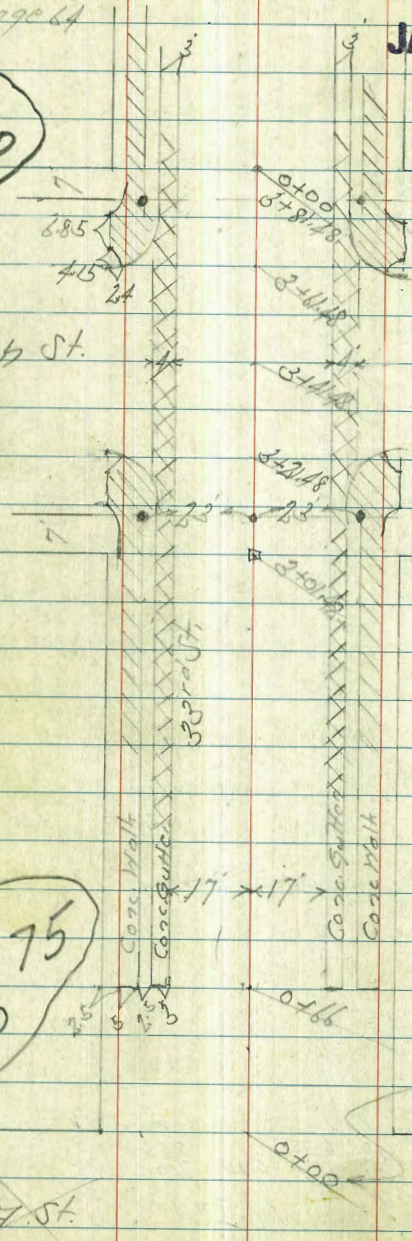
Level page 64

See F.B.  
2349/60

INDEXED  
W.K.  
JAN 12 1950

H St.

See p 75  
Also



33rd St.  
H St.

H St.

Jan. 10. 50  
A. Sisson  
D. Smith  
Roral

62

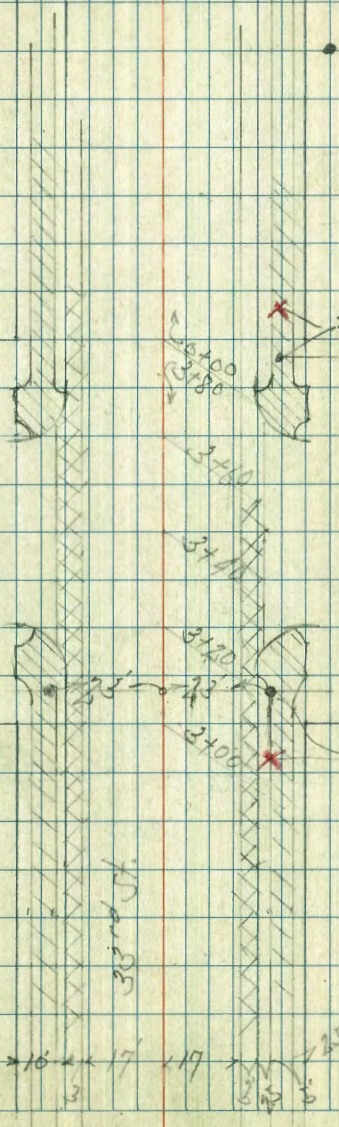
Chavez  
110.5/590  
Indicator  
Landmark Found

Notes reduced.  
1-13-49 H.R.

25' = chisel cross.  
R.R. 2-20-51

25' chisel  
cross R.R.  
9-20-51

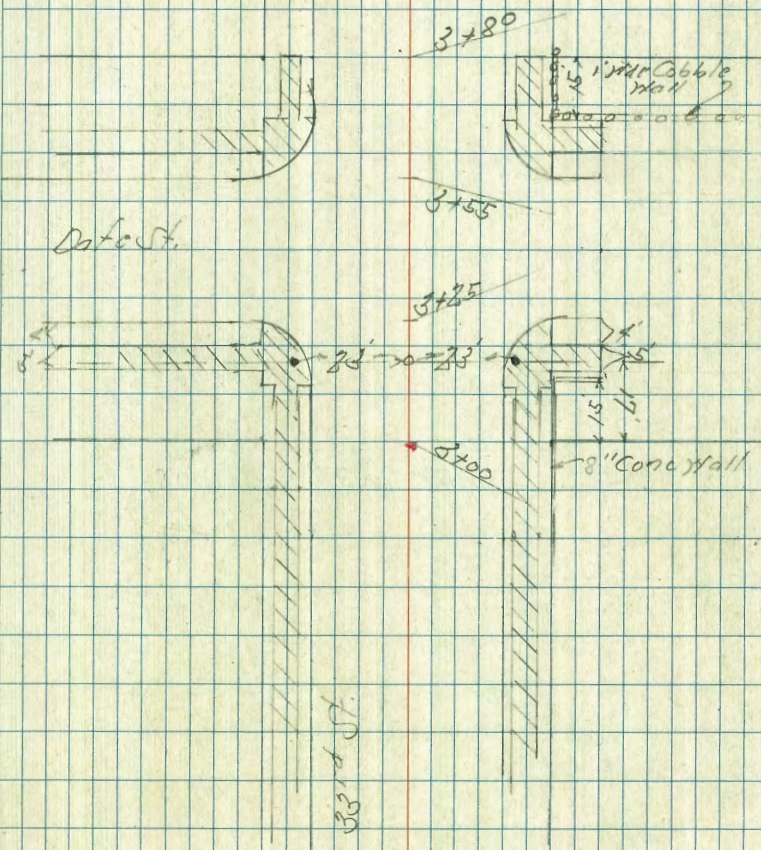
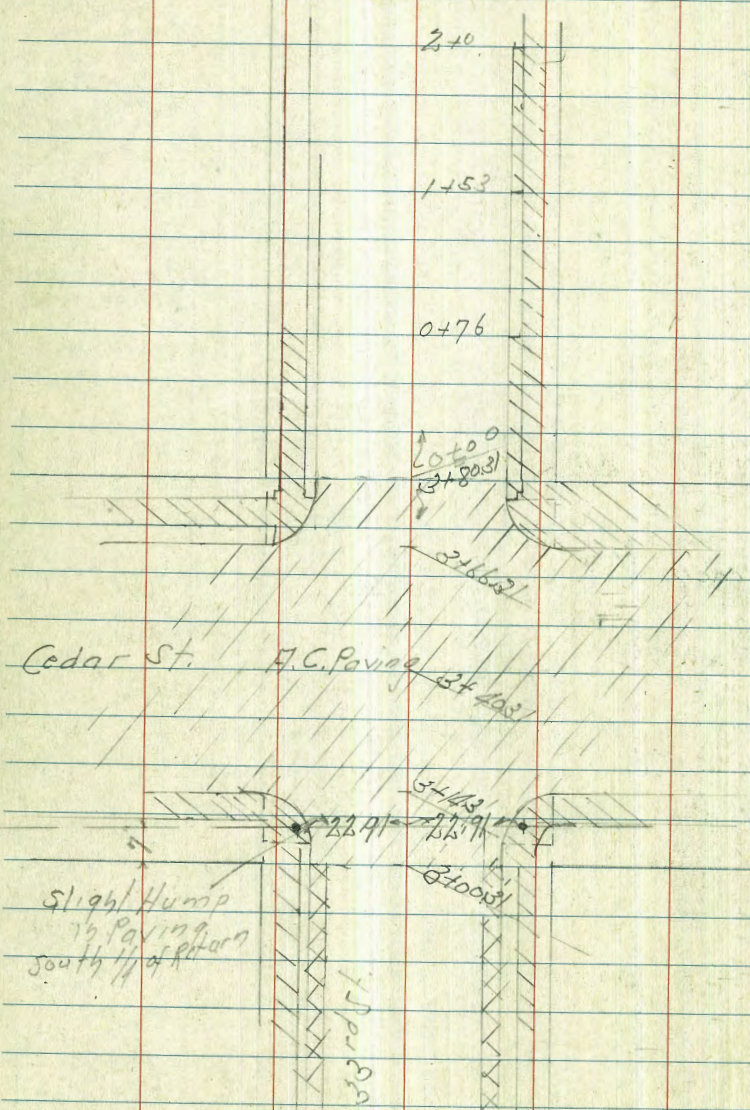
Beech St.



33rd St.

16' x 17' x 17' x 17'  
3















+50

TP 1294 22321 0.00 210.27

+10

+50

+10

210.21 03

TP 1318 210.27 0.05 197.09

+50

0+10  
278.48 = 116 705 ST

08  
197.7

212.6	212.02	212.23	212.43	212.1	213.4	212.7	212.45	213.30	214.07	214.9
106	106	108	107	106	98	95	970	985	908	830
30	30	30	30	30	30	15	10	30	30	30
	EX	EX	EX	EX	EX	EX	EX	EX	EX	EX

208.1	208.01	207.21	207.44	208.0	208.4	208.5	208.36	208.19	209.02	209.6
21	22	200	277	32	18	17	185	202	119	26
30	30	30	30	30	30	30	30	30	30	30

202.9	203.00	202.17	202.27	202.0	202.6	203.6	202.41	202.26	202.06	205.3
73	72	804	794	72	66	66	680	685	665	68
30	30	30	30	30	30	30	30	30	30	30
	EX	EX	EX	EX	EX	EX	EX	EX	EX	EX

198.3	198.01	197.21	197.37	198.0	198.4	198.6	198.36	198.27	199.07	199.9
119	122	1200	1284	132	148	116	1185	1194	1114	103
30	30	30	30	30	30	30	30	30	30	30
	EX	EX	EX	EX	EX	EX	EX	EX	EX	EX

192.5	192.09	192.27	192.34	193.0	192.4	192.6	192.41	192.31	194.07	194.9
36	299	481	474	41	37	35	367	377	301	27
30	30	30	30	30	30	30	30	30	30	30

189.2	188.06	187.35	187.49	188.7	189.3	189.3	188.45	188.23	189.00	190.2
78	202	220	259	24	78	78	863	885	898	69
30	30	30	30	30	30	30	30	30	30	30
	EX	EX	EX	EX	EX	EX	EX	EX	EX	EX

197.7











Lt

S

PL

140

235.0	234.27	233.9	234.0	234.0	233.7	232.8	233.29	233.5
56	57.79	57.8	57	57	57.4	6.3	5.77	5.6
30	30-C6	30	30	30	30	30	30-C6	30

750

234.7	234.16	233.6	233.7	233.7	233.4	232.7	232.90	233.13
56	57.1	55	57	57	57	6.4	6.16	5.82
30	30-C6	30	30	30	30	30	30-C6	30 or cont. trail

0700 ↑

3+80.3/7 = North Line Cedar St = N of AC Parking

BM

6.50

232.82

56 N of AC Parking Cedar St

+66.3/ = North of Carb Cedar

234.5	234.02	233.29	233.40	233.37	232.79	232.10	232.51	232.74
56	57.4	57.7	56.6	56.9	6.27	6.96	6.55	6.32
30	30-C6	30-C6	30	30	30	30-C6	30-C6	30 or cont. trail

234.13	233.48	233.40	233.24	233.01	232.72	232.34	232.01	232.48
56	55.8	56.6	58.2	60.5	6.31	6.72	7.05	6.52
30	30-C6	30	30	30	30	30	30-C6	30-C6

3+40.3/ = S Cedar St

233.88	233.65	233.54	233.36	233.14	232.88	232.62
56	57.1	55.8	57.0	59.2	6.18	6.44
30	30	30	30	30	30	30

3+14.3/ = South of Carb Cedar

234.11	233.51	233.54	233.48	233.30	232.84	232.35	231.98	232.52
56	55.5	55.7	55.8	57.6	6.22	6.71	7.02	6.54
30-C6	30-C6	30	30	30	30	30	30-C6	30-C6

06  
239.78

04  
239.78



+25 = South Carb Line Date

234.64

5.66  
10.26

233.7	234.96	233.9	234.1	234.6	234.9	234.7	234.5	235.0	234.96	235.16
46	53	64	63	57	54	56	58	58	53	54
40	30	30	30	10		10	10	10	30	40

+15 = Carb BC Rt + Lt

235.0	235.2	234.96	234.3	234.6	234.9	234.7	234.4	234.92	235.2	235.5
53	51	53	60	57	54	56	59	53	51	48
40	30	30	30	10		10	10	30	30	10

3+0 = Old South Line Date St

235.3	234.91	234.2	234.6	234.9	234.7	234.3	234.82	235.09
50	53	61	57	54	56	60	54	58
30	30	30	10		10	30	30	30

+50

235.2	234.89	234.3	234.7	234.9	234.4	234.1	234.50	234.8
51	54	60	56	54	59	63	58	55
30	30	30	10		10	10	30	30

2+0

235.0	234.60	234.2	234.4	234.5	234.1	233.7	234.08	234.35
50	57	61	59	58	62	66	62	59
30	30	30	10		10	20	30	30

IP 5.81 240.36 4.57 234.58

240.36

1+50

235.1	234.45	233.86	234.2	234.2	233.9	233.3	233.78	234.0
40	46	53	49	49	53	58	53	51
30	30	30	10		10	10	30	30

239.73

239.73



BM 8.92 213.70 <sup>34</sup> N.Y.M. Co.  
 Date of  
 Fall on  
 2.13.58

TP 4.01 222.32 <sup>26</sup> 10.96 218.34 <sup>25</sup>

TP 2.02 229.27 <sup>21</sup> 13.11 227.25 <sup>19</sup>

3490

235.1 235.6 235.8 236.3 235.3 236.2 236.6 236.8 236.6  
 52/40 47/30 45/30 40/30 50/30 41/30 57/30 55/30 57/40

3480 = North Line Date St.

225.5 224.6 233.54 233.9 224.6 224.4 224.8 224.3 233.54 232.9 237.3 236.7  
 48/40 57/30 67/30 64/20 57/10 59/30 55/10 60/30 67/20 64/30 30/30 30/30  
 Top Curb  
 Fall

3465 = Curb E.C. Rt + Lt

224.3 224.2 223.97 223.8 223.7 223.9 224.3 224.2 223.77 224.0 224.5  
 60/40 61/30 65/30 65/20 66/10 64/30 60/10 61/30 65/30 63/30 58/40

3455 = North Curb

222.6 223.1 224.01 223.5 223.7 223.9 224.2 224.2 224.3 224.6 223.88 225.1 224.16  
 62/40 57/30 67/30 68/30 66/30 64/10 61/10 60/20 57/30 64/30 52/30 61/40 61/40  
 Top Curb  
 Fall

3440 = Date St

223.8 224.2 224.3 224.5 224.6 224.5 224.5 224.5 225.1  
 65/40 61/30 60/20 58/10 57/30 58/10 58/30 58/30 52/40

30  
3405

30  
3405



Cross Section Birch St  
Bancroft to 33rd St.

Levels next page

INDEXED

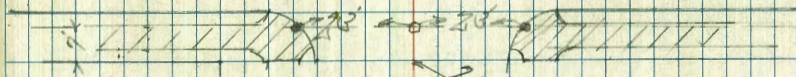
W.K.  
JAN 12 1950

Jan. 11-50  
H.S. Simon  
D. Smith  
R. R. Cramer

72

W.O. 31590

33rd St.

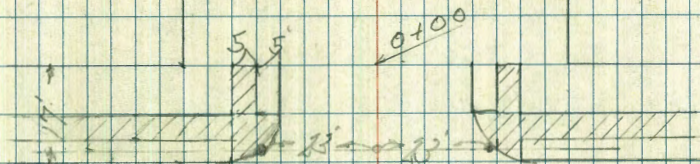


5' 9"

Board Fence

1431 - 34.7

Birch



Bancroft



Levels Beach St Bancroft to 33rd St  
 Sketch page 72

+0/ 225 ft of  $\frac{1}{2}$  = Fly Power Pole # P 3275

+ 93  $\frac{1}{2}$  Conc Dr.

+77 293 ft of  $\frac{1}{2}$  =  $\frac{1}{2}$  18" Acacia Tree

+66 =  $\frac{1}{2}$  2.5" Conc Walk on Lt.

+32

+29 285 ft of  $\frac{1}{2}$  =  $\frac{1}{2}$  20" Acacia Tree

0+0 = East Line Bancroft = Fly Spruce Rt + Lt

0-10 = Curb EC. Rt + Lt.

0-20 = East Curb Line Bancroft

BM 3.72 223.33

55 SECTION  
 219.51 Beach to 33rd

Lt. North

Rt. = South 73

220.69	220.12	219.1	218.0	217.5	217.0	216.5	215.9	215.3	214.6	
58 30	8.15 30	12 30	5.9 20	5.9 10	6.0	6.8 10	7.4 20	8.0 30	8.7 10	
Conc Dr.										
220.44	219.93	218.8	218.1	217.4	216.8	216.2	215.9	215.4	214.8	
283 115	334 30	45 30	5.9 20	5.9 10	6.5	7.1 10	7.4 20	7.9 30	8.5 10	
Conc Dr.										
219.8	218.4	217.4	216.3	215.9	215.3	215.0	214.6	214.5		
58 40	4.9 30	5.9 30	7.0 10	7.4	8.0 10	8.2 20	8.7 30	8.8 10		
Fly Wall										
217.7	213.40	214.22	214.0	213.9	213.8	213.4	213.5	213.04	213.30	213.1
56 40	9.87 30	9.05 30	9.2 30	9.1 10	9.5	9.9 10	9.8 20	10.23 20	9.97 30	10.2 10
Fly Wall										
214.8	214.28	214.22	213.6	213.4	213.3	213.0	213.02	213.31	213.1	
8.5 40	8.99 30	9.05 30	9.7 20	9.9 10	10.0	10.2 10	10.25 20	9.96 30	10.3 10	
Fly Wall										
214.0	214.2	213.9	213.6	213.4	213.2	212.9	212.6	212.4	213.09	
9.2 10	9.6 30	9.4 30	9.7 20	9.9 10	10.1	10.4 10	10.7 10	10.9 30	10.8 30	
Fly Wall										
							27			
							223.33			
							211.9	27	10.26	
							40 = G	40 = G	40 = G	



2+10.2 = West Line 33<sup>rd</sup> St.

+80

+58 - 2.5 Core Walk on Rt.

+31 = Fly Core Drive on Rt.

1+11 = Wly Core Drive on Rt.

27  
223.32

219.5	219.12	219.05	218.3	218.3	218.4	218.1	218.0	218.02	218.22	218.1	
58	415	422	50	50	49	52	53	525	505	53	
40	30	20	20	10	10	10	20	30	30	20	
		30.005		30.005		30.005		30.005		30.005	
30.005											

219.4	218.9	218.0	217.6	217.4	216.9	216.9	216.5	216.3
58	44	52	57	59	64	64	68	70
48	30	30	10	10	10	20	30	20

219.4	218.9	218.1	217.3	217.0	216.7	216.7	215.9	215.88	215.85
58	44	52	60	62	66	66	74	739	742
40	30	20	10	10	10	20	30	30	40

219.3	218.4	218.0	217.4	216.9	216.6	216.6	216.0	215.07	215.05
48	49	53	59	64	67	67	73	820	823
40	30	20	10	10	10	20	30	39.5	39.5

215.03  
824  
39.5 = 11.11 Core Drive

215.09  
827  
39.5 = 11.11 Core Drive

27  
223.32

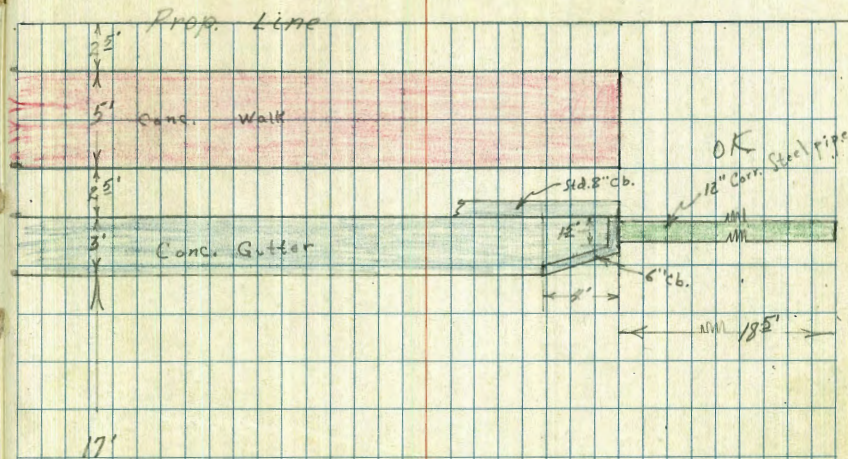


Additional Levels on 33<sup>rd</sup> St  
 at Dead End South of Ash St.  
 (See pg. 62 & 64 this Book)

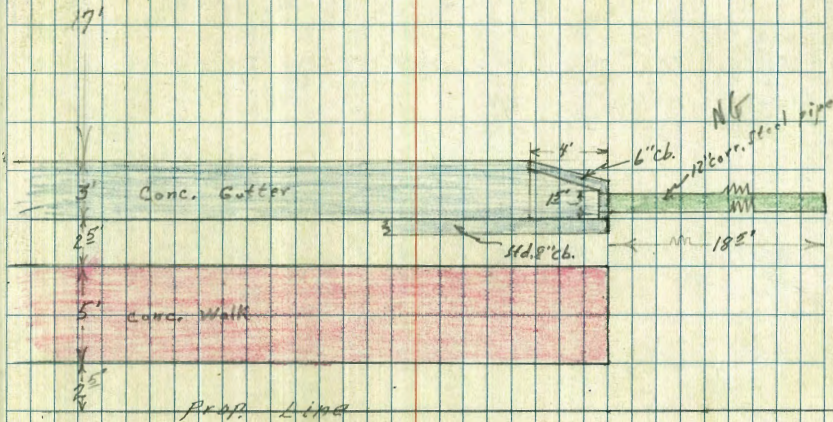
Roberts  
 Garber  
 Moore  
 Clark  
 1-27-50  
 W.D. 31590

INDEXED  
 M.K.  
 JAN 30 1950

Reduced 1-31-50  
 Remington



17'  
 33<sup>rd</sup> St.





O+70 End Inlet Boxes

170.7  
4.5  
40  
385 50%

170.4	170.3	169.71	168.86	169.09	170.4	170.6	170.9	169.49	169.34	170.0	171.0	171.0	172.2
4.8	4.9	5.47	6.34	6.11	4.8	4.6	4.3	5.71	5.88	5.12	4.2	4.2	3.0
30	20	20	20	17	17	17	17	17	20	20	20	30	40
	Dirt	cb	Gutt	conc Gutt Edge	Dirt		Dirt	Cont. Gutt Edge	Gutt	cb	Dirt		

O+66 Begin Curbs, Walks & Inlet Boxes

170.8  
4.4  
40

170.5	170.1	169.19	168.94	167.45	168.85	170.5	170.6	170.7	169.44	167.93	169.44	169.44	170.5
4.7	5.1	6.01	6.24	7.75	6.32	4.7	4.6	4.5	5.74	3.27	5.76	5.33	4.4
30	20	20	20	19	18.5	18	18	18	18.5	19	20	20	30
	Dirt	cb	cb	Invert	cb	Dirt		Dirt	cb Box	Invert	cb Box	cb Box	Dirt

O+47.5 19' Lt & 18.7' Rt to & of Ends of 12" pipes

167.7	164.2	161.2	162.7	161.7	161.3	160.95	161.3	163.3
7.5	11.0	14.02	12.5	13.5	13.9	14.25	13.9	11.9
40	30	19	19		18.7	18.7	30	40
		Invert	Dirt		Dirt	Invert		

O+00 (See pg. 62) So. Line S.P. Prop. Union Subd.

BM

12.77 175.20

162.43 N.E. Mon  
A 4.33

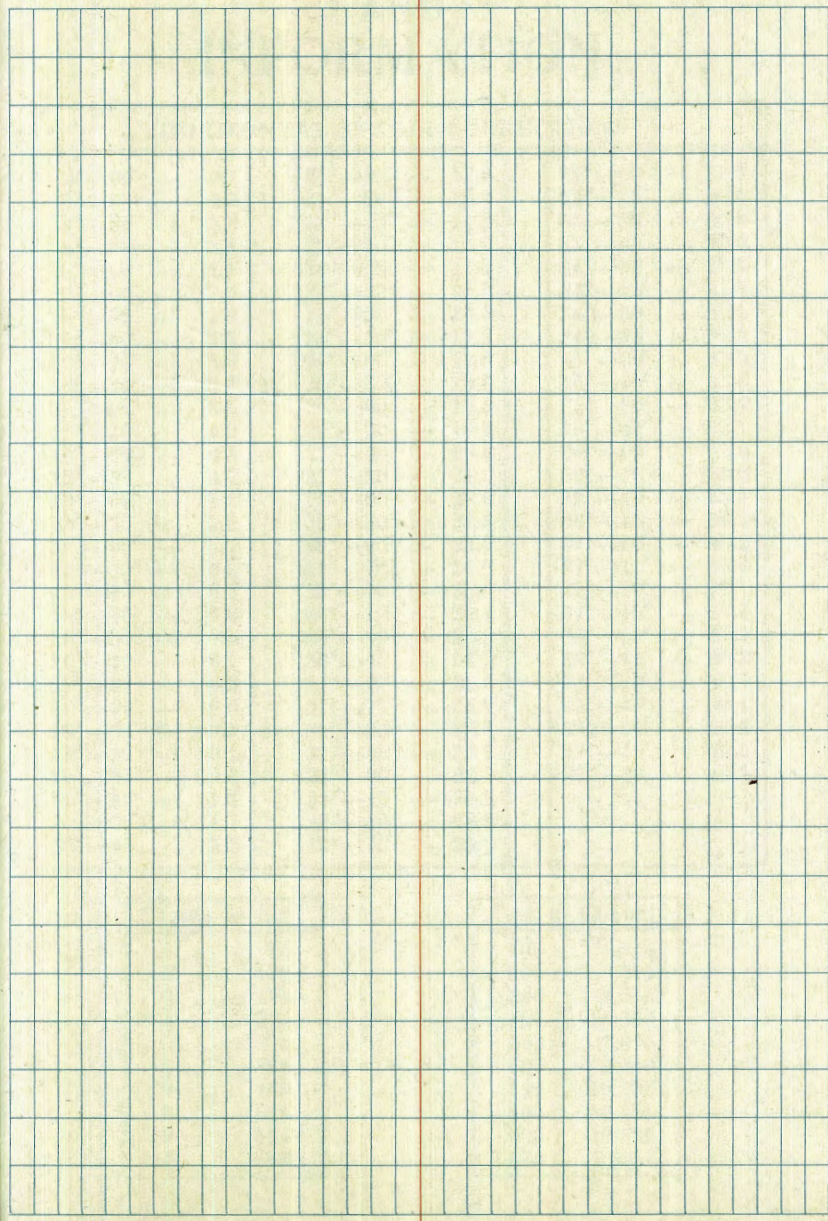
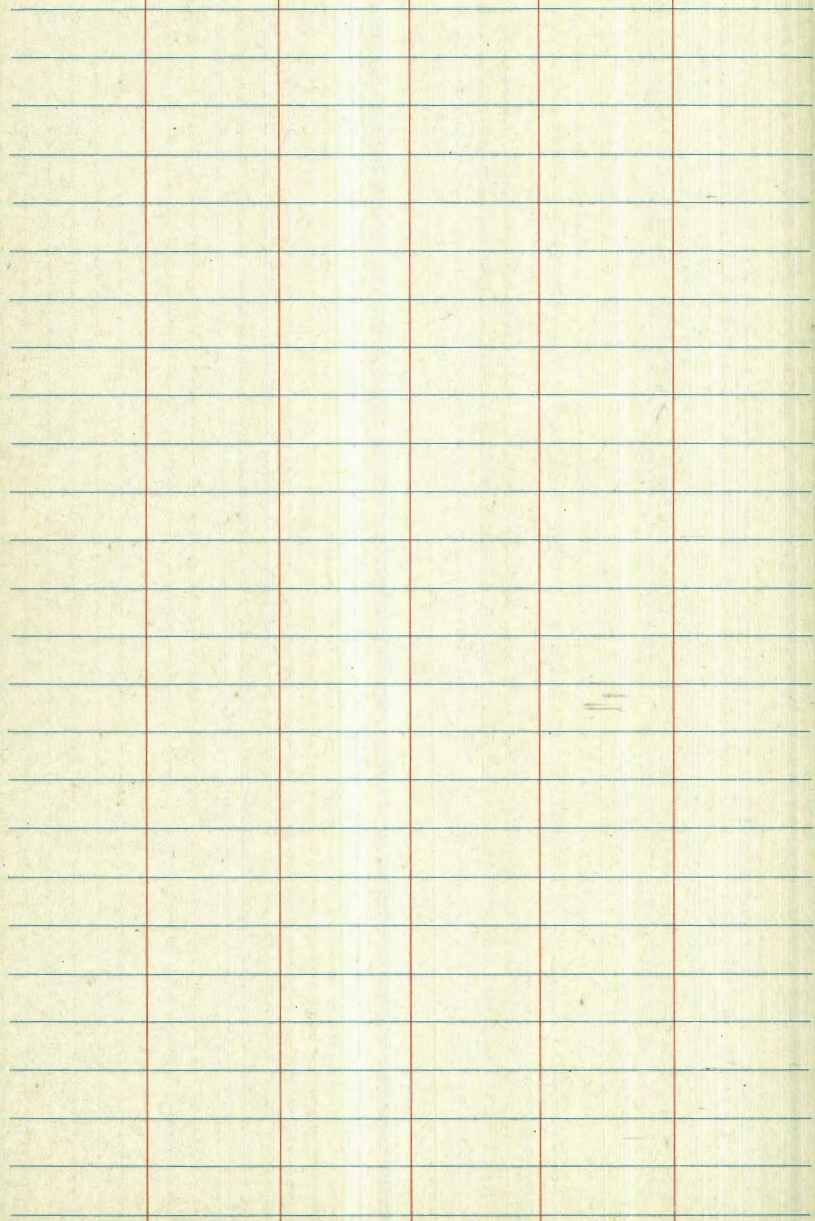
175.20



A ledger page with a grid of blue horizontal lines and three vertical red lines. The grid is approximately 20 rows high and 10 columns wide, with the three red lines defining the column widths.

A ledger page with a grid of blue horizontal and vertical lines. The grid is approximately 20 rows high and 15 columns wide. A vertical red line is present on the right side of the page, approximately one-third of the way from the right edge.







## DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope  $1\frac{1}{2}$  to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

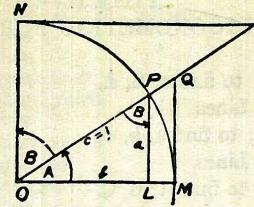


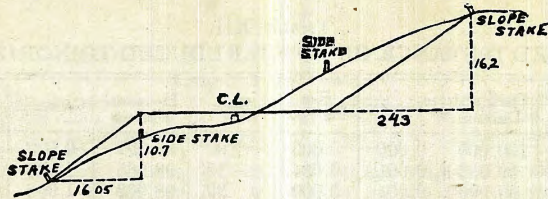
TABLE II  
TRIGONOMETRIC FORMULÆ.

2011 - oslon

6.51 ct  
5.53 rt.

$$\begin{aligned} \angle A &= \angle MOP & \angle B &= \angle PON = \angle OPL \\ R &= OB = c = 1 \\ \sin A &= \frac{a}{c} = \frac{a}{1} = a = \cos B = LP \\ \cos A &= \frac{b}{c} = \frac{b}{1} = b = \sin B = OL \\ \tan A &= \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ \\ \cot A &= \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT \\ \sec A &= \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ \\ \csc A &= \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT \\ \text{vers } A &= \frac{LM}{OP} = LM = \text{covers } B \# \\ \text{covers } A &= \frac{OP - LP}{OP} = OP - LP = \text{vers } B \\ \text{exsec } A &= PQ = \text{coexsec } B \\ \text{coexsec } A &= PT = \text{exsec } B \\ \sin \frac{1}{2} A &= \sqrt{\frac{1 - \cos A}{2}} & \cos \frac{1}{2} A &= \sqrt{\frac{1 + \cos A}{2}} \\ \sin 2A &= 2 \sin A \cos A & \cos 2A &= \cos^2 A - \sin^2 A \\ \text{Law of Lines} & \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C} \\ \text{Law of Cosines} & c^2 = a^2 + b^2 - 2ab \cos C \\ \text{Law of Tangents} & \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)} \end{aligned}$$





DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 05	1 20	1 35	1 50	1 65	1 80	1 95	2 10	2 25	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

61  
85  
14.6  
9  
66

330  
660  
185  
49.5



5.9 12.9

36.57  
27.73  
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8.84

284  
97.77  
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381.77

NW 163.91