

1764



FIELD BOOK

1885

1764

MICROFILMED

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CHICAGO

INDEXED

to page # 176

Mt Soledad + Pac. Beach	
Drainage Area to Cross	1 to 6 X
Mission Blvd + Turquoise	15 to 35
S.D.E.R., Rt. of Way to Turquoise	7 to 14
Storm Drain Nly. from Archer	
300' ± west of Cass	36 to 45
X Sect. Alley Block 178 Pacific Beach	46 - 53
X Sect. Alley Block 2 La Jolla Park	54 - 60
Storm Drain Easement Tyrian St to Blk 2	68
X Sect. Dawson - Trojan to El Cajon	71 - 76
chs. Garnet Events to Haines	77 + 78
" Emerald + Gresham	

4-21-47 Survey for Drainage

From Top of Mt. Soledad To

□ = Set 2x2 R.W. Hub.

Distances by Stadia

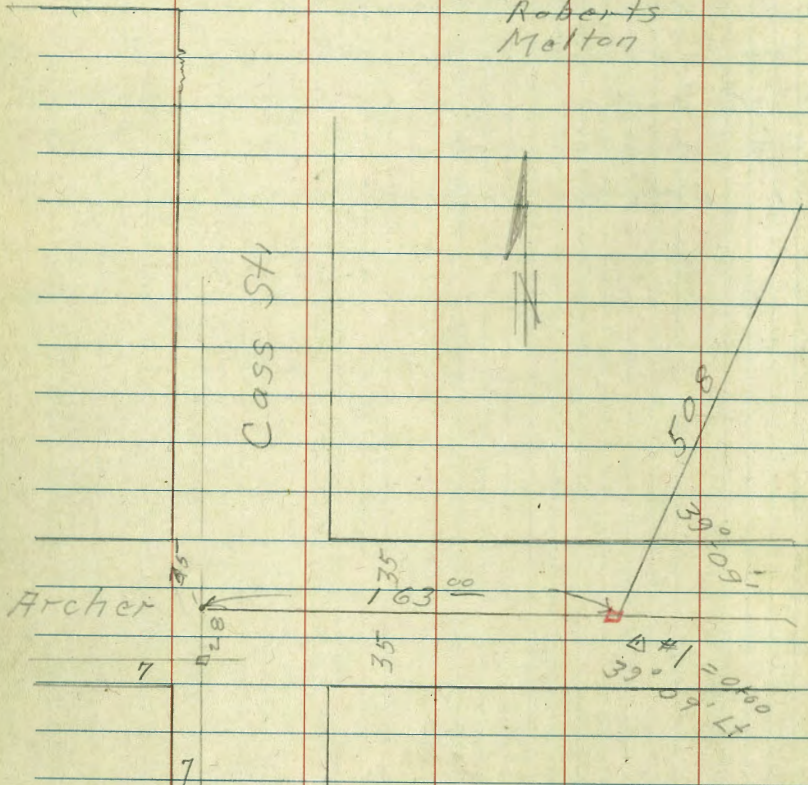
INDEXED

Sammermeyer

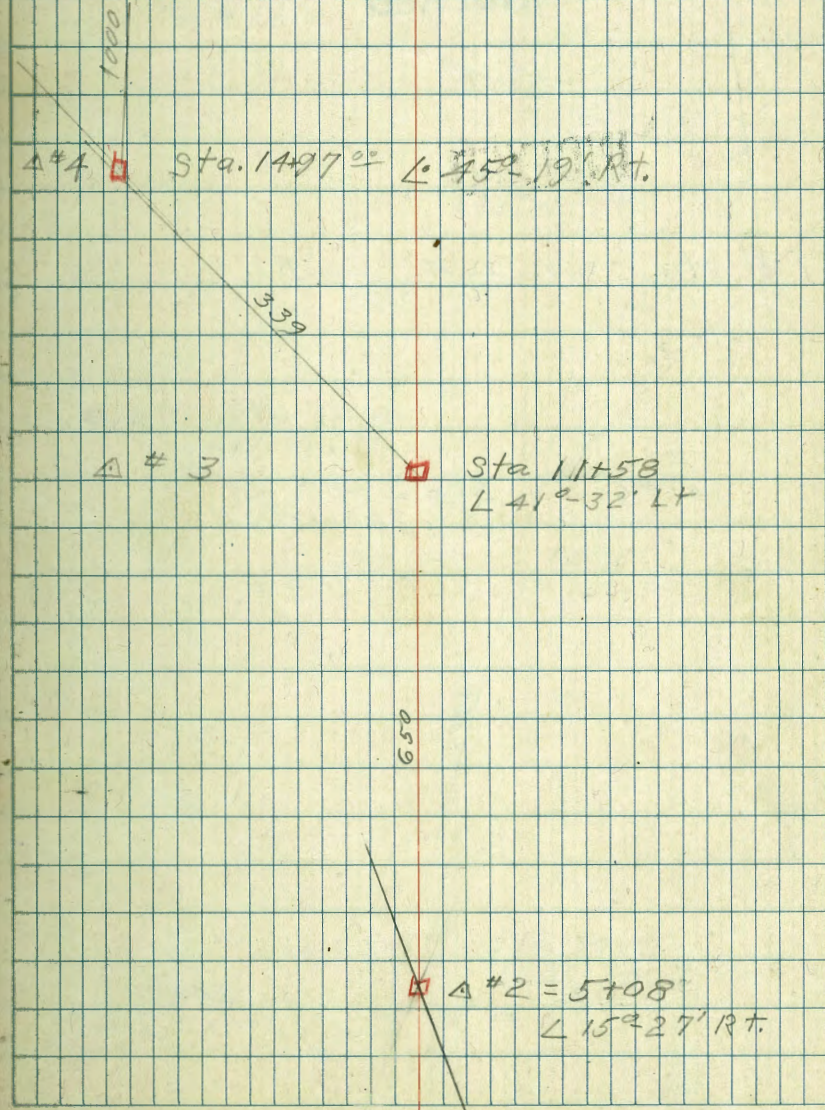
W Moore

Roberts

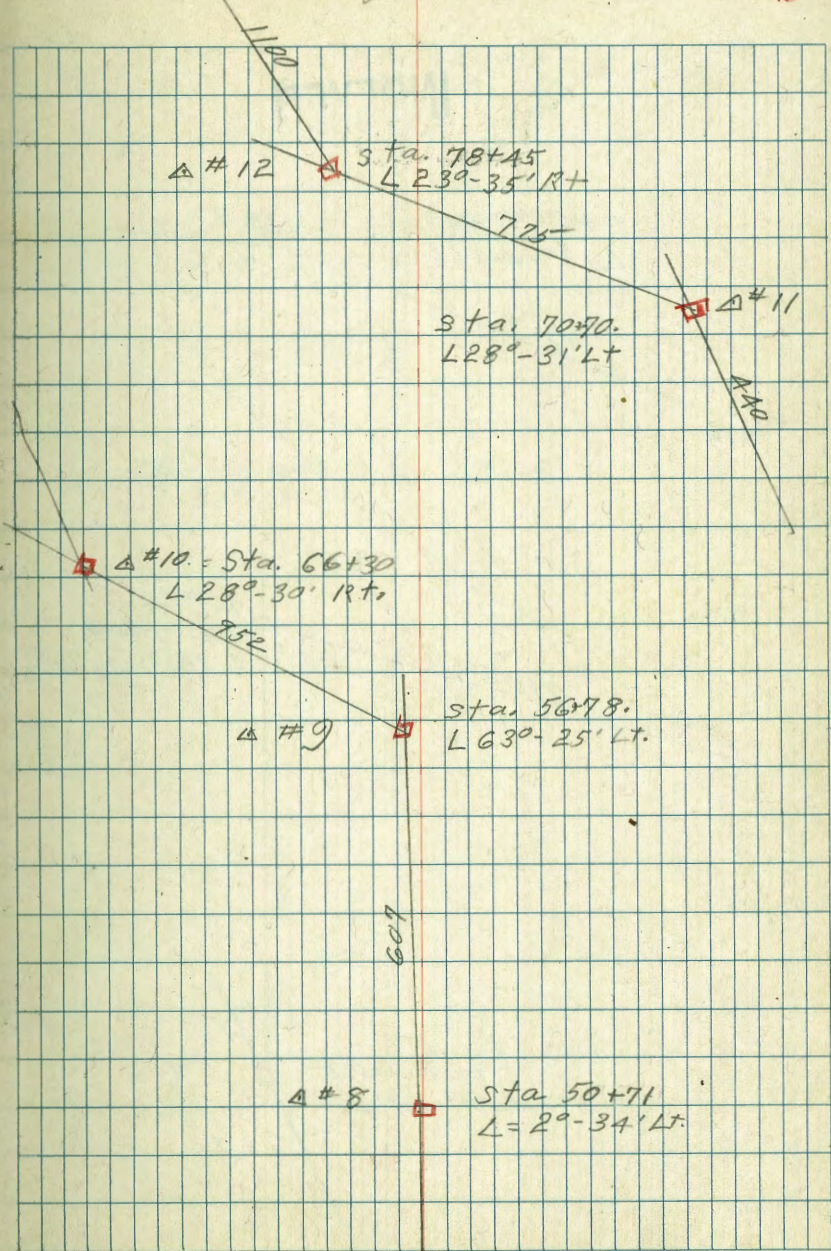
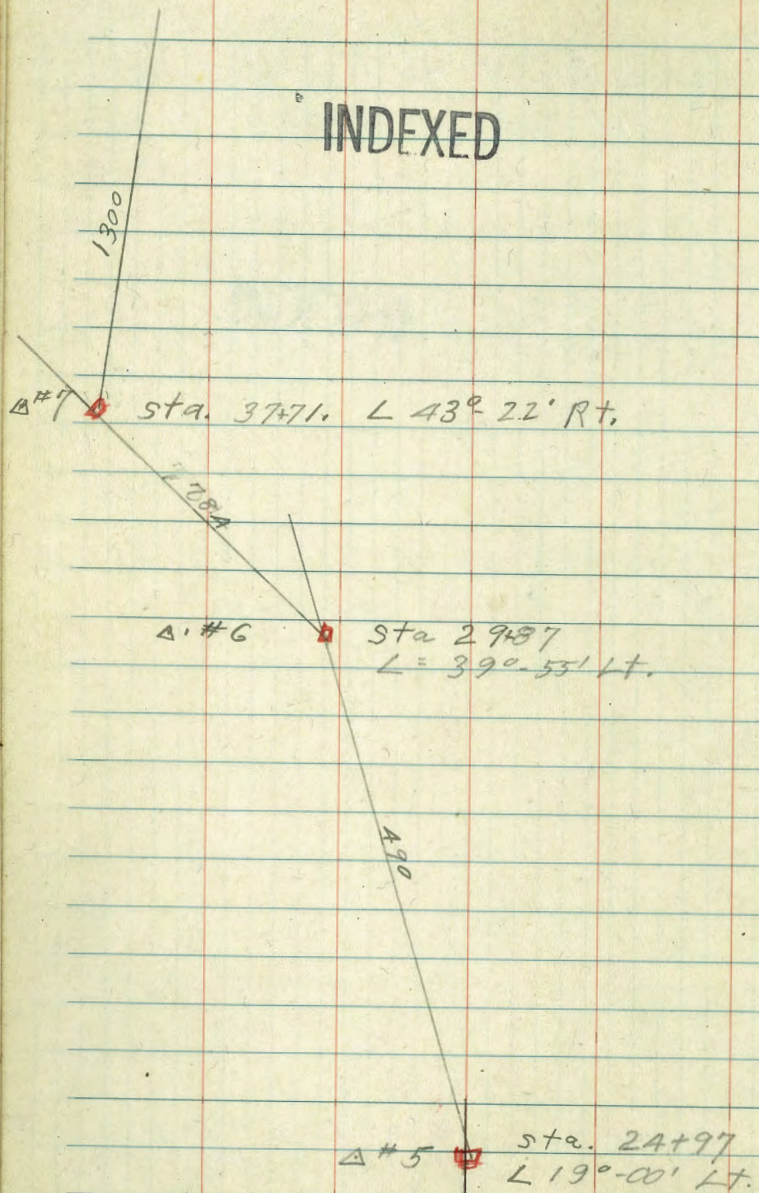
Melton



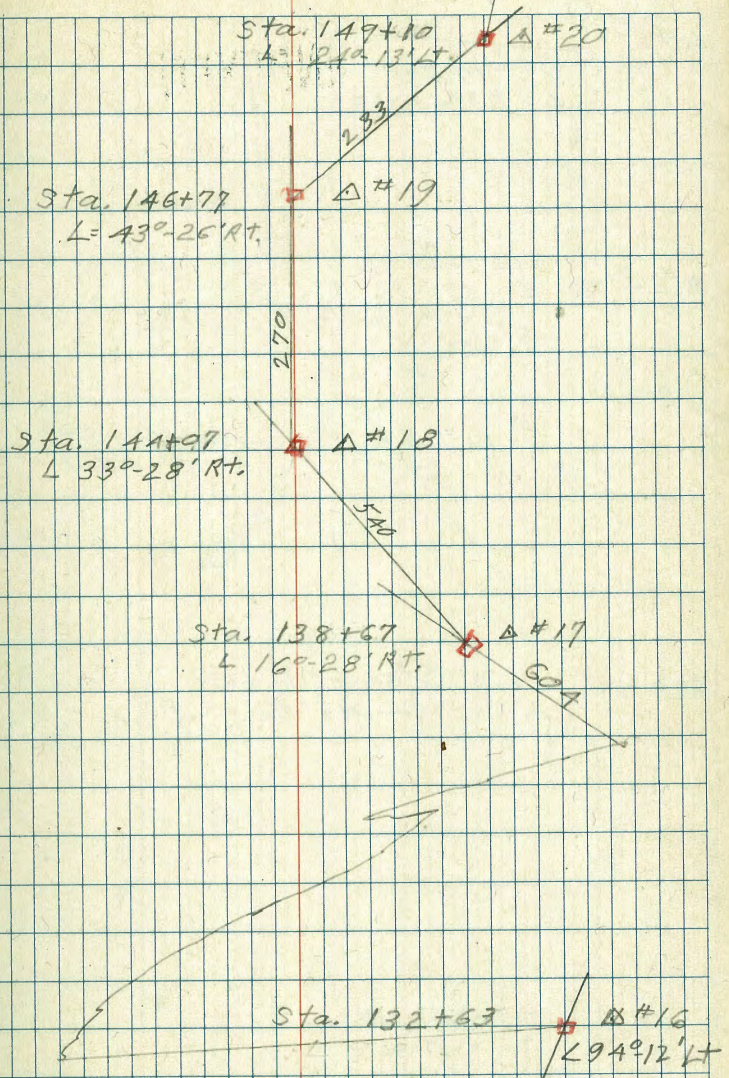
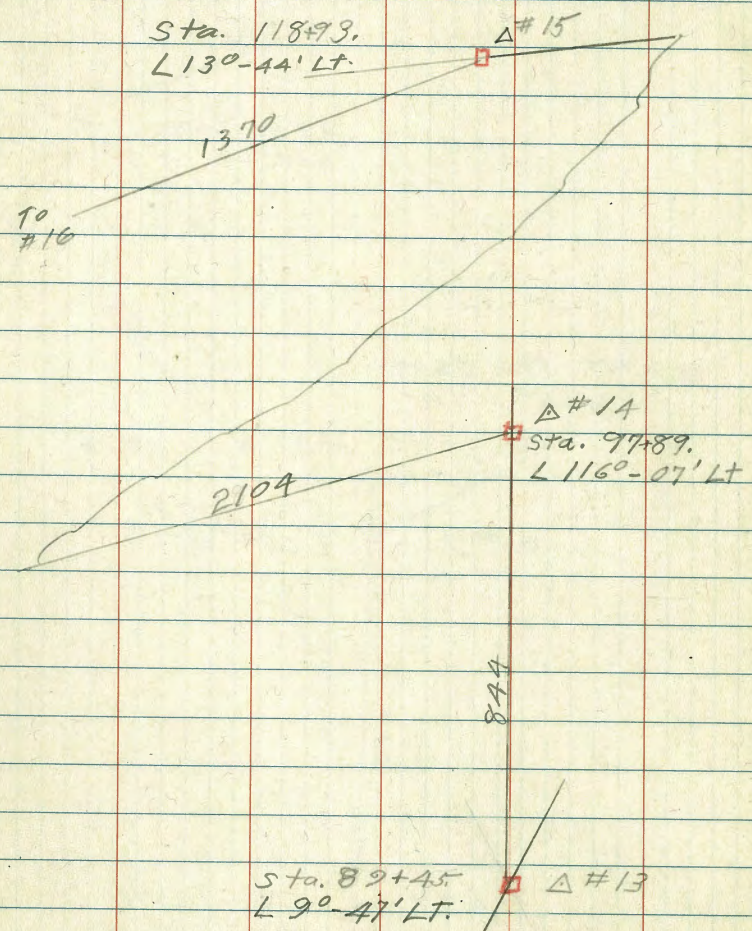
Area. Crossing ^{Indexed} Turquoise + Mission Blvd. 1
Mission Blvd + Turquoise.
V.O. # 90041

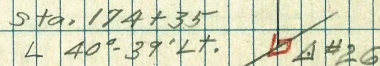
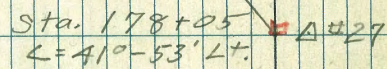
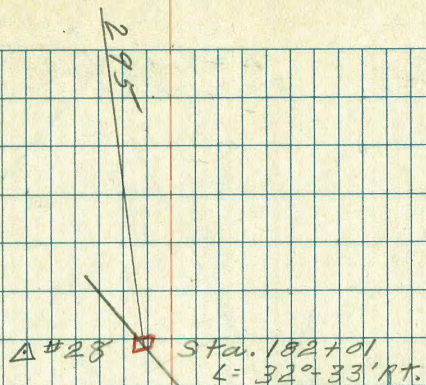
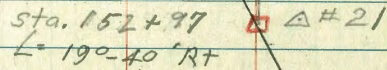
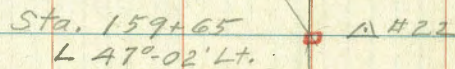
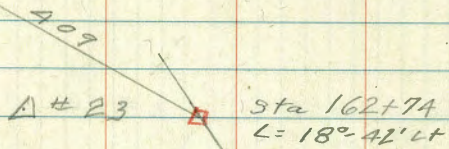
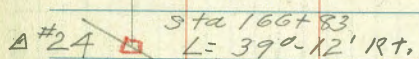
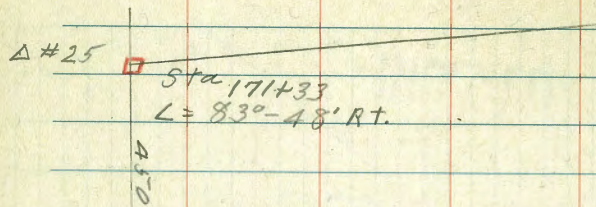


INDEXED



INDREVER





Storm Drain N.E. From
Mission Bld & Turquoise

NO 80090

Sommermeier
W Moore
Melfort

H = set 212 Hub
ch. = chained distance

INDEXED

Mission Blvd.

30

30

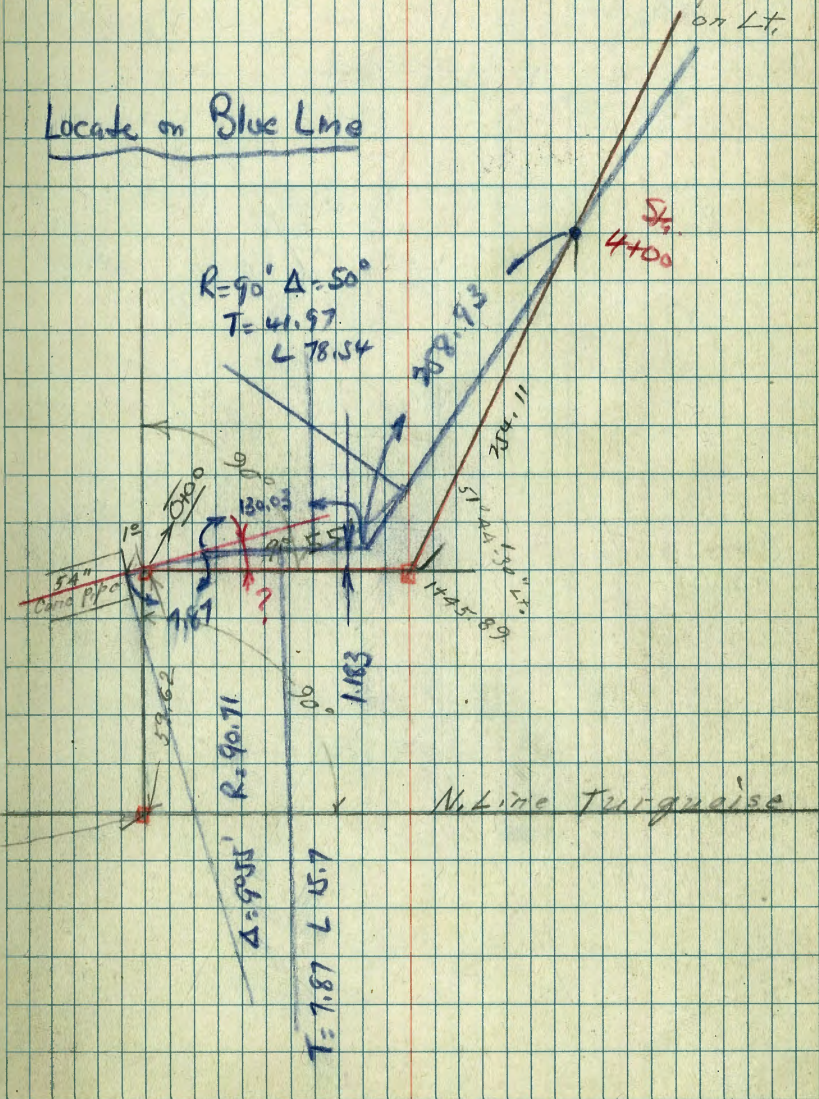
16733 -

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AUG 16 1951

Continued Page 15
on Lt.

Locate on Blue Line

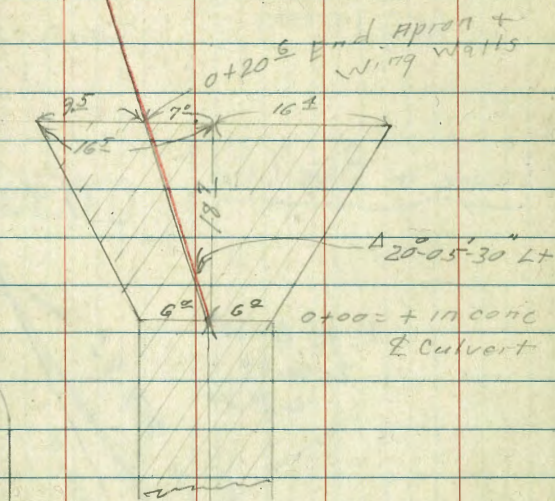


S.D.E.R.Y. Rt. of Way to Mission Blvd. + Turquoise - Storm Drain

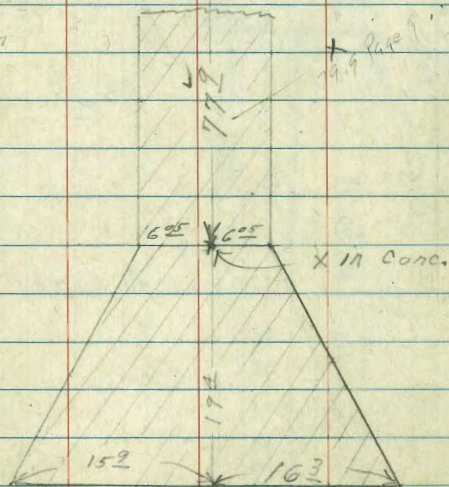
Sommermeier
Moore
Melton

4/23/47

INDEXED



opening
Cross Section
Culvert

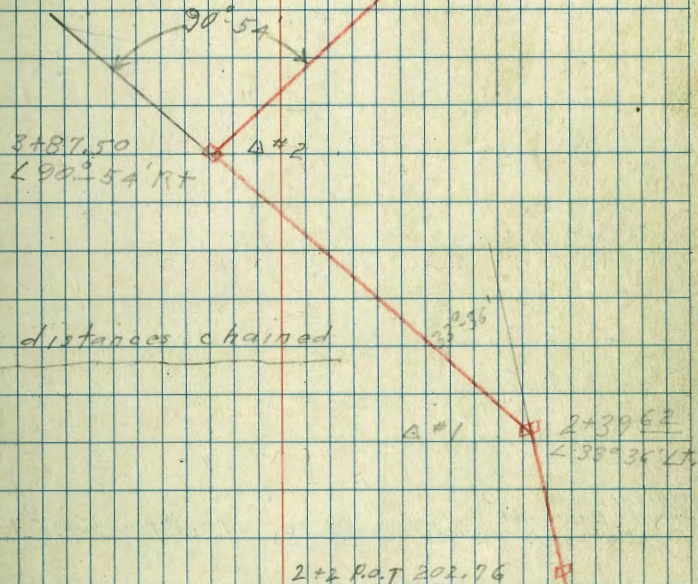


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Cont. Page 8

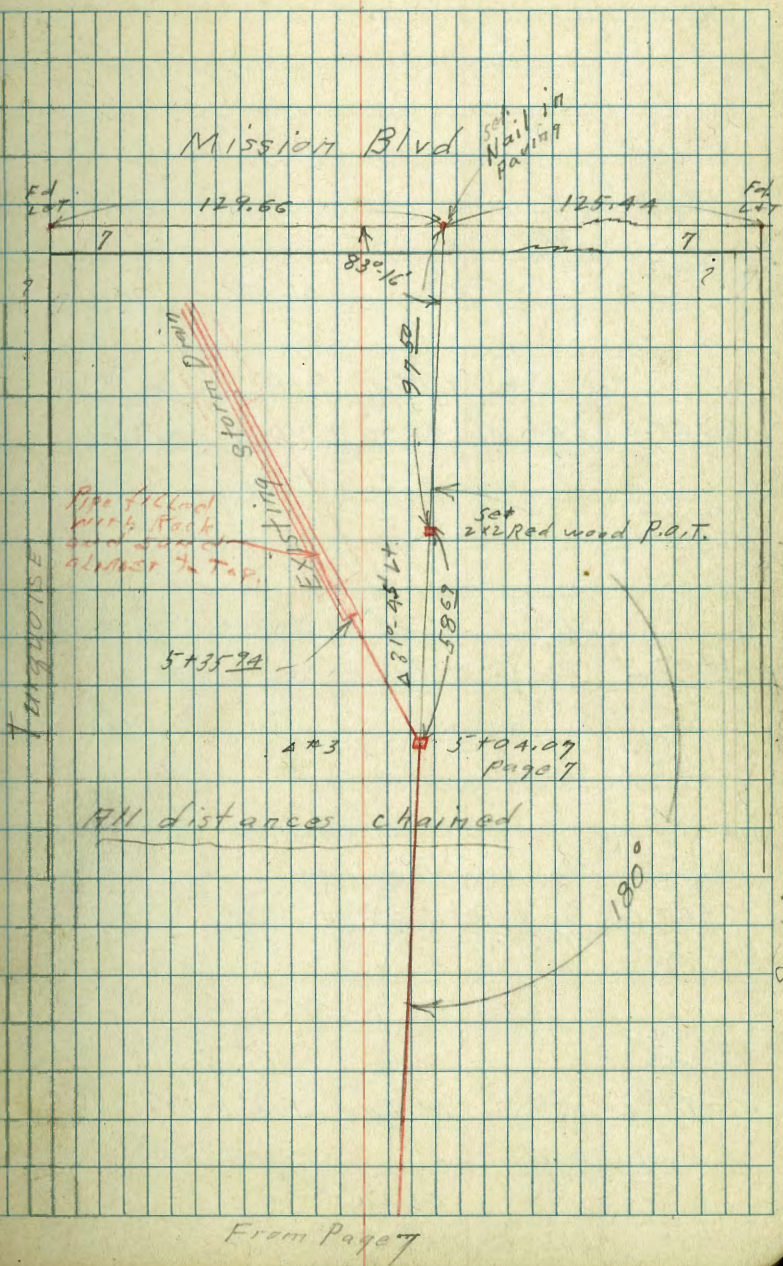
W.O. # 900A1

AUG 16 1951



2+2 P.O.T 202.76

W.O. 90041



Chisela 0+00 East end Ry culvert.	7.17	61.70	12.51	54.53
T.P.	0.65	67.04	13.11	66.39
T.P.	1.74	79.50	13.08	77.76
T.P.	0.28	90.84	8.76	90.56
Sapphire + Mission Blvd	0.78	99.32	—	98.54 NWBR

From Page 7

section continued

17.5	1.0	58.1	58.4	58.2	61.9	61
99	60	30	53	2.5	+3.2	+30
		15	95	8.1	58	89
			atol.			

section at 90° to Axis of culvert

0+20.6 End of apron + wing walls

58.89	58.39	55.29	55.18	55.26	61.70
2.81	6.31	6.46	6.52	6.44	2.94
2.5	9.5		7	23.4	23.4
top wing wall end	culvert		± Culvert	floor culvert	top wing wall

section at 90° to Axis of culvert

0+03.2 Break in top of wing walls

61.3	61.3
+7.6	+7.6
6.4	81.7
top wing wall	81.7 - top wing wall

0+00 = ± culvert - East end culvert
Along Face of culvert

69.3	54.61	54.53	54.50	69.3
+7.6	7.09	17.17	7.10	+7.6
6	6		6	6
top wing wall				top wing wall

-17.9
0-79.2 = West end Ry. Culvert (Page 7)

51.4
10.29

61.70

61.70 ✓

21.88.52
 Δ 39' 19.64"

9.07

1+55

1+40

1+15

0+90

T.P. 12.85 74.27 0.28 61.42

0+70

0+43

61.70

86.9	67.3	62.7	61.3	59.9	60.2	60.3	62.4	65.7	62.4
+12.6	7.0	11.6	13.0	14.4	14.1	12.0	13.2	8.6	+10.1
70	28	8	6	3		10	33	47.4	75

61.5	61.3	59.5	60.7	62.8	65.4	62.0
12.8	13.0	14.5	13.6	11.5	8.9	
34	20	8		5	20	8.4
8.4						
						+17.7
						65

92.7	61.1	61.9	58.7	59.5	62.7	66.7	91.8
+17.9	13.2	12.4	15.6	14.8	11.6	7.6	+17.3
78	55	22	20	1		10.8	37
	0.4						

62.3	60.7	61.0	59.0	57.4	66.1	69.3	91.4
11.0	13.6	13.3	15.3	16.7	8.2	+17	+17.1
75	60	75	12		7.4	30	35
8.4							
							74.271

83.7	69.8	60.7	57.7	57.9	56.9	57.5	61.3	61.7	91.5
+22.0	1.3	1.0	7.0	3.8	5.3	4.2	9.7	9.0	+17.8
100	56	16	13	4		8	8	10	95

88.7	88.9	80.7	55.8	57.1	57.1	66.8	82.3
3.0	3.3	5.0	5.7	4.6	2.6	+5.1	+20.6
30	14	6		7	8	67	100

61.70

W.O. 90041

Lott
T.P. 7.37 83.26 0.67 75.89

2+73

T.P. 11.36 76.56 9.07 65.20

2+39 ^{Δ 33° 36' 41"}
taken on split of L

2+28

2+00

1+90

1+67

74.27

^{93.1} ^{79.5} ^{72.5} ^{70.0} ^{67.5} ^{67.1} ^{73.3} ^{78.8} ^{84.7}
 $\frac{+16.5}{48}$ $\frac{+2.7}{36}$ $\frac{4.3}{24}$ $\frac{6.6}{12}$ 9.3 $\frac{8.7}{5}$ $\frac{3.3}{10}$ $\frac{+2.2}{25}$ $\frac{+12.6}{58}$
 76.56

^{79.8} ^{67.9} ^{65.7} ^{64.0} ^{64.4} ^{71.6} ^{70.3} ^{90.1}
 $\frac{+5.5}{17}$ $\frac{6.4}{6}$ 9.1 $\frac{3.3}{5}$ $\frac{4.9}{12}$ $\frac{2.8}{36}$ $\frac{+1.0}{55}$ $\frac{+22.4}{94}$
 84.14

^{77.8} ^{77.8} ^{77.1} ^{77.8} ^{67.9} ^{69.9} ^{67.1} ^{67.1} ^{72.1} ^{96.7}
 $\frac{+18.5}{65}$ $\frac{+8.5}{56}$ $\frac{+4.8}{53}$ $\frac{+5.5}{8}$ 5.4 3.4 2.2 $\frac{4.6}{25}$ $\frac{2.2}{53}$ $\frac{+22.4}{76}$
 77.14

^{91.5} ^{87.9} ^{87.8} ^{78.5} ^{78.6} ^{73.8} ^{67.1} ^{66.5} ^{63.5} ^{67.6} ^{68.6} ^{77.5} ^{94.0}
 $\frac{+18.2}{83}$ $\frac{+13.6}{75}$ $\frac{+13.5}{70}$ $\frac{+4.2}{65}$ $\frac{+4.9}{91}$ $\frac{0.5}{24}$ 5.6 7.8 10.8 6.2 5.7 $\frac{+5.2}{70}$ $\frac{+17.7}{97}$
 74.14

^{91.7} ^{87.3} ^{88.1} ^{78.5} ^{67.8} ^{66.9} ^{63.3} ^{65.8} ^{68.4} ^{93.1}
 $\frac{+17.4}{82}$ $\frac{+13.0}{71}$ $\frac{+13.3}{56}$ $\frac{+4.2}{42}$ 6.5 $\frac{7.4}{27}$ $\frac{11.0}{33}$ $\frac{8.5}{40}$ $\frac{5.9}{30}$ $\frac{+17.4}{93}$
 74.14

^{91.7} ^{88.0} ^{87.6} ^{77.1} ^{72.0} ^{67.9} ^{63.3} ^{67.1} ^{67.1} ^{64.5} ^{91.1}
 $\frac{+18.2}{75}$ $\frac{+13.7}{85}$ $\frac{+13.3}{65}$ 2.6 $\frac{2.3}{25}$ 10.4 11.0 13.6 11.2 7.8 $\frac{+18.7}{85}$
 74.14
 T.P.
 canyon

74.27

3+87⁵⁰ } Δ 90° 54' Rt. Taken on split.

3+83

3+67

3+53

3+32

3+00

83.26

Lt.

±

Rt.

97.8

12

97.5

+11.5
87

+11.2
140

97.8
+16.5
4.5
R177

75.9
7.4
9

75.7
7.6

76.5
6.8
15

77.9
10.4
16

72.9
10.4
23

79.8
3.5
32

94.0
+10.7
22.5

92.4
+12.9
82

96.4
+12.9
33
R177

75.7
7.5
4 22

75.5
7.8

94.1
+12.8
42
R177

89.6
+6.3
38

79.8
3.5
46

75.4
8.1

72.8
10.5
5

71.7
11.6
10

72.1
11.2
14.01

90.6
+13.3
42
R177

83.3
0.0
22

78.0
5.3
15

72.6
10.7

71.5
11.8
6

71.7
11.5
8

73.4
9.9
10

75.8
7.5
22.01

92.8
+9.5
51

95.4
+11.9
44

75.0
8.3
0.01

71.3
12.0
5

71.0
12.3

72.0
11.3
5

72.1
11.2
18

90.1
76.8
53

92.5
+9.2
65

91.8
+14.5
70

95.6
+12.3
5.5
R177

72.1
11.2
22

71.9
11.4
5

71.3
12.0

70.8
12.5
7

68.9
14.7
10

69.9
13.4
18

86.6
+5.8
43

83.26 ✓

W.O. 90041

4+65

4+40

4+32

T.P.

9.36

89.07

3.55

79.71

4+29

4+04

4+03

83.26

101.9
+12.8
2.3
Rim

83.0
6.1

76.9
12.2
9

76.6
12.5
13

70.7
+1.6
10

78.3
+7.2
2.5
Rim

96.9
+7.8
5.2

101.8
+12.7
3.6
Rim

76.1
12.4
9.2

76.6
12.6

75.6
13.5
3

75.6
13.5
10

97.1
+3.0
16

97.3
+8.2
2.3
Rim

91.9
+12.8
3.6
Rim

75.9
13.7
5.2

75.3
13.8
89.07

75.5
13.6
7.4

89.1
0.0
14

94.3
+5.2
2.0

102.4
+19.1
2.0
Rim

75.6
7.7
3.8

75.6
7.7
1

80.4
2.7
1

89.1
+5.8
1.3

102.3
+19.0
4.3
Rim

73.9
10.3
3.4

73.0
10.3

102.3
+19.0
7.3
Rim

76.6
6.8
6.8

76.5
6.8

83.26

N.W.B.P.
Saphire
Mission Blvd

W.O. 900 A1

98.54

6.81

98.53

T.P. 4.67 105.34 0.26 100.67

T.P. 12.82 100.98 0.96 88.11

5+55

5+35.94 = outlet 54" culvert.

5+35.9

5+25

5+04.92 Δ 31'-45" Lt taken on split

4+85

89.07

Lt.

±

Rt

14

101.1
+ 12.0

18.53
10.54
Invert

100.1
+ 14.6
14
Rim

82.4
6.7
7

82.1
7.0

82.3
6.8
3

99.1
+ 11.5
20

101.1
+ 12.0
29
Rim

81.6
7.5
7
8.2

81.3
7.8

81.9
7.2
10
8-X

100.1
+ 11.0
42
Rim

99.4
+ 10.3
27
Rim

80.9
8.2
5
8.5

79.25
9.32
on Hub.

77.1
9.4
5

81.1
0.8
9

97.3
+ 10.2
26
Rim

106.9
+ 12.8
20
Rim

82.7
5.2
8.5

81.2
7.9

77.5
11.6
5

92.1
+ 3.0
6

97.9
+ 8.8
27
Rim

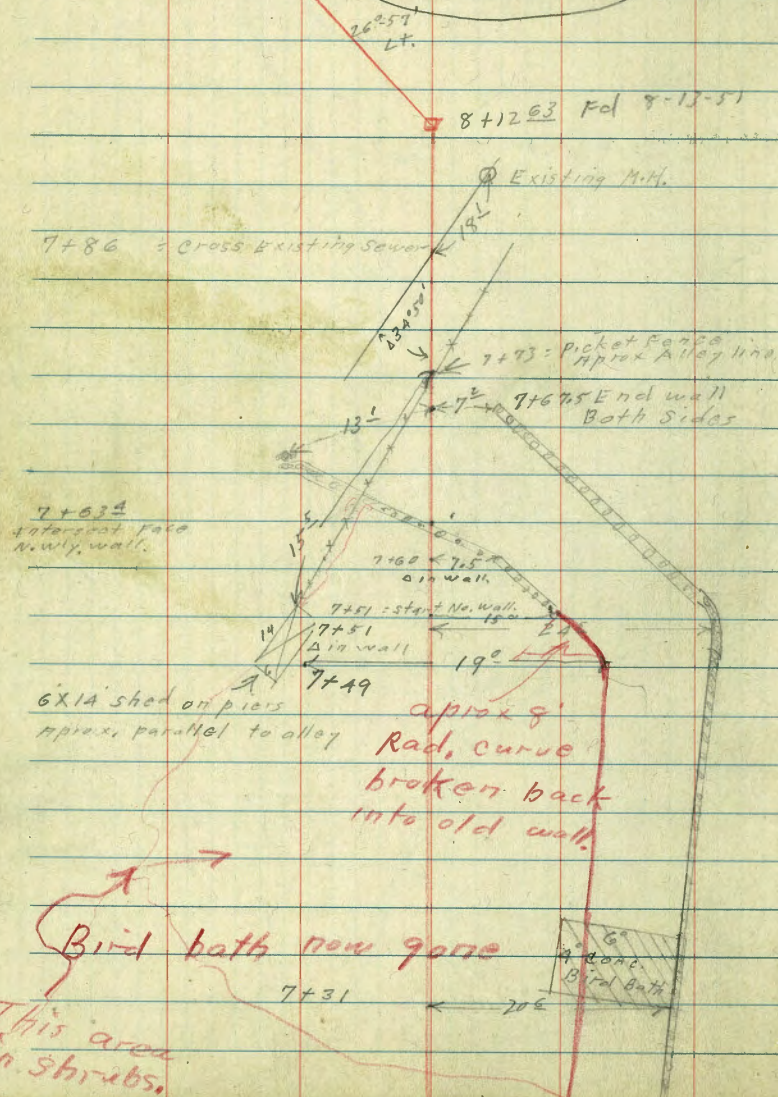
98.1
+ 3.0
40

89.07

W.O. 90041

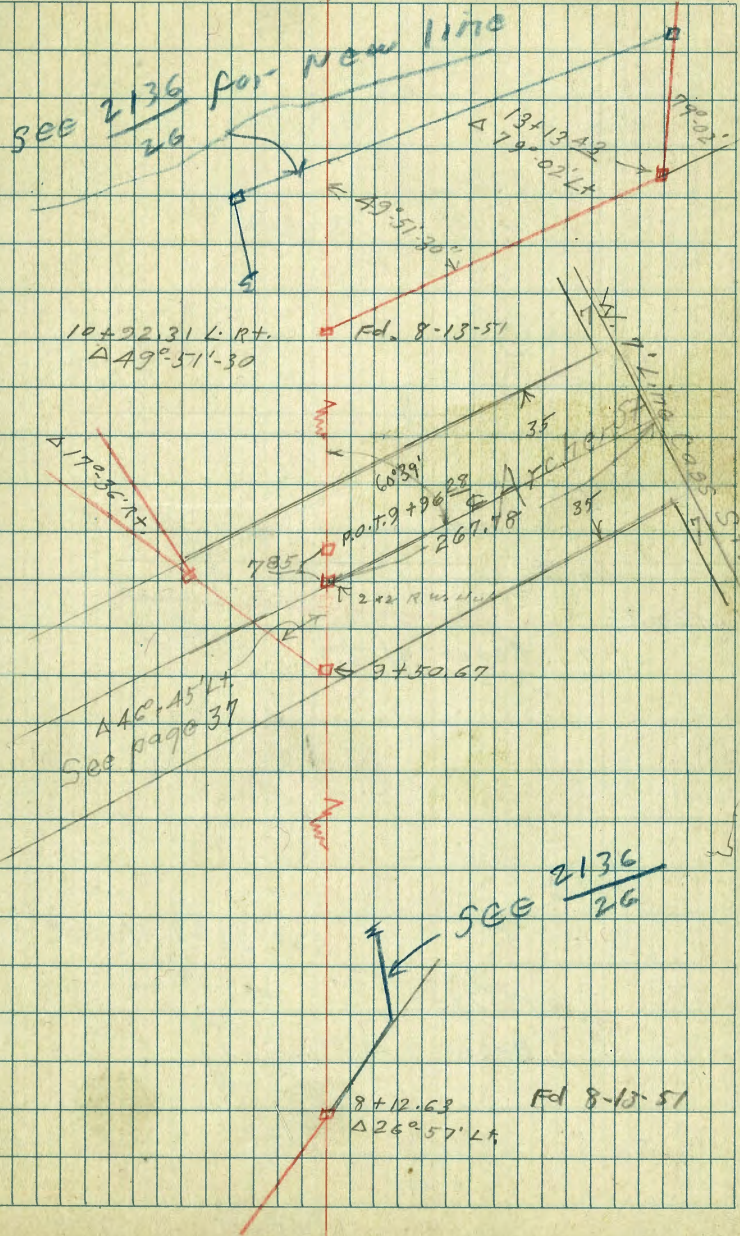
Proposed Drain

Continued detail
for page 15 Lt.



16

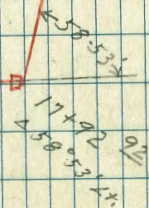
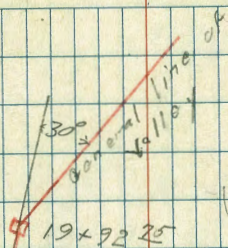
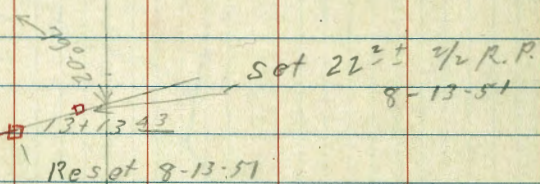
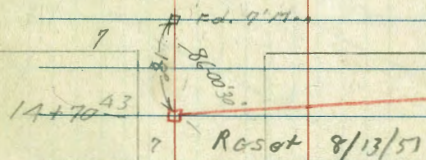
Cont. P. 17 on Lt



W.O. 90041

Cass. Sta

Van Nuys



W.O. 90041

1+10

Sammermeyer
W Moore
Melton

0+85

0+48

0+36

0+14.7

97.7 98.4 99.8
6 12.0

0+00

2x2 Hub. (sketch P.6)

0-1e

Inlet ^{5A} culvert; sketch P.6

T.P.

2.70

110.49 ✓

0.48

107.79

N.W.B.P.
Saphira +
Mission Blvd

9.73

108.77 ✓

—

98.54

Lt.

⊖

Rt.

18

108.5	107.0	106.5	105.8	99.7	99.3	99.6	105.5	105.7
20	35	40	47	10.8	11.2	10.9	5.0	9.8
20	15	15		2	10	18	20	30

105.9	105.9	98.7	98.0	98.3	99.9	106.2	105.0
5.2	3.6	4.8	12.5	12.2	10.6	4.3	5.5
30		20	6	15	18	20	50

104.7	106.3	108.0	99.9	97.3	97.0	101.3
9.8	7.7	14.5	10.6	13.2	13.5	7.2
25	13	11		7	12	16

105.8	105.8	99.6	97.1	96.5	96.2	102.4	102.7
4.7	7.7	10.9	14.0	14.3	8.1	7.8	
23	3	6	12	10	11	20	

110.5	96.5	93.8	96.8	97.9	102.6
9.0	14.0	13.7	13.7	12.6	7.9
28	6	9	9	22	35

93.8 ✓

16.67

Invert

110.49 ✓

2+65E Intersect sewer in 11167

2+65

2+53

2+10

1+80

1+65

∠ 1+45.89 267.51° 14' 30" TAKEN ON SPIRE

T.P. 12.18 117.14 5.53 102.96
110.494

L+

+

R+

19

1137	1171	115.1	1144	1126	1100	1101	1136	107.96	Intersect
46.6	41	41	2.7	5.0	2.1	2.0	3.5	9.18	
85	55	12		19	23	34	45	53.0	
								14.4	

1136	1171	115.8	1148	1121	1111	1088	109.9	123.1
46.5	41	43	2.3	5.0	6.0	3.3	2.2	46.0
90	60	20		19	31	34	43	65

1201	1140	115.0	1113	1111	1047	1047	107.2	111.6
4.30	21	41	5.8	6.0	12.4	12.1	9.9	5.5
85	50	17		2	8	11	15	35

109.8	109.1	106.9	102.4	108.2	107
73	80	10.2	14.7	8.9	6.1
75	3	7	16	30	

108.2	107.9	107.9	101.8	108.0	108.3
89	92	8.2	13.3	9.1	4.2
13	9	10	17	35	

110.5	108.2	107.47	107.1	101.3	101.3	110.7	119.7
66	69	9.67	14.0	15.8	15.8	6.4	42.6
75	55	3	8	12	19	40	

117.14

W.O. 90041

3+65

3+25

3+20

2+90

2+78

2+70

T.P. 9.91 124.76 2.29 114.85

L+

⊕

R+

20

128.3	127.2	116.3	118.3	127.8	121.6	121.8	127.7
125	127	85	65	41	42	30	129
100	81	80	31	13		30	45

127.4	127.2	114.9	114.2	123	115.9	114.2	116.6	123.9
126	124	99	106	125	89	86	82	89
75	83	86	30	11	8		9	35

127.4	127.0	121.9	114.0	112.3	115.6	115.4	116.5	123.9
126	122	2.9	10.8	125	9.3	94	83	09
75	63	50	30	7	4		7	35

116.8	112.8	110.6	110.8	112.5	112.8	114.7
90	120	102	140	123	120	121
30	12	10	5	3		15

116.4	114.2	110.5	110.5	110.8	112.1	114.5
84	106	103	103	120	127	103
25	7	2		7	2	30

115.9	114.3	113.1	110.0	109.7	113.0	125.6
89	10.5	11.7	14.8	15.1	11.8	10.8
15		5	7	17	40	62

124.76

L+

⊖

R+

5+05

132.8	132.1	132.5	132.5	132.0	131.3	131.5
106	51	47	47	52	109	87
60	35	14		30	15	60

4+65

128.3	128.6	129	128.8	128.9	128.4	121.5	131.8
39	36	93	94	83	118	107	94
50	30	15		21	39	46	57

T.P. 9.46 132.17. 2.05 122.71

132.17 ✓

1+30

130.4	121.5	122.1	122.0	120.9	120.8	122.3	120.4	122.8	124.8
151	33	27	28	39	40	55	44	20	80
50	32		7	10	18	24	30	32	30

3+98

130.3	126.8	121.0	119.7	128.4	121.4	123.0	124.5	125.3	121.6
151	40	32	56	64	34	28	13	10.5	12.8
73	50	30	17		13	23	32	25	58

3+76

127.3	127.8	116.8	118.9	121.4	121.3	121.9
125	70	80	39	34	35	29
80	71	70	35	18		15

122.76 ✓

VX.0. 90041

6+04

T.P. ON HUB
AT 659500

9.70

137.35

4.52

127.65

L 5+9500

L 1802 RIGHT

TAKEN ON SPLIT

5+63

5+60

5+25

L+

±

R+

22

126.8	126.6	127.4	127.4	127.4	127.3	127.8
86	87	99	102	99	807	86
20	4	2		18	19	12
				600	Foot	
					Wall	

137.35 ✓

134.7	130.7	128.1	126.8	127.6	127.6	127.4
72.0	2.0	4.1	5.4	4.6	2.6	3.8
50	35		3	6	17	20

126.8	127.9
5.4	4.3
	5.3

130.7	130.7	127.3	126.8	127.9	130.1
4.5	1.5	4.9	5.4	4.3	2.1
38	23	19		30	23

133.2	127.5	127.2	126.6	123.8	127.9	129.7	132.8
4.0	4.7	5.0	5.6	8.4	9.3	2.5	4.6
57	36		10	20	53	50	65

132.171

Lt.

RT

6+63.5

133.7	132.4	131.4	130.8	131.8	131.2
47	38	30	6.6	55	51
14	8	0.5	Top Wall	4	7
			Geo. E		

6+57 END OF WALL ON LEFT

132.9	131.2	128.4	129.0	130.8	130.8	131.2
43	67	92	84	65	66	67
15	10	10	27	25		4
Geo.	Top Wall	Geo	Geo	Top Wall		

6+50

132.8	130.4
46	70
8	
Bed	
Bed	

6+41

132.7	130.0	127.6	128.8	130.4	129.6	129.6	129.2	131.4
49	74	92	86	69.5	77	78	81	59
18	13.2	12.2	5.2	5	4		7	15
	Top Wall		Top Wall					

6+29

132.0	129.8	127.6	128.6	129.6	128.6	126.4	128.8	130.8
54	76	96	83	73.0	86	89	85	66
20	12.6	11	5.0	4.6	3.7		9	18
	Top Wall	Geo	Geo	Top Wall	Geo			

6+11

129.0	129.0	127.4	128.0	129.5	128.0	128.0
83	84	101	93	72.2	93	94
15	7	Geo	0.1	4	1	10
	Top Wall		Geo	Top Wall		

137.951

WP. 90041

LT

E

RT

24

7+35 STEPUP IN WALL & CENTER OF
6" N. & S. CONC. WALL.

133.9	136.6
8.2	5.5
21.6	21.6
TOP OF WALL	STEPUP

7+33 CENTER OF BIRD BATH

130.1
12.9
1.8

7+31

134.5	132.4	131.7	130.1	130.1	130.2	130.8	131.7
26	8.9	9.4	12.0	12.0	9.8	8.3	7.2
15		10	15	20	20.6	20.8	27
				TOP	TOP WALL	STEPUP	WALL

TP 7.55 14212 2.78 134.57

14212

7+12

SEE F.B. 2136
29

134.4	133.0	131.2	129.4	129.8	131.8	134.8
37	4.3	6.1	7.9	7.5	5.5	2.5
15		9	11	17.5	13	25
					TOP WALL	

6+80.7 TOP OF S' GROUND LAY.

131.91
5.14

137.35

7+672 END OF WALLS - BOTH SIDES

7+632

7+632 ± TOP OF WALL

7+51

7+49 STEP-DOWN IN WALL

7+48

134.6	134.0	132.1	130.9	131.6	133.0	134.0	137.1
7.5	8.1	11.0	11.2	10.5	9.1	8.1	5.0
20	13.1	13		7.0	7.2	15	20
	TOP WALL	GRD		GRD	TOP WALL		

132.8

11.3

133.6

8.5

135.3	134.8	134.0	132.7	130.5	130.4	133.1	136.2	139.1
6.8	7.3	8.1	9.8	11.6	11.7	9.0	5.9	3.0
15	6		15	15.5	24	24.5	26	30
				TOP WALL	GRD	TOP WALL	GRD	GRD

133.1

9.0

25

130.2

136.6

11.9

5.5

24.5

25.5

TOP WALL

142.12

9+70

9+56

9+48

9+41

9+03

T.P. 7.68 150.77 0.73 143.09

8+75

143.82

L+

E

R+

27

187.1	185.8	182.2	184.9	185.0	180.7	180.7	181.3	139.7	139.5	182.7	152.9
3.7	5.0	8.6	5.9	5.8	10.1	10.1	9.5	11.1	11.3	8.1	+2.1
50	40	35	25	11	5		15	23	34	4.0	4.9

148.5	187.5	182.1	183.2	189.7	181.1	181.2	181.3	139.7	152.6
3.3	3.3	8.7	7.6	6.1	9.7	9.6	9.5	11.1	+1.8
50	40	34	20	17	9		13	30	5.5

188.8	187.7	181.9	181.1	181.6	181.8	139.6	185.1	152.0
2.0	3.1	8.9	7.7	7.2	7.0	11.2	5.7	+1.2
50	35	28	6		9	38	50	70

150.9	188.3	146.9	185.1	180.6	181.4	180.1	186.0
0.9	2.5	3.9	5.9	10.2	7.4	12.7	7.8
50	30	18	9		12	15	60

188.8	185.2	182.9	138.2	138.6	182.1
2.0	5.6	6.7	12.9	12.2	8.7
50	5		17	38	50

150.79 ✓

187.8	187.9	184.9	139.1	138.1	136.1	136.6	139.7	182.8
+4.0	+3.6	+1.1	4.7	5.7	7.7	7.2	3.1	0.0
50	40	15		8	16	24	33	15

143.82 ✓

W.O. 900A1

10+05

10+01

P.O. Hub.

T.P.

9+96.28

8.79

159.49

0.07

150.70

9+95

9+92

9+85

9+76

150.77

L7

Φ

R7

28

126.7	126.9	128.3	129.7	132.0	133.9	139.3
$\frac{12.8}{50}$	$\frac{12.5}{24}$	$\frac{15.2}{10}$	$\frac{14.8}{4}$	$\frac{7.5}{2}$	$\frac{5.6}{20}$	$\frac{5.2}{21}$

126.9	126.9	128.3	129.6	131.1	132.3	133.9
$\frac{12.6}{50}$	$\frac{12.5}{27}$	$\frac{15.2}{15}$	$\frac{14.9}{4}$	8.4	$\frac{6.2}{17}$	$\frac{5.6}{35}$
			159.49			

126.6	126.9	128.3	129.2	129.6	130.6	132.9	139.8	143.8
$\frac{4.2}{50}$	$\frac{4.4}{29}$	$\frac{7.5}{24}$	$\frac{6.5}{9}$	$\frac{12}{5}$	0.2	$\frac{+2.5}{20}$	$\frac{11.0}{22}$	$\frac{+3.0}{44}$

130.3	130.8	139.7	139.9	139.8	153.8
0.5	$\frac{0.9}{5}$	$\frac{11.1}{6}$	$\frac{10.9}{15}$	$\frac{11.0}{32}$	$\frac{+3.0}{44}$

129.2	129.3	129.8	129.0	129.7	130.2	133.2
1.6	$\frac{1.5}{1}$	$\frac{10.0}{2}$	$\frac{10.8}{6}$	$\frac{10.1}{10}$	$\frac{11.6}{38}$	$\frac{+2.6}{42}$

126.1	122.6	125.3	129.9	129.5	129.5	129.9	129.3	129.2	133.0
$\frac{4.7}{37}$	$\frac{3.2}{35}$	$\frac{5.5}{17}$	$\frac{6.4}{7}$	$\frac{10.3}{1}$	10.3	$\frac{10.4}{5}$	$\frac{9.5}{10}$	$\frac{11.6}{39}$	$\frac{+2.7}{44}$

150.77

11+02

10+92.31 $\Delta 49^{\circ}51'30''$ Rt taken on split

10+82

10+68

10+59

10+30

159.49

Lt.

E

Rt.

29

186.9	149.9	148.9	159.5	155.1	155.9
$\frac{2.6}{54}$	$\frac{18.1}{40}$	$\frac{10.6}{15}$	5.0	$\frac{4.4}{10}$	$\frac{4.1}{25}$

156.2	155.8	147.1	148.2	151.7	153.62	155.0	156.2
$\frac{3.3}{50}$	$\frac{3.7}{44}$	$\frac{12.4}{26}$	$\frac{11.3}{12}$	$\frac{7.8}{10}$	$\frac{5.87}{4.46}$	$\frac{4.5}{7}$	$\frac{3.3}{40}$

155.1	158.7	149.5	146.5	147.8	151.8	159.2
$\frac{4.4}{50}$	$\frac{4.8}{40}$	$\frac{10.4}{22}$	$\frac{13.0}{20}$	$\frac{11.7}{8}$	$\frac{7.7}{6}$	5.3

153.8	152.9	148.6	146.5	146.9	150.5	159.7
$\frac{5.7}{50}$	$\frac{7.1}{32}$	$\frac{10.9}{13}$	$\frac{13.0}{19}$	$\frac{13.1}{9}$	9.0	$\frac{4.8}{15}$

152.3	150.9	147.0	145.5	145.5	149.6	155.3
$\frac{8.2}{30}$	$\frac{8.6}{24}$	$\frac{12.5}{15}$	$\frac{14.0}{6}$	14.0	$\frac{9.9}{3}$	$\frac{4.7}{20}$

147.7	147.7	146.9	145.8	149.9	148.9	153.3	152.9
$\frac{11.8}{50}$	$\frac{11.8}{20}$	$\frac{12.5}{7}$	13.7	$\frac{14.6}{3}$	$\frac{14.6}{8}$	$\frac{6.2}{13}$	$\frac{4.6}{30}$

159.49 ✓

W.O. 90041

11+68

11+58

11+54 ♀ creek (cross creek)

11+50 Cross creek.

11+38

11+10

159.49

157.8 157.5 152.1 152.8 159.3 159.0 153.9 155.3 158.0

$\frac{1.7}{40}$ $\frac{2.0}{25}$ $\frac{7.4}{20}$ $\frac{6.7}{15}$ $\frac{5.2}{12}$ 5.5 5.6 $\frac{4.2}{38}$ $\frac{1.5}{50}$

153.0

5.9

151.6

7.9

152.5

7.0

157.7 159.5 152.9 151.9 150.9 153.1 153.1 158.2

$\frac{1.8}{25}$ $\frac{5.0}{15}$ 6.6 $\frac{3.1}{5}$ $\frac{3.6}{17}$ 6.4 6.4 $\frac{1.3}{30}$

157.1 150.0 149.3 152.0 152.2 155.9

$\frac{2.4}{25}$ $\frac{7.5}{35}$ 10.2 7.5 $\frac{7.3}{24}$ 3.6

159.49 ✓

30

13+00

157.6	158.8	168.7	169.2
7.0	$\frac{5.8}{11}$	$\frac{4.1}{16}$	$\frac{4.6}{25}$

12+75

160.1	157.6	156.9	156.5	156.7	160.5	167.5
$\frac{4.5}{25}$	$\frac{7.0}{6}$	$\frac{8.2}{4}$	8.1	$\frac{7.9}{13}$	$\frac{4.7}{17}$	$\frac{4.9}{25}$

12+50

161.6	161.1	158.6	157.2	155.5	156.2	155.3	157.1	159.1	163.1
$\frac{3.0}{30}$	$\frac{3.5}{21}$	$\frac{6.0}{8}$	$\frac{7.4}{8}$	$\frac{9.1}{6}$	9.4	$\frac{9.3}{3}$	$\frac{7.5}{6}$	$\frac{5.5}{14}$	$\frac{1.5}{35}$
162.57 ✓									

T.P.

8.34 164.57 3.26 156.23

12+23

160.8	159.5	159.7	157.2	158.3	161.5
$\frac{4.9}{20}$	$\frac{5.0}{7}$	4.8	$\frac{2.3}{3}$	$\frac{1.2}{25}$	$\frac{4.0}{50}$

12+17

161.0	153.9	159.0	156.7	156.3	157.7	160.9
$\frac{4.5}{21}$	$\frac{5.6}{7}$	$\frac{5.5}{1}$	2.8	$\frac{2.7}{10}$	$\frac{1.8}{37}$	$\frac{4.9}{50}$

12+00

159.3	155.3	153.0	153.0	155.6	156.8	156.0	155.7	156.1	160.7
$\frac{9.6}{26}$	$\frac{4.2}{22}$	$\frac{6.5}{1}$	$\frac{6.5}{6}$	$\frac{3.9}{5}$	3.7	$\frac{3.5}{15}$	$\frac{3.8}{22}$	$\frac{3.4}{48}$	$\frac{4.2}{36}$

159.49

159.49 ✓

V.O. 900A1

13+90

169.2	160.8	159.9	161.6	163.1	163.3	165.1	159.5
$\frac{8.3}{20}$	$\frac{11.7}{33}$	$\frac{12.6}{6}$	$\frac{10.9}{4}$	3.1	$\frac{7.2}{11}$	$\frac{7.9}{25}$	$\frac{3.0}{27}$

13+76

162.3	160.8	159.9	159.3	160.0	161.9	162.8	169.2
$\frac{10.2}{15}$	$\frac{11.7}{6}$	$\frac{13.1}{5}$	$\frac{13.2}{172.46}$	$\frac{12.5}{4}$	$\frac{10.6}{5}$	$\frac{2.7}{16}$	$\frac{3.1}{31}$

T.P. 11.88 172.46 3.99 160.58

13+65

162.3	161.7	160.9	158.8	159.1	161.7	163.1	170.9
$\frac{2.3}{30}$	$\frac{2.9}{17}$	3.7	$\frac{5.8}{2}$	$\frac{5.5}{7}$	$\frac{2.9}{10}$	$\frac{1.5}{16}$	$\frac{+5.8}{32}$

13+40 75 Rt. = Φ pole # 5324 PB1-78

13+34

159.1	159.9	158.3	158.2	159.7	169.0
$\frac{5.5}{10}$	5.2	$\frac{6.3}{1}$	$\frac{5.7}{8}$	$\frac{4.9}{11}$	$\frac{+4.4}{23}$

13+23

152.7
6.9

13+13^{A3} $\Delta 79^{\circ} 02'$ Lt. Taken on split of L

13

162.2	159.9	158.9	158.0	157.7	158.52	159.1	168.6
$\frac{2.4}{35}$	$\frac{5.2}{37}$	$\frac{5.7}{14}$	$\frac{6.6}{10}$	$\frac{6.9}{3}$	6.05	$\frac{5.5}{2}$	$\frac{+4.0}{10}$

164.57

Lt.

Φ

Rt.

32

14+93 8² Rt. = outlet 30" culvert

169.0	167.3	166.7	163.39
$\frac{3.5}{2}$	5.2	$\frac{5.8}{5}$	$\frac{9.07}{14}$
Invert + Ground			

14+90⁴³ Δ Taken on split

168.5	167.82	166.5	162.5
$\frac{4.0}{25}$	$\frac{5.04}{4.26}$	$\frac{5.9}{11}$	$\frac{9.7}{17}$

14+56

168.9
6.1

14+46

167.0	166.7	161.9	162.0	165.1	163.8
$\frac{5.5}{30}$	$\frac{5.8}{20}$	10.0	$\frac{10.5}{4}$	$\frac{7.4}{14}$	$\frac{3.7}{30}$

14+35

166.5	166.3	161.3	169.5	166.3	168.9
$\frac{6.0}{30}$	$\frac{6.2}{26}$	$\frac{11.2}{11}$	8.0	$\frac{6.2}{20}$	$\frac{3.6}{32}$

14+15

163.5	162.9	160.9	161.0	162.9	169.0	165.9	169.0
$\frac{9.0}{43}$	$\frac{10.1}{24}$	$\frac{11.6}{19}$	$\frac{11.5}{15}$	$\frac{7.6}{13}$	8.5	$\frac{6.6}{26}$	$\frac{3.5}{30}$
172.46 ✓							

172.46

W.O. 90041

16+50

T.P. 11.88 183.72 0.62 171.84

16+00

15+29

15+24 3² Lt. = 1/2 IN let 30" Culvert

15+20

14+98

172.46

Lt.

E

Rt.

34

173.9	173.1	169.8	169.7	171.8	171.9
$\frac{9.8}{30}$	$\frac{10.6}{14}$	$\frac{13.9}{11}$	14.0	$\frac{12.3}{6}$	$\frac{11.8}{30}$
<u>183.72</u> ✓					

171.6	170.2	168.2	168.1	169.2	169.0	170.8
$\frac{0.9}{30}$	$\frac{2.3}{14}$	$\frac{4.3}{10}$	$\frac{4.4}{7}$	3.1	$\frac{3.5}{21}$	$\frac{1.7}{30}$

169.0	168.7	165.6	165.1	166.5	167.6	167.3
$\frac{3.5}{30}$	$\frac{3.8}{15}$	$\frac{6.9}{9}$	$\frac{7.4}{1}$	6.0	$\frac{4.9}{11}$	$\frac{5.2}{30}$

169.2	168.9	165.2	165.15	167.3	168.7	168.1
$\frac{3.3}{30}$	$\frac{3.6}{10}$	$\frac{3.3}{27}$ <small>0.2</small>	$\frac{3.1}{3.3}$ <small>1/100.4</small>	5.2	$\frac{3.8}{6}$	$\frac{4.4}{20}$

169.4	169.1	168.9
$\frac{3.1}{20}$	3.4	$\frac{3.6}{20}$

169.3	168.8	168.7
$\frac{3.2}{10}$	3.7	$\frac{3.8}{20}$

T.P. 9.96 187.96 5.72 178.00

18+27

18+22

17+92⁹² Δ

L₂ taken on split

17+70

17+35

17+00

183.72

176.9

6.8

178.9

3.8

179.7 177.9 179.5 173.8 176.0 178.7 178.73 180.1 181.3

$\frac{1.0}{60}$ $\frac{5.8}{40}$ $\frac{9.4}{30}$ $\frac{9.9}{24}$ $\frac{7.7}{22}$ $\frac{5.0}{13}$ $\frac{4.177}{446}$ $\frac{3.6}{15}$ $\frac{2.4}{25}$

177.9 173.6 173.9 175.2 177.3 178.6 179.4 180.3

$\frac{5.8}{30}$ $\frac{10.4}{20}$ $\frac{10.3}{14}$ $\frac{8.5}{13}$ $\frac{6.4}{12}$ 5.1 $\frac{4.2}{10}$ $\frac{3.4}{30}$

172.4 176.6 175.0 172.9 173.0 173.2 174.9 176.2

$\frac{6.3}{25}$ $\frac{7.6}{18}$ $\frac{8.7}{10}$ $\frac{10.8}{8}$ 10.7 $\frac{10.5}{4}$ $\frac{8.8}{8}$ $\frac{7.5}{52}$

176.9 176.0 171.9 171.7 172.1 172.8 172.7

$\frac{7.3}{30}$ $\frac{7.7}{10}$ $\frac{11.8}{7}$ 12.0 $\frac{11.6}{18}$ $\frac{10.9}{55}$ $\frac{6.0}{40}$

183.72 ✓

N.O. 90041

S.W. 7th Mon.
Archer + Cass

Error 0.05
163.06 shown as
10.62 163.01 ✓ 163.06

T.P. 4.57 173.63 12.74 169.06

S.W. 7th Mon.
Van Noy + Cass S.S. 13.32 168.48 ✓

T.P. 2.81 181.80 8.97 178.99

19+72⁷⁵ ex Hub.

19+60 L in Wash

19+26

18+50

187.96

Lt.

♀

R+

36

Notes Reduced 5-15-97

186.5 185.1 182.2 189.50 186.1 186.5

$\frac{1.5}{55}$ $\frac{2.9}{47}$ $\frac{5.8}{40}$ 3.46 on Hub $\frac{1.7}{10}$ $\frac{1.5}{25}$

183.8 183.0 182.8 186.1 179.9 183.9 185.2 186.1

$\frac{4.2}{30}$ $\frac{5.9}{11}$ $\frac{5.6}{3}$ 7.7 8.1 $\frac{4.6}{9}$ $\frac{2.8}{20}$ $\frac{1.8}{30}$

182.6 182.6 179.1 179.8 182.6 188.0

$\frac{5.4}{30}$ $\frac{5.4}{13}$ $\frac{8.9}{7}$ 8.2 5.4 $\frac{0.2}{12}$

179.7 179.1 175.5 175.8 177.1 179.1 189.1

$\frac{8.8}{25}$ $\frac{8.2}{11}$ 12.5 $\frac{12.2}{4}$ $\frac{10.8}{6}$ $\frac{8.9}{19}$ $\frac{3.9}{25}$

187.96 ✓

Drainage Area Crossing
Mission Blvd. at Targuaise

"B" Line
Work Order 90041.

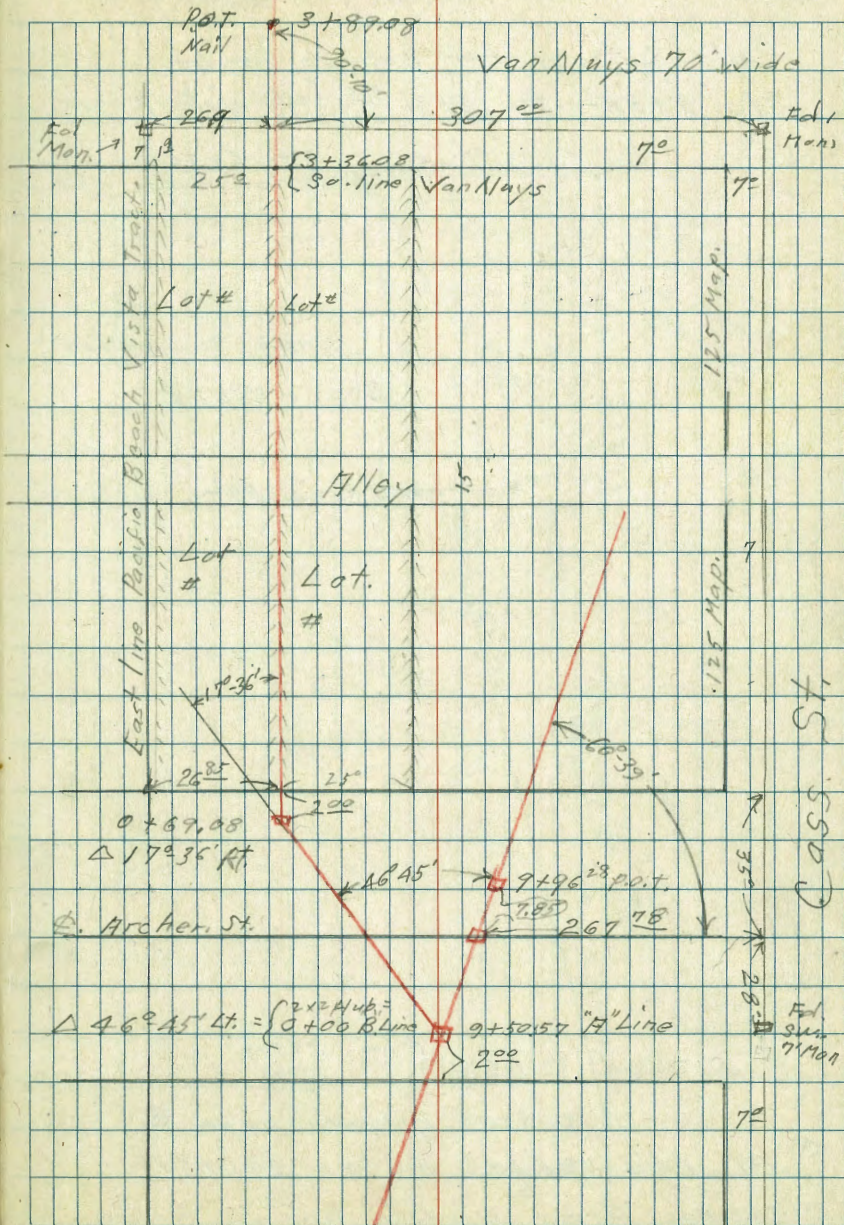
Samuel Meyer
W Moore
L Maltzer.
5-12-47

INDEXED

"B" Line run from 9+50.57 on
"H" Line, to mouth of canyon
North of Van Nuys and west
of Cass. Flood waters
west to Mission Blvd. can
be taken care of by the
streets when they are improved.

Archer St. (300' West of Cass) N.Y. 37

Cont. P. 38 on Rt.



Levels "B" line W.O 90041

Sketch on pages 37+38

0+46

0+43

0+28

0+18

0+14

△ 46°-45' Lt.

0+00 = 2 x 2 Hub 9 + 50.57 = on "A" line

P.O.T. H. 69 + 2628

Page 28

1.13

151.83 ✓

— 150.70 ✓

Lt.

±

Rt.

39

195.9 192.5 193.1

$\frac{5.9}{10}$ 9.3 $\frac{8.7}{10}$

192.6 192.5 193.8

$\frac{9.2}{10}$ 9.3 $\frac{8.0}{10}$

192.9 199.9 195.1

$\frac{8.9}{10}$ 6.9 $\frac{6.7}{10}$

192.5 199.7 199.3 198.4 192.5

$\frac{9.3}{10}$ $\frac{7.1}{5}$ 9.5 $\frac{7.6}{7}$ $\frac{9.3}{10}$

191.6 191.5 190.5

$\frac{10.2}{10}$ 10.3 $\frac{11.3}{10}$

191.9

10.4

151.83 ✓

W.O. 90041

"B" Line

0+35

1+22

T.P. 11.82 161.53 2.12 149.71

1+08

0+69.08 = Δ 17° 36' Rt. Taken on split.

0+51

0+48

151.83 ✓

Lt.

±

Rt.

40

152.2	153.0	152.6	153.9
$\frac{9.8}{40}$	$\frac{8.5}{35}$	8.9	$\frac{7.6}{20}$

151.7	151.9	151.0	151.5
$\frac{9.8}{45}$	$\frac{10.1}{13}$	10.5	$\frac{10.5}{10}$
		161.53 ✓	

198.3	197.5	197.7
$\frac{3.5}{10}$	4.3	$\frac{4.1}{10}$

196.2	196.9	196.2
$\frac{5.6}{10}$	5.4	$\frac{5.4}{10}$

195.9	196.0	196.1
$\frac{5.9}{10}$	5.8	$\frac{5.7}{10}$

196.0	195.9	193.2
$\frac{5.8}{10}$	5.9	$\frac{8.6}{10}$

151.83 ✓

"B" Line

T.P. 12.24 173.31 0.46 161.07

3+35 27 Lt = 10" tree Also cross East - West ^{Hedge}

3+30 19 Lt = 10" tree

3+00

2+95 =

2+92 - 16' Lt = 10" tree

2+70 29' Lt = L in wash & wash

End Misc. rabbit hutches + chicken Coops

2+40 44' Lt = Edge of wash running S.W. by waste

start Misc. Rabbit Hutches an chicken Coops.

2+10 Cross East West wire fence

2+00

1+54

161.83

160.8	161.1	159.9	161.1	161.3	161.6
$\frac{0.7}{50}$	$\frac{0.3}{27}$	$\frac{1.6}{25}$	$\frac{0.9}{24}$	$\frac{0.2}{25}$	$\frac{+0.1}{25}$
160.7	161.0	160.7	159.5	160.8	161.2
$\frac{0.8}{50}$	$\frac{0.5}{35}$	$\frac{0.8}{27}$	$\frac{3.0}{26}$	$\frac{0.7}{24}$	$\frac{0.9}{25}$
159.0	159.5	158.9	156.6	160.1	160.0
$\frac{2.1}{50}$	$\frac{2.0}{40}$	$\frac{5.6}{35}$	$\frac{4.9}{23}$	$\frac{1.4}{14}$	$\frac{1.5}{25}$
157.7	157.6	158.3	159.1		
$\frac{8.8}{48}$	$\frac{8.7}{25}$	$\frac{3.2}{25}$	$\frac{2.3}{25}$		
155.6	156.1	156.8	157.2	157.5	
$\frac{5.7}{50}$	$\frac{5.4}{25}$	$\frac{4.7}{25}$	$\frac{4.1}{25}$	$\frac{4.0}{50}$	
152.1	152.2	159.5	155.2	155.5	
$\frac{8.4}{40}$	$\frac{7.3}{20}$	$\frac{7.0}{15}$	$\frac{6.3}{15}$	$\frac{6.0}{45}$	
		161.53 ✓			

"B" Lines

3+79

3+73 8⁵ Lt. = ϕ 30" Cor. Iron Culvert.

3+53

3+91

3+38 Continued

3+38

173.31

Lt.

ϕ

Rt.

42

146.1	146.5	145.7
$\frac{7.2}{25}$	7.1	$\frac{7.6}{25}$

165.3	166.1	161.9	141.6	145.9	166.3	165.5
8.0	7.2	11.4	11.7	7.4	7.0	7.8
50	18	16	8.6	6	5	25
			INVERT			

168.1	165.1	161.3	161.0	162.9	165.1	162.9
9.2	8.2	13.0	13.3	8.4	8.2	8.9
50	21	17	13	9		25

162.7	163.7	160.7	161.9	162.8	162.8
10.4	9.6	12.6	11.7	10.5	10.5
50	25	23		10	25

162.6	163.2	162.7
14.7	9.9	14.6
50	25	25

160.7	160.9	162.1	163.2	163.6	163.7
13.6	12.4	11.2	9.9	9.7	9.6
24	22	21	11		25
44	45	44			

173.31 ✓

T.P. 11.21 182.58 1.94 191.37

4+61

4+35

at the way from here until noted

4+20 Wash is filled with trash most

3+96

3+92 6³ Lt. = 30" Corrugated culvert

3+91

173.31

172.1	171.6	167.6	167.4	171.4	172.0	171.5	171.4
$\frac{1.2}{25}$	$\frac{1.7}{11}$	$\frac{5.7}{8}$	$\frac{5.9}{4}$	1.9	$\frac{1.3}{9}$	$\frac{1.8}{14}$	$\frac{1.9}{25}$
169.8	170.3	170.0	168.3	166.3	169.8	169.3	
$\frac{3.5}{25}$	$\frac{3.0}{13}$	$\frac{3.9}{5}$	5.0	$\frac{7.0}{4}$	$\frac{3.5}{11}$	$\frac{4.0}{25}$	
169.1	169.2	165.2	165.0	168.6	168.9	169.1	168.5
$\frac{4.2}{25}$	$\frac{4.1}{10}$	$\frac{8.1}{7}$	8.3	$\frac{4.7}{2}$	$\frac{4.9}{5}$	$\frac{4.2}{11}$	$\frac{4.8}{25}$
167.4	167.7	163.3	163.6	167.6	167.6	167.1	167.2
$\frac{5.9}{25}$	$\frac{5.6}{12}$	$\frac{10.0}{10}$	$\frac{9.7}{3}$	$\frac{5.7}{5}$	5.7	$\frac{6.2}{15}$	$\frac{6.1}{25}$
167.3	166.5	162.8	166.6	167.2			
$\frac{6.0}{12}$	$\frac{6.8}{7}$	$\frac{10.5}{6.7}$ invert	$\frac{6.7}{5}$	6.1			
	166.6		166.7			166.5	
	$\frac{6.7}{25}$		6.6			$\frac{6.8}{25}$	

173.31 ✓

5+40

5+31

wooden hand rails

5+23 3' wide wooden foot bridge

4+92

4+80

4+73

182.58

176.8	176.7	173.0	174.9	176.2	176.5
$\frac{5.8}{20}$	$\frac{5.9}{10}$	$\frac{9.6}{6}$	7.7	$\frac{6.4}{3}$	$\frac{6.1}{15}$

177.0	176.8	173.0	173.0	175.3	175.7	176.1	175.9
$\frac{5.6}{15}$	$\frac{5.8}{11}$	$\frac{9.6}{7}$	$\frac{9.6}{5}$	$\frac{7.3}{2}$	6.9	$\frac{6.5}{2}$	$\frac{6.7}{15}$

175.8	175.72	175.7
$\frac{6.8}{14}$	6.86	$\frac{6.9}{2.3}$
End bridge		End bridge

174.2	174.3	170.1	170.2	173.8	173.8	172.8	173.1
$\frac{8.4}{20}$	$\frac{8.3}{14}$	$\frac{12.5}{10}$	$\frac{12.4}{6}$	$\frac{8.8}{2}$	8.8	$\frac{8.8}{3}$	$\frac{9.5}{15}$

173.4	173.4	168.8	169.2	172.0	173.2	172.5
$\frac{9.2}{15}$	$\frac{9.2}{14}$	$\frac{13.8}{9}$	$\frac{13.4}{5}$	10.6	$\frac{9.4}{3}$	$\frac{10.1}{15}$

173.3	172.9	168.3	169.7	172.6	172.1
$\frac{9.3}{15}$	$\frac{9.7}{11}$	$\frac{14.3}{4}$	$\frac{12.9}{7}$	10.0	$\frac{14.5}{15}$

182.58 ✓

W.O. 90041 "B" Lino

S.W. 7' Men.
Van Noy's +
Cass.

2.04
169.48
3.59 168.44 ✓ Page 36
168.48

T.P. 2.49 172.03 12.90 169.54

T.P. 1.56 182.44 5.65 180.88
6+31⁵ Junction of washes

6+10 L in wash under house

T.P. 5.63 186.53 1.68 180.90

5+88¹ start frame Bldg. L in wash

T.P. 5.63 186.53 1.68 180.90

5+77 3² Rt. start rubble + Conc. wall. 1² wide

5+65

182.58

45

Haste Reduced - 5-15-07

181.5 181.3 178.6 181.3 181.9
5.0 5.2 7.9 5.2 4.6
20 15 8 15

177.6 177.6 179.1 180.8 181.1
5.9 8.7 7.4 5.7 5.4
Apr 20 75 Def. wash
under house 2 10

186.53 ✓

181.0 180.6 180.5 180.7 177.2 177.1 177.2 179.3 179.6
1.6 2.0 2.1 1.9 5.4 5.5 5.4 3.3 3.0
10 6 5 12 4 6 7 15
top wall top wall

179.1 178.6 176.5 176.9 178.4 180.5 179.6 180.0
5.5 4.0 6.0 6.0 4.8 2.1 3.0 2.6
15 7 5 3 13.2 4.5 15
top wall Brd

178.14 176.8 175.4 176.9 178.9 178.4
4.2 5.8 7.2 5.7 4.7 4.2
15 8 2 4 15

182.58 ✓

25005

CROSS SECTION ALLEY BLK. 178
PACIFIC BEACH
Between Emerald and Felspar
from Olney St to Noyes St.

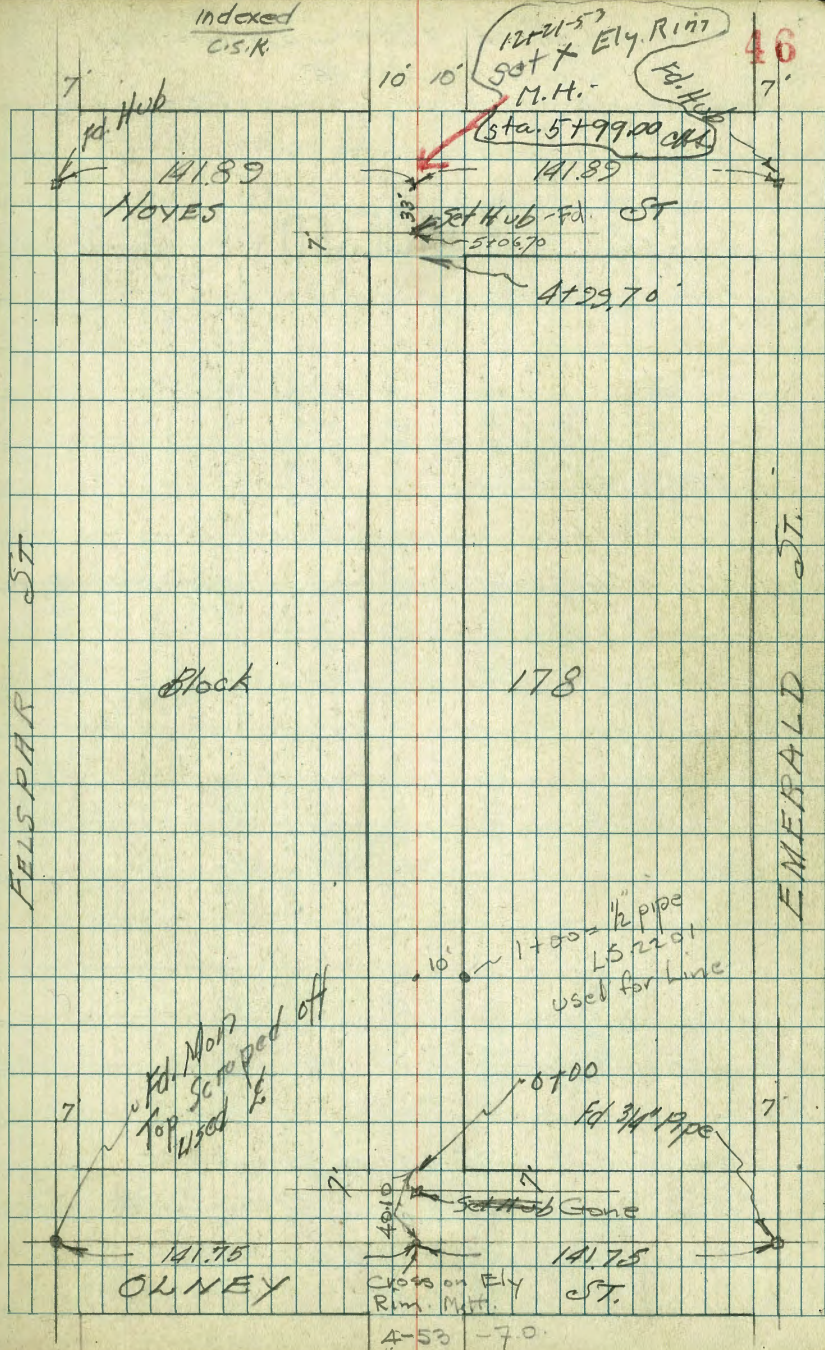
Walker
Boeker
Williams
4-13-48

INDEXED

See Book 2268 - P. 9 for New
Sections

U.O. 31786

Indexed
C.S.K.



Alley Block 178 - Cross Sections

Cont. from P-46

+ X - E1

INDEXED

0+50

0+00 = W.L. Olney

0-7 on Hub

66.73
8.76

0-17.7 = Elec Pole P-4624 10.3' W - Hedge

0-22

0-23

0-40 = P. Olney

1.0

T.P. 5.89 75.49 0.24 69.60

T.P. 7.87 69.84 6.36 61.97

T.P. 2.07 68.33 6.09 66.26

6.52 72.35 65.83

Lt.

R

P. 47

66.7	67.0	66.7	67.2	68.1	68.6	68.3
8.8 20	8.5 14	8.8 12	8.3 10	7.4	6.9 10	6.2 20
		65.3	66.7	66.7	67.4	67.8
		10.2 30	8.8 10	8.8	1.0 1	1.7 10
						1.0 30
63.8	64.2	65.8	65.5	65.5	66.2	66.8
11.7 40	11.3 23	9.7 10	10.0 7	10.0	9.3 7	8.7 10
		63.3	64.8	65.1	65.6	66.7
		12.2 40	10.7 10	10.4	1.9 10	1.5 10
		63.8	65.1	65.5	66.0	67.2
		11.7 40	10.4 10	10.0	9.8 10	8.3 10
			75.49			
NW. BR Garnet and NOYES ST.						
NW. BR Garnet and Morrell ST.						
SW. BR Garnet and Lament						

INDEXED

2+41 = End 4 Car Garage on Top Conc. Foundation
 2+04 = Beg. 4 Car Garage Under Const.

2+30 = Pole Anchor 8.1' L.

2+09 to 2+21 = 12x18 Frame Bld. 7.7 Ft.

2+09 to 2+21 =

2+04 = Elec. Pole A-21.50 7.7' L. = N edge

2+00

1+85

1+65

See P. 52 Also.

1+32

1+00

7549

48

69.1	69.8	70.5	70.9	71.2	70.5	70.3	70.3
6.4 10	5.7	5.0 10	4.6 8	4.3 10	5.0 3	5.2 4	5.2
				2.84 Conc. Foundation			
	70.6	71.4	71.9	72.5	72.8		
	4.9 20	4.1 10	3.6	3.0 10	2.7 20		
	70.6	71.4	71.4	71.8	72.4		
	4.9 20	4.1 10	4.1	3.7 10	3.1 20		
	70.1	70.4	71.0	71.4	71.9		
	4.4 20	5.1 10	4.5	4.1 10	3.6 20		
	69.5	69.8	69.9	70.3	70.6		
	5.0 20	5.7 10	5.6	5.2 10	4.9 20		
68.7	69.1	69.9	69.6	69.7			
5.8 20	5.4	5.6	5.9 10	5.8 20			

7549

Alley BK. 178, Pacific Beach
 Survey to Determine if
 encroachments exist.

Roberts
 W. Moore
 Clark
 2-4-49
 W.O. 21001

Resident at 2131 Emerald
 believes builder of apartment across
 alley to be in error for
 grading alley. Dirt has been
 removed by one of 2131 Emerald's
 bldgs. and more filled in by "KAT.
 Kennels" thereby impairing proper
 drainage (city has ^{since} helped drainage),
 and endangering one bldg. by
 a cut.

Following is a supplement to
 foregoing survey, Pgs. 46-51 - Sections
 shown only where question and changes
 exist.

2700

1796

1765

Begin Grading See P. 48 Also

B.M.

6.57

73.27

66.73

47' Sub
 other st.
 See page
 47

INDEXED

WK
 FEB 8 1949

68.9	69.4	70.5	69.8	70.1	70.8	72.3	72.3
$\frac{4.4}{20}$	$\frac{3.9}{10}$	$\frac{2.8}{7}$	$\frac{3.5}{5}$	3.2	$\frac{2.5}{6}$	$\frac{4.0}{8}$	$\frac{1.0}{10}$

70.4	70.7	71.0	70.1	70.1	70.8	72.3	72.2
$\frac{2.9}{25}$	$\frac{2.6}{10}$	$\frac{2.5}{7}$	$\frac{3.2}{5}$	3.2	$\frac{2.5}{6}$	$\frac{1.0}{8}$	$\frac{1.1}{10}$

70.4	70.8	71.3
$\frac{3.9}{20}$	2.5	$\frac{2.0}{10}$

73.27

Cont'd From Page 52

3+10 Toe of Fill

3+00

2+95

2+75

2+50

2+35 Appears to be end of cut and begin of fill.

2+21 End Bldg.

2+09 12x18 Bldg. 7.7 Ft.

73.27

Lt.

R

Rt

53

65.4	65.8	65.9	66.1						
$\frac{7.9}{20}$	$\frac{7.5}{10}$	7.4	$\frac{7.3}{8.5}$						
			Fence						
65.7	66.7	66.9	66.2						
$\frac{7.6}{10}$	$\frac{8.6}{8}$	6.4	$\frac{7.1}{7}$						
			Bldg.						
67.5	67.5	67.3	67.0	66.3					
$\frac{3.8}{20}$	$\frac{3.8}{10}$	6.0	$\frac{6.3}{5}$	$\frac{7.0}{8}$					
				Fence					
67.4	67.8	68.3	68.1	66.6					
$\frac{3.9}{20}$	$\frac{5.5}{10}$	5.0	$\frac{5.2}{5}$	$\frac{6.7}{7.5}$					
				Bldg. + Toe of Fill					
68.2	68.2	68.4	68.1	69.02	69.3	68.1			
$\frac{5.1}{20}$	$\frac{5.1}{10}$	$\frac{4.9}{7}$	$\frac{1.2}{2}$	$\frac{4.25}{12.5}$	$\frac{4.0}{5}$	$\frac{5.2}{8.5}$			
				Rim M.H.		Fence + Toe of Fill			
68.4	68.3	68.6	69.1	69.5	70.3	69.9			
$\frac{4.9}{19.6}$	$\frac{5.0}{10}$	$\frac{4.7}{7}$	4.2	$\frac{3.8}{3}$	$\frac{3.0}{6}$	$\frac{3.4}{8.8}$			
						Fence			
68.6	68.2	68.4	69.0	69.4	70.3	71.9	71.9	71.9	
$\frac{4.9}{19.6}$	$\frac{5.1}{14}$	$\frac{4.9}{10}$	$\frac{4.3}{7}$	3.9	$\frac{3.0}{5}$	$\frac{4.4}{20}$	$\frac{4.4}{7.7}$	$\frac{4.4}{7.7}$	
									Footng Foundation
68.5	68.62	68.3	68.9	69.4	69.9	70.8	72.3	72.3	72.1
$\frac{4.7}{19.6}$	$\frac{4.6}{19.6}$	$\frac{3.0}{12}$	$\frac{4.4}{10}$	$\frac{3.9}{6}$	3.4	$\frac{2.5}{5}$	$\frac{4.0}{7}$	$\frac{4.0}{7.7}$	$\frac{4.2}{7.7}$
									Footng Foundation

Proposed Level on Floor of unfinished Apt. Garage 73.27 ✓

INDEXED

65 Starting 1317 1.04 65.06 65.06

TP 10.33 66.10 10.22 55.77

4+00.31 End (Floor of Garage)

3+98.5 Beg. Conc. Ramp to Garage

3+95.5 Beg 5' Conc. Sidewalk
End Conc Ramp 10.2 Rt.

3+74

3+58.7 @ 14' Garage 10.9 Lt.

6599

NEBP La Jolla Blvd & Pearl

64.95	64.92	64.67
1.04	1.07	1.32
82. Fl.	Fl.	Fl.
64.78	64.67	64.47
1.21	1.32	1.52
81		8.7

63.66	64.27	63.68	64.25
10.2	10.2	16	16
Ramp SW	Ramp SW	Ramp SW	Ramp SW
63.56	63.72		
1.23	1.27		
10.3	16.5		
Ramp	Fl		

64.6	64.3	63.9	63.56	63.72
1.14	1.17	1.21	1.23	1.27
10			10.3	16.5
			Ramp	Fl
64.33	63.79			
1.16	1.20			
16	10.9			
Fl	Ramp			

6599

3-17-49

Hendricks Additional Notes
Alley Block 2 La Jolla Park

3+50.4 End 19' Conc Drive 10.3 ft.

6320	6320
X 10	X 10
25	10.3

3+399 E 19' Drive 10.3 ft.

6321	6321
X 9	X 9
25	10.3

3+314 End Conc Ramp Beg 19' Conc Drive.

6322	6322
X 8	X 8
27	10.3

BM 5.48

62.82

Rim Sence M H Page 52 This Book

68.30

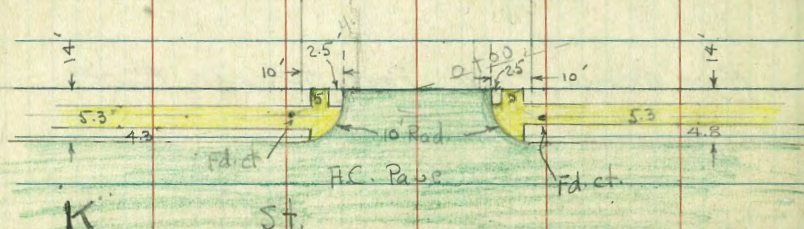
Set Lat. et.
for P.O.T. in
conc. step out
from Wall

29' 3+46

St.

30' 30'

Langley

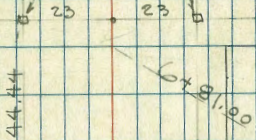


Island

St

Set Hubs

7' Line - from 27th
To 28th



Fid. Hub

St

30' 30'

Langley

X-Sect. Langley - from K to Island
60' st. - 10' cbs. Dirt - Graded.

3601

5-19-49

W.O. 21178

102.90

Osborne
Hardin
Hatch
Shepard

Rods around Returns.

N.W. Ret. - 19.6' around - 4 parts - 4.9' each

Beq. W. end = W.L. Langley	5.89 ^{97.01}	T - Top
	6.60 ^{96.80}	9 = gut.
4.9'	5.84 ^{97.06}	T
	6.64 ^{96.26}	9
"	5.78 ^{97.12}	T
	6.58 ^{96.82}	9
"	5.74 ^{97.16}	T
	6.45 ^{96.45}	9
	5.68 ^{97.22}	T
4.9' end = N.L. K.	6.41 ^{96.49}	9

INDEXED

WK

MAY 20 1949

B.M. 5.69 102.90 8.71 97.21 NW.B.P.
2.93 105.92 102.99 27' K

Lt.

±

Rt.

62

102.90

NE Ret. 19.9' around - 4 parts - 5' each

Beq. - N. end = N.L. K	6.82 ^{96.26}	T
	7.39 ^{95.51}	9
5'	6.90 ^{96.0}	T
	7.41 ^{95.49}	9
"	6.91 ^{95.99}	T
	7.53 ^{95.87}	9
"	6.91 ^{95.98}	T
	7.58 ^{95.32}	9
5' = end = E.L. Langley	6.93 ^{95.77}	T
	7.73 ^{95.17}	9

102.90

2+75- 19.9 Rt. = Beg. cb. + 5' walk

T.P. 11.66 139.60 0.28 127.94

30.2 Rt. = 15' of N. edge of 5.8' Conc. Steps thru wall
2+50- 30' Lt. = Beg. 8" Conc. wall

2+36- 30.1 Rt. = Beg. 6" Conc. block wall

2+27- 30.3 Rt. = Wly. of 6" Conc. block wall
walls on sides

2+25- 30.8 Lt. = ± 3.2' Conc. steps - with 6" Conc.

2+15- 30.3 Rt. = ± 3' Conc. steps

2+00- 30' Lt. = end of wall

1+96- 29.9 Lt. = ± of 6' Conc. steps Thru wall

1+51- 30.3 Lt. = Beg. Reck + Conc. wall - 18" wide

1+50

	131.1	130.4	128.1	128.6	128.6	128.4	124.1	129.53	729.61	129.8	131.9
8.5	9.2	11.0	11.0	10.9	11.0	11.7	10.13	10.07	9.99	7.8	7.70
30	21	14	7	139.60	8	19.9	19.9	22.5	27.5	30.3	30
along wall							Top	end of walk		Top	wall
+ 182.5	+ 185.7	+ 148.6	+ 142.2	+ 125.7	+ 145.6	+ 125.3	+ 126.5	+ 126.3	+ 128.4	+ 128.4	
Top of bank	Top of S.							Bottom of Step		Top of Steps	
2.6	2.4	2.6	2.9	2.2	2.2	2.2	2.2	2.2	2.2	2.2	2.2
ground											
136.0	142.84	127.0	124.7	124.7	124.7	124.7	124.7	124.7	124.7	124.7	124.7
43.8	43.8	43.8	43.8	43.8	43.8	43.8	43.8	43.8	43.8	43.8	43.8
Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank
133.7	129.77	122.8	121.5	119.6	119.2	119.2	119.2	119.2	119.2	119.2	119.2
Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank
130.7	129.77	122.8	121.5	119.6	119.2	119.2	119.2	119.2	119.2	119.2	119.2
Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank	Top of bank
128.22											
bank											Bank

T.P. 5.69 111.35 9.39 105.66 - on s.w. 7 Hub

6+71 - 12.2 Lt. = end fence

6+50 - House on Rt.

6+25

6+38 - 12.3 Lt. = Beg old wire fence

6+26 - 30.4 Rt. = end wire fence

6+00

T.P. 0.39 115.05 12.92 114.64

5+50

5+22 29 Rt. = Beg wire fence

5+00 - 30.5 Lt. = end of wall

T.P. 0.96 127.48 13.08 126.52

4+76 - see page 67

4+50 - 30.4 Lt. = Sly. of 3' Conc. Steps - thru wall

4+42 see page 67

4+25 - 29.2 Rt. = end of wall

4+12 - 30.8 Lt. = end of conc. walk - behind wall

Lt # Rt

6+71	12.2	Lt.	108.7	108.7	108.4	104.3	104.4	103.9	103.8	102.8	102.3
6+50			108.7	108.7	108.4	104.3	104.4	103.9	103.8	102.8	102.3
6+25			108.7	108.7	108.4	104.3	104.4	103.9	103.8	102.8	102.3
6+38	12.3	Lt.	108.7	108.7	108.4	104.3	104.4	103.9	103.8	102.8	102.3
6+26	30.4	Rt.	108.7	108.7	108.4	104.3	104.4	103.9	103.8	102.8	102.3
6+00			108.7	108.7	108.4	104.3	104.4	103.9	103.8	102.8	102.3
5+50			114.2	114.2	114.6	113.8	113.8	113.5	113.5	114.1	111.8
5+22	29	Rt.	114.2	114.2	114.6	113.8	113.8	113.5	113.5	114.1	111.8
5+00	30.5	Lt.	114.2	114.2	114.6	113.8	113.8	113.5	113.5	114.1	111.8
4+76			127.48	127.48	127.4	126.7	126.7	126.7	126.7	127.9	127.9
4+50	30.4	Lt.	127.48	127.48	127.4	126.7	126.7	126.7	126.7	127.9	127.9
4+42			127.48	127.48	127.4	126.7	126.7	126.7	126.7	127.9	127.9
4+25	29.2	Rt.	127.48	127.48	127.4	126.7	126.7	126.7	126.7	127.9	127.9
4+12	30.8	Lt.	127.48	127.48	127.4	126.7	126.7	126.7	126.7	127.9	127.9

129.60 30.8 end.

cont.

BM starting			453	706	70 ¹⁵ NEBP La Jolla Blvd Center St
TP	482	7462	620	6982	
BM			982	7665	NEBP Pearl + La Jolla Blvd (65 ⁰⁰ pages) 152066
TP	620	7652	430	6982	

50' North of end alley & Alley

20' North of end alley & Alley

0+66 1st RT SW cor board fence

0+65 7² 0⁸⁵ Lt NE cor garage con floor
25' int line + Back end Alley B/K 2 La Jolla P^{ark}

0+45

0+44 7³ Lt SE cor garage con floor

0+41 E crosses wooden Back Steps to house

0+39 2nd RT SW cor frame house

70

Lt

Rt

Rt

64.7

94

65.8

83

66.47
720
085
floor

66.47
765
on Hub

66.8

66.9

67.0

73

72

71

69.3

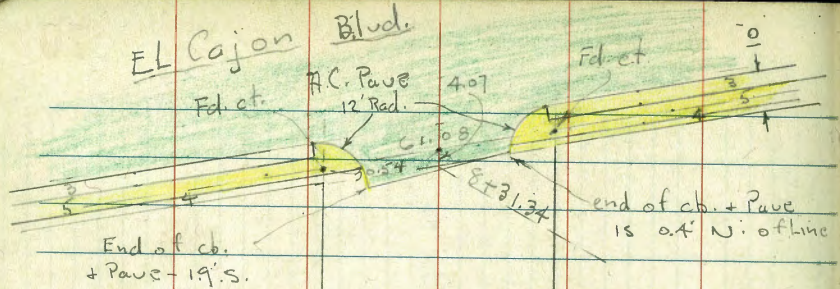
48

22

floor

7413

EL Cajon Blvd.



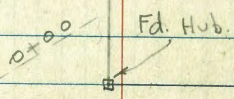
End of cb. + Pavé - 19' S.

INDEXED
W.K.
JAN 24 1950



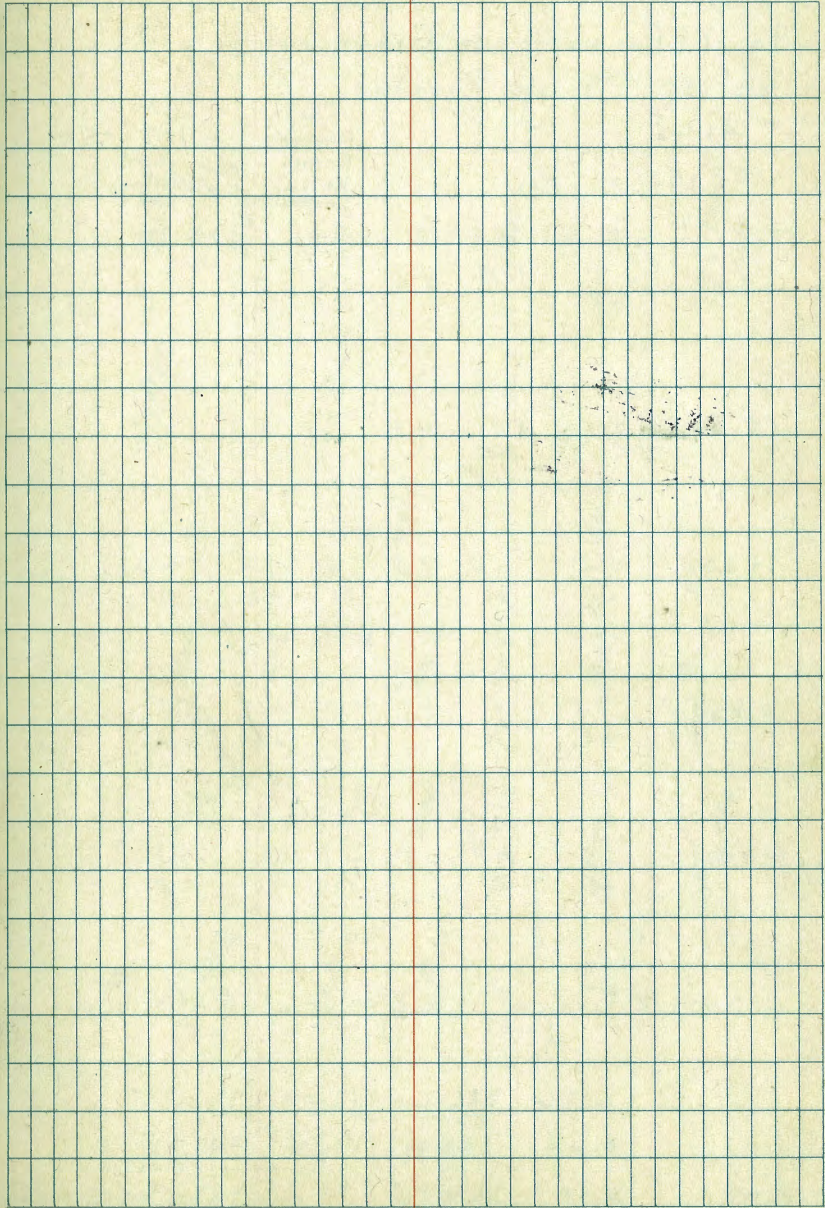
Hub

Dawson



Trojan

Hub



7+53 - 25.3 Lt. = ± 3' Conc. walk

of Drive - Below

7+41 - 25.7 Lt. = Ely. of 6" Conc. wall = W. edge

7+37 - 30' Rt. = Nly. of C.L. Dr.

To Sing. Car. Conc. floor (under House)

7+36 - 25.9 Lt. = ± 12 Conc. Dr. + Coldlay apron

7+25

Drive

7+16 - 29.9 Rt. = wly. of 8" Conc. wall = Sly. of C.L.

7+16 - 21.9 Lt. = ± Pipe # 4384

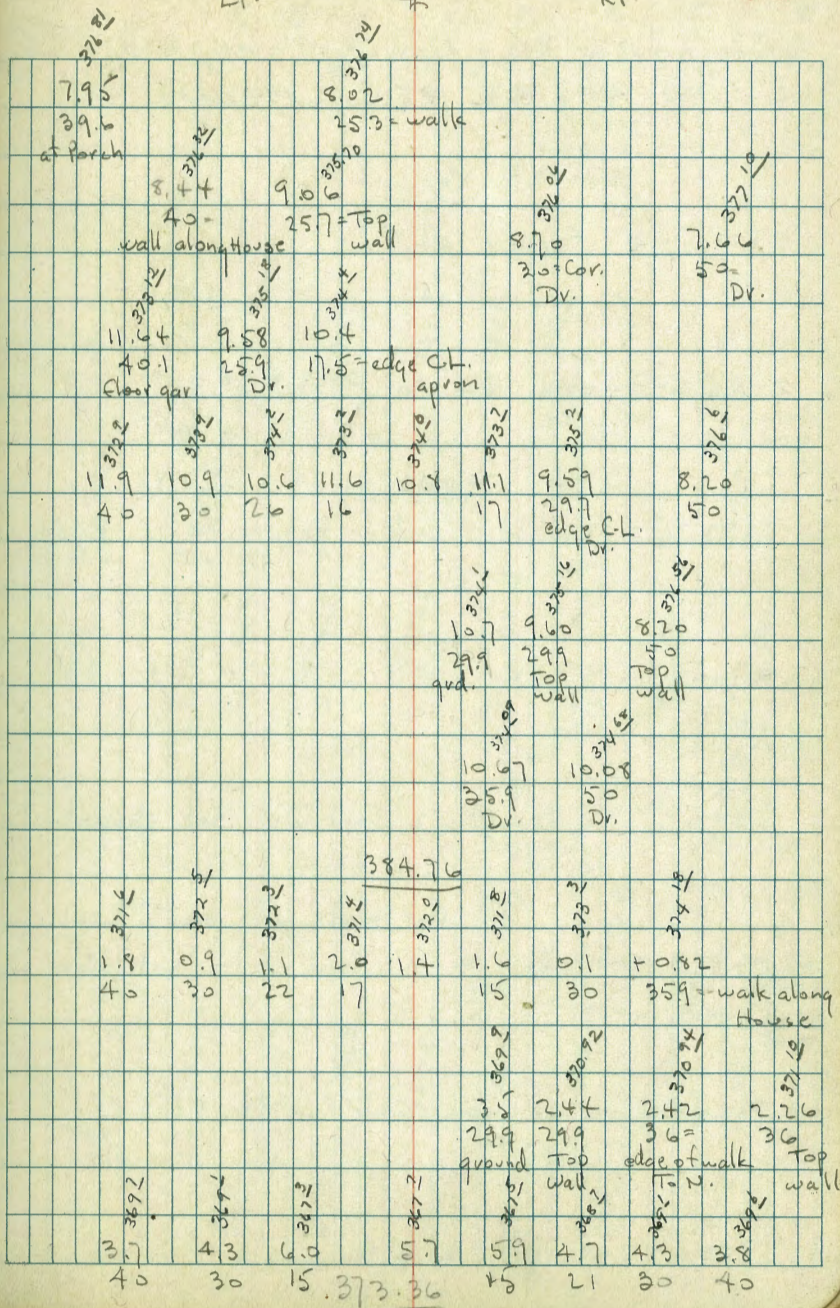
7+11 - 35.9 Rt. = ± 9' Conc. Dr.

T.P. 12.35 384.76 0.95 372.41

7+00

6+60 - 29.9 Rt. = wly. of 6" Conc. - Walk to N.

6+50



Note: - end of Ret. + edge of A.C. is 0.4' N. of S.L.
 8+31.34 = \pm + S.L. El Cajon - sect on S.L.

8+29.5 = \pm at edge A.C. Pave

8+25.64 = opp. S.W. Cor. - sect. at 90°

T.P. 7.74 390.62 1.88 382.88

8+23.75 - 18.6' Lt. = end of Return + A.C. Pave

8+00

7+92 - 29.1 Rt. = \pm 12' Conc. Dr. - Bet. shops

Gar. made into Beauty shop

7+81 - 20.1' Rt. = \pm 9' Conc. Dr. - (not used -

7+65 = on 2.5' Conc. walk on Lt.

7+60 - 20.1' Rt. = \pm 2' Conc. walk

Station	Dist	Angle	Height	Notes
8+31.34	30.54	382.20	8.6	Cor.
8+29.5	19.7	382.37	8.23	
8+25.64	19.7	381.20	8.92	get.
8+23.75	9.0	382.55	8.07	
8+20.0	7.39	382.23	7.39	
8+18.6	6.98	383.23	6.98	end of cb. 15' 0.4' North
8+15.0	6.50	384.11	6.50	
8+12.2	5.89	384.74	5.89	Top
8+9.5	5.18	385.5	5.18	Cor.
8+25.64	30.7	381.2	8.6	along shop
8+23.75	18.6	382.25	8.23	Top
8+20.0	11.6	382.25	8.34	edge A.C.
8+18.6	9.0	382.25	7.8	
8+15.0	7.6	383.0	7.6	
8+12.2	7.4	383.7	7.4	
8+9.5	6.5	384.1	6.5	
8+6.8	6.0	384.7	6.0	
8+4.1	5.1	385.5	5.1	
8+1.4	4.2	386.2	4.2	
8+0.0	3.3	387.0	3.3	
7+92	29.1	387.0	4.0	
7+81	20.1	387.0	3.4	
7+65	2.5	387.0	3.3	
7+60	20.1	387.0	3.3	
7+57.5	18.6	387.0	3.4	along shop
7+55.0	17.1	387.0	3.4	along shop
7+52.5	15.6	387.0	3.4	along shop
7+50.0	14.1	387.0	3.4	along shop
7+47.5	12.6	387.0	3.4	along shop
7+45.0	11.1	387.0	3.4	along shop
7+42.5	9.6	387.0	3.4	along shop
7+40.0	8.1	387.0	3.4	along shop
7+37.5	6.6	387.0	3.4	along shop
7+35.0	5.1	387.0	3.4	along shop
7+32.5	3.6	387.0	3.4	along shop
7+30.0	2.1	387.0	3.4	along shop
7+27.5	0.6	387.0	3.4	along shop
7+25.0	0.0	387.0	3.4	along shop
7+22.5	0.0	387.0	3.4	along shop
7+20.0	0.0	387.0	3.4	along shop
7+17.5	0.0	387.0	3.4	along shop
7+15.0	0.0	387.0	3.4	along shop
7+12.5	0.0	387.0	3.4	along shop
7+10.0	0.0	387.0	3.4	along shop
7+7.5	0.0	387.0	3.4	along shop
7+5.0	0.0	387.0	3.4	along shop
7+2.5	0.0	387.0	3.4	along shop
7+0.0	0.0	387.0	3.4	along shop

394.76

20.1 = walk

33 = at Porch

Elev. Curb ends

Events

Gresham } at Garnet

Haines

Gresham + Garnet Temp.
Temp. B.M. = End N.E. cb. 4.96 54.18 B.M. #1

N. End. N.E. cb. Gresham + Garnet

Curb end on N. line Garnet

N. end N.W. cb. Gresham + Garnet

T.P. 9.06 59.14 2.64 50.08

T.P. 7.09 52.72 2.96 45.63

T.P. 7.74 48.59 5.12 40.85

Nly end cb. N.E. Garnet + Events

{ 1/2 block existing curb on Ely, Events
80' Existing cb. on nly Events }

N.W. Cor. Events + Garnet
Nly end Curb

6.64 46.17

39.53

54.18
4.96 5.60
cc G

53.24
5.70 6.38
cc gutter

59.14

43.07

3.10

cb. at alley E.C.

Ret. B.C.

123' N. Nly line Garnet

Ely cb. Events

41.19

4.98

Curb

792' N. N. line Garnet

W. cb. Events 46.17

39.99

6.18

G

N. line Garnet

40.62

5.55

cb

39.39

6.84

G

cb. at
N. line
Garnet

39.57

6.60

N.W.B.P. Garnet + Events

Haines from Felspar to Diamond is
city school grounds. Grade at
Emerald + Haines will not affect grade
at Felspar + Haines. (No street.)

Ely. end west ab. Emerald
S. W. cor. Emerald + Grosham
(ab. ends on wly. line Grosham
No return.)

	6.88	66.26	2.23	59.38
Temp. B.M. #1	7.43	61.61	—	54.18
P. 77				

N. end Ely ab. Haines + Garnet

Chords on N. line Garnet

N. end wly ab. N.W. Haine + Garnet

T.P.	6.22	72.51	2.39	66.29
T.P.	10.00	68.68	0.46	58.68

59.14

62.07

4.19
ab.

No Pavc.

66.26

68.67
3.84
ab.

68.34
4.17
gutter

69.06
3.45
ab.

68.65
3.86
gutter

72.51

604
450
1650

163.06

31.34
5.7
25.64
1.9
23.74

134
407
541

63
2
626