

1754



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SAN DIEGO, CALIF.

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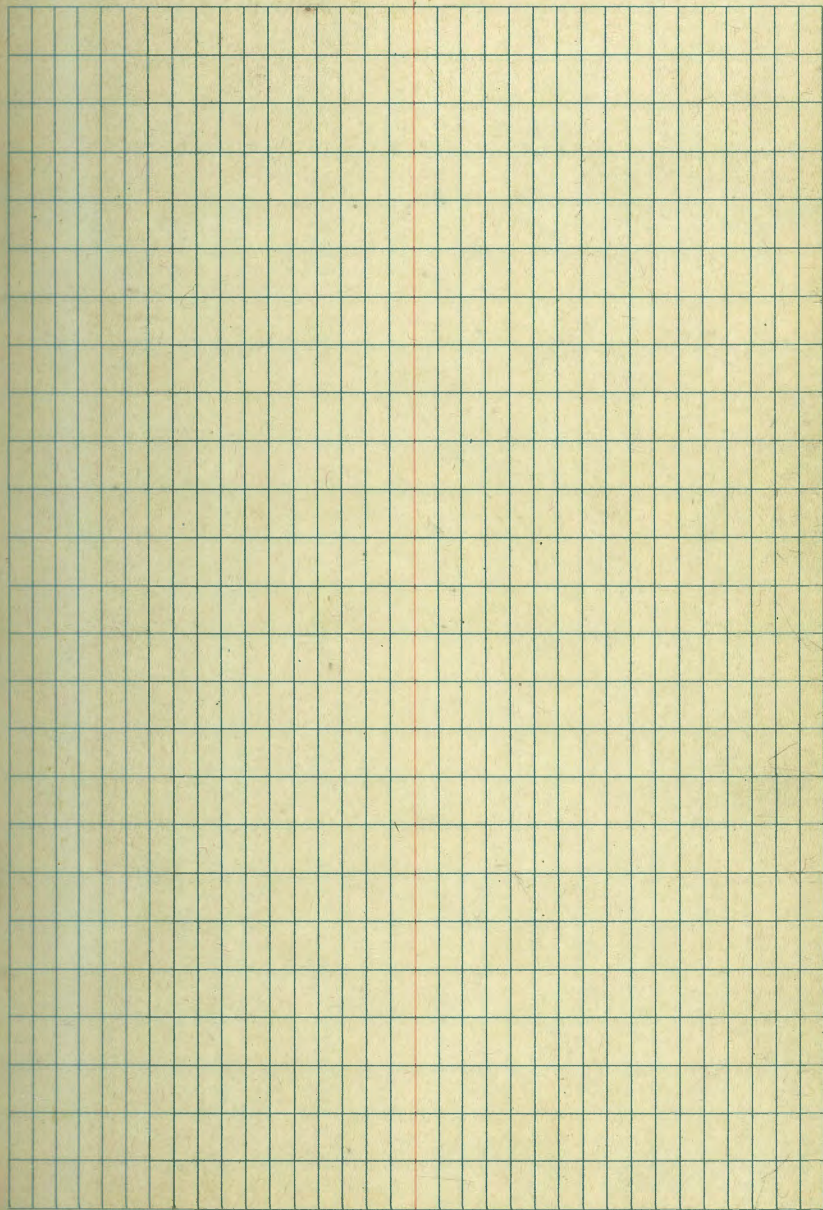
P. O. Box 803

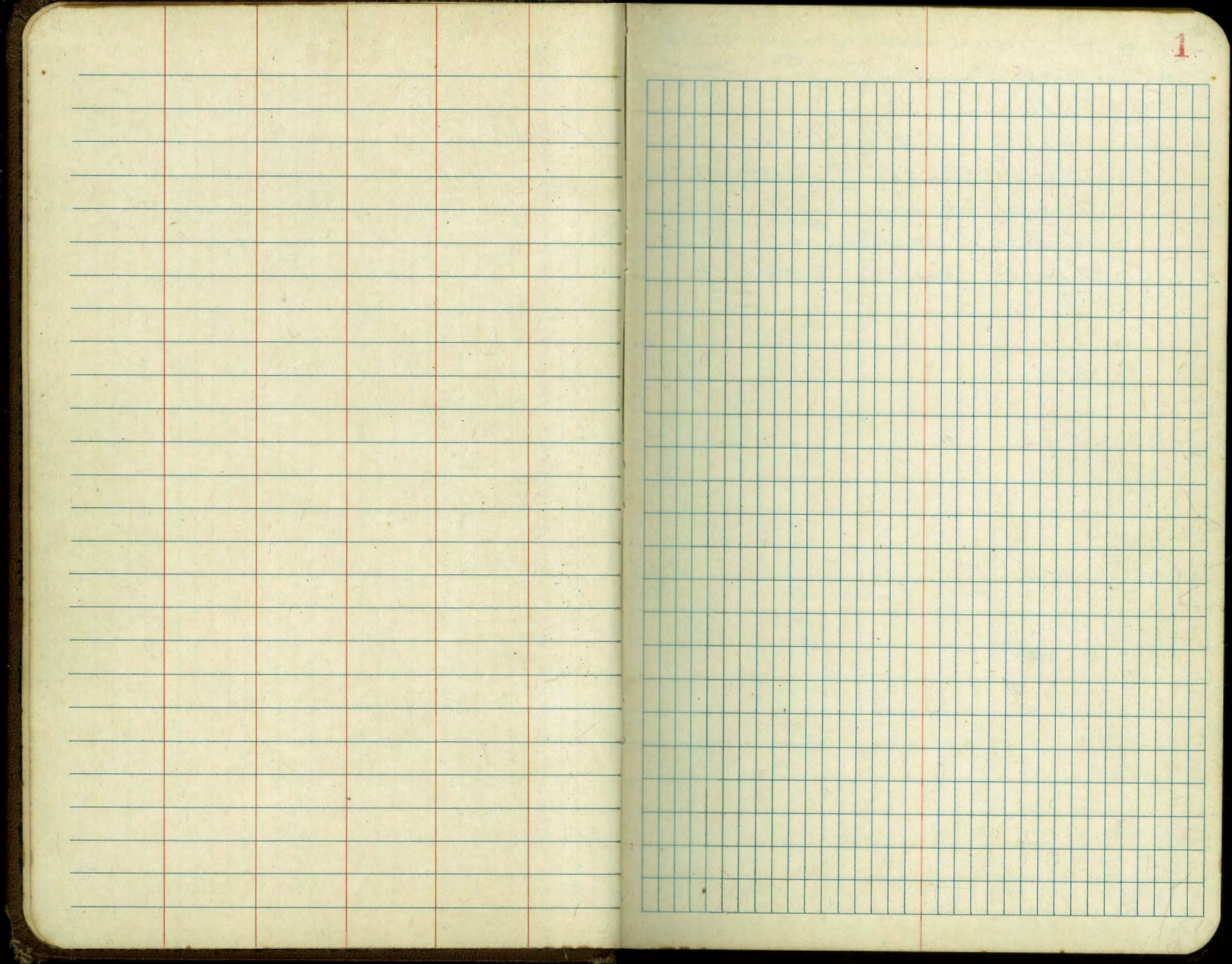
CHICAGO

INDEXED

to page # 76
except page # 1

1754





Proposed Extension of Havergal Road
North of Williams Park Sub.

Levels next Page

Fd Pipe + Disc

San Diego City Limits

Williams Park

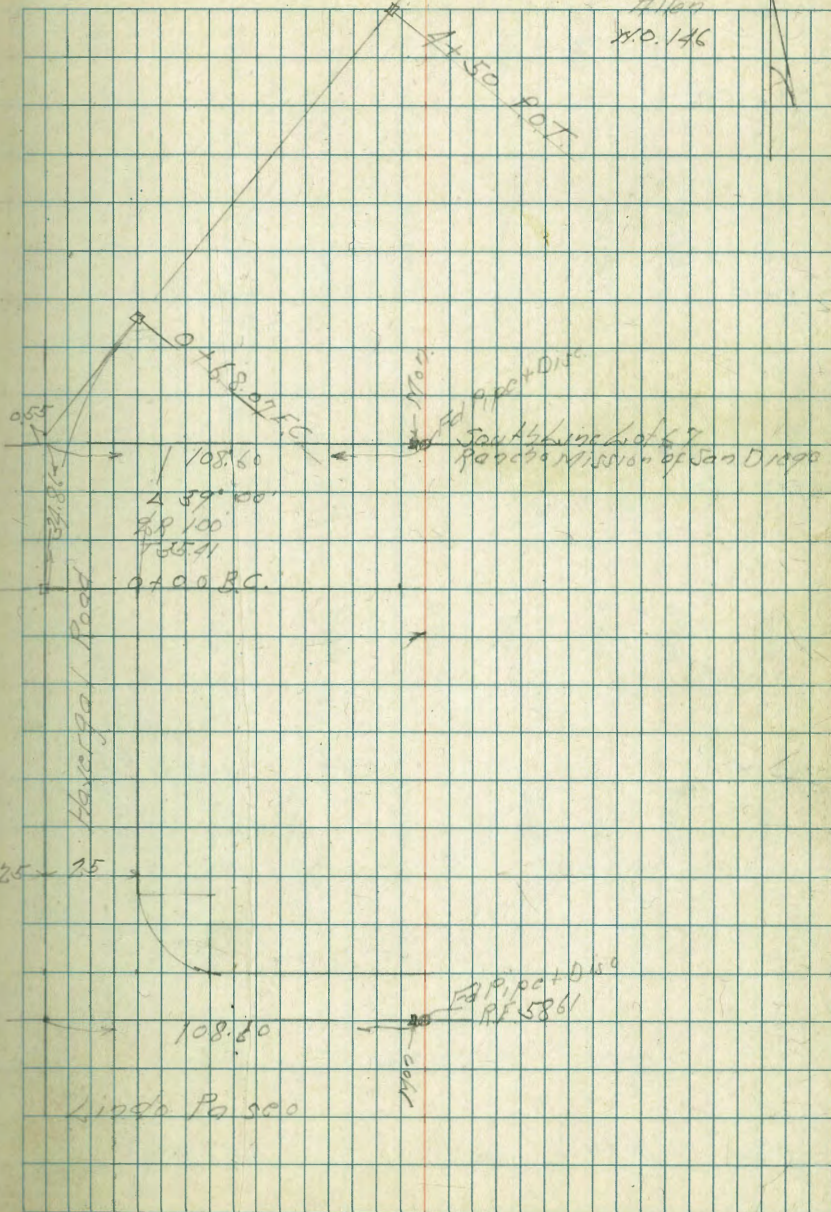
L.S. 2317

Fd Pipe
RF 5861

Indexed
C.S.K.

Dec. 20. 46
J. S. O.
M. C. O.
M. D. O.
M. L. O.
No. 146

4



Cross Section Haverca/St.

Sketch Page 1

1+50

1+0

0+68.07

0+34.03

BM

0+0 = B.C.R.L.

TP 4.30 445.23 11.09 440.95

TP 0.21 452.02 4.57 451.81

BM 3.87 456.38 452.51

Spot Elevations
at
H.K. Cor.
at
Haverca
Park

Spot Elevations
at
Haverca
Park

Lt. N

2

pt 1

5

418.2	418.8	421.5	420.3	431.1	435.3	439.8	442.7
210 70	211 50	227 75	169	141 25	99 50	68 75	85 100
416.8	419.3	421.6	427.9	432.3	437.7	440.8	440.0
224 75	219 50	198 75	172	139 25	71 50	44 75	12 100
418.7	421.0	425.9	429.0	433.7	437.4	441.3	445.2
215 75	212 50	198 75	162	115 25	78 50	39 75	0 110
422.3	425.9	427.1	430.8	435.7	440.0	442.0	445.1
229 75	198 50	181 25	144	95 25	58 50	24 75	9 100
429.8	430.9	432.0	439.68	438.9	440.9	443.1	445.2
152 100	153 75	143 50	105 75	68 75	48 50	21 75	0 100
			445.23				

TP 0.77 421.41 12.56 420.64

4+50 P.O.T

4+0

3+50

TP 0.44 432.20 12.47 432.76

3+0

2+50

2+0

445.23

Lt

St

Pt

6

	421.7	420.1	420.6	420.68	420.7	419.2	418.7	416.1
	20.5 75	15.1 50	13.6 25	12.56 0.75 12.81	12.5 25	14.0 50	14.5 75	17.1 100
	411.5	417.5	420.3	421.5	421.8	421.9	423.0	422.2
	21.7 75	15.7 50	12.9 25	11.7	11.4 25	11.3 50	10.9 75	11.9 100
	409.8	415.7	417.7	421.5	424.3	427.3	427.3	425.0
	21.1 75	17.5 50	15.5 25	11.7	8.9 25	5.9 50	5.9 75	7.3 100
	407.9	412.9	419.3	422.7	427.0	430.0	431.5	430.8
	37.3 75	32.2 50	25.9 25	22.5	18.2 25	15.2 50	13.7 75	14.1 100
	407.8	415.1	420.3	423.2	428.2	431.2	435.2	437.2
	37.4 75	32.1 50	24.9 25	21.0	17.0 25	14.0 50	10.0 75	8.0 100
	410.8	417.8	421.8	425.1	429.5	434.0	436.9	441.7
	34.4 75	27.1 50	23.1 25	20.1	15.7 25	11.2 50	8.3 75	5.5 100

445.23

X-Sect. 20' Alley Blk 143 Univ. Hts.
 + Drain E. to Florida St.

ct. 156.54

1-10-47

Osborne
 Hardin
 Worrell

712

W.O. 12.30

N

Notes Reduced - Georgia St

1-16-47 - Wherry -

Georgia St

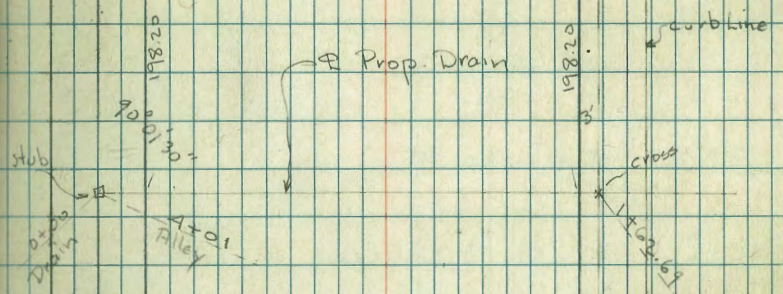
7'

ct. 156.67

Indexed
 C.S.K.

8

Fd ct Howard St
 Paved AC. 166.54
 5x99.20



10 10
 Paved Conc Polk St
 Fd ct. 166.67
 ct.

0+95 - 18' Lt. = Φ Sing Gar. - wood floor

0+90 - 9' Rt. = Φ Tel. pole

0+85 - Φ Sing. Gar. on Lt. - wood floor + apron

0+83 10' Rt. - Nly. Conc. apron

0+75 - 9.2 Lt. = Φ P. pole

0+74 - 9.9 Lt. = Φ 1' Conc wall along Gar and apron
Drain on top

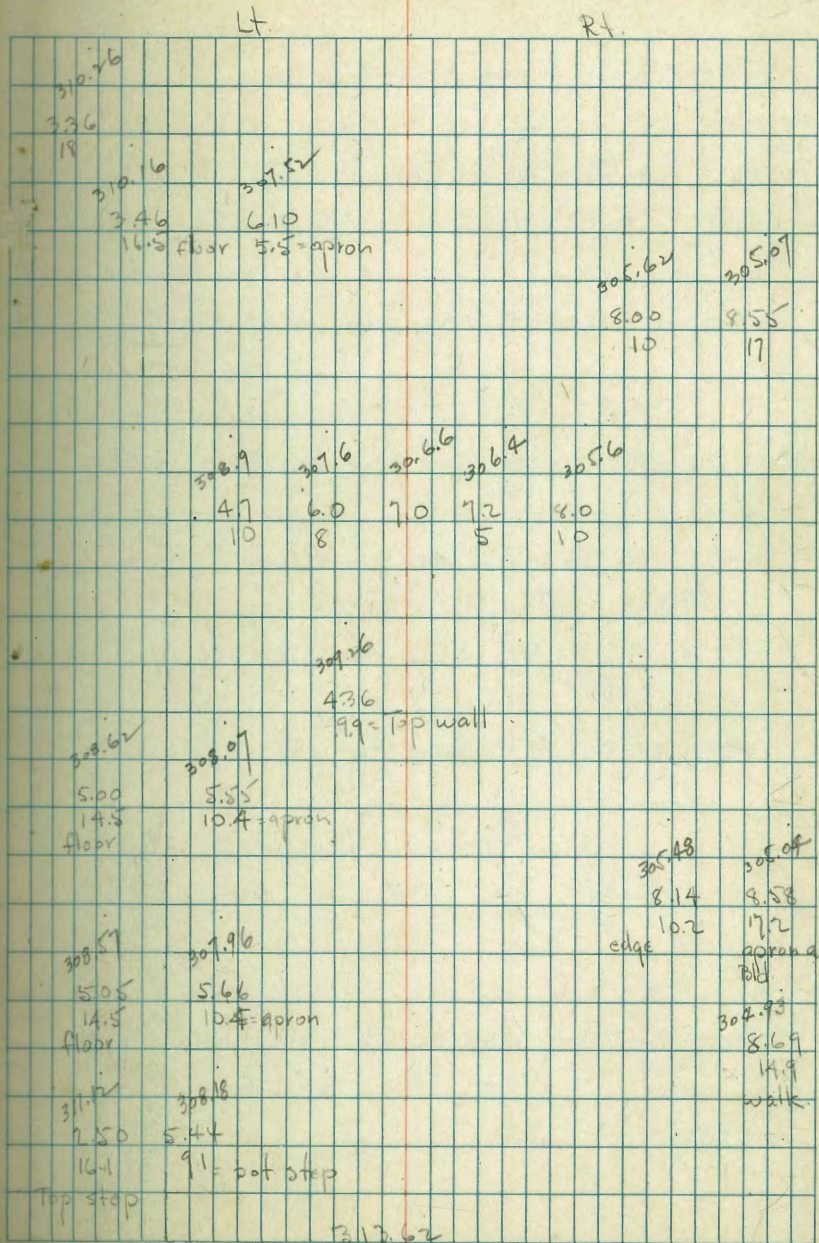
0+73 - N. end Gar. on Lt.

0+58 - 10.2 Rt. = sly. Conc. apron to apt. Bld.

0+56 - 10.4 Lt. = S. end Doub. Gar. Conc. apron + floor

0+55 - 14.9 Rt. = Φ 2' Conc. walk

0+52 - 9.1 Lt. = Φ 3.5 Conc. Steps



3+63- 9.7 Rt = S. end Doub Gar - Conc floor

3+52- 39' Rt = Φ Doub Gar - Conc. floor

3+50 - 15' Lt = S. end f' Car Gar - Conc. floor

3+44 - 10' Rt = end 6" Conc. wall

3+41 - 10' Rt = N.W. Cor. Gar. at opening - Dirt floor

S. end 6" Conc. wall for found.

3+25 - 10' Rt = S.W. Cor. of Sing. Gar. opening N. +

3+24 - 8.5' Lt = Φ P. pole

3+18 - 9.7 Rt = Φ Sing. Gar. Not used for Car. Dirt floor - Conc found.

3+12 - 9.9 Rt = end fence

3+05 - 8' Rt = Φ Tel. pole

3+01 - 9.4 Rt = Φ 4x4 Post support for Gar. door

3+00

2+88 - 9.7 Rt = Beg wire fence

2+80 - 9.7 Rt = N.W. Cor. shed

Lt.		Rt	
		208.5	29.7
		6.6	59.8 - floor
		9.7	24.45
		ground	10.70
			39 - floor
300.5	300.0	299.1	298.8
5.00	5.1	6.0	298.6
15 - floor	10	4	298.1
			296.4
			8.7
			20
			4.5
			5.70
			10 - Top wall
			298.0
			7.1
			10 floor
301.8	301.5	299.2	299.0
3.3	3.6	8.9	299.1
15	10	4	298.9
			299.50
			5.5 = Top
			10 ground
			10 wall
			298.7
			6.38
			298.5
			7.00
			8.9 - Top Conc
			6 - Wall in front of Gar.
			9.7 - Top Conc found
302.6	301.5	300.3	299.8
2.5	3.6	4.8	299.7
20	10	4	298.7
			298.1
			297.6
			7.5
			20
			300.17
			49.8 - floor
			9.7
			305.5

4+17- 12.4 Rt = E Sing Gar. - Conc floor
 4+16 - 18.3 Lt = S Sing Gar. - Dirt floor
 4+07 - 18.3 Lt = S Sing Gar. - Dirt floor
 4+06 - 12.5 Rt = S Sing Gar. Conc floor
 4+01 - Stub = 0+00 for Drain 7.55 298.52
 T.P. 7.58 306.07 6.66 298.49

4+00

3+95 - 9.8 Rt = 30' Euc. tree

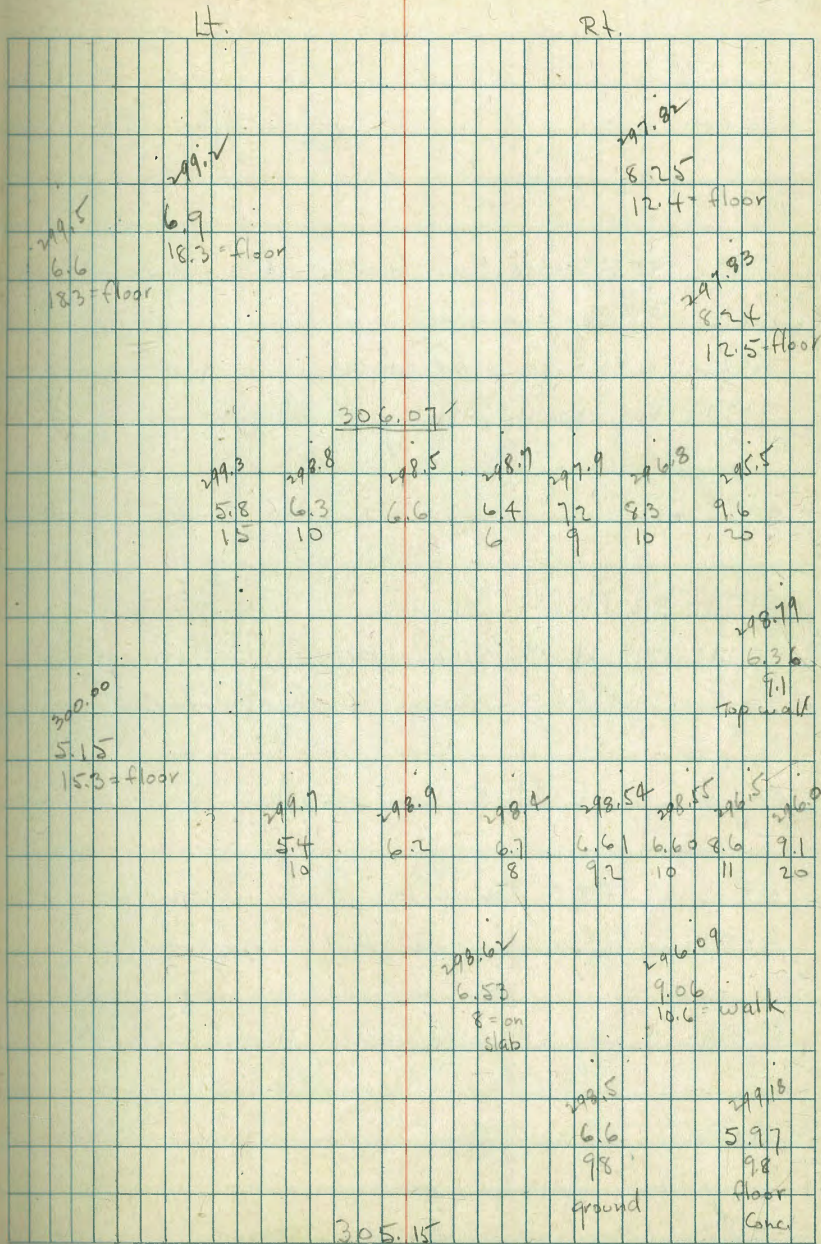
3+93 - 9.1 Rt = end Ret. wall

3+88 - 15.3 Lt = N. end Gar. 4 car.

3+85 - 9.2 Rt = S. end 1.5' Rough Conc Ret wall

3+84 - 8' Rt = edge Rough Slab Conc in alley =
 10.6 Rt = E 2.7' Conc. walk

3+82 - 9.8 Rt = N. end Gar.



Levels on Prop. Drain along lot line
 19820 S. of S. Howard from Alley to
 Florida St

B.M. 0.66 299.18 298.52 ^{Stub 4+01} Alley-P14

0+00 = Stub - Sta 4+01 on Alley Sta

⊕ on Stub 0.66 298.52

0+06

⊕ 0.6 298.6

0+09.8 - 0.4 Rt = ⊕ Euc. Tree

⊕ 0+10 1.5 297.7

0+12 - 0.7 Lt = S.W. Cor. Gar. Conc. floor

⊕ 2.4 296.8

0.7 Lt. on ground 2.4 296.8

Top conc. found 1.36 297.82

5' Rt 2.8 296.4

0+27 - 2.8 Rt = N.W. Cor. House

⊕ 3.6 295.6

2.8 Rt. along House 4.4 294.8

2.8 Rt = floor 3.44 295.74

0+30 - 0.9 Lt = S.E. Cor. Gar.

⊕ 3.7 295.5

0.9 Lt = ground 3.7 295.5

0+48 - 1.9 Lt = Beg 2.5 Conc. walk - S. side

⊕ 4.9 294.3

1.9 Lt = edge walk 4.30 294.88

1-14-47

70.

18

299.18

0+52 - 2.7 Rt = N.E. Cor. House

2.7 Rt = ground at House 5.1 294.1

0+53 - 1.7 Rt = Beg ⊕ 2' Hedge 3' high

0+71 - 1.8 Lt = end S. side walk + 4.7 Lt = Cor. Porch

⊕ 5.6 293.6

1.8 Lt = Conc walk 4.78 294.40

4.7 Lt = ground at House 4.8 294.4

" " floor House 2.24 296.94

5' Rt. 5.8 293.4

0+74 - 1.1 Lt = ⊕ 3.5' wood porch

1.1 Lt = Top porch 2.88 296.20

0+79 - 4.8 Lt = Cor. Porch

0+92 - 5.1 Rt = N.W. Cor. House

⊕ 5.9 293.3

1.5 Rt = ⊕ Hedge

5.1 Rt = ground at House 6.2 293.0

" " floor at House 5.18 294.00

5' Lt. ? - H. Wherry 5.1 294.1

1+11 - 2.3 Rt = S.W. Cor. House

⊕ 6.7 292.5

2.3 Rt = ground 6.6 292.5

" " floor House 3.92 295.26

5' Rt. 6.9 292.3

1+30 - 3.9 Rt = ⊕ 5' Brick chimney along House

3.9 Rt. ground at chimney 7.5 291.7

1+38- 5.2 Rt. = N.E. Cor House				
±	7.7	291.5		
5.2 Rt. = ground at House	8.1	291.1		
1+41- 2.6 Lt. = S.E. Cor House				
2.6 Lt. = ground at House	7.3	291.9		
T.P.	9.58	296.79	11.97	287.21
1+557 = W. side 0.5' Conc wall				
± - ground	6.1	290.7		
± - Top wall	5.22	291.57		
1' Rt. = Top-end wall	5.22	291.57		
5' Rt.	6.6	290.2		
5' Lt. = Top wall + ground	5.18	291.61		
1+562 = E. side wall				
± = ground at base wall	6.9	289.9		
5' Lt.	7.2	289.6		
5' Rt.	6.7	290.1		
1+597 = face of 0.6 Conc Ret. wall				
± = Top wall + ground	7.27	289.52		
5' Lt. = Top wall	7.24	289.55		
5' Rt. " "	7.13	289.66		
1+597 = Base of Ret wall + wedge Sidewalk				
± on walk	10.82	285.97		

296.79

1+64.7 = E. side of walk				
±	10.96		285.83	
5 Lt. = on walk	10.87		285.92	
5 Rt. " "	11.07		285.72	
1+69.7 = W. side face of Florida				
± = Top cb	11.12		285.67	
± = gut	11.97		284.82	
10 Lt. = Top	10.95		285.84	
10 " = gut	11.81		284.98	
50 Lt. = Top	10.19		286.50	
50 " = gut	11.10		285.69	
10 Rt. = Top	11.22		285.57	
10 " = gut	12.19		284.60	
50 Rt. = Top	12.07		284.72	
50 " = gut.	13.03		283.76	
1+69.7 ± Florida = Low point in Dip Sect				
±	12.81		283.98	
50 Lt.	11.94		284.85	
50 Rt.	13.81		282.98	
end				
T.P.	7.22	293.35	10.66	286.13
check P.M.			2.76	290.59

NW. Howard
Florida

Levels for Prop. Drain from W. curb of Havergal + Int with City Line - Sec. P 4 To Ext. Ditch at top of bank to Canyon.

783

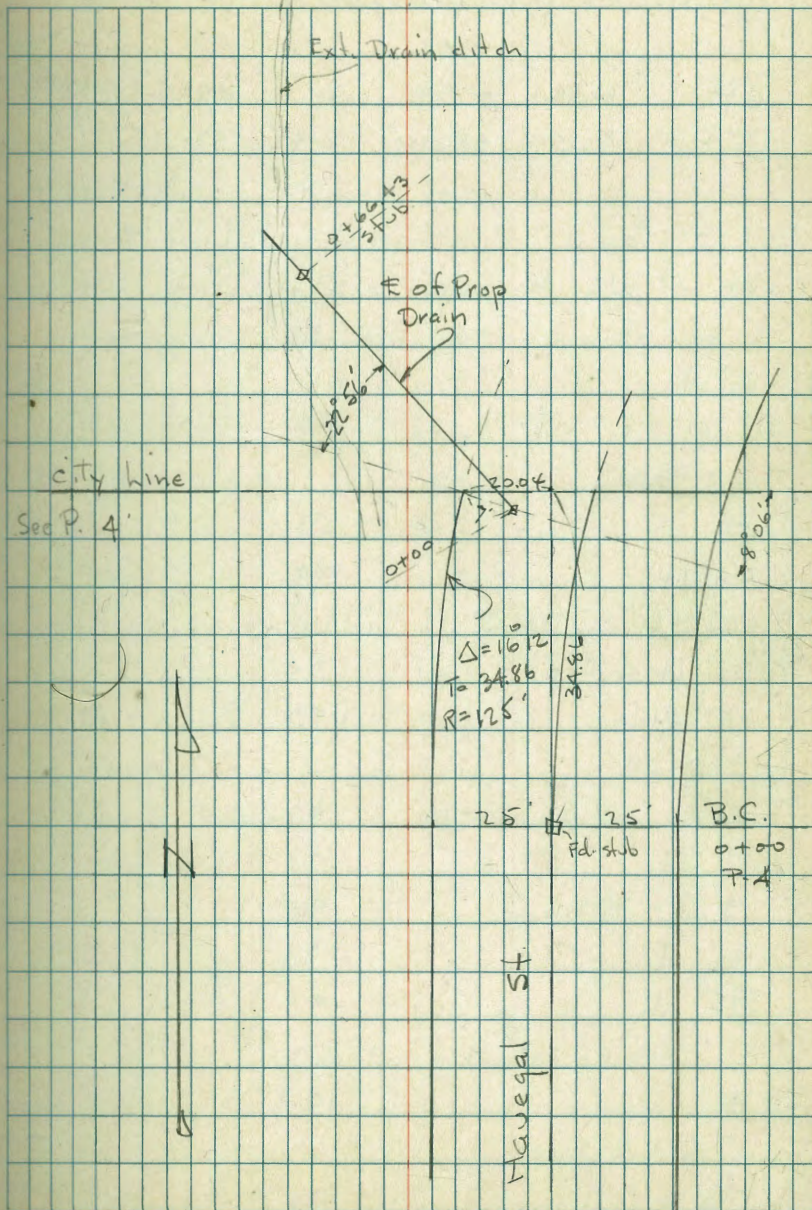
W.O. 230

2-24-47

Osborne
Harden
Smith

Indexed
O.S.K.

20



Levels on Prop. Drain - P. 20

B.M.	0.56	443.17	442.61	Mon. U.E. Cor. Williams Park
T.P.	0.10	430.95	430.75	P.S

0+00 = face of 7' cb. on Radial Line from
Int. of w.l. Havergal + City Line.

± on Stub.	1.57
10' Lt.	1.1
10' Rt.	2.8
0+30	
±	5.3
21' Lt.	3.8
26' Lt. = ± Ditch	6.2
30' Lt. = Top	3.5
15' Rt.	7.7
0+50	
±	8.3
7' Lt.	7.8
9' Lt. = ± Ditch	9.5
12' Lt.	7.6
15' Rt.	9.9
0+68 = E. bank of Ditch	
±	10.1
7' Lt. = ± Ditch	13.7
15' Lt.	9.5

430.85

15' Rt.	10.7
0+83 = ± Ditch - where it breaks over the bank	
±	16.2
9' Lt. = Top	10.9
6' Rt. = Top	13.0
15' Rt.	14.2
0+90 = w. bank of Ditch	
±	13.7
10' Lt.	11.6
4' Rt. = ± Ditch	17.6
8' Rt.	14.7
15' Rt.	15.3
1+10 - To show line of Ditch down the Hill	
±	16.9
17' Rt. = w. bank	20.6
27' Rt. = ± Ditch	26.0
31' Rt. = E. bank	23.7
End.	

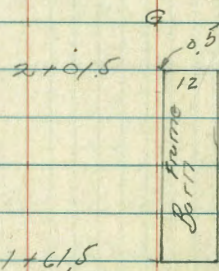
Walker
Hendricks
Becker
Johnson
5-13-17

Cross Sections Parcel/land
NE. Cor. Imp. Ave. & Ozark St
Par. lot 42, Hartens Purchase

Cross Sections P. 23

2.49 168.26 158.77

Lot - E Imperial
+ W. 10' Ozark
3-1673-P3

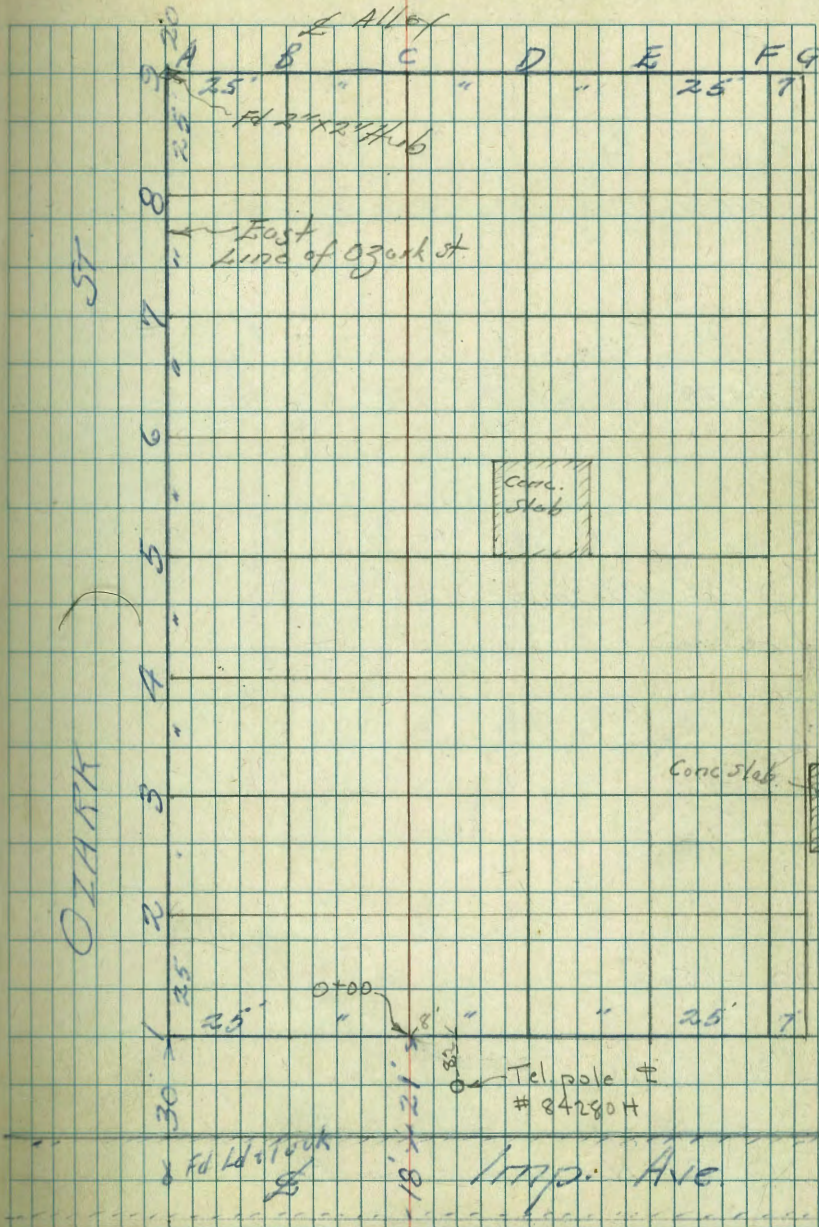


indexed
c. 51K

5" Conc. Ret. Wall

58

22



Cross Sections N.E. Imp & Ozark Mt

14

RT

23

"C"

0+50

80	75	82	79	83	77	85	80
160.3	160.8	162.1	162.4	163.0	163.6	164.8	166.3

0+25

86	79	70	63	85	78	87	82
159.7	160.4	161.3	162.0	163.1	164.1	165.6	166.0

0+00 = N.E. Imp

80	83	73	62	82	70	86	82
159.3	161.0	161.0	162.1	163.1	164.3	165.7	166.1

0-11

89	81	67	54	85	33	75	79
159.4	160.2	161.6	162.9	163.8	165.0	166.0	166.4

0-15

89	79	68	61	85	37	72	83
159.4	160.4	161.5	162.2	163.4	164.6	165.9	166.2

0-21 = N. edge East. Conc. Pav
16326

88	80	65	54	88	34	70	82
159.7	161.57	161.67	162.77	163.98	165.12	166.27	166.62

16836

NE Imp. Ave and Ozark St.

Lt

Rt 34

1+61.5 = SW Cor From Bar 17

"C"

164.8
23.5
82.5

1+50

9.0 75	159.3 81	160.2 81	160.9 81	162.0 83	162.3 85	162.6 87	163.8 89	164.1 91	164.5 93	165.1 95
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1+25

2.1 75	160.8 81	162.1 81	162.6 81	163.3 81	163.6 81	164.2 81	164.9 81	165.0 81
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1+00

2.1 75	160.9 81	162.3 81	162.6 81	163.1 81	163.5 81	163.7 81	164.7 81	164.8 81	164.9 81	164.9 81
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0+75

160.6 77 75	64 72 56	62 62 44	62.6 57 30	62.3 50 25	162.75 5.5	163.1 5.2	163.5 18	163.7 18	164.7 25	164.8 30	164.9 35	164.9 40	164.9 45
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0+55.5 = NW Cor Conc. Slab

165.81
245
805
on Conc.

0+38 = SW Cor Conc. Slab

1682.6

1682.6

165.86
240
805
on Conc. slab

NE Imp. Ave

to Ozark St

chk starting B 111

949 158.77

2+20 = NL Alley

2+00 = SL Alley

1+75

16826

L+

R+

25

"C"

117 75	156.6	1055 50	157.71	108 50	157.5	229 25	158.97	26 25	158.77	84	159.9	79 25	74 25	161.17	74 25	160.9	64 50	161.81	70 58	161.3	55 75	162.16	51 82	163.2
		20 10 11				20 10 11																		
112 75	157.1	42 65	157.1	103 61	158.0	100 50	158.8	31 25	159.2	79	160.4	6 25	6	161.5	5 50	162.2	5 75	163.2	86 82	163.7	82.5 82	163.9		
100 75	158.3	131 24	158.2	134 50	159.9	75 26	160.8	68 25	161.5	67	161.9	60 25	4.7 50	162.3	4.7 50	163.6	3.8 75	164.4	3.9 82	164.4				

16826

Mon

Indexed
c.s.k.

See P. 27

straight bet. Mon + ct.

N

st

741.66

7

1

Fd. old Hub
Took average

Fd. old Hub

R.P. Hubs Buried

179.98

Fd. ct.

Imperial

ct.

cross

Ozark
240.00

10'

30'

15'

01.00

cross

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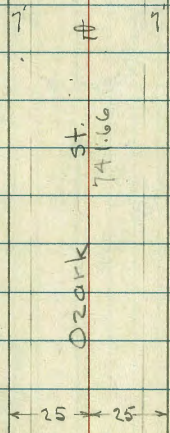
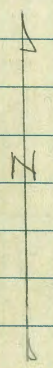
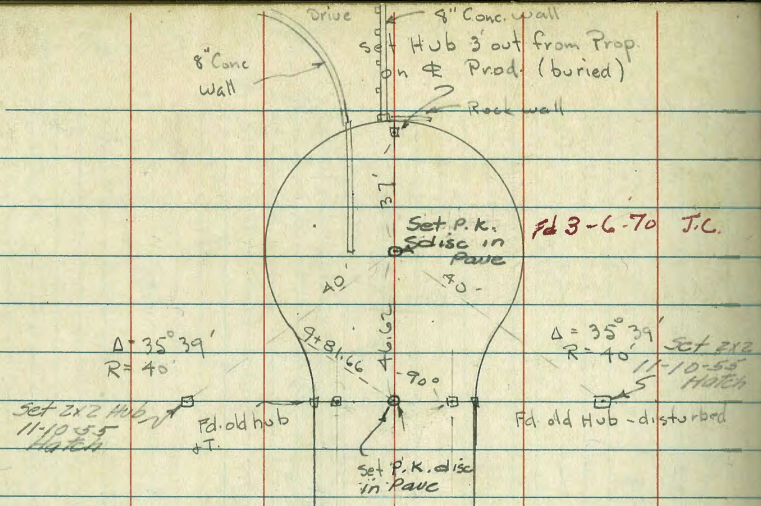
10'

10'

10'

10'

1



24 Pipe NW 50th + Alley 3.14 167.69
 T.P. 9.50 170.83 0.25 161.33

6+82.07 - for Profile

6+32.07 = End. = Wire fence - Sect along prop
 Line - See sketch

5+90

5+60

5+20

T.P. 6.75 161.58 11.07 154.93

5+00

4+50

162.3	160.8	158.9	157.6	155.8	152.6
162.1	160.5	157.3	157.0	155.3	152.6
161.8	159.8	157.5	156.3	154.7	152.1
161.5	159.3	157.5	155.4	153.4	151.7
161.5	159.0	156.4	154.5	152.7	150.0
161.2	158.8	155.6	153.9	151.9	149.6
161.6	158.1	154.6	152.6	150.6	
161.8	157.5	154.9	152.6	150.0	
162.0	159.3	154.9	152.6	150.0	

165.90

5-28-47
7.0

X-Sect. Ozark st. from Imperial to
N. end. - 50' st. - 10' cbs.

Lt. = W.

A

Rt = E

1+27- 17.6 Lt. = \pm P. pole # P 76088
1+00 = 30.2 Lt. = \pm Sing. Gar. Conc floor

0+95- 23' Lt. = \pm end Hedge

0+70

0+59- 23.2 Lt. = \pm 18' Eugenia Hedge 4' High

0+30 = N.L. Imperial

0+14 = edge Cold Lay shoulder

0+09 = N. edge Conc pave

0+00 = \pm Imperial - \pm 18' Conc. strip pave

B.M. 6.66 165.43 158.77

ct. \pm Imper
+ w 10' or 16'
BTL 15' P 3

155.03	154.96	158.8	160.2	160.63
157.19	157.11	156.7	160.2	160.7
158.30	158.27	157.9	160.0	160.7
158.77	158.75	158.6	159.9	160.5
159.47	159.40	159.4	160.0	160.6
160.19	160.11	159.9	160.1	161.3
160.64	160.56	160.4	160.4	162.0
161.80	161.69	161.4	160.9	
164.09	164.01			

4+96- 25.3 Lt. = end Conc. wall

4+87- 22' Rt. = # 12" Palm

4+50

4+30- 25.3 Lt. = Beg. 6" Conc. wall

4+14- 17.4 Lt. = # P. pole - # P 76090

4+00

3+79- 25' Rt. = # 4' Conc. walk

T.P. 4.02 159.73 9.72 155.71

3+50

3+37- 24.9 Rt. = # 10' Conc Drive

3+00

2+80- 25.3 Rt. = # 3' Conc walk

2+76- 17.1 Lt. = # P. pole # P 76089

156.17	156.2	156.21	156.1	155.4	155.2	155.4	155.9	155.2	155.4	155.9	156.5
35	35	35	35	35	35	35	35	35	35	35	35
155.2	155.3	155.7	155.1	155.7	156.0	155.9	156.0	156.2	156.4	157.0	156.12
35	35	35	35	35	35	35	35	35	35	35	35
155.6	155.7	156.0	156.4	156.0	156.2	156.4	156.0	156.2	157.0	157.02	157.36
35	35	35	35	35	35	35	35	35	35	35	35
155.2	155.3	155.7	155.1	155.7	156.0	155.9	156.0	156.2	156.4	157.0	156.12
35	35	35	35	35	35	35	35	35	35	35	35
155.6	155.7	156.0	156.4	156.0	156.2	156.4	156.0	156.2	157.0	157.02	157.36
35	35	35	35	35	35	35	35	35	35	35	35

8+50

8+10

7+85

7+50

7+27- 17.3 Lt. = P pole # P 760 92

7+20

6+90

T.P. 3.23 149.99 12.97 146.76

6+60

6+48- 22.8 Rt. = wly. end Hedge

6+30

153.8	150.2	149.6	149.2	149.4	147.7	147.7	151.2	151.7	148.5	148.9	142.3	144.2	145.3
2.9	2.5	2.1	2.5	2.3	2.6	2.8	2.5	2.0	2.5	2.5	2.5	2.8	2.5
144.4	144.4	144.4	144.4	144.4	144.1	145.0	146.2	146.2	146.2	146.2	142.0	144.8	143.7
142.7	142.2	141.8	142.3	142.5	143.4	143.4	143.4	143.4	143.4	143.4	141.5	143.2	143.7
140.5	140.5	140.5	140.5	140.5	140.5	140.7	140.7	140.7	140.7	140.7	140.8	140.8	140.8
138.4	138.4	138.4	138.4	138.4	138.4	138.4	138.4	138.4	138.4	138.4	138.4	138.4	138.4
136.1	136.1	136.1	136.1	136.1	136.1	136.1	136.1	136.1	136.1	136.1	136.1	136.1	136.1
134.5	134.5	134.5	134.5	134.5	134.5	134.5	134.5	134.5	134.5	134.5	134.5	134.5	134.5
132.4	132.4	132.4	132.4	132.4	132.4	132.4	132.4	132.4	132.4	132.4	132.4	132.4	132.4

159.73

check B.M. on Hub - 3 + 86.63
Book 1673 - P. 2

6.53 140.67 140.64

11 + 18.28 = for Profile

12" x 12" Pilaster 7' High at end
of 6" Rock + Conc. wall, + 1.5 Lt. = S. end 8" Conc. wall
10 + 68.28 = ϕ Prod. + Nly. end Ozark - Banjo = W. end

Lt.		Rt.	
12.5 35	134.5	15.3 25	131.9
12.1 25	135.1	15.1 2	131.7
10.7 4	137.01	12.58 14	132.1
10.8 14	136.4	13.1 10	134.62
10.4 3	136.8	11.9 10	134.1
8.0 5	139.16		135.3
8.1 5	139.1		136.5
6.62 Top Rock wall	140.58		
7.4 10.5 ground	139.8		
6.24 10.5 ground	140.96		
7.0 5	140.2		
5.9 5	140.3		
	147.20		

X-Section 20' Alley - N. of Imperial - from
 W. end - W. of Ozark to W. 50th St.

1+00

0+70

0+40

0+10

0+00 - W. end Alley at Pueblo Line

0-10

0-40 - for profile

T.P.-P. 34 2.12 157.83

155.71

5-28-47
 7.0.

Indexed
 C.S.K.

39

Lt. = N.

Rt. = S.

143.5	146.1	149.4	152.0	152.4
144.1	146.9	149.6	151.8	152.1
144.6	146.9	149.6	151.3	152.6
146.0	146.7	149.6	151.0	152.1
145.7	146.9	149.6	150.4	151.3
139.1	143.1	144.2	145.8	151.0
139.8	144.2	144.2	145.8	151.0
139.6	145.8	145.8	145.8	151.0

157.83

3+73.28 = E.L. Ozark

T.P. 12.21 169.31 0.73 157.10
See Ozark Sections

3+23.18 = W.L. Ozark St.

2+80

2+60 - 8.6 Rt. = end wire fence

2+40

2+00 - 8.6 Rt. = fence

1+70 - 8' Rt. = Reg. wire fence

1+70 - 8' Rt. = Cor. chicken House

1+62 - 8' Rt. = Cor. chicken House

1+62 - 7.3 Rt. = end fence

1+50

1+30 - 7.5 Rt. = Reg. wire fence

Lt.				Rt.
	157.4		157.6	158.2
	$\begin{array}{r} 11.9 \\ -0 \\ \hline 11.9 \end{array}$		$\begin{array}{r} 11.7 \\ -0 \\ \hline 11.7 \end{array}$	$\begin{array}{r} 11.1 \\ -0 \\ \hline 11.1 \end{array}$
			<u>169.31</u>	
		$\begin{array}{r} 154.5 \\ -0.3 \\ \hline 154.2 \end{array}$	$\begin{array}{r} 156.5 \\ -0.2 \\ \hline 156.3 \end{array}$	
		$\begin{array}{r} 154.6 \\ -0.2 \\ \hline 154.4 \end{array}$	$\begin{array}{r} 156.6 \\ -0.2 \\ \hline 156.4 \end{array}$	
		$\begin{array}{r} 155.2 \\ -0.6 \\ \hline 154.6 \end{array}$	$\begin{array}{r} 157.4 \\ -0.4 \\ \hline 157.0 \end{array}$	
		$\begin{array}{r} 156.2 \\ -0.6 \\ \hline 155.6 \end{array}$		
		$\begin{array}{r} 153.9 \\ -0.2 \\ \hline 153.7 \end{array}$	$\begin{array}{r} 154.0 \\ -0.2 \\ \hline 153.8 \end{array}$	
		$\begin{array}{r} 154.4 \\ -0.4 \\ \hline 154.0 \end{array}$	$\begin{array}{r} 154.6 \\ -0.2 \\ \hline 154.4 \end{array}$	
	$\begin{array}{r} 153.1 \\ -0.4 \\ \hline 152.7 \end{array}$	$\begin{array}{r} 152.6 \\ -0.2 \\ \hline 152.4 \end{array}$	$\begin{array}{r} 154.4 \\ -0.4 \\ \hline 154.0 \end{array}$	
		$\begin{array}{r} 152.9 \\ -0.1 \\ \hline 152.8 \end{array}$	$\begin{array}{r} 154.6 \\ -0.2 \\ \hline 154.4 \end{array}$	
		$\begin{array}{r} 152.9 \\ -0.1 \\ \hline 152.8 \end{array}$	$\begin{array}{r} 153.3 \\ -0.2 \\ \hline 153.1 \end{array}$	
		$\begin{array}{r} 153.3 \\ -0.1 \\ \hline 153.2 \end{array}$	$\begin{array}{r} 153.3 \\ -0.1 \\ \hline 153.2 \end{array}$	
		$\begin{array}{r} 152.9 \\ -0.1 \\ \hline 152.8 \end{array}$	$\begin{array}{r} 153.3 \\ -0.1 \\ \hline 153.2 \end{array}$	
	$\begin{array}{r} 153.3 \\ -0.1 \\ \hline 153.2 \end{array}$	$\begin{array}{r} 152.6 \\ -0.1 \\ \hline 152.5 \end{array}$	$\begin{array}{r} 154.6 \\ -0.2 \\ \hline 154.4 \end{array}$	
		$\begin{array}{r} 152.9 \\ -0.1 \\ \hline 152.8 \end{array}$	$\begin{array}{r} 154.6 \\ -0.2 \\ \hline 154.4 \end{array}$	
		$\begin{array}{r} 152.9 \\ -0.1 \\ \hline 152.8 \end{array}$	$\begin{array}{r} 154.6 \\ -0.2 \\ \hline 154.4 \end{array}$	
		$\begin{array}{r} 152.9 \\ -0.1 \\ \hline 152.8 \end{array}$	$\begin{array}{r} 154.6 \\ -0.2 \\ \hline 154.4 \end{array}$	
	$\begin{array}{r} 153.3 \\ -0.1 \\ \hline 153.2 \end{array}$	$\begin{array}{r} 152.6 \\ -0.1 \\ \hline 152.5 \end{array}$	$\begin{array}{r} 154.6 \\ -0.2 \\ \hline 154.4 \end{array}$	
		$\begin{array}{r} 152.9 \\ -0.1 \\ \hline 152.8 \end{array}$	$\begin{array}{r} 154.6 \\ -0.2 \\ \hline 154.4 \end{array}$	
		$\begin{array}{r} 152.9 \\ -0.1 \\ \hline 152.8 \end{array}$	$\begin{array}{r} 154.6 \\ -0.2 \\ \hline 154.4 \end{array}$	
		$\begin{array}{r} 152.9 \\ -0.1 \\ \hline 152.8 \end{array}$	$\begin{array}{r} 154.6 \\ -0.2 \\ \hline 154.4 \end{array}$	
	$\begin{array}{r} 153.3 \\ -0.1 \\ \hline 153.2 \end{array}$	$\begin{array}{r} 152.6 \\ -0.1 \\ \hline 152.5 \end{array}$	$\begin{array}{r} 154.6 \\ -0.2 \\ \hline 154.4 \end{array}$	
		$\begin{array}{r} 152.9 \\ -0.1 \\ \hline 152.8 \end{array}$	$\begin{array}{r} 154.6 \\ -0.2 \\ \hline 154.4 \end{array}$	
		$\begin{array}{r} 152.9 \\ -0.1 \\ \hline 152.8 \end{array}$	$\begin{array}{r} 154.6 \\ -0.2 \\ \hline 154.4 \end{array}$	
		$\begin{array}{r} 152.9 \\ -0.1 \\ \hline 152.8 \end{array}$	$\begin{array}{r} 154.6 \\ -0.2 \\ \hline 154.4 \end{array}$	
	$\begin{array}{r} 153.3 \\ -0.1 \\ \hline 153.2 \end{array}$	$\begin{array}{r} 152.6 \\ -0.1 \\ \hline 152.5 \end{array}$	$\begin{array}{r} 154.6 \\ -0.2 \\ \hline 154.4 \end{array}$	

153.28
floor

5+05 = 8.6' Rt. = Beg. Shed - wood floor

5+00

Gar. on Last 4' of wall

4+81 - 10.4 Lt. = end Conc. wall - lean to from

4+75

+ end of Conc. Dr.

4+57 - 14' Lt. = S.W. Cor. Gar. conc. floor - opens w.

4+50

4+25

4+00

3+74 - 10.7 Lt. = Beg. 4" Conc. wall - base for wire fence

162.02	162.6	163.0	163.5	163.6	164.99
7.29	2.5	5.3	5.8	2.7	8.6
Top wall	0	0.5	0.8	0	floor
	161.2	161.6	162.3	162.9	
	14	10.4	10.0	2.4	
along Gar.	Top wall				
161.33	161.77	161.3	162.3	162.9	
7.98	7.04	8.0	0.0	2.4	
14	10.4	10.0	0.0	2.4	
floor	Top wall				
	160.93	161.31	161.6	161.7	
	2.38	2.00	0.0	2.6	
	14	10.4	10.0	2.0	
	edge Dr.	Top wall			
	159.56	160.07	160.6	161.1	
	9.2	9.22	2.9	2.0	
	18.2	10.6	0.0	2.0	
	edge Conc.	Top wall			
	158.94	159.9	160.4	161.1	
	10.7	9.4	2.9	2.0	
	Drive (see Ozark)	Top wall			
	157.7	158.6	159.2	159.5	
	10.7	10.7	0.8	0.2	
	Top wall				
	160.3				
	10.0				
	Top				
	10.0				
	Ground				
	169.31				

7+00

6+67- 10.7 Beg. Board fence + Step up in Conc. ^{base}
 6+67- 11 Rt. = end shed

T.P. 5.36 172.41 2.26 167.05

along same Conc. wall as fence

6+50- 10.4 Rt. = end fence + Beg. Shed - Conc. floor

6+37- 9.4 Lt. = N Ly Pole stub - 3' High
 Board fence

6+37- 9.7 Rt. = end shed + 10' Rt. = 6" Conc. base for

6+25- 9.6 Rt. = end Conc. wall + fence + Beg. wood ^{shed.}

6+00

for slat fence

5+70- 8.6 Rt. = end Rail fence + Beg. 8" Conc. base

5+40

5+31- 8.6 Rt. = Beg. rail fence

5+31- 8.6 Rt. = end shed.

166.8	166.9	167.3	167.6	168.17	
20	0	1	4.8	4.24	
			10	10.9 = Top Conc.	
				167.43	
				4.98	
				11 = Floor Shed.	
					4.25
					10.7 = Top Conc. base
166.7	167.1	172.41	167.0	167.43	
2.6	2.2	2.6	2.3	2.88	
20	10	2.6	10	10.4 on Conc.	
					167.27
					2.04 = Top Conc.
					167.3
					2.0
					9.6 floor shed.
166.4	166.5	166.3	166.5	167.1	
2.9	2.8	3.0	2.8	2.2	
20	0.8	0	9.1	9.2	
			ground		
					Top wall
					9.6
					167.70
					2.04 = Top Conc.
					167.3
					2.0
					167.3
					2.0
					166.9
					2.4
					2.0
164.0	164.7	166.0	166.1	167.12	
3.3	0.8	3.3	3.2	3.0	
20	0	0	0.6	0.6	
					ground
					Top
					167.12
					3.0
					166.7
					2.6
					166.9
					2.4
					2.0

Lt.

Rt.

check B.M. pipe on NW.

4.73 167.68 167.69
R. 31

7+73.45 = W.L. 50th

7+69-113 Rt. = end Conc. + fence

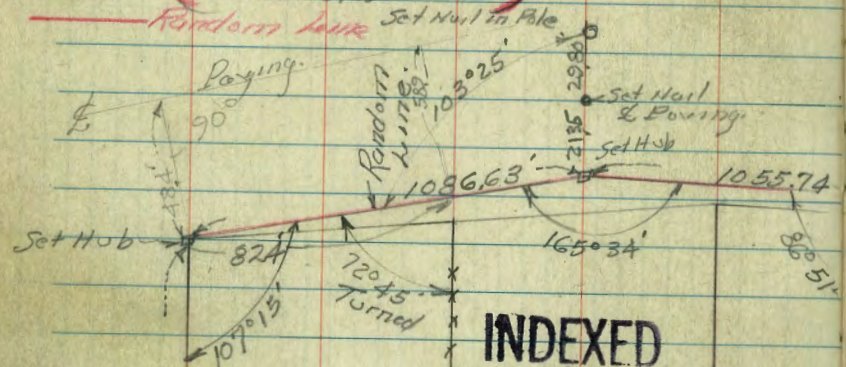
7+30-

167.6	168.4	168.9	
4.8 10	4.0	3.5 10	
167.6	168.3	168.3	168.62
4.8 10	4.1	4.1 10	3.79 11.3 Top Conc
		168.26	
		4.15 11.1 Top Conc.	

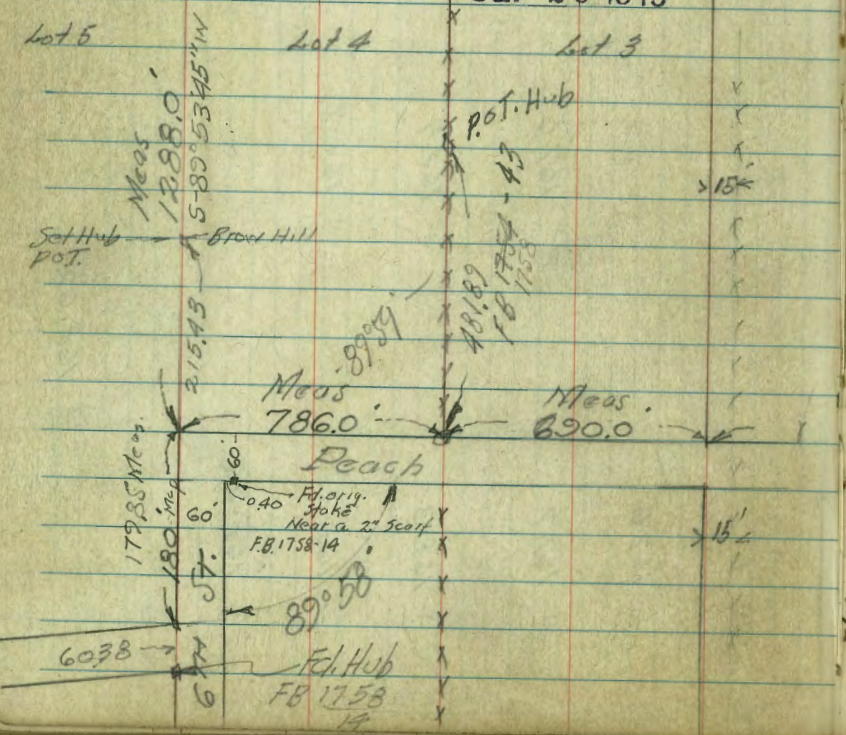
172.41

Survey for Topography Control
 in City owned lots 1, 2, 3, 4.
 Walker
 Becker
 Johnson
 Melton
 7-31-47

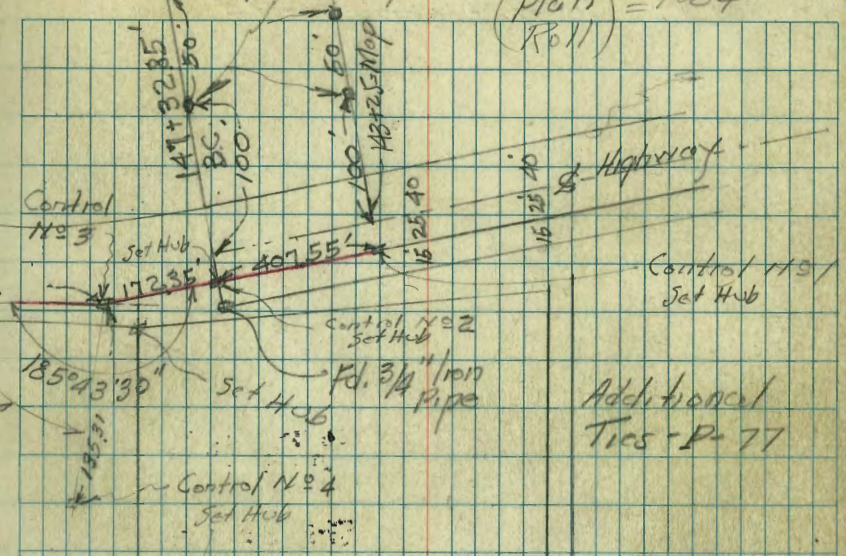
Block 2.7 - Rosedale Subdivision
 (Coordinates P-63)



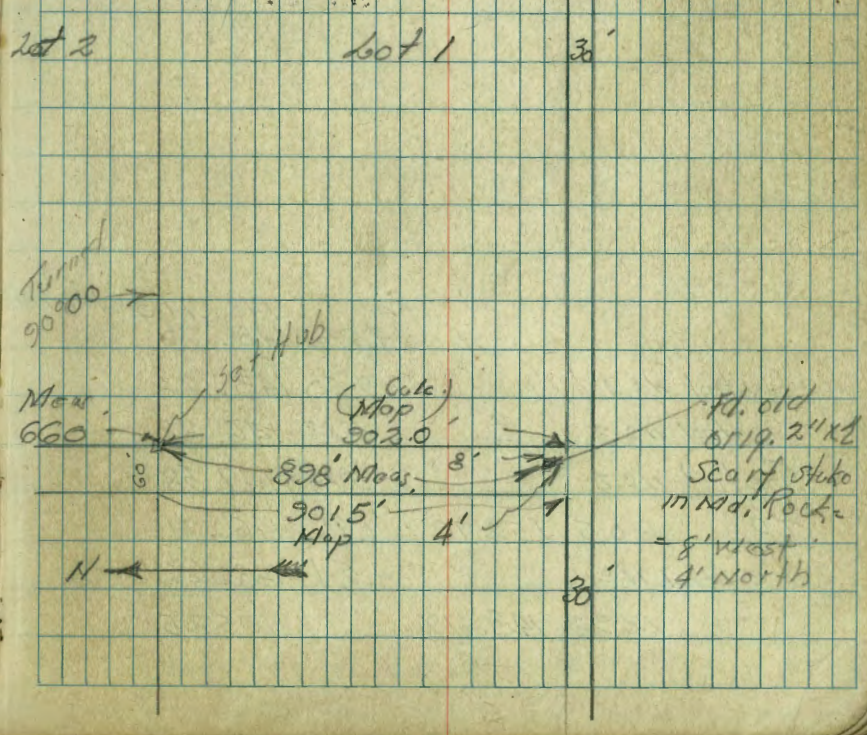
INDEXED
 W.K.
SEP 29 1949



Fd. 60 Spikes R.P.S.
 (Plan) # 7054
 (Roll)



Additional
 Ties - P-77



Topography Control Data
Cont. from P-44

			148.713 = Point of Elev.
	4.06	148.70	
Control No 4	9.50	143.26	
Control No 3	5.88	146.88	
Control No 2	5.18	147.58	
TP	6.05	152.76	1.46 146.71
Control No 1	4.51	143.66	
	12.22	148.17	135.25

chk State B.M. 153+36

State B.M. on Hd. Wall on Rt. Mile Post 2.0
139+82 Plan Roll 705A
Elev. Printed on Conc. Hd. Wall
Had Not Shown on Plans.

Walker
Hendricks
Becker
10-17-47

Location

Proposed 8" Water Line
LINDA VISTA ROAD
Between City Boundary
and Gibbs Airport.

Note: Line Constructed to Inked Line.
- Construction Grades in Grade Book 232

2+38.01 - Alt 1034 2°47'30"

1+10.00 - Alt 1019'

0+05.45 = Intersection City Line

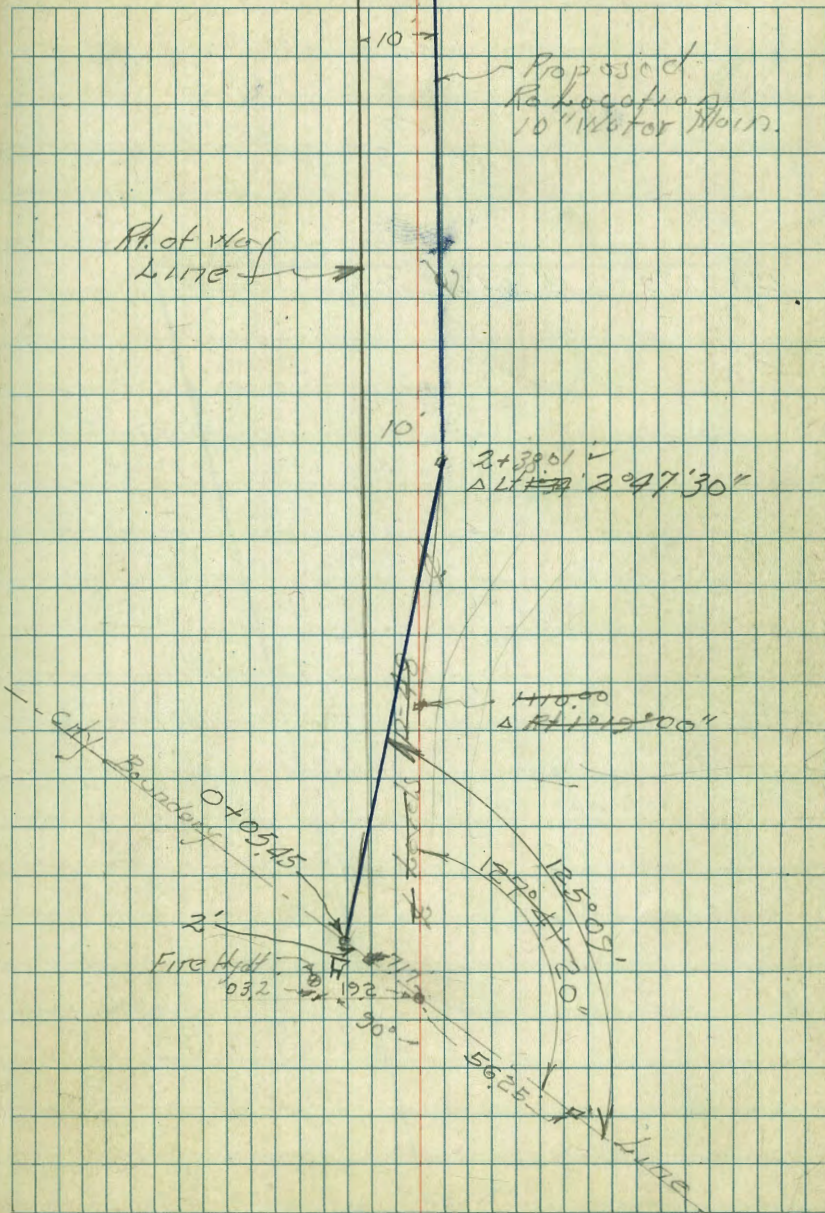
0+04.4 = E. End East-T

0+03.3 = E. Fire Hydrant 12.2' Lt.

0+00 = Intersection city line

Indexed
C.R.H.

46



T.P. 0.04 410.99 12,54410,45

0+46

83 92 118 122 131
12 7 3

10.6

0+40

87 112 118 128
15 6 10

11.2

0+10

56 78 101 107 110
19 12 2 10

12.3

0+00 = "city line"

60 68 102 102 109
14 7 3 10

12.8

0-50

43 48 71 71 75
12 6 4 10

15.9

0-100

16 28 28 36 36 40
12 8 8 4 10

17.4

721 422.99

415.78

State B.M. 422.99

3+00

73	86	96	140
9		4	10
at Fence			

2+75

63	66	80	124	129
9	5		5	10
at Fence				

2+380/ = ΔH 1°34'

47	52	866	98	107
9	7	op	1	10
at Fence		14.4		

2+00

15	33	78	78	86
16	6	2		10

1+50

40	06	53	53	60
15	8	2		10

1+00

+ 33	+ 29	51	31	36
15	10	2		10

41049

41049

6+00

80	89	91	86	85
9	6		10	10

5+50

63	73	71	69	67	65
9	6		5	5	10
				old	new

5+00

41	55	48	45	42
10	5		3	10

4+50

70.5	80	2.6	2.3	2.1
9	5		3	10
			old	new

398.63

TR 1.06 398.63 12.92 397.57

4+00

81	119	125	122	120	117	116
11	6	5		3	55	10
				old	old	old

00.5

3+50

94	100	104
8		11

110.9

410.49

8+50

2.6
92.9
6

2.7

85.9
5
10
102.3
10
10

388.26

TP 1.95 388.26 12.32 386.31

8+00

12.4
912.7
6

12.5

86.3
5
1012.3
10

7+50

11.5
9

11.9

86.9
5
10
1011.7
10
10

7+00

10.8
911.4
4

11.1

87.7
5
1010.9
10

6+81 = 1st. 18" Conc. Pipe Culvert

12.0
1012.58
3
on Flow10.9
3
on 114.46 ft

10.8

88.0
5
1010.6
1014.0
37
on Flow

6+50

398.63

10.4
910.6
8

10.3

88.3
5
1010.2
10

398.63

11+50

24	27	66	63	82.0	5.8
18	10	5		5.0	10
at fence					

11+00

40	47	61	57	82.6	5.3
13	8	5		5.9	10
at fence					

10+48.65 - POT. This here

51	55	516	83.10	1.83	4.7
9	5			5.5	10
				at fence	

10+00

42	51	46	83.7	4.3	4.7
9	5			5.0	10
				at fence	

9+50

38	42	40	84.3	3.7	3.6
9	5			5.6	10
				at fence	

9+00

30	35	32	85.1	3.1	2.9
9	6			5.2	10
				at fence	

388.26

388.36

13+35

82
10

79.7

79.8

85
10

13+15

84
10

80.0

80.1

82
5

79
8

13+50⁰⁶

58
8

84
2

80.0

80.1

83

82
6

92
9

13+00

51
9

84
3

80.1

80.6

82

77
6

93

12+50

37
10

77
4

80.9

81.1

74

72
5

71
10

12+00

28
23
at fence

31
12

71
8

81.5

6.8

81.7

66
5

65
10

38826
3

38826
3

14+20

14+07.3

13+24.8

13+80

TP 606 386.91 741 380.85

13+80

13+45

38826

24

24

PT 54

112 70 67 61
14 8 8 10

80.2

80.16

675 61
on Top 10
Box Culvert

80.14

80.6

779 610 67 677 63
32 14 13 on Conc. 10
on HW Wall Box Culvert
or inside

80.1

35 75 68 64
10 7 10

386.91

CHK state BR #3

checked against on W HW Wall State BR 1750-1
Sta 16+23

79.9

66 71 86 84 83
12 4 10

38826

16+00

15+77

15+70

15+32

15+30

14+9710 = Δ θ 20°

L

R

θ

55

18
10

81

89
10

83.4

21
10

85

49

81.2

57

61.2

57

81.7

52

81.83

5.08

386.91

17+35

 $\frac{0.3}{10}$

0.61.6

 $\frac{0.3}{10}$

16+85

 $\frac{1.06}{10}$

0.61.8

0.3

16+50 = Approx Pt. of Way Line

 $\frac{0.7}{10}$

0.55

 $\frac{3.2}{10}$

16+25

 $\frac{1.7}{10}$

0.3.3

3.6

7.7

386.21

Levels - Proposed Re-location
 10" Water Main
 Alternate Line

12+55

2.0
10 2.3 2.4
 7 6.4
 13

84.6

12+23

1.0
10 0.7 0.8 6.1
 4 11

88.2

12+00

1.1
10 1.7 2.0 5.8 5.7
 12 8 10

86.2

11+60

1.1 1.1
10 2 2.1 5.4 5.0
 4 10

84.8

11+25

1.2
10 2.1 4.9 4.4
 4 10

82.0

10+18.5 = 11

83.1

2.3

386.91

13+70

138	13.7	10.8	6.8
10		7	14
Not Ground	Not Ground	Fill	10 Fill

73.2

13+45

128	12.7	8.8	5.1	5.1
10	7		7	15
Not Ground	Not Ground	10 Fill	10 Fill	10 Fill

78.1

13+34

10.1	10.3	8.0
10		10

76.6

13+17

7.6	7.5	7.1
10		10

79.4

13+00

2.1	3.3	3.6
10		10

83.6

12+80

1.3	1.6	3.1
10		10

85.3

14+45

86
1078.5
8483
10

14+09

121
1074.6
123123
10

14+05 in channel

176
1070.3
166

154

13+98

170
1070.3
166154
10

17 channel

17 channel

13+97

139
1073.0
139139
10

13+85

150
1071.9
150148
10129
10

14 + 9770
15 + 3589

15 + 31

15 + 27

14 + 9893 Δ R4.

81.83
5.08

51
10

81.4
5.5

56
10

40
10

82.3
4.6

55
10

57
10
North

66
10
West

80.85
6.06

Additional Profile Levels
 Re-Proposed Location 8" Water Main

2+00

1+50

1+10

1+00

0+55

0+10

0+144 on Top 10" T.
 318 415.27 412.79

	402.8	2
	13.2	403.2
		12.8
	405.3	Edge Pav
	10.7	9.406.1
	10.7	9.9
		Edge Pav
		408.1
		7.9
		Edge Pav
	408.9	
	7.1	
	412.5	411.1
	3.5	4.9
		Edge Pav
	412.4	
	3.6	
	411.6	
	4.4	
B.M. on stake	0+00	Grade Book 3.33
	415.27	21

2+38

14.7
415.97

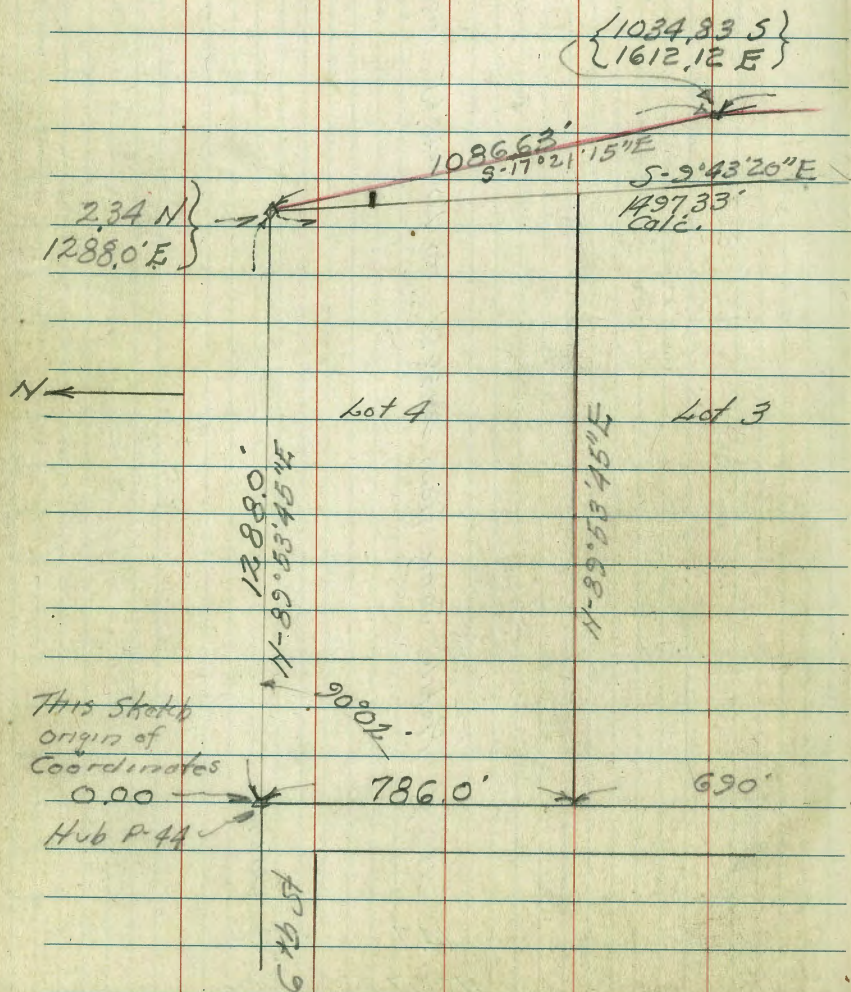
Profile some from 2+38.01 to 10+48.65 Page 49-52

150
Por
Edge

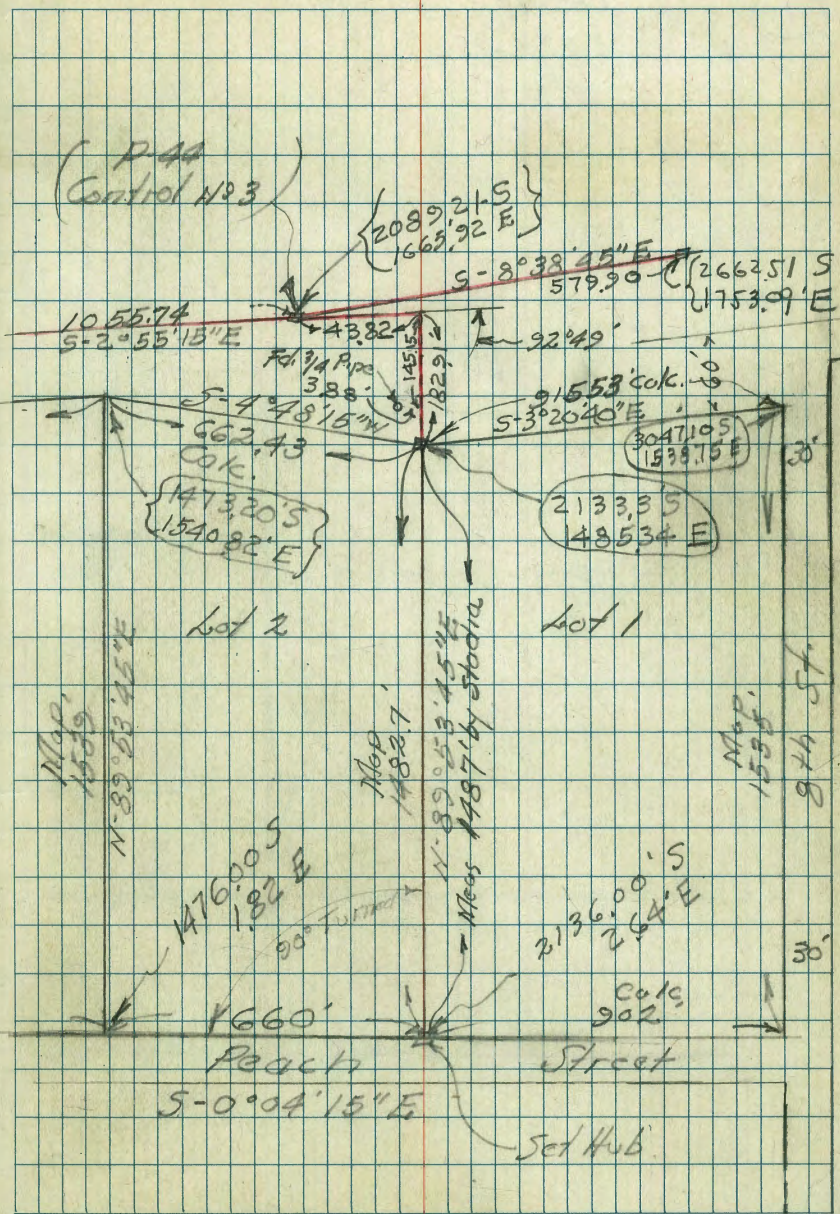
Additional Data
Block 27 - Rosedale Sub.

Cont. from P. 44

Random Line



This sketch
origin of
coordinates
0.00



1+13.17 13C	460	163.27	160.13	C 3.14
+90	469	163.18	160.29	2.89
+65	487	163.00	160.63	2.27
+40N	529	162.58	161.09	1.49
0+15N	538	162.49	161.55	0.94
0+00N	559	162.28	163.96	F 168
0+62				
140N	5.29	162.58	159.48	C 3.10
165N	6.06	161.81	159.35	2.46
190N	7.05	160.82	159.75	1.07
0+55				
00N	5.93	161.94	163.40	F 1.46
15N	6.05	161.82	161.33	C 0.49
40N	5.54	162.33	160.87	1.46
65N	5.13	162.74	160.41	2.33
90N	5.02	162.85	159.95	2.90
115N	4.68	163.19	159.49	3.70
190N	7.15	160.72	159.33	1.39
0+50				
140N	5.51	162.36	159.05	3.31
165N	5.97	161.90	158.86	3.04
190N	7.30	160.57	159.10	1.47
0+45				
167.87				

T.P. 6.29 17001 4.15 163.72

140 H 3.76 164.11 163.82 C 0.29 ✓

1+05

165 H 4.45 163.42 163.40 0.02 ✓

190 H 5.58 162.29 161.66 0.63 ✓

1+00 E

140 H 3.79 164.08 163.45 0.63 ✓

0+95 E

165 H 4.83 163.04 163.01 0.03 ✓

190 H 5.86 162.01 162.69 F 0.68 ✓

0+90 E

165 H 5.29 162.48 162.08 C 0.40 ✓

190 H 6.16 161.71 162.29 F 0.58 ✓

0+80 E

190 H 6.31 161.56 160.49 C 1.07 ✓

0+75 E

190 H 6.57 161.30 161.36 F 0.06 ✓

0+70 E

140 H 4.80 163.07 160.36 C 2.71 ✓

165 H 5.43 162.44 160.30 C 2.14 ✓

190 H 6.71 161.16 160.76 C 0.40 ✓

0+65 E

167.87

8.17	4.98	16503	16500
44.23	4.84	16517	16466
65	5.04	16497	16450
90	5.01	16500	16437
124.17	5.23	16478	16420
140	4.88	16513	16408
165	5.39	16462	16372
190	6.29	16372	16315

1+22 E

190	6.47	16354	16297
165	5.31	16470	16352
140	5.00	16501	16388
124.17	5.15	16486	16400
90	5.17	16484	16417
65	5.19	16482	16430
44.23	5.26	16475	16440

1+29 E

44.23	5.48	16453	16460
65	4.90	16511	16450
90	4.83	16518	16437
124.17	5.06	16495	16420
140.11	5.34	16467	16408
165.11	5.86	16415	16372
190.11	6.72	16329	16315

1+24 E

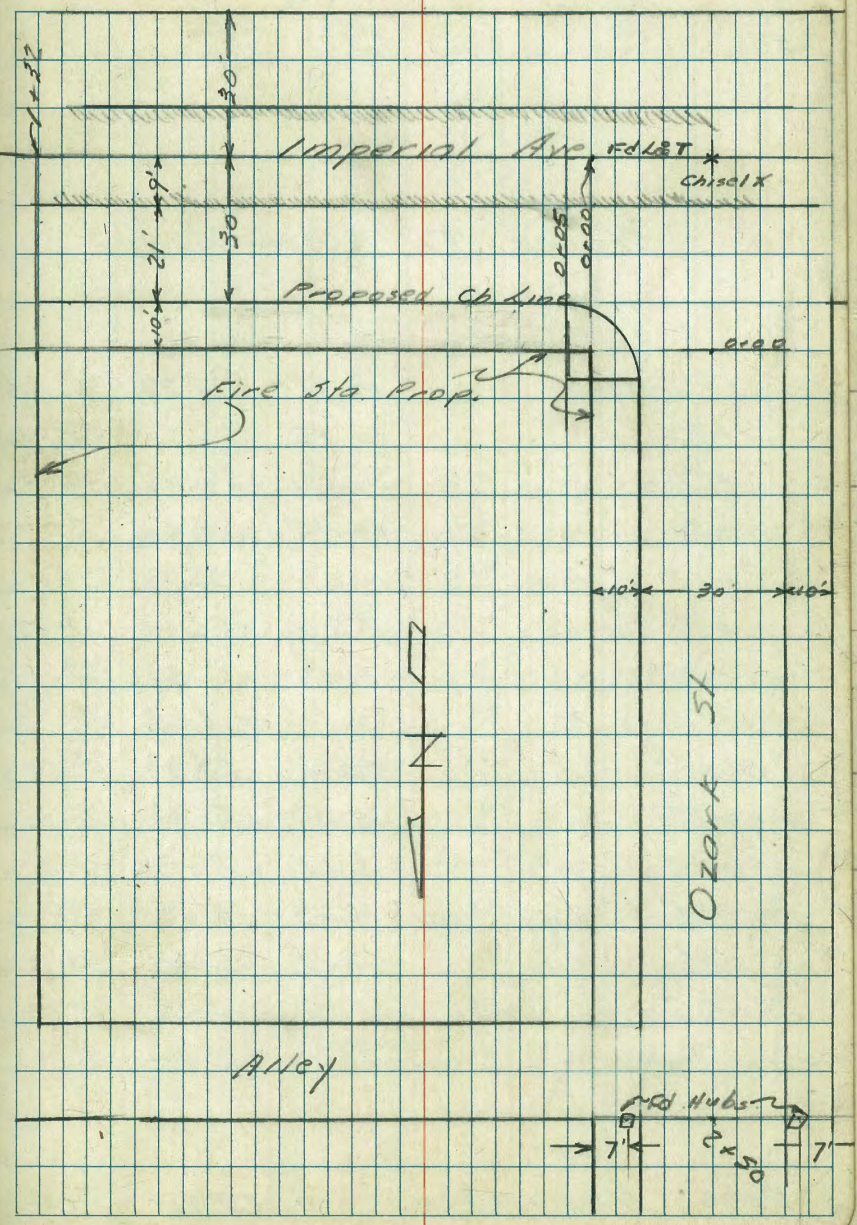
170.01

CR El Floor Fire Station

C 0.57	✓
0.47	✓
0.63	✓
0.58	✓
1.05	✓
0.90	✓
0.57	✓
0.57	✓
1.18	✓
1.13	✓
0.86	✓
0.67	✓
0.52	✓
0.35	✓
F 0.07	✓
C 0.61	✓
0.81	✓
0.75	✓
0.59	✓
0.33	✓
0.14	✓

7.6-48
Hendricks
Roberts
Greer
Rohr

Grade Stokes for Grading
Ozark & Imperial Around
Fire Station No 12



Levels for Grades on
Imperial Ave. Ozark to
E-line Fire Sta. Prop.

Sta	+ H.L.	-	^{3/4" to} Elev.	Elev Grade
-----	--------	---	-----------------------------	---------------

C or F

Stated To Gutter Grade

CK starting B.M.	7.97	158.77	158.77	
------------------	------	--------	--------	--

7+32.00	0.48	166.26	166.41	F 0'5"
---------	------	--------	--------	--------

1+00.25	1.84	164.90	164.94	F 0'4"
---------	------	--------	--------	--------

0+68.50	4.05	162.69	163.58	F 0'8 1/2"
---------	------	--------	--------	------------

0+36.75	4.94	161.80	162.02	F 0'2 1/2"
---------	------	--------	--------	------------

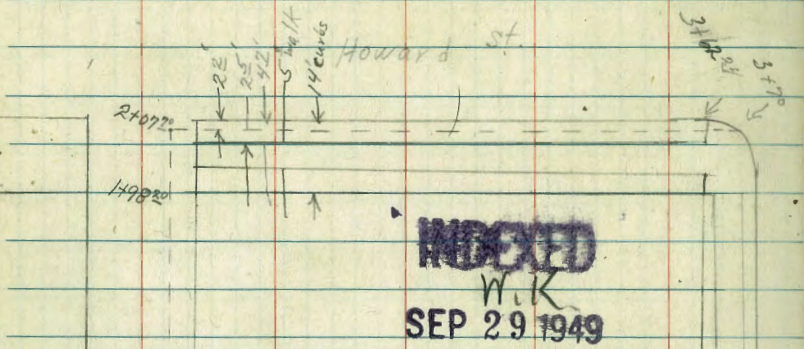
0+05	6.34	160.40	160.56	F 0'6"
------	------	--------	--------	--------

7.97	166.74	158.77		
------	--------	--------	--	--

D. Smith
W. Moore
S. Clark
E. Gregory

Profile Levels proposed Storm Drain

Note further sketch (page 8).



← 20 →

← 10 → ← 5 → ← 5 →

Florida St

4401
Stub of 400 Drain

BIK 143 Univ Hts.
Profile Line

W.O. 20008 72
9-28-49

Station	Elevation	Notes	Profile W/O	Profile W/O	Profile W/O
42+07.20	302.47 302.30				288.41 17.30 289.47
	302.53		3+70		289.54 289.67
41+98.20	302.67 303.00	Howard St Prep			17.30 16.66 16.53
41+75	302.00		3462 ²⁴ West Prop. Florida		
	302.2				289.99 290.67 290.6
41+50	301.5				16.21 15.50 15.6
	301.5				292.21 292.76
41+25	300.9		3425 drive		13.20 13.44
	300.9				294.44 295.00 295.0
41+00	299.5		3400		11.76 11.20 11.2
	299.5				296.56 297.15 297.2
0+75	298.7		2475		9.68 9.85 9.9
	298.7				298.75 299.18
0+50	298.4		2450 drive		7.85 7.00
	298.4				300.88 301.49 301.5
0+25	298.6		2425		5.80 4.71 4.2
	298.6				302.25 302.57
0+00	17.5		2412 ² East of Hwy		3.00 3.63 Gutter Top
TP	346	306.20	0.30	302.24	
BM	12.25	303.04		290.52	N.W.P.P. Howard St Profile

Roberts
Gaitor
Moore
Clark
1-6-59
W.O. 20622

Survey for Curb Inlets #74 and Market

F.B. 1673

.. 1550

.. 514

Market

BM

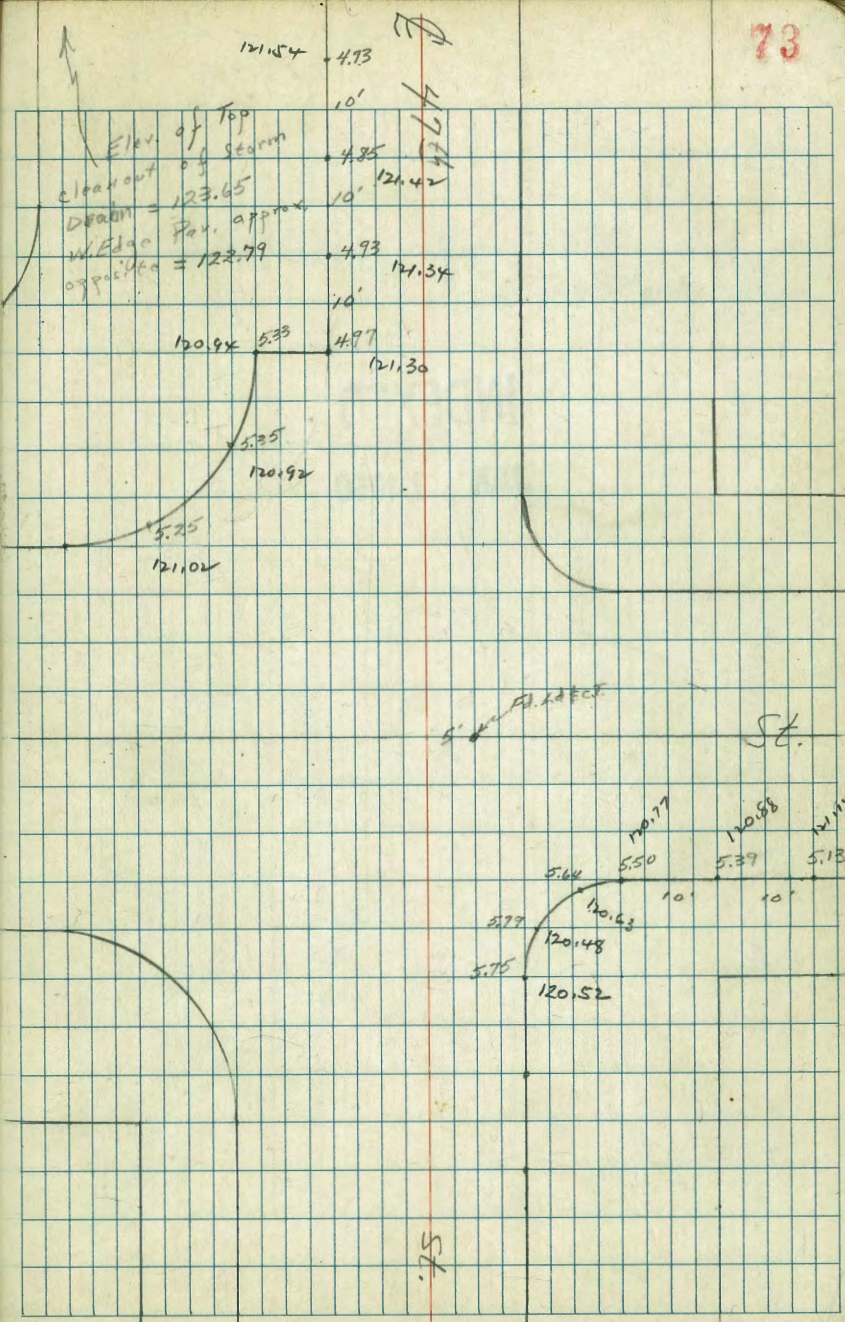
5.31

126.27

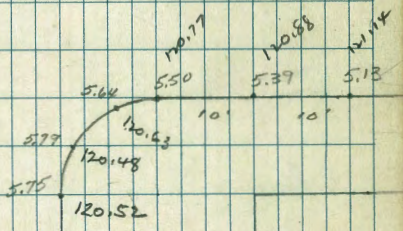
No Record

120.96

at d.c.t.
#74 &
Market



St.



Cont'd From Page 74

Lt

Barometer

Rt

75

0+61 5' Lt. End Woven Wire Fence

0+59.5 13.5' Rt. Conc. Ret. Wall on R.R. Bridge

0+56

87.4	87.4	87.3	87.4	89.4	89.8	92.4
5.0	5.0	5.1	5.0	3.0	2.6	0.0
15	5		4	6	11	16

0+48

87.8	87.7	87.4	87.4	87.5	89.3	89.3	92.4
4.6	4.7	5.0	5.0	4.9	4.1	5.1	0.0
15	6	4		5	6	11	16

0+35 8.4' Lt. 4" Apricot Tree

0+21

88.1	88.1	87.6	88.0	89.2	92.4
4.3	4.3	4.8	4.4	3.2	0.0
15	2		6	13	17

0+20 9.5' Lt. 4" Apricot Tree

0+13 8.6' Lt. Begin Woven Wire Fence

0+11

88.6	89.1	89.6	92.4
3.8	3.3	2.8	0.0
15		12	18

0+00

87.5	87.8	88.2	88.63	88.7	91.0
5.1	4.6	4.2	4.73	3.7	1.4
15		12	10	10	15

BM

8.18

92.36

84.18

N.E. B.P. Perre #4754

Holes Reduced 1-12-50

0+779.2 Curb and Gutter 47th St.

84.74	85.21	85.38	85.81	86.49	85.96	87.04	86.40
7.02	7.15	6.98	6.55	5.87	6.40	5.36	5.96
200 Gutt.	100 CB	50 Gutt	50 CB	50 CB	50 Gutt	50 CB	50 Gutt

0+72.1 E. Edge Walk (Walk changes at 82th of Base Line to comb. WIK # cb at RR Bridge)
(Tele. Cond. Under Walk)

86.47	86.61	86.70	86.96
5.85	5.75	5.66	5.40
15	8.2		16.8 abit.

0+65

87.1	87.4	87.1	86.9	87.1	89.4	89.7
5.3	5.0	5.3	5.5	5.3	3.0	2.7
15	5	3		4	8	15

92.36

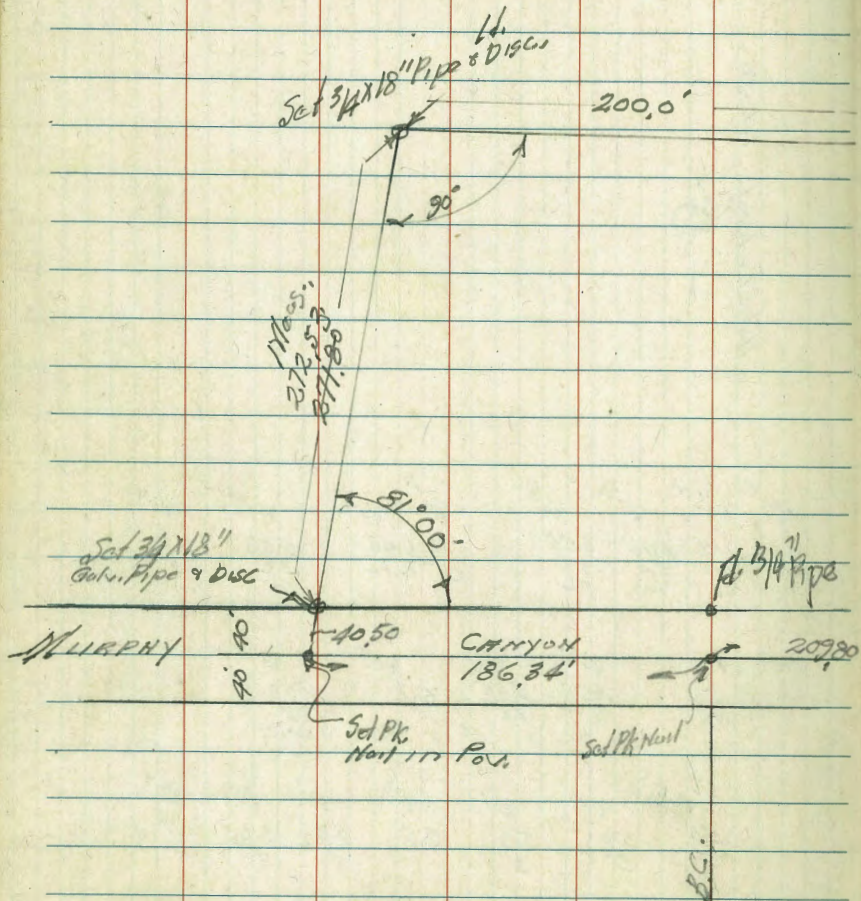
92.36 ✓

SURVEY PROPOSED GARBAGE HOPPER SITE

PORTION LOTS 1, 2, 43, ROSADALE TRACT.
And old County Right of Way

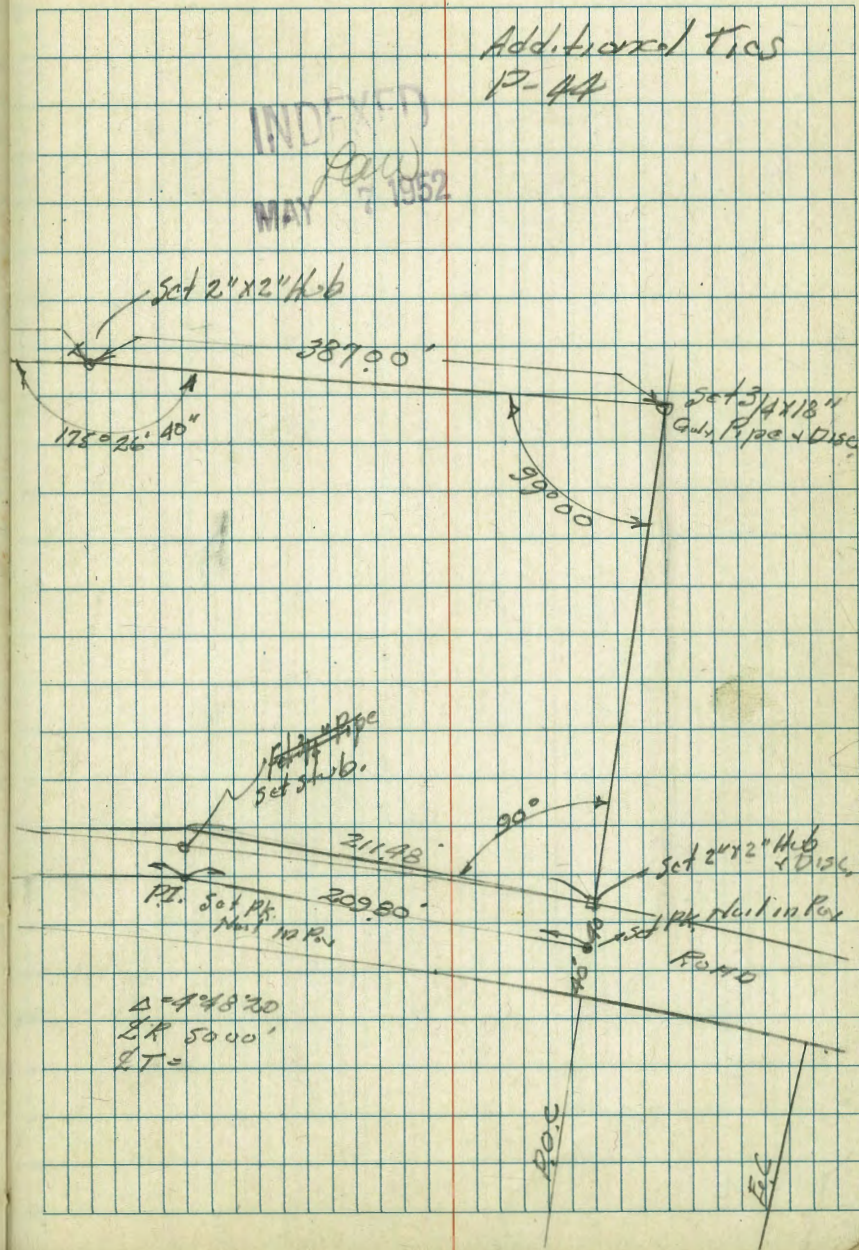
Walker Plat 3437-B

Popo
Cota
5-6-52



Additional Ties
P-44

INDEXED
MAY 7 1952



$\Delta = 148.30$
BR 5000'
BT =

A ledger page with horizontal blue lines and five vertical red lines. The page is divided into six columns by the red lines. The first column is the widest, followed by four columns of equal width, and a narrow column on the far right. There are 25 horizontal blue lines across the page.

A ledger page with horizontal blue lines, a vertical red line, and a grid of blue lines. The page is divided into two columns by the red line. The left column is wider than the right column. The right column contains a grid of 20 vertical blue lines and 25 horizontal blue lines, creating a 20x25 grid. There are 25 horizontal blue lines across the page.

IMPROVED TABLES AND INFORMATION

HORIZONTAL STADIA CORRECTIONS

2°-00' — 0.1	21°-00' — 12.3	33°-00' — 29.7
3°-00' — 0.3	21°-30' — 13.4	33°-15' — 30.1
4°-00' — 0.5	22°-00' — 14.0	33°-30' — 30.5
5°-00' — 0.8	22°-30' — 14.7	33°-45' — 30.9
6°-00' — 1.1	23°-00' — 15.3	34°-00' — 31.3
7°-00' — 1.5	23°-30' — 15.9	34°-15' — 31.7
8°-00' — 1.9	24°-00' — 16.5	34°-30' — 32.1
9°-00' — 2.5	24°-30' — 17.2	34°-45' — 32.5
10°-00' — 3.0	25°-00' — 17.9	35°-00' — 32.9
10°-30' — 3.3	25°-30' — 18.6	35°-15' — 33.3
11°-00' — 3.6	26°-00' — 19.2	35°-30' — 33.7
11°-30' — 4.0	26°-30' — 19.9	35°-45' — 34.1
12°-00' — 4.3	27°-00' — 20.6	36°-00' — 34.6
12°-30' — 4.7	27°-30' — 21.3	36°-15' — 35.0
13°-00' — 5.1	28°-00' — 22.0	36°-30' — 35.4
13°-30' — 5.5	28°-30' — 22.8	36°-45' — 35.8
14°-00' — 5.9	29°-00' — 23.5	37°-00' — 36.2
14°-30' — 6.3	29°-30' — 24.3	37°-15' — 36.6
15°-00' — 6.7	30°-00' — 25.0	37°-30' — 37.1
15°-30' — 7.2	30°-15' — 25.4	37°-45' — 37.5
16°-00' — 7.6	30°-30' — 25.8	38°-00' — 37.9
16°-30' — 8.1	30°-45' — 26.2	38°-15' — 38.3
17°-00' — 8.5	31°-00' — 26.5	38°-30' — 38.7
17°-30' — 9.0	31°-15' — 26.9	38°-45' — 39.1
18°-00' — 9.5	31°-30' — 27.3	39°-00' — 39.6
18°-30' — 10.1	31°-45' — 27.7	39°-15' — 40.0
19°-00' — 10.6	32°-00' — 28.1	39°-30' — 40.5
19°-30' — 11.2	32°-15' — 28.5	
20°-00' — 11.7	32°-30' — 28.9	
20°-30' — 12.3	32°-45' — 29.3	

Chains to Feet

1	66
2	132
3	198
4	264
5	330
6	396
7	462
8	528
9	594
10	660

Feet to Chains

100	1.515
200	3.030
300	4.545
400	6.060
500	7.575
600	9.090
700	10.606
800	12.121
900	13.636
1,000	15.151

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

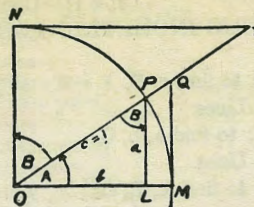
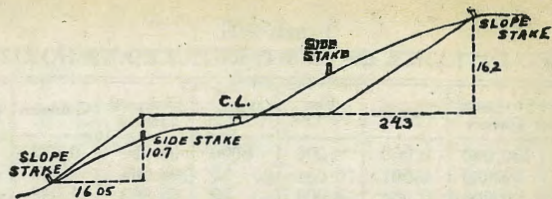


TABLE II
TRIGONOMETRIC FORMULÆ.

$\angle A = \angle MOP$ $\angle B = \angle PON = \angle OPL$
 $R = OB = c = 1$

$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$
 $\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$
 $\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$
 $\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$
 $\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$
 $\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$
 $\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$
 $\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$
 $\text{exsec } A = PQ = \text{coexsec } B$
 $\text{coexsec } A = PT = \text{exsec } B$
 $\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \qquad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$
 $\sin 2A = 2 \sin A \cos A \qquad \cos 2A = \cos^2 A - \sin^2 A$
 $\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$
 $\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$
 $\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 05	1 20	1 35	1 50	1 65	1 80	1 95	2 10	2 25	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
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9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
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16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
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19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
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21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
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Computed by L. Leland Locke.

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