

1765



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1765

CITY ENGINEER'S OFFICE

MICROFILMED

DEC 29 1964

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- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
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THE FREDERICK POST CO.

ENGINEERING and DRAFTING SUPPLIES

P. O. Box 803

CHICAGO

INDEXED

to page # 25.
except page # 1

Pages

2-7 - Location Prop. Row. Thru Navy
Destroyer Base Main to 32nd

8-10 - Ties - for above Job.

Xsec Alley Blk 79 Park Villas P. 14
23

24-31 - X-Sect. Delta - 40th to 41st

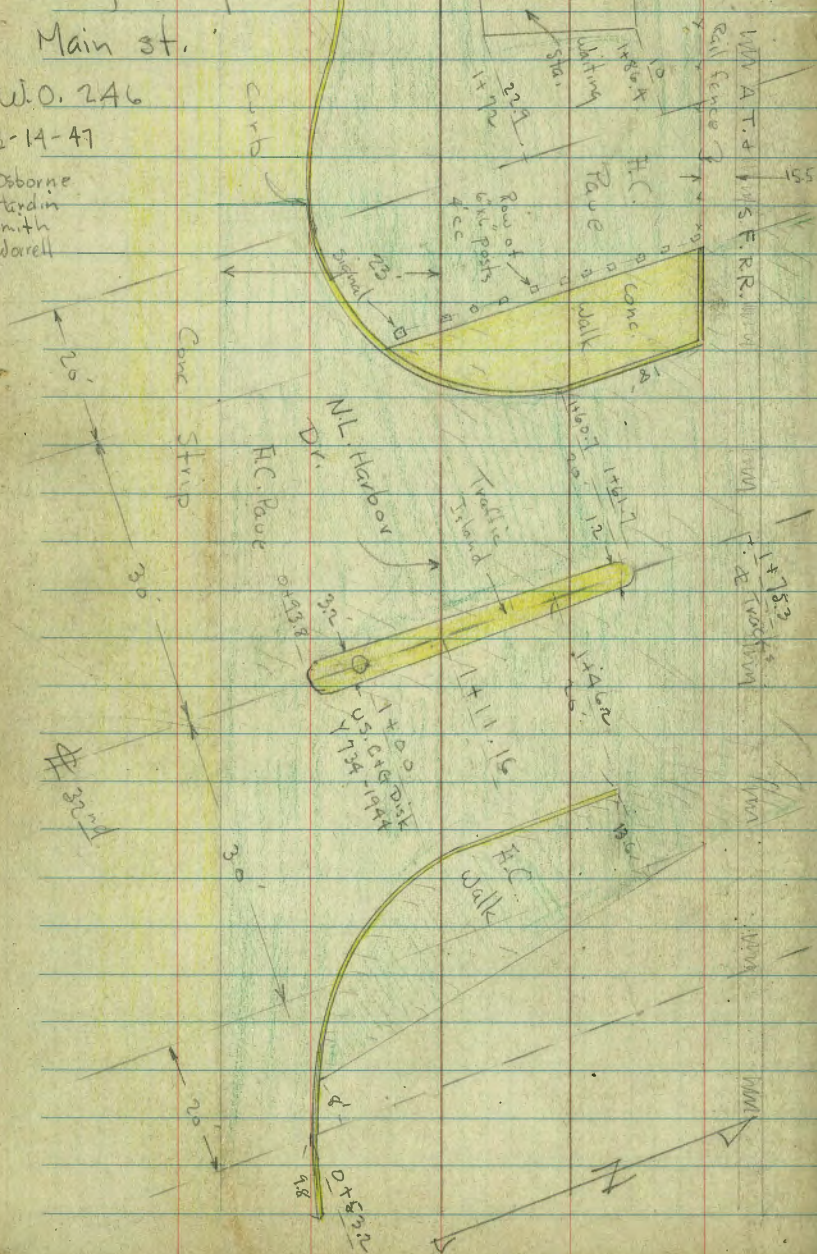
32-51 - X-Sect. Low - Cass to Everts

Location + Topo for Prop R.O.W. Thru
Navy Prop. from 32nd + Harbor to
Main st.

U.O. 246

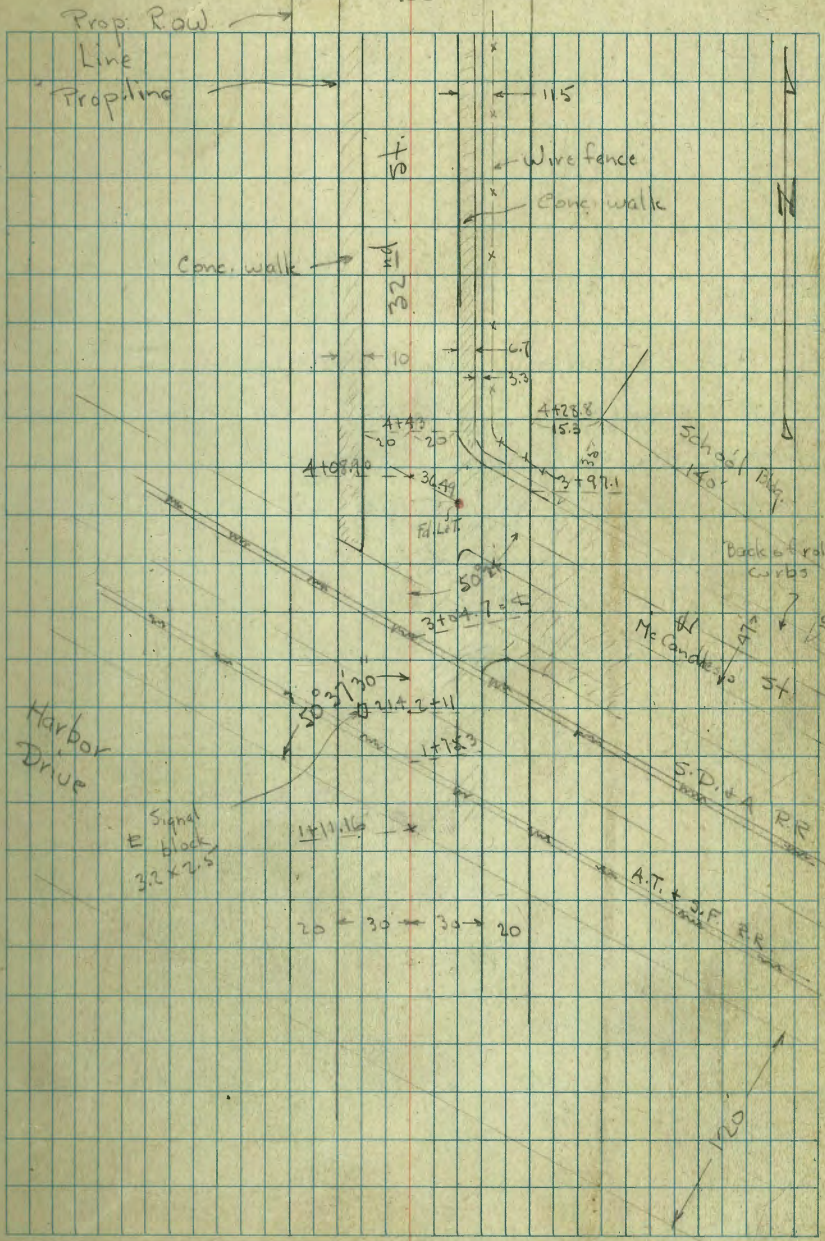
3-14-47

Osborne
Hardin
Smith
Warrell



20 - 30 - 30 - 20
100

Indexed
C.S.K. 2



∅ Int. - c.t. in pave Sta 7+98.42 Ang. $29^{\circ}37'$ Pt.

7+78 - Cross fence on Pt - 7+94.5 - 326 ft. - Cor Traffic office

7+35.23 = ∅ + Line in Norman Scott Rd.

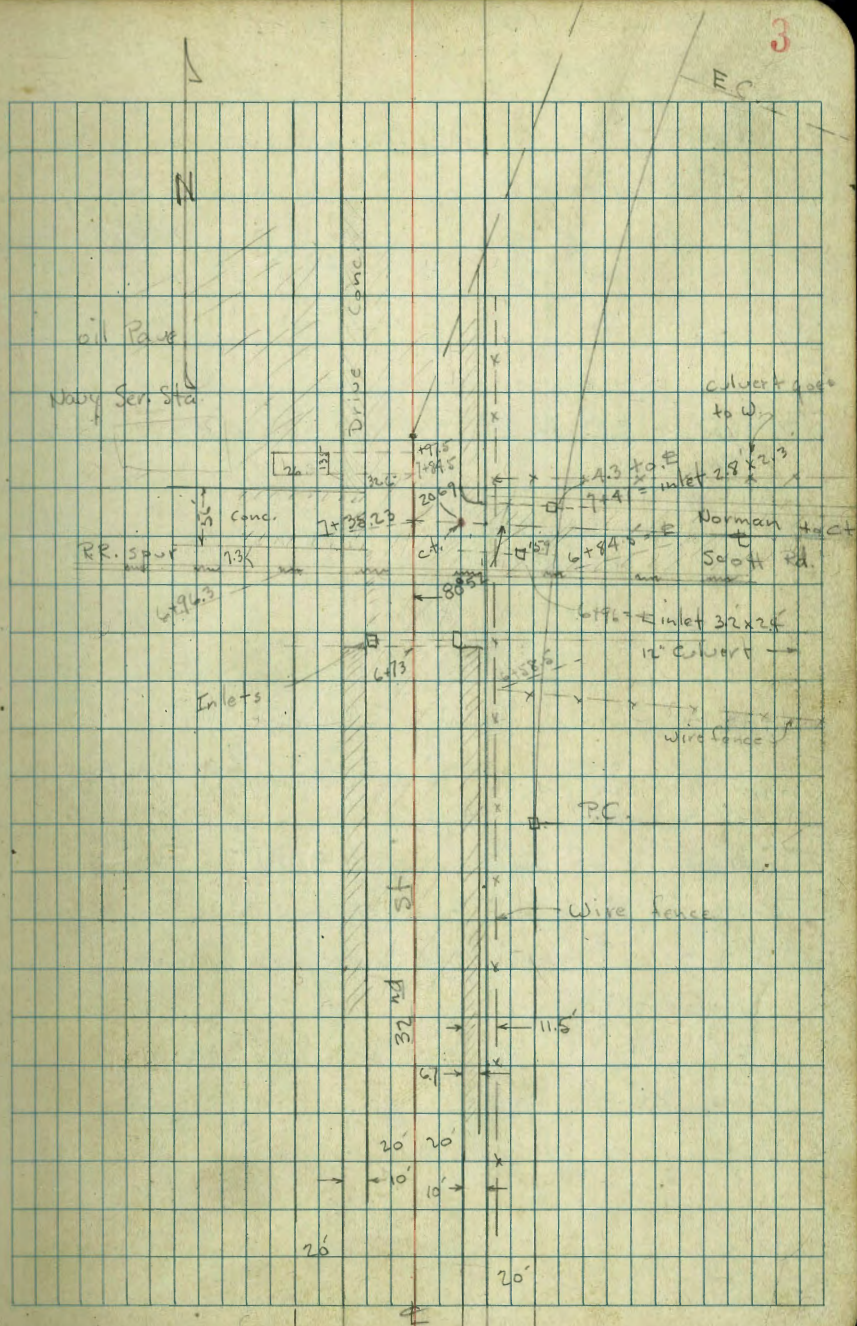
$A = 29^{\circ}37'$ - 6+96.3 = ∅ Tracks + W.L. - 6+84.6 = ∅ Tracks + E.L. curbs

E.L.R = 950 6+73 = S. side of 32x25 Inlets + end of

L = 491.06

T = 251.15

E.L.P.C. Sta 5+34.05



$\Delta = 13^{\circ}04'30''$ $\pm R = 1000$
 $L = 228.20$ $T = 114.60$
 $16+25.40 = P.C.$

$16+00 - 32'$ Lt. = edge of 10' strip of planting
 $15+73 - 26'$ Rt. = \pm F.H.

$14+93 -$ Int. E.L. Row + W.L. Road

$13+95 =$ Int. E.L. Row. + E.L. Road.
 $13+82 - 54.7'$ Rt. = \pm Lamp post.

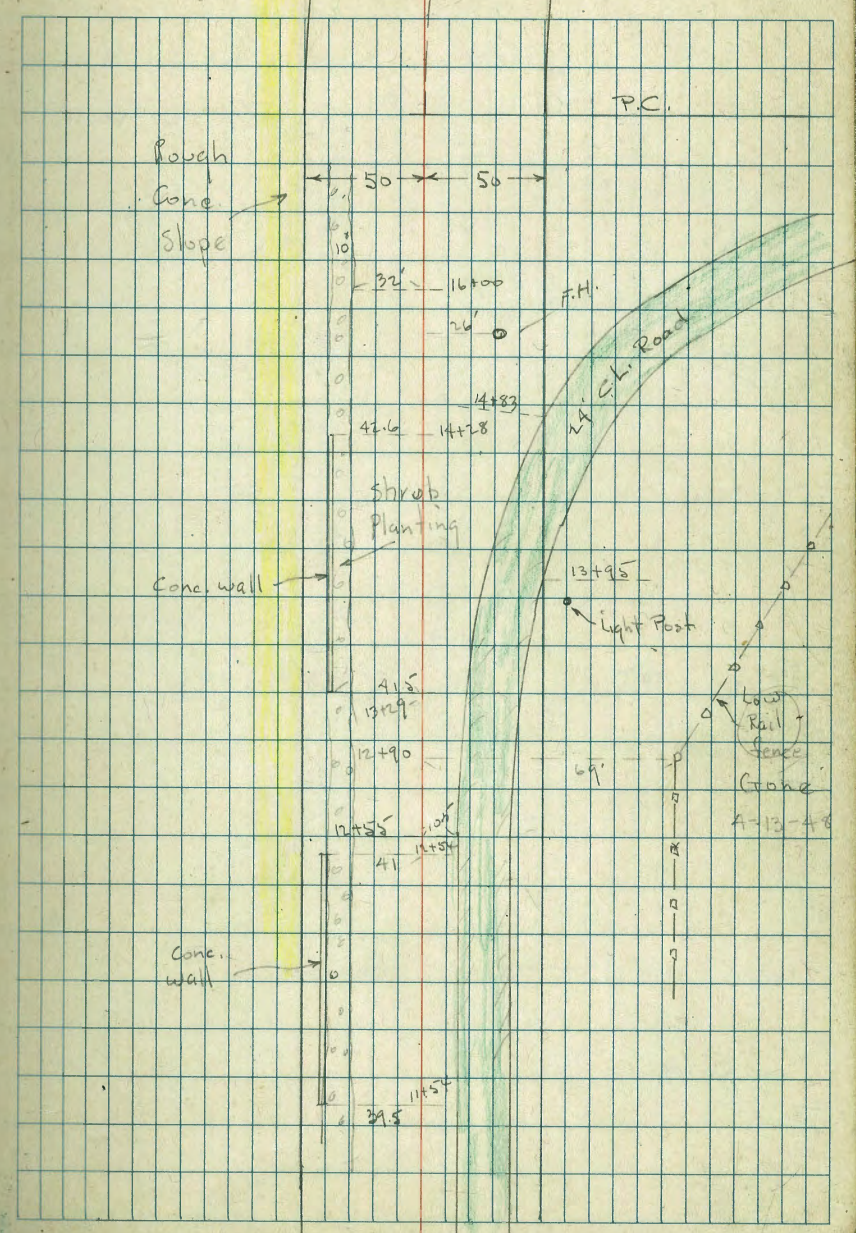
$13+29 - 41.5'$ Lt. = Beg. 6" Conc. wall

$12+90 - 69'$ Rt. = Ang. in Rail fence

$12+55 - 10.5'$ Rt. = W. side Rd. - P.C.

$12+54 - 41'$ Lt. = end Conc. wall

$11+54 - 39.5'$ Lt. = Beg. 6" Conc. wall



18+53.60 = E.C.

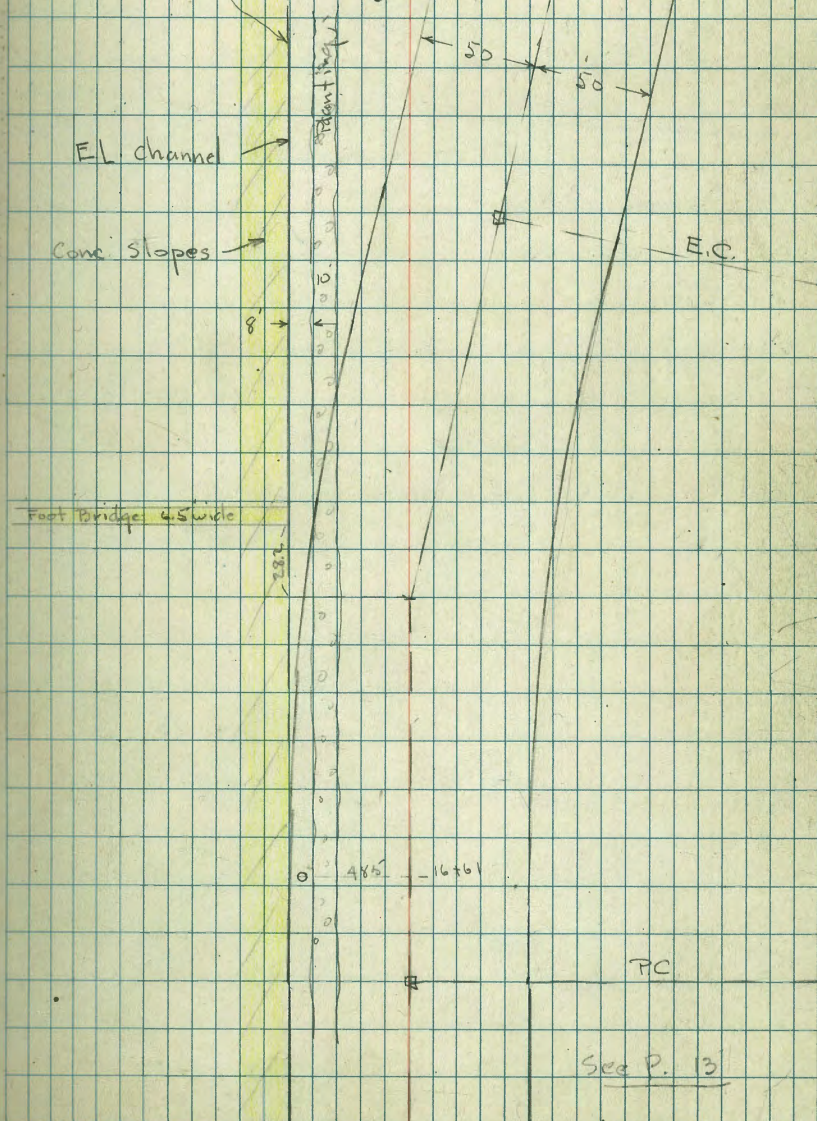
17+40 = P.I.

Ang. $13^{\circ} 04' 30''$ Rt.

16+61 = 485 ft. = E.P. pole Cone

16+25.40 = P.C.

Line of E. Side of
channel as est. by Navig.



VZFD-4-1-82
GR

NOTED.

Back of
Abutment
of Bridge

310.197 - Chisel bit
249.830 in cb.

16.5
21
127.00
End of
Rail
ct in rail

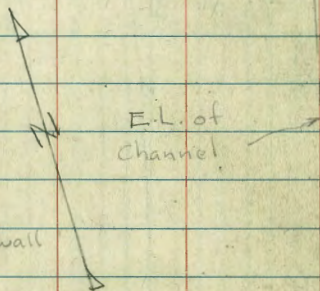
20+63 = Wire fence

20+58 = \pm of Row of small Euc. Trees

20+39 - 19 Rt. = \pm 3' x 33' Grate

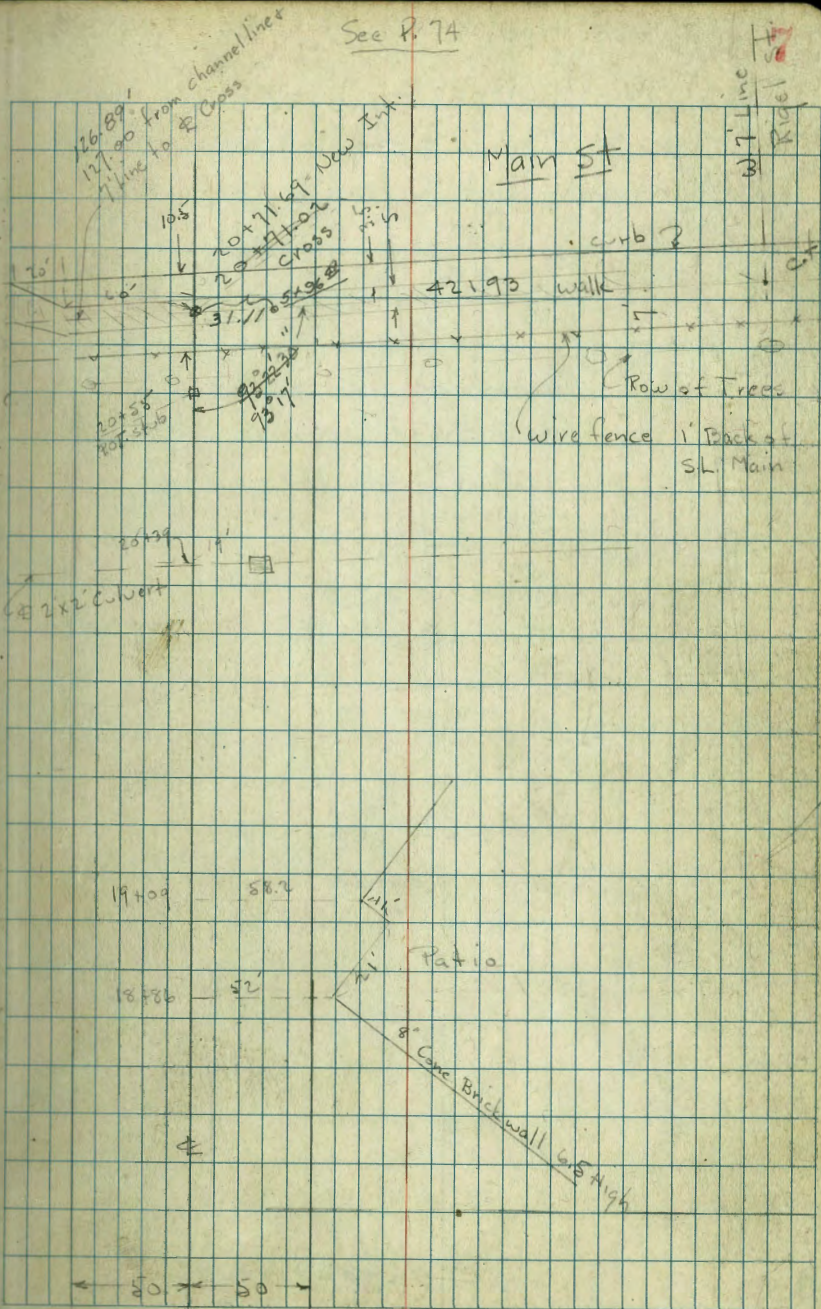
Inlet for 2' x 2' box Conc. Culvert

outlet -
conc slab
+ headwall



18+86 - 52' Rt. = Near Cor. Conc. wall

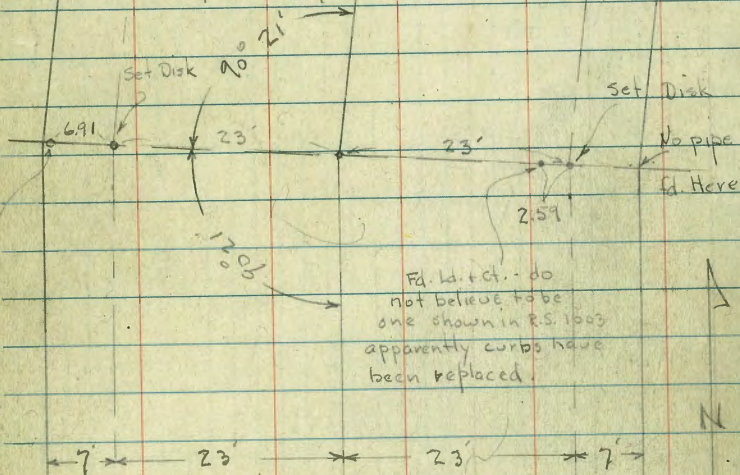
See P. 74



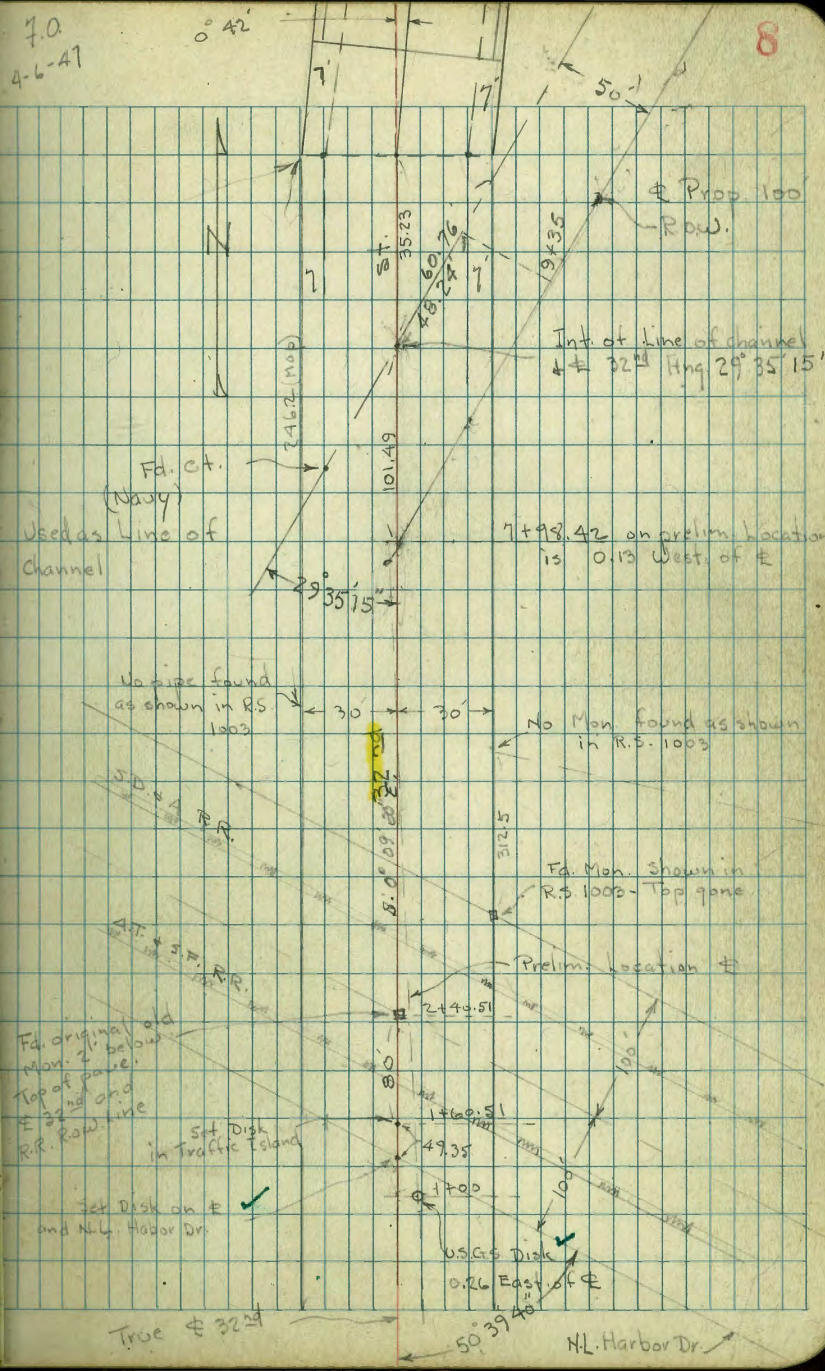
Ties for Prop. R.O.W. along 32nd St.
 Also Traverse along E. 7' Line of 32nd
 To Main St. Thence along S. 7' Line of Main
 to Point of Int. with Prop. R.O.W.
 See Page 2

Detail of Ties at
 Angle shown opposite
 Adj. to Meet improvements
 and previously Noted Ties.

Fd. 3/4" Pipe - Shown in R.S. 1003
 has been disturbed



✓ = FO-3-29-82
 G.P.



Fd. Ct. (Navy)
 Used as Line of Channel

No pipe found as shown in R.S. 1003

No Mon. found as shown in R.S. 1003

Fd. Mon. Shown in R.S. 1003 - Top gone

Prelim. Location #

Fd. original old Mon. 2' below Top of pave. E 32nd and R.R. Row. line

Set Disk in Traffic Island

Set Disk on E and N.L. Harbor Dr.

USGS Disk 0.26 East of #

True # 32nd

N.L. Harbor Dr.

4-9-41
7.0.

Set Disk
Int. of 7' Lines

84.27 To Id. ct. on N. 7' Line
Main T.P. 4-53 **9**

Fd. Id. ct.
T.P. Book 14-P 53



32 rd
st.

599.05

88° 41' 50"

95

43.5

Fd. ct. in curb
Book 1573-80 + RS. 1003

Set Disk on
7' Line Int.
0° 12' 50" Rt.

90° 51' 20" (Calc. from RS. 1003)

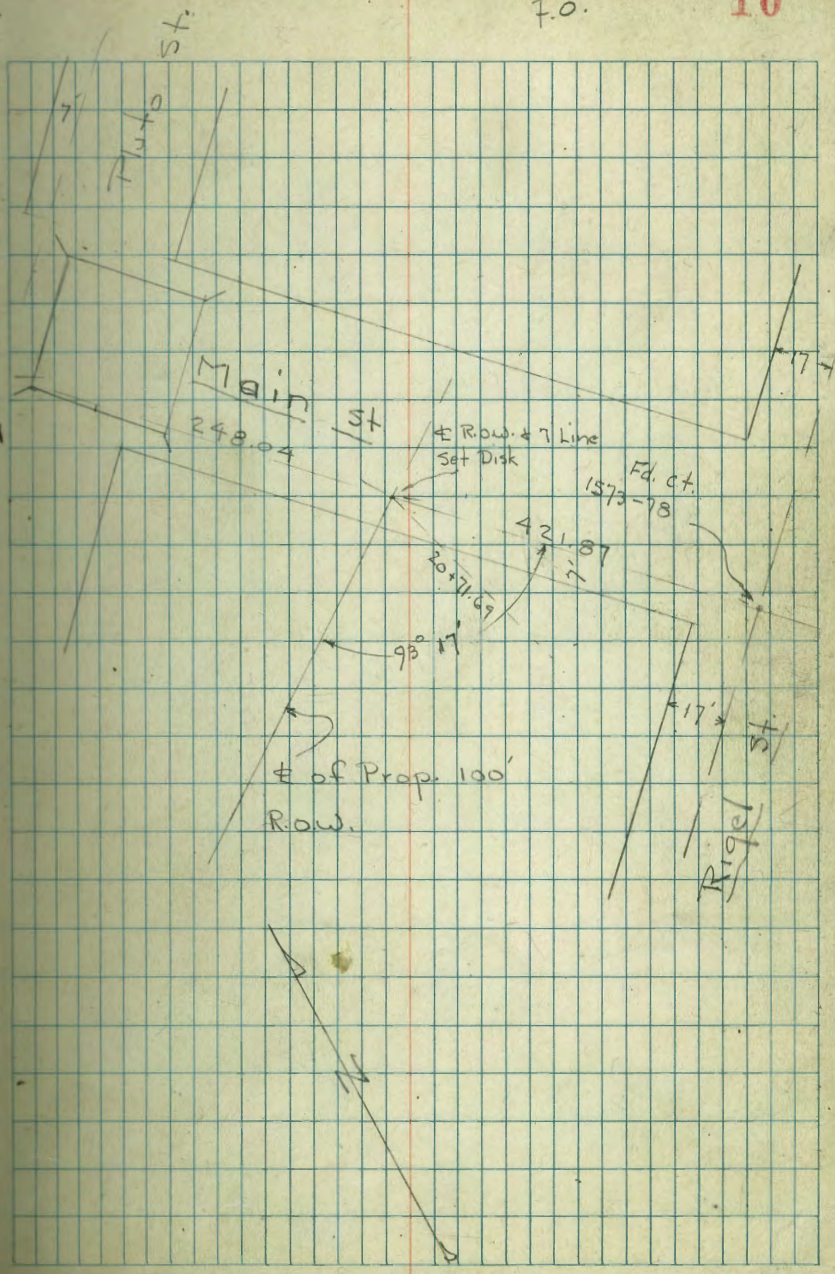
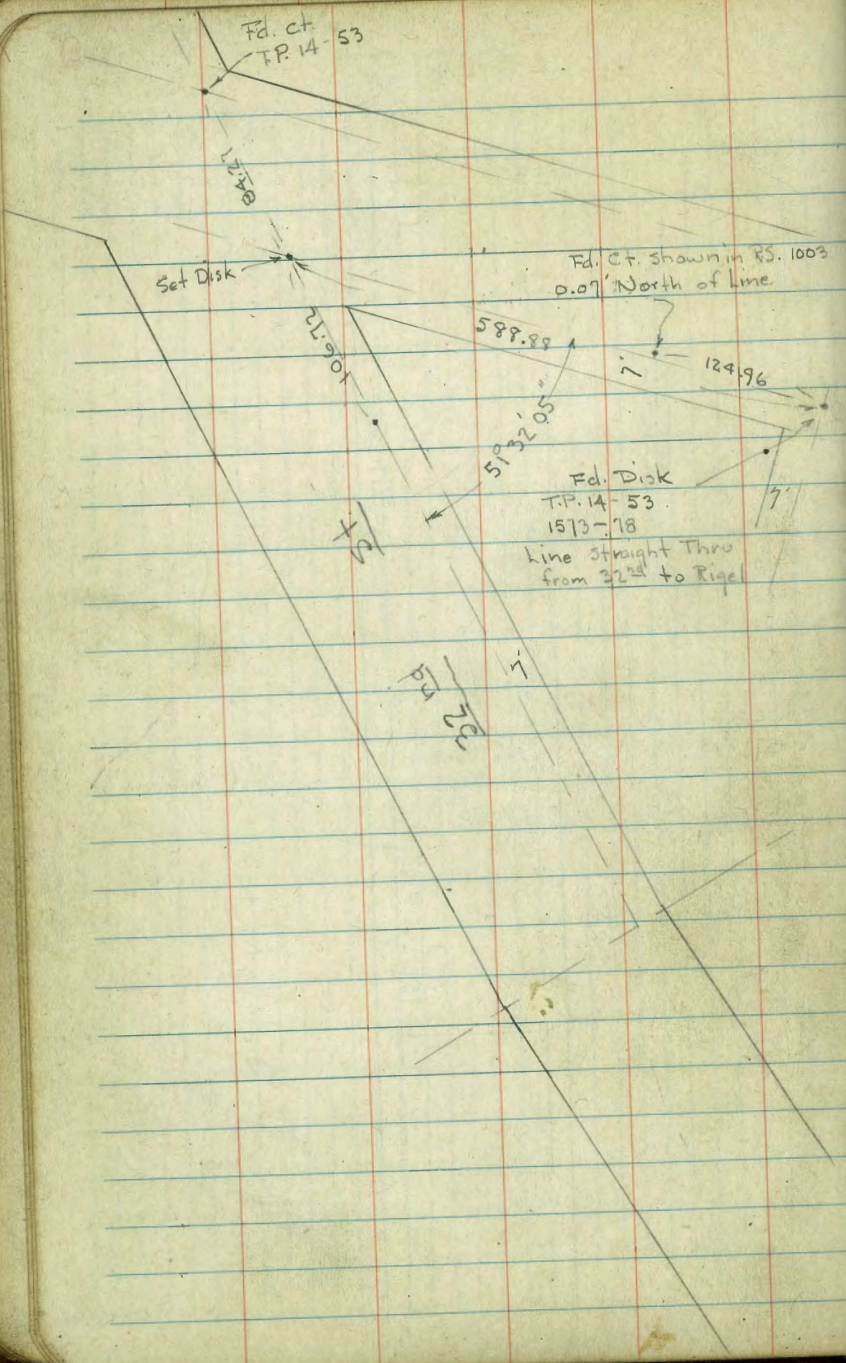
752.26

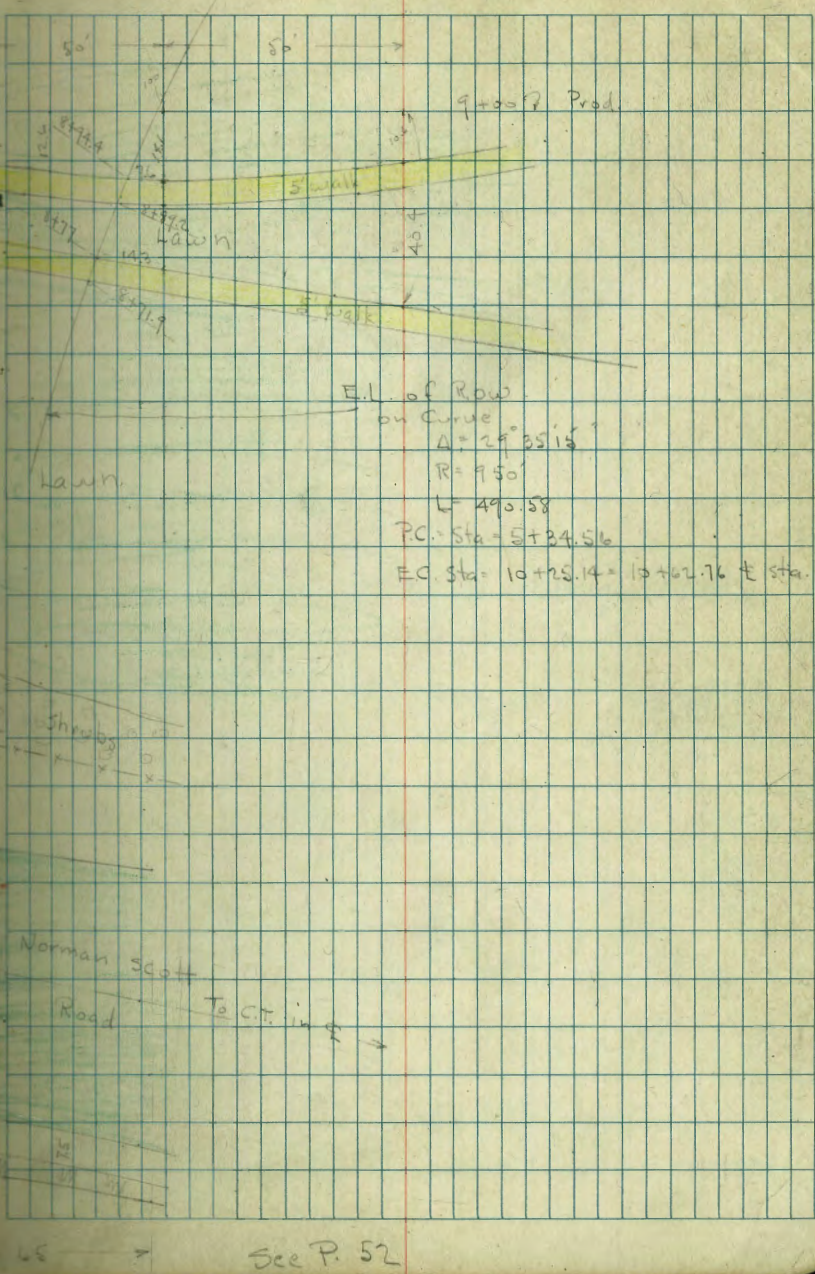
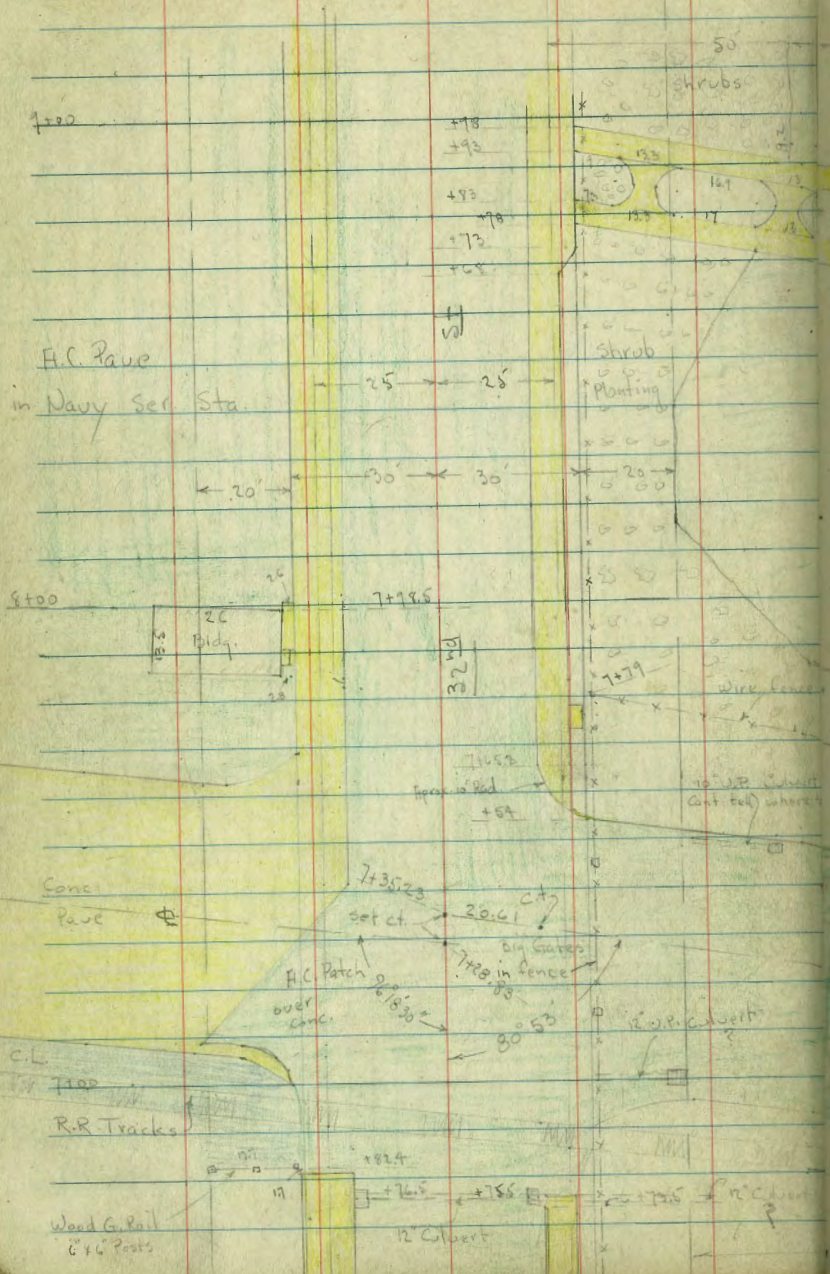


V. = FD.
3-25-82
G.P.

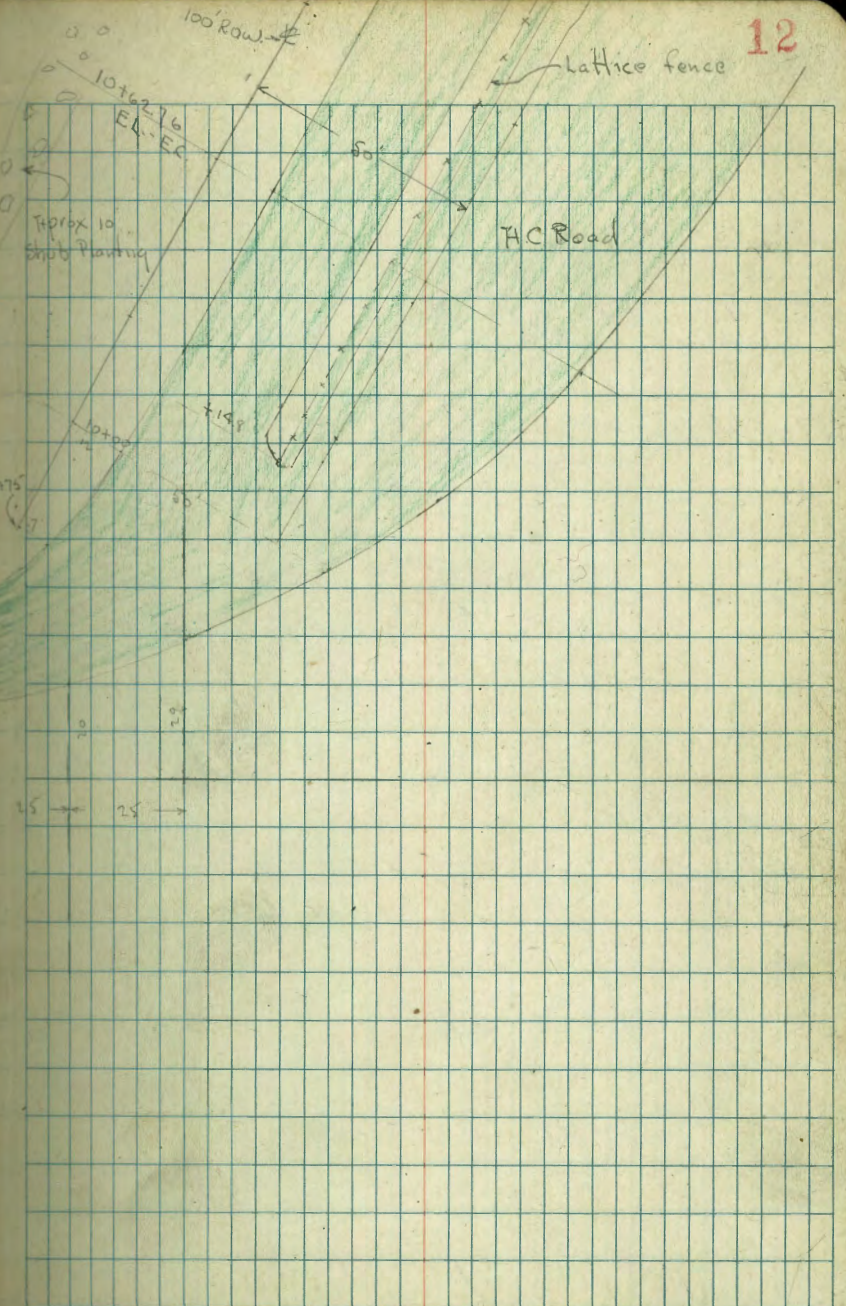
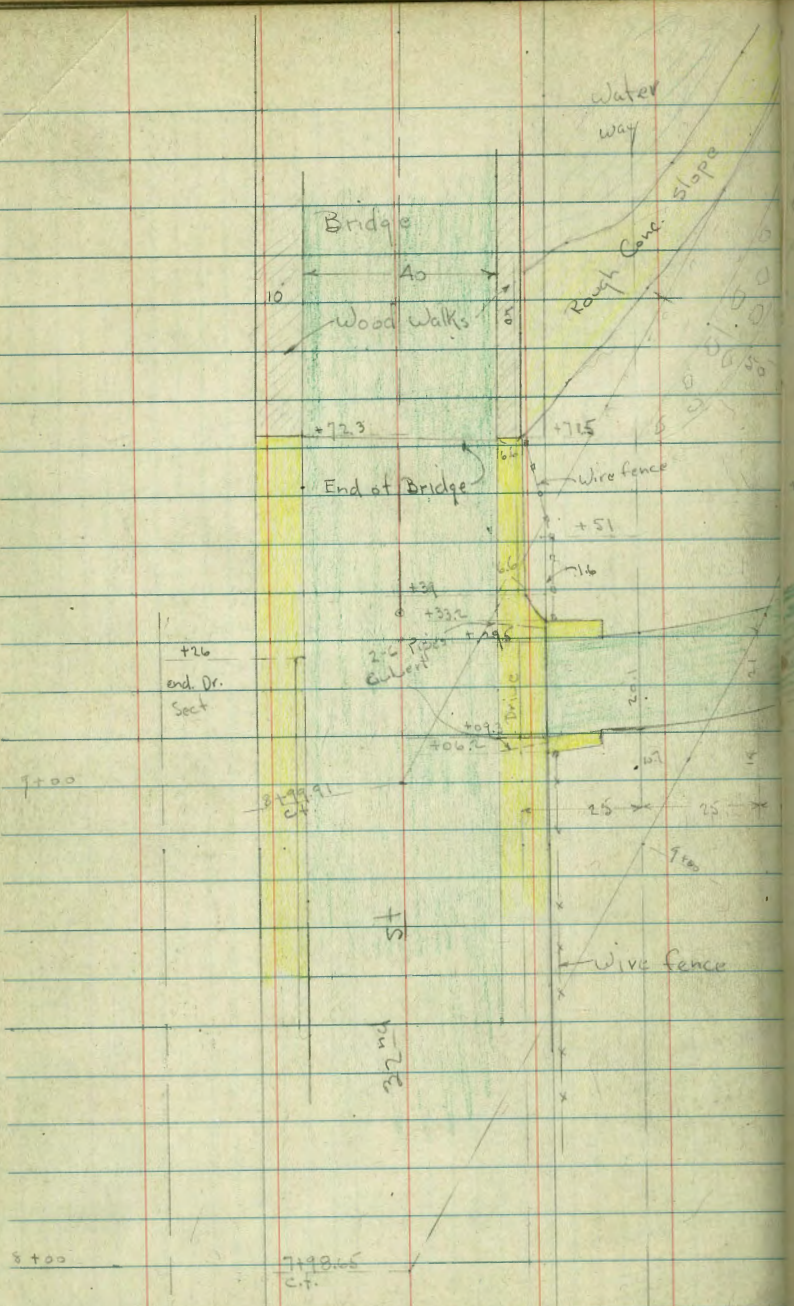
4-10-47
7.0.

10





See P. 52



See P 11

Φ - 100' Row.

See p. 5

6" Conc Wall

+28

Aprox. 10 shrub. planting

13+00

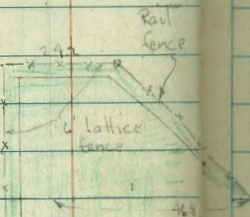


+53.5

12+19

6" Conc Wall

12+00



16+00

+54.5

H.C. Pavc

H.C. Pavc

2' Rad H.C. Curb

15+00

14+00

11+00

00

50 50

0 + 79.5 12.5 L 5 line Obl garage conc

0 + 79.5 7.5 R 4' 3" Walk conc

0 + 77 6.3 R N edge of apron

+ 65 6.2 R conc apron cont'd

+ 55 7.9 Lt A 9615 Power Pole

0 + 52.5 5.9 R Conc Apron

T.P. 5.73 292.73 1.49 287.00

0 + 48 5.8 R South edge of 4 1/2 conc walk

0 + 30

288.49

287.07

4.86
12.5

286.33

4.40
7.5
288.14

288.39

4.59
6.3

4.34
19.5
garage conc

287.71

5.02
6.2 R

287.94

4.79
21
N side of garage

287.4

5.3
7.5

287.0

5.7

287.36

5.37
5.9
conc walk conception

287.51

5.22
5.9
conception

287.82

4.91
81
S side of garage

286.9

1.6
7.5

286.3

2.2
5.0

286.2

2.9

286.9

1.6
7.5

287.27

1.22
5.8

287.33

1.16
7.5

6.7 rock wall cont'd

288.49

Alley BIK. 79 Park Villas
+ HI -

T.P. 468 293.49 658 298.91

3 + 00 7.5 L end of board fence

2 + 75

2 + 74 8.3 L beg. board fence

2 + 70 7.8 L NE cor. Shed

+ 67 6.0 Rt Tel Pole 412395 H

+ 61 7.8 L SE cor. Shed

+ 56 ^{14.0 L} 5.179 L garage

2 + 50

0 + 48 7.9 R by Picket fence

295.39

Lr

R

R 19

6.5 20 288.9
4.0 7.5 289.4
293.49
289.16
6.23 6.2 289.2

5.6 20 289.8
5.3 7.5 290.1
5.6 7.5 289.8

5.3 7.5 290.1
5.3 7.7 290.1
5.3 7.5 290.1

5.0 15 290.4
5.0 14 290.4
5.0 7.5 290.4

5.0 15 290.4
4.6 7.5 290.8
4.2 7.5 291.2

5.0 15 290.4
4.6 7.5 290.8
4.2 7.5 291.2

295.39

4+00 7.9 L end of board fence SE cor garage
 +95 7.6 R end of board fence
 +73 7.8 L beg Picket fence

287.3

+70

6.2
2.5

+59 13.0 L Single garage 15.4 L
apron floor

+56 8.0 R end of Picket & beg board fence

+50 7.4 L end of fence board

3 +35

+32 7.9 L beg Picket

3+21 7.0 Lt Power Pole A3647

3+09 12.5 Single garage 15.5 L
apron

293.49
summed

286.7

6.6
1.5

287.3

6.2
1.2

288.1

5.4
1.0

289.1

5.4
1.0

290.1

5.3
1.5

291.1

5.1
1.0

292.1

5.1
1.0

293.1

5.1
1.0

294.1

5.1
1.0

295.1

5.1
1.0

296.1

286.9

6.6
1.0

287.9

5.4
1.5

289.1

5.4
1.5

290.1

5.4
1.5

291.1

5.4
1.5

292.1

5.4
1.5

293.1

5.4
1.5

294.1

5.4
1.5

295.1

5.4
1.5

296.1

5.4
1.5

297.1

286.9

6.6
1.0

287.9

5.1
1.0

288.9

5.1
1.0

289.9

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290.9

5.1
1.0

291.9

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1.0

292.9

5.1
1.0

293.9

5.1
1.0

294.9

5.1
1.0

295.9

5.1
1.0

296.9

5.1
1.0

288.4

5.1
1.0

289.4

5.1
1.0

290.4

5.1
1.0

291.4

5.1
1.0

292.4

5.1
1.0

293.4

5.1
1.0

294.4

5.1
1.0

295.4

5.1
1.0

296.4

5.1
1.0

297.4

5.1
1.0

298.4

5.1
1.0

288.4

5.1
1.0

289.4

5.1
1.0

290.4

5.1
1.0

291.4

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292.4

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293.4

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294.4

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295.4

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1.0

296.4

5.1
1.0

297.4

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298.4

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288.4

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289.4

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1.0

290.4

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1.0

291.4

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1.0

292.4

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1.0

293.4

5.1
1.0

294.4

5.1
1.0

295.4

5.1
1.0

296.4

5.1
1.0

297.4

5.1
1.0

298.4

5.1
1.0

288.4

5.1
1.0

289.4

5.1
1.0

290.4

5.1
1.0

291.4

5.1
1.0

292.4

5.1
1.0

293.4

5.1
1.0

294.4

5.1
1.0

295.4

5.1
1.0

296.4

5.1
1.0

297.4

5.1
1.0

298.4

5.1
1.0

7.6
fence

5.2
7.5
2.0

7.9
fence cont

288.6

4.9
2.0

293.49

Alley
+Blk 79 Park Villas
#1 -check to SE BP Landis
Arnold 1.63 291.96 291.85
0.11check to BM brass Plug
SE Arizona + Landis 8.26 285.39 285.31
0.026+1040 Scurb Landis
+99 88 L East edge of PR6 2585

T.P. 5.23 293.59 5.30 288.36

6+024 7.2 L conc Walk s edge
7.5 R

6+004 S line of Landis

5+90

293.66

L

d

Rt

23

285.40	284.93	287.6	288.00	287.8	288.51	288.0	290.56	291.04
8.9	8.66	6.0	5.59	5.8	5.08	5.6	9.03	2.55
136.5	132	13	7.16	7.7	7.7	7.7	9132.5	ch
	R.P.			curb end		got.	HCPay	
	288.38				293.59		288.74	
	5.28			Note!		4.92		
	7.2			No alley		7.5		
				Return				
	288.4		288.3		288.3		288.6	
	5.3		5.4		5.4		5.1	
	289.6		289.0		288.6		289.0	
	4.1		4.7		5.1		4.7	
	7.5		6		6		7.5	
							289.2	
							290.3	
							3.4	
							14	

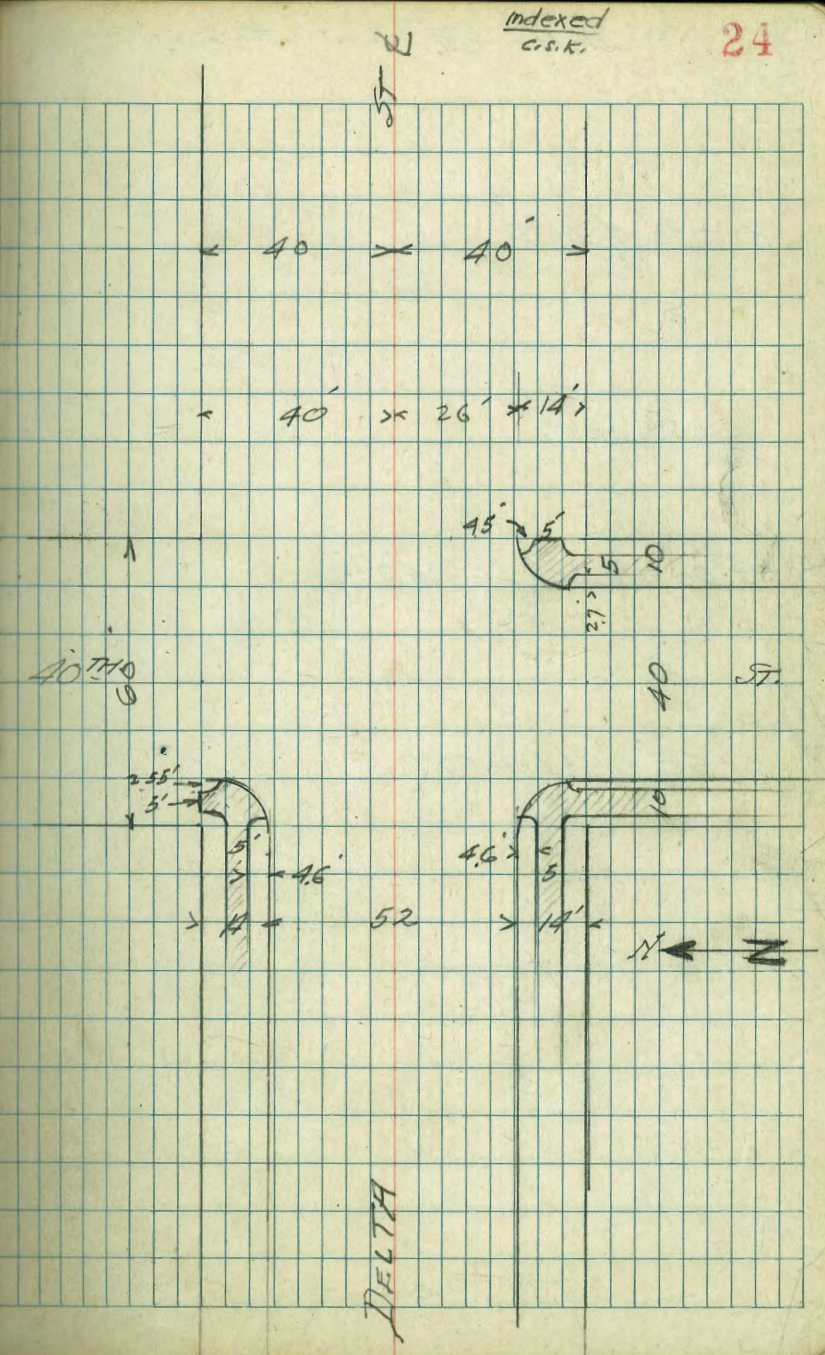
293.66

Walker
Becker
Johnson from 40th to 41st St

14.0. 31048

Indexed
C.S.K.

24



0-30' = 40th

72.7	68.2	64.8	64.2	63.56	62.5	62.0	60.8	59.3
40.3	48	82	88	94.6	10.5	11.0	12.2	13.7
140	90	40	26	RM 26 MH.	26	40	90	140

0+50 Cont.

72.2	67.9						58.7	59.40
0.8	51						14.3	13.62
140	90						140 RM	140 CB

0+50' = West cb Line 40th

63.53	64.1	63.5	62.8	61.9	61.3	62.24	58.7	59.40
94.9	89	94.5	10.2	11.1	11.7	10.78	14.3	13.62
40 CB	40 Sub. 24 cb	26		26	40 RM.	40 CB	90 RM	140 CB

0-60' = West Line 40th

63.31	62.7	62.5	61.5	61.5	62.48
94.7	10.3	10.5	11.5	10.79	
26 RM	26 RM		26 RM	26 RM	26 CB

0-110'

62.03	61.3	61.2	60.1	61.08
10.99	11.7	11.8	12.9	11.94
26 CB	26 RM		26 RM	26 CB

0-160'

60.76	60.0	59.8	58.7	59.66
12.26	13.0	13.2	14.3	13.36
26 CB	26 RM		26 RM	26 CB

9.73 73.02

63.29

RM NW BR Delta 40th

Delta St. X-Sections

Sta 13' West Delta St 41st

840

73.71 ± 0.03 Error
73.68

7+60 = East corner Ret wall on Rt

7+10.5 = Bay, Corner Ret. Wall on Rt 38.5' Rt of L

7+10

6+85

6+60.5 = East Line 41st

6+50.5 = E. Line 41st St. ^{cutb}

6+40.5

82.08

Rt. 31

Sta	78.6	78.1	76.0	73.1	72.5	71.8	71.0	70.2	69.31	68.4		
7+60	3.5 50	4.0 40	6.1 36	9.0 17	9.6 15	10.3 10	11.1 12	11.9 17	12.77 37 Wall	13.7 50		
7+10.5			8.21 50	8.07 40	7.55 25	7.43 20	7.35 10	7.16 22	7.01 40	6.93 50		
7+10		83.2 50	81.4 40	79.2 25	76.5 14	75.3 14	74.6 11	70.8 37	70.1 40	69.2 50		
6+85			84.3 50	82.7 25	79.5 14	77.5 14	75.6 11	74.4 10	71.0 40	69.8 50		
6+60.5				+2.2 10	+0.6 40	2.6 23	4.6 16	6.5 15	7.7 10	11.1 40	12.7 50	
6+50.5	100.7	91.3 116 150	90.5 130	87.3 115	83.4 115	80.8 115	77.4 115	73.7 115	73.4 115	70.8 115	66.5 115	63.8 115
6+40.5		80.4 150	91.2 130	90.6 115	86.5 115	81.4 115	75.8 115	73.0 115	70.7 115	67.1 115	63.6 115	
		+8.3 150	+9.1 130	+8.5 115	+4.4 115	0.7 115	0.3 115	2.1 115	11.4 115	15.8 115	18.5 115	

X-Sept. Law St. from Cass to Everets
With Rods on Intersections + Cross Sts

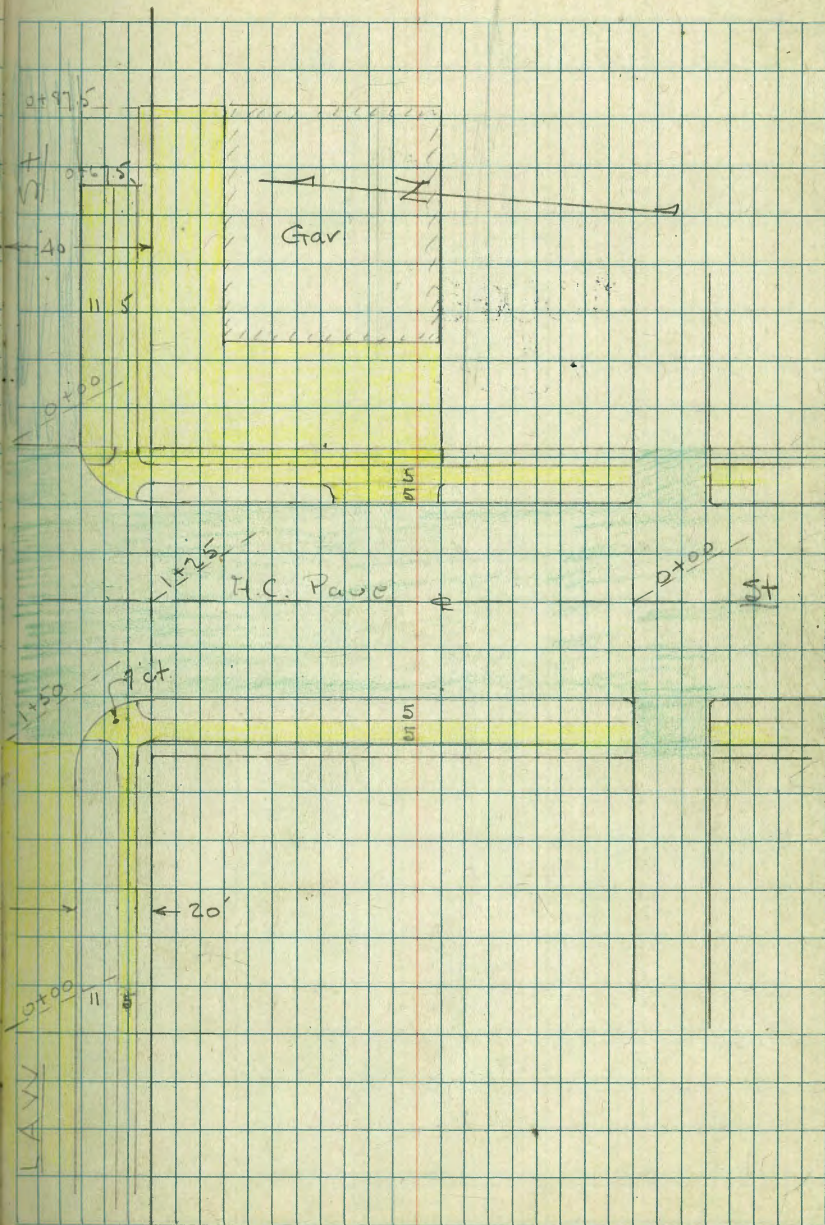
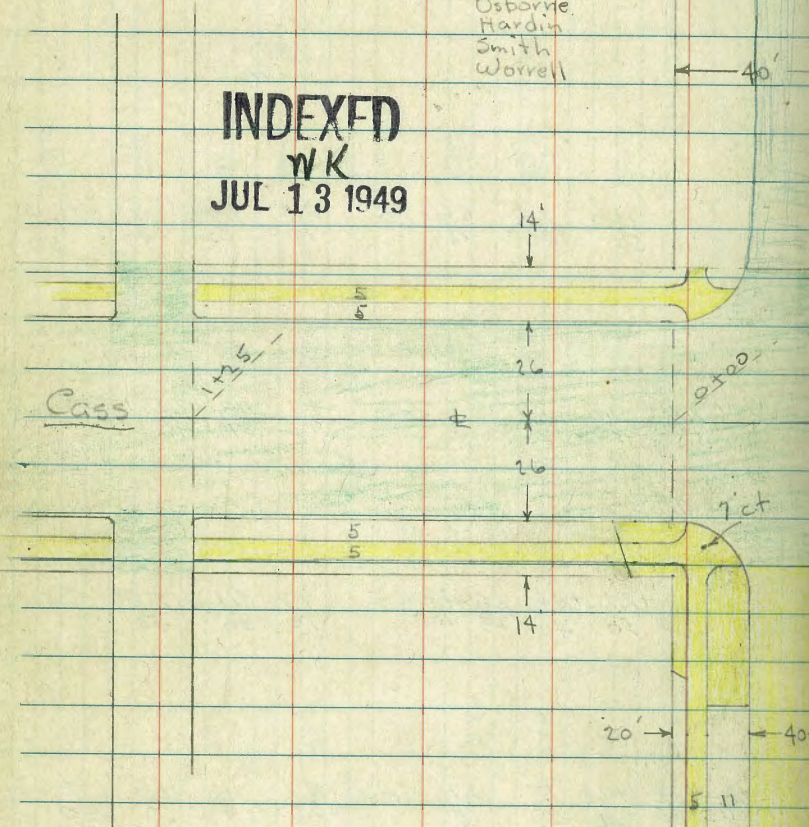
1821

W.O. 31266

10-10-47

Osborne
Hardin
Smith
Worrell

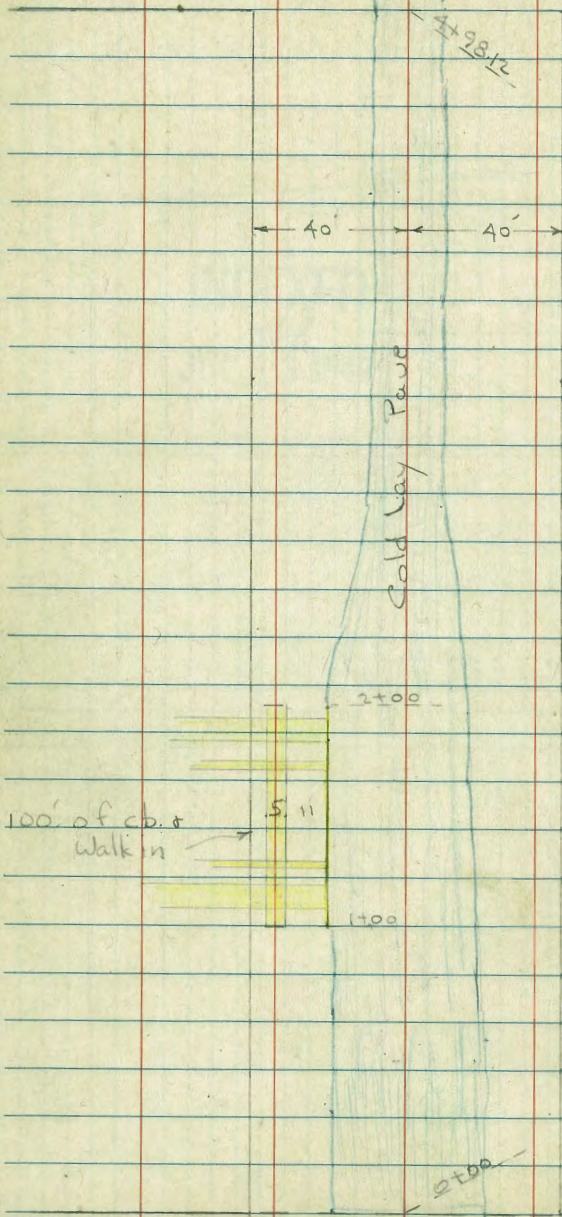
INDEXED
WK
JUL 13 1949



Blue = Cold Lay Pave
Green = H.C. Pave
Yellow = Concr.

Dawes

st



Cass

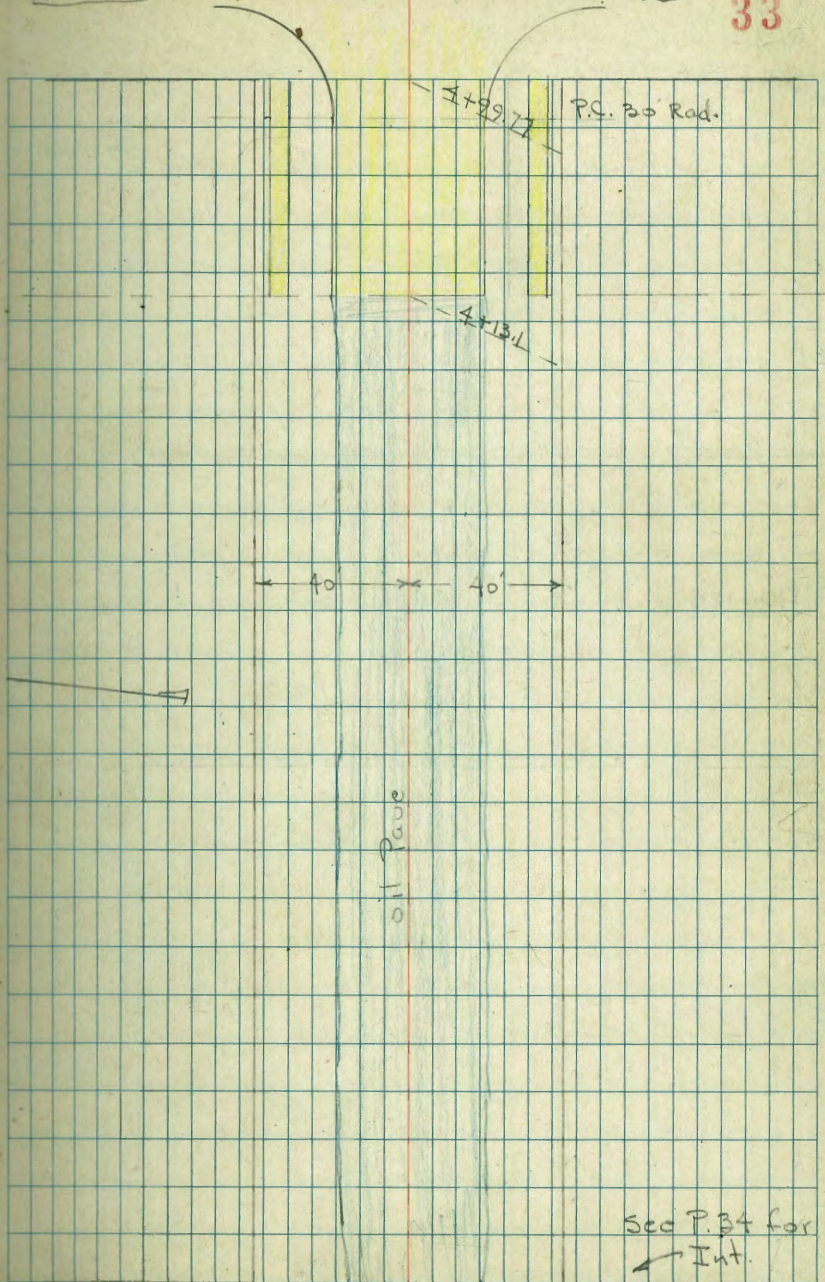
st

Everts

See P. 35 for Int.

st

33



Dawes

st

Dawes

1+25

A

40'
40'

40' 40'

Oil Pave

0+00

7 Mon.
7+P

Cold Lay Pave

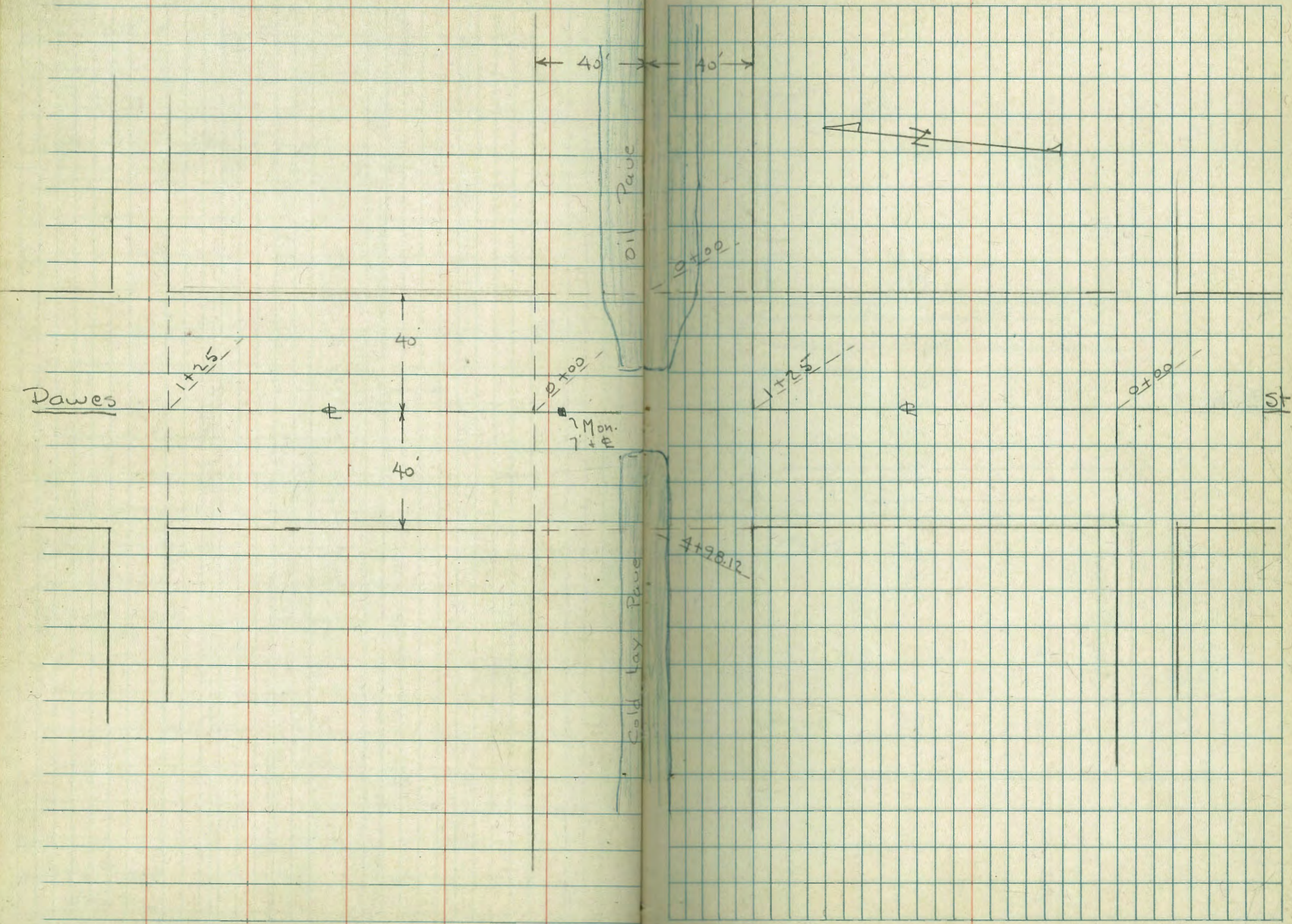
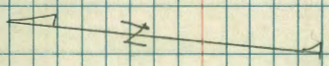
4+98.12

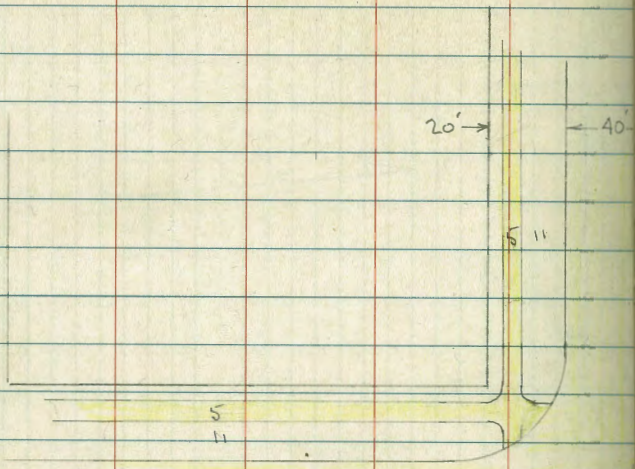
1+25

A

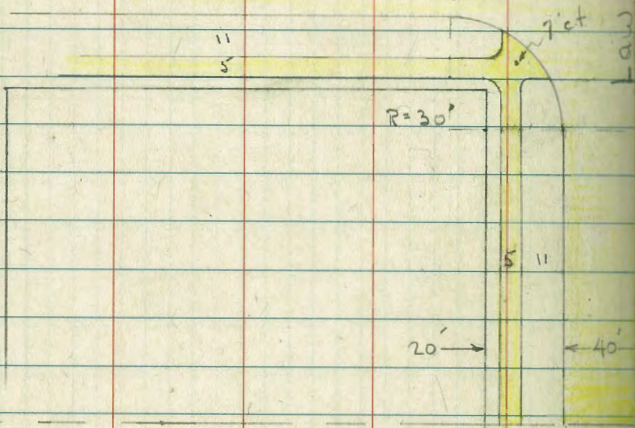
0+20

St

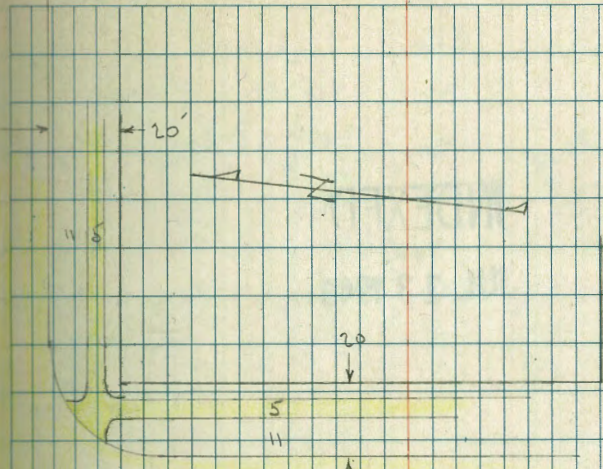




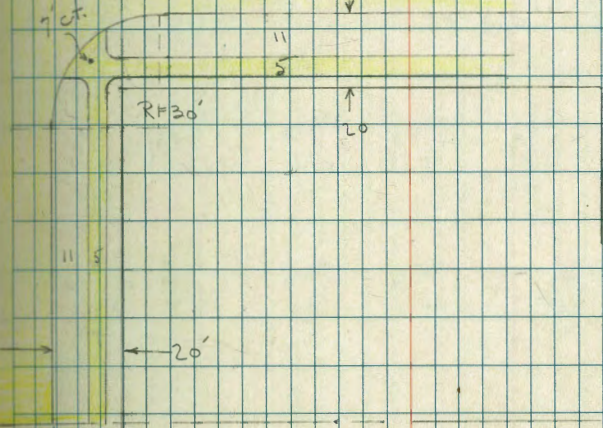
Everts



oil
Pipes



St



X-Sept Cass from N.L. Alley S of
Law to S.L. of Alley N. of Law
See sketch - P. 32 - 80' st. 14' cbs.
Paved - H.C.

0+25

INDEXED
WK
JUL 13 1949

0+00 = N.L. Law.

for rest of Int See Law Sections.

1+25 = S.L. Law

1+00

0+50

0+00 = N.L. 20' Alley - S. of Law.

B.M.

7.62

74.02

66.40

SW.B.P.
Law + Cass

Lt. = W

E

Rt = E

68.25 5.77 26 Top	67.95 6.17 26 Cut	65.36 5.66 13	64.62 5.40	65.35 5.64 13	65.04 5.98 26 Cut	68.76 5.26 26 Top			
61.96 6.06 26 Top 20' Rad. Ret.	67.65 6.37 26 Cut	65.08 5.94 13	68.73 5.79	69.10 5.92 13	67.71 6.31 26 Cut	68.47 5.55 26 Top P.C.			
66.69 7.33 26 Top - P.C. 20' Rad. Ret.	66.30 7.72 26 Cut	66.63 7.39 13	66.78 7.24	66.67 7.40 13	66.36 7.66 26 Cut	67.05 6.97 26 Top P.C.			
66.12 7.90 26 Top	65.63 8.39 26 Cut	66.16 7.86 13	66.31 7.71	66.19 7.83 13	65.87 8.15 26 Cut	66.47 7.55 26 Top			
65.09 8.93 26 Top	64.65 9.37 26 Cut	65.15 8.87 13	65.25 8.77	65.11 8.91 13	64.78 9.24 26 Cut	65.50 8.52 26 Top			
64.40 9.86 40 Top End Ret	64.10 9.92 26 Top 3' Rad. Ret	63.75 10.27 26 Cut	64.15 9.87 13	64.28 9.74	64.11 9.91 13 Cut	63.82 10.26 26 Top 3' Rad. Ret	64.39 9.63 26 Top 3' Rad. Ret	64.39 9.72 40 Cut	64.50 9.52 40 Top End Ret
				74.02					

Lt.

Rt.

End.

1 + 25 = S.L. of 20' Alley - N. of Law.

0 + 75

69.92	69.85	69.75	69.34	69.86	70.09	69.98	69.70	70.37	70.36	70.89
4.10	4.17	4.27	4.68	4.16	3.93	4.04	4.32	3.65	3.66	3.53
40	40	26	26	13		13	26	26	40	40
Topch end Alley Ret	gut	Top 3 Rad. Ret	gut				gut.	Top 3 Rad. Ret.	gut.	Top end. Ret.
69.00	68.55	69.12	69.32	69.24	68.83	69.54				
5.02	5.47	4.90	4.70	4.78	5.19	4.48				
26	26	3		13	26	26				
Top	gut.				gut.	Top				

74.02

Rods around Returns at Law + Cass.

N.W. Ret - 317' around - 5 parts - 6.3' each

Req. - PC = C.W. of W.L. on N. cb. Law	6.72	67.30	T = Top
	7.21	66.81	q = gut
6.3 E = W.L. Cass	6.65	67.37	T
	7.03	66.99	q
6.3	6.44	67.58	T
"	6.91	67.11	q
"	6.33	67.69	T
"	6.71	67.31	q
"	6.23	67.79	T
"	6.53	67.49	q
6.3 = EC = N.L. Law	6.06	67.96	T
	6.36	67.66	q

N.E. Ret. = 252' around - 4 - 6.3 each. Ret
is not complete - stops on E.L. of Cass

Req. = P.C. = N.L. Law	5.55	68.47	T
	6.31	67.71	q
6.3 - S	5.65	68.37	T
"	6.33	67.69	q
"	5.70	68.32	T
"	6.33	67.69	q
"	5.66	68.36	T
	6.26	67.76	q
6.3 = end. = E.L. Cass	5.55	68.47	T
	6.13	67.89	q

S.E. Ret. - 25.3' around. - 4 - 6.3 each

74.02

38

Req. - E.L. Cass

	6.54	67.48	T
	6.98	67.04	q
6.3 W.	6.67	67.35	T
"	7.24	66.78	q
"	6.86	67.16	T
"	7.41	66.61	q
"	6.95	67.07	T
"	7.54	66.48	q
6.3 = PC = S.L. Law.	6.97	67.05	T
	7.66	66.36	q
S.W. Ret. - 317' - 5 - 6.3 each			
Req. - S.L. Law	7.33	66.69	T
	7.72	66.30	q
6.3 N.	7.40	66.62	T
"	7.72	66.30	q
"	7.43	66.59	T
"	7.76	66.26	q
"	7.42	66.60	T
"	7.79	66.23	q
6.3 = W.L. Cass	7.52	66.50	T
"	7.78	66.24	q
6.3 = EC.	7.58	66.44	T
"	7.96	66.06	q

X-sect. Law St. - 80' 20' cbs
 from 150' W. of W.L. Cass - Conc.
 Pauc W. of Cass - See sketch - P. 32

27' E.

14' E = W. cb. Cass

1+50 = W.L. Cass

1+44 = P.C. 20' Rad. Ret.

1+00

0+50

0+00 = 150' W. of W.L. Cass

Lt. N.

Rt. S

68.08 5.94 40	67.76 6.24 20	67.62 6.40 10	67.49 6.53	67.28 6.74 10	67.03 6.99 20	66.63 7.39 40		
67.96 6.06 40	67.66 6.36 40 gut.	67.34 6.68 20	67.36 6.66 10	67.31 6.71	67.06 6.96 10	66.67 7.35 20	66.30 7.72 40 gut.	66.69 7.33 40 Top
67.37 6.65 20 Top	66.99 7.03 20 gut.	67.07 6.95 10	67.07 6.95	66.76 7.26 10	66.23 7.79 20 gut.	66.50 7.52 20 Top		
67.26 6.72 20 Top	66.81 7.21 20 gut.	66.93 7.09 10	66.92 7.10	66.66 7.36 10	66.06 7.96 20 gut.	66.44 7.58 20 Top		
66.65 7.37 20 Top	65.97 8.05 20 gut.	66.09 7.93 10	66.05 7.97	65.83 8.19 10	65.29 8.73 20 gut.	65.72 8.30 20 Top		
65.89 8.13 20 Top	65.19 8.83 20 gut.	65.25 8.67 10	65.29 8.73	64.98 9.04	64.52 9.50 20 gut.	64.96 9.06 20 Top		
65.02 9.00 20 Top	64.37 9.65 20 gut.	64.50 9.52 10	64.48 9.54	64.19 9.83 10	63.7 10.3 20 gut.	64.17 9.85 20 Top		

74.02 - P. 36

4+87-34.7 Lt. = ± 3.5' Conc. walk

4+81-39.7 Rt. = ± 3' Conc. walk

4+50

4+43-40.8 Rt. = ± 7' Dr - 2-2' Conc strips

4+27-38.2 Lt. = ± 3' Conc. walk

4+18-40.1 Rt. = ± 3' Conc. walk

4+08-38.3 Lt. = ± 2' Conc. walk

4+00

3+94-39.3 Rt. = ± 7' Conc. Dr.

3+84-35.1 Lt. = ± 3' Conc. walk

3+69-40' Rt. = ± 3' Conc. walk

3+59-35' Lt. = ± 8.7' Conc. Dr.

3+50

76.18 4.17 40 walk	76.60 4.35 34.7 end walk							74.80 6.15 39.7-walk			
76.00 4.9 40	75.1 5.8 20	74.8 6.1 10 edge	74.7 6.2	74.5 6.4 9 edge	74.4 6.5 20	74.6 6.3 23	74.5 6.4 40	74.70 6.25 - Level 40.8 Dr.			
75.73 5.22 40 walk	75.64 5.31 35.2 end walk							75.39 5.56 40.1 walk			
	75.43 5.52 40 walk	75.38 5.87 35.3 end walk									
75.3 5.6 50	75.1 5.8 40	74.8 6.1 23	74.5 6.4 20	74.4 6.8 10 edge	74.3 6.6	74.1 6.8 9 edge	74.0 6.9 20	74.1 6.7 25	74.3 6.8 40	73.9 7.0 50	
							74.03 6.92 39.3 Dr.				
	75.4 5.81 40 walk			75.09 5.86 35.1 end walk						73.87 7.08 40 walk	
74.63 4.30 40 Dr.		74.59 6.36 35 Dr.									
74.6 6.3 40	74.3 6.6 23	73.9 7.0 20	73.8 7.1 10 edge	73.8 7.1				73.6 7.3 9 edge	73.4 7.5 20	73.7 7.2 22	73.3 7.6 40

80.95

Cont. on Page 47

80' E = E.L. Dawes = 0+00 ahead.

60' E = E.cb.

55' E = Cross gutter + Beg. Oil pane strip (poor Cond.)

50' E

40' E = €

30' E

25' E = end cold lay + Cross Dirt gutter

20' E = w.cb.

1+98.12 = w.l. Dawes

	Lt.			Rt.			
77.9	77.1	76.6	76.7	76.6	76.4	75.9	76.0
3.1	3.9	4.5	4.3	4.4	4.6	5.1	5.0
40	20	10 edge	10	10	10	20 edge	40
77.9	77.2	76.0	75.9	75.6	75.4	75.4	75.1
3.2	3.8	5.0	5.1	5.1	5.4	5.6	5.9
40	20	10 edge	10	10 edge	20	40	
76.7	75.9	75.9	75.8	75.5	75.2	74.5	
4.8	5.1	5.1	5.2	5.5	5.8	6.5	
40	20	10 edge oil	10	10 edge oil	20	40	
76.7	76.3	76.1	75.8	75.6	75.3	74.8	
4.3	4.7	4.9	5.2	5.4	5.7	6.2	
40	20	10	10	10	20	40	
77.0	76.4	76.1	75.9	75.7	75.5	75.2	
4.0	4.6	4.9	5.1	5.3	5.5	5.8	
40	20	10	10	10	20	40	
76.7	76.1	75.8	75.6	75.4	75.2	74.8	
4.3	4.9	5.2	5.4	5.6	5.8	6.2	
40	20	10	10	10	20	40	
76.3	75.8	75.6	75.4	75.2	74.9	74.4	
4.7	5.2	5.4	5.6	5.8	6.1	6.6	
40	20	10 edge end	10	10 edge-end	20	40	
76.7	76.0	75.8	75.5	75.2	74.8	74.7	
4.3	5.0	5.2	5.5	5.8	6.2	6.3	
40	20	10 edge	10	10 edge	20	40	
76.5	75.9	75.6	75.4	75.1	74.9	74.9	
4.2	5.1	5.4	5.6	5.9	6.1	6.1	
40	20	10 edge	10	10 edge	20	40	

1+00

T.P. - 8.07 88.71 0.31 80.64

0+78 - 38.7 Lt. = ± 4' Conc. walk

0+78 - 18.7 Lt. = sly. of 3' wide - 2 Conc. Steps

0+75

0+58

① ~~0+38~~ 38.8 Lt. = ± 7.5' Conc. Dr.

0+50

0+27 - 40 Rt. = ± 3' Conc. walk

0+25

0+18 - 38.7 Lt. = ± 4' Conc. walk

0+00 - E.L. of Dawes - 41.8 Rt. = Nly. of
11' Conc. Dr. on Diagonal

Lt.

±

Rt.

81.2	79.1	80.9	79.8	79.6	79.7	79.3	78.7	79.6	79.2	78.9
6.5	6.6	7.8	9.3	9.1	9.0	9.4	10.0	9.1	9.5	9.8
50	40	22	18	10		10	21	24	40	50
			edge				edge			

88.71

80.79										
0.16										
38.7	80.39		79.30							
walk	0.56		1.65							
	23.2		18.7							
	Top edge		Bottom step							
	Nly.									

80.8	79.9	78.7	79.0	79.0	78.8	78.3	79.1	78.7
0.2	1.1	2.3	2.0	2.0	2.2	2.7	1.9	2.3
40	20	18	10		10	20	23	40
		edge				edge		

79.85
11.0
38.8
Dr

79.4	78.9	77.9	78.2	78.2	78.0	77.4	78.0	77.6
1.6	2.1	2.1	2.8	2.8	3.0	3.6	3.0	3.4
40	21	18	10		10	20	25	40
		edge						

76.59
4.36
to walk

78.5	77.9	77.1	77.4	77.4	77.2	76.7	76.5
2.5	3.1	3.9	3.6	3.6	3.8	4.3	4.5
40	20	17	10	36	10	20	40
		edge				edge	

78.35
26.0
38.7
walk

75.93
5.02
41.8

80.95

check starting B.M.	9.18	66.41	66.40
2.12	75.59	7.47	73.47
T.P.	0.06	80.94	11.72
			80.88

4+39.77 = Φ Everets

5+19.77 Cont.

5+19.77 = w.c.b.

4+99.77 = w.l. Everts

4+89.7 = P.C. 30 Rad Returns

Lt.

Φ

Rt.

50

89.92	89.03	88.15	87.82	87.25	86.70	86.08	85.51	85.28	84.61	84.03
2.68	3.57	4.45	4.78	5.35	5.90	6.52	7.09	7.32	7.99	8.57
100	75	50	40	20	20	20	40	50	75	100
89.76	89.16	88.81	88.25			83.90	84.48	83.24	82.86	
2.84	3.44	3.79	4.35			4.70	5.12	9.36	4.74	
100	100	75	75			75	75	100	100	
Top	gut.	Top	gut.			gut.	Top	gut.	Top	
88.00	87.42	87.03	86.71	86.52	86.36	86.05	85.16	84.72	84.47	85.11
4.60	5.18	5.57	5.89	6.08	6.24	6.55	6.94	7.88	8.13	7.49
50	50	40	20	10		10	20	40	50	50
Top	gut.								gut.	Top
PC										PC
86.70	85.96	85.06		85.97		85.54	84.82	85.35		
5.90	6.64	6.54		6.68		7.06	7.78	7.25		
21.6	21.6	10				10	22	22		
Top	gut.						gut.	Top		
86.33	85.73	85.84	85.70	85.33		84.80	85.30			
6.27	6.87	6.76	6.90	7.27		7.80	7.30			
20	20	10		10		20	20			
Top	gut.									
PC										
				92.60						

Rods around N.W. + S.W. Returns

at Law + Everets

N.W. Ret 47.4 around - 6 parts - 7.9 each.

N.L. Law

Beg. - N end. 10' N of

4.60 88.00 T = Top

5.18 87.42 q = gut.

7.9 S. 4.97 87.63 T

5.50 87.10 q

5.21 87.39 T

5.82 86.78 q

5.50 87.10 T

6.10 86.50 q

5.81 86.79 T

6.45 86.15 q

5.98 86.62 T

6.21 85.89 q

7.9 = end = P.C. 6.27 86.33 T

10' W of W.L. Everets 6.87 85.73 q

S.W. Ret. - 47.4 around - 6 - 7.9 each.

Beg. - W end - 10' W of W.L. Everets 7.30 85.30 T

7.80 84.80 q

7.9 E 7.25 85.35 T

7.79 84.81 q

" 7.24 85.36 T

7.78 84.82 q

" 7.18 85.42 T

7.80 84.80 q

" 7.21 85.29 T

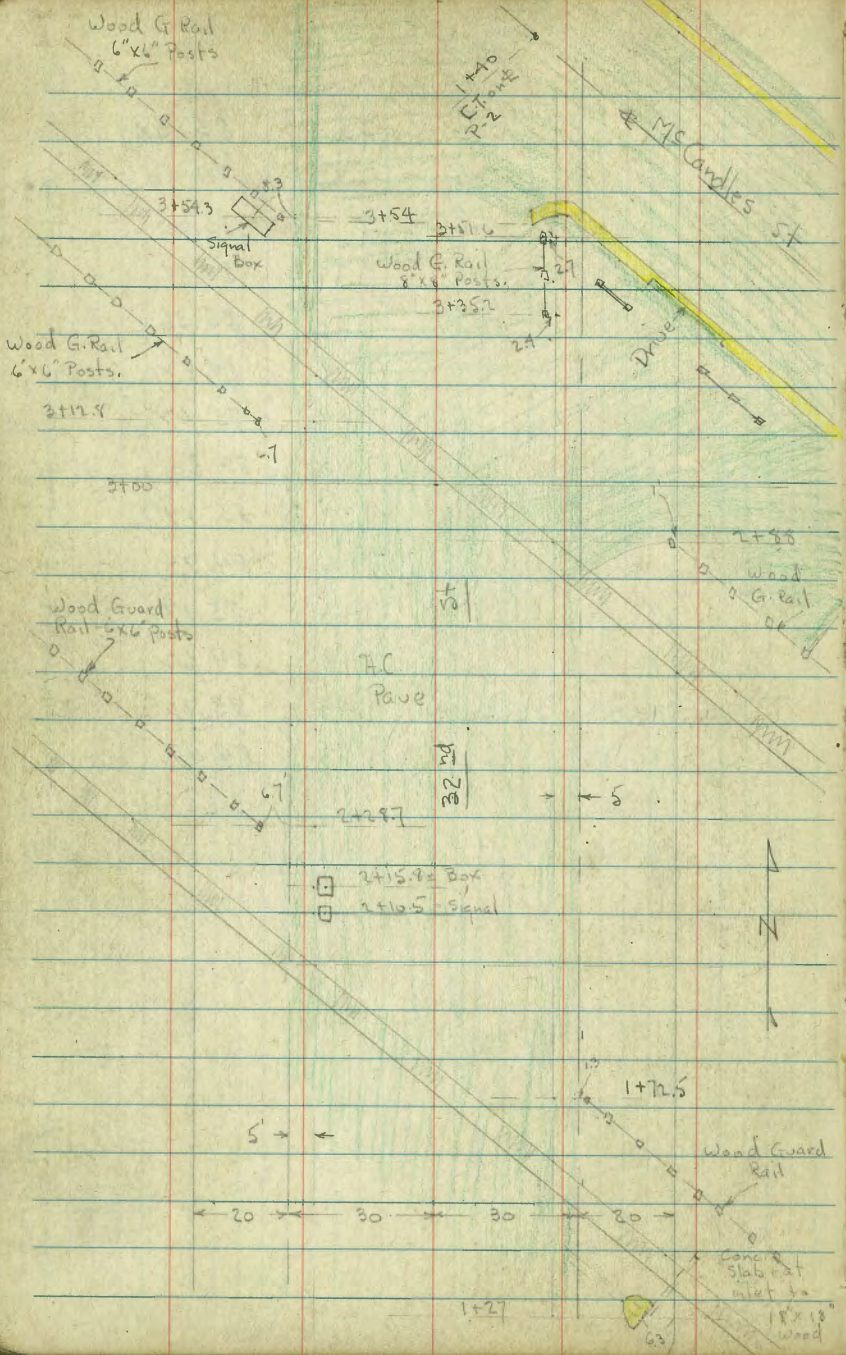
7.86 84.74 q

" 7.43 85.17 T

7.98 84.62 q

7.9 = P.C. = 10' S. of S.L. Law 7.49 85.11 T

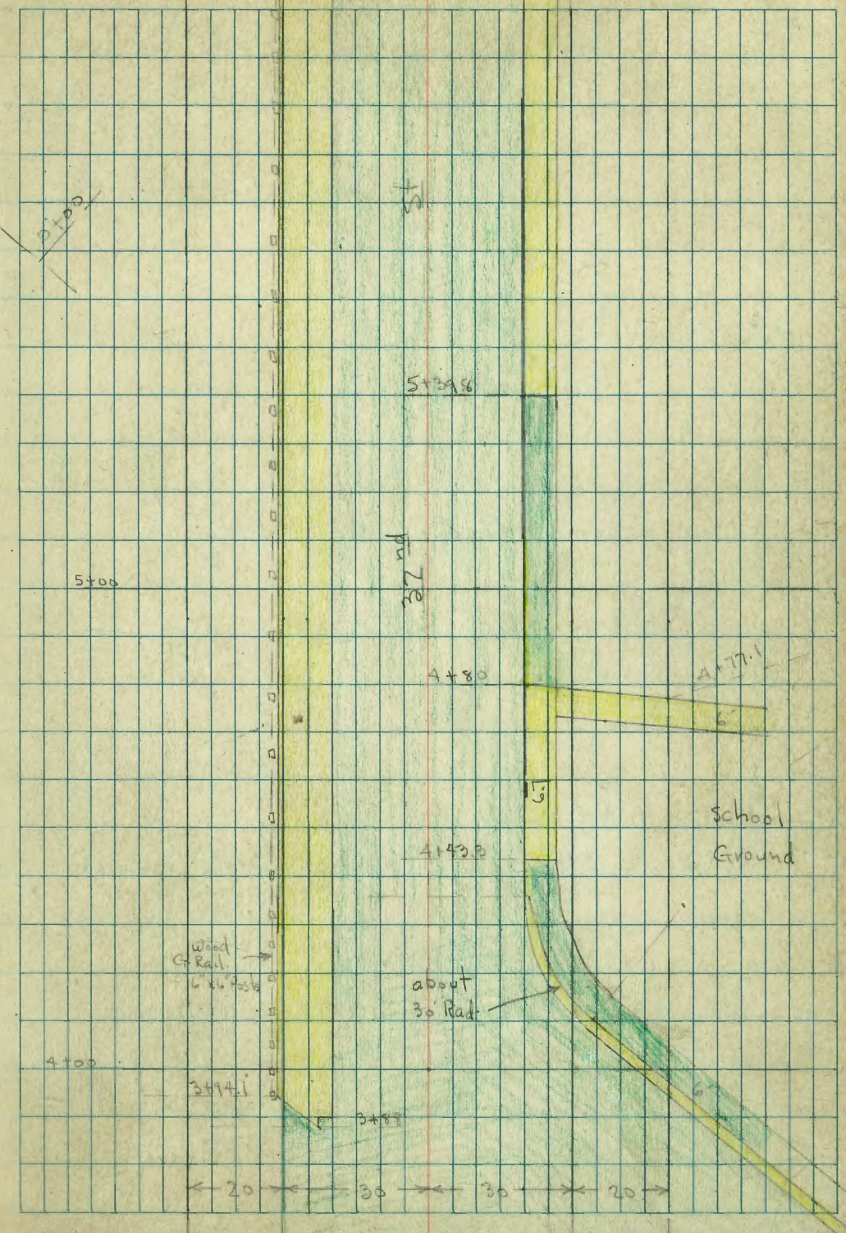
8.13 84.47 q



east Rail.

6+24.6

Cont. on P. 11
52



T.P. 3.10 9.67 10.52 7.02 6.57 7.42

✓ 2+77 - 46.5 Lt = E P. pole

2+75

✓ 2+60.8 - 50 Rt = S Rail + E.L. Row.

2+50

✓ 2+34.3 - 227 Lt = 2x2 Meter box - in Conc

✓ 2+31.4 - 213 Lt = E P. pole # 1798

2+25

✓ 2+15.8 - 22.8 Lt = E of 42' x 33' Conc Signal box

✓ 2+14.6 - 22 Rt = 6' x 8' Post.

✓ 2+13.6 - 50 Lt = W.L. Row. + S. Rail - N. Rail at 90°

✓ 2+11.6 - 215 Rt = E P. pole # 82280 H

✓ 2+10.5 - 22.6 Lt = 3' x 2.5' Conc base for R.R. Signal

✓ 2+07.2 - 22 Rt = 8' x 8' R.R. sign

2+00

5.35 5.9 6.7
572 572 50
edge of
Pave

✓ 1+88.5 = opp end of Conc walk on Lt

6.2	7.39	7.30	7.19	6.79	5.89
5.33	7.95	7.80	7.19	6.49	5.89
5.33	7.92	7.80	7.19	6.49	5.89
5.33	7.98	7.80	7.19	6.49	5.89
5.33	7.99	7.80	7.19	6.49	5.89
5.33	8.04	7.80	7.19	6.49	5.89
5.33	7.91	7.80	7.19	6.49	5.89
5.33	7.19	7.80	7.19	6.49	5.89
5.33	7.55	7.80	7.19	6.49	5.89
5.33	7.34	7.80	7.19	6.49	5.89
5.33	7.09	7.80	7.19	6.49	5.89
5.33	7.09	7.80	7.19	6.49	5.89

end of

13.59
14.77

5+00

- 4+70.7 - 23' Rt. = ϕ Water Meter
- 4+68.2 - 22.5' Rt. = ϕ 6" Gas Valve
- 4+52.6 - 22.5' Rt. = ϕ Tel. pole
- 4+50.

4+41.2 - Beg. Reg. cb. on Rt.
Roll to Reg. curb.

- 4+36.2 = opp. P.C. of Ret. on Rt. - changing from
- 4+26 - 25' Lt. = end Dr. Section cb.

4+25

- 4+22 - 33' Rt. = ϕ Sewer M.H. 5.38 on Rim.

4+00

- 3+97.2 - 50' Rt. = Top of Roll cb.
- 3+96.3 - 22' Lt. = ϕ 5' x 8" P.R. Crossing sign.
- 3+94.1 - 50' Rt. = Bottom of Roll cb.
- 3+94.1 - 31' Lt. = Back Cor. of Walk

Station	Description	Value	Value	Value	Value	Value	Value	Value	Value
5+00		5.00	4.67	4.60	4.26	3.66	4.06	3.68	4.23
4+70.7	Water Meter	5.00	4.67	4.60	4.26	3.66	4.06	3.68	4.23
4+68.2	Gas Valve	5.00	4.67	4.60	4.26	3.66	4.06	3.68	4.23
4+52.6	Tel. pole	5.00	4.67	4.60	4.26	3.66	4.06	3.68	4.23
4+50.		5.00	4.67	4.60	4.26	3.66	4.06	3.68	4.23
4+41.2	Beg. Reg. cb. on Rt.	5.00	4.67	4.60	4.26	3.66	4.06	3.68	4.23
4+36.2	opp. P.C. of Ret. on Rt.	5.00	4.67	4.60	4.26	3.66	4.06	3.68	4.23
4+26	end Dr. Section cb.	5.00	4.67	4.60	4.26	3.66	4.06	3.68	4.23
4+25		5.00	4.67	4.60	4.26	3.66	4.06	3.68	4.23
4+22	Sewer M.H.	5.38	4.67	4.60	4.26	3.66	4.06	3.68	4.23
4+00		5.00	4.67	4.60	4.26	3.66	4.06	3.68	4.23
3+97.2	Top of Roll cb.	5.00	4.67	4.60	4.26	3.66	4.06	3.68	4.23
3+96.3	5' x 8" P.R. Crossing sign.	5.00	4.67	4.60	4.26	3.66	4.06	3.68	4.23
3+94.1	Bottom of Roll cb.	5.00	4.67	4.60	4.26	3.66	4.06	3.68	4.23
3+94.1	Back Cor. of Walk	5.00	4.67	4.60	4.26	3.66	4.06	3.68	4.23

4.78
3.1
for Walk

9.67
10.57

4.12
0.05
0.05

5.1
0.05
0.05

9+08-30 Rt = \pm of 3' Conc. Dip gutter. along H.C.

steel pipes under the wall

9+06 = end of cb. at Dr. on Rt. = gut. = outlet of 9-6"

9+00 - Reg. Sect

walk below - Note walk is curved.

8+95.6 - 30' Rt = \pm N. S Conc walk - same profile as

8+94.5 - 21.5 Lt = \pm P. pole # 1648

Curve of the Row. Hits. - See P. 11

along walk + show both sides where the F.L.

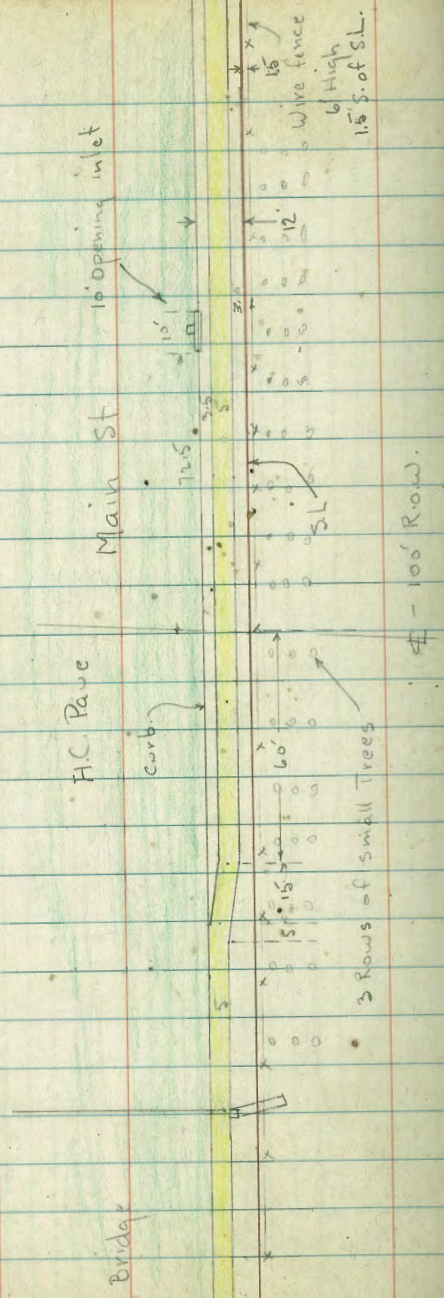
8+80.5 - 30' Rt = \pm 5' Conc walk - Will take \pm Profile

J.P. 5.60 $\frac{9.82}{9.87}$ 5.05 3.42 $\frac{4.27}{4.27}$ disk by Bridge

8+50

8+00

4.95	5.02	5.17	5.28	5.46	5.58	5.72	5.83	5.92	6.00	6.08	6.15	6.22	6.28	6.33	6.38	6.43	6.47	6.53	6.58	6.63	6.67	6.71	6.75	6.79	6.83	6.87	6.91	6.95	6.99	7.03	7.07	7.11	7.15	7.19	7.23	7.27	7.31	7.35	7.39	7.43	7.47	7.51	7.55	7.59	7.63	7.67	7.71	7.75	7.79	7.83	7.87	7.91	7.95	7.99	8.03	8.07	8.11	8.15	8.19	8.23	8.27	8.31	8.35	8.39	8.43	8.47	8.51	8.55	8.59	8.63	8.67	8.71	8.75	8.79	8.83	8.87	8.91	8.95	8.99	9.03	9.07	9.11	9.15	9.19	9.23	9.27	9.31	9.35	9.39	9.43	9.47	9.51	9.55	9.59	9.63	9.67	9.71	9.75	9.79	9.83	9.87	9.91	9.95	9.99	10.03	10.07	10.11	10.15	10.19	10.23	10.27	10.31	10.35	10.39	10.43	10.47	10.51	10.55	10.59	10.63	10.67	10.71	10.75	10.79	10.83	10.87	10.91	10.95	10.99	11.03	11.07	11.11	11.15	11.19	11.23	11.27	11.31	11.35	11.39	11.43	11.47	11.51	11.55	11.59	11.63	11.67	11.71	11.75	11.79	11.83	11.87	11.91	11.95	11.99	12.03	12.07	12.11	12.15	12.19	12.23	12.27	12.31	12.35	12.39	12.43	12.47	12.51	12.55	12.59	12.63	12.67	12.71	12.75	12.79	12.83	12.87	12.91	12.95	12.99	13.03	13.07	13.11	13.15	13.19	13.23	13.27	13.31	13.35	13.39	13.43	13.47	13.51	13.55	13.59	13.63	13.67	13.71	13.75	13.79	13.83	13.87	13.91	13.95	13.99	14.03	14.07	14.11	14.15	14.19	14.23	14.27	14.31	14.35	14.39	14.43	14.47	14.51	14.55	14.59	14.63	14.67	14.71	14.75	14.79	14.83	14.87	14.91	14.95	14.99	15.03	15.07	15.11	15.15	15.19	15.23	15.27	15.31	15.35	15.39	15.43	15.47	15.51	15.55	15.59	15.63	15.67	15.71	15.75	15.79	15.83	15.87	15.91	15.95	15.99	16.03	16.07	16.11	16.15	16.19	16.23	16.27	16.31	16.35	16.39	16.43	16.47	16.51	16.55	16.59	16.63	16.67	16.71	16.75	16.79	16.83	16.87	16.91	16.95	16.99	17.03	17.07	17.11	17.15	17.19	17.23	17.27	17.31	17.35	17.39	17.43	17.47	17.51	17.55	17.59	17.63	17.67	17.71	17.75	17.79	17.83	17.87	17.91	17.95	17.99	18.03	18.07	18.11	18.15	18.19	18.23	18.27	18.31	18.35	18.39	18.43	18.47	18.51	18.55	18.59	18.63	18.67	18.71	18.75	18.79	18.83	18.87	18.91	18.95	18.99	19.03	19.07	19.11	19.15	19.19	19.23	19.27	19.31	19.35	19.39	19.43	19.47	19.51	19.55	19.59	19.63	19.67	19.71	19.75	19.79	19.83	19.87	19.91	19.95	19.99	20.03	20.07	20.11	20.15	20.19	20.23	20.27	20.31	20.35	20.39	20.43	20.47	20.51	20.55	20.59	20.63	20.67	20.71	20.75	20.79	20.83	20.87	20.91	20.95	20.99	21.03	21.07	21.11	21.15	21.19	21.23	21.27	21.31	21.35	21.39	21.43	21.47	21.51	21.55	21.59	21.63	21.67	21.71	21.75	21.79	21.83	21.87	21.91	21.95	21.99	22.03	22.07	22.11	22.15	22.19	22.23	22.27	22.31	22.35	22.39	22.43	22.47	22.51	22.55	22.59	22.63	22.67	22.71	22.75	22.79	22.83	22.87	22.91	22.95	22.99	23.03	23.07	23.11	23.15	23.19	23.23	23.27	23.31	23.35	23.39	23.43	23.47	23.51	23.55	23.59	23.63	23.67	23.71	23.75	23.79	23.83	23.87	23.91	23.95	23.99	24.03	24.07	24.11	24.15	24.19	24.23	24.27	24.31	24.35	24.39	24.43	24.47	24.51	24.55	24.59	24.63	24.67	24.71	24.75	24.79	24.83	24.87	24.91	24.95	24.99	25.03	25.07	25.11	25.15	25.19	25.23	25.27	25.31	25.35	25.39	25.43	25.47	25.51	25.55	25.59	25.63	25.67	25.71	25.75	25.79	25.83	25.87	25.91	25.95	25.99	26.03	26.07	26.11	26.15	26.19	26.23	26.27	26.31	26.35	26.39	26.43	26.47	26.51	26.55	26.59	26.63	26.67	26.71	26.75	26.79	26.83	26.87	26.91	26.95	26.99	27.03	27.07	27.11	27.15	27.19	27.23	27.27	27.31	27.35	27.39	27.43	27.47	27.51	27.55	27.59	27.63	27.67	27.71	27.75	27.79	27.83	27.87	27.91	27.95	27.99	28.03	28.07	28.11	28.15	28.19	28.23	28.27	28.31	28.35	28.39	28.43	28.47	28.51	28.55	28.59	28.63	28.67	28.71	28.75	28.79	28.83	28.87	28.91	28.95	28.99	29.03	29.07	29.11	29.15	29.19	29.23	29.27	29.31	29.35	29.39	29.43	29.47	29.51	29.55	29.59	29.63	29.67	29.71	29.75	29.79	29.83	29.87	29.91	29.95	29.99	30.03	30.07	30.11	30.15	30.19	30.23	30.27	30.31	30.35	30.39	30.43	30.47	30.51	30.55	30.59	30.63	30.67	30.71	30.75	30.79	30.83	30.87	30.91	30.95	30.99	31.03	31.07	31.11	31.15	31.19	31.23	31.27	31.31	31.35	31.39	31.43	31.47	31.51	31.55	31.59	31.63	31.67	31.71	31.75	31.79	31.83	31.87	31.91	31.95	31.99	32.03	32.07	32.11	32.15	32.19	32.23	32.27	32.31	32.35	32.39	32.43	32.47	32.51	32.55	32.59	32.63	32.67	32.71	32.75	32.79	32.83	32.87	32.91	32.95	32.99	33.03	33.07	33.11	33.15	33.19	33.23	33.27	33.31	33.35	33.39	33.43	33.47	33.51	33.55	33.59	33.63	33.67	33.71	33.75	33.79	33.83	33.87	33.91	33.95	33.99	34.03	34.07	34.11	34.15	34.19	34.23	34.27	34.31	34.35	34.39	34.43	34.47	34.51	34.55	34.59	34.63	34.67	34.71	34.75	34.79	34.83	34.87	34.91	34.95	34.99	35.03	35.07	35.11	35.15	35.19	35.23	35.27	35.31	35.35	35.39	35.43	35.47	35.51	35.55	35.59	35.63	35.67	35.71	35.75	35.79	35.83	35.87	35.91	35.95	35.99	36.03	36.07	36.11	36.15	36.19	36.23	36.27	36.31	36.35	36.39	36.43	36.47	36.51	36.55	36.59	36.63	36.67	36.71	36.75	36.79	36.83	36.87	36.91	36.95	36.99	37.03	37.07	37.11	37.15	37.19	37.23	37.27	37.31	37.35	37.39	37.43	37.47	37.51	37.55	37.59	37.63	37.67	37.71	37.75	37.79	37.83	37.87	37.91	37.95	37.99	38.03	38.07	38.11	38.15	38.19	38.23	38.27	38.31	38.35	38.39	38.43	38.47	38.51	38.55	38.59	38.63	38.67	38.71	38.75	38.79	38.83	38.87	38.91	38.95	38.99	39.03	39.07	39.11	39.15	39.19	39.23	39.27	39.31	39.35	39.39	39.43	39.47	39.51	39.55	39.59	39.63	39.67	39.71	39.75	39.79	39.83	39.87	39.91	39.95	39.99	40.03	40.07	40.11	40.15	40.19	40.23	40.27	40.31	40.35	40.39	40.43	40.47	40.51	40.55	40.59	40.63	40.67	40.71	40.75	40.79	40.83	40.87	40.91	40.95	40.99	41.03	41.07	41.11	41.15	41.19	41.23	41.27	41.31	41.35	41.39	41.43	41.47	41.51	41.55	41.59	41.63	41.67	41.71	41.75	41.79	41.83	41.87	41.91	41.95	41.99	42.03	42.07	42.11	42.15	42.19	42.23	42.27	42.31	42.35	42.39	42.43	42.47	42.51	42.55	42.59	42.63	42.67	42.71	42.75	42.79	42.83	42.87	42.91	42.95	42.99	43.03	43.07	43.11	43.15	43.19	43.23	43.27	43.31	43.35	43.39	43.43	43.47	43.51	43.55	43.59	43.63	43.67	43.71	43.75	43.79	43.83	43.87	43.91	43.95	43.99	44.03	44.07	44.11	44.15	44.19	44.23	44.27	44.31	44.35	44.39	44.43	44.47	44.51	44.55	44.59	44.63	44.67	44.71	44.75	44.79	44.83	44.87	44.91	44.95	44.99	45.03	45.07	45.11	45.15	45.19	45.23	45.27	45.31	45.35	45.39	45.43	45.47	45.51	45.55	45.59	45.63	45.67	45.71	45.75	45.79	45.83	45.87	45.91	45.95	45.99	46.03	46.07	46.11	46.15	46.19	46.23	46.27	46.31	46.35	46.39	46.43	46.47	46.51	46.55	46.59	46.63	46.67	46.71	46.75	46.79	46.83	46.87	46.91	46.95	46.99	47.03	47.07	47.11	47.15	47.19	47.23	47.27	47.31	47.35	47.39	47.43	47.47	47.51	47.55	47.59	47.63	47.67	47.71	47.75	47.79	47.83	47.87	47.91	47.95	47.99	48.03	48.07	48.11	48.15
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100' Row.

3 Rows of small Trees

curb

H.C. Pave

Main St

10' opening inlet

12'

15'

15'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

Moore
Begg
Sheep Cuts for W.M. on Delta St
Sisson
7-12-49, 40 to 41 ST.

W/O 31048

So. Curb
0100 check at 41 ST

INDEXED

W.K.
JUL 13 1949

5+56		6x.00	
		10.04	
		9.96	
		60.08	
5+31	64.34		
	9.70		
	7.80		
4+76	F0.10	65.08	
		8.96	
		8.46	
4+26		60.50	65.75
			8.29
			8.62
4+06	66.22		F0.33
	8.02		
	8.16		
3+64	F0.14	66.60	
		7.36	
		7.15	7 4 04
2+49		60.19	6 8 14
			5 90
			27
1+98	74.04		6 3 2
	6 8 78		
	5 26		
	2 55		
1+15	6 2 71	74.04	
		6 9 95	
		4 0 9	
		2 2	
0+20		6 1 8	74.04
			71.23
			2 8 1
			2 2 1
			6 6 0
			63.29
NWBP	10.75	74.04	
40th Delta			

N 06

5+76		64.71	
		5.74	
		4.84	
		60.90	
5+15		65.55	
		4.90	
		3.60	
T.P.	159	70.45	6 1 3
			10.01
3+17			6 8 2 2
			10 6 5
			10 0 5
			6 0 10
1+82		70.05	
		8.82	
		6.02	
		6 2 8	
0+78			71.45
			7 4 2
			4 2
			6 3 2 2
0+04			72.45
			6 4 2
			0 5 0
			6 5 2
T.P.	6.02	78.87	119
			72.85
		74.04	

Levels National Ave At Hobart Ave.
Old paving

+75

+50

+25

9+0

+75

8+50

BM

698

1228

620

11 Corcoran
#3265
National
Hwy

March 16, 54
H. S. ...
C. ...
Kelley

LT=11

2

= South 77

6.50

6.71

5.00
6.00
7.23

6.00
7.27

5.00
7.36

5.00
7.43
Old Pav.

5.00
7.45
Old Pav.

1228

8

+50

~~10.23~~
0.05

~~10.24~~
0.94
26

+25

~~10.23~~
1.46

~~10.23~~
2.35
26

11 + 10.83

~~10.01~~
2.27

~~10.01~~
2.97
22

~~10.23~~
2.96
Hemigaster

+90 E. end Island

~~9.78~~
3.50

~~9.07~~
4.21
23

10 + 37.80 W. end Island

~~7.38~~
5.90
0.21 Pa.

~~5.97~~
7.31
25

13.28

13.28

Cross Section 6" Line Sta
 NY End Imperial Fire Overpass

+75

+50

+25

9+15

IT

+95

+80

8+50

BM

0.30

61.78
~~51.78~~

10.64

61.48

303

72.12
~~63.12~~

68.79
~~58.79~~

NY End
 Imperial
 Fire Overpass

March 17-54

#5 Sta

Garber Lt=North

Chipman

Perfit

Kelley

79

z

51.7 51.2 45.7 40.2
 41 46 16.1 20.9
 50.3 33.0 15.7 0.6

51.1 50.1 47.1 41.1
 47.7 57.0 16.1 20.7
 17.7 38.0 2.6 0.6

48.8 48.5 48.0 46.6 45.2 42.8
 22.8 23 28 12.2 16.1 18.8
 11.5 39.0 38.6 30.7 25 6.0

47.4 47.3 46.9 46.2 44.9 41.8
 40.4 38.3 35.8 28.6 17.0 20.0
 17.0 31.3 28.6 24 24

61.78
~~51.78~~

60.5 60.5 60.1 58.2 53.4 50.1
 57.5 9.6 12.0 13.9 28.7 31.4
 57.0 27.0 33 28 2.8 0.0

60.8 60.1 40.1 38.4
 10.8 11.4 61.4 33.9
 37 30 2.1 0.0

60.8 60.2 59.3 38.0
 10.8 14.9 32.8 31.1
 37 30 2.1 0.0

58.79

IMPROVED TABLES AND INFORMATION

1250
180
22430

HORIZONTAL STADIA CORRECTIONS

2°-00' — 0.1	21°-00' — 12.8	33°-00' — 29.7
3°-00' — 0.3	21°-30' — 13.4	33°-15' — 30.1
4°-00' — 0.5	22°-00' — 14.0	33°-30' — 30.5
5°-00' — 0.8	22°-30' — 14.7	33°-45' — 30.9
6°-00' — 1.1	23°-00' — 15.3	34°-00' — 31.3
7°-00' — 1.5	23°-30' — 15.9	34°-15' — 31.7
8°-00' — 1.9	24°-00' — 16.5	34°-30' — 32.1
9°-00' — 2.5	24°-30' — 17.2	34°-45' — 32.5
10°-00' — 3.0	25°-00' — 17.9	35°-00' — 32.9
10°-30' — 3.3	25°-30' — 18.6	35°-15' — 33.3
11°-00' — 3.6	26°-00' — 19.2	35°-30' — 33.7
11°-30' — 4.0	26°-30' — 19.9	35°-45' — 34.1
12°-00' — 4.3	27°-00' — 20.6	36°-00' — 34.6
12°-30' — 4.7	27°-30' — 21.3	36°-15' — 35.0
13°-00' — 5.1	28°-00' — 22.0	36°-30' — 35.4
13°-30' — 5.5	28°-30' — 22.8	36°-45' — 35.8
14°-00' — 5.9	29°-00' — 23.5	37°-00' — 36.2
14°-30' — 6.3	29°-30' — 24.3	37°-15' — 36.6
15°-00' — 6.7	30°-00' — 25.0	37°-30' — 37.1
15°-30' — 7.2	30°-15' — 25.4	37°-45' — 37.5
16°-00' — 7.6	30°-30' — 25.8	38°-00' — 37.9
16°-30' — 8.1	30°-45' — 26.2	38°-15' — 38.3
17°-00' — 8.5	31°-00' — 26.5	38°-30' — 38.7
17°-30' — 9.0	31°-15' — 26.9	38°-45' — 39.1
18°-00' — 9.5	31°-30' — 27.3	39°-00' — 39.6
18°-30' — 10.1	31°-45' — 27.7	39°-15' — 40.0
19°-00' — 10.6	32°-00' — 28.1	39°-30' — 40.5
19°-30' — 11.2	32°-15' — 28.5	
20°-00' — 11.7	32°-30' — 28.9	
20°-30' — 12.3	32°-45' — 29.3	

Chains to Feet

1	66
2	132
3	198
4	264
5	330
6	396
7	462
8	528
9	594
10	660

Feet to Chains

100	1.515
200	3.030
300	4.545
400	6.060
500	7.575
600	9.090
700	10.606
800	12.121
900	13.636
1,000	15.151

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

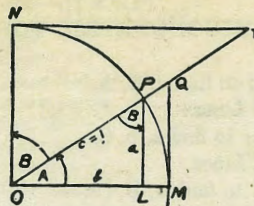
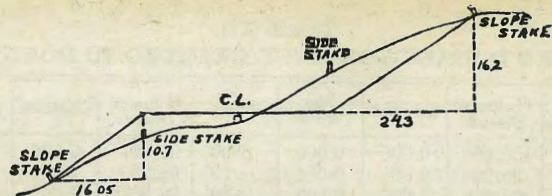


TABLE II
TRIGONOMETRIC FORMULÆ.

$$\begin{aligned} \angle A &= \angle MOP & \angle B &= \angle PON = \angle OPL \\ R &= OB = c = 1 \\ \sin A &= \frac{a}{c} = \frac{a}{1} = a = \cos B = LP \\ \cos A &= \frac{b}{c} = \frac{b}{1} = b = \sin B = OL \\ \tan A &= \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ \\ \cot A &= \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT \\ \sec A &= \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ \\ \csc A &= \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT \\ \text{vers } A &= \frac{LM}{OP} = LM = \text{covers } B \# \\ \text{covers } A &= \frac{OP - LP}{OP} = OP - LP = \text{vers } B \\ \text{exsec } A &= PQ = \text{coexsec } B \\ \text{coexsec } A &= PT = \text{exsec } B \\ \sin \frac{1}{2} A &= \sqrt{\frac{1 - \cos A}{2}} & \cos \frac{1}{2} A &= \sqrt{\frac{1 + \cos A}{2}} \\ \sin 2A &= 2 \sin A \cos A & \cos 2A &= \cos^2 A - \sin^2 A \\ \text{Law of Lines} & \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C} \\ \text{Law of Cosines} & c^2 = a^2 + b^2 - 2ab \cos C \\ \text{Law of Tangents} & \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)} \end{aligned}$$



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH.

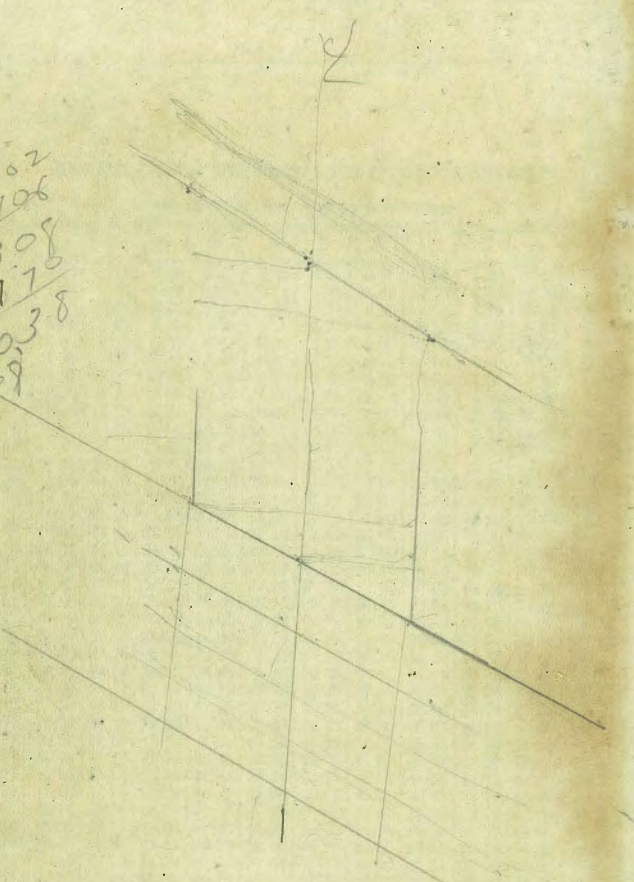
	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 05	1 20	1 35	1 50	1 65	1 80	1 95	2 10	2 25	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

10.00 = D.P. in Plant
 7.56
 17.56
 4.80
 12.76
 4.85
 17.61
 7.63
 9.98
 3.22
 13.20
 4.96
 8.24 C+G Mon.

9.13
 859
 17.72
 8.86

$$\begin{array}{r} 66.02 \\ 7.06 \\ \hline 73.08 \\ 4.76 \\ \hline 70.38 \\ 6.9 \end{array}$$



	9.09	Dist.	13.74	9.07	13.17
	<u>5.35</u>		<u>1.51</u>	<u>8.24</u>	<u>1.17</u>
	14.44		.73	.85	
	<u>7.02</u>				
	7.42				12.53
	<u>3.10</u>				<u>1.09</u>
	10.52				13.62
9.47	<u>5.36</u>				
<u>9.8</u>	5.16				
8.62	<u>4.42</u>				
	9.88				60.81
	<u>5.31</u>				<u>49.35</u>
	4.27				11.16
	<u>5.05</u>				
	9.32				
4.27	<u>5.60</u>				
<u>5.18</u>	9.87				
9.45					