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CITY ENGINEER'S OFFICE
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1752

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- No. 380 LEVEL BOOK. Left and Right Hand Page
the same as Left Hand Page
of this Book.
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Book, Right Hand Page 4x4
to the inch, Center Line Red.
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Book, Right Hand Page 8x8
to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this
Book, Right Hand Page 8 ver-
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CHICAGO

1752

7-19	Proposed Perry Lact. Heights #3 + 4
21-31	" " Imperial Bldg. + 47 th St.
32-46	Cross Section Kendall St. Corning Pt. Dr. to Pac. Beach Dr.
47-64	Cross Sections - Branson Place
65	Profile Catalina Blvd. - Grade.
66-74	Alley BIK 83 Pt. Loma Hqts - X-Section.

Blank ledger page with horizontal blue lines and three vertical red margin lines.

Blank ledger page with a grid of blue lines and a vertical red margin line.

Walker
Hendricks
Böcker
Greer
12-9-46

Proposed Sewer Las Alturas #74
Additional Levels in First
North & South Alley East
of Euclid Ave. - Location FB. 1664
39

	5.86	110.08		109.22
T.P.	8.39	117.73	0.74	109.34
Existing Sewer = 0+00 FB 1664-P42				
3+00	"	"	10.9	106.8
3+25			8.5	109.2
(3+25)	57' RT - SW Car House	11.6	106.1	Ground
"	" " Floor of "	9.5	108.2	
(3+00)	14' RT - East edge Cottage Floor	11.2	106.5	
3+50		6.5	111.2	
+63		6.6	111.1	
+65		7.1	110.6	
+73482	Naranja	6.6	111.1	
4+00		6.0	111.7	
"	100' R	10.1	107.6	
"	135' R	11.7	106.0	
4+15		5.3	112.4	
750		4.0	113.7	
5+00		19	115.8	
"	70' R	2.5	115.2	
"	100' R	3.6	114.1	
T.P.	1202	128.79	0.96	116.77 4+85

128.79

5+30		10.9	117.9
+60		6.7	122.1
TP	11.93	139.06	1.66
6+00		7.2	131.9
+12		3.3	135.8
+50		2.1	137.0
+82		1.1	138.0
7+08.28	E Groveland A 90° 35' RT	1.6	137.5
+35.28	A 90° 37' 30" LT	1.9	137.2
+50		1.8	137.3
8+00		2.1	137.0
TP	8.05	148.31	1.80
8+28	85' RT NE Car House	9.5	Ground 135.8
+50		7.1	138.2
+92	85' RT NE Car House	7.9	Ground 137.4
9+00		6.2	139.1
+50		5.7	139.6
10+00		4.5	140.8
+30		4.3	141.0
+45		6.6	138.7
+57		12.4	122.9'
TP	10.55	143.78	12.08
10+78		17.7	126.1
"	100' RT	20.4	123.4

Cont'd Page 3

Walker
 Hendric
 Becker
 Greet
 12-9-46

Contd from page 2

π
 143.78

TP
 8 Exist
 = 0100

3+00
 3+20
 (3+20
 "

(3+00
 3+50

+60
 +65
 +73

4+00
 "

4+15
 +50

5+00
 "

"
 TP

11+00		175	126.3
+18		168	127.0
+50		95	134.3
+60	3' Rt Conc Ret Wall	2.39	Top of Wall 141.3
"	"	5.5	Ground 138.3
+66		4.5	139.3
+74	End Conc Ret Wall	2.29	Top of Wall 141.3
"	"	3.9	Ground 139.3
+95	79' Rt SE Cor House	2.7	Ground 141.3
12+00		2.1	141.7
+03	Rt NE Cor House	2.4	Ground 141.3
+50		0.8	143.0
TP	10.98	154.05	0.71 143.07
12+96	SE Cor House 79' Rt	10.6	143.5 Ground
13+00		9.2	144.9
+03	NE Cor House 79' Rt	10.6	143.5 Ground
+40		7.8	146.3
+50		8.2	145.9
+95		7.3	146.8
14+00		6.3	147.8
+50		4.8	149.3
+70		5.1	149.0
15+00		7.1	147.0
"	75' Rt	11.3	Ground 142.0
+50		6.7	147.4

π
 154.05

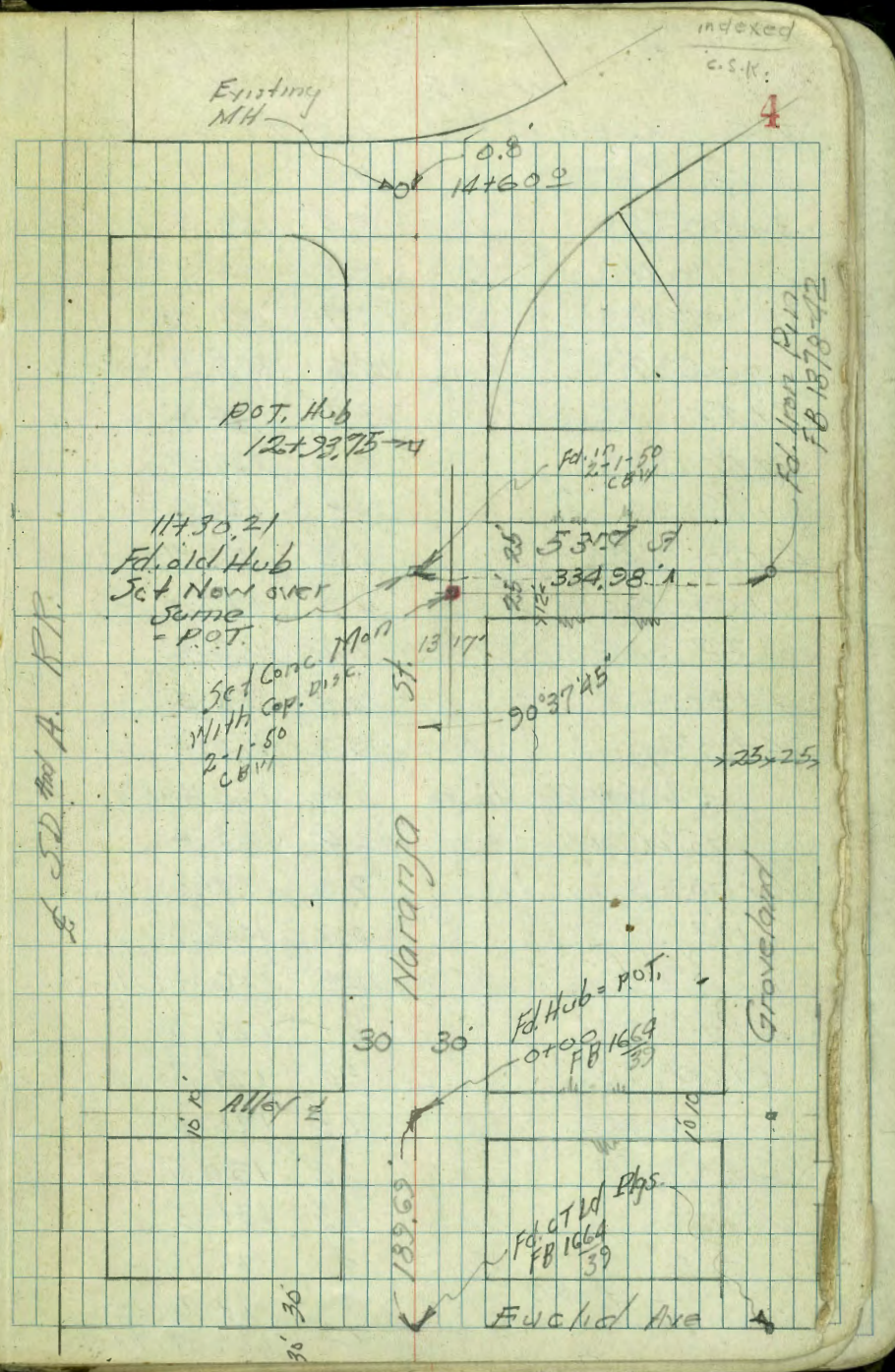
3

+73		20	152.1
+82.72	Alley to East	0.91	on hub 153.14
11.93			165.07
+82.72	30' Lt	14.4	on Ground 150.7
+100		9.9	155.2
+30		8.7	156.4
+50		5.8	159.3
"	35' Rt	7.5	Ground 157.3
"	70' Rt	8.4	156.7
+72		30	162.1
+86		2.2	162.9
TP	11.95	175.56	1.46 163.61
17+00		9.5	166.1
+35		6.1	169.5
"	80' Rt Ground	10.0	165.6
TP	11.06	185.72	1.42 174.14
B.M.	In Care Imperial & Churchward	0.36	184.86
			184.88
			02 OK

Walker
Hendricks
Becker
Greer
12-9-46

Proposed Sewer in Naraia St
from Euclid to 54th

Page 2	008	11685	
= B.M.	on Hub & Alley		116.77
0+00 going West	5.96	110.89	
+20	6.4	110.5	
+60	9.6	107.3	
+80	10.4	106.5	
+100	10.6	106.3	
40' RT	12.3	104.6	
+150	11.2	105.7	
+70	10.4	106.5	
+76	10.7	106.2	
+79.7	10.50	106.35	
+89.69 = Euclid	10.37	106.48	on l.d. ch.
from Alley East			
on Hub & Alley			
= 0+00 going East	5.96	110.89	
0+50	4.5	112.4	
45' LT	3.8	113.1	
70' LT	9.2	107.6	
97' LT	10.3	106.3	
108' LT	13.4	103.5	
+100	3.1	113.8	
+50	1.8	115.1	
2+00	9.5	116.4	
- 23' LT	5.1	116.8	
" 78' LT	9.5	107.4	
" 130' LT	12.3	104.1	



Proposed Sewer Muranga St.
116.85 Cont. from P 4

T.P	12.43	128.89	0.39	116.46
2+50			2.8	119.1
3+00			5.4	123.5
" 60' Lt.			5.0	123.9
" 95' Lt.			9.7	119.2
123' Lt.			15.2	113.7
3+25			3.3	125.6
+50			2.2	126.7
+75			1.4	127.5
4+00			1.2	127.7
100' Lt.			1.9	127.0
T.P	10.02	137.83	1.08	127.81
4+50			2.5	128.3
4+83' Lt.			2.2	128.6
50' = SW Cor House			2.4	128.4
95' Lt. = NW " "			12.4	125.4
5+00			9.0	128.8
+13			2.0	128.8
(5+13) 95' Lt. = NE Cor House			11.4	126.4
5+50			8.7	129.1
6+00			8.0	129.8
" 100' Lt.			11.5	126.3
6+50			7.3	130.6
7+00			6.3	131.5
+09			6.1	131.7
122' Lt. = NE Cor. House			9.8	128.0
"			7.9	129.9

Plumbing this side

Ground Floor

385 50%

137.83

5

7+50			5.1	132.7
8+00			3.7	134.1
8+07			3.6	134.2
(8+07) 135' Lt. = NW Cor. House			2.7	128.1
" " " " "			4.2	133.6
8+50			3.0	134.8
9+00			2.7	135.1
75' Lt.			4.0	133.8
135' Lt.			7.2	130.6
9+50			2.8	135.0
10+00			3.8	134.8
(10+00) 75' Lt.			5.4	132.4
" 150' Lt.			11.7	126.1
10+50			4.6	133.2
+80			4.5	133.3
45' Lt. in Canyon			14.0	123.8
11+30.21 on Hub			3.46	134.37
" " Ground			3.3	134.5
T.P	2.56	143.93	3.46	134.37
11+50			8.4	135.5
55' Lt.			8.6	135.3
90' Lt.			13.3	130.6
12+00			6.1	137.8
75' Lt.			6.3	137.6
100' Lt.			8.6	135.3
115' Lt. = Brown Hill			11.1	132.8

Ground

Floor

E 53rd St.

Proposed Sewer - Narosiju St
Cont. from P. 5

TR 12	143.93		
2+50	12+50	4.4	139.5
3+00	12+93.75 = POT Hub.	3.81	140.12
" 65' Lt.	13+00	3.8	140.1
" 95' Lt.	82' Lt.	6.1	137.8
129' Lt.	104' Lt. = Brown Hill.	12.8	131.1
3+25	13+50	4.4	139.5
+50	13+60	4.7	139.2
+75	79' Lt. - NW Cor. House	6.5	137.4
4+00	" " " "	3.2	140.7
100' Lt.	13+70	5.3	138.6
TR 10	14+00	8.6	135.3
4+50	+25	10.9	133.0
4+83	+35	11.4	132.5
50' Lt. = 51	+45 = West edge Conc. Pav	11.25	132.68
95' Lt. = 1	+60 = 54th St	10.95	132.98
5+00	Drop MH Flow to West	16.21	127.72
+13	Flow North & South	17.70	126.23
(5+13) 95' Lt. = 1	TR 0.49	132.55	1187
5+50	Chk SW Bridge Near Market	11.52	121.03
6+00	F.B. 1632 - Page 28		121.05
" 100' Lt.	FB 1618 " 40		121.12
6+50	FB 1378 " 40		
7+00	" " 51		
+09			
122' Lt.			
"			

Walter
 Hendricks
 Walter
 51281
 12-11-46

Proposed Sewer
 West & East Alley Las Alturas #.4
 Block 16 Location See FB 1664-40

	273	155.87	153.14	E Hub 2000 See Page
0+00		273	en hub	this work
+30		5.1	150.8	
+35		6.6	149.3	
"	50' Lt	8.9	147.0	Ground
+40		4.8	151.1	
+50		4.7	151.2	
"	50' Lt	6.1	149.8	Ground
+85		2.1	153.8	
1+00		1.7	154.2	
"	100' Lt	5.4	150.5	
+50		1.5	154.4	
2+00		3.4	152.5	
"	100' Lt	8.0	147.9	Ground
+30	7.6 Rt	4.19	151.78	4.83 Conc Ramp
+50		5.4	150.5	
3+00		6.2	149.9	
"	100' Lt	9.1	146.8	
+50		6.3	149.6	
+61.40	Alt. 6'09"	6.40	149.47	Hub
"	100' Lt	9.2	146.7	
+80		7.2	148.7	
4+00		8.7	147.2	
"	100' Lt	9.4	146.5	

Indexed
 C.S.K.

7

T
 155.87

+50		9.9	146.0	
+50		8.7	147.2	
+70		11.3	144.6	
+83		11.8	144.1	
+90		14.2	141.7	
+97		11.0	144.9	
5+20		9.8	146.1	
5+35.48	Alt. 7.14 = TP	8.75	147.12	Hub
5+85.90	5'00" 30' Lt			
Location Ahead FB 1664-41				
		7.64	154.76	
6+00		7.2	147.6	
+30		7.1	147.7	
+50		7.2	147.6	
"	40' Rt	6.2	148.6	
7+00	Prop. 20' Rt above B	5.8	149.0	
+50		4.5	150.3	
8+00		4.8	150.0	
"	100' Lt	6.0	148.8	Ground
+50		4.8	150.0	
+90		5.7	149.1	
9+00		6.2	148.6	
"	125' Lt	7.1	147.7	

Cont'd page 8

Cont'd from Page 7

 T
 15476

9+40		5.5	149.3	
+50		5.2	149.6	
+92.48	ART 16°12'	5.35	149.41	Hub
10+00		5.0	149.8	
+50		4.9	149.9	
"	150' Lt	8.2	146.6	
+97		4.7	150.1	
11+03		5.7	149.1	
+50		5.2	149.6	
+70		5.0	149.8	
"	185' Lt SE Cor. House	7.6	147.2	Floor
"	TP	8.8	146.0	Ground
11+99.67	ART 27.06 15746	4.42	150.34	
	7°16'	8.6	149.8	Floor
12+10	170' Lt SW Cor. House	10.6	146.8	Ground
+42		6.2	151.2	
"	155' Lt SW Cor. House	7.6	149.8	Floor
"		8.7	146.7	Ground
13+00		5.5	151.9	
+46		5.1	152.3	
"	130' Lt SE Cor. House	6.4	151.0	Floor
"		8.1	149.3	Ground
+75		4.9	152.5	
+78		6.5	150.9	
+84		5.9	151.5	
14+00.5	Approx. E 53rd St.	6.1	150.3	
		2.44	154.96	154.96

8

L&T. E. Imperial & 53rd St. per F.R. 166A P. 45

Walker
 Handrichs
 Becker
 Greer
 12-11-46

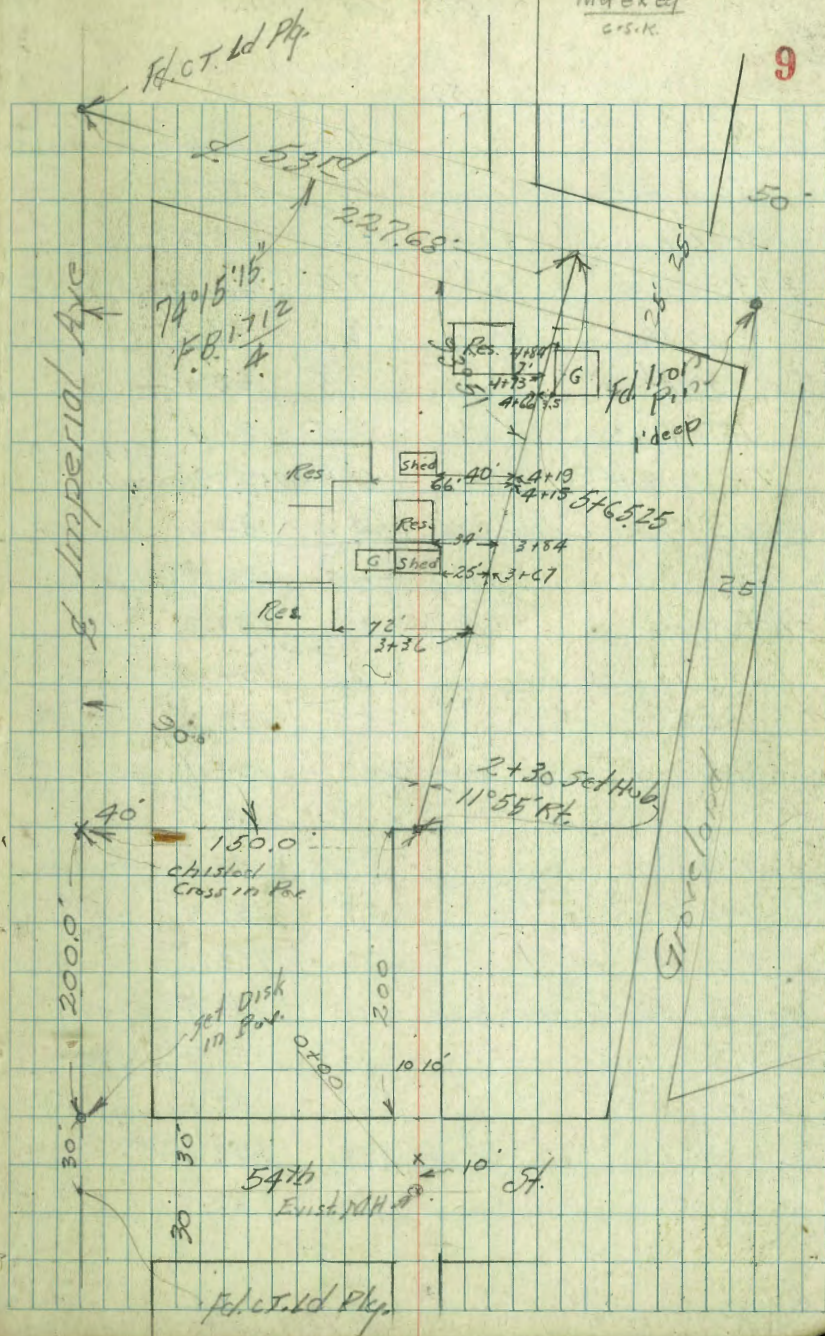
Proposed Sewer Blk. 1
 Las Alturas No 2
 between Imp. Ave and Gavieland
 from 54th St to 53rd St

5th Ct. Id & Imp. & 53rd

Page 8	5.61	160.59	154.98	
0+00				
E. Rm. MH	5.60		154.99	
E. MH Flow	12.04		148.55	
Flow to West	12.05		148.54	
0+15 - West edge Conc. Pav	5.86		154.73	
+25	6.0		154.6	
+50	5.6		155.0	
+77	6.0		154.6	
25' Rt. = SW Cor. House	4.4		156.2	Floor
	6.3		154.3	Ground
1+00	5.8		154.8	
+50	6.6		154.0	
50' Rt	7.0		153.6	
2+00	6.9		153.7	
+26	6.7		153.9	
	6.3		154.6	Floor
72' Rt = SW Cor. House	7.7		152.9	Ground
1+95 67' Rt. NW Cor. Gar	7.3		153.3	Truss
2+30 = Δ Rt 11°55'	6.66		153.93	
2+50	6.8		153.8	
30' Lt	5.9		154.7	
30' R	7.5		153.1	

Index of
 c.s.k.

9



Blk. 1

160.59

2+20		-7.0	153.6	
30' R		7.9	152.7	
30' L		6.3	154.3	
3+30		7.4	153.2	
30' Lt.		6.6	154.0	
30' Rt.		7.5	153.1	
100' R		2.5	151.1	
TP 4+48	158.41	6.66	153.93	2+30 on Hub
3+65	75' Lt. N.W. Cor. House	4.4	154.0	Ground
"	"	1.5	156.9	Floor
3+70		5.2	153.2	
25' Lt		4.4	154.0	
35' Rt.		5.5	152.9	
3+84	34' Lt. N.E. Cor. House	4.3	154.1	Ground
"	"	+4.7	163.1	Floor
4+00		5.6	152.8	
40' Rt.		6.7	151.7	
20' Lt.		5.3	153.1	
4+23	N.W. Cor. House, 70' Lt	5.0	153.4	Ground
"	"	2.7	155.7	Floor
+50		6.3	152.1	
30' Lt		5.8	152.6	
20' Rt.		7.3	151.1	

T
158.41

10

4+73	7' Lt. N.E. Cor. House	6.5	151.9	Ground
"	"	4.0	154.4	Floor
TP 5+41	157.00	6.82	151.59	
5+00		5.4	151.6	
35' Rt.		6.1	150.9	
40' Lt.		4.7	152.3	
+65	25' 53rd St	5.7	151.3	
40' Lt.		4.9	152.1	
40' Lt.		6.9	150.1	
L&T	83rd & Imperial	7.00	155.00	154.98
				155.00
				OK. 02

Hendricks
Becker
Greer
12-12-46

Proposed Sewer Line
San Jacinto Drive
Imperial Ave. to Churchward

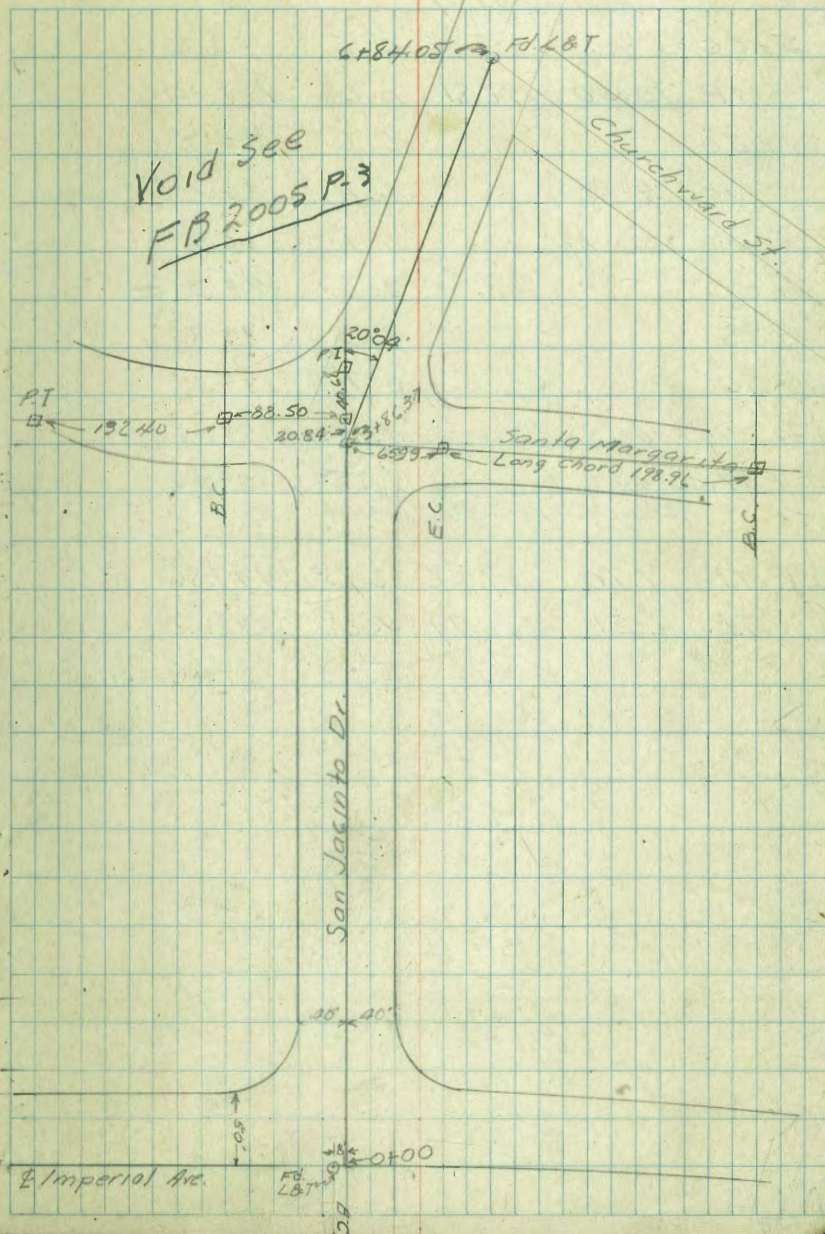
B.M. on Hub in Alley Las Alturas #4 Block 16

5+35.48
5+85.90 see page 7 this book

	12.28	159.40	147.17
0+00	4.23	155.17	
0+09	4.25	155.15	Edge of Paving
+20	4.1	155.3	
+50	3.4	156.0	
"	4.5	154.9	100' Rt.
1+00	1.8	157.6	
TP	12.72	171.65	0.47 158.95
+50	11.8	159.9	
"	11.8	159.9	100' Rt.
2+00	9.3	162.4	
+50	6.5	165.2	
"	5.6	166.1	100' Rt.
3+00	3.0	168.7	
TP	12.33	183.09	0.89 170.76
+50	10.8	172.3	
3+86.37	8.45	174.64	20°04' Rt. Hub
4+00	7.1	176.0	
"	9.1	174.0	100' Rt.
+50	4.4	178.7	

Indexed
e.s.R.

11



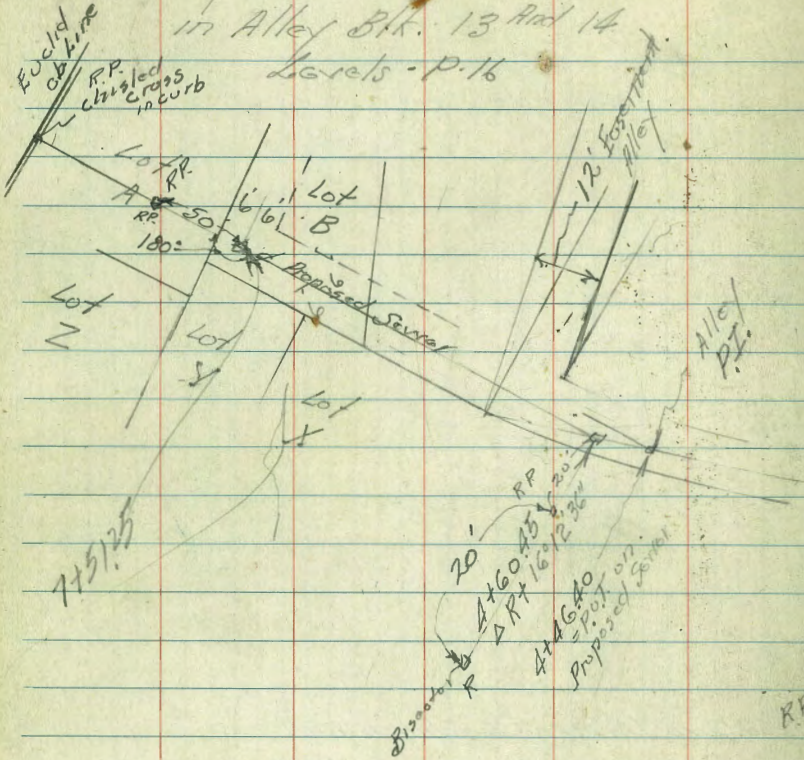
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π
783.09

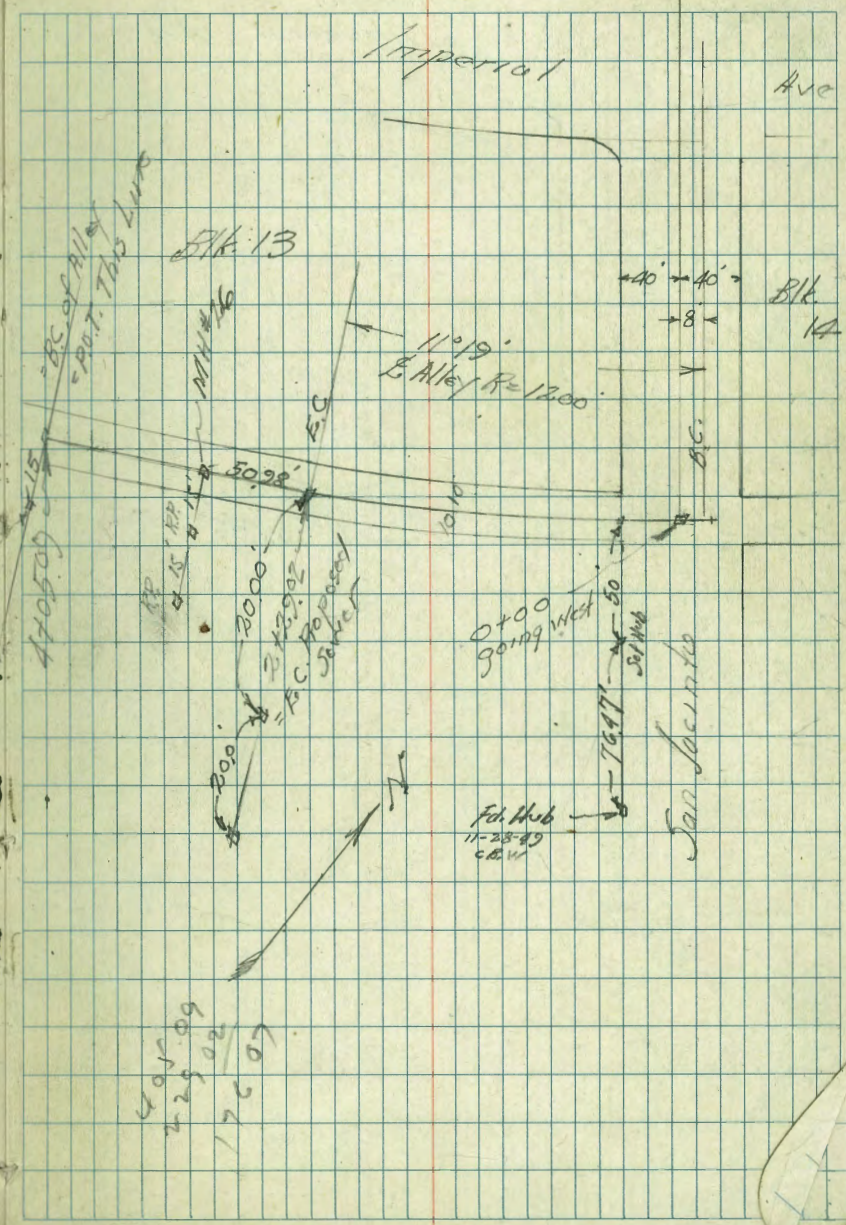
5+00		0.5	182.6
TP 10.40	192.81	0.68	182.41
150		6.6	186.2
" 89' Rt		6.4	186.4
" 150' Rt		11.9	180.9
6+00		3.8	189.0
135		3.0	189.8
150		3.7	189.1
+56 Edge of Paving	4.14		188.67
6+84.05 L&T &	3.35		189.46
Churchward & San Jacinto			
TP 9.70	189.56	12.95	179.86
TP 2.51	190.79	1.28	189.28
		5.93	184.86
			184.88
			184.82
		ck	0.02

BP 50 Curb Imperial & Churchward

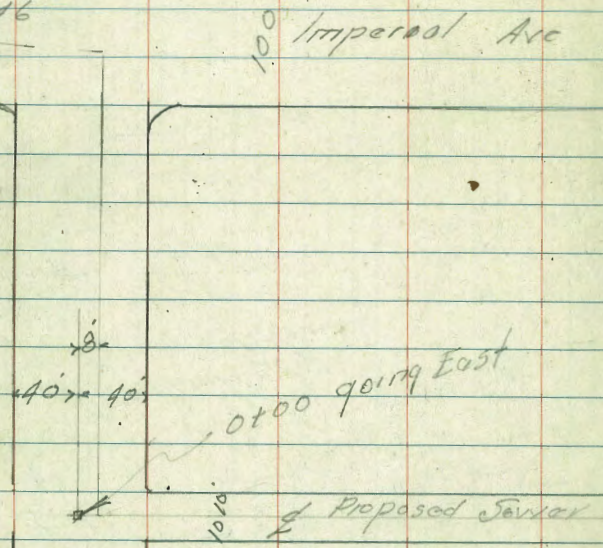
Proposed Sewer - Las Alturas No 4
 in Alley Bk. 13 and 14
 Levels - p. 16



indexed
 c.s.k.

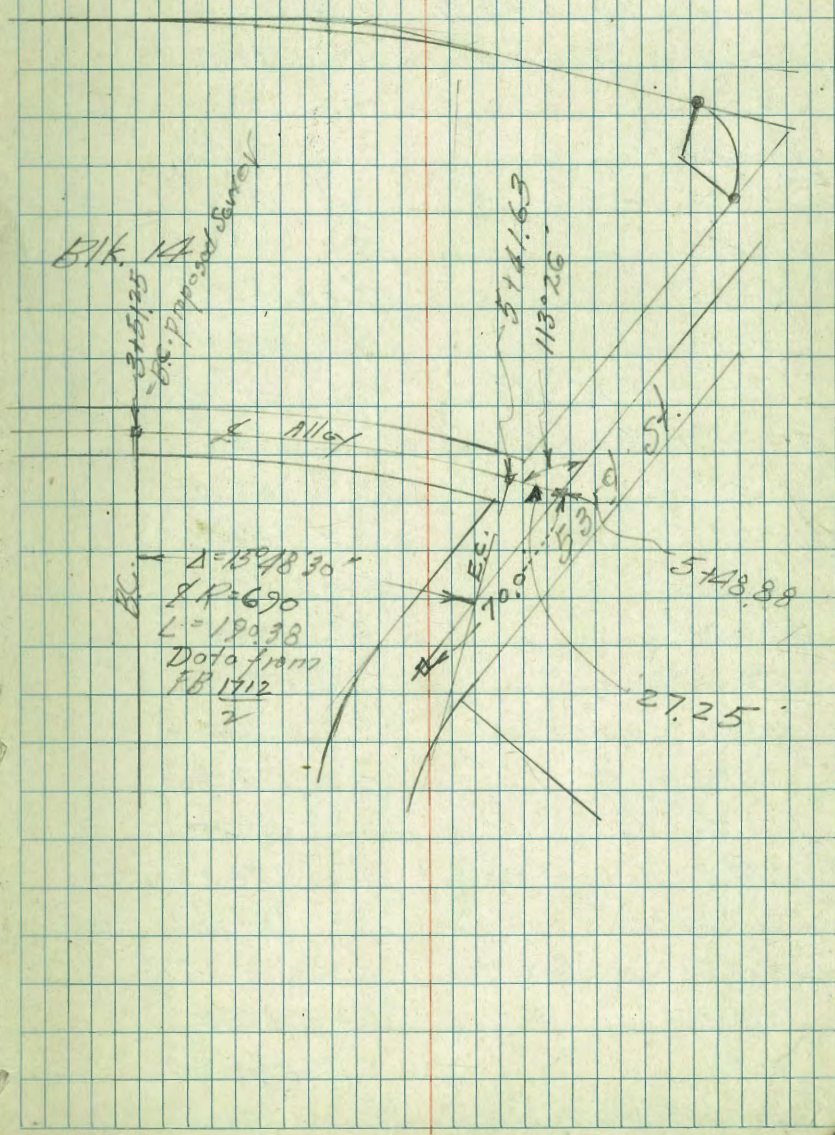


Walker
Handicks
Becker
Greer
12-13-46



San Jacinto

Las Alturas N 4
Proposed Sewer Location
in Alley Blk 14
(Levels P. 18) 14



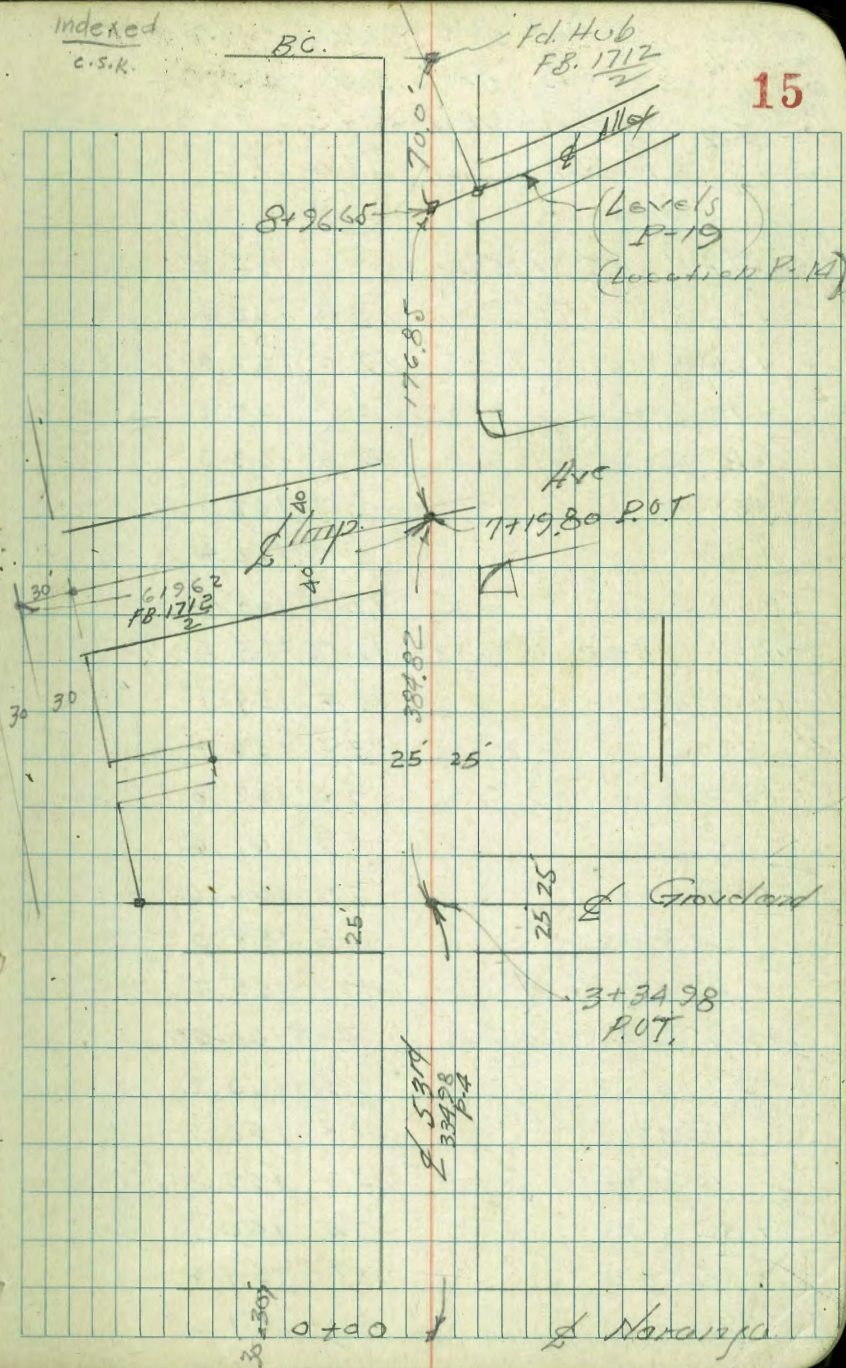
$\Delta = 15^\circ 18' 30''$
 $R = 690$
 $L = 190.38$
Data from
FB 1712

Walker Proposed Sewer Line
 Hendricks on 53rd St. Naranja to E 1st
 Baker Alley So. of Imperial
 75-1346

B.M. & Hub 53rd & Naranja

10.92	145.29	134.37	
0+00	E 53rd & Naranja	10.6	134.7
+50		10.6	134.7
1+00		9.5	135.8
+50		7.7	137.6
2+00		5.4	139.9
+50		2.4	143.9
3+00		+0.1	145.4
T.P.	13.35	157.63	1.01 144.28
3+34.98	E Grandland	11.2	146.4
+50		10.6	147.0
4+00		8.8	148.8
+50		7.4	150.2
5+00		6.2	151.4
+50		5.6	152.0
6+00		5.0	152.6
+50		4.2	153.4
7+00		3.2	154.4
+10.8	N edge Conc Pav	2.8	154.82
+19.80	E Imp. Ave	2.70	154.93 P-8
+28.8	S. edge Conc Pav	2.75	154.88
7+50		3.4	154.2
8+00		2.9	154.9
+50		3.1	154.5
+26.65	on Hub	2.96	154.67 P-19

Indexed
 c.s.k.



Walker
Hendricks
Becker
Greer
72-1346

Alleg. Blk 13 - Las Alturas N-4
Levels - Proposed Sewer
Location P-13

Note: Elev. on Lt = Above E.

g.M. on Hub			
3+8637 P11	0.52	175.16	174.64
0+00 = San Jacinto	12.8	162.4	
+25	13.0	162.2	
+40	12.7	162.5	
+46	11.9	163.3	
+65	12.5	162.7	
+80	12.8	162.4	
1+00	12.0	163.2	
T.P.	5.93	162.53	1156 163.60
(1400) 60' R		10.4	159.1
" 120"		13.1	156.4
1+40		7.5	162.0
+85		7.9	161.6
2+00		7.9	161.6
50' R		11.5	158.0
100' R		14.0	155.5
2+2902 = E.C. on Hub		8.85	160.68
+50		9.3	160.2
55' R		12.8	156.7
100' R		14.2	155.3
2+82		9.4	160.1
+85		11.7	157.8
+90		9.9	159.6

169.53

16

3+00		9.4	160.1
60' R		10.0	159.5
100' R		10.1	159.4
3+50		7.3	162.2
3+20	(ok but not in order)	8.0	161.5
+60		5.7	163.8
+75		4.0	165.5
+85		2.1	167.4
+95	12.74		
4+05.09 = P.P.T.	180.45	1.82	167.71
60' R		14.2	166.3
100' R		14.1	166.4
4+35		9.4	171.1
+50		6.2	174.3
4+60.45 = Δ P.P.T.	1692.36	4.20	176.3
+75		4.1	176.4
+80		5.0	175.5
5+00		5.1	175.4
50' R		8.8	171.7
100' R		12.5	168.0
5+50		4.7	175.8
+75		4.4	176.1
+85		3.8	176.7
6+00		3.3	177.2
50' R		3.9	170.6
100' R		11.4	169.1
Cont. P.		17	

Alley. Blk. - 13.

Cont. from p. 16

180.45

6+50 2.1 178.4

7+00 1.3 179.2

30'R 3.5 177.0

50'R 6.4 174.1

100'R 9.0 171.5

7+25 0.5 180.0

T.P. 11.22 190.99 0.68 179.77

7+51.25 on Hub 10.40 180.6

" 25'R 13.4 177.6

45'R 15.3 175.7

85'R 18.0 173.0

7+75 10.4 180.6

8+00 9.7 181.3

" 35'R 12.6 178.4

" 65'R 15.0 176.0

chk. 8M. BP 6.13 184.86

church wood
& trip. p. 17

17

Walker
Hendricks
Becker
Giesel
72-73-46

Levels Proposed Sewer
Alley 81K. 14
Los Altos N54
Location P-14

172	176.36	174.64
+0700 P.O.C.	13.9	162.3
+08 F.C. on Hub	13.93	162.43
+30	13.7	162.7
+40 on Hub P.O.T.	11.41	164.95
+50	10.9	165.5
+75	9.5	166.9
1+00	7.7	168.7
" 50' Lt.	12.1	164.3
100' Lt.	16.4	161.0
130' Lt.	19.0	157.4
50' R	3.6	172.8
100' R	0.3	176.1
1+50	5.4	171.0
2+00	4.0	172.4
55' Lt.	7.9	168.5
100' Lt.	12.0	164.4
150' Lt.	17.2	159.2
40' R	1.3	175.1
100' R	+3.0	179.4
2+50	1.5	174.9
T.P.	4.23	180.18
	111	175.25

180.18

18

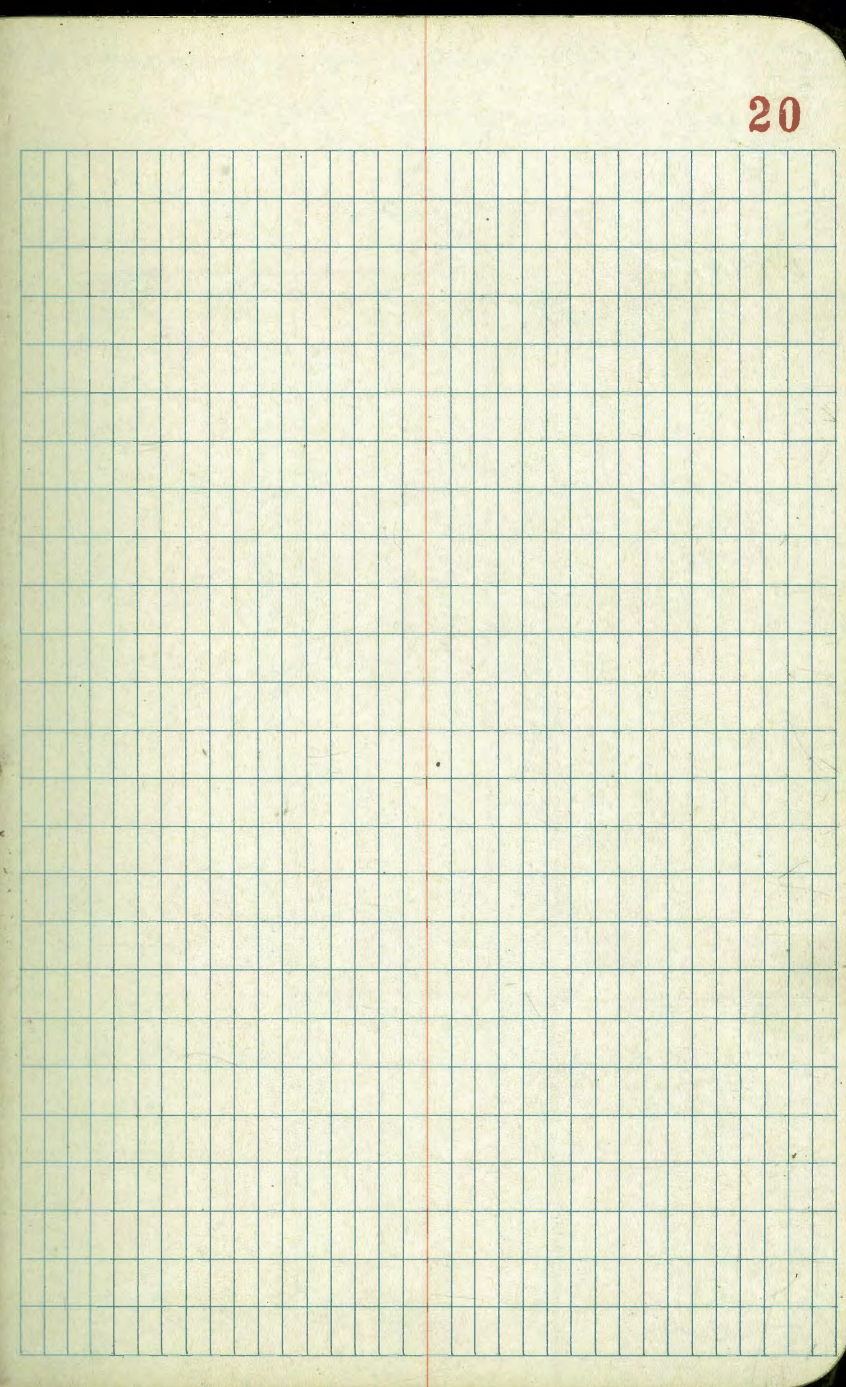
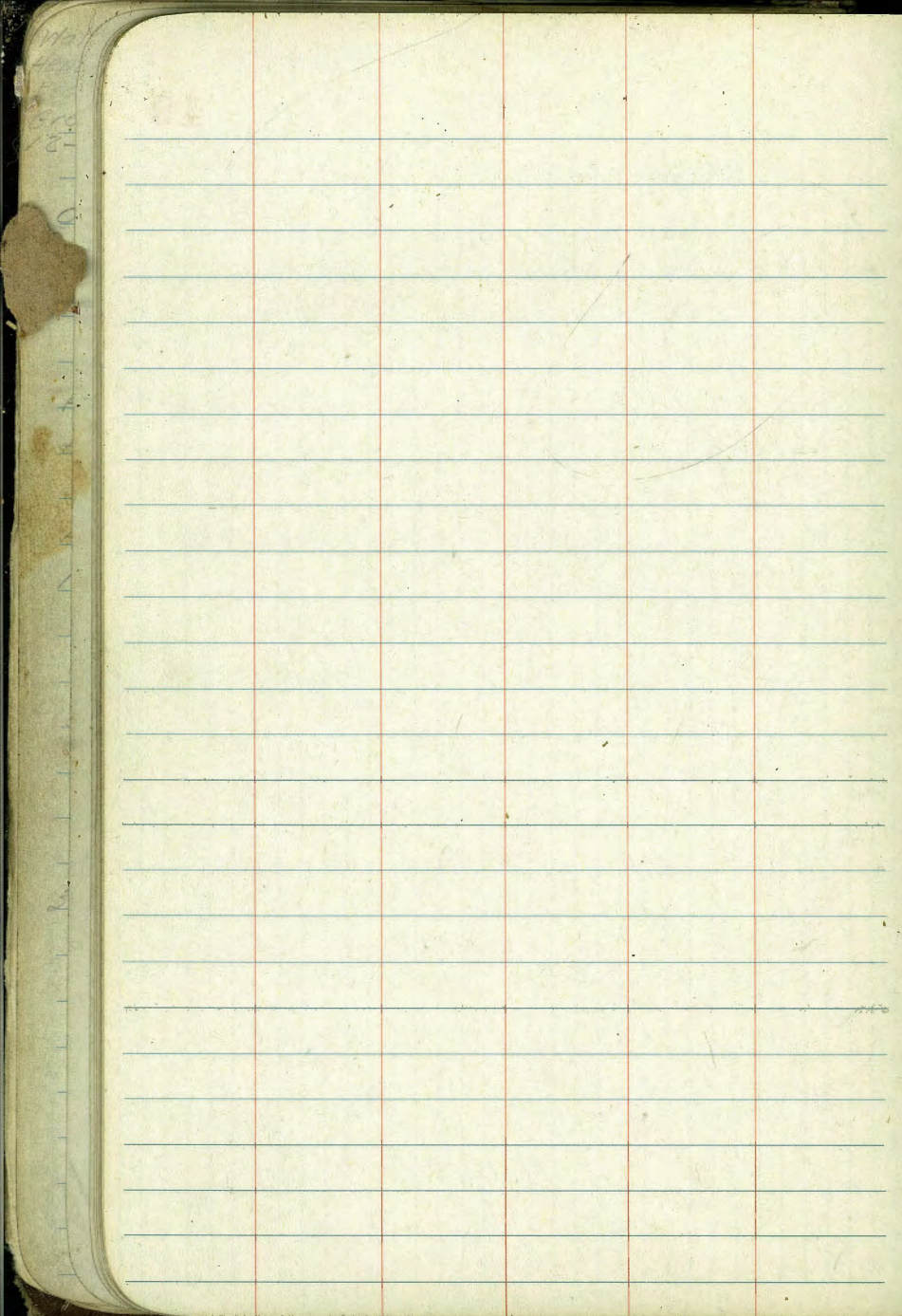
3+00	4.4	175.8
55' Lt.	5.8	174.4
80' Lt.	7.3	172.9
97' Lt.	17.1	163.1
120' Lt.	20.8	159.4
130' Lt.	23.3	156.9
50' R	3.1	177.1
100' R	4.0	176.2
3+51.25 = B.C. Pt.	49.5	175.23
3+65	4.7	175.5
90' Lt.	8.3	171.9
105' Lt.	17.6	162.6
140' Lt.	19.5	160.7
65' R	5.7	174.5
85' R	8.1	172.1
100' R	9.1	171.1
4+00	8.9	172.1
+25	11.0	169.2
+50	13.3	166.9
T.P. 146	168.58	13.06
100' Lt.	11	167.5
128' Lt.	5.2	163.4
137' Lt.	9.4	159.2
170' Lt.	11.5	157.1
100' R	4.8	163.8

Alley Blk 14
Cont. from P-18

168.58

4+94	6.7	161.9
5+25	10.7	157.9
100' H	13.1	155.5
50' R	10.4	158.2
5+4163 = F.C.	12.87	155.71
TP 444 160.15	12.87	155.71
5+60	5.2	155.0
+61	5.5	154.7
+48.88 = 5314	5.42	154.73
Page 15		154.67
		0.06

19



INDEXED
C.S.R.

Profile for Sewer proposed for

Sammermeyer
W. Moore
J. Green

2+69.91 = @ Hiloy
To south L 90°

IMPERIAL HVE

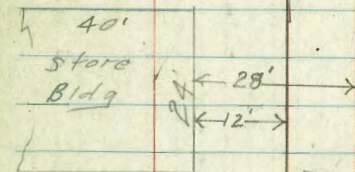
0+83.6
D.E. 8" in
6"

Conc.
Drive

← 16' → * 14' → 30' →
2+20.5

← 192' → 1+96

South line Imp.



Service Station

Approx. position of two
550 gal Gas tanks

1+20.35 L 45° Rt.

47th to South

0+85
L 45° Lt.

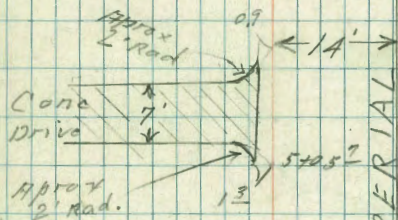
El. line lot 44
Imperial
to North

2 x 12'
pump Island
on line

0+00 → Existing D.E. (8")

Imperial Ave. at 47th ^{80' West} _{644' East}
Work Order 216 Feb. 14, 1947 **21**

Proposed Sewer



IMPERIAL

26'

51'

4+61 = S.W. Cox House

Manzanilla
3+65.28

90°
L 45°

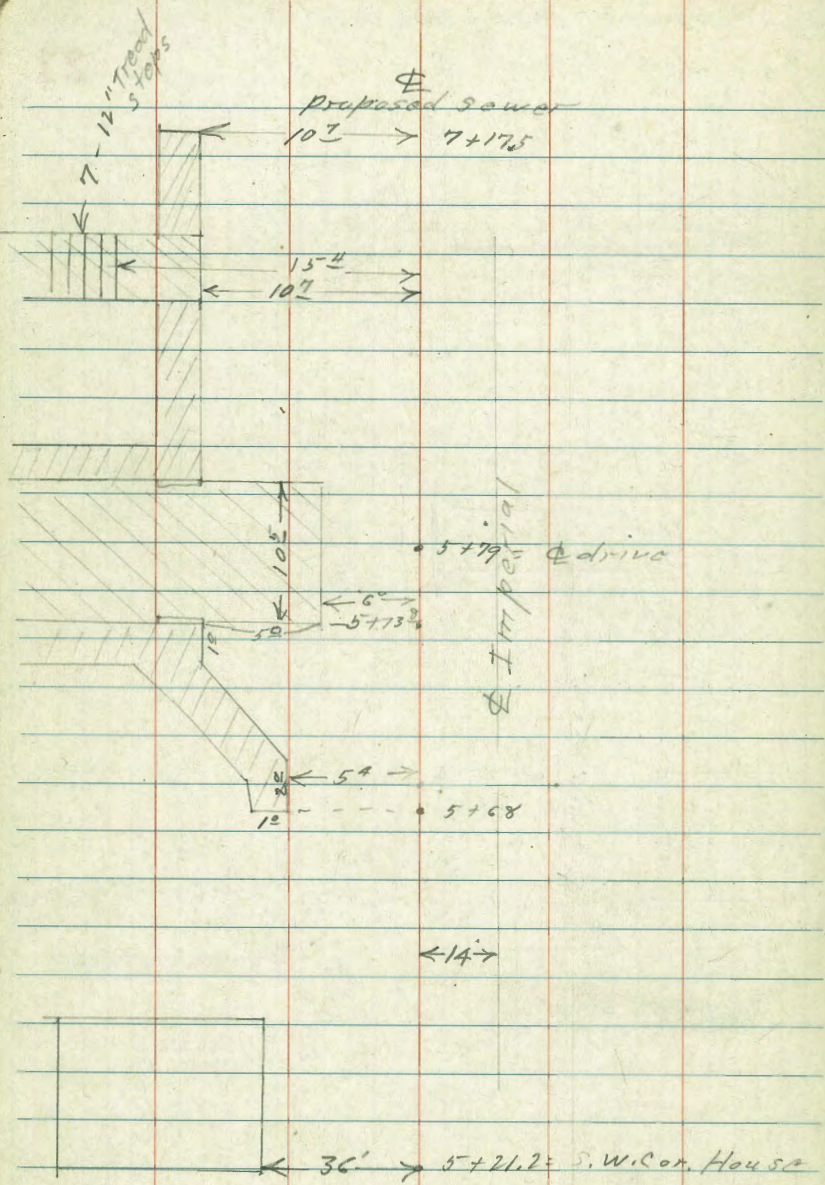
0+85

26'

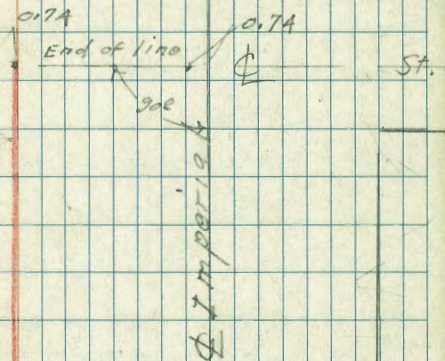
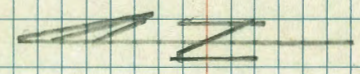
35'

26'

3+04 S.W. Cox Stucco House



Proposed Sewer



Levels. Proposed Sewer at

47th on Imperial.
Sketches Pages 21+22

2/11/47
W.O. 216 23

1+00

0+85⁰⁰ - L. 45° Lt

0+70⁵ = start conc. paving

47TH ST.
0+60 = W.L. Imperial

0+00 = D.E. Existing 8" Line 100' west
of W. Line 47th on Imperial.

SE.B.P.
47th + Imperial 7.33 119.50 — 112.17

±
sewer

112.34
7.16

111.81
7.61 7.69 7.87
3 5

111.39
8.09 8.11 8.2
pav 5 oil pav. patch

111.0
8.54 8.5 8.2
3 pav. 5

109.1
10.31 10.4 10.4
5 Pav. 5

119.50

2+04 Start Conc drive (W. Line drive)

114.9
 $\frac{4.02}{16}$ $\frac{4.51}{16}$ $\frac{4.6}{16}$
 6' 11" S.W. Cor. Drive

1+61 63 Lt. S.W. Cor. Frame house

116.52 113.9 113.7
 $\frac{2.98}{83}$ $\frac{5.6}{83}$ $\frac{5.8}{83}$ $\frac{5.75}{83}$
 Floor 6' 5" Ground 2 1/2 pav.

1+52 Φ Store doorway

114.35 113.3
 $\frac{5.15}{28}$ $\frac{6.2}{28}$ $\frac{6.2}{28}$
 Store floor Ground

1+25 Φ Station (Page 21)

112.95
 $\frac{6.55}{16}$ $\frac{6.9}{16}$ $\frac{6.89}{16}$
 Floor Dirt Island deck

1+20.35
 $120+35 = \angle 45^\circ$ Rt.
 75

112.65
 $\frac{70}{5}$ $\frac{6.85}{4}$ $\frac{6.75}{4}$
 Edges pav.

1+149 = End Conc. Pav.

112.60
 $\frac{6.90}{4}$

119.50

119.50

SE
 47
 Imp

3+04² 26' Lt = S.W. Cor. house

121.66

118.2

7.39

10.2

10.80

2.6
Floor

.26
Edg.

10.9

4.00

129.05

T.P. 10.66 129.05 1.11 118.39

119.50

3+00

118.0

1.1
5

1.5

1.41

4.00

2+74 9' Lt = 1A" pepper tree

2+69.91 = Alley to south

116.9

2.7
5

2.6

2.43

4.00
Edge Pav.

+62 34' Rt = 1A" power pole

2+62 9' Lt = 7" pepper tree

2+33 = 7' Lt = Ctr. 10" Tel. pole

2+31 7' Lt = Ctr. 12" Power pole

2+10.5 End Conc. drive (East Line of drive)

115.5

3.83

4.07

4.0

3.97

16

SE. Cor.
drive

4.00
Edge Pav.

119.50

119.50

5400

8.0	10.2	127.2	
<u>17</u>	<u>2</u>	10.6	12.56
Top bank	Top		4 par

4+98 7° Lt = ctr. 10" Tel. pole

132.02

4+61 51' Lt S.W. Cor. house

5.79	7.7	125.2	
<u>51</u>	<u>51</u>	12.6	
Floor	Alt		

12.56 137.81 3.80 125.25

137.81

T.P.

129.05

4+50

3.2	4.4	124.8	
<u>9</u>	<u>2</u>	4.3	4.25
Top bank	Top		4 par

4+00

5.1	6.8	122.3	
<u>5</u>	<u>2</u>	6.8	6.67
Top bank	Top bank		4 par

3+92 7° Lt = ctr. 10" Tel. pole

3+91 7° Lt = ctr. 10" Power pole

3+50

7.0	120.0	
<u>5</u>	9.1	8.78
		4 par

129.05

129.05

5+21.2 36' Lt. S.W. Cor. house

5+20

+15.7 = 0.9 Lt. = S.E. Cor. Cono. drive.

5+19.7 = E. Line Cono. drive

5+09 = W. Line 7² Main drive (Page 21)

5+05⁷ = S.W. Cor Cono drive

137.81
~~129.05~~

137.88

0.43	4.2
<u>36</u>	<u>36</u>
Floor	od.

128.0

5.8	5.5	7.8	9.63
<u>8</u>	<u>700</u>		<u>4 par</u>
Top bank			

7.85
0.9

6.93	9.13	9.84	127.9
<u>16</u>	<u>3.6</u>	<u>0.9</u>	<u>7.9</u>

7.07	9.29	10.03	127.6
<u>16</u>	<u>4</u>	<u>1.3</u>	<u>10.2</u>

10.3
1.3
end drive
137.81
~~129.05~~

5+93.8 W. line conc. dr.

5+68 54 ft - start of wall (Page 22)

6+55 8' L1 = ctr 10" Tel. pole

6+50

T.P. 10.81 144.19 4.43 133.38
129.05

6+00

5+49

129.05

7.91	8.58	9.16
16	17	6
00 Dr.	00 Dr.	5.44.00 Dr.

7.09	9.3
5.4	5.4
top	cd.
Wall	

5.3	10.6	133.5	
10	2	10.7	10.72
top	top bank		4 pay.
		144.19	

0.0	9.2	6.4	6.35
9	1		4 pay
top bank	top		

3.5	4.3	8.6	8.55
10	3	137.81	3.20
	top bank	129.2	

T.P.

10.81 133.38

144.19

7+64.17 End of Imperial Line

7+26 110' Lt = S.W. Cor House

7+19

7+17E 107' Lt = End wall (Page 22)

6+99 - Φ 3' wide walk 107' Lt5+84.3 East line Conn. Dr. - Page 22
also S.W. Cor. house 82' Lt

144.19

 Φ

137.7

 $\frac{6.4}{5}$

6.5

 $\frac{6.35}{4 \text{ pav}}$

148.99

+4.9

110
floor

136.4

7.8

136.1

 $\frac{5.5}{10}$ $\frac{7.9}{2}$
Top

8.1

8.00

1. pav

 $\frac{7.3}{10.7}$
adj.

135.6

7.66

7.79

8.6

8.68

4 pav.

15.4
Bot of
Botstop10.7
@ walk

7.71

16
on Dr

8.47

on Dr

8.86

S.E. Cor
Dr. into

*2.0

82
Chol

+4.0

Floor
82

144.19

Profile for sewer in 19104 East

of A 7.th Imperial South.

30

123.05

0+44 So. line Imperial.

116.2		
$\frac{4.8}{70}$	6.9	$\frac{8.1}{75}$

0+22 S. Edge Imperial paving

117.06		
$\frac{5.84}{5}$	5.99	$\frac{6.15}{5}$

0+13 Φ Paving

117.15		
	5.90	

0+04 N. Edge Imperial paving

117.08		
$\frac{5.84}{5}$	5.97	$\frac{6.12}{5}$

0+00 = sta. 2+69.91 Page 25

117.0		
	6.1	

T.P. 163 123.05 12.51 121.42

0.55 133.93 — 133.38

orig B.M.
page 23

10.88 112.17 ok

123.05

0+83.64 = D.E. Existing 6" in alley

$\frac{6.2}{70}$

115.5
7.6

$\frac{85}{75}$

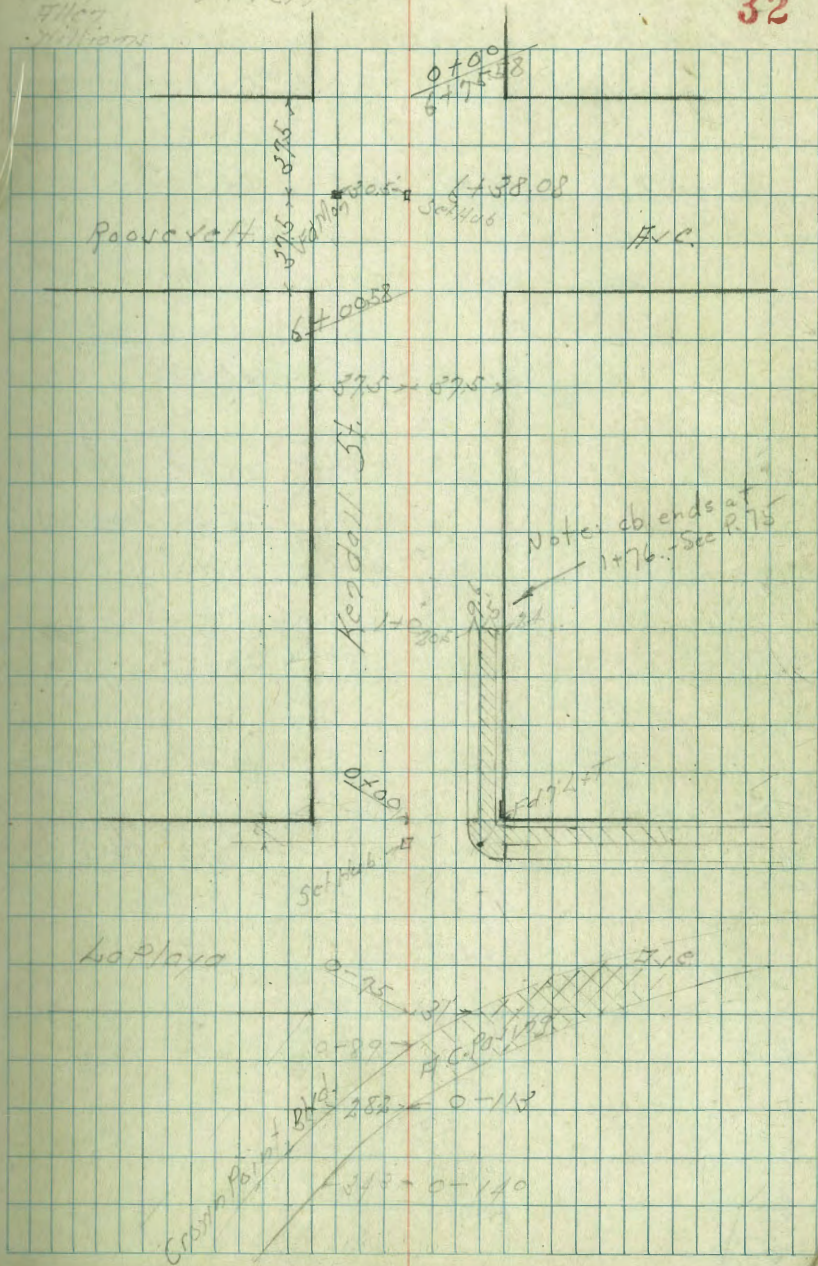
129.05

Cross Section Kendall St
 Crown Point Drive to Pacific Beach Drive

June 26-47
 S.W. McCoy
 Tiller
 Williams

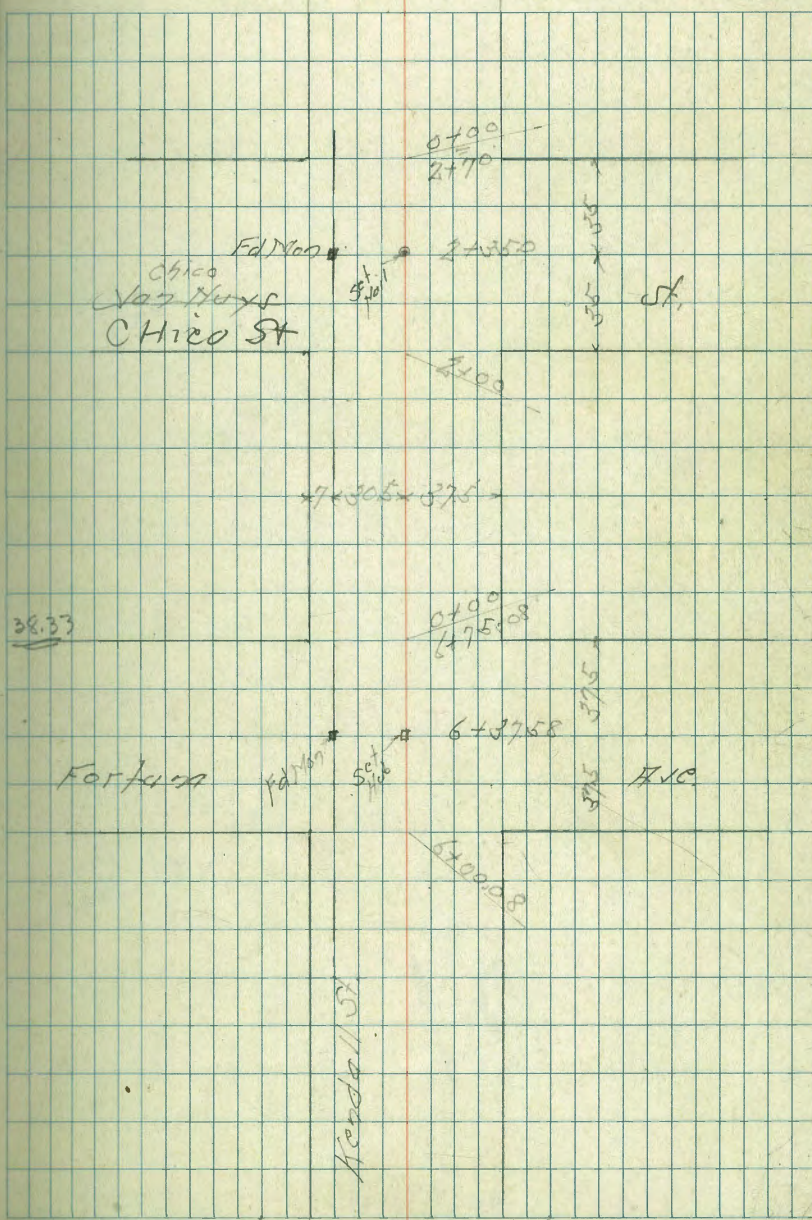
Indexed
 C.S.K.

32



Re Check BM Kendall St
 Grand Ave to La Playa
 Adjusted to Bench Levels + Cross Sections

BM	5.11	5.6.62		51.51	1188 P. Grand Ave Kendall
	3.31	56.91	3.02	52.60	
	1.86	52.85	5.92	50.99	
	3.96	50.47	6.34	46.51	
BM	2.34	47.74	5.07	45.40	524.7' Lot Pacific Beach Co. Kendall
			2.33	45.41	073' Tia So
	2.16	41.56	8.34	39.40	
			Something Wrong		
BM	4.32	36.99	8.89	32.69	65? Mon 2101116 Kendall
	0.74	31.58	6.15	30.84	
BM	6.09	31.81	5.86	25.75	70' Mont Roosevelt 172' Kendall
	3.19	29.57	5.43	26.38	
BM			4.54	25.03	02' NIT Lot La Playa + Kendall



Bench Levels Kendall St. No. 900

BM 5.99 57.50 51.51 NW 1/4 Grand Ave. Kendall

TP 1.89 54.66 4.73 52.77

TP 3.39 50.82 7.14 47.52

BM 0.87 46.46 5.23 45.59 SW 1/4 Pacific Beach Kendall

TP 3.07 39.62 9.91 36.55

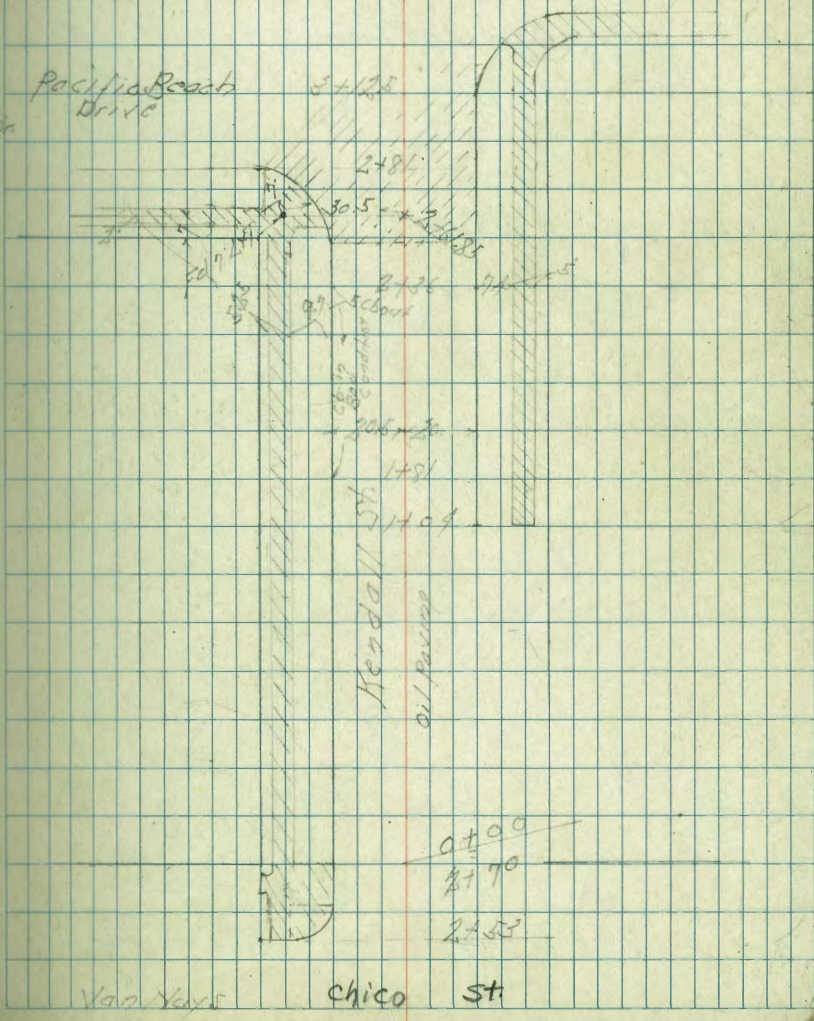
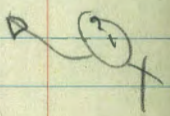
BM 3.39 36.24 6.77 32.85 No. 2 Fort St. Kendall

TP 3.63 31.46 8.41 27.23

BM 5.16 31.06 5.56 25.90 No. 2 Roosevelt Kendall

BM 5.84 25.22 NE 1/4 La Playa Kendall

0.2 High



TP 534 30.36 4.75 2502 ^{24.52+1} La Playa + Headfall

140 ✓ - Note: Sect. checked in Red have changes. - Actual Elev. Shown.

Sections checked thus are
0+79 O.K. - Checked 9-28-50
7.0.

0+50 ✓

0+00 ✓ - Nil La Playa

0-17 ✓ = 5 cb Line La Playa

0-37 ✓ = 2 La Playa

29.77

Note: this Sect. reduced wrong.

27

28

pt.

36

272	262	258	255	25.0	24.9	25.1	25.80	26.1	26.9
37.5	38	38.5	39	38.5	38.5	38.5	38.5	38.5	38.5
	27.97		25.77						
	180		400						
	41-Top of Step.		366-Edge of Headfall						
	263	251	247	24.7	24.6	25.06		25.3	
37.5	38	38.5	39	38.5	38.5	38.5	38.5	38.5	38.5
	26.2	25.0	24.3	24.4	24.1	24.92		25.2	
37.5	38	38.5	39	38.5	38.5	38.5	38.5	38.5	38.5
	24.8	24.5	24.2	24.2	23.7	23.8		24.74	
37.5	38	38.5	39	38.5	38.5	38.5	38.5	38.5	38.5
	24.7	24.4	24.1	24.1	23.8	23.5			
37.5	38	38.5	39	38.5	38.5	38.5	38.5	38.5	38.5
	29.77		29.77						

Kendall St

3+63 P. 75

±50

31.4

41
Top
bank

3+0 ✓

2+50 ✓

2+08 ✓

2+05 ✓

1+97 ✓

1+50 ✓

See P. 75 for add. Improvements

30.36

Lt.

Rt.

Rt.

37

29.9	26.7	26.4	25.5	25.7	25.8	26.9	26.7	28.0
30.5	30.2	30.9	30.9	30.7	30.5	30.5	30.7	30.5
29.1	26.6	26.5	25.3	25.7	25.6	26.7	26.3	27.8
30.5	30.8	30.9	30.8	30.7	30.5	30.5	30.4	30.5
28.4	26.4	26.3	25.3	25.5	25.2	26.4	26.2	27.7
30.5	30.2	30.5	30.6	30.9	30.7	30.5	30.4	30.5
29.88	26.34	25.8	25.4	25.4	25.1	26.2	26.3	26.8
30.5	30.5	30.5	30.5	30.5	30.5	30.5	30.5	30.5
27.5	26.5	25.6	25.0	25.4	25.8	25.0	25.47	25.57
30.5	30.5	30.5	30.5	30.5	30.5	30.5	30.5	30.5

385, 50%

Top
bank

Top
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+42 - P. 75

+13 ✓

5+0 ✓

+95 ✓

+77 ✓

+50 ✓

+12 - P. 75

4+0 ✓

30.36

47

48

pt.

38

37.5	24.2	29.6	28.1	27.49	26.1	26.2	26.8	26.9	27.7
37	26.7	27.6	26.6	26.0	26.1	26.2	26.8	26.9	27.7
39	26.5	26.9	26.6	26.0	26.1	26.2	26.8	26.9	27.7
20.5	25.6	25.7	26.0	26.0	26.1	26.2	26.8	26.9	27.7
35	25.9	26.0	26.0	26.0	26.1	26.2	26.8	26.9	27.7
37	26.7	26.7	26.0	26.0	26.1	26.2	26.8	26.9	27.7
20.5	26.7	26.7	26.0	26.0	26.1	26.2	26.8	26.9	27.7
38	26.6	26.9	26.0	26.0	26.1	26.2	26.8	26.9	27.7
37.5	28.4	28.0	26.0	26.0	26.1	26.2	26.8	26.9	27.7

28.7
 35.6
 38.1
 37.5
 39
 20.5
 37
 20.5
 38
 37.5
 28.02
 27.63
 28.88
 28.88
 28.0
 28.0
 28.0
 28.0

30.36

Kendall St.

6+75.58 = N Roosevelt Ave

+58.52 = N Curb Line

TP 8.72 3442 466 2570 ✓ ²⁷¹¹⁰⁰ Roosevelt
⁴⁹² Kendall

+3808 = S Roosevelt Ave ✓

+1758 = S Curb Line

6+00.58 = S Roosevelt Ave

+5+85 = P. 25

5+50 ✓

50.36

St.

St.

Pt.

39

27.1	27.2	26.6	26.2	26.3	27.3	27.6
$\frac{7.2}{87.5}$	$\frac{7.2}{87.5}$	$\frac{7.8}{88}$	$\frac{8.2}{88}$	$\frac{8.1}{85}$	$\frac{7.1}{80.5}$	$\frac{6.8}{87.5}$
27.2	26.7	26.1	26.2	26.3	27.4	27.3
$\frac{7.2}{87.5}$	$\frac{7.9}{80.5}$	$\frac{8.2}{88}$	$\frac{8.2}{88}$	$\frac{8.1}{86}$	$\frac{7.0}{80.5}$	$\frac{7.1}{87.5}$
27.0 ✓	26.3 ✓	26.2 ✓	26.4 ✓	26.2 ✓	26.1 ✓	
$\frac{7.2}{87.5}$	$\frac{6.5}{80.5}$	$\frac{7.1}{88}$	$\frac{7.1}{88}$	$\frac{7.2}{80.5}$	$\frac{7.3}{87.5}$	
27.4	26.7	26.5	26.5	26.3	26.7	27.0
$\frac{7.0}{87.5}$	$\frac{6.7}{87.4}$	$\frac{6.9}{80.5}$	$\frac{6.9}{80.5}$	$\frac{7.1}{86}$	$\frac{6.7}{80.5}$	$\frac{7.0}{87.5}$
27.8	27.3	26.8	26.1	26.4 ✓	26.2	27.1
$\frac{7.6}{87.5}$	$\frac{7.1}{87.5}$	$\frac{6.6}{80.5}$	$\frac{7.3}{88}$	$\frac{7.0}{88}$	$\frac{7.1}{85}$	$\frac{6.6}{80.5}$
28.2	26.8	26.1	26.2 ✓	25.9 ✓	27.1	27.3
$\frac{7.2}{87.5}$	$\frac{6.6}{80.5}$	$\frac{7.3}{88}$	$\frac{7.0}{88}$	$\frac{7.5}{88}$	$\frac{7.0}{80.5}$	$\frac{6.6}{87.5}$
27.9						
$\frac{7.5}{87.5}$						

50.36

+50 - New Sect - P. 76

TP 9.30 +56.6' 2.16 36.36'

+70 - 37.5' Lt = Beg. 8" Brick Ret. Wall

39.00
37.5
Top
Wall

0+74 = P. 76

+50 ✓

+45 25' Rt of 1/2 = N 1/4 18" Palm Tree

+30.5 25' " " " " " " " " " "

+24 +17 25' Rt of 1/2 = " " " " " " " " " "

+03 25' Rt of 1/2 = N 1/4 18" Palm Tree

6+75.08 = N.L. Fortune Ave

+57.08 = N. Cb line

6+37.58 = Fortune Ave

		37.6	37.6	37.6	37.0	37.0	38.1	39.0
	37.5	37.5	37.5	37.5	37.5	37.5	37.5	37.5
		35.8	35.1	35.0	34.2	34.7	34.4	35.2
	37.5	37.5	37.5	37.5	37.5	37.5	37.5	37.5
		35.1	34.2	34.4	33.7	33.8	33.4	34.2
	37.5	37.5	37.5	37.5	37.5	37.5	37.5	37.5
		34.5	34.0	33.8	33.6	33.6	33.4	33.9
	37.5	37.5	37.5	37.5	37.5	37.5	37.5	37.5
		34.1	34.1	33.3	33.4	33.4	33.6	33.9
	37.5	37.5	37.5	37.5	37.5	37.5	37.5	37.5
		34.1	34.1	33.3	33.4	33.4	33.6	33.9
	37.5	37.5	37.5	37.5	37.5	37.5	37.5	37.5

153 = N C 6 line

135 ✓ = S 109 N 45 S

119 = S C 6 line = S 1/2 oil Paring

(CHICO ST.)

210 ✓ = S 1/2 109 N 45 S - 373 ft. end fence

1499

1477

45.66

60.8 37.5 20.5 Top Carb.	39.58	60.8 37.5 20.5 ground	39.5	60.8 37.5 20.5 S 1/2 109 N 45 S	39.0	60.8 37.5 20.5 S 1/2 109 N 45 S	39.3	60.8 37.5 20.5 S 1/2 109 N 45 S	39.2	60.8 37.5 20.5 S 1/2 109 N 45 S	39.0
60.8 37.5 20.5 S 1/2 109 N 45 S	39.2	60.8 37.5 20.5 S 1/2 109 N 45 S	39.1	60.8 37.5 20.5 S 1/2 109 N 45 S	38.7	60.8 37.5 20.5 S 1/2 109 N 45 S	38.9	60.8 37.5 20.5 S 1/2 109 N 45 S	38.9	60.8 37.5 20.5 S 1/2 109 N 45 S	39.1
60.8 37.5 20.5 S 1/2 109 N 45 S	40.0	60.8 37.5 20.5 S 1/2 109 N 45 S	38.6	60.8 37.5 20.5 S 1/2 109 N 45 S	38.7	60.8 37.5 20.5 S 1/2 109 N 45 S	38.9	60.8 37.5 20.5 S 1/2 109 N 45 S	38.9	60.8 37.5 20.5 S 1/2 109 N 45 S	39.6
60.8 37.5 20.5 S 1/2 109 N 45 S	39.57	60.8 37.5 20.5 S 1/2 109 N 45 S	38.0	60.8 37.5 20.5 S 1/2 109 N 45 S	38.3	60.8 37.5 20.5 S 1/2 109 N 45 S	38.0	60.8 37.5 20.5 S 1/2 109 N 45 S	38.8	60.8 37.5 20.5 S 1/2 109 N 45 S	39.6
60.8 37.5 20.5 S 1/2 109 N 45 S	39.58	60.8 37.5 20.5 S 1/2 109 N 45 S	38.8	60.8 37.5 20.5 S 1/2 109 N 45 S	38.3	60.8 37.5 20.5 S 1/2 109 N 45 S	38.0	60.8 37.5 20.5 S 1/2 109 N 45 S	38.8	60.8 37.5 20.5 S 1/2 109 N 45 S	39.6

45.66

270 ✓

+50 ✓

+04 ✓ = Sky Curb + Walk on Rt

170

0.795 P. 76

+50 ✓

0.700 ✓
2770 = H. Van Nuys (Chico St.)

45.66

44.11	43.3	44.0	44.3 ✓	44.0	43.3	43.84 ✓
1.55 20.5	2.1 20.5	1.7 10	1.4 10	1.7 10	2.1 20	1.82 20.5 = 66
42.94	42.2	42.8	43.0 ✓	42.8	42.2	42.69 ✓
2.77 20.5	3.5 20.5	2.9 10	2.7 10	2.9 10	3.5 20.5	2.99 20.5 = 66
41.71	40.9	41.4	41.6 ✓	41.3	42.1	43.5
3.95 20.5	4.8 20.5	4.8 10	4.1 10	4.4 20.5	5.6 20	5.52 20.5
40.61	39.7	40.4 ✓	40.4	40.4	41.1	40.66
5.05 20.5	6.0 20.5	5.5 10	5.5 10	5.7 20.5	6.6 20.5	6.52 20.5
39.48	39.2	39.4 ✓	39.4	39.2	39.9	40.66
6.18 20.5 = 66	6.5 20.5 = 66	6.2 10	6.2 10	6.5 20.5	7.8 20.5	7.52 20.5
						40.5

45.66 ✓

Lt.

Z

Rt.

B.M. 6.07 51.52 ^{1/2 W 8P}
^{Grand Ave}
^{W. Kendall}
^{51.51}

TP 4.93 57.59 0.88 52.86

TP 6.69 53.51 3.33 46.85

3+12.5 ✓ = curb BC on Rt

B.M. 4.78 45.40 ^{5/21.7 Lt}
^{102-102 Grand}
^{W. Kendall}

2+8 ✓ = curb EC on Lt

TP 5.01 50.18 0.49 45.19

2+5 ✓ = 5/4 Curb, Paving

2+41 = 2.76
 45.66

45.23	44.83	45.16	45.36	45.20	44.82	45.44
4.95 10	5.35 19	5.02 10	4.82	4.98 10	5.36 20.1-60 ft	4.71 20.1-60
45.27	44.79	44.68	45.25	45.11	44.71	45.28
4.91 10-60	5.39 10-60 ft	5.50 20.5	4.92	5.07 10	5.17 20.3-60 ft	4.90 20.2-60
45.31	44.63	45.08	45.22 ✓	45.09	44.61	45.13
4.95 20.5-60	5.39 20.5-60 ft	5.58 10	4.41	4.57 10	5.05 20-60 ft	4.53 20-60

45.66

Re. PAV. Strip on
 Capistrano Pl
 Lot D Blk 33 Miss. Beach

B.M.	2.48	9.47	6.99	BP
T.P.	2.07	9.13	2.41	7.06
T.P.	6.34	5.46	10.01	-0.88
T.P.	4.61	4.86	5.21	0.25

Top Pav 5.00 -0.14

" " 4.56 0.30

sdw Bayside wk. 4.33 0.53 Walk grade

5.00

fill 0.67

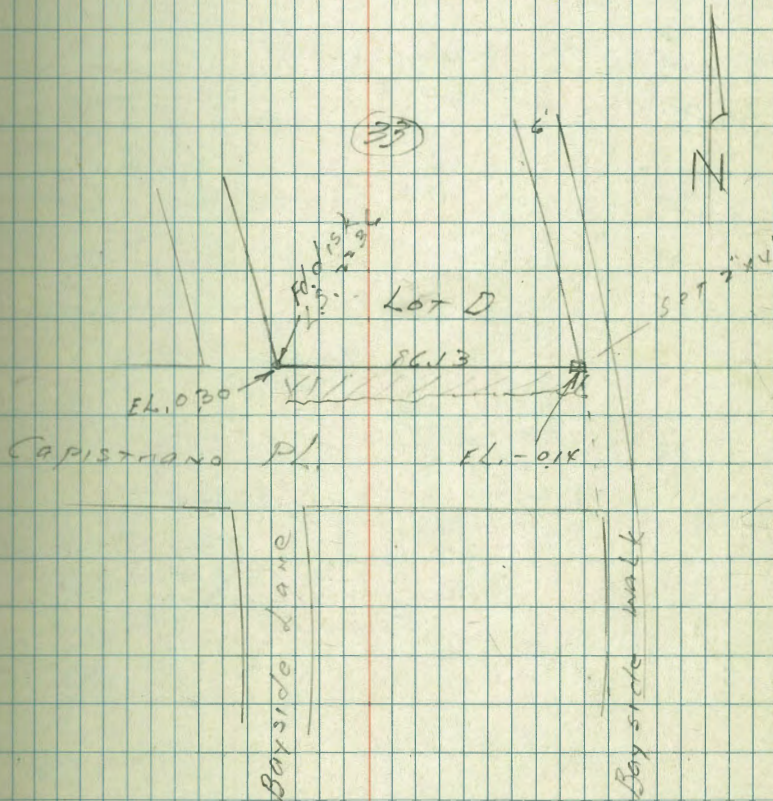
Nolan
 Bogg
 Green
 Robson

W.O. 60135

47

8-25-47

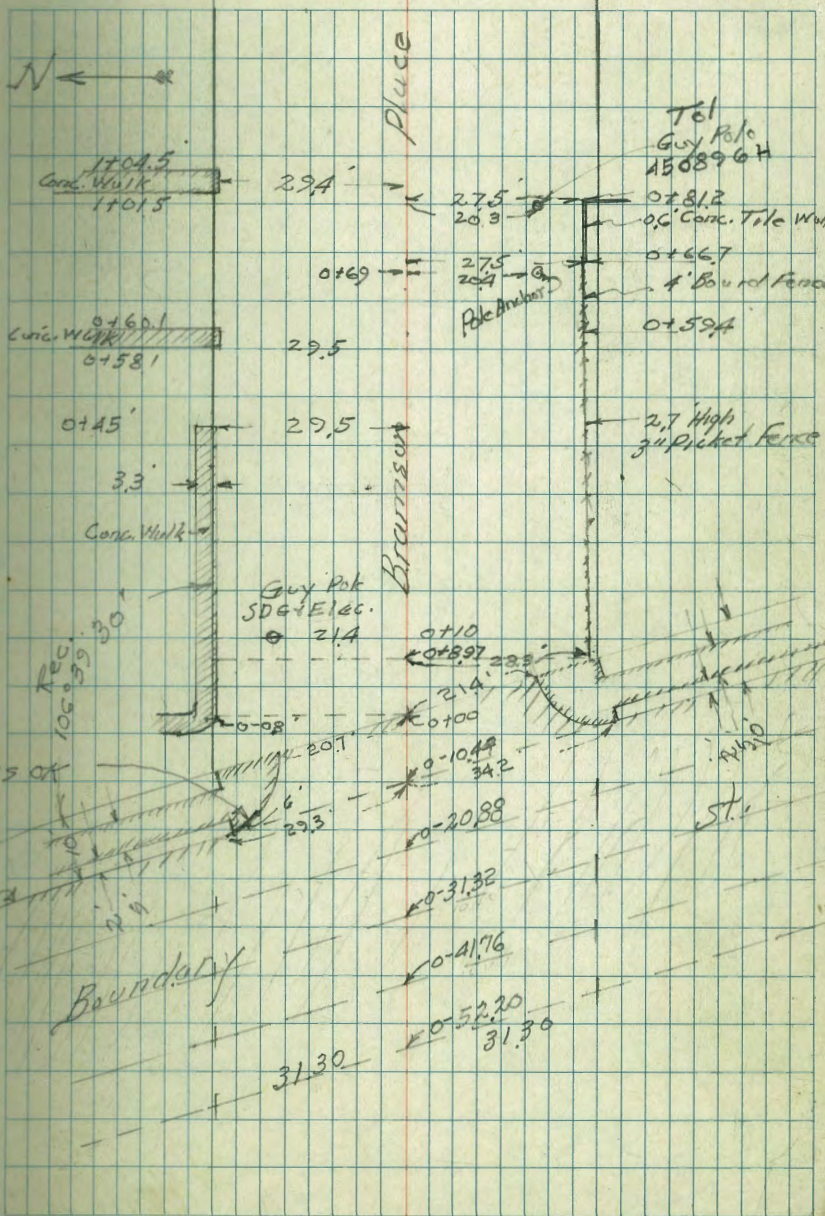
See San Gabriel Pl. and Seawalk



Indexed
CRS:K.

CROSS SECTION - BRAMSON PL. from Boundary St. to 33rd Street.

1+25.7
Conc. Ribbon Dr. 1+23.7
30.4' 27' 1+26.5
Conc. Drive
1+19.5 **48**



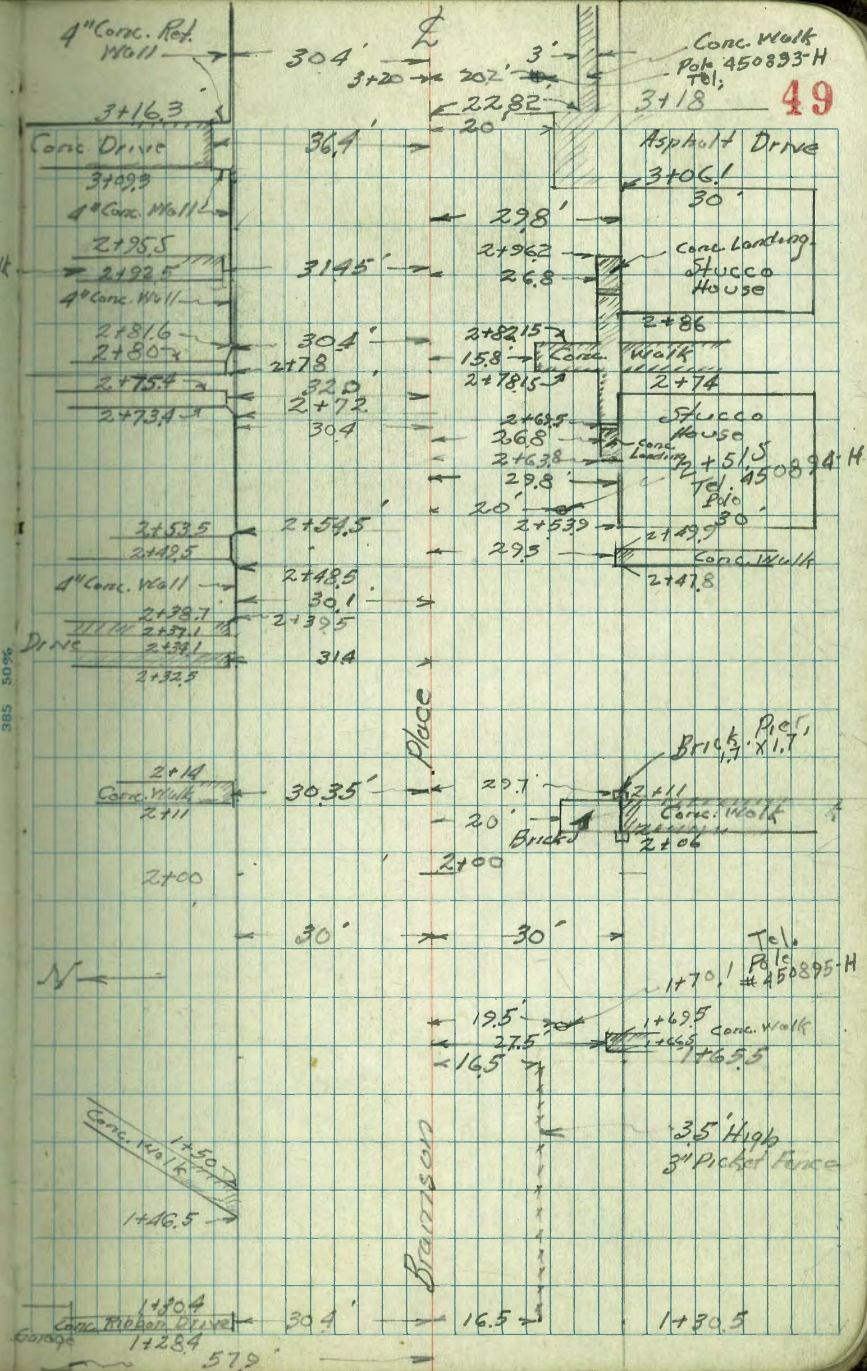
0+22 21.9' 1/4 Guy Anchor

Note:
This portion of cb
The rest of Return
cb wall should be
rebuilt

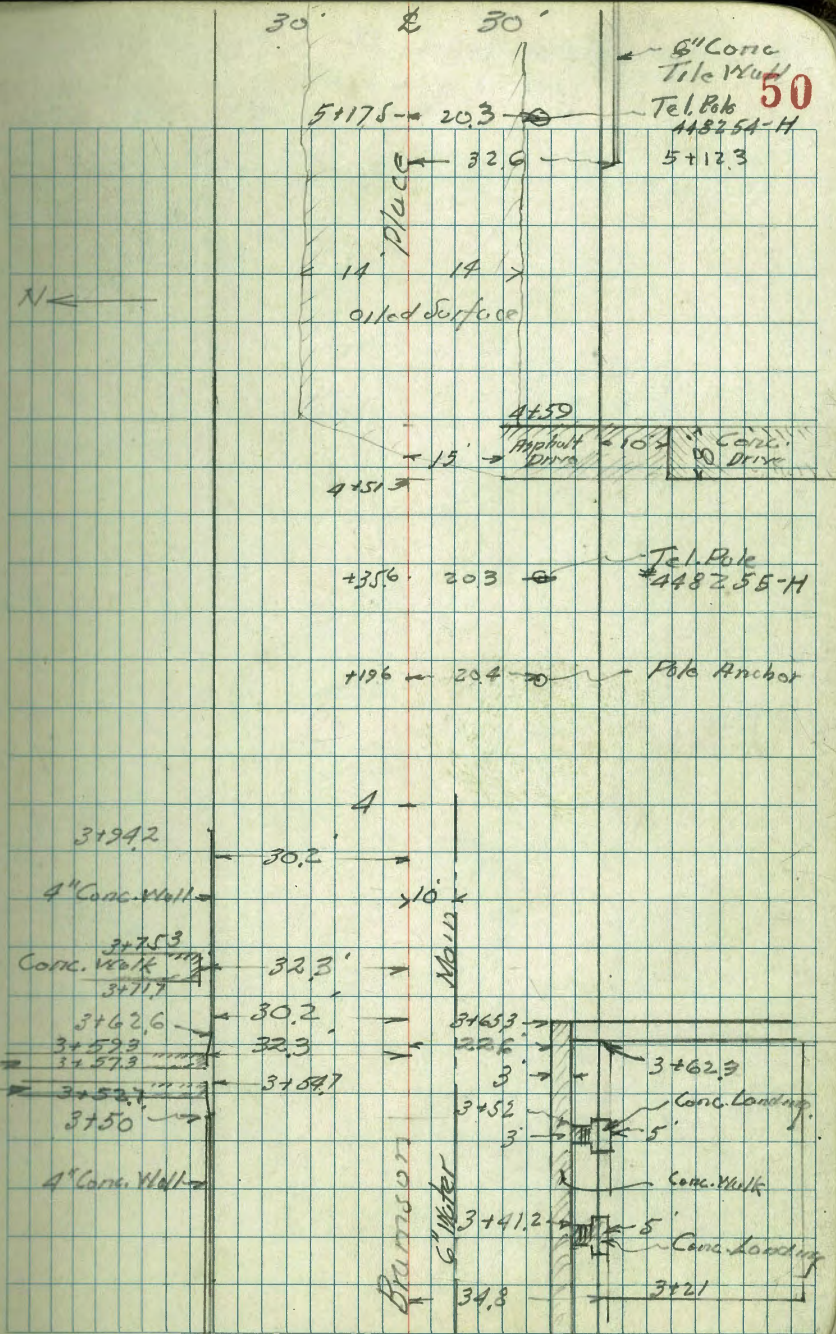
Cb. Line

Boundary

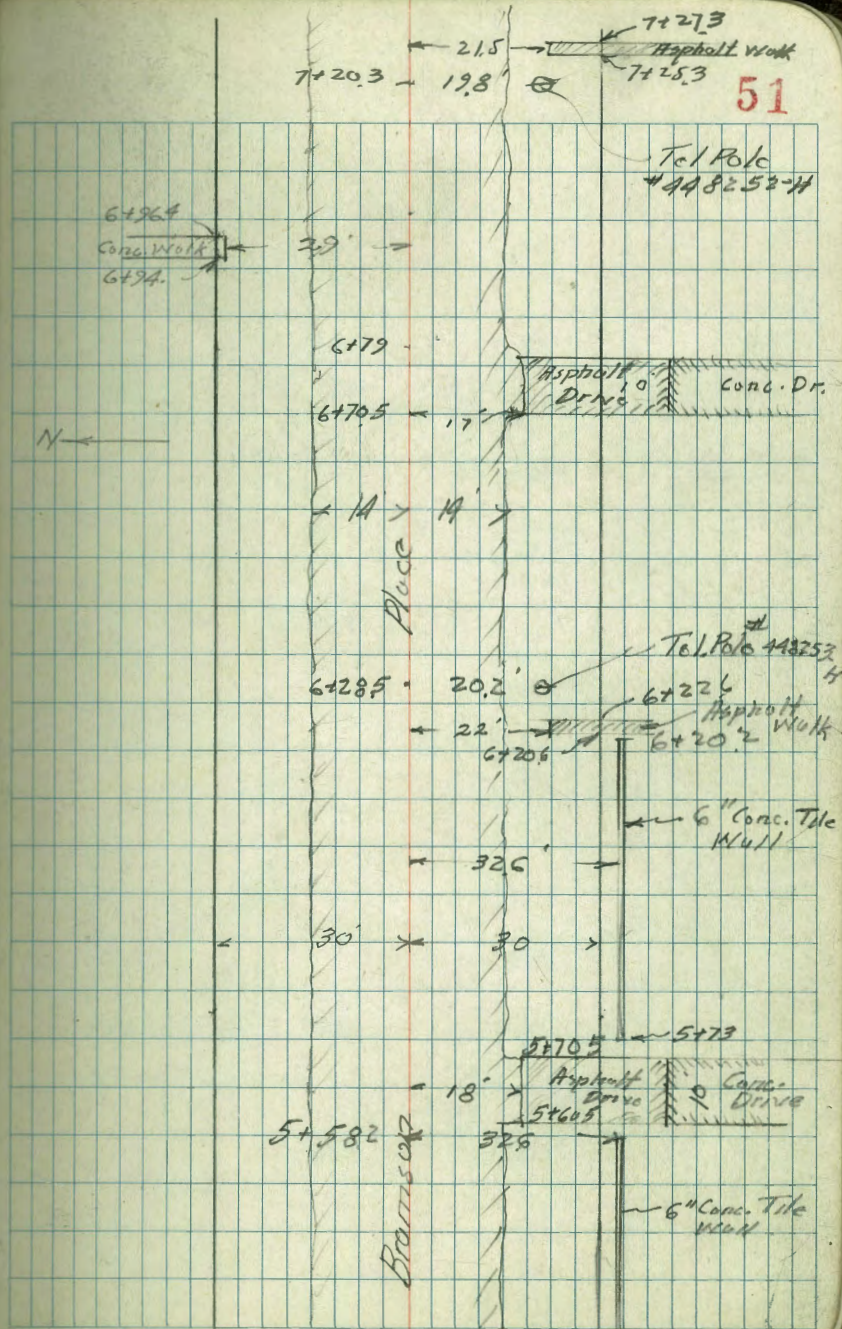
Bramson Pl. X-Sections



Bramson Pl. X-Sections



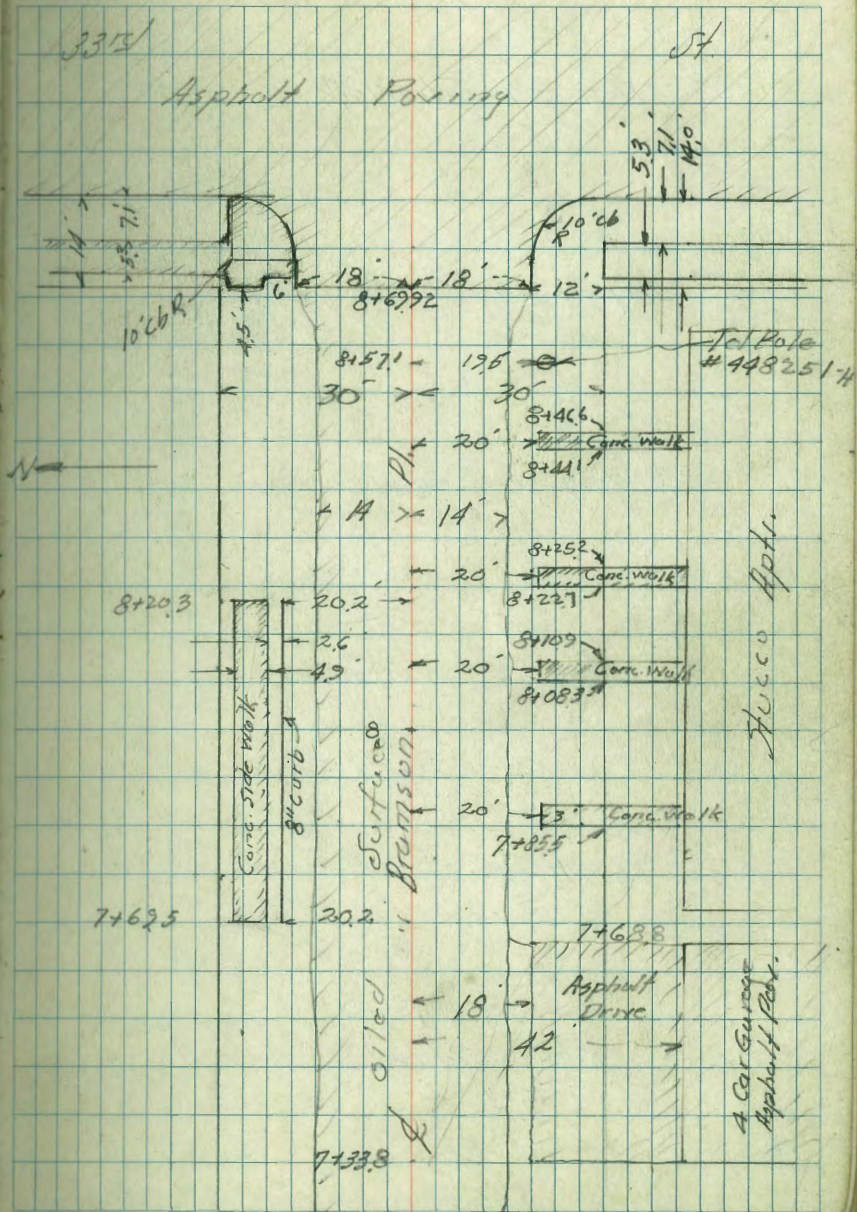
Bramson Pl. X-Sections



Bramson Pl.

X-Sections

52



Bramson Pl.
X-Sections

0-8.36 = West edge Side Walk

0-10.44 = diag Sec East cb Boundary St.

0-20.88 = diag Sec. on Paving

0-31.32 = diag Sec on Pav

0-41.76 = Diag Sec. on Paving

0-52.20 = West cb Line Boundary St. Diag. Sec.

T.P. 5.54 374.48 2.30 368.96

T.P. 3.07 371.26 7.39 368.19

1.33 375.58 374.25

		H	A	H	
					53
		371.61		371.01	
		287 813 cb		347 523	
		371.13		370.41	
		335 813 cut		369.90	
		407 313 cb		370.38	
		458 313 cut		369.85	
		410 233 cb		370.49	
		463 233 cut		369.44	
		504		369.01	
		556 342 cb		368.92	
		616 342 cut		368.43	
		676 813 cb		367.72	
		730 813		367.18	
				371.68	
		289 813		370.41	
		401 313		369.69	
				369.74	
		280 813		369.09	
		397 313		368.26	
				371.38	
		310 813		370.19	
		429 313		369.51	
				369.51	
		589 313 Pav		368.89	
		626 813 Pav		368.22	
				371.40	
		308 813 cb		369.00	
		366 813 cut		369.52	
		424 313 cb		368.84	
		481 313 cut		368.37	
		548 233 cut		367.87	
		496 313 cb		367.187	
		504 313 cut			
		611 313 cut			
		661 813 cb			

B10 SWBR. E1 Canyon - 39rd

Bramson Pl. X. Sections

2+00

1+66

1+50

1+28.4

1+23.7

TP 3.32 371.73 6.07 368.41

1+19.5

1+01.5

374.48

3.33
35

270
40
Walk

231
404
Drive

4.82
29.4
Walk

369.42

243
104
Drive

262
304
Drive

5.3
29.3

2.88
30

2.66
304
Drive

278
30
Walk

279
30

2.78
30
Walk

2.79
30

2.66
304
Drive

369.03

368.95

368.8

369.30

369.07

3.8

4.1

3.6

3.6

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374.48

Bramson Pl. X Sections

3+18

3+121 = Asphalt Drive

3+100

2+962

2+925

2+905

2+816

2+778

2+734

37173

					546 22.82 Walk	366.77		540 25.82 Walk	366.33	
		484 464 Drive	366.89	514 364 Conc. Drive	366.15		540 22 Drive	366.33		525 537 30 40 Drive Drive
		489 30.4 Wall	366.84	522 30 Wall	366.15		540 29.8 of House on Ground	366.17		
		49 40	366.8	527 28 Wall	366.7		540 26.8 Conc. Landing	366.17		
		481 37.45 Wall	366.92	547 30 Wall	366.7		540 26.8 Wall	366.17		
		488 42 Drive	367.45	547 30 Wall	367.26		473 15.8 Conc. Wall	367.11		
		445 32 Drive	367.28	541 31 Wall	367.26		475 30 Wall	367.11		
		428 42 Drive	367.45	541 31 Wall	367.26		475 30 Wall	367.11		
		428 42 Drive	367.45	541 31 Wall	367.26		475 30 Wall	367.11		
		428 42 Drive	367.45	541 31 Wall	367.26		475 30 Wall	367.11		

37173

Bramson Pl. X-Sections

3+65.3

3+94.2 = East end 4" Wall on Lt

3+771.7

3+626

3+593

3+527

3+50

3+397

6.2	6.2	6.7	6.6	6.9	6.8	6.8	6.8
30	30.8	30.4	30.6	22	22.8	25.8	30
Walk	4" Wall	Walk	Walk	Walk	Walk	Walk	Walk
365.5	365.5	365.5	365.5	364.8	364.1	364.8	364.9
6.5	6.4	6.5	6.6	6.5	6.5	6.6	6.8
30	32	30.4	30	30	30	30	30
Walk	Walk	4" Wall	Walk	Walk	Walk	Walk	Walk
365.2	365.3	365.2	365.2	365.7	365.1	365.2	365.3
6.7	6.7	6.7	6.7	6.7	6.7	6.7	6.7
30	30	30	30	30	30	30	30
Walk	Walk	Walk	Walk	Walk	Walk	Walk	Walk
365.1	365.1	365.1	365.1	365.1	365.1	365.1	365.1
6.8	6.8	6.8	6.8	6.8	6.8	6.8	6.8
22	22	22	22	22	22	22	22
Walk	Walk	Walk	Walk	Walk	Walk	Walk	Walk
364.9	364.9	364.9	364.9	364.9	364.9	364.9	364.9
6.8	6.8	6.8	6.8	6.8	6.8	6.8	6.8
25	25	25	25	25	25	25	25
Walk	Walk	Walk	Walk	Walk	Walk	Walk	Walk
364.8	364.8	364.8	364.8	364.8	364.8	364.8	364.8
6.8	6.8	6.8	6.8	6.8	6.8	6.8	6.8
30	30	30	30	30	30	30	30
Walk	Walk	Walk	Walk	Walk	Walk	Walk	Walk
364.9	364.9	364.9	364.9	364.9	364.9	364.9	364.9
6.8	6.8	6.8	6.8	6.8	6.8	6.8	6.8
30	30	30	30	30	30	30	30
Walk	Walk	Walk	Walk	Walk	Walk	Walk	Walk
364.8	364.8	364.8	364.8	364.8	364.8	364.8	364.8
6.8	6.8	6.8	6.8	6.8	6.8	6.8	6.8
30	30	30	30	30	30	30	30
Walk	Walk	Walk	Walk	Walk	Walk	Walk	Walk
364.9	364.9	364.9	364.9	364.9	364.9	364.9	364.9
6.8	6.8	6.8	6.8	6.8	6.8	6.8	6.8
30	30	30	30	30	30	30	30
Walk	Walk	Walk	Walk	Walk	Walk	Walk	Walk
364.8	364.8	364.8	364.8	364.8	364.8	364.8	364.8
6.8	6.8	6.8	6.8	6.8	6.8	6.8	6.8
30	30	30	30	30	30	30	30
Walk	Walk	Walk	Walk	Walk	Walk	Walk	Walk
364.9	364.9	364.9	364.9	364.9	364.9	364.9	364.9
6.8	6.8	6.8	6.8	6.8	6.8	6.8	6.8
30	30	30	30	30	30	30	30
Walk	Walk	Walk	Walk	Walk	Walk	Walk	Walk
364.8	364.8	364.8	364.8	364.8	364.8	364.8	364.8
6.8	6.8	6.8	6.8	6.8	6.8	6.8	6.8
30	30	30	30	30	30	30	30
Walk	Walk	Walk	Walk	Walk	Walk	Walk	Walk
364.9	364.9	364.9	364.9	364.9	364.9	364.9	364.9
6.8	6.8	6.8	6.8	6.8	6.8	6.8	6.8
30	30	30	30	30	30	30	30
Walk	Walk	Walk	Walk	Walk	Walk	Walk	Walk
364.8	364.8	364.8	364.8	364.8	364.8	364.8	364.8
6.8	6.8	6.8	6.8	6.8	6.8	6.8	6.8
30	30	30	30	30	30	30	30
Walk	Walk	Walk	Walk	Walk	Walk	Walk	Walk
364.9	364.9	364.9	364.9	364.9	364.9	364.9	364.9
6.8	6.8	6.8	6.8	6.8	6.8	6.8	6.8
30	30	30	30	30	30	30	30
Walk	Walk	Walk	Walk	Walk	Walk	Walk	Walk
364.8	364.8	364.8	364.8	364.8	364.8	364.8	364.8
6.8	6.8	6.8	6.8	6.8	6.8	6.8	6.8
30	30	30	30	30	30	30	30
Walk	Walk	Walk	Walk	Walk	Walk	Walk	Walk
364.9	364.9	364.9	364.9	364.9	364.9	364.9	364.9
6.8	6.8	6.8	6.8	6.8	6.8	6.8	6.8
30	30	30	30	30	30	30	30
Walk	Walk	Walk	Walk	Walk	Walk	Walk	Walk
364.8	364.8	364.8	364.8	364.8	364.8	364.8	364.8
6.8	6.8	6.8	6.8	6.8	6.8	6.8	6.8
30	30	30	30	30	30	30	30
Walk	Walk	Walk	Walk	Walk	Walk	Walk	Walk
364.9	364.9	364.9	364.9	364.9	364.9	364.9	364.9

371.73

58

Locality

Bramson Pl. X-Sections

TR 4.70 375.63 1.60 370.93

7+50

7+33.8

7+26.3

7+00

6+94

6+75.5

6+50

372.53

Station	Value	Notes
40	369.3	
38	369.5	
37	369.5	
36	369.2	
35	369.5	
2.6	369.9	
3.0	369.5	
27.5	369.76	Drive
243	370.10	Drive
220	370.33	Garage Floor
16.0	369.2	Drive
28.3	369.70	Drive
30.0	370.05	Drive
2.0	370.23	Garage Floor
2.5	369.7	Walk
2.5	369.95	Walk
2.0	370.10	Walk
2.0	370.06	Walk
40	369.0	
38	368.9	
37	368.9	
36	368.6	
35	368.9	
3	369.4	
6	368.8	
19	369.2	
30	369.4	
36	369.4	
40	369.0	
38	369.0	
37	369.20	Walk
36	369.0	
35	368.6	
34	369.03	
33	369.19	
32	369.17	
31	369.09	
30	368.5	
29	369.0	
28	368.4	
27	368.8	
26	368.9	
25	368.9	
24	368.1	
23	368.1	
22	368.6	
21	368.1	
20	368.1	
19	368.1	
18	368.1	
17	368.1	
16	368.1	
15	368.1	
14	368.1	
13	368.1	
12	368.1	
11	368.1	
10	368.1	
9	368.1	
8	368.1	
7	368.1	
6	368.1	
5	368.1	
4	368.1	
3	368.1	
2	368.1	
1	368.1	

Branson Pl. X-Sections

8+29,92 = 33rd

8+26,92 = 14 1/2 33rd

8+83,92 = West cb. 33rd

8+76,8 = East edge Walk. 33rd St.

8+71,5 = West edge side walk 33rd St.

8+6,922 = West Line 33rd St.

8+50

4.8	371.3	47	370.9	45	371.58	419	371.50	414	371.49	398	371.65
30		30		80		80		80		80	
		Wall		Wall		Wall					
4.5	371.1	469	370.94	431	371.32	449	371.70	439	371.24	429	371.34
30		28.5		55		55		55		55	
		Wall		Wall		Wall					
5.0	370.6	476	370.87	466	370.97	469	370.94	467	370.94	451	371.12
21		24		30		30		30		30	
		Wall		Wall		Wall					
5.2	370.4	487	370.76	482	370.81	479	370.84	490	370.73	464	370.99
19		18		13		13		18		18	
		Wall		cb		cb					
5.0	370.6	528	370.55					514	370.49	491	370.72
15		18									
		Wall									
4.7	370.9	518	370.45					536	370.27	505	370.58
17		18						18		18	
		Wall									
5.0	370.6	522	369.81					564	369.99	532	370.31
17		18						30		30	
		Wall									
4.7	370.9	539	370.24					587	369.76	562	370.10
18		18						55		55	
		Wall									
4.6	371.1	559	370.3					614	369.49	535	370.68
30		30						80		80	
		Wall									
4.6	371.0	570	369.12					675	368.88	535	370.68
30		54						80		80	
		Wall									
								602	369.31		

33
33

chk starting BM

139

¹⁰¹
379.25
374.24

9+2592 Cont.

9+3592 = E Cb

331^d

2+2292

37563

411 30	469 30	443 30	496 30	463 18	516 18	487 18	548	567 18	507 18	575 30	512 30	597 55	533 30
cb	cut	cb	cut	cb	cut	cut		cut	cb	cut	cb	cut	cb
	271.52	371.20	370.67	371.37	371.09	370.98	370.68	370.53	370.53	370.53	370.03	369.81	270.24
	371.52	370.99	371.20	371.00	370.47	370.76	370.15	369.94	370.56	369.88	370.51	269.66	270.24
			680 ⁰	440 ⁸⁰					900 ⁰	600 ⁰	600 ⁰		
			371.73	371.23					369.32	369.95			

37563

4/7/48
Sammormayer
W Moore
Sherman

Profile East edge pavement.

Catalina Blvd. - Nty line of
Pt. Loma Manor to Talbot. St.

Santa Barbara + Catalina	3.09	263.77	→	260.68	N.W.B.P.
0+00 = Nty line Pt. Loma Manor		6.6			
+ 25		6.5			
+ 50		6.5			
+ 75		6.6			
1+00		6.6			
+ 25		6.6			
+ 50		6.6			
+ 75		6.6			
2+00		6.6			
+ 25		6.6			
+ 50		6.6			
+ 75		6.5			
3+00		6.5			
+ 25		6.3			
+ 50		6.2			
+ 75		5.8			
4+00		5.0			
± Talbot		2.9			
B.M. Non. wly Catalina at Talbot.	2.22	261.55	(261 ⁹⁰)		
Orig B.M.	3.09	260.68			

Cross Sec. Alley BIK 83 Pt. Loma Hgts.
 Santa Barbara to Guizot
 Between Coronado & Santa Cruz

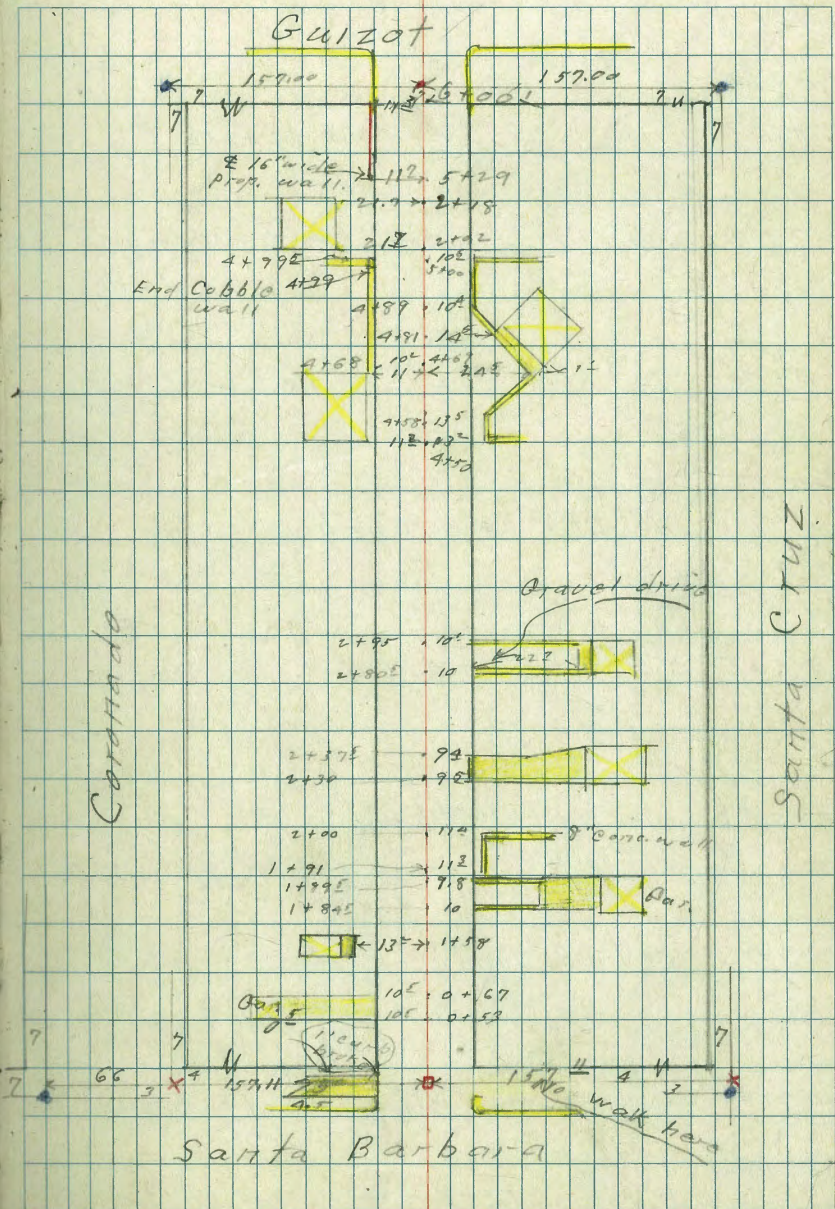
Indexed
 C.S.K.

7-16-48
 W.O. 25001

Sommermeier
 Macey &
 Malton
 Decker

- = Fd. L+T.
- = set 2x2 + disk
- X = cut cross
- = set nail

Also see P 77



0+04

T.P. 10.13 257.69 3.44 247.56

0+00 = W. line Santa Barbara.

0-00⁵ 10⁸ Lt. = Back edge walk

0-01 10³ Lt. = End. Curb

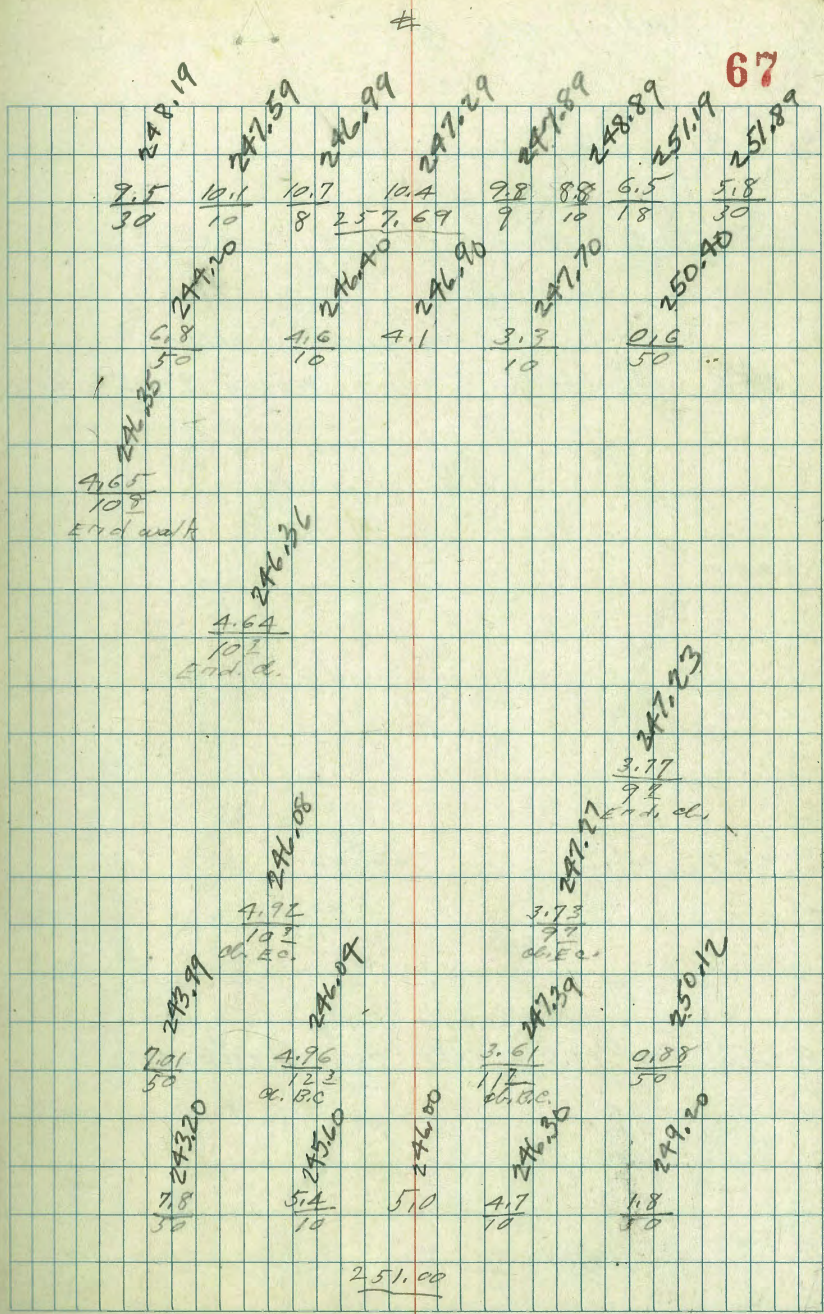
0-05³ 9² Rt. = End Curb

0-08 = Curb. Rot. F.C.

0-10 = W. Ob. line

0-10¹ = W. Gutter line Santa Barbara on dirt.

Coronado
Santa Barbara 10.83 251.00 — 240.17 S.W.B.P.



1+84^E 10' Nt. to Garage.
 = $\frac{1}{2}$ East. 2' ribbon of drive

Gar. N. Edge apron is level.

1+58 13^E Lt. = $\frac{1}{2}$ 8' wide Apron to Singl.

1+50

1+00

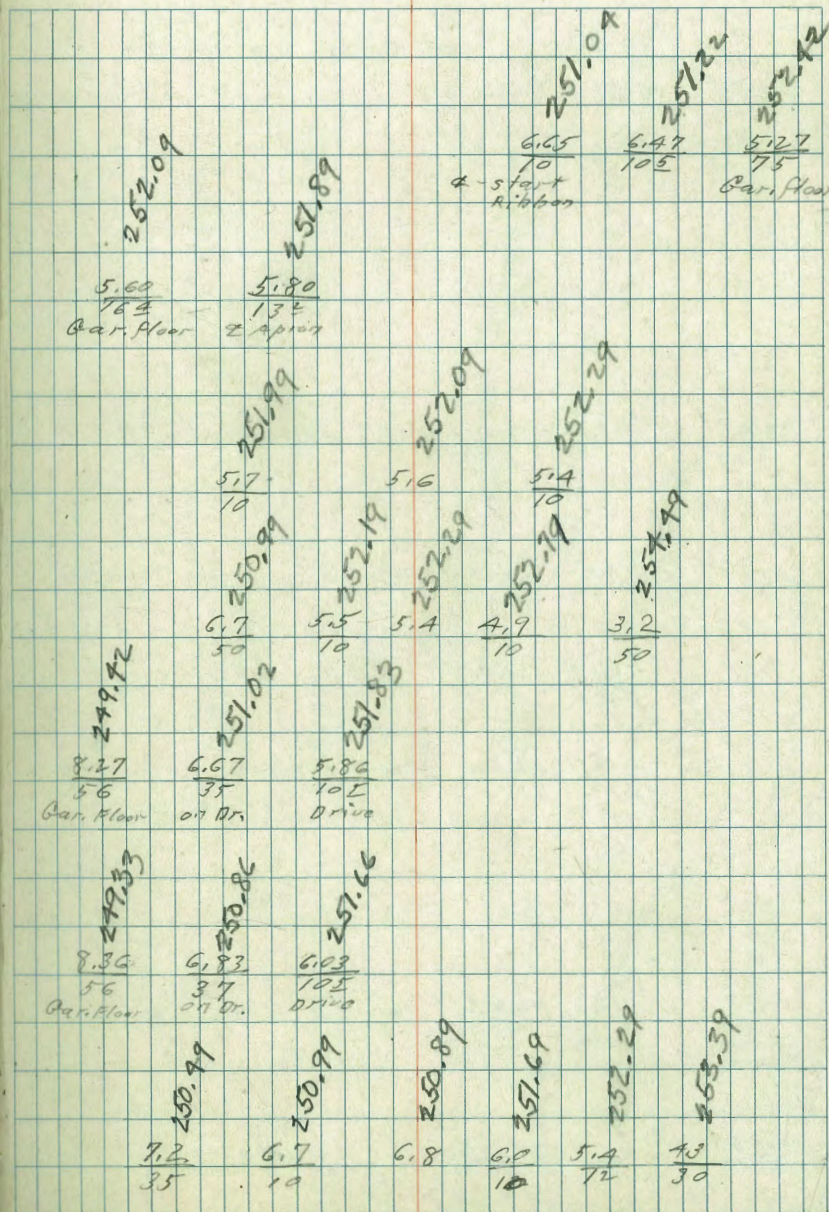
0+67 10^E Lt. = End drive

double Gar.

0+53 10^E Lt. = start conc. drive to.

0+50

257.69



257.69

Alloy Blk. 83 Pt. Loma Hqts

32nd Rt = start Conc. Apron to
 2+80^E 10' Pt. = E. Face 6" Conc. Wall along drive

2+50

2+37^E 7th Rt. = End Conc. drive

2+30 9th Rt. = start Conc. drive to Bar.

T.P. 1129 250.89 8.09 249.60

= West face 8" wide N+S. Conc. wall.
 11th Rt.

2+00 = End 8" wide Conc. wall. also

1+91 11th Rt. = face 8" wide Conc. wall.

1+89^E 9th Rt. = West. 2' wide ribbon to
 257.69

#

246.39
 4.8
 10
 End

246.09
 4.8
 10
 Base wall

246.49
 4.40
 10
 Top of wall

246.96
 3.93
 322
 Apron
 +
 Top of wall

247.04
 3.85
 37
 Bar.
 + floor

247.79
 3.1
 23

247.79
 3.1
 10

247.59
 3.3

247.89
 3.0
 10

247.89
 3.0
 25

248.33
 2.56
 94

248.43
 2.46
 10

248.57
 2.32
 115

250.18
 0.71
 52

248.70
 2.19
 95

248.79
 2.10
 10

248.97
 1.92
 12

250.19
 0.70
 52
 Bar, Floor

250.89

250.29
 7.4
 50

250.49
 7.2
 10

250.49
 7.2

250.39
 7.3
 10

249.99
 7.7
 112
 Base wall

252.06
 5.65
 113
 Top of wall

250.69
 7.0
 50

250.89
 6.8
 114
 End

251.01

6.68
 98
 Ribbon

250.19
 7.5
 113
 Base of wall

251.21

6.48
 105
 on ribbon

252.11
 5.58
 112
 Top of wall

252.41

5.28
 75
 Bar, floor

257.69

385 50%

Alley BIK 83,

4+58 13⁵ Rt = Δ in wall.

4+50 Cont.

also = start 8" wide E+W wall.
13² Rt = East face 8" wide Conc. Block wall
11³ Lt = start @ ar. Conc. Floor. No. Apron

4+50 T.P. 1.87 240.59 12.17 238.72

4+05

3+95

3+50

3+00

2+95 10² Rt = End Conc. Apron.
along drive
10¹ Rt = W. Face 6" wide Conc. N+D wall

250.89

Station	Description	Dist	Start	End	Notes
3+00		4.8 50	246.09	245.09	
3+50		9.8 50	241.09	238.09	
4+05		10.0 50	240.89	238.69	
4+50		4.51 11 ³	236.08	235.89	
4+50		4.7 10	235.89	235.89	
4+58	13 ⁵ Rt = Δ in wall.	5.4 13 ⁵ Ord	235.19	234.59	
3+00		5.6 10	245.29	245.69	
3+50		8.0 10	242.09	242.19	
4+05		12.0 10	238.49	237.99	
4+50		12.8 10	238.09	237.89	
4+50		12.9 10	238.09	237.99	
4+50		12.9 20	238.89	240.19	
4+50		12.8 50	238.69	240.89	
2+95	10 ² Rt = End Conc. Apron. along drive	4.9 10 Ord	246.99	246.15	
2+95	10 ¹ Rt = W. Face 6" wide Conc. N+D wall	5.2 10 Base wall	245.69	246.72	
2+95	10 ² Rt = W. Face 6" wide Conc. N+D wall	4.74 10 Apron	246.15	249.10	
2+95	10 ² Rt = W. Face 6" wide Conc. N+D wall	3.97 10 Ord	246.72	249.10	

4+99^E 10² Lt. = \pm 10" wide N. + S. Conc. wall.

4+99 10² Lt. = End ^{cobble} ~~rock~~ wall

block wall. = Δ in wall.

also 10² Rt. = Face 8" wide Conc.

4+89 10' Rt. = Footing for wall and

wide Conc. block wall.

4+81^E 16 Rt. = End garage + start 8"

4+81 14^E Rt. = End Conc. Apron to Gar.

26^o Rt. = start Gar. Conc. floor

4+69 10² Lt. = start cobble wall

24^E Rt. = start Conc. Apron to double ^{Gar.}

4+68 11^o Lt. = end garage

240.59

235.69
4.9
10²
top of wall

233.69
6.90
10²
top of wall

232.89
7.7
10²
Base wall

232.59
8.0
10²
Base wall

233.39
7.1
10²
End

233.29

7.3
10
End

232.19

8.4
10
Base Footing

239.09

1.5
10
top of wall

234.33

6.26

16
Gar. floor

233.89

6.70
14^E
Apron

234.31

6.28

26
Gar. floor

234.28

6.31

24^E
Apron

240.59

237.69

2.9
10²
top of wall

235.09

5.5
10²
Base wall

235.79

4.8
10
End

235.99

4.60
11
Gar. floor

235.69

4.7
11
End

that were filled.)
 on south + east of lots
 (Report by property owner
 lot on north side of alley.
 cut down to use dirt to fill
 From here on Alley has been

5+25

8.3	9.2	9.6	9.5	9.7	9.0	11.1
$\frac{40}{}$	$\frac{10}{}$		$\frac{7}{}$	$\frac{10}{}$	$\frac{10}{}$	$\frac{45}{}$
233.19	232.19	230.91	231.09	231.89	231.59	229.49
					Fill	Natural Ord.

5+18 21² Lt = End same

7.40	7.8
$\frac{213}{}$	$\frac{219}{}$
Bar. floor	Ord.

Conc. floor. No Apron.

5+02 21² Lt. = start double bar.

7.37	9.7
$\frac{218}{}$	$\frac{218}{}$
Bar. floor	Ord.

5+00 Cont.

7.6
$\frac{50}{}$
Ord. at wall

10⁶ Rt. = End 8" wide conc. block wall

5+00 10⁰ Rt. = End footing

6.0	7.5	8.1	7.8	8.5	1.5
$\frac{35}{}$	$\frac{10}{}$		$\frac{10}{}$	$\frac{10}{}$	$\frac{10}{}$
234.59	233.09	232.49	232.79	232.09	239.09
			Ord.	Base Footing	Top of wall

240.59

240.59

240.59

6+09

prop. wall.

6+00^l - E. line Quizat - 11³Lt - End
start pave + cur. (old Pave)

5+95 11³Lt. = $\frac{1}{2}$ prop. wall

5+66 Cont.

T.P. 0.25 228.48 12.36 228.23

double cur. west front.

5+66 11⁵Rt = S.E. Cor. Conc. block

T.P. Here. 228.48

5+50

issued. wall under Const.
 wall. Permit has been
 footing for proposed conc.

5+29 11³Lt. = $\frac{1}{2}$ start of dug

240.59

				5.04		5.34				6.10	5.85
				10		10				10	10
				66.8.0.		6				66.8.0.	
				222.98		223.64				222.75	222.63
				5.5	4.84	5.13	5.3		5.90	5.73	73
				11 ³	10	10			10	10	
				End	0.1 End	0			0	0.1 End	
				Trench							
				230.78	230.48	223.98	224.78	223.58	222.58	223.78	
				15	14	13	10	11.9	10		
				231.88	224.28	223.98	224.78	223.58	222.58	223.78	
				13.4		13.3					
				20	15						
				227.68	228.48	228.98	226.78	226.68	229.98	230.18	
				9.8	0.0	0.0	1.6	1.7	1.8	1.7	
				11 ²	10	8	6	8	10	20	
				Bottom Trench							
				230.37	228.19	230.39	228.29	228.29	228.19	230.59	231.19
				12	11.4	10.2	10.6	12.3	12.3	10.0	9.4
				10	11 ²	10	7	6	8	9	15
				Bottom Trench							
				229.59							
				11.9							
				11 ²							
				Bottom Trench							
				228.19							
				9.4							
				11							
				6+0							

240.59

Add Sections or Elevations of New
Improvements - along Kendall - Sec P. 37
Note - actual Elev. Shown.

1+32 - 37.5 Rt. = \pm 3' Conc. Walk
1+05 - 37.5 Rt. = \pm 2.5' Conc. walk
0+86 - 36.5 Lt. = \pm 3' Conc. walk
0+74 - 37.8 Rt. = \pm 3.3 Conc. walk
0+12 - 37.5 Lt. = \pm 3' Conc. Steps + walk
Bet. Roosevelt + Fortuna
5+85 - 37.6 Rt. = \pm 3' Conc. Steps + walk

5+42 - 37.8 Rt. = \pm 8.5' Conc. Dr
4+48 - 36.2 Lt. = \pm 2.5' Conc. Steps

4+12 - 35.6 Lt. = \pm 2.8' Conc. Steps

3+63 - 37.5 Rt. = Bot. of Steps to 2.5' Conc. walk

1+76 - 20.4 Rt. = end cb. (was Covered Before)
1+37 - 37.5 Lt. = \pm 16' Conc. Dr.

1+11 - 37.37 - 37.4 Lt. = \pm 3' Conc. walk
Bet. La Playa + Roosevelt.

Lt.

#

Rt

75

28.37			27.56		27.54
51			37.5	27.76	49.8
at Parch			walk	walk	at Parch
		28.10			27.76
		36.6			47
		walk			at Parch
28.02	27.98	27.43	27.32	27.27	
50	38.5	37.5	37.8	52	
at Parch	Top	Bot.	walk	at Parch	
	+ walk				
			27.92	28.42	28.62
			37.6	39.6	48.4
			Bot.	Top	at Parch
				walk	
			28.04	29.23	
31.14	30.95	28.23	37.8	53	
50	41.3	36.2	Dr	floor	
at Parch	Top	= Bot		Gar.	
walk	steps	step			
	31.21	27.68			
walk	41.3	35.6			
flat.	Top	Bot			
	steps	step			
			27.53	29.29	29.56
			37.5	45	50
			Bot.	Top	
				walk	
			25.41	25.56	25.62
			20.4	30	35.8
			Top	Cor. walk	
			cb.		
28.46		27.33			
58		37.5			
floor		Dr.			
Gar.					
28.79	28.35	27.10			
53	46	37.4			
at		walk			
steps					

2+41- 19.9' Rt. = ± 14' Conc. Dr.

0+95- 32.2' Rt. = ± 8.5' Conc. Dr.

Bet. chico + Pac. Beach Dr.

1+50- 37.5' Lt. = end wall + Beg. wire fence

1+21- 37.3' Rt. = ± 3' Conc. from top wall

1+23- 36.6' Rt. = ± 3' Conc. Steps + Walk-Thru wall

0+96- 37.7' Lt. = ± 8' Conc. Dr.

0+75- 37' Rt. = Beg. 6" Conc. wall

0+74- 37.5' Lt. = ± 2.5' Conc. walk
Low wall

0+24- 37.5' Rt. = ± 6' Conc. Steps thru

Bet. Fortuna + Chico

5+43- 38.9' Lt. = ± 8' Dr. - 2 - 2.5' Conc. Strips

5+28- 36.5' Rt. = ± 3' Conc. walk

5+04- 37.4' Rt. = ± 7' Dr. - 2 - 2' Conc. Strips

4+55- 18.5' Lt. = ± 2.4' Conc. Walk

2+55- 37.3' Rt. = ± 8' Conc. Dr.

2+20- 37.3' Rt. = ± 3' Conc. walk

Bet. Roosevelt + Fortuna.

Lt.

±

Rt.

76

					44.20 19.9 oil	44.32 19.9 Conc.	44.93 27.4 walk
					41.51 32.2 Dr.	41.84 5.0 Dr.	
37.2	37.08	38.6	38.1	36.0	36.8	36.8	36.0
45	37.5 top wall	37.5	26	15	22.5	25	36.6
						38.88 end wall	37.5
						38.74	45
						37.3 walk + top wall	39.05 48.5 at porch
					37.08	38.23 38.7 top walk	38.32 5.0 walk
	37.95 5.0 Dr.	37.55 37.7-Dr.			36.6 Bot. step	36.3 37 ground	37.77 37 top wall
		38.01 5.2 at porch	37.67 37.5 walk		35.30 37.5 Bot. step	36.44 39.3 top walk	36.68 5.8 walk
	34.04 8.8 Dr.	33.71 38.9 Dr.				33.28 36.5 walk	33.59 46.7 = steps
					32.69 37.4 Dr.		32.75 5.0 Dr.
	32.93 4.9 at porch	31.77 18.5 walk			29.24 37.3 Dr.		29.31 5.0 Dr.
					28.46 37.3 walk	28.48 5.2 at porch	

Additional notes

Alley BIK. 83 Pt. Loma Hgts

Original notes - P-66 - P-74

Sommermeier **INDEXED**

21-June 51

JUN 22 1951

Elevations on P-73.

6+00¹ = start A.C. Pavc + Alley elev.

4+49 9² Lt. = Pole # P.A. 1A74

4+15 16² Rt. = ^{110 apron} double Gar. Conc. floor

238.52
10³
Floor

3+45 10⁸ Rt. = end Conc. apron

242.98 244.11
10⁸ 215
Apron Gar. Floor

3+49 10⁰ Lt. = pole # P.A. 4A60

3+33 10⁸ Rt. = start conc drive

243.49 244.11
10⁸ 215
Apron Gar. Floor

2+50 9⁵ Lt. = Pole # P.A. 4A40

1+50 9³ Lt. = Pole # SPA 4A26

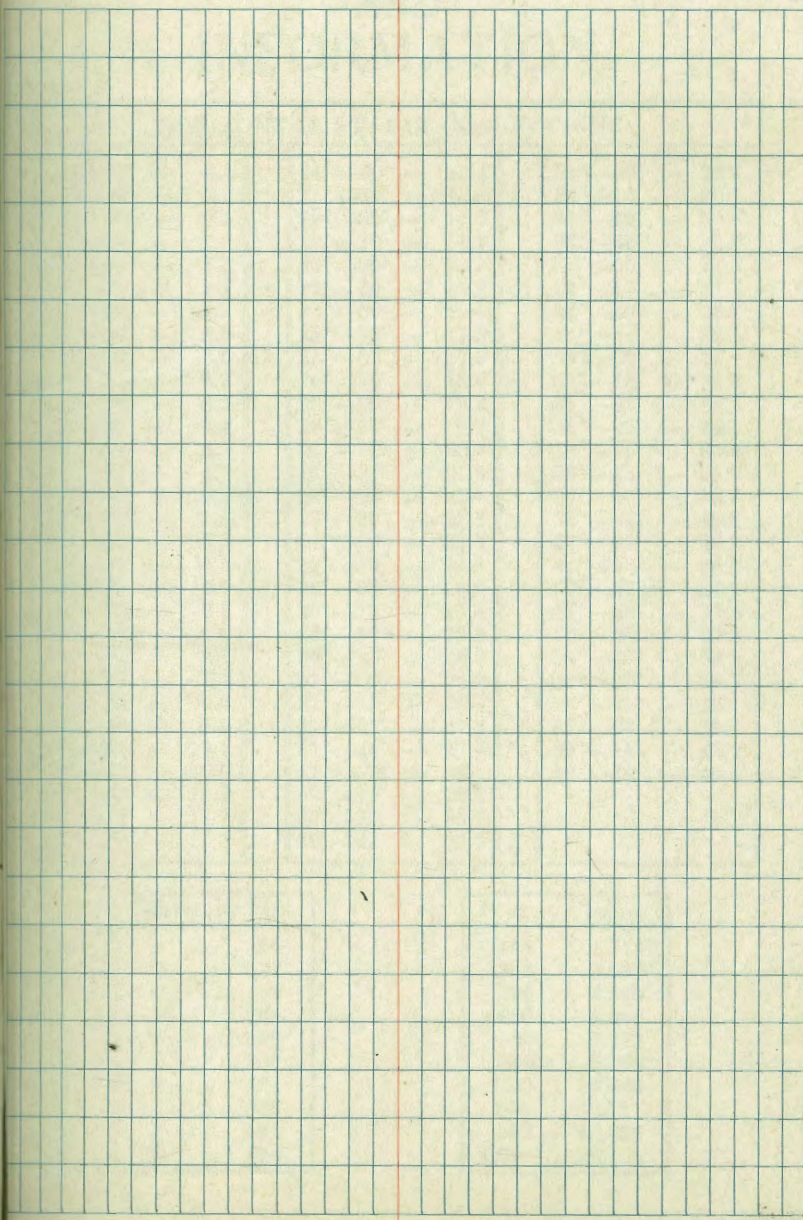
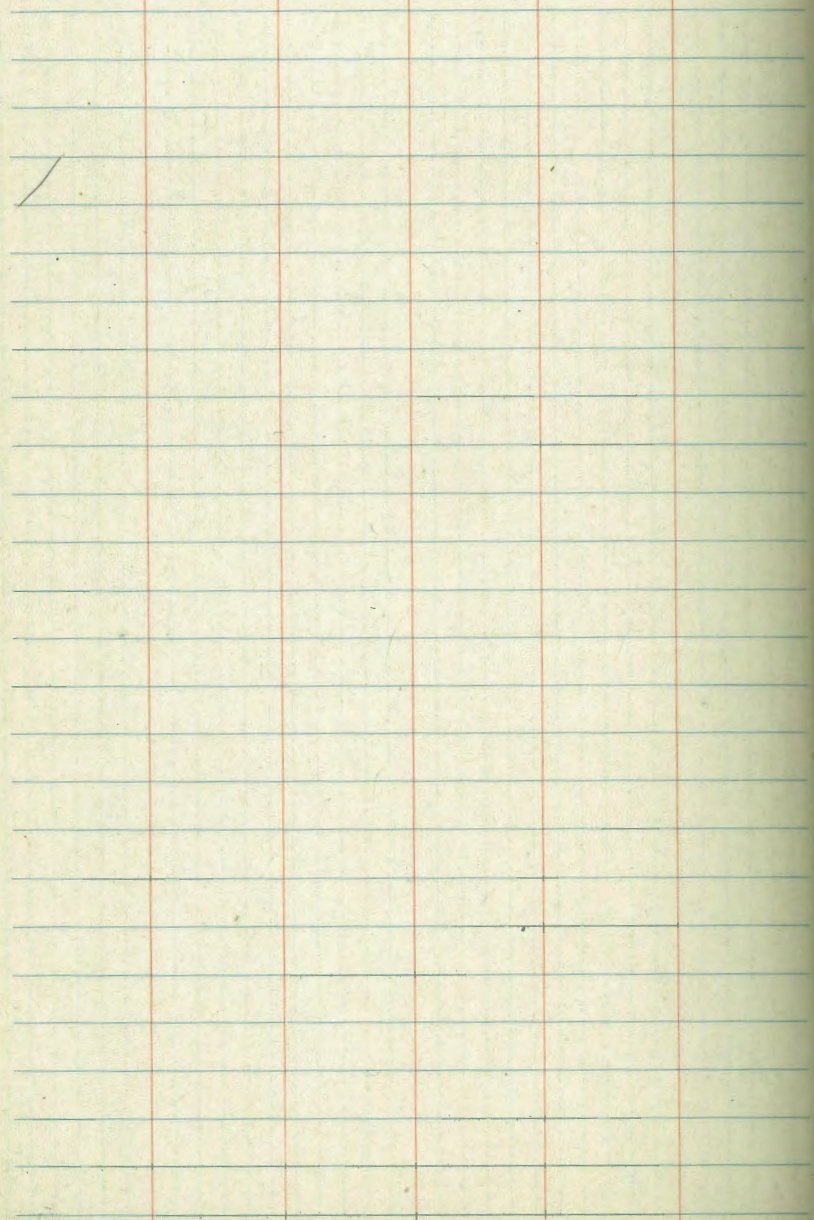
0+50 10² Lt. = Pole # J.P.A. 4A10

0+00⁵ End A.C. Pavc + alley elev.

246.00	246.35	246.63	246.97	247.50
10	10		10	10
66	G		G	66

This page features a ledger-style grid. It has a wide left margin, followed by a narrow column, and then 18 narrow columns. There are 25 horizontal rows. The grid is formed by light blue lines.

This page features a ledger-style grid, identical in layout to the left page. It has a wide left margin, followed by a narrow column, and then 18 narrow columns. There are 25 horizontal rows. The grid is formed by light blue lines.



IMPROVED TABLES AND INFORMATION

HORIZONTAL STADIA CORRECTIONS

2°-00' — 0.1	21°-00' — 12.3	33°-00' — 29.7
3°-00' — 0.3	21°-30' — 13.4	33°-15' — 30.1
4°-00' — 0.5	22°-00' — 14.0	33°-30' — 30.5
5°-00' — 0.8	22°-30' — 14.7	33°-45' — 30.9
6°-00' — 1.1	23°-00' — 15.3	34°-00' — 31.3
7°-00' — 1.5	23°-30' — 15.9	34°-15' — 31.7
8°-00' — 1.9	24°-00' — 16.5	34°-30' — 32.1
9°-00' — 2.5	24°-30' — 17.2	34°-45' — 32.5
10°-00' — 3.0	25°-00' — 17.9	35°-00' — 32.9
10°-30' — 3.3	25°-30' — 18.6	35°-15' — 33.3
11°-00' — 3.6	26°-00' — 19.2	35°-30' — 33.7
11°-30' — 4.0	26°-30' — 19.9	35°-45' — 34.1
12°-00' — 4.3	27°-00' — 20.6	36°-00' — 34.6
12°-30' — 4.7	27°-30' — 21.3	36°-15' — 35.0
13°-00' — 5.1	28°-00' — 22.0	36°-30' — 35.4
13°-30' — 5.5	28°-30' — 22.8	36°-45' — 35.8
14°-00' — 5.9	29°-00' — 23.5	37°-00' — 36.2
14°-30' — 6.3	29°-30' — 24.3	37°-15' — 36.6
15°-00' — 6.7	30°-00' — 25.0	37°-30' — 37.1
15°-30' — 7.2	30°-15' — 25.4	37°-45' — 37.5
16°-00' — 7.6	30°-30' — 25.8	38°-00' — 37.9
16°-30' — 8.1	30°-45' — 26.2	38°-15' — 38.3
17°-00' — 8.5	31°-00' — 26.5	38°-30' — 38.7
17°-30' — 9.0	31°-15' — 26.9	38°-45' — 39.1
18°-00' — 9.5	31°-30' — 27.3	39°-00' — 39.6
18°-30' — 10.1	31°-45' — 27.7	39°-15' — 40.0
19°-00' — 10.6	32°-00' — 28.1	39°-30' — 40.5
19°-30' — 11.2	32°-15' — 28.5	
20°-00' — 11.7	32°-30' — 28.9	
20°-30' — 12.3	32°-45' — 29.3	

Chains to Feet

1	66
2	132
3	198
4	264
5	330
6	396
7	462
8	528
9	594
10	660

Feet to Chains

100	1.515
200	3.030
300	4.545
400	6.060
500	7.575
600	9.090
700	10.606
800	12.121
900	13.636
1,000	15.151

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

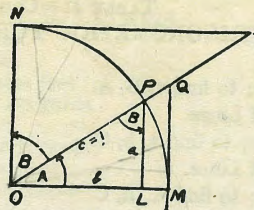


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\begin{aligned} \angle A &= \angle MOP & \angle B &= \angle PON = \angle OPL \\ R &= OB = c = 1 \\ \sin A &= \frac{a}{c} = \frac{a}{1} = a = \cos B = LP \\ \cos A &= \frac{b}{c} = \frac{b}{1} = b = \sin B = OL \\ \tan A &= \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ \\ \cot A &= \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT \\ \sec A &= \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ \\ \csc A &= \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT \\ \text{vers } A &= \frac{LM}{OP} = LM = \text{covers } B \# \\ \text{covers } A &= \frac{OP - LP}{OP} = OP - LP = \text{vers } B \\ \text{exsec } A &= PQ = \text{coexsec } B \\ \text{coexsec } A &= PT = \text{exsec } B \\ \sin \frac{1}{2} A &= \sqrt{\frac{1 - \cos A}{2}} & \cos \frac{1}{2} A &= \sqrt{\frac{1 + \cos A}{2}} \\ \sin 2A &= 2 \sin A \cos A & \cos 2A &= \cos^2 A - \sin^2 A \\ \text{Law of Lines} & \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C} \\ \text{Law of Cosines} & c^2 = a^2 + b^2 - 2ab \cos C \\ \text{Law of Tangents} & \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)} \end{aligned}$$

TABLE II—Continued
- TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Lines.

Given A, B, c; to find a, b, C.

Use Law of Lines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a}$$

$$\tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6} (B+b+4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11
$\frac{1}{16}$.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219
$\frac{1}{8}$.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271
$\frac{3}{16}$.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323
$\frac{1}{4}$.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375
$\frac{5}{16}$.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427
$\frac{3}{8}$.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479
$\frac{7}{16}$.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531
$\frac{1}{2}$.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583
$\frac{9}{16}$.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635
$\frac{5}{8}$.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688
$\frac{11}{16}$.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740
$\frac{3}{4}$.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792
$\frac{7}{8}$.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844
$\frac{15}{16}$.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896
$\frac{1}{1}$.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948
	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.000
	0	1	2	3	4	5	6	7	8	9	10	11

TABLE IV
USEFUL RELATIONS.

Lineal feet	×.00019	= miles
Lineal yards	×.0006	= miles
Square inches	×.007	= square feet
Square feet	×.111	= square yards
Square yards	×.0002067	= acres
Acres	×4840	= square yards
Cubic inches	×.00058	= cubic feet
Cubic feet	×.03704	= cubic yards
Links	×.22	= yards
Links	×.66	= feet
Feet	×1.5	= links
360° = 21600' = 1296000"		
Radius = arc of 57.2957790°		
Arc of 1° (radius = 1) = .017453292		
Arc of 1' (radius = 1) = .000290888		
Arc of 1" (radius = 1) = .000004848		

$$\pi = 3.141592654$$

$$\sqrt{\frac{1}{\pi}} = 0.564190$$

$$\frac{\pi}{4} = 0.785398163$$

$$\sqrt{\frac{6}{\pi}} = 1.240700982$$

$$\frac{\pi}{6} = 0.523598776$$

$$\pi^2 = 9.869604401$$

$$\sqrt{\frac{4}{\pi}} = 1.128379167$$

$$\frac{1}{\pi^2} = 0.101321184$$

$$\frac{\pi}{6} = 0.523598776$$

$$\sqrt{\pi} = 1.772453851$$

$$\frac{4\pi}{3} = 4.188790205$$

$$\frac{1}{\pi} = 0.3183099$$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = 0.667 (Dist. in miles)²

Difference between arc and chord length, 0.05 feet in 11½ miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{\sum v^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULAE.

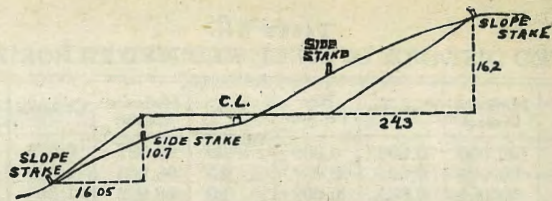
Horizontal Distance = R - R sin² a + C cos a

Vertical Distance = R ½ sin 2 a + C sin a

R = Reading × $\frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

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