

1757

MS

1757

175

MICROFILMED

DEC 29 1964

CITY ENGINEER'S OFFICE
SAN DIEGO, CALIF.

172.15 = ct. m
243.12
415.27

172.15
249.1
197.06
4.03
193.03
42.93
150.10

243.12

172.15

249.1
ct.
7-8

200 + 155

MADE IN U.S.A.

1757

Our Leather Bound Engineers Note Books
are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4x4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book,) which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

THE FREDERICK POST CO.

ENGINEERING and DRAFTING SUPPLIES

P. O. Box 803

CHICAGO

INDEXED
to page # 76

Page.

- 1-A - Prop. Ties - Washington Ext. - Lincoln to Normal
 5 - Adams & Texas Topog.
 10-12 - Add. Prop. ties - Washington Ext.
 13-16 - X-Sect Cloue - Hugo to Ingelow
 17-35 Cross Sec 47th St Imperial/Kurtz Market St
 36 Survey Lots 29 to 33 Blk 139 U.H.
 37 Alley B/R. (A) Sunset Crest
 44-48 - X-Sect Alley in Block 6 - Alhambra park
 49-56 - X-Sect Lots 47-49 inc. in Block 6 - Alhambra Park
 57-68 Culvert B/R 195 City Hgts
 70 " 33rd Lincoln + Bdry

Property ties for Washington St ext.
 Lincoln to Normal

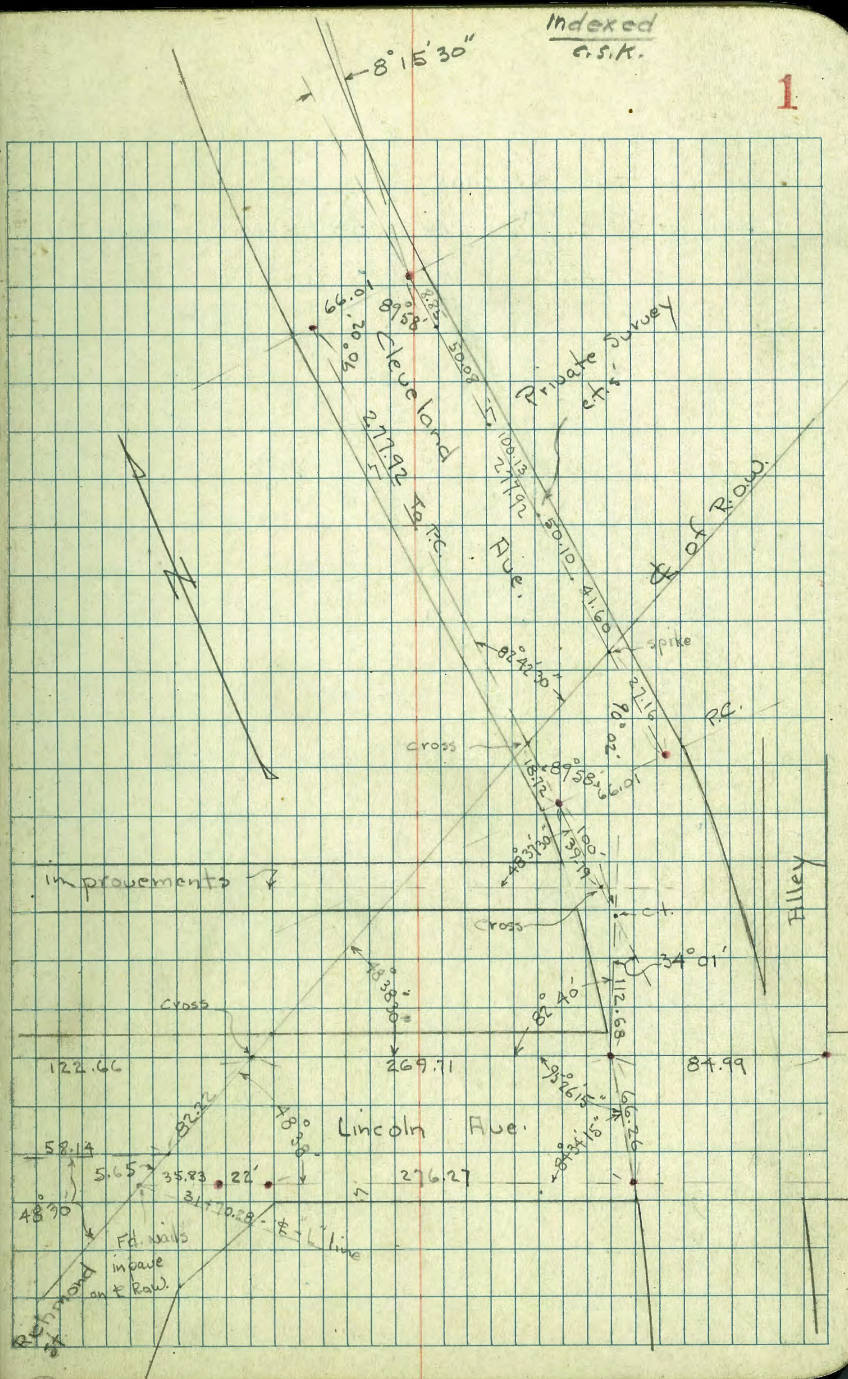
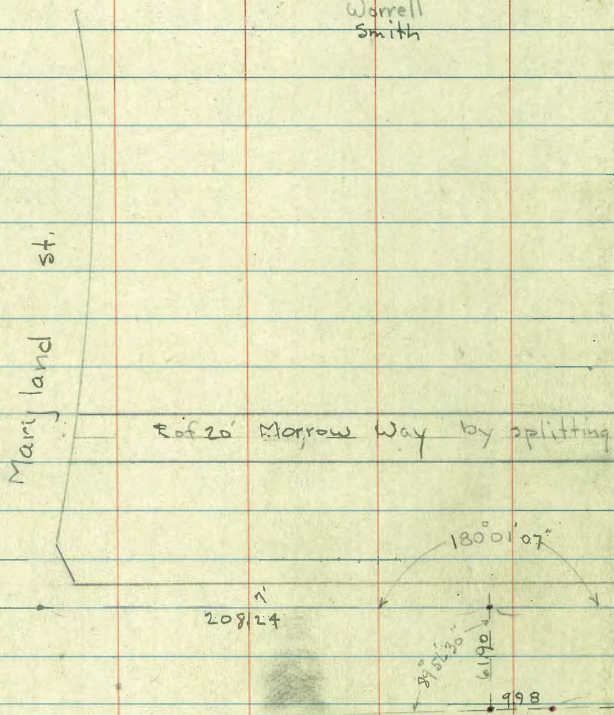
Ld. + c.t. Tie points shown on sheets + some found
 that were not shown - are marked with Red thus:

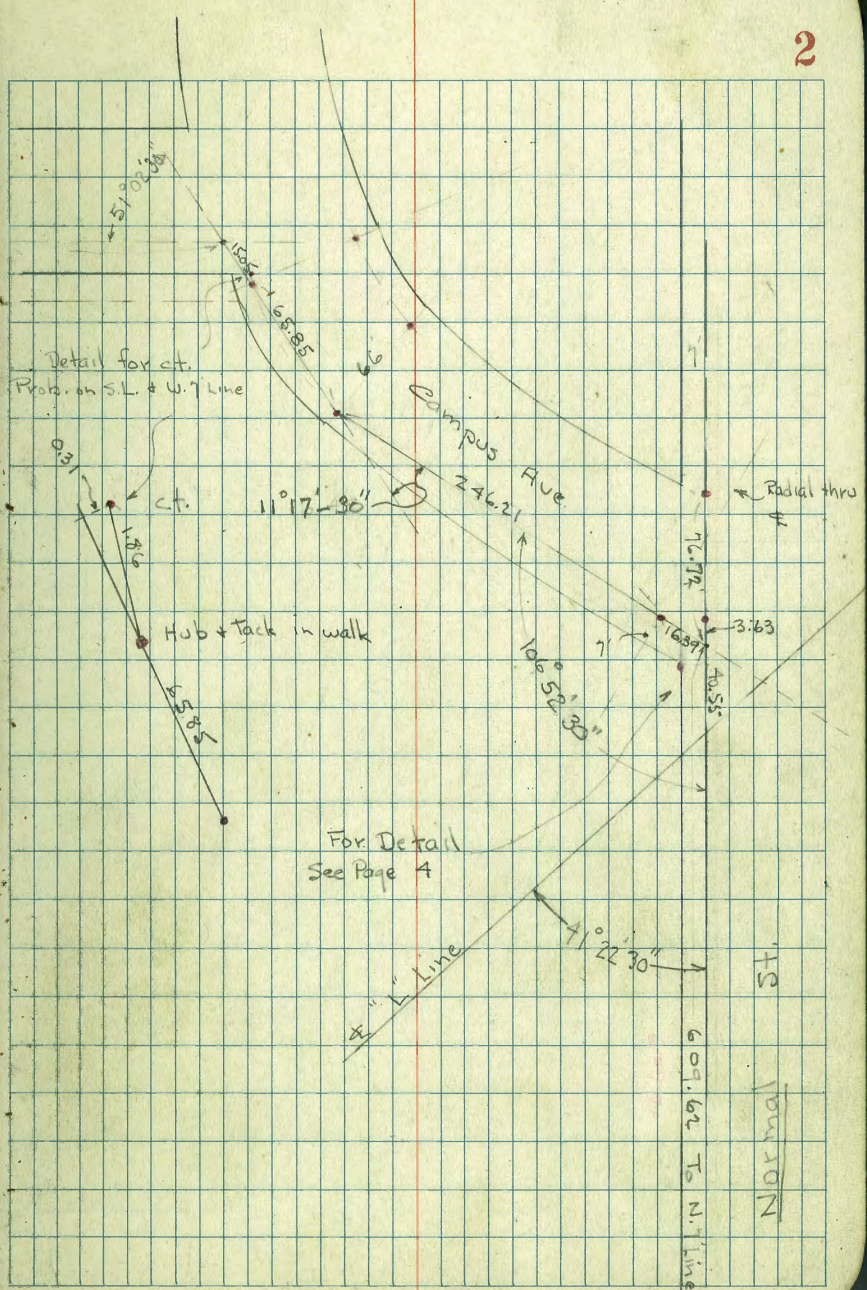
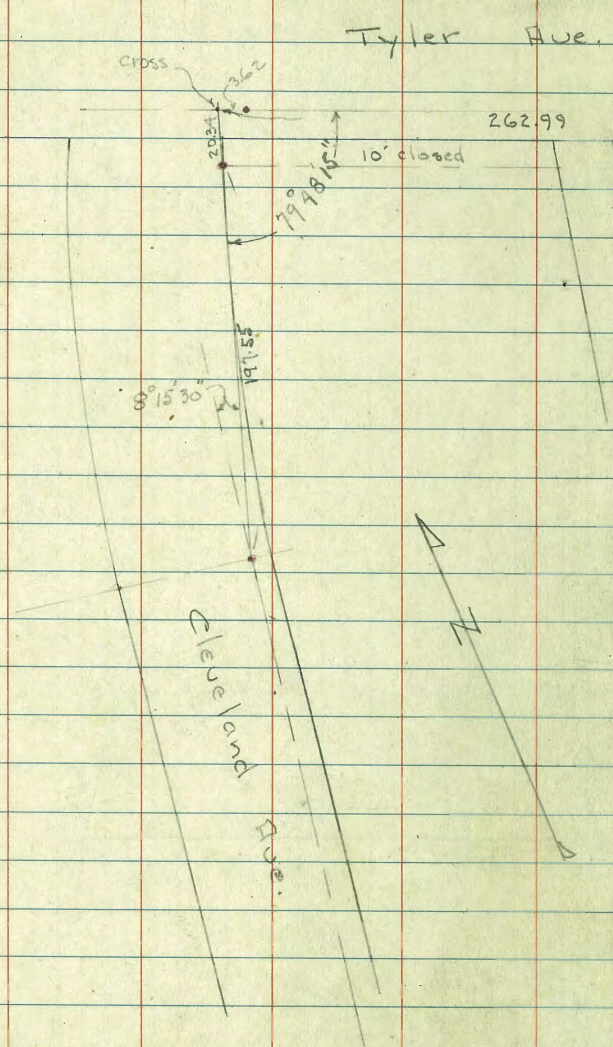
668

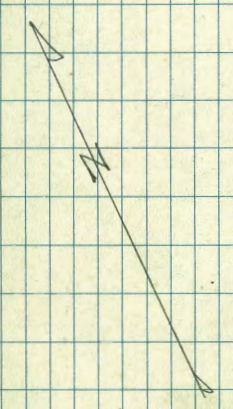
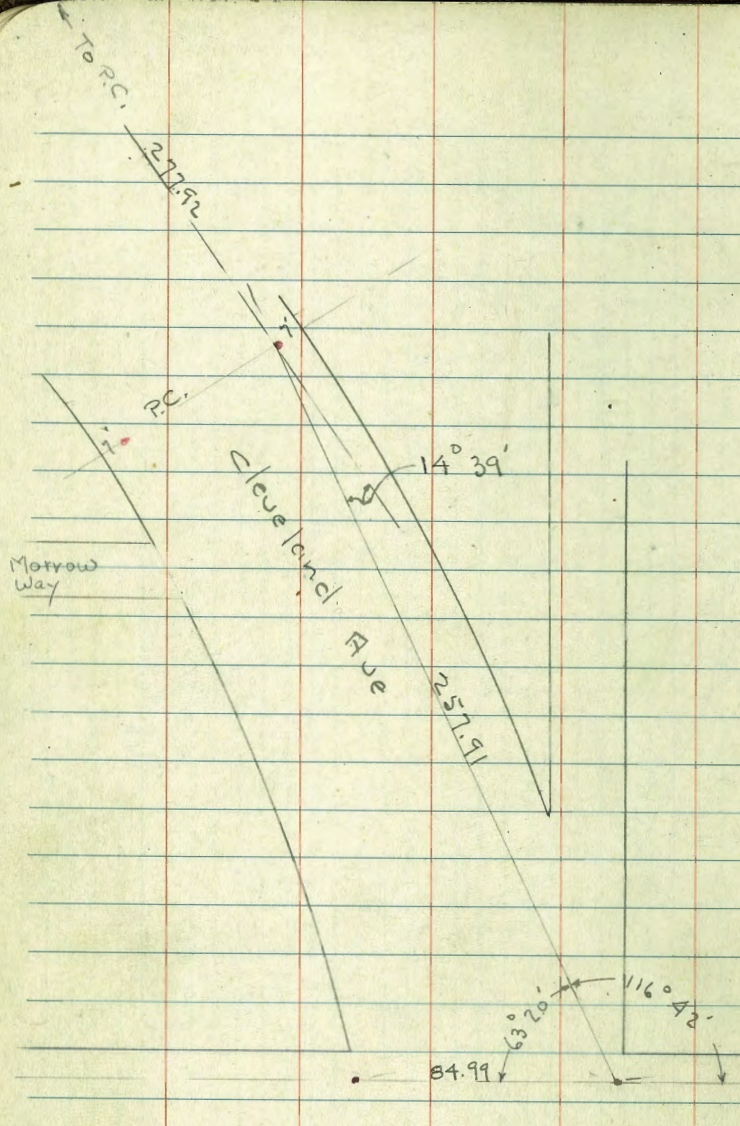
W.O. 233

Dec. - 7 to 9th - 1946

Osborne
 Hardin
 Worrell
 Smith



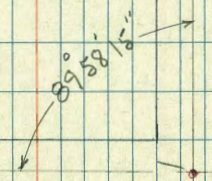




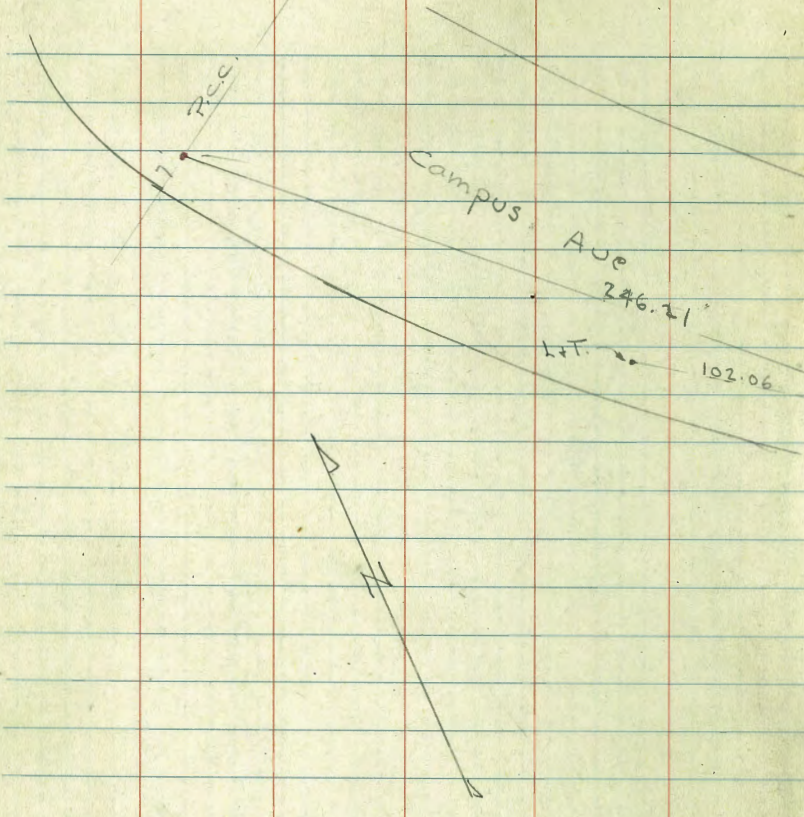
609.47 to Tang. on S. side of Campus

Normal st.

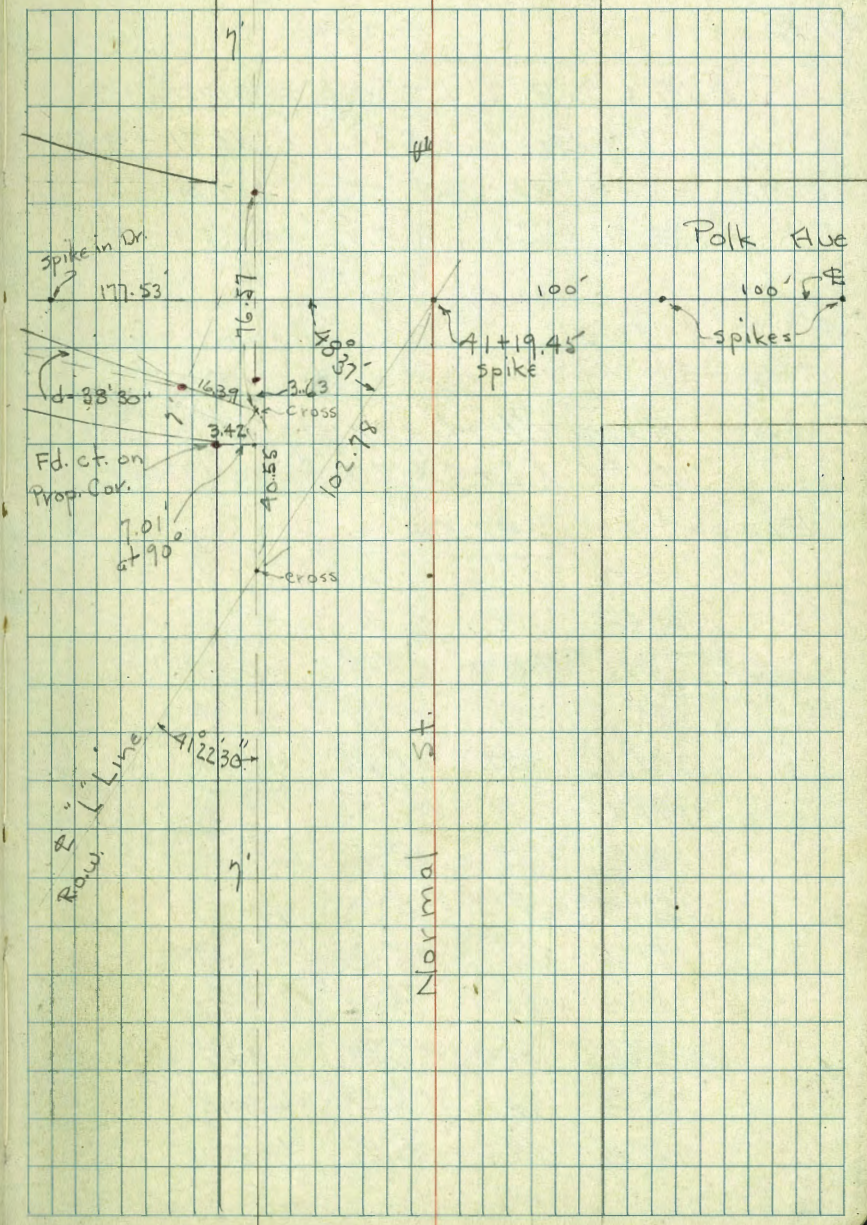
146.69



Lincoln Ave



Found No points on
 line in Block - Used
 Ang. shown at Φ for Dir.
 of this Line \rightarrow



2-7-47
 Sammermeyer
 W Moore
 J Green

Additional Topog

B.M. = S.E. 7' L+T Louisiana +

Adams - See F.B. 1671-46

B.M. 1.18 351.92 - 350.74

T.P. = Δ #1 (see sketch) 9.38 342.54

Δ #1 \leftarrow 5.00 cross hair for stadia
 set on 5.00

From Δ #1 Azimuth bearing $0^{\circ}00'$ on
 L. #1 (2+43 on base line)

Elevation 342.54

azimuth	stadia	vert. L	
161°48'	102	-1°00'	-1.75
166°38'	102	+0°19'	+0.55
185°17'	98	+0°51'	+1.48
194°14'	100	+1°48'	+3.14
193°27'	71	+1°57'	+2.61
176°56'	65	+0°06'	+0.12
158°35'	71	0°00'	—
151°00'	75	-3°25'	-5.96
144°12'	62	-5°25'	-9.44
143°30'	65	-7°39'	-12.31
128°24'	68	-8°25'	-14.64
131°09'	69	-11°00'	-19.08
			-13.20

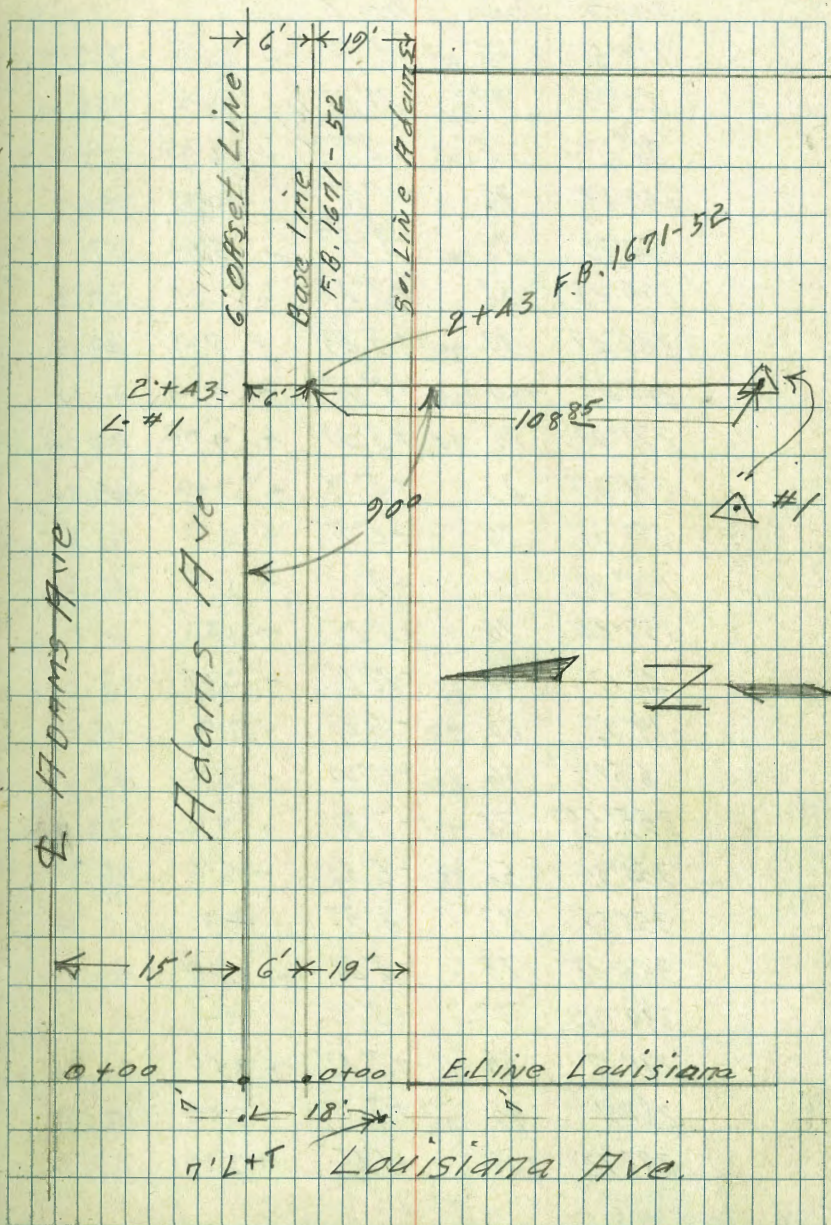
385 50%

Adams + Texas

Melexool
 C.S.K.

Adams South W.O. #237

5

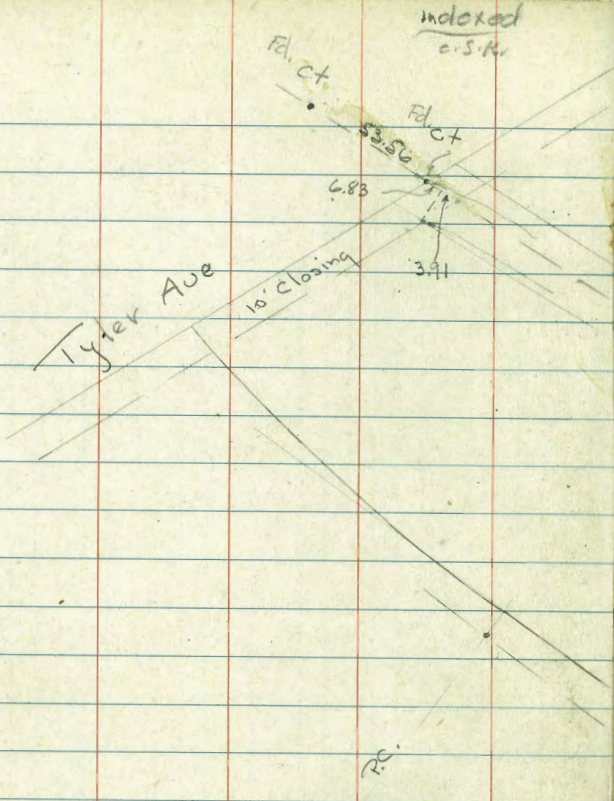


34257

6

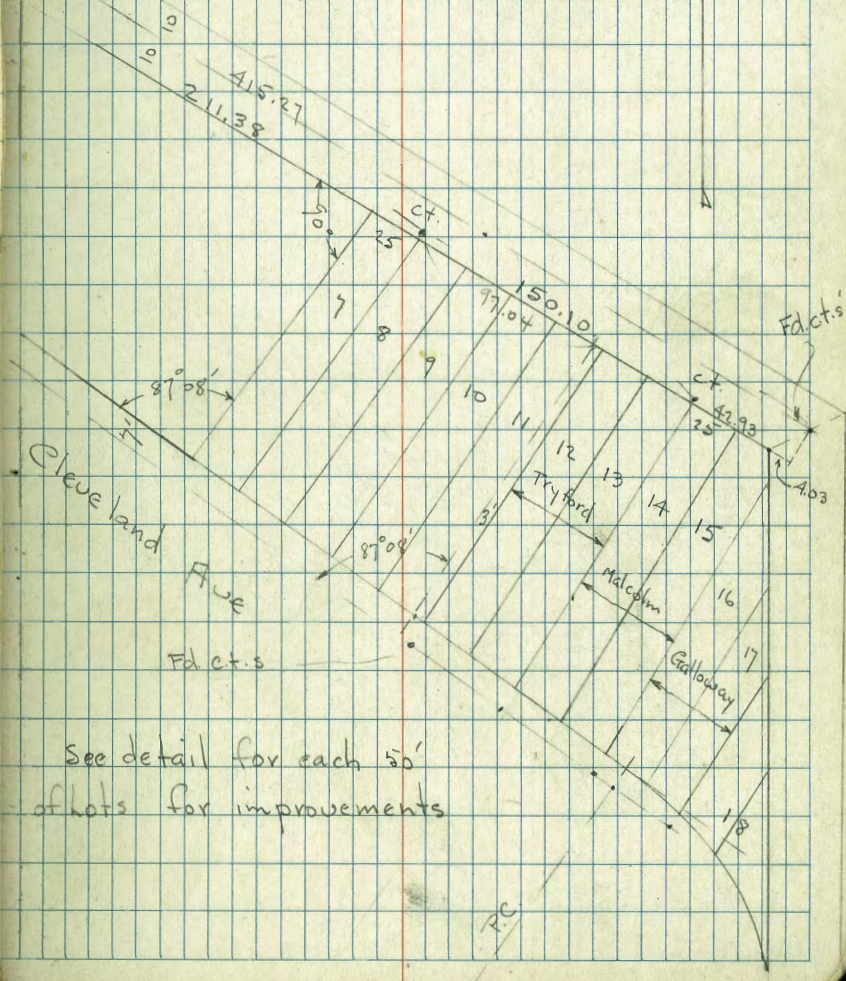
AZIMUTH	STADIA	VERT. L		
113°56'	50 47	-15°50'	- 13.7	329.34
84°09'	37 ₃₂₅	-20°28'	- 12.2	330.34
86°12'	13 ₁₂₈	-12°37'	- 2.75	39.8
150°13'	36	-1°22'	- 0.85	41.7
134°20'	35 ₃₄	-8°57'	- 5.40	37.14
190°45'	34	+3°15'	+ 2.25	44.8
239°47'	80 79	+3°43'	+ 5.27	47.8
211°49'	110 108	+2°07'	+ 4.10	46.64
271°00'	76 75	+3°30'	+ 4.70	47.24
271°00'	43	+4°29'	+ 3.40	45.94
271°00'	20	+2°31'	+ 0.87	43.41
176°29'	21	+3°00'	+ 1.08	43.6
157°34'	20	-4°25'	- 1.33	41.0
46°17'	41 35	-22°11'	- 13.25	29.3
19°02'	63 57	-16°23'	- 17.0	25.54
6°52'	66 64	-12°00'	- 13.5	29
355°58'	74 73	-7°30'	- 9.6	33.
354°35'	56 55	-5°54'	- 5.8	36.74
354°58'	37	-6°37'	- 4.3	38.14
355°48'	23	-3°20'	- 1.34	41.2
339°24'	33	+0°00'	—	
291°07'	65	+2°42'	+ 3.10	46.64
280°51'	95	+3°37'	+ 5.80	48.34
297°12'	109	+1°45'	+ 3.30	45.84

AZIMUTH	STADIA	VERT. L.		
		342.54		
312°25'	76	+1°08'	+1.50	344.04
337°00'	60	-2°35'	-2.7	339.84
308°30'	126	+1°35'	+3.5	346.04
311°48'	138	+2°40'	+6.5	349.04
316°42'	131	+2°04'	+4.75	47.30
317°15'	112	0°00'	—	
310°50'	82	-2°20'	-3.35	39.2
313°45'	100	-4°35'	-8.65	33.9
154°28'	8			12" Power Pole
258°39'	59			1" Pepper Tree
205°18'	78			24" Fan Palm Tree
202°41'	87			" " " Tree
201°15'	97			" " " Tree
184°05'	110			18" Power Pole



Location of Improvements + Prop. Ties in Block 140 - Univ. Hts. 8

Checked actual occupancy of lots. Tax Records Show lots Numbered as shown - But some deeds seem to Differ. 2-28-47 Osborne Hardin Smith Worrell N # 854 W.O. 233



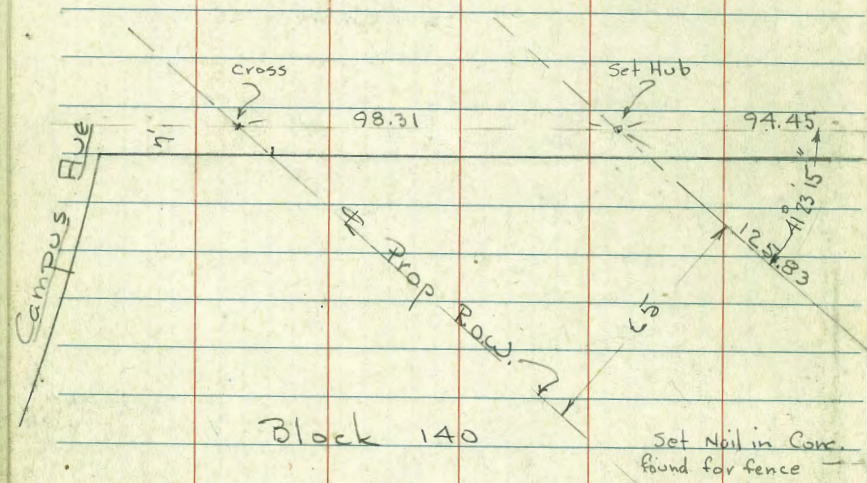
See detail for each 50' of lots for improvements

PC

1186
W.O. 90026

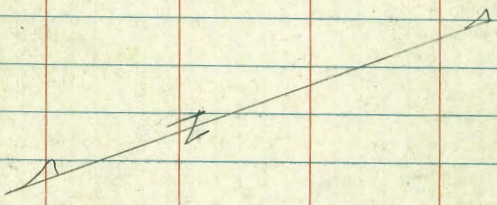
Indexed
OSK

6-13-47
Osborne
Hardin
Smith
Warrell



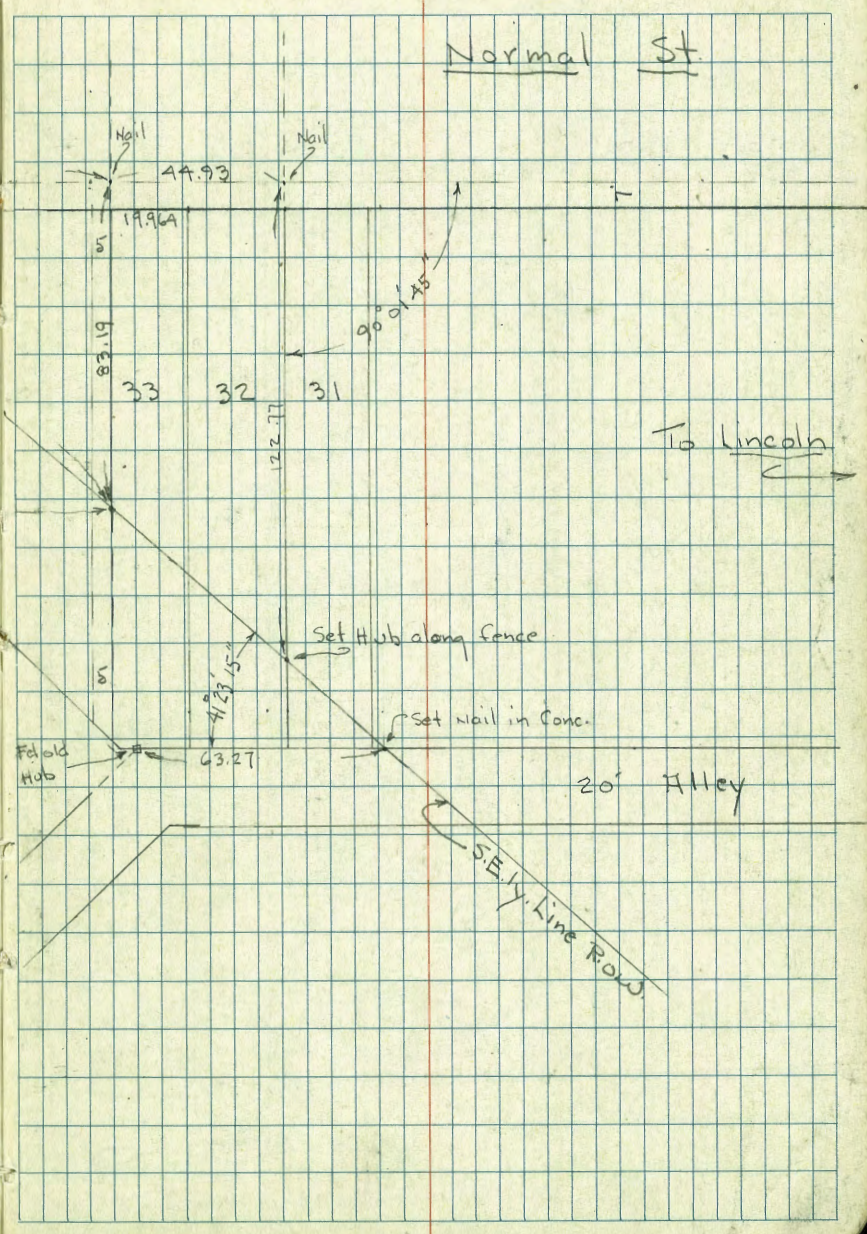
Block 140

Set Nail in Conc.
found for fence



Prop Ties - Along S.E. ly. line of 130' Row.
Block 140 - Lots 30 to 35

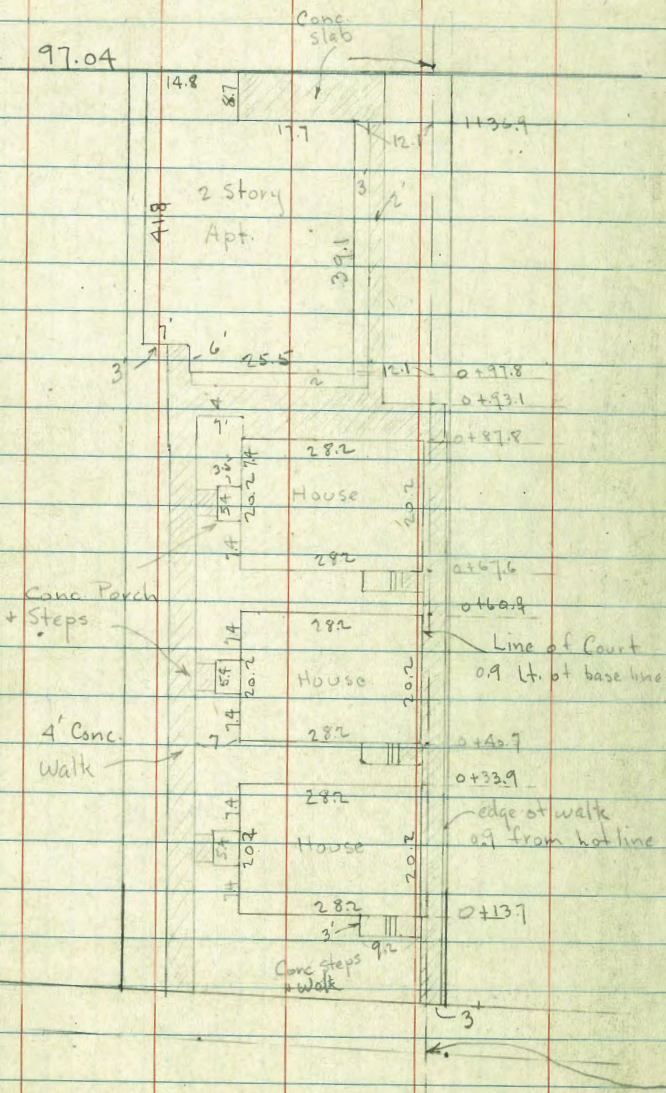
9



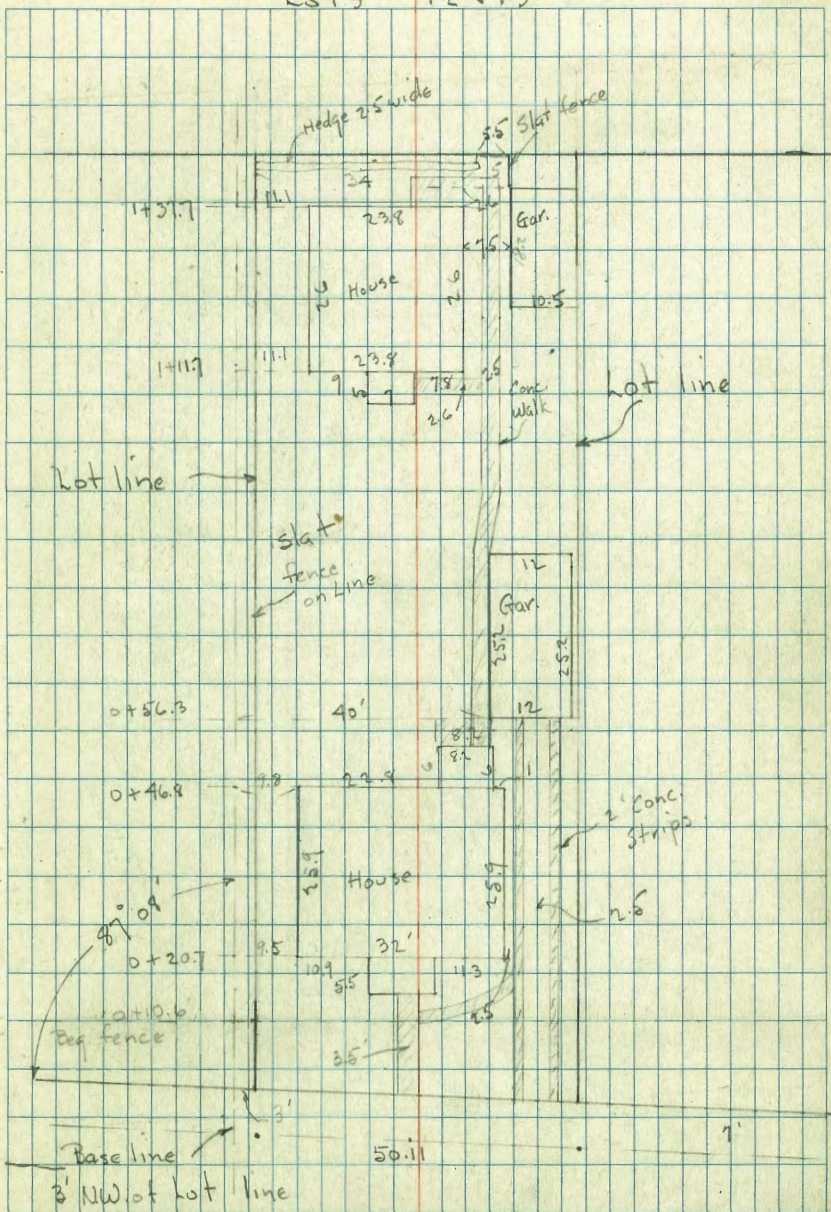
Detail of 50' of lots - scale 1" = 30'

lots 10 + 11

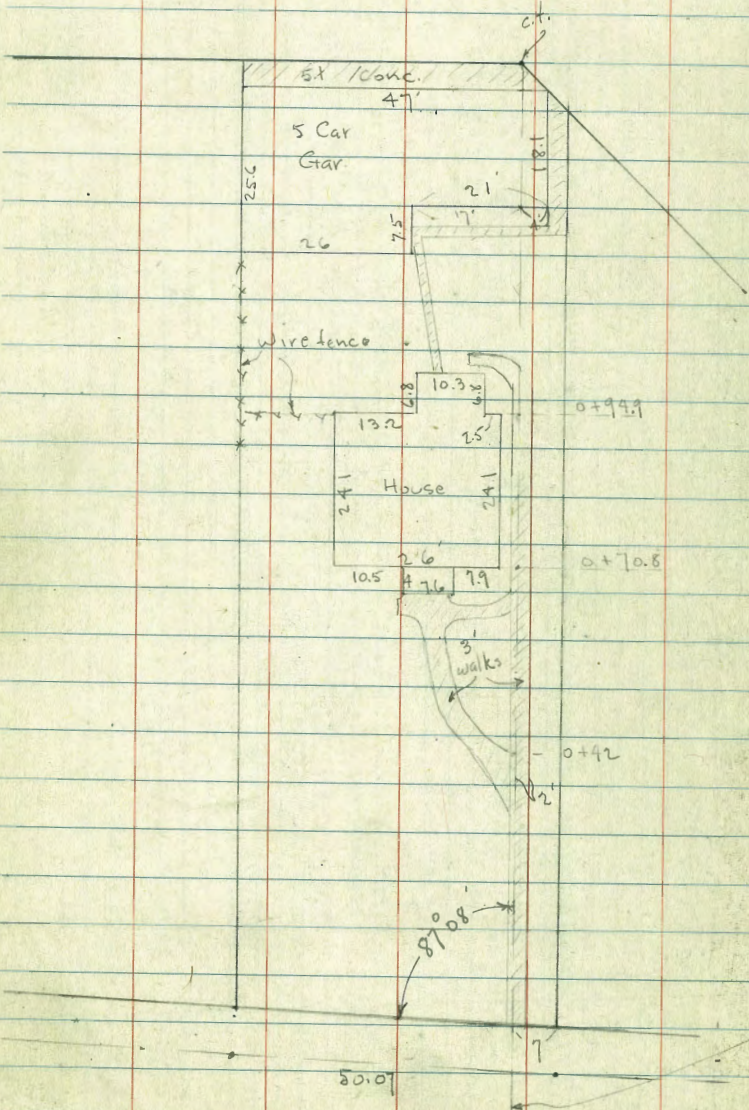
To ct. bet 97.04
lots 7+8



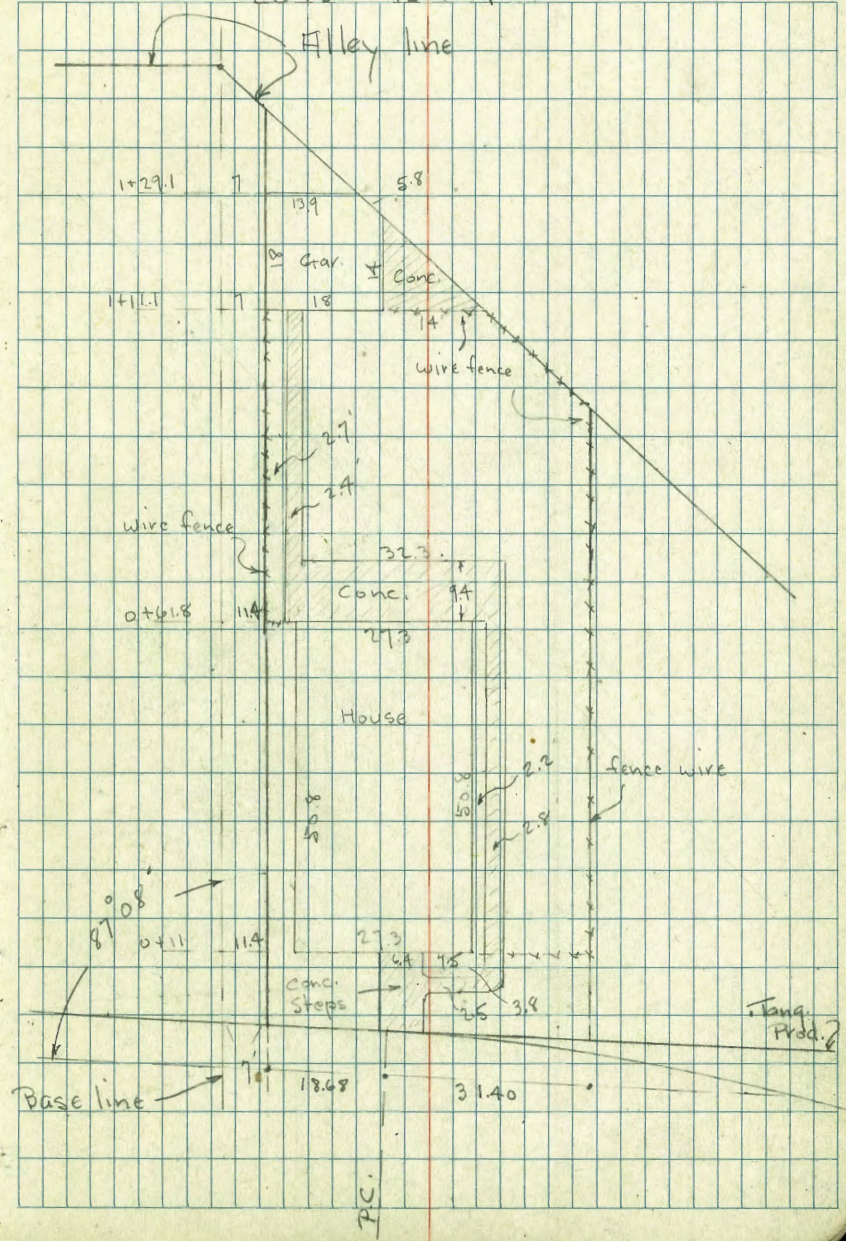
lots 12 + 13



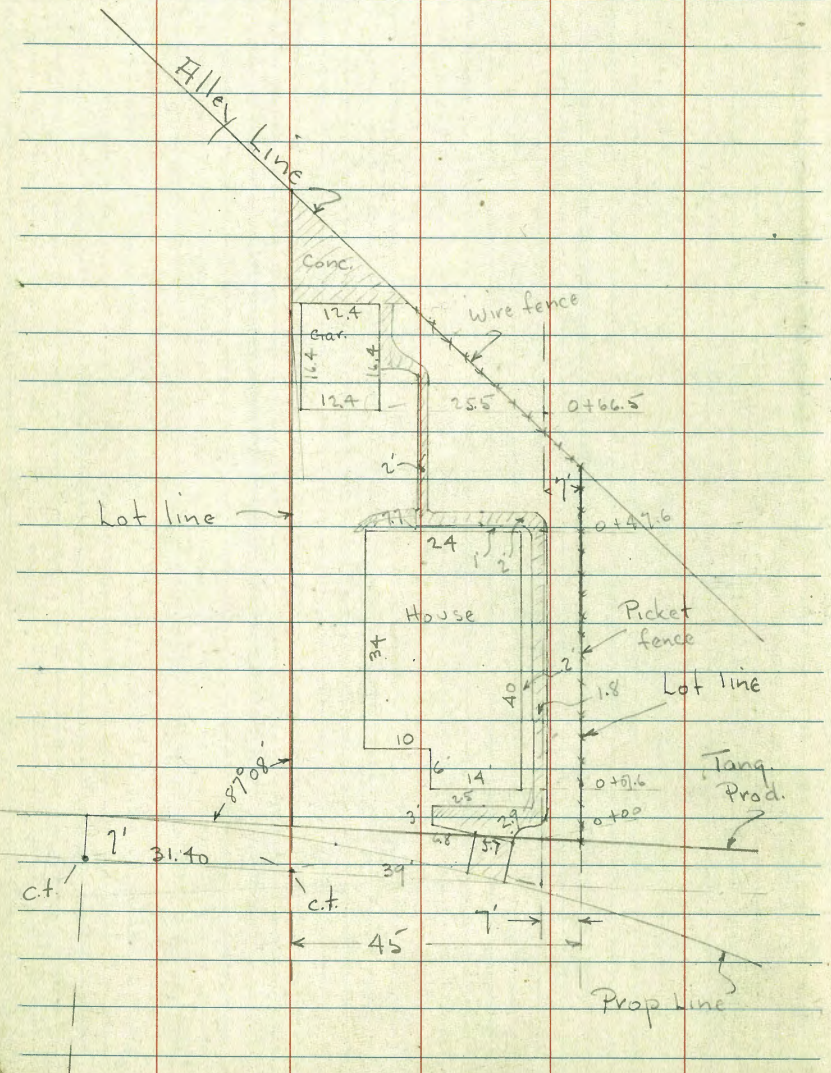
lots 14 + 15



lots 16 + 17



N wly 45° of Lot 18



X-Sect. Clave from S.W. Hugo
to N.W. Ingelow St.

884

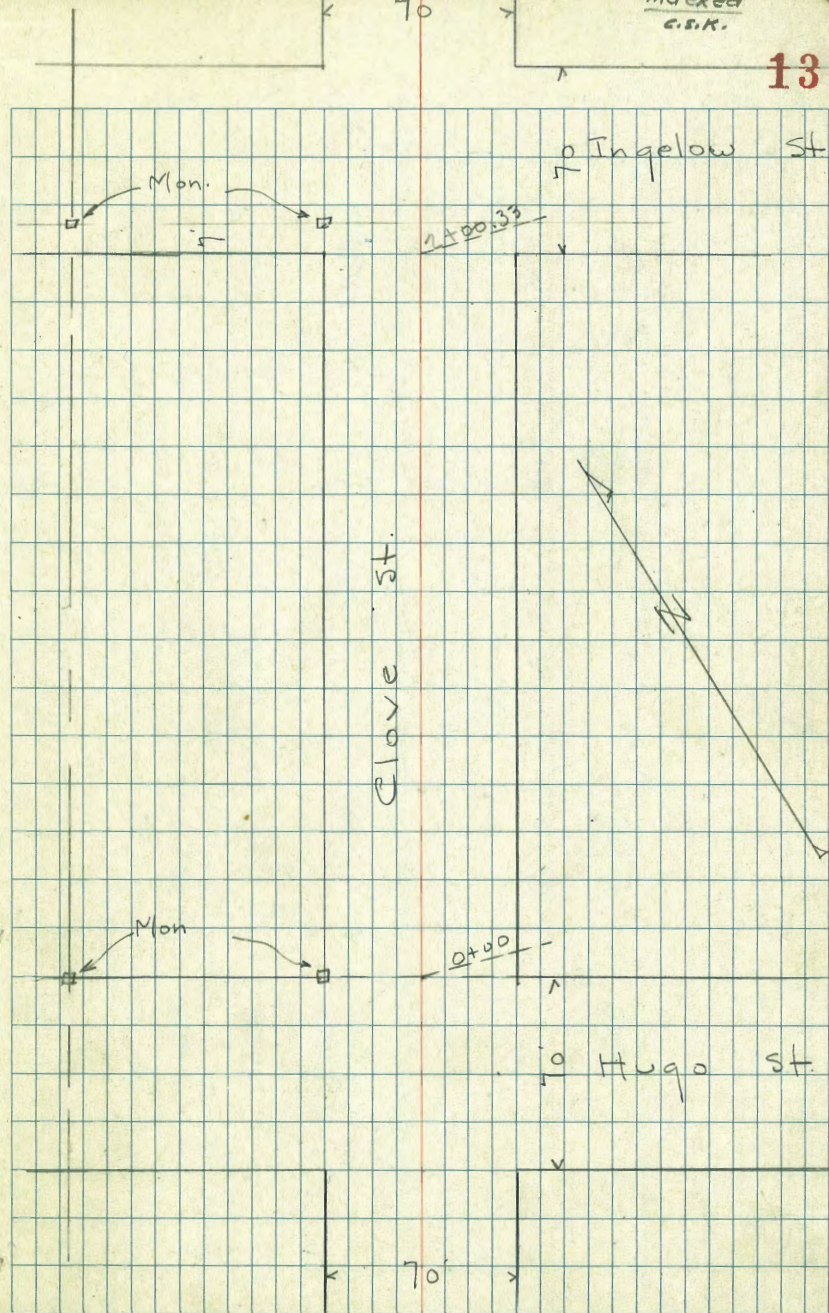
3-20-47

W.O. 230

Osborne
Hardin
Smith
Worrell

Indexed
G.S.K.

13



1+60

1+30

1+00

0+60 - Wash - Not Much drainage area

0+30

0+00 - N.L. Hugo

135.5	130.4	126.0	130.8	134.7	137.3
50	50	60	60	50	50
134.1	129.7	123.0	127.5	132.5	134.4
50	50	35	35	35	35
132.2	127.1	120.8	124.9	129.9	131.5
50	50	50	50	50	50
130.3	125.1	118.6	123.3	127.8	128.8
8.9	14.1	6.6	5.9	11.4	6.4
128.7	122.9	116.6	122.1	125.4	126.9
50	50	50	50	50	50
126.4	120.0	114.3	120.3	123.6	124.1
12.8	19.2	24.9	18.9	15.6	15.1
134.5	117.7	110.7	116.6	121.3	122.1
50	50	60	50	50	50
139.16					

70' N = N.L. Ingebow = end.

52' N = N.cb.

35' N = #

18' N = S.cb.

2+00.33 = S.L. Ingebow

	Lt.		Rt.
2.6	50	136.6	135.7
5.6	35	133.6	133.1
8.5	50	130.7	131.2
10.2	50	129.0	129.1
12.3	50	126.9	127.1
14.1	35	125.1	124.3
15.9	50	123.3	123.0
17.9	50	119.1	122.3
20.1	50	121.0	125.4
22.4	35	123.8	127.4
25.1	50	126.8	129.4
27.7	50	129.9	131.5
30.3	35	131.7	133.7
32.9	50	133.5	135.1
35.5	50	134.9	
38.1	50		
40.7	50		
43.3	50		
45.9	50		
48.5	50		
51.1	50		
53.7	50		
56.3	50		
58.9	50		
61.5	50		
64.1	50		
66.7	50		
69.3	50		
71.9	50		
74.5	50		
77.1	50		
79.7	50		
82.3	50		
84.9	50		
87.5	50		
90.1	50		
92.7	50		
95.3	50		
97.9	50		
100.5	50		
103.1	50		
105.7	50		
108.3	50		
110.9	50		
113.5	50		
116.1	50		
118.7	50		
121.3	50		
123.9	50		
126.5	50		
129.1	50		
131.7	50		
134.3	50		
136.9	50		
139.5	50		
142.1	50		
144.7	50		
147.3	50		
149.9	50		
152.5	50		
155.1	50		
157.7	50		
160.3	50		
162.9	50		
165.5	50		
168.1	50		
170.7	50		
173.3	50		
175.9	50		
178.5	50		
181.1	50		
183.7	50		
186.3	50		
188.9	50		
191.5	50		
194.1	50		
196.7	50		
199.3	50		
201.9	50		
204.5	50		
207.1	50		
209.7	50		
212.3	50		
214.9	50		
217.5	50		
220.1	50		
222.7	50		
225.3	50		
227.9	50		
230.5	50		
233.1	50		
235.7	50		
238.3	50		
240.9	50		
243.5	50		
246.1	50		
248.7	50		
251.3	50		
253.9	50		
256.5	50		
259.1	50		
261.7	50		
264.3	50		
266.9	50		
269.5	50		
272.1	50		
274.7	50		
277.3	50		
279.9	50		
282.5	50		
285.1	50		
287.7	50		
290.3	50		
292.9	50		
295.5	50		
298.1	50		
300.7	50		
303.3	50		
305.9	50		
308.5	50		
311.1	50		
313.7	50		
316.3	50		
318.9	50		
321.5	50		
324.1	50		
326.7	50		
329.3	50		
331.9	50		
334.5	50		
337.1	50		
339.7	50		
342.3	50		
344.9	50		
347.5	50		
350.1	50		
352.7	50		
355.3	50		
357.9	50		
360.5	50		
363.1	50		
365.7	50		
368.3	50		
370.9	50		
373.5	50		
376.1	50		
378.7	50		
381.3	50		
383.9	50		
386.5	50		
389.1	50		
391.7	50		
394.3	50		
396.9	50		
399.5	50		
402.1	50		
404.7	50		
407.3	50		
409.9	50		
412.5	50		
415.1	50		
417.7	50		
420.3	50		
422.9	50		
425.5	50		
428.1	50		
430.7	50		
433.3	50		
435.9	50		
438.5	50		
441.1	50		
443.7	50		
446.3	50		
448.9	50		
451.5	50		
454.1	50		
456.7	50		
459.3	50		
461.9	50		
464.5	50		
467.1	50		
469.7	50		
472.3	50		
474.9	50		
477.5	50		
480.1	50		
482.7	50		
485.3	50		
487.9	50		
490.5	50		
493.1	50		
495.7	50		
498.3	50		
500.9	50		

139.16

Cross Section 47th St. Imperial Ave
to Market St.

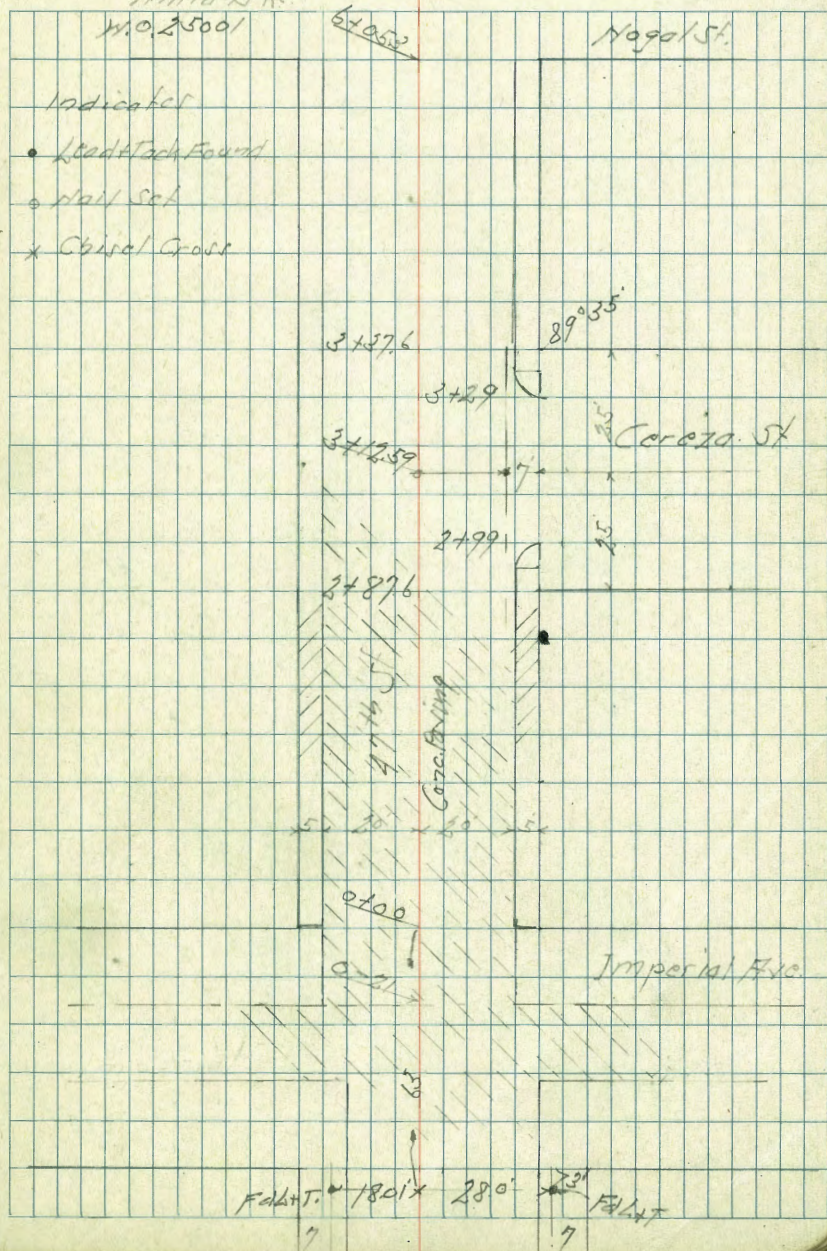
Levels Page 21

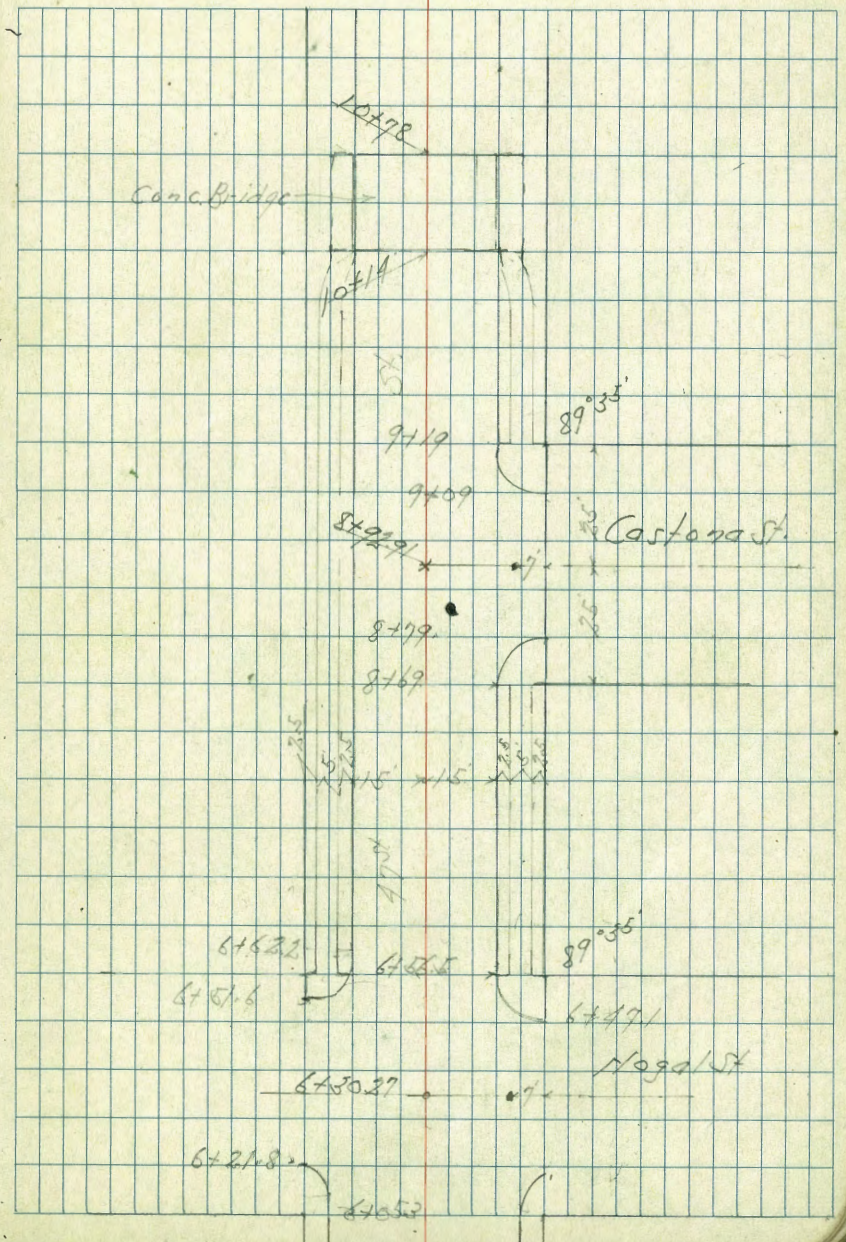
385 50%

June 24-47
Sisson
McCoy X
Filer H.
Millions RC

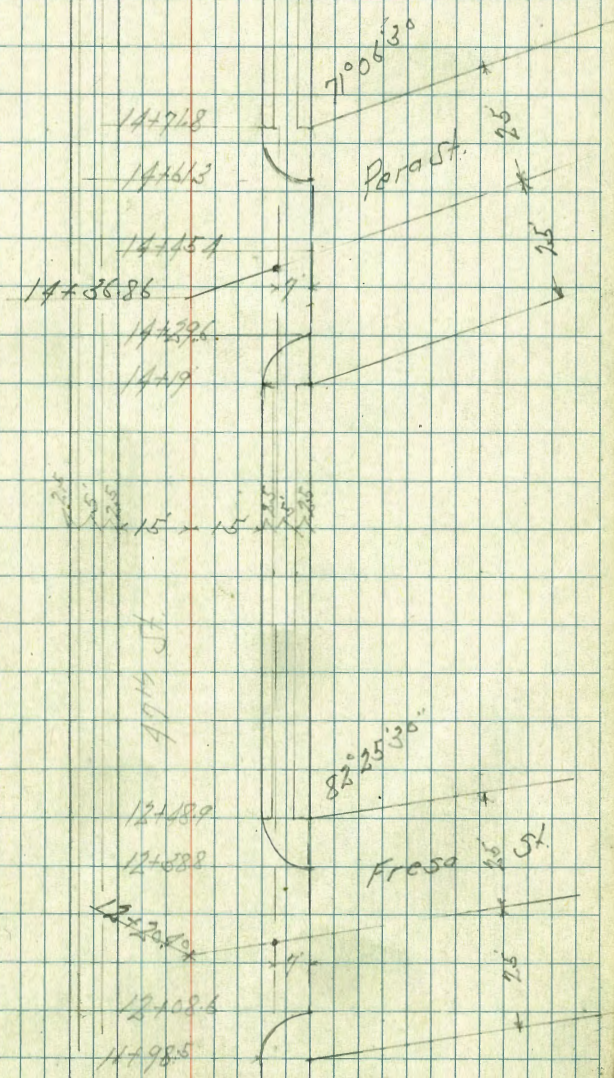
Indexed
c.s.k.

17





47135 St.



Market St

26427.76

26402.95

21801

25180.76



21793.65

Hochst

21751.6



21709.68

21966

15 - 15

Cross Section 47th St.
Imperial Ave. to Market St.
Sketch Page 17

TP 1.33 104.88 12.96 108.55

+50

+10

+50

0+0 - N.L. Imperial

0-21 = North Edge Conc. Pav 129

B.M. 4.34 116.51 112.17

S.E.P.
Imperial
47th St

June 25-1
Sisson T111181
McCoy Rod Lt. W
Allen Tape
Williams Flag

X

Rt. E

21

$\frac{109.92}{11.59}$ 19.9 20.6	$\frac{109.62}{11.87}$ 19.9 20.1 Butler	$\frac{109.23}{11.78}$ 18	$\frac{109.93}{11.58}$	$\frac{109.79}{11.72}$ 10	$\frac{109.93}{12.08}$ 20.1 Butler	$\frac{108.01}{11.50}$ 20.1 20.6
$\frac{107.31}{9.20}$ 19.9	$\frac{106.80}{9.71}$ 19.9	$\frac{107.17}{9.34}$ 10	$\frac{107.27}{9.24}$	$\frac{107.11}{9.46}$ 10	$\frac{106.79}{9.72}$ 20.1	$\frac{107.90}{9.11}$ 20.1
$\frac{109.70}{6.81}$ 19.9	$\frac{109.12}{7.02}$ 19.9	$\frac{109.50}{7.01}$ 10	$\frac{109.67}{6.84}$	$\frac{109.20}{6.92}$ 10	$\frac{109.85}{7.06}$ 20.2	$\frac{109.95}{6.56}$ 20.3
$\frac{111.92}{4.53}$ 19.9 20.3	$\frac{111.32}{5.12}$ 19.8 20.4	$\frac{111.68}{4.88}$ 10	$\frac{111.85}{4.66}$	$\frac{111.86}{4.65}$ 10	$\frac{111.96}{4.55}$ 20 = Butler	$\frac{111.15}{4.51}$ 20 = 60' End 110' line
$\frac{109.94}{7.07}$ 7.5	$\frac{111.06}{5.45}$ 2.5	$\frac{111.29}{5.22}$ 20 = Wilson's 10' line	$\frac{111.84}{4.67}$	$\frac{112.57}{3.94}$ 20 = Wilson's 10' line	$\frac{112.76}{3.75}$ 2.5	$\frac{114.04}{2.41}$ 3.5
						116.51

385 50%

3+29 = 4 Cb line to East

3+12.59 = 2 Carcast

+99

+876 = S. Carcast to East

+50

2+0

10488

97.10 7.68 19.9 19.9+DIVE	97.10 7.78 19.9 19.9	97.29 7.59 10 10	97.39 7.49 10 10	97.27 7.61 10 10	97.00 7.88 20 20	96.94 7.94 25.1 25.1	97.50 7.38 25.1 25.1
97.92 6.96 19.9 19.9	97.54 7.84 19.9 19.9	97.75 7.63 10 10	97.88 7.00 10 10	97.73 7.15 10 10	97.98 7.40 20.2 20.2	97.50 7.38 24.9 24.9	
98.22 6.66 19.8 19.8	97.93 6.95 19.8 19.8	98.13 6.75 10 10	98.30 6.58 10 10	98.16 6.73 10 10	97.84 7.04 20.2 20.2	97.89 6.99 25.1 25.1	98.98 6.40 25.1 25.1
98.52 6.31 19.8 19.8	98.24 6.61 19.8 19.8	98.50 6.38 10 10	98.65 6.23 10 10	98.84 6.43 10 10	98.22 6.66 20.2 20.2	98.68 6.50 20.2 20.2	
100.73 4.65 19.8 19.8	99.77 5.11 19.8 19.8	100.10 4.78 10 10	100.38 4.50 10 10	100.05 4.83 10 10	99.63 5.25 20.2 20.2	100.26 4.65 20.2 20.2	
102.63 3.25 19.8 19.8	102.10 2.78 19.8 19.8	102.00 2.48 10 10	102.55 2.53 10 10	102.92 2.46 10 10	102.04 2.81 20.2 20.2	102.62 2.36 20.2 20.2	

10488

4735A

TP 0.74 80.05 12.97 79.31

+50

+50

+50

TP 0.08 92.28 12.68 92.20

+10

+50

37376 = N.A. Carcra

10488

L

S

R

23

80.31	79.75	80.14	80.38	80.10	79.69	80.20
11.97	12.53	13.14	11.90	13.18	12.59	13.08
20.00	20.00	10		20	20.00	20.00

84.25	83.84	84.12	84.38	84.10	83.77	84.22
8.03	8.44	8.11	7.90	8.09	8.56	8.05
20	20	10		20	20.1	20.1

88.28	87.76	88.20	88.37	88.21	87.88	88.93
4.00	4.52	4.08	3.91	4.07	4.10	3.85
20	20	10		20	20.1	20.1

92.28

92.01	91.83	92.22	92.37	92.28	92.05	92.66
12.87	12.99	12.66	13.56	12.60	13.82	12.22
19.80	19.8	10		10	20.1	20.1

96.74	96.83	96.17	96.23	96.70	96.08	96.61
8.53	9.05	8.71	8.55	8.58	8.80	8.37
19.9	19.9	10		20	20.1	20.1

97.27	96.71	96.98	97.07	97.03	96.90	97.95
7.59	8.17	7.90	7.81	7.85	7.99	7.48
19.9	19.9	10		10	20.0	20.0

10488

+516 = NCB on Lt.

+471 = NCB on Pt.

B.M.

470

75.35

64721090
57647160
7537

+3027 = $\frac{1}{2}$ Nagal St.

+248 = SCB on Lt.

+153 = CB Fzd on Pt.

64053 = CB BC on Pt.

80.05

Lt.

Pt.

Pt.

24

75.52

4.53
247

75.94

5.11
247

75.11

4.91
15

75.32

178

Gather

75.39

166

75.28

477
10

75.15

490
15

75.18

487
15

75.03

483
15

Gather

75.22

4.23
15

75.20

4.25
20

75.02

4.53
10

75.51

4.54

75.44

4.61
10

75.39

4.66
20

75.55

4.56
24.5

Gather

75.62

4.41
15

75.18

4.87
25

75.28

4.77
10

75.50

4.55
10

75.52

4.53

SCB

Gather

75.01

4.44

75.38

4.97
10

75.15

4.60
20

75.15

4.60
24.6

75.73

4.38
24.6

Gather

76.03

4.02
20

75.75

4.30
20

76.00

4.05
10

76.04

4.01

75.93

4.13
10

75.61

4.44
19.9

75.94

4.11
19.9

CB

Gather

Gather

80.05

47th St.

Lt.

S

Pt

25

750

$$\begin{array}{r} 74.90 \\ 5.06 \\ 15.2 = Cb \end{array}$$

$$\begin{array}{r} 74.80 \\ 5.45 \\ 15.2 = Gutter \end{array}$$

$$\begin{array}{r} 74.75 \\ 5.30 \end{array}$$

$$\begin{array}{r} 74.35 \\ 5.70 \\ 14.8 = Gutter \end{array}$$

$$\begin{array}{r} 74.90 \\ 5.09 \\ 14.8 = Cb \end{array}$$

870

$$\begin{array}{r} 75.13 \\ 4.99 \\ 15.2 \end{array}$$

$$\begin{array}{r} 74.60 \\ 5.26 \\ 15.2 \end{array}$$

$$\begin{array}{r} 74.91 \\ 5.44 \end{array}$$

$$\begin{array}{r} 74.58 \\ 5.47 \\ 14.8 \end{array}$$

$$\begin{array}{r} 75.12 \\ 4.90 \\ 14.8 \end{array}$$

750

$$\begin{array}{r} 75.07 \\ 4.98 \\ 15.2 \end{array}$$

$$\begin{array}{r} 74.71 \\ 5.28 \\ 15.2 \end{array}$$

$$\begin{array}{r} 75.04 \\ 5.01 \end{array}$$

$$\begin{array}{r} 74.71 \\ 5.34 \\ 14.8 \end{array}$$

$$\begin{array}{r} 75.20 \\ 4.85 \\ 14.8 \end{array}$$

770

$$\begin{array}{r} 75.24 \\ 4.71 \\ 15 \end{array}$$

$$\begin{array}{r} 74.92 \\ 5.13 \\ 15 \end{array}$$

$$\begin{array}{r} 75.21 \\ 4.84 \end{array}$$

$$\begin{array}{r} 74.80 \\ 5.16 \\ 14.9 \end{array}$$

$$\begin{array}{r} 75.24 \\ 4.81 \\ 14.9 \end{array}$$

64622 = Cb F.C. of Lt.

$$\begin{array}{r} 75.55 \\ 4.50 \\ 15 = Cb \end{array}$$

$$\begin{array}{r} 74.98 \\ 5.07 \\ 15 = Gutter \end{array}$$

$$\begin{array}{r} 75.28 \\ 4.77 \end{array}$$

$$\begin{array}{r} 75.01 \\ 5.04 \\ 15 \end{array}$$

$$\begin{array}{r} 75.99 \\ 4.56 \\ 15 \end{array}$$

64565 = Cb F.C. of Pt

$$\begin{array}{r} 75.70 \\ 4.75 \end{array}$$

$$\begin{array}{r} 75.03 \\ 5.07 \\ 15 = Gutter \end{array}$$

$$\begin{array}{r} 75.49 \\ 4.56 \\ 15 = Cb \end{array}$$

80.05

80.05

750

9719 = Cb F.C. on Pt.

9709 = 11 Cb Line on Pt.

879291 = 2 Castoro St. to East

779 = 5 Cb Castoro St on Pt.

8769 = Cb Bk. on Pt.

80.05

Lt.

S

Rt

26

7522 483 152-Cb	7488 517 152-Gutter	7505 500	7470 533 148-Gutter	7519 486 148-Cb
7402 503 152	7478 527 152	7490 515	7474 511 15	7514 491 15
		7480 525	7460 545 15	7491 564 25-Gutter
				7514 491 25-Cb
	7415 539 150-Gutter	7470 532	7463 542 15	7459 541 24.3-E.Por.
		7451 554	7438 567 15	7411 594 25-Gutter
				7488 517 25-Cb
	7404 511 151-Cb	7460 545 151-Gut.	7455 550	7436 519 14.9-Gutter
				7496 509 14.9-Cb
		80.05		

47^{1/2} St.

+50

11+0

+78 = 11/4 Conc Bridge

+50

+11 = 5/4 Conc Bridge

TP 5.45 81.09 4.41 75.64

10+0

80.05

Lt.

Z

Rt.

27

75.18

5.91

15.3

= Conc

74.60

6.19

15.3

= Gutter

74.20

6.19

74.58

6.51

14.7

= Gutter

75.06

6.03

14.7

= Conc

75.47

5.62

15.2

74.85

6.21

15.2

75.06

6.05

74.85

6.21

14.8

75.29

5.80

14.8

74.60

5.48

15.2

75.02

6.07

15.2

75.10

5.99

74.94

6.15

14.8

75.54

5.55

14.8

75.50

5.53

15.3

74.84

6.13

15.3

75.17

5.92

74.89

6.30

14.7

75.49

5.50

14.7

75.64

5.45

15.6

75.04

6.05

15.2

75.24

5.83

74.95

6.14

14.7

75.56

5.53

14.7

81.09

74.92

6.3

15.5

= Conc

75.00

5.05

15.5

= Gutter

75.22

7.83

74.90

5.15

14.8

= Gutter

75.37

4.68

14.8

= G

80.05

TP 976 90.48 0.37 80.72

1310

12+189 = N.L. Fresa St to East

12+388 = N.C6

12+237 = S. Fresa St to East

12+086 = South C6

11+98.5 = S.L. Fresa to East

81.09

Lt

+

Rt

28

77.77

3.32
15.5 = C6

77.29

3.80
16.5 = gutter

77.66

3.43

77.37

3.32
14.0 = gutter

77.89

3.20
14.6 = C6

75.60

5.49
15.4

75.03

6.06
15.4

75.35

5.74

75.12

5.97
14.6 = gutter

75.54

5.53
14.6 = C6

75.06

6.03

75.01

6.08
14.7

75.07

6.09
24.7 = gutter

75.61

5.48
24.7 = C6

75.21

5.78
15.3

74.89

6.60
15.3

74.72

6.32

74.04

6.25
14.7

75.00

6.09
24.5 = gutter

74.93

6.51

74.58

6.51
14.7

74.70

6.39
24.7 = gutter

75.18

5.91
24.7 = C6

75.11

5.98
15.3 = curb

74.10

6.09
15.3 = gutter

74.37

6.72

74.89

6.60
14.7 = gutter

75.07

6.03
14.7 = C6

81.09

47+3 St.

+613 = H Carb 07 Pt.

14+45A = L Para St. 07 Pt.

+296 = S Carb Para 07 Pt.

+19 = S.L. Para St 07 Pt.

14+0

13+50

90.48

L.W

S

Pt. 2E

29

83.83

6.65

83.59

6.89

83.81

6.67

84.90

6.88

248.50

50.1

248.00

83.97

6.51

15.4

= Carb

83.94

7.04

15.4

= Gutter

83.66

6.82

83.37

7.11

14.5

83.58

6.90

245.11

10.0

83.93

7.05

83.11

7.37

14.5

83.02

7.46

245.50

5.0

83.48

7.00

245.00

5.0

82.57

6.95

15.5

82.94

7.54

15.5

82.70

7.22

82.91

7.57

14.5

83.90

7.08

14.5

82.19

8.39

15.17

= D.P.H.

82.97

8.01

82.09

8.39

4.5

82.60

7.88

14.7

80.93

10.45

15.50

79.57

10.81

15.50

= Gutter

79.97

10.51

79.74

10.74

14.7

= Gutter

80.13

10.35

14.7

= Carb

90.43

Notes Reduced
East 6-30-17

17+0

<u>87.57</u>	<u>86.94</u>	<u>87.31</u>	<u>87.12</u>	<u>87.63</u>
291 151 56	351 151 56	317	336 147 50	285 147 50

150

<u>86.83</u>	<u>86.38</u>	<u>86.59</u>	<u>86.31</u>	<u>86.83</u>
365 152	310 152	389	417 148	365 148

16+0

<u>86.70</u>	<u>85.70</u>	<u>85.84</u>	<u>85.62</u>	<u>86.16</u>
128 153	128 153	264	486 148	133 148

150

<u>85.52</u>	<u>84.85</u>	<u>85.24</u>	<u>85.13</u>	<u>85.55</u>
496 153	553 153	527	555 148	493 148

15+0

<u>84.68</u>	<u>84.12</u>	<u>84.43</u>	<u>84.23</u>	<u>84.72</u>
580 153	636 153	505	525 147	576 147

B.M

6.09

84.39

NF BP
Perot + 474

14+718 - 112 Perot + 07 Rt

90.48

<u>88.33</u>	<u>88.78</u>	<u>89.01</u>	<u>88.83</u>	<u>89.32</u>
616 153 56	670 153 56	647	665 147 50	611 147 50

90.48

Notes
CAS 6.30.17

47th St.

20+0

+50

TP 12.00 113.46 0.31 101.46

19+0

+50

18+0

TP 12.10 101.77 0.81 89.67

17+50

90.48

Lt

2

Rt.

31

<u>107.45</u>	<u>106.89</u>	<u>107.71</u>	<u>106.87</u>	<u>107.45</u>
6.01 15.1-Curb	6.57 15.1-Gutter	6.26	6.59 14.9-Gutter	6.91 14.9-Curb

<u>103.22</u>	<u>102.70</u>	<u>103.00</u>	<u>102.63</u>	<u>103.18</u>
10.81 15.1	10.76 15.1	10.46	10.83 14.9	10.38 14.9
		113.46		

<u>96.99</u>	<u>98.93</u>	<u>98.72</u>	<u>98.44</u>	<u>98.99</u>
2.78 15.1	3.34 15.1	2.25	2.33 14.9	2.78 14.9

<u>94.82</u>	<u>94.70</u>	<u>94.60</u>	<u>94.25</u>	<u>94.80</u>
6.96 15.2	7.07 15.2	7.17	7.52 14.8	6.77 14.8

<u>91.34</u>	<u>90.81</u>	<u>91.05</u>	<u>90.62</u>	<u>91.22</u>
10.43 15.2	10.96 15.2	10.72	11.08 14.8	10.55 14.8
		101.77		

<u>89.00</u>	<u>88.45</u>	<u>88.71</u>	<u>88.43</u>	<u>88.38</u>
1.48 15.2-Curb	2.03 15.2-Gutter	1.77	2.05 14.8-Gutter	1.59 14.8-Curb
		90.48		

22+25

21+93.65 = Prop. C & BC 07/11

21+51.6 = $\frac{1}{2}$ Hartloyst to west

21+09.60 = Prop. C & BC 07/11

21+0

TP 11.21 124.17 0.50 112.96

20+50

113.46

Lt

Z

Rt

32

<u>119.74</u>	<u>118.19</u>	<u>118.52</u>	<u>118.19</u>	<u>118.69</u>
5.43	5.98	5.65	5.98	5.48
15	15	15	15	15
Carb	Sulfur		Sulfur	Carb

<u>117.90</u>	<u>117.32</u>	<u>117.60</u>	<u>117.90</u>	<u>117.95</u>
5.77	6.80	6.98	6.77	6.23
15	15	15	15	15

<u>116.40</u>	<u>115.86</u>	<u>116.18</u>	<u>115.86</u>	<u>116.37</u>
7.77	8.81	7.99	8.31	7.80
15	15	15	15	15

<u>114.51</u>	<u>113.93</u>	<u>114.31</u>	<u>113.98</u>	<u>114.49</u>
9.66	10.25	9.88	10.19	9.68
15	15	15	15	15

<u>114.02</u>	<u>113.92</u>	<u>113.83</u>	<u>113.51</u>	<u>113.98</u>
10.25	10.25	10.31	10.66	10.19
15	15	15	15	15

124.17

<u>111.11</u>	<u>110.55</u>	<u>110.85</u>	<u>110.59</u>	<u>111.13</u>
7.34	7.91	7.61	7.87	7.33
15	15	15	15	15
Carb	Sulfur		Sulfur	

113.46

47135A

2510
 TP 5.49 12599 367 120.50

+50

2110

+50

2310 = 114 Goldbox Patch

22150

12417

385 50%

Lt.

R

Rt.

33

<u>120.82</u> 5.15 15 = Gold	<u>120.32</u> 5.67 15 = Gold	<u>120.50</u> 5.19 12599	<u>120.14</u> 5.85 15 = Gold	<u>120.62</u> 5.37 15 = Gold
<u>120.97</u> 3.20 15	<u>119.92</u> 4.35 15	<u>120.23</u> 3.94	<u>119.97</u> 4.30 15	<u>120.98</u> 3.69 15
<u>120.02</u> 4.15 15	<u>119.44</u> 4.23 15	<u>119.82</u> 4.35	<u>119.63</u> 4.54 15	<u>120.12</u> 4.05 15
<u>119.74</u> 4.43 15	<u>119.19</u> 4.98 15	<u>119.55</u> 4.62	<u>119.37</u> 4.80 15	<u>119.81</u> 4.36 15
<u>119.95</u> 4.78 15.1	<u>119.04</u> 5.73 15.1	<u>119.29</u> 4.88	<u>119.21</u> 4.96 15	<u>119.53</u> 4.64 15
<u>119.17</u> 5.40 15 = Gold	<u>118.25</u> 5.42 15 = Gold	<u>119.02</u> 5.15 12417	<u>118.67</u> 5.58 15 = Gold	<u>119.14</u> 5.93 15 = Gold

Cont next page

BM

4.82 12.17

267
Market St
1775 St
12096

26+2776 = 1/2 Market St to West

26+12 = South Carb Line to East

26+0976 = South Carb Line to West

26+02 = C6 RC on Rt

25+8796 = 1/2 Market St to West = C6 RC on Lt

25450

125.99

Lt.

Rt

Rt

34

<u>122.56</u> 343 35	<u>121.32</u> 415 15	<u>121.21</u> 498	<u>121.14</u> 485 15	<u>121.34</u> 465 35
		<u>121.12</u> 487	<u>120.79</u> 520 15	<u>121.01</u> 498 15 = gutter
		<u>121.07</u> 492 15 = C6 Rd		
<u>122.37</u> 352 35 = Carb	<u>121.94</u> 405 35 = gutter	<u>121.13</u> 486 15	<u>121.11</u> 488	
		<u>121.79</u> 490 15 = Carb	<u>121.15</u> 481 15 = gutter	<u>121.09</u> 490
		<u>120.72</u> 521 15.2	<u>121.19</u> 480 15.2	
		<u>121.32</u> 462	<u>120.88</u> 511 14.8	<u>121.01</u> 498
		<u>120.79</u> 520 15.2	<u>121.21</u> 498 15.2	
		<u>121.01</u> 498 15 = Carb	<u>120.69</u> 530 17.9 = 15.2	<u>120.81</u> 518 15.1 = Carb
		<u>120.81</u> 518	<u>120.39</u> 540 15.1 = gutter	<u>120.81</u> 518 15.1 = Carb
		<u>125.99</u>		

Check Levels 47th St.
Market St. to Imperial Ave.

35

BM 3.89 125.06 121.17 ^{L+T}
Market 47
Page 34

TP 0.16 113.80 11.92 113.64

TP 0.20 101.30 12.70 101.10

TP 1.81 90.54 12.57 88.73

BM 1.44 85.85 6.31 84.41 ^{N.E. 8P}
Perot 47th
84.39
Page 34

TP 5.35 80.43 10.77 75.08

BM 12.71 88.10 5.04 75.39 ^{L+T 47th St.}
E 7 47th St.
75.39
Page 34

TP 12.64 100.60 0.14 87.96

TP 11.96 112.36 0.20 100.40

TP 3.53 115.33 0.56 111.80

BM 3.14 112.19 ^{S.E. 8P}
Imperial 47
112.19

Washington St. EXT.

Set Lot Cor's on Sky ROW.

Blk 139 Univ Hrs

Moore no. 90026
Begg
Green
Roberts
7-14-47 □ = set 2x2 Hubs

Marconi Way

Blk 139

ROW

18' 3" 30"

86.60

10.57

9.33

28 29

30

37.83

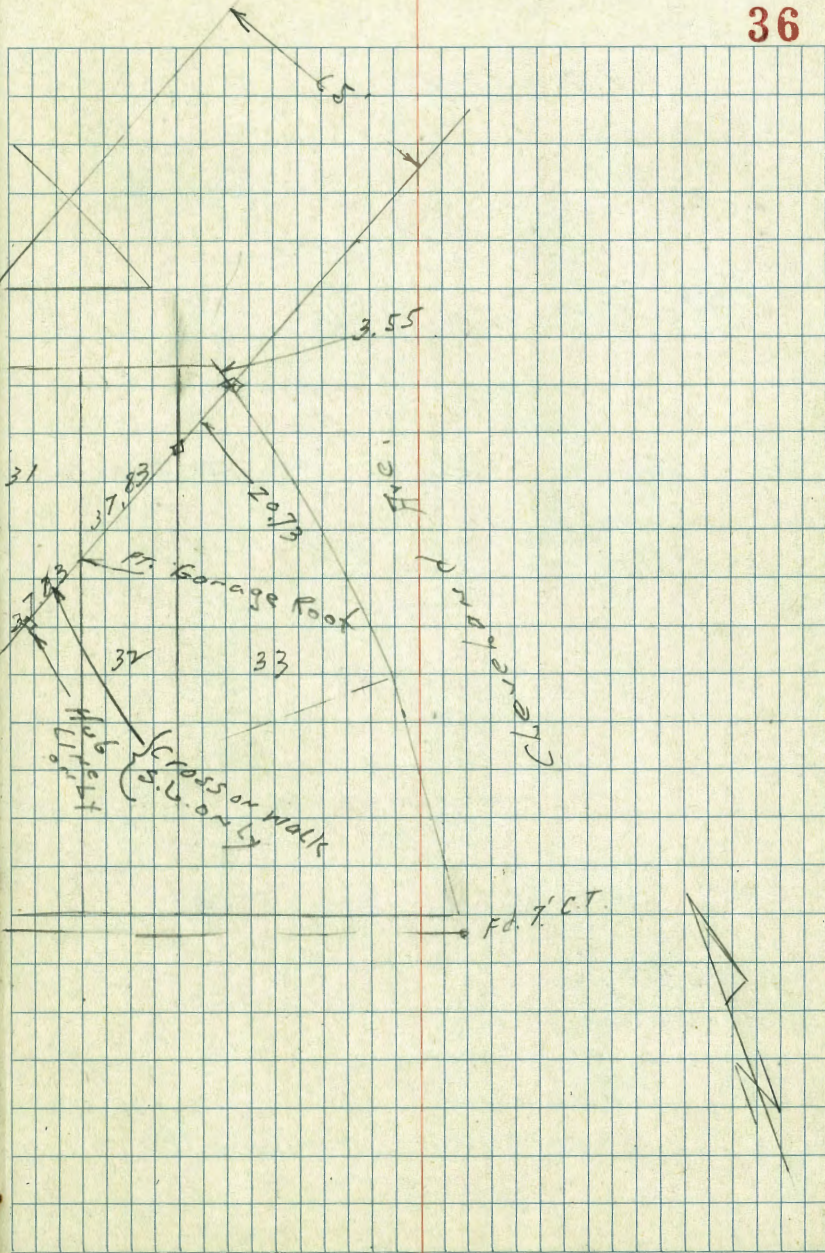
37.83

Fd. Cross
Page 1

Lincoln Ave.

Indexed m₂
8-15-47

36



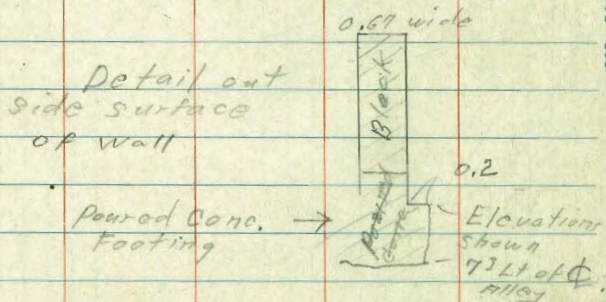
Cross Section Alley - 15' wide
BIK (A) Sunset Crest

VX.O. 25001

Sommermeier
W Moore
E Sherman
8-13-47

- - Fd. 2" Iron pipe - wood plug + tack. Map # 2030
- + - Fd. L x T. P.I. - check ads, etc.
- o - set nail in paving
- ⊙ - set Load + Disk in Conc. Walk

Note: New notes taken 7-22-54 in FB-2264-45
for gd profile + new const. job



T.P. 11.78 293.21 1.00 281.43

Set B.M. N.E. Prop. P.I.
Load + tack
Trieste + Valencia Dr. 12.01 270.42

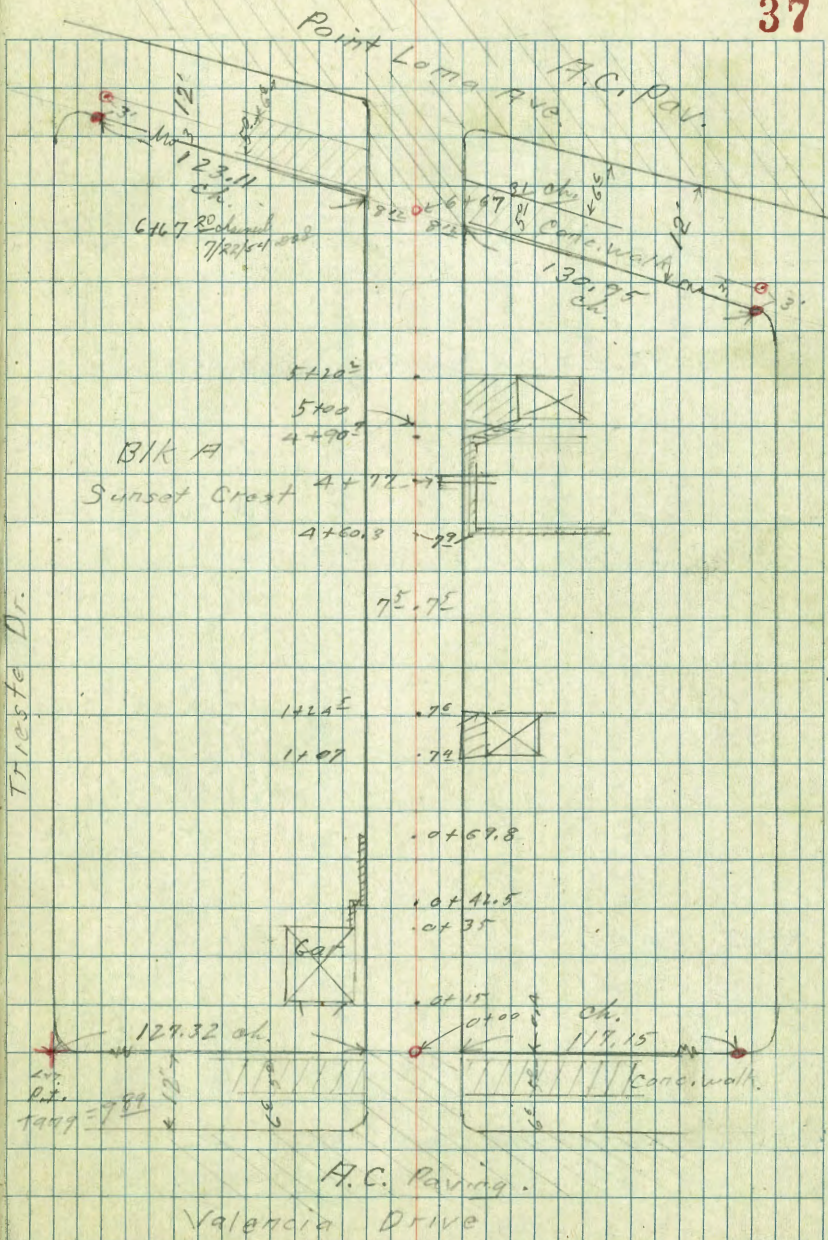
T.P. 12.01 282.43 1.54 270.42

N.E. B.P. 13.04 271.96 - 258.92
Santa Barbara X
Trieste

Indexed m2
8-15-47

81107

37



0+42^E 7' Lt + 9' Lt = 1' in wall
 = 2' offset in block wall

See Page 37

0+35 9'

Conc footing
 Starts Conc Block wall. Ort. poured
 Lt. = N.E. Cor Bar.

0+15 9' Lt. = S.E. Cor. Bar. South Entrance

0+00 = N. Line Valencia Dr.

0-94

Notes returned
 9-19-47
 R. Johnson

0-12 Cont.

0-12 = N. Curb line Valencia Dr.

293.21

L+

4

R+

38

287.8	287.7	287.2	286.7	287.8	287.8	288.5	289.0
5.4 9.5 Brd. at wall	5.5 7.5 Brd. at wall	6.0 7.3 Top Footing	6.5 7.3 Bottom of Footing	5.4	5.4 3	4.7 7.5	4.2 20
		287.61	287.6	288.0	288.1	289.0	289.0
		5.60 7.9 Ctr door	5.6 7.5	5.2	5.1 4	4.2 7.5	3.2 20
	287.58	287.58	287.37	287.58	288.27	289.12	
	5.63 7.3 Back of Curb	5.63 7.33 Top of Cl.	5.84 7.3 pav	5.63 on Nail	4.94 7.5 pav	4.09 7.53 Top of Cl.	
			287.64				
			5.57 7.5 Top of Cl.				
	285.49	289.87	289.26	287.02	287.65		
	7.74 30 Top of Cl.	13.34 7.5 Top of Cl.	13.95 7.5 Brd.	6.19 7.5 Brd.	5.56 7.5 Top of Cl.		
	284.93	287.23	287.72	288.19	288.86	288.82	289.46
	8.28 30 Curb	5.98 7.5 Curb in Drive	5.49	5.04 7.5 Curb	4.35 7.5 Top of Cl.	4.39 30 Curb	3.75 30 Top of Cl.

293.21

1+50

1+25

1+24.5 = End Conc. Apron + Gar.

1+07 7th Rt. = start Conc. Apron + Double Gar.

1+07 7th Lt. = ^{7' 1 1/2" ± 18"} P. Pole = J.P.A. 1285 (90816 H)
_{Wly edge}

1+00

T.P. }
P.A. 90916 H } 0.20 284.88 8.53 284.68
J.P.A. 1285 }

285.0

0+69 8th 7th Lt. = End Conc. Block wall 8.2
7th Lt. = End Footing 20
293.21

	277.5	279.0	279.1	279.9	280.6
	7.4 20	5.9 7.5	5.8	5.0 7.5	3.3 20
	279.2	281.0	281.4	282.2	283.0
	5.7 20	3.9 7.5	3.5	2.7 7.5	1.9 20
			282.3	282.38	284.51
			2.6 7.5 Grid	2.50 7.6 Apron	0.37 17.8 Bar Floor
			283.4	283.45	284.54
			1.9 7.3 Grid	1.83 7.2 Edge Apron	0.34 17.6 Bar Floor
	282.2	282.9	283.0	283.4	283.9
	2.7 20	2.0 7.5	1.9	1.5 5	1.0 7.5
		284.88			
	286.1	285.0	285.3	286.0	286.7
	7.1 7.5 Grid at wall	8.2 7.3 B. Hory ap Footing	7.9 7.3 Top Footing	7.1	7.2 3
			286.1	286.0	286.7
				6.5 7.5	5.7 20
					287.5
					293.21

T.P. 0.44 248.38 13.02 247.94

3+90 on Φ is 1.8" tree. Eucalyptus

3+60

3+58 ^{OK w/ly} 6" Lt. = P. Pole ^{JPA 1328} 9081A H
63 Lt. 14" P. Pole

3+35

T.P. 0.73 260.96 12.55 260.23

3+08 4" Lt. = 6" tree. (gone) ^{old}

3+00

2+99 3' Lt. = 10" tree (gone) ^{old}

2+52 \rightarrow 8" Lt. = P. Pole ^{OK w/ly} JPA 1301 + 90815 H
2+42 \rightarrow 7" Lt. 12" P. Pole \uparrow

2+50

T.P. 0.46 272.78 12.56 272.32

2+00

284.88

Lt.

Φ

Rt.

40

250.4	250.2	249.5	249.5	250.4
$\frac{10.6}{20}$	$\frac{10.8}{7.5}$	11.5	$\frac{11.5}{7.5}$	$\frac{10.6}{20}$
256.1	255.7	255.4	254.8	254.8
$\frac{4.7}{20}$	$\frac{5.3}{7.5}$	5.6	$\frac{6.2}{7.5}$	$\frac{6.2}{20}$
		260.96		
	261.5	261.1	261.1	
22	$\frac{11.3}{7.5}$	11.7	$\frac{11.7}{7.5}$	
268.3	267.6	267.2	267.3	266.7
$\frac{4.5}{20}$	$\frac{5.2}{7.5}$	5.6	$\frac{5.5}{7.5}$	$\frac{5.1}{20}$
273.4	273.4	272.78	273.7	274.6
$\frac{11.5}{20}$	$\frac{11.5}{7.5}$	11.5	$\frac{11.2}{7.5}$	$\frac{10.3}{20}$
		284.88		
		284.88		

Lt.

+

Rt.

6⁷/₁₆ x 15" ∇ D33223 T
 6+10 7^L Lt = P. pole J.P.M. 1387
 or why else

6+00

5+50

5+20² Rt. = End Double Bar
 7.6 Rt. = End Apron

5+00 { 17^L Rt. = End wall. start Garage
 7^R Rt. = start. Conc Apron + Doub. Bar

4+90² { 7^R Rt. = Face of wall.
 7^L Rt. = Δ in tile & stucco wall, Footing

6²/₁₆ x 12" ∇
 4+90 7^L Lt = P. pole # J.P.M. 1353 - D33224 T.
 or why

T.P. 2.60 240.70 10.28 238.10

248.38

2341.7	2351.7	2351.5	2361.0	2381.0	2391.0
6.0 20	5.0 7.5	5.2	4.7 7.5	2.7 19	1.7 20
2351.0	2351.7	2351.9	2361.4	2381.9	
5.7 20	5.0 7.5	4.8	4.3 7.5	1.8 20	
		2361.9	2376.0	2391.7	
		5.8	3.02 7.6 Apron	1.23 19.6 Bar Floor	
2371.0	2371.2	2371.7	2381.3	2381.7	2391.60
3.7 20	3.5 7.5	3.0	2.4 7.5	2.41 9.9 Apron	1.10 17.7 Bar Floor
		2381.1	2381.6	2381.4	2371.7
		2.6	2.1 7.5 ard	2.3 7.5 top of Footing	3.0 7.5 Bottom of Footing
			240.70		

S.E. B.R. Santa Barbara
+ P.T. Loma

	12.63	188.55	188.52
T.P.	0.12	201.18	12.77 201.06
T.P.	0.12	213.85	13.01 213.63
T.P.	0.132	226.64	12.74 226.32

S. Ob. line Pt. Loma Ave.

6467^{sl} { taken along line of Pt. Loma Ave.
S. Line Pt. Loma Ave.

T.P. & Nail
6467.31 7.36 239.06 9.00 231.70

6450

6432 6^s LF & dead man

6425

240.70

Lt.

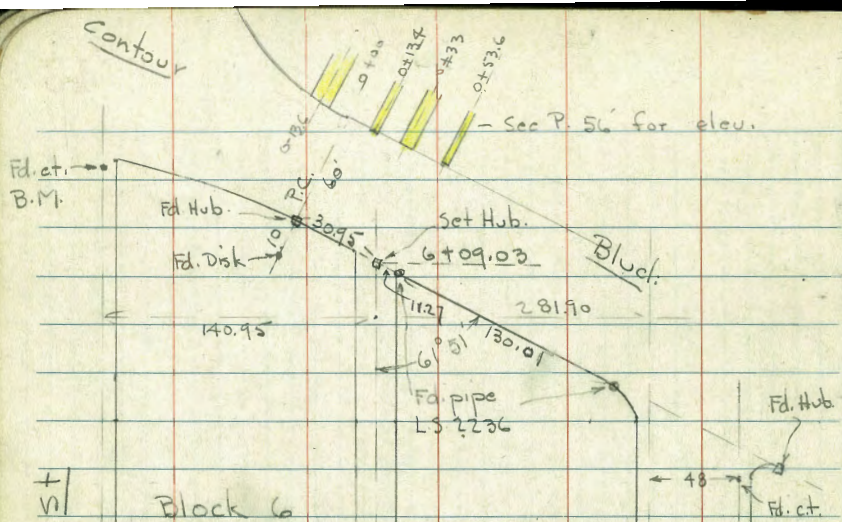
☐

Rt.

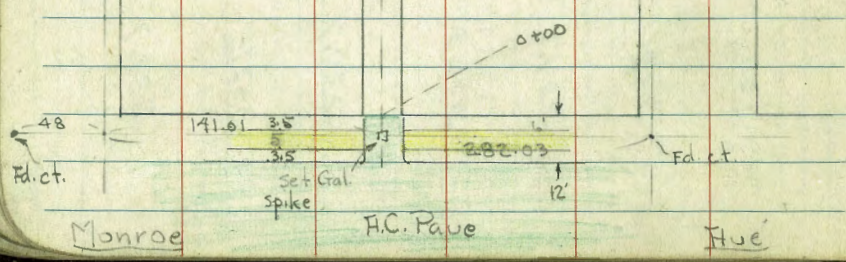
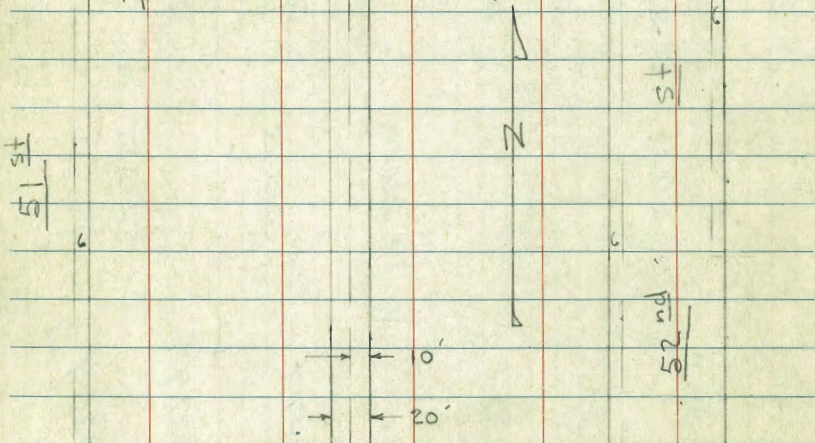
43

224.60	222.93	230.33	227.75	230.86	232.10	233.03	237.88	234.59
11.46 to top of	15.18 to cut	8.73 8.4 top of cut	9.33 8.1 cut	9.20	6.76 8.1 cut	6.03 8.7 cut	11.8 to cut	0.47 to top of
	231.32	230.97		231.70	233.13		233.51	
	7.74 8.1 top of	8.09 8.1 cut		7.36 on nail	5.93 8.2 cut		5.55 8.2 top of	
				234.06				
	233.1	234.1	232.8	233.3	234.4	237.9	234.4	
	6.9 20	6.6 7.5	7.9 5	7.4	6.3 7.5	2.8 12	2.3 20	
234.1	235.5	234.6	234.1	233.7	235.7	234.2	238.9	
6.0 20	5.2 7.5	6.1 5		5.9	5.0 7.5	2.5 11	1.8 20	

240.70



+
N/ Block 6
Alhambra Park
Map 1488



Indexed

X-Sept. 20 Alley in Block 6 - Alhambra Park

#1915
W.O. 31200

11-26-47
Osborne
Hardin
Smith
Worrell

Book - 1601 - P. 15
1679

3+24- 10.3 Lt. = Wly. P. pole # PA. 4575

3+17- 12.7 Lt. = ^{Back of} Sing Gar. - Conc. floor - opens W.
 3+15.4- 1.2 Rt. = Sewer M.H. 3.57 on Rim

3+08- 11.4 Rt. = 12' Cong. Slab - for Gar.

3+00

2+90- 13' Lt. = Frame House - Conc. found

2+50

2+17- 13' Lt. = Frame house

2+10- 10.5 Lt. = Wly. P. pole # PA 4555

2+00

1+87- 13.4 Lt. = Sing Gar. - Dirt floor

1+77- 13.4 Lt. = Sing Gar. - Dirt floor

1+50

1+46- 10.9 Rt. = NW Cor. House

1+04- 11.4 Rt. = SW Cor. House - Stucco

Station	Description	Notes	Value 1	Value 2	Value 3	Value 4	Value 5	Value 6
3+24	10.3 Lt.	Wly. P. pole # PA. 4575						
3+17	12.7 Lt.	Sing Gar. - Conc. floor - opens W.						
3+15.4	1.2 Rt.	Sewer M.H.	3.57					
3+08	11.4 Rt.	12' Cong. Slab - for Gar.						
3+00								
2+90	13' Lt.	Frame House - Conc. found						
2+50								
2+17	13' Lt.	Frame house						
2+10	10.5 Lt.	Wly. P. pole # PA 4555						
2+00								
1+87	13.4 Lt.	Sing Gar. - Dirt floor						
1+77	13.4 Lt.	Sing Gar. - Dirt floor						
1+50								
1+46	10.9 Rt.	NW Cor. House						
1+04	11.4 Rt.	SW Cor. House - Stucco						

390 71

check B.M. 428 386.83 ✓ cct. SE. Madison & 51st
 T.P. 5.23 391.11 2.73 385.88 B1679 P 37

6+18-12 Lt. = end Conc. wall 4.90
 12 Bottom wall
 6+14.6 = Opp. Prop. Cor. on Lt. = end.

6+09.03 = Alley + S.L. Contour Blvd

6+03.5 = opp. Prop. Cor. on Rt.
 6+02-12.7 Rt. = end of wly. Conc. Dr.

5+80

5+76-11A Lt. = Beg. 8" Conc. wall
 5+74-10.7 Lt. = Wly. P. pole # P.A. 4595
 8" Conc. Dr.

5+61-11 Rt. = N.W. Cor. Gar. # 12' Rt. = Beg. wly.

5+50

360	385.01				
4.2	384.11				
3.4	385.21				
3.43	385.18				
4.0	384.61				
4.2	384.31				
5.1	383.11				
6.0	382.61				
6.4	382.21				
16 = gut.					
3.2	385.41				
3.2	385.34				
3.2	384.71				
4.1	384.51				
5.4	383.21				
5.8	382.71				
30 = gut (divt)					
5.1	385.41				
3.1	385.43				
3.9	384.71				
4.2	384.41				
5.4	383.21				
5.8	382.51				
5.1	382.93				
2.9	385.71				
2.9	385.65				
3.6	385.01				
4.9	383.71				
5.1	383.51				
5.05	383.56				
12' +					
Wly. Conc. Dr.					
2.94	385.67				
3.94	384.47				
3.2	385.41				
11.4					
Top wall					
11.4					
Bottom wall					
11.4					
ground.					
3.1	385.51				
3.4	385.21				
4.2	384.41				
388.61					
4.2	384.91				
4.2	384.01				
11.6					
ground					
4.26	384.41				
12					
Dr.					

Lt Rt

Indexed

Note: Both Houses have
Conc. Foundation walls

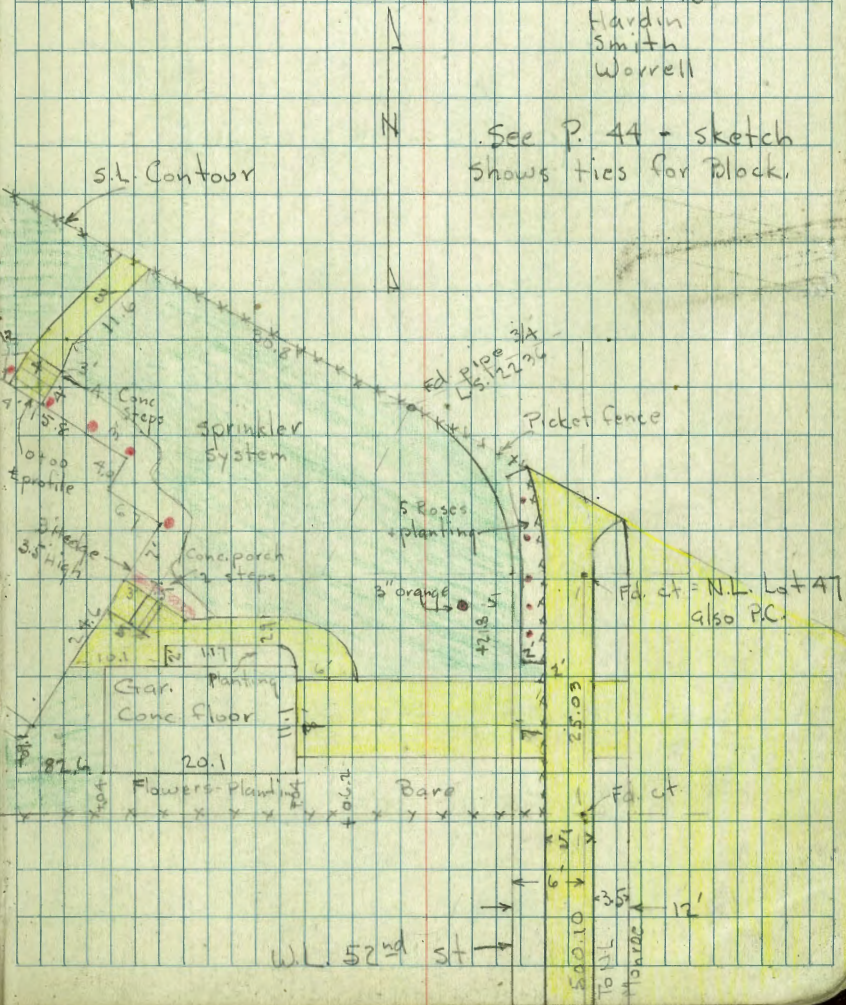
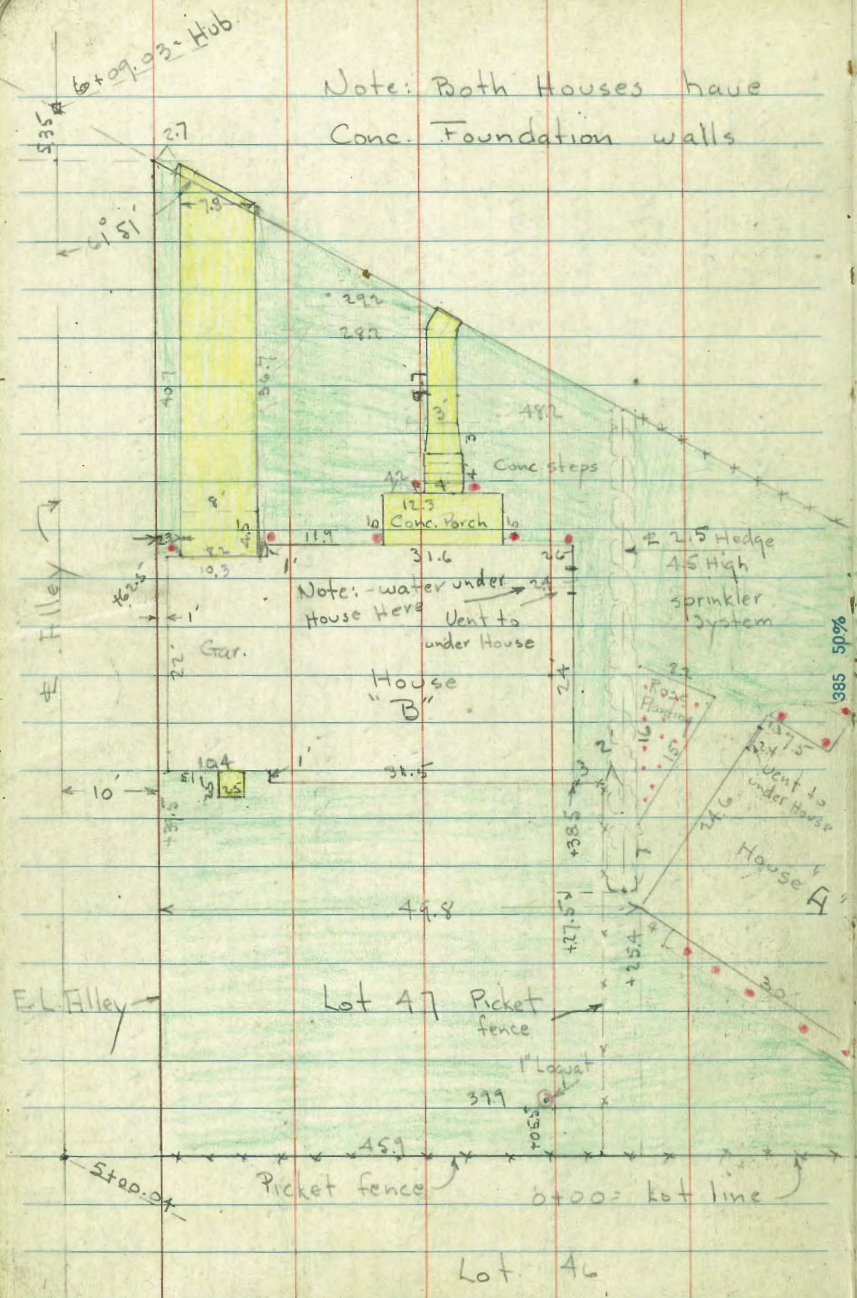
shrubs = ●
Lawn = ■
Conc = ■
X-Sect. + Topo - of Lots
A7 to A9 - Inc - in Blk. G
Hilhambra Park - Map 488

1935
W.O. 90050

12-8-47

Osborne
Hardin
Smith
Worrell

See P. 44 - sketch
Shows ties for Block.



Levels on lots 47 to 49 incl.

0+17.1 = S. edge of 2.9 walk along Gar.

0+15.1 = S. edge Conc. walk Bet. House & Gar.
= N. side Gar.

0+13.2 = N. edge Conc. Dr.

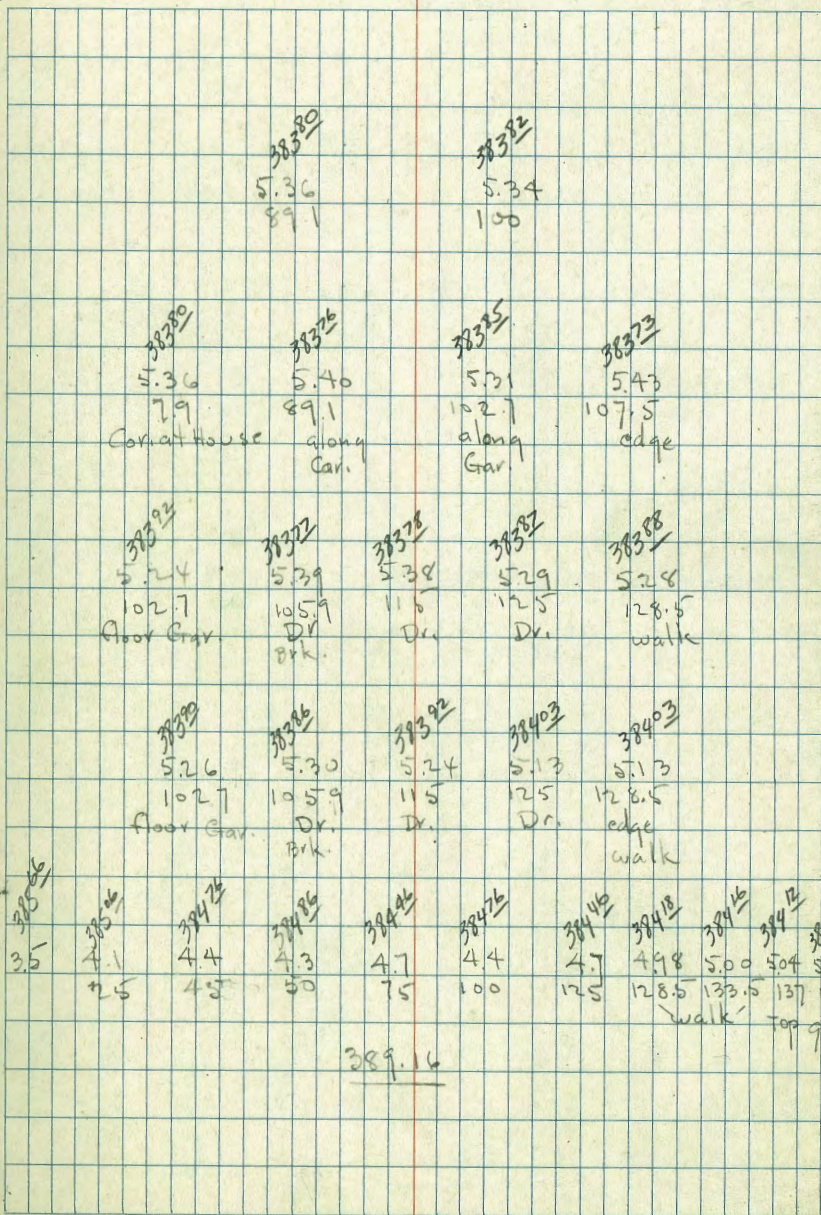
0+06.2 = S. edge Conc. Dr. to 52nd

0+00 = Lot line = Bet 46 + 47

	5.52	389.16	5.45	382.64	ct. opp. Pt. 52nd
			6.26	382.83	Pipe - Alley Cor.
B.M.	2.26	389.09		386.83	6' ct. P. 48

Base line =
E.L. Alley

Rt. = E. 50



0+03.68 = E.L. Hilley + S.L. Contour.

0+95

0+80

0+62.5 - Cont.

0+62.5 = along N. side House "B"

38292 4.56	38248 5.0 10									
38312 4.3	38312 4.31 26 w. edge Dr.	38285 4.63 10.4 E. edge	38248 5.0 16.4 S.L. Contour	38208 5.4 17	38178 5.7 30					
38358 3.9	38358 3.90 24 w. edge Dr.	38344 4.06 10.3 E.	38308 4.4 14	38288 4.8 22	38247 5.0 28 w. edge Conc. walk	38245 5.03 31 E.	38208 5.4 46	38198 5.5 44 S.L. Contour	38158 5.9 45	38148 6.0 60
38258 4.9	38258 5.0 42.9	38218 5.3 50	38208 5.4 65	38188 5.6 76.4 S.L. Contour	38168 5.8 100					
38108 3.4	38420 3.11 25 w. edge Dr.	38421 3.21 10.4 E. edge	38328 3.7 14 along House	38424 2.72 14 = E + ground	38358 4.1 25.2 Bottom of 6' x 14" Vent	38521 2.27 23.7 Top Conc. Porch. w.	38521 2.27 35.5 Top Porch E.			

± Profiles on on Conc. Dr. from House
"B"

3.89 = ± at end. (notes out in street.)

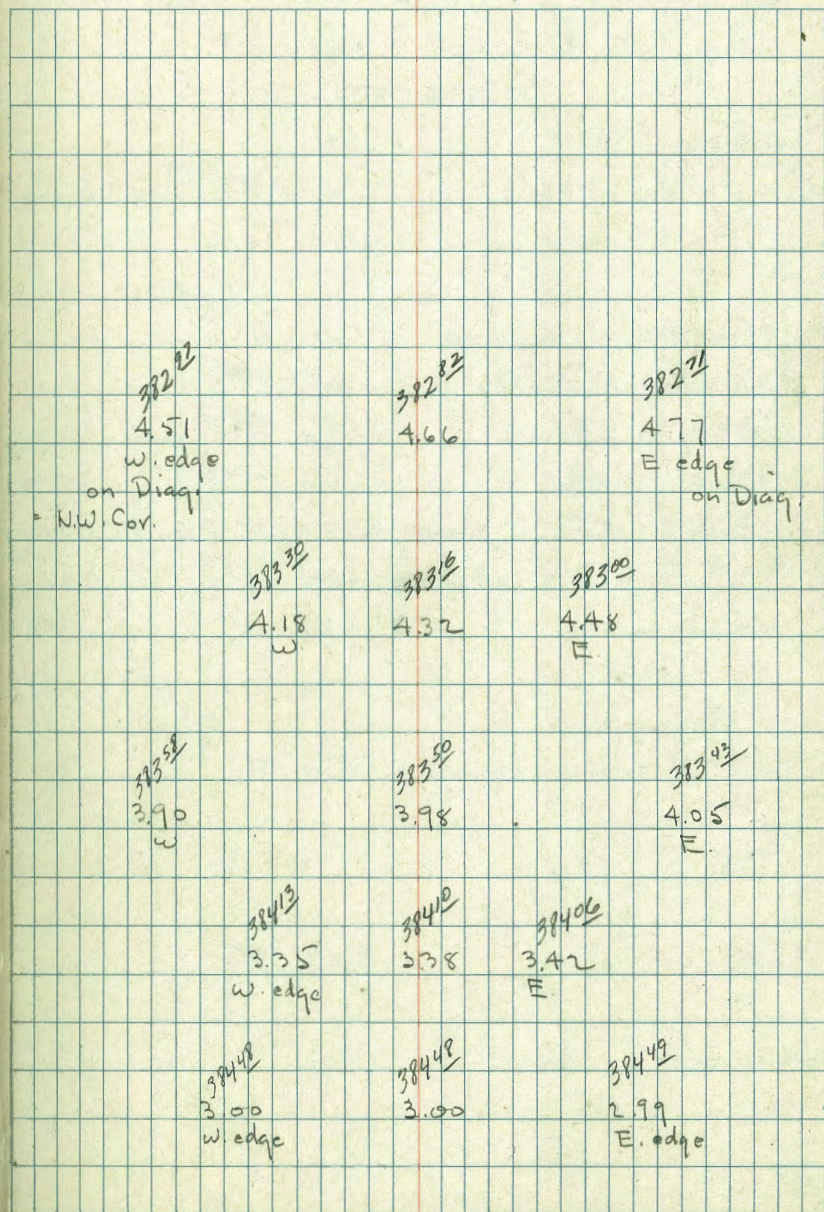
0+30

0+19.3 = Const joint

0+04.5 = Brk. in Line + grade

0+00 = ± Dr. at N. side of Gar. to House "B"
See sketch

385 50%



387.48 - P. 52

± Profile of Conc. Porch - steps +
walk at N. side of House "B"

387.48 - P. 52

Floor elev. of House	2.13		
± Conc. Porch. 12.3 wide			
0+00 = N. side of House	2.27	385 ²¹	Top Conc.

0+05 = Top. - N. edge porch 2.38 385¹⁰

+06 Top 1st Step 2.88 384⁶⁰

+07 Top 2nd " 3.36 384¹²

+08 " 3rd " 3.86 383⁶²

+09 " 4th " = Bottom 4.36 383¹²

+09 = Top walk at bottom step 4.78 382⁷⁰

+12 = Brk. in Line 4.86 382⁶²

+21.7 = Beg. curve in walk 5.14 382³⁴

+25 = end. at ± 5.24 382²⁴

Walk nearly Level.

± Profile of Conc. Porch - Steps +
Walk at N. side of House "A"

387.48

Floor elev. of House	1.99	385 ⁴⁹	
0+00 = N. edge of House ±	2.20	385 ²⁸	Top Porch.
Conc. porch.			

0+01 = Top 1st step. 2.71 384⁷²

0+02 = " 2nd " 3.21 384²⁷

0+03 = " 3rd " 3.71 383²³

0+04 = " 4th " 4.22 383²⁵

0+04 = ± walk at bottom step 4.67 382⁸¹

0+07 = Brk. in Line + grade 4.95 382⁵³

Beg. curve

0+12 = along ± 5.16 382³²

0+18.6 = end. = ± 5.37 382¹¹

Rods on Vents in House "B"

5.65	<u>38848</u>	382.93
------	--------------	--------

2.4' x 1.8' Vent - or door to underneath House
"B" - N.E. Cor. - See sketch for loc.

Top of Vent. - \oplus	3.95	<u>38453</u>
-------------------------	------	--------------

Bottom - Top of sill = Conc.	5.72	<u>38276</u>
------------------------------	------	--------------

approx. ground under House	6.0	<u>38248</u>
----------------------------	-----	--------------

by Vent.

2-6" x 14" Vents at \oplus of E. side	3.76	<u>38472</u>	Vent.
all seem to be level around House			Bottom of

Rods on Vents in House "A"

2.4' x 1.6' Vent - or door to under House at N.W. Cor.
See sketch.

Top of vent.	3.80	<u>38468</u>
--------------	------	--------------

Bottom " " = Top conc. sill	5.08	<u>38340</u>
-----------------------------	------	--------------

approx. ground under House	5.6	<u>38288</u>
at Vent.		

2-6" x 14" Vents at S.W. Cor. House "A"

Bottom of Vents.	3.60	<u>38488</u>
------------------	------	--------------

Rods on New walks + Conc Drives on
 N. side of Contour Blvd. - near P.C.
 N. of Alley in Blk. C - Dist. from P.C. -
 Both ways - P.C. = 0+00 - See P. 44 - sketch

5.88 388.71 382.83 - Pipe at Alley

0-13.6 = ± 8' Conc. Dr. out to prop line

± at N.L. 4.11 384⁶⁰

35.6 N. = floor Gar - Conc. 3.77 384²⁴

0+00 = P.C.

0+13.4 = ± 3' Conc. walk

0.3 S. of N.L. = Top - end. 4.50 384²¹

16 N. = at porch 4.37 384³⁴

0+33 = ± 8' Conc Dr.

0.2 N. of N.L. = ± at end. 4.75 383⁸⁶

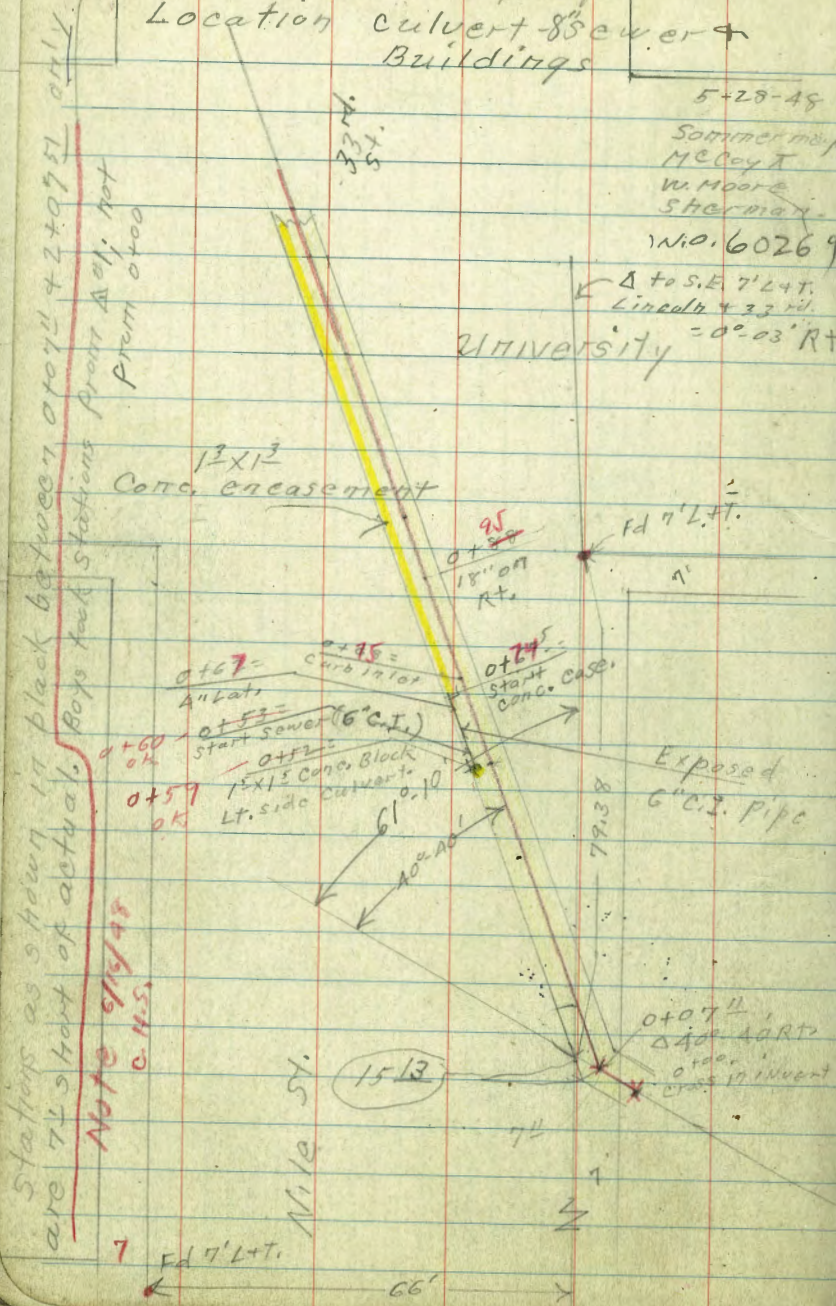
17' N. of end 4.42 384²²

0+53.6 = ± 3' Conc. walk

0.5' N. of N.L. = end - ± 4.69 384⁰²

15.4 N. of end = at porch 4.16 384⁵⁵

BIK 195 City Hqts
 Location culvert & sewer &
 Buildings



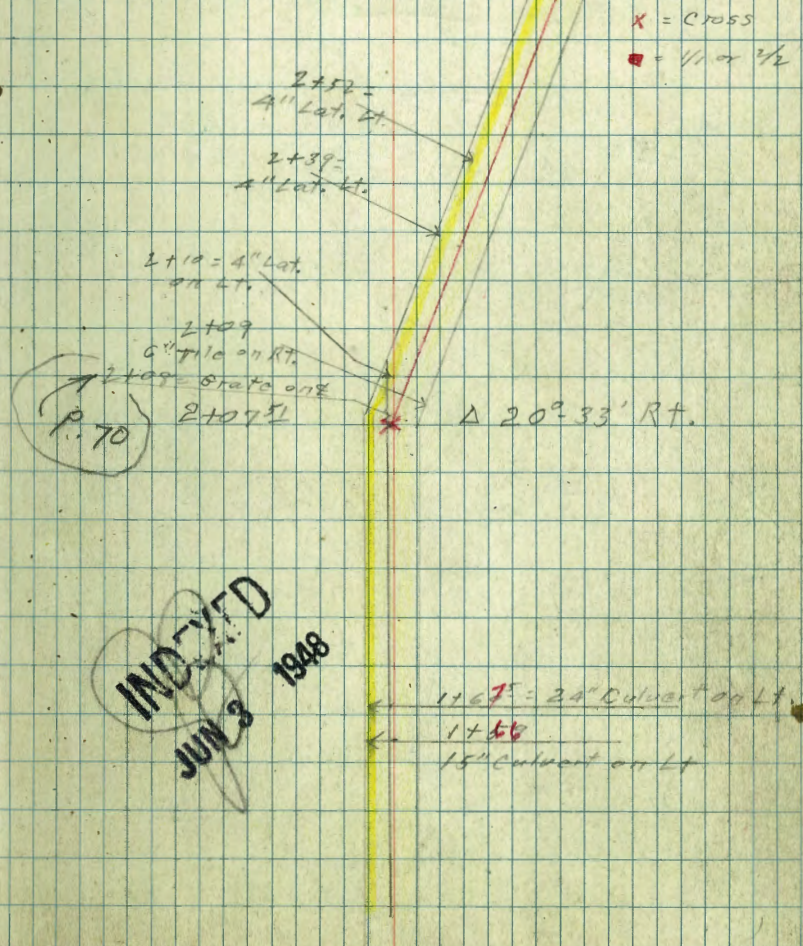
Stations as shown in black between 0+00 and 0+75 ONLY are 72' short of actual. Boys had stations from 0+00, not from 0+00
 Note 9/15/48 C.H.S.
 Mile St.

5+28-49
 Sommermaier
 McCoy T
 W. Moore
 Sherman
 No. 60269

University
 Δ to S.E. 7' L.T.
 Lincoln 4 33' RT.
 = 0° 03' RT.

For Cross Sections of
 Culvert see page 69

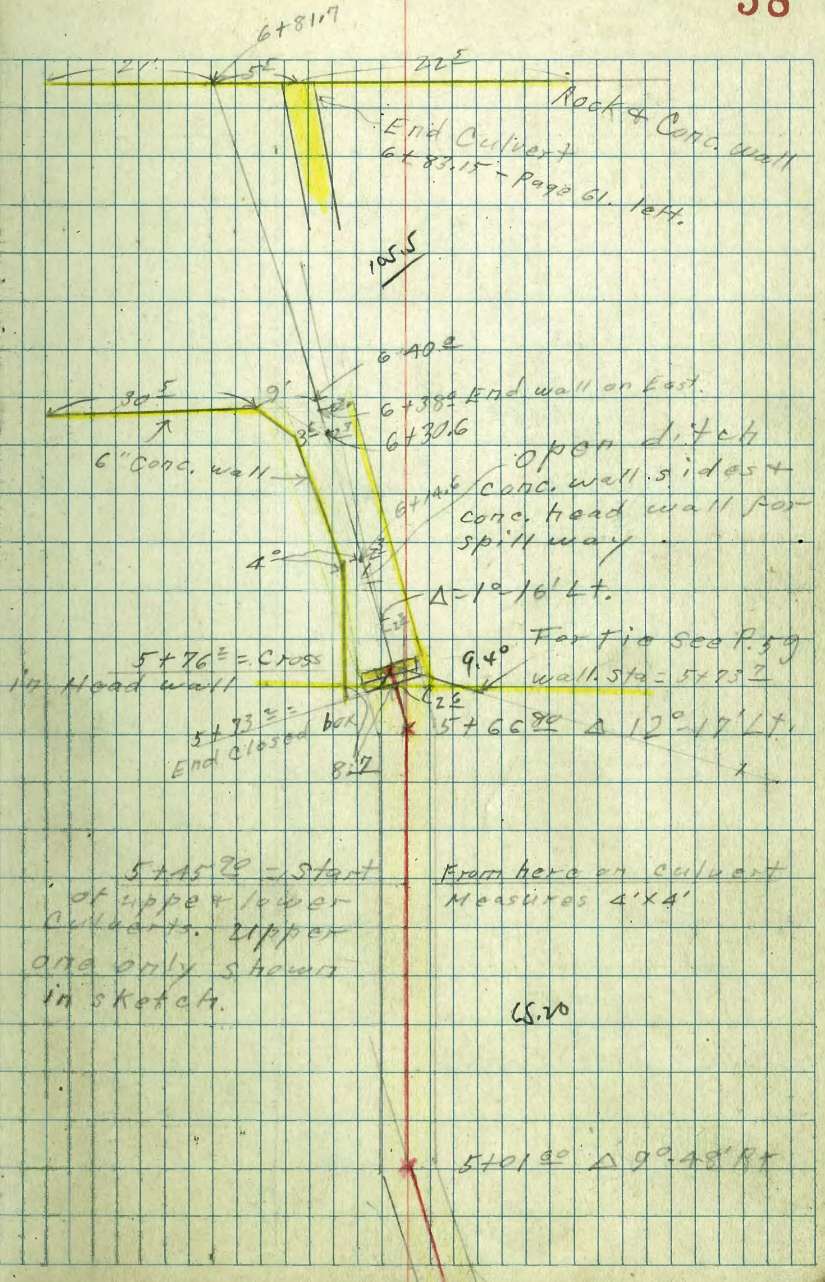
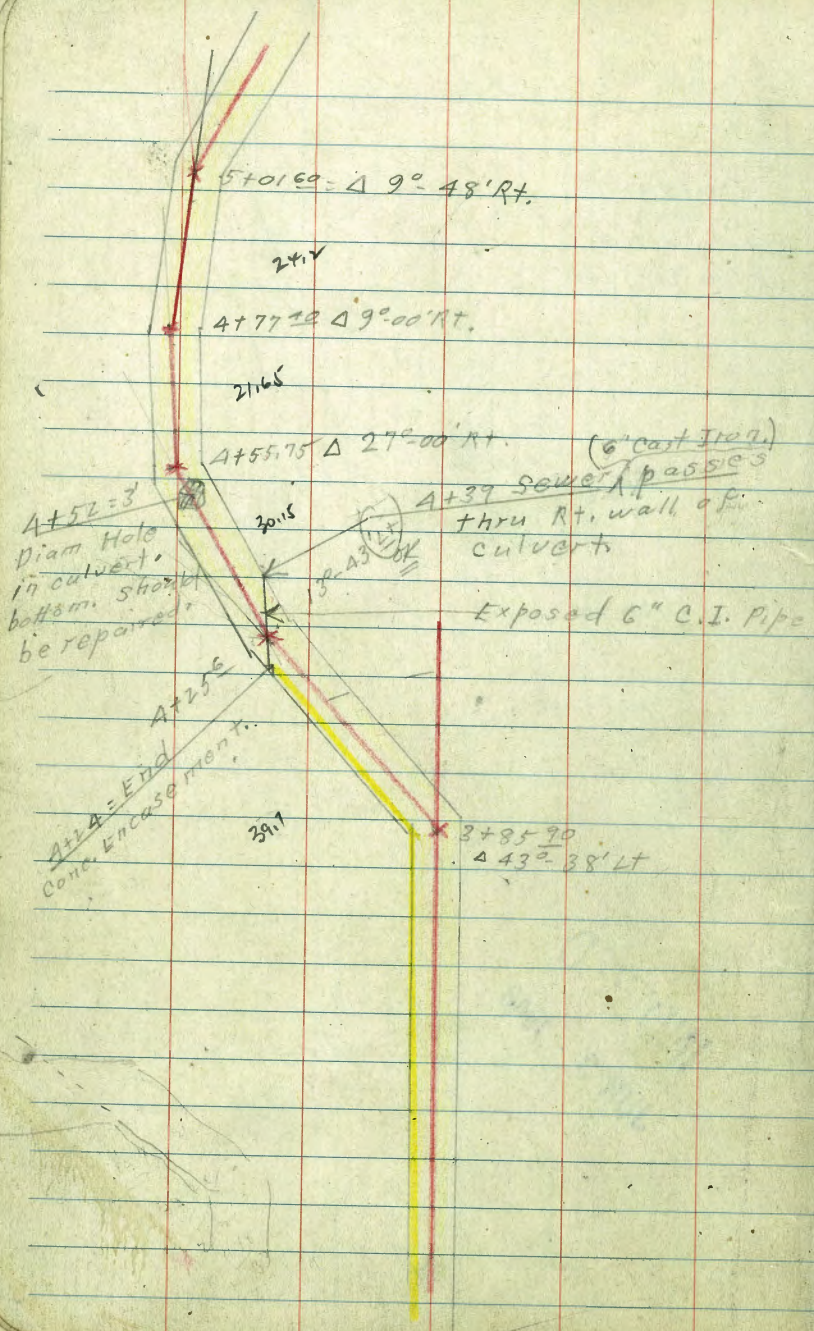
Culvert
 4' wide
 5' ± High



P. 70

INDEXED
 JUN 3 1948

1+67 = 24" Culvert on Lt.
 1+56 = 15" Culvert on Lt.

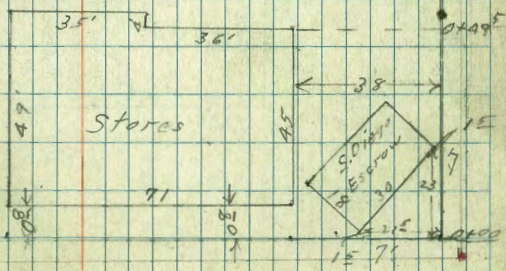
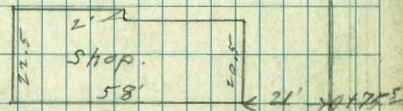
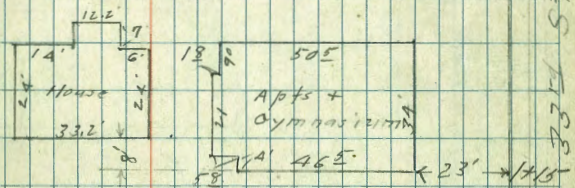
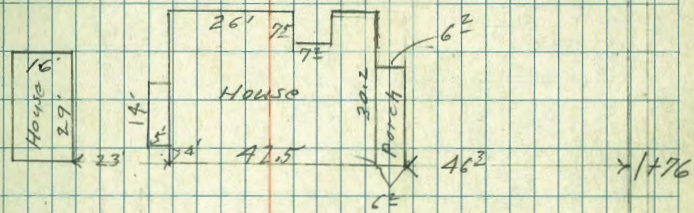
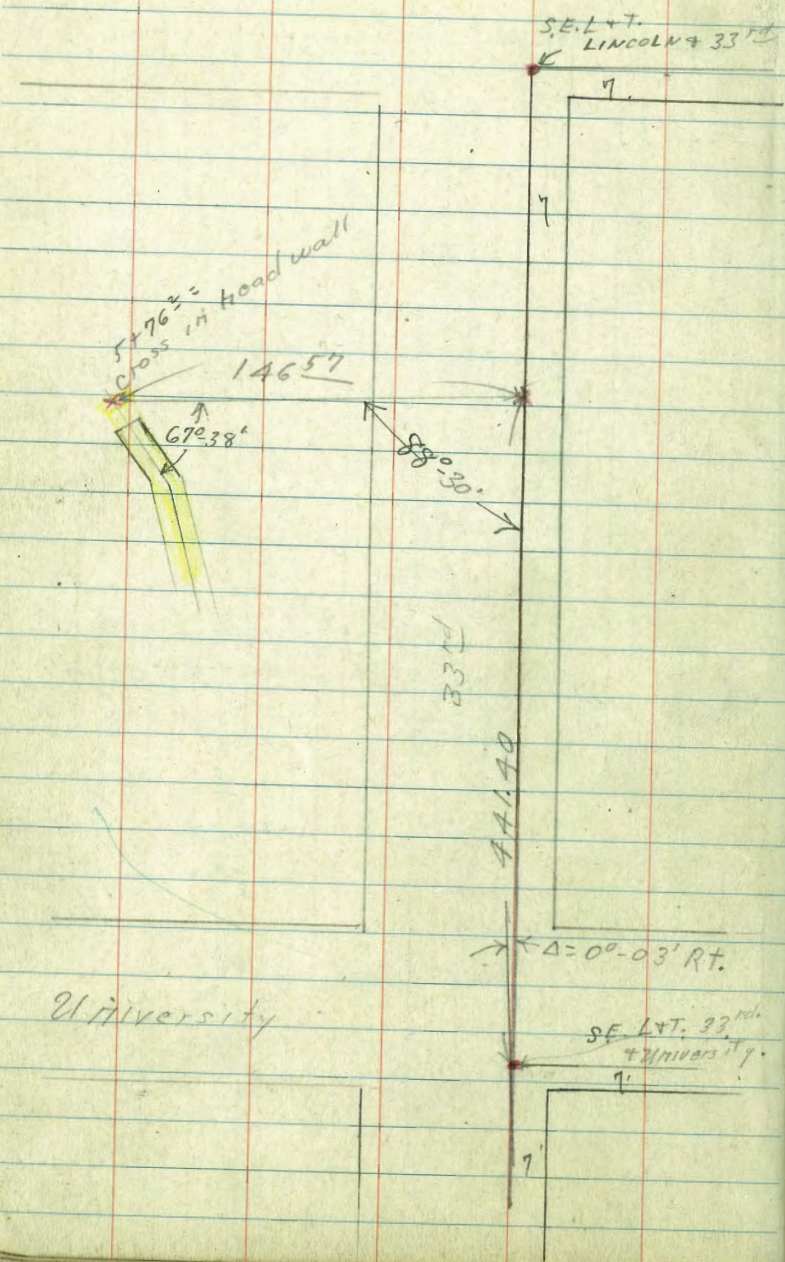


5+45.20 = Start of upper & lower Culverts. Zipper and only shown in sketch.

From here on culvert Measures 4'x4'

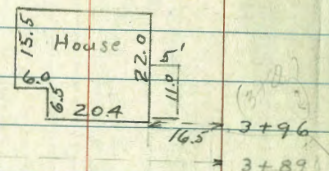
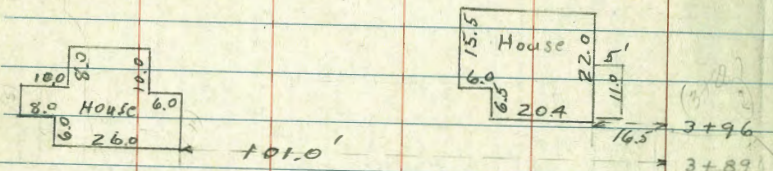
65.20

5+01.60 Δ 9° 48' RT

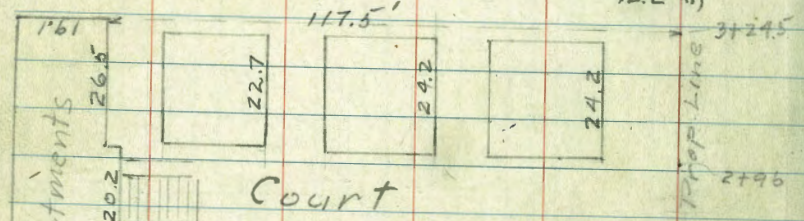
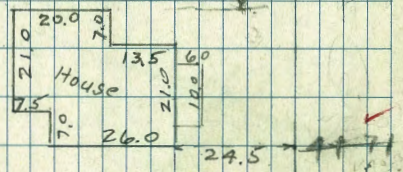
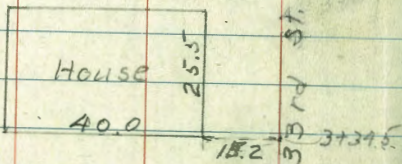


University

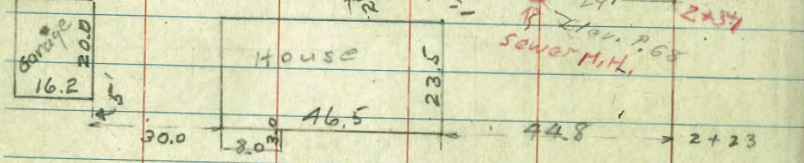
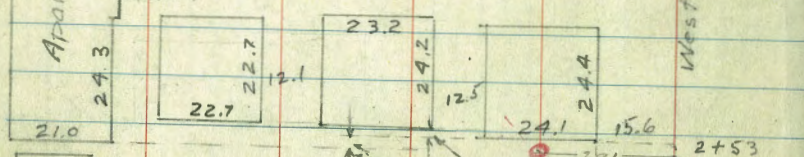
Lincoln



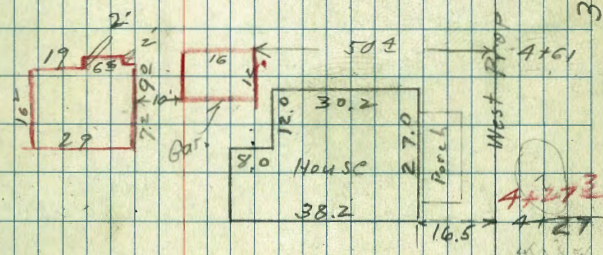
Wall 3+62.4



Court



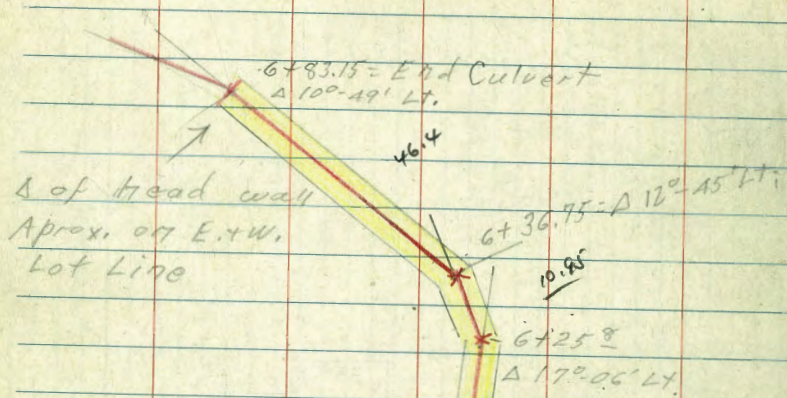
Sewer M.H.



West Prop Line

4+27

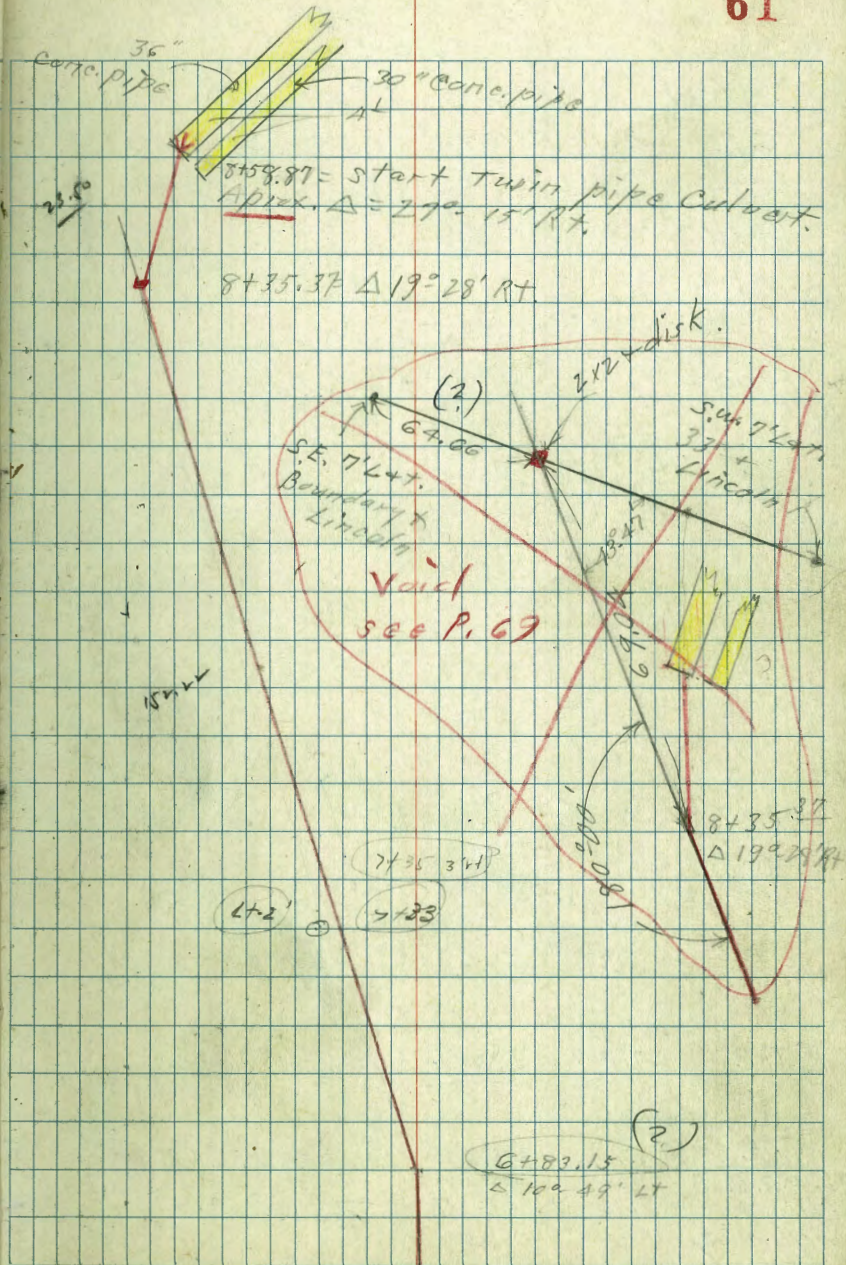
Lower Culvert sta 5+45.9 to End.



Property owner
Says sewer is 3° LT
of ϕ at this point

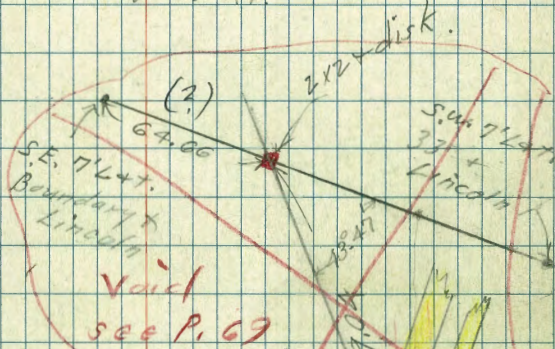
5+45.9 = start
upper + lower culvert.
 $\Delta 2° 15' RT$. Lower
culvert only.
See P. 58 for
upper culvert.

5+01.6 $\Delta 9° 48' RT$
(Page 58)



8+58.87 = start twin pipe culvert.
Aprox. $\Delta = 270.15' RT$.

8+35.37 $\Delta 19° 28' RT$.



7+35.31

(L+2)

7+33

6+83.15
 $\Delta 100.49' LT$

(?)

Profile Drain B/K 195

City Hqts.

Sketch Pages 57 to 58 & 61

T.P. 4.11 315.74 0.28 311.63

1+50

1+00

0+60 Top. C.t. 6" sewer

0+50

0+07" Δ 40°-40' Mt.

0+00

T.P. 4.49 311.91 7.27 307.42

T.P. 3.07 316.69 11.65 313.62

S.W.B.P. Nile to University 3.12 325.27 — 322.15

⊕

310.41 ✓
1.50

309.24 ✓
2.67

1.17
232 1/2

309.19 ✓
2.72
1.2
103.51
C.I. sewer pipe

308.51 ✓
3.59

307.47 ✓
4.44

307.42 ✓
4.49

311.91

4+37

T.P. 4.88 320.26 3.10 315.384+25^E Δ 13°-43' Rt. - 1 1/2" C.I. Line top exposed3+85²⁰ Δ 43°-38' Lt.

3+50

T.P. 5.18 318.48 ✓ 2.44 313.30 ✓

3+00

2+50

2+07^{5L} Δ 20°-33' Rt.

2+00

315.74 ✓

4

915¹⁸
5.08

310.26

316²⁶

2.22

1 1/2
top of pipe318³⁸

315

5.10

9+00 →

319.67

314²⁵ ✓

4.23

313¹¹ ✓

4.77

318.48312⁹⁶ ✓

2.78

312⁶ ✓

3.58

2+18.67

311⁵⁴ ✓

4.20

311⁴⁷ ✓

4.27

315.74 ✓

311.70
S. 1/2

T.P. 3.05 321.38 3.05 318.33 TP#7

= Start double culvert...

Pull of holes. Bad Condition

lower culvert is broken &

From here on floor of (1)

5+452 = start double box culverts

End 4'x5' Box Culvert.

5+0180 Δ 90° RT.

318³³
3.05

318⁰⁴
3.34

4+7740 Δ 90° RT

317⁷⁰
3.68

4+5525 Δ 270° RT.

317⁰⁸
4.30

Cone floor ahead approx. 6" thick,
old head wall.

back is 1' thick. looks like

4+32' } At this place cone floor to

T.P. 4.27 321.38 3.15 317.11

thru culvert wall.

4+39 2' RT. where 6" pipe passes

320.26

321.38

316²⁴ 2 elev of
4.02 top what?
2

320.26

Temp. Rock 10' R. of
 B.M. 6+83 0.37 322.46 #2

6+83¹⁵ End (Inlet) Lower Box Culvert

T.P. 2.56 322.83 1.11 120.27

6+36.75 Δ 12° 45' Lt.

6+25² 17° 00' Lt.

box. 4' wide
 5+45² Cont. = Levels in lower
 321.38

320⁰

2.2

322.83

320⁰

1.2

320¹

1.3

321.38

LEVELS Upper Box
Size Roughly 4'x4' Box.

6+30^E L in west Ret. wall.

6+14^E L in west Ret. wall.

wall along prop. line (E+W)

5+77 7³ ft. = start conc. Ret. wall at

T.P. 6.71 332.04 0.66 325.33

with Conc. side walls.

5+76²⁰ Top of Wall End Culvert. start ditch
Cross on wall.

built flush with side of culvert.
2' R.T. = start conc. Retaining wall.

5+71⁸ End of Floor = roof of box.

5+66⁸⁰ ALT

upper box culvert.

5+48 = start 8" thick conc. floor in

5+45² start double Culvert.

T.P. #7 7.66 325.99 — 318.33
R64

327 ⁷	327 ⁹	326 ⁵	326 ³	326 ⁷	328 ¹	327 ⁸
4.3	4.1	5.5	5.7	5.3	3.9	4.2
10	3 ^E TOP wall	3 ^E Ord.		2.9 Ord.	2.3 TOP wall	10
327 ⁶	327 ⁸	326 ¹	326 ³	326 ⁴	328 ⁰	327 ⁸
4.4	4.2	5.9	5.7	5.4	4.0	4.2
10	4 TOP wall	4 Ord.		2.3 Ord.	2.3 TOP wall	10
326 ⁶	326 ²	325 ³	325 ³	327 ⁸	327 ⁸	327 ⁸
4.4	5.8	6.7	6.7	4.2	4.2	4.2
10	3 ^E Ord.		2.3 Ord.	2.2 TOP wall	10	
		332.04				
			325 ³³			
			0.66			
			323 ⁰⁴		327 ⁸	
			2.95		+1.8	
					2	
					TOP Box wall	
			323 ⁰¹			
			2.92			
			322 ⁶			
			3.4			
			325.99			

7+12

stationing cont from P. 61

Page 65
Temp. BM 22

T.P. 9.76 332.18 9.62 332.42 (322.96)

5⁵RT = \pm lower culvert.

6+82 Along base of wall.

ground level to south

prop. line (Page 58). Wall top =

6+81.2 = top Conc. & Rock wall. Approx. along

taken on Δ

= Δ 7' 6" wide Conc. Ret. wall.

6+40 9' left along approx lot line

6+38 2³RT = End east Ret. wall

332.04

324 ⁵	323 ⁰	321 ³	322 ⁷	324 ⁷
7.8	9.2	10.9	9.5	7.5
3		4	6	11

332.18

325 ²	321 ⁵	320 ⁶	321 ¹	327 ⁶
7.8	10.5	11.4	10.5	4.4
11		5.2	10	30

\pm Box Culvert

327 ⁸	327 ⁴	327 ⁶
4.2	4.6	4.4
21		28

End wall End of wall

328 ¹	328 ²	327 ⁹	327 ¹	327 ⁷
3.3	3.8	5.0	4.9	4.6
3.75	9.0	9.0	5.2	7.0

End wall End wall

326 ¹	326 ⁸	328 ¹	327 ⁷
5.3	5.7	3.9	4.3
	2.3	2.3	10

End wall End wall

332.04

Levels with transit by flashlight.

Error in culvert 0.13

S.W. O.P. N1/2
+ U710.

7.14 322.28 (322.15)

Sewer M.H. (Page 60)

T.P. 3.33 329.42 8.26 326.09

T.P. 6.48 334.35 11.45 327.87

T.P. 11.52 339.32 — 327.90

Arrow

8+59.87 ~~cross~~, top of 36" pipe 1.47 327.80

See plans for location?

8+58.87 INVERT 36" CONC. pipe Δ Approx. 27° RT.

8+35.87 Δ 19° 28' RT.

T.P. 4.35 329.27 7.26 324.92

7+80

322.18

315.98
320.84
13.44 2.58
INVERT R/W
329.42

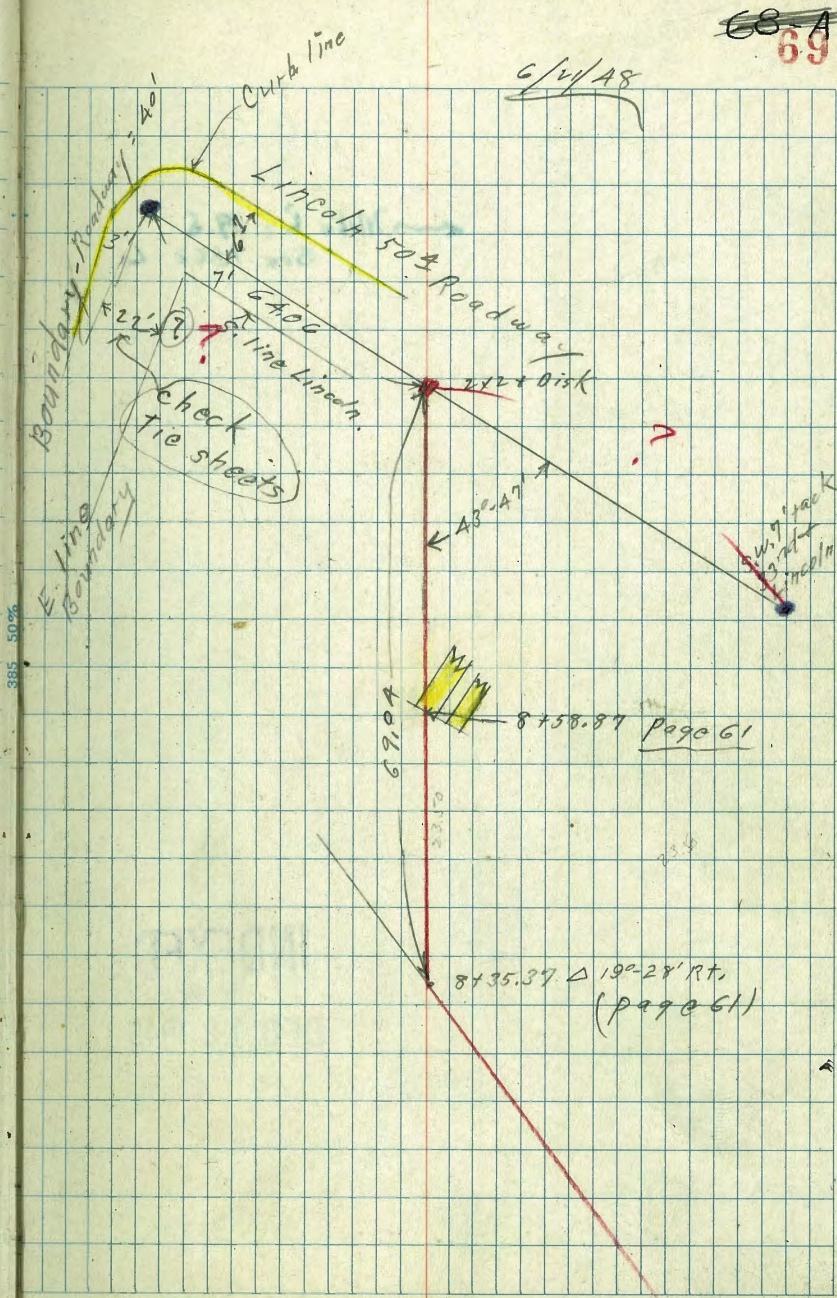
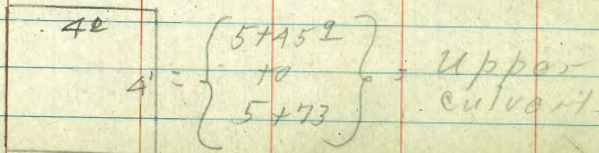
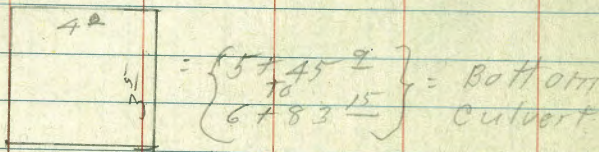
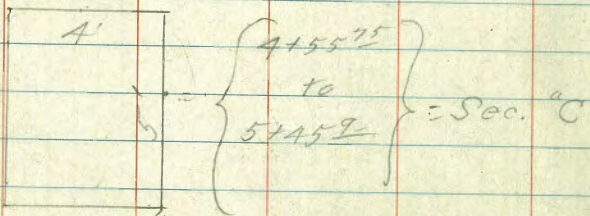
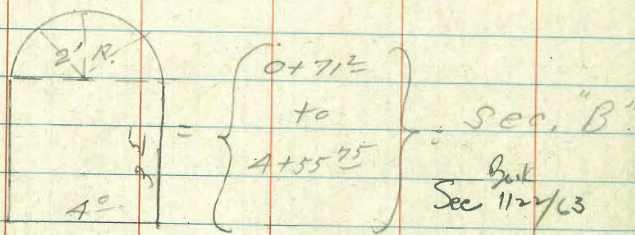
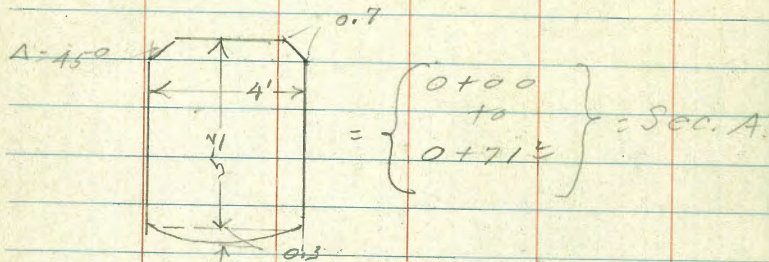
320.8	321.7	324.47	324.37	324.6	329.27
0.5	4.5	4.80	4.90	4.7	0.0
7	2	Invert 36"	4.5 Invert 36"	6	7

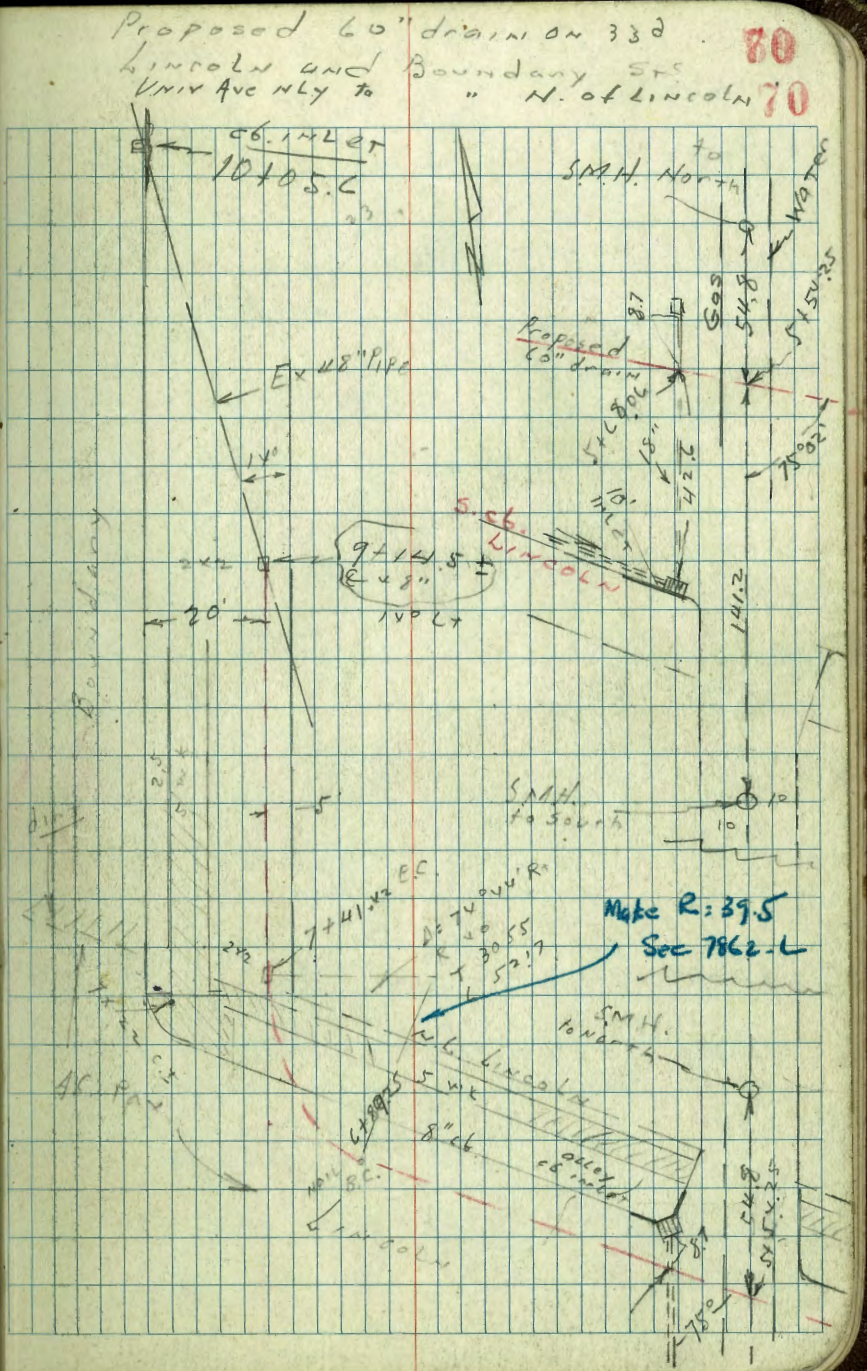
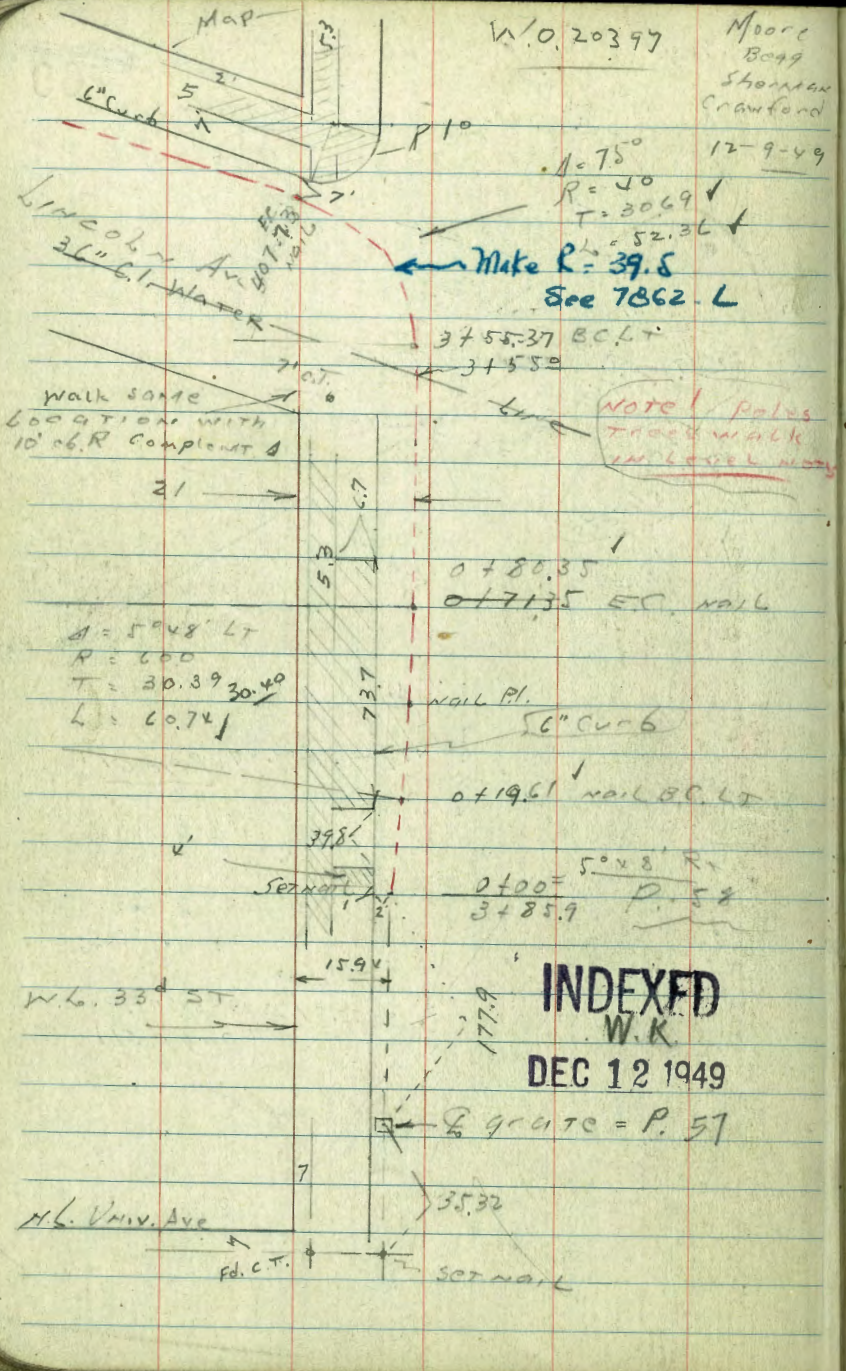
325.3	320.3	325.3	324.8	324.8	327.3
4.0	0.0	4.0	4.5	4.5	4.80
20	15	15	7	7	20
			329.27		

329.4	323.8	323.0	323.5	327.6
2.8	8.4	9.2	8.7	4.6
15	2		2	12

322.18

Internal Sections





Levels Proposed drain

1796 E 3' Con walk Back of Comb

1781 E 7' Con do.

1769 8.5 LT PP 2960

1750

1700

078035 EC

0776 11 LT 14" ACASIA

0150

741 9 LT 12" ACASIA

071961 BC LT

718.5 4.5 LT 12" d ACASIA

0700

T.P.	560	333.31	1.88	327.71
SWBP	7.40	329.59		322.15 ✓
WAIN				
MILE				

Lr

E

Rr

71
71

2.31	2.91	2.34	
2.8	2.8		
0.5			
3.5	3.5	2.97	3.102
2.9	2.9		2.79
0.6			10
328.99	328.27	328.95	329.63
4.3	4.5	4.3	2.58
1.9	1.9		10
0.6			
327.11	326.41	327.13	327.63
0.7	0.5	0.8	5.58
0.7	0.7		10
326.63	326.03	326.57	327.15
0.8	2.8	0.77	0.1
0.6	0.7		10
326.21	325.47	325.96	326.57
7.10	7.8	7.35	6.7
0.4	0.4		10
0.6	0.7		
325.56	324.96	325.26	325.95
7.75	8.35	8.05	7.34
0.4	0.4		10
0.6	0.7		
325.53	324.74	324.8	325.51
7.78	8.57	8.5	7.80
0.2	0.2		10
0.6	0.7		

333.31
Under Cam ✓

3+5537 BC LT

LT
4.47 337.59
10
337.91
15
338.21
15+
3.79
10

3+55 Cross 30" CIW

3+29 BC Per LT

336.91
15
336.01
15
336.97
10
337.79
10
4.27

+28.5 90 LT PF 3998

3+10

336.12
5.94
7
335.49
6.57
70
5.89
336.17
505
70
337.01
5.05
70

2+50 2 7' Cow Ln

332.90
7.20
97
333.48
858
334.30
2.70
70

2+38 10.8 LT 8" Acacia

2+34 6.8 LT 3' walk back cb

T.P. 9.9 342.06 0.44 332.87

3 x 2.06

2+24 10.8 LT 8" Acacia

2+00

331.26
2.02
6.8
330.65
6.8
2.10
331.21
70
331.92
333.31

333.31

72
72

T.P 6.4v 343.55 v 95 337.11

See 845

5+54.25 / N - Ex Sowers
see water E Alley

4v37

5

4v50

x+07.73 EC

3+90.3

3+72.8

342.04

LT	E	RT
237.2 14.4 FL. MH	318.34 19.07 R. MH	336.71 5.33 FL. MH
5.28 10	5.33 10	5.38 8.7
4.99 10	5.09 10	5.08 9.2
4.79 10	4.81 10	4.90 7.6
4.55 10	4.66 10	4.71 9.7
4.32 10	4.35 10	4.38 10
4.15 10	4.87 10	3.61 10
		342.06

73
73

T.P. B.P. 3.3
34640 047 34308 SW

6+8925 BC RT

6+77 14" RT 14" PLUMOSA

6+67 14" RT 18" di. PLUMOSA

6+50

+49 13.6 Rose bush

+41 13.5 Rose bush

+25 13 RT 18" PLUMOSA FALM

6+00

+80 13' RT 20" di. ACACIA

5+6804 1/2" drain (18") CAN

34355

B.P. LINCOLN & Bdry 34315 MILLER
34310 MOORE

339.26
11.9
10
339.34
4.21
10.5
97
338.87
4.14
10.5
96
339.41
16" PLUMOSA
14.5

337.76
5.75
10
337.75
80
337.37
4.18
10
97
337.88
5.67
10
96

336.90
4.65
10
336.92
6.3
336.77
4.78
9.4
97
337.45
6.10
9.4
96

336.26
13.29
42.6
335.36
8.9
12.8
336.25
7.30
29
336.57
4.88
10
336.75
6.80
10
336.65
6.90
336.38
7.20
8.7
TOP GRATE
336.77
9.78
8.7
F.L. BOT BOV

34355

+ 50

8

+ 50

7+41.27 EC

7+33.8

7+28! s edge walk

7+191

7+15.33

346.40 ↓

LT

±

RT

75

x 9 341.4

5.4 340.9

5.3 341.0

5.4 340.93

5.37 341.03

5.50 340.90

340.50

5.90

10

6.03 340.57
70

340.04

6.32

97

6.45 339.95
97

340.64

5.76

97

6.71 339.69
97

340.28

6.17

89

66

10+056 TOP E C6 INLET approx.
12' opening

9+14.5 ± = 48" Pipe 14° Lt.
← This is about a 48"

9+00

8

76
79

332.07
14.33
FL.
48"
PIPE

342.94
B.XL
C6

342.02
4.38
9.7472

342.1
4.3

4.7 341.7

346.40 ✓

Notes Reduced - 12-12-49

77 78

A ledger page with horizontal blue lines and four vertical red margin lines. The page is blank.

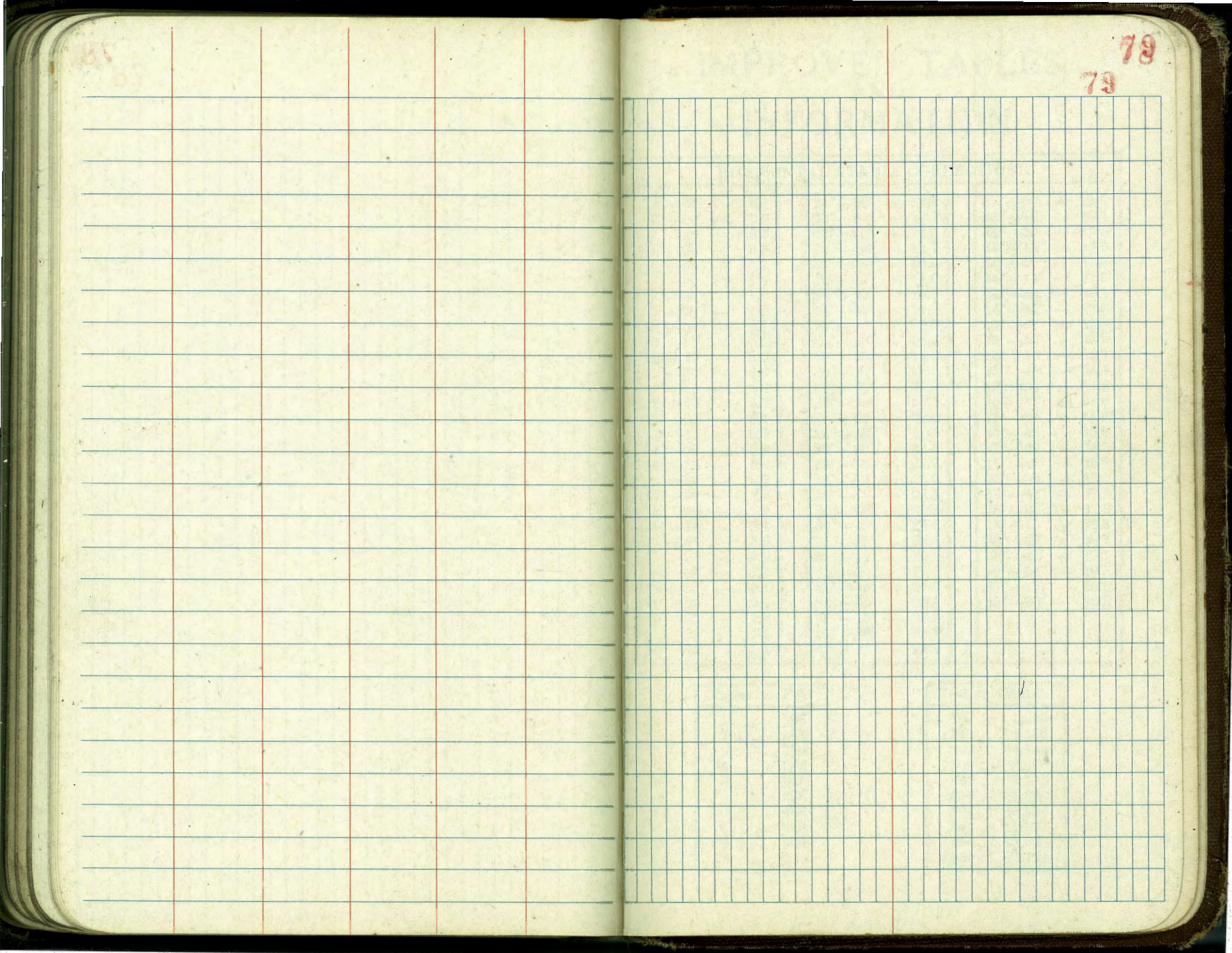
A ledger page with horizontal blue lines, a vertical red margin line, and a grid of 15 vertical blue lines. The page is blank.

77

78 78

A table with 5 columns and 20 rows. The columns are defined by vertical red lines. The first column is the widest, followed by three columns of equal width, and a final narrow column on the right. The rows are defined by horizontal blue lines.

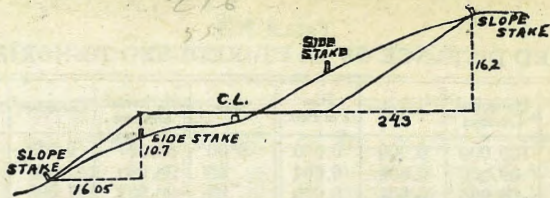
A table with 1 column and 20 rows. The column is defined by a vertical red line on the left. The rows are defined by horizontal blue lines. The entire page area is filled with a fine grid of blue lines.



79

79
79

A



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 60	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

6 05
4 26
1 85

2 0 6 3

12.74
32
12.42
271
1513

271 204
1202
1446

201.19
12.63
188.56

SE 18852

SW 19226

112°-30'±

0106
885
1253