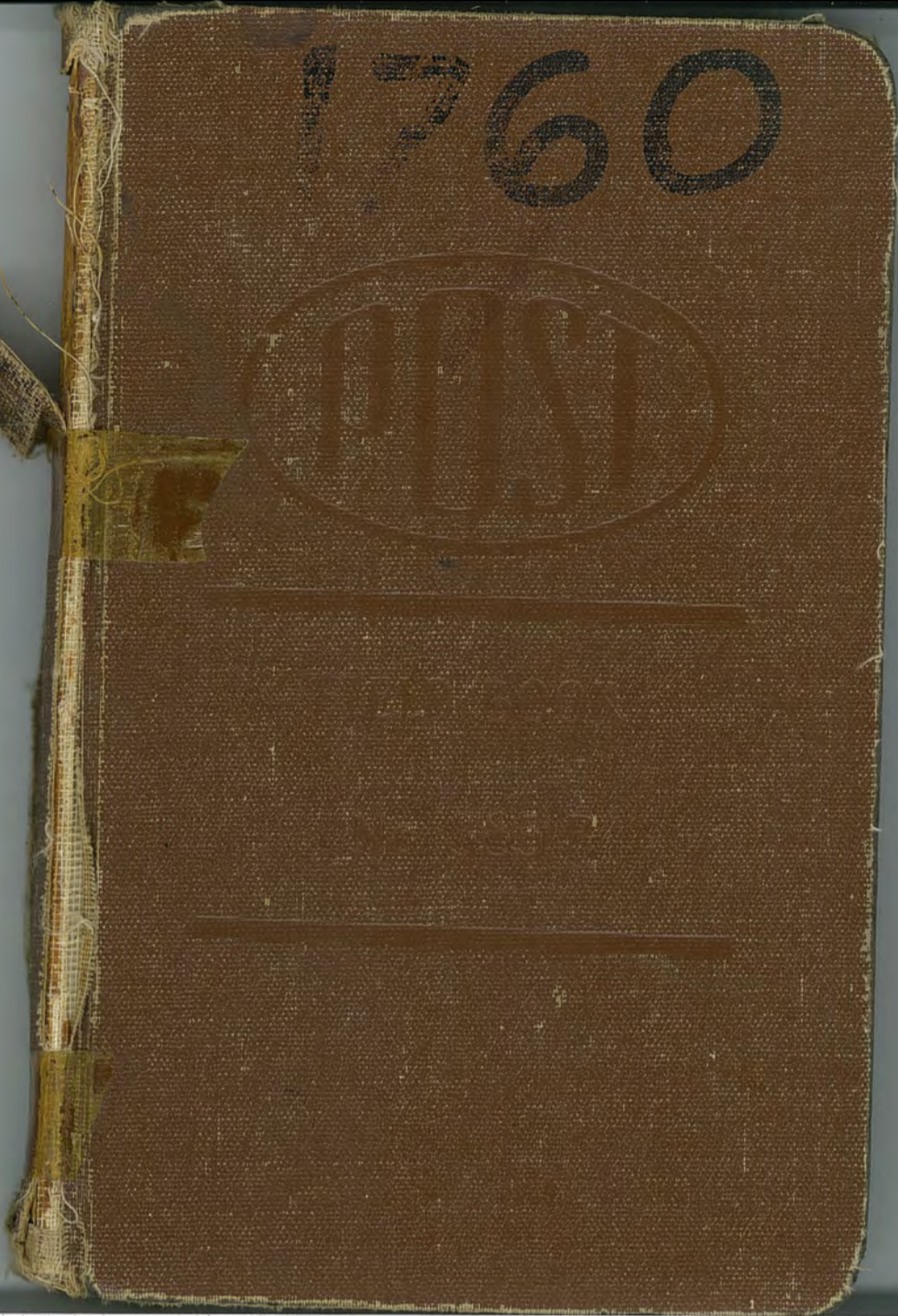


1760

1760



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CHICAGO

INDEXED

to page # 68

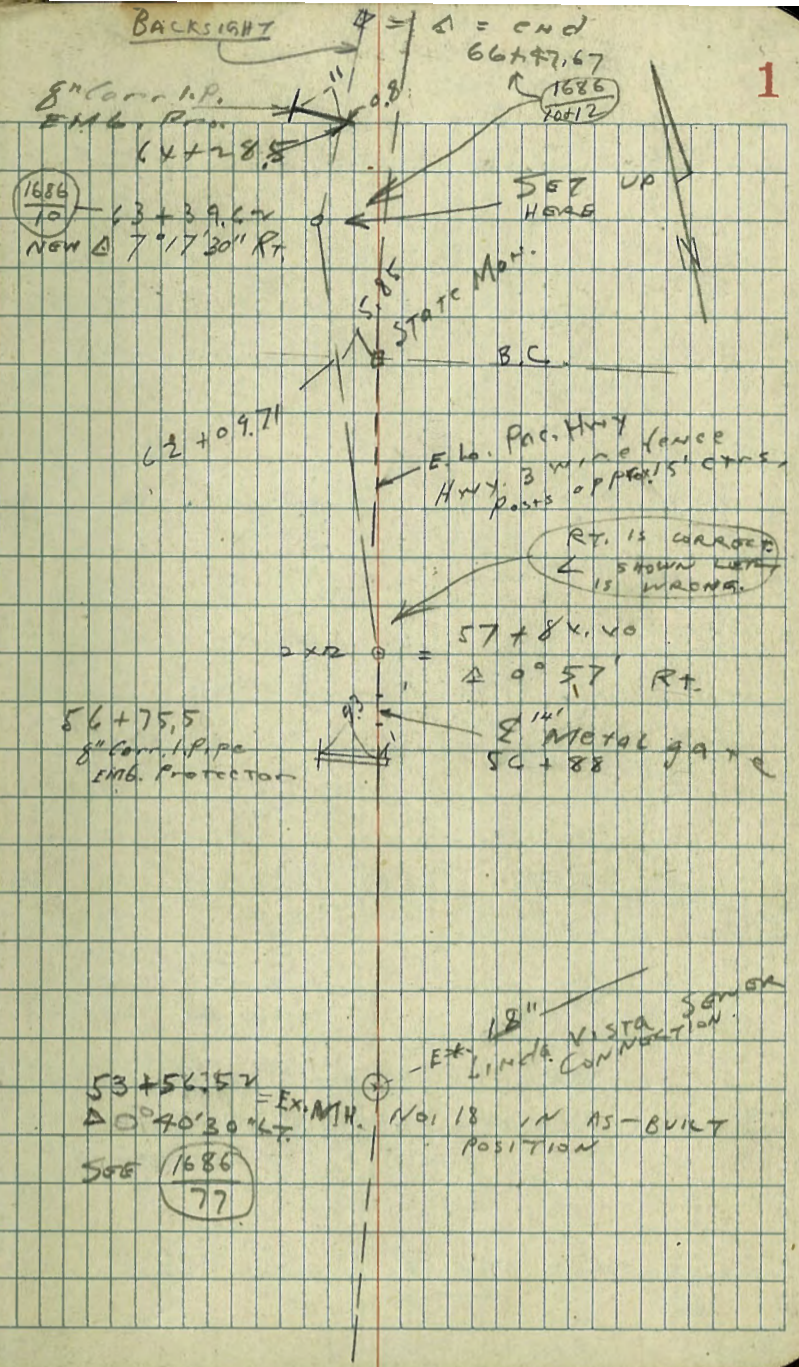
Trunk Sewer #2 P1 to

Survey City Line RPR/er
Balboa Ave at Pacific Hwy PLU

TRUNK SEWER #2 4/16/47
 Sewer Line Change
 Tecolote To Pac. Beach Line

H. Cole Director
 C. Moore Notes
 SIMPLYX Inst
 W. Moore Chain
 E 1399

INDEXED
 W.K.
 NOV 1 1949



56

LT	E		R			
EL. 3.67	3.6	3.9	-0.5	-0.9	-2.1	-2.3
3.50	3.0	3.3	7.7	8.1	9.3	9.5
18.5	17	10		5	7	15

2

+ 50

EL. 3.78	3.7	4.0	-0.9	-1.7	-2.0
3.39	3.5	3.7	8.1	8.9	9.2
18.7	13	10		8	15

55

EL. 3.89	3.7	4.0	-0.6	-1.7	-2.0
3.28	3.5	3.7	7.8	8.9	9.2
19x EP	13	10		8	15

+ 50

EL. 4.03	3.9	4.4	-0.3	-1.6	-1.9
3.14	3.3	3.8	7.5	8.8	9.1
20 E.P.	14	12		8	15

54

EL. 4.16	4.1	4.5	-0.3	5.7	?
3.01	3.1	3.7	7.5	15.4	
20.6 edge of shoulder	15	13		8	

ELEV.	3.11	-4.95	1.0
	4.06	11.62	6.3
	TOP	F.L.	9th.

53 + 56.52 EX. MH. Beg. Misplant ON SHOULDER ("Top")

B.M.B.P. 232 7.7 4.85

TOP F. Adm. STATE BAY CULV. OF 53 + 50

EL.	3.20	3.5	0.4	-1.5	RT -1.9	-2.5
	3.97	3.7	7.6	8.7	9.1	9.7
	16.2	8		3	8	15

EL.	3.22	3.5	-0.8	-1.8	-2.0	-2.4
	3.95	3.7	8.0	9.0	9.2	9.6
		7		2	9	15

EL.	3.35	3.4	0.2	-1.2	-2.0
	3.82	3.8	7.0	8.2	9.2
	17.2	9		7	15

EL.	3.37	3.3	3.4	2.2	-0.5
	3.80	3.9	3.8	5.0	7.7
	17	11	10		15

EL.	2.6				-0.9
	K.C				8.1
	13				F.L. outlet
	F.L. inlet				8" pipe

EL.	3.44	3.3	3.7	0.0	-0.8	-1.1
	3.73	3.9	3.5	7.7	8.0	8.3
	17.3	11	9		8	15

EL.	3.50	3.3	3.7	-0.7	-1.1	-1.7	-2.3
	3.67	3.9	3.5	7.9	8.3	8.9	9.5
	17	12	10		5	7	15

+60

+50

57

+94 wedge Heavy Ramp
with gate

+75.5 Imp. Prot.

+71

86 + 50

7.7

7.7

+50

EL	2.97	2.9	3.4	-0.8	-1.7	-2.6
	4.20	4.3	3.7	8.0	8.9	9.8
	16.5	10	8		3	15

+20

EL	3.07	3.1	-0.6	-1.7	-2.9
	4.10	4.1	7.8	8.9	10.1
	16.5	8		3	15

+08

EL	3.10	3.5	1.9	0.1	-2.2
	4.07	3.7	5.3	7.1	9.4
	16.2	7		8	15

58

EL	3.10	3.4	2.2	1.6	
	4.07	3.8	5.0	5.0	
	16.1	7		15	

57+844 Δ = 0° 57' RT. = on Pump

EL	3.13	3.3	2.4	1.9	1.7
	4.04	3.9	4.8	5.3	5.5
	10.1	7		8	15

57+70

EL	3.17	3.4	1.9	0.1	-0.9
	4.00	3.8	5.3	7.1	8.1
	16	7		8	15
	E.P.				

7.7

7.7

L + £ P +

+50

EL.	2.55	2.5	2.9	-0.9	-1.4	-1.8
	5.39	5.4	5.0	8.8	9.7	9.7
	18	11	10		2	15

61

EL.	2.52	2.4	2.9	-1.0	-1.7	-2.0
	5.42	5.5	5.0	8.9	9.6	9.9
	17.8	11	9		3	15

+50

EL.	2.55	2.5	3.0	-1.3	-2.2	-2.7
	5.39	5.4	4.9	9.2	10.1	10.5
	17.5	11	9		3	15

T.P. 548 2.94 471 2.46

60

EL.	2.62	2.5	2.9	-1.6	-2.7	-2.8
	4.55	4.7	4.3	8.8	9.9	10.0
	17	11	9		3	15

+50

EL.	2.73	2.6	3.0	-1.9	-2.6	-2.6
	4.44	4.6	4.2	9.1	9.8	9.8
	16.8	11	9		2	15

59+00

EL.	2.87	2.8	3.3	-0.8	-2.5	-2.9
	4.30	4.4	3.9	8.0	9.7	10.1
	16.8	11	9		2	15

Edge Pav.

1.7

1.7

+28,5 8" Emb. Prot.

EL	2.19										-3.13
	<u>5.80</u>										<u>11.07</u>
	11										<u>5.8</u>
	FL										FL
EL	3.19	3.1	-1.9	-2.0							
	<u>4.75</u>	<u>4.8</u>	<u>9.8</u>	<u>9.9</u>							
	18.5	10		15							
EL	3.10	3.0	3.3	-0.5	-2.0	-2.1					
	<u>4.8x</u>	<u>4.9</u>	<u>4.5</u>	<u>8x</u>	<u>9.9</u>	<u>10.0</u>					
	15.1	9	7		x	15					
EL	3.00	2.9	3.5	-0.3	-1.4	-2.2	-3.2				
	<u>4.9x</u>	<u>5.0</u>	<u>4.5</u>	<u>8x</u>	<u>9.5</u>	<u>10.1</u>	<u>11.1</u>				
	17	11	9		15	15	27				slough
EL	2.85	2.9	3.4	-0.8	-1.9	-2.5	-1.5				
	<u>5.9</u>	<u>5.0</u>	<u>4.5</u>	<u>8.7</u>	<u>9.8</u>	<u>10.4</u>	<u>9.4</u>				
	18.3	12	10		3	8	15				slough
EL	2.68	2.7	3.0	-0.9	-1.4	-1.8					
	<u>5.2x</u>	<u>5.2</u>	<u>4.9</u>	<u>8.8</u>	<u>9.3</u>	<u>9.7</u>					
	18.2	12	9		2	15					
	Pavichgc										

C4

+39.6 ~ old A

C3

+50

C2

79x

79x

check out 818 - 024 - 025
to BM

BM Top RR. from RR Cor
100' E of C2 + 50

(ICE)
+LS end of "A" PLANT
ON SHOULDER

EL 3.95	37	3.9	-2.4	-2.7	-2.8
3.99	42	4.0	10.3	10.6	10.7
35	27	23	9		15
edge Pan.					

66 - 47.67 old Δ Section split

EL 3.91	3.8	4.3	-0.9	-2.4	-2.4
4.03	4.1	3.6	8.8	10.3	10.3
15.6	9	7		5	15

66

EL 3.79	3.6	4.2	-2.0	-2.5	-2.5
4.15	4.3	3.7	9.9	10.4	10.4
18.6	13	10		4	15

65

EL 3.46	3.3	-2.2	-2.2	-2.2	
4.48	4.6	10.1	10.1	10.1	
20.5	11	2		15	

7.94

7.94

Trunk Sewer #2 W.O. # 155

Line change to
N side Barbosa Ave.
Pacific to Revolution.

Maere
JOHNSON

2-4-47

Barb

8

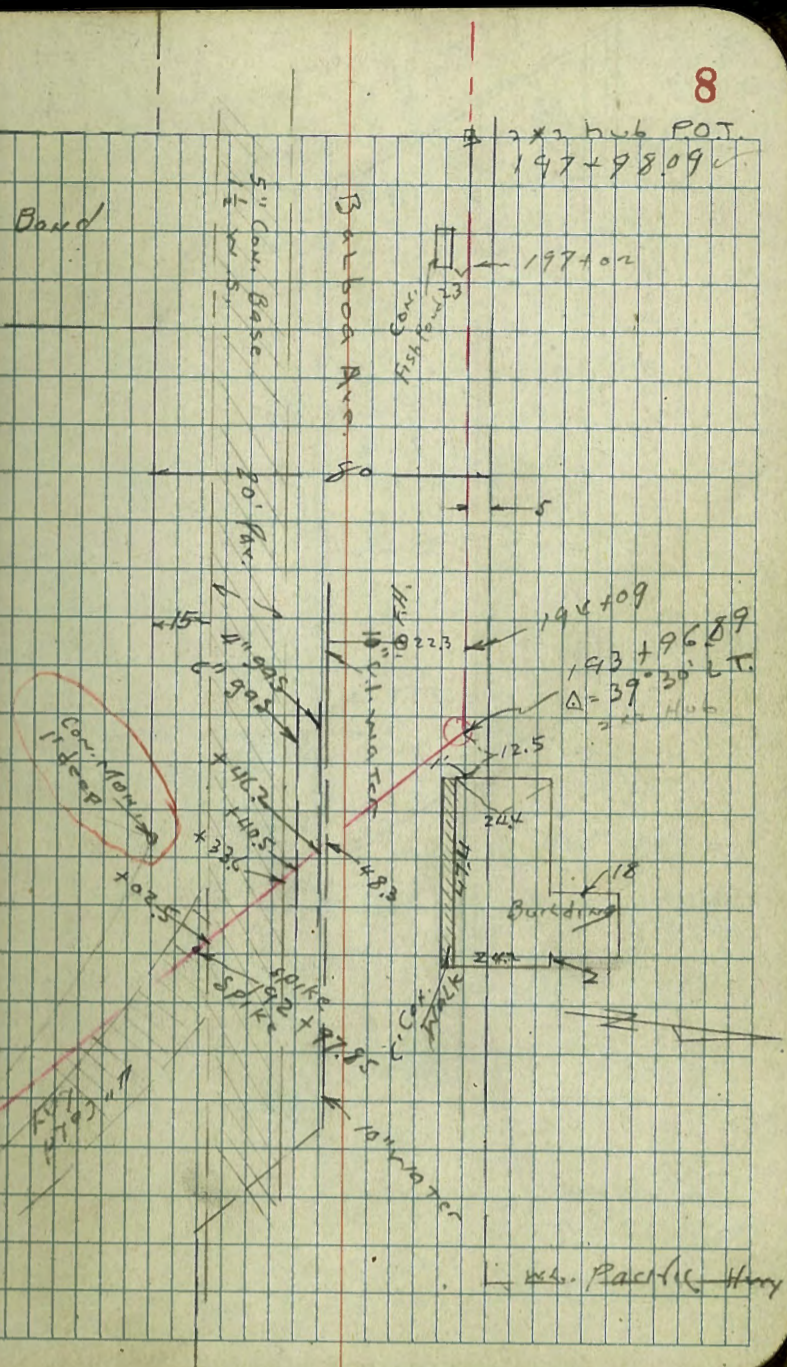
ch

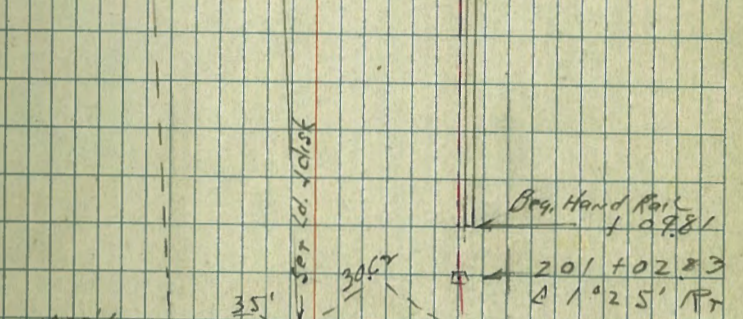
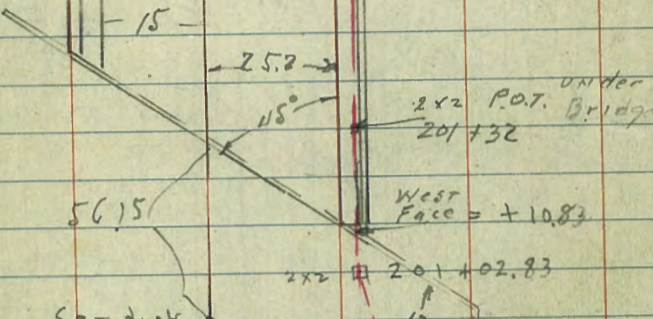
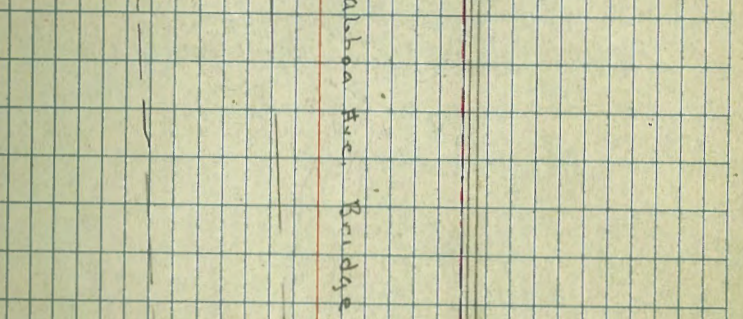
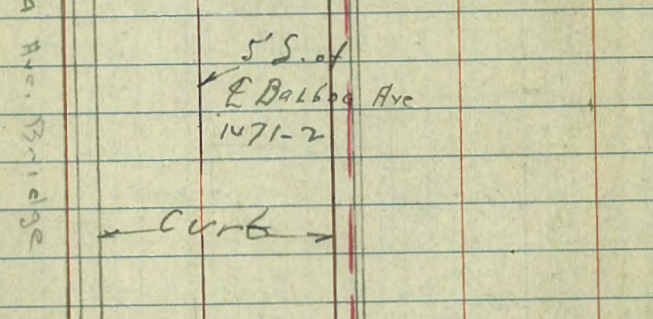
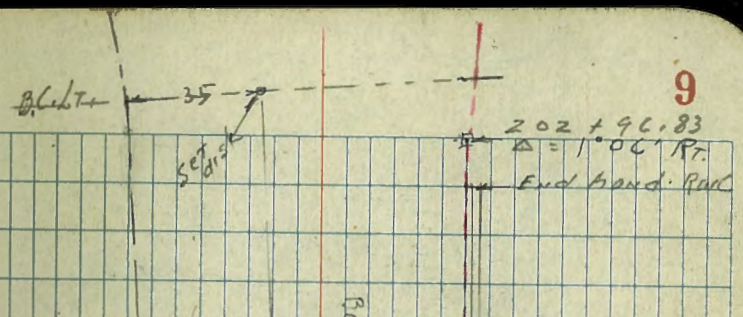
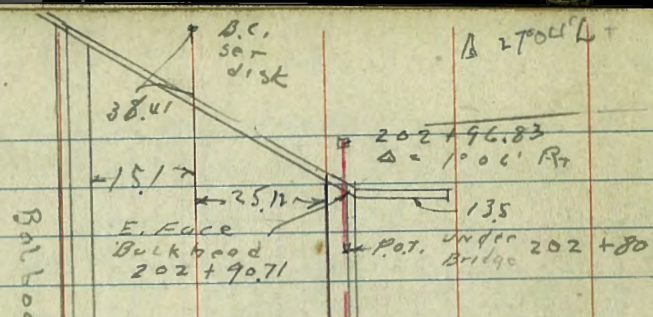
66

66

65

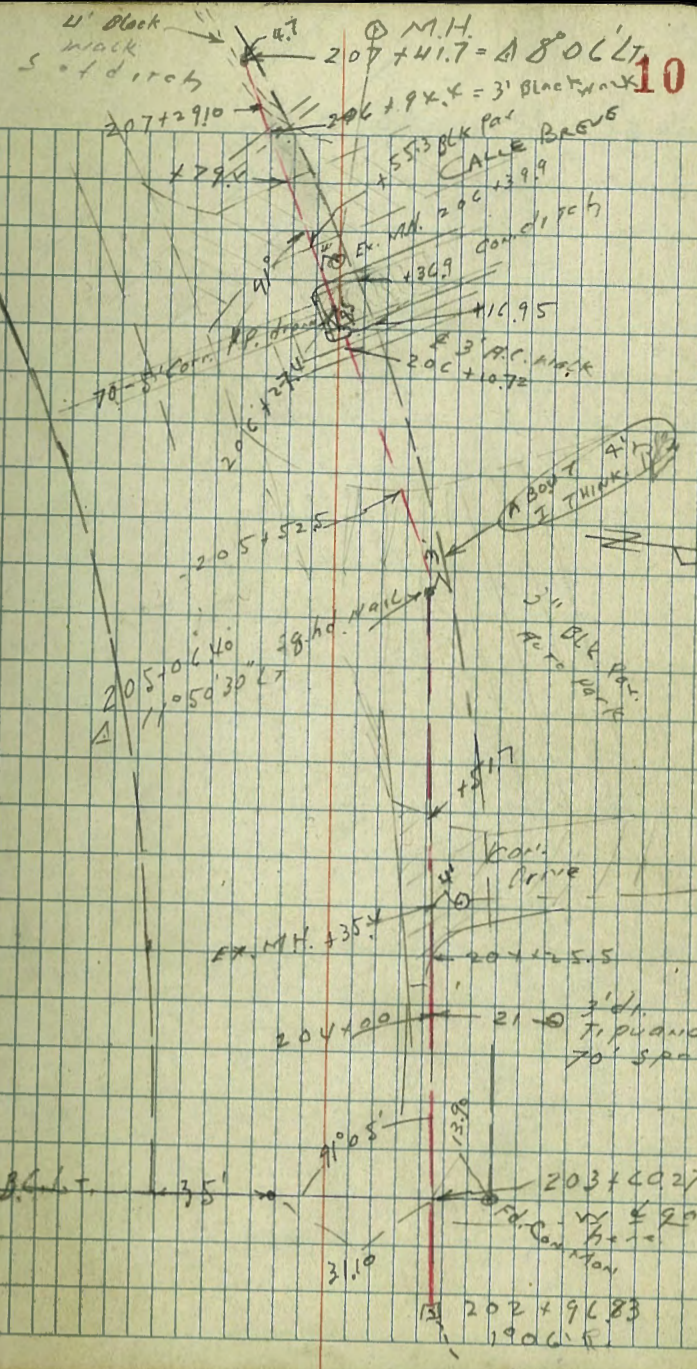
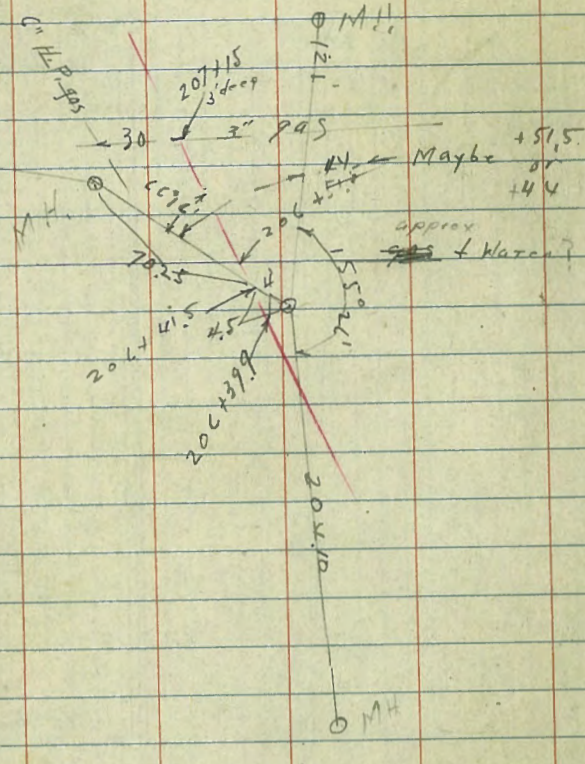
Note! at 192+45 Ed. wooden box?
top about 1' below
2" gas line. also check
this with gas Co.





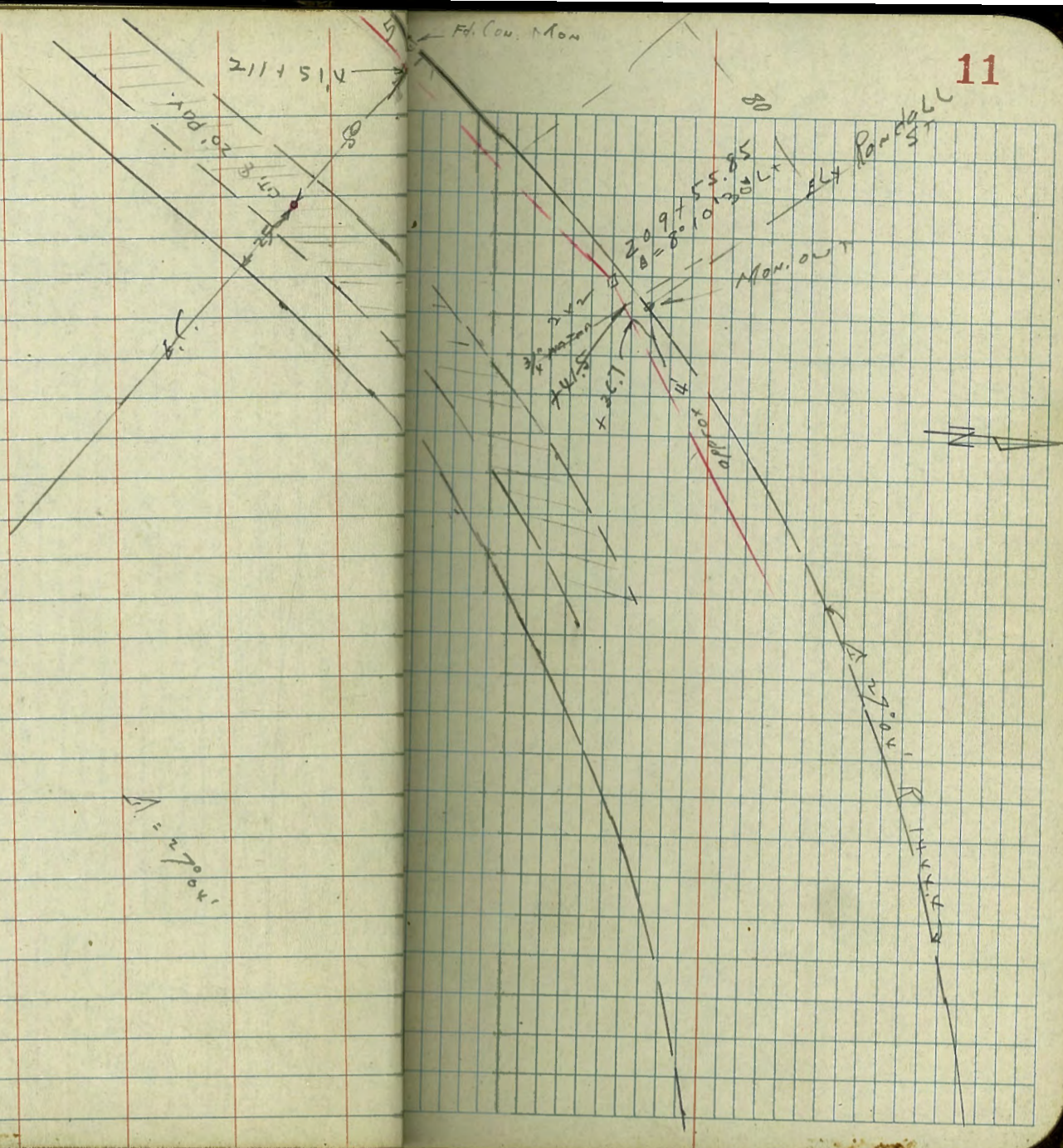
See page 39.

ch
66
66
65



Fd. Con. Non

211 + 514



Randall St

Mon. out



2700'

ch

66

66

65

5" Con. 1 1/2" W/S
Edge +77.8

edge Col Lay
+65.5
also 6" H.C. 945

2 x 2 @ 217+07.45

+6.17

89° 59'

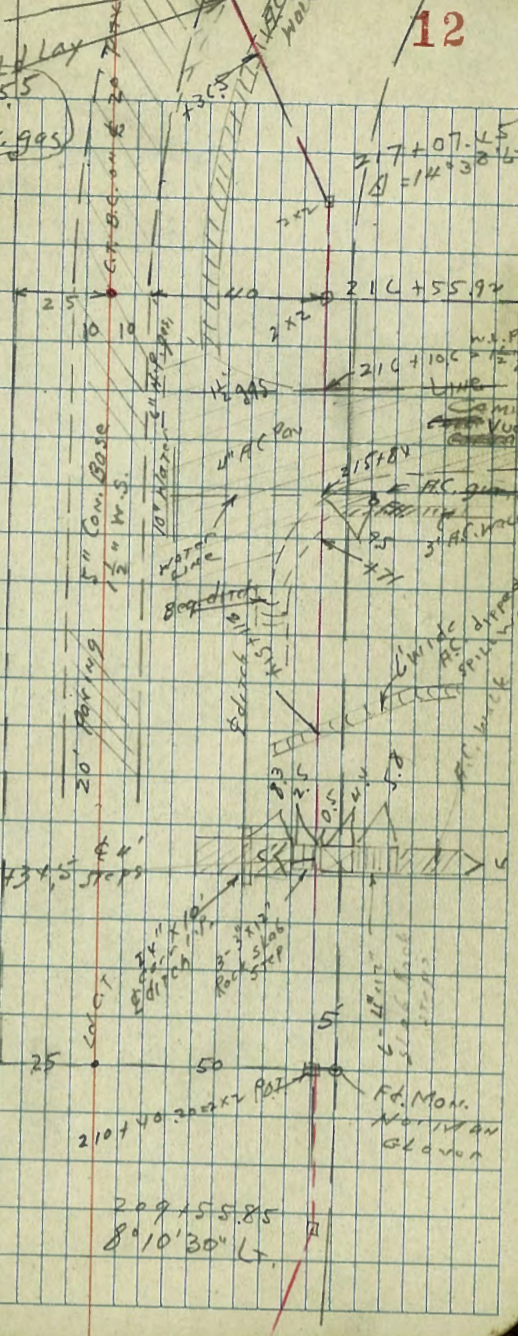
145.3

CAMINO PUERTO

See
for
F.I.

216+33.85

8' Proposed
Sewer



211434.5
steps

EC

210407.0
20955.85
84.25

210140.30 x 2
50

Rd. Mon.
North Van
Glover

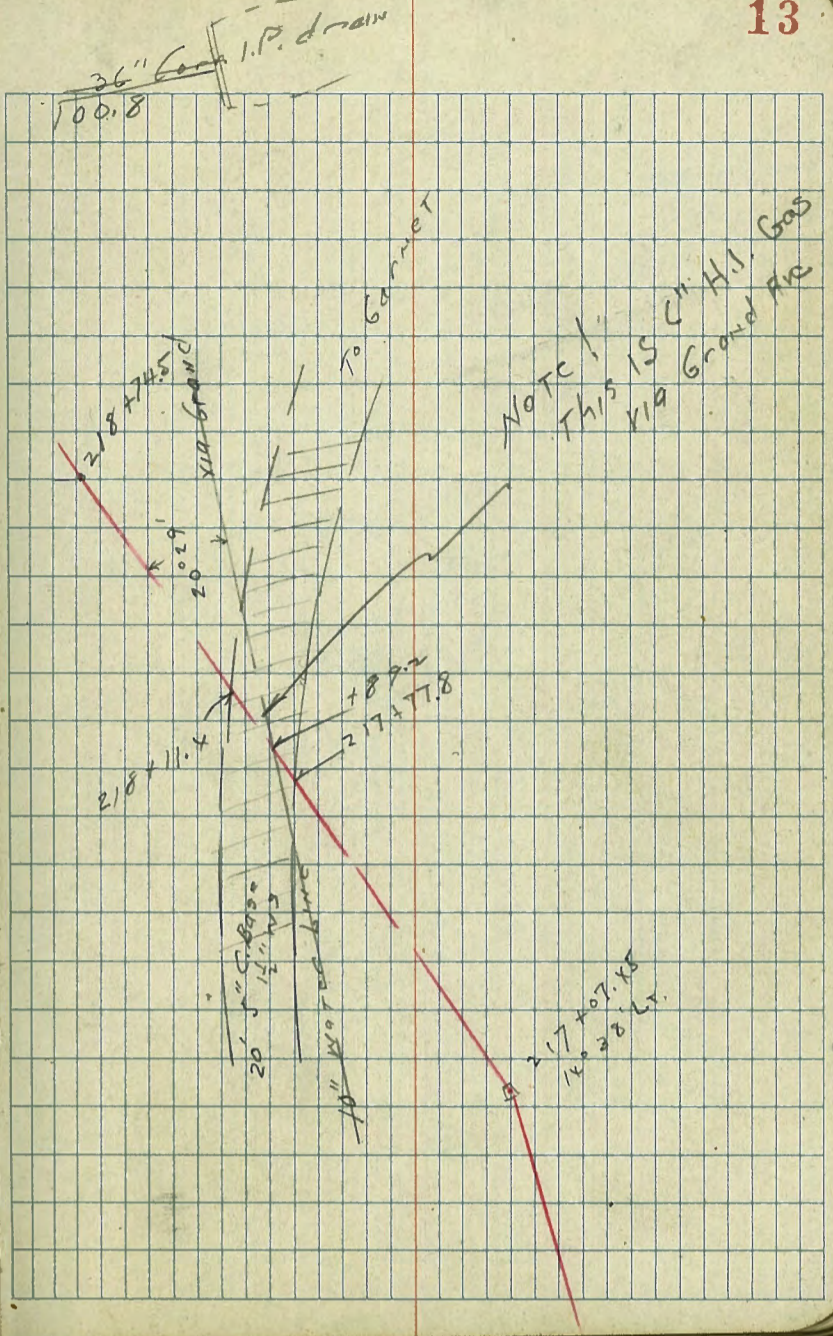
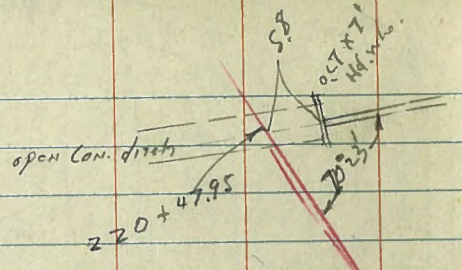
209155.85
8°10'30" LT

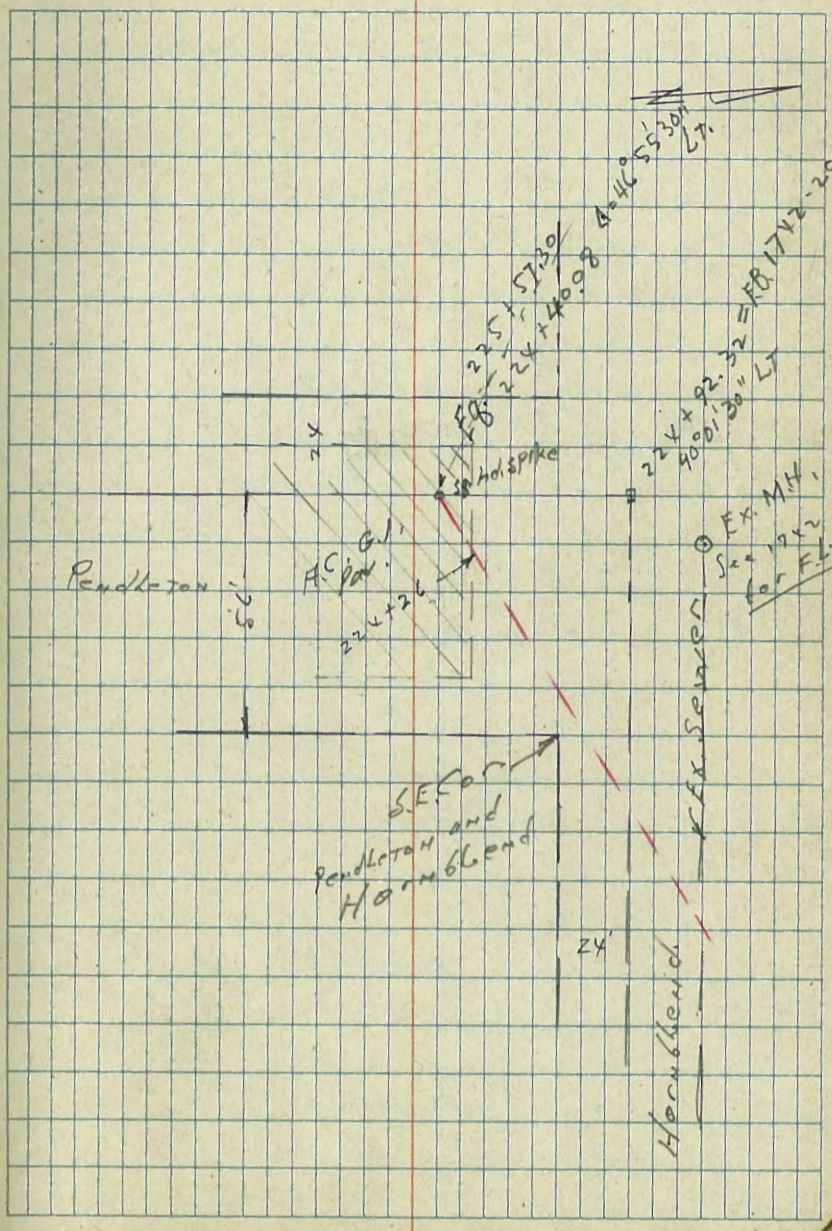
ch

cc

cc

LS





Sewer Levels Sketch P. 8

+483 = 10" CI Water Line

+462 4" H.I.P. gas (old line)

+405 6" H.I. Press. gas

+335 n edge Pav

+937 025 s edge Pav

+92+97,85 old 41 spike in Pav.

I.P.	3.90	17.71	13.81
Start		18.71	7.28
B.M. B-1	2.81	21.09	19.28
17+2-7			

Moore notes
Begg Level
Roberts
Green 1-10-46

EL. 13.9
10" gas in T 3.8
10.60
7.11
Top 10" water

EL. 13.9
3.8
10.60
7.11
Top 4" gas

EL. 13.71
4.0
10.71
7.00
Top 6" gas line

EL. 13.61
4.10

EL. 13.90
3.81

EL. 13.99
3.77

Correction
of Levels
P. 21
17.71
~~18.71~~

+50

+43 18.8 LT TEL P.

196

+68 5 LT TEL P. L

195 +50

198

+50

194 +19 4 LT TEL P.

193 +96.89 A

+70 8.5 LT P.P.

17.71
~~+8.71~~

EL. 11.0
1.7

EL. 11.3

1.4

EL. 12.0

5.7

EL. 12.1

5.4

EL. 12.4

5.3

EL. 12.8

4.9

EL. 13.5

4.2

17.71
~~+8.71~~

197+98.09 POT WL Bond

EL 9.7
8.0

+100

EL 10.0
7.7

+120

EL 12.8
4.9

+150

EL 12.2
5.5

+145 7' LT Tel P.

EL 10.1
7.5

+135

+115 7.5 ft 10" acacia tree

T.P. 6.51 17.69 11.08
18.49 6.63 12.08

EL 10.9
7.3

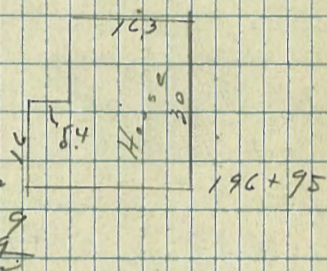
197

+81 11 Lt 15" Eucal tree

17.71
18.71

17.71
18.71

385 50%



200

+62 22 Rt 30° Eucal

+50

+17- 6' Lt Tel. P

199+02.83 Δ 2° 58' 30" Lt

+50

+40

+39 17 Rt 24° di Eucal

198+26

1769
1869

EL. 13.0

4.7

EL. 12.1

5.9

EL. 12.9

5.3

EL. 12.7

5.9

EL. 12.7

5.0

EL. 9.0

7.7

1769
1869

202

+70

+50

T.P. 0.55 ^{8.09} 4.09 10.15 ^{7.54} 8.54

201+10.83 mud

+9.81

201+02.83 $\lambda = 1^{\circ} 25' Pr$

+87 1.6 Pr Tol P.

+50

17.69
18.19

EL. 1.1
7.0

EL. 1.9
6.2

EL. 2.1
4.0

^{8.09}
~~9.09~~

EL. 6.7
11.0

EL. 13.84
Top edge \rightarrow 3.85

13.11
4.58
Top hdl

EL. 13.6
4.1

EL. 13.4
4.3

17.69
18.19

+10 2.3 Rt Tcl, P

203

202+96.83 A 1'00' Rt

202+90.71

T.P. 10.14 18.23 8.09
~~19.23~~ 0.00 ~~4.09~~

+90.71 MUD

+80 16 Rt 30" Eucal

+70 7 Rt 24 Eucal STIMP

+65

202+46

8.09
~~7.09~~

EL. 13.11 20
5.1

EL. 13.3
4.9

EL. 12.78 13.61
5.45
← TOP BK HD. 4.02
TOP EDWI

18.23
~~19.23~~

EL. 2.3
5.8

EL. 2.4
5.7

EL. 1.1
7.0

EL. 0.8
7.3
8.09
~~7.09~~

+25.5 Beg. Cov. da,

204

203 + 0.27

Now Resume Sewer Levels

sw B.P.	4.54	18.26	13.72
on curb			
Balboa			
Ave. Bridge			

error on 1st + Rod of 3.81 = should have been 2.81

State B.M.	2.81	2.109	18.28
level same			
setup			

Resume Levels

sw B.P.	4.51	13.72	13.72	0.00
check to Balboa Ave		14.70		
Bridge			100	
			error	
	18.23			
	19.23			

EL 12.88

5.38

EL 13.3

5.0

EL 13.7

4.6

18.26

Correction of Levels P.15

385 50%

206

+54 12 R+ Sd, Eucal

+52.5 end HC Pav

Loc A 11° 50' 30" LT,

205

+78 217.2' LT
14 LT Tel Pole

+51.7 end Con. and Beg HC Pav

+35.4

LT

EL 13.7

4.9

EL 13.31

4.95

EL 13.66

4.60 SRA

EL 13.59

4.57

EL 13.04

5.22

EL 12.92

5.38

12.70

5.54

14.24
14.24

4.05

14.21

14.21

14.21

14.21

14.21

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14.21

14.21

14.21

14.21

14.21

14.21

14.21

+27.4 E ditch

+24.5

+18 Shoulder of Main ditch

+17

+16.95 Top Cam Curved b/w

20041072 9 3' AC walk

1826

EL 13.53	941	4.62	5.71
4.73	13.85	13.44	12.55
4	3.85		25 - E ditch
4" top	4.61 5'		
4" b/w	inlet		

EL 9.91

8.35

EL 9.98

8.28

EL 10.21

8.05

EL 13.64

4.62

EL 13.56

4.70

1826

+553 Black Pay

EL. 12.90
5.36

+44 Maybe C.I. Waterline
Size?

+39.9

EL. 13.3 13.12 3.52
5.0 5.1x 14.7x
4 4
M.H. F.L.M.H.P.
R.M.

+369 Top covered 4' dink

EL. 13.52
4.74

+37

EL. 10.35
7.91

+34

EL. 10.12
8.1x

206 +30.8

EL. ~~9.63~~
~~7.89~~

+30.4

EL. 4.92
13.34
18.75

18.25

+29/0 Beg. 4' wide AC walk
and storm ditch

T.P. 520 18.87 4.59 13.67

+15

207

+924 E 3' Blk walk

+794 edge Blk Pav

+67

18.26

EL. 13.55	13.57	10.67	10.67	12.3
532	5.30	8.70	8.70	6.0
	3.7	9	10.3	15

18.87

EL. 13.6

4.7

3" gas. line 3" deep

EL. 13.9

4.9

EL. 13.31

4.95

EL. 13.04

5.22

EL. 12.78

5.48

18.26

209 = end

208 + 70V

+75 9' LT DM, 17' LT PP, Guy Pole

+50

+15 15' RT - DM, 11' LT Tel. P.

208

+70.7

+47 4.5' LT - D.M., 19' LT Tel. P.

207 + 41.7 Δ 8' 0.6' LT. Sec on split

EL 13.17 13.16 11.97 11.47 12.39 13.01 P 26
5.70 5.71 7.40 7.40 6.48 5.86

12.3 8.3 4.5 2.5 1.5

EL. 12.88 12.91 11.37 11.31 11.37 13.07
5.99 5.96 7.50 7.56 7.50 5.80
9 5 1 1 5.7

EL. 12.76 12.76 11.41 11.16 11.16 12.73
6.11 6.11 7.46 7.7 7.7 6.14
7.5 3.5 7 2.3 7.3

EL. 12.98 12.99 12.52 11.01 11.01 12.73
5.89 5.88 6.35 7.86 7.86 6.44
5.7 1.3 3.4 5.9 10.3

EL. 13.17 13.24 10.90 10.90 12.75
5.70 5.63 7.97 7.97 6.12
4 6.5 11

EL. 13.44 13.50 13.5 10.72 10.72 12.5
5.43 5.37 5.4 8.15 8.15 6.4
7.5 15 6.3 8.2 12.6
Edge Walk 18.87

+32.5 E wk + steps

T.P. 7.15 22.00 4.02 14.85

EL 19.65

4.22

19.9

211

+514

210

EL 13.59

5.28

20.4

+55.85 Δ 8° 10' 30" LT

209 + 09

18.87

EL 19.32 16.57 18.00 18.43 18.60

7.68

5.43

4.00

3.57

3.40

25.5

2.5

0.5

4.9

middle

wreck

TOP

Landing

22.00

14.72 13.1 13.1 14.55 16.7

4.15 5.8 5.8 4.30 2.7

15.9 12.3 9.5 6.5

EL 15.2

3.7

EL 14.6

4.3

13.62 11.78 11.78 13.53 15.02

5.25 7.09 7.09 5.34 3.85 = 2x

16.4 12 10.5 7

EL 13.23 13.26 11.51 11.51 12.94

5.64 5.61 7.34 7.34 5.93

13.4 9.4 5.4 3.4

18.87

214 EL. 16.04

$$\begin{array}{r} 596 \\ \underline{2012} \end{array}$$

+50

213

+50

212

EL. 15.22

$$\begin{array}{r} 6.75 \\ \underline{19.25} \end{array}$$

211 + 514 E side spillway

22.00

16.08	19.70	19.70	15.74	16.6
592	730	730	620	54
15.7	110	97	59	

EL. 16.7

5.3

EL. 17.6

4.4

EL. 18.2

3.8

15.07	13.75	13.75	15.28	18.0	21.9
6.93	8.25	8.25	6.72	4.0	0.1
13.5	12.7	9.7	5.9		8.4

EL. 17.2

4.8

22.00

L+ EL. 16.60 16.74 16.75 P+ 17.98
 5.40 5.55 5.75 4.02
 20 7 17 edge Pax

EL. 16.94 16.27 16.58 17.58
 5.50 5.73 5.42 4.44
 20 2 3.8 E 3' walk

EL. 17.15 16.33 16.20 17.45
 4.85 5.47 5.80 4.65
 21 15 4.7 edge
 direct paved direct

EL. 17.27 16.0 16.0 16.90 17.5
 4.73 6.0 4.0 5.10 4.5
 20.5 14 8.0 1.5
 direct

EL. 17.1
 4.9

EL. 16.9
 5.1

EL. 16.3
 5.7

2200

+84

+75, 3

+71

+50

+50

315

214 + 50

2200

+30.5 E 3' H.C. WALK

217 +07.45 Δ 1x° 38' Lt

+55.92

+13.83 Int Gen Sewer

+10.5 wedge Pav. ↓ 1/2 gas 30' deep

216

T.P. 7.11 26.34 277 19.23
 Top CTR
 NUT ON
 G.I.P.H. 22.00

EL 21.72
11.62

EL 20.99
535 2x

EL 19.7
11

EL 17.39	21.74	15.62
90	460	10.72
	<u>145.3</u>	185.3
	R.M.	R.L.
	M.H.	

EL 17.24
910

EL 16.95
939

26.34

←

+11.4

218

+89.2 INT. WATER

10"

+77.8

+15.5

217 +51

2634

EL 23.76

2.58

EL 23.19

3.15

EL 22.61

3.73

EL 21.99

4.35

EL 21.11

5.2

EL 22.0

4.3

2634

¢

+35

EL. 19.0

7.3

+33

EL. 21.3

5.0

220

EL. 21.8

4.5

+50

EL. 20.8

5.5

219

EL. 21.6

4.7

+50

EL. 23.0

3.3

2634

26.34

+57

EL. 20.6

5.7

+52 Wedge Can ditch

EL. 18.82

7.52

+50

EL. 16.90

9.44

220+4775 E ditch 1/3' Canal P. down
Δ 70° 23' see sketch
P. 13

EL. 16.79

16.99

20.93

9.55

9.35

5.41

5.8

5.8

EL. 3' pipe to wall

+46

EL. 17.03

9.31

220+429 Can. Broken

EL. 18.1

8.7

26.34

26.34

385 50%

←

EL. 22.1

4.6

EL. 21.9

4.8

EL. 21.1

5.6

EL. 20.5

6.7

EL. 19.6

7.1

EL. 19.7

7.0

24.65

+50

223

+50

222

+50

221

T.P. 5.71 26.65 5x0 20.94

26.74

check to old stub 2.89 23.76 23.76
~~224.92.32~~
F. Bk. 1742-27 002

$225 + 57.30$
 $224 + 40.08 = \text{Eq. } \Delta \quad \angle \quad 46^\circ 55' 30'' \text{ LT.}$

to Beg. Pav.

224

24.65

EL. 23.07

3.58
to Beg. Pav.

EL. 22.87

3.78

EL. 23.0

3.7

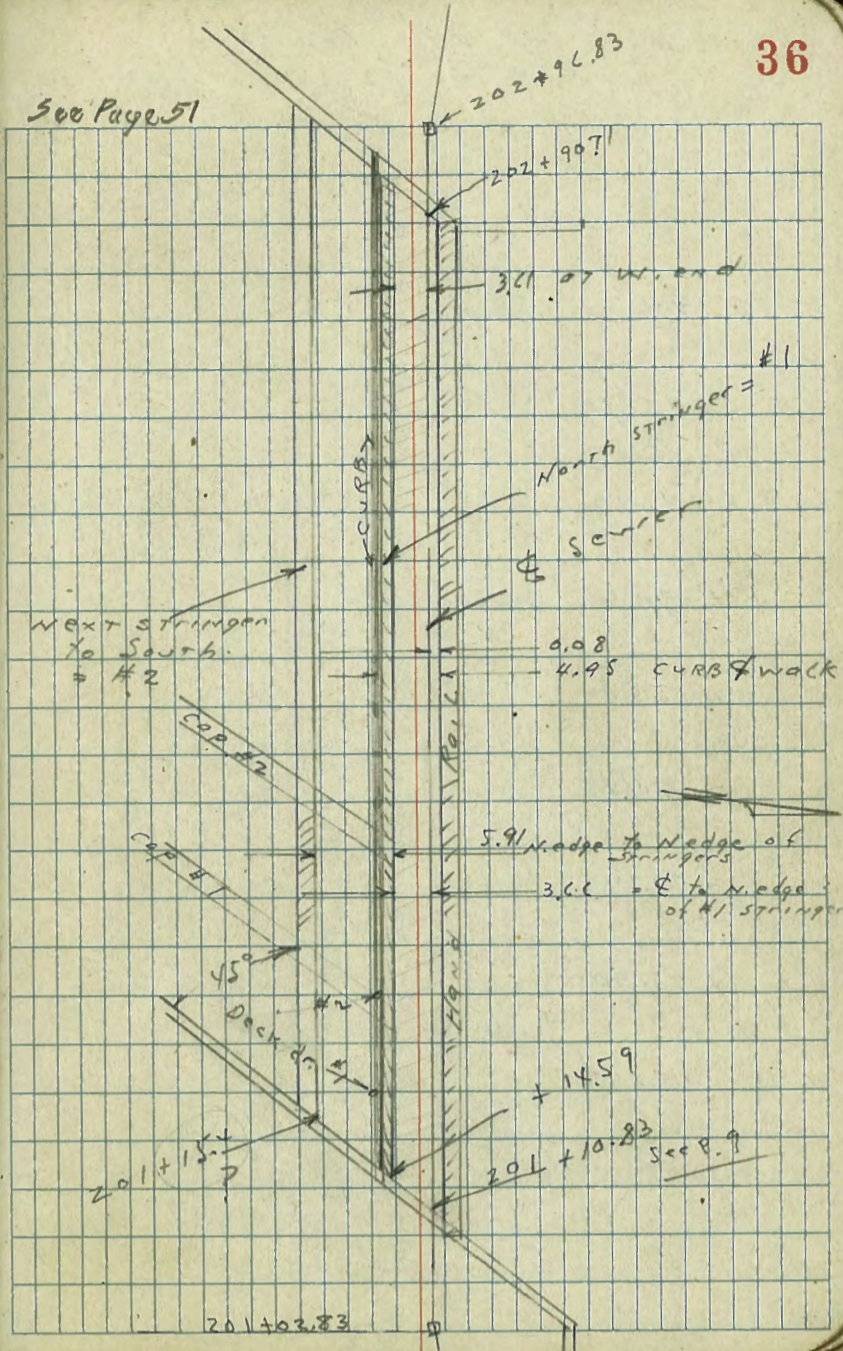
24.65

Stra. of 4" deck drains
on curb line

Moore
Beig
Roberts
Green
2-13-57

+30.10 #11	
+20.85 #10	
+10.5 #9	
202 + 0.0 #8	202 + 96.10 #17
+92.23 #7	+81.70 #16
+83.4 #6	+70.90 #15
+68.7 #5	+60.65 #14
+58.23 #4	+51.55 #13
+49.23 #3	202 + 41.65 = #12
+35.13 #2	
201 + 25.23 = #1 Vent drain	

See Page 51



Sta. of sdw. Brackets
E to E of 12" wide Brackets

202 + 19.63 Single

+ 5.70

double

202 + 04.42

201 + 90.00 Single

+ 75.80

double

+ 74.55

+ 60.79 Single

double } + 45.90

Brackets } + 43.89

+ 30.28 Single

201 + 15.54 = Ely Bracket Single

385 50%

202 + 80.10 Single

+ 6.57

double

+ 64.51

202 + 50.11 Single Bracket

202 + 35.80

double

202 + 34.50

Sta. on N. edge of
#1 Stringer = Most Nly
at Caps Stringer

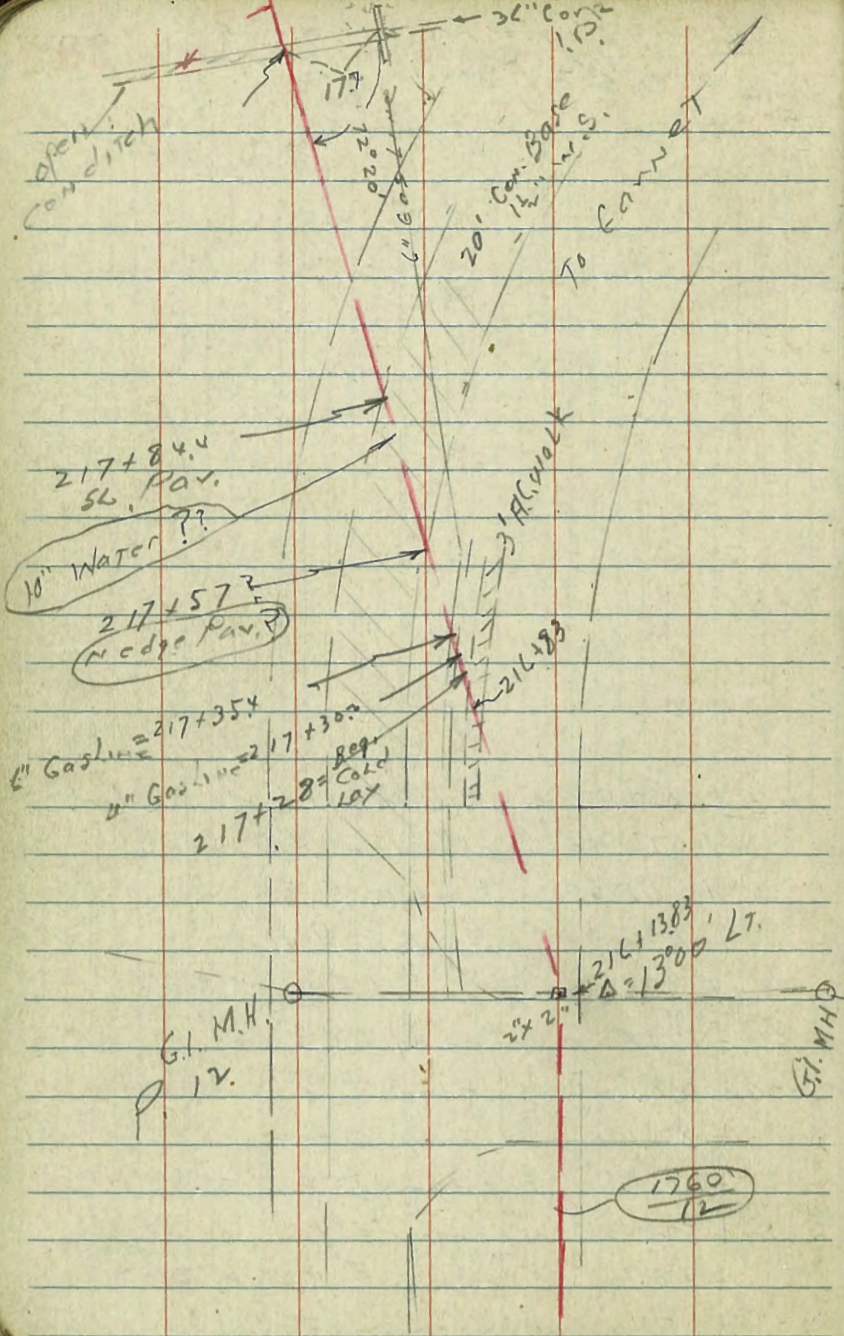
1.75 = width of Stringers

207 + 94.35 = E. face of W. Bulkhead
+ 66.25 W edge #5 Cap
+ 62.82 E edge #5 Cap } Most
+ 36.38 W edge #4 } WLY
+ 32.78 E edge #4
+ 06.20 W edge #3
202 + 02.71 E edge #3 Cap
+ 76.10 W edge #2
+ 72.80 E edge #2
+ 46.28 = W edge #1
+ 42.81 = E edge #1 Cap
201 + 14.59 = W. face of E Bulkhead

Sta. on N. edge of
#2 Stringer
at Caps

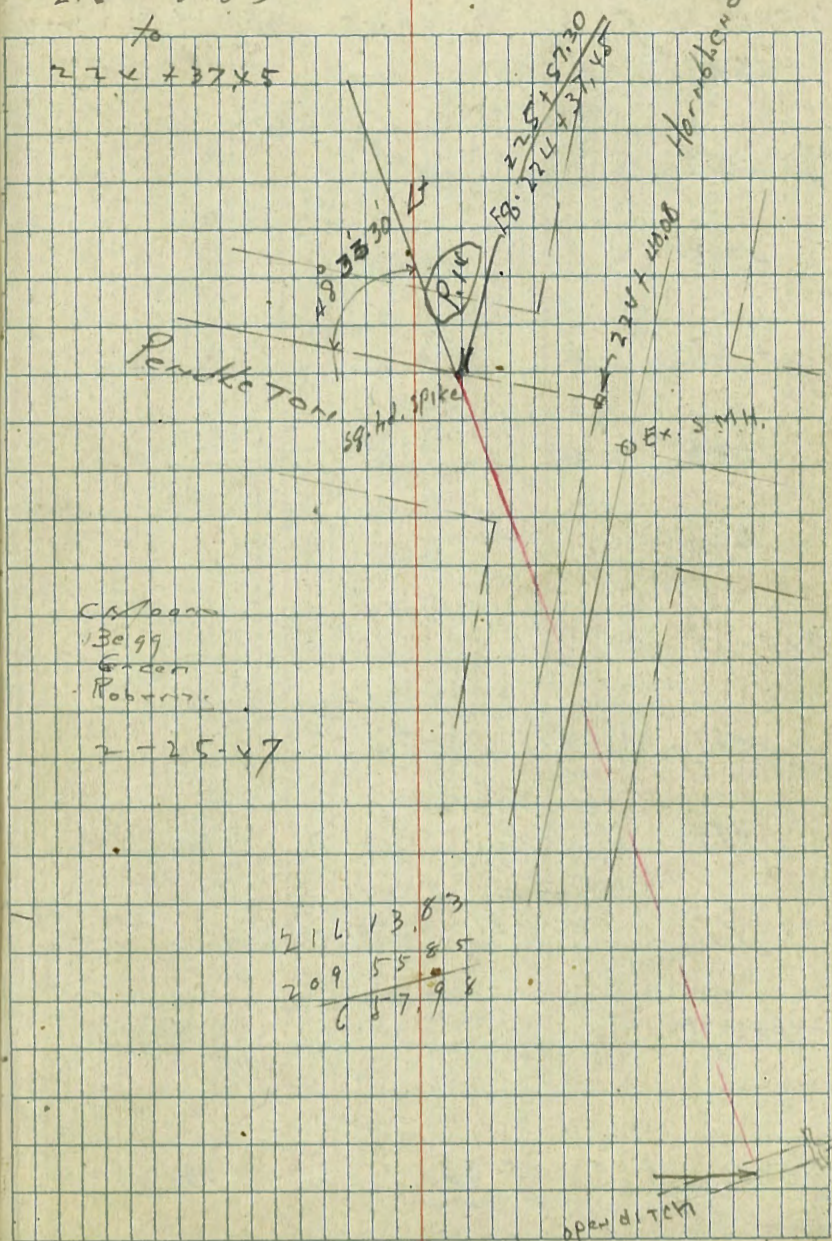
38

203 + 00.42 E. face of W. Bulkhead
+ 72.12 W edge #5 Cap
+ 68.55 E edge #5
+ 42.99 W edge #4
+ 38.62 E edge #4
+ 12.15 W edge #3
207 + 08.60 E edge #3
+ 82.10 W edge #2
+ 78.55 E edge #2
+ 52.23 W edge #1
+ 48.70 E edge #1 Cap
201 + 15.46 W. face of E Bulkhead



Line change from P. 12
TRUNK SENSOR #2 THIS BK. 39

216+13.83
to
224+37.5



C. Adams
Beag
Green
Roberts

2-25-47

216 13.83
209 55.85
6 37.98

1760
12

	+	#1	-	El	
+ 57				EL 21.45	3.88 of 20 ft per also approx 10" Water
354				EL 20.31	5.02 6" Gas 34" to top of gas main
+ 30				EL 20.09	5.24 = 4" Gas
+ 28				EL 20.10	5.33 Begin Cold Lay
+ 24					30" El 7.5 ft
+ 14				EL 21.1	4.3
217 + 0				EL 20.7	4.6
+ 83				EL 20.3	5.0 23' AC Walk
+ 54					48" El 13 ft
216 + 50				EL 19.7	5.6
216 + 1383				EL 17.4	7.9 new orgic pt
Top str out 6-10	25.33		19.23	see p 30	25.33
00 GI FHyd					

220 +49 of conc ditch $\begin{matrix} 8.25 \\ \text{---} \\ 2.10 \end{matrix}$

+448 edge of conc ditch

220

+ 65

+ 50

+ 43

+34

219

1.16 23.61

TP 2.88 22.45

+50

218

217 +8A 4 \rightarrow Line of Paring
85.33

Rod EL.

7.19 16.42

5.10 18.51

3.7 19.9

3.1 20.5

4.1 19.5

4.8 18.8

3.9 19.7

2.6 21.0

23.61

3.2 22.1

2.30 23.03

3.56 22.77

25.33

$\frac{225+57.30}{224+37.45}$ + H1 -
 4.19 23.06 $\frac{23.07}{.001}$

224

+50

223

5.80 27.25

TP 2.16 21.45

+50

222

221+50

Head wall

221

+58

220+53.7

23.61

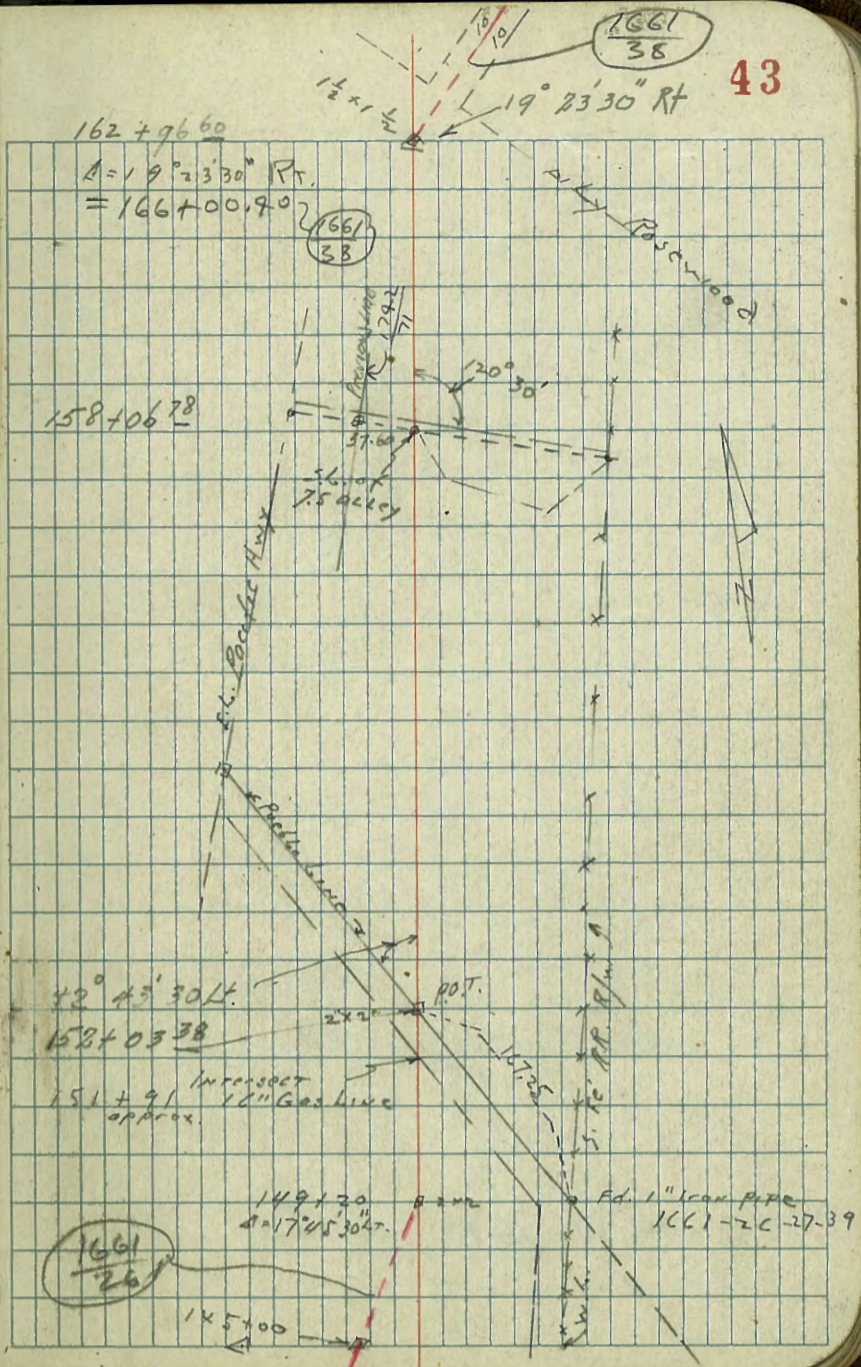
Page 35	4.19	23.06	nail in foot.
begin of oil	4.41	22.84	
	4.3	22.95	
	5.3	21.95	
	5.4	21.85	
	<u>27.25</u>		
	8.70	20.91	
	3.25	20.36	
	4.1	19.5	
	20.94		
	2.67	20.94	
	5.0	18.6	
	4.3	19.3	
	5.33	18.38	
	<u>23.61</u>		

TRUNK SEWER #2

LINE CHANGE #2 Sewer
W.O. #155

Sta. 149+20 to 166+00.00

C. J. Adams
B. G. G.
C. J. Adams
Roberts
2-26-47



Sewer Levels Sketch P. 43

	←	ROD	EL.
+ 78		6.5	10.3
+ 50		5.9	10.9
+ 22		7.3	9.5
+ 16		6.1	10.7
150		6.0	10.8
+ 50		5.9	10.9
149+20 A	17° 45' 30" LT.	5.16	11.64
TP 1 1/2 x 1/2 149+24 1.001-37	4.80	<u>16.80</u>	12.00
		<u>16.80</u>	

	HI	-		
92				
+74				
+60				
+44				
TP	11-01	<u>27.14</u>	0.67	16.13
+30				
151				
+80		<u>16.80</u>		

	ROD	EL.
	2.2	29.9
	4.0	23.1
	6.9	20.2
	9.7	17.4
	<u>37.14</u>	
	25	14.3
	45	12.3
	54	11.4
	<u>16.80</u>	

¢

Rad

Fl.

TP 1.77 18.80
10.11 17.03

154

9.0

18.1

+50

6.0

21.1

153

3.4

23.7

+83

Pepper tree 3 ft 12"

3.0

24.1

+50

1.6

25.5

152 + 03²⁸ POT on Pueblo line 2 x 2 hole

2.20

24.94

+91

gas line

2.1

25.0

27.14

27.14

£

ROD

EL

156

3.8

15.0

+50

4.1

14.7

155

3.9

14.9

+92

4.6

14.2

+89

7.6

11.2

+86

4.5

14.3

+76

3.8

15.5

15A

+50

7.2

16.6

18.80

18.80

	+	#1	-	E1
+50				
	6.01	<u>23.32</u>		
TP			1.49	17.31
157				
+60				
+32	6" Fig 1' Lt			
+27				
+22				
156 +16				
		<u>18.80</u>		

	<u>R₀₀</u>	<u>E_L</u>
	5.98	17.34
	<u>23.32</u>	
	8.1	16.7
	2.7	16.1
	3.4	15.4
	5.2	13.6
	4.0	14.8
	<u>18.80</u>	

E
Roe

EL

+50

5.9

17.4

161

4.9

18.4

+50

4.1

18.5

160

4.8

18.5

+50

4.8

18.5

159

4.4

18.9

+50

5.0

18.3

158+0675 POT mail

5.2

18.1

23.32

23.32

~~EL~~
Rep

~~EL~~

TP. on Meter Box 7.62 15.70 15.65

$\frac{162 + 96}{166 + 0042}$ ahead

$\frac{1661}{38}$

+83

8.48

17.84

+78

8.4

14.9

+75

10.4

12.9

+50

7.3

16.0

162

8.5

14.8

7.3

16.0

23 32

23 32

Levels on Bottoms of Girders
on Babcoo Ave. Bridge
See P. 9 and 36

check to orig. BM	3.91	13.70	13.72	
T.P.	12.65	17.61	0.62	4.96
202 + 78.04				
+ 62.04				
+ 46.04				
+ 30.04				
+ 18.04				
202 + 02.04				
+ 86.04				
T.P.	3.53	5.58	5.68	2.05
+ 70.04				
+ 58.04				
+ 42.04				
201 + 28.54				
B.M. B.P. Sw	0.22	7.73	8.75	7.51
Babcoo Ave Bridge	2.54	16.26	13.72	P. 21

Moore
5899, level W.O. #155
Green
4-9-47

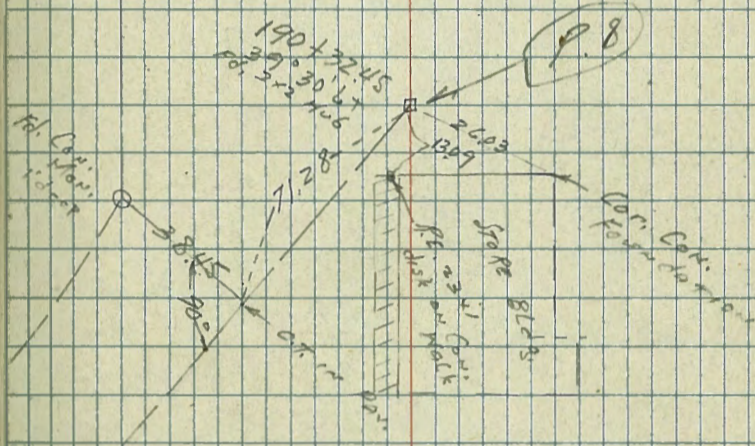
Indexed
C.S.K.

Next Sky #2 Girders	A1 Girders	Most likely done
10.05	9.96	
+ 4.47	+ 4.38	
10.10	10.05	
+ 4.52	+ 4.47	
10.10	10.03	
+ 4.52	+ 4.45	
10.08	10.03	
+ 4.50	+ 4.44	
10.12	10.02	
+ 4.54	+ 4.44	
10.11	10.11	
+ 4.53	+ 4.53	
10.22	10.11	
+ 4.64	+ 4.53	
10.20	5.58	10.20
+ 2.47		+ 2.47
10.22		10.15
+ 2.49		+ 2.42
10.23		10.23
+ 2.50		+ 2.50
10.23		10.17
+ 2.50		+ 2.44
		7.73

Tie to Con. Max. B.C. Pt. INDEXED
on S.L. Balboa Ave. 8-8-47

Moore
Green
Roberts W.O. 60057
8-7-47

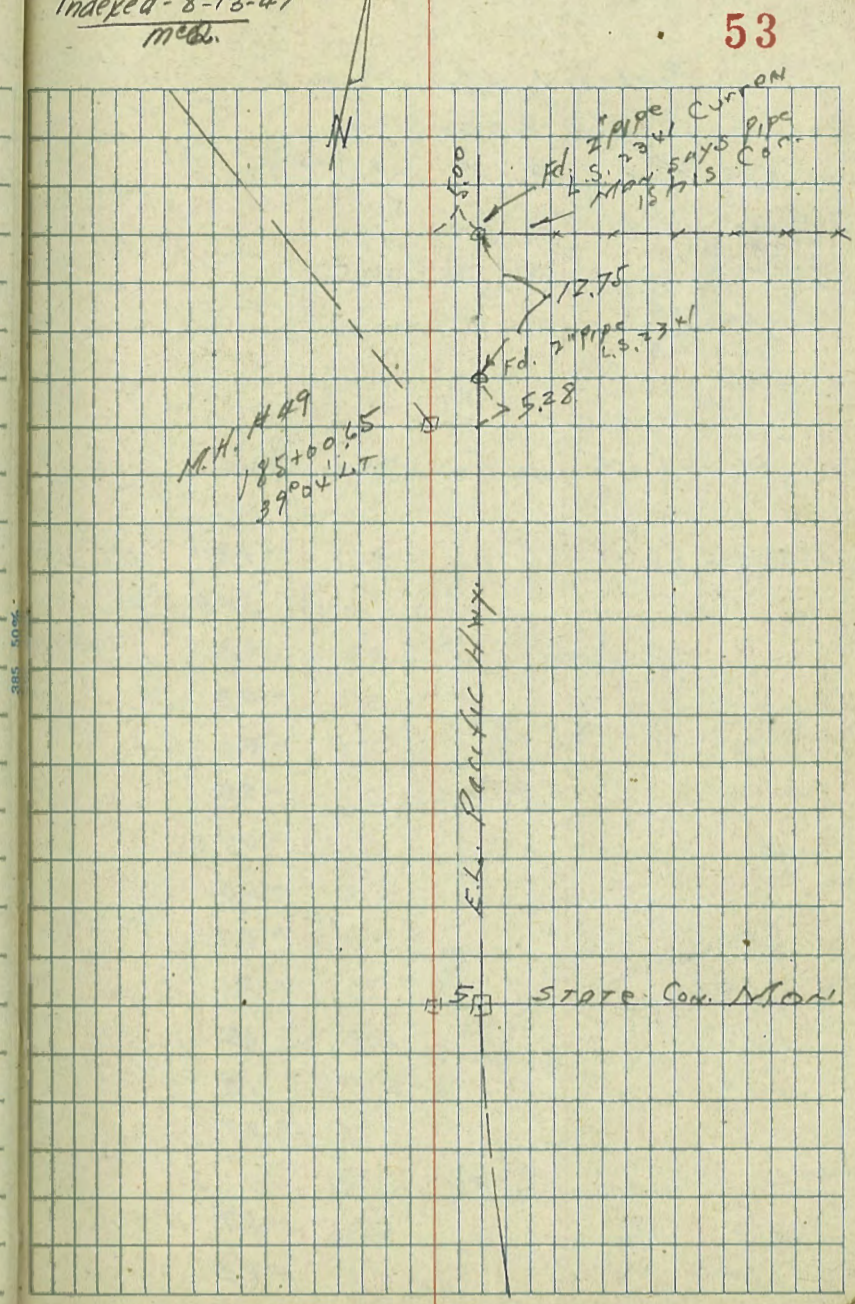
S.L. Balboa Ave



Indexed-8-12-47
meb.

Tie M.H. #49 to
E.L. Pacific Hwy
S of Balboa Ave

Mass
Green
Pobozz WO 60057
8-12-47



Proposed Line change

Trunk Sewer #2

M.H. #18 to M.H. #21

Name
Boyer
Green
Roberts

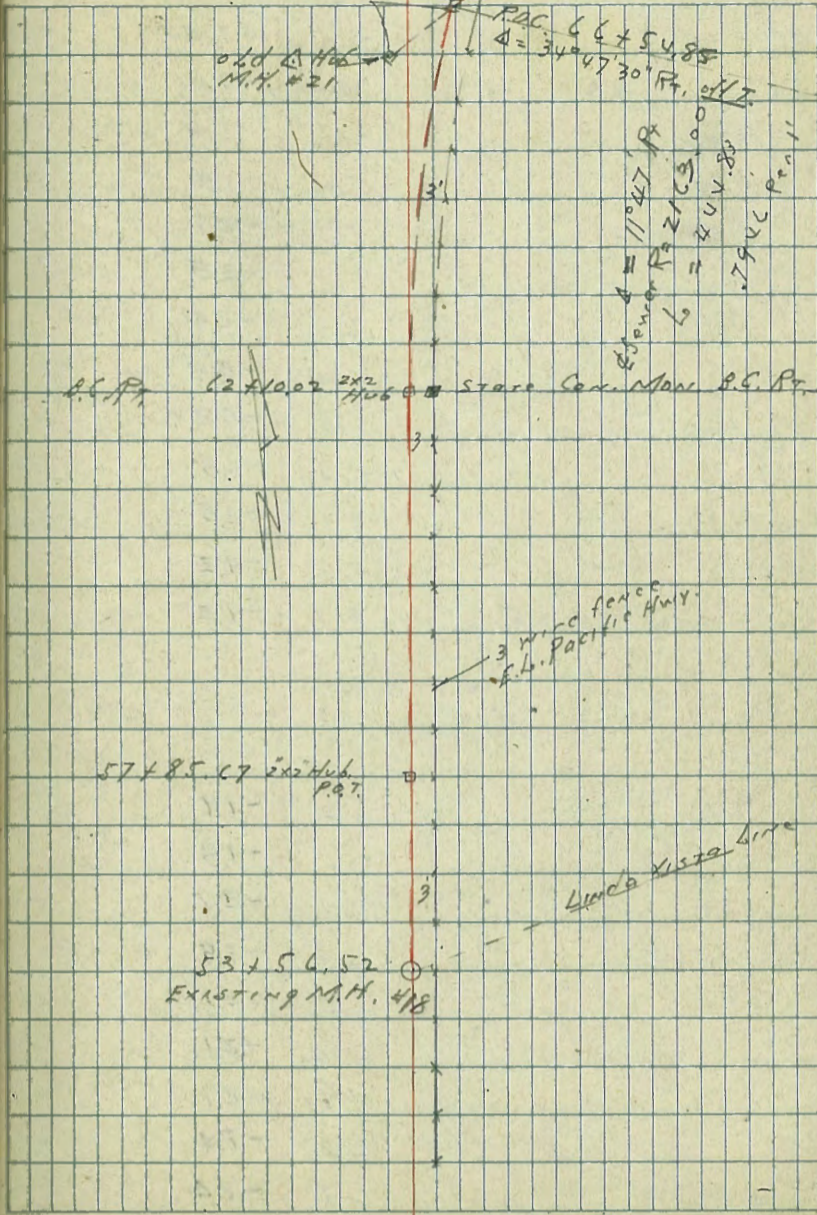
W.D. 60057

13-14-47

SM.B.P. Eddm
Box Culv.
579 57737

647-50 0.30 5.15 4.85

53+56.52	Ex. M.H. #18	9.65	-4.50	FL.
"	"	2.07	3.08	R.I.M.
"	"	4.0	1.2	Average GROUND
54		5.5	-0.3	
+50		5.3	-0.1	
55		6.0	-0.8	
+50		6.1	-0.9	
56		5.8	-0.6	
+50		5.9	-0.7	
+75		5.3	-0.1	
+81		3.7	1.5	
+94		3.9	1.3	
57		5.9	-0.7	
T.P.	3.42 3.58	5.19	-0.04	
+50		5.3	-1.7	
+65		4.8	-1.2	



57+75	2.2	+1.4
58	2.0	+1.6
+06	2.2	1.4
+14	5.0	-1.4
+50	5.7	-2.1
59	6.1	-2.5
+50	6.0	-2.4
60	6.4	-2.8
+50	5.8	-2.2
61	5.4	-1.8
+50	5.1	-1.5
62	4.8	-1.2
62 + 1002 B.C. RT.	4.8	-1.2

T.P. 5.63 4.38 4.83 -1.25 B.C. H26

62 + 50	6.3	-1.9
63	6.2	-1.8
+50	6.4	-2.0
64	6.3	-1.9
+50	6.5	-2.1
65	6.5	-2.1
+50	6.5	-2.1
66	6.8	-2.4
+50	6.8	-2.4

66 + 54.85 H.H. H21 6.8 -2.4

Chick A BMBP E 6dml
Box only approx. Ctn.
if first course
North of Cudahy

220	2.8	2.17
		0.01

Proposed line change
M.H. #32 to M.H. #35
Trunk Sewer #2

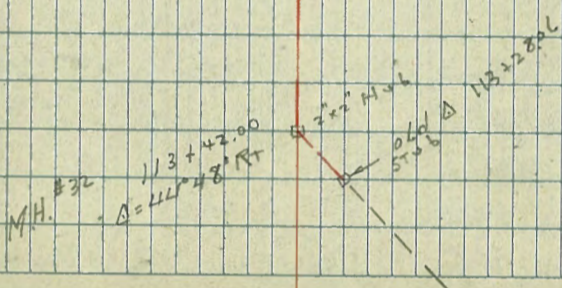
Mason
Begg
Gross
Roberts
10-15-47

134+65.6
M.H. #38 recenter 90° Lt off Back Tang, and 1/2" 15' R.

to #36 126+35.14
add a station 123+25.87 = P.B. Δ = 6°29' Lt.
#35 123+28.35

#34 120+21.04
Δ = 2°47'15" Lt.

#33 117+10.20
Δ = 5°30'30" Lt.



Location of Trees
and Edge of State Park
MH #22 to #35

113+50	34.6	LT	edge Pav.
114+02	14.3	Rt	6" Eucal.
114+77	15	Rt	" "
115	17	Rt	6" Acacia
115+50	34.4	LT	edge Pav.
115+89	1	LT	6" Eucal
+97	13	Rt	4" "
116+08	5	LT	6" "
+17	13	Rt	" "
+37	115	Rt	3" acacia
+40	6	LT	6" Eucal
+58	3	LT	3" acacia
+59	13	Rt	7" Eucal
+90	14.6	Rt	5" acacia
+99	10	Rt	8" Eucal
117	39.9	LT	edge Pav.
+06	5	LT	8" Eucal
+20	10	LT	10 Rt 3" acacia
+31	5	LT	6" Eucal
+37	10	LT	4" acacia
+42	12	Rt	10" Eucal
+45	4	LT	8" "
+55	9	LT	3" acacia
+61	11	Rt	5" "

Suggest removal of trees to 10' Rt. or Lt.

117+64	4	LT	8" Eucal
+81	9	LT	6" acacia
+84	12	Rt	8" Eucal
+93	2	LT	8" "
118+05	10.2	Rt	10" acacia + 11 Rt 3" acacia
+18	2	LT	8" Eucal
+25	11	Rt	6" "
+36	10	LT	8" acacia
+44	2	LT	6" Eucal
+50	10.7	Rt	" "
+53	8	LT	6" acacia
+61	8	LT	8" Eucal on line
+73	8	LT	8" acacia + 12 Rt 4" Eucal
+82	15	Rt	8" Eucal
+93	12	Rt	12" "
+94	8	LT	10" acacia
119+20	30.5	LT	edge Pav.
+07	1	LT	6" Eucal
+13	11	Rt	4" acacia
+31	2	LT	4" Eucal
+34	11	Rt	12" "
+41	8	LT	4" acacia
+50	10.2	Rt	" "
+53	3	LT	4" Eucal
+68	9	LT	" acacia
+71	8	Rt	3" "

119+76 45 Lt 6" Eucal.
 +88 10 Lt 6" acasia
 120+02 4 Lt 6" Eucal
 +10 11 Lt 2" acasia + 9 Rt 4" acasia
 +28 4 Lt 6" Eucal
 +33 9 Rt 10" "
 +40 10 Lt 4" acasia
 +50 375 Lt. edge Pav.
 +52 3 Lt 4" acasia + 9 Rt 6" Eucal
 +60 9 Lt 4" "
 +75 2 Lt 8" Eucal, + 10 Rt 5" acasia
 +87 10 Lt 8" di. acasia
 +96 9 Rt 3" "
 121 1 Lt 6" Eucal.
 +15 10 Lt 6" acasia
 +18 8 Rt 4" "
 +41 9 Lt 4" acasia + 9 Rt 4" acasia
 +65 10 Rt " "
 +69 9 Lt " "
 +75 12 Rt 6" "
 +80 2 Lt 12" Eucal
 +95 10 Lt 8" acasia
 122+12 2 Lt 10" Eucal
 +29 10 Lt 6" acasia
 +40 2 Lt 12" Eucal
 +57 12 Lt 8" acasia

122+68 4 Lt 10" Eucal
 +79 12 Lt 6" acasia
 +90 4 Lt 10" Eucal
 +98 11 Lt 5" acasia

T.P. 4.85 14.20 2.79 9.35

+50

115

+50

114

+50

113+4200 A 44'x8' P.

T.P. 4.33 12.14 7.31 7.81

Brass Plug
B.M. Mon.
S. & C.
JELLETTE
AND
Morena Blvd.
inside R.R. R/W
Fence

4.11

15.52

11.41

	6.6	7.8	9.0
	5.5	4.3	3.1
	10		8
	6.6	7.1	8.1
	5.5	5.0	4.0
	10		10
	6.3	6.6	7.8
	5.8	5.6	4.9
	10		10
	6.2	6.6	7.5
	33.8	5.5	4.6
edge Pav.	10		10
	6.0	6.4	7.5
	6.1	5.7	4.6
	10		10
		6.3	
		5.8	
			<u>12.14</u>

T.P. 3.29 ^L1304 4.45 9.75

119

+50

118

+50

117 +1020 5°30'30" L+

117

+50

116

^L1420

21

8

84

60

7.5 8.4 11.4
6.7 5.8 2.8
10

7.4 8.4 10.6
6.8 5.6 3.6
10

7.2 8.4 10.4
7.0 5.8 3.8
10

7.4 8.4 11.0
6.8 5.8 3.2
10

7.5 8.8 11.5
6.7 5.4 2.7
10

7.4 8.6 11.4
6.8 5.6 2.8
10

7.2 8.1 9.9
7.0 6.1 4.3
10

7.3 8.4 9.7
6.9 5.8 4.5
10

^L1420

750

T.P. 471 1293 482 822

122

750

121

750

120 + 2194 2° 47' 15" Lt on split

120

119750

1304

67

6.9
6.0
7.0

7.4
5.5

7.7
5.2
7.0

1293

6.2
6.8
7.0

7.2
5.8

8.3
4.7
7.0

5.9
7.1
7.0

6.5
6.5

8.4
4.6
7.0

6.0
7.0
7.0

6.4
6.6

8.4
4.6
7.0

6.8
6.2
7.0

8.1
4.9

9.7
3.3
7.0

6.84
6.20
3.83
edge 1894

7.1
5.9
7.0

8.3
4.7

10.7
2.3
7.0

7.5
5.5
7.0

8.3
4.7

10.1
2.9
7.0

7.6
5.4
7.0

9.0
4.9

10.4
2.6
7.0

1304

$$\begin{array}{r} 123 + 25.87 \\ \hline 123 + 28.35 = \text{Eg.} = \Delta \quad 6^{\circ} 29' 27'' \end{array}$$

123

$$\begin{array}{r} \checkmark \\ 1293 \\ \hline \end{array}$$

6.8
 0.5
 4.4
 ← check profile of ground

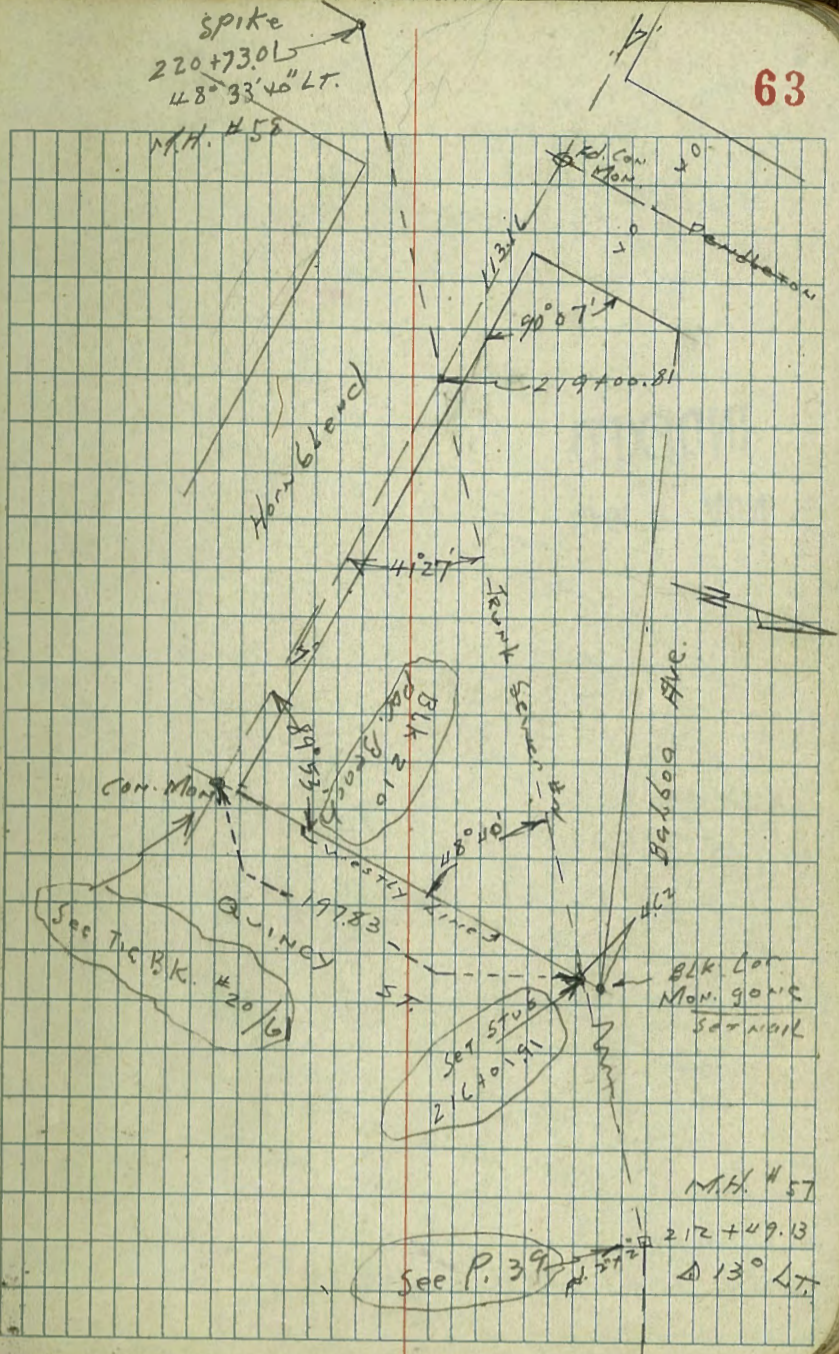
7.3	7.5	8.4
5.6	5.4	4.5
7e		7e
		$\frac{4.5}{10}$
		$\frac{7}{10}$
		$\frac{1293}{10}$

Property Ties in
Blk 210 Pacific Beach
For Trunk Sewer #2

Moore
Begg
Green
Roberts
2-9-48

W.O. # 60057

INDEXED
FEB 9 1948



10-28-49

Survey of N by line
of Balboa Ave
D. Sisson Pico St. to Pacific Hwy

Ed. Con. Mon.

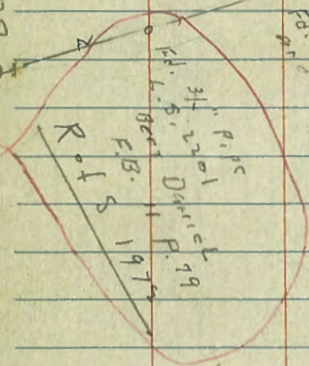
W.O.?

changed to 180°
FBG-237-49
TR-11-SR

INDEXED

NOV 1 1949

Glover Pt.

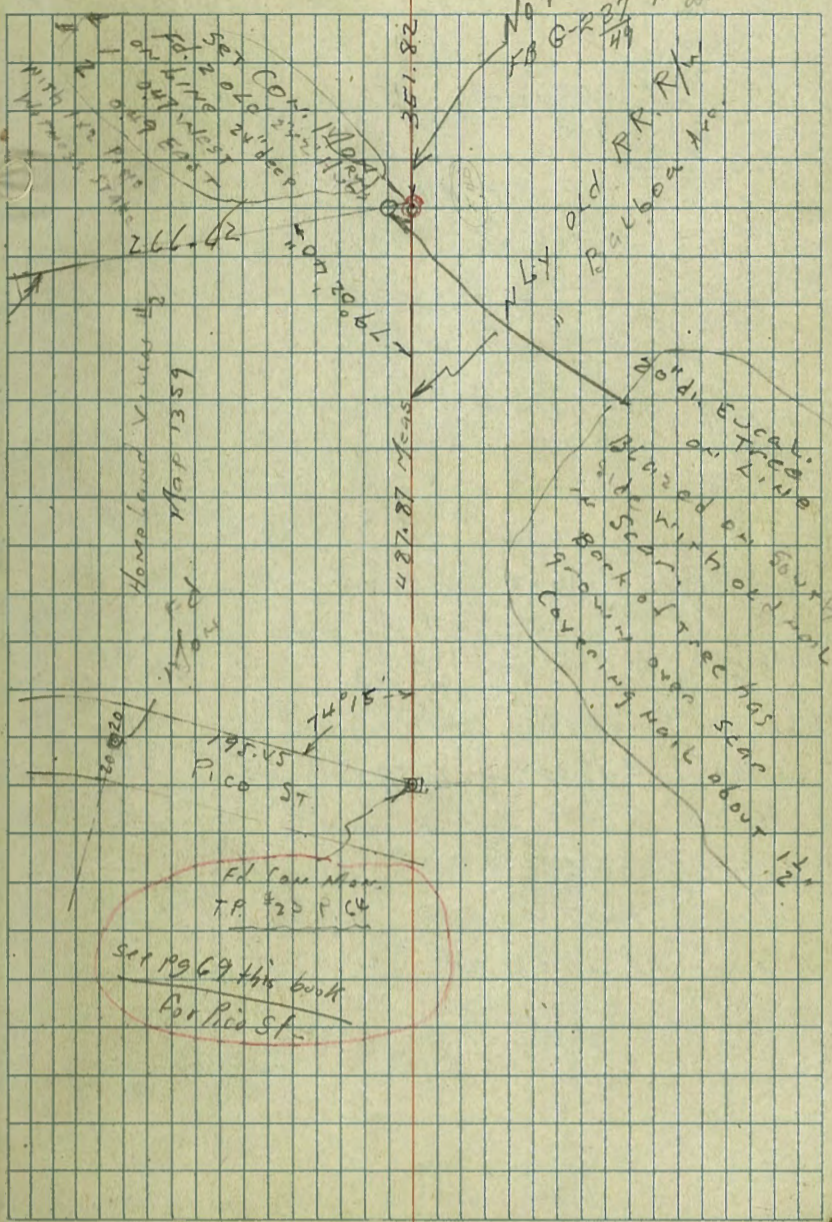


Ed. Con. Mon. 1979

NOTE: MARKING
ED. CON. MON. 1979

0400
set 2x2 H46 P.C.S
B.C.R.

Note changes
FBG-237-49
12-11-52
64



Ed. Con. Mon.
TR 20 F.C.
set 1969 this book
for Pico St.

Moore chief SAT. 8 hrs
 A. Sisson * 10-29-49
 D. Sisson *
 Sherman } chain
 W. Moore }
 Balboa Ave

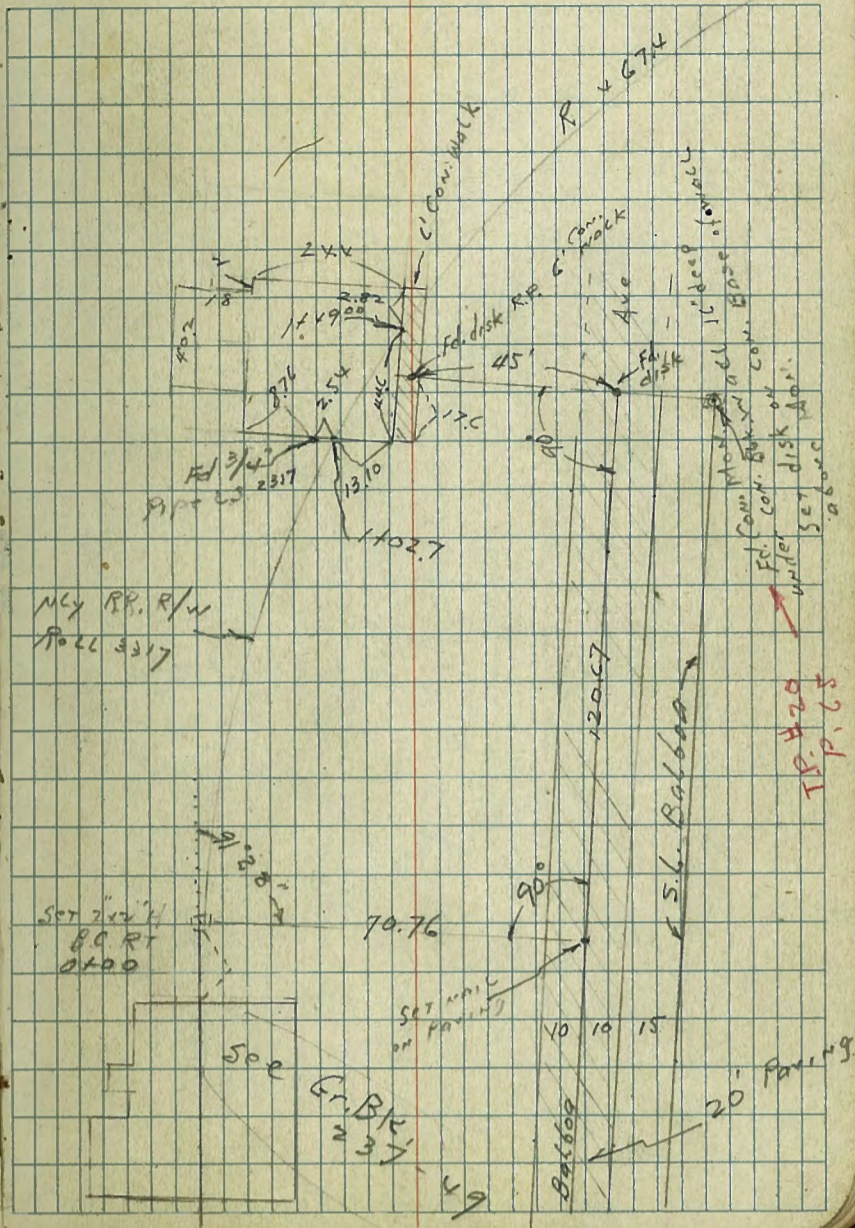
Ref. Maps, Books etc

L.S. # 2201
 Beet Daniel ER #11 - p 79
 " " Rols 1972

City Engn. data

- ✓ F.B. # 94 - P 11
- ✓ " # 95 - P 23
- ✓ " 1052 - P 1 and 2 and 28
- ✓ " 1216 P 13 - 14
- ✓ " 1013 P 12
- ✓ " 1471 P 2 - 12
- ✓ Gr. Bk 237 P 23
- FB. 1760-8 = This Book
- ✓ Maps # 1530 & 1359
- ✓ 1260 D = Trunk sewer
- ✓ Roll 4006 RR R/W
- ✓ " 3317 ✓ access MAP
- State R/W 281 M
- 3691 B

Con. Floor
 Wood Frame
 Shinney's
 Market



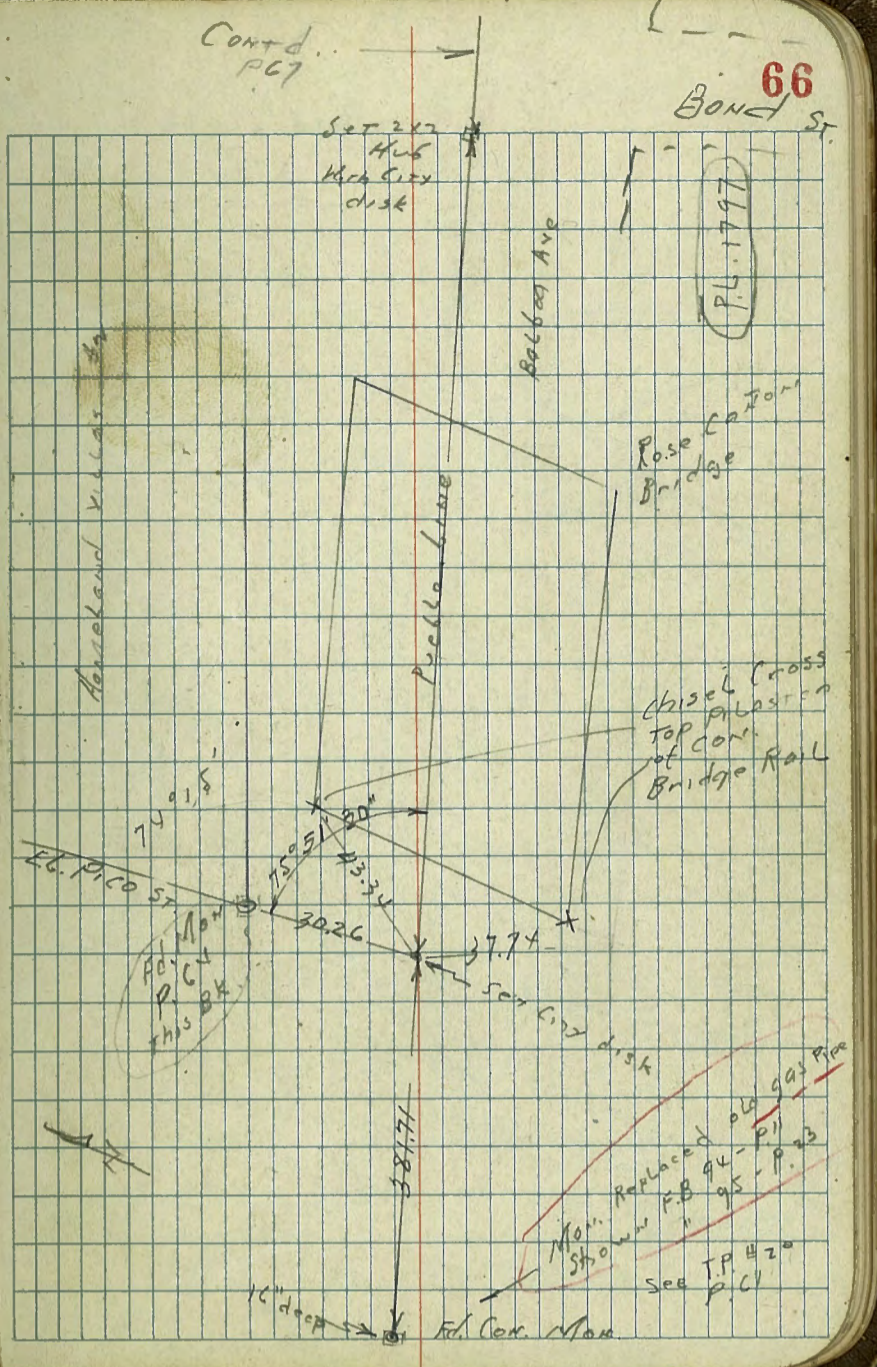
Balboa Ave

Cont'd
P67

66
BOND ST

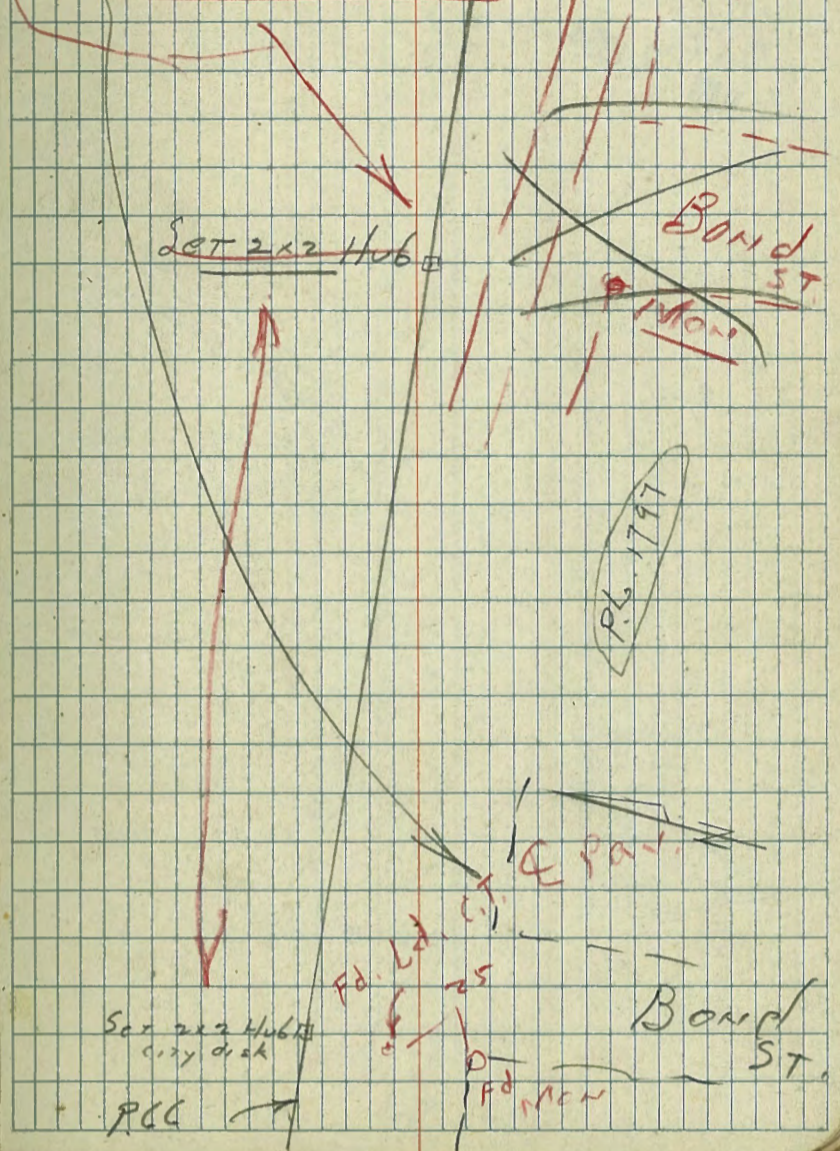
Set 217
HL6
Mark City
disk

PL-1797



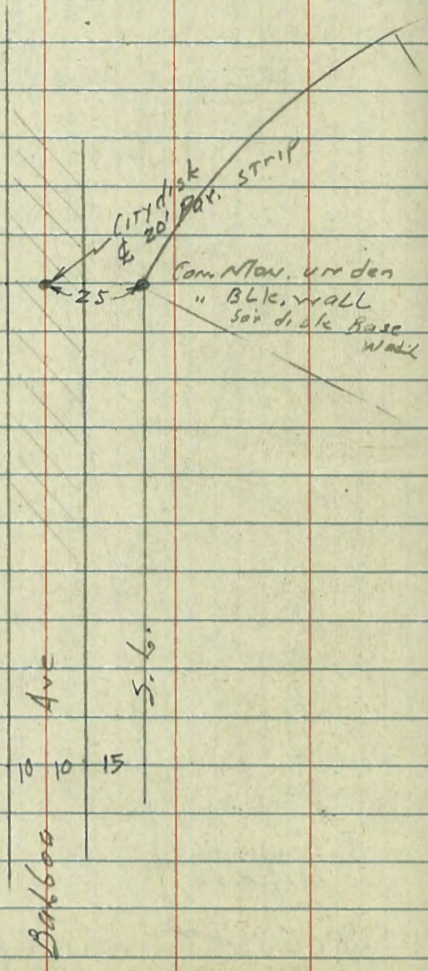
Balboa Ave

NOTES CONTD.
IN GB. 537, P. 49

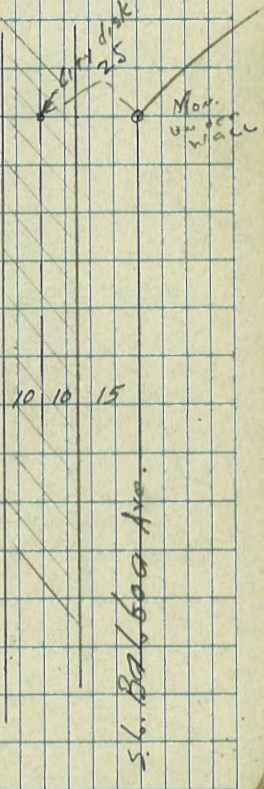


Balboa Ave
at Pacific

INDEXED
JUN 7 1954



P.C.S

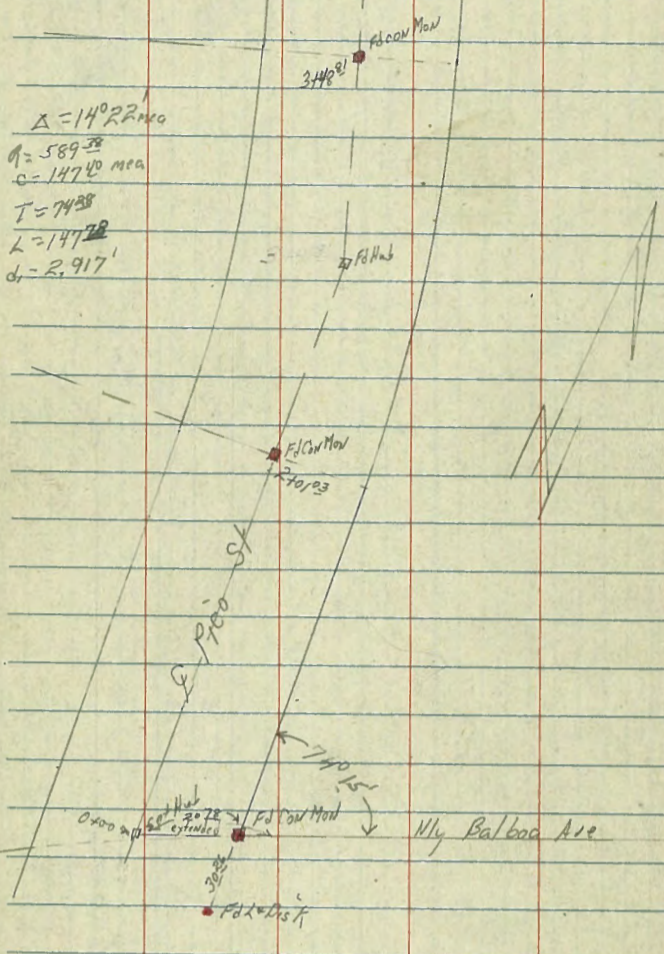


D. Smith
J. Reed
C. Powell

WOL 25020
6/4/54

Ref 1964 this Book
TP 20 061
GR37 018
FD 2162 My Balboa Ave

$\Delta = 14^{\circ} 22' 00''$
 $a = 589.38$
 $c = 147.40$ mea
 $T = 74.38$
 $L = 147.22$
 $d = 2,917'$



385 5896

Lt=Wly

A

Rt=Ely

1+60 13° Lt SE cor cyclod fence 6'

1+60 11° Lt & 16" twin tree

1+50

1+28 13° Lt & 8" tree

1+25

1+00

0+75

0+50

0+37 16° Rt & 10" P.P. & 3783 H

0+25

0+20 16° Rt & dead man

0+00 Wly line Balboa Ave to Ely extended to intersect
Pico St to North,
taken along line of Balboa.

BM, 5²⁴ 1896

13 22

B.P. SE cor
Pos. Creek
Bridge and
Balboa Ave

	6 13.7	6 13.7	6 13.0	6 12.7	6 12.7	6 11.7		
	40	20	10	20	20	40		
		6 13.4	6 12.9	6 12.4	6 12.4	6 11.9		
		40	20	20	20	40		
		6 13.0	6 12.4	6 11.2	6 11.2	6 11.8		
		40	20	20	20	40		
	6 12.7	6 12.4	6 12.0	6 11.8	6 11.3			
	40	20	20	20	40			
		6 12.4	6 12.0	6 11.9	6 11.6	6 11.3		
		40	20	20	20	40		
		6 12.1	6 12.0	6 12.3	6 12.2	6 11.7		
		40	20	20	20	40		
		6 12.6	6 13.1	6 12.4	6 12.1			
		40	20	20	40			

see x sep. Balboa Ave
for 3/4 notes if needed.

7 1896

TP 7⁸⁷ 23⁸⁵ 2⁹⁸ 15²⁸ ECOMON

3758 18° at end 2⁵ picket fence & cypress hedge
 3748⁸¹ EC 7° 11'

3725 6° 01.053'

3700 4° 48.763' also cypress hedge

2780 172 at Begin 2⁵ picket fence
 D=1482
 EA=58938
 L=14778

2775 3° 35.843'

2768 18° at dead man

2750 2° 22.923'

2741 18° at 10' PP 1/2 74657

2725 1° 10.003'

2701⁰³ BC Lt 0° 00'

2700 16' Lt & 18' twin Paper tree

1777 14° Lt & 24" tree

1775

1778	1777	1770	1766	1761	1758	1756
40	26	20	18	29	20	40
	16.8	16.6	15.9	15.4	15.4	15.1
	40	20	15	34	20	40
16.5	16.2	16.0	15.3	15.0	15.2	14.8
40	20	16	14	40	20	40
	16.3	16.1	14.8	14.4	14.8	13.6
27	20	12	40	42	40	40
40						
14.1	13.2	14.4	14.1	14.6	13.6	13.6
40	20	12	40	20	35	40
	13.7	14.7	13.6	14.2	12.9	12.9
	33	20	54	48	40	40
	14.8	14.9	14.9	13.4	14.6	14.5
43	41	41	56	54	65	65
40	20	20	20	20	40	40
	14.4	14.3	14.3	13.1	13.0	11.7
44	42	42	59	60	40	40
40	20	17	20	20	40	40

1890

BM starting 10¹³ 13⁷³

5126 this is into gov Housing for slave

5112 over Lt & (2) deadmen

5107 20⁵ Lt & 12¹ P.P. 1. 6118⁰

5100

4175

4150

4143 22² Rt & 3⁵ con walk

4125

4108 38⁴ Rt & double garage under const floor 12 64

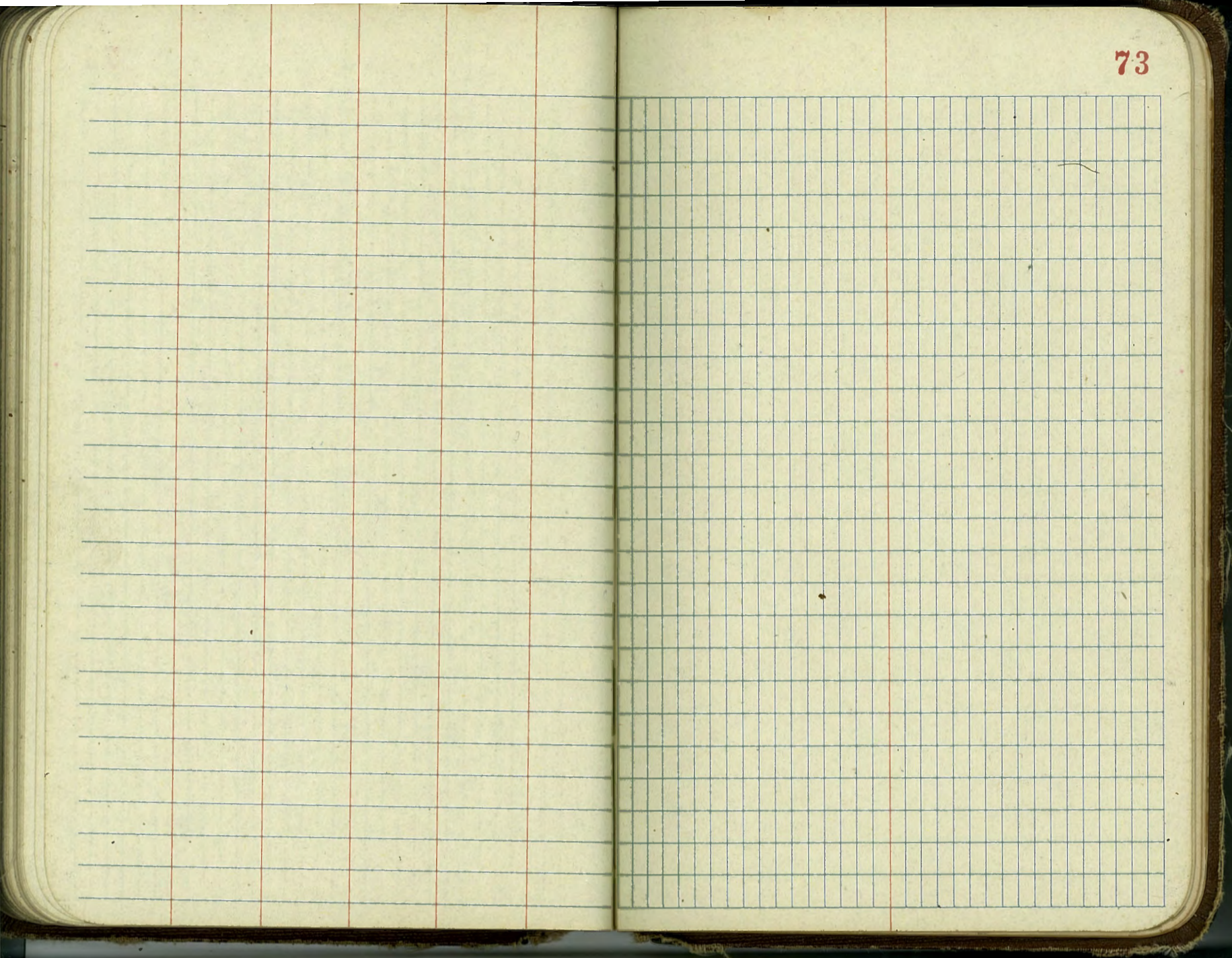
4100

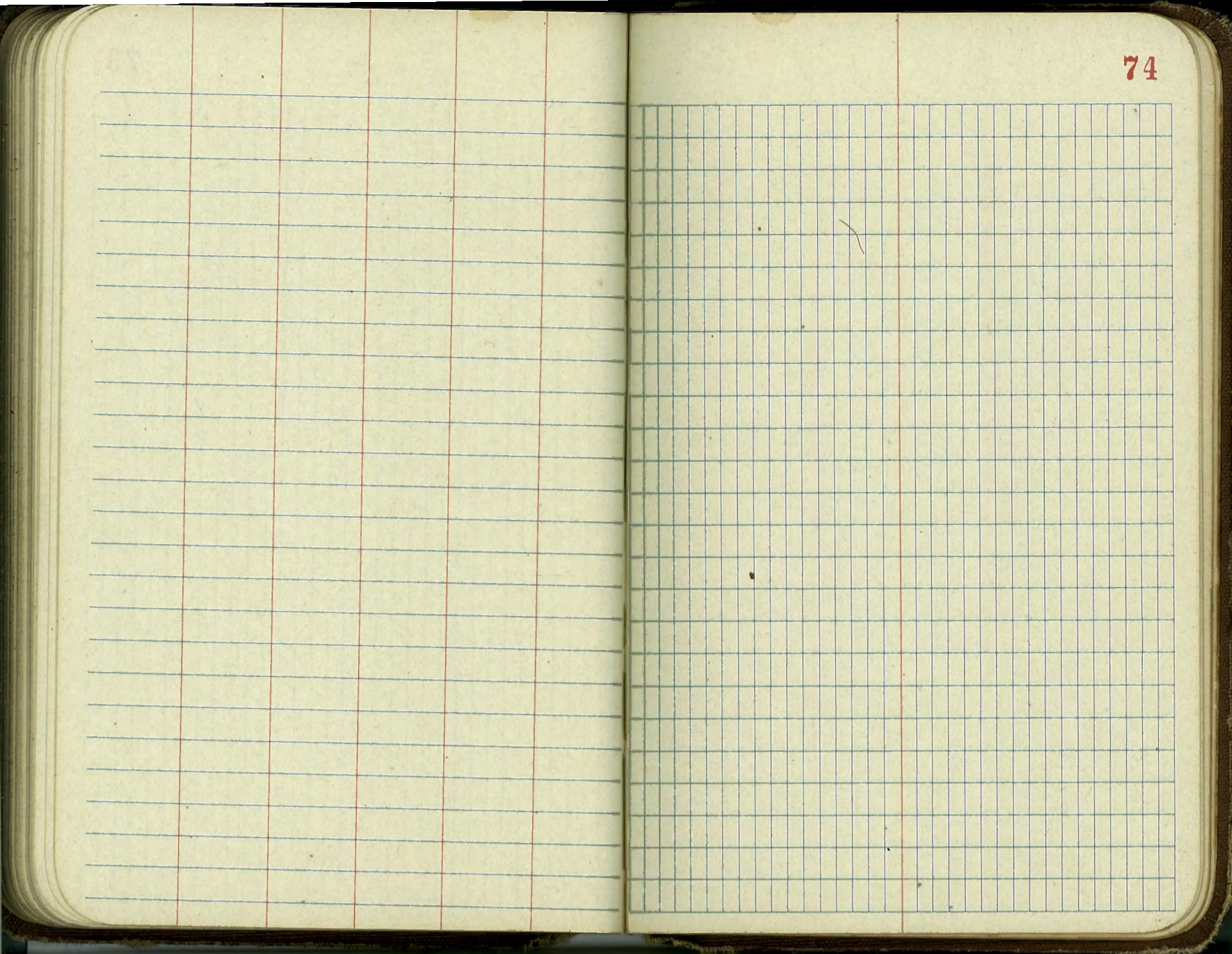
3175

3173 24² Rt & double garage non floor 12 100

Station	Lat	Why	E	N+E	Ely
BM starting	22.7				
5126	21.8		21.9	20.8	20.1
5112	21.5		20.7	20.6	20.1
5107	21.4		20.1	20.6	20.1
5100	21.5		20.9	20.4	20.1
4175	20.8		20.1	19.8	19.6
4150	20.6		19.6	19.2	19.6
4143	20.6		19.6	19.2	19.6
4125	19.7		18.9	18.8	19.1
4108	19.6		18.8	18.8	19.1
4100	19.1		17.8	18.4	19.1
3175	18.8		17.4	18.4	19.1
3173	18.5		17.0	18.0	19.1

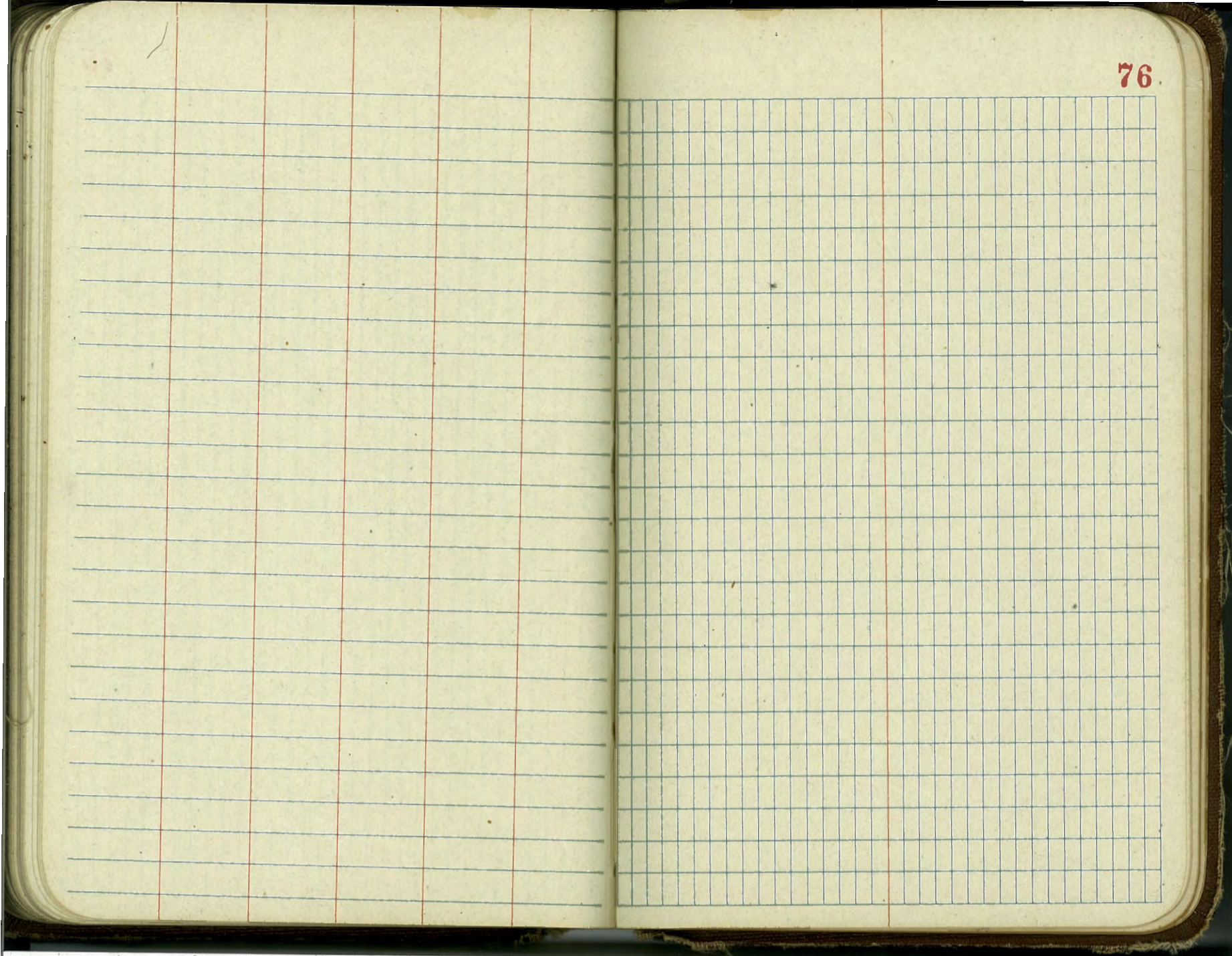
Σ 23 85

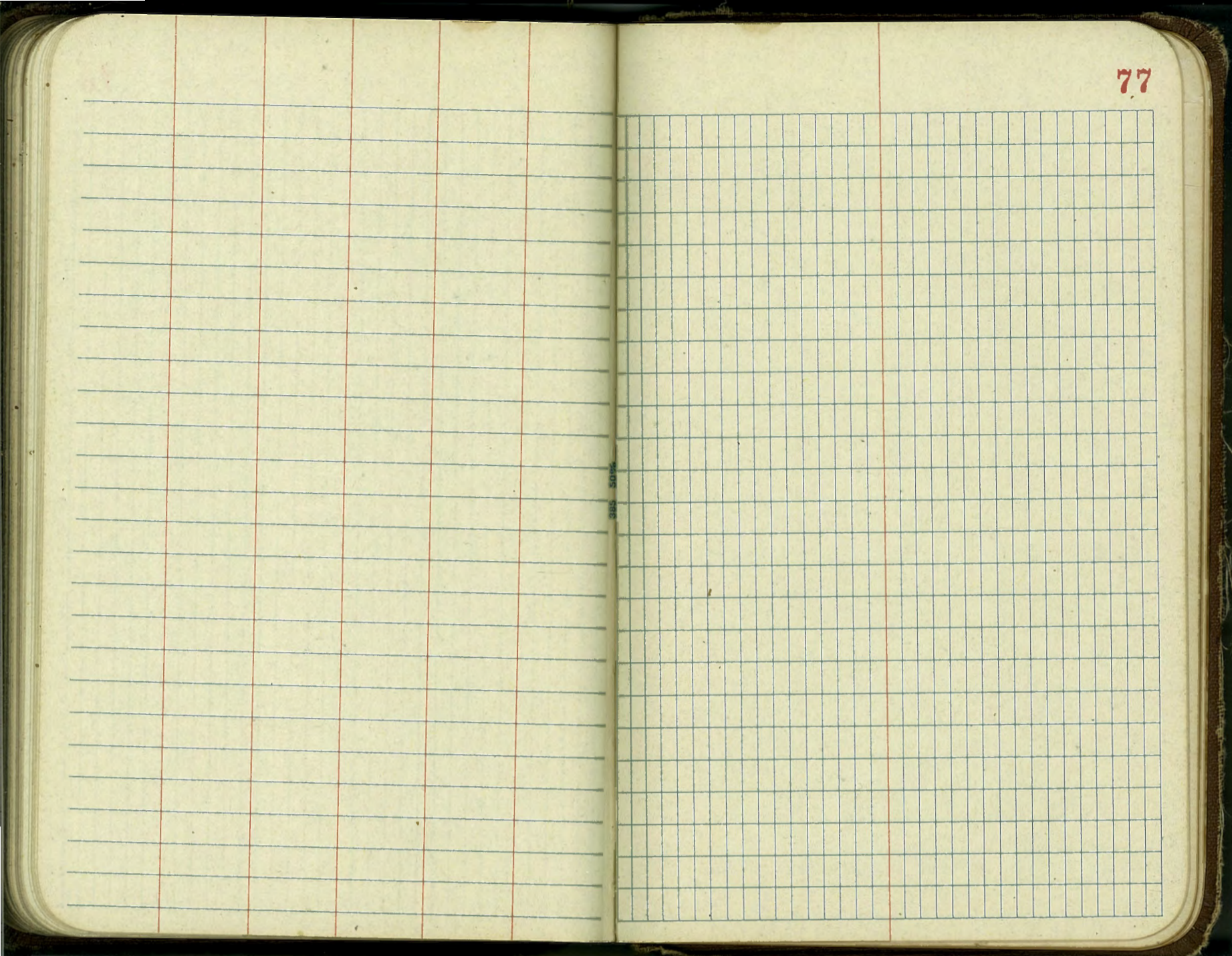


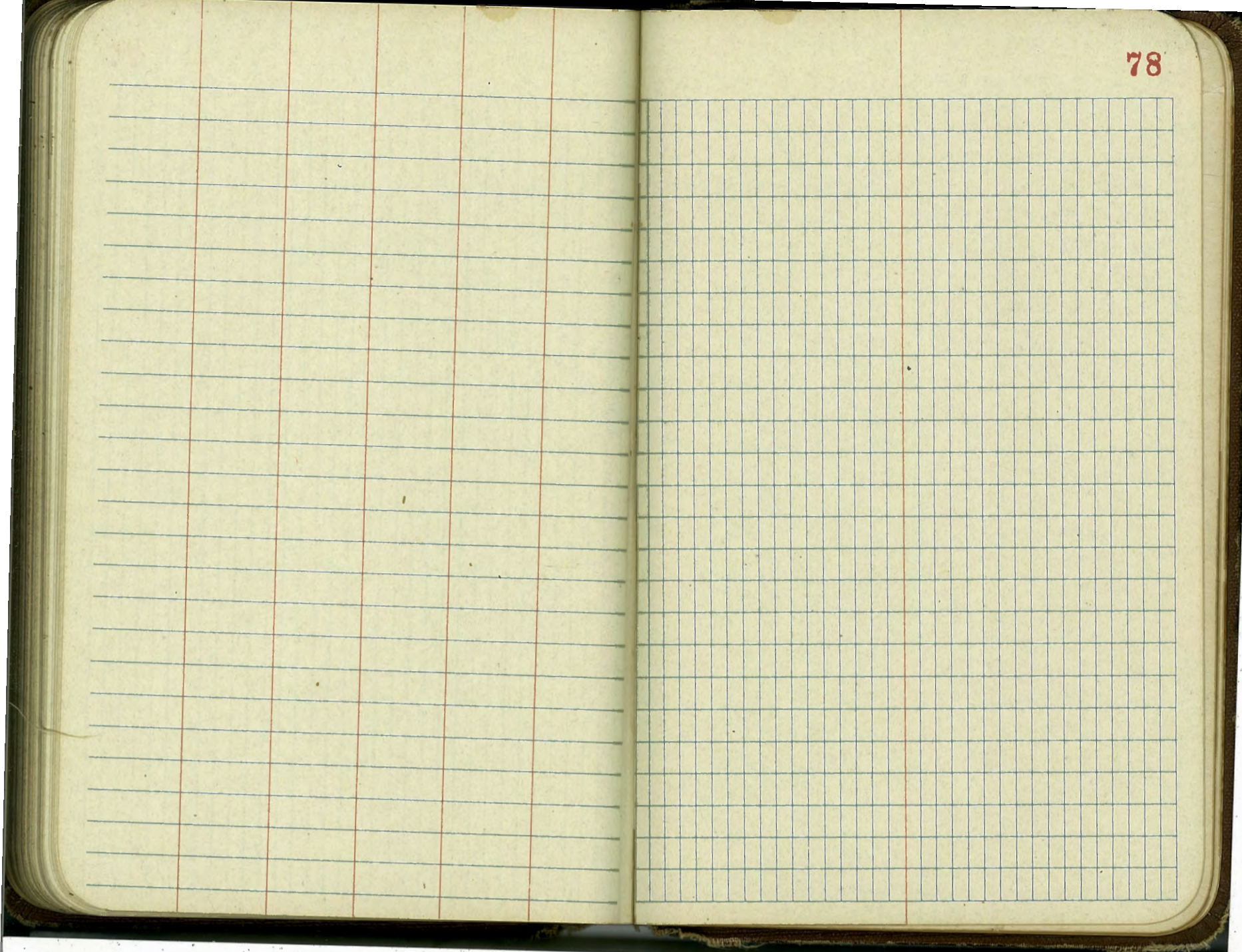


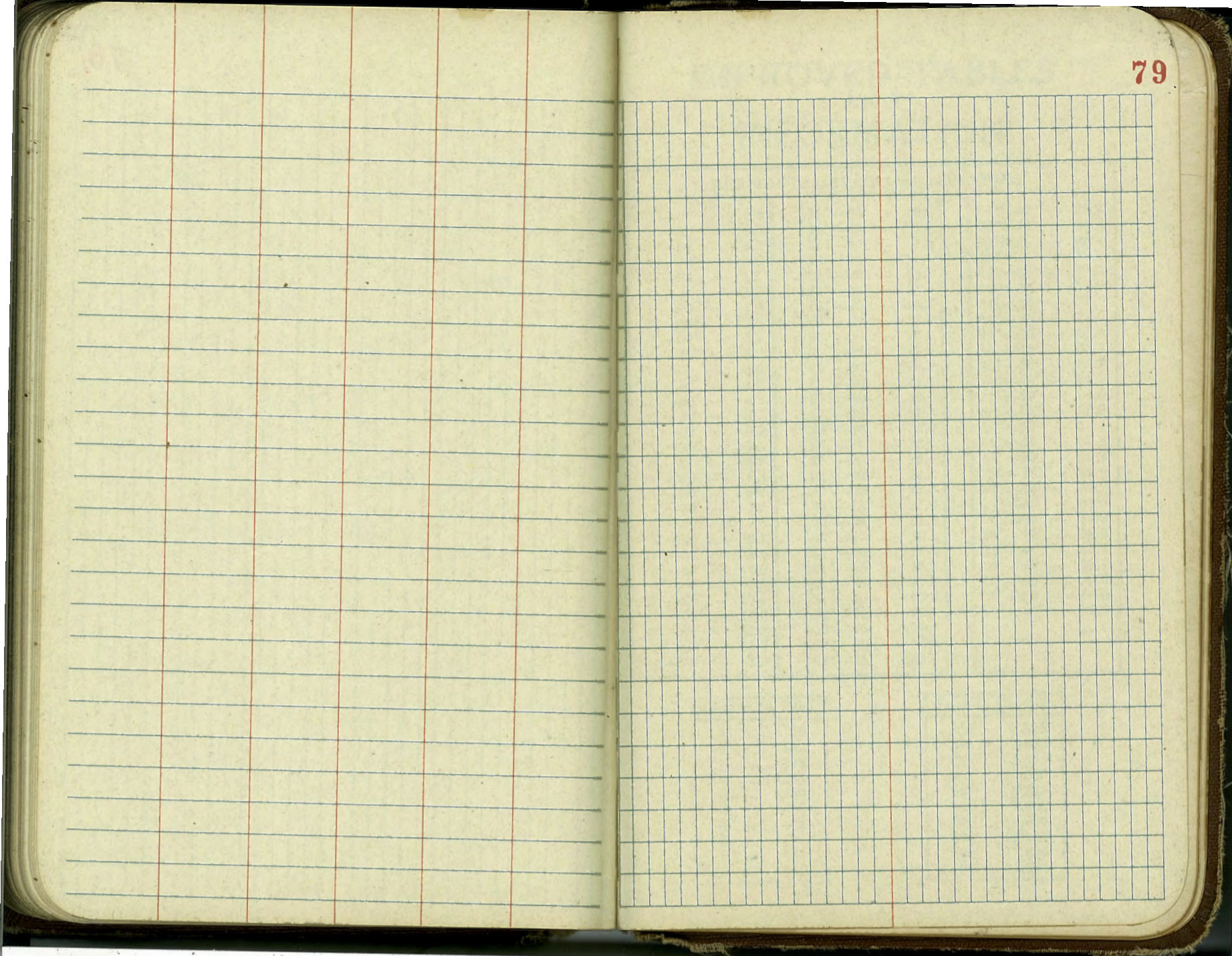
A page from a notebook with horizontal blue lines and three vertical red margin lines. The page is blank.

A page from a notebook with a grid pattern and a vertical red margin line. The page is blank.









DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

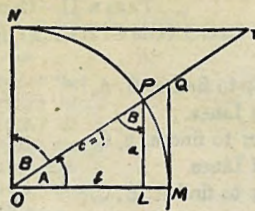


TABLE II
TRIGONOMETRIC FORMULAE.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OB = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

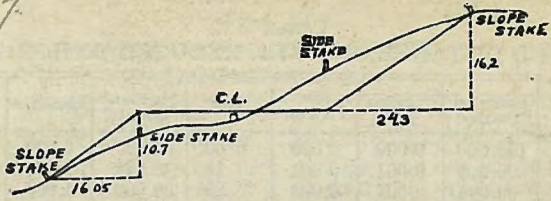
$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

36.94
71147.78
27
24
37
36
18
2+38
2475
3+12
3+49

2.17

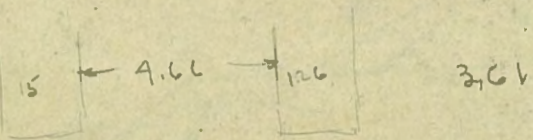


DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.



$$\begin{array}{r}
 4 + 1.97 \\
 45.9 \\
 \hline
 487.87
 \end{array}$$

1.28 4.65 1.30 3.57

1.26 4.63 1.28 3.62

1.26 4.66 1.27 3.65

1.25 4.67 1.26 3.68

$11.84 = E \text{ face } w/ B4$
 134.63
 33.41

 179.88

33.41
 8

 41.41

49
 41.41

 7.59